

FACILITY FORM 502

N65-24570

(ACCESSION NUMBER)

19

(PAGES)

(THRU)

(CODE)

17

(CATEGORY)

(NASA CR OR TMX OR AD NUMBER)



CAVITATION DAMAGE IN LIQUID METALS

by

A. Thiruvengadam, H. S. Preiser and S. L. Rudy

prepared for

NATIONAL AERONAUTICS AND SPACE ADMINISTRATION

CONTRACT NAS 3-4172

GPO PRICE \$ _____

OTS PRICE(S) \$ _____

28 APRIL 1965

Hard copy (HC) 1.00

Microfiche (MF) .50

HYDRONAUTICS, incorporated research in hydrodynamics

Research, consulting, and advanced engineering in the fields of NAVAL and INDUSTRIAL HYDRODYNAMICS. Offices and Laboratory in the Washington, D. C., area: Pindell School Road, Howard County, Laurel, Md.

(over)

NOTICE

This report was prepared as an account of Government sponsored work. Neither the United States, nor the National Aeronautics and Space Administration (NASA), nor any person acting on behalf of NASA:

- (a) Makes any warranty or representation, expressed or implied, with respect to the accuracy, completeness, or usefulness of the information contained in this report, or that the use of any information, apparatus, method, or process disclosed in this report may not infringe privately owned rights; or
- (b) Assumes any liabilities with respect to the use of, or for damages resulting from the use of any information, apparatus, method or process disclosed in this report.

As used above, "person acting on behalf of NASA" includes any employee or contractor of NASA, or employee of such contractor, to the extent that such employee or contractor of NASA, or employee of such contractor prepares, disseminates, or provides access to, any information pursuant to his employment or contract with NASA, or his employment with such contractor.

Requests for copies of this report should be referred to:

National Aeronautics and Space Administration
Office of Scientific and Technical Information
Washington, D. C., 20546
Attention: AFSS-A

CASE FILE COPY

HYDRONAUTICS, Incorporated

NASA CR-54391

TPR 467-2

TECHNICAL PROGRESS REPORT 467-2
For the Period
1 January - 31 March 1965

CAVITATION DAMAGE IN LIQUID METALS

By

A. Thiruvengadam, H. S. Preiser and S. L. Rudy

Prepared for

National Aeronautics and Space Administration
April 28, 1965
Contract NAS3-4172

Technical Management
NASA Lewis Research Center
Cleveland, Ohio
Nuclear Power Technology Branch
James P. Couch

HYDRONAUTICS, Incorporated
Pindell School Road
Laurel, Maryland

TABLE OF CONTENTS

	Page
ABSTRACT.....	1
INTRODUCTION.....	2
RESULTS AND DISCUSSION.....	3
Effect of Testing Time.....	3
Effect of Temperature of Sodium.....	3
CONCLUSIONS.....	6
WORK TO BE ACCOMPLISHED DURING NEXT REPORTING PERIOD.....	7
REFERENCES.....	8

LIST OF FIGURES

- Figure 1 - Effect of Testing Time on Cavitation Damage Rate in 400^oF., Liquid Sodium
- Figure 2 - Effect of Temperature on the Cavitation Damage Rate of 316 Stainless Steel in Pure Liquid Sodium
- Figure 3 - Effect of Temperature on Strain Energy
- Figure 4 - Effect of Temperature on the Intensity of Cavitation Damage in Liquid Sodium
- Figure 5 - Effect of Temperature on the Relative Intensity of Cavitation Damage in Liquid Sodium

CAVITATION DAMAGE IN LIQUID METALS

Technical Progress Report
For the Period

1 January - 31 March 1965

24570

I. ABSTRACT

24570

Progress for the period 1 January 1965 to 31 March 1965 is reported herein. The significant result achieved during this period is the determination of the effect of temperature on the rate of cavitation damage of 316 stainless steel in pure liquid sodium at temperatures up to 1500°F. The intensity of cavitation damage was estimated for each temperature using the rate of damage obtained from these experiments and published strain energy values. The intensity is found to be very much less at higher temperatures. The intensity of damage at 1000°F is about a tenth of the intensity at 400°F; at 1500°F the intensity of damage is about a thousandth of that at 400°F.

Author

II. INTRODUCTION

An understanding of the mechanism of cavitation damage in high temperature liquid metals such as sodium and potassium would greatly aid the designer of equipment and systems using these liquid metals. With this motivation, a series of systematic experiments are being performed at HYDRONAUTICS, Incorporated with the help of a controlled environment test facility described in detail in References 1 and 4. This is the second technical progress report describing additional experiments performed in this facility. The most significant among these experiments deals with the effect of the temperature of the liquid sodium on the cavitation damage rate of 316 stainless steel. There was an earlier attempt to obtain similar data using eutectic NaK up to 1000°F which showed that the cavitation damage on 316 stainless steel was strongly dependent on the temperature, Reference 2. These tests were reported to be inconclusive because of the lack of control of "sound factors". However, the general trend was that the damage was much lower at higher temperatures in conformity with the observations made in common liquids such as water, Reference 3.

More recently, 100A titanium was tested in liquid sodium up to 1000°F and again the results showed reduction in damage rate at higher temperatures, Reference 4. However, these experiments also proved to be less valuable in the sense that the oxide impurity in the liquid sodium was not known. Because of the limitations of the earlier purge type dry box (atmosphere displaced by pressurized argon without benefit of vacuum pump-down), the

oxide levels were believed to be near saturation values for each of the test temperatures. These considerations, among others, led to the design of an improved facility in which sodium purity could be maintained around 30 ppm of oxygen over a test duration of 8 hours. It was decided to test 316 stainless steel in low oxide sodium among other tests planned. The results of this phase experiments are presented in this report.

III. RESULTS AND DISCUSSION

Effect of Testing Time.

It has been established that the rate of cavitation damage is time dependent, Reference 4. The initial run of experiments on 316 stainless steel, Reference 1, aimed at obtaining the relationship between the rate of weight loss and the test time in 1000°F sodium, showed that the intensity at this temperature was so low that only a few surface indentations could be observed up to 25 hours of testing. There was no observable weight loss. For this reason, the damage rate versus time relationship was obtained at 400°F sodium and the results are shown in Figure 1. The steady state was reached in approximately 5 to 6 hours.

Effect of Temperature of Sodium.

Using a 316 stainless steel specimen that had reached the steady state zone as shown in Figure 1, a series of experiments was conducted over a range of temperatures between 300°F to 1500°F at 100°F intervals in order to determine the variation of the rate of cavitation damage with the temperature of the sodium.

The duration of each test run was one hour. The damage rate was determined from one one-hour experiment for each reading. A minimum of three readings were taken at each temperature in order to check the reproducibility of the data. The precautions for obtaining high purity sodium as described in Reference 1 were maintained throughout these experiments. The results are shown in Figure 2. The rate of weight loss at 1500°F is of the order of a hundredth of a milligram per hour as compared to 16 mg/hour at 400°F.

An understanding of this experimental result involves the knowledge of how the material properties as well as the liquid properties change as the temperature varies. One of the properties of the material that is known to control the energy absorbing capacity of the material in fracture due to cavitation damage is the strain energy of the metal, Reference 4. The strain energy is given by the area under the stress-strain diagram. Unfortunately, the stress-strain data are not available for the high temperatures of interest in these experiments. However, the values of yield strength, ultimate strength and ultimate elongation are available for each temperature, and using these data, the strain energy was estimated from the following approximate relationship.

$$S_e = \frac{(Y + T)\epsilon}{2} \quad [1]$$

where

S_e is the strain energy

Y is the yield strength

T is the ultimate strength

ϵ is the ultimate elongation

The variation of strain energy with temperature for 316 stainless steel was computed from data given in Reference 5 and is shown in Figure 3.

The intensity of cavitation damage is defined as the power absorbed by the material per unit area and is given by

$$I = \frac{\Delta w S_e}{\rho A_e t} \quad [2]$$

where

I is the intensity of cavitation damage

Δw is the weight loss

t is the test duration

S_e is the strain energy of the metal

ρ is the density of the metal

A_e is the area eroded

The intensity of cavitation damage was estimated using the weight loss data shown in Figure 2 and the strain energy values shown in Figure 3 for various temperatures (see Table I). Figure 4 shows the effect of temperature of liquid sodium on the intensity of cavitation damage. In order to obtain a relative idea of the order of magnitude of the decrease in intensity at higher temperatures, the relative intensity with respect to the intensity at 400°F is plotted in Figure 5 as a function of temperature. It is interesting to note that the relative intensity of cavitation damage at 1500°F is of the order of 10^{-3} . This result is to be expected from the fact that the vapor pressure increases from an order of 10^{-7} atmosphere at 400°F to nearly one atmosphere at 1500°F, Reference 6. From the designers' point of view, this result is useful since it gives him a rough idea of how the damage rate varies with temperature, when the material and cavitation conditions remain constant.

IV. CONCLUSIONS

The following conclusions may be drawn from the data obtained thus far.

1. The relative intensity of cavitation damage at 1500°F with respect to that at 400°F is of the order of 10^{-3} .
2. The relative intensity at 1000°F relative to 400°F is of the order of 10^{-1} .

HYDRONAUTICS, Incorporated

-7-

V. WORK TO BE ACCOMPLISHED DURING NEXT REPORTING PERIOD

During the next reporting period it is planned to complete the cavitation damage experiments on TZM, T-222 Stellite 6B and CB-132M at 400, 1000 and 1500^oF and compare their cavitation damage resistance.

REFERENCES

1. Couchman, C., III, Preiser, H. S., and Thiruvengadam, A., "Cavitation Damage in Liquid Metals," NASA CR-54332, TPR-467-1, HYDRONAUTICS, Incorporated, Laurel, Maryland, March 1965.
2. "Development of Hermetically Sealed Centrifugal Pump Units for Liquid Metals," Final Report No. 43-112, Nuclear Power Section, Allis-Chalmers Manufacturing Company, Milwaukee, Wisconsin, June 30, 1953.
3. Eisenberg, Phillip, "Cavitation Damage," HYDRONAUTICS, Incorporated Technical Report 233-1, Laurel, Maryland, 1963.
4. Preiser, H. S., Thiruvengadam, A., and Couchman, C., III, "Cavitation Damage in Liquid Sodium," NASA CR-54071, TR-235-1, HYDRONAUTICS, Incorporated, Laurel, Maryland April 1964.
5. "Steels for Elevated Temperature Service," United States Steel, Pittsburgh, Pennsylvania, P. 46, 1961.
6. Jackson, C. D., Editor, Liquid Metals Handbook, Sodium-NaK Supplement, 3rd Edition, TID 5277, Government Printing Office, Washington, D. C., P. 31, July 1955.

TABLE I

Intensity of Cavitation Damage as a Function of
Temperature in Liquid Sodium and 316 Stainless Steel

$$I = W.S_e \times 2.9 \times 10^{-6} \frac{\text{Watts}}{\text{Meter}^2}; \quad W - \text{mgs/hour}; \quad S_e - \text{psi.}$$

Temp.	Weight Loss* mg/hour	Strain Energy psi x 10 ⁻³	Intensity watts/meter ²	$\frac{I_T}{I_{400}}$
300	13	29.0	1.10	0.88
400	16	27.0	1.25	1.0
500	6	25.0	0.44	.35
600	3	23.5	0.20	.16
700	6	23.0	0.40	.32
800	6	22.0	0.38	.30
900	4	21.0	0.24	.19
1000	2	20.0	0.12	.96x10 ⁻¹
1100	0.70	19.0	0.04	.32x10 ⁻¹
1200	0.25	16.5	0.012	.96x10 ⁻²
1300	0.70	13.5	0.027	.22x10 ⁻¹
1400	0.50	11.5	0.017	.14x10 ⁻¹
1500	0.01	10.0	0.003	.24x10 ⁻²
* Average of three readings.				

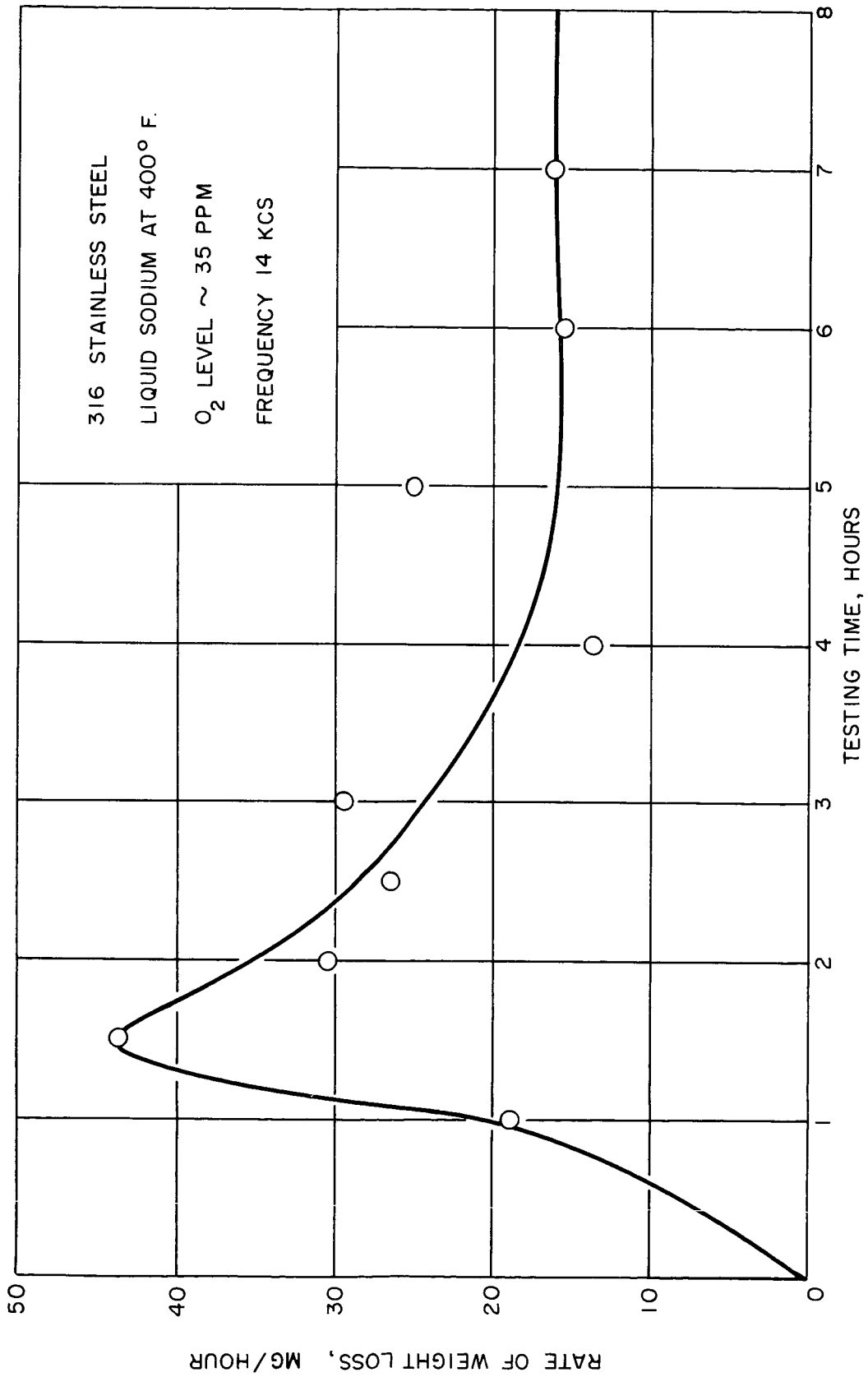


FIGURE I- EFFECT OF TESTING TIME ON CAVITATION DAMAGE RATE IN 400° F, LIQUID SODIUM

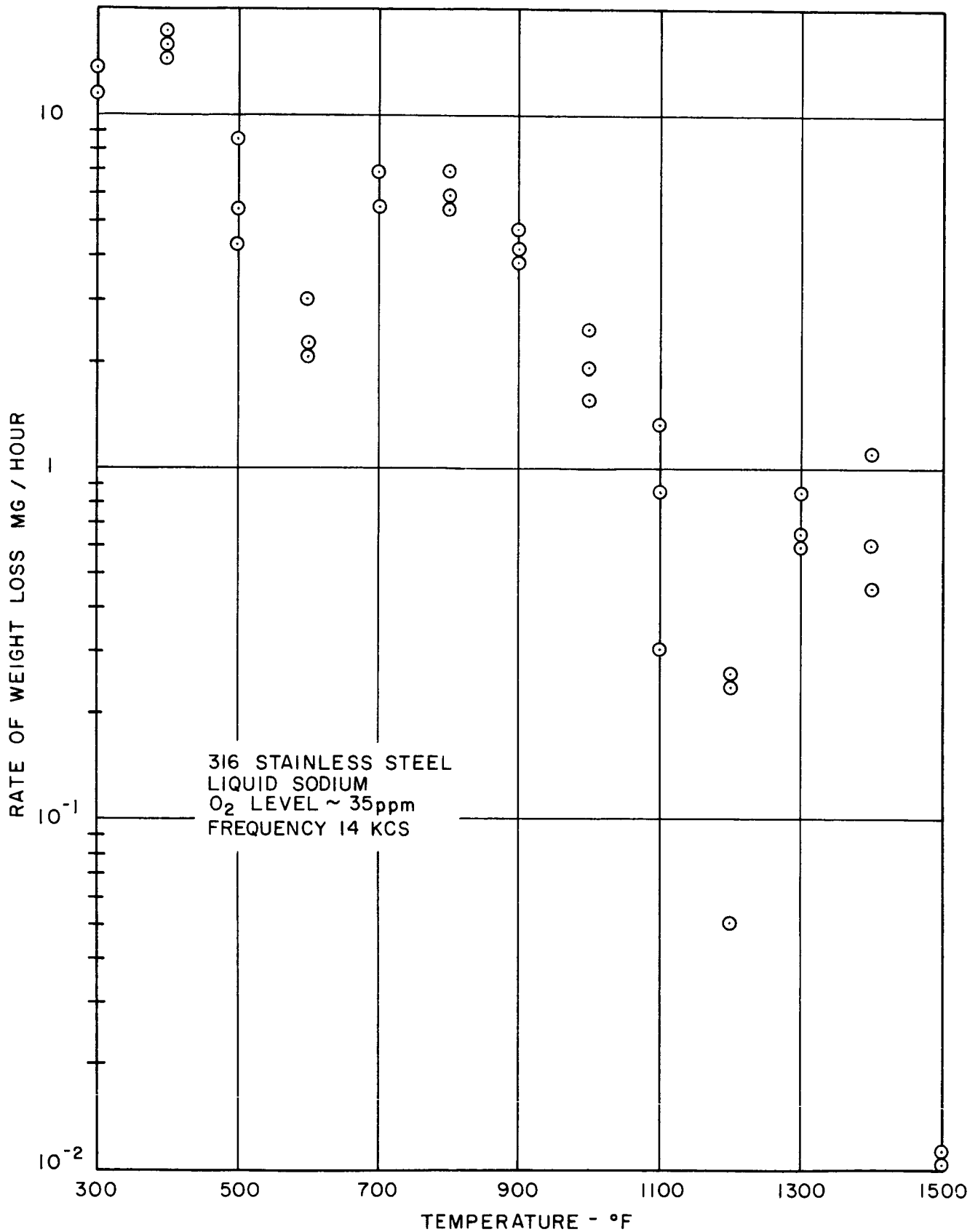


FIGURE 2 - EFFECT OF TEMPERATURE ON THE CAVITATION DAMAGE RATE OF 316 STAINLESS STEEL IN PURE LIQUID SODIUM

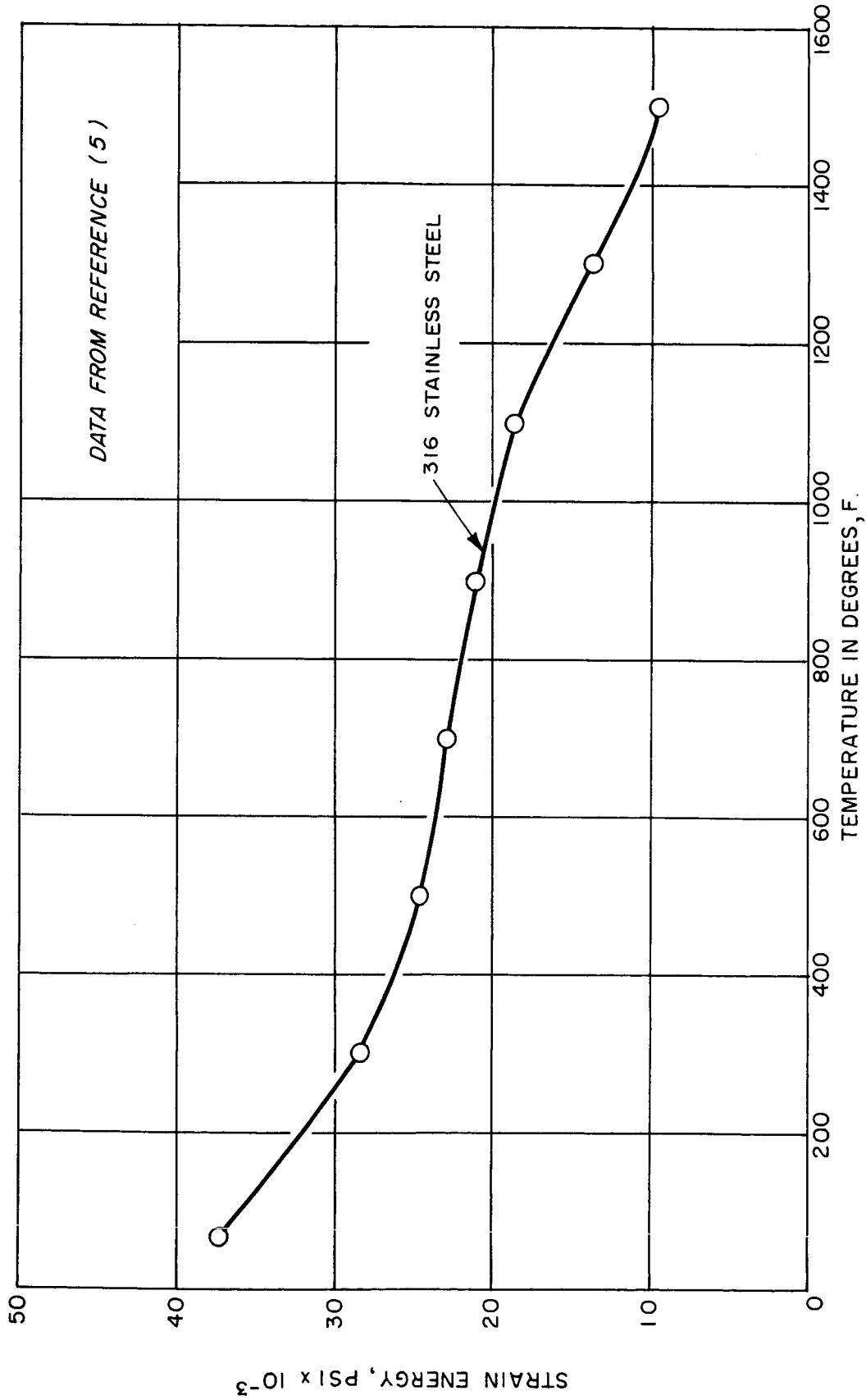


FIGURE 3- EFFECT OF TEMPERATURE ON STRAIN ENERGY

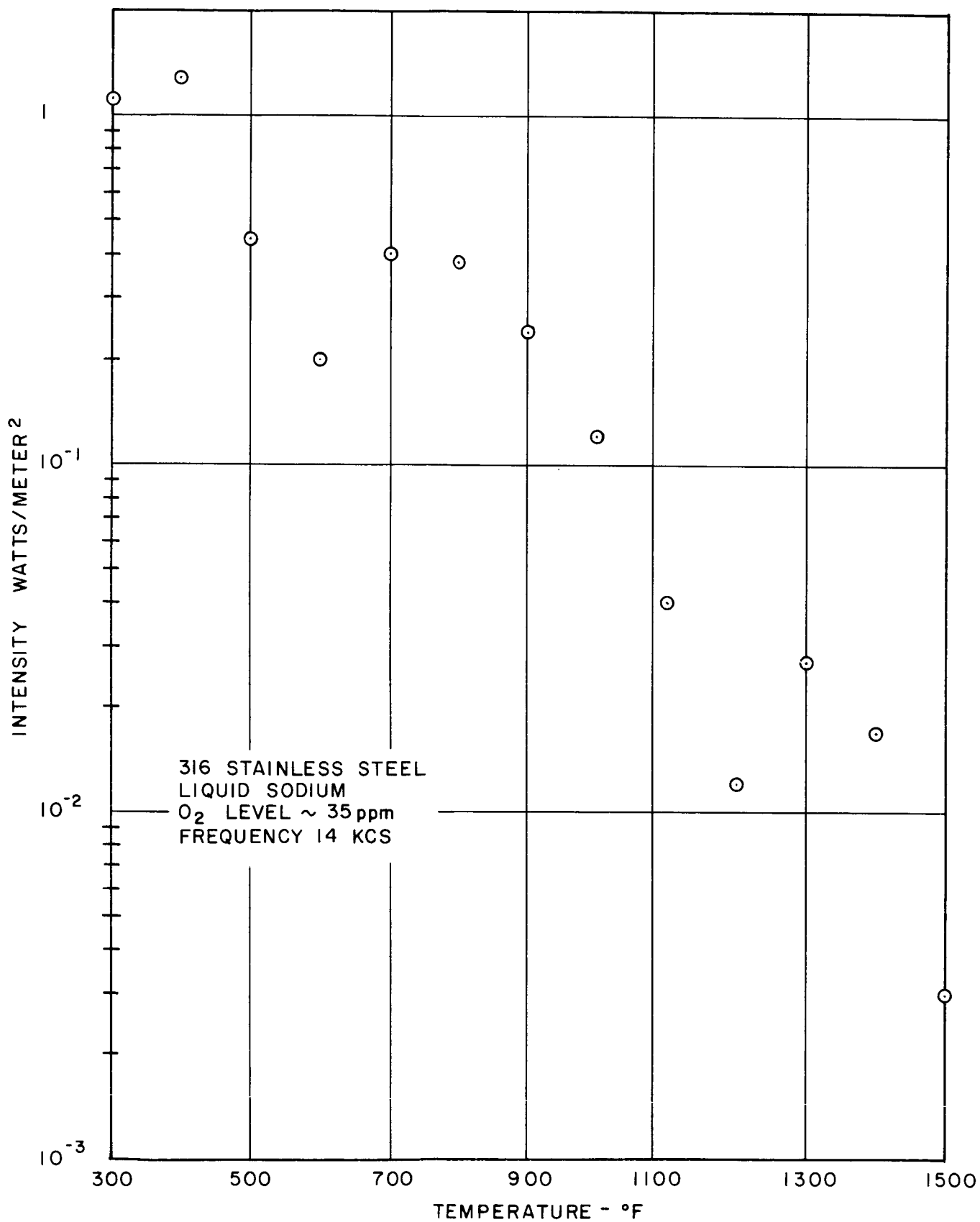


FIGURE 4 - EFFECT OF TEMPERATURE ON THE INTENSITY OF CAVITATION DAMAGE IN LIQUID SODIUM

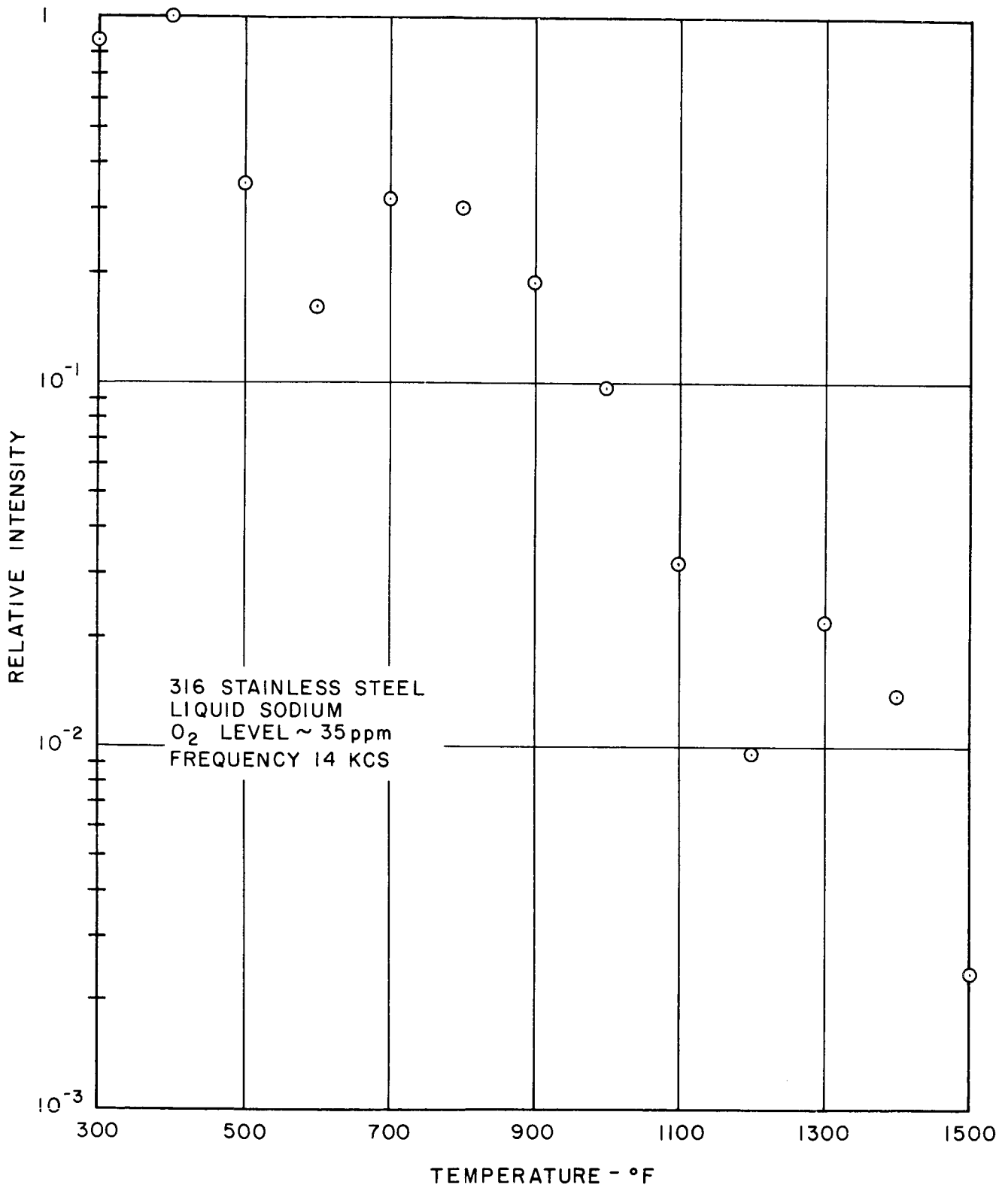


FIGURE 5 - EFFECT OF TEMPERATURE ON THE RELATIVE INTENSITY OF CAVITATION DAMAGE IN LIQUID SODIUM

HYDRONAUTICS, Incorporated

DISTRIBUTION LIST
(Contract No. NAS3-4172)

National Aeronautics and Space Administration Washington, D. C. 20546 Attention: J. J. Lynch (RNP)	1	NASA-Marshall Space Flight Center Huntsville, Alabama 35812 Attention: Library	1
U. S. Atomic Energy Commission Washington, D. C. 20545 Attention: H. D. Rothen (SNAP-50/SPUR) NASA-AEC Deputy	1	NASA-Scientific and Technical Information Facility Box 5700 Bethesda, Maryland 20014 Attn: NASA Representative	2
NASA-Ames Research Center Moffett Field, California 94035 Attention: Library	1	Jet Propulsion Laboratory 4800 Oak Grove Drive Pasadena, California 91103 Attn: Library	1
NASA-Langley Research Center Langley Station Hampton, Virginia 23365 Attention: Library	1	Argonne National Laboratory P. O. Box 299 Lemont, Illinois 60439 Attn: Library	1
NASA-Lewis Research Center 21000 Brookpark Road Cleveland, Ohio 44135 Attn: J. E. Dilley (500-309) Dr. B. Lubarsky (500-201) R. F. Mather (500-309) J. P. Couch (500-309) M. J. Hartmann (5-9) C. H. Hauser (5-9) S. G. Young (49-1) Library (3-7) Office of Reliability and Quality Assurance (500-203) Technology Utilization Office (3-16)	1 1 1 1 1 1 1 1 1 1	Brookhaven National Laboratory Upton, New York 11973 Attn: Dr. O. E. Dwyer Library U. S. Atomic Energy Commission Division of Technical Information Extension P. O. Box 62 Oak Ridge, Tennessee 37831 Air Force Materials Laboratory Research and Technology Division Air Force Systems Command Wright-Patterson AFB, Ohio 45433 Attn: K. A. Davis (MANL)	1 1 1 1 2 1

HYDRONAUTICS, Incorporated

-2-

Department of Navy Office of Naval Research Mechanics Branch Washington, D. C. 20390 Attn: S. Doroff	1	Thompson Ramo Wooldridge, Inc. Electromechanical Division 23555 Euclid Avenue Cleveland, Ohio 44117 Attn: J. N. McCarthy	1
--	---	--	---

Department of Navy U. S. Naval Applied Science Laboratory Material Sciences Division Brooklyn, New York 11201 Attn: Dr. J. Lichtman	1	United Aircraft Corporation Pratt and Whitney Aircraft Division CANEL, P. O. Box 611 Middletown, Connecticut 06458 Attn: G. M. Wood	1
--	---	--	---

Department of Navy U. S. Applied Science Laboratory Physical Sciences Division Brooklyn, New York 11201 Attn: W. L. Miller	1	University of Michigan Department of Nuclear Engineering North Campus Ann Arbor, Michigan 48103 Attn: Dr. F.G. Hammitt	1
--	---	--	---

Defense Documentation Center Cameron Station 5010 Duke Street Alexandria 4, Virginia	2	Ingersoll-Rand Corporation 942 Memorial Highway Phillipsburg, New Jersey 08865 Attn: Dr. A.J. Stepanoff	1
---	---	--	---

Allis-Chalmers Manufacturing Co. York, Pennsylvania Attn: W. J. Rheingans, Assist. Gen. Mgr.	1	Pennsylvania State University Ordnance Research Laboratory P. O. Box 30 State College, Pennsylvania Attn: Dr. G.P. Wislicenus Dr. J.W. Holl	1 1
---	---	--	--------

California Institute of Technology Department of Applied Mechanics Pasadena, California 91103 Attn: Dr. A. T. Ellis Dr. M. S. Plesset	1 1	AiResearch Manufacturing Company Sky Harbor Airport 402 South 35th Street Phoenix, Arizona Attn: Librarian Mr. John Dannan	1 1
--	--------	---	--------

General Electric Company Missile and Space Division Space Power and Propulsion Section Cincinnati, Ohio 45215 Attn: Dr. J. W. Semmel E. Schnetzer	1 1		
--	--------	--	--

HYDRONAUTICS, Incorporated

-3-

Lockheed Missiles and Space Division
Sunnyvale, California
Building 526, Dept. 65-33
Attn: John N. Cox
Staff Engineer 1

Pratt and Whitney Aircraft
Connecticut Operations-CANEL
P. O. Box 611
Middletown, Connecticut 06458
Attn: Librarian 1
Dr. Robert Strough 1

CANEL Project Office
U. S. Atomic Energy Commission
P. O. Box 1102
Middletown, Connecticut 06458
Attn: W. H. Pennington 1

Aeronautical Systems Division
Wright-Patterson Air Force Base
Ohio
Attn: Mr. George E. Thompson
APIP-1 1
Mr. George Sherman
API 1

U. S. Atomic Energy Commission
Germantown, Maryland
Attn: Col. E.L. Douthett 1

National Aeronautics and Space
Administration
Lewis Research Center
21000 Brookpark Road
Cleveland, Ohio 44135
Attn: Mr. I.I. Pinkel 1
Dr. L. Rosenblum 1