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ELECTROLYTIC PREPARATION OF HIGH DIELECTRIC FILMS

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Section 1

INTRODUCTION

The objective of this investigation is the preparation of high dielectric materials in thin film form on refractory metal substrates by electrochemical techniques. Work performed during this quarter has been directed toward improving the capacitance of titanate, zirconate, niobate and tantalate films by vacuum heat treatment. The baths used have been of the EDTA type previously described and have used Group IIA and IA cations as complexed potential film modifiers. Reoxidation of the reduced films (produced in the vacuum heat treatment) by heating in air restores the insulative nature of the films, and in certain cases, a film with a lower loss and a higher capacity than the original films is produced.

This quarterly report is concerned only with the results of the vacuum heat treatment in terms of electrical measurements of capacitance and loss factors. The final report will contain additional information concerning the electrical properties as well as information concerning the composition and crystallinity of the coatings.

Section 2

HEAT TREATMENT OF COATINGS

2.1 INTRODUCTION

Repeated spectrographic examination of films formed on titanium, zirconium, and niobium under certain conditions in a bath containing an EDTA complex of barium or calcium have shown the presence of barium or calcium. However, the electrical properties of these films indicated a lack of crystallinity of the type that is associated with a high dielectric material. Attempts were made to induce the formation of a crystalline material by heating the films in air. Although the results were encouraging, oxidation of the substrate limited the temperatures at which the films could be processed. Thus a series of experiments were performed in which the films were heated in a vacuum and then reoxidized to eliminate film conductivity. The time and temperature of processing are the important factors in determining the final capacity of the films.

2.2 GENERAL PROCEDURE

Films have been formed on titanium, zirconium, niobium, and tantalum substrates using EDTA baths containing complexed barium, calcium, magnesium, sodium or potassium. All films have been formed at 100 ma/cm^2 for five minutes. The formation parameters used have varied only slightly and variations in electrical properties due to these factors are small compared to improvements noted if any.

Films were given a preliminary evaluation, then placed in quartz tubes, pumped until a vacuum of less than $5 \mu \text{ Hg}$ was obtained and then sealed. These samples were placed in a preheated furnace. The samples were removed from the furnace, cooled and then opened. They were then placed in an air oven at between 200 and 300°C and allowed to reoxidize.

2.3 RESULTS OF HEAT TREATMENT

2.3.1 Coatings on Titanium Substrates

The data obtained from coatings prepared and vacuum heat treated on titanium substrates is shown in Table 1. All samples heat treated at 700°C for any length of time were damaged to such a degree that air oxidation did not heal them. The extent of this damage was not visible as physical damage but appears as high loss factors. The treatment at 600°C was found to be the most satisfactory. The best treatment times used were 15 and 30 minutes. As the treatment time is extended, healing of the film by air oxidation becomes increasingly difficult.

2.3.2 Coatings on Zirconium Substrates

Attempts were made to improve the capacitance of films formed on zirconium by vacuum heat treatment. This data is shown in Table 2. All attempts resulted in either no improvement or drastically deteriorated capacitance and loss factors. These results here are in keeping with those observed when air heat treatment is used and indicated that zirconium films respond differently than titanium films.

2.3.3 Coatings on Niobium Substrates

The types of baths used to produce coatings on niobium were extended to include complexed magnesium, potassium, and sodium. The films produced in the latter baths are very white, glassy, and are formed at lower current densities than those used with calcium, barium, or magnesium. The electrical data is shown in Table 3 for these films before and after the vacuum heat treatment.

It should be noted first that treatment at 600°C for 15 minutes without subsequent air oxidation produces minimal if any increases in losses while the capacitance is increased by about a factor of 50. Further processing in air reduces the losses to acceptable values with drastic reduction of the capacitance, to levels about the same as the initial values.

TABLE 1

HEAT TREATMENT OF COATINGS ON TITANIUM

| Sample Number | EDTA Bath Used | VACUUM HEAT TREATMENT | | INITIAL CAPACITANCE | | CAPACITANCE AFTER HEATING | | OXIDATION TREATMENT | | FINAL CAPACITANCE | |
|---------------|----------------|-----------------------|-----------|--------------------------|--------|---------------------------|--------|---------------------|------------|--------------------------|--------|
| | | Temp. °C | Time Min. | Cs(1) nf/cm ² | Loss D | Cp(2) nf/cm ² | Loss D | Temp. °C | Time Hours | Cs(1) nf/cm ² | Loss D |
| 11-90-A | Calcium | 600 | 15 | 7.1 | 0.16 | 940 | 2.5 | 200 | 1 | 157 | 0.26 |
| B | | 600 | 15 | 9.6 | 0.18 | 775 | 3.7 | 200 | 1.5 | 168 | 0.18 |
| C | | 700 | 15 | 7.6 | 0.165 | 6100 | 9.5 | 300 | 2 | 190(P) | 2.1 |
| D | | 700 | 15 | 8.6 | 0.14 | 4000 | 12 | 200 | 4 | 1200(P) | 14 |
| E | | 700 | 60 | 8.3 | 0.18 | 2400 | 8 | | | | |
| F | | 700 | 60 | 10.3 | 0.19 | 1500 | 12.5 | | | | |
| 11-92-C | Calcium | 600 | 30 | 10.8 | 0.12 | -- | -- | 300,000 | 1.5,114 | 100 | 0.044 |
| D | | 600 | 30 | 11.7 | 0.14 | 175 | 20 | 200,300 | 16,1 | 117(P) | 0.22 |
| E | | 600 | 30 | 7.05 | 0.11 | 95 | 28 | 200,300 | 16,1 | 375 | 0.65 |
| F | | 600 | 30 | 6.55 | 0.14 | -- | -- | 300,200 | 1.5,114 | 104 | 0.056 |
| 11-94-A | Calcium | 600 | 15 | 13 | 0.29 | 25 | 0.82 | -- | -- | | |
| B | | 600 | 15 | 15.4 | 0.28 | -- | -- | 200 | 70 | 117 | 0.086 |
| C | | 600 | 15 | 17.1 | 0.34 | 215 | 0.95 | -- | -- | | |
| E | | 600 | 15 | 7.35 | 0.19 | -- | -- | 200 | 70 | 143 | 0.23 |
| ER | | 600 | 15 | 20.3 | 0.27 | -- | -- | 200 | 70 | 118 | 0.06 |
| F | | 600 | 15 | 18.5 | 0.26 | 8.0 | 0.38 | -- | -- | | |
| 11-91-A | Barium | 700 | 60 | 6.6 | 0.078 | 8500 | 7 | 200 | 1.5 | 2250(P) | 3.8 |
| B | | 700 | 60 | 5.4 | 0.095 | 7750 | 9.2 | 200 | 1 | 10,000(P) | 0.088 |
| C | | 600 | 15 | 6.4 | 0.096 | 575 | 18 | 300,200 | 1, 15 | 91 | 0.088 |
| D | | 600 | 15 | 8.1 | 0.11 | 525 | 26 | 200 | 19 | 150 | 0.38 |

TABLE 1 - HEAT TREATMENT OF COATINGS ON TITANIUM (Continued)

| Sample Number | EDTA Bath Used | VACUUM HEAT TREATMENT | | INITIAL CAPACITANCE | | CAPACITANCE AFTER HEATING | | OXIDATION TREATMENT Temp. °C | Time Hours | FINAL CAPACITANCE | |
|---------------|----------------|-----------------------|-----------|---------------------------|--------|---------------------------|--------|------------------------------|------------|---------------------------|--------|
| | | Temp. °C | Time Min. | Cs (1) nf/cm ² | Loss D | Cp (2) nf/cm ² | Loss D | | | Cs (1) nf/cm ² | Loss D |
| 11-93-C | Barium | 600 | 15 | 17.1 | 0.36 | -- | -- | 200 | 92 | 120 | 0.075 |
| D | | 600 | 15 | 10.9 | 0.38 | (3) | | 200 | 92 | 105 | 0.09 |
| E | | 600 | 15 | 1.08 | 0.25 | 675 | 2.2 | 200 | 92 | 36.8 | 0.5 |
| F | | 600 | 15 | 5.35 | 0.35 | -- | | 200 | 92 | 94 | 0.46 |
| 11-95-A | Barium | 600 | 15 | 10.8 | 0.31 | 0.35 | 4.6 | 200 | 70 | 115 | 0.08 |
| B | | 600 | 15 | 20.1 | 0.31 | | | 200 | 70 | | |
| C | | 600 | 15 | 17.8 | 0.30 | 40(s) | 0.95 | 200 | 70 | 96.5 | 0.062 |
| D | | 600 | 15 | 20.8 | 0.33 | | | 200 | 70 | | |
| E | | 600 | 15 | 19.8 | 0.28 | 8.0 | 1.1 | 200 | 70 | 150 | 0.055 |
| F | | 600 | 15 | 11.2 | 0.28 | | | 200 | 70 | | |

(1) Series Capacitance unless noted by (P)

(2) Parallel Capacitance unless noted by (S)

(3) Bridge would not null.

TABLE 2

HEAT TREATMENT OF COATINGS ON ZIRCONIUM

| Sample Number | EDTA Bath Used | VACUUM HEAT TREATMENT | | INITIAL CAPACITANCE | | CAPACITANCE AFTER HEATING | | OXIDATION TREATMENT | | FINAL CAPACITANCE | |
|---------------|----------------|-----------------------|-----------|--------------------------|--------|---------------------------|---------|---------------------|------------|--------------------------|--------|
| | | Temp. °C | Time Min. | Cs(1) nf/cm ² | Loss D | Cp(2) nf/cm ² | Loss D | Temp. °C | Time Hours | Cp(2) nf/cm ² | Loss D |
| 11-104-A | Barium | 600 | 15 | 4.65 | 0.025 | 62.5 | 33 | 200 | 4.5 | 0.6(S) | 1.8 |
| B | | 600 | 15 | 3.42 | 0.028 | 25 | 46 | 200 | 4.5 | 0.8(S) | 0.76 |
| E | | 700 | 15 | 2.94 | 0.025 | 218 | 18 | 200 | 17 | 3.5 | 21 |
| F | | 700 | 15 | 1.72 | 0.025 | 150 | 31 | 200 | 17 | 25 | 36 |
| G | | 600 | 15 | 2.01 | 0.034 | | 2.2 | 200,300 | 72,1 | (3) | |
| H | | 600 | 15 | 2.43 | 0.036 | | 1.0 | 200 | 72 | 7.5x10 ⁻³ | 3.7 |
| I | | 500 | 30 | 2.14 | 0.032 | | 2.40(S) | | | | |
| 11-105-A | Calcium | 500 | 30 | 1.59 | 0.026 | | 1.71(S) | | | | |
| C | | 700 | 15 | 1.54 | 0.028 | 3,500 | 14 | 200 | 17 | 24 | 12.5 |
| D | | 700 | 15 | 1.32 | 0.024 | 4,000 | 14.5 | 200 | 17 | 26 | 15 |
| E | | 700 | 15 | 2.95 | 0.030 | 9,250 | 8 | 200,300 | 17,1 | 22.5 | 8 |
| F | | 700 | 15 | 3.4 | 0.026 | 250 | 17 | 200 | 17 | 22.5 | 16.5 |
| G | | 650 | 15 | 1.59 | 0.028 | 150 | 10 | 200,300 | 24,1 | 4.1(S) | 0.077 |
| H | | 650 | 15 | 2.42 | 0.032 | 205 | 18 | 200,300 | 24,1 | 4.3(S) | 0.12 |

(1) Series Capacitance unless noted by (P)

(2) Parallel Capacitance unless noted by (S)

(3) Bridge would not null

TABLE 3

HEAT TREATMENT OF COATINGS ON NIOBIUM

| Sample Number | EDTA Bath Used | VACUUM HEAT TREATMENT | | INITIAL CAPACITANCE | | CAPACITANCE AFTER HEATING | | OXIDATION TREATMENT | | FINAL CAPACITANCE | |
|---------------|----------------|-----------------------|-----------|--------------------------|--------|---------------------------|--------|---------------------|------------|--------------------------|--------|
| | | Temp. °C | Time Min. | Cs(1) nf/cm ² | Loss D | Cs(1) nf/cm ² | Loss D | Temp. °C | Time Hours | Cs(1) nf/cm ² | Loss D |
| 11-108-A | Barium | 600 | 15 | 2.4 | 0.18 | 145 | 0.22 | 200 | 104 | 3.8 | 0.049 |
| B | | 700 | 30 | 2.5 | 0.19 | 354 | 0.56 | 200 | 99 | 3.6 | 0.048 |
| C | | 600 | 15 | 6.0 | 0.14 | 137 | 0.12 | 300,250 | 1,17 | 5.9 | 0.059 |
| D | | 700 | 60 | 4.6 | 0.14 | 174(P) | 5.5 | 300 | 41 | 500(P) | 48 |
| E | | 600 | 15 | 10.4 | 0.15 | 122 | 0.09 | 200 | 104 | 2.45(P) | 3.6 |
| F | | 700 | 30 | 8.9 | 0.16 | 144 | 0.21 | 200 | 99 | 40.5 | 0.25 |
| G | | 600 | 15 | 7.0 | 0.14 | 98 | 0.12 | 300,250 | 1,17 | 66 | 0.057 |
| H | | 700 | 60 | 6.0 | 0.12 | 127(P) | 5.8 | 300 | 41 | 400(P) | 30 |
| I | | 650 | 15 | 5.1 | 0.14 | 186 | 0.78 | 200 | 17 | 52 | 0.06 |
| J | | 650 | 15 | 8.8 | 0.115 | 2430 | 0.70 | 200 | 17 | 59 | 0.09 |
| 11-109-A | Calcium | 650 | 15 | 2.77 | 0.17 | 2.11(P) | 30 | 200 | 17 | 1.4(P) | 1.7 |
| B | | 700 | 30 | 2.82 | 0.18 | 21(P) | 23 | 200 | 99 | 5.6 | 0.22 |
| C | | 650 | 15 | 5.9 | 0.13 | 130(P) | 5.8 | 200 | 17 | 1.8(P) | 1.4 |
| D | | 650 | 15 | 4.2 | 0.12 | -- | -- | 200 | 70 | 101 | 0.27 |
| E | | 650 | 15 | 9.4 | 0.135 | -- | -- | 200 | 70 | 37.5 | 0.77 |
| F | | 700 | 30 | 12.2 | 0.14 | 1.2(P) | 9.5 | 200 | 34 | 91 | 0.125 |
| G | | 700 | 60 | 4.6 | 0.098 | 1000(P) | 33 | 300 | 41 | 400(P) | 20 |
| H | | 700 | 60 | 5.3 | 0.08 | 7250(P) | 18 | 300 | 41 | 1400(P) | 20 |
| I | | 650 | 15 | 4.2 | 0.075 | -- | -- | 200 | 70 | 206 | 0.54 |
| J | | 650 | 15 | 6.9 | 0.12 | -- | -- | 200 | 70 | 75 | 0.68 |

TABLE 3 - HEAT TREATMENT OF COATINGS ON NIOBIUM (Cont.)

| Sample Number | EDTA Bath Used | VACUUM HEAT TREATMENT | | INITIAL CAPACITANCE | | CAPACITANCE AFTER HEATING | | OXIDATION TREATMENT | | FINAL CAPACITANCE | |
|---------------|----------------|-----------------------|-----------|--------------------------|--------|---------------------------|--------|---------------------|------------|--------------------------|--------|
| | | Temp. °C | Time Min. | Cs(l) nf/cm ² | Loss D | Cs(l) nf/cm ² | Loss D | Temp. °C | Time Hours | Cs(l) nf/cm ² | Loss D |
| 11-110-A | Magnesium | 650 | 15 | 3.2 | 0.135 | 200(P) | 8.7 | 200 | 179 | 2.145 | 0.043 |
| B | | 600 | 40 | 5.5 | 0.26 | 1600(P) | 10.5 | 300 | 26 | (3) | |
| D | | 650 | 15 | 8.8 | 0.26 | -- | -- | 200 | 70 | 169 | 0.064 |
| E | | 700 | 60 | 9.8 | 0.23 | 7400(P) | 26 | 300 | 17 | 340(P) | 17 |
| F | | 600 | 40 | 14.8 | 0.21 | 700(P) | 18 | 200 | 87 | (3) | |
| H | | 650 | 15 | 8.3 | 0.21 | -- | -- | 200 | 70 | 178 | 0.08 |
| I | | 650 | 15 | -- | -- | -- | -- | 200 | 70 | 5.4 | 0.045 |
| 11-118-C | Potassium | 700 | 40 | 2.9 | 0.058 | 850(P) | 32 | 300 | 31 | 1000(P) | 20 |
| D | | 650 | 15 | 2.7 | 0.085 | 240(P) | 24 | 200 | 109 | | |
| E | | 650 | 15 | 18.9 | 0.055 | 210(P) | 21 | 200 | 109 | 103 | 0.07 |
| F | | 650 | 15 | 11.5 | 0.069 | 0.40(P) | 40 | 200 | 109 | 136 | 0.07 |
| G | | 650 | 15 | 30.2 | 0.033 | 3 | | 200 | 109 | 76 | 0.16 |
| 11-125-B | Sodium | 650 | 15 | 1.84 | 0.042 | 3 | | 200 | 94 | 3.05 | 0.18 |
| C | | 650 | 15 | 1.69 | 0.04 | 600(P) | 14 | 200 | 24 | 225 | 0.95 |
| D | | 650 | 15 | 2.20 | 0.048 | | | 200 | 70 | 1.35 | 0.096 |
| E | | 650 | 15 | 1.13 | 0.035 | | | 200 | 70 | 1.49 | 0.037 |
| F | | 650 | 15 | 1.0 | 0.03 | | | 200 | 70 | 1.47 | 0.078 |
| G | | 650 | 15 | 1.18 | 0.036 | | | 200 | 70 | 1.25 | 0.065 |

(1) Series Capacitance unless noted by (P)

(2) Parallel Capacitance unless noted by (S)

(3) Bridge would not null.

Processing at 700°C or at any temperature for time periods beyond 15 minutes produces films that cannot be healed by the subsequent air oxidation.

The best processing technique observed in this data uses films formed in the potassium or magnesium bath and heat treatments at 650°C for 15 minutes. Films processed by this technique have shown electrical properties similar to the titanium films. This result is not unusual inasmuch as niobium and titanium have quite a few other properties that are similar.

Time has not permitted a compositional analysis of these coatings. An extension of this program would logically include this study as these coatings are quite promising.

2.3.4 Coatings on Tantalum Substrates

The results of processing coatings formed on tantalum in the EDTA baths are shown in Table 4. Attempts were made to form coatings on tantalum in the potassium and sodium EDTA bath. However, only thin interference coatings were obtained. The magnesium-EDTA bath did produce coatings similar in appearance to the coatings formed on niobium. However, only slight or no improvement in the capacitance and loss factors was observed when the coatings were heat treated. At best the capacitance was doubled, but at the same time higher loss factors were observed.

TABLE 4

HEAT TREATMENT OF COATINGS ON TANTALUM

| Sample Number | EDTA Bath Used | VACUUM HEAT TREATMENT | | INITIAL CAPACITANCE | | CAPACITANCE AFTER HEATING | | OXIDATION TREATMENT | | FINAL CAPACITANCE | |
|---------------|----------------|-----------------------|-----------|--------------------------|--------|---------------------------|--------|---------------------|------------|--------------------------|--------|
| | | Temp. °C | Time Min. | Cs(1) nf/cm ² | Loss D | Cp(2) nf/cm ² | Loss D | Temp. °C | Time Hours | Cs(1) nf/cm ² | Loss D |
| 11-112-A | Barium | 700 | 30 | 4.15 | 0.048 | 5.4(S) | 0.21 | 300,200 | 24, 65 | 4.53 | 0.048 |
| B | | 700 | 30 | 3.78 | 0.048 | 5.4(S) | 0.165 | 300,200 | 24, 65 | 4.58 | 0.05 |
| C | | 600 | 40 | 5.15 | 0.053 | 1.5 | 7.2 | 200 | 82 | 9.05 | 0.076 |
| D | | 600 | 40 | 7.48 | 0.002 | 2.0 | 8.3 | 200 | 82 | 10.1 | 0.09 |
| E | | 700 | 60 | 10.8 | 0.042 | 34.5 | 29 | 300 | 46 | 21.5(P) | 2.5 |
| F | | 700 | 60 | 13.7 | 0.031 | (3) | | 300 | 46 | 20.1(P) | 1.7 |
| G | | 650 | 15 | 7.35 | 0.058 | (3) | | 200 | 17 | 0.06(P) | 3.3 |
| H | | 650 | 15 | 6.75 | 0.064 | (3) | | 200 | 17 | 11.0 | 0.12 |
| 11-113-A | Calcium | 650 | 15 | 5.40 | 0.054 | 10.8 | 0.28 | 200 | 17 | 8.85 | 0.115 |
| B | | 650 | 15 | 5.65 | 0.060 | 11.4(S) | 0.26 | 200 | 17 | 7.85 | 0.105 |
| E | | 700 | 60 | 16.7 | 0.053 | (3) | | 300 | 41 | 0.1 | 20 |
| F | | 700 | 60 | 15.7 | 0.065 | (3) | | 300 | 41 | 4.8(P) | 2.5 |
| 11-114-E | Magnesium | 700 | 60 | 10.0 | 0.085 | (3) | | 200,300 | 65, 63 | (3) | |
| F | | 700 | 60 | 16.4 | 0.18 | (3) | | 200,300 | 65, 63 | 2100 | 14 |
| G | | 650 | 15 | 9.35 | 0.115 | 31.4 | 5.6 | 200 | 17 | 20.1 | 0.25 |
| H | | 650 | 15 | 9.35 | 0.13 | 29.4 | 3.6 | 200 | 179 | 16.9 | 0.14 |

(1) Series Capacity unless noted by (P).

(2) Parallel Capacity unless noted by (S).

(3) Bridge would not null.

Section 3

CONCLUSIONS

Vacuum heat treatment of coatings formed in EDTA baths on titanium and niobium produces a low resistance film. When reoxidized in air at 200 to 300°C the coating becomes a dielectric with enhanced capacitance and lower losses. Using the values of coatings on titanium treated in such a manner, and thickness measurements made by the Dermatron instrument, the apparent dielectric constants have been calculated.

TABLE 5

Apparent Dielectric Constants

| Sample Number | Substrate | EDTA Bath | As Formed | Fired & Oxidized |
|---------------|-----------|-----------|-----------|------------------|
| 11-92-F | Titanium | Calcium | 160 | 1600 |
| 11-93-F | Titanium | Barium | 120 | 1900 |
| 11-94-F | Titanium | Calcium | 160 | 760 |
| 11-95-F | Titanium | Barium | 95 | 1300 |
| 11-110-D | Niobium | Magnesium | 99.5 | 1900 |
| 11-118-F | Niobium | Potassium | 58 | 690 |

These values show that a high dielectric thin film can be produced by use of the technique described. The vacuum heating and reoxidation-healing steps produce an order of magnitude improvement for titanium and niobium-based films.



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