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PARAMETER DEPENDENCE OF PHASE AND LOG AMPLITUDE SCINTILLATION

by

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Abstract:

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By means of numerical computation based on the equations developed by Yeh [1962] for phase and log amplitude correlation of waves transmitted through a slab of random irregularities, the effects of variations in transmitter height, slab thickness, slab height and irregularity size are studied. A selected number of curves illustrating the effects of changes in these parameters are drawn. Using these curves as a basis, it is shown that, from experimental data, bounds may be established for some of these parameters.

Author

Introduction

Studies of wave propagation through a random medium are complicated by the presence of a large number of parameters. The basic formulation of the problem for the case of weak irregularities has been summarized in books by Chernov [1961] and Tatarski [1961]. However, difficulties arise when specific values and the dependence of these values with respect to certain parameters are desired. This is especially true if irregularities are anisotropic, as usually is the case in experimental investigations. Therefore, it is desirable to compute numerically the phase departure and the logarithmic amplitude departure. The numerical values used are those found in the ionosphere work of studying scintillation of satellite radio signals. These results are presented graphically in this report.

The specific problem of interest is the signal statistics of a spherical wave emitted by a transmitter through an intervening slab of irregularities. This problem has been studied by a number of authors [Budden, 1965; deWolf, 1965; Komissarov, 1964; Yeh, 1962; Yoneyama, 1964; Yoneyama and Mushiake, 1965]. As far as possible the notations used here will follow those in the earlier paper [Yeh, 1962] except that the distances will not be normalized. The geometry of the problem is illustrated by Fig. 1 where the distances a , b , c , and z are shown clearly. Other parameters are the three-dimensional "sizes" of irregularities l_x , l_y and l_z . The mean square values of the phase departure and the logarithmic amplitude departure are obtained by numerically integrating (30) which is then substituted into the equations (41) and (42) of Yeh [1962].

Presentation of Graphs

Figs. 2 and 3 show the effect on phase and log amplitude departure, respectively, caused by variations in slab thickness, slab height, transmitter height, and transmitter location above the slab. Each set of curves assumes $l_x = 1.0$ km and a value of l_y from .25 km to 32 km. The curves of a set are grouped by the value of b , the slab thickness. The individual curves represent departure vs. transmitter height, z , for a given transmitter location above the slab, a . The actual value of the departure is dependent upon l_z as well as $\langle \mu^2 \rangle$ and $\langle \epsilon^2 \rangle$. The frequency chosen for the graphs is 19.1 Mc/s.

It is immediately apparent that, for small values of l_y , the layer thickness b has the predominant effect on both phase and amplitude departure. The transmitter location above the slab, a , appears to be the major secondary factor. Moving from left to right, in Figure 2 we see that as l_y increases, the phase departure markedly increases until l_y is about 4 km; but in contrast, as shown in Figure 3, the amplitude departure markedly decreases as l_y increases until l_y reaches a "critical" value, in this case, approximately 8 km. For values of l_y larger than the "critical" values, changes in l_y appear to have little effect on either the phase or amplitude departure.

Fig. 2 also shows that for small b the phase departure is nearly independent of l_y and weakly dependent on a . However, for larger values of b the dependency on a becomes increasingly stronger as either b or l_y is increased, provided that l_y is less than its "critical" value. For large values of l_y , the set of curves differ little as l_y is increased. This shows that if irregularities are extremely anisotropic the phase scintillation is more dependent on other parameters than l_y .

In contrast, the amplitude departure shown in Fig. 3 decreases markedly with increasing l_y even for small values of slab thickness, b . However, we again find that the dependency of amplitude departure on a becomes increasingly stronger as both b and l_y increase, provided that l_y is less than about 8 km, which appears to be a "critical" value. In addition, a similar dependency is shown with respect to transmitter height, z . As before, when l_y is greater than the "critical" value the sets of curves look very similar.

Studying the interdependence of these parameters gives rise to the question of whether minimal "critical" values for l_y existed and their dependency on l_x . For this reason, as well as a general interest in the effect of the relationship of the ratio of l_y to l_x on phase and amplitude departure, Figs. 4 and 5 were constructed.

The curves in these figures are plots of phase and amplitude departure vs. l_y with a , b and l_x as parameters. Each set represents a given value of l_x and, as with Figs. 2 and 3, the curves in each set are grouped by the value of slab thickness b . The curves in Fig. 4 are subgrouped by the transmitter height z .

In constructing Fig. 4, it was found to be impossible to draw meaningful curves which included more than one transmitter height z . The latter's effect on the log phase departure was greatly exceeded by the effect of variations in a . Furthermore, the sets of curves for a given value of b for various values of a were very similar for a wide range of choices of z . The fixed $z = 12,800$ km was therefore selected solely on the basis of graphic presentability.

The curves in both Figs. 4 and 5 appear to verify the existence of lower "critical" values for l_y for all values of l_x . They can be estimated to be

in the neighborhood of .25 km except for very small values of b . Again, for all ratios of l_x to l_y , we find that the major factor affecting the phase and log amplitude departures, as might be expected, is the slab thickness b . Additionally, we note that the phase departure increases fairly rapidly with increases in either l_x or l_y if they are less than some "critical" value, which, for the most part, apparently lies in the neighborhood of 4 km to 8 km.

Perhaps the most striking result is the effect of irregularity size on log amplitude departure as shown by Fig. 5. The graphs for $l_x = 4$ km and $l_x = 16$ km show marked drops as l_y increases.

In an effort to exploit the contrasting effect of slab thickness b on the phase and log amplitude departure, we computed the curves in Figs. 6, 7 and 8. A transmitter height z of 1200 km was chosen to correspond to the then probable height of the satellite S-66. The integrals were changed to permit the use of a mean layer height h rather than the distance c , as shown in the insert of Fig. 6. The latest experimental evidence seems to indicate that $h = 350$ km is a reasonable figure [McClure, 1964]. Random checks of plots for other values of h verified that this height yielded representative curves. Note that the new normalization makes the phase and log amplitude departure scales independent of frequency. It is hoped that these curves might lead to realizable experimental techniques for at least gross estimation of these parameters.

Fig. 6 is a plot of phase vs. amplitude departure for various values of l_x . For all curves in this set $f = 20$ mc and $l_x = l_y$. The plot makes use of the important property

$$\langle Q^2 \rangle + \langle S^2 \rangle = Kb/f^2 \quad (1)$$

where

$$K = 4 \langle \epsilon^2 \rangle \langle \mu_0^2 \rangle \pi^{5/2} l_z / c^2$$

Thus the curves superimposed for constant b are arcs of circles with a center at the origin.

The sets of curves in Fig. 6 have at least three characteristics which may be exploited. First, since

$$\langle S^2 \rangle / \langle Q^2 \rangle \leq 1 \quad (2)$$

we obtain, when (2) is substituted into (1),

$$Kb/f^2 \geq \langle Q^2 \rangle \geq Kb/2f^2 \text{ and } \langle S^2 \rangle \leq Kb/2f^2 \quad (3)$$

The relation (3) establishes the upper and lower bounds for phase scintillation, and the upper bound for amplitude scintillation.

Second, a line through the origin having slope $\langle S^2 \rangle / \langle Q^2 \rangle$ intersects $\langle Q^2 \rangle$ at a distance Kb/f^2 from the origin. Thus if b can be determined independently or estimated, we may find the normalized phase and amplitude departures which in turn yield the values of $\langle \epsilon^2 \rangle \langle \mu_0^2 \rangle l_z$. The factors $\langle \epsilon^2 \rangle$, $\langle \mu_0^2 \rangle$, and l_z cannot be separated.

Third, for a fixed ratio of $\langle S^2 \rangle / \langle Q^2 \rangle$, l_x changes very slowly as the slab thickness b is increased. In fact, for b less than about 300 km, the curves for constant l_x are almost straight lines through the origin. It may be verified easily that the scaling factor for b is inversely proportional to the frequency (e.g. for 40 Mc/s signals, the slab thickness is $b/2$ as shown in Fig. 6). Thus, if the curve for a given l_x is independent of frequency, we must have

$$\frac{\langle Q^2 \rangle_{20 \text{ mc}}}{\langle Q^2 \rangle_{40 \text{ mc}}} = \frac{\langle S^2 \rangle_{20 \text{ mc}}}{\langle S^2 \rangle_{40 \text{ mc}}} = 2$$

where $\langle Q^2 \rangle_{40 \text{ mc}}$ and $\langle S^2 \rangle_{40 \text{ mc}}$ are read from Fig. 6 by assuming $b/2$ is the slab thickness. If the curve is not independent of frequency then

$$\langle Q^2 \rangle_{20 \text{ mc}} - 2 \langle Q^2 \rangle_{40 \text{ mc}} = \delta$$

and the stronger the frequency dependency the larger the value of δ . We illustrate this graphically as follows.

For simplicity, let $l_x = l_y$. If the phase departure at 20 mc has a value q_1 and $l_x = l_{x_1}$, as shown in Fig. 7, then $b = b_1'$ and the phase departure at 40 mc should intersect the curve $l_x = l_{x_1}$ at $b_2' = b_1'/2$, i.e. $q_2 = q_1/2$.

If for the same phase departure at 20 mc, $l_x = l_{x_2}$, then $b = b_1$ and the phase departure at 40 mc should have the value $q_3 > q_1/2$ determined by the arc $b = b_2 = b_1/2$ and the curve for $l_x = l_{x_2}$, $f = 40 \text{ mc}$.

By using separate phase and amplitude departure scales for each frequency (ratio f_1/f_2), and thus the same scale for b , we can reduce Fig. 7 to Fig. 8.

The curves in Fig. 9 were computed to study frequency dependence. In order to compare easily the change in departure due to frequency shift, frequency was eliminated as a scaling factor for b as illustrated above.

It will be noted that for values of l_x such that $1 \text{ km} \leq l_x \leq 3.0 \text{ km}$, the frequency dependence is sufficiently strong to be verified experimentally. This is just the range of irregularities observed in the ionosphere work.

The question therefore arose as to whether this non-linearity existed in this range when $l_x \neq l_y$ and the curves in Fig. 10 were computed to examine the spacings for $l_y = 5 l_x$, $l_y = 10 l_x$, and $l_y = 15 l_x$. The latter two sets of curves were identical within the plotting accuracy and $l_y = 15 l_x$ was therefore omitted.

It is immediately apparent that the range of non-linearity includes $1.0 \text{ km} \leq l_x \leq 3.0 \text{ km}$. Further, it is also noted that for $l_x \geq 2.6 \text{ km}$, the two sets of curves are almost indistinguishable indicating that the anisotropic effect is unimportant in this region, a property also shown clearly in Figs. 4 and 5.

Conclusions

The study of ionospheric irregularities based upon measurement by a single receiver of the scintillation of radio signals from a satellite, even when supplemented by other information such as layer height and layer thickness, is plagued not only by the inherent difficulties of accurately measuring the scintillation itself, but also by the fact that there are a large number of combinations of parameters which would cause the same scintillation. However, it would appear that accurate measurement of both phase departure and amplitude departure coupled with measurements of layer height and thickness could do much toward establishing bounds for certain parameters and for some confirmation of theoretical results.

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Figures

Fig. 1 Geometry of the Problem

Fig. 2 Normalized Root Mean Square Value of Phase Departure
($l_x = 1$ km, $f = 19.1$ Mc/s)

Fig. 3 Normalized Root Mean Square Value of Logarithmic Amplitude Departure
($l_x = 1$ km, $f = 19.1$ Mc/s)

Fig. 4 Normalized Root Mean Square Value of Phase Departure
($z = 12,800$ km, $f = 19.1$ Mc/s)

Fig. 5 Normalized Root Mean Square Value of Logarithmic Amplitude Departure
($f = 19.1$ Mc/s)

Fig. 6 Phase Departure vs. Logarithmic Amplitude Departure

Fig. 7 Effect of Frequency Dependence on Departure

Fig. 8 Effect of Normalization on Frequency Dependent Curves

Fig. 9 Effect of Frequency on Phase Departure vs. Logarithmic Amplitude Departure

Fig. 10 Effect of Ratio l_y/l_x on Phase Departure vs. Logarithmic Amplitude Departure

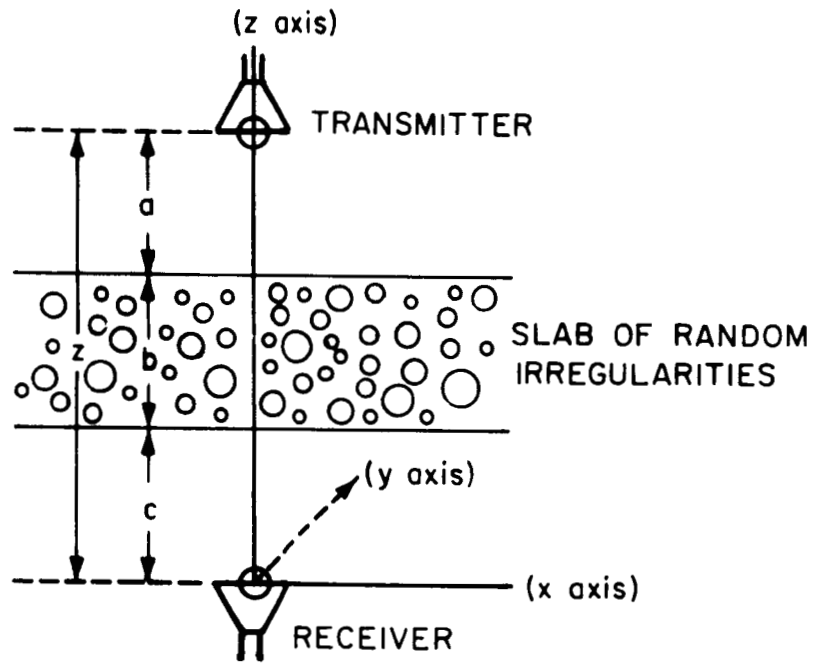


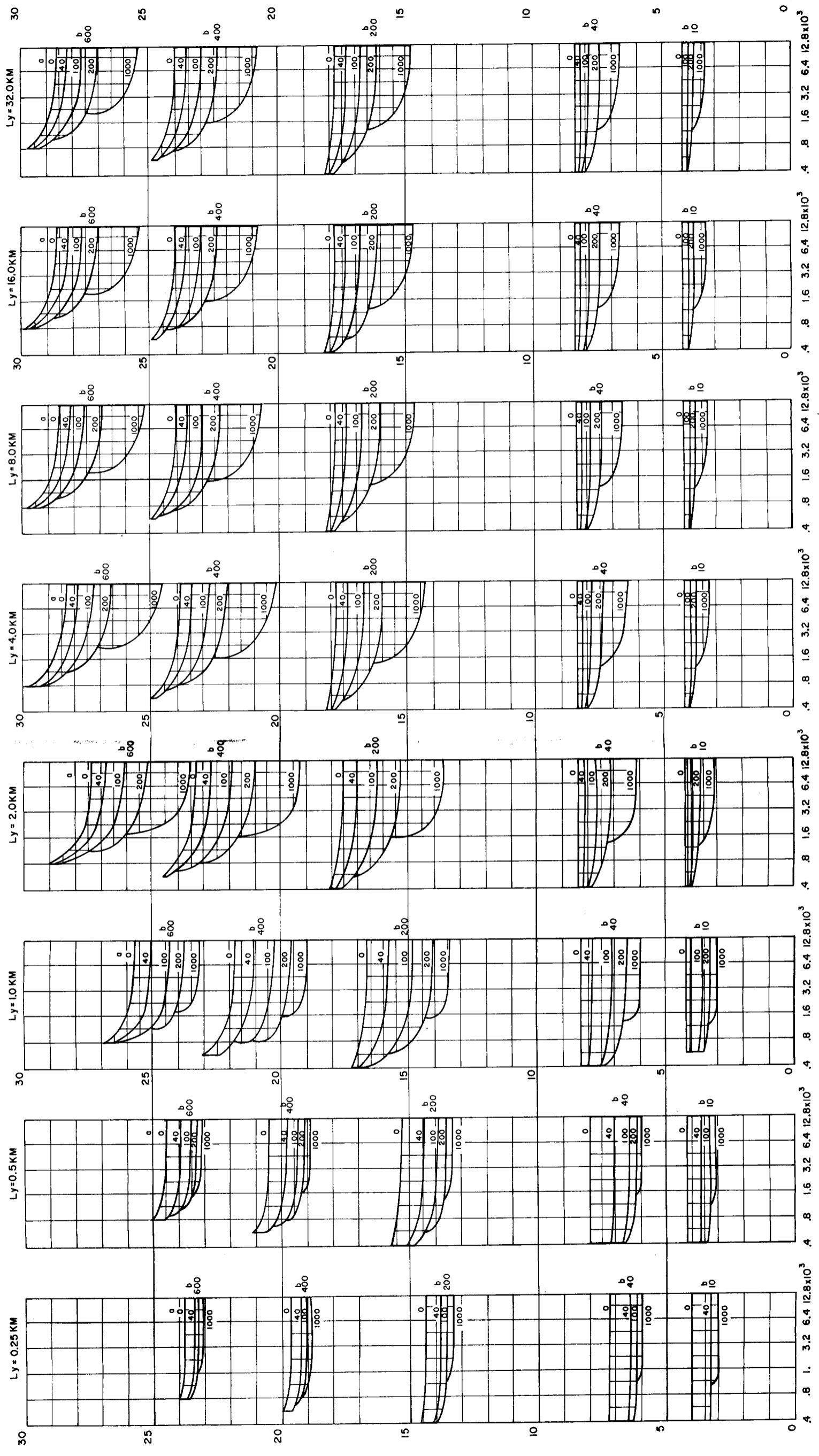
FIGURE 1.

FIGURE 2
 NORMALIZED
 ROOT MEAN SQUARE VALUE PHASE DEPARTURE

a = LAYER HEIGHT IN KM $L_x = 1.0 \text{ KM}$ $f = 19.1 \text{ MC}$ b = LAYER THICKNESS IN KM

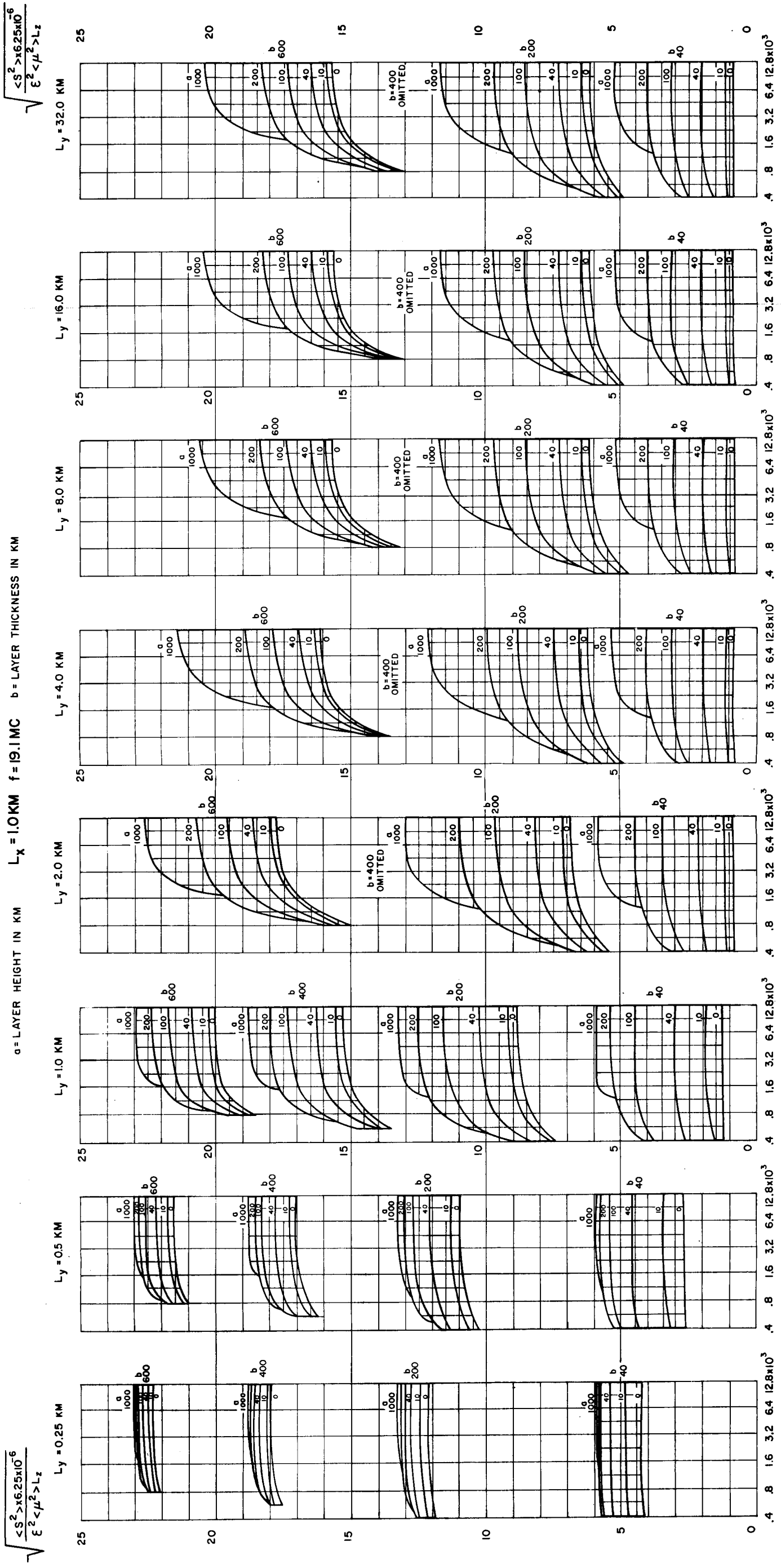
$$\sqrt{\frac{\langle Q^2 \rangle > 6.25 \times 10^{-6}}{\langle \epsilon^2 \rangle < \mu^2 > L_z}}$$

$$\sqrt{\frac{\langle Q^2 \rangle > 6.25 \times 10^{-6}}{\langle \epsilon^2 \rangle < \mu^2 > L_z}}$$



TRANSMITTER HEIGHT KILOMETERS

FIGURE 3
 NORMALIZED ROOT MEAN SQUARE VALUE LOG AMPLITUDE DEPARTURE



NORMALIZED ROOT MEAN SQUARE VALUE PHASE DEPARTURE

f = 19.1 MC

a = LAYER HEIGHT IN KM b = LAYER THICKNESS IN KM z (TRANSMITTER HEIGHT IN KM) = 12,800 KM

Lx = IRREGULARITY x-AXIS IN KM Ly = IRREGULARITY y-AXIS IN KM Lz = IRREGULARITY z-AXIS IN KM

$$\sqrt{\frac{\langle Q^2 \rangle + 6.25a^2}{\langle \xi^2 \rangle + \mu^2} > L_z}$$

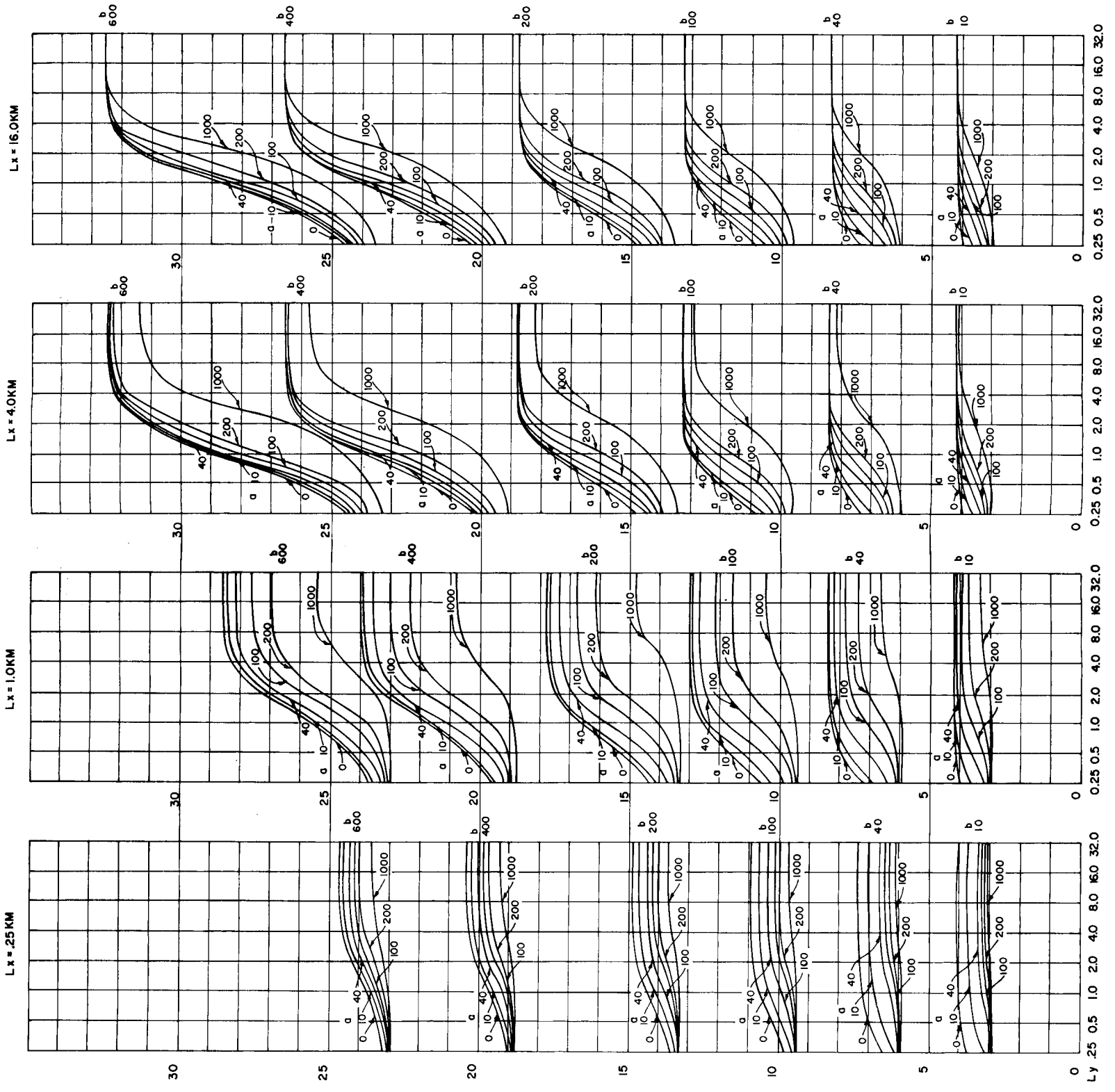


FIGURE 4.

**NORMALIZED
ROOT MEAN SQUARE VALUE LOG AMPLITUDE DEPARTURE**

$f = 19.1 \text{ MC}$

$$\sqrt{\frac{\langle S^2 \rangle \times 6.25 \times 10^6}{\langle \epsilon^2 \rangle \times \mu^2}} > L_z$$

a = LAYER HEIGHT IN KM b = LAYER THICKNESS IN KM z = TRANSMITTER HEIGHT IN KM
 L_x = IRRREGULARITY x-AXIS IN KM L_z = IRRREGULARITY z-AXIS IN KM L_y = IRRREGULARITY y-AXIS IN KM

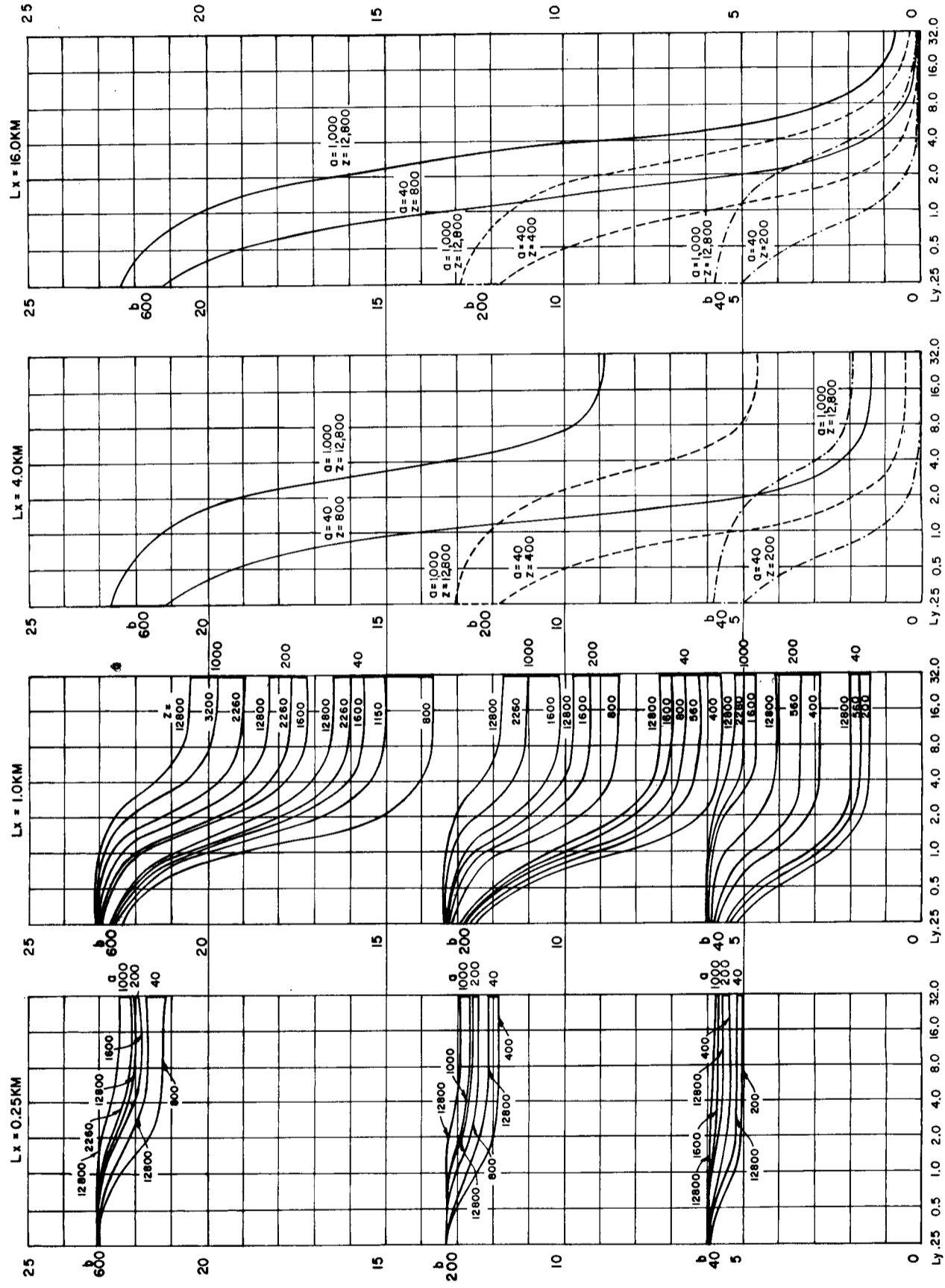
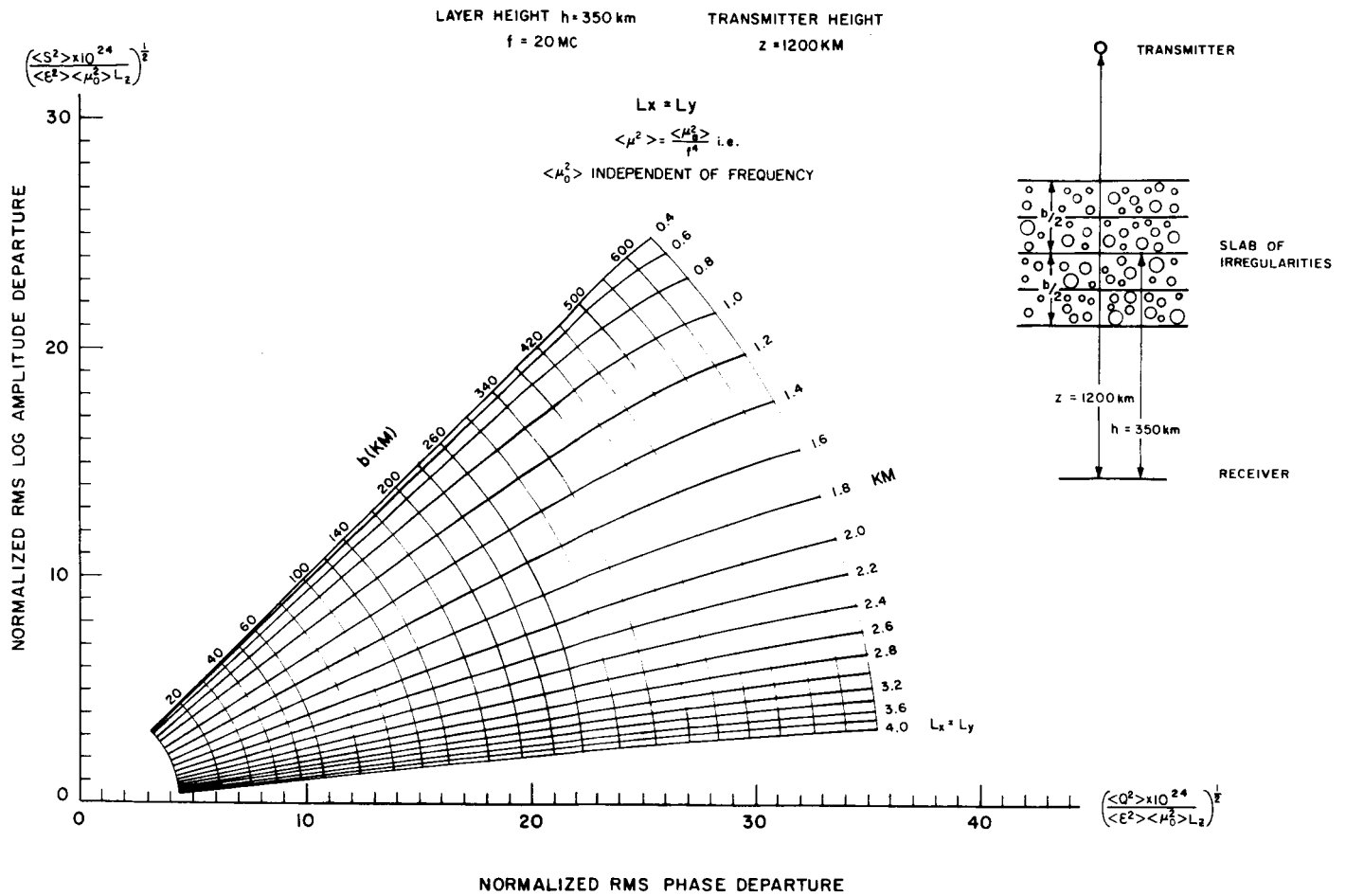


FIGURE 5.

FIGURE 6
RMS PHASE DEPARTURE vs. LOG AMPLITUDE
FOR VARIOUS LAYER THICKNESSES



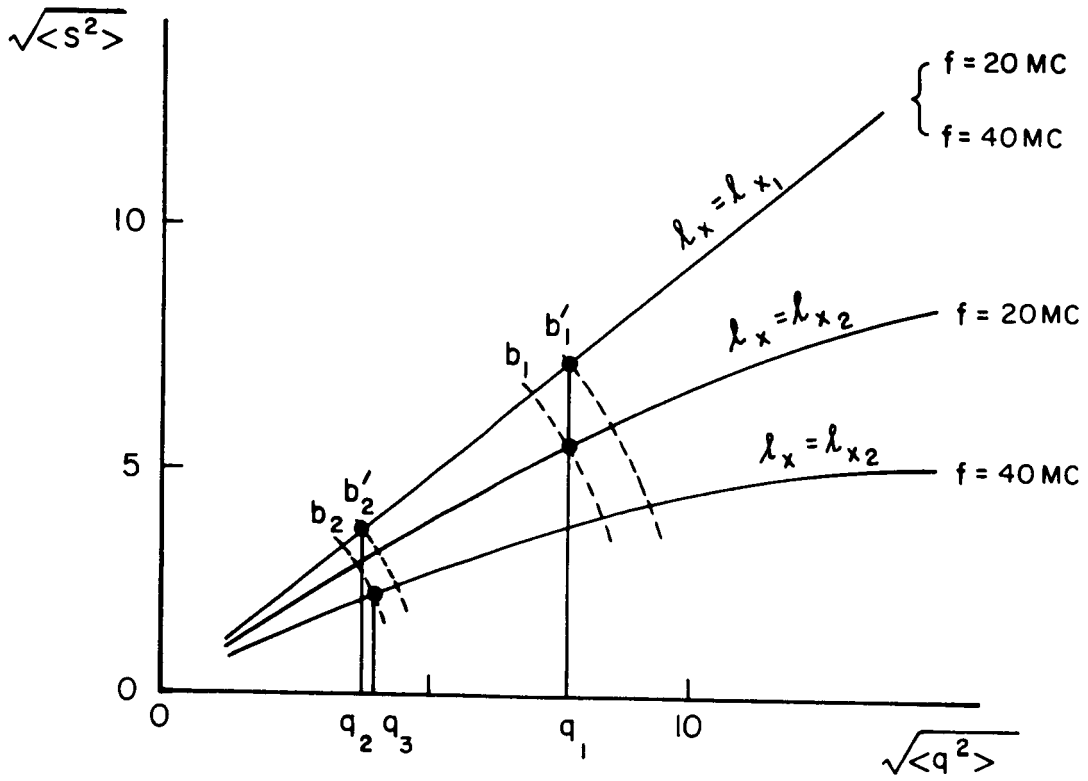


Figure 7.

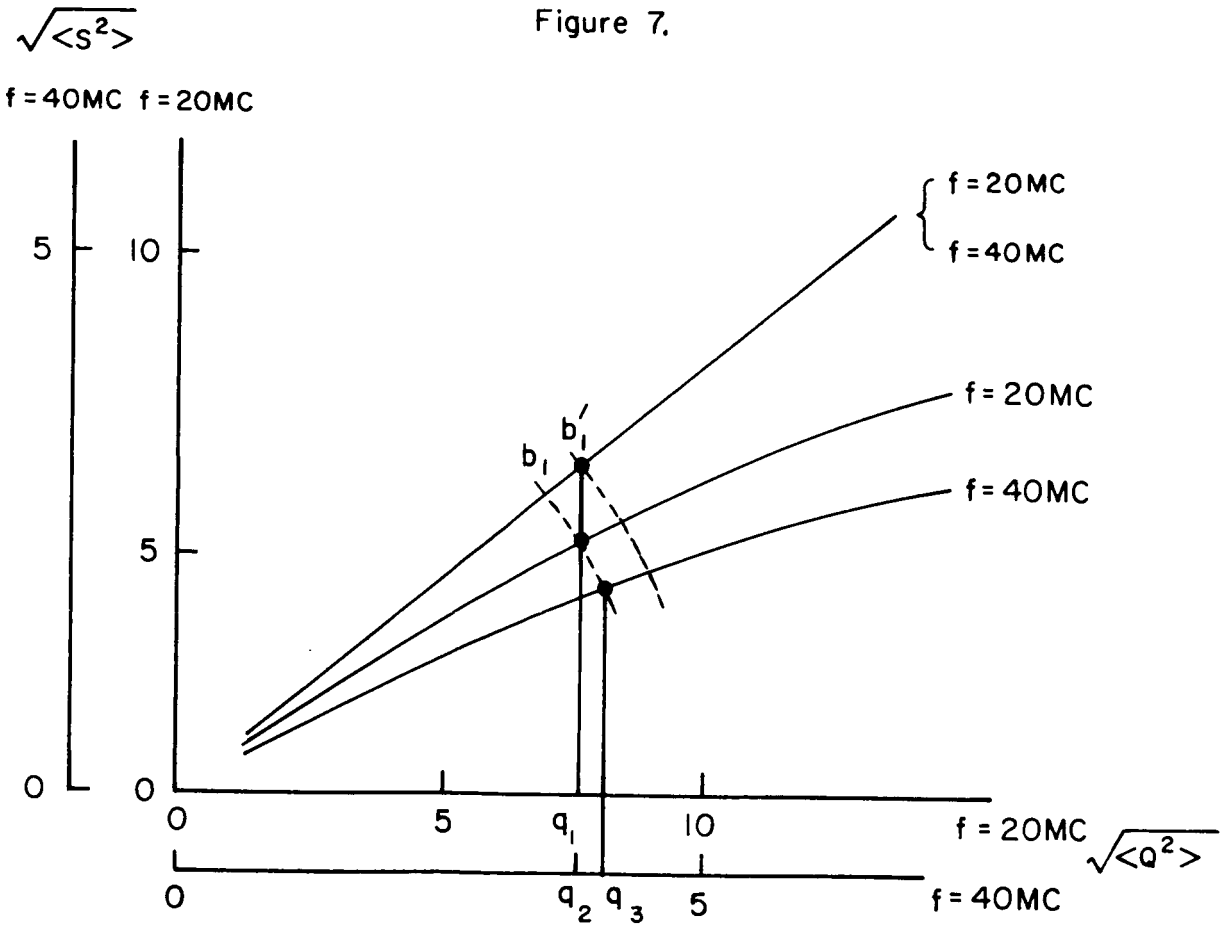


Figure 8.

FIGURE 9
EFFECT OF FREQUENCY ON PHASE DEPARTURE
AND LOG AMPLITUDE

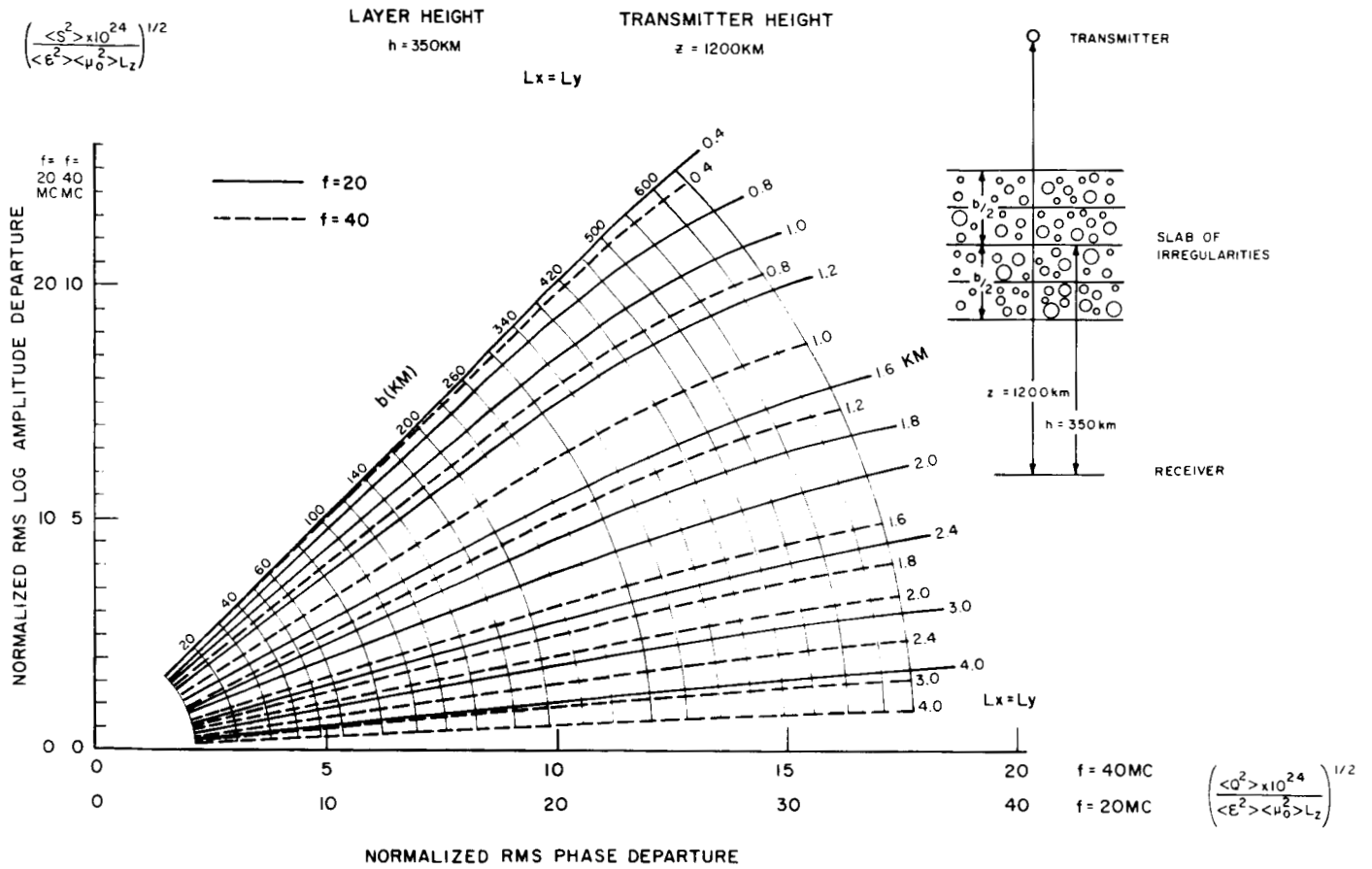


FIGURE 10
EFFECT OF RATIO L_y/L_x ON PHASE DEPARTURE
AND LOG AMPLITUDE

