



**Power Generation from Salinity Gradient Solar Ponds Using  
Thermoelectric Generators**

A thesis submitted in fulfilment of the requirements for the degree of  
Doctor of Philosophy

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February 2017

## **Declaration**

I certify that except where due acknowledgement has been made, the work is that of the author alone; the work has not been submitted previously, in whole or in part, to qualify for any other academic award; the content of the thesis is the result of work which has been carried out since the official commencement date of the approved research program; any editorial work, paid or unpaid, carried out by a third party is acknowledged; and, ethics procedures and guidelines have been followed.

I acknowledge the support I have received for my research through the provision of an Australian Government Research Training Program Scholarship

Lai Chet, DING

February 2017

## Acknowledgement

- Firstly, I would like to thank and praise Lord Jesus Christ for his grace, wisdom, and inspiration that He has imparted to me, which lead me to the completion of this study.
- I would like to deliver my deepest appreciation to my senior supervisor, Professor Aliakbar Akbarzadeh for his unwavering paternal guidance and Dr. Abhijit Date, my second supervisor for his continuous technical or non-technical advice and helps.
- Besides, I am grateful to RMIT University for granting International Postgraduate Research Scholarship/RMIT Ph.D. International Scholarship throughout the candidature and Thermal Technology Division of Fujikura Ltd. (Japan) for providing me a fruitful research internship on thermoelectric technologies in Tokyo.
- Nevertheless, I will like to appreciate the technical officers from the SAMME RMIT, friends, and colleagues for their supports whenever help is needed throughout the candidature.
- To my family members of K23 back home in Malaysia, thank you for every good thing that you did for me and to my sister, Dr. Ding at Singapore, thank you for lending your ear to all my grumbles at night throughout this period.

*‘Perita manus mens exculpta’ (Skill hand, cultivated mind)*

Lai Chet, DING

**February 2017**

- ***“We must accept that we have to make hard choices in this generation to bring about real changes for the future generation and the planet. Politicians and the industry must get real.” – World Energy Council***
- ***For the generation who looking for greener earth, this work is dedicated to you.***
  - ***“For wisdom will come into your heart, and knowledge will be pleasant to your soul; discretion will watch over you, understanding will guard you.”***  
***Proverbs 2:10-11***
  - ***What makes a man a man?***
  - ***Cogito, ergo sum. [I think, therefore I am]***  
***-René Descartes***

## **Abstract**

The thermoelectric devices have been introduced for over 50 years and numerous research and methods have been carried out to improve its conversion efficiency, represented by the figure of merit,  $ZT$ . Despite having a low conversion efficiency compared to other heat engine, thermoelectric is gaining attention owing to its stationary and simplest operating condition that requires no maintenance. From the literature study conducted, most of the applications of the thermoelectric generators are focusing on generating electricity from a non-storage heat source, which means in order to avoid intermittency in the power supply due to temporary unavailability of adequate heat source; a battery storage system is needed. In order to address an alternative for the aforementioned scenario, a thermal storage system that will able to constantly providing sufficient heat for power generation is proposed, which introduces the solar pond (SP) as the heat source. Acting as a solar energy collector as well as thermal storage, solar ponds have been available in large scale for providing low grade heat source from 50 °C to 100 °C. Moreover, in terms of scalability, both thermoelectric generators and solar pond are highly scalable in size. As the thermoelectric cells are able to work interchangeably between heat pump and heat engine, it results in two variations of the thermoelectric cells available in the market, being sold as Peltier cooler and thermoelectric generators, with a significant price difference (the former is costing less than the latter). This study has started by investigating the performance and reliability of the thermoelectric cooler available functioning as thermoelectric generator. Later, in the next chapter, the performance of the thermoelectric cells is incorporated and coupled with a transient heat transfer for solar pond, in order to set up the potential of the thermoelectric-solar pond power generation system. Two practical power generation systems have been brought to fruition and presented in this thesis, which are a plate type power generation unit operating at atmospheric pressure and a submersible type thermoelectric power generation unit, and their comprehensive investigation have been delineated separately in the following chapters. Finally, the outcomes from the prior chapters (the system's performance via transient model and prototype testing) are joined in the last part of this thesis, to form a sound feasibility study of the system. From the establishment of theoretical framework to the examination of the system's feasibility from the potential and practical viewpoint, this thesis had attended the essential of power generation from solar pond using thermoelectric generators.

**Keywords:** energy conversion, power generation, thermoelectric, solar pond

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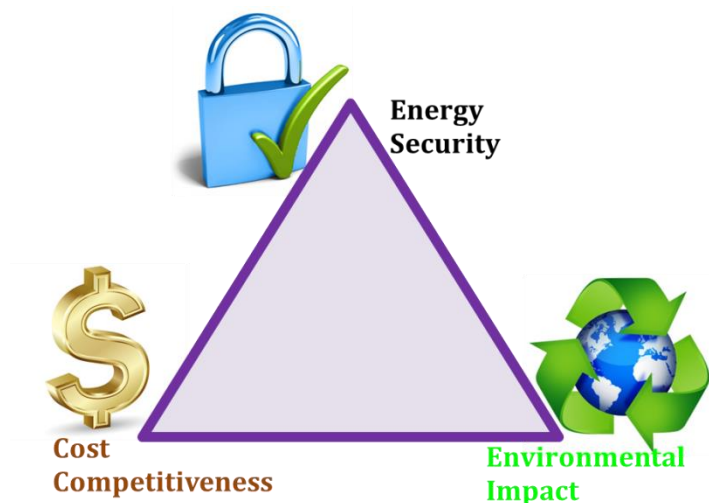
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# Chapter 1: Introduction

## 1.1 Research Background

### 1.1.1 Renewable Energy: A Global and Local Scenario

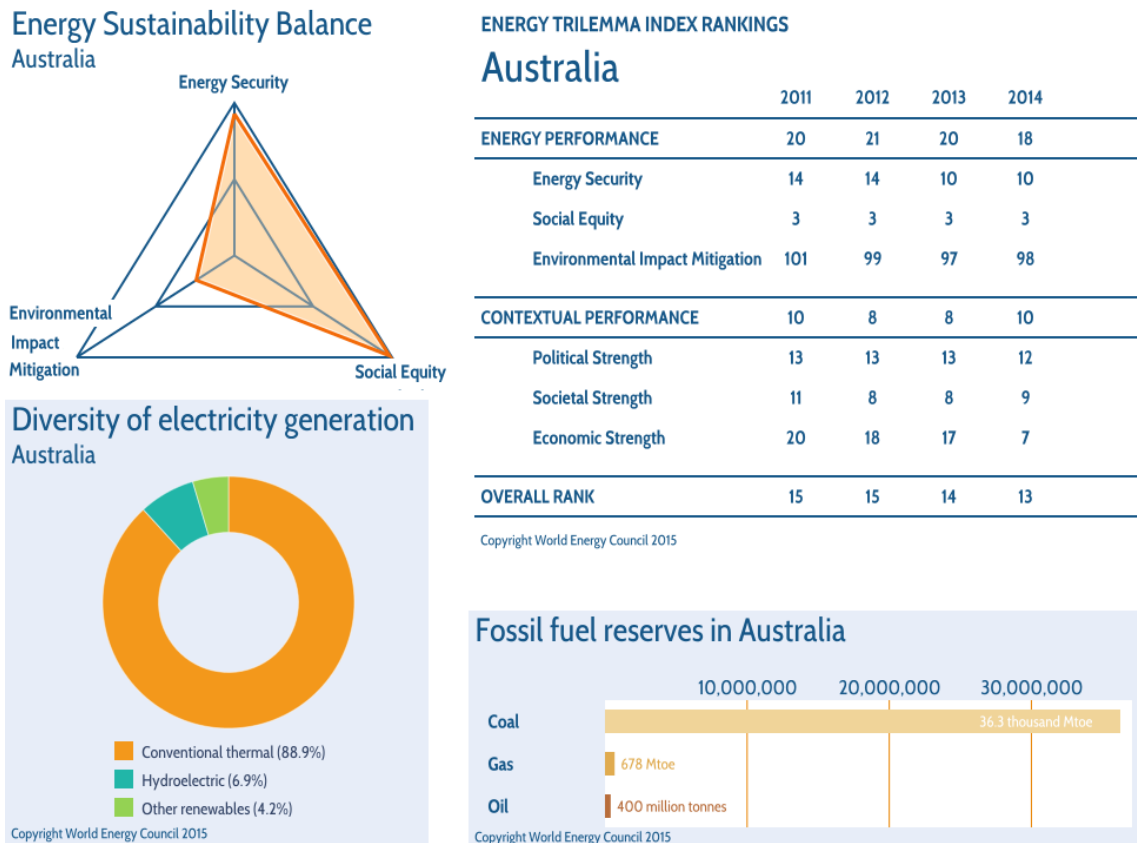
Up to this point, coal, oil, gas, and nuclear remains the major sources of world energy consumption, while renewable energy resources such as solar energy, hydropower, wind energy, biomass, geothermal remain a relatively small portion of the global energy sources. When we deal with the choice of energy, energy trilemma appears and often, policy makers made a compromise between the reliability of the resources for current and future demands, its adorability and the environmental impact (Fig. 1). From the year 1993 to 2011, the world electricity production had risen from 12607 TWh to 22202 TWh per year and fossil source of energy occupied 82% of the primary energy supply, renewable energy (including hydropower) and nuclear energy filled up the remaining energy sources with 13% and 5%, respectively. With the increasing demand of electricity supply and the status of the fossil as the main source of energy (which is also the source of CO<sub>2</sub> emission) remains unchanged, the total CO<sub>2</sub> emissions has increased by almost 50% from 1993 to 30 Gt CO<sub>2</sub> per year (World Energy Council, 2014). Hence, discernibly, the trade-off resulted from the energy trilemma to date is clear, the reliability and affordability of the source of energy overweight the consideration of environmental impact.



**Fig.1.** Energy trilemma.

In the local context, Australia relies on the conventional thermal power plant for electricity production using coal, gas, and oil. Australia ranked high on providing a secure, affordable and accessible supply of electricity in the world. However, in terms of environmental sustainability, Australia performs weakly, compared to other advanced economies (Fig. 2).

The latest report published by British Petroleum (June 2014) on statistic review of global energy consumption reveals that renewable energy consumption in Australia accounts for 1.2 % ( the equivalent of 3.4 million tons of oil) of global renewable energy consumption (BP, 2014). Meanwhile, solar energy has been widely used as a source for power production using solar photovoltaic (PV) panel. With the extensive application of solar PV, Australia ranked 8th globally with an installed capacity of 1.0 GW (Pazheri, 2014).



**Fig. 2.** Energy in Australia. (World Energy Council, 2014)

### 1.1.2 Solar Pond and Thermoelectric Generators: An Amalgamation for Remote Area Power Supply

The power supply for a remote area often relies on the off-grid power supply on one hand, which can be either with the use of the solar panel, wind turbine, geothermal sources, diesel or biofuel generator, micro hydro turbine. On the other hand, in terms of power storage, often deep cycle batteries are being used. Without a storage system, the solar energy utilisation will be in the form of instantaneous usage, be it solar hot water, solar PV or wind turbine.

Despite the need of external storage system, solar pond with a different design as a large-scale solar energy collector and storage has been used extensively in process heating, desalination or solar power generation (El-Sebaei et al., 2011; Garmana & Muntasser, 2008).

The heat stored in the bottom part of the solar pond and hence possesses the highest temperature, while the top part of the pond will remain almost identical to daily average ambient temperature. This pool of saltwater requires constant replenishment of salt due to surface evaporation and hence, the facility is normally built in the area within proximity with salt supply (e.g. sea side). It is worthwhile to mention that the largest solar pond operated, Beit HaArava of Isreal with built area of 210,000 m<sup>2</sup> had produced 5 MW of electricity, as a result from the scalability of energy output with the solar pond area, like other selection of renewable energy generation. With a typical efficiency of 20% (Wang & Akbarzadeh, 1982), a solar pond will able to provide 40 W/m<sup>2</sup> of heat at annual average solar radiation of 200 W/m<sup>2</sup>.

Meanwhile, the use of thermoelectric generators (TEGs) as a potential source of for both large scale electric powers as well as alternative source for low power generation from the temperature difference created from the heat input at hot and cold junction had been delineated by Rowe that presented in his previous publications (Rowe 1992; Rowe 1994; Rowe 1999). Apart from being environmentally friendly, from the economics point of view, the increase of fuel cost will lead to the demand of alternative mean for power generation. The inclusion of externalities consideration will certainly favour the use of TEGs as a supplement for electrical energy production (Patyk, 2013).

From the review conducted, which will be presented in the forthcoming chapter, a thermal-storage based heat source (e.g. in this study, the solar pond) could be utilised for small-scale electric power generation, despite its usual function as low-grade heat source provider through heat extraction. With the abundant of heat available in the solar pond, electric power can be produced by using the simplest possible method, and in this case, thermoelectric modules which are working under static condition will be favourable for small-scale electric power generation.

## **1.2 Research Significance**

While solar energy is one of the extensive sources of renewable energy that being sought after along with the booming interest exploring greener method replacing the conventional source of energy, solar pond offers both the functions as solar energy collector and solar energy storage. This work will delineate the study on one of the methods for electric power generation using the heat stored from the solar pond using thermoelectric generators (a static device that offers a lifespan of 200,000 hours to 300,000 hours). From the study of physical attribute on solar pond, to the design and fabrication of the electric power generation unit,



until the evaluation on the prospect of electric power generation, this work provides a *comprehensive and niche study on an alternative method of electric power generation, particularly to be availed in remote area* where electric grid connection is out of reach, not to mention its environmentally friendly nature of electric power generation in line with developing the application of the renewable energy for the future. While the heat from the solar pond can be the heat source for power generation unit, *the off-pond electric power generation unit conceived, in a broader context, the unit will able to be extended for recovering the waste heat of the high-temperature waste water* from the industry (e.g. steel cooling), or using the hot water accessible from the hot water solar collector. Hence, the off-pond power generation unit designed will able to cater and apply for recovering the waste heat from the water. Nevertheless, the outcomes of this research on the performance of the electric power generation unit can be used as the benchmark or baseline study for the application of power generation using thermoelectric modules, aiming to avail consulting engineer in the decision making on project implementation, in view of the possible advancement of TEGs' performance in the future.

### **1.3 Research Rationale**

Different methods have been used for the electric power generation with solar pond such as the use of organic Rankine cycle to power a turbine for power generation. Recent work carried out by Singh et al. (2011) had shown that the electric power generation with the exclusion of bulky devices such as boiler and turbine can be achieved by integrating the thermosiphon and thermoelectric modules. The main motivation that drives this study is to achieve an electric power generation system design that is fully passive, low cost, reliable and simple.

To date, there exist knowledge gap on assessing the feasibility of the power generation from salinity gradient solar ponds using thermometric generators via both fully passive design and active design. Certainly, this study will provide the insight on how much cost and electrical output one should expect from thermometric generators via fully passive design as well as active design. This work will delineate a thorough methodology on assessing a novel electrical power generation design starting with the conceptual design, to the fabrication and performance assessment of the proposed system.

### **1.4 Scope**

The intent of this work is not to sensationalize sustainability or disseminate it as an elixir that can remedy all development and environmental concerns, but rather to realistically

address a single question: “Will the synthesis of solar pond and thermoelectric generators creates an auspicious alternative for electric power generation, particularly in a remote area?”

In light of the concern stated, the scope of this work will concentrate on the modelling, design and the testing of an innovative electric power generation using the heat available from the solar pond. As the overall reliability and verification of the SP-TEGs system require an on-site installation and undergo long-term field test (which could possibly at least a year). Thus, this scope was not covered in this thesis.

### **1.5 Objectives**

- i. To examine the prospect of electric power generation by using solar pond with thermoelectric generators.
- ii. To develop thermoelectric power generation unit for electric power generation using the heat available from the solar pond.
- iii. To provide an insight on the economics feasibility on electric power generation using low-grade heat from the solar pond.

### **1.6 Research Questions**

- i. How will the commercially available thermoelectric modules perform under the operating temperature of solar pond and the reliability of the thermoelectric module?
- ii. How much electrical power generation one should expect from the proposed system annually, e.g. per m<sup>2</sup> solar pond? How will the proposed electric power generation systems perform under solar pond build in different climate condition (i.e. different region in the world) and/or different solar pond design parameters?
- iii. Under limited number of thermoelectric modules (i.e. limited expenditure), for a given dimension of the solar pond as well as certain temperature profile (heat source), what kind of configuration of power generation unit in plate type design will result in maximum electric power generation with minimum amount of cooling water usage? Also, how much output power we could expect?
- iv. For small scale electric power generation, what are the design parameters that will contribute to the optimal design of electric power generation using solar pond at lower convective zone with fully passive design and how do the parameters influence the system performance?
- v. Furthermore, in line with research questions (ii–iv), in economics point of view, what is the cost and benefit for the system with the given size? Is the design both performance and economically feasible to be extended for large scale power production?

The research questions are constructed and refined in such a way that the research questions (i) and (ii) are linked to objective (i), research questions (iii) and (iv) are linked to objective (ii) and finally research question (v) is linked to objective (iii). There are strong originalities in this work and RMIT is the pioneer in trying to study the combined SP-TE system. As a result, the completion of this study will lead to one publication from each of the five research questions addressed, which are presented through a series of publication and incorporated as Chapter 3 to Chapter 7 in this thesis respectively.

### **1.7 Original Contributions**

The original contributions in this work through the series of publication included in this thesis are listed as follows:

- i. Delineated a method of continuous electricity generation from solar energy without the use of a battery.
- ii. Theoretical modelling of the transient thermal performance of solar pond under heat extraction mode for various climatic conditions along with validation.
- iii. Evaluated the full potential of solar pond-thermoelectric power generation under various climatic condition and heat extraction modes.
- iv. Established the range of thermal-electric conversion efficiency of the solar pond-thermoelectric system as a rule of thumb.
- v. Evaluated the performance and reliability of commercially available thermoelectric cells for power generation under continuous and thermal cycling operation.
- vi. Modelled, designed and tested an open channel plate type thermoelectric modules-embedded power generation unit operating at atmospheric pressure.
- vii. Evaluated the performance enhancement of plate type power generation unit with copper mesh insertion.
- viii. Modelled, designed and tested a passive syphon-based multilayer power generation module with solar pond.
- ix. Established the feasibility of solar pond-thermoelectric power generation.

## 1.8 Publication List and Thesis Structure

The publications listed below have been *peer reviewed and published* as the first author:

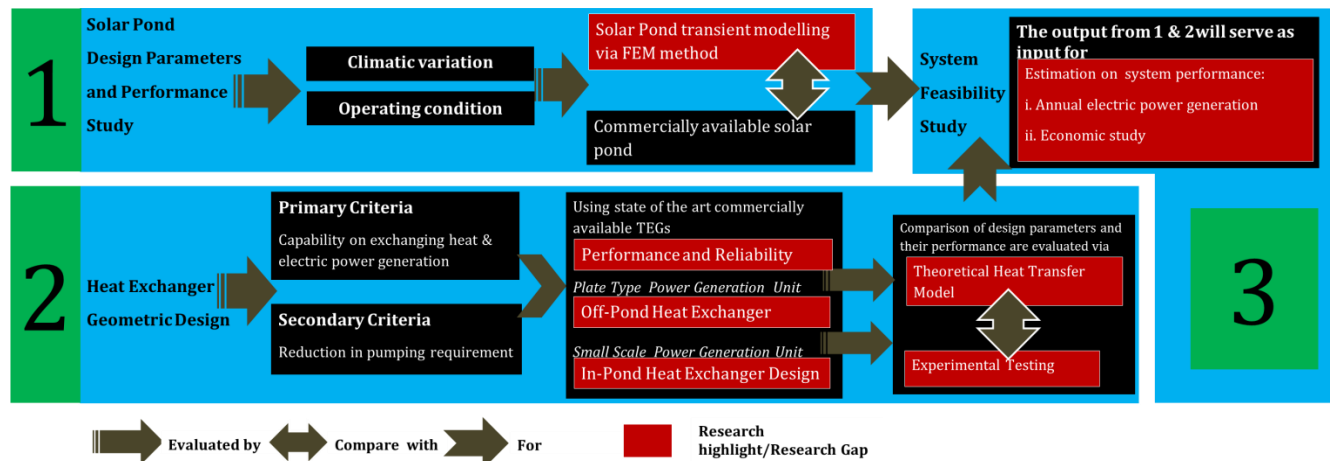
- i. **Ding, L.C.**, Akbarzadeh, A. and Date, A., 2016. Performance and reliability of commercially available thermoelectric cells for power generation. *Applied Thermal Engineering*, 102, pp.548-556. (As Chapter 3)
- ii. **Ding, L.C.**, Akbarzadeh, A. and Date, A., 2016. Transient model to predict the performance of thermoelectric generators coupled with solar pond. *Energy*, 103, pp.271-289. (As Chapter 4)
- iii. **Ding, L.C.**, Akbarzadeh, A. and Date, A., 2016. Electric power generation via plate type power generation unit from solar pond using thermoelectric cells. *Applied Energy*, 183, pp.61-76. (As Chapter 5)
- iv. **Ding, L.C.**, Akbarzadeh, A., Date, A. and Frawley D.J., 2016. Passive small scale electric power generation using thermoelectric cells in solar pond. *Energy*, 117, pp. 149-165. (As Chapter 6)
- v. **Ding, L.C.**, Akbarzadeh, A., Singh B.,and Remeli M.F., 2017. Feasibility of electrical power generation using thermoelectric modules via solar pond heat extraction. *Energy Conversion and Management*, 135, pp. 74-83. (As Chapter 7)

The work listed below has been *submitted and under review* for publication (fully integrated as Chapter 2-Literature Review):

- vi. **Ding, L.C.**, Akbarzadeh, A. A Review on Solar Pond for Power Generation and Its Alternative with Thermoelectric System. *Renewable & Sustainable Energy Reviews*.

This thesis was structured by using “thesis with publication” method. This thesis is started by the Introduction section (as Chapter 1), followed by Literature Review section (as Chapter 2), and then Chapter 3 to Chapter 7 with the publications as listed above in ordinal. Finally, the conclusions (both general and specific) and recommendation are presented in Chapter 8. As the bibliography of the references for Chapter 2 to Chapter 7 is readily available in the journal published, *only the list of references for Chapter 1 is provided at the end of Chapter 1.*

## 1.9 Expected Deliverables



**Fig. 3.** Schematic of research framework.

The framework for this research work is delineated in Fig. 3. Consequently, following workflow is adopted in order to achieve the objectives and comply with the framework.

i. *Thermal and electrical characteristic testing of thermoelectric cells*

Thermal and electrical characteristic were modelled and studied in order to perform theoretical modelling and parametric study of the heat exchanger in stage (iii and iv).

ii. *A transient modelling on the solar pond on the solar pond's performance*

The thermal performance of the solar pond was studied by using finite element method. The finding established will be used to predict the annual performance of the solar pond, which includes the performance in terms of thermal performance as well as the prospect of annual electrical power generation using the solar pond.

iii. *Electric power generation using solar pond with off-pond heat exchanger design*

The concept of a plate type heat exchanger was explored by incorporating thermoelectric cells. Heat exchanger design was optimised by taking into the account the dimensions of the heat exchanger, the flow rate of the system, the gap between hot and cold plates. The design selection will base on the consideration on maximum net power and maximum specific power of the system. An experimented test rig was built and fabricated according to the optimised design in order to verify and to compare with the theoretical model.

iv. *Electric power generation using solar pond at lower convective zone with fully passive design*

A submersible type siphoned based heat exchanger will be conceived for the in-pond small-scale electrical power generation. Different polygon geometry will be explored for both the outer and inner tube. Since this method requires no pumping

power, hence the design with maximum output and minimum volume are most desirable. This fully passive design will further extend to the fabrication of the test rig as proof to the concept developed.

- v. *Amalgamating the annual performance of solar pond and prototype performance to estimate annual system performance in conjunction with economics analysis*

The outcome from the stage (ii) will combine with the outcome from the stage (iii and iv). The ultimate outcome when reaching this stage is, for a given annual solar insolation data, the annual power generation from the system can be estimated.

Besides, the work performed at this stage will provide two main desired which are the cost of electricity and carbon dioxide emission reduction.

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World Energy Council. <<http://www.worldenergy.org/data/trilemma-index/>> (accessed 16.2.2017)

## **Chapter 2: A review on power generation with thermoelectric system and its alternative with solar ponds**

A copy of the manuscript submitted is attached following the end of this thesis.

## **Chapter 3: Performance and reliability of thermoelectric cooler for power generation**

Published As: Ding, L.C., Akbarzadeh, A. and Date, A., 2016. Performance and reliability of commercially available thermoelectric cells for power generation. *Applied Thermal Engineering*, **102**, pp.548-556. doi:10.1016/j.applthermaleng.2016.04.001  
<http://www.sciencedirect.com/science/article/pii/S1359431116304847>

## **Chapter 4: Transient model to predict the performance of thermoelectric generators coupled with solar pond**

Published As: Ding, L.C., Akbarzadeh, A. and Date, A., 2016. Transient model to predict the performance of thermoelectric generators coupled with solar pond. *Energy*, **103**, pp.271-289. doi:10.1016/j.energy.2016.02.124  
<http://www.sciencedirect.com/science/article/pii/S0360544216301864>

## **Chapter 5: Electric power generation via plate type power generation unit**

Published As: Ding, L.C., Akbarzadeh, A. and Date, A., 2016. Electric power generation via plate type power generation unit from solar pond using thermoelectric cells. *Applied Energy*, **183**, pp.61-76. doi:10.1016/j.apenergy.2016.08.161.  
<http://www.sciencedirect.com/science/article/pii/S0306261916312703>

## **Chapter 6: Passive small scale electric power generation using thermoelectric cells in solar pond**

Published As: Ding, L.C., Akbarzadeh, A., Date, A. and Frawley D.J., 2016. Passive small scale electric power generation using thermoelectric cells in solar pond. *Energy*, **117**, pp.149-165. doi: 10.1016/j.energy.2016.10.085  
<http://www.sciencedirect.com/science/article/pii/S0360544216315195>

## **Chapter 7: Feasibility of electrical power generation using thermoelectric modules via solar pond heat extraction**

Published As: Ding, L.C., Akbarzadeh, A., Singh B., and Remeli M.F., 2017. Feasibility of electrical power generation using thermoelectric modules via solar pond heat extraction. *Energy Conversion and Management*, **135**, pp. 74-83. doi: 10.1016/j.enconman.2016.12.069  
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# Chapter 8: Conclusion & Recommendations

## 8.1 Conclusion

### 8.1.1 General

This thesis had presented a comprehensive study on the potential of electric power generation from the solar pond using thermoelectric modules. The work had been started by evaluating the suitability of commercially available Peltier cells in terms of performance and reliability for power generation. Upon the confirmation of its applicability, the tested performance of the TECs was used in the estimation of the transient performance of the TECs operate with the solar ponds (SPs). A validated transient heat transfer model was coupled with the actual performance of the TECs in order to have a good estimate of the potential (i.e. upper limit) of the SP-TE system. Then, the evaluation of the SP-TE system was subjected to experimental testing after the design optimisation. Two different designs had been conceptualised and realised, which were in the plate type counter flow configuration and also submersible power generation unit. Overall, the SP-TE system is infeasible for large-scale application and hence SP-TE system is only suitable for auxiliary electrical supply. The specific conclusion to the research questions is as in the following subsection.

### 8.1.2 Specific Answers to Research Questions

- *How will the commercially available thermoelectric modules perform under the operating temperature of solar pond and the reliability of the thermoelectric module?*

*This research question has been addressed in the publication corresponds to Chapter 3.*

In the first part of the testing on commercially available thermoelectric cell (normally used for cooling application), it provides a direct answer on the thermal resistance, thermal-electric conversion efficiency and the estimation of the electric output of power generated by the cells that will be embodied in the heat exchanger in terms of the temperature difference,  $\Delta T$  across the TEC. On average, a commercially available TEC is able to convert the thermal heat supplied to electricity at conversion efficiency in the vicinity of 8.67% of its Carnot efficiency. Also, it had been shown that, exposing the cells at high temperature for prolonged period should be avoided since it eventually leads to a permanent reduction of the electrical output generated. Furthermore, from the testing conducted, commercially available TECs tested are reliable to be used under thermally cycled hot side temperature  $< 90\text{ }^{\circ}\text{C}$  and cooled at ambient temperature, for at least 500 cycles as tested. However, one may encounter TECs



malfunction when the TEC is exposed to a thermal cycling to a hot temperature in vicinity of 150 °C.

- *How much electrical power generation one should expect from the proposed system annually, e.g. per m<sup>2</sup> solar pond? How will the proposed electric power generation systems perform under solar pond build in different climate condition (i.e. different region in the world) and/or different solar pond design parameters?*

*This research question has been addressed in the publication corresponds to Chapter 4.*

In order to address this research question, various considerations had been explored, which include the effect climates, the possibility of manipulating the rate of heat transfer to optimise the generation of electrical power as well as the effect of temperature polarisation on the performance of the system. The solar pond that operates in Riyadh (Bwf) will perform the best, followed by Granada (Csa), while the solar pond in Kuala Lumpur (Af) and Melbourne (Cfb) will have almost similar performance in generating electricity. For a typical SP with UCZ, NCZ and LCZ thickness of 0.2 m, 1.0 m and 1.0 m, respectively; the theoretical performances of the SP-TE system in terms of electrical energy at the above-mentioned location with a typical 15% of annual average horizontal solar radiation are: Riyadh (4.834 kWh/year-m<sup>2</sup>), Granada (3.173 kWh/year-m<sup>2</sup>), Kuala Lumpur (2.498 kWh/year-m<sup>2</sup>) and Melbourne (2.412 kWh/year-m<sup>2</sup>). Even though the thermal-electrical conversion efficiency  $\eta_t$  is in the range of 1% – 1.5% from the heat extracted, the unconverted thermal energy extracted (which is about 98.5% – 99%) could be beneficial for any industrial process that requires low grade heat source from solar pond.

- *Under limited number of thermoelectric modules (i.e. limited expenditure), for a given dimension of the solar pond as well as certain temperature profile (heat source), what kind of configuration of power generation unit in plate type design will result in maximum electric power generation with minimum amount of cooling water usage? Also, how much output power we could expect?*

*This research question has been addressed in the publication corresponds to Chapter 5.*

In order to address this research question, a proof of concept on the electric power generation by TECs with solar ponds had been carried out experimentally and operated under different conditions. The plate type power generation unit (PTPGU) proposed was subjected to an open channel flow, which consists of 20 plates with 25 TEGs (at 5 × 5 arrays) as a result of the optimisation along with estimating the electric output using the performance curve of

single TEC. The PTPGU fabricated was then tested after ensuring a good flow distribution via visualisation. From the testing conducted, electrical power output of 35.9 W was generated under the condition of  $\dot{V}_c = 18.5$  LPM and  $\dot{V}_h = 5.1$  LPM at the temperature of  $T_{c,in} = 25$  °C and  $T_{h,in} = 81$  °C, which corresponds to 0.43% thermal to electrical conversion efficiency and power density of 3.3 kW/m<sup>3</sup>. The flow rates tested in the experiments are within the regime of laminar flow (achievable by using the supply from the main without the use of pump), hence there will be no significant different or improvement due to the flow increment within this regime. It had been shown that the theoretical model proposed is adequate to predict the performance of the PTPGU after comparing the performance of the PTPGU obtained experimentally with the theatrical prediction. Furthermore, it has been shown that, small degree in performance enhancement of the PTPGU is possible through copper mesh insertion. A separate test on the PTPGU shows that, the water head requirement is about 0.4 mH<sub>2</sub>O (4 kPa) in delivering 4.5 LPM for each channel, which was tested at twice the maximum flow rate of the testing result presented. The head required is much lower than regulated maximum water supply pressure under building regulation, which is around 5.0 mH<sub>2</sub>O (e.g. plumbing code of Australia).

- *For small scale electric power generation, what are the design parameters that will contribute to the optimal design of electric power generation using solar pond at lower convective zone with fully passive design and how do the parameters influence the system performance?*

*This research question has been addressed in the publication corresponds to Chapter 6.*

In order to address this research question, an immersive type power generation unit (PGU) was devised. The unit is expected to be submerged in the LCZ of the solar ponds, and the cold water at the UCZ is circulated through the PGU with the use of siphoning action. Beginning with the theoretical modelling, the estimated performance for different geometries at varying gap size and the flow rate was studied. Based on the outcome derived from the theoretical study, a PGU with Q-Q configurations was selected, due to its simplicity and there is no significant different on the geometry selection to its maximum performance. In order to include a higher number of TECs in the PGU, a dual layer PGU was fabricated in this work. From the tests conducted, additional 67% of the number of TECs at outer layer into inner layer will generate extra 44% of output power. The PGU produced a maximum power of 40.8 W under the condition of  $T_h = 99$  °C. Realistically, under the normal operation of solar ponds, the LCZ will have a temperature lies in the range of 40 °C – 80 °C. Thus, maximum output in

the range of 19.5 W – 27.4 W is more realistic for this SP-TE system proposed with the heat to electric conversion efficiency ranges between 0.37% – 0.68 %.

- *Furthermore, in line with research questions (ii-iv), in economics point of view, what is the cost and benefit for the system with the given size? Is the design both performance and economically feasible to be extended for large scale power production?*

*This research question has been addressed in the publication corresponds to Chapter 7.*

The feasibility study of the SP-TE system was analysed in different operating climate condition, which are Group A, B, and C of Köppen climate classification represented by Kuala Lumpur, Riyadh, Melbourne, and Granada. The feasibility study was based on the combination of a verified theoretical transient model for SPs and experimentally tested TE system. The cost of this system was analysed in terms of area per unit power, giving the flexibility in the sizing of the system. Furthermore, since the itemised cost of the SPs was presented, it provides the reader with the information on the practical costing for the solar pond. Later, the energy cost of the SP-TE system by considering its lifetime operation as well as the carbon emission reduction by the operation of SP-TE system was analysed and discussed. Overall, the SP-TECs system is at least 10 times costly compared with other renewable energy sources solar PV system with storage at the cost of \$5.4/ kWh<sub>e</sub> for ideal case and of \$41.9/ kWh<sub>e</sub> for the practical case. The lowest cost of \$5.4/ kWh<sub>e</sub> presented was based on (tested) conservative efficiency ratio with  $r = 8.85\%$ . If the thermoelectric module used has a  $ZT$  value of 1.3, then it is equivalent to efficiency ratio of 20%. With the increase of electrical power generated, the lowest cost of the system will reduce by 2.25 times, to \$2.4/ kWh<sub>e</sub>. This value suggests the SP-TE system is not a profitable mean for large power generation; rather, it serves as an option of electricity generation in meeting limited electrical energy demand. Also, this study provides the insight on the potential of the SP-TE system and reveals that, under its best operating climate (which is Riyadh), this system will able to achieve annual CO<sub>2</sub> reduction of 2.38 kg/m<sup>2</sup>-year in practical case.

## **8.2 Recommendations**

As the SPs possess a limited range of hot water temperature in the LCZ, it limits the widespread of the SP-TE system. Hence, it is viable to embrace another type of heat source that utilise solar energy for higher output power and conversion efficiency such as augmented solar collector. The SP-TE system is a viable option for small scale electric power generation

and as found from this work, submersible power generation unit will be able to generate adequate electric power to power some on-site facilities (such as lighting) that require a relatively small amount of electric power. However, this study has not addressed the long term reliability of this system when the TECs operate in the hot saline condition in LCZ. Thus, this opens another research question that can be investigated further. SP is a reliable supply of low-grade heat. Generating the electricity from the heat available by using certain mechanism (such as ORC, or TECs as in this study) will result in the diminishing of overall system efficiency (from incoming solar radiation to electric output) since the overall system conversion efficiency is the product of SP's efficiency and thermal to electrical conversion efficiency of the mechanism adopted. Put it the other way around, despite generating electricity from the SP directly, research can be explored on how the heat from the SP can be used for reducing heating demand for the particular heating process. It will able to reduce the electricity consumption and indirectly 'generated' positive balance of electric supply.

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*The End*

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# 1 **A Review of Power Generation with Thermoelectric System and Its** 2 **Alternative with Solar Ponds**

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## 7 **Highlights**

- 8 • A review of the recent research of thermoelectric generators is presented.
- 9 • The research on the solar pond as a heat source is discussed.
- 10 • Power generation with thermoelectric generators and solar ponds is possible.

## 11 **Abstract**

12 By using the Seebeck effect to produce electrical voltage, thermoelectric as a highly scalable,  
13 stationary and silent heat engine has undergone a state of vigorous research. Starting with the  
14 review on thermoelectric generators, it shows that thermoelectric is gaining more attention  
15 since the past decade. Generally, the research conducted on the thermoelectric generators  
16 concentrate on the material development, mathematical and numerical model development as  
17 well as the application of thermoelectric generators. For this article, attention is given to the  
18 application research of the thermoelectric generators. From the survey conducted, most of the  
19 application research carried out is based on intermittent electrical power generation (e.g. the  
20 direct use of solar energy available or waste heat recovery). Hence, it opens an opportunity  
21 for the research on the application of thermoelectric generators by utilising a heat source that  
22 is continuously ready for thermal-electrical energy conversion, such as phase change material,  
23 geothermal heat or solar pond. In the later section, the review is continued by introducing  
24 solar pond, a facility that has been used as a supply of low-grade heat source at the remote  
25 area or industrial process heating. The research on the fundamentals of solar pond and its  
26 applications, but not limited to, the power generation has also been summarised. The ultimate  
27 idea of this review is to provide an insight that a thermal-storage based heat source (e.g. in  
28 this review, the solar pond) could be useful for small-scale electric power generation, despite  
29 its ordinary function as low-grade heat source provider via heat extraction.

30 **Keywords:** Renewable energy; Power generation; Thermoelectric; Solar energy; Solar pond

## 31 1. Introduction

32 Countries around the globe have been aware of the rise in global average temperature  
33 and start to implement energy policies that will hopefully curb the temperature rise below 2°  
34 C at the end of the century. Some researchers have argued that the notion of global  
35 temperature rise is invalid and using the temperature rise as an ‘achievement indicator’ is  
36 futile due to its incapability in fathoming human activities that undermining the earth [1]. The  
37 Kyoto Protocol set up in 1997 aimed to reduce the emission of greenhouse gasses with an  
38 average cut around 5% relative to 1990 levels by 2012. Seemingly, not all of the countries  
39 with the binding target successfully achieve the aim and overall, the change in the global CO<sub>2</sub>  
40 emission had increased by 11.3 GT from 1990 to 2011, with China and other developing  
41 countries contribute the most increment in CO<sub>2</sub> emission. It was only in the recent COP21  
42 meeting at Paris, a clear binding agreement in reducing the in CO<sub>2</sub> emission and aiming to  
43 keep the temperature rise at 1.5°C in the end of the century. Clearly, in order to achieve the  
44 mission, there is a need to speed up the move to low carbon electric producing technology  
45 and preferably renewable energy. The selection of technology in implementing renewable  
46 energy power supply is depending on the types green resource that is conveniently available  
47 due to geographical advantage, human resources or technological resources that a country  
48 readily advanced. With the abundance of heat available, either from the sources that are  
49 freely available such as solar energy, geothermal energy or unutilised energy in the form of  
50 waste heat. This paper begins with a review on the thermoelectric generators (TEGs), a  
51 device that producing electric power as a result temperature difference through the flow of  
52 heat with the focus on recent development of TEGs’ application. Current development on the  
53 thermoelectric materials is impeded by thermoelectric figure of merit,  $ZT$ . Unless there is a  
54 quantum leap in the breakthrough of , otherwise thermoelectric technology in driving a  
55 primary role in the electric source is impossible and it will remain as an supplementary  
56 technology that enhances the performance of current renewable energy power generation.  
57 Then, in the later part, the review of the solar pond, a facility that collects and stores solar  
58 energy is delineated. Realising the electrical storage-based system (i.e. the use of batteries at  
59 the post-electric generation stage) will be the most commonly adopted method for the long  
60 term power storage. Overall, through this review, the authors would like to introduce the  
61 option of thermal storage-based electric power generation system using TEGs.

## 63 2. Thermoelectric Generator (TEG)

64 The use of TEGs as a potential source of for both large scale electric powers as well  
65 as an alternative source for low power generation had been delineated by Rowe that presented  
66 in his publications [2, 3]. From the life cycle analysis conducted, apart from being  
67 environmentally friendly, from the economics point of view, the increase in fuel cost will  
68 lead to the demand of alternative mean for power generation. The inclusion of externalities  
69 consideration will certainly favour the use of TEG as a supplement for electrical energy  
70 production [4].

### 71 2.1 Properties, Material, Structure, and Characteristics

72 Dueto the existence of temperature gradient, the TEG's operation is based on Seebeck  
73 effect and Peltier effect. The former phenomenon, refers to the relation between  
74 thermoelectric potential under open circuit condition and the temperature difference is  
75 correlated by the Seebeck coefficient,  $\alpha$  (V/K). Hamid Elsheikh et al. [5] in the recent review  
76 described the important parameters that govern the performance of the thermoelectric cells.  
77 The authors analyse the parameters from the viewpoint of thermoelectric properties and  
78 material properties, and extended the discussion on the life expectancy of the thermoelectric  
79 cells. They strongly believed that the study on the relation of both electrical and thermal  
80 conductivity is the key for improving the performance of thermoelectric cells.

81 There are different materials available for TEG in order to cater a different range of  
82 operating temperature. Different categories of materials had been explored, such as ceramics  
83 [6], alloys [7], bulk material [8], complex crystals, oxide materials [9, 10], nano-composites.  
84 Table 1 summarises the TEG materials, working temperature as well as the  $ZT$  value of these  
85 materials.

86 **Table 1**  
87 TEG materials and its performance [11-13].

Operating Temperature, °C	Type	Materials	Maximum $ZT$
<150	p	$\text{Bi}_{0.5}\text{Sb}_{1.5}\text{Te}_3$	1.4
	n	$\text{Bi}_2\text{Se}_{0.3}\text{Te}_{2.7}$	1.0
	p,n	$\text{Bi}_2\text{Te}_3$	0.8
150-500	p	$\text{Zn}_4\text{Sb}_3$	-
	p,n	PbTe	0.7-0.8
	p	TeAgGeSb	1.2
500-700	p	$\text{CeFe}_4\text{Sb}_2$	1.1
	n	$\text{CoSb}_3$	0.8
700-900	p,n	SiGe	0.6-1.0
	p	LaTe	0.4

89 From Table 1, it is clearly seen that under current development, the BiTe-based material is  
90 the most suitable commercially available material to suit the need of recovering low-grade  
91 heat (<150°C). Although the TEGs operate base on the temperature difference across its hot  
92 and cold junction, there exists a difference in maximum electric power in spite of the fact that  
93 the temperature difference across the junction remains constant, since the specification of  
94 temperature difference gives two degrees of freedom for the values of cold and hot  
95 temperature. Specifically on Bi<sub>2</sub>Te<sub>3</sub>, which operates at temperature <150°C, for a fixed  
96 temperature, there exist both upward and downward concavity in the graphs of maximum  
97 power versus mean temperature (average of temperatures at the hot and cold junction). In the  
98 other words, in order to achieve similar maximum power output, for a given fixed  
99 temperature difference, the number of thermoelectric cells needed varies [14]. For the middle  
100 and high range of temperature, research had been carried out in the searching and  
101 characterisation of new thermoelectric materials [15] and reducing the cost for TEG [10].

## 102 **2.2 Mathematical and Numerical Model Development of TEG**

103 In the mathematical modelling of the TEG, often the heat transfer between the TEG and  
104 its environment are modelled by Newtonian heat transfer law with the heat transfer rate,  $\dot{Q}$  is  
105 directly proportional to the temperature difference,  $\Delta T$ . In order to take into account the  
106 thermodynamics irreversibility of TEG, Chen et al. [16] developed an advanced model of  
107 TEG by considering the irreversibility characteristic of TEG. The five heat transfer laws  
108 under consideration were Newtonian, linear phenomenological, radiative, Dulong-Petit as  
109 well as special complex transfer law. The study showed, external heat transfer model using  
110 Newtonian law yield highest efficiency and power output compared the other four heat  
111 transfer laws, and external heat transfer models considered will vary working electrical  
112 current that results the optimum operating condition of TEG. Besides, Montecucco et al. [17]  
113 proposed the solution to the 1-Dimension transient heat conduction equation by incorporating  
114 the internal heat generation of TEG. As a result, without fixing the hot side and cold side  
115 temperature of the TEG, the transient characteristic of TEG can be evaluated.

116 With the advancement of the computational method, TEG model can be accurately  
117 simulated [18,19]. When the TEG is exposed to the heat source with a temperature difference,  
118 the device is undergoing transient state before the thermal and electrical dynamically stabilise.  
119 Peltier, Seebeck, Thomson, and Joule are the main effects that taking place in the TEG.  
120 Montecucco and Knox [20] modelled the response of TEG under the changing operating  
121 condition by using a computer aided model. By taken into account of the important



122 thermoelectric effect such as Joule heating and Peltier effect, the computer model developed  
123 will able to predict the TEG response in high accuracy. Although the model did not include  
124 the Thomson effect, however, according to Nguyen and Pochiraju [21], Thomson effect is  
125 significant in giving impact on the power generation rather than the thermal behaviour of the  
126 TEG.

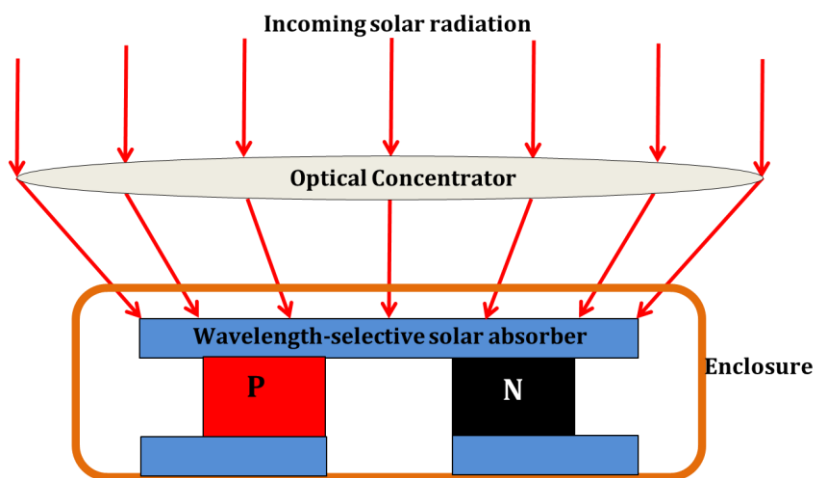
### 127 **2.3 Recent Development on TEGs' Application**

128 The TEG can be integrated into various systems, such as, but not limited to heat  
129 exchanger system, exhaust gas heat extraction, solar heat extraction, industrial waste heat  
130 recovery, or couple with other renewable energy sources, e.g. solar photovoltaic system,  
131 forming a hybrid system for better power conversion efficiency as delineated by Kremer et  
132 al. [22]. TEG may also be used for electricity generation for terrestrial application by using  
133 optical concentrator and solar absorber with wavelength-selective surface [23] or generating  
134 electricity from human body heat with the aid of heat sink [24, 25]. Although the use of TEG  
135 for remote area power supply is far away to be realised. However, it had been shown from the  
136 experimental study that the use of TEG in powering autonomous sensor at the remote area is  
137 feasible [26]. The innovative design of heat exchanger for electric power generation using  
138 TEG had been conducted. Different design of heat exchanger were considered: (i) roll cake  
139 type heat exchanger; a helical flow system, (ii) cylindrical multi-tubes design; including  
140 counter flow, parallel flow and isothermal heat exchanger [27-29].

### 141 **2.4 TEG in Solar Heat Extraction System**

142 As a source of green energy, solar energy can be utilised to generate electricity  
143 through the photovoltaic panel, space heating, or solar thermal energy storage via the solar  
144 collector. The research on generating electricity with TEG by harvesting the solar energy was  
145 mainly conducted base on the concentration of solar radiation in order to achieve higher hot  
146 side temperature for higher conversion efficiency. The sunlight concentration was either  
147 achieved via parabolic concentrator [30] or with the use of a lens to focus the light beam at  
148 the hot surface of the TEG. Besides using lens to increase the hot side temperate of the TEG,  
149 the performance of the TEG can be further enhanced by concentrating the thermal energy to  
150 the TEG with the use of a thermal absorber, thermal collector or in the recent study, the use  
151 of carbon nanotubes sheet to absorb the solar energy [31]. In 2011, the NanoEngineering  
152 research group from MIT made a breakthrough in the development of flat-panel solar  
153 thermoelectric generator with high thermal concentration at high performance. The solar TEG  
154 (STEG) system (shown in Fig. 1) was conceived to capture the heat resulted from solar  
155 radiation and serve as the heat source for TEG to generate electric power. The theoretical

156 study [32] of STEG had been established and according to Chen, the efficiency of the STEG  
157 is depending on both opto-thermal efficiency and the TEG efficiency, the improvement in the  
158 hot side temperature will favour the increasing of TEG efficiency [33] but such increment  
159 will cause a reduction in the opto-thermal efficiency of the STEG. Hence, according to the  
160 model, there exists an optimum point of hot side temperature for maximum system efficiency.  
161 Subsequently, for low-grade heat for electric power generation, using the commercially  
162 available TEG with  $\text{Bi}_2\text{Te}_3$  in STEG system will able to achieve efficiency greater than 5%,  
163 theoretically. With the same layout as depicted in Fig. 1, Kraemer et al. [34] conducted the  
164 experimental study on the STEG system and verified that such system can achieve an  
165 efficiency at a record-breaking 7.4% with concentrated solar irradiance of  $211\text{kW/m}^2$  With  
166 the advancement of the figure of merit,  $ZT$  of the thermoelectric material, the STEG  
167 efficiency can be improved further. The research on the STEG had been studied theoretically  
168 in terms of exergetic analysis [35, 36], geometrical optimisation [37] and performance  
169 estimation through finite elements computational modelling [38, 39]. Also, The operation of  
170 STEG ( $\text{Si}_{80}\text{Ge}_{20}$ ) at high concentration ratio ( $>100$ ) and high temperature ( $>450\text{ }^\circ\text{C}$ ) had been  
171 modelled and validated by Pereira et al. [40].

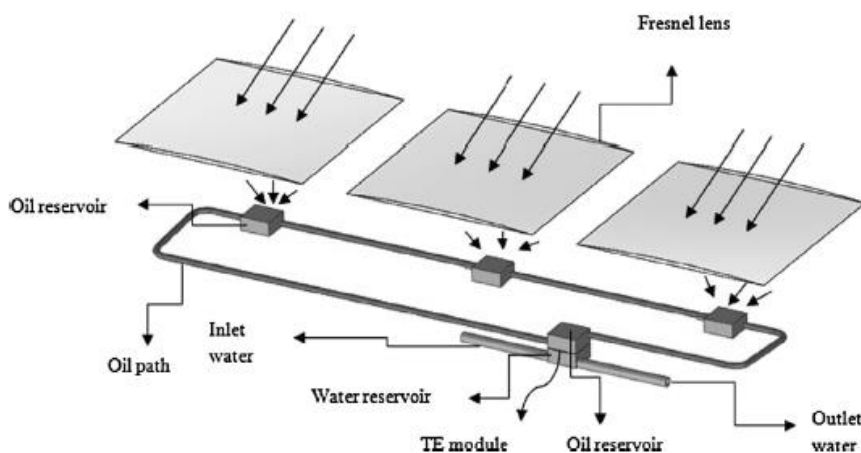


172 **Fig.1.** The STEG system.  
173

174 Furthermore, Tayebi et al. [41] suggested a potential improvement of the planar thin  
175 film thermoelectric devices for solar power generation through the deposition and patterning  
176 of thermoelectric layers and the substrate coating selection. The study of introducing  
177 spectrally selective high-temperature absorber coating (which is stable up to  $512\text{ }^\circ\text{C}$ ) on the  
178 STEG had been investigated by Candadai et al.[42]. Their study illustrated that a conversion  
179 efficiency of 4.7% can be achieved in their STEG system at hot side temperature of  $300\text{ }^\circ\text{C}$   
180 and cold side temperature of  $30\text{ }^\circ\text{C}$  for commercially available  $\text{Bi}_2\text{Te}_3$  TEG of  $ZT = 0.4$ . So  
181 far, at a conversion efficiency of 3%, the work conducted by Amatya and Ram [43] is the

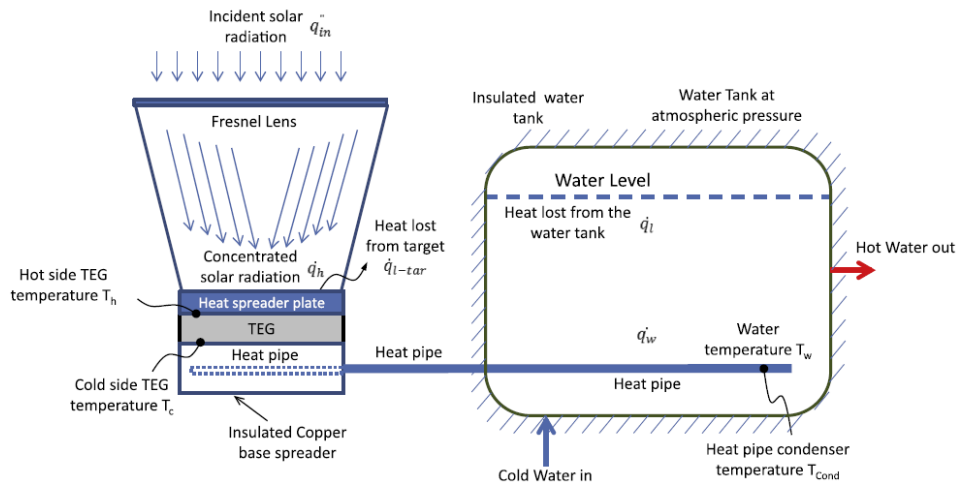
182 highest efficiency reported by using commercially available  $\text{Bi}_2\text{Te}_3$  modules under optical  
183 solar energy concentration of 66 suns. However, the alleged performance of the  
184 aforementioned studies should be subjected to further justification via a long term operation  
185 at hot side temperature of  $300\text{ }^\circ\text{C}$  since previous study conducted by Ding et al. [44] indicates  
186 that at continuous operation at hot side temperature  $> 200\text{ }^\circ\text{C}$  will result in the degradation in  
187 the performance of the commercially available  $\text{Bi}_2\text{Te}_3$  thermoelectric module. For improving  
188 the performance of STEG system, minimizing the heat loss through maintaining a vacuum  
189 condition in the enclosure of the STEG system is equally important. The effect of the  
190 enclosure pressure on the performance of STEG had been addressed in the publication by  
191 Sudharshan et al. [45]. It is worthwhile to mention, for microscale electric power generation  
192 to power devices with low input power such as wires sensors, flexible thin film STEG by  
193 using BiTe as base material had also been researched recently [46, 47].

194 The application research of concentrating the sunlight using Fresnel lens coupled with  
195 TEG had been reported by Olsen et al.[48] and Nia et al. [49]. The system investigated by  
196 Nia et al. is shown in Fig. 2. In contrast to the use of a flowing working fluid (usually water)  
197 to provide the cooling at the cold side of TEG, Date et al. [50] carried out an experiment by  
198 using different cooling approach as depicted in Fig. 3. In the system proposed, heat pipes  
199 were being used to transfer the heat to a water tank, which in turn, the heated water in the hot  
200 water tank is ready for domestic consumption. As heat pipe is an efficient heat transfer device  
201 that possesses high thermal conductivity and hence has the potential to improve the heat  
202 transfer performance of the STEG system. In addition to the study carried out by Date et al.,  
203 theoretical [51] and experimental study [52] had been carried out to explore the system with  
204 STEG-heat pipe combination.



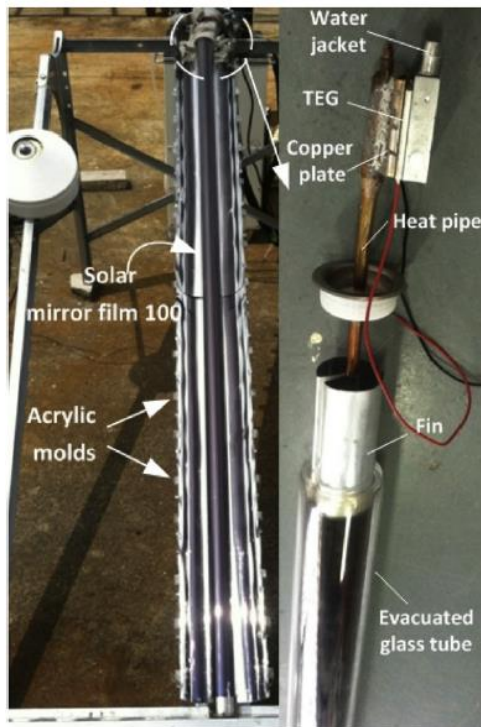
205  
206

**Fig.2.** The cogeneration STEG system using the thermoelectric module and fresnel lens [49].



207  
 208 **Fig.3.** The heat pipe cooled thermoelectric generators using concentrated solar thermal  
 209 energy [50].

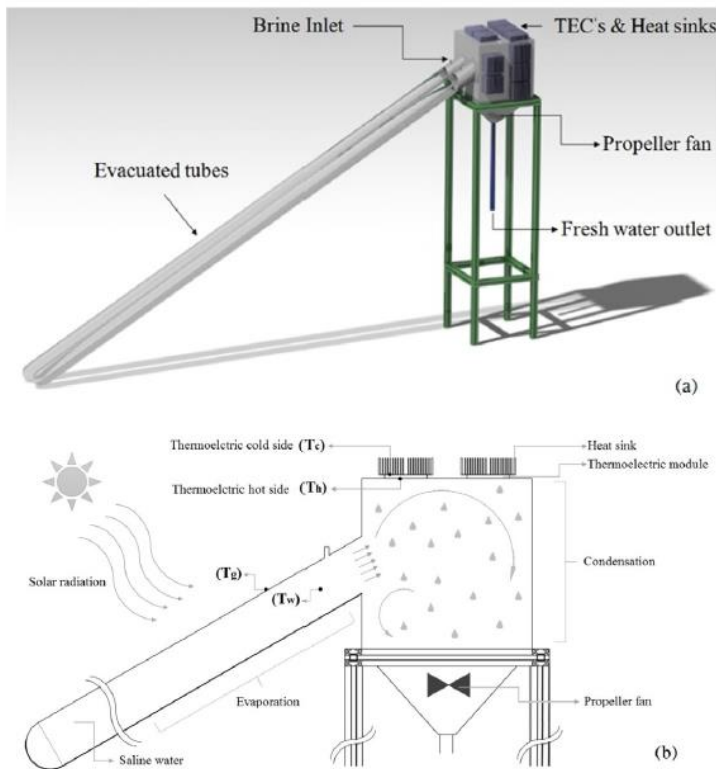
210 With the concentrated solar radiation and a vacuum environment that reduce the heat loss to  
 211 the surrounding, the investigation had been carried out for incorporating the TEG into solar  
 212 evacuated tube to achieve the functions as both hot water supply and generating electric  
 213 power. Dai et al. [53] through their experimental study, investigated the possibility of  
 214 generating electric from the solar hot water system with the additional aid of a parabolic  
 215 concentrator as shown in Fig. 4. Introducing the TEG into the solar evacuated tube requires  
 216 careful consideration since the high resistance across the thermoelectric elements is a  
 217 favorable condition for the operation of the TEG. However, imposing the high resistance  
 218 from the TEG on the solar evacuated tube will detriment the performance of the solar  
 219 evacuated tube since least thermal resistance is desired for the heat transfer in the solar  
 220 evacuated tube.



221  
222 **Fig.4.** Mini-CPC hybrid STEG unit [53].

223 In order to maximize the net electric power output generated by the TEG system,  
224 ideally the need of external pumping for the cooling of the system should be avoided.  
225 Furthermore, the amount of electric power generated from the solar evacuated tube relies on  
226 several environmental factors such as solar insolation that location dependent [54],  
227 atmospheric temperature [55] and wind speed. The influence of parameters mentioned earlier  
228 on the performance of the TEG system has been addressed by Li et al. [56]. Generally, higher  
229 solar insolation is beneficial since this will improve the conversion efficiency of the system,  
230 although thermal losses are greater at higher solar insolation. Meanwhile, the study concluded  
231 concluded that the increase in the wind speed and environmental temperature possess a  
232 negative effect on the performance of this system. On the flip side, the importance of the  
233 existence of wind in providing the cooling of the TEG to improve the performance of the  
234 TEG has been demonstrated by Moraes et al. [57] since in this study, the wind serves as an  
235 important mean to dissipate the heat at the cold side of the TEG. It had also been shown that,  
236 still air will result in extremely low electric power generation and by introducing the wind at  
237 even relatively low speed ( $<1$  m/s), it will result in a steep increase in the amount of power  
238 generated. Similarly, Özdemir et al. [58] designed and tested a TEG-solar evacuated tube  
239 system by using a wind chimney to serve as the heat sink with a reported maximum power  
240 output of 0.83 W with single  $\text{Bi}_2\text{Te}_3$  thermoelectric module that consists of 126 junctions.

241 Moreover, apart from desalinating the water with the use of a solar still, several  
 242 research had been done in combining the solar still with TEG. A typical design of the solar  
 243 still-TEG system is presented in Fig. 5, from the experimental work conducted by Shafii et al.  
 244 [59] with the use of solar evacuated tube. The energy from the condensed vapor was utilised  
 245 for electricity conversion. Due to the cost consideration, instead of using expensive TEG,  
 246 thermoelectric coolers which have an interchangeable function as TEGs were used. The power  
 247 generated by the thermoelectric modules (highest value of 1.32W) was used to power the  
 248 propeller fan in the condensation chamber. As a result of introducing forced convection via  
 249 the power generated from the TEG, the highest hourly water yield increased from 0.97  
 250 kg/m<sup>2</sup>h to 1.11 kg/m<sup>2</sup>h.



251  
 252 **Fig.5.** The evacuated tube collectors and thermoelectric modules equipped solar still [59].

253 Solar photovoltaic (PV) system and TEG have a common aim of generating electricity.  
 254 Throughout the years, numerous research had been conducted to amalgamate these two  
 255 systems. Regular crystalline silicon PV system utilise the solar energy in the lower range of  
 256 wavelength in the radiation spectrum and filters out the radiation in the wavelength higher  
 257 than 1200 nm in the infrared radiation since radiation at the wavelength higher than 1200 nm  
 258 is unusable and contributes to the heating of the PV cells. Realising the need of segregating  
 259 the solar radiation according its wavelength, Li et al. [60] proposed a spectrum beam splitting

260 technique and using the unusable solar radiation energy in PV electric generation for  
261 converting it into electricity through TEG. According to the calculation, the system proposed  
262 was having a potential of 30% improvement in the output power. However, the improvement  
263 is depending on the how the comparison was done. The integration of the PV-TEG will also  
264 lead to a poorer performance in terms of efficiency compared with the PV system alone, as  
265 discussed by Bjørk [61] after examining recent works conducted in the hybrid PV-TEG  
266 system. Theoretical study on the hybrid PV-TEG system had been conducted on the  
267 generalized thermodynamic model given by Kwan et al. [62], and analytical model of the PV-  
268 TEG system had been developed by Su et al. [63] for their performance optimization study,  
269 in addition to the previous work on the general performance optimization methodology  
270 published by Kraemer [22]. Current work on the novel PV-TE hybrid system had focused in  
271 the photon management, but not limited to the work carried out by Xu et al. [64]. The work  
272 presented by Da et al. [65] proposed the photon and thermal management of the PV-TE in  
273 order to improve the efficiency of the system. Particularly in the photon management, in  
274 order to reduce the reflection loss of the photons, a moth-eye structured surface had been  
275 discussed and analysed. For ZnO based dye-sensitised solar cell, Dou et al. [66] demonstrated  
276 a  $\text{Bi}_2\text{Te}_3/\text{ZnO}$  composite photoanode that will able to convert both photo and thermal energy  
277 simultaneously at an improved efficiency of 4.27%. In their design,  $\text{Bi}_2\text{Te}_3$  nanotubes were  
278 embedded into ZnO nanoparticles, providing a direct path for the electrons transfer and  
279 eventually improving the efficiency of dye-sensitised solar cell.

## 280 **2.5 *TE Power Generation Using Waste Heat***

281 The heat generated during the operation of the equipment will normally be wasted and  
282 discharged to the environment. Instead of being disposed, certain amount of heat can be  
283 recovered and be used to convert the energy from the waste heat into another form of energy.  
284 The analysis of power generation using waste heat had been studied by Wu [67]. Considering  
285 a hot junction with 400K and a temperature difference of 100K across hot and cold junction,  
286 an ideal Carnot cycle tells us that the efficiency of the system will be at 25% efficiency.  
287 However, due to thermodynamics irreversibility, an ideal system for waste heat recovery  
288 using TEG could only achieve efficiency of 4% for the boundary condition specified.  
289 Without transforming the energy from the waste heat into electrical energy, the energy  
290 recovered will able to serve as the energy source for a preheating process, for instance pre-  
291 heating in space heating, by the mean of utilising a heat exchanger. Recent prototype study  
292 on the use of liquid metal as the medium to transfer waste heat to the TEG showed favourable

293 result and leave a room for future exploration [68]. If the electrical energy is the desired  
294 output from the waste heat recovery process, then the use of Organic Rankine Cycle (ORC)  
295 or thermoelectric power generation will serve as a candidate for reaching the outcome. For a  
296 waste heat recovery system using ORC, working fluid with low boiling temperature and low  
297 operating pressure is used, such as R123 refrigerant (which will be phased out under  
298 Montreal Protocol). Both of the TEG and ORC can be combined into a system, according to  
299 Shu et al. [69] and theoretically, the system can achieve better efficiency compared to using  
300 ORC alone. There are several source of low-grade waste heat, for instance from cogeneration  
301 process, solar thermal, geothermal, and industrial waste thermal.

302         Recently, thermoelectric cogeneration system for domestic use had gained attention.  
303 Besides the potential for reducing the CO<sub>2</sub> emission, such system is able to perform both  
304 electric power generation and pre-heating process for domestic heating [70]. However, to  
305 date, the exploration of the application of TEG for domestic purpose is still limited. In order  
306 for a TEG to perform well with minimal variation in the amount output power generated, a  
307 relatively stable heat source is required. In the residential area, the most common appliance  
308 that can serve as the heat source for the TEG is, but not limited to the water heater. The water  
309 heater can be either gas-fired type or electric powered or a combination of solar heating. For  
310 the case of the gas-fired water heater, Qiu and Hayden [71] conceived a self-powered heating  
311 system by the heat generated from the natural gas-fired burner. In their further work [72], the  
312 design of the system was improved by preheating the air prior entering the burner with a heat  
313 recuperating process. From the study, the total power output generated from the TEG is  
314 1072W, with heat recuperation and a burner operating temperature of 1082°C.

315         Nuwayhid et al. [73] explored the feasibility of electricity generation using TEG  
316 through the heat extraction from the commonly available item in the house-the stove-top,  
317 which is beneficial to the area with inconstant power supply. In the study, low cost and  
318 simplistic were the main pillar of the design for the system. By using commercially available  
319 Bi<sub>2</sub>Te<sub>3</sub> modules and subjected to hot side temperature fluctuation of the stove, a 3.3W power  
320 production from a bare TEG module (i.e. without insulating wafer) was achievable.  
321 Nonetheless, with the option to upgrade the cost of TEG module, 6.5 W of power generation  
322 is attainable. On the other hand, Champier et al. [74] found, the use of Bi<sub>2</sub>Te<sub>3</sub> modules (which  
323 is a combination of four thermoelectric modules) in biomass cook stoves was able to produce  
324 6 W of electricity power to end user, after considering the trade-off of power losses as the  
325 result of power conversion.



326 In the country which the use of geothermal power generation is feasible, the  
327 geothermal low power heat can be utilised to serve as the heat source for the electricity power  
328 generation using TEG. Some studies had been attempted, on the electricity generation from  
329 geothermal heat source using TEG. It included, but not limited to the research carried out on  
330 the modelling and geometrical optimisation of the stack, combining the counter flow heat  
331 exchanger and the TEG modules [75], or even crossflow heat exchanger [76]. Moreover, it is  
332 worth to mention the successful work demonstrated by Sasaki et al. [77] in harvesting the hot  
333 spring thermal energy for electrical energy conversion using TEG. With a capacity of  
334 generating 900 W of electricity, the prototype fabricated coupled with the hot spring was able  
335 to generate 1.927 MWh in 8966 hours of operation throughout one and a half year of field  
336 test.

337 Another source of heat that can be recovered for electric power generation is via  
338 automobile exhaust. There were numerous studies had been conducted, for example, Yu and  
339 Chau [78] on the waste heat recovery automotive vehicle exhaust since it is one of the  
340 medium-high range of waste heat source for TEG application. Tzeng et al. [79] pointed out,  
341 besides the temperature difference across the TEG being the main parameter affecting the  
342 performance, other factor such as the operating condition of the TEG is crucial for electric  
343 power generation for automotive vehicle exhaust heat recovery. Under the operating  
344 condition domain, the study focused on the flow rate and the temperature of the inlet hot air  
345 as well as the flow rate of cooling air. Besides automobile exhaust as a subject for waste heat  
346 recovery for electric power generation, the study had been extended to recovering the heat  
347 from internal combustion engine, and the electric power generated is stored in the battery  
348 which control method adapted [78]. Low-grade heat can also be recovered from the heavy  
349 industry. The possible heat source for recovering the waste heat to generate electricity using  
350 TEG are from the furnace in the industry[80].

## 351 **2.6 On the Performance and Efficiency Improvement of TE Power Generation System**

352 Several designs of test rig were proposed for the performance testing of TEG [81-85].  
353 One of the challenges of the testing and development of TEG was the characterisation of  
354 TEG. The main issue lies on the measurement of heat flow, which the heat loss during the  
355 process of transferring heat from heat source to the hot side surface of TEG cannot be  
356 quantified accurately. As pointed by Rauscher et al. [81], the use of reference material to  
357 evaluate the heat flow by measuring the temperature difference can lead to systematic error.  
358 Due to the relatively high temperature difference between the heat source (i.e. heater) and the

359 ambient conditions, significant heat transfer via radiation happened. Hence in the efficiency  
360 measurement conducted by Rauscher et al. [81], Takazawa et al. [82], Anatychuk and  
361 Havrylyuk [83], the research had used a radiation shield around the heat source in order to  
362 reduce the radiation heat exchange to the surrounding. After the aforementioned precaution  
363 measure was implemented, the calculation for the efficiency should be based on the heat flow  
364 at the cold side of TEG, together with the power generated by the TEG.

365         There are few external parameters that will affect the power generation by the TEG  
366 when the TEG is coupling with the exchanger. The parameters such as load resistance, the  
367 flow rate of the working fluid and its properties, design of heat exchanger play a significant  
368 role in the power generation using TEG. Their respective influence on the power generation  
369 had been studied [86, 87]. With the currently available technology, the power conversion  
370 efficiency of TEG falls into the range of 5-6%. In order to produce the temperature difference  
371 across the thermoelectric modules, often the hot side is attached to a heat source and the cold  
372 side is attached to a heat sink. The heat sink can be either air-cooled or water-cooled. An  
373 interesting finding discovered by Chen et al. [88] revealed that the water flow rates as well as  
374 the flow pattern at the heat sink had an insignificant effect on the power generation of TEG  
375 and they further concluded that the heat source is the defining part on giving the TEG better  
376 performance. Meanwhile, Gou et al. [89] have different findings, in their study; they  
377 concluded that the heat dissipation by the heat sink will provide significant improvement on  
378 the TEG performance.

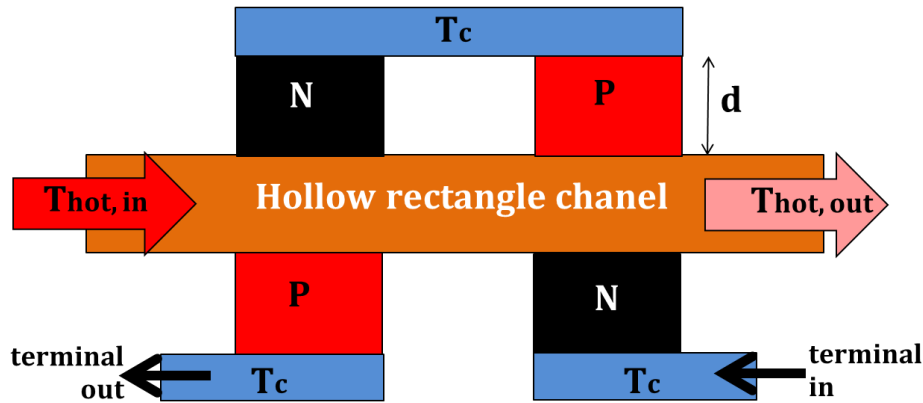
379         When a TEG is used as a device to generate electricity from the source of waste heat,  
380 a good strategy coupled with an efficient design of the heat harvesting system to capture the  
381 waste heat is crucial in order to yield a promising electrical output. Hence, optimisation  
382 should be performed on the attachment of TEG to the heat source. There were numbers of  
383 study performed on the design improvement in order to enhance the heat transfer from the  
384 heat source to the TEGs. Lee [90] pointed out those parameters such as the efficiency, power,  
385 and geometry of thermoelectric elements as well as the thermal resistance of heat sink were  
386 essential in optimising the design. An important conclusion from the dimensional analysis  
387 was, for a known heat source and heat sink temperature, there is an optimum design available.

388         When there is a number of TEGs attached together in order to produce greater power  
389 output, the spacing between TEG modules will give significant impact on the density of  
390 output power generated. Hence, the spacing between the TEG modules needs to be optimised.

391 As reported, the used of a spreader, attached between the surface of heat source and the hot  
392 side of the TEG will give a better temperature distribution on the hot side of the TEG and by  
393 the better temperature distribution, higher power density can be achieved [91]. In any  
394 thermofluids, the reduction of energy when the fluid travel downstream due to the heat  
395 transfer losses cause the variation on the temperature on a surface where the fluid passing by.  
396 When there is arrays of TEGs connected in either series or parallel in order to yield greater  
397 output power of the system, such ununiformed temperature profile creates an ununiformed  
398 temperature gradient across the TEGs and this means that each TEG will experience different  
399 temperature difference across their hot and cold surface. Eventually, this will result in, the  
400 significant reduction in the actual output power compared to the predicted maximum total  
401 output power. In regards with the aforementioned condition, Montecucco et al. [92] studied  
402 the mismatch condition of TEGs, by using 3 TEGs connected in both series and parallel.  
403 They summarised, such temperature maldistribution condition can cause significant power  
404 loss. However, by comparing the connection in series and parallel, the connection in parallel  
405 will cause more power loss compare with the connection in series, due to the fact that the  
406 connection in series will able to minimise the Joule heat loss in the system.

407 Furthermore, in recovering the waste heat from the automotive vehicle, particularly at  
408 the exhaust, from the study, it had been shown that, after certain number of TEGs attached in  
409 the heat recovery system, the total electric power generated will not increase as desired. In  
410 the other words, there will be a reduction of average power generated per TEG, since the  
411 “marginal power”, which is the power generated of the last TEG introduced into the system is  
412 reduced. Such condition happened, due to the limit of heat available to be recovered, causing  
413 the reduction of temperature of exhaust gas as it travels along the exhaust pipe [93]. The  
414 aforementioned scenario can be explained theoretically and had been modelled by Gou et al.  
415 [94], which stated that there will be a limit of electric power generated even though with the  
416 increasing area of cold side heat exchanger. Although logic tells us that more power can be  
417 produced if there are more TEGs being used in electric power generation using TEG,  
418 however, there exists a room for optimisation by altering the occupancy rate, which is was  
419 defined by Faveral et al. [95] to produce highest electric power using genetic algorithm. For  
420 the cases studied, maximum power was achieved when the TEGs do not occupy the whole  
421 range of hot side of heat exchanger, which is in accordance with the finding reached by Weng  
422 and Huang [93]. Reddy et al. [96] performed a study on multistage integrated TEG based on  
423 thermoelectric-hydraulic principle. As illustrated in Fig. 6, this system consists of

424 thermoelectric element bonded with high thermal and electric conduction material with  
 425 hollow rectangle flow channel. From the numerical study, the increase in the length of the  
 426 thermoelectric leg,  $d$  will optimise the maximum power, and both the increase in the volume  
 427 or temperature of hot fluid flowing into the channel will enhance the performance of the  
 428 system.

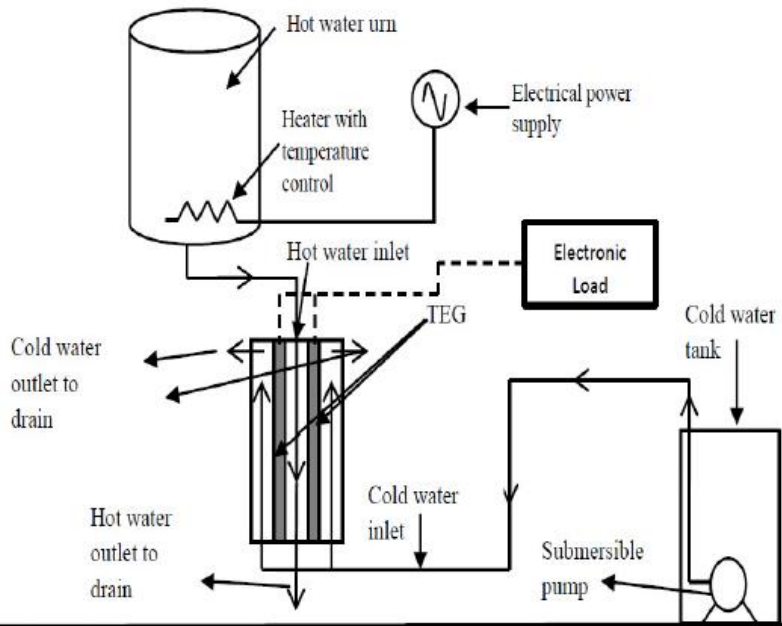


429  
 430 **Fig. 6.** Multistage integrated TEG [96].

431 **2.7 The Storage of Thermoelectric Power**

432 So far, the studies on the thermoelectric power generation were mainly focus on the  
 433 production of the electricity. Most of the time, the production of the electricity was  
 434 instantaneous, for example in the exhaust heat conversion and energy conversion from solar  
 435 energy. Hence, in this case, the power generated is either need to the instantaneously  
 436 consumed or, being stored in batteries. The process of maximising power extraction for the  
 437 charging of the battery is often equipped with maximum power point tracking (MPPT) and  
 438 it has gained attention over the wide range of thermoelectric power generated, from the  
 439 magnitude of  $\times 10^{-6}$  W [97, 98] to  $\times 10^3$  W [99]. The objective of the continuous power supply  
 440 can be achieved via two means, either through the continuous withdrawal of electricity from  
 441 a battery (storage of electrical energy) or, continuous withdrawal of thermal energy from the  
 442 heat storage of thermal energy [100]. However, thermal energy storage will result in the  
 443 higher storage volume, which is strongly dependent on the specific energy capacity of the  
 444 storage material. Moreover, due to the low thermoelectric conversion efficiency, the amount  
 445 of thermal energy to be stored is relatively higher than the storage of electrical energy. The  
 446 utilisation of the heat available from energy storage for electric power generation with TEG  
 447 had been demonstrated by the research carried out by Jaworski et al. [101]. Furthermore, a  
 448 proof of concept on the using the low-grade heat available from solar pond had also been  
 449 performed by Singh et al. [102] and Tundee et al. [103]. With a maximum possible

450 temperature difference of  $100^{\circ}\text{C}$ , the system open channel power generation unit constructed  
 451 by Singh et al. (in Fig. 7) was generating 0.6 W per TEG from his 16-TECs system at low  
 452 flow rate. Furthermore, a transient model by coupling the TEGs with a solar pond for electric  
 453 power generation had revealed that with a TEG's  $ZT$  value of 1.0, the solar pond at the  
 454 climate with high annual solar insolation has the potential of generating electric energy of 9.7  
 455 kWh/year- $\text{m}^2$  [104].



456  
 457 **Fig. 7.** The open channel power generation unit by Singh et al. [102].

458 **2.8 Summary**

459 At low temperature heat source  $<150^{\circ}\text{C}$ , BiTe-based material remains the most  
 460 common material for thermoelectric application, despite there will be potential of evaporation  
 461 of tellurium at high temperature operation. The research on the application of TEG in  
 462 producing electric power in the range  $>1\text{W}$  was mainly focused on two heat sources, which  
 463 are waste heat recovery as well as the conversion from solar energy. With the benefit of no  
 464 moving part and having long term reliability in its operation, the TEG remains a favourable  
 465 mean for energy conversion although low  $ZT$  value appear to the biggest hurdle for the  
 466 widespread of TEG application and in turn, possess low economic feasibility. As pointed out  
 467 by Muto [105], in order for TEG to compete with Rankine cycle for existing solar thermal  
 468 plant, a TEG material with  $ZT = 15.5$  is needed, due to the fact that Rankine cycle has a much  
 469 higher fraction of Carnot of  $\approx 65\%$ . Thus, it is reasonable to not anticipate thermoelectric  
 470 technology emerge as a dominant position in large scale electricity generation. The best that a  
 471 thermoelectric system could achieve is to serve as an auxiliary power generation system.

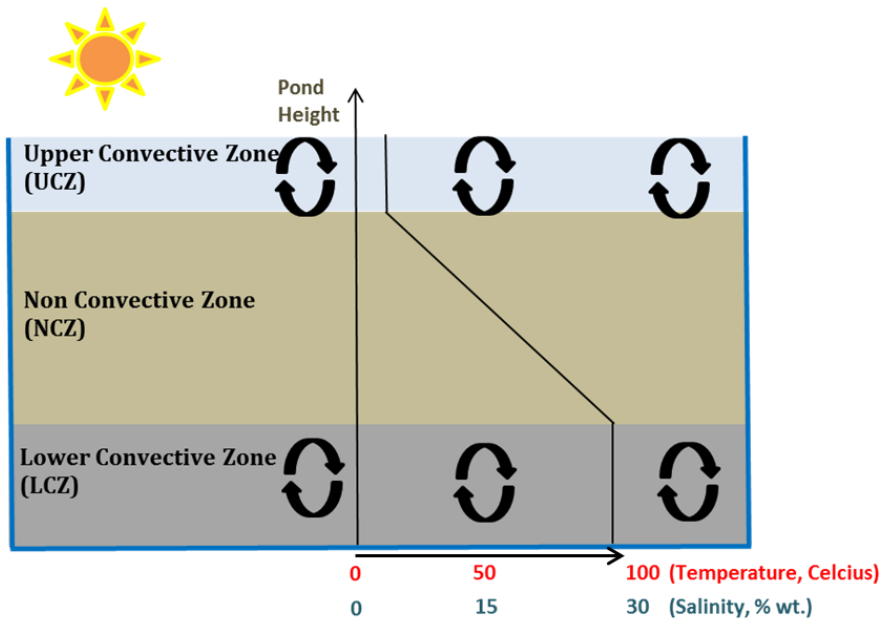
472 From the survey conducted, the research on the application of thermoelectric system is yet to  
473 address the issue in the intermittency of the power supply if the thermoelectric technology  
474 kicks in since either of the waste heat supply or solar (radiation) energy supply is usually  
475 intermittent, unless additional heat storage or battery storage is available.

### 476 **3. The Solar Pond**

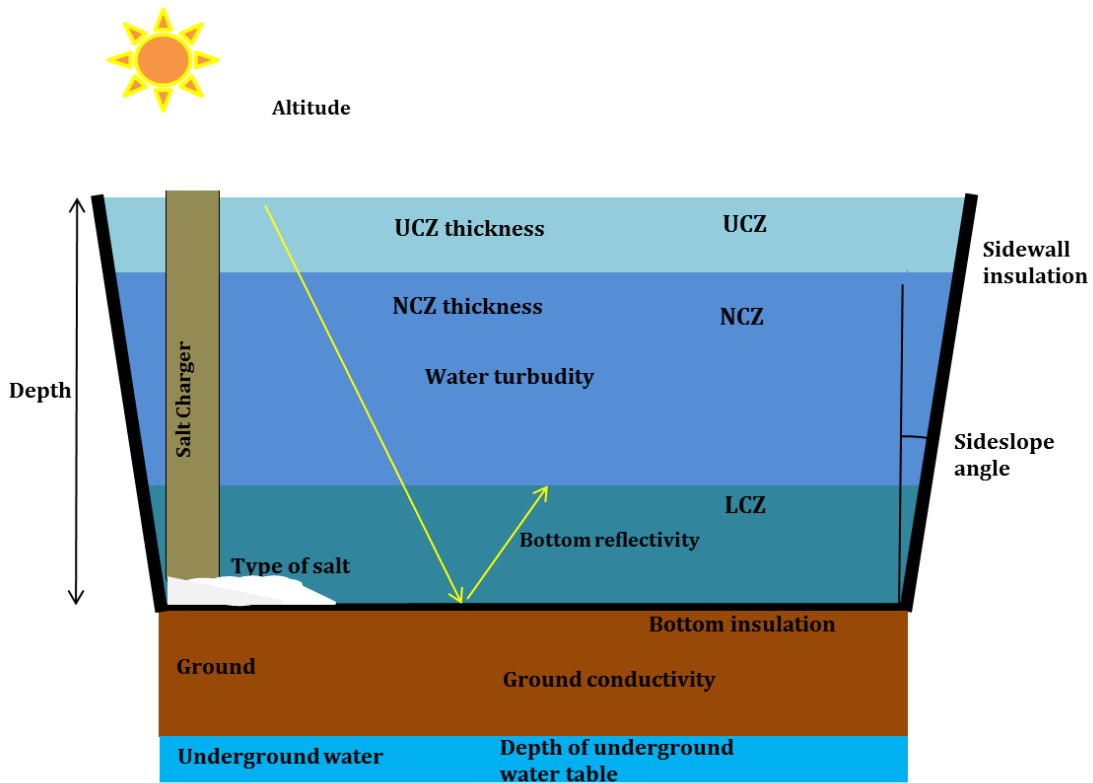
477 As reported by Anderson [106], and followed by the series of observation around the  
478 world from 1960's to 1970's [107-111], the discovery of solar pond phenomena had excited  
479 the scientific community and since then, the solar pond became a famous method to extract  
480 low-grade heat for decades, at an operating temperature of 40°C to up to boiling point  
481  $\approx 100^\circ\text{C}$ . The descriptions for the different types of solar pond had been summarised by El-  
482 Sebaei et al. [112]. Historically, different types of solar ponds had been designed to enhance  
483 its heat storage capability such as salinity gradient solar pond (SGSP), partitioned solar pond,  
484 viscosity stabilised solar pond, membrane stratified solar pond, shallow solar pond [113] as  
485 well as saturated solar pond.

#### 486 **3.1 Salinity Gradient Solar Pond (SGSP)**

487 Later in 1980's, researchers around the world had started to research in detail on the  
488 characteristic of salinity gradient solar pond (Fig. 8) and massive work had been conducted  
489 on the parametric study on the performance of a solar pond as well as the stability criterion  
490 on maintaining salinity gradient from thermophoresis point of view [114]. At the same time,  
491 researchers had devoted themselves to understand the hydrodynamics of the solar pond.  
492 Detail discourse on the hydrodynamics of solar pond was discussed by Zangrando [115],  
493 especially on the maintenance and stability of the salinity gradient. Research had shown that  
494 the coexistent of distinct molecular diffusivity of salt and water as well as the buoyancy force  
495 contribute to the transport and mixing of these binary substances [116, 117]. With some  
496 proper controls [118], such as controlling the salinity at the upper zone, or a routine heat  
497 extraction from UCZ, high temperature operation of the SGSP (Fig. 8) can be maintained.  
498 Some salient parameters that affect the performance of solar ponds as depicted in Fig. 9 from  
499 the research conducted are summarised in Table 2.



500  
501 **Fig.8.** Salinity gradient solar pond.



502  
503 **Fig.9.** Parameters that influenced the performance of the solar pond.

504 **Table 2**  
505 Parametric study on the performance of the solar pond.

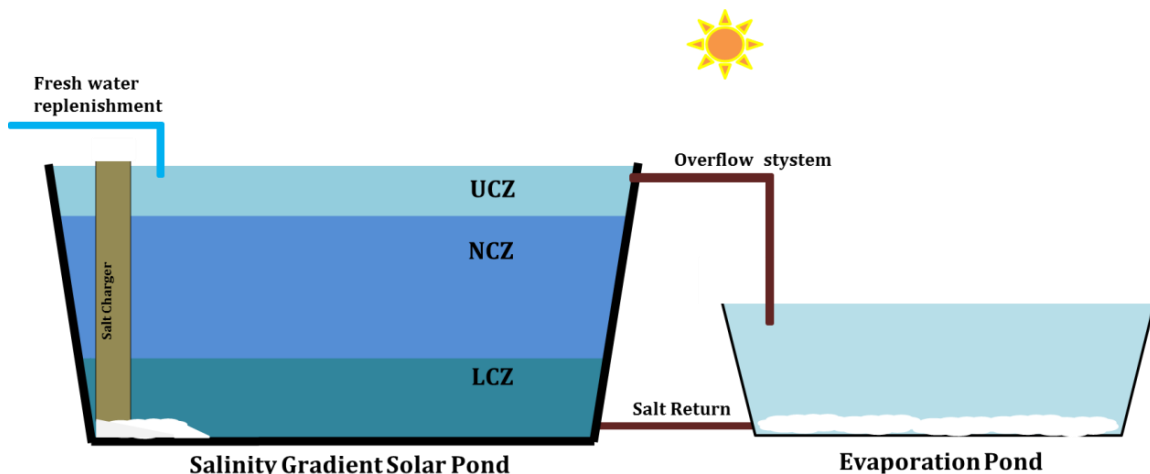
Parameters	Findings
Shape of the solar pond	Circular solar pond performs better than rectangular solar pond [119].
Side slope of the solar pond	The slope of the solar pond will affect the steady state salinity profile [120]. The losses through side wall increase with the decrease

	in side-slope angle. Hence, with increasing the side-slope angle improves the temperature at LCZ [119].
Size of solar pond	The maximum temperature at the LCZ increases asymptotically up to 10000 m <sup>2</sup> [119]. Insignificant changes on thermal loading per unit area pond size when the pond becomes larger [121].
Ground conductivity	Lower ground conductivity will significantly increase the temperature at LCZ [119]. Ground thermal insulation should be provided for the case of high underground water level [122]. Site with deep underground water flow should be favourable to reduce further heat loss [123]. However, there exist a depth of water table whereby further depression of water table will not further improve the maximum temperature at LCZ [124].
Thickness of NCZ	Increasing the thickness of NCZ will reduce the sun radiation penetration into NCZ. Decreasing the thickness of NCZ will enhance the conduction heat loss to the surface of solar pond [123].
Thickness of the UCZ	Increasing the thickness of UCZ will dissipates the solar radiation into the solar pond. Reducing the UCZ thickness will increase the solar pond performance [122]. However, this will expose to higher risk of perturbation by the rain [119].
Solar pond bottom reflectivity	High bottom reflectivity is more detrimental to the functionality of a shallow SGSP (about 1-2 m) than a deeper SGSP [125]. Increasing the reflectivity will drastically reduce the temperature at LCZ [123]. The existence of undissolved salt will increase the reflectivity of the pond while the accumulation of the dirt has insignificant changes on the performance of the solar pond [126].
Insulation	Side wall insulation is important for the small scale solar pond (<100 m <sup>2</sup> ). For larger solar pond (>100 m <sup>2</sup> ), bottom insulation is crucial [121].
Water turbidity	The magnitude of extinction coefficient (the availability of fraction of incident radiation at the different level of SGSP) is affected by turbidity of water [127]. High turbidity level retards the solar pond ability to store energy [128].
Type of salt	Sodium carbonate (Na <sub>2</sub> CO <sub>3</sub> ) [129] and seawater (bittern) [130] are both suitable to be used as the salt in the solar pond for heat storage.
Insulation	With sidewall insulation, the rise in the effective temperature of SGSP promotes the movement of solute molecule. Hence, the thickness of LCZ will increase and at the same time, the thickness of NCZ reduces.
Altitude	Owing to seasonal variation, a solar pond located at higher altitude will require deeper depth [131].



506 **3.2 Closed Cycle Salt Gradient Solar Pond (CCSGSP)**

507 Due to the evaporation at the surface of the solar pond, which cause a loss of water  
508 and increase in the salinity at the UCZ, fresh water supply is needed in order to maintain the  
509 salinity and water level at the upper surface. In Australia, Alagao et al. [132] proposed the  
510 design and construction of a closed cycle salt gradient solar pond, as shown in Fig. 10. Later,  
511 a similar study was conducted on the design methodology and the maintenance of closed-  
512 cycle SGSP based on the climate at Libya, a subtropical semi-arid climate by considering  
513 both summer and winter [133, 134]. Inasmuch as the evaporation loss, the salinity at the  
514 UCZ increases and hence the portion of the water at the UCZ need to be removed and  
515 replaced by fresh water. The extracted water from the UCZ is sent to an external evaporation  
516 pond, to extract the salt in the mixture before being recycled to the salt charger. Alternatively,  
517 since the actual evaporation rate is abstruse in most of the cases, as emphasised by Alagao et  
518 al. [132], the estimation of the evaporation should be done in a careful manner.



519 **Fig.10.** Closed cycle salt gradient solar pond.  
520

521 **3.3 Solar Pond in Different Climatic Condition**

522 As solar pond at cold climates is more susceptible to freezing in winter, and the  
523 impact of shading due to the lower elevation angle of the sun, the feasibility study of the use  
524 of solar pond for the northern cold climate in Scandinavia was incepted by Lund and Routti  
525 [135]. The research shown, in northern cold climate, large scale solar pond for the use of  
526 district heating surpass the use of small solar pond for the heating of the single house in terms  
527 of both economic and efficiency consideration.

528 The study on the performance of the solar pond in the tropics had been conducted at  
529 Bangalore, India [119]. Throughout the five years of the experimental period, the temperature

530 in the LCZ (storage zone) for the 240 m<sup>2</sup> solar pond fluctuated within 50°C- 75°C, with the  
531 ability to extract up to 1200 MJ of heat with average heat extraction efficiency of 13%. As  
532 one of the main characteristic with tropical climates is its high rainfall during the monsoon  
533 period, along with the study, the maximum penetration of rainfall during monsoon period is  
534 about 50 cm from the surface of the solar pond. A comparative study had been conducted by  
535 Hawlader [131] in order to compare the performance of the solar pond located at different  
536 altitude. In the study, solar pond located in Singapore (tropical rainforest climate) was  
537 compared the solar pond located at Kew, UK (temperate oceanic climate). Despite the fact  
538 that the solar pond located at Kew achieved lower temperature under the comparative study,  
539 yet, the heat from the solar pond will still able to supply adequate thermal energy for space  
540 heating.

541 Previous research had been conducted for the solar pond transient behaviour located  
542 in southern part of Tunisia, which possesses a steppe climate [136]. SGSP has been  
543 successfully operated under such climate condition, with the maximum heat extraction  
544 capacity of 80W/m<sup>2</sup> and the potential of operating with a desalination plant. Meanwhile,  
545 under a Mediterranean climate, Haj Khalil et al. [137] explored the potential of electric power  
546 generation in that region. Potentially, 5 MW of electric power can be generated with a solar  
547 pond area of 1.5 km<sup>2</sup>. For a solar pond in the Mediterranean climate, highest exergy  
548 efficiency and the energy efficiency of the solar pond is reported to be 28% and 27%,  
549 respectively [138]. A recently built 50 m<sup>2</sup> ×3 m (depth) small solar pond at Catalonia (north-  
550 east of Spain) showed, maximum temperature of 55°C can be reached in summer [139] and it  
551 was predicted that maximum temperature of 75°C can be achieved for the solar pond built at  
552 south-east region of Spain [140].

### 553 **3.4 Numerical Study on Solar Pond**

554 The advance of computational science in the recent decades avail the development for  
555 the simulation of the salinity gradient solar pond and different modelling approaches emerge  
556 since then, as shown in Table 3. For the SGSP, unless the environmental parameter (such as  
557 climatic condition) does not vary throughout the year, else, the solar pond should be modelled  
558 under transient state condition [141]. Besides utilising the numerical model to study the  
559 transient behaviour of SGSP, in the earlier year, Alagao [142] had developed a one-  
560 dimensional numerical model for the closed-cycle SGSP, as a tool to estimate the minimum  
561 area of evaporation pond needed for a specific solar pond available. In the study conducted

562 by Kurt et al. [143], instead of using numerical approach, a machine learning method had  
 563 been used to predict the density and temperature in the solar pond. By using artificial neural  
 564 network method, this study opens an alternative technique to evaluate the performance of  
 565 SGSP; in spite of the input for the training of the network will be case specific. A series of a  
 566 comprehensive guide on the simulation procedure and the parametric study on the solar pond  
 567 is given by Subhakar and Murthy [144, 145]. The use of finite element method such as  
 568 Crank-Nicholsen method [146] revealed that the use of daily variation of ambient data as the  
 569 input for the simulation performs as best as the hourly variation data input. In turn, this  
 570 resulted in a reduction in computational cost.

571 **Table 3**  
 572 Numerical studies on solar pond.

<b>Numerical models</b>	<b>Key findings</b>
1-dimensional transient model	For a SGSP, the replenishment of salt at LCZ and the flushing of fresh water at UCZ is a must in order to guarantee the sustainability of the solar pond for the long run. The thermodiffusion (Soret effect) will destabilise the salinity gradient layer, especially under the condition of high temperature and salinity gradient [147, 148].
1- dimensional transient model	By using finite element approach, the temperature and density profile of SGSP can be predicted in good agreement. The minimum density difference between UCZ and LCZ in order to establish salinity gradient for NaCl-based SGSP is 216 kg/m <sup>3</sup> .
1- dimensional transient model [150]	The numerical study on heat extraction at both NCZ and LCZ was conducted. It was found that extracting the heat from NCZ only will reduce the density stability of the SGSP [149].
1- dimensional transient model	Numerical study on heat extraction at both NCZ and LCZ was carried out and a simple method to estimate the SGSP performance using a new definition for instantaneous efficiency for SGSP [151].
2-dimensional transient double diffusive convective model (Suárez et al., 2010)	The exclusion of the double-diffusive convection will overestimate the temperature at the LCZ [152].
2- dimensional transient model (Mansour et al., 2006)	Hot seasons will favour the solar heating effect than cold season. Extracting heat at the LCZ will aid to stabilise the temperature profile at LCZ. Besides, SGSP with low turbidity will tend to develop instability in the temperature profile of SGSP [153].
2-dimensional computational fluid dynamics (CFD) model	The study of heat extraction scheme for solar pond is studied via CFD simulations is possible, provided realistic boundary conditions are given [154]. The impact of internal Rayleigh number and aspect ratio of the solar pond onto the temperature, velocity and

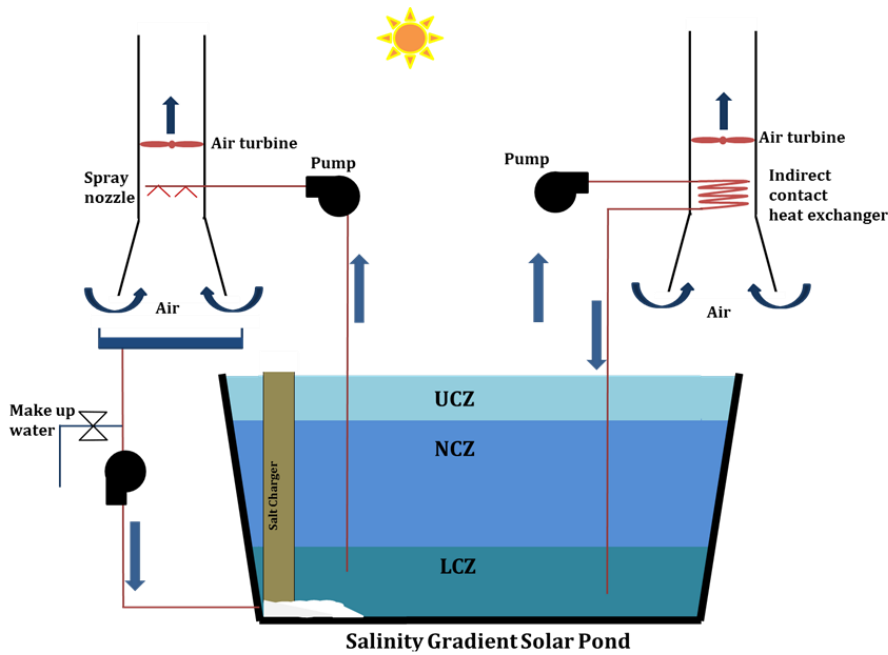
### 573 3.5 *Solar Pond Research in Recent Decade*

574 The heat stored at the LCZ is extracted via two methods. The first method of heat  
575 extraction is via circulating the working fluid in an in-pond heat exchanger located at the  
576 bottom of the solar pond, for example, the solar pond at Pyramid Hill, Australia [156].  
577 Alternatively, by using external heat exchanger located outside the solar pond, saturated hot  
578 brine in the LCZ is pumped out from the pond and exchanging heat with cold inlet water at  
579 the external heat exchanger before returning to LCZ. This method had been used to extract  
580 the heat at the 3000 m<sup>2</sup> solar pond at El Paso [157]. By using these conventional heat  
581 extraction methods, the thermal efficiency (defined as the ratio of total heat extraction to total  
582 solar radiation incident on the pond surface) was around 15-18% [158]. Andrews and  
583 Akbarzadeh [156] in their studies, instead of extracting heat through conventional methods,  
584 additional heat was extracted at NCZ by extending the heat exchanger looping to the side  
585 wall of NCZ. Using this method, the thermal efficiency of the solar pond can be boosted up  
586 to 55%. Furthermore, concentrating the surface discharge of saline in an evaporation pond  
587 followed by its re-circulation to the base of the pond via a salt charger had also proven to be a  
588 method that could enhance the both thermal and mechanical efficiency of the SP [159].

589 The aforementioned research were mainly focusing on improving the system  
590 efficiency. In order to reduce the energy cost (defined by the price of producing unit electric  
591 energy), either the efficiency of the system has to be improved or the cost (both fixed and  
592 variable cost) of the system has to be reduced in order to achieve this goal. Straatman and van  
593 Sack [160] conducted a cost optimisation study for a hybrid solar thermal electricity  
594 generation system consists of ocean thermal energy conversion and offshore solar pond  
595 (OTEC-OSP). In the design, the low cost floating solar pond serves as a medium to enhance  
596 the temperature input for the OTEC plant for power generation. With a low operation and  
597 maintenance cost couple with the capability to produce electricity continuously, the OTEC-  
598 OSP system design was found to have the lowest energy cost of 0.04 €/kWh for all solar  
599 thermal electricity system.

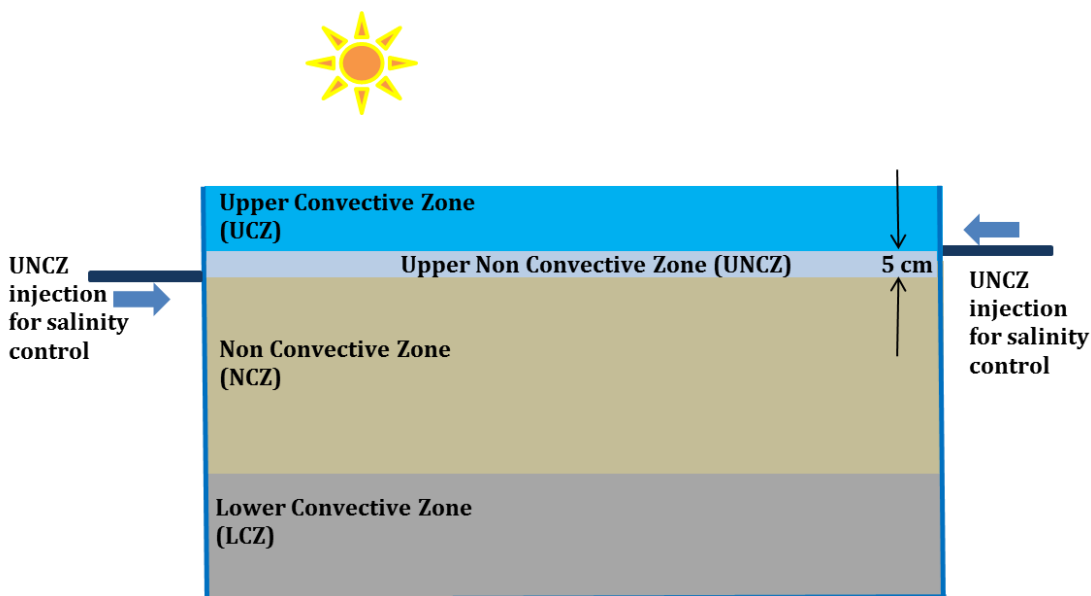
600 Despite the disadvantage in low thermal to mechanical conversion efficiency,  
601 Akbarzadeh et al. [161] proposed a system that combines solar chimney with SGSP (Fig. 11).  
602 The heat from the LCZ of the solar pond was transferred via a heat exchanger and being

603 released in the chimney. Due to the density difference exists between ambient air and the  
 604 heated air inside the chimney, air movement was induced and powered the air turbine.



605  
 606 **Fig.11.** Combined solar chimney with SGSP [161].

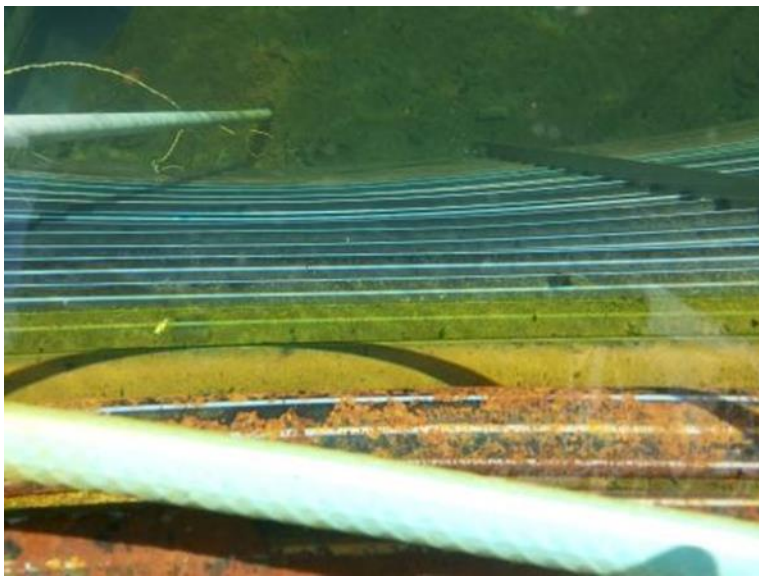
607 For increasing the temperature at the storage zone (LCZ), Husain et al. [162] in their  
 608 study suggested the introduction of a 5 cm intermediate zone between UCZ and LCZ, which  
 609 is illustrated in Fig. 12. However, for such system, continuous maintenance work is needed in  
 610 controlling the salinity for this additional layer in order to maintain the overall salinity  
 611 stability of the SGSP.



612  
 613 **Fig. 12.** The introduction of a 5 cm intermediate zone between UCZ and LCZ.

614 The evaporation at the top surface of the solar pond and the growth of algae and  
 615 microbes are the common problems faced by the solar pond. Evaporation at the top surface

616 causes heat loss from solar pond via entrainment, while the growth of algae at NCZ blocks  
617 the penetration of sunlight to LCZ. Mimic to the concept of a shallow solar pond, a two layer  
618 nanofluid solar pond that is able to eliminate the deficiencies of solar pond operates with  
619 brine as mentioned before has been researched [163]. The nanofluid solar pond consisted of a  
620 transparent mineral oil layer at the top and a water based nanofluid at the bottom. By making  
621 use of the nanofluid in the solar pond, it was found that nanofluid pond outperformed in  
622 terms of energy stored per unit area with the capacity storing the heat of 2.16 times than a  
623 brine pond. Besides, Malik et al. [164] found that the use of diluted hydrochloric acid (HCl)  
624 will able to reduce the pH and turbidity at NCZ. However, this method should be done  
625 judiciously, since acid injection near to the LCZ will lead to crystallisation due to the reaction  
626 of the acid with high salinity solution exists in the LCZ. Nevertheless, as pointed out earlier,  
627 evaporation at the top surface of the solar pond is undesired since it causes evaporative heat  
628 loss from the solar pond. By using some floating elements (such as floating disc and floating  
629 hemisphere) [165], the evaporative heat loss from the solar pond can be reduced. Thus, more  
630 heat can be withdrawn from the NCZ and LCZ of the SGSP. The growth of algae and  
631 microbes in the solar pond has an adverse effect in increasing the turbidity of solar pond and  
632 retard the transmissibility of sunlight to LCZ and its growth along the heat exchanger pipeline  
633 is obvious (for example, RMIT solar pond in Fig. 13). The experiment has been conducted on  
634 the use of low-cost chemical, such as alum ( $KAl(SO_4)_2 \cdot 12H_2O$ ) was able to mitigate the  
635 problem of high turbidity for turbidity control [166].



636 **Fig.13.** Algae problem in the solar pond.  
637

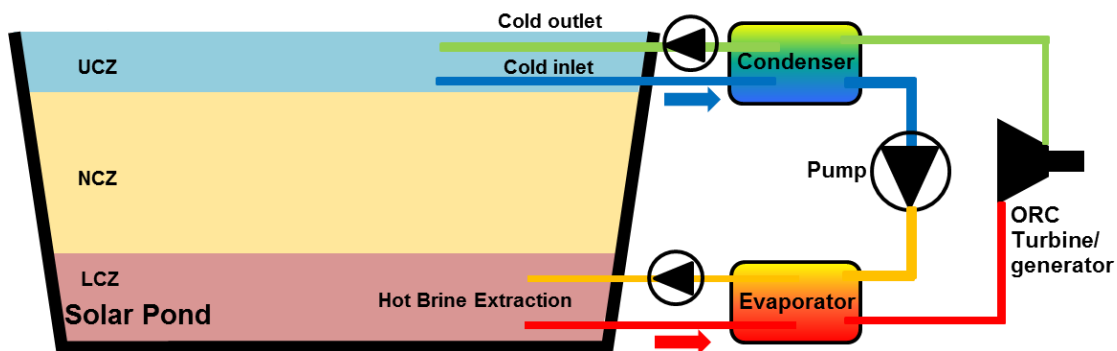
638 In addition to water desalination process using desalination unit with solar pond [167,  
639 168], the solar pond can be combined with a solar still. Utilising the evaporation process to

640 produce distilled water from saline water, studies had shown, with some modifications by  
 641 incorporating a mini solar pond into a solar still as a medium to preheat the saline water will  
 642 able to augment and double the production of distilled water [169, 170]. A similar concept  
 643 had been researched by El-Sebaili et al. [171]. Through the study an active single basin solar  
 644 still with a shallow solar pond will increase the daily production of distilled water up to 200%.

645 Both solar collector and solar pond are two distinct systems that utilising solar energy  
 646 as the heat source for renewable energy system. For the renewable energy system designer, a  
 647 dilemma exists, on choosing the most suitable system in their design. For the underfloor  
 648 heating system, solar collector system avails in terms of economic consideration compare to  
 649 solar pond system attributed to lower electrical energy consumption in catering the underfloor  
 650 heating [172]. From the research conducted on solar ponds over decades, it was found that  
 651 most of the studies on the solar pond were performed under laboratory scale or by conducting  
 652 theoretical modelling of the system. The research studies on a large scale solar pond in long  
 653 run are relatively limited. The underlying reason, besides the high setup cost of the large  
 654 scale solar pond, large-scale solar pond is vulnerable to the change in climatic and  
 655 environment condition if it is not properly maintained

### 656 3.6 Solar Pond for Power Generation

657 Finally, for electric power generation with solar ponds, ORC has been a successful  
 658 method to generate electric power from the solar pond. The system illustrated in Fig. 14  
 659 represents a solar pond-ORC power plant with a typical efficiency of solar to electrical  
 660 efficiency of 0.8% to 2%. A review on low-grade heat conversion using ORC is already  
 661 available from the literature presented by Tchanche et al. [173] which included solar pond-  
 662 ORC system. The overall performance for the solar pond-ORC power plants reported isis  
 663 summarised in Table 4.



664 Fig. 14. Electric power generation from the solar pond using ORC.  
 665

666 **Table 4**  
 667 Power generation from the solar pond using ORC [173].

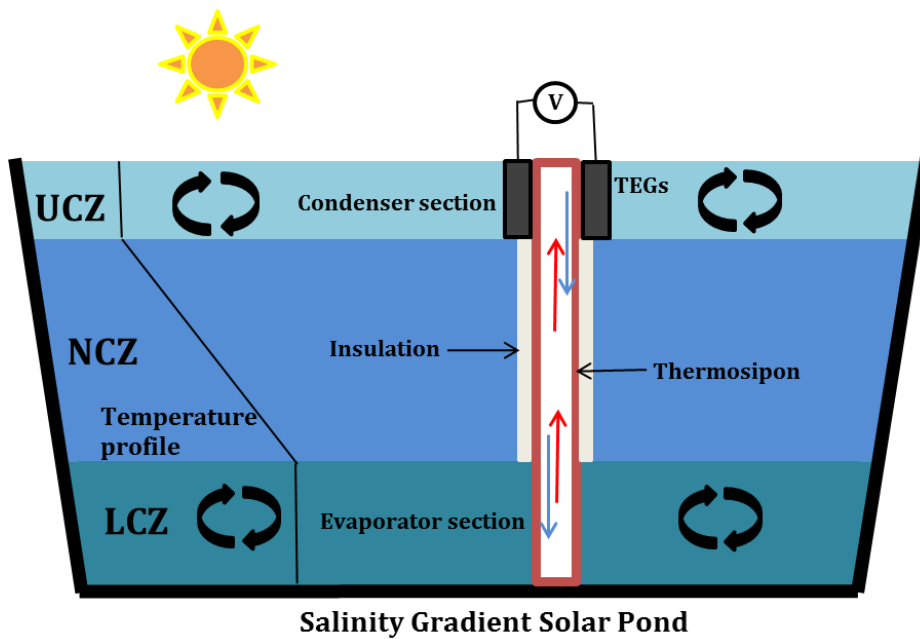
Location/Size	Capacity
Ein Bogenk (Israel), 6250m <sup>2</sup>	150kW
Beith Ha'Arava (Israel), 25000m <sup>2</sup>	5000MW
Alice Spring (Australia) 1600m <sup>2</sup>	15kW
El Paso (USA), 3350m <sup>2</sup>	70kW (electric); 330kW (thermal)

668

669 For small-scale electric power generation using the solar pond, a novel method of  
 670 integrating heat pipes and TEG for electric power generation in the solar pond (Fig. 15) was  
 671 first demonstrated by Singh [174] through the proof of concept. A temperature difference of  
 672 40-60 °C is readily available across UCZ and LCZ in the solar pond. Hence, by transferring  
 673 the heat from LCZ to UCZ using wickless heat pipes, electric power can be generated by  
 674 using TEG, to a temperature difference as low as 27 °C. Later, the research was continued  
 675 with a transient model to study the potential of power generation from the solar pond using  
 676 TEGs. After taking into account the effect of climatic variation, the conversion efficiency of the  
 677 the TEGs, the amount of heat extraction from the solar pond as well as the efficiency of the  
 678 heat exchanger; it was concluded that BiTe-based TEGs that operate at 20% of its Carnot  
 679 efficiency will able to produce electricity up to 10.9 kWh per m<sup>2</sup> of solar pond in a year [104].  
 680 Furthermore, two different experimental units had been tested, which were an open channel  
 681 plate type power generation unit [176] and a submersible power generation unit [177] with  
 682 TEGs. Both experiments had attempted to eliminate the use of the pump in transferring both  
 683 hot and cold fluids to the TEGs in ensuring net positive electric power generation. The idea  
 684 of eliminating the use of the pump in the solar pond-TEGs system is achievable since as  
 685 mentioned in the previous section, a proper maintenance of solar pond requires a low-flow,  
 686 constant fresh water flushing at the solar pond's surface. The water used for this process is  
 687 usually supplied by main water services and this is applicable to an industrial size solar pond.  
 688 By incorporating the piping of power generation unit into solar pond's maintenance services,  
 689 a pumpless power generation system is possible while generating electric power of 40 W.

690





691  
692 **Fig. 15.** Integration of thermosiphon and TEG for electric power generation.

693 **3.7 Summary**

694 The solar pond has been a reliable supply for the low grade heat source. To date, the  
695 macro scale parametric study on the performance of solar pond is considered established.  
696 However, the fundamental physics on the behaviour of the solar pond continue to be a subject  
697 that captivates researchers, supported by the advancement of computational science. For  
698 electric power generation, organic Rankine cycle has been a successful method of for  
699 generating electric power. For thermal-electric conversion, the use of solar pond as the heat  
700 source requires a large area due to low conversion efficiency of the system (as a result of the  
701 multiplication of solar pond efficiency and efficiency of the heat engine) and large area of  
702 solar pond requires a careful upkeep such as controlling the growth of algae and density  
703 gradient maintenance.

704 **4. Concluding Remarks**

705 This review has introduced the solar pond, particularly on the design parameters study  
706 since the inception of the solar pond as a way to provide the low-grade heat source and  
707 numerical approach that can be adopted to characterise the solar pond. Owing to its reliable  
708 supply of heat, it has been an ancillary resource in reducing heating demand in industrial  
709 scale. Its potential in generating electricity in large scale has been demonstrated through  
710 successful projects in the past. Meanwhile, as discussed in the beginning of this review, the  
711 ability for TEG to generate electric from the available heat opens a chance for electrical

712 power generation from the solar pond, besides using the conventional method with organic  
713 Rankine cycle.

714         Functioning as both collector and storage of solar energy, the operation of the solar  
715 ponds has a setback which is the efficiency limit and the amount of heat that can be  
716 withdrawn without risking its normal operation. In order to increase the heat extraction, the  
717 solar pond has to pursue the expansion in size (either with or without modular approach) or  
718 extent the heat extraction zone to non-convection zone, while the latter has need of a careful  
719 design to avoid disturbing the stability criteria of the solar pond. At the same time, the  
720 combination of solar pond-TEGs system will possess a limit of the amount of electric power  
721 for a given surface area of the solar pond, due to the combined limitation of solar pond's  
722 efficiency caused by the attenuation of solar radiation in water and the current  $ZT$  limit of  
723 the TEG. However, there exists a silver lining as a result of the combination of both systems,  
724 which is the elimination of the electrical energy storage system and open up another option  
725 for electric power generation utilising solar energy in small scale. By using the same concept,  
726 the TEG system could be potentially coupled with other storage-based heat source such as  
727 phase change material. In the other words, the electric power generation could be in 'on-  
728 demand' basis. For the heat to electric conversion using TEG, the heat extraction from the  
729 solar pond through heat exchanger in solar pond is necessary, which share the common  
730 ground with the existing solar pond functionality as an industrial scale provider for low-grade  
731 heat. This means, there will be no difference for the heat extraction technique and hence, the  
732 solar pond with electric power generation through TEG will able to work interchangeably  
733 between providing heat and electric power.

#### 734 **Acknowledgement**

735 The authors would like to thank RMIT University for supporting this work through the  
736 Higher Degree by Research Publications Grant (HDRPG).

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