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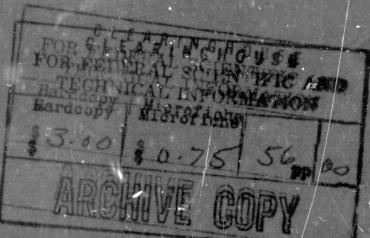
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NRL Report 6246

# High-Temperature Properties of Cesium

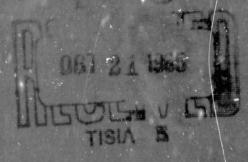
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#### ABSTRACT

The experimental program at this Laboratory to measure various thermophysical properties of sodium, potassium, and cesium has been completed. Final reports on two of the alkali metals, sodium and potassium, have been published; and this is the final reporting on cesium. Experimental results are presented for the density and vapor pressure of the liquid and for various saturation and superheat properties of the vapor. A virial equation of state is advanced and is used thermodynamically to derive additional properties of the vapor. For example, enthalpy, entropy, specific volume, and specific heat are tabulated for some 1100 selected vapor states in the temperature range from 1250° to 2550°F and in the pressure range from 0.2 to 34.0 atm.

#### PROBLEM STATUS

This is the final report on the experimental work with cesium and the final report on this problem. All contracted measurements have been completed except for the surface tension of liquid potassium and cesium. This problem will be considered closed with the issuance of this report.

#### AUTHORIZATION

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#### HIGH-TEMPERATURE PROPERTIES OF CESIUM

#### INTRODUCTION

In the development of compact turboelectric systems for space vehicles, the National Aeronautics and Space Administration is sponsoring a property measurement program for the evaluation of several liquid metals as possible working fluids. As an integral part of this program, the U.S. Naval Research Laboratory contracted to measure several thermophysical properties of potassium to 2300°F, sodium to 2500°F, and cesium to 2300°F.

The saturated liquid properties which have been determined experimentally include density, vapor pressure, and specific heat (except for cesium). Saturated and superheated vapor properties, including specific volume, specific heat, enthalpy and entropy, have been derived from experimental pressure-volume-temperature (PVT) studies. All phases of this measurement program have been completed. The final properties of sodium (2) and potassium (1) have been published in companion reports; those of cesium are presented in this report.

### EXPERIMENTAL MATERIALS AND METHODS COMMON TO ALL MEASUREMENTS

A number of materials, methods, and techniques were common to many of the experimental measurements. These include the container alloy, the high-pressure furnace system, the temperature measurement, and techniques for purifying and transferring the alkali metals. All are discussed at some length in the companion report on potassium (1), and only a short section to describe the purity of the cesium will be included in this report.

The cesium samples for the density determinations were distilled directly from a small glass still into the pycnometers. However, for the PVT determinations this procedure was impractical, and the metal was distilled and introduced into small columbium alloy capsules for subsequent transfer (1) into the PVT apparatus. Cesium introduced to the distillation retort for the density experiments, the PVT experiments, and one vapor-pressure experiment was a high-purity grade from MSA Research Corporation; and a typical spectrographic analysis of this cesium after one distillation at this Laboratory is presented in Table 1. Although the metal was distilled at low temperature under high vacuum, the still may have introduced some of the metal impurities, particularly silicon and sodium. A high-purity grade of cesium from Dow Chemical Company was used for one vapor-pressure experiment. The distilled sample of this cesium for analysis was lost, and the data reported in Table 1 are for an "as received" sample oxidized on Pyrex glass. It is very probable that silicon, aluminum, and sodium were introduced by reaction with glass under these conditions, and it is recognized that the analysis is unsatisfactory. However, since the volatile and nonvolatile impurities in the MSA metal (and probably the Dow sample, too) are present in concentrations too low to produce a measurable vapor-pressure change, no additional analytical work was performed.

Table 1
Spectrographic Analyses of Cesium at NRL

Metal Impurity	MSAR Sample (ppm)	Dow Chemical Sample (ppm)		
Rb	500*	10*		
K	<10	1		
Na	100*	1000*		
Li	Not detected	Not detected		
Ca	1 to 10	10 to 100		
Ва	Not detected	Not detected		
Sr	Not detected	Not detected		
Al	Not detected	100 to 1000		
В	<1	-		
Si	10 to 100	100 to 1000		
Mn	Not detected <1			
Fe	Not detected	<1		
Mg	<1	<1		
Cu	Not detected	10 to 100		

<sup>\*</sup>Used standard samples for comparison; figures should be close to quantitative.

#### EXPERIMENTAL MEASUREMENTS

Pressure-Volume-Temperature Measurements of Cesium

Experimental Superheat Results - The PVT measurements in both the superheat and saturation regions were made with small closed chambers of columbium-1%zirconium using flexible diaphragms as null-detectors. This high-temperature apparatus and the methods employed are described in detail for potassium (1), and only the experimental results for cesium are included in this report.

The twelve PVT experiments for cesium (Table 2) covered a broad range in the superheat region with measured temperatures extending from 1305° to 2570°F and pressures from 1.1 to 33.2 atm. For each experimental point in this table, pressure and temperature were directly observed, and the specific volume was computed from the weight of cesium added to the chamber. The nominal volume of all chambers was 57 cc, and the weights of the cesium samples varied from 0.1173 g in experiment 30 to 2.4205 g in experiment 37.

To obtain the data at each equilibrium point in Table 2, multiple readings of temperature and pressure were made at 5 to 10 min intervals until successive readings showed a temperature drift of  $0.07^{\circ}F/min$  or less and a temperature difference across the chamber less than  $2^{\circ}F$ , and generally less than  $1^{\circ}F$ . In the measurement of pressures with the diaphragm device, the excellent reproducibility obtained during the other alkali metal measurements (1,2) continued for cesium. Measurements for each experiment (except

Table 2
Pressure-Volume-Temperature Measurements of
Cesium Superheat Region

Temp.	Pressure (abs atm)	Specific Volume (cu ft/lb)	Temp.	Pressure (abs atm)	Specific Volume (cu ft/lb)	
	Experiment 27			Experiment 30		
1785.3	6.989	1.5321	1341.5	1.1489	8.0140	
1953.8	7.697	1.5358	1460.8	1.2438	8.0266	
2095.4	8.255	1.5390	1581.4	1.3384	8.0397	
2201.6	8.679	1.5415	1712.7	1.4337	8.0543	
2319.7	9.122	1.5443	1777.9	1.4772	8.0617	
2425.8	9.528	1.5469	1901.5	1.5616	8.0760	
2558.6	10.010	1.5502	1996.8	1.6275	8.0873	
2520.4	9.873	1.5492	2094.8	1.6958	8.0991	
2366.6	9.310	1.5454	2212.0	1.7752	8.1135	
2262.5	8.914	1.5429	2314.1	1.8425	8.1263	
2163.2	8.542	1.5406	2424.6	1.9155	8.1405	
2044.8	8.050	1.5378	2571.4	2.0137	8.1597	
1884.5	7.414	1.5342	2518.7	1.9786	8.1528	
1826.2	7.167	1.5329	2465.0	1.9420	8.1457	
1724.3	6.736	1.5307	2369.2	1.8827	8.1333	
1741.1	6.808	1.5311	2257.5	1.8069	8.1192	
			2139.4	1.7288	8.1045	
	Experiment	28	2029.2	1.6527	8.0912	
	T		1948.5	1.5970	8.0815	
1649.0	4.849	2.0879	1847.8	1.5262	8.0697	
1703.2	5.024	2.0894	1649.8	1.3853	8.0473	
1822.0	5.378	2.0929	1515.0	1.2853	8.0325	
1612.7	4.745	2.0868	1391.1	1.1901	8.0192	
1737.2	5.138	2.0904	1305.0	1.1227	8.0103	
1854.8	<b>5.4</b> 80	2.0939				
1978.8	5.862	2.0977		Experiment	91	
2081.0	6.145	2.1009		Experiment	31	
2178.4	6.419	2.1040				
2275.0	6.697	2.1071	1909,1	9.615	1.1606	
2379.1	6.971	2.1105	2037.4	10.327	1.1628	
2485.2	7.258	2.1141	2143.7	10.881	1.1646	
2565.6	7.488	2.1169	2236.7	11.375	1.1663	
2523.2	7.370	2.1154	2363.0	12.033	1.1686	
2441.6	7.143	2.1126	2462.0	12.515	1.1704	
2329.0	6.848	2.1089	2568.2	13.044	1.1724	
2221.4	6.552	2.1054	2518.6	12.800	1.1715	
2116.9	6.252	2.1020	2415.6	12.290	1.1695	
2038.2	6.033	2.0995	2305.0	11.722	1.1675	
1919.5	5.699	2.0959	2186.5	11.115	1.1654	
1766.5	5.223	2.0913	2081.2	10.558	1.1635	
1624.3	4.793	2.0871	1959.5	9.890	1.1614	
1647.5	4.859	2.0878	1827.0	9.158	1.1592	

(Table continues)

Table 2 (cont'd)
Pressure-Volume-Temperature Measurements of
Cesium Superheat Region

Temp.	Pressure (abs atm)	Specific Volume (cu ft/lb)	Temp.	Pressure (abs atm)	Specific Volume (cu ft/lb)	
Experiment 32			Experiment 37			
1846.9 1944.1	9.367 9.909	1.1468 1.1484	2405.0 2512.7	31.319 33.112	.38763 .38830	
2058.5	10.549	1.1504	2519.7	33.223	.38835	
2175.7	11.176	1.1524	2487.5	32.688	.38815	
2291.4	11.781	1.1545	2445.9	31.988	.38789	
2396.2	12.331	1.1564	2355.1	30.470	.38733	
2497.5	12.866	1.1582	2315.1	29.779	.38709	
2558.8	13.169	1.1594				
2452.0	12.613	1.1574		Experiment	38	
2363.8	12.182	1.1558	1578.9	3.3677	3.0146	
2238.3	11.523	1.1535	1684.9	3.560	3.0190	
2140.1	10.993	1.1518	1801.0	3.805	3.0239	
1973.9	10.082	1.1489	1921.5	4.067	3.0292	
1894.9	9.643	1.1476	2015.7	4.237	3.0334	
1830.5	9.283	1.1465	2136.8	4.462	3.0389	
			2230.5	4.649	3.0432	
Experiment 34		34	2348.2	4.871	3.0488	
			2437.7	5.041	3.0531	
2068.0	15.241	.75273	2523.8	5.191	3.0574	
2174.2	16.156	.75394	2479.4	5.116	3.0552	
2184.2	16.245	.75405	2314.0	4.816	3.0472	
2294.0	17.171	.75533	2193.8	4.579	3.0415	
2387.8	17.938	.75644	2076.7	4.359	3.0361	
2483.7	18.723	.75760	1970.3	4.162	3.0314	
2543.1	19.212	.75833	1864.1	3.958	3.0267	
2516.5	18.990	.75800	1777.8	3.768	3.0230	
2437.0	18.360	.75703	1640.8	3.488	3.0172	
2347.6	17.622	.75596	1521.8	3.2316	3.0123	
2247.9	16.797	.75479		Experiment 39		
2119.4	15.700	.75331	0100 7			
2024.9	14.880	.75225	2183.7	21.758	.52803	
	E	25	2320.2	23.438	.52915	
	Experiment	. 35	2423.6 2540.7	24.691 26.064	.53001 .53101	
2126 4	17 650	25720				
2126.4 2223.6	17.659 18.612	.65739 .65836	2487.0 2379.4	25.440 24.173	.53055 .52964	
2329.0	19.636	.65944	2260.0	22.717	.52865	
2492.6	21.162	.66115	2222.7	22.717	.52835	
2447.0	20.727	.66067	2149.9	21.356	.52776	
2401.2	20.727	.66019	2170,0			
2290.3	19.263	.65904		Experiment	40	
2172.1	18.102	.65784	2355.6	27.309	.44574	
2061.6	17.013	.65675	2469.1	28.975	.44654	
2001.0	11.010	.00010	2527.9	29.820	.44696	
-	Experiment	36	2414.6	28.214	.44615	
			2309.9	26.695	.44542	
2300.6	26.112	.45493	2263.9	25.998	.44510	
2397.6	27.503	.45563	2228.8	25.491	.44486	

experiment 36) were made over a minimum of one full cycle from the normal boiling point to about  $2550^{\circ}$ F, and equilibrium pressures were generally reproduced in the superheat region to better than  $\pm 0.1$  psi (0.0068 atm) before, during, and after cycling.

Specific Volumes of Saturated Vapor — Specific volumes of several saturated vapor states (Table 3) were observed over the temperature range from 1251° to 2269°F. The measurements were made in the course of the PVT studies, and each point represents an intersection of the saturated and superheated vapor curves for one of the twelve PVT experiments. In the previous experiments with potassium (1) and sodium (2), observed pressures in the temperature region near the intersection of the saturated and superheat curves were always abnormally low. This phenomenon was also observed for cesium and was particularly noticeable in the low-weight, low-pressure experiments. The several factors which may contribute to this lowering phenomenon include the existence of dual states, elevation of the boiling point by nonvolatile impurities, and the retention of condensed alkali metal on the walls of the chamber by adsorption and capillarity effects. These factors are discussed in detail in the potassium report (1).

Table 3
Specific Volume of Saturated Cesium Vapor

Experiment Number	Temperature (°F)	Specific Volume (cu ft/lb)
30	1250.9	8.005
38	1484.3	3.011
28	1588.2	2.086
27	1687.3	1.530
31	1784.8	1.159
32	1789.9	1.146
34	1955.8	0.7515
35	2014.2	0.6561
39	2114.6	0.5275
36	2187.0	0.4542
40	2197.4	0.4448
37	2269.4	0.3869

The saturated specific volume for each PVT experiment was obtained by a short extrapolation of the superheated vapor curve to the true saturation curve as defined by the vapor-pressure equation (Eq. (1)). Although this extrapolation procedure tended to minimize any error in the saturated specific volume resulting from the depression phenomenon, it is believed that specific volumes obtained from the virial equation (Eq. (13)) and the vapor-pressure equation (Eq. (1)) will be of higher reliability than those observed at the intersection points (Table 3). Even so, corresponding values computed from the virial equation show an average deviation of only  $\pm 0.43\%$  from the observed values.

Discussion of Superheat Results - The sources and magnitudes of errors in the PVT measurements are discussed in detail for potassium (1). Many of these were common to the PVT studies of the three alkali metals, and only those which are specific to the cesium work are included here.

Although the procedures developed with potassium and sodium for degassing and closing of null-point apparatuses were very effective, the possibility of inadvertently trapping gas in a chamber still existed. Each cesium apparatus was checked for gas at the

conclusion of an experiment by opening the chamber to an evacuated manometer. Gas pressures as low as 0.01 psi were detectable in this manner, and no gas was detected in any of the twelve cesium chambers.

In previous studies with sodium and potassium, two apparatuses (57 cc and 113 cc) with significantly different surface-to-volume ratios were used for each metal. A comparison for each metal of the compressibility factors measured with the two apparatuses provided evidence that adsorption of the alkali metal on the container surfaces was insignificant. Hence, for cesium the standard 57-cc apparatus was used for all experiments.

The possible significance of any thermal ionization in potassium and sodium vapors is discussed in the compa. on reports (1,2). It was shown that the degree of ionization to be expected in metal vapor may be obtained from its ionization potential (3). A maximum figure of  $10^{-6}$  was estimated for cesium vapor at  $2500^{\circ}F$ ; this leads to the conclusion that the degree of ionization is several magnitudes too low to produce a measurable increase in pressure.

The results of PVT measurements are generally reported in the form of compressibility factors since these, in one form or another, are employed directly in the thermodynamic reduction of data. It is therefore desirable to express experimental error in terms of these factors. If we take into account all known uncertainties, the percent probable error in the observed compressibility factor ranges from  $\pm 0.25$  to  $\pm 0.28$ .

Experimental Saturation Pressures - Saturation pressures of cesium from 1.00 atm at 1236°F to 33.53 atm at 2346°F were measured with two separate PVT apparatuses using in each a large excess of the alkali metal. Redistilled cesium metal from two sources (MSA Research Corporation and Dow Chemical Company) was used for these determinations, and the results are presented in the "Vapor-Pressure Experiments" section of Table 4. Pressures up to 24.7 atm were also measured in the course of twelve PVT experiments and are presented in the second section of the same table. It has been shown that the saturation pressures observed for each experiment near the intersection of the saturation and superheat curves were below corresponding values on the true saturation curve. This lowering of the vapor pressure can be satisfactorily explained (1), and observed pressures in these regions are not included in the table.

The vapor-pressure data in Table 4 are presented graphically in Fig. 1. It is evident from a larger scale plot of this figure that  $\log p$  versus 1/T for cesium is not linear. The data can be effectively fitted for the full temperature range (normal boiling point to 2346°F) with one three-term equation of the Kirchhoff type. Three vapor-pressure equations

$$\log p = 5.87303 - \frac{7040.7}{T} - 0.53290 \log T \tag{1}$$

$$\log p = 5.87275 - \frac{7039.4}{T} - 0.53290 \log T \tag{2}$$

$$\log p = 5.79014 - \frac{7020.7}{T} - 0.51090 \log T \tag{3}$$

for cesium were obtained by least-squares (computer) treatments of the data. Equation (1) was derived from a treatment using all the observed vapor pressures above the normal boiling point, Eq. (2) was derived from the data of the two vapor-pressure experiments in the first section of Table 4, and Eq. (3) was derived from twenty points selected at equal intervals of 1/T from a smoothed plot of  $\log p$  versus 1/T for all the data. The average deviation of all the observed vapor pressures in Table 4 from corresponding values computed with any one of the three equations is  $\pm 0.35\%$ . The three equations are, therefore, equivalent; and the thermodynamic quantities in this report are arbitrarily based on Eq. (1). The normal boiling point as obtained from Eqs. (1) and (3) is  $1236.0^{\circ}F$  ( $668.9^{\circ}C$ ) and from Eq. (2) is  $1235.8^{\circ}F$  ( $668.8^{\circ}C$ ).

Table 4
Saturated Vapor Pressures of Cesium

(°F)         (abs atm)         (°F)         (abs atm)         (°F)         (abs atm)         (°F)         (abs atm)           Vapor-Pressure Experiments           Vapor Pressures from PVT Experiment           (MSA Research Corporation Sample)         1277.0         1.2421         1284.0         1.2672           1238.0         1.0169         2276.1         29.384         1509.5         3.465         1197.4         0.8110           13428.4         2.5054         2169.5         23.632         1322.8         1.5498         1480.4         3.1044           1535.0         3.829         2140.1         22.178         1229.6         0.9662         1619.1         5.234           1618.3         5.179         2067.7         18.833         1214.5         0.8794         1546.9         4.026           1699.8         6.625         2027.3         17.108         1361.1         1.8492         1420.4         2.4223           1785.9         8.918         1943.3         13.885         1495.8         3.2740         1312.5         1.4970           1885.2         11.577         1857.1         11.013         1391.6         2.1516         1264.0         1.1811           1977.8								
(MSA Research Corporation Sample)    1277.0								Pressure (abs atm)
1440.6   2.6328   1449.7   2.7180   1346.6   1.7426   2218.7   26.195   1377.5   1.9968   1342.0   1.7030   1.5122   1.6123   1	Vapor-Pressure Experiments			Vapor P	ressures fro	om PVT E	xperiments	
1238.0	(MSA Research Corporation Sample)		The second secon			1.2672		
1238.0			1		111010	2.0020		
1346.6	1238.0	1.0169	2276.1	29.384	1509.5	3.465		
1428.4         2.5054         2169.5         23.632         1322.8         1.5498         1480.4         3.1044           1535.0         3.829         2140.1         22.178         1229.6         0.9662         1619.1         5.234           1618.3         5.179         2067.7         18.833         1214.5         0.8794         1546.9         4.026           1699.8         6.025         2027.3         17.108         1361.1         1.8492         1420.4         2.4223           1785.9         8.918         1943.3         13.885         1495.8         3.2740         1312.5         1.4970           1885.2         11.857         1857.1         11.013         1391.6         2.1516         1264.0         1.1811           1977.8         15.108         1759.2         8.263         1510.7         3.503         1404.9         2.2671           2100.8         20.264         1677.6         6.354         1606.9         5.000         1547.7         4.045           2183.5         24.276         1588.6         4.672         1447.6         2.7089         1689.7         6.636           2243.1         27.471         1491.5         3.2325         1340.5         1.6879				The second secon				
1535.0								
1618.3         5.179         2067.7         18.833         1214.5         0.8794         1546.9         4.026           1699.8         6.025         2027.3         17.108         1361.1         1.8492         1420.4         2.4223           1785.9         8.918         1943.3         13.885         1495.8         3.2740         1312.5         1.4970           1885.2         11.857         1857.1         11.013         1391.8         2.1516         1264.0         1.1811           1977.8         15.108         1759.2         8.263         1510.7         3.503         1404.9         2.2671           2100.8         20.264         1677.6         6.354         1606.9         5.000         1547.7         4.045           2183.5         24.276         1588.6         4.672         1447.6         2.7089         1689.7         6.636           2243.1         27.471         1491.5         3.2325         1340.5         1.6879         1262.4         1.1450           2345.5         33.530         1318.6         1.5122         1403.3         2.2469         1560.5         4.226           2316.6         31.738         1214.5         0.8849         1553.9         4.135								
1699.8         6.825         2027.3         17.108         1361.1         1.8492         1420.4         2.4223           1785.9         8.918         1943.3         13.885         1495.8         3.2740         1312.5         1.4970           1885.2         11.857         1857.1         11.013         1391.6         2.1516         1264.0         1.1811           1977.8         15.108         1759.2         8.263         1510.7         3.503         1404.9         2.2671           2100.8         20.264         1677.6         6.354         1606.9         5.000         1547.7         4.045           2183.5         24.276         1588.6         4.672         1447.6         2.7089         1689.7         6.636           2243.1         27.471         1491.5         3.2325         1340.5         1.6879         1262.4         1.1450           2291.0         30.241         1440.0         2.6191         1251.9         1.0936         1387.9         2.0987           2345.5         33.530         1318.6         1.5122         1403.3         2.2469         1560.5         4.226           2316.6         31.738         1214.5         0.8849         1553.9         4.135	the second of th							
1785.9       8.918       1943.3       13.885       1495.8       3.2740       1312.5       1.4970         1885.2       11.857       1857.1       11.013       1391.6       2.1516       1264.0       1.1811         1977.8       15.108       1759.2       8.263       1510.7       3.503       1404.9       2.2671         2100.8       20.264       1677.6       6.354       1606.9       5.000       1547.7       4.045         2183.5       24.276       1588.6       4.672       1447.6       2.7089       1689.7       6.636         2243.1       27.471       1491.5       3.2325       1340.5       1.6879       1262.4       1.1450         2291.0       30.241       1440.0       2.6191       1251.9       1.0936       1387.9       2.0987         2345.5       33.530       1318.6       1.5122       1403.3       2.2469       1560.5       4.226         2316.6       31.738       1214.5       0.8849       1553.9       4.135       1685.6       6.532         1688.5       6.607       1827.6       10.072       1822.1       9.998       1747.5       7.947         1353.4       1.7991       2247.2       27.730								COOK LONG TO SELECT
1885.2         11.857         1857.1         11.013         1391.6         2.1516         1264.0         1.1811           1977.8         15.108         1759.2         8.263         1510.7         3.503         1404.9         2.2671           2100.8         20.264         1677.6         6.354         1606.9         5.000         1547.7         4.045           2183.5         24.276         1588.6         4.672         1447.6         2.7089         1689.7         6.636           2243.1         27.471         1491.5         3.2325         1340.5         1.6879         1262.4         1.1450           2291.0         30.241         1440.0         2.6191         1251.9         1.0936         1387.9         2.0987           2345.5         33.530         1318.6         1.5122         1403.3         2.2469         1560.5         4.226           2316.6         31.738         1214.5         0.8849         1553.9         4.135         1685.6         6.532           1688.5         6.607         1827.6         10.072         1822.1         9.998         1747.5         7.947           1974.5         15.034         1642.6         5.654         1436.1         2.5700								
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2291.0   30.241   1440.0   2.6191   1251.9   1.0936   1387.9   2.0987	2243.1	27.471	1491.5	3.2325	1340.5			
2345.5   33.530   1318.6   1.5122   1403.3   2.2469   1560.5   4.226		30.241	1440.0	2.6191	1251.9			2.0987
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(Dow Chemical Company Sample)	2316.6	31.738	1214.5	0.8849	1553.9	4.135		6.532
(Dow Chemical Company Sample)					1688.5	6.607	1827.6	
(Dow Chemical Company Sample)     1285.4     1.2836     1489.5     3.1996       1436.1     2.5700     1363.5     1.8702       1573.6     4.415     1532.3     3.786       1708.0     7.006     1930.4     13.395       1505.6     3.438     2177.2     24.015     1985.7     15.495     1474.3     3.0178					1822.1	9.998		
1436.1     2.5700     1363.5     1.8702       1573.6     4.415     1532.3     3.786       1708.0     7.006     1930.4     13.395       1353.4     1.7991     2247.2     27.730     1852.8     10.844     1755.8     8.158       1505.6     3.438     2177.2     24.015     1985.7     15.495     1474.3     3.0178					1974.5	15.034	1642.6	5.654
1436.1     2.5700     1363.5     1.8702       1573.6     4.415     1532.3     3.786       1708.0     7.006     1930.4     13.395       1353.4     1.7991     2247.2     27.730     1852.8     10.844     1755.8     8.158       1505.6     3.438     2177.2     24.015     1985.7     15.495     1474.3     3.0178	(Dow	Chemical C	Company	Sample)	1285.4	1.2836	1489.5	3.1996
1353.4     1.7991     2247.2     27.730     1852.8     10.844     1755.8     8.158       1505.6     3.438     2177.2     24.015     1985.7     15.495     1474.3     3.0178					1436.1	2.5700	1363.5	1.8702
1353.4     1.7991     2247.2     27.730     1852.8     10.844     1755.8     8.158       1505.6     3.438     2177.2     24.015     1985.7     15.495     1474.3     3.0178					1573.6	4.415	1532.3	3.786
1505.6 3.438 2177.2 24.015 1985.7 15.495 1474.3 3.0178					1708.0	7.006	1930.4	13.395
	1353.4	1.7991	2247.2	27.730	1852.8	10.844	1755.8	8.158
1654.4   5.905   2130.5   21.720   2131.9   21.796   1281.9   1.2674	1505.6	3.438	2177.2	24.015	1985.7	15.495	1474.3	3.0178
	1654.4	5.905	2130.5	21.720	2131.9	21.796	1281.9	1.2674
		9.543	2034.2	17.392	2194.4	24.725	1333.3	1.6746
	1948.3		1888.4	12.039	2080.8	19.346	1465.2	2.9205
	2091.8	19.909	1761.6	8.396		13.164	1480.8	3.1151
	2201.0		1601.8	4.925	1776.1	8.683	1373.5	1.9549
			1431.5	2.5592		5.821	1252.8	1.0887
2287.9   30.071   1245.5   1.0629   1514.5   3.533	2287.9	30.071	1245.5	1.0629	1514.5	3.533		

The current vapor-pressure results are compared to those of three previous investigators in Fig. 2. Vapor pressures of cesium above the normal boiling point have been observed by Achener (4) over the temperature range from 893° to 1600°F, by Tepper et al. (5) over the temperature range from 852° to 1941°F, and by Bonilla et al. (6) over the temperature range from 754° to 1700°F. In Fig. 2 the NRL results have been arbitrarily taken as standard, and the percent deviation of the vapor pressure of each other investigator is plotted as a function of temperature. It is noteworthy that all data show good agreement, the deviation between any two sets being generally accounted for by the combined experimental errors.

A third-law calculation of the heat of vaporization to the monomer (at a temperature of absolute zero) can be made from saturation pressure data with Eq. (4) if other thermal quantities are known.

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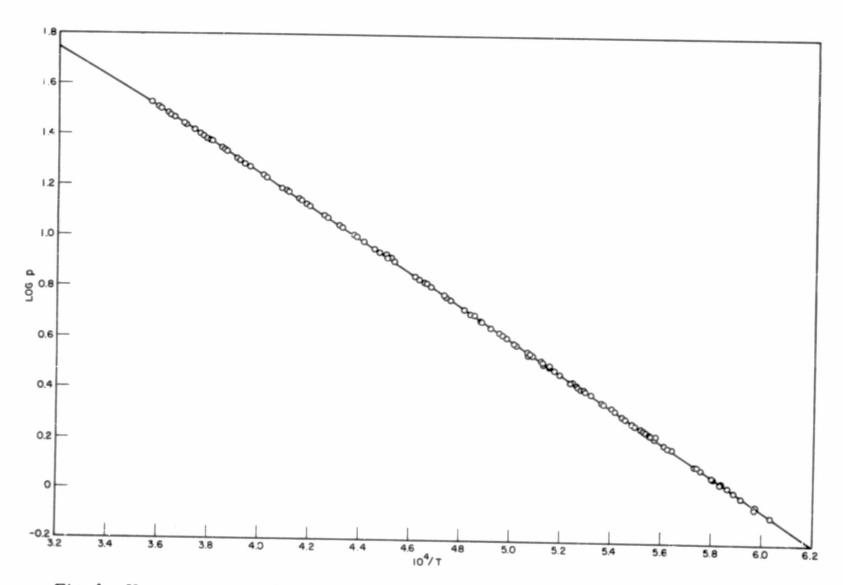


Fig. 1 - Vapor pressure of cesium as a function of the reciprocal absolute temperature

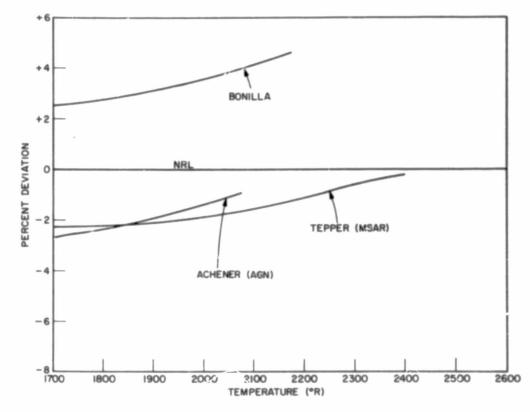


Fig. 2 - Comparison of vapor-pressure data of cesium by several investigators using the NRL data as standard

$$(\Delta h_0^o)_v = -\frac{RT}{M_1} \left( \frac{2B}{\widetilde{V}} + \frac{3C}{2\widetilde{V}^2} + \frac{4D}{3\widetilde{V}^3} + \frac{5E}{4\widetilde{V}^4} + \ln p_s - \ln \frac{p_s\widetilde{V}}{RT} \right) - T \left[ \left( \frac{f^o - h_0^o}{T} \right) \right]_1^g$$
(4)

The virial coefficients for cesium, which appear in the imperfection term, are developed later in this report. The free-energy functions for monomeric cesium gas can be obtained from Evans et al. (7), and corresponding functions for the liquid may be derived from heat-capacity results. Three recent measurements for cesium were found in the literature and pertinent data related to each are summarized in Table 5. It will be noted that there is significant disagreement in the magnitude of the specific heat and the shape of its temperature curve. Since there was no apparent reason to select one set of specific heat data over another, it was decided to base the selection of both  $c_p^l$  and  $(\Delta h_0^o)_v$  on a third-law analysis of the NRL vapor-pressure results. Normally a third-law analysis is used to check the internal consistency of vapor-pressure measurements. In this case, the analysis was used to obtain the most consistent values for the specific heat of the liquid and the vaporization constant.

Table 5
Summary of Heat Capacity Measurements of Liquid Cesium

Investigator and Reference	Temperature Range (°F)	Heat Capacity Equation
Achener (4)	152 to 1656	$c_p^l = 0.08543 - 9.605 \times 10^{-5} t + 5.985 \times 10^{-8} t^2$
Tepper (5)	620 to 1770	$c_p^l = 0.0545$
Lemmon (8)	570 to 2100	$c_p^l = 0.0600$

In two preliminary analyses, the value of  $(\Delta h_0^o)_v$  was computed over the temperature range from 1215° to 2346°F from the vapor-pressure data in Table 4, using in one case a constant liquid heat capacity of 0.0545 and in the other 0.0600 Btu/lb-°F. It will be noted that these are the heat capacities reported by Tepper et al. (5) and Lemmon et al. (8), respectively. (Thermal data at lower temperatures are also required in these analyses, and the data selected are presented in the section entitled "Enthalpy and Entropy of Liquid Cesium.") When the vaporization quantities were plotted against temperature, those computed with a liquid specific-heat value of 0.0600 exhibited a negative slope, and those computed with a value of 0.0545 exhibited a positive slope. It followed that a constant value, intermediate between those chosen, would lead to a nearly constant value of  $(\Delta h_0^0)$ for all saturation results. By a trial and error procedure this value for the specific heat of the liquid was found to be 0.5683 Btu/lb-°F. The vaporization heats (converted to cgs units) computed from this specific-heat value are plotted as a function of temperature in Fig. 3. The value of  $(\Delta h_0^o)$ , obtained by this procedure is 18.62 mean kcal/mole. Although the agreement is perhaps fortuitous, this is practically the same as the value of 18.66 selected by Hultgren et al. (9), which was obtained by a third-law treatment of several vapor-pressure measurements at lower temperatures.

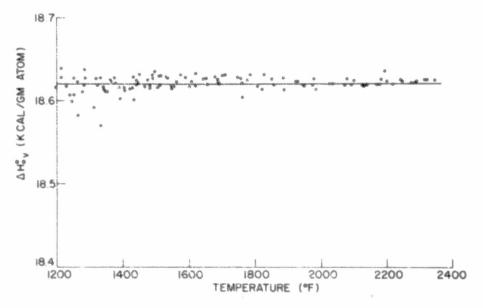
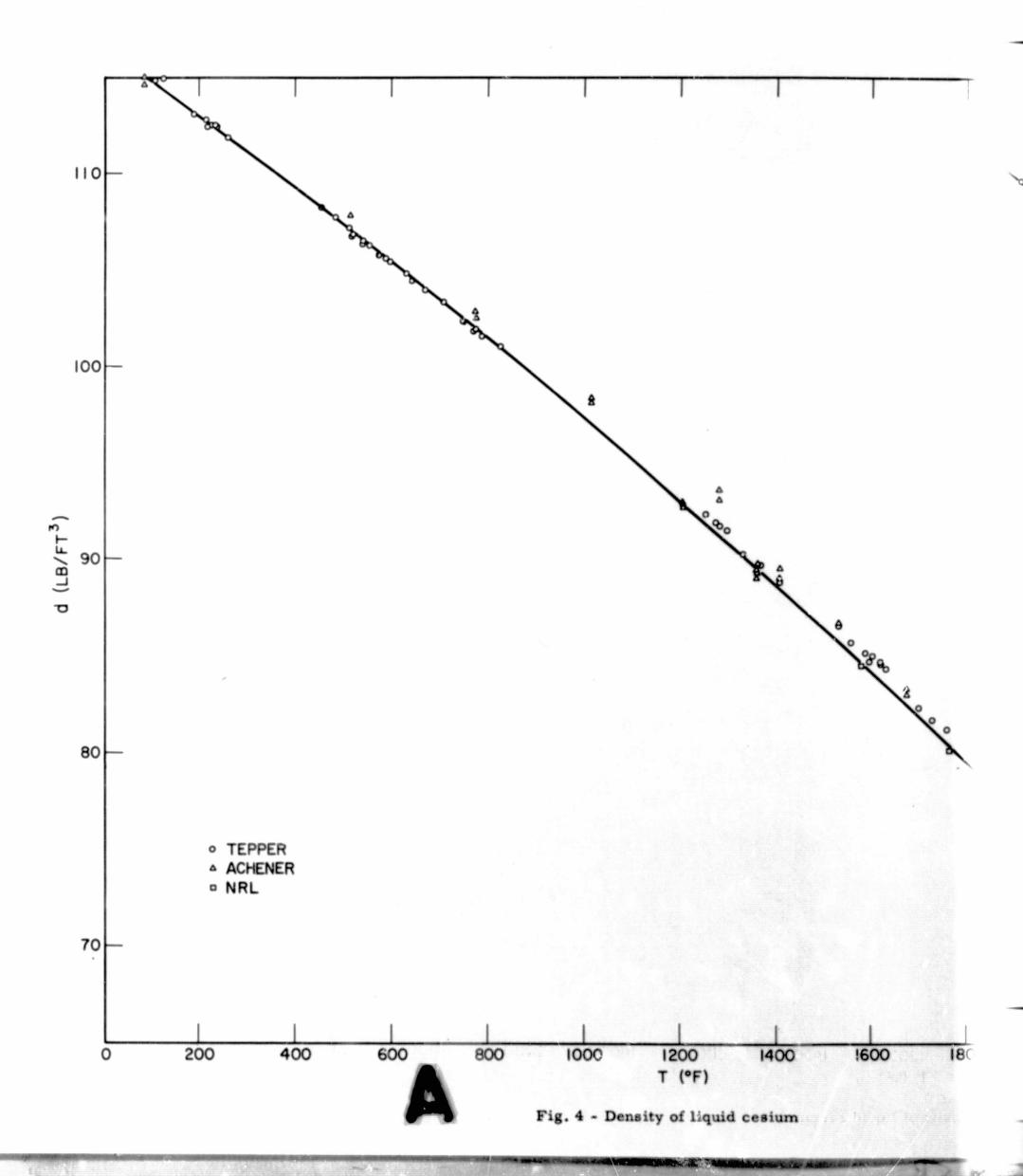


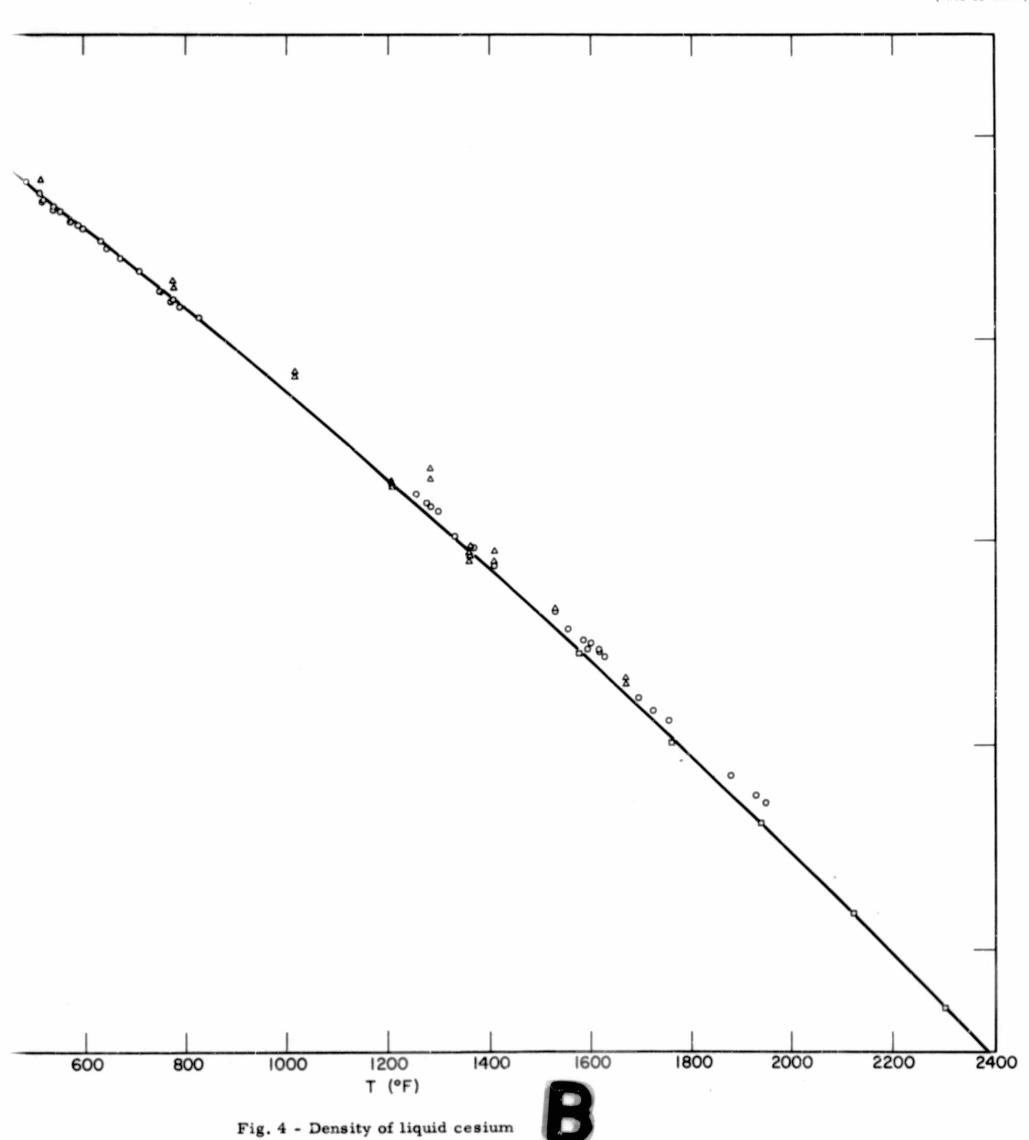
Fig. 3 - Heat of vaporization of monomeric cesium at absolute zero as computed from observed vapor-pressure data

Discussion of Saturation Pressures - Saturation results are presented in Table 4 for cesium samples from two sources, MSA Research Corporation and Dow Chemical Company. Spectrographic analyses of these materials are presented in Table 1. It will be noted that while the impurities differ considerably both as to type and magnitude, the vapor pressures observed are in good agreement. The average deviation of Eq. (1) from the data for the MSAR metal is  $\pm 0.25\%$  and for the Dow metal is  $\pm 0.32\%$ . This agreement confirms that the two samples are effectively equivalent and that the impurities present do not significantly affect the reported vapor pressures.

The measurement of saturation pressures directly with a diaphragm detector is new to the high-temperature field. The relative merits of the apparatus and the uncertainties to be expected in the various measurement parameters were discussed in the potassium report (1). If all known sources of error in the saturation measurements are considered, the probable error in the reported vapor pressure for cesium at 1 atm is  $\pm 0.67\%$  and at 34 atm is  $\pm 0.49\%$ .







#### Density Measurements of Liquid Cesium

The density of liquid cesium was determined with columbium-1%zirconium pycnometers of 30 cc nominal volume by the method described for potassium (1). Measured densities over the temperature range from 1577.0° to 2303.8°F are reported in Table 6 and presented graphically in Fig. 4 along with those of two other investigators. The uncertainties

to be expected in the various parameters of the NRL density measurements are discussed in the potassium report (1). If all known sources are taken into account, the probable error of the reported densities range from  $\pm 0.25\%$  at  $1577\,^{\circ}\text{F}$  to  $\pm 0.30\%$  at  $2304\,^{\circ}\text{F}$ .

The recommended density equation for liquid cesium from the melting point to 2300°F is

$$d^{l} = 124.181 - 1.5970 \times 10^{-2} T - 1.6855 \times 10^{-6} T^{2}.$$
 (5)

This equation was derived by fitting the best curve to the density determinations of Achener (4), Tepper et al. (5), and NRL (Table 6). These three independent sets of measurements are summarized in Table 7. For each investigation, the temperature range, the general method, and the average deviation of the observed densities from

Table 6
Density of Liquid Cesium

Temperature (°F)	Density (lb/cu ft)
1577.0	84.563
1762.2	80.209
1939.9	76.267
2122.5	71.845
2303.8	67.189

those calculated with Eq. (5) are presented. The three sets of measurements show fair internal consistency over the full temperature range, and it is believed that Eq. (5) will give density values which are accurate to  $\pm 0.6\%$  between the melting point and 2300°F.

Table 7
Summary of Density Measurements

Investigator	Method	Temp. Range (°F)	% Average Deviation  Obs Calc. (Eq. (5))  Calc.
Achener	Dilatometric (pycnometers)	(83 to 1671)	±0.70
Tepper	Dilatometric	(105 to 1950)	±0.35
NRL	Dilatometric (pycnometers)	(1577 to 2304)	±0.14

#### SUMMARY OF FUNDAMENTAL PROPERTIES USED IN THE THERMODYNAMIC TREATMENTS

Density of Liquid Cesium

The density of the condensed phase was required to compute the enthalpy of vaporization from the Clapeyron equation and was obtained from Eq. (5).

Enthalpy and Entropy of Monomeric Cesium Vapor

The monomeric gas properties, together with the values selected for the enthalpy of sublimation, largely determine the absolute accuracy of the superheat properties tabulated in Appendixes A and B. The equations for the enthalpy and entropy of the gas were derived directly from the work of Evans et al. (7) and are based on their standard properties over the temperature range from 0° to 3100°F and on the enthalpy of vaporization to 0°R (18.62 mean kcal/mole) as derived in this report. The equations for the monomeric gas at 1 atm (relative to the solid crystal at 0°R) are

$$(h^g)^o = 252.18 + 0.037361 T + 2480 e^{-31,290/T}$$
 (6)

$$(s^g)^o = 0.037361 \ln T + 0.080604 + 0.371 e^{-28,598/T}$$
 (7)

Specific Heat at Constant Pressure of Monomeric Cesium Vapor

The specific heat of monomeric cesium vapor at constant pressure largely determines the absolute accuracy of the values reported for the specific heat of the equilibrium vapor in Appendix B. The equation for the specific heat of the monomeric gas was derived from the work of Evans et al. (7) and is based on their computed properties over the temperature range from 0° to 2800°F. The relation for the monomeric gas at 1 atm is

$$(c_p^g)^o = 0.037361 + 1.3099 e^{-25,663/T}$$
 (8)

Enthalpy and Entropy of Liquid Cesium

The tabulated thermodynamic properties in this report are based on the properties of the monomeric gas at 1 atm, but comparison calculations were made using the properties of the saturated liquid as a starting point. The absolute properties of the liquid (relative to the solid at 0°R) were computed with

$$h_s^l = -2.6969 + 0.05683 T (9)$$

 $T > 1030 \,{}^{\circ}\,R$ 

$$s_s^l = 0.05683 \ln T - 0.19387.$$
 (10)

T > 1030°R

In order to obtain these equations, a knowledge of the specific heat of the liquid was required. In a previous section of this report, a constant value of 0.05683 Btu/lb-°F was shown to give the greatest degree of internal consistency in third-law calculations. A constant value has also been reported in two recent measurements; Tepper et al. (5) reported a value of 0.0546, and Lemmon et al. (8) reported 0.0600. The third-law value of 0.05683 is intermediate between the two published values and was used in deriving Eqs. (9) and (10).

These two equations are based on the absolute properties of solid cesium at 77.0°F by Hultgren et al. (9). Although only a short solidus region remains above this temperature, the change in the properties for this region and the required enthalpy of fusion were taken from the work of Lemmon et al. (8). There is an anomaly (5,8) in the heat-content

curve of the liquid in the temperature range to 570°F. The enthalpy change for Eq. (9) in this region was obtained from Lemmon (8). On the other hand, the entropy equation ignores the anomaly in heat content and was derived by assuming the specific heat of the liquid to be constant for the whole liquid range.

Saturation Pressure of Liquid Cesium

Three equivalent vapor-pressure equations (Eqs. (1), (2), and (3)) were derived from least-squares correlations. All thermodynamic quantities in this report are arbitrarily based on Eq. (1).

Enthalpy and Entropy of Vaporization of Cesium

Heats of vaporization were calculated with

$$\Delta h_v = Jp_s \left[ \frac{16,211.8}{T} - 0.53290 \right] (v_s^g - v_s^l)$$
 (11)

which was derived by a differentiation of Eq. (1) and subsequent substitution into the Clapeyron equation. A value of  $v_s^l$  at each temperature was obtained from Eq. (5) and a value of  $v_s^g$  from the virial equation of state (Eq. (13)).

The heats of vaporization so obtained from the Clapeyron equation are presented graphically in Fig. 5 and are compared with values reported by Achener (4). The four results by Achener were measured directly by noting the heat required to vaporize a given mass of the liquid. The agreement is good; three of Achener's points are within 1% of the corresponding NRL values and the fourth is within 3% of the NRL value.

The entropy of vaporization at each saturation point was obtained by dividing the appropriate enthalpy change by the absolute temperature.

#### THERMODYNAMIC TREATMENT OF PVT AND ASSOCIATED PROPERTIES

The imperfections which occur in the alkali metal vapors and the various treatments of these imperfections in the reduction of PVT data are discussed at some length in the companion reports (1,2). Quasi-chemical analyses of the PVT data for sodium and potassium have shown that dimeric and, perhaps, tetrameric molecules are present in the metal vapors. From a similar analysis of the cesium system, which is discussed later in this report, it is believed that the major imperfection in cesium also stems from the existence of higher-molecular-weight species.

For a strongly associating gas the important properties (enthalpy, entropy, and specific heat) may be reduced from PVT data by the use of either of two methods, the virial or the quasi-chemical. The two methods were shown for sodium and potassium to be effectively equivalent, so only the virial method was used in the reduction of the cesium data. The virial equation of state for cesium with coefficients through the fifth virial was obtained from raw PVT data and used to compute enthalpies, entropies, specific volumes, and specific heats of the vapor.

The thermodynamic properties of cesium by the virial method were computed along constant temperature lines. The starting point for a particular property could have been

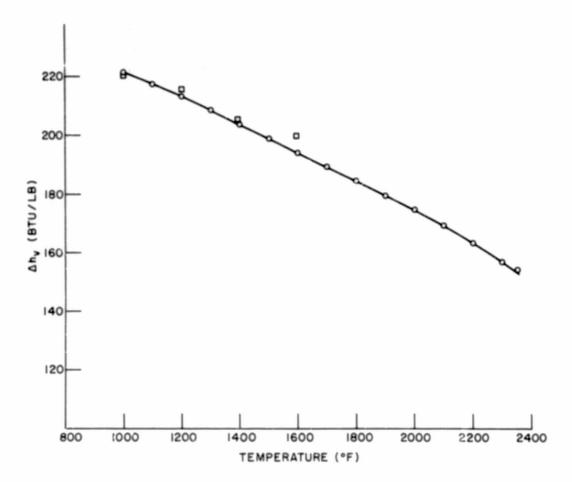


Fig. 5 - Enthalpy of vaporization of cesium 

Achener, ONRL

the absolute value of that property for either the saturated liquid or the monomeric gas. Therefore, two computational paths exist for obtaining each absolute property in the superheat region. The properties were computed along both paths, and the results are compared in this report.

### Virial Coefficients of Cesium

The virial equation of state in its volume expansion form,

$$\frac{p\widetilde{V}}{RT} = 1 + \frac{B}{\widetilde{V}} + \frac{C}{\widetilde{V}^2} + \frac{D}{\widetilde{V}^3} + \frac{E}{\widetilde{V}^4} + \dots$$
 (12)

was chosen for the analyses of all three alkali metal systems.

The PVT data for cesium were more precise than those obtained for either sodium or potassium, and the adjustment procedure (1,2) used to facilitate the graphical reduction of the sodium and potassium tata was not required. The coefficients, however, were still derived graphically from the PVT data by plotting functions along constant temperature lines. As a first step,  $(z-1)\tilde{V}$  was plotted as a function of  $1/\tilde{V}$  for isotherms at 50-degree intervals between  $2050^\circ$  and  $2550^\circ$ F, and preliminary second virial coefficients were obtained as the  $\lim_{z\to 0} (z-1)\tilde{V}$  as  $1/\tilde{V}\to 0$ . The final coefficient at each temperature was obtained by adjusting the preliminary value to give the best internal consistency between the low- and high-pressure results as determined from a plot of  $[(z-1)\tilde{V}-B]\tilde{V}$  versus  $1/\tilde{V}$ . A final plot of  $(z-1)\tilde{V}$  versus  $1/\tilde{V}$  is illustrated in Fig. 6 for the isotherm at  $2400^\circ$ F. In the intermediate temperature range from  $1600^\circ$  to  $2050^\circ$ F, final second virial coefficients were taken as the  $\lim_{z\to 0} (z-1)\tilde{V}$  as  $1/\tilde{V}\to 0$ . The coefficients for the full measured range from  $1550^\circ$  to  $2550^\circ$ F may be represented by a simple exponential relationship (Eq. (13)).

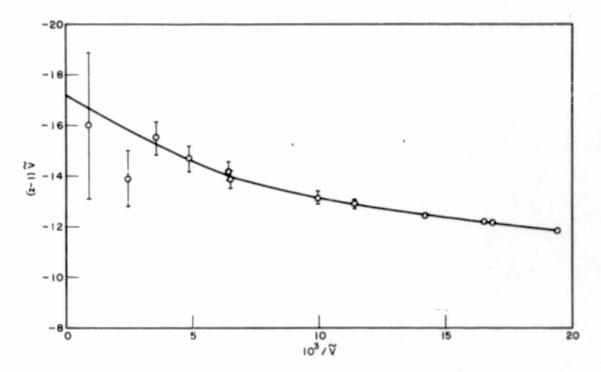


Fig. 6 - Plot of  $(s - 1)\tilde{V}$  versus  $1/\tilde{V}$  for cesium at 2400 °F (vertical line for each point represents probable error)

From a preliminary analysis in which third and fourth virial coefficients were derived in the temperature range from 2050° to 2550°F, it was apparent that a fifth virial would be required to precisely fit all the data along any given isotherm. Only a rough value of this higher virial was required, and this was obtained mathematically. With preliminary values for the third virial,  $\{[(z-1)\widetilde{V}-B]\widetilde{V}^2-C\widetilde{V}\}$  was plotted versus  $1/\widetilde{V}$  for several higher temperature isotherms, and the value of 600,000 for E was selected from the average apparent slope of the curves at higher pressures.

Final third and fourth virial coefficients in the same temperature range between 2050° and 2550°F were obtained by plotting the revised quantity  $\{[(z-1)\widetilde{V}-B]\widetilde{V}-E/\widetilde{V}^2\}$  versus  $1/\widetilde{V}$  for isotherms at 50-degree intervals. This is illustrated in Fig. 7 for the isotherm at 2400°F. From the best linear curve for each isotherm the third virial was obtained as the intercept and the fourth as the slope. The fourth virial coefficient may be represented for the full temperature range as a simple first-degree exponential equation in 1/T (Eq. (13)). Additional third virial coefficients were obtained in the intermediate temperature range from 1550° to 2050°F by computing the average value of  $\{[(z-1)\widetilde{V}-B]\widetilde{V}-D/\widetilde{V}-E/\widetilde{V}^2\}$  for the higher pressure points on each isotherm. The third virial coefficient for the full range from 1550° to 2550°F may be represented by a second-degree exponential equation (Eq. (13)).

Experimental PVT data were also obtained in a lower temperature range between 1550° and 1275°F, but the number of experimental points along an isotherm was insufficient to permit one to obtain reliable virial coefficients by the graphical method. Consequently, before the virial equation of state for cesium was acceptable for calculations below 1550°F, it was necessary to determine its fit to the observed lower temperature data. At temperatures and pressures corresponding to the observed low-temperature states, compressibility factors were calculated and compared to the observed values. The fit of the virial equation of state to the lower temperature data was found to be equivalent to that obtained at higher temperatures.

#### Virial Equation of State of Cesium

2)

The virial equation of state of cesium with coefficients through the fifth virial is

$$\frac{p\widetilde{V}}{RT} = 1 + \frac{B}{\widetilde{V}} + \frac{C}{\widetilde{V}^2} + \frac{D}{\widetilde{V}^3} + \frac{E}{\widetilde{V}^4} + \dots$$
 (13)

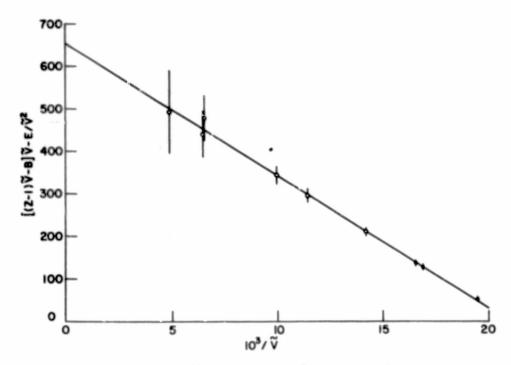


Fig. 7 - Plot of  $\{[(s-1)\widetilde{V}-B]\widetilde{V}-E/\widetilde{V}^2\}$  versus  $1/\widetilde{V}$  for cesium at 2400°F (vertical line for each point represents probable error)

where

$$\log |B| = -3.6200 + 4000.0/T + \log T$$

$$B < 0$$

$$\log C = 3.3551 - 5331.5/T + 10.825 \times 10^6/T^2$$

$$C > 0$$

$$\log |D| = 4.1856 + 880/T$$

$$D < 0$$

E = +600,000.

The degree to which the virial equation was fitted to the measured data is shown graphically in Fig. 8, where compressibility isotherms generated with Eq. (13) are compared to experimental compressibilities at 100-degree intervals from  $1350^{\circ}$  to  $2550^{\circ}$  F. The degree of fit can also be shown mathematically. For example, all the observed specific-volume data in Table 2 (or compressibility factors derived from that data) may be calculated from the virial equation with an average deviation of only  $\pm 0.15\%$ . It is significant that this deviation is of a magnitude predicted by random and systematic errors in the null-point measurements.

## Thermodynamic Properties of Cesium by the Virial Method (Monomeric Gas Path)

Expressions for the thermodynamic properties in terms of the second and third virial coefficients were derived by Hirschfelder et al. (10). By the same method, similar equations were derived to include the fourth and fifth virial coefficients. These equations which were used to compute the thermodynamic properties of cesium vapor (Appendixes A and B) are presented below.

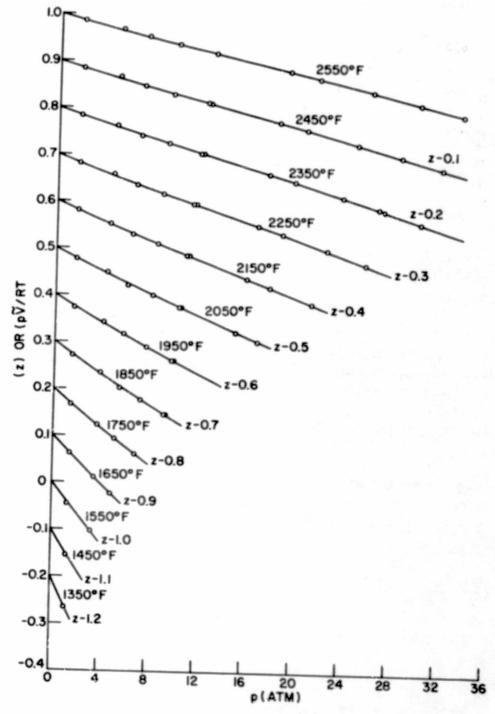


Fig. 8 - Compressibility of cesium vapor at several temperatures

Enthalpy, Entropy, and Specific Heat of Saturated and Superheated Vapor - These properties at all vapor states were computed along isotherms using the following equations:

$$h_{i}^{g} = (h^{g})^{o} + \frac{RT}{M_{1}} \left\{ \frac{1}{\widetilde{v}} \left[ B - T \left( \frac{dB}{dT} \right) \right] + \frac{1}{\widetilde{v}^{2}} \left[ C - \frac{T}{2} \left( \frac{dC}{dT} \right) \right] + \frac{1}{\widetilde{v}^{3}} \left[ D - \frac{T}{3} \left( \frac{dD}{dT} \right) \right] + \frac{1}{\widetilde{v}^{4}} \left[ E - \frac{T}{4} \left( \frac{dE}{dT} \right) \right] \right\}$$

$$(14)$$

$$s_{i}^{g} = (s^{g})^{o} - \frac{R}{M_{1}} \left\{ \ln p - \ln \frac{p\widetilde{V}}{RT} + \frac{B}{\widetilde{V}} + \frac{T}{\widetilde{V}} \left( \frac{dE}{dT} \right) + \frac{C}{2\widetilde{V}^{2}} + \frac{T}{2\widetilde{V}^{2}} \left( \frac{dC}{dT} \right) + \frac{D}{3\widetilde{V}^{3}} + \frac{T}{3\widetilde{V}^{3}} \left( \frac{dD}{dT} \right) + \frac{E}{4\widetilde{V}^{4}} + \frac{T}{4\widetilde{V}^{4}} \left( \frac{dE}{dT} \right) \right\}$$
 (15)

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$$\begin{aligned} \left(c_{p}^{g}\right)_{i} &= \left(c_{p}^{g}\right)^{o} - \frac{R}{\mathit{M}_{1}} + \frac{R}{\mathit{M}_{1}} \left\{ \frac{\left[1 + \frac{1}{\widetilde{\mathcal{V}}}\left(B + T\frac{dB}{dT}\right) + \frac{1}{\widetilde{\mathcal{V}}^{2}}\left(C + T\frac{dC}{dT}\right) + \frac{1}{\widetilde{\mathcal{V}}^{3}}\left(D + T\frac{dD}{dT}\right) + \frac{1}{\widetilde{\mathcal{V}}^{4}}\left(E + T\frac{dE}{dT}\right)\right]^{2}}{\left[1 + 2\frac{B}{\widetilde{\mathcal{V}}} + 3\frac{C}{\widetilde{\mathcal{V}}^{2}} + 4\frac{D}{\widetilde{\mathcal{V}}^{3}} + 5\frac{E}{\widetilde{\mathcal{V}}^{4}}\right]} \end{aligned} \right\}$$

$$-\frac{RT}{\widetilde{V}M_{1}}\left\{\left(T\frac{d^{2}B}{dT^{2}}+2\frac{dB}{dT}\right)+\frac{1}{2\widetilde{V}}\left(T\frac{d^{2}C}{dT^{2}}+2\frac{dC}{dT}\right)+\frac{1}{3\widetilde{V}^{2}}\left(T\frac{d^{2}D}{dT^{2}}+2\frac{dD}{dT}\right)+\frac{1}{4\widetilde{V}^{3}}\left(T\frac{d^{2}E}{dT^{2}}+2\frac{dE}{dT}\right)\right\}.$$
 (16)

Specific Volume of Saturated and Superheated Vapor - This property at all the vapor states in Appendixes A and B was computed from the virial equation of state (Eq. (13)) by a trial and error solution.

Enthalpy and Entropy of the Condensed Phase - These properties of the saturated liquid (Appendix A) at each temperature were obtained by subtracting the enthalpy or entropy of vaporization from the corresponding properties of the saturated vapor.

Thermodynamic Properties of Cesium by the Virial Method (Liquid Path)

Expressions for the thermodynamic quantities with the properties of the condensed liquid as a base were derived directly from those in the preceding section. These new equations together with a procedural outline of the methods of calculation are presented below.

Enthalpy, Entropy, and Specific Heat of the Saturated Vapor - The enthalpy or entropy of the saturated vapor at a given temperature was obtained by adding the enthalpy or entropy of vaporization to the corresponding property of the saturated liquid. The specific heat at saturation was obtained by numerically evaluating at 50-degree intervals the differential

$$(c_p^g)_s = \left[ \left( \frac{\partial h}{\partial T} \right)_p^g \right]_s = \left[ \left( \frac{\Delta h}{\Delta T} \right)_p^g \right]_s.$$
 (17)

Enthalpy, Entropy, and Specific Heat of Superheated Vapor - These properties in the superheat region were computed along constant temperature lines with each saturation state as a starting point. The general equations in virial form are

$$h_{i}^{g} = h_{s}^{g} - \frac{RT}{M_{1}} \left[ \frac{1}{\widetilde{V}} \left( B - \frac{TdB}{dT} \right) + \frac{1}{\widetilde{V}^{2}} \left( C - \frac{TdC}{2dT} \right) + \frac{1}{\widetilde{V}^{3}} \left( D - \frac{TdD}{3dT} \right) + \frac{1}{\widetilde{V}^{4}} \left( E - \frac{TdE}{4dT} \right) \right]_{\widetilde{V}_{s}}^{\widetilde{V}_{s}}$$
(18)

$$s_{i}^{g} = s_{s}^{g} + \frac{R}{M_{1}} \left[ \ln p - \ln \frac{p\widetilde{V}}{RT} + \frac{B}{\widetilde{V}} + \frac{TdB}{\widetilde{V}dT} + \frac{C}{2\widetilde{V}^{2}} + \frac{T}{2\widetilde{V}^{2}} \frac{dC}{dT} + \frac{D}{3\widetilde{V}^{3}} + \frac{T}{3\widetilde{V}^{3}} \frac{dD}{dT} + \frac{E}{4\widetilde{V}^{4}} + \frac{T}{4\widetilde{V}^{4}} \frac{dE}{dT} \right]_{\widetilde{V}_{i}}^{\widetilde{V}_{s}}$$
(19)

$$(c_{p}^{g})_{i} = (c_{p}^{g})_{s} - \frac{R}{M_{1}} \left[ \frac{\left\{ 1 + \frac{1}{\widetilde{V}} \left( B + T \frac{dB}{dT} \right) + \frac{1}{\widetilde{V}^{2}} \left( C + T \frac{dC}{dT} \right) + \frac{1}{\widetilde{V}^{3}} \left( D + T \frac{dD}{dT} \right) + \frac{1}{\widetilde{V}^{4}} \left( E + T \frac{dE}{dT} \right) \right\}^{\widetilde{V}_{s}}}{\left\{ 1 + \frac{2B}{\widetilde{V}} + \frac{3C}{\widetilde{V}^{2}} + \frac{4D}{\widetilde{V}^{3}} + \frac{5E}{\widetilde{V}^{4}} \right\}}$$

$$+ \frac{RT}{\widetilde{V}M_{1}} \left[ \left( T \frac{d^{2}B}{dT^{2}} + 2 \frac{dB}{dT} \right) + \frac{1}{2\widetilde{V}} \left( T \frac{d^{2}C}{dT^{2}} + 2 \frac{dC}{dT} \right) + \frac{1}{3\widetilde{V}^{2}} \left( T \frac{d^{2}D}{dT^{2}} + 2 \frac{dD}{dT} \right) + \frac{1}{4\widetilde{V}^{3}} \left( T \frac{d^{2}E}{dT^{2}} + 2 \frac{dE}{dT} \right) \right]^{\widetilde{V}_{s}}_{\widetilde{V}_{s}}.$$
 (20)

## A Comparison of the Monomeric Gas Path and the Liquid Path for Thermodynamic Calculations

The thermodynamic properties of cesium were computed along constant temperature lines. The starting point for a particular property could have been the absolute value of that property for either the saturated liquid or the monomeric gas at 1 atm. The three properties (enthalpy, entropy, and specific heat) of the superheated vapor were computed by both paths, and values at selected states are compared in Table 8. In the temperature range from 1250° to 2350°F, absolute enthalpies in the superheat region, based on enthalpies of the saturated liquid, were 0.2 to 6.9 Btu/lb (approximately 0.1 to 2.0%) lower than corresponding values based on the monomeric gas enthalpies. Likewise, entropies by the liquid path were 0 to 0.0025 Btu/lb-°F (approximately 0 to 0.8%) lower, and specific heats differed by 5.3 to 31%.

The small divergence of the absolute enthalpies (Table 8) as computed along the two paths over the temperature range from 1250° to 2050°F suggests that the selected value of either the specific heat of the liquid or its temperature coefficient is slightly in error. It will also be noted that the enthalpy of the superheated vapor at a given pressure, if computed from the liquid base, exhibits an abnormal change in slope at temperatures above 2100°F. This is reflected in the specific heat values which at 2250°F are 16 to 31% lower and at 2350°F are 7 to 15% higher than those computed by the monomeric gas path. Part of this apparent error at higher temperatures in the enthalpy as computed along the liquid path may have resulted from errors in various quantities along the two computational paths. It is believed that a large part must also be attributed either to errors in the enthalpy of vaporization resulting from small inconsistencies in the virial equation of state or to error generated by the rather arbitrary selection and extrapolation of the liquid specific heat.

Engineering design calculations put prime emphasis on the change in enthalpy or entropy when moving from one state to another rather than on their absolute values; therefore, the choice of path is of minor importance for both these properties. However, the specific heat of the vapor would be expected to be more accurate if computed from the monomeric gas, since this path is independent of vaporization quantities and does not require a knowledge of the specific heat of the liquid. Therefore, the monomeric gas path has been chosen to compute all the tabular properties in this report.

#### DISCUSSION OF QUASI-CHEMICAL EQUATION OF STATE AND THE COMPOSITION OF CESIUM VAPOR

The PVT results for sodium and potassium were satisfactorily interpreted by a quasi-chemical approach based on the assumption that each metal vapor is an ideal mixture of monomeric, dimeric, and tetrameric species. Although this model of the physical

Table 8
Comparison of Monomeric Gas and Liquid Path Calculations

Temp.	Pressure	Monor	Monomeric Gas Path Liquid			iquid Pa	Path		
(°F)	(atm)	h <sup>g</sup>	89	¢g p	$h^g$	89	cg p		
1250	1.0	306.4	0.3541	0.0653	306.2	0.3540	0.0619		
	0.2	314.1	0.3818	0.0435	313.9	0.3817	0.0400		
1450	2.0	312.4	0.3479	0.0645	311.4	0.3473	0.0602		
	1.0	317.9	0.3605	0.0514	316.9	0.3600	0.0471		
	0.2	322.4	0.3864	0.0402	321.4	0.3859	0.0360		
1650	5.0	313.5	0.3361	0.0719	311.7	0.3353	0.0685		
	1.0	327.4	0.3653	0.0447	325.6	0.3644	0.0413		
	0.2	330.3	0.3904	0.0388	328.5	0.3895	0.0354		
1850	10.0	315.0	0.3280	0.0748	312.5	0.3268	0.0707		
	5.0	326.4	0.3420	0.0582	323.9	0.3409	0.0541		
	1.0	336.0	0.3692	0.0416	333.6	0.3681	0.0375		
	0.2	338.0	0.3939	0.0382	335.5	0.3928	0.0342		
2030	18.0	315.9	0.3212	0.0756	312.2	0.3196	0.0657		
	15.0	320.6	0.3252	0.0718	316.8	0.3237	0.0619		
	10.0	328.7	0.3336	0.0623	324.9	0.3321	0.0524		
	5.0	337.2	0.3465	0.0503	333.4	0.3449	0.0404		
	1.0	344.2	0.3726	0.0400	340.4	0.3710	0.0301		
	0.2	345.6	0.3970	0.0379	341.8	0.3955	0.0280		
2250	25.0	321.2	0.3193	0.0742	314.9	0.3170	0.0625		
	20.0	327.6	0.3244	0.0684	321.3	0.3220	0.0567		
	15.0	333.9	0.3303	0.0616	327.6	0.3280	0.0500		
	10.0	340.2	0.3381	0.0541	333.9	0.3357	0.0424		
	5.0	346.8	0.3501	0.0459	340.4	0.3478	0.0343		
	1.0	352.1	0.3756	0.0392	345.8	0.3732	0.0275		
	0.2	353.2	0.3999	0.0378	346.9	0.3976	0.0261		
2350	33.0	318.9	0.3153	0.0768	312.0	0.3129	0.0824		
	25.0	323.4	0.3219	0.0697	321.6	0.3196	0.0753		
	20.0	334.2	0.3268	0.0638	327.4	0.3243	0.0694		
	15.0	339.8	0.3325	0.0577	333.0	0.3300	0.0632		
	10.0	345.5	0.3400	0.0512	338.7	0.3375	0.0568		
	5.0	351.3	0.3518	0.0445	344.5	0.3493	0.0500		
	1.0	356.0	0.3770	0.0389	349.2	0.3746	0.0445		
	0.2	357.0	0.4013	0.0378	350.1	0.3988	0.0433		

state of the vapor was believed to be the most probable, other models including several imperfect mixtures of two or more molecular species were shown to be equally effective in comparable quasi-chemical treatments. It was concluded from this study of molecular models (2) that all close-approach imperfections may be properly treated from a thermodynamic standpoint as either interactions of the van der Waals type or as molecular associations. It then follows that the molecular species present in a particular metal vapor cannot be positively identified from an analysis of its PVT data. Even so, a quasi-chemical study of the cesium PVT data was made in the hope that this analysis, combined with those previously made for sodium and potassium, would provide some evidence as to the actual molecular state of an alkali metal vapor.

For the quasi-chemical analysis of an alkali metal vapor, the association of the vapor into ideal molecular compounds can be represented by a series of independent equilibria of the type,  $n \ X_1 = X_n$ . For such a system, the apparent equilibrium constant of dimerization  $k_2'$  (when all association is taken to be dimerization), can be expressed as a power series (11)

$$k_2' = k_2 + 2k_3p + 3k_4p^2 + 2k_3^2p^3 - 2k_2k_4p^3 + \dots$$
 (21)

in terms of the pressure and the true equilibrium constants of the association reactions. The apparent dimerization constants at any given temperature may be readily computed from the raw PVT data, and the relationship of these apparent constants to pressure may be used to predict the compounds present in the vapor.

The apparent dimerization constant  $k_2$  for cesium was computed for each experimental point at a temperature of  $2400^{\circ}$ F, and these apparent constants are shown plotted against  $p^2$  in Fig. 9. Similar plots for the sodium and potassium systems were effectively linear and predicted the existence of the tetramer as the higher-molecular-weight species. It will be noted that cesium appears to require an even higher degree of imperfection to satisfy the quasi-chemical picture. This additional imperfection may be in the form of associations higher than the tetramer or in gas imperfections of the interaction type. In any event, a vapor model involving a perfect mixture of monomeric, dimeric, and tetrameric species is not satisfactory for cesium.

It has been mentioned that in the companion reports (1,2) several molecular models provided satisfactory quasi-chemical fits to the PVT data for the sodium and potassium systems. The principal model tested, other than the perfect mixture of monomeric, dimeric, and tetrameric species, was an imperfect mixture of monomeric and dimeric species. The cesium results were likewise analyzed with this model. A simplified van der Waals equation was again chosen to treat the gas imperfections (interactions not

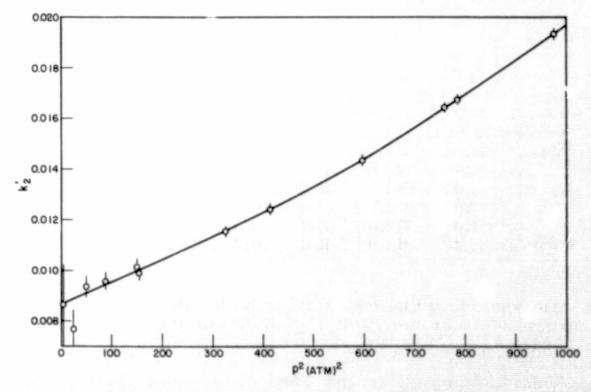


Fig. 9 - Plot of  $k_2'$  versus  $p^2$  for cesium at 2400°F (vertical line for each point represents probable error)

leading to stable molecules). This van der Waals relationship

$$\left(p + \frac{\widetilde{a}_1}{\widetilde{V}^2}\right) \left(\widetilde{V} - \widetilde{b}_1\right) = \frac{M_1 R T}{M_a}$$
 (22)

was developed by Vukalovich et al. (12) for an associating gas. For this equation the excluded volume coefficient  $\widetilde{b}_1$  was reliably estimated (1) from the condensed volume of the vapor, but the pressure coefficient  $\widetilde{a}_1$  had to be obtained empirically. This latter coefficient was assumed to be constant and was evaluated by selecting a value for which the corresponding dimerization constants were independent of pressure along isotherms for the full temperature range. The object was to see whether or not this physical picture of the vapor would correlate with the PVT results, and no attempt was made to determine exact equational fits. It was shown, however, that an effective equation of state could be obtained in terms of Eq. (22) and the relationship  $k_2 = A + B/T$  for the corresponding dimerization reaction.

A direct implication of this analysis is that other physical models of the vapor, including an imperfect mixture of monomeric, dimeric, and tetrameric species, would also satisfy the cesium PVT data. It is believed that any one of these quasi-chemical equations of state, if it had been developed, would have been equivalent to the virial form and could also have been used to derive the thermodynamic properties of the vapor. Quasi-chemical equations are more satisfactory for extrapolation of the thermodynamic quantities beyond the measured range of the PVT data. If an extrapolation of the cesium data becomes important in the future, a second equation of state will be developed.

This study, unfortunately, gives no definitive insight into the composition of cesium vapor. The magnitudes of the pressure coefficients in the van der Waals equation, which are required to correlate the data if one assumes either an imprefect mixture of monomeric and dimeric species, or an imperfect mixture of monomeric, dimeric, and trimeric species, do appear to be high. This suggests that the correct model is either an imperfect mixture of monomeric, dimeric, and tetrameric species or a similar mixture of near perfect gases with a fourth species of molecular weight higher than the tetramer.

Equilibrium Constants of the Dimerization Reaction in Cesium Vapor - Although the higher-molecular-weight reactions in cesium vapor could not be identified, it was still possible to obtain reliable dimerization constants. These were obtained by plotting  $k_2'$  versus  $p^2$  for isotherms at 50-degree intervals from 1750° to 2550°F and taking the  $\lim_{k_2'} k_2'$  for each isotherm as  $p^2 - 0$ . This procedure is illustrated in Fig. 10 for isotherms at 100-degree intervals over the temperature range. It will be noted upon close inspection of this figure that the low-pressure experiments for cesium accurately define the intercepts. Thus, the magnitudes of the dimerization constants are not influenced by our lack of knowledge regarding the imperfections present in the vapor.

The observed dimerization constants are shown graphically in Fig. 11. They are well represented by the equation

$$\log k_2 = -3.6561 + \frac{4570}{T}. \tag{23}$$

was obtained with the van't Hoff equation - The enthalpy of dimerization

$$\frac{d \ln k_2}{dT} = \frac{\Delta H_2^o}{RT^2} \tag{24}$$

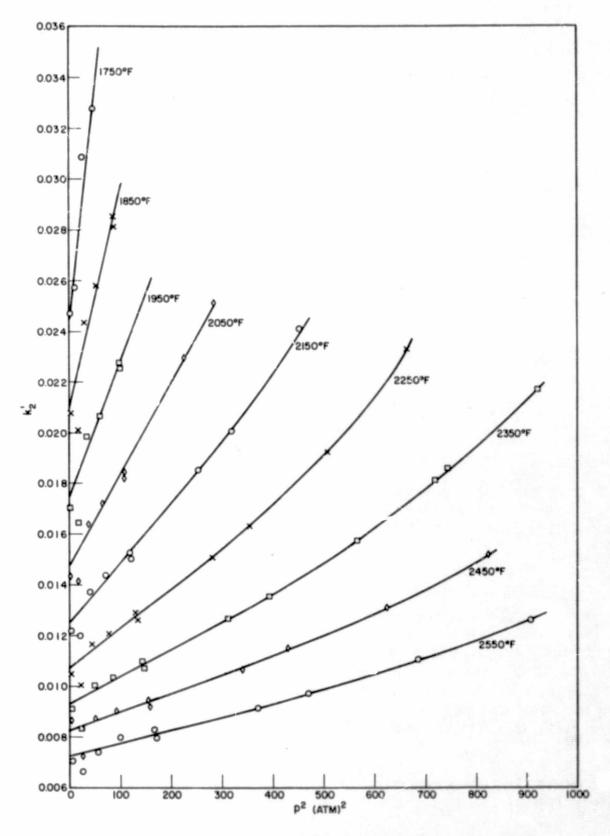


Fig. 10 - Apparent dimerization constants of cesium vapor at several temperatures

by substituting the known differential from Eq. (23). The standard enthalpy so obtained is

$$2 Cs = Cs_2$$
,  $\Delta H_2 = -20,900$  Btu/lb-mole or -11.61 mean kcal/mole.

The association enthalpy at absolute zero of the dimeric reaction was calculated by two methods. A value of -10.7 kcal/mole was obtained at an average temperature of 2250°F with the equation

$$(\Delta H_0^o)_2 = \Delta H_2^o - \Delta (H^o - H_0^o)_{2Cs}^{Cs_2}$$
 (25)

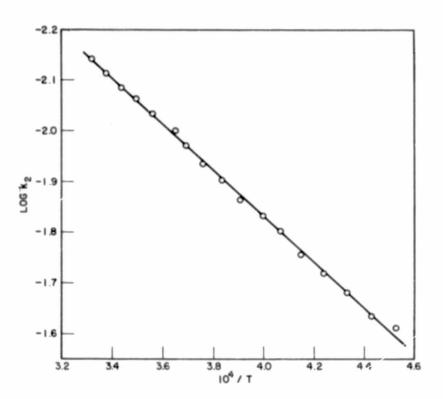


Fig. 11 - Equilibrium constants of dimerization reaction in cesium vapor

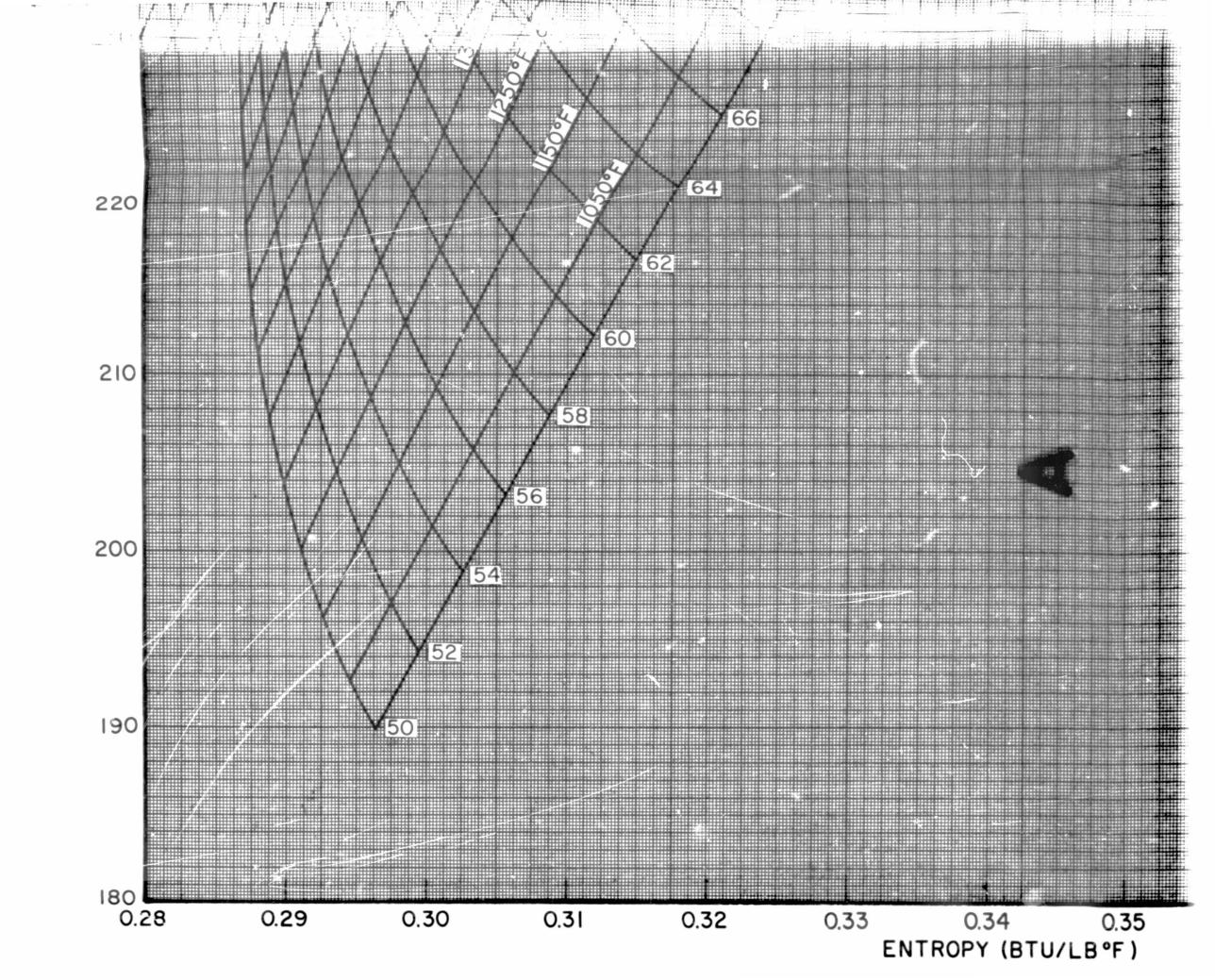
using the observed value of -11.6 for  $\Delta H_2^o$  and the tabular values of Evans et al. (7) for the enthalpy functions. Another value of -11.0±0.1 kcal/mole (which is an average for the temperature range from 2000° to 2400°F) was obtained with the equation

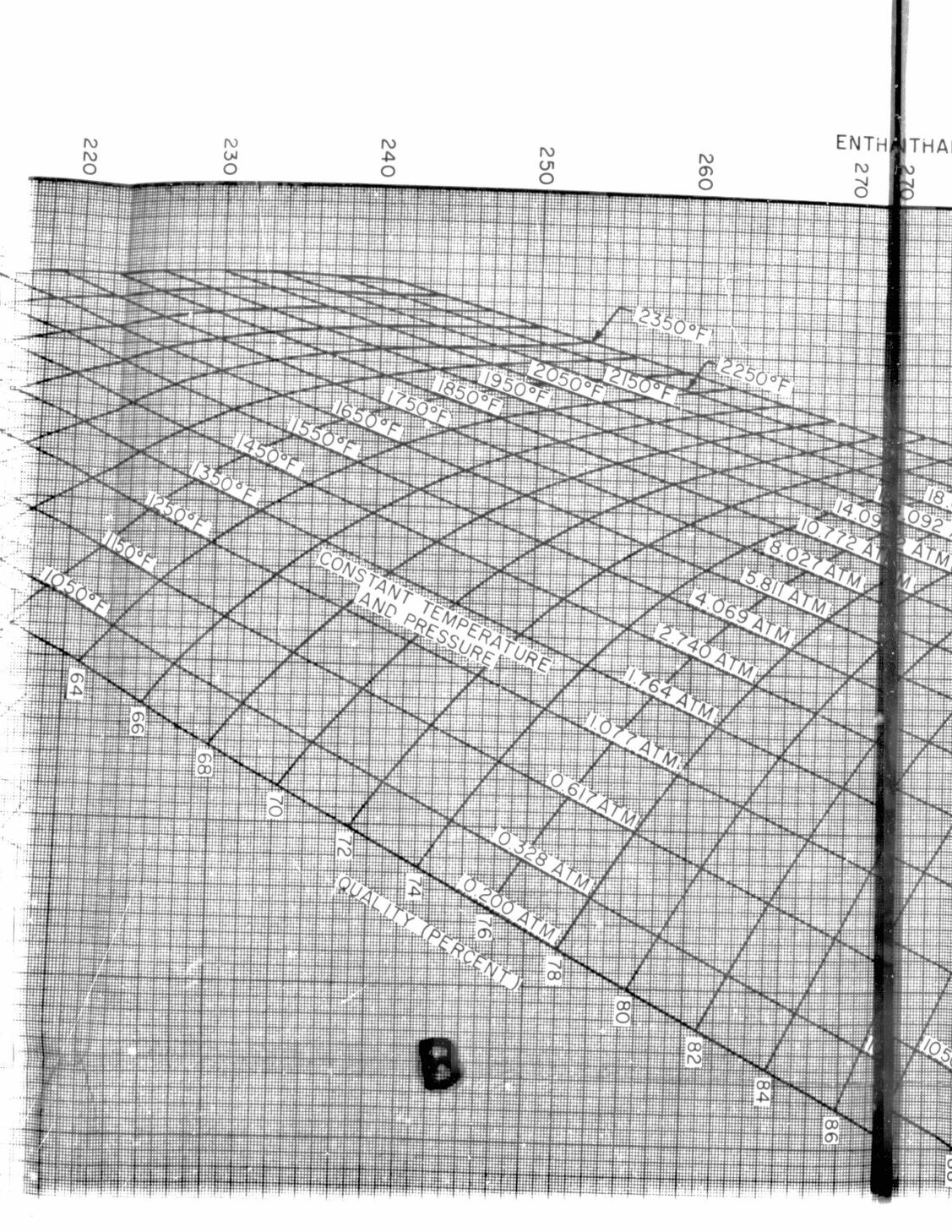
$$\frac{(\Delta H_0^o)_2}{T} = R \ln k_2 - \Delta \left[ \frac{F^o - H_0^o}{T} \right]_{2Cs}^{Cs_2}$$
 (26)

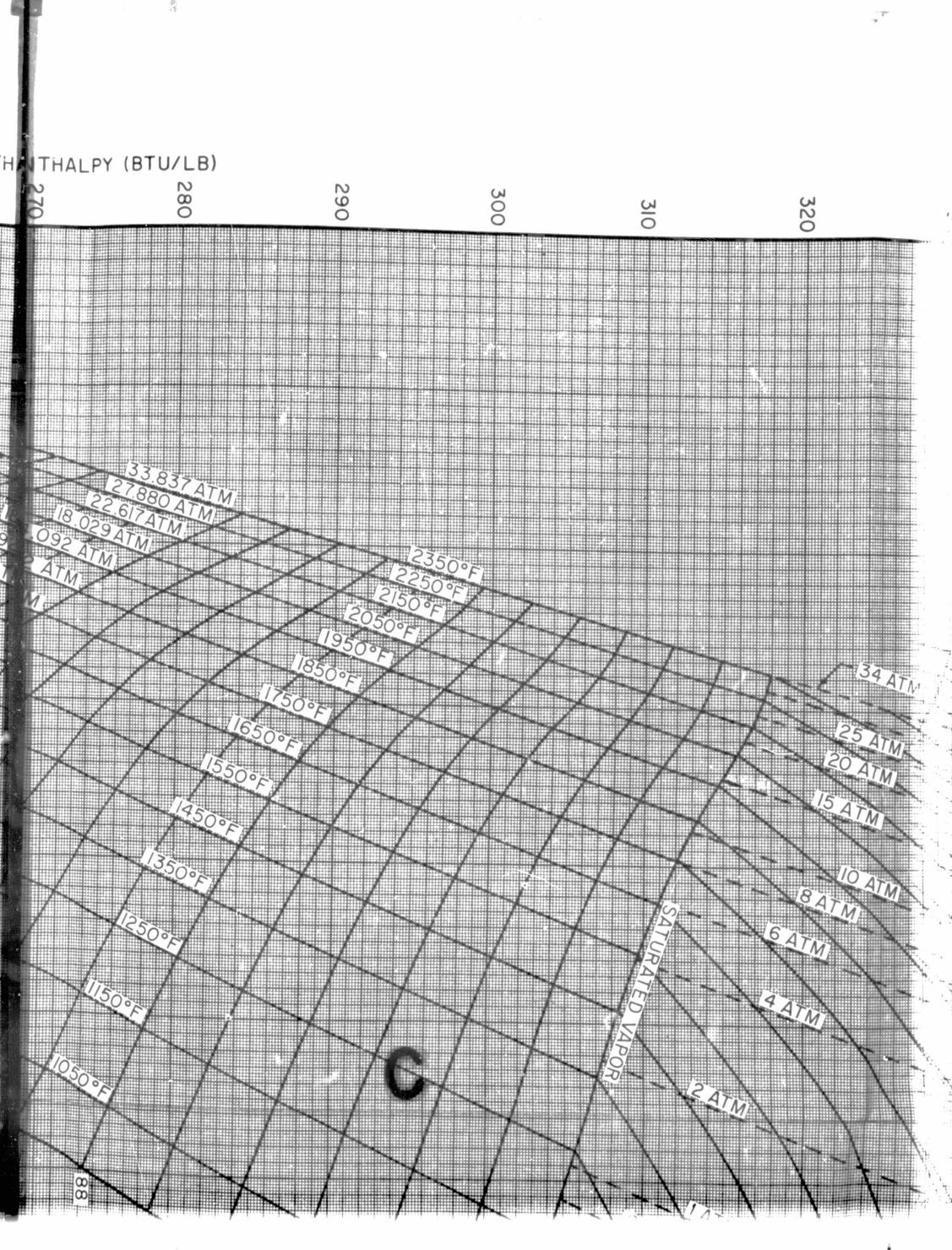
using observed equilibrium constants and the free-energy functions of Evans. The difference between the values as computed by the two methods may be the result of errors in either of the thermal functions or in either of the observed quantities. In any event, since the observed standard enthalpy is probably more reliable than the equilibrium constant and the computed enthalpy function is probably more reliable than the free-energy function, the value of -10.7 is believed to be the more reliable one. This is in reasonable agreement with the spectroscopic value of -10.38 by Herzberg (13).

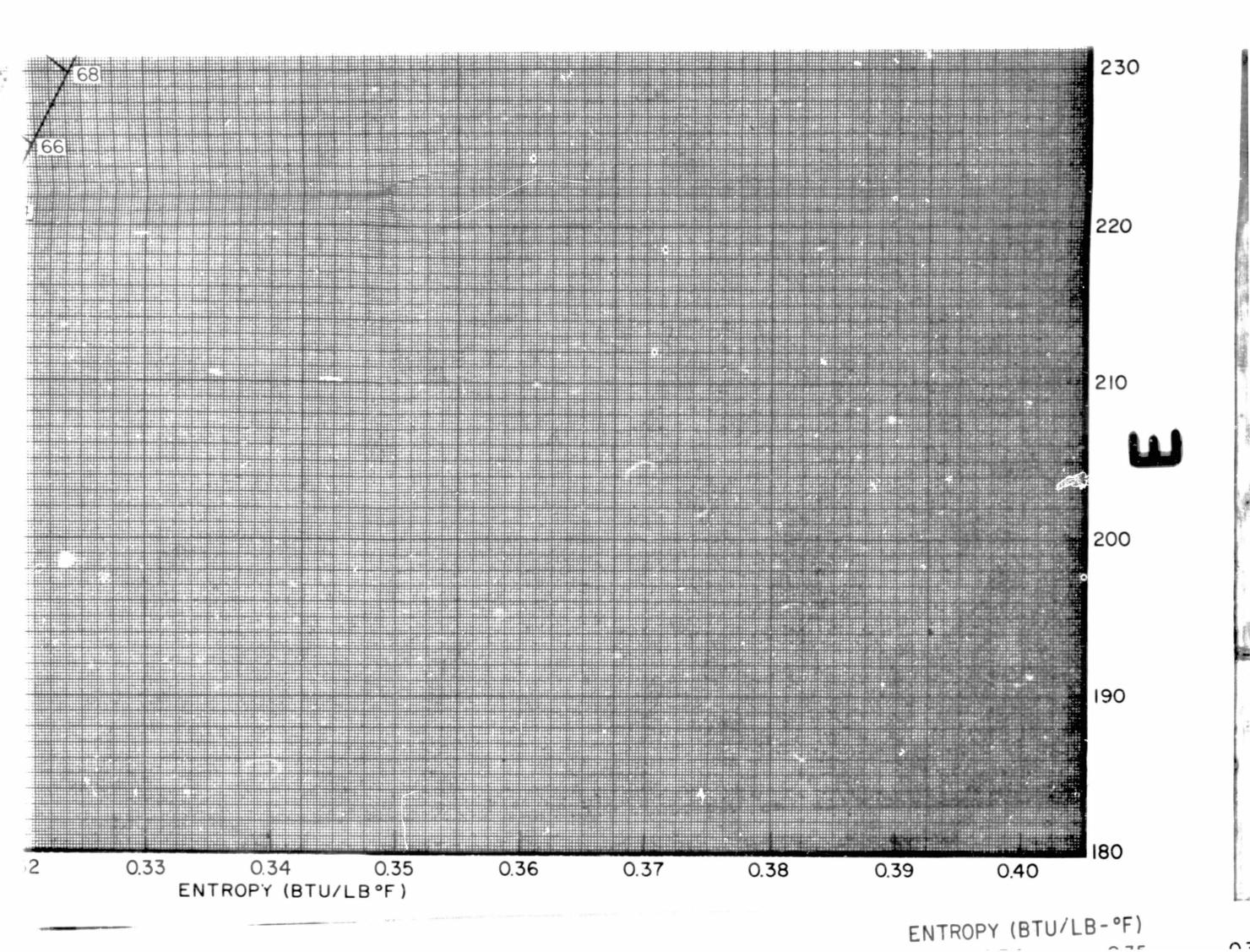
### DISCUSSION OF THERMODYNAMIC AND ENGINEERING PROPERTIES OF CESIUM

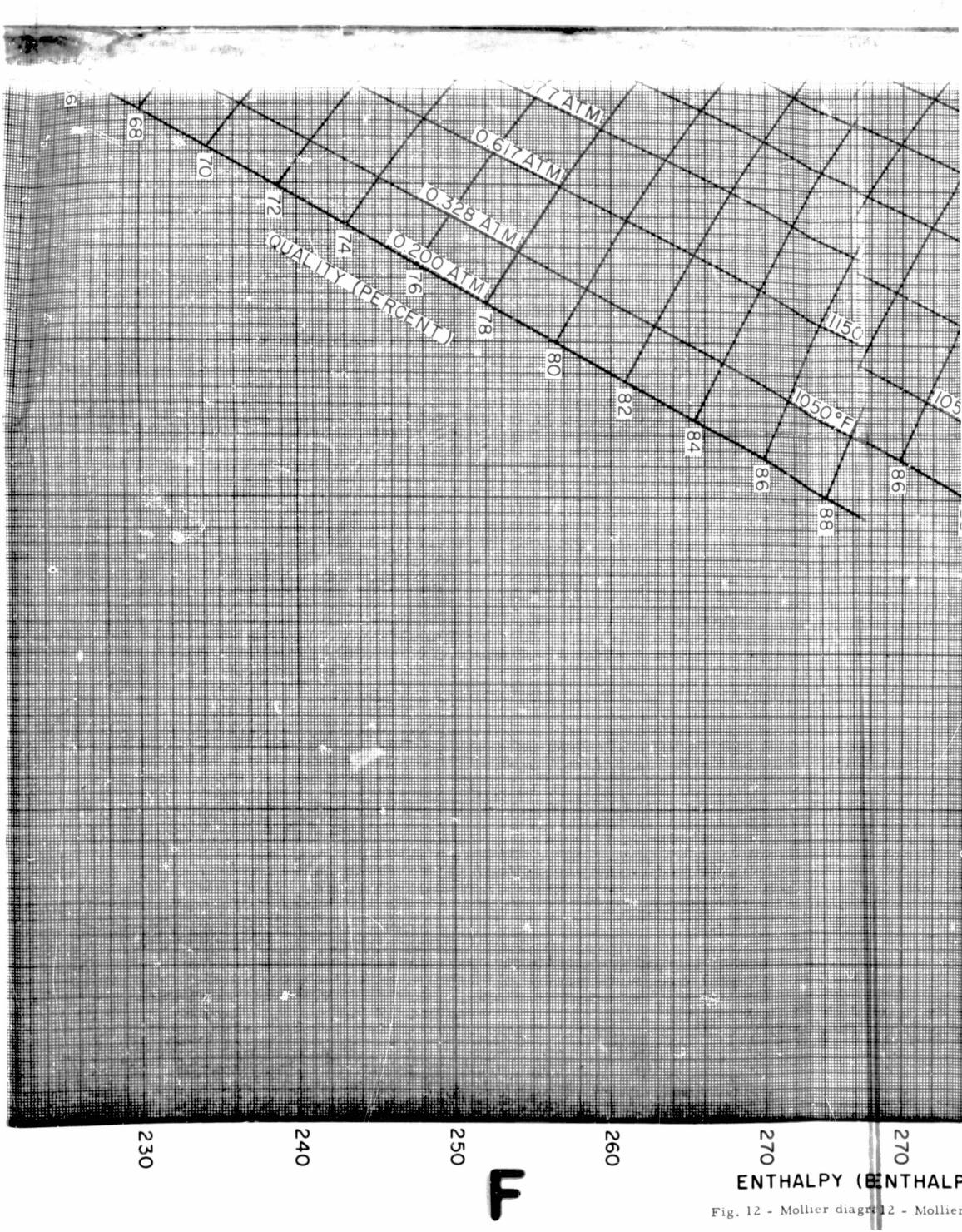
The engineering and thermodynamic properties of cesium, which are presented in Appendixes A and B and in the large Mollier plot (Fig. 12) were computed by the virial method and are based on the properties of the monomeric gas at 1 atm. Two property relationships, the virial equation of state and the vapor-pressure equation, were used with the basic thermodynamic relationships to derive superheat and saturation properties. The virial equation was reduced from PVT data covering a pressure range of 1.12 to 33.2 atm and a temperature range of 1305° to 2571°F. The vapor-pressure equation represents saturation data covering a range of 1.00 to 33.5 atm. Since the reported properties have been limited to a pressure of 34.0 atm and to a temperature of 2550°F, the range of the observed data covers all states in Appendixes A and B except those with pressures below 1.12 atm. For these lower pressure states, short extrapolations with Eqs. (1) and (13) were required. The reported properties have been examined by several methods and evaluated for internal consistency. It is believed that they represent the best values and that they will be satisfactory for any current calculation required in the design of turbines using cesium as working fluid.

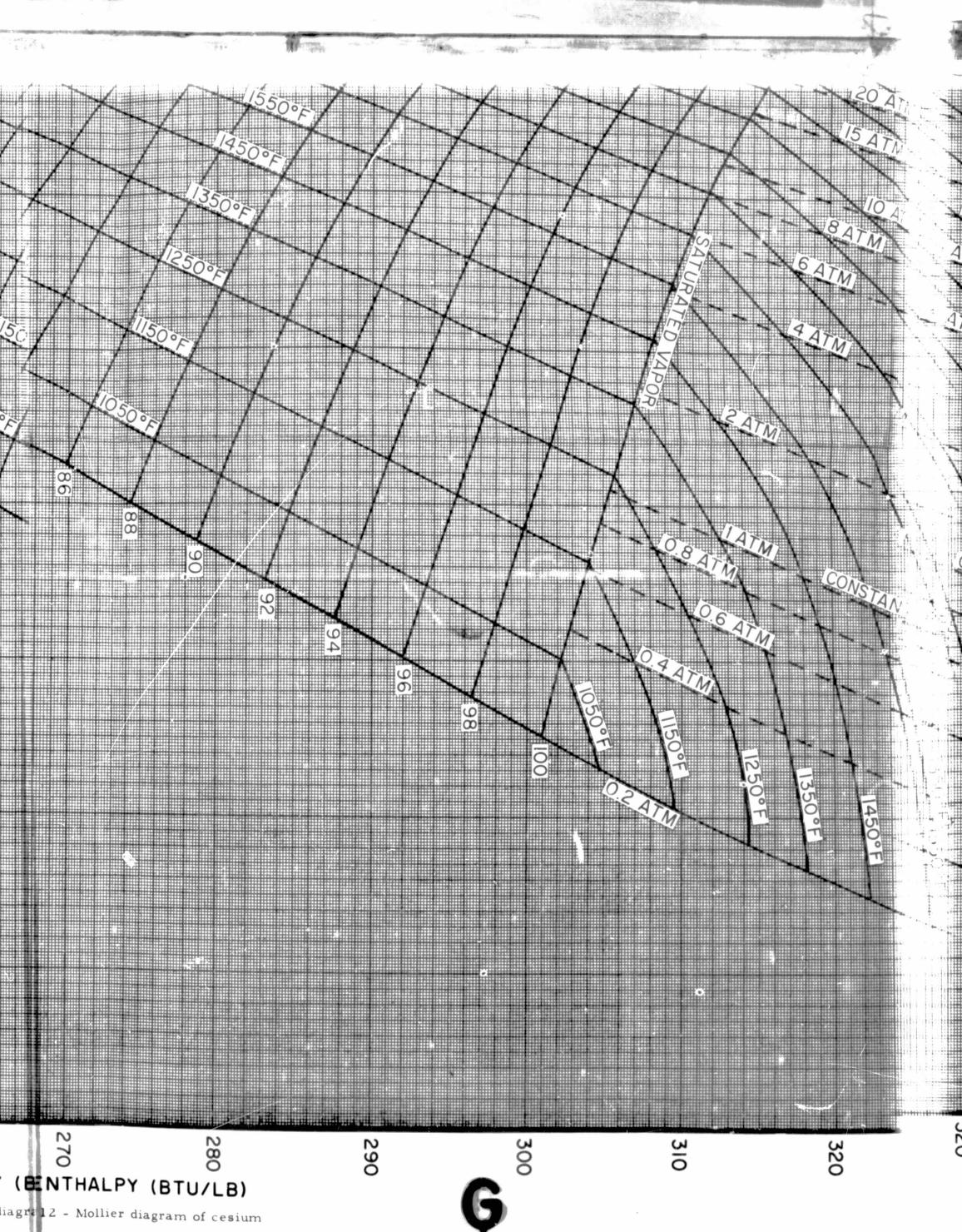


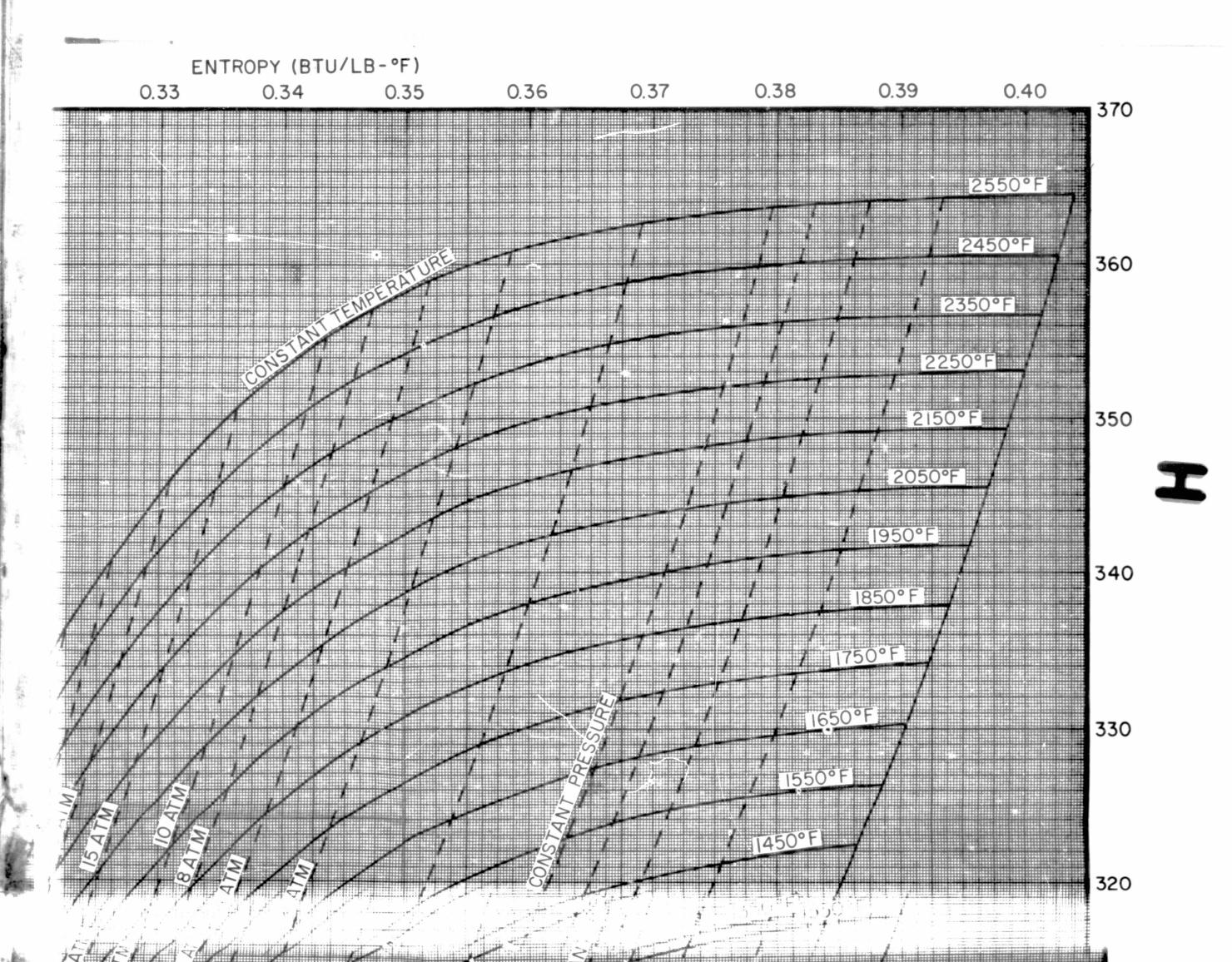












#### NAVAL RESEARCH LABORATORY

The present study represents the only known PVT measurements of cesium which have been published. Measurements in the intermediate temperature range have been in progress at MSAR (5), and the results should be available for comparison in the near future. There are several publications in which thermodynamic properties of the vapor have been computed from saturation pressures, spectroscopic data, and published thermodynamic functions of the monomeric and dimeric vapors. The properties derived in this report from the PVT study were compared with those computed in two recent publications by Agapova et al. (14) and Weatherford et al. (15). If we arbitrarily take the NRL data as a reference and compare at each temperature enthalpy and entropy changes from  $p_s$  to 0.2 atm, enthalpy changes reported by Agapova are 23 to 44% lower, and entropy changes are 9% lower. The enthalpy changes reported by Weatherford are 8 to 41% lower and the entropy changes 4 to 8% lower.

Saturation pressures of cesium were measured between 1215° and 2346°F with the null-point apparatus. The precision and internal consistency of the saturation measurements are attested by the small deviation ( $\pm 0.35\%$ ) of all measured data from a simple three-term equation. In the previous studies in sodium (2) and potassium (1), an equation of the Kirchhoff type was effective in fitting the saturation pressures. This study with cesium reaffirms that an equation of this type is required to describe accurately the dependence of vapor pressure on temperature.

Densities of the condensed phase were measured in the temperature range from 1577° to 2304°F with pycnometers. This method was time consuming, since an independent measurement was required at each temperature, but results of unquestionable accuracy were obtained. With these measurements and those generated in other investigations at lower temperatures, overlapping determinations have been made from the melting point to 2304°F, and the density of liquid cesium is well defined for the full temperature range.

The liquid metal program at this Laboratory is a small part of the national effort in this area. The internal consistency and the confidence limits of the properties of sodium, potassium, and cesium can be more fully evaluated as additional properties are measured for the three metals. Particularly important would be reliable determinations of the heat of vaporization, the specific heat of the liquid and vapor, and the electrical conductivity of the vapor. A good example of this type of evaluation is provided by recent measurements at Aerojet-General Nucleonics (4) of the heats of vaporization of cesium. These were measured directly and have been shown to substantiate those computed in this report from the Clapeyron equation. Similarly, a direct determination of the specific heat of the vapor would test the values computed from the virial equation of state, and a determination of the electrical conductivity would provide additional information on the degree of ionization of the vapor.

### ACKNOWLEDGMENTS

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#### NOMENCLATURE AND UNITS

- B second virial coefficient, cu ft/mole
- c third virial coefficient, (cu ft)<sup>2</sup>/(mole)<sup>2</sup>

# 30 NAVAL RESEARCH LABORATORY D fourth virial coefficient, (cu ft)<sup>3</sup>/(mole)<sup>3</sup> Efifth virial coefficient, (cu ft)4/(mole)4 specific heat at constant pressure, Btu/lb-°F ddensity, lb/cu ft free energy, Btu/lb free energy, Btu/lb-mole enthalpy per unit mass, Btu/lb enthalpy change per unit mass, Btu/lb $\Delta h$ enthalpy change for the formation of a unit mass of dimer from monomer, Btu/lb $\Delta h_2$ enthalpy change upon vaporization of a unit mass at equilibrium, Btu/lb $\Delta h_{ij}$ enthalpy per mole, Btu/lb-mole Н $\Delta H$ enthalpy change per mole, Btu/lb-mole $\Delta H_2$ enthalpy change for the formation of one mole of dimer from monomer, Btu/lb-mole enthalpy change upon vaporization of a mole at equilibrium, Btu/lb-mole $\Delta H_{o}$ any unit conversion equilibrium constant $k_2'$ apparent equilibrium constant assuming only diatomic and monatomic species molecular weight absolute pressure, atm Rgas constant entropy per unit mass, Btu/lb-°F entropy change upon vaporization of a unit mass at equilibrium, Btu/lb-°F $\Delta s_{n}$ absolute temperature, °R Ttemperature, °F $\widetilde{v}$ molal volume (normally per formula weight of monomer), cu ft/lb-mole

specific volume, cu ft/lb

compressibility factor,  $p\widetilde{V}/RT$ 

#### NAVAL RESEARCH LABORATORY

# Subscripts

- a quantity for equilibrium molecular mixture
- quantity for the vapor in a state
- o quantity at 0°R
- p constant pressure change
- s quantity at saturation
- constant temperature change
- quantity for monatomic species
- quantity for diatomic species
- 3 quantity for triatomic species
- 4 quantity for tetratomic species

# Superscripts

- quantity in gas state
- quantity in liquid state
- standard state, 1 atm for gas
- apparent quantity, when assuming only diatomic and monatomic species

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APPENDIX A SATURATION PROPERTIES OF CESIUM

1250.00	1.0768	.01088	8.0598	94.69	210.99	305.69	.2293	.1234	.3527
1275.00	1.2249	.01094	7.1572	96.20	209.85	306.06	.2302	.1210	.3511
1300.00	1.3882	.01101	6.3778	97.72	208.70	306.41	.2310	.1186	.3496
1325.00	1.5676	.01107	5.7022	99.24	207.53	306.76	.2319	.1163	.3402
350.00	1.7641	.01114	5.1146	100.76	206.34	307.10	.2327	.1140	.3467
375.00	1.9786	.01121	4.6015	102.28	205.15	307.43	.2336		
400.00	2.2122	.01128	4.1522	103.81	203.95	307.76	.2344	.1118	.3454
1425.00	2.4657	.01135	3.7574	105.34	202.74	307,76		.1097	.3441
1450.00	2.7403	.01142	3.4093	106.86	201.53	308.08	.2352	.1076	.3428
1475.00	3.0369	.01150	3.1017	108.39	200.31	308.39	.2360	.1055	.3415
1500.00	3,3565	.01157	2.8289			308.70	.2368	.1035	.3403
1525.00	3,7000	.01165	2.5864	109.91	199.10	309.01	.2376	.1016	.3392
1550.00	4.0685	.01173		111.43	197.88	309.31	.2383	.0997	.3380
1575.00	4.4629		2.3703	112.95	196.66	309.62	.2391	.0979	.3369
1600.00	4.8842	.01181	2.1771	114.47	195.45	309.92	.2398	.0961	.3359
1625.00	7.0042	.01189	2.0041	115.98	194.24	310.22	.2406	.0943	.3349
	5.3333	.61197	1.8487	117.49	193.03	310,53	.2413	.0926	.3339
1650.00	5.8111	.01205	1.7089	119.00	191.83	310.83	.2420	.0909	.3329
675.00	6.3185	.01213	1.5827	120.51	190.63	311.14	.2427	.0893	.3320
1700.00	6.8565	.01222	1.4687	122.01	189.44	311.45	.2434	.0877	.3311
725.00	7.4258	.01231	1.3654	123.51	188.26	311.77	.2441	.0862	.3302
750.00	8.0273	.01240	1.2715	125.01	187.07	312.08	.2447	.0847	.3294
775.00	8.6619	.01249	1.1862	126.51	185.89	312,40	.2454	.0832	.3286
.800.00	9.3302	.01258	1.1083	128.02	184.71	312.73	.2461	.0817	.3270
825.00	10.0332	.01268	1.0372	129.53	183.52	313.05	.2467	.0803	.3270
850.00	10,7715	.01277	.9721	131.05	182.33	313.38	.2474	.0789	.3263
875.00	11.5459	.01267	.9124	132.57	181.13	313.71	.2480	.0776	.3256
900.00	12.3570	.01297	.8576	134.11	179.92	314.04	.2487	.0762	.3249
925,00	13,2054	.01307	.8070	135.66	178.70	314.36	.2493	.0749	.3242
950.00	14.0919	.01317	.7604	137.23	177.45	314.68	.2499		
975.00	15.0170	.01328	.7173	138.82	176.18			.0736	.3236
000.00	15.9812	.01339	.6774	140.43	174.88	315.00	.2506	.0724	.3229
025.00	16,9852	.01350	.6404	142.06	173.55	315.31	.2512	.0711	. 3223
050.00	18,6294	.01361	.6059	143.72	172.18	315.61	.2519	.0698	.3217
075.00	19.1142	.01372	.5739	145.40		315,90	. 2525	.0686	.3211
100.00	20.2402	.01384			170.77	316.17	.2532	.0674	.3205
125.00	21.4077	.01396	.5440	147.10	169.32	316.43	.2538	.0661	.3200
150.00	22.6171	.01408	.5161	148.83	167.83	316,66	.2545	.0649	.3194
175.00	23.8687		.4900	150.58	166.29	316.87	.2551	.0637	.3189
200.00	25.1630	.01420	. 4656	152.35	164.72	317.06	. 2558	.0625	.3103
		.01433	.4427	154.12	163.11	317.23	.2564	.0613	.3178
225.00	26.5001	.01446	.4213	155.88	161.49	317.37	.2571	.0602	.3172
250.00	27.8803	.01459	.4014	157.61	159.88	317,49	.2577	.0590	.3167
275.00	29.3039	.01473	.3828	159.30	158.29	317.59	.2583	.0579	.3162
300.00	30.7711	.01487	. 3655	160.91	156.77	317.68	.2589	.0568	.3157
325.00	32.2820	.01501	.3495	162.42	155.35	317,77	. 2594	.0558	.3152
350.00	33.8367	.01515	.3348	163.79	154.09	317.88	. 2599	.0548	.3147

APPENDIX B
THERMODYNAMIC PROPERTIES OF CESIUM VAPOR

t	р	v	8	hg.	8.9	cg p
250.00	1.0768	8.0598	.92387	305.69	.35270	.0671
250.00	1.0000	8.7283	.92917	306.40	.35414	.0653
250.00	.8000	11.0740	.94310	308.28	.35836	.0604
50.00	.6000	14.9858	.95718	310.19	.36357	.0551
50.00	.4000	22.8122	.97138	312.13	.37055	.0494
50.00	.2000	46.2952	.98566	314.09	.38183	.0435
75.00	1.2249	7.1572	.91983	306.06	.35114	.0679
75.00	1.0000	8.9045	.93426	308.01	.35507	.0631
75.00	.8000	11.2853	.94724	309.77	.35923	.0584
75.00	.6000	15.2549	.96033	311.55	.36436	.0539
75.00	.4000	23.1962	.97350	313.35	.37126	.0483
75.00	.2000	47.0230	.98673	315.17	.38246	.0429
00.00	1.3882	6.3778	.91574	306.41	.34963	.0688
00.00	1.0000	9.0778	.93890	309.56	.35596	.061
00.00	.8000	11.4933	.95100	311.20	.36005	.0566
300.00	.6000	15.5206	.96317	312.87	.36511	.0520
00.00	.4000	23.5767	,97541	314.54	.37194	.0473
00.00	.2000	47.7471	.98769	316.23	.38307	.0424
25.00	1.5676	5.7022	.91160	306.76	.34816	.0696
25.00	1.0000	9.2482	.94313	311.06	.35681	.0590
325,00	.8000	11.6985	.95441	312.60	.36084	.0549
325,00	.6000	15.7833	.96575	314.15	.36583	.0507
25.00	.4000	23.9540	.97714	315.71	.37260	.046
25.00	.2000	48.4680	.98856	317.28	.38367	.0419
50.00	1.7641	5.1146	.90742	307.10	.34675	.0703
50.00 50.00	1.0000	9.4160	.94698	312.51	.35761	.0572
50.00	.8000	11.9009	.95751	313.95	.36159	.0534
50.00	.6000	16.0432	.96809	315.40	.36653	.0495
50.00	.4000	24.3286	.97870	316.86	.37324	.0455
375.00	1.9786	49.1860 4.6015	.98934	318.33	.38425	.0415
75.00	1.0000	9.5815	.90319	307.43	34538	.0710
75.00	.0000	12.1009	.95050 .96034	313.92 315.27	.35839	. 0555
375.00	.6000	16.3005	.97022	316.63	.36231	.0520
75.00	.4000	24.7005	.98013	317.99	.36720 .37386	.0484
75.00	.2000	49.9015	.99006	319.36	.38481	.0448
60.00	2.2122	4.1522	.89895	307.76	.34405	.0411
00.00	2.0000	4.6407	.90835	309.05	.34611	.0689
00.00	1.0000	9.7448	.95370	315.29	.35913	.0540
00.00	.8000	12.2987	.96291	316.55	.36301	.0508
00.00	.6000	16.5556	.97216	317,83	.36785	.0475
00.00	.4000	25.0702	.98142	319.10	.37446	.0441
20.00	.2000	50.5146	.99070	320.38	.38537	.0408
25,00	2.4657	3.7574	.89468	308.08	.34277	.0724
25.00	2.0000	4.7325	.91402	310.74	.34701	.0666
25.00	1.0000	9.9061	.95663	316.62	.35984	.0528
25.00	.8000	12.4944	.96526	317.81	.36368	.0496
25,00	.6000	16.8087	.97392	319.00	.36848	.0466
25.00	.4000	25.4377	.98260	320.20	.37504	.0435
25,00	.2000	51.3256	.99130	321.40	.38591	.0405
50.00	2,7403	3.4093	.89040	308.39	.34152	.0730
50.00	2,0000	4.8227	.91925	312.38	,34787	.0645
50.00	1.0000	10.0656	.95931	317.92	.36053	.0514
50.00	.8000	12.6883	.96741	319.04	.36432	.0486
50.00	.6000	17.0599	.97554	320.16	.36909	.0458
50.00	.4000	25.8034	.98368	321.28	.37561	.0430
50.00	.2000	52.0347	.99184	322.40	.38644	.0402
75.00	3.0369	3.1017	.88612	308.70	.34032	.0735
75.00	3.0000	3.1445	.88745	308.89	.34058	.0732
75.00	2.0000	4.9114	.92407	313.97	.34870	, , , , ,

APPENDIX B
THERMODYNAMIC PROPERTIES OF CESIUM VAPOR (cont'd)

t	P	$v^g$		hg.	8.9	cg p
1475.00	1.0000	10.2235	.96176	319.19	.36119	.0502
1475.00	.8000	12.8806	.96938	320.24	.36495	.0477
475.00	.6000	17.3094	.97702	321.29	.36968	
475.00	.4000	26.1674	.98467	322.35	.37617	.045
475.00	.2000	52.7421	.99233	323.41	.38696	.042
500.00	3.3565	2.8289	.88185	309.01		.0400
500.00	3,0000	3.2082	.89388	310.69	.33916	.0740
500.00	2.0000	4.9987	.92850	315.50	.34150	.0708
500,00	1.0000	10.3799	.96401		.34949	.060
500.00	.8000	13.0713	.97118	320.43	.36182	.0492
500.00	.6000	17.5574		321.42	.36556	.0468
500.00	.4000	26.5299	.97837	322.41	.37026	.0445
500.00			.98557	323.41	.37671	.0421
525.00	.2000	53.4480	.99278	324.40	.38747	.0397
	3.7000	2.5864	.87759	309.31	.33803	.0745
525.00	3.0000	3.2708	.89984	312.43	.34238	.0685
525.00	2.0000	5.0848	.93259	317.00	.35024	.0588
525.00	1.0000	10.5348	.96608	321.65	.36244	.0483
525,00	.8000	13.2607	.97284	322.58	.36615	.0461
525.00	.6000	17.8040	.97962	323.52	.37082	.0439
525.00	.4000	26.8910	.98640	324.46	.37725	.0417
525,00	.2000	54.1525	.99320	325.39	.38797	.0396
550.00	4.0685	2.3703	.87335	309.62	.33694	.0749
550.00	4.0000	2.4165	.87536	309.90	.33730	.0744
550.00	3.0000	3.3324	.90537	314.11	.34323	.0664
550.00	2.0000	5.1697	.93636	318.45	.35097	
550.00	1.0000	10.6886	.96799	322.84	.36304	.0572
550.00	.8000	13.4488	.97437	323.73	.36672	.0474
550.00	.6000	18.0493	.98076	324.61		.0454
550.00	.4000	27.2508	.98716	325.50	.37136	.0434
550.00	.2000	54.8557	.99358	325.50	.37777	.0414
575.00	4.4629	2.1771		326.38	.38847	.0394
575.00	4.0000	2.4650	.86914	309.92	.33588	.0753
575.00	3.0000	3.3929	.88198	311.73	.33821	.0721
575.00			.91050	315.75	.34404	.0644
575.00	2.0000	5.2534	.93984	319.86	.35167	.0557
575.00	1.0000	10.8412	.96975	324.02	.36362	.0466
	.8000	13.6357	.97578	324.85	.36728	.0448
575,00	.6000	18.2935	.98182	325.69	.37190	.0429
575.00	.4000	27.6095	.98787	326.53	.37828	.0411
575.00	.2000	55.5577	.99393	327.36	.38895	.0392
600.00	4.8842	2.0041	.86496	310.22	.33486	.0756
600.00	4.0000	2.5127	.88814	313.51	.33907	.0699
600.00	3.0000	3.4526	.91525	317.33	.34481	.0625
600.00	2.0000	5.3362	.94306	321.23	.35234	.0544
600,00	1.0000	10.9928	.97137	325.18	.36419	.0459
600,00	.8000	13.8216	.97707	325.97	.36782	.0442
600.00	.6000	18.5367	.98279	326.76	.37242	
600.00	.4000	27.9671	.98852	327.55		.0425
600.00	.2000	56.2587	.99425	328.34	.37878	.0408
625.00	5.3333	1.8487	.86082		.38943	.0391
625.00	5.0000	1.9906	.86892	310.53	.33388	.0759
625.00	4.0000	2.5597		311.68	.33526	.0741
625.00	3.0000	3.5113	.89389	315.23	.33991	.0678
625.00			.91966	318.87	.34555	.0607
	2.0000	5.4181	.94604	322.58	.35299	.0532
625.00	1.0000	11.1434	.97287	326.32	.36474	.0453
625.00	.8000	14.0066	.97827	327.07	.36835	.0437
625.00	.6000	18.7789	.98369	327.82	.37293	.0421
625,00	.4000	20.3237	.98912	328.57	.37927	.0405
625.00	.2000	56.9588	.99456	329.32	.38990	.0390
650.00	5.8111	1.7089	.85672	310.83	.33292	.0761
650.00	5.0000	2.0295	.87542	313.50	.33613	.0719

APPENDIX B

THERMODYNAMIC PROPERTIES OF CESIUM VAPOR (cont'd)

						$c_p^g$
1650.00	4.0000	2.6059	.89924	316.20	.34070	.0658
1650.00	3.0000	3.5692	.92376	320.37	.34627	.059
650.00	2.0000	5.4990	.94881	323.89	.35362	.052
650,00	1.0000	11.2931	.97426	327.44	.36527	.044
650.00	.8000	14.1907	.97939	328.15	.36887	.043
650.00	.6000	19.0202	.98453	328.87	.37343	
650.00	.4000	28.6795	.98967	329.58	.37975	.041
650.00	.2000	57.6580	.99483	330.29	.39037	.040
675.00	6.3185	1.5827	.85265	311.14	.33200	.038
675.00	6.0000	1.6801	.85949	312.12		.076
675.00	5.0000	2.0678	.88150	315.28	.33312	.074
675.00	4.0000	2.6514	.90423		.33697	.069
675.00	3.0000	3.6264	.92757	318.52	.34147	. 064
675.00	2.0000	5.5792		321.83	.34696	.057
675.00	1.0000		.95137	325.18	.35422	.051
675.00		11.4420	. 97555	328.55	.36580	.044
675.00	.8000	14.3740	.98042	329.23	.36938	.0428
675.00	.6000	19.2607	.98530	329.91	.37392	.041
	.4000	29.0345	.99019	330.58	.38022	.040:
675.00	.2000	58.3563	.99509	331.26	.39082	.0387
700.00	6.8565	1.4687	.84863	311.45	.33110	.0765
700.00	6.0000	1.7129	.86611	313.97	.33398	.0728
700.00	5.0000	2.1055	.88719	316.99	.33777	.0678
700.00	4.0000	2.6963	.90889	320.10	.34220	.0622
700.00	3.0000	3.6829	.93111	323.25	.34762	.0563
700.00	2.0000	5.6587	.95375	326.44	.35481	.0501
700.00	1.0000	11.5902	.97674	329.65	.36631	.0437
700.00	.8000	14.5565	.98137	330.30	.36987	.0425
700.00	6000	19.5005	.98602	330.94	.37440	.0412
700.00	.4000	29.3887	.99067	331.58	.38069	.0399
700.00	.2000	59.0540	.99533	332.23	.39127	.0386
725.00	7,4258	1.3654	.84465	311.77	.33024	
725.00	7.0000	1.4623	.85277	312.94	.33152	.0766
725,00	6.0000	1.7452	.87233	315.76		.0750
725.00	5.0000	2.1427	.89251	318.67	.33480	.0708
725.00	4.0000	2.7405	.91323		.33854	.0659
725.00	3.0000	3.7387		321.63	.34291	.0606
725.00	2.0000	5./375	.93441	324.64	.34826	.0550
725.00	1.0000	11.7377	.95597	327.68	.35538	.0492
725.00			.97786	330.74	.36681	.0433
725.00	.8000	14.7384	.98227	331.35	.37036	.0421
725.00	.6000	19.7396	.98669	331.97	.37487	.0409
	.4000	29.7423	.99111	332.58	.38115	.0397
725.00	.2000	59.7509	.99555	333.19	.39172	.0386
750.00	8.0273	1.2715	.84071	312.08	. 32940	.0766
750.00	8.0000	1.2766	.84120	312.15	.32948	.0765
756.00	7.0000	1.4905	.85939	314.79	.33236	.0730
50.00	6.0000	1.7770	.87817	317.51	.33560	.0688
750.00	5.0000	2.1793	.89749	320.29	.33928	.0641
750.00	4.0000	2.7842	.91728	323.13	.34359	.0591
750.00	3.0000	3.7940	.93748	326.00	.34888	.0538
750.00	2.0000	5.8157	.95804	328.90	.35594	.0484
750.00	1.0000	11.8846	.97889	331.82	.36730	.0429
50.00	.8000	14.9196	.98309	332.40	.37084	.0418
750.00	.6000	19.9780	.98731	332.99	.37534	.0407
750.00	.4000	30.0952	.99153	333.57	.38160	.0396
750.00	.2000	60.4472	.99576	334.15	.39216	.0385
775.00	8.6619	1.1862	.83679	312.40	.32859	
775.00	8.0000	1.3016	.84810	314.04	.33033	.0766
775.00	7.0000	1.5183	.86563	316.59	.33318	.0746
775.00	6.0000	1.8083	.88366			.0710
775.00	5.0000	2.2154	.90216	319.20 321.87	.33636	.0670

APPENDIX B
THERMODYNAMIC PROPERTIES OF CESIUM VAPOR (cont'd)

t	P	vg.		49	80	cop
775.00	4.0000	2.8273	.92107	324.59	.34424	.057
775.00	3.0000	3.8486	.94035	327.33	.34948	.052
775.00	2.0000	5.8933	.95996	330.10	.35648	.047
775.00	1.0000	12.0310	.97986	332.88	.36778	.042
775.00	.8000	15.1003	.98387	333.44	.37130	.041
775.00	.6000	20.2159	.98789	334.00	.37579	.040
775.00	.4000	30.4476	.99192	334.56	.38204	.039
775.00	.2000	61.1430	.99595	335.11	.39259	A CONTRACT OF THE PARTY OF THE
800.00	9.3302	1.1083	.83290	312.73	.32781	.038
800.00	9.0000	1.1563	.83822	313.50	.32860	.076
800.00	8.0000	1.3263	.85463	315.88	.33115	.075
800.00	7.0000	1.5458	.87150	318.34		.072
800.00	6.0000	1.8392			.33395	.069
800.00	5.0000		.88881	320.85	.33710	.065
800.00		2.2510	.90653	323.42	.34068	.060
	4.0000	2.8699	.92461	326.01	.34488	.056
800.00	3.0000	3.9028	.94303	328.64	.35008	,051
800.00	2.0000	5.9704	.96.76	331.29	.35700	.047
800.00	1.0000	12.1768	.98076	333.94	.36825	.042
800.00	.8000	15.2804	.98459	334.48	37176	.041
800.00	.6000	20.4533	.98843	335.01	.37624	.040
.00,00	.4000	30.7994	.99228	335.54	.38248	.039
800.00	.2000	61.8382	.99613	336.07	.39302	.038
825.00	10.0332	1.0372	.82903	313.05	.32705	.076
325.00	10.0000	1.0413	.82953	313.13	.32712	.076
825.00	9.0000	1.1785	.84496	315.37	.32942	.073
825.00	8.0000	1.3507	.86080	317.68	.33194	.070
825.00	7.0000	1.5728	.87704	320.05	.33471	.067
825.00	6.0000	1.8697	.89365	322.46	.33780	.063
825,00	5.0000	2.2862	.91062	324.92	.34134	.059
825.00	4.0000	2.9121	.92793	327.41	.34549	.055
825.00	3.0000	3.9565	.94554	329.92	.35062	.050
825.00	2.0000	6.0470	.96344	332.45	.35752	.046
825.00	1.0000	12.3221	.98160	334.99	.36871	.041
825.00	.8000	15.4600	.98526	335.50	.37222	.041
825.00	.6000	20.6902	.98893	336.01	.37668	A SALAMAN MARKET SALAMAN SALAM
825.00	.4000	31.1507	.99261	336.52	.38291	.040
825.00	.2000	62.5330	.99630	337.03	.39344	
850.00	10.7715	.9721	.82515			.038
850.00	10.0000	1.0615	.83643	313.38	.32631	.076
850.00	9.0000	1.2005		315.02	.32795	.074
850.00	8.0000	1.3747	.85136	317.19	.33022	.072
850.00	7.0000	1.5994	.86664	319.43	.33270	.069
850.00	6.0000		.88225	321.71	.33543	.065
850.00		1.8997	.89820	324.03	.33849	.062
	5.0000	2.3210	.91446	326.39	.34198	.058
850.00	4.0000	2.9538	.93103	328.78	.34609	.054
850.00	3.0000	4.0097	.94789	331.18	.35117	.050
850.00	2.0000	6.1232	.96501	333.61	.35802	.045
850.00	1.0000	12.4669	.98239	336.04	.36917	.041
850.00	.8000	15.6392	.98590	336.53	.37266	.040
850.00	.6000	20.9266	.98941	337.01	.37712	.039
850.00	.4000	31.5016	.99293	337.50	.38334	.039
850.00	.2000	63.2272	.99646	337.99	.39385	.038
875.00	11.5459	.9124	.82126	313.71	.32560	.076
875,00	11.0000	.9666	.82886	314.81	.32667	.075
875.00	10.0000	1.0814	.84299	316.86	.32374	.073
875.00	9.0000	1.2221	.85742	318.97	,33098	.070
875.00	8.0000	1.3985	.87214	321.13	.33343	.067
875.00	7.0000	1.6258	.88716	323.33	.33613	.064
875.00	6.0000	1.9294	.90247	325.57	.33915	.060
875.00	5.0000	2.3553	.91807	327.83	.34260	.056

APPENDIX B

THERMODYNAMIC PROPERTIES OF CESIUM VAPOR (cont'd)

t	p	v <sup>g</sup>	8	$h^g$	89	$c_p^g$
1875.00	4.0000	2.9951	.93394	330.12	.34667	.053:
1875.00	3.0000	4.0625	.95009	332.42	.35171	.049
1875.00	2.0000	6.1989	.96649	334.74	.35851	.045
1875.00	1.0000	12.6113	.98313	337.07	.36962	
1875.00	.8000	15.8180	.98649	337.54	.37310	.041
1875.00	.6000	21.1626	.98985	338.01	.37755	.040
1875.00	.4000	31.8521	.99323	338.48		.039
1875.00	.2000	63.9211	.99661	338.94	.38376	.039
1900.00	12.3570	.8576	.81734		.39427	.038
1900.00	12.0000	.8882	.82209	314.04	32491	.076
1900.00	11.0000	.9848		314.72	.32556	.075
1900.00	10.0000	1.1010	.83554	316.67	.32746	.0737
1900.00	9.0000	1.2434	.84923	318.67	.32951	.0713
1900.00	8.0000		.86316	320.71	.33172	.0687
1900.00		1.4219	.87734	322.80	.33414	.0657
1900.00	7.0000	1.6517	.89179	324.91	.33680	.0626
1900.00	6.0000	1.9588	.90649	327.06	.33979	.0592
	5.0000	2.3893	.92146	329.24	.34320	.0558
1900.00	4.0000	3.0360	.93668	331.43	.34723	.0522
1900.00	3.0000	4.1149	.95215	333.65	.35223	.0485
1905.00	2.0000	6.2743	.96787	335.87	.35899	.0448
1900.00	1.0000	12.7554	.98383	338.11	.37005	.0411
1900.00	.8000	15.9964	.98704	338.55	.37353	.0404
1900.00	.6000	21.3982	.99027	339.00	.37797	.0396
1900.00	.4000	32.2022	.99350	339.45	.38417	.0389
900.00	.2000	64.6146	.99675	339.90	.39467	.0381
925.00	13.2054	.8070	.81338	314.36	.32424	.0761
925.00	13,0000	.8224	.81601	314.74	.32459	.0758
1925.00	12.0000	.9050	.82887	316.59	.32635	.0741
925,00	11.0000	1.0028	.84191	318.49	.32823	.0720
1925.00	10,0000	1.1205	. 85515	320.43	.33025	
925.00	9.0000	1.2645	.86859	322.41		.0697
925.00	8.0000	1.4450	.88225	324.42	.33244	.0670
925.00	7.0000	1.6774	.89614	326.46	.33482	.0642
925.00	6.0000	1.9878	.91027		.33745	.0612
925.00	5.0000	2.4230	.92464	328.53	.34040	.0580
925.00	4.0000	3.0766	.93925	330.62	.34378	.0547
925.00	3.0000	4.1670	.95409	332.73	.34777	.0513
925.00	2.0000	6.3493	.96917	334.85	.35273	.0479
925.00	1.0000	12.8991		336.99	.35946	.0444
925.00	.8000	16.1744	.98448	339.13	.37049	.0409
925.00	.6000		.98756	339.56	.37395	.0402
925.00		21.6335	.99066	339.99	37839	.0395
925.00	.4000	32.5519	.99377	340.42	.38458	.0388
950.00	.2000	65.3077	.99688	340.85	.39507	.0381
950.00	14.0919	.7604	.80936	314.68	.32358	.0760
	14.0000	.7665	.81049	314.85	.32373	.0759
950.00	13.0000	.8380	.82286	316.61	.32537	.0744
950.00	12.0000	.9217	.83535	318.42	.32711	.0725
950.00	11.0000	1.0206	.84797	320.27	.32897	.0704
950.00	10.0000	1.1396	.86076	322.15	.33097	.0681
950,00	9.0000	1.2853	.87373	324.06	.33313	.0655
950.00	8.0000	1.4678	.88689	326.01	.33549	.0627
950,00	7.0000	1.7027	.90025	327.97	.33809	.0598
950.00	6.0000	2.0165	.91383	329.96	.34100	.0568
950.00	5.0000	2.4563	.92764	331.97	.34434	.0537
950,00	4.0000	3.1169	.94166	334.00	.34830	.0505
950.00	3.0000	4.2187	.95592	336.04	.35323	.0472
950.00	2.0000	6.4239	.97039	338.09	.35992	.0440
950.00	1.0000	13.0424	.98509	340.15	.37091	
950.00	.8000	16.3521	.98806	340.56	.37437	.0407
950.00	.6000	21.8684	.99103	340.97	.37880	.0400

APPENDIX B

THERMODYNAMIC PROPERTIES OF CESIUM VAPOR (cont'd)

t	p	$v^g$	8	ħg.	89	cg p
950.00	.4000	32.9013	.99401	341.39	.38498	.038
.950.00	.2000	66.0005	.99700	341.80	.39547	.038
975.00	15.0170	.7173	.80526	315.00	.32295	.075
975.00	15.0000	.7183	.80546	315.03	.32297	.075
975.00	14.0000	.7810	.81740	316.73	.32451	.074
975.00	13.0000	.8535	.82942	318.46	.32613	.072
975.00	12.0000	.9381	.84152	320.22	.32785	
975.00	11.0000	1.0382	.85373	322.01		.071
975.00	10.0000	1.1586	.86609	323.83	.32969	.068
975.00	9.0000	1.3059	.87859	325.68	.33167	.066
975.00	8.0000	1.4903	.89127		.33380	.064
975.00	7.0000	1.7278	.90413	327.56	.33613	.061
975.00	6.0000			329.45	.33870	.058
975.00		2.0449	.91719	331.37	.34158	.055
975.00	5.0000	2.4894	.93046	333.30	.34489	.052
	4.0000	3.1568	.94394	335.25	.34882	.049
975.00	3.0000	4.2701	.95763	337.21	.35371	.046
975.00	2.0000	6.4982	.97154	339.18	.36037	.043
975.00	1.0000	13.1854	.98567	341.16	.37133	.040
975.00	.8000	16.5294	.98852	341.56	.37479	.039
975.00	.6000	22.1030	.99138	341.96	.37920	.039
975.00	.4000	33.2503	.99424	342.35	.38538	.038
975.00	.2000	66.6929	.99712	342.75	.39586	.038
000.00	15,9812	.6774	.80105	315.31	.32233	.075
000.00	15,0000	.7320	.81242	316.91	.32374	.074
000.00	14.0000	.7955	.82403	318.57	.32526	.073
000.00	13,0000	.8688	.83568	320.26	.32687	
000.00	12.0000	.9543	.84740	321.97	.32857	.071
00.00	11.0000	1.0556	.85921	323.71		.069
000.00	10.0000	1.1773	.87113	325.48	.33039	.067
000.00	9.0000	1.3262	.88319		.33234	.065
000.00	8.0000	1.5126		327.27	.33445	.062
000.00	7.0000	1.7526	.89541	329.07	.33675	.060
000.00				330.90	.33929	.057
000.00	6.0000	2.0730	.92036	332.75	.34215	.054
	5.0000	2.5221	.93312	334.61	.34543	.0519
000.00	4.0000	3.1965	.94608	336.49	.34932	.049
000.00	3.0000	4.3213	.95925	338.37	.35419	.046
000.00	2.0000	6.5723	.97263	340.27	.36082	.043
000,00	1.0000	13.3282	.98621	342.17	.37174	.040
000.00	.8000	16.7065	.98895	342.56	.37519	.0397
00.00	.6000	22.3373	.99170	342.94	.37960	.039
00.00	.4000	33.5991	.99446	343.32	.38578	.0386
00.00	.2000	67.3851	.99723	343.70	39625	.0380
25.00	16.9852	.6404	.79673	315.61	.32172	.0757
025.00	16.0000	.6893	.80785	317.16	.32306	.0746
025.00	15.0000	.7455	.81911	318.76	.32449	.0732
25.00	1 0000	.8097	.83037	320.38	.32599	.0716
025.00	13.0000	.8839	.84165	322.02	.32758	.0699
025.00	12.0000	.9704	.85299	323.69	.32926	
025.00	11.0000	1.0728	.86440	325.38	.33106	.0679
25.00	10.0000	1.1958	.87591	327.09		.0659
025.00	9.0000	1.3463	.88755		.33299	.0636
25.00	8.0000	1.5347		328.82	.33507	.0613
25.00	7.0000	1.7772	.89932	330.56	.33735	.0589
25,00			.91125	332.32	.33986	.0563
25.00	6.0000	2.1009	.92335	334.10	.34269	.0537
	5.0000	2.5546	.93563	335.90	.34595	.0511
025.00	4.0000	3.2358	.94810	337.70	.34982	.0484
025,00	3.0000	4.3721	.96077	339.52	.35465	.0457
025.00	2.0000	6.6461	.97365	341.35	.36125	.0429
025.00	1.0000	13.4706	.98672	343.18	.37215	.0402
025.00	.8000	16.8833	.98936	343.55	.37559	.0396

APPENDIX B

THERMODYNAMIC PROPERTIES OF CESIUM VAPOR (cont'd)

		vg	8	h <sup>g</sup>	88	$c_p^g$
t	P				70000	.039
025.00	.6000	22.5713	.99201	343.91	38000 38617	.039
025,00	.4000	33.9476	.99466	344.28	.39664	.038
025.00	.2000	68.0770	.99733	344.65	.32113	.075
050.00	18.0294	.6059	.79227	315.90	.32117	.075
050.00	18,0000	.6072	.79260	315.94		.074
050,00	17,0000	.6318	.80362	317.47	.32245	.073
050.00	16.0000	.7020	.81458	319.01	.32380	.071
050.00	15.0000	.7589	.82551	320.57	.32522	.070
050.00	14.0000	.8238	.83642	322.15	.32670	
050.00	13,0000	.8988	.84734	323.75	.32827 .32994	.068
050.00	12.0000	.9863	.85831	325.37		.064
050.00	11.0000	1.0898	.86934	327.01	.33171	
050.00	10.0000	1.2141	.88045	328.66	.33362	.062
050.00	9.0000	1.3662	.89167	330.33	.33568	.060
2050.00	8,0000	1.5565	.90302	332.02	.33793	.057
050.00	7.0000	1.8015	.91452	333.72	.34042	.055
050.00	6.0000	2.1285	.92617	335.44	.34323	.052
050.00	5.0000	2.5869	.93800	337.16	.34646	.050
2050.00	4.0000	3.2750	.95001	338.91	.35030	.047
2050.00	3.0000	4.4227	.96221	340.66	.35511	.04
050.00	2.0000	6.7196	.97461	342.42	.36168	.042
2050.00	1.0000	13.6128	.98721	344.18	.37255	.040
2050.00	.8000	17.0599	.98975	344.54	.37599	.039
2050.00	.6000	22.8051	.99230	344.89	.38039	.039
2050.00	.4000	34.2958	.99486	345.24	.38655	.036
2050.00		68.7687	.99743	345.60	.39701	.03
2050.00	.2000	.5739	.78767	316.17	.32055	.07
2075.00	19.1142	.5783	.78891	316.34	.32068	.07
2075.00	19.0000	.6187	.79970	317.82	.32191	.074
2075.00	18,0000	.6639	.81041	319.31	.32319	.07
2075.00	17.0000	.7146	.82105	320.82	.32452	.07
2075.00	16.0000	.7721	.83163	322.35	.32592	.07
2075,00	15.0000		.84220	323.89	.32739	.06
2075.00	14.0000	.8378	.85277	325.45	.32894	.06
2075.00	13.0000	.9136	.86337	327.02	.33059	.06
2075.00	12.0000	1.0020	.87402	328.60	.33235	.06
2075.00	11.0000	1.1066	.88475	330.20	.33423	.06
2075.00	10.0000	1.2322		331.82	.33627	.05
2075.00	9.0000	1.3858	.89558	333.45	.33850	.05
2075.00	8.0000	1.5781	.90652		.34097	.05
2075.00	7.0000	1.8256	.91761	335.09	.34375	.05
2075.00	6.0000	2.1559	.92884	336.75		.04
2075.00	5.0000	2.6189	.94024	338.41	.34695 .35077	.04
2075.00	4.0000	3.3139	.95181	340.09		.04
2075.00	3.0000	4.4731	.96357	341.78	.35555	.04
2075.00	2.0000	6.7928	.97552	343.48	.36210	.03
2075.00	1.0000	13.7548	.98766	345.18	.37295	.03
2075.00	.8000	17.2362	.99011	345.52	.37638	
2075.00	.6000	23.0386	.99257	345.86	.38078	.03
2075.00	.4000	34.6439	.99504	346.20	.38693	.03
2075.00	.2000	69.4601	.99752	346.55	.39739	.03
2100,00	20,2402	.5440	.78290	316.43	.31998	.07
2100.00	20.0000	.5523	.78546	316.77	.32025	.07
2100.00	19.0000	.5893	.79606	318.21	.32142	.07
2100.00	18,0000	.6302	.80654	319.67	.32263	.07
2100.00	17.0000	.6758	.81693	321.13	.32390	.07
2100.00	16.0000	.7271	.82723	322.61	.32522	.07
	15.0000	.7852	.83749	324.09	.32661	.06
2100.00	14.0000	.8516	.84771	325.59	.32806	.06
2100.00	13.0000	.9281	.85793	327.10	.32960	.06
2100.00	12.0000	1.0175	.86818	328.63	.33122	.06

APPENDIX B

THERMODYNAMIC PROPERTIES OF CESIUM VAPOR (cont'd)

t	, F	• 29	8	hg.	8.9	cg p
2100.00	11.0000	1.1232	.87847	330.17	.33296	.061
2100.00	10.0000	1.2500	.88883	331.72	.33482	.059
2100.00	9.0000	1.4053	.89928	333.28	.33684	.057
100.00	8.0000	1.5995	.90984	334.85	.33905	.055
100.00	7.0000	1.8495	.92053	336.44	.34150	.053
100.00	6.0000	2.1831	.93137	338.04	.34425	.051
100.00	5.0000	2.6507	.94236	339.65	.34744	.049
100.00	4.0000	3.3526	.95352	341.27	.35123	.046
100.00	3,0000	4.5232	.96486	342.90	.35599	.044
100.00	2.0000	. 6.8659	.97535	344.53	.36251	.042
100.00	1.0000	13.8965	.98810	346.18	.37334	
100.00	.8000	17.4122	.99046	346.50	.37677	.039
100.00	.6000	23.2720	.99283			.039
100.00	.4000	34.9916	.99521	346.83	.38116	.038
100.00	.2000	70.1513		347.16	.38731	.038
			.99760	347.49	.39776	.037
125.00	21.4077	.5161	.77797	316.66	.31941	.075
125.00	21.0000	.5290	.78225	317.23	.31986	.075
125.00	20.0000	.5628	.79267	318.64	.32098	.074
125.00	19.0000	.6002	.80295	320.06	.32214	.073
125.00	18.0000	.6415	.81311	321.48	.32334	.072
125.00	17.0000	.6877	.82317	322.91	.32459	.070
125.00	16.0000	.7395	.83315	324.35	.32590	.069
125,00	15.0000	.7982	.84307	325.80	.32727	.067
125.00	14.0000	.8652	.85296	327.26	.32871	.066
125,00	13.0000	.9426	.86285	328.73	.33023	.064
125.00	12.0000	1.0328	.87275	330.21	.33184	.062
125.00	11.0000	1.1396	.88269	331.70	.33355	
125.00	10.0000	1.2677	.89270	333.20	.33540	.060
125.00	9.0000	1.4245	.90279	334.71	.33740	.058
125.00	8.0000	1.6207	.91299	336.23	.33959	.056
125.00	7.0000	1.8732	.92330			.054
125.00	6.0000	2.2101	.93376	337.77	.34201	.052
125.00	5.0000	2.6822		339.31	.34475	.050
125.00	4.0000		.94436	340.86	.34791	.048
125.00		3.3910	.95513	342.43	.35168	.046
125.00	3.0000	4.5732	.96608	344.00	.35642	.044
	2.0000	6.9387	.97720	345.58	.36292	.041
125.00	1.0000	14.0381	.98850	347.17	.37372	.039
125.00	.8000	17.5881	.99079	347.49	.37715	.039
125.00	.6000	23.5051	.99308	347.80	.38153	.038
125.00	.4000	35.3392	.99538	348.12	.3876%	.038
125.00	.2000	70.8422	.99769	348.44	.79813	.037
150.00	22.6171	.4900	.77288	316.87	.31866	.075
150.00	22,0000	.5079	.77927	317:72	.31950	.075
150,00	21.0000	.5391	.78952	319.10	.32058	.074
150.00	20.0000	.5733	.79961	320.49	.32169	.073
50.00	19.0000	.6110	.80957	321.88	.32284	.072
150.00	18.0000	.6527	.81941	323.27	.32403	.070
50.00	17.0000	.6993	.82915	324.67	.32527	.069
50.00	16.0000	.7517	.83881	326.07	.32656	
50.00	15.0000	.8110	.84841	327.48	.32792	.067
50.00	14.0000	.8787	.85797	328.90		.066
50.00	13.0000	.9569	.86753	330.32	,32934	.064
50.00	12.0000	1.0480	.87710	331.76	.33084	.063
150.00	11.0000	1.1558			.33243	.061
150.00	10.0000		.88671	333.20	.33413	.059
		1.2053	.89637	334.65	.33596	.057
150.00	9.0000	1.4436	.90612	336.12	.33794	.055
150.00	8.0000	1.6417	.91597	337.59	.34011	.053
150.00	7.0000	1.8967	.92593	339.07	.34251	.051
150.00	6.0000	2.2369	.93603	340.57	.34523	.049
150.00	5.0000	2.7136	.94627	342.07	.34837	.047

APPENDIX B
THERMODYNAMIC PROPERTIES OF CESIUM VAPOR (cont'd)

THERMODYNAMIC PROPERTIES OF CESIUM VAPOR (cont'd)									
t	P	$v^g$	a	hg	89	$c_p^g$			
2150.00	4.0000	3.4293	.95666	343.58	.35212	.045			
2150.00	3.0000	4.6229	.96723	345.10	.35684	.043			
2150.00	2.0000	7.0114	.97797	346.62	.36332	.041			
2150.00	1.0000	14.1794	.98889	348.16	.37410	.039			
2150.00	.8000	17./638	.99110	348.46	.37752	.039			
2150.00	.6000	23.7380	.99331	348.77	.38191	.038			
2150.00	.4000	35.6866	.99553	349.08	.38805	.038			
2150.00	.2000	71.5330	.99776	349.39	.39850	.037			
2175.00	23.8687	.4656	.76765	317.06	.31831	.075			
2175.00	23.0000	.4887	.77652	318.24	.31918	075			
2175.00	22.0000	.5176	.78659	319.59	.32022	.074			
2175.00	21.0000	.5491	.79651	320.95	.32128	.073			
2175.00	20.0000	.5836	.80629	322.30	.32238	.072			
2175.00	19.0000	.6217	.81593	323.66	.32352	.070			
2175.00	18.0000	.6638	.82545	325.02	.32470	.069			
2175,00	17.0000	./109	.83487						
2175.00	16.0000	.7638	.84421	326.38 327.75	.32592	.068			
2175.00	15.0000	.8237			.32720	.066			
			.85349	329.12	.32854	.065			
2175.00	14.0000	.8921	.86274	330.50	.32995	.063			
2175.00	13,0000	.9710	.87198	331.88	.33144	.061			
2175.00	12.0000	1.0631	.88124	333.28	.33301	.060			
2175.00	11.0000	1.1719	.89052	334.68	.33470	.058			
173.00	10.0000	1.3026	.89987	336.08	.33651	.056			
175.00	9.0000	1.4625	.90928	337.50	.33847	.054			
175.00	8.0000	1.6626	.91880	338.93	.34062	.053			
2175.00	7.0000	1.9200	.92842	340.36	.34301	.051			
2175.00	6.0000	2.2635	.93817	341.80	.34570	.049			
2175.00	5.0000	2./449	.94807	343.26	.34883	.047			
2175.00	4.0000	3.4674	.95811	344.72	.35256	.045			
175.00	3.0000	4.6725	.96832	346.19	.35726	.043			
175.00	2.0000	7.0839	.97870	347.66	.36372	.041			
2175.00	1.0000	14.3206	.98926	349.14	.37448	.039			
2175.00	.8000	17.9393	.99139	349.44	.37790	.039			
175.00	.6000	23.9707	.99353	349.74	.38228	.038			
175.00	.4000	36.0338	.99568	350.04	.38842	.038			
175.00	.2000	72.2236	.99784	350.33	.39886	.037			
2200.00	25.1630	.4427	.76233	317.23	.31777	.076			
200.00	25.0000	. 4466	.76397	317.44	.31792	.076			
200.00	24.0000	.4713	.77399	318.78	.31889	.075			
200.00	23.0000	.4981	.78389	320.11	.31989	.074			
200.00	22.0000	.5272	.79364	321.44	.32091	.073			
200.00	21.0000	.5590	.80324	322.76	.32197	.072			
200.00	20.0000	.5938	.81269	324.09	.32306	.070			
200.00	19.0000	.6322	.82202	325.42	.32418	.069			
200.00	18.0000	.6748	.83123	326.74	.32535	.068			
200.00		.7224							
200.00	17.0000	.7758	.84034	328.07	.32656	.066			
	16.0000		.94937	329.40	.32783	.065			
200.00	15.0000	.8362	.85635	330.74	.32915	.063			
200.00	14.0000	.9053	.86729	332.07	.33054	.062			
200.00	13.0000	.9850	.87623	333.42	.33202	.060			
200.00	12.0000	1.0779	.88517	334.77	.33358	.059			
200.00	11.0000	1.1879	.89415	336.13	.33524	.057			
200.00	10.0000	1.3199	.90318	337.49	.33704	.055			
200.00	9.0000	1.4813	.91229	338.86	.33898	.054			
200.00	8.0000	1.6833	.92149	340.24	.34112	.052			
200.00	7.0000	1.9431	.93079	341.63	.34349	.050			
200.00	6.0000	2.2900	.94021	343.03	.34617	.048			
2200.00	5.0000	2.7759	.94978	344.43	.34927	.046			
2200.00	4.0000	3.5053	.95949	345.85	.35298	.045			
2200.00	3.0000	4.7219	.96936	347.27	PART NO SERVICE PROPERTY AND THE PARTY OF TH				

APPENDIX B

THERMODYNAMIC PROPERTIES OF CESIUM VAPOR (cont'd)

ŧ	p	vg	,	ħg.	89	$c_p^g$
2200.00	2.0000	7.1562	.97940	348.69	.36411	.041
2200.00	1.0000	14.4615	.98961	350.13	.37485	.039
2200.00	.8000	18.1146	.99167	350.42	.37826	.038
2200.00	.6000	24.2033	.99374	350.70	.38264	.038
2200.00	.4000	36.3808	.99582	350.99	.38878	.038
2200.00	.2000	72.9140	.99791	351.28	.39921	.037
2225.00	26.5001	.4213	.75696	317.37	.31723	.076
2225.00	26.0000	.4323	.76189	318.02	.31769	.076
2225.00	25.0000	. 4553	.77170	319.33	.31863	.075
2225.00	24.0000	.4803	.78141	320.64	.31959	.074
2225.00	23.0000	.5073	.79098	321.95	.32058	
2225.00	22.0000	.5367	.80041	323.25		.073
2225.00	21.0000	.5687	.80969		.32159	.072
2225.00	20.0000			324.55	.32264	.070
2225.00		.6039	.81884	325.85	.32371	.069
2225.00	19.00,00	.6427	.82785	327.14	.32483	.068
	18.0000	.6857	.83675	328.43	.32598	.067
2225.00	17.0000	.7337	.84556	329.73	.32718	.065
2225.00	16.0000	./876	.85429	331.02	.32843	.064
2225,00	15,0000	.8486	.86298	332.32	.32974	.062
2225.00	14,0000	.9184	.87163	333.62	.33112	.061
2225.00	13,0000	.9988	.88027	334.92	.33258	.059
2225.00	12.0000	1.0927	.88892	336.23	.33413	.058
2225,00	11,0000	1.2037	.89760	337.55	.33578	.056
2225.00	10.0000	1.3369	.90634	338.87	.33755	.054
2225.00	9.0000	1.4999	.91515	340.20	.33948	.053
2225.00	8.0000	1.7038	.92404	341.54	.34160	.051
225.00	7.0000	1.9661	.93304	342.88	.34395	.049
2225.00	6.0000	2.3162	.94215	344.24	.34682	.048
2225.00	5.0000	2.8068	.95140	345.60	.34971	.046
2225.00	4.0000	3.5431	.96079	346.96	.35340	.044
2225.00	3.0000	4.7711	.97034	348.34	.35807	
2225.00	2.0000	7.2283	.98006	349.72	.36449	.042
2225.00	1.0000	14.6024	.98994	351.11		.041
2225.00	.8000	18.2898	.99194		.37522	.039
2225.00	.6000	24.4357	.99394	351.39	.37863	.038
225.00				351.67	.38300	.038
	.4000	36.7277	.99595	351.95	.38913	.038
225.00	.2000	73.6043	.99797	352.22	.39957	.037
2250.00	27,8803	.4014	.75165	317.49	.31670	.076
2250.00	27.0000	.4191	.76009	318.62	.31749	.076
250.00	26.0000	.4407	.76967	319.91	.31839	.075
250.00	25,0000	.4640	.77917	321.20	.31932	.074
250.00	24.0000	.4892	.78856	322.49	.32028	.073
2250.00	23.0000	.5164	.79781	323.76	.32125	.072
250.00	22.0000	.5461	.80692	325.04	.32225	.070
250.00	21.0000	.5784	.81589	326.31	.32329	.069
250.00	20.0000	.6139	.82472	327.57	.32435	.068
250.00	19.0000	.6531	.83343	328.83	.32545	.067
250.00	18.0000	.6965	.84203	330.09	.32660	.065
250.00	17.0000	.7449	.85055	331.35	.32778	.064
250,00	16.0000	.7993	.85900	332.61	.32902	.063
250.00	15.0000	.8609	.86739	333.87	.33032	CONTRACT CONTRACTOR
250.00	14.0000	.9313	.87576	335.14	.33169	.061
250.00	13.0000	1.0125	.88412	336.40	.33313	.060
250.00	12.0000	1.1073	.89249			.058
250.00	11.0000			337.68	.33466	.057
250.00		1.2193	.90089	338.95	.33630	.055
	10.0000	1.3538	.90934	340.24	.33806	.054
2250.00	9.0000	1.5184	.91786	341.52	.33997	.052
2250.00	8.0000	1.7242	.92647	342.82	.34208	.050
2250.00	7.0000	1.9890	.93517	344.12	.34441	.049
2250.00	6.0000	2.3424	.94399	345.43	.34706	.047

APPENDIX B

THERMODYNAMIC PROPERTIES OF CESIUM VAPOR (cont'd)

t	p	$v^g$	8	$h^g$	89	$c_p^g$
250.00	5.0000	2.8375	.95294	346.75	.35013	.0459
250.00	4.3000	3.5807	.96204	348.07	.35382	.0442
250.00	3.0000	4.8202	.97128	349.41	.35846	.0426
250.00	2.0000	7.3003	.98068	350.75	.36487	.0409
250.00	1.0000	14.7430	.99025	352.09	.37558	.0392
250.00	.8000	18.4648	.99219	352.36	.37899	.0388
250.00	.6000	24.6679	.99413	352.63	.38336	.0389
250.00	.4000	37.0744	.99608	352.90	.38949	.038
250.00	.2000	74.2944	.99804	353.17	.39992	.0378
275.00	29.3039	.3828	.74650	317.59	.31618	.0768
275.00	29.0000	.3882	.74930	317.97	.31644	.076
275.00	28.0000	.4071	.75858	319.24	.31730	.076
275.00	27.0000	.4273	.76790	320.51	.31818	.075
275,00	26.0000	.4491	.77717	321.78	.31908	.0742
275.00	25.0000	.4726	.78636	323.04	.32000	.0731
275,00	24.0000	.4980	.79543	324.30	.32094	.0720
275.00	23.0000	5255	.80436	325.55	.32191	.0709
275.00	22.0000	.5554	.81316	326.79	.32290	.069
275.00	21.0000	.5880	.82182	328.03	.32392	.068
275.00	20.0000	.6238	.83035	329.27	.32497	.067
275.00	19.0000	.6633	.83877	330.50	.32606	.065
275.00	18.0000	.7071	.84708	331.72	.32719	.064
275.00	17.0000	.7560	.85532	332.95	.32837	.063
275.00	16.0000	.8109	.86349	334.17	.32960	.061
275.00	15.0000	.8731	.87161	335.40	.33088	.060
275.00 <b>275.</b> 00	14.0000	.9441	.87970	336.63	.33223	.0592
275.00	13.0000	1.0261	.88779	337.86	.33366	.057
275.00	12.0000 11.0000	1.1218 1.2348	.89589 .90402	339.09	.33518	.0563
275.00	10.0000	1.3706	.91220	340.33 341.58	.33680	.0548
275.00	9.0000	1.5367	.92045	342.83	.33855	.0533
275.00	8.0000	1./444	.92878	344.08	.34254	.0518
275.00	7.0000	2.0117	.93721	345.35	.34486	.0487
275.00	6.0000	2.3684	.94575	346.62	.34750	.0471
275.00	5.0000	2.8681	.95441	347.89	.35055	.045
275,00	4.0000	3.6182	.96322	349.18	.35422	.0439
275,00	3.0000	4.8691	.97217	350.47	.35885	.0423
275.00	2.0000	7.3721	.98128	351.76	.36525	.0407
275,00	1.0000	14.8835	.99055	353.07	.37594	.0391
275.00	.8000	18.6397	.99243	353.33	.37934	.0388
275,00	.6000	24.9000	.99431	353.59	.38371	.0384
275.00	.4000	37.4210	.99620	353.85	.38984	.0381
275.00	.2000	74.9844	.99810	354.11	.40026	.0378
300.00	30,7711	.3655	.74169	317.68	.31567	.0770
300.00	30.0000	.3783	.74846	318.64	.31630	.0766
300.00	29,0000	.3960	.75739	319.88	.31714	.0759
300.00	28.0000	.4150	.76640	321.13	.31799	.0751
300.00	27,0000	. 4355	.77542	322.38	.31886	.0742
300.00	26.0000	.4574	.78439	323.62	.31975	.0731
300.00	25,0000	.4811	.79326	324.86	.32066	.0720
300.00	24.0000	.5067	.80202	326.09	.32159	0709
300.00	23.0000	.5344	.81064	327.31	.32255	.0697
300.00	22.0000	.5646	.81914	328.52	.32353	.0685
300.00	21.0000	.5975	.82750	329.73	.32454	.0673
300.00	20.0000	.6336	.83574	330.93	.32558	.0660
300.00	19.0000	.6734	.84387	332.13	.32666	.0648
300.00	18.0000	.7176	.85191	333.33	.32778	.0635
300.00	17.0000	.7669	.85987	334.52	.32894	.0622
300.00	16.0000	.8224	.86777	335.71	.33016	.0609
300.00	15.0000	.8851	.87563	336.90	.33143	.0596

APPENDIX B
THERMODYNAMIC PROPERTIES OF CESIUM VAPOR (cont'd)

t	p	$v^g$		hg .	80	$c_p^g$
2300.00	14.0000	.9568	.88346	338.10	.33277	.058
2300.00	13.0000	1.0396	.89129	339.29	.33418	.056
2300.00	12.0000	1.1361	.89913	340.49	.33569	.055
300.00	11.0000	1.2503	.90700	341.69	.33730	.054
300.00	10.0000	1.3873	.91493	342.90	.33903	.052
300.00	9.0000	1.5549	.92291	344.11	.34092	
300.00	8.0000	1.7645	.93098	345.33	.34299	.051
300.00	7.0000	2.0343	.93914	349.33		.049
300.00				346.56	.34530	.048
	6.0000	2.3942	.94741	347.79	.34792	.046
300.00	5.0000	2.8986	.95581	349.03	.35097	.045
300.00	4.0000	3.6555	.96434	350.27	.35462	.043
300.00	3,0000	4.9179	.97302	351.52	.35924	.042
300.00	2.0000	7.4438	.98185	352.78	.36562	.040
300.00	1.0000	15.0239	.99084	354.04	.37630	.039
300.00	.8000	18.8144	.99266	354.30	.37970	.038
300.00	.6000	25.1320	.99448	354.55	.38406	.038
300.00	.4000	37.7674	.99632	354.81	.39019	.038
300.00	.2000	75.6742	.99815	355.06	.40061	.037
325.00	32.2820	.3495	.73741	317.77	.31518	.077
325.00	32.0000	.3537	.73968	318.11	.31540	.077
325.00	31.0000	.3692	.74797	319.32	.31618	
325.00	30.0000	.3858	.75652			.076
325.00	29.0000	.4037	.76520	320.54	.31699	.075
				321.77	.31782	.075
325.00	28.0000	.4229	.77395	323.00	.31866	.074
325.00	27.0000	.4435	.78267	324.22	.31952	.073
325.00	26.0000	.4657	.79133	325.44	.32040	.072
325.00	25.0000	.4895	.79990	326.64	.32130	.070
325.00	24.0000	.5153	.80834	327.84	.32223	.069
325.00	23.0000	.5433	.81667	329.04	.32317	.068
325.00	22.0000	.5737	.82486	330.22	.32414	.067
325.00	21.0000	.6069	.83294	331.40	.32514	.066
325.00	20.0000	.6433	.84090	332.57	.32617	.064
325.00	19.0000	.6835	.84876	333.74	.32724	.063
325.00	18.0000	.7281	.85653	334.90	.32835	.062
325.00	17.0000	.1778	.86422	336.06	.32950	
325.00	16.0000	.8337	.87187	337.22	.33070	.061
325.00	15.0000	.8971	.87947			.059
				338.38	.33196	.058
325.00	14.0000	.9694	.88705	339.54	.33329	.057
325.00	13.0000	1.0529	.89463	340.70	.33469	.056
325.00	12.0000	1.1503	.90222	341.87	.33619	.054
325.00	11.0000	1.2655	.90985	343.03	.33778	.053
325.00	10.0000	1.4038	.91752	344.21	.33951	.051
325.00	9.0000	1.5730	.92526	345.38	.34138	.050
325.00	8.0000	1.7845	.93307	346.57	.34344	.049
325.00	7.0000	2.0567	.94098	347.76	.34574	.047
325.00	6.0000	2.4200	.94900	348.95	.34834	.046
325.00	5.0000	2.9289	.95714	350.15	.35137	.044
325.00	4.0000	3.6927	.96541	351.36	.35501	.043
325,00	3.0000	4.9666	.97382	352.57	.35962	.041
325.00	2.0000	7.5154	.98239	353.79		
325.00	1.0000	15.1642	.99111	355.02	.36598	.040
					.37665	.039
325.00	.8000	18.9890	.99288	355.27	.38005	.038
325.00	.6000	25.3638	.99465	355.51	.38441	.038
325.00	.4000	38.1137	.99642	355.76	.39053	.038
325.00	.2000	76.3639	.99821	356.00	.40095	.037
350.00	33.8367	.3348	.73386	317.88	.31470	.076
350.00	33.0000	.3462	.74005	318.85	.31532	.076
350.00	32,0000	.3608	.74786	320.03	.31608	.076
350.00	31.0000	.3765	.75598	321.22	.31686	.075
2350.00	30.0000	.3933	.76431	322.43	.31767	.075

APPENDIX B

THERMODYNAMIC PROPERTIES OF CESIUM VAPOR (cont'd)

t	P	$v^g$	8	ħ <sup>g</sup>	89	$c_p^g$
2350.00	29.0000	.4114	.77275	323.63	.31848	.0741
350.00	28.0000	.4307	.78121	324.84	.31932	.0731
2350.00	27.0000	. 4515	.78964	326.03	.32017	.0720
	26.0000	.4738	.79800	327.22	.32104	.0709
2350.00		.4979	.80626	328.40	.32193	.0697
2350.00	25.0000			329.57	.32284	.0686
2350.00	24.0000	.5239	.81441 .82244	330.73	.32378	.0674
2350.00	23.0000	.5520			.32474	.066
2350.00	22.0000	.5827	.83035	331.89	.32573	.065
2350.00	21.0000	.6161	.83814	333.04		
2350.00	20.0000	.6529	.84583	334.18	,32675	.063
2350.00	19.0000	.6934	.85343	335.31	.32780	.062
2350.00	18.0000	.7384	.86094	336.45	.32890	.061
2350.00	17.0000	.7886	.86838	337.58	.33004	.060
2350.00	16.0000	.8450	.87578	338.70	.33123	.058
2350.00	15.0000	.9089	.88314	339.83	.33248	.057
2350.00	14.0000	.9819	.89048	340.96	.33380	.056
2350.00	13,0000	1.0662	.89782	342.09	.33519	.055
2350.00	12.0000	1.1645	.90517	343.22	.33667	.053
2350.00	11.0000	1.2807	.91256	344.36	.33826	.052
2350.00	10.0000	1.4202	.92000	345.50	.33997	.051
2350.00	9.0000	1.5909	.92750	346.64	.34183	.049
2350.00	8.0000	1.8044	.93507	347.79	.34388	.048
2350.00	7.0000	2.0791	.94274	348.94	.34616	.047
		2.4456	.95052	350.10	.34875	.045
2350,00	6.0000	2.9591	.95841	351.27	.35177	.044
2350.00	5.0000		.96643	352.44	35540	.043
2350.00	4.0000	3.7298			.35999	.041
2350.00	3.0000	5.0151	.97459	353.62	.36634	.040
2350.00	2.0000	7.5868	.98290	354.80		
2350.00	1.0000	15.3043	.99137	355.99	.37700	.038
2350.00	.8000	19.1635	.99308	356.23	.38039	.038
2350.00	.6000	25.5955	.99480	356.47	.38475	.038
2350.00	.4000	38.4599	.99653	356.71	.39087	.038
2350.00	.2000	77.0535	.99826	356.95	.40129	.037
2375.00	34.0000	.3394	.74083	319.61	.31526	.076
2375.00	33.0000	.3531	./4813	320.76	.31600	.076
2375.00	32.0000	.36/9	.75580	321.93	.31676	.075
2375.00	31.0000	.3837	.76374	323.11	.31/53	.074
2375.00	30.0000	.4007	.77184	324.29	.31833	.074
2375.00	29.0000	.4189	./8001	325.4/	.31914	.073
2375.00	28.0000	.4384	.78819	326.65	.31996	.072
2375.00	27.0000	. 4594	.79632	32/.82	.32080	.070
2375.00	26.0000	.4819	.86439	328.98	.32167	.069
2375.00	25.0000	.5061	.81236	330.13	.32255	.068
2375.00	24.0000	.5323	.82022	331.27	.32345	.067
2375.00	23.0000	.5607	.82796	332.41	.32437	.066
2375.00	22.0000	.5916	.83560	333.53	.32532	.065
2375.00	21.0000	.6253	.84312	334.65	.32630	.063
	20.0000	.6624	.85055	335.76	.32/31	.062
2375.00		./032	.85789	336.87	.32835	.061
2375.00	19.0000	./486	.86516	337.9/	.32944	,060
2375.00	18.0000	.7992	.87236	339.0/	.33057	.059
2375.00	17.0000		.87952	340.17	.33175	.058
2375.00	16.0000	.8561	.88664	341.26	.33299	.056
2375.00	15.0000	.9206			.33429	.055
2375.00	14.0000	.9943	.89375	342.36		
2375.00	13.0000	1.0793	.90086	343.46	.33567	.054
2375.00	12.0000	1.1785	.90799	344.56	.33/14	.053
2375.00	11.0000	1.2958	.91515	345.66	.33872	.051
2375.00	10.0000	1.4366	.92236	346.77	.34042	.050
2375.00	9.0000	1.6088	.92963	347.88	.34227	.049

APPENDIX B

THERMODYNAMIC PROPERTIES OF CESIUM VAPOR (cont'd)

t	P	$v^g$	8	hg.	8.9	og p
2375.00	8.0000	1.8242	.93698	349.00	.34430	.048
2375.00	7.0000	2.1013	.94442	350.12	.34658	.046
2375.00	6.0000	2.4711	. 95196	351.24	.34916	.045
2375.00	5.0000	2.9892	.95962	352.38	.35216	.044
2375.00	4.0000	3./668	.96740	353.51	.35578	.042
2375.00	3.0000	5.0635	.97533	354.66	.36036	.041
2375.00	2.0000	7.6581	. 98340	355.81	.36670	.040
2375.00	1.0000	15.4443	.99162	356.96	.37734	.038
2375.00	.8000	19.3378	.99328	35/.20	.38073	
2375.00	.6000	25.8271	.99495	357.43	.38509	.038
375.00	.4000	38.8059	.99663	357.66	.39121	.038
375.00	.2000	77./430	.99831	357.89	.40162	.038
400.00	34.0000	.3460	.74878	321.52		.037
400.00	33.0000	.3599	.75598		.31593	.076
400.00	32.0000	.3749		322.66	.31666	.075
2400.00	31.0000	.3909	.76350	323.81	.31/42	.074
400.00	30.0000	.4080		324.9/	.31819	.073
400.00	29.0000		.77908	326.13	.31897	.073
		.4264	.78699	327.28	.31977	.071
400.00	28.0000	.4461	.79489	328.43	.32059	.070
400.00	27.0000	.4671	.80274	329.58	.32142	.069
400.00	26.0000	.4898	.81051	330.71	.32227	.068
400.00	25.0000	.5142	.81820	331.83	.32314	.067
400.00	24.0000	.5406	.82578	332.94	.32403	.066
400.00	23.0000	.5692	.83325	334.05	.32495	.065
400.00	22.0000	.6004	.84062	335.15	.32589	.064
400.00	21.0000	.6344	.84789	336.23	.32685	.062
400.00	20.0000	.6718	.85507	337.32	.32/85	.061
400.00	19.0000	.7130	.86216	338.39	.32889	.060
400.00	18.0000	./587	.86919	339.47	.32996	.059
2400,00	17.0000	.8098	.87616	340.54	.33108	.058
400.00	16.0000	.8672	.88309	341.61	.33225	.057
400.00	15.0000	.9323	.88999	342.67	.33348	.056
400.00	14.0000	1.0066	.89688	343.74	.33478	.054
400.00	13.0000	1.0923	.90377	344.81	.33615	.053
400.00	12.0000	1.1924	.91068	345.88	.33761	.052
400.00	11.0000	1.3107	.91762	346,95	.33917	.051
400.00	10.0000	1.4528	.92462	348.03	.34086	.050
400.00	9.0000	1.6265	.93107	349.11	.34270	.048
400.00	8.0000	1.8438	.93880	350.19	.34472	.047
400.00	7.0000	2.1234	.94602	351.28	.34699	.046
400.00	6.0000	2.4965	.95334	352.38		
400.00	5.0000	3.0192	.96077	353.48	.34956	.045
400.00	4.0000	3.8037	.96833		.35255	.043
400.00	3.0000	5.1119	.97603	354.58	.35615	.042
400.00	2.0000	7./294		355.69	.36072	.041
			.98386	356.81	.36705	.040
400.00	1.0000	15.5843	.99185	357.93	.3/768	.038
	.8000	19.5121	.99347	358.16	.38107	.038
400.00	.6000	26.0586	.99509	358.39	.38543	.038
400.00	.4000	39.1519	.99672	358.61	.39154	.038
400.00	.2000	78.4323	.99836	358.84	.40195	.0378
425.00	34.0000	.3527	.75652	323.41	.31659	.075
425.00	33,0000	.3667	.76360	324.54	.31732	.0746
425.00	32.0000	.3818	.77094	325.67	.31806	.0738
425.00	31.0000	.3980	.77845	326.80	.31882	.0729
425.00	30.0000	.4153	.78605	327.94	.31960	.0719
425.00	29.0000	.4338	.79369	329.07	.32039	.0708
425.00	28.0000	.4536	.80131	330.19	.32120	.069/
425.00	27.0000	.4748	.80889	331.30	.32202	.0686
425.00	26.0000	.4977	.81638	332.41	.32287	.0675

APPENDIX B

THERMODYNAMIC PROPERTIES OF CESIUM VAPOR (cont'd)

	P	vg	a	hg.	88	cg p
2425.00	25.0000	.5223	.82379	333.50	.32373	.0664
2425.00	24.0000	.5489	. 83111	334.59	.32461	.0652
2425.00	23.0000	.5777	.83832	335.67	.32551	.0641
2425.00	22.0000	.6091	.84543	336./3	.32644	.0630
2425.00	21.0000	.6434	.85246	337.79	.32741	.0619
2425.00	20.0000	.6811	.85939	338.85	.32839	.0608
2425.00	19.0000	. /226	.86625	339.90	.32941	.0597
2425.00	18.0000	./688	.87305	340.94	.33048	
2425.00	17.0000	.8203	.87980	341.99		.0586
2425.00	16.0000	.8782	.88651		33159	.0575
2425.00	15.0000	.9438		343.03	.33275	.0564
2425.00			.89319	344.06	.33397	.0552
2425.00	14.0000	1.0188	.89987	345.10	.33525	.0541
		1.1053	.90655	346.14	.33661	.0530
2425.00	12.0000	1.2062	.91325	347.18	.33806	.0518
2425.00	11.0000	1.3256	.91999	348.23	.33962	.050/
2425.00	10.0000	1.4689	.92677	349.27	.34129	.0495
2425,00	9.0000	1.6442	.93362	350.32	.34312	.0484
2425.00	8.0000	1.8634	.94054	351.38	.34514	.0472
2425.00	7.0000	2.1455	.94755	352.44	.34739	.0460
2425.00	6.0000	2.5218	.95465	353.50	.34995	.0448
2425.00	5.0000	3.0491	.96188	354.57	.35293	.0436
2425.00	4.0000	3.8404	.96922	355.64	. 35652	.0424
2425.00	3.0000	5.1601	.97670	356.73	.36108	
2425.00	2.0000	7.8005	.98431	35/.81		.0412
2425.00	1.0000	15./241	.99208		.36740	.0400
2425.00	.8000	19.6862		358.90	.37802	.0388
2425.00			.99365	359.12	.38141	.0385
2425.00	.6000	26.2900	.99523	35 34	.38576	.0383
	.4000	39.4978	.99681	359.56	.39187	.0380
2425.00	.2000	79.1216	.99840	359.78	.40228	.0378
2450.00	34.0000	.3593	.76403	325.28	.31724	.0744
2450.00	33.0000	. 3735	.77096	326.39	.31796	.0736
2450.00	32.0000	.3887	./7811	327.50	.31870	.0728
2450.00	31.0000	.4050	.78539	328.61	.31945	.0718
2450.00	30.0000	.4225	.79275	329./2	.32022	.0708
2450.00	29.0000	.4411	.80012	330.82	.32100	.069/
2450.00	28.0000	.4610	.80748	331.92	.32180	.0686
2450.00	27.0000	.4824	.81478	333.01	.32261	
2450.00	26.0000	.5054	.82201	334.08		.0675
2450.00	25.0000	.5302	.82916		.32344	.0664
2450.00	24.0000	.5570		335.15	.32429	.0653
450.00	23.0000		.83621	336.21	.32516	.0642
2450.00		.5861	.84317	337.26	.32606	.0531
	22.0000	.6177	.85004	338.30	.32698	.0620
450.00	21.0000	.6523	.85682	339.33	.32793	.0609
450.00	20.0000	.6903	.86353	340.36	.32891	.0599
450.00	19.0000	./322	.87017	341.38	.32992	.0588
450.00	18.0000	./787	.87675	342.40	.33098	.0577
450.00	17.0000	.8306	.88328	343.41	.33208	.0567
450.00	16.0000	.8891	.88978	344.42	.33323	.0556
450.00	15.0000	.9552	.89626	345.44	.33444	.0545
2450.00	14.0000	1.0309	.90273	346.45	.33572	
450.00	13.0000	1.1181	.90921	347.46		.0534
2450.00	12.0000	1.2200	.91571	348.47	.33707	.0523
2450.00	11.0000	1.3404	.92225		.33851	.0512
450.00	10.0000			349.49	.34905	.0501
2450.00		1.4849	.92883	350.50	.34172	.0490
	9.0000	1.6617	.93548	351.53	.34354	.0479
2450.00	8.0000	1.8829	.94220	352.55	.34554	.0468
2450.00	7.0000	2.1674	.94901	353.58	.34778	.0456
2450.00	6.0000	2.5470	.95591	354.62	.35033	.0445
2450.00	5.0000	3.0789	.96293	355.66	.35331	.0434
2450.00	4.0000	3.8771	.97007	356.70	.35689	

APPENDIX B

THERMODYNAMIC PROPERTIES OF CESIUM VAPOR (cont'd)

9/

t	P	v <sup>Q</sup>		h <sup>g</sup>	**	cg
2450.00	3.0000	5.2082	.97733	357.75	.36144	.041
2450.00	2.0000	7.8715	. 98474	358.81	.36775	.039
2450.00	1.0000	15.8638	.99229	359.87	.37835	.038
2450.00	.8000	19.8603	.99382	360.09	.38174	.038
2450.00	.6000	26.5213	.99536	360.30	.38609	.038
2450.00	.4000	39.8435	.99690	360.51	.39220	.038
2450.00	.2000	79.8107	.99845	360.73	.40261	
475.00	34.0000	.3658	.77130	327.13		.037
2475.00	33.0000	.3802	.77806		.31787	.073
2475.00	32.0000	.3956		328.22	.31858	.072
2475.00	31.0000		.78501	329.31	.31931	.071
2475.00		.4120	./9206	330.39	.32006	.070
	30.0000	.4295	.79917	331.48	.32082	.069
2475.00	29.0000	.4483	.80629	332.55	.32159	.068
475.00	28,0000	.4684	.81339	333.62	.32238	.067
2475.00	27.0000	.4900	.82043	334.68	.32318	.066
2475.00	26.0000	.5131	.82740	335.73	.32401	.065
475.00	25.0000	.5381	.83429	336.77	.32485	.064
475.00	24.0000	.5651	.84110	337.80	.32571	.063
475.00	23.0000	.5944	.84782	338.82	.32660	.062
475.00	22.0000	,6262	.85445	339.83	.32751	.061
475.00	21.0000	.6511	.86101	340.84	.32845	.060
475.00	20.0000	.6994	.86749	341.84	.32942	
475.00	19.0000	./416	.87391	342.84	.33042	.059
475.00	18.0000	./886	.88028			.057
475.00	17.0000	.8409	.88651	343.83	.33147	.056
475.00	16.0000	.8998		344.82	.33256	.055
475.00	15.0000		.89291	345.80	.33370	.054
		.9666	.89919	346.79	.33490	.053
475.00	14.0000	1.0429	.90547	347.77	.33617	.052
475.00	13.0000	1.1309	.91175	348.76	.33/51	.051
475.00	12.0000	1.2336	.91806	349.75	.33894	.050
475,00	11.0000	1.3550	.92441	350.73	.34048	.049
475.00	10.0000	1.5009	93080	351.72	.34214	.048
475.00	9.0000	1.6792	.93726	352.72	.34395	.047
475.00	8.0000	1.9022	.94379	353.72	.34594	.046
475.00	7.0000	2.1892	.95040	354.72	.34817	.045
475.00	6.0000	2.5721	.95712	355.73	.35071	.044
475.00	5.0000	3.1086	.96394	356.74	.35368	.043
475.00	4.0000	3.9137	.97088	357.75	.35725	.042
475.00	3.0000	5.2562	.97795	358.78	.36179	.040
475.00	2.0000	7.9425	.98515	359.81	.36809	.039
475.00	1.0000	16.0034	.99250	360.84	.37869	
475.00	.8000	20.0342	.99399	361.05	.38207	.038
475.00	.6000	26.7525				.038
475.00	.4000		.99548	361.26	.38642	.038
		40.1892	.99698	361.46	.39252	.038
475.00	.2000	80.4998	.99849	361.67	.40293	.037
500.00	34.0000	.3723	.77832	328.95	.31849	.072
500.00	33.0000	.3868	.78491	330.02	.31919	.071
500.00	32.0000	.4023	.79164	331.08	.31992	.070
500.00	31.0000	.4189	.79847	332.15	.32065	.069
500.00	30.0000	.4365	.80534	333.20	.32140	.068
500.00	29.0000	.4554	.81221	334.25	.32217	.067
500.00	28.0000	.4757	.81905	335.29	.32295	066
500.00	27.0000	.4974	.82584	336.33	.32374	.065
500.00	26.0000	.5207	.83256	337.35	.32456	.064
500.00	25.0000	.5459	.83921	338.36	.32539	.063
500.00	24.0000	.5731	.84578	339.37	.32624	
500.00	23.0000	.6026	.85227	340.36	.32712	.062
500.00	22.0000	.6347	.85868	341.35		.061
500.00	21.0000	.6698			.32802	.060
500.00	20.0000	.7084	.86502 .87129	342.33	.32895	.059
		./1109	-0/1/4	343.31	.32991	.058:

APPENDIX B

THERMODYNAMIC PROPERTIES OF CESIUM VAPOR (cont'd)

t	p	$v^g$	8	Ya.	89	$c_p^g$
2500.00	19.0000	.7510	.87750	344.28	.33091	.057
2500.00	18.0000	. /983	.88367	345.24	.33195	.056
2500.00	17.0000	.8512	.88980	346.21	.33303	.055
2500.00	16.0000	.9106	.89590	347.17	.33417	.054
2500.00	15.0000	.9779	.90200	348.13	.33536	.053
2500.00	14.0000	1.0548	.90809	349.09	.33661	
2500.00	13.0000	1.1436	.91419	350.04	.33/95	.052
2500.00	12.0000	1.2472	.92031	351.01	.33937	.051
2500.00	11.0000	1.3696	.92648	351.97	.34090	.0501
2500.00	10.0000	1.5167	.93269			.049
				352.93	.34255	.048
2500.00	9.0000	1.6966	.93895	353.90	.34435	.047
2500.00	8.0000	1.9215	.94531	354.8/	.34633	.0460
2500.00	7.0000	2.2110	.95174	355.85	.34856	.045
2500.00	6.0000	2.5972	.95827	356.83	.35109	.0439
2500.00	5.0000	3.1382	.96490	357.81	.35404	.0429
2500.00	4.0000	3.9502	.97165	358.80	.35760	.0416
2500.00	3.0000	5.3042	.97853	359.80	.36213	.0408
2500.00	2.0000	8.0133	.98554	360.80	,36842	.0397
2500.00	1.0000	16.1429	.99270	361.81	.37901	.038
2500.00	.8000	20.2081	.99415	362.01	.38240	.0384
2500.00	.6000	26.9836	.99560	362.21	.38674	.0382
2500.00	.4000	40.5348	.99706	362.41	.39285	.0380
2500.00	.2000	81.1888	.99853	362.62	.40325	.0376
2525.00	34.0000	.3787	.78509	330.75		
2525.00	33.0000	.3933	.79149	331.79	.31909	.0714
					.31979	.0709
2525.00	32.0000	.4090	.79802	332.83	.32051	.0699
2525.00	31.0000	.4256	.80462	333.8/	.32123	.0685
2525.00	30.0000	.4435	.81125	334.90	.32198	.0679
2525.00	29.0000	.4625	.81788	335.93	.32273	.0664
2525.00	28.0000	.4829	.82448	336.94	.32350	.0654
2525.00	27.0000	.5047	.83102	337.95	.32429	.0643
2525.00	26.0000	.5282	.83751	338.94	.32509	.0633
2525.00	25.0000	.5536	.84393	339.93	.32592	.0623
2525.00	24.0000	.5810	.85027	340.91	.32676	.0613
2525.00	23.0000	.6107	.85653	341.88	.32763	.0603
2525.00	22.0000	.6431	.86273	342.84	.32852	.0593
2525.00	21.0000	.6785	.86886	343.80	.32945	.0583
2525.00	20.0000	.7174	.87492	344.75	.33040	.0573
2525.00	19.0000	./603	.88094	345.70	.33139	.0564
2525.00	18.0000	.8080	.88691	346.64	.33242	
					The second secon	.0554
2525.00	17.0000	.8613	.89286	347.58	.33349	.0545
2525.00	16.0000	.9212	.89878	348.51	.33462	.0539
2525.00	15.0000	.9891	.90468	349.45	.33580	.0525
2525.00	14.0000	1.0666	.91060	350.38	.33705	.0516
2525.00	13.0000	1.1562	.91652	351.32	.33838	.0506
2525.00	12.0000	1.2606	.92247	352.25	.33979	.0496
2525.00	11.0000	1.3842	.92846	353.19	.34131	.0486
2525.00	10.0000	1.5325	.93449	354.13	.34295	.0477
2525.00	9.0000	1./139	.94059	355.07	.34474	.0467
2525.00	8.0000	1.9408	.94676	356.02	.34672	.0457
2525.00	7.0000	2.2327	.95302	356.97	.34893	.044/
2525.00	6.0000	2.6221	.95937	357.92	.35146	.0437
2525.00	5.0000	3.1677	.96582	358.88	.35440	.042/
2525.00	4.0000	3.9866	.97240	359.85	.35796	
	3.0000	5.3521	.97909	360.82		.0417
2525.00					.36248	.0407
2525.00	2.0000	8.0841	.98592	361.79	.36876	.0396
2525.00	1.0000	16.2824	.99289	362.77	.37934	.0386
2525.00	.8000	20.3819	.99430	362.97	.38272	.0384
2525.00	.6000	27.2146	.99571	363.17	.38706	.0382
2525.00	.4000	40.8803	.99714	363.36	.39317	.0380

APPENDIX B
THERMODYNAMIC PROPERTIES OF CESIUM VAPOR (cont'd)

t	p	vg		ħg.	89	c <sub>p</sub>
2525.00	.2000	81.8777	.99857	363.56	.40357	.037
2550.00	34.0000	.3850	.79161	332.52	.31968	.070
2550.00	33.0000	. 5998	.79782	333.54	.32037	.069
2550.00	32.0000	.4156	.80414	334.56	.32108	.068
2550.00	31.0000	.4324	.81052	335.57	.32180	.067
2550.00	30.0000	.4503	.81692	336.58	.32253	.066
2550.00	29.0000	.4695	.82331	337.57	.32328	.065
2550.00	28.0000	.4900	.82968	338.56	.32404	:064
550.00	27.0000	.5120	.83599	339.54	.32482	.063
550.00	26.0000	.5357	.84225	340.52	.32562	.062
550.00	25.0000	.5612	.84844	341.48	.32643	.061
550.00	24.0000	.5888	.85457	342.43	.32727	.060
550.00	23,0000	.6188	.86062	343.38	.32813	.059
550.00	22.0000	.6514	.86661	344.32	.32901	.058
550.00	21.0000	.6871	.87254	345.25	.32993	.057
550.00	20.0000	.7263	.87841	346.17	.33087	.056
550.00	19.0000	./696	.88424	347.10	.33186	.055
550.00	18.0000	.8177	.89003	348.01	.33288	.054
550.00	17.0000	.8714	.89579	348.93	.33394	.053
2550.00	16.0000	.9318	.90153	349.84	.33506	.052
550.00	15.0000	1.0002	.90726	350.75	.33624	.051
550.00	14.0000	1.0784	.91300	351.66	.33748	.051
550.00	13.0000	1.1687	.91875	352.5/	.33880	.050
550.00	12.0000	1.2740	.92453	353.49	.34020	.049
550.00	11.0000	1.3986	.93035	354.40	.34171	.048
550.00	10.0000	1.5482	.93622	355.32	.34334	.047
550.00	9.0000	1.7311	.94215	356.23	.34513	.046
550.00	8.0000	1.9599	.94816	357.16	.34710	.045
550.00	7.0000	2.2543	.95424	358.08	.34930	.044
550.00	6.0000	2.6470	.96042	359.01	.35182	.043
550.00	5.0000	3.1972	.96671	359.95	.35476	.042
550.00	4.0000	4.0229	.97311	360.89	.35830	.041
550.00	3.0000	5.3998	.97963	361.83	.36281	.040
550.00	2.0000	8.1548	.98628	362.78	.36909	.039
550.00	1.0000	16.4218	.99307	363.74	.37966	.038
550.00	.8000	20.5556	.99444	363.93	.38304	.038
550.00	.6000	27.4456	.99582	364.12	.38738	.038
550.00	.4000	41.2257	.99721	364.32	.39348	.038
2550.00	.2000	82.5665	.99860	364.51	.40389	.037

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Security Classification					
DOCUMENT (Security classification of title, body of abstract and i	CONTROL DATA - R&D		the overall report is classified)		
1. ORIGINATING ACTIVITY (Corporate author)		UNCLASSIFIED			
U.S. Naval Research Laboratory Washington, D.C. 20390	ERTIES OF CESIUM	UP			
3. REPORT TITLE HIGH-TEMPERATURE PROPER	ries of cesium				
A final report on the problem.	•)				
Ewing, C.T., Stone, J.P., Spann, and Miller, R.R.	J.R., Steinkuller, E	.w.,	Williams, D.D.,		
September 24, 1965		GES			
NASA C-76320 b. PROJECT NO. NRL Problem C05-15					
c. d.	9 b. OTHER REPORT NO(S) (Any other numbers that may be assisting report)				
Unlimited availability - Available	e at CFSTI - \$3.00				
11. SUPPLEMENTARY NOTES	NASA	ARY ACT	rivity		

13. ABSTRACT

The experimental program at this Laboratory to measure various thermophysical properties of sodium, potassium, and cesium has been completed. Final reports on two of the alkali metals, sodium and potassium, have been published; and this is the final reporting on cesium. Experimental results are presented for the density and vapor pressure of the liquid and for various saturation and superheat properties of the vapor. A virial equation of state is advanced and is used thermodynamically to derive additional properties of the vapor. For example, enthalpy, entropy, specific volume, and specific heat are tabulated for some 1100 selected vapor states in the temperature range from 1250° to 2550°F and in the pressure range from 0.2 to 34.0 atm.

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Security Classification

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•	LIN	LINK A		LINK B		LINK C	
KEY WORDS	ROLE	WT	ROLE	WT	ROLE	WT	
Cesium							
High-temperature properties							
Compressibility data							
Saturated vapor							
Superheated vapor							
Monomeric gas path							
Liquid path							
Virial equation of state							
Thermodynamic properties							
Thermophysical properties							
Association							
Liquid metals							

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