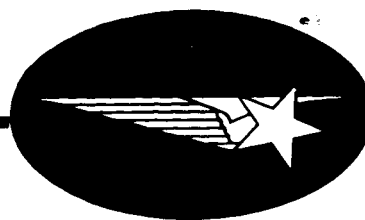


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JUNCTURE STRESS FIELDS IN MULTICELLULAR SHELL STRUCTURES

VOL. IV STRESSES AND DEFORMATIONS OF FIXED-EDGE SEGMENTAL SPHERICAL SHELLS

by
E. Y. W. TSUI
C. T. CHEN
P. STERN

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STRESSES AND DEFORMATIONS OF FIXED-EDGE
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Lockheed

MISSILES & SPACE COMPANY

A GROUP DIVISION OF LOCKHEED AIRCRAFT CORPORATION

SUNNYVALE, CALIFORNIA

SUMMARY

13836
This report presents a set of basic equations for thin elastic spherical shells and a digital program for the analysis of the static response of segmental spherical shells with fixed edges under the following loading conditions:

- Uniform pressure
- Linear thermal gradient through the thickness of shell

The problem is solved numerically by means of finite-difference technique, using a direct method of solving a large system of simultaneous equations. A numerical example showing the stresses and deformations of a spherical sector under uniform pressure is also presented. For completeness as a self-contained report, much of the information presented in Vol. II is repeated here.

Author

FOREWORD

This report is the result of a study on the numerical analysis of stresses and deformations of fixed-edge isotropic segmental spherical shells under uniform and hydrostatic pressures as well as linear thermal gradient across the thickness of the shell. Work on this study was performed by staff members of Lockheed Missiles & Space Company in cooperation with the George C. Marshall Space Flight Center of the National Aeronautics and Space Administration under Contract NAS 8-11480. Contract technical representative was H. Coldwater.

This volume is the fourth of a nine-volume final report of studies conducted by the department of Solid Mechanics, Aerospace Sciences Laboratory, Lockheed Missiles & Space Company. Project Manager was K. J. Forsberg; E. Y. W. Tsui was Technical Director for the work.

The nine volumes of the final report have the following titles:

- Vol. I Numerical Methods of Solving Large Matrices
- Vol. II Stresses and Deformations of Fixed-Edge Orthotropic Segmental Cylindrical Shells
- Vol. III Stresses and Deformations of Fixed-Edge Segmental Conical Shells
- Vol. IV Stresses and Deformations of Fixed-Edge Segmental Spherical Shells
- Vol. V Influence Coefficients of Segmental Shells
- Vol. VI Analysis of Multicellular Propellant Pressure Vessels by the Stiffness Method
- Vol. VII Buckling Analysis of Segmental Orthotropic Cylinders Under Uniform Stress Distribution
- Vol. VIII Buckling Analysis of Segmental Orthotropic Cylinders Under Non-uniform Stress Distribution
- Vol. IX Summary of Results and Recommendations

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NOTATION

| | |
|----------------------------------|--|
| $a_i, b_i, c_i, A, B, C, \kappa$ | nondimensional parameters defined in text |
| $D = Eh^3/12(1 - \nu^2)$ | flexural rigidity of shell |
| E | modulus of elasticity |
| F_i | boundary force at Station i |
| F^f | boundary forces of fixed-edge shell due to applied forces or thermal gradients |
| G | shear modulus |
| \hat{h} | thickness of shell |
| \bar{h}, \bar{k} | mesh spacings in ϕ - and θ -coordinate directions |
| m, n | number of columns and rows of the mesh |
| i, j | dummy subscripts |
| k, k_{ij} | stiffness influence coefficients |
| $\hat{M}_{()}, \hat{N}_{()}$ | moments and stress resultants |
| $p_{()}$ | surface or body forces |
| $\hat{Q}_{()}$ | transverse shears |
| R | radius of curvature |
| T | change of temperature from a zero thermal stress condition |
| $\hat{u}, \hat{v}, \hat{w}$ | displacement components in directions $\phi, \theta,$ and \hat{z} |
| ϕ, θ, \hat{z} | shell coordinates |

| | |
|--------------------------|--|
| α | coefficient of thermal expansion |
| ζ, η | orthogonal coordinates along boundaries of shell |
| δ_i | boundary deformations (displacements or rotations) at Station i |
| $\epsilon(), \gamma()$ | direct and shear strains |
| $\hat{\chi}()$ | changes of curvature or torsion of middle-surface |
| ν | Poisson's ratio |
| $\omega()$ | rotations of the normal at the middle-surface |
| $(), \phi$ | $\frac{\partial()}{\partial\phi}$ |
| $()_i^j$ | functions at a discrete point i, j where i, j implies the ϕ - and θ -directions respectively |
| Φ | rotation in the middle-surface around the normal |

Additional notations and symbols are defined in the text.

Section 1
INTRODUCTION

As a result of an investigation of juncture stress fields peculiar to the multicellular pressure vessels (Fig. 1), a theory for the prediction of the membrane and bending stresses and the corresponding deformations for such shell structures was formulated.*

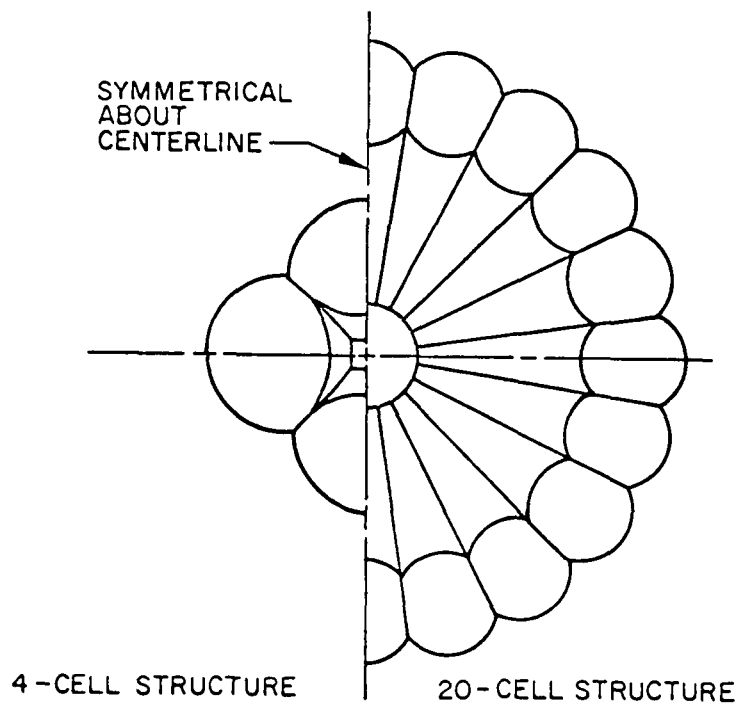


Fig. 1 Multicellular Shell Structure

*"Investigation of Juncture Stress Fields in Multicellular Shell Structures," by E. Y. W. Tsui, F. A. Brogan, J. M. Massard, P. Stern, and C. E. Stuhlman, Technical Report M-03-63-1, Lockheed Missiles & Space Company, Sunnyvale, Calif., Feb 1964 - NASA CR-61050.

Due to the fact that analytic solutions are still lacking, it was decided to solve the problem numerically by means of finite-difference technique. To ensure the feasibility of such a numerical solution, a direct method of solving large matrices with a high-speed digital computer was also developed.

According to the previous work, if the stiffness or displacement method is used, the total forces and hence the corresponding stresses along the juncture of the shell segments (Fig. 2) may be expressed concisely in the following matrix form

$$F = k\delta + F^f \quad (1.1)$$

where k is the stiffness matrix; δ , the deformations; and F^f , the fixed-end forces due to applied loads or thermal gradients. In view of this situation, it is logical to solve the problem systematically by the established general procedure of analysis already described.* This procedure may be stated briefly as follows:

1. Determination of the fixed-end forces, F^f , along the boundary as well as stresses and deformations in the interior of shell segments due to loads
2. Determination of the influence coefficients, k_{ij} , along the boundaries of shell segments, i. e., the induced forces at points i due to unit deformations ($\delta = 1$) at points j
3. Determination of the actual deformations, δ , along the shell boundaries; this requires the satisfaction of both compatibility and equilibrium conditions at the junctures of the structure

Once all the work involved in these three steps is completed, the total stresses and deformations in the specific discrete interior locations may be obtained.

*"Investigation of Juncture Stress Fields in Multicellular Shell Structures," by E. Y. W. Tsui, F. A. Brogan, J. M. Massard, P. Stern, and C. E. Stuhlman, Technical Report M-03-63-1, Lockheed Missiles & Space Company, Sunnyvale, Calif., Feb 1964 - NASA CR-61050.

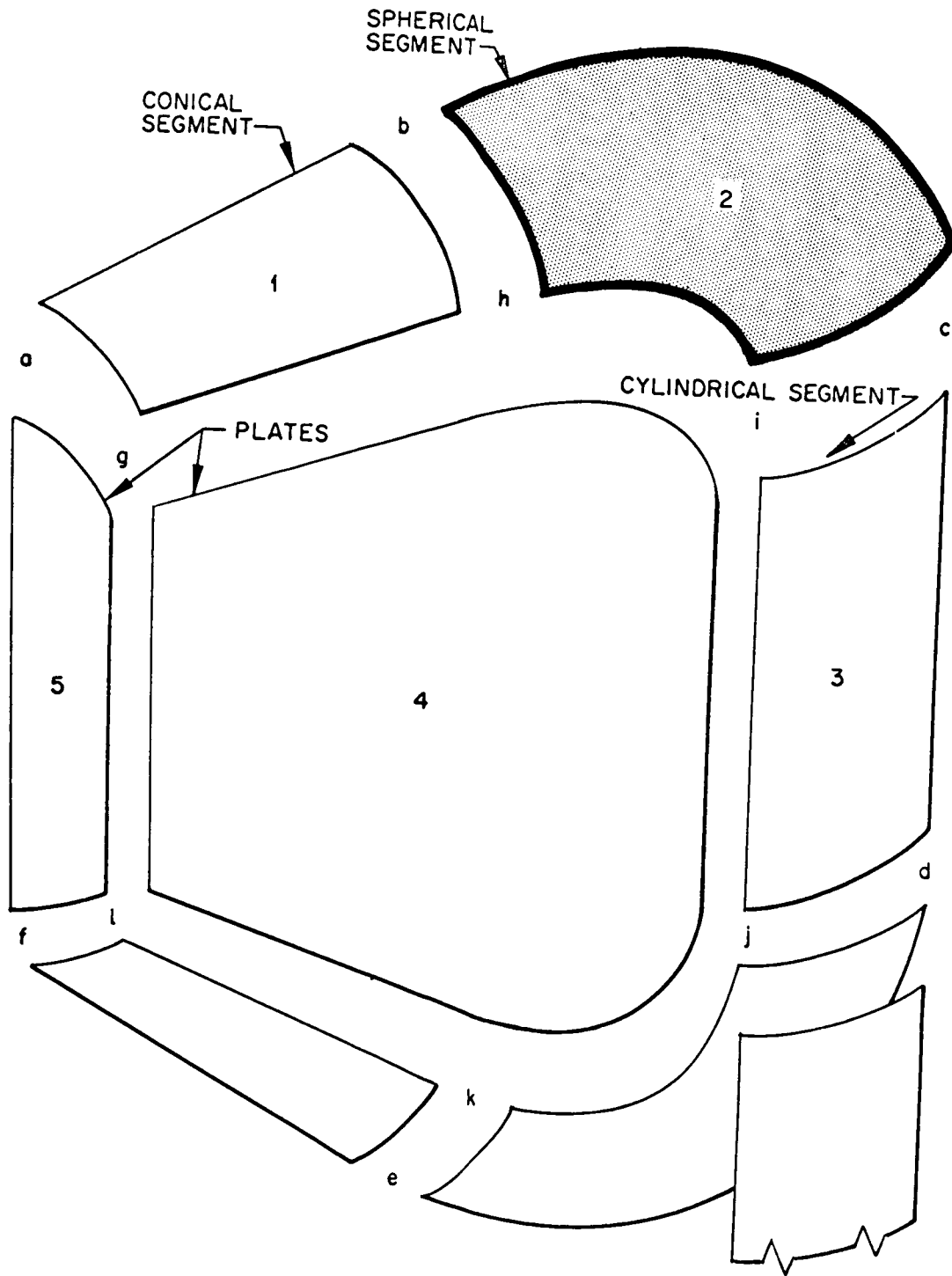


Fig. 2 Basic Shell Elements of Multicellular Structure

This volume presents results of the work involved in Step 1 only and covers the following items:

- Nondimensional formulation of the problem
- Detailed description of a workable digital program for the generation of solutions
- Example including tabulation of stresses and deformations of an isotropic spherical shell with fixed edges under uniform internal pressure

Section 2 FORMULATION OF THE PROBLEM

The necessary analytical expressions for a spherical shell have already been presented.* All the required equations are repeated in this report to make it a complete unit.

2.1 ANALYTICAL FORMULATION

The isotropic segmental spherical shell under consideration is of uniform thickness. It is bounded by a cylindrical panel, a segmental conical shell, and two radial plates as shown in Fig. 2. Only one half of the cell structure is shown in this figure because of the symmetry of the structure and the loading.

The geometry of the spherical segment is shown in Fig. 3. The orthogonal coordinates, ϕ and θ , can be oriented in a number of ways in the sphere so as to obtain a convenient description of the boundary curve. For example, in the orientation of Fig. 3 the intersection of the cylinder and sphere occurs at $\theta = 0$. It should be noted, however, that these coordinates are not parallel to all the intersections with the sphere.

In the formulation which follows the dependent variables and geometry have been non-dimensionalized by the radius of curvature, R , as follows:

$$u = \frac{\hat{u}}{R} \quad (2.1a)$$

*"Investigation of Juncture Stress Fields in Multicellular Shell Structures," by E. Y. W. Tsui, F. A. Brogan, J. M. Massard, P. Stern, and C. E. Stuhlman, Technical Report M-03-63-1, Lockheed Missiles & Space Company, Sunnyvale, Calif., Feb 1964 - NASA CR-61050.

$$v = \frac{\hat{v}}{R} \quad (2.1b)$$

$$w = \frac{\hat{z}}{R} \quad (2.1c)$$

$$z = \frac{\hat{z}}{R} \quad (2.1d)$$

$$h = \frac{\hat{h}}{R} \quad (2.1e)$$

Other nondimensional quantities will be defined as they are introduced. Note that the coordinates ϕ and θ have not been normalized.

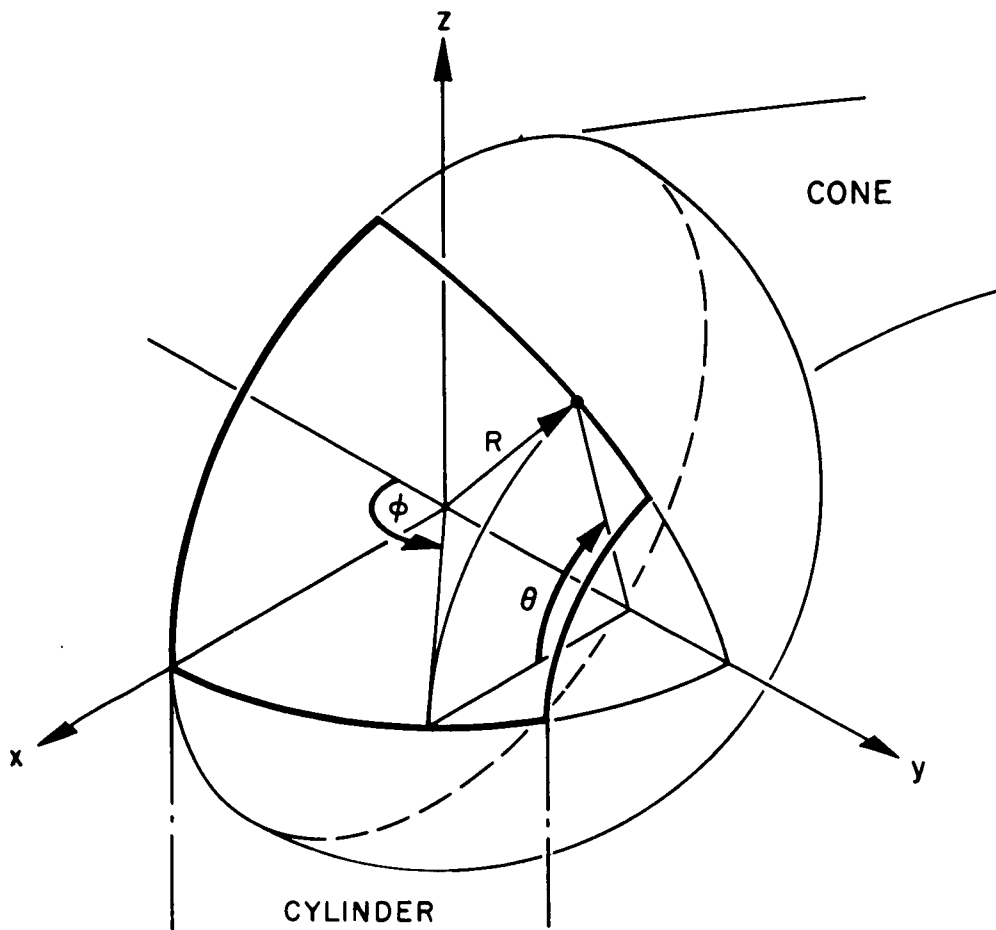


Fig. 3 Geometry of Segmental Spherical Shell

2.1.1 Rotation-Displacement Relations

Positive displacements and rotations of the middle-surface are shown in Fig. 4 and are related by equations:

$$\omega_{\phi} = u - w_{,\phi} \quad (2.2a)$$

$$\omega_{\theta} = v - \left(\frac{1}{\sin \phi}\right) w_{,\theta} \quad (2.2b)$$

$$\Phi = \frac{[v_{,\phi} - (1/\sin \phi)u_{,\theta} + \cot \phi v]}{2} \quad (2.2c)$$

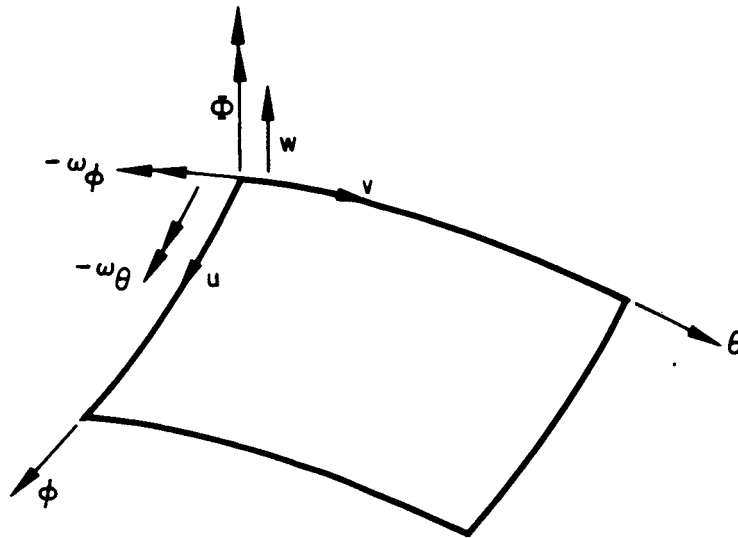


Fig. 4 Displacements and Rotations

2.1.2 Strain-Displacement Relations

The strains of the middle-surface are related to displacements by

$$\bar{\epsilon}_{\phi} = u_{,\phi} + w \quad (2.3a)$$

$$\bar{\epsilon}_{\theta} = \left(\frac{1}{\sin \phi}\right)v_{,\theta} + \cot \phi u + w \quad (2.3b)$$

$$\bar{\gamma}_{\phi\theta} = v_{,\phi} - \cot \phi v + \left(\frac{1}{\sin \phi}\right)u_{,\theta} \quad (2.3c)$$

and the changes of curvature and torsion are

$$\chi_{\phi} = [\hat{\chi}_{\phi} R] = u_{,\phi} - w_{,\phi\phi} \quad (2.4a)$$

$$\chi_{\theta} = [\hat{\chi}_{\theta} R] = \frac{[v_{,\theta} - (1/\sin \phi)w_{,\theta\theta} + (u - w_{,\phi}) \cos \phi]}{\sin \phi} \quad (2.4b)$$

$$\chi_{\phi\theta} = [\hat{\chi}_{\phi\theta} R] = \frac{[-w_{,\phi\theta} + \cot \phi w_{,\theta} + u_{,\theta} + \sin \phi v_{,\phi} - \cos \phi v]}{\sin \phi} \quad (2.4c)$$

The strains at a distance z from the middle-surface are

$$\epsilon_{\phi} = \bar{\epsilon}_{\phi} + z\chi_{\phi} \quad (2.5a)$$

$$\epsilon_{\theta} = \bar{\epsilon}_{\theta} + z\chi_{\theta} \quad (2.5b)$$

$$\gamma_{\phi\theta} = \bar{\gamma}_{\phi\theta} + 2z\chi_{\phi\theta} \quad (2.5c)$$

2.1.3 Constitutive Relations

Positive stress resultants are shown in Fig. 5. Nondimensional stress resultants are related to them and to strains by the following equations:

$$N_{\phi} = \left[\frac{\hat{N}_{\phi}(1 - \nu^2)}{E\hat{h}} \right] = \bar{\epsilon}_{\phi} + \nu\bar{\epsilon}_{\theta} + N^T \quad (2.6a)$$

$$N_{\theta} = \left[\frac{\hat{N}_{\theta}(1 - \nu^2)}{E\hat{h}} \right] = \bar{\epsilon}_{\theta} + \nu\bar{\epsilon}_{\phi} + N^T \quad (2.6b)$$

$$N_{\theta\phi} = N_{\phi\theta} = \left(\frac{\hat{N}_{\phi\theta}}{\hat{h}G} \right) = \bar{\gamma}_{\phi\theta} + 2\kappa\chi_{\phi\theta} \quad (2.6c)$$

$$M_{\phi} = \left(\frac{\hat{M}_{\phi}R}{D} \right) = \chi_{\phi} + \nu\chi_{\theta} + M^T \quad (2.6d)$$

$$M_{\theta} = \left(\frac{\hat{M}_{\theta}R}{D} \right) = \chi_{\theta} + \nu\chi_{\phi} + M^T \quad (2.6e)$$

$$M_{\phi\theta} = M_{\theta\phi} = \left[\frac{\hat{M}_{\phi\theta}R}{(1 - \nu)D} \right] = \chi_{\phi\theta} \quad (2.6f)$$

$$Q_{\phi} = \left(\frac{\hat{Q}_{\phi}R^2}{D} \right) = \chi_{\phi,\phi} + \nu\chi_{\theta,\phi} + (1 - \nu) \cot \phi (\chi_{\phi} - \chi_{\theta}) + \left[\frac{(1 - \nu)}{\sin \phi} \right] \chi_{\phi\theta,\phi} + M^T_{,\phi} \quad (2.6g)$$

$$Q_{\theta} = \left(\frac{\hat{Q}_{\theta}R^2}{D} \right) = \chi_{\theta,\theta} + \nu\chi_{\phi,\theta} + 2(1 - \nu) \cot \phi \chi_{\phi\theta} + (1 - \nu)\chi_{\phi\theta,\phi} + M^T_{,\theta} \quad (2.6h)$$

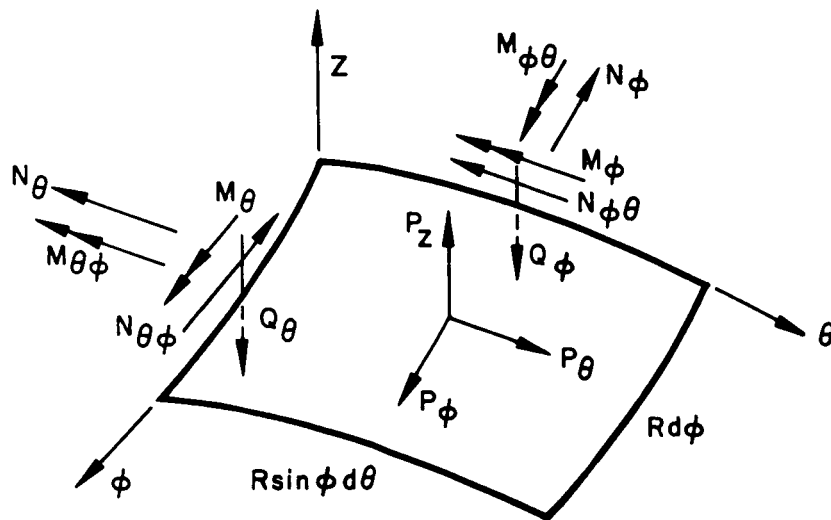


Fig. 5 Stress Resultants, Moments, and Loads

where

$$N^T = \left[\frac{\hat{N}^T (1 - \nu^2)}{E\hat{h}} \right] = -(1 + \nu) \frac{1}{\hat{h}} \int_{-h/2}^{h/2} \alpha T dz$$

$$M^T = \left(\frac{\hat{M}^T_R}{D} \right) = -12(1 + \nu) \frac{1}{\hat{h}^3} \int_{-h/2}^{h/2} \alpha T z dz$$

and T is temperature change relative to a zero thermal stress condition; α , the coefficient of thermal expansion; and $\kappa = h^2/12$.

2. 1. 4 Governing Differential Equations

The governing differential equations for a spherical shell in terms of displacement components u , v , and w are given by

$$a_1^{u, \phi\phi} + a_2^{u, \theta\theta} + a_3^{u, \phi} + a_4^u + a_5^{v, \phi\theta} + a_6^{v, \theta}$$

$$+ a_7^{w, \phi\phi\phi} + a_8^{w, \phi\theta\theta} + a_9^{w, \phi\phi} + a_{10}^{w, \theta\theta} + a_{11}^{w, \phi} = A \quad (2.7a)$$

$$b_1^{u, \phi\theta} + b_2^{u, \theta} + b_3^{v, \phi\phi} + b_4^{v, \theta\theta} + b_5^{v, \phi} + b_6^v$$

$$+ b_7^{w, \phi\phi\theta} + b_8^{w, \theta\theta\theta} + b_9^{w, \phi\theta} + b_{10}^{w, \theta} = B \quad (2.7b)$$

$$c_1^{u, \phi\phi\phi} + c_2^{u, \phi\theta\theta} + c_3^{u, \phi\phi} + c_4^{u, \theta\theta} + c_5^{u, \phi} + c_6^u$$

$$+ c_7^{v, \phi\phi\theta} + c_8^{v, \theta\theta\theta} + c_9^{v, \phi\theta} + c_{10}^{v, \theta}$$

$$+ c_{11}^{w, \phi\phi\phi\phi} + c_{12}^{w, \phi\phi\theta\theta} + c_{13}^{w, \theta\theta\theta\theta}$$

$$+ c_{14}^{w, \phi\phi\phi} + c_{15}^{w, \phi\theta\theta} + c_{16}^{w, \phi\phi} + c_{17}^{w, \theta\theta}$$

$$+ c_{18}^{w, \phi} + c_{19}^w = C \quad (2.7c)$$

where

$$a_1 = (1 + \kappa) \sin \phi$$

$$a_2 = (1 + 4\kappa) \frac{1 - \nu}{2 \sin \phi}$$

$$a_3 = (1 + \kappa) \cos \phi$$

$$a_4 = - \frac{\cos^2 \phi + \nu \sin^2 \phi}{\sin \phi} (1 + \kappa)$$

$$a_5 = \frac{1 + \nu}{2} + (2 - \nu)\kappa$$

$$a_6 = - \frac{\cot \phi}{2} [3 - \nu + 2\kappa(3 - 2\nu)]$$

$$a_7 = - \kappa \sin \phi$$

$$a_8 = -(2 - \nu) \frac{\kappa}{\sin \phi}$$

$$a_9 = - \kappa \cos \phi$$

$$a_{10} = (3 - \nu) \frac{\kappa}{\sin \phi} \cot \phi$$

$$a_{11} = (1 + \nu) \sin \phi + \frac{\cos^2 \phi + \nu \sin^2 \phi}{\sin \phi} \kappa$$

$$b_1 = \frac{1 + \nu}{2} + (2 - \nu)\kappa$$

$$b_2 = \left[\frac{3 - \nu}{2} + (3 - 2\nu)\kappa \right] \cot \phi$$

$$b_3 = \frac{1 - \nu}{2} (1 + 4\kappa) \sin \phi$$

$$b_4 = \frac{1 + \kappa}{\sin \phi}$$

$$b_5 = \frac{1 - \nu}{2} (1 + 4\kappa) \cos \phi$$

$$b_6 = \frac{1 - \nu}{2} \left(\frac{\sin^2 \phi - \cos^2 \phi}{\sin \phi} \right) (1 + 4\kappa)$$

$$b_7 = -(2 - \nu)\kappa$$

$$b_8 = -\frac{\kappa}{\sin^2 \phi}$$

$$b_9 = -\kappa \cot \phi$$

$$b_{10} = (1 + \nu) - 2\kappa(1 - \nu)$$

$$c_1 = \sin \phi$$

$$c_2 = \frac{2 - \nu}{\sin \phi}$$

$$c_3 = 2 \cos \phi$$

$$c_4 = \frac{\cos \phi}{\sin^2 \phi}$$

$$c_5 = - \left(\frac{1 + \nu \sin^2 \phi}{\sin \phi} + \frac{1 + \nu}{\kappa} \sin \phi \right)$$

$$c_6 = \left(1 - \nu - \frac{1 + \nu}{\kappa} + \frac{1}{\sin^2 \phi} \right) \cos \phi$$

$$c_7 = 2 - \nu$$

$$c_8 = \frac{1}{\sin^2 \phi}$$

$$c_9 = - \cot \phi$$

$$c_{10} = \left[2(1 - \nu) - \frac{1 + \nu}{\kappa} + \frac{1}{\sin^2 \phi} \right]$$

$$c_{11} = - \sin \phi$$

$$c_{12} = - \frac{2}{\sin \phi}$$

$$c_{13} = - \frac{1}{\sin^3 \phi}$$

$$c_{14} = - 2 \cos \phi$$

$$c_{15} = 2 \frac{\cos \phi}{\sin^2 \phi}$$

$$c_{16} = \frac{1 + \nu \sin^2 \phi}{\sin \phi}$$

$$c_{17} = -\frac{4 - (1 + \nu) \sin^2 \phi}{\sin^3 \phi}$$

$$c_{18} = -\left(1 - \nu + \frac{1}{\sin^2 \phi}\right) \cos \phi$$

$$c_{19} = -2 \frac{1 + \nu}{\kappa} \sin \phi$$

In general, the loading functions are

$$A = -\sin \phi \left[(1 - \nu^2) \frac{p_\phi R}{E \hat{h}} + N_{,\phi}^T + \kappa M_{,\phi}^T \right] \quad (2.8a)$$

$$B = -\left[(1 - \nu^2) p_\theta R \frac{\sin \phi}{E \hat{h}} + N_{,\theta}^T + \kappa M_{,\theta}^T \right] \quad (2.8b)$$

$$C = -\sin \phi \left[R^3 \frac{p_z}{D} - \frac{2N^T}{\kappa} + M_{,\phi\phi}^T + \cot \phi M_{,\phi}^T + \left(\frac{1}{\sin^2 \phi} \right) M_{,\theta\theta}^T \right] \quad (2.8c)$$

As mentioned in Sec. 4, the digital computer program which has been prepared has two options for loading. Specialization of the loading functions for each of these options follows:

- Uniform pressure

$$A = B = 0$$

$$C = -\sin \phi \frac{R^2 p_z}{D} = -\sin \phi$$

This will yield solutions normalized by $R^3 p_z / D$. For a given pressure, modulus, and value of Poisson's ratio this quantity can be found. The values of the dimensional dependent variables, \hat{u} , \hat{v} , and \hat{w} , can be

computed from the nondimensional u , v , and w , obtained from the computer solution as

$$\hat{u} = \left(\frac{R^4 p_z}{D} \right) u$$

$$\hat{v} = \left(\frac{R^4 p_z}{D} \right) v$$

$$\hat{w} = \left(\frac{R^4 p_z}{D} \right) w$$

- Linear thermal gradient through the thickness of the shell
For this special case T is given by

$$T = T_1 + T_2 z$$

where

$$T_1 = \frac{1}{2} (T_e + T_i) - 2T_o$$

$$T_2 = \frac{(T_e - T_i)}{h}$$

and

T_e = temperature at external surface $\left(z = \frac{h}{2} \right)$

T_i = temperature at internal surface $\left(z = -\frac{h}{2} \right)$

T_o = reference temperature

Then in nondimensional form

$$N^T = -(1 + \nu) \alpha T_1$$

$$M^T = -(1 + \nu) \alpha T_2$$

The loading functions in nondimensional form become

$$A = B = 0$$

$$C = -2 \sin \varphi \frac{(1 + \nu) \alpha T_1}{\kappa}$$

Dimensional displacements can be computed from the nondimensional solutions for u , v , and w through the relationships

$$\hat{u} = uR$$

$$\hat{v} = vR$$

$$\hat{w} = wR$$

2.2 BOUNDARY CONDITIONS

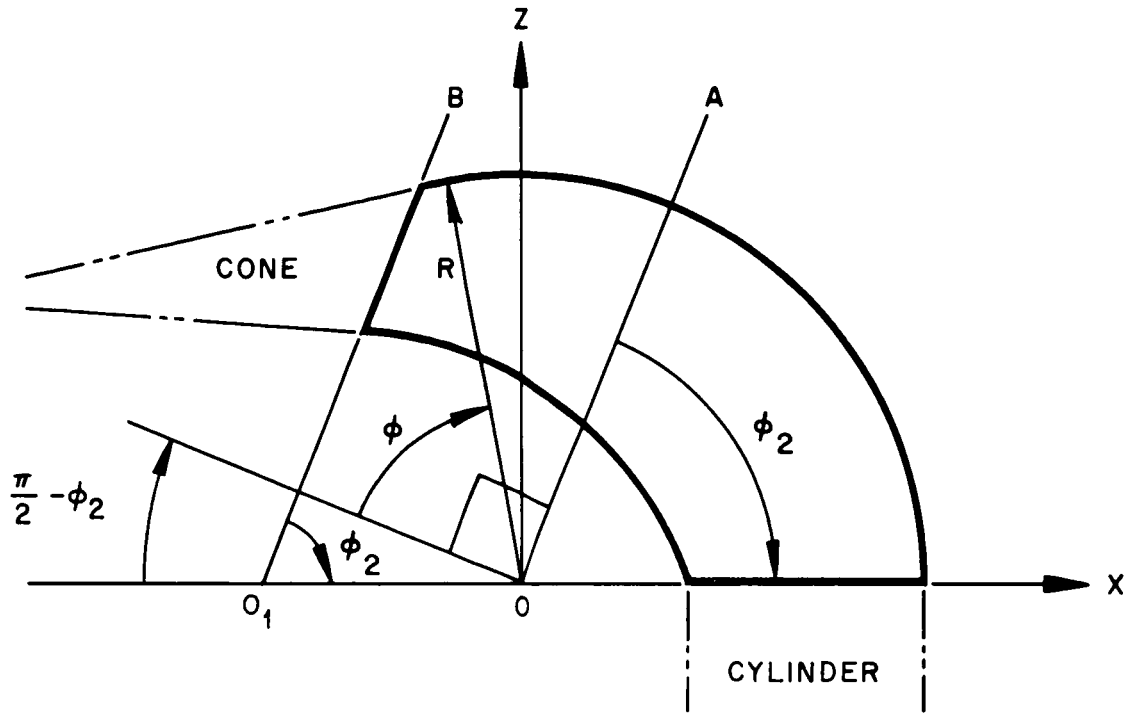
It was pointed out in Sec. 2.1 that the coordinates can be oriented so as to obtain a convenient description of the boundary curve. By such a description it is implied that the boundary is parallel or nearly parallel to coordinate lines. Two orientations of the orthogonal coordinates ϕ and θ are shown in Fig. 6. The coordinates in the two orientations are related to the rectangular coordinate system as follows:

Orientation 1

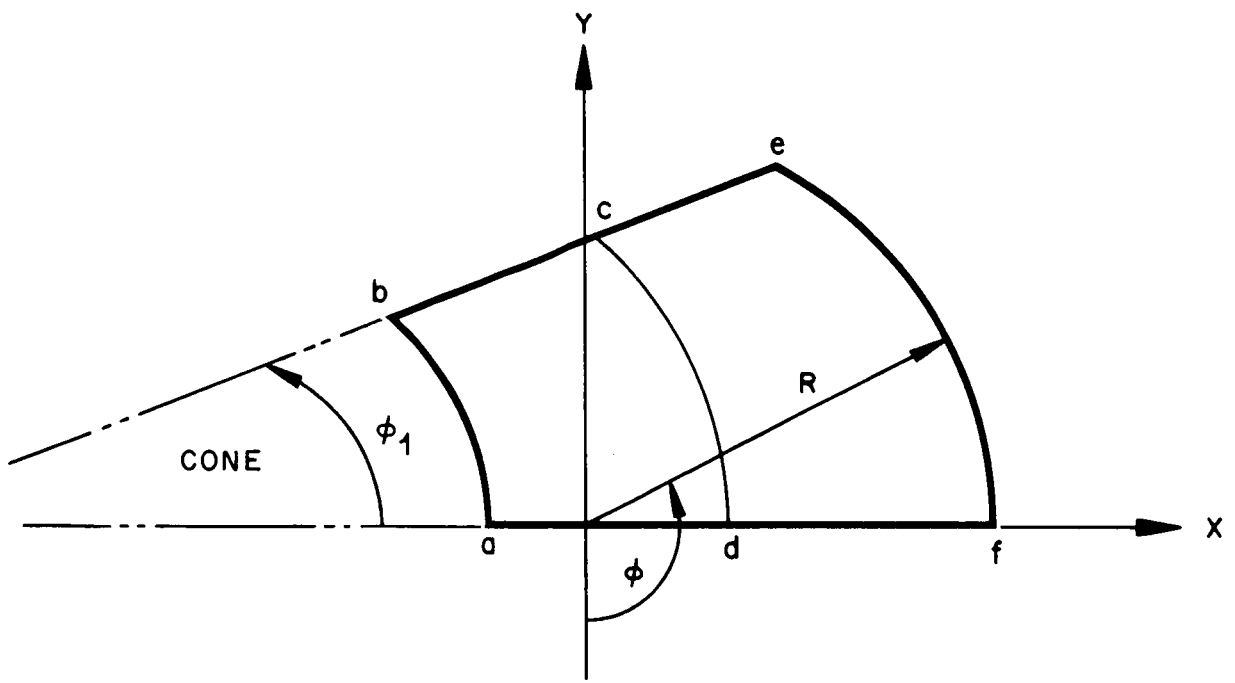
$$x = R(\sin \phi \cos \phi_2 \cos \theta - \cos \phi \sin \phi_2) \quad (2.9a)$$

$$y = R \sin \phi \sin \theta \quad (2.9b)$$

$$z = R(\cos \phi \cos \phi_2 + \sin \phi \cos \theta \sin \phi_2) \quad (2.9c)$$



Orientation 1 (Side View)



Orientation 2 (Top View)

Fig. 6 Orientations of Coordinate ϕ

Orientation 2

$$x = R \sin \phi \cos \theta \quad (2.10a)$$

$$y = -R \cos \phi \quad (2.10b)$$

$$z = R \sin \phi \sin \theta \quad (2.10c)$$

To use these orientations, consider the sphere cut as shown in Fig. 6 by the plane OA which is parallel to plane O_1B . That part of the sphere which is between the cone and plane OA is described by Orientation 1; the remaining portion, by Orientation 2. Thus, the sphere is divided into two parts each of which has two boundaries parallel to the curvilinear coordinates. The boundary curve and boundary conditions of Orientation 1 are given as shown in Fig. 7.

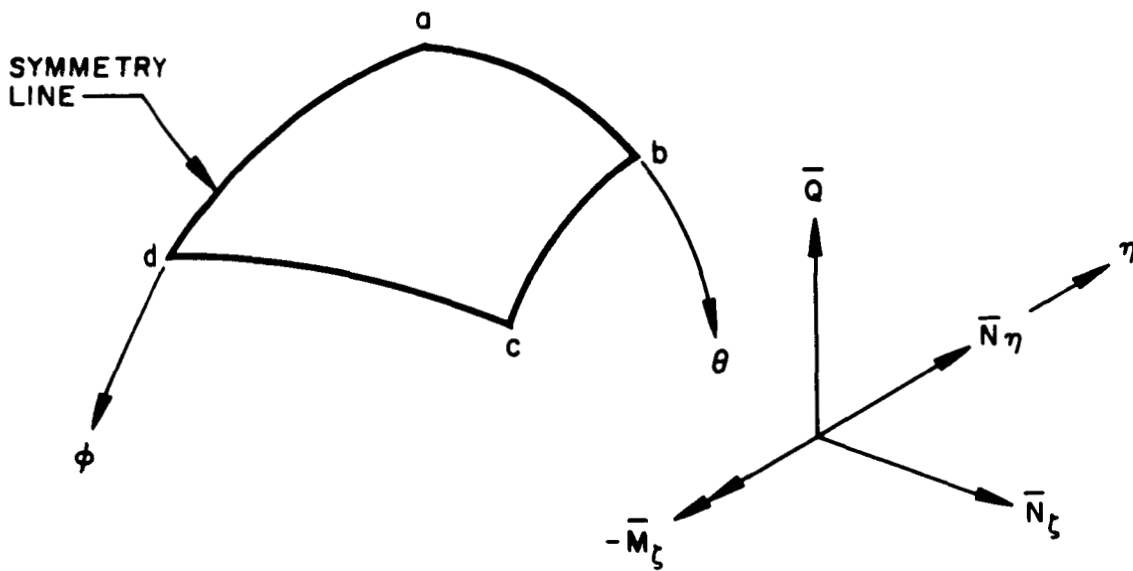


Fig. 7 Boundary Curve and Forces for Orientation 1

The boundary forces along the edges of the shell are given by the equations:

along \overline{ab}

$$\bar{N}_\eta = N_{\phi\theta} + 2\kappa M_{\phi\theta}$$

$$\bar{N}_\zeta = N_\phi$$

$$\bar{Q} = - \left[Q_\phi + \frac{(1 - \nu)}{\sin \phi} M_{\phi\theta, \theta} \right]$$

$$\bar{M}_\zeta = M_\phi$$

along \overline{cd}

$$\bar{N}_\eta = N_{\phi\theta} + 2\kappa M_{\phi\theta}$$

$$\bar{N}_\zeta = N_\phi$$

$$\bar{Q} = Q_\phi + \frac{(1 - \nu)}{\sin \phi} M_{\phi\theta, \theta}$$

$$\bar{M}_\zeta = M_\phi$$

along \overline{bc}

Since the curve \overline{bc} is not parallel to a coordinate line the boundary forces are given by the general expressions:

$$\hat{N}_\eta = \hat{N}_\eta + \frac{1}{R} \hat{M}_{\zeta\eta}$$

$$\hat{N}_\zeta = \hat{N}_\zeta$$

$$\hat{Q} = \hat{Q}_3 + \frac{1}{A_\eta} \frac{\partial \hat{M}_{\zeta\eta}}{\partial \eta}$$

$$\hat{M}_\zeta = \hat{M}_\zeta$$

where

$$\hat{N}_\zeta = \cos^2 \lambda \hat{N}_\theta + \sin^2 \lambda \hat{N}_\phi + \sin 2\lambda \hat{N}_{\phi\theta}$$

$$\hat{N}_\eta = \frac{1}{2} \sin 2\lambda (\hat{N}_\theta - \hat{N}_\phi) + (\sin^2 \lambda - \cos^2 \lambda) \hat{N}_{\phi\theta}$$

$$\hat{Q}_3 = \sin \lambda \hat{Q}_\phi + \cos \lambda \hat{Q}_\theta$$

$$\hat{M}_\zeta = \cos^2 \lambda \hat{M}_\theta + \sin^2 \lambda \hat{M}_\phi + \sin 2\lambda \hat{M}_{\phi\theta}$$

$$\hat{M}_{\zeta\eta} = \frac{1}{2} \sin 2\lambda (M_\theta - M_\phi) + (\sin^2 \lambda - \cos^2 \lambda) \hat{M}_{\phi\theta}.$$

The direction cosine must be found from the following intersection relations:

$$\cos \lambda = \pm \frac{1}{[f^2 \sin^2 \phi + 1]^{1/2}}$$

where λ is the angle between the boundary curve and the ϕ -axis and

$$f = \frac{\tan \phi_1}{\sin^2 \phi} \left[\frac{-(R_1/R - 1) \cos \phi + \sin \phi_2}{\cos \theta + \tan \phi_1 \cos \phi_2 \sin \theta} \right]$$

The relation between θ and ϕ is found by the relation

$$\sin \theta - \tan \phi_1 \cos \phi_2 \cos \theta = \frac{\tan \phi_1}{\sin \phi} \left[\left(\frac{R_1}{R} - 1 \right) - \sin \phi_2 \cos \phi \right].$$

For the spherical segment to have fixed edges, the displacement components are all zero. Hence, the required boundary conditions are as follows:

$$\overline{ab} \quad u \equiv v \equiv w \equiv \frac{\partial w}{\partial \phi} \equiv 0$$

$$\overline{bc} \quad u \equiv v \equiv w \equiv \frac{\partial w}{\partial \xi} \equiv 0$$

$$\overline{cd} \quad u \equiv v \equiv w \equiv \frac{\partial w}{\partial \phi} \equiv 0$$

The boundary curve and boundary condition of Orientation 2 are given as shown in Fig. 8.

The boundary forces along the edges of the shell are given by the equations:

along \overline{dc}

$$\bar{N}_\eta = -N_{\theta\phi} - 2\kappa M_{\phi\theta}$$

$$\bar{N}_\xi = N_\theta$$

$$\bar{Q} = Q_\theta + (1 - \nu)M_{\phi\theta, \phi}$$

$$\bar{M}_\xi = M_\theta$$

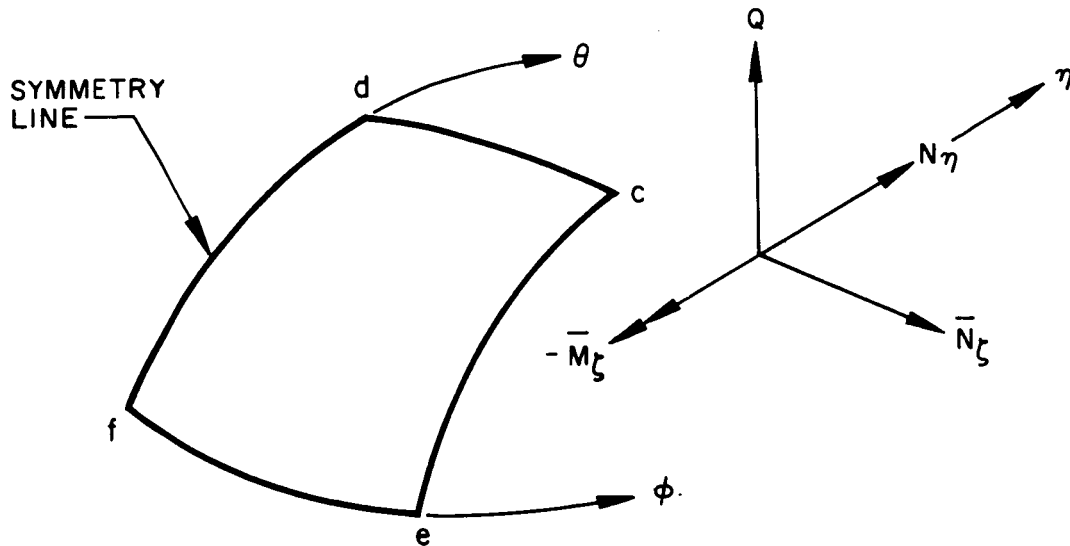


Fig. 8 Boundary Curve and Forces for Orientation 2

along \overline{ef}

$$\bar{N}_\eta = -N_{\theta\phi} - 2\kappa M_{\phi\theta}$$

$$\bar{N}_\zeta = N_\theta$$

$$\bar{Q} = -[Q + (1 - \nu)M_{\phi\theta,\phi}]$$

$$\bar{M}_\zeta = M_\theta$$

along \overline{ce}

The curve \overline{ce} is not parallel to a coordinate lines as was the case for line \overline{bc} for Orientation 1. Thus, the boundary forces are given by the general expressions:

$$\hat{N}_\eta = \hat{N}_\eta + \frac{1}{R} \hat{M}_{\zeta\eta}$$

$$\hat{N}_\zeta = \hat{N}_\zeta$$

$$\hat{Q} = \hat{Q}_3 + \frac{1}{A_\eta} \frac{\partial \hat{M}_{\zeta\eta}}{\partial \eta}$$

$$\hat{M}_\zeta = \hat{M}_\zeta$$

The quantities \hat{N}_η , \hat{N}_ξ , \hat{Q}_3 , \hat{M}_ξ , $\hat{M}_{\xi\eta}$ can be found by the equations given for Orientation 1, once $\cos \lambda$ is known. For the curve \overline{ce} , the relation between θ and ϕ is

$$\cos \theta = - \frac{[\cos \phi + \tan \phi_1 (R_1/R - 1)]}{\sin \phi \tan \phi_1}$$

The direction cosine is given by

$$\begin{aligned} \cos \lambda \\ = \pm \frac{\left\{ \tan^2 \phi_1 \sin^2 \phi - \left[\cos \phi + \tan \phi_1 (R_1/R - 1) \right]^2 \right\}^{1/2}}{\left\{ \left[1 + \tan \phi_1 (R_1/R - 1) \cos \phi \right]^2 + \tan^2 \phi_1 \sin^2 \phi - \left[\cos \phi + \tan \phi_1 (R_1/R - 1) \right]^2 \right\}^{1/2}} \end{aligned}$$

For the spherical segment, \overline{dcfe} , the boundary conditions for a fixed edge are as follows:

$$\overline{dc} \quad u \equiv v \equiv w \equiv \frac{\partial w}{\partial \theta} \equiv 0$$

$$\overline{bc} \quad u \equiv v \equiv w \equiv \frac{\partial w}{\partial \xi} \equiv 0$$

$$\overline{cd} \quad u \equiv v \equiv w \equiv \frac{\partial w}{\partial \theta} \equiv 0$$

2.3 STRESS IN SKIN

Once the stress resultant and couples are known, the corresponding maximum and minimum stress of an isotropic shell can be computed by the relations:

$$\sigma_\phi = \frac{1}{h} \hat{N}_\phi \pm \frac{6}{h^2} \hat{M}_\phi \quad (2.11a)$$

$$\sigma_\theta = \frac{1}{h} \hat{N}_\theta \pm \frac{6}{h^2} \hat{M}_\theta \quad (2.11b)$$

This development is based on the assumption of a linear stress variation through the thickness given by

$$\sigma_i = \bar{\sigma}_i + z\sigma_i^b$$

where $\bar{\sigma}_i$ is a membrane stress and $z\sigma_i^b$ is the stress due to bending.

Section 3
NUMERICAL ANALYSIS

The finite-difference method is used to solve the governing equations of a spherical shell segment with fixed edges. The scheme in this numerical method is to replace the continuous problem of a continuous coordinate system by one defined at a finite number of coordinate points. To accomplish this discretization, the continuous two dimensional (ϕ, θ) domain of the spherical shell is covered by a uniform rectangular net as shown in Fig. 9. Lattice points of this net which are within the domain \tilde{D}

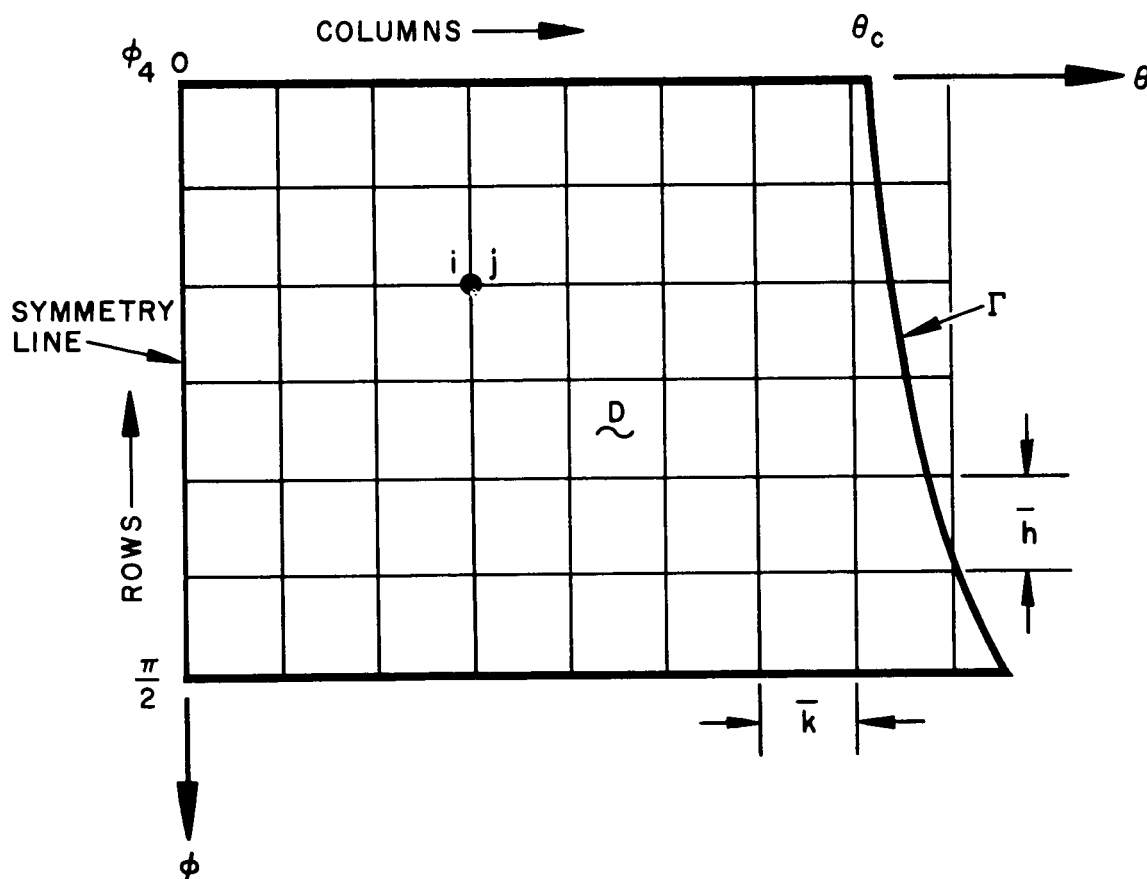


Fig. 9 Domain and Boundary of Spherical Shell Segment

are called mesh points, and lattice points on the boundary curve Γ are called boundary points. At these lattice points the dependent variables (u, v, w) of the governing differential equations are replaced by the discrete values of u_i^j, v_i^j, w_i^j . The subscript i of u_i^j denotes the row number and corresponds to the ϕ -coordinate while the superscript j denotes the column number and corresponds to the θ -coordinate. In general, the boundary curve does not coincide with the net as seen in Fig. 9. For the present numerical analysis, it is desirable to have the boundary curve coincide with the net so as to avoid computational complications. With the orthogonal coordinates ϕ, θ , it is not possible to have all the coordinate lines coincide exactly with the boundary. However, the coordinates can be orientated in such a manner that at least two boundary curves are parallel to coordinate lines. Two orientations are given in Sec. 2.2 which accomplish this objective. The domain shown in Fig. 9 corresponds to Orientation 1 which indicates the degree to which the actual boundary curve deviates from the rectangular net.

The difference equations which are a set of algebraic relations representing the governing equations and boundary conditions are formed by first approximating the derivatives at a given point by a function of the variable at neighboring points. These functions replace the derivatives of the governing equations. Thus, at each mesh point three algebraic equations can be written in terms of neighboring points. When the boundary conditions are accounted for in these equations the resulting set of simultaneous algebraic equations

$$\tilde{A}X = \tilde{B}$$

replaces the continuous problem. The solution of this set of algebraic equations can be accomplished by methods described in Vol. I.

3.1 APPROXIMATION OF DERIVATIVES

The derivatives of u, v, w are expressed in terms of their values at neighboring mesh points to transform the governing equations to difference form. These

derivatives are determined by a Taylor series approximation* for a rectangular net and are given by the following equations:

$$f_{,\phi} = 1/2\bar{h}(f_1^0 - f_{-1}^0) \quad (3.1a)$$

$$f_{,\phi\phi} = 1/\bar{h}^2(f_1^0 - 2f_0^0 + f_{-1}^0) \quad (3.1b)$$

$$f_{,\phi\phi\phi} = 1/2\bar{h}^3(f_2^0 - 2f_1^0 + 2f_{-1}^0 - f_{-2}^0) \quad (3.1c)$$

$$f_{,\phi\phi\phi\phi} = 1/\bar{h}^4(f_2^0 - 4f_1^0 + 6f_0^0 - 4f_{-1}^0 + f_{-2}^0) \quad (3.1d)$$

$$f_{,\theta} = 1/2\bar{k}(f_0^1 - f_0^{-1}) \quad (3.1e)$$

$$f_{,\theta\theta} = 1/\bar{k}^2(f_0^1 - 2f_0^0 + f_0^{-1}) \quad (3.1f)$$

$$f_{,\theta\theta\theta} = 1/2\bar{k}^3(f_0^2 - 2f_0^1 + 2f_0^{-1} - f_0^{-2}) \quad (3.1g)$$

$$f_{,\theta\theta\theta\theta} = 1/\bar{k}^4(f_0^2 - 4f_0^1 + 6f_0^0 - 4f_0^{-1} + f_0^{-2}) \quad (3.1h)$$

$$f_{,\phi\theta} = 1/4\bar{h}\bar{k}(f_1^1 - f_{-1}^1 - f_1^{-1} + f_{-1}^{-1}) \quad (3.1i)$$

$$f_{,\phi\phi\theta} = 1/2\bar{h}^2\bar{k}(-2f_0^1 + 2f_0^{-1} + f_1^1 + f_{-1}^1 - f_1^{-1} - f_{-1}^{-1}) \quad (3.1j)$$

*"Investigation of Juncture Stress Fields in Multicellular Shell Structures," by E. Y. W. Tsui, F. A. Brogan, J. M. Massard, P. Stern, and C. E. Stuhlman, Technical Report M-03-63-1, Lockheed Missiles & Space Company, Sunnyvale, Calif., Feb 1964 - NASA CR-61050.

$$f_{,\phi\theta\theta} = 1/2\bar{h}\bar{k}^{-2} \left(-2f_1^0 + 2f_{-1}^0 + f_1^1 + f_1^{-1} - f_{-1}^1 - f_{-1}^{-1} \right) \quad (3.1k)$$

$$f_{,\phi\phi\theta\theta} = 1/\bar{h}^2\bar{k}^{-2} \left(-2f_1^0 - 2f_{-1}^0 - 2f_0^1 - 2f_0^{-1} + f_1^1 + f_{-1}^1 + f_1^{-1} + f_{-1}^{-1} + 4f_0^0 \right) \quad (3.1l)$$

Lower order approximations to be used as noted

$$u_{,\phi\phi\phi} = 1/\bar{h}^3 \left(u_2^0 - 3u_1^0 + 3u_0^0 - u_{-1}^0 \right) \quad (3.1m)$$

$$u_{,\phi\phi\phi} = 1/\bar{h}^3 \left(u_1^0 - 3u_0^0 + 3u_{-1}^0 - u_{-2}^0 \right) \quad (3.1n)$$

$$v_{,\theta\theta\theta} = 1/\bar{k}^3 \left(v_0^1 - 3v_0^0 + 3v_0^{-1} - v_0^{-2} \right) \quad (3.1o)$$

3.2 DIFFERENCE EQUATIONS

The formation of the difference equations is effected in a straightforward manner by substituting the appropriate expressions of Eqs. (3.1) into the governing equation [Eqs. (2.7)]. Only when the equations are written one row or column from the boundary, the low-order third derivatives of u with respect to ϕ [Eqs. (3.1m and n)] or the third derivative of v with respect to θ [Eq. (3.1o)] are used to obtain a sufficient number of unknowns for the given number of equations. With these substitutions the three governing equations in difference form at a point $0, 0$ are as follows:

$$\begin{aligned} A_1 u_1^0 + A_2 u_{-1}^0 + A_3 (u_0^1 + u_0^{-1}) + A_4 u_0^0 + A_5 (v_1^1 - v_1^{-1} - v_{-1}^1 + v_{-1}^{-1}) \\ + A_6 (v_0^1 - v_0^{-1}) + A_7 (w_2^0 - w_{-2}^0) + A_8 w_1^0 + A_9 w_{-1}^0 + A_{10} (w_0^1 + w_0^{-1}) \\ + A_{11} (w_1^1 + w_1^{-1} - w_{-1}^1 - w_{-1}^{-1}) + A_{12} w_0^0 = A_0^0 \quad (3.2a) \end{aligned}$$

$$\begin{aligned}
& B_1(u_1^1 - u_{-1}^1 - u_1^{-1} + u_{-1}^{-1}) + B_2(u_0^1 - u_0^{-1}) + B_3v_1^0 + B_4v_{-1}^0 + B_5(v_0^1 + v_0^{-1}) \\
& + B_6v_0^0 + B_7(w_0^1 - w_0^{-1}) + B_8(w_1^1 - w_1^{-1}) + B_9(w_{-1}^1 - w_{-1}^{-1}) + B_{10}(w_0^2 - w_0^{-2}) = B_0^0
\end{aligned}
\tag{3.2b}$$

$$\begin{aligned}
& C_1(u_2^0 - u_2^0) + C_2u_1^0 + C_3u_{-1}^0 + C_4(-u_0^1 - u_0^{-1}) + C_5(u_1^1 - u_{-1}^1 + u_1^{-1} - u_{-1}^{-1}) \\
& + C_6u_0^0 + C_7(v_0^1 - v_0^{-1}) + C_8(v_1^1 - v_1^{-1}) + C_9(v_{-1}^1 - v_{-1}^{-1}) + C_{10}(v_0^2 - v_0^{-2}) \\
& + C_{11}w_2^0 + C_{12}w_{-2}^0 + C_{13}(w_0^2 + w_0^{-2}) + C_{14}w_1^0 + C_{15}w_{-1}^0 + C_{16}(w_0^1 + w_0^{-1}) \\
& + C_{17}(w_1^1 + w_1^{-1}) + C_{18}(w_{-1}^1 + w_{-1}^{-1}) + C_{19}w_0^0 = C_0^0
\end{aligned}
\tag{3.2c}$$

where

$$A_1 = \frac{a_1}{h^2} + \frac{a_3}{2h}$$

$$A_2 = \frac{a_1}{h^2} - \frac{a_3}{2h}$$

$$A_3 = \frac{a_2}{\bar{k}^2}$$

$$A_4 = a_4 - (A_1 + A_2) - 2A_3$$

$$A_5 = \frac{a_5}{4hk}$$

$$A_6 = \frac{a_6}{2k}$$

$$A_7 = \frac{a_7}{2\bar{h}^3}$$

$$A_8 = -2A_7 - 2A_{11} + \frac{a_9}{\bar{h}^2} + \frac{a_{11}}{2\bar{h}}$$

$$A_9 = 2A_7 + 2A_{11} + \frac{a_9}{\bar{h}^2} - \frac{a_{11}}{2\bar{h}}$$

$$A_{10} = \frac{a_{10}}{k^2}$$

$$A_{11} = \frac{a_8}{2\bar{h}k^2}$$

$$A_{12} = -\frac{2a_9}{\bar{h}^2} - 2A_{10}$$

$$A_0 = A$$

$$B_1 = \frac{b_1}{4\bar{h}k}$$

$$B_2 = \frac{b_2}{2k}$$

$$B_3 = \frac{b_3}{\bar{h}^2} + \frac{b_5}{2\bar{h}}$$

$$B_4 = \frac{b_3}{\bar{h}^2} - \frac{b_5}{2\bar{h}}$$

$$B_5 = \frac{b_4}{\bar{k}^2}$$

$$B_6 = -(B_3 + B_4) - 2B_5 + b_6$$

$$B_7 = \left(-\frac{b_7}{2\bar{h}^2\bar{k}} + \frac{b_{10}}{2\bar{k}} - \frac{b_8}{\bar{k}^3} \right)$$

$$B_8 = \left(\frac{b_7}{2\bar{h}^2\bar{k}} + \frac{b_9}{4\bar{h}\bar{k}} \right)$$

$$B_9 = \left(\frac{b_7}{2\bar{h}^2\bar{k}} - \frac{b_9}{4\bar{h}\bar{k}} \right)$$

$$B_{10} = \frac{b_8}{2\bar{k}^3}$$

$$B_0 = B$$

$$C_1 = \frac{c_1}{2\bar{h}^3}$$

$$C_2 = -2C_1 - 2C_5 + \frac{c_3}{\bar{h}^2} + \frac{c_5}{2\bar{h}}$$

$$C_3 = \frac{c_1}{\bar{h}^3} + \frac{c_2}{\bar{h}\bar{k}^2} + \frac{c_3}{\bar{h}^2} - \frac{c_5}{2\bar{h}}$$

$$C_4 = \frac{c_4}{\bar{k}^2}$$

$$C_5 = \frac{c_2}{2\bar{h}\bar{k}^2}$$

$$C_6 = -2\frac{c_3}{\bar{h}^2} - 2\frac{c_4}{\bar{k}^2} + c_6$$

$$C_7 = -\frac{c_7}{\bar{h}^2\bar{k}} - \frac{c_8}{\bar{k}^3} + \frac{c_{10}}{2\bar{k}}$$

$$C_8 = \frac{c_7}{2\bar{h}^2\bar{k}} + \frac{c_9}{4\bar{h}\bar{k}}$$

$$C_9 = \frac{c_7}{2\bar{h}^2\bar{k}} - \frac{c_9}{4\bar{h}\bar{k}}$$

$$C_{10} = \frac{c_8}{2\bar{k}^3}$$

$$C_{11} = \frac{c_{11}}{\bar{h}^4} + \frac{c_{14}}{2\bar{h}^3}$$

$$C_{12} = \frac{c_{11}}{\bar{h}^4} - \frac{c_{14}}{2\bar{h}^3}$$

$$C_{13} = \frac{c_{13}}{\bar{k}^4}$$

$$C_{14} = -4 \frac{c_{11}}{\bar{h}^4} - 2 \frac{c_{12}}{\bar{h}^2 \bar{k}^2} - \frac{c_{14}}{\bar{h}^3} - \frac{c_{15}}{\bar{h} \bar{k}^2} + \frac{c_{16}}{\bar{h}^2} + \frac{c_{18}}{2\bar{h}}$$

$$C_{15} = -4 \frac{c_{11}}{\bar{h}^4} - 2 \frac{c_{12}}{\bar{h}^2 \bar{k}^2} + \frac{c_{14}}{\bar{h}^3} + \frac{c_{15}}{\bar{h} \bar{k}^2} + \frac{c_{16}}{\bar{h}^2} - \frac{c_{18}}{2\bar{h}}$$

$$C_{16} = -2 \frac{c_{12}}{\bar{h}^2 \bar{k}^2} - 4 \frac{c_{13}}{\bar{k}^4} + \frac{c_{17}}{\bar{k}^2}$$

$$C_{17} = \frac{c_{12}}{\bar{h}^2 \bar{k}^2} + \frac{c_{15}}{2\bar{h} \bar{k}^2}$$

$$C_{18} = \frac{c_{12}}{\bar{h}^2 \bar{k}^2} - \frac{c_{15}}{2\bar{h} \bar{k}^2}$$

$$C_{19} = 6 \frac{c_{11}}{\bar{h}^4} + 4 \frac{c_{12}}{\bar{h}^2 \bar{k}^2} + 6 \frac{c_{13}}{\bar{k}^4} - 2 \frac{c_{16}}{\bar{h}^2} - 2 \frac{c_{17}}{\bar{k}^2} + c_{19}$$

$$C_o^o = C$$

The complete set of difference equations are obtained by writing these equations at each mesh point. Along lines of symmetry only two equations are necessary since one of the variables will be zero. After incorporation of fixed-edge boundary

conditions, a sufficient number of equations for unknowns yields a set of simultaneous algebraic equations which are written in matrix form as

$$\underline{A}X = \underline{B}$$

Unless care is exercised in ordering the equations and unknowns, the square matrix \underline{A} can be full. From the aspect of solving a large number of equations (Vol. I), the ordering is important. To establish an insight into the idea of the ordering employed, it is noticed from the difference expressions [Eqs. (3.1)] that the highest derivatives are in terms of at most two rows "above;" two rows "below;" two columns to the "left," and two columns to the "right" of a given mesh point. If all the equations for a given column were written and stored in submatrix form, the unknowns would involve two columns to the "right" and "left." Thus, any column would involve, at most, five submatrices. The matrix \underline{A} is accordingly partitioned in the manner shown below, where m is the number of columns in the finite-difference net.

$$\underline{A} = \begin{bmatrix} E_1 & F_1 & G_1 & \dots & & & & 0 \\ D_2 & E_2 & F_2 & G_2 & & & & \\ C_3 & D_3 & E_3 & F_3 & G_3 & 0 & & \\ \vdots & & & & & & & \\ & & & & & & & G_{n-2} \\ & & & & & & & F_{m-1} \\ & & & & & & & C_m & D_m & E_m \end{bmatrix}$$

This matrix \underline{A} is obtained by writing Eqs. (3.1) in \underline{D} and not on the boundary Γ . The boundary and symmetry conditions have been used to eliminate certain equations. Fixed-edge boundary conditions are well-suited for this formulation, since they do not require complex algebraic expressions. Specifically, if Eqs. (3.1) are written one column from the boundary, then the submatrix F_m is zero ($u = v = w = 0$)

and the submatrix G_m contains only w terms which are reflected into E_m due to the boundary condition. Along a symmetry line, all terms are either reflected with the same or opposite sign. This fact accounts for the missing C_1 and D_1 matrices. Similar alterations are made in each matrix to account for boundary and symmetry conditions.

Because of the boundary behavior of shells it is desirable to incorporate a means of decreasing the mesh spacing in order to reveal the boundary solution with greater detail and accuracy. A rather simple method called grading which does not destroy the form of matrix \tilde{A} is incorporated in the numerical solution. An explanation of grading was given in Vol. II, Sec. 3.3.

Section 4
DIGITAL PROGRAM

4.1 GENERAL DESCRIPTION

The present program provides solutions for fixed-edge spherical shell segments under loads and changes of temperature. The method of solution consists basically in obtaining the displacement components u , v , and w at various discrete stations of the structure by finite-difference approximation (see Secs. 2 and 3). The corresponding strains and stresses may then be computed.

The program is designed to compute the fixed-edge forces due to intermediate loads or thermal gradient. However, displacements, strains, and stresses in the loaded region are also evaluated simultaneously. The following program options are available:

- Finite-difference mesh
 - (a) Uniform spacing
 - (b) Graded spacing in the ϕ -direction
 - (c) Symmetry in the ϕ -direction
- Loading conditions
 - (a) Uniform normal pressure
 - (b) Linear temperature gradient through the skin thickness

There are no restrictions on the geometrical dimensions of panels. However, the accuracy with which the basic differential equations are approximated may vary for different configurations of the shell.

The finite-difference mesh network is specified completely by prescribing the number of rows and columns exclusive of the boundaries, together with the grading options which have been chosen. Rows in the finite-difference mesh are parallel to the

θ -direction, and columns are parallel to the ϕ -direction. The number of rows may vary from 4 to 24 and the number of columns from 4 to 80. Thus, a maximum of 5760 unknowns can be solved. Greater accuracy near the boundaries can often be obtained by selective grading. By this means, it is possible to use a mesh spacing at the boundary as little as 1/32 of that at the middle portion of the panel.

There are certain restrictions on the use of the grading option. When such an option is used, a separate input card is required to specify a mesh spacing exponent MM(J) for each row J. The finite-difference equations are written along Row J, then the mesh spacing $XH/2^{**}MM(J)$ is used. This distance must be the least of the two distances from Row J to the row above and the row below. XH is the basic input mesh spacing along the ϕ -direction. For any Row J. MM(J) and MM(J + 1) must not differ by more than 1. Also, three consecutive rows cannot have three distinct exponents. MM(J) may vary from 0 to 5.

The description of symbols and input data are shown in Tables 1 and 2; Fig. 10 shows the flow diagram of this program.

Table 1

DESCRIPTION OF SYMBOLS

| Symbol | | Description |
|--------------|---|--|
| RECORD | | Hollerith information describing problem |
| I ϕ PT1 | 0 | Uniform mesh spacing |
| | 1 | Graded mesh spacing in ϕ -direction |
| I ϕ PT2 | 0 | Symmetry in the ϕ -direction |
| | 1 | Row 1 is symmetry line |
| | 2 | Row 2 is adjacent to boundary |
| I ϕ PT3 | 0 | Omit shell strains |
| | 1 | Print shell strains |
| I ϕ PT4 | 0 | Uniform normal pressure |
| | 1 | Linear temperature gradient through the skin thickness |

Table 1 (cont'd)

| Symbol | | Description |
|--------------------------|---|---|
| I ϕ PT5 | 0 | Not last case with plots |
| | 1 | Last case with plots |
| R ϕ W | | Number of rows in the finite-difference mesh |
| C ϕ L | | Number of columns in the finite-difference mesh |
| XH | | Basic distance between rows in the mesh |
| XK | | Basic distance between columns in the mesh |
| ZNU | | Poisson's ratio |
| THC | | Half angle of segment θ_c |
| PH1 | | Angle ϕ of upper boundary |
| FF | | Ratio of angle of ϕ of lower boundary to ϕ of upper boundary |
| RH | | Radius to thickness ratio, R/h |
| TE | | External temperature |
| TI | | Internal temperature |
| T ϕ | | Ambient temperature for zero stress |
| ϕ C | | Coefficient of thermal expansion |
| MM(J), J = 1, R ϕ W | | Grading mesh constants, mesh spacing used for difference equations on Row J is equal to XH/2. **MM(J) |
| MM(31) | | Number of rows to be plotted |
| MM(32) | | Four row numbers for which plot output is desired |
| MM(33) | | (u, v, w, N $_{\phi}$, M $_{\phi}$, N $_{\theta}$, M $_{\theta}$) |
| MM(34) | | |
| MM(35) | | |
| CILBL(I, 1), I = 1, 6 | | Curve labels appearing on the plot output to identify the rows selected CILBL(I, 1) corresponds to MM(32); etc. |
| CILBL(I, 2), I = 1, 6 | | |
| CILBL(I, 3), I = 1, 6 | | |
| CILBL(I, 4), I = 1, 6 | | |

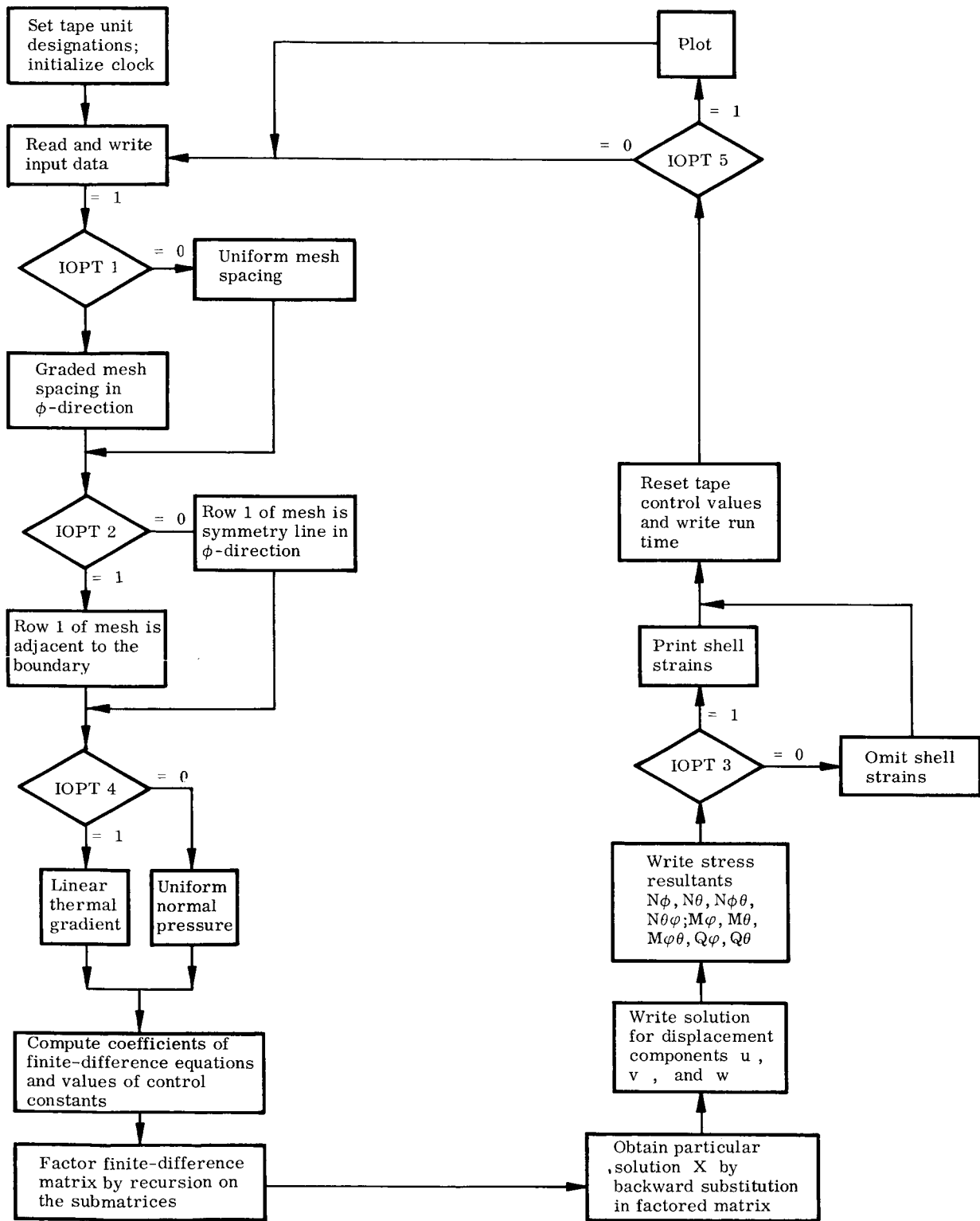


Fig. 10 Flow Chart

Table 2

INPUT DATA SEQUENCE AND FORMAT

| Card | FORTRAN Symbol | Format |
|-------------------|---|--------|
| 1 | RECORD | 72H |
| 2 | $I\phi PT1, I\phi PT2, I\phi PT3, I\phi PT4, I\phi PT5$ | 10I1 |
| 3 | $R\phi W, C\phi L, XH, XK$ | 3E12.8 |
| 4 | ZNU, THC, PH1, FF, RH | 6E12.8 |
| 5 ^(a) | $MM(J), J = 1, R\phi W$ | 35I2 |
| 6 ^(b) | TE, TI, $T\phi, \phi C$ | 4E12.8 |
| 7 | $MM(J), J = 31, 35$ | 5I2 |
| 8 ^(c) | $CILBL(I, 1), I = 1, 6$ | 6A6 |
| 9 ^(c) | $CILBL(I, 2), I = 1, 6$ | 6A6 |
| 10 ^(c) | $CILBL(I, 3), I = 1, 6$ | 6A6 |
| 11 ^(c) | $CILBL(I, 4), I = 1, 6$ | 6A6 |

(a) Omitted unless $I\phi PT1 = 1$.

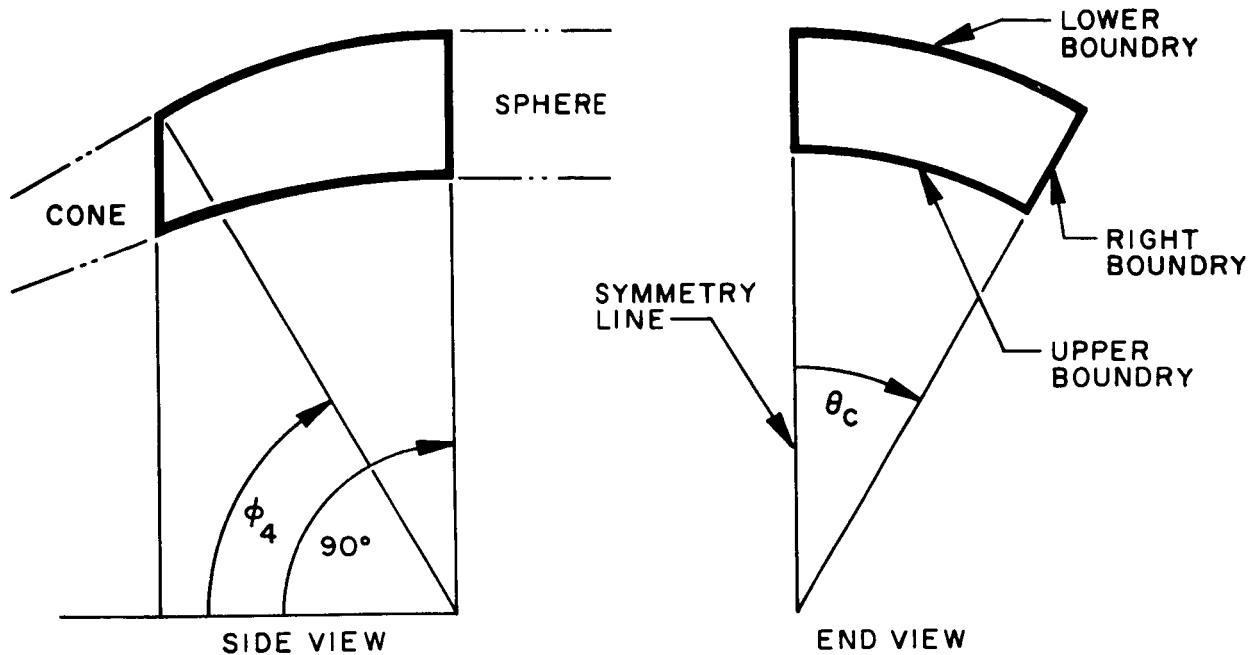
(b) Omitted unless $I\phi PT4 = 1$.

(c) Omitted if $MM(31) = 0$.

4.2 NUMERICAL EXAMPLE

Analysis of the spherical shell segment shown in Fig. 11 will serve as an example to illustrate input data, format, and the type of information that can be obtained through use of the program described in this volume.

The example is for the loading option of uniform normal pressure ($p_z = \text{constant}$). Grading is used in the ϕ -coordinate so as to obtain a reasonable solution with the present restrictions of the computer program (24 rows, 80 columns). The actual



$$\theta_c = \text{THC} = 0.61 \text{ RAD, US}$$

$$\phi_4 = \text{PHI} = 1.0297 \text{ RAD, US}$$

$$FF = \frac{\pi}{2} / 1.0297 = 1.5708$$

$$\frac{R}{h} = \text{RH} = 100$$

Fig. 11 Segmented Spherical Shell

mesh spacing which yields a solution of desired accuracy must be obtained by exploratory runs using different number of rows and columns. Such runs were made with the given geometry. It was found that 17 rows and 30 columns were required to obtain satisfactory results in both displacements and stress resultants. More accurate results can be obtained by use of an even finer mesh spacing.

Values of input quantities for the 17 by 30 case are given in Table 3 and a listing of the corresponding input data cards is presented in Table 4. For convenience, the ϕ -coordinate corresponding to the row number follows:

Table 3
INPUT VALUES FOR THE EXAMPLE

| Symbol | Value | Symbol | Value |
|--------------|----------|-----------------------------|---------------------|
| I ϕ PT1 | 1.0 | MM(8) | 0 |
| I ϕ PT2 | 1.0 | MM(9) | 0 |
| I ϕ PT3 | 0 | MM(10) | 0 |
| I ϕ PT4 | 0 | MM(11) | 1.0 |
| I ϕ PT5 | 1.0 | MM(12) | 1.0 |
| R ϕ W | 17.0 | MM(13) | 2.0 |
| C ϕ L | 30.0 | MM(14) | 2.0 |
| XH | 0.067635 | MM(15) | 2.0 |
| XK | 0.02033 | MM(16) | 3.0 |
| ZNU | 0.3 | MM(17) | 3.0 |
| THC | 0.61 | TE, TI, T ϕ , ϕ C | Not required |
| PH1 | 1.0297 | MM(31) | 4.0 |
| FF | 1.5255 | MM(32) | 5.0 |
| RH | 100.0 | MM(33) | 9.0 |
| MM(1) | 3.0 | MM(34) | 16.0 |
| MM(2) | 3.0 | MM(35) | 17.0 |
| MM(3) | 2.0 | CILBL(I, 1)I = 1,6 | PHI = 1.503, Row 5 |
| MM(4) | 2.0 | CILBL(I, 2)I = 1,6 | PHI = 1.300, Row 9 |
| MM(5) | 2.0 | CILBL(I, 3)I = 1,6 | PHI = 1.038, Row 16 |
| MM(6) | 1.0 | CILBL(I, 4)I = 1,6 | PHI = 1.029, Row 17 |
| MM(7) | 1.0 | | |

| | |
|----------------------------------|---------------------------------|
| $\phi = 1.0297 - \text{Row } 18$ | $\phi = 1.3679 - \text{Row } 8$ |
| $\phi = 1.0381 - \text{Row } 17$ | $\phi = 1.4355 - \text{Row } 7$ |
| $\phi = 1.0466 - \text{Row } 16$ | $\phi = 1.4693 - \text{Row } 6$ |
| $\phi = 1.0635 - \text{Row } 15$ | $\phi = 1.5031 - \text{Row } 5$ |
| $\phi = 1.0804 - \text{Row } 14$ | $\phi = 1.5200 - \text{Row } 4$ |
| $\phi = 1.0973 - \text{Row } 13$ | $\phi = 1.5369 - \text{Row } 3$ |
| $\phi = 1.1311 - \text{Row } 12$ | $\phi = 1.5539 - \text{Row } 2$ |
| $\phi = 1.1650 - \text{Row } 11$ | $\phi = 1.5623 - \text{Row } 1$ |
| $\phi = 1.2326 - \text{Row } 10$ | $\phi = 1.5703 - \text{Row } 0$ |
| $\phi = 1.3002 - \text{Row } 9$ | |

Results from the computer program are in the form of printed digital values and selected plots. Sample printed output given in Table 5 presents displacement components (u, v, w) , stress resultants $(N_\phi, N_\theta, N_{\theta\phi}, N_{\phi\theta}, M_\phi, M_\theta, M_{\phi\theta}, Q_\phi, Q_\theta)$, and boundary stress resultants $(N_{\text{tan}}, N_{\text{norm}}, Q, M)$. (Note that these quantities are in nondimensional form as defined in Sec. 2.) Plotted output includes displacement components (u, v, w) and stress resultants $(N_\phi, N_\theta, M_\phi, M_\theta)$ along Rows 1, 2, 10, and 16 and boundary stress resultants $(N_{\text{tan}}, N_{\text{norm}}, Q, M)$ along the boundary curve. This plotted output is shown in Figs. 12a through o.

Table 5

EXAMPLE SPHERICAL SEGMENT UNDER UNIFORM NORMAL PRESSURE

SPHERE DISPLACEMENT COMPONENTS (U,V,W)

| COL | ROW | U | V | W |
|-----|-----|---------------|---------------|--------------|
| 19, | 20 | 0. | 0. | 3.658652E-02 |
| 19, | 19 | -2.638945E-03 | 1.021954E-03 | 7.759879E-03 |
| 19, | 18 | BCUNDARY | 0. | 0. |
| 19, | 17 | 2.602412E-03 | -9.899542E-04 | 7.759879E-03 |
| 19, | 16 | 5.086261E-03 | -1.945970E-03 | 2.549251E-02 |
| 19, | 15 | 9.652772E-03 | -3.786246E-03 | 7.057005E-02 |
| 19, | 14 | 1.323534E-02 | -5.476061E-03 | 1.238788E-01 |
| 19, | 13 | 1.572938E-02 | -7.016443E-03 | 1.787364E-01 |
| 19, | 12 | 1.853742E-02 | -9.803262E-03 | 2.864289E-01 |
| 19, | 11 | 1.769688E-02 | -1.200326E-02 | 3.637405E-01 |
| 19, | 10 | 1.115614E-02 | -1.531577E-02 | 4.653016E-01 |
| 19, | 9 | -1.421190E-04 | -1.615930E-02 | 4.937291E-01 |
| 19, | 8 | -1.144092E-02 | -1.475764E-02 | 4.663140E-01 |
| 19, | 7 | -1.792110E-02 | -1.120068E-02 | 3.641097E-01 |
| 19, | 6 | -1.868753E-02 | -8.990277E-03 | 2.861686E-01 |
| 19, | 5 | -1.578401E-02 | -6.338675E-03 | 1.780603E-01 |
| 19, | 4 | -1.324659E-02 | -4.903025E-03 | 1.231290E-01 |
| 19, | 3 | -9.636059E-03 | -3.359861E-03 | 6.997208E-02 |
| 19, | 2 | -5.067179E-03 | -1.713557E-03 | 2.523418E-02 |
| 19, | 1 | -2.589518E-03 | -8.672638E-04 | 7.664569E-03 |
| 19, | -0 | BCUNDARY | 0. | 0. |
| 19, | -1 | 2.620010E-03 | 8.860647E-04 | 7.664569E-03 |
| 19, | -2 | 0. | 0. | 3.608237E-02 |

SPHERE STRESS RESULTANTS.

| ROW | COL | NX | NTHETA | NXTHETA | NTHETAX |
|-----|-----|------------|------------|------------|------------|
| 7, | 30 | 1.0666E-01 | 3.1256E-01 | 1.8012E-01 | 1.8012E-01 |
| 7, | 31 | 9.4004E-02 | 3.1335E-01 | 1.9175E-01 | 1.9175E-01 |
| 8, | 1 | 4.1548E-01 | 4.9208E-01 | 0. | 0. |
| 8, | 2 | 4.1553E-01 | 4.9204E-01 | 1.0850E-03 | 1.0850E-03 |
| 8, | 3 | 4.1566E-01 | 4.9192E-01 | 2.1802E-03 | 2.1802E-03 |
| 8, | 4 | 4.1588E-01 | 4.9173E-01 | 3.2953E-03 | 3.2953E-03 |
| 8, | 5 | 4.1619E-01 | 4.9145E-01 | 4.4417E-03 | 4.4417E-03 |
| 8, | 6 | 4.1662E-01 | 4.9108E-01 | 5.6343E-03 | 5.6343E-03 |
| 8, | 7 | 4.1721E-01 | 4.9062E-01 | 6.8937E-03 | 6.8937E-03 |
| 8, | 8 | 4.1799E-01 | 4.9007E-01 | 8.2481E-03 | 8.2481E-03 |
| 8, | 9 | 4.1901E-01 | 4.8942E-01 | 9.7361E-03 | 9.7361E-03 |
| 8, | 10 | 4.2033E-01 | 4.8865E-01 | 1.1409E-02 | 1.1409E-02 |
| 8, | 11 | 4.2202E-01 | 4.8777E-01 | 1.3331E-02 | 1.3331E-02 |
| 8, | 12 | 4.2413E-01 | 4.8674E-01 | 1.5584E-02 | 1.5584E-02 |
| 8, | 13 | 4.2670E-01 | 4.8555E-01 | 1.8265E-02 | 1.8265E-02 |
| 8, | 14 | 4.2975E-01 | 4.8417E-01 | 2.1481E-02 | 2.1481E-02 |

Table 5 (cont'd)

| | | | | |
|-------|------------|------------|------------|------------|
| 8, 15 | 4.3322E-01 | 4.8256E-01 | 2.5349E-02 | 2.5349E-02 |
| 8, 16 | 4.3699E-01 | 4.8068E-01 | 2.9978E-02 | 2.9978E-02 |
| 8, 17 | 4.4079E-01 | 4.7845E-01 | 3.5459E-02 | 3.5459E-02 |
| 8, 18 | 4.4419E-01 | 4.7582E-01 | 4.1842E-02 | 4.1842E-02 |
| 8, 19 | 4.4655E-01 | 4.7268E-01 | 4.9109E-02 | 4.9109E-02 |
| 8, 20 | 4.4694E-01 | 4.6895E-01 | 5.7146E-02 | 5.7146E-02 |
| 8, 21 | 4.4417E-01 | 4.6452E-01 | 6.5720E-02 | 6.5720E-02 |
| 8, 22 | 4.3677E-01 | 4.5927E-01 | 7.4460E-02 | 7.4460E-02 |
| 8, 23 | 4.2304E-01 | 4.5309E-01 | 8.2873E-02 | 8.2873E-02 |
| 8, 24 | 4.0125E-01 | 4.4589E-01 | 9.0384E-02 | 9.0384E-02 |
| 8, 25 | 3.6991E-01 | 4.3757E-01 | 9.6441E-02 | 9.6441E-02 |
| 8, 26 | 3.2827E-01 | 4.2804E-01 | 1.0068E-01 | 1.0068E-01 |
| 8, 27 | 2.7705E-01 | 4.1721E-01 | 1.0312E-01 | 1.0312E-01 |
| 8, 28 | 2.1947E-01 | 4.0492E-01 | 1.0444E-01 | 1.0444E-01 |
| 8, 29 | 1.6251E-01 | 3.9095E-01 | 1.0609E-01 | 1.0609E-01 |
| 8, 30 | 1.1856E-01 | 3.7494E-01 | 1.1031E-01 | 1.1031E-01 |
| 8, 31 | 1.1186E-01 | 3.7287E-01 | 1.1898E-01 | 1.1898E-01 |
| 9, 1 | 4.0953E-01 | 5.1282E-01 | 0. | 0. |
| 9, 2 | 4.0958E-01 | 5.1279E-01 | 3.6104E-04 | 3.6104E-04 |
| 9, 3 | 4.0973E-01 | 5.1267E-01 | 7.2488E-04 | 7.2488E-04 |
| 9, 4 | 4.0998E-01 | 5.1246E-01 | 1.0946E-03 | 1.0946E-03 |
| 9, 5 | 4.1034E-01 | 5.1217E-01 | 1.4736E-03 | 1.4736E-03 |
| 9, 6 | 4.1084E-01 | 5.1179E-01 | 1.8661E-03 | 1.8661E-03 |
| 9, 7 | 4.1152E-01 | 5.1131E-01 | 2.2768E-03 | 2.2768E-03 |
| 9, 8 | 4.1242E-01 | 5.1073E-01 | 2.7111E-03 | 2.7111E-03 |

SPHERE STRESS RESULTANTS.

| ROW | COL | MX | MTHETA | MXTHETA | QX | QTHETA |
|-------|-------------|-------------|-------------|------------|-------------|--------|
| 7, 30 | -1.8034E 01 | -6.6409E 01 | -6.3016E 00 | 3.9493E 01 | -3.2650E 03 | |
| 7, 31 | -4.3271E 01 | -1.4424E 02 | -1.9175E-01 | 1.1332E 02 | -3.7978E 03 | |
| 8, 1 | 1.4440E 01 | 4.1252E 00 | 0. | 4.8136E 01 | 2.0322E-05 | |
| 8, 2 | 1.4450E 01 | 4.1492E 00 | 2.8456E-02 | 4.8305E 01 | 6.7031E-01 | |
| 8, 3 | 1.4456E 01 | 4.1439E 00 | 5.7105E-02 | 4.8467E 01 | -5.3604E-01 | |
| 8, 4 | 1.4459E 01 | 4.1103E 00 | 8.8090E-02 | 4.8636E 01 | -1.6947E 00 | |
| 8, 5 | 1.4460E 01 | 4.0489E 00 | 1.2348E-01 | 4.8820E 01 | -2.7939E 00 | |
| 8, 6 | 1.4460E 01 | 3.9603E 00 | 1.6520E-01 | 4.9025E 01 | -3.7863E 00 | |
| 8, 7 | 1.4460E 01 | 3.8464E 00 | 2.1487E-01 | 4.9254E 01 | -4.5651E 00 | |
| 8, 8 | 1.4464E 01 | 3.7113E 00 | 2.7354E-01 | 4.9504E 01 | -4.9409E 00 | |
| 8, 9 | 1.4477E 01 | 3.5639E 00 | 3.4131E-01 | 4.9767E 01 | -4.6206E 00 | |
| 8, 10 | 1.4507E 01 | 3.4198E 00 | 4.1674E-01 | 5.0022E 01 | -3.1864E 00 | |
| 8, 11 | 1.4563E 01 | 3.3043E 00 | 4.9617E-01 | 5.0236E 01 | -7.5807E-02 | |
| 8, 12 | 1.4661E 01 | 3.2559E 00 | 5.7280E-01 | 5.0357E 01 | 5.4176E 00 | |
| 8, 13 | 1.4817E 01 | 3.3298E 00 | 6.3573E-01 | 5.0313E 01 | 1.4113E 01 | |
| 8, 14 | 1.5055E 01 | 3.5998E 00 | 6.6901E-01 | 5.0000E 01 | 2.6885E 01 | |
| 8, 15 | 1.5399E 01 | 4.1605E 00 | 6.5092E-01 | 4.9288E 01 | 4.4558E 01 | |
| 8, 16 | 1.5875E 01 | 5.1257E 00 | 5.5373E-01 | 4.8016E 01 | 6.7715E 01 | |
| 8, 17 | 1.6506E 01 | 6.6226E 00 | 3.4453E-01 | 4.5998E 01 | 9.6405E 01 | |

Table 5 (cont'd)

| | | | | | |
|-------|-------------|-------------|-------------|-------------|-------------|
| 8, 18 | 1.7305E 01 | 8.7797E 00 | -1.2557E-02 | 4.3033E 01 | 1.2975E 02 |
| 8, 19 | 1.8270E 01 | 1.1705E 01 | -5.5192E-01 | 3.8932E 01 | 1.6538E 02 |
| 8, 20 | 1.9365E 01 | 1.5449E 01 | -1.2993E 00 | 3.3554E 01 | 1.9877E 02 |
| 8, 21 | 2.0513E 01 | 1.9955E 01 | -2.2616E 00 | 2.6866E 01 | 2.2244E 02 |
| 8, 22 | 2.1569E 01 | 2.4989E 01 | -3.4135E 00 | 1.9017E 01 | 2.2506E 02 |
| 8, 23 | 2.2308E 01 | 3.0042E 01 | -4.6830E 00 | 1.0435E 01 | 1.9068E 02 |
| 8, 24 | 2.2397E 01 | 3.4225E 01 | -5.9383E 00 | 1.9232E 00 | 9.8242E 01 |
| 8, 25 | 2.1385E 01 | 3.6142E 01 | -6.9821E 00 | -5.2742E 00 | -7.8293E 01 |
| 8, 26 | 1.8690E 01 | 3.3776E 01 | -7.5634E 00 | -9.4875E 00 | -3.6866E 02 |
| 8, 27 | 1.3609E 01 | 2.4408E 01 | -7.4186E 00 | -8.8120E 00 | -8.0323E 02 |
| 8, 28 | 5.3436E 00 | 4.6353E 00 | -6.3573E 00 | -1.5812E 00 | -1.4073E 03 |
| 8, 29 | -6.9531E 00 | -2.9455E 01 | -4.4022E 00 | 1.2757E 01 | -2.1924E 03 |
| 8, 30 | -2.4093E 01 | -8.1850E 01 | -1.9791E 00 | 3.2301E 01 | -3.1434E 03 |
| 8, 31 | -4.6744E 01 | -1.5581E 02 | -1.1898E-01 | 5.0972E 01 | -3.6314E 03 |
| 9, 1 | 1.0706E 01 | 2.7788E 00 | 0. | 4.7328E 00 | 2.0558E-05 |
| 9, 2 | 1.0717E 01 | 2.8047E 00 | 5.5560E-03 | 5.0009E 00 | 7.0565E-01 |
| 9, 3 | 1.0724E 01 | 2.7964E 00 | 1.1408E-02 | 5.2746E 00 | -6.7898E-01 |
| 9, 4 | 1.0729E 01 | 2.7549E 00 | 1.8096E-02 | 5.5704E 00 | -1.9872E 00 |
| 9, 5 | 1.0732E 01 | 2.6814E 00 | 2.6100E-02 | 5.9019E 00 | -3.1939E 00 |
| 9, 6 | 1.0734E 01 | 2.5774E 00 | 3.5800E-02 | 6.2796E 00 | -4.2344E 00 |
| 9, 7 | 1.0739E 01 | 2.4462E 00 | 4.7404E-02 | 6.7091E 00 | -4.9696E 00 |
| 9, 8 | 1.0750E 01 | 2.2943E 00 | 6.0844E-02 | 7.1881E 00 | -5.1727E 00 |

BOUNDARY STRESS RESULTANTS.

| ROW | COL | NTAN | NNORM | Q | M |
|--------|-------------|------|------------|-------------|-------------|
| 18, 1 | 0. | | 3.1654E-01 | -8.3278E 03 | -1.9934E 02 |
| 18, 2 | -2.8194E-03 | | 3.1655E-01 | -8.3267E 03 | -1.9937E 02 |
| 18, 3 | -5.6834E-03 | | 3.1656E-01 | -8.3274E 03 | -1.9944E 02 |
| 18, 4 | -8.6365E-03 | | 3.1658E-01 | -8.3296E 03 | -1.9956E 02 |
| 18, 5 | -1.1726E-02 | | 3.1661E-01 | -8.3332E 03 | -1.9972E 02 |
| 18, 6 | -1.5005E-02 | | 3.1666E-01 | -8.3385E 03 | -1.9995E 02 |
| 18, 7 | -1.8534E-02 | | 3.1671E-01 | -8.3457E 03 | -2.0025E 02 |
| 18, 8 | -2.2385E-02 | | 3.1677E-01 | -8.3555E 03 | -2.0065E 02 |
| 18, 9 | -2.6642E-02 | | 3.1684E-01 | -8.3686E 03 | -2.0116E 02 |
| 18, 10 | -3.1405E-02 | | 3.1691E-01 | -8.3861E 03 | -2.0183E 02 |
| 18, 11 | -3.6790E-02 | | 3.1697E-01 | -8.4092E 03 | -2.0268E 02 |
| 18, 12 | -4.2930E-02 | | 3.1699E-01 | -8.4394E 03 | -2.0374E 02 |
| 18, 13 | -4.9972E-02 | | 3.1694E-01 | -8.4785E 03 | -2.0504E 02 |
| 18, 14 | -5.8073E-02 | | 3.1676E-01 | -8.5283E 03 | -2.0660E 02 |
| 18, 15 | -6.7390E-02 | | 3.1638E-01 | -8.5906E 03 | -2.0843E 02 |
| 18, 16 | -7.8067E-02 | | 3.1568E-01 | -8.6666E 03 | -2.1049E 02 |
| 18, 17 | -9.0212E-02 | | 3.1452E-01 | -8.7569E 03 | -2.1269E 02 |
| 18, 18 | -1.0387E-01 | | 3.1269E-01 | -8.8602E 03 | -2.1489E 02 |

Table 5 (cont'd)

| | | | | | | |
|--------|-------------|------------|----------|----|----------|----|
| 18, 19 | -1.1899E-01 | 3.0996E-01 | -8.9730E | 03 | -2.1682E | 02 |
| 18, 20 | -1.3537E-01 | 3.0607E-01 | -9.0883E | 03 | -2.1812E | 02 |
| 18, 21 | -1.5260E-01 | 3.0064E-01 | -9.1941E | 03 | -2.1823E | 02 |
| 18, 22 | -1.7003E-01 | 2.9327E-01 | -9.2718E | 03 | -2.1646E | 02 |
| 18, 23 | -1.8669E-01 | 2.8354E-01 | -9.2945E | 03 | -2.1188E | 02 |
| 18, 24 | -2.0125E-01 | 2.7100E-01 | -9.2247E | 03 | -2.0338E | 02 |
| 18, 25 | -2.1202E-01 | 2.5518E-01 | -9.0124E | 03 | -1.8972E | 02 |
| 18, 26 | -2.1695E-01 | 2.3562E-01 | -8.5922E | 03 | -1.6964E | 02 |
| 18, 27 | -2.1369E-01 | 2.1185E-01 | -7.8802E | 03 | -1.4214E | 02 |
| 18, 28 | -1.9971E-01 | 1.8329E-01 | -6.7676E | 03 | -1.0698E | 02 |
| 18, 29 | -1.7204E-01 | 1.4896E-01 | -5.1084E | 03 | -6.5787E | 01 |
| 18, 30 | -1.2332E-01 | 1.0458E-01 | -2.7357E | 03 | -2.4507E | 01 |
| 18, 31 | 0. | 0. | -3.7534E | 00 | -0. | |
| 18, 31 | | | | | | |
| 18, 31 | -0. | 0. | -0. | | 0. | |
| 17, 31 | 6.2429E-02 | 6.6763E-02 | -1.8459E | 02 | -5.6682E | 00 |
| 16, 31 | 1.0333E-01 | 1.0408E-01 | -5.8460E | 02 | -1.7943E | 01 |
| 15, 31 | 1.5904E-01 | 1.5705E-01 | -1.5130E | 03 | -4.7199E | 01 |
| 14, 31 | 1.8736E-01 | 1.9392E-01 | -2.2564E | 03 | -7.4360E | 01 |
| 13, 31 | 2.0035E-01 | 2.2494E-01 | -2.7428E | 03 | -9.5980E | 01 |
| 12, 31 | 2.0334E-01 | 2.8463E-01 | -3.4037E | 03 | -1.3038E | 02 |
| 11, 31 | 1.7540E-01 | 3.2177E-01 | -3.5660E | 03 | -1.4594E | 02 |
| 10, 31 | 9.3693E-02 | 3.7727E-01 | -3.4916E | 03 | -1.5588E | 02 |
| 9, 31 | -1.3941E-02 | 3.8796E-01 | -3.4799E | 03 | -1.5683E | 02 |
| 8, 31 | -1.1898E-01 | 3.7287E-01 | -3.6314E | 03 | -1.5581E | 02 |
| 7, 31 | -1.9174E-01 | 3.1335E-01 | -3.7978E | 03 | -1.4424E | 02 |
| 6, 31 | -2.1314E-01 | 2.7501E-01 | -3.6301E | 03 | -1.2743E | 02 |
| 5, 31 | -2.0256E-01 | 2.1514E-01 | -2.8917E | 03 | -9.1868E | 01 |
| 4, 31 | -1.8584E-01 | 1.8463E-01 | -2.3600E | 03 | -7.0433E | 01 |
| 3, 31 | -1.5398E-01 | 1.4857E-01 | -1.5637E | 03 | -4.4102E | 01 |
| 2, 31 | -9.6554E-02 | 9.7046E-02 | -5.9817E | 02 | -1.6483E | 01 |
| 1, 31 | -5.6772E-02 | 6.1051E-02 | -1.9192E | 02 | -5.1964E | 00 |
| 0, 31 | 0. | 0. | 0. | | 0. | |
| 0, 31 | | | | | | |
| 0, 31 | -0. | -0. | -3.3510E | 00 | -0. | |
| 0, 30 | 1.2570E-01 | 1.0769E-01 | -2.1392E | 02 | -3.0291E | 01 |
| 0, 29 | 1.7161E-01 | 1.5369E-01 | -2.1461E | 03 | -7.5918E | 01 |
| 0, 28 | 1.9603E-01 | 1.8906E-01 | -4.1497E | 03 | -1.1849E | 02 |
| 0, 27 | 2.0635E-01 | 2.1778E-01 | -5.8101E | 03 | -1.5281E | 02 |
| 0, 26 | 2.0607E-01 | 2.4103E-01 | -7.0648E | 03 | -1.7822E | 02 |
| 0, 25 | 1.9817E-01 | 2.5964E-01 | -7.9498E | 03 | -1.9574E | 02 |
| 0, 24 | 1.8526E-01 | 2.7427E-01 | -8.5311E | 03 | -2.0689E | 02 |
| 0, 23 | 1.6945E-01 | 2.8556E-01 | -8.8790E | 03 | -2.1324E | 02 |
| 0, 22 | 1.5239E-01 | 2.9408E-01 | -9.0566E | 03 | -2.1614E | 02 |
| 0, 21 | 1.3526E-01 | 3.0037E-01 | -9.1169E | 03 | -2.1673E | 02 |

Table 5 (concl'd)

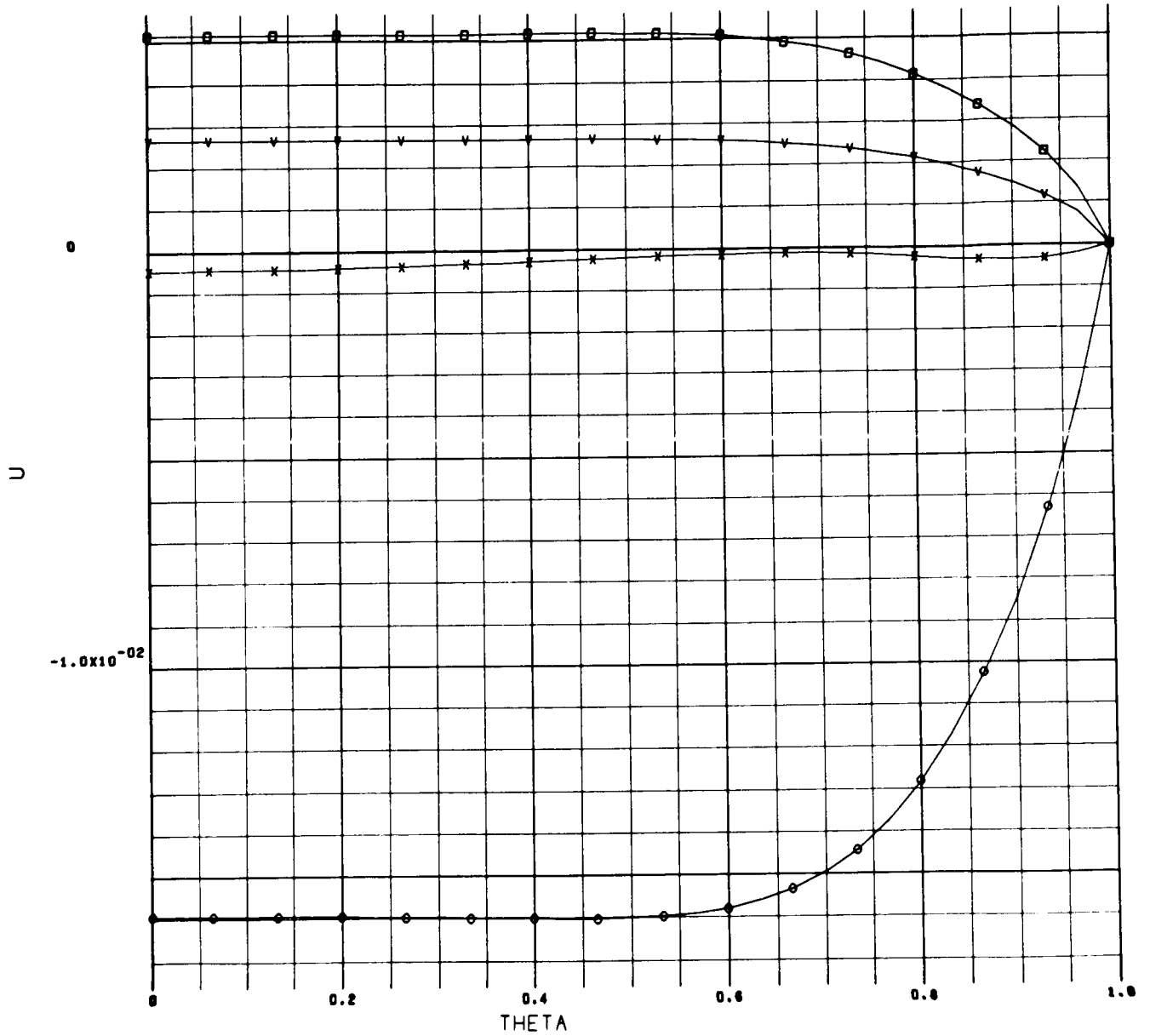
| | | | | | | |
|-------|------------|------------|----------|----|----------|----|
| 0, 20 | 1.1887E-01 | 3.0491E-01 | -9.1010E | 03 | -2.1585E | 02 |
| 0, 19 | 1.0370E-01 | 3.0810E-01 | -9.0399E | 03 | -2.1416E | 02 |
| 0, 18 | 9.0002E-02 | 3.1028E-01 | -8.9560E | 03 | -2.1208E | 02 |
| 0, 17 | 7.7856E-02 | 3.1173E-01 | -8.8641E | 03 | -2.0992E | 02 |
| 0, 16 | 6.7221E-02 | 3.1266E-01 | -8.7739E | 03 | -2.0787E | 02 |
| 0, 15 | 5.7985E-02 | 3.1324E-01 | -8.6910E | 03 | -2.0602E | 02 |
| 0, 14 | 4.9999E-02 | 3.1360E-01 | -8.6181E | 03 | -2.0441E | 02 |
| 0, 13 | 4.3097E-02 | 3.1380E-01 | -8.5561E | 03 | -2.0306E | 02 |
| 0, 12 | 3.7116E-02 | 3.1393E-01 | -8.5046E | 03 | -2.0194E | 02 |
| 0, 11 | 3.1904E-02 | 3.1400E-01 | -8.4627E | 03 | -2.0104E | 02 |
| 0, 10 | 2.7324E-02 | 3.1406E-01 | -8.4292E | 03 | -2.0032E | 02 |
| 0, 9 | 2.3258E-02 | 3.1410E-01 | -8.4025E | 03 | -1.9975E | 02 |
| 0, 8 | 1.9604E-02 | 3.1414E-01 | -8.3816E | 03 | -1.9931E | 02 |
| 0, 7 | 1.6279E-02 | 3.1418E-01 | -8.3652E | 03 | -1.9896E | 02 |
| 0, 6 | 1.3213E-02 | 3.1422E-01 | -8.3524E | 03 | -1.9869E | 02 |
| 0, 5 | 1.0347E-02 | 3.1425E-01 | -8.3425E | 03 | -1.9849E | 02 |
| 0, 4 | 7.6330E-03 | 3.1428E-01 | -8.3350E | 03 | -1.9833E | 02 |
| 0, 3 | 5.0287E-03 | 3.1430E-01 | -8.3293E | 03 | -1.9823E | 02 |
| 0, 2 | 2.4962E-03 | 3.1431E-01 | -8.3251E | 03 | -1.9816E | 02 |
| 0, 1 | -0. | 3.1431E-01 | -8.3224E | 03 | -1.9813E | 02 |

EXAMPLE SPHERICAL SEGMENT UNDER UNIFORM NORMAL PRESSURE

44BFY4
001 000

○ PHI = 1.503 , ROW 5
x PHI = 1.300 , ROW 9

□ PHI = 1.038 , ROW 16
y PHI = 1.029 , ROW 17



a - Sphere Displacement Components

Fig. 12 Output Plot for the Example: Spherical Segment Under Uniform Normal Pressure

EXAMPLE SPHERICAL SEGMENT UNDER UNIFORM NORMAL PRESSURE

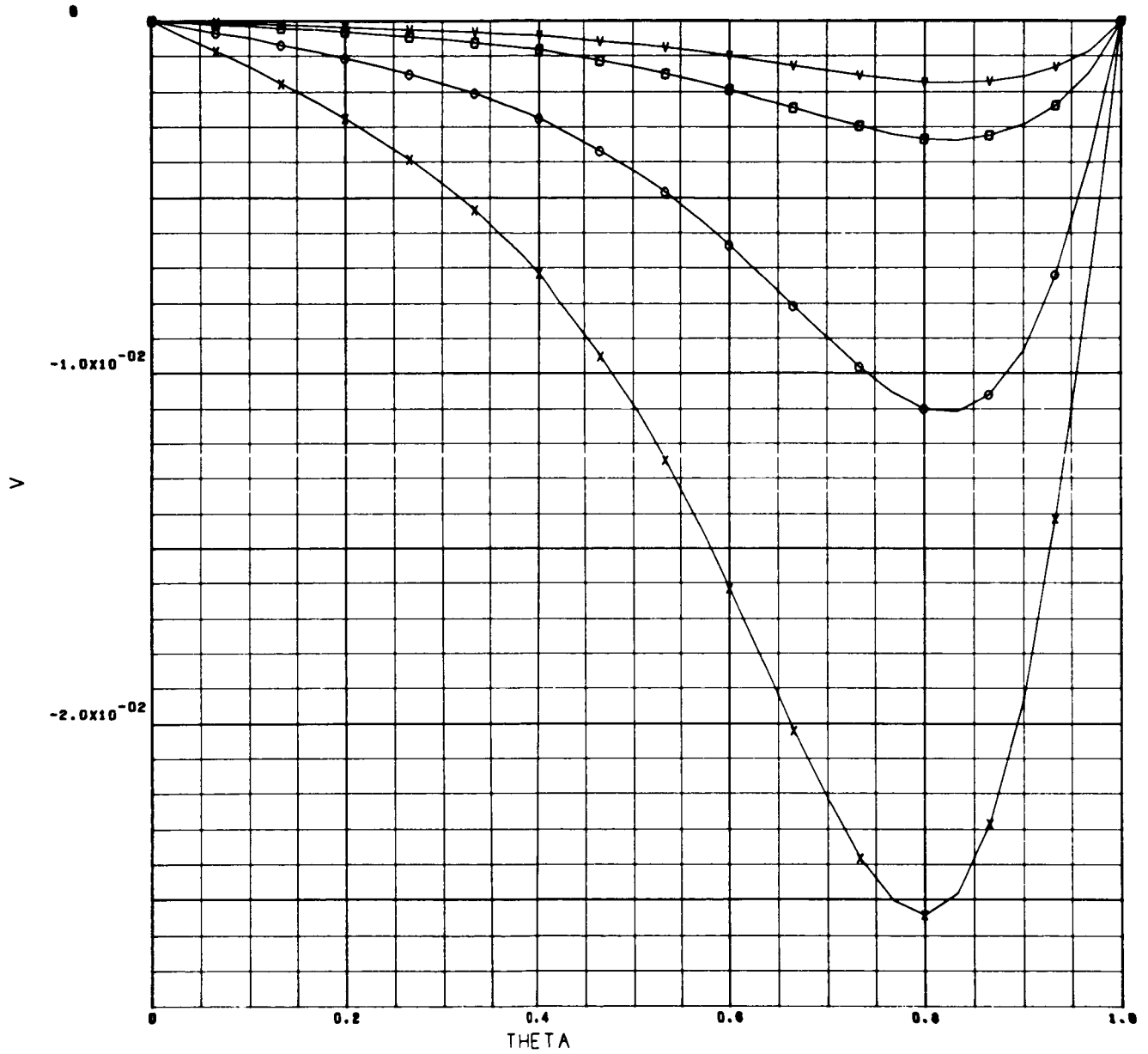
44BFY4
002 000

○ PHI = 1.503 , ROW 5

◻ PHI = 1.038 , ROW 16

x PHI = 1.300 , ROW 9

∨ PHI = 1.029 , ROW 17



b - Sphere Displacement Components

EXAMPLE SPHERICAL SEGMENT UNDER UNIFORM NORMAL PRESSURE

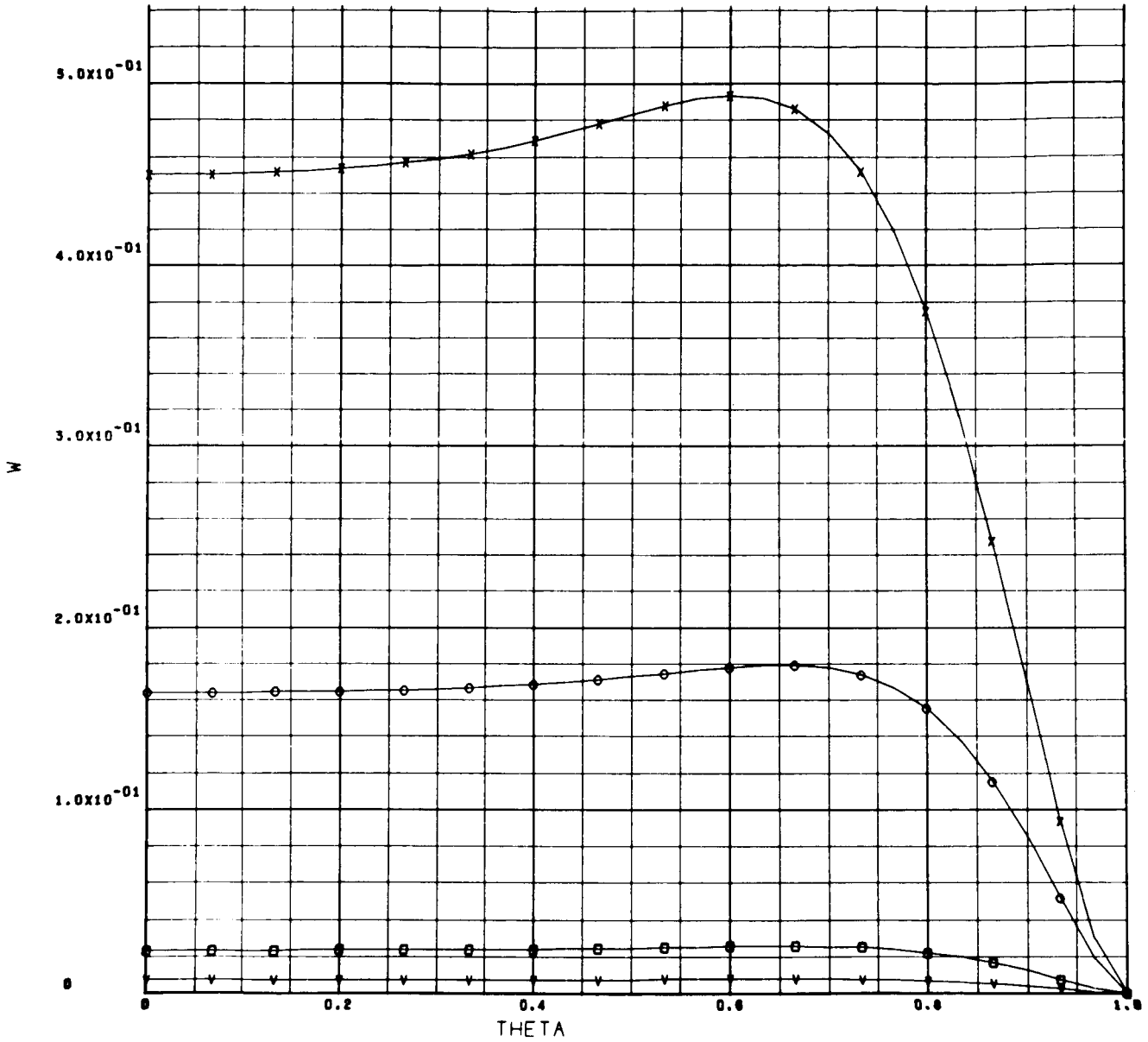
44BFY4
003 000

o PHI = 1.503 , ROW 5

□ PHI = 1.038 , ROW 16

x PHI = 1.300 , ROW 9

y PHI = 1.029 , ROW 17



c - Sphere Displacement Components

EXAMPLE SPHERICAL SEGMENT UNDER UNIFORM NORMAL PRESSURE

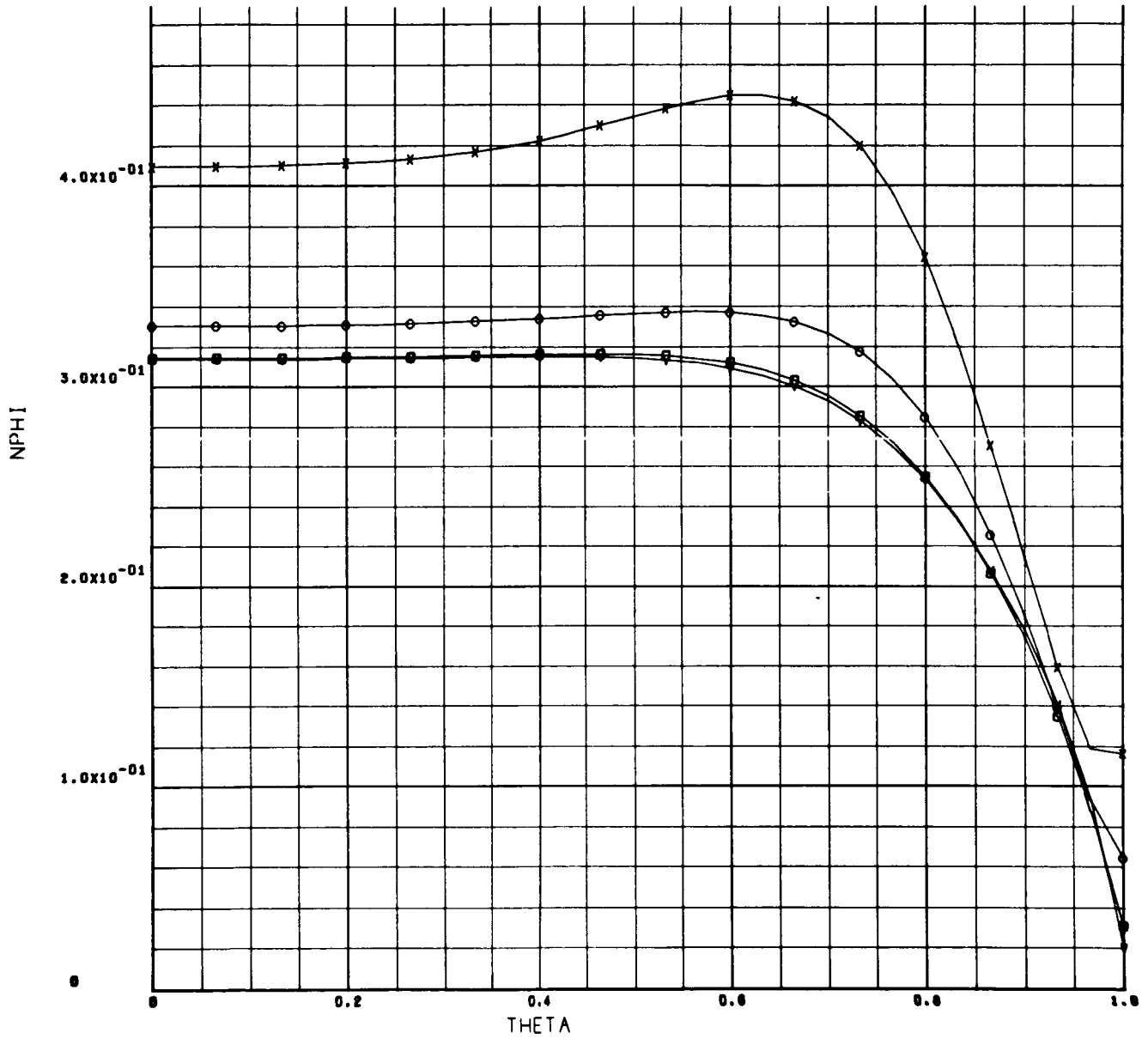
44BFY
004 000

○ PHI = 1.503 , ROW 5

◻ PHI = 1.038 , ROW 16

× PHI = 1.300 , ROW 9

● PHI = 1.029 , ROW 17



d - Sphere Stress Resultants

EXAMPLE SPHERICAL SEGMENT UNDER UNIFORM NORMAL PRESSURE

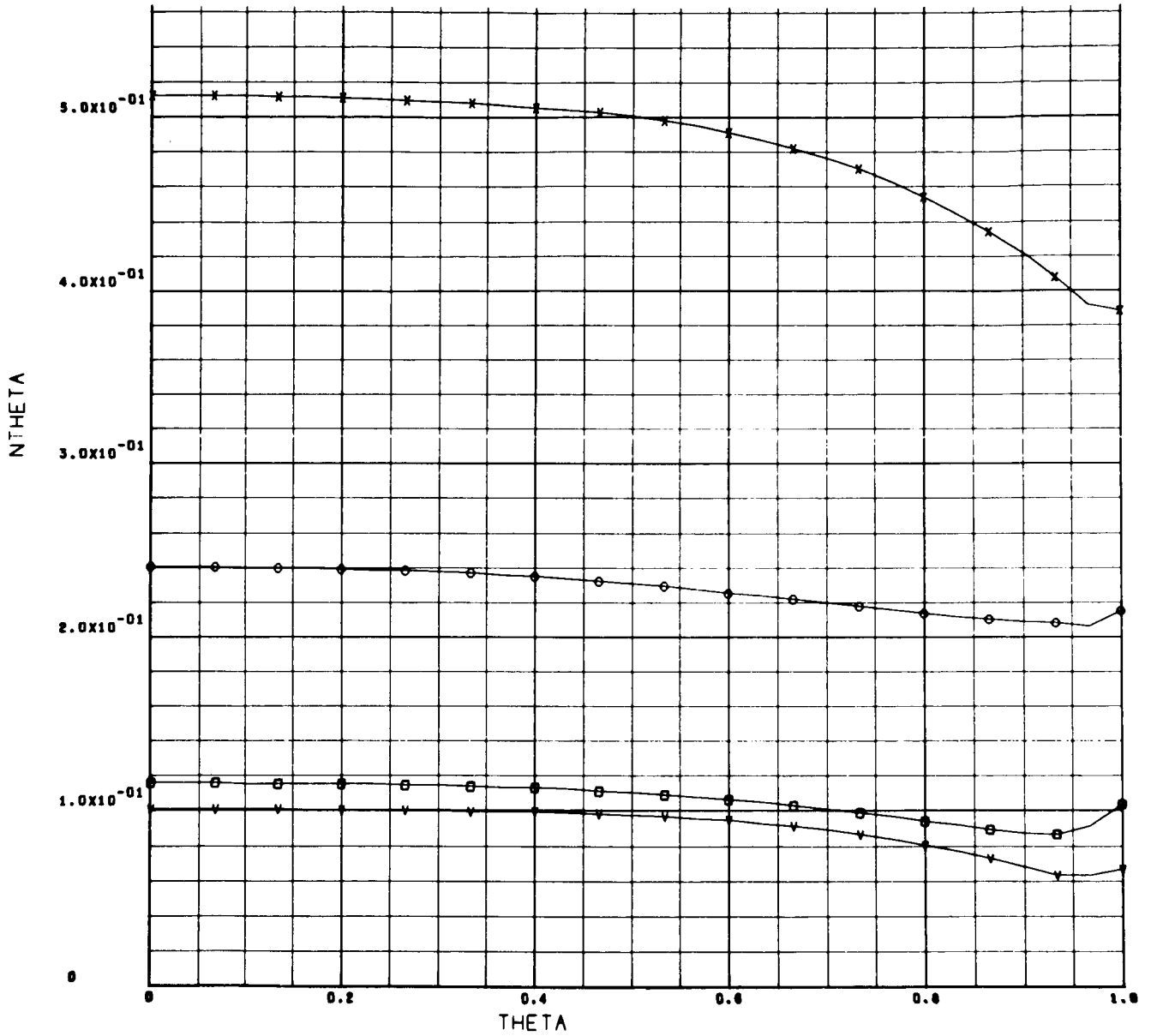
005 000

○ PHI = 1.503 , ROW 5

□ PHI = 1.030 , ROW 16

x PHI = 1.300 , ROW 9

y PHI = 1.029 , ROW 17



e - Sphere Stress Resultants

EXAMPLE SPHERICAL SEGMENT UNDER UNIFORM NORMAL PRESSURE

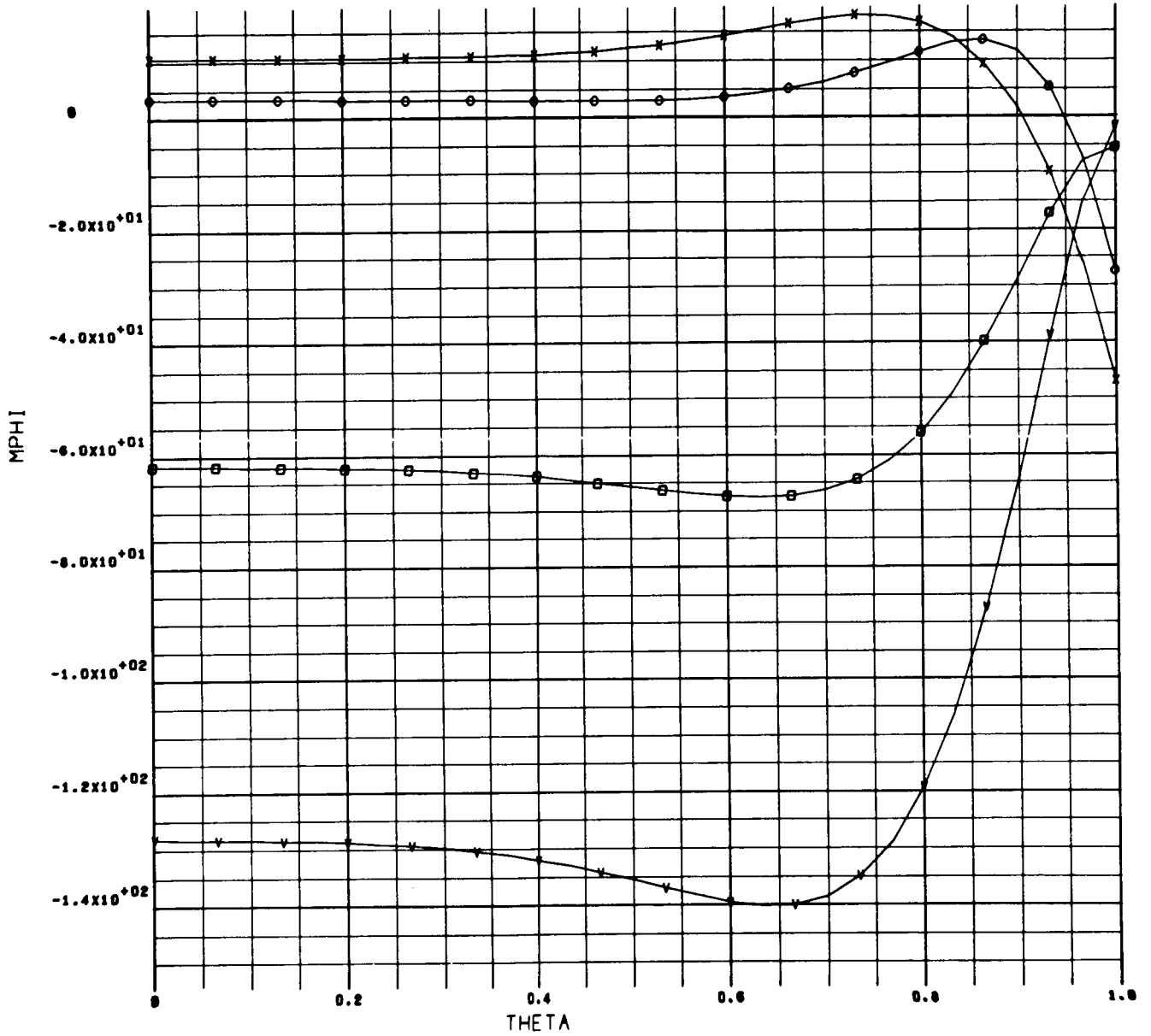
4JBFY4
006 000

○ PHI = 1.503 , ROW 5

□ PHI = 1.038 , ROW 16

× PHI = 1.300 , ROW 9

∇ PHI = 1.029 , ROW 17



f - Sphere Stress Resultants

EXAMPLE SPHERICAL SEGMENT UNDER UNIFORM NORMAL PRESSURE

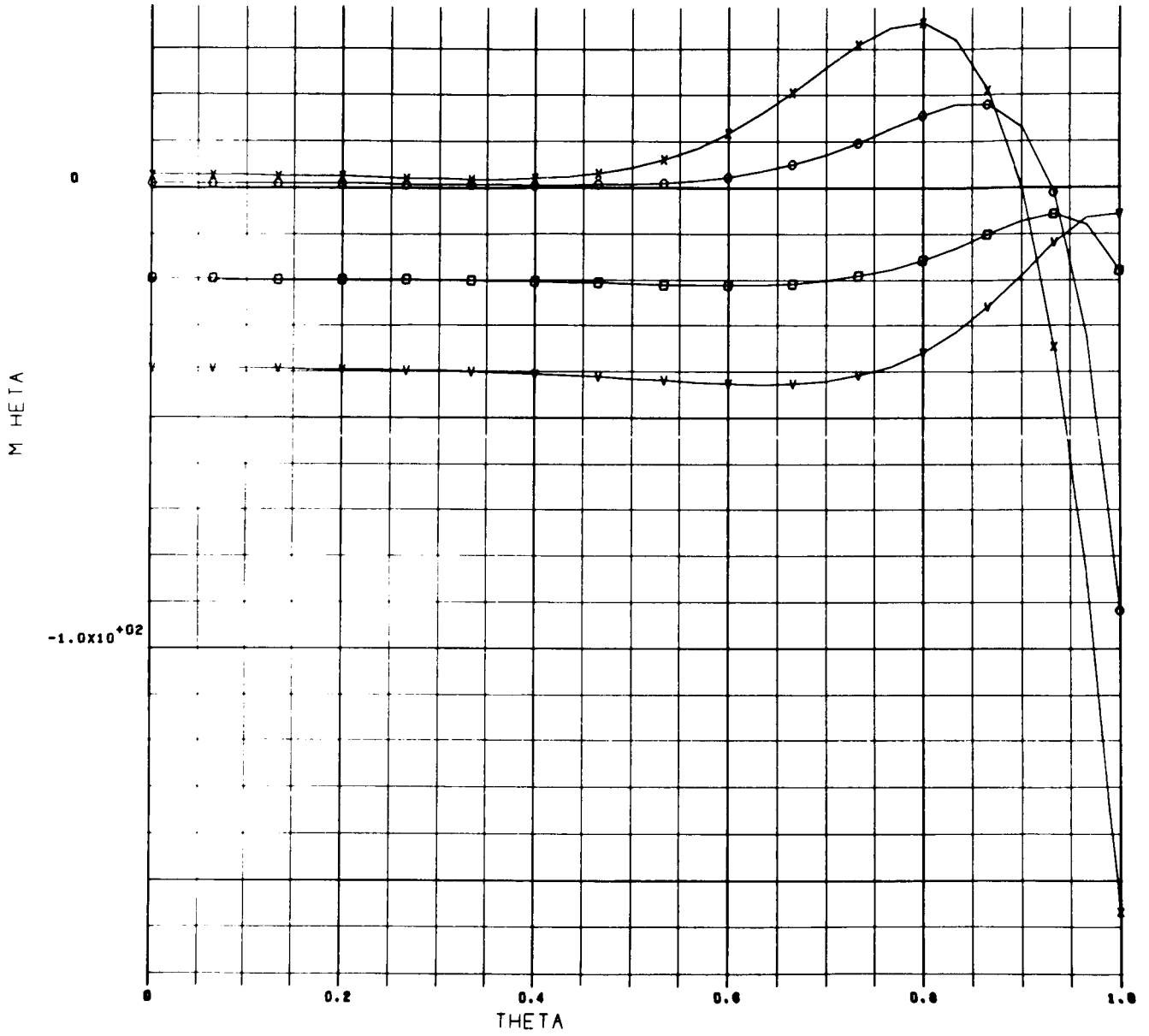
44BFY4
007 000

O PHI = 1.503 , ROW 5

□ PHI = 1.038 , ROW 16

X PHI = 1.300 , ROW 9

Y PHI = 1.029 , ROW 17

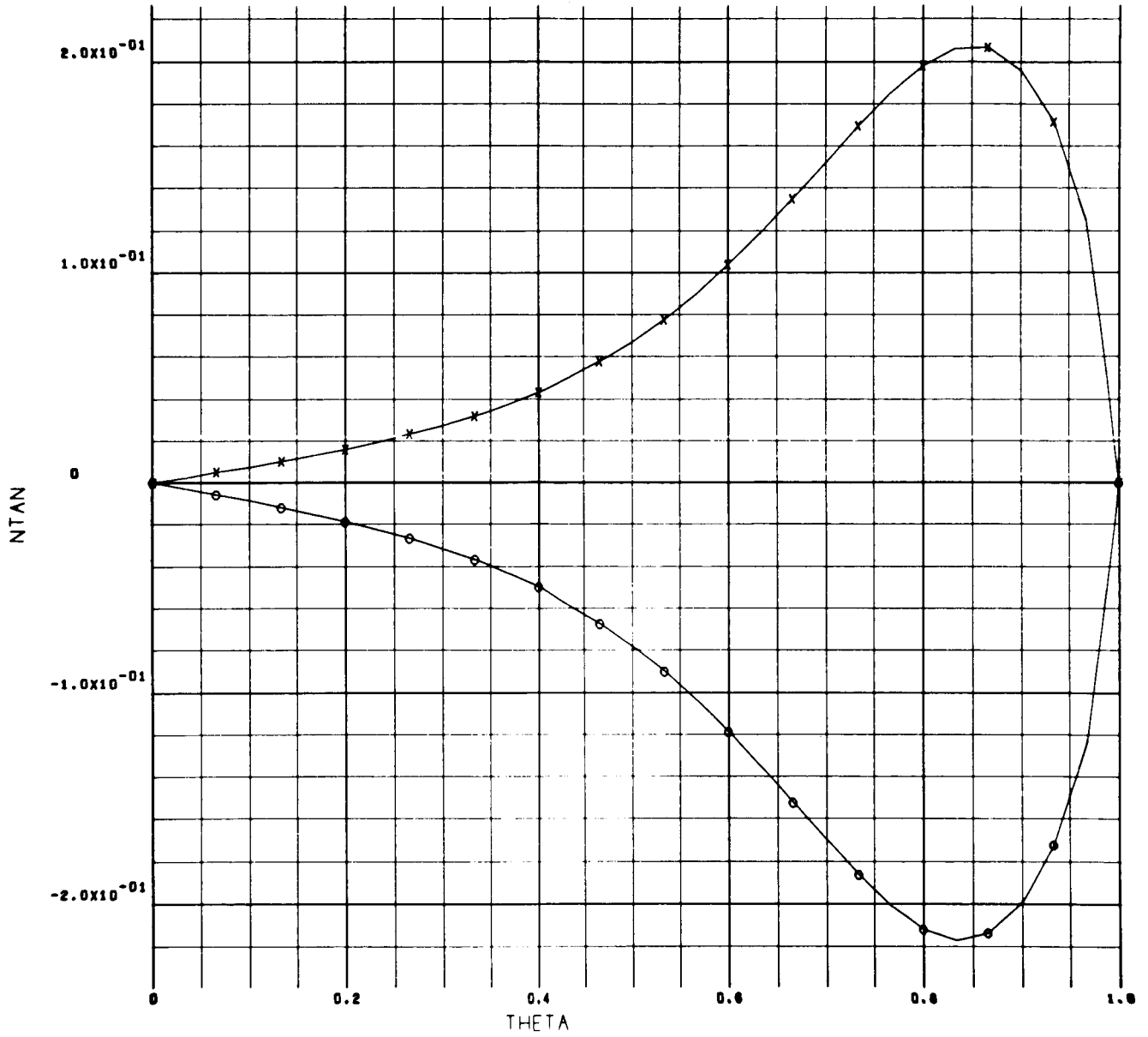


g - Sphere Stress Resultants

EXAMPLE SPHERICAL SEGMENT UNDER UNIFORM NORMAL PRESSURE

48BFYd
000 000

- o CURVE 1= UPPER BOUNDARY
- x CURVE 2= LOWER BOUNDARY

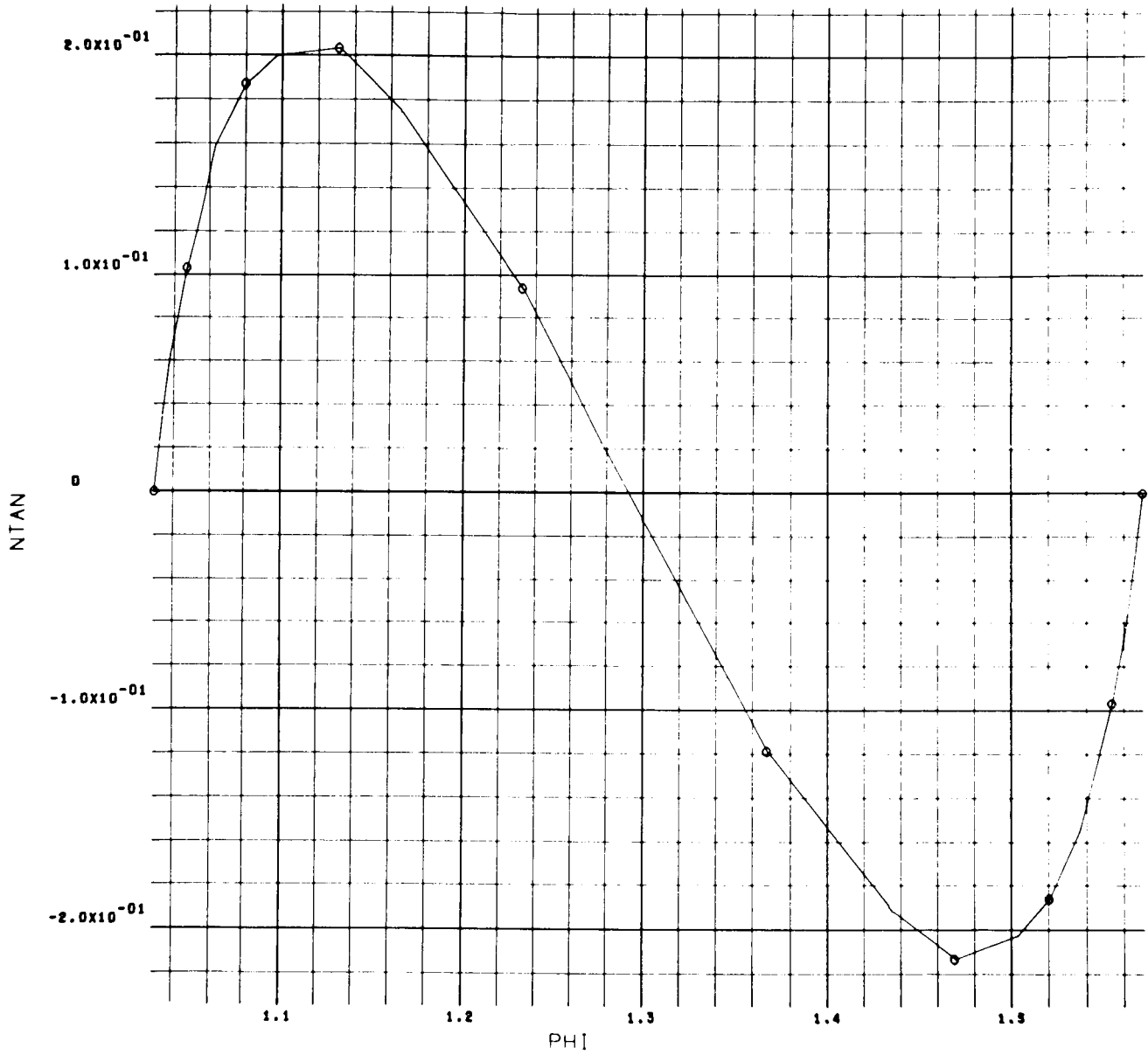


h - Boundary Stress Resultants

EXAMPLE SPHERICAL SEGMENT UNDER UNIFORM NORMAL PRESSURE

44BFY
009 060

o RIGHT BOUNDARY

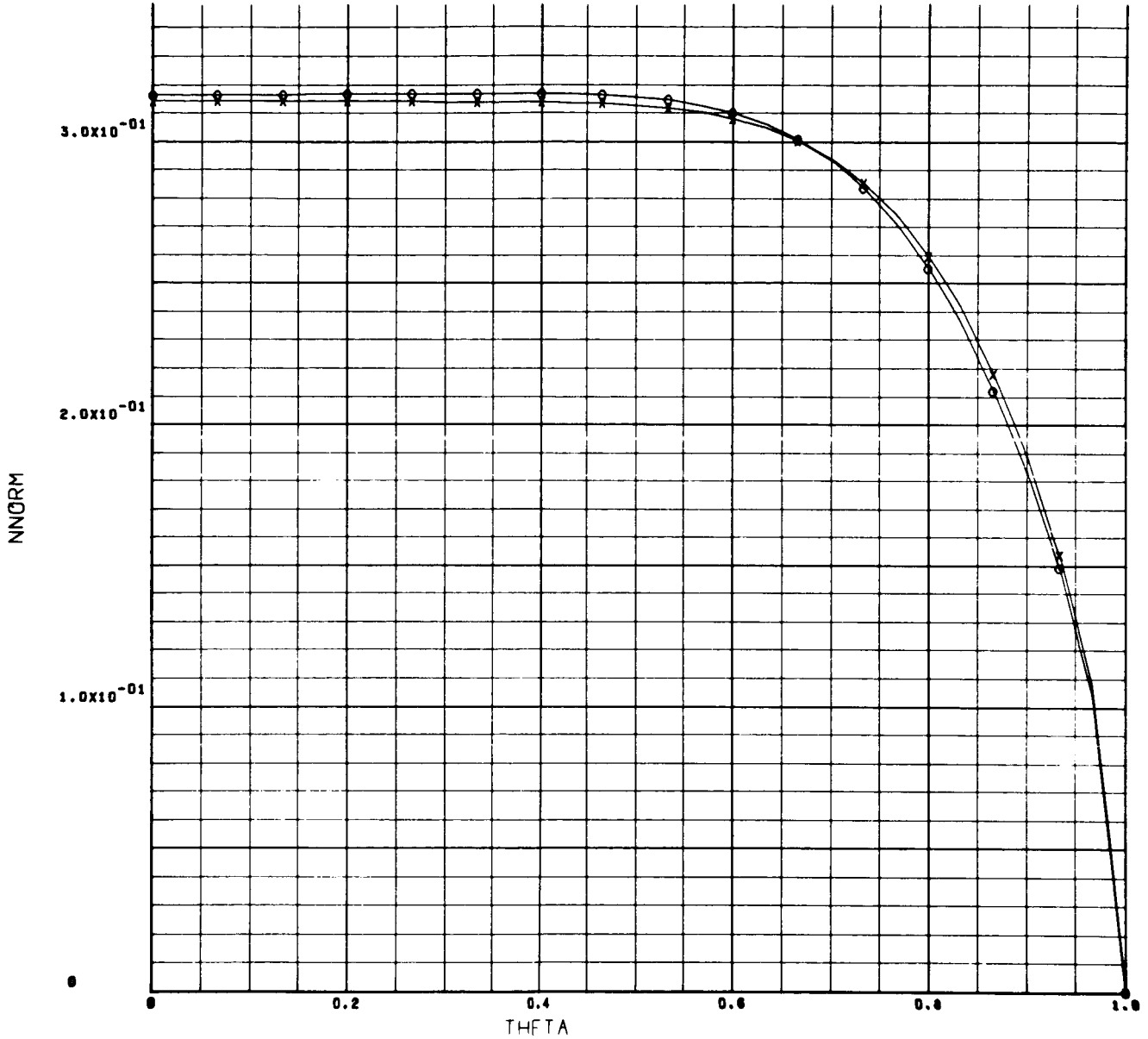


i - Boundary Stress Resultants

EXAMPLE SPHERICAL SEGMENT UNDER UNIFORM NORMAL PRESSURE

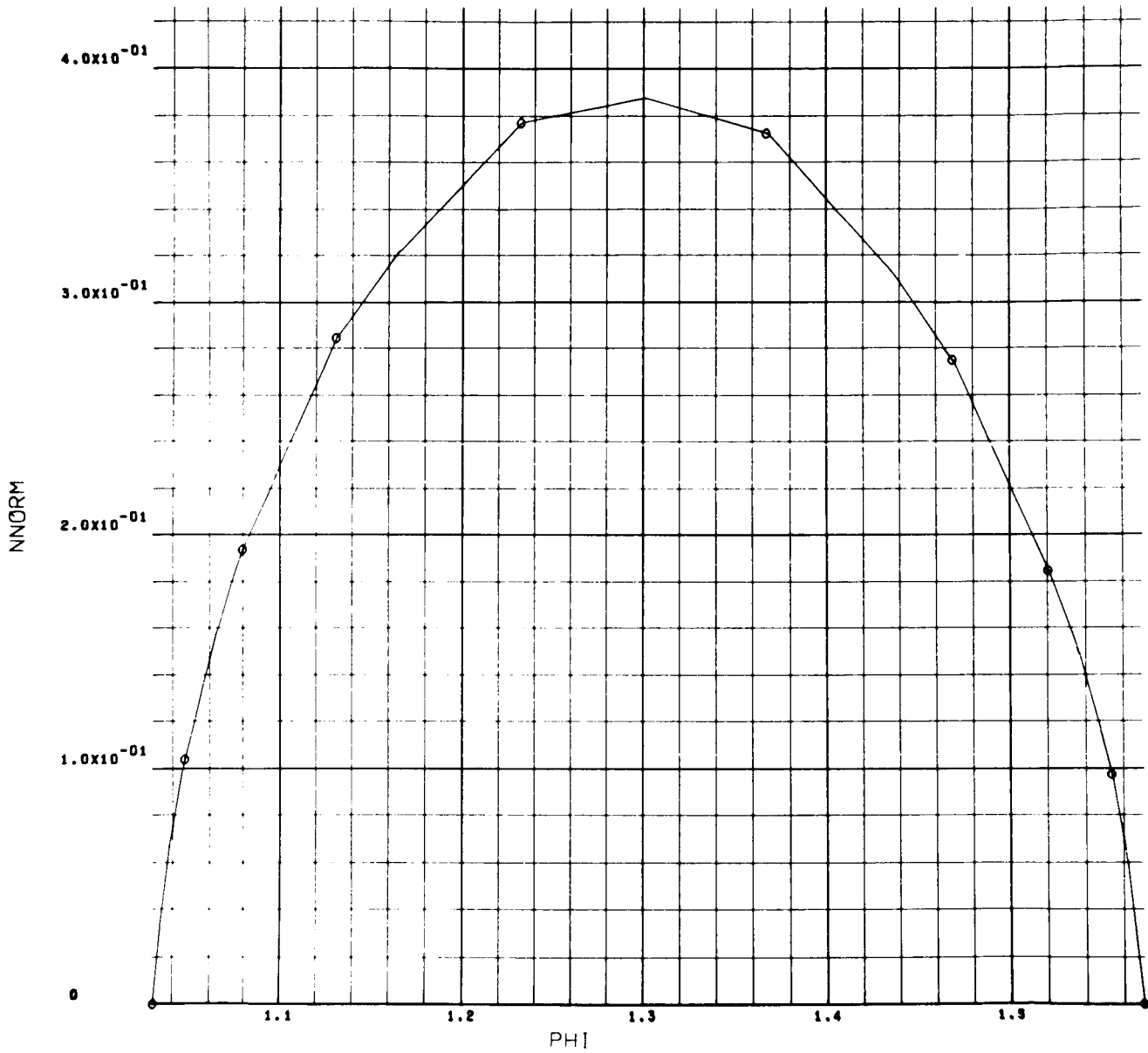
44BFY4
010 000

- o CURVE 1= UPPER BOUNDARY
- x CURVE 2= LOWER BOUNDARY



j - Boundary Stress Resultants

○ RIGHT BOUNDARY

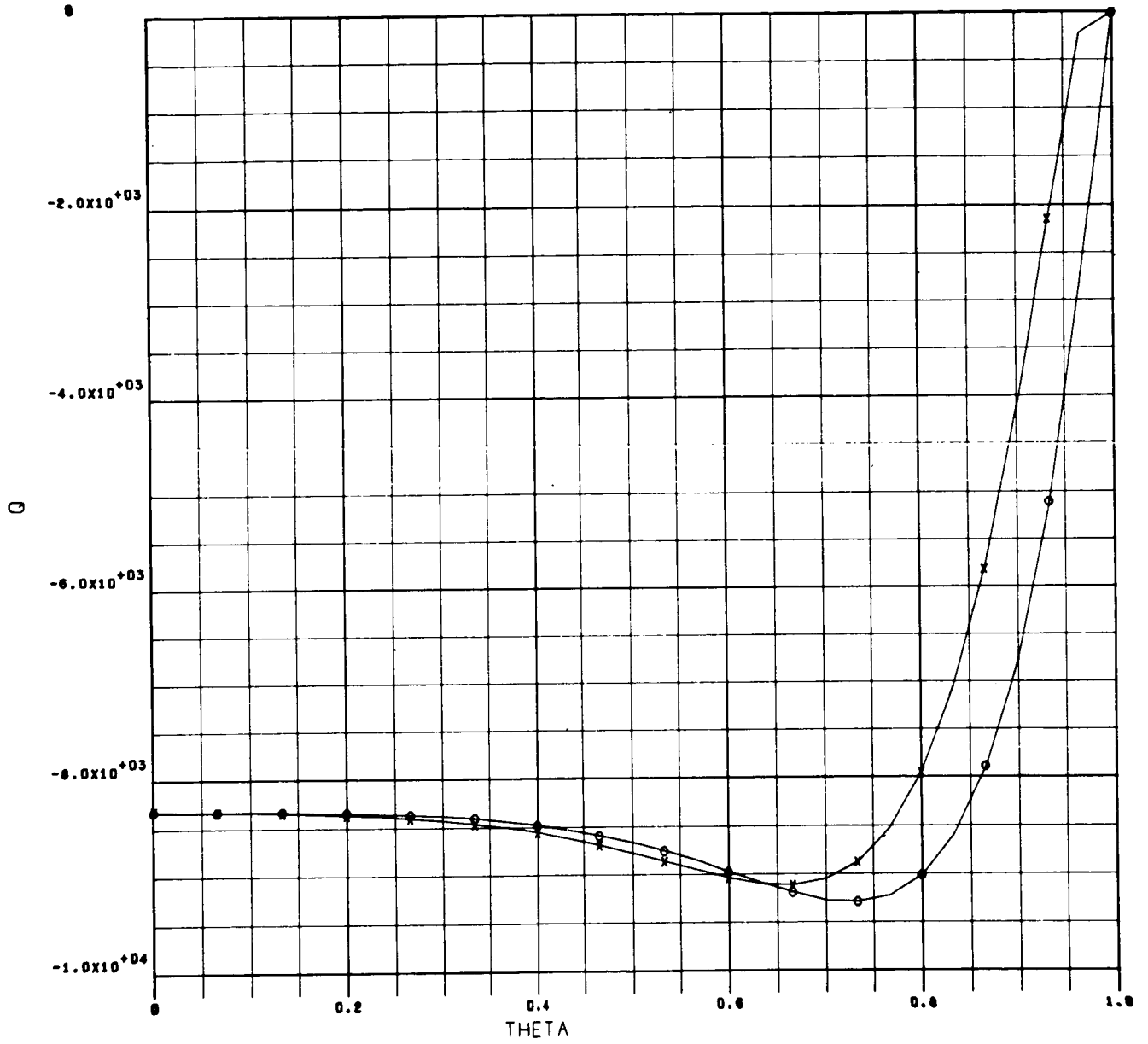


k - Boundary Stress Resultants

EXAMPLE SPHERICAL SEGMENT UNDER UNIFORM NORMAL PRESSURE

48FY
012 000

- o CURVE 1= UPPER BOUNDARY
- x CURVE 2= LOWER BOUNDARY

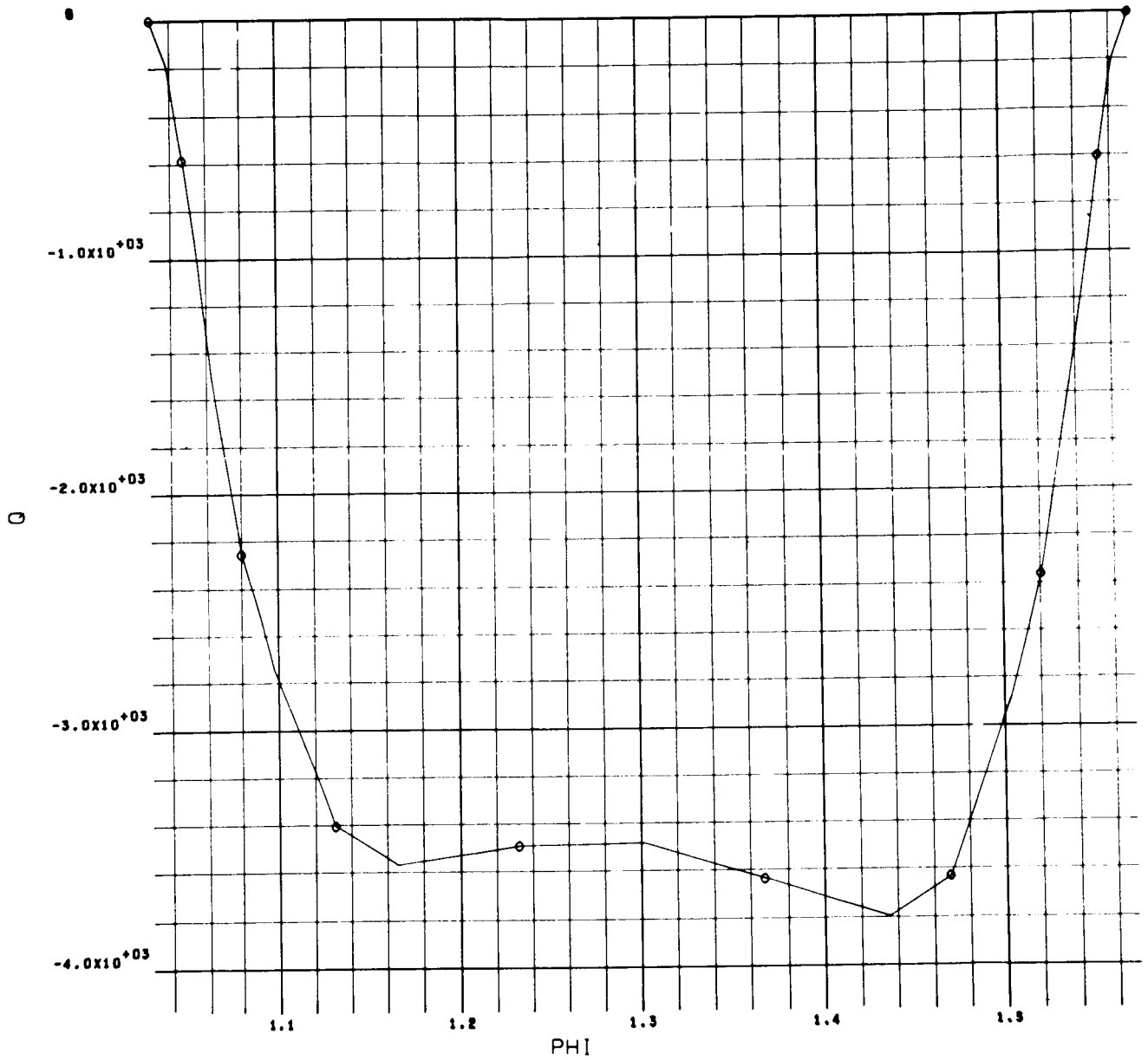


1 - Boundary Stress Resultants

EXAMPLE SPHERICAL SEGMENT UNDER UNIFORM NORMAL PRESSURE

48FY4
013 000

o RIGHT BOUNDARY

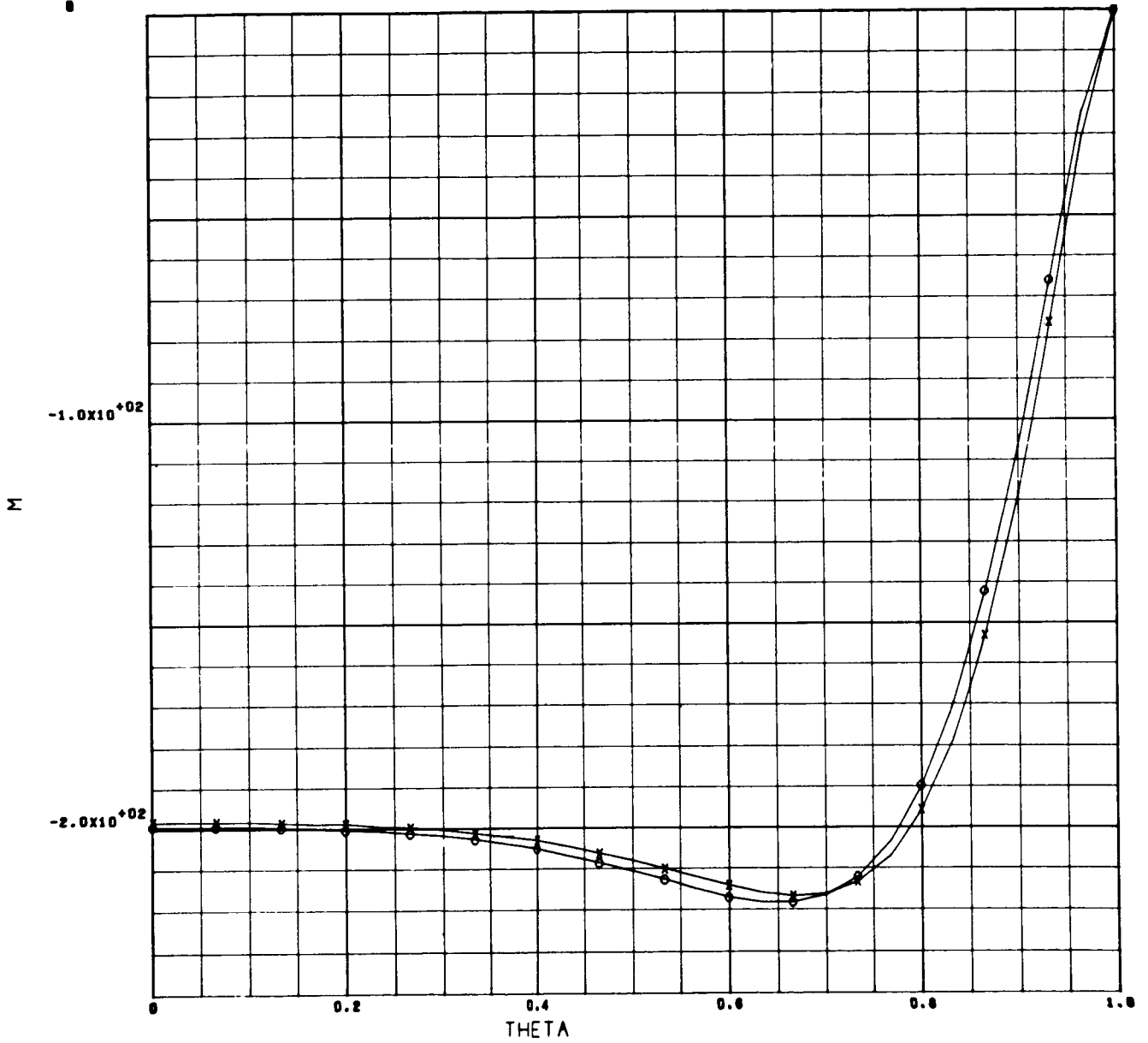


m - Boundary Stress Resultants

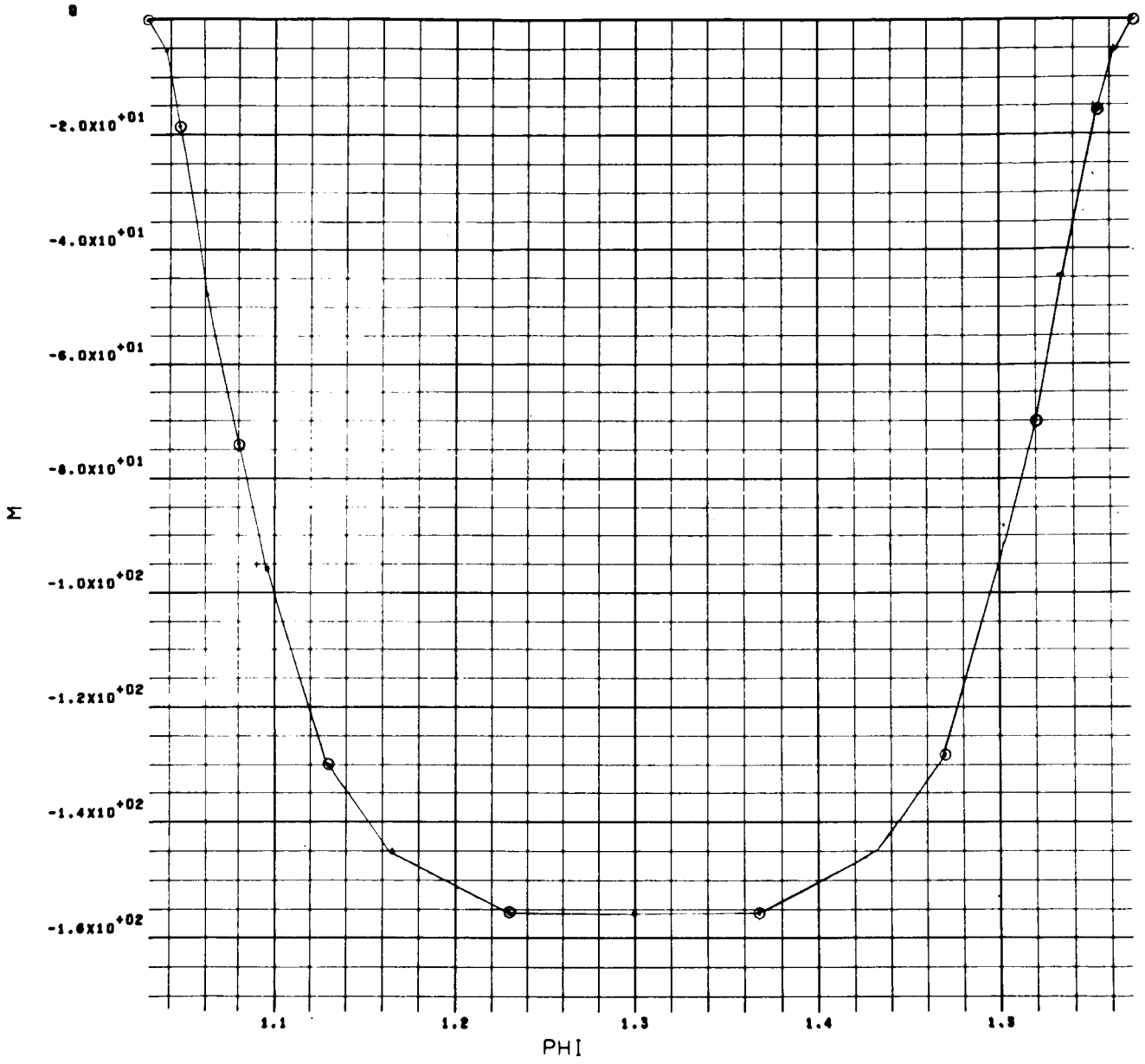
EXAMPLE SPHERICAL SEGMENT UNDER UNIFORM NORMAL PRESSURE

44BFYd
014 000

- o CURVE 1= UPPER BOUNDARY
- x CURVE 2= LOWER BOUNDARY



n - Boundary Stress Resultants



o - Boundary Stress Resultants

4.3 LISTING OF THE PROGRAM

The complete program is given in Table 6.

Table 6

STUDY OF JUNCTURE STRESS FIELD: SPHERICAL SEGMENT

| | |
|---|----------|
| * CHAIN(1,2) | S1P00010 |
| * FORTRAN | S1P00020 |
| * LIST | S1P00030 |
| C S1P SPHERICAL SEGMENT , STUDY OF JUNCTURE STRESS FIELD , | S1P00040 |
| C CONTRACT NAS 8-114800 TO NASA G.C. MARSHALL SPACE FLIGHT CENTER | S1P00050 |
| C HUNTSVILLE, ALABAMA | S1P00060 |
| C BY SOLID MECHANICS , AEROSPACE SCIENCES LABORATORY , 52-20 | S1P00070 |
| C LOCKHEED MISSILES AND SPACE COMPANY, PALO ALTO CALIF | S1P00080 |
| C THIS PROGRAM IS FOR USE ONLY ON FORTRAN II, VERSION II | S1P00090 |
| C COMMON IOPT1, IOPT2, IOPT3, IOPT4, IOPT5, IOPT6, IOPT7, IOPT8 | S1P00100 |
| C COMMON NCF | S1P00110 |
| C COMMON NDIM, NROW, NCOL, MM, MFLAG, XM,XLD | S1P00120 |
| C COMMON ISW1, ISW2, ISW3 | S1P00130 |
| C COMMON A | S1P00140 |
| C COMMON TMP, YK, YL | S1P00150 |
| C COMMON T1, T2, XX, XX1, Z, Z1, Z2 | S1P00160 |
| C COMMON ZNU, THC, PHI, FF, RH, DD, XH, XK | S1P00170 |
| C COMMON ZETA | S1P00180 |
| C COMMON TE, TI, TO, OC, TC, TD, DDL | S1P00190 |
| C COMMON RECORD | S1P00200 |
| C COMMON TIM1,TIM2, KTIME | S1P00210 |
| C DIMENSION A(1232) | S1P00220 |
| C DIMENSION MM(40) | S1P00230 |
| C DIMENSION T1(89), T2(89), XX(89), XX1(89), Z(89), Z1(89), Z2(89) | S1P00240 |
| C DIMENSION TMP(5184), YK(5184), YL(4,4,324) | S1P00250 |
| C DIMENSION ZETA (30) | S1P00260 |
| C DIMENSION RECORD (12) | S1P00270 |
| 1 FORMAT (1H1, 12A6) | S1P00280 |
| 2 FORMAT (6E12.8) | S1P00290 |
| 3 FORMAT (1H1) | S1P00300 |
| 4 FORMAT (35I2) | S1P00310 |
| 5 FORMAT (1H1,3X,3HCOL , 15, 8I14/4H ROW) | S1P00320 |
| 6 FORMAT (14, 1P9E14.6) | S1P00330 |
| 7 FORMAT (10I1) | S1P00340 |

8 FORMAT (12A6) SIP000350
 14 FORMAT (26H0 FINITE DIFFERENCE MESH. I2, 7H ROWS, I2,27H COLUMNSS) SIP000360
 1. MESH SPACING. H= F15.7, 4H, K= E15.7) SIP000370
 15 FORMAT (21H0INPUT CONSTANTS. NU= 1PE12.5, 9H, THETAC= 1PE12.5, SIP000380
 1 7H, PH11= 1PE12.5, 12H, PH11/PHI2= 1PE12.5, 6H, R/H= 1PE12.5) SIP000390
 17 FORMAT (42H0 SPHERE DISPLACEMENT COMPONENTS (U,V,W) / SIP000400
 1 10H0 COL ROW , 17X, 1HU, 15X, 1HV, 15X, 1HW) SIP000410
 18 FORMAT (53H ROW COL NX NTHETA NXTHETA NTHETA) SIP000420
 19 FORMAT (125HOROW COL EPSX EPST GAMMA R*SIP000430
 1X1 R*X12 OMEGAX P S1P000440
 2HI) SIP000450
 20 FORMAT (28H0 SPHERE STRESS RESULTANTS.) SIP000460
 919 FORMAT (34H GRADED MESH IN ZETA DIRECTION) SIP000470
 920 FORMAT (2X, 4H ROW, 15I8/ 6X, 15I8) SIP000480
 921 FORMAT (6H ZETA=, 15F8.5/ 6X, 15F8.5) SIP000490
 922 FORMAT (27H ROW 1 IS A SYMMETRY LINE) SIP000500
 925 FORMAT (25H0UNIFORM RADIAL PRESSURE) SIP000510
 930 FORMAT (1H I3, 1H, I3, 10X, 1P3E16.6) SIP000520
 931 FORMAT (1H I3, 1H, I3,10H BOUNDARY , 1P3E16.6) SIP000530
 932 FORMAT (1H I3, 1H, I3,10H SMTY LINE ,1P3E16.6) SIP000540
 936 FORMAT (30H0 BOUNDARY STRESS RESULTANTS. /84HOROW COL NTAN SIP000550
 1 NNORM Q M RBAR) SIP000560
 937 FORMAT(I3,1H, I3, 1P5E12.4) SIP000570
 938 FORMAT (I3, 2H, I3, 66X, 1PE16.7) SIP000580
 939 FORMAT (59H0 SPHERE STRAINS, CHANGES OF CURVATURE AND ROTATIO) SIP000590
 1N.) SIP000600
 945 FORMAT (1H0 // 8H CASE NR I2,13H COMPLETED IN F8.3, 9H MINUTES.) SIP000610
 951 FORMAT (33H0LINEAR TEMPERATURE GRADIENT. TE=E15.7,5H, TI=E15.7, SIP000620
 1 5H, TO=E15.7, 5H, OC=E15.7) SIP000630
 962 FORMAT (90H ROW COL MX MTHETA MXTHETA QX) SIP000640
 1 QTHETA) SIP000650
 C SET TAPE ASSIGNMENTS. SIP000660
 KTAPE=15 SIP000670
 MTAPE=7 SIP000680
 B XMTP=000000002221 SIP000690
 B XZTP=000000002223 SIP000700
 B XNTP=000000001224 SIP000710
 B NTAPE=4 SIP000720
 IZTAPE=3 SIP000730

SIP00740
 SIP00750
 SIP00760
 SIP00770
 SIP00780
 SIP00790
 SIP00800
 SIP00810
 SIP00820
 SIP00830
 SIP00840
 SIP00850
 SIP00860
 SIP00870
 SIP00880
 SIP00890
 SIP00900
 SIP00910
 SIP00920
 SIP00930
 SIP00940
 SIP00950
 SIP00960
 SIP00970
 SIP00980
 SIP00990
 SIP01000
 SIP01010
 SIP01020
 SIP01030
 SIP01040
 SIP01050
 SIP01060
 SIP01070
 SIP01080
 SIP01090
 SIP01100
 SIP01110
 SIP01120

```

REWIND MTAPE
REWIND NTAPE
REWIND IZTAPE
CALL CLOCK (TIM1)
NCF = 44
C READ AND WRITE INPUT DATA
21 READ INPUT TAPE 5, 8, RECORD
WRITE OUTPUT TAPE 6, 1, RECORD
C IOPT1 = 0 CONSTANT MESH SPACING
C IOPT1 = 1 GRADED MESH SPACING IN X DIRECTION
C IOPT2=0 SYMMETRY LINE AT PHI=PHI/2*(1+FF)
C IOPT2=1 NO SYMMETRY LINE
C IOPT3 = 0 OMIT SPHERE STRAINS, CHANGES IN CURVATURE AND ROTATION
C IOPT3 = 1 PRINT OUT STRAINS, ETC.
C IOPT4=0 UNIFORM NORMAL PRESSURE
C IOPT4=1 LINEAR TEMPERATURE GRADIENT
C IOPT5=0 NOT FINAL CASE WITH PLOTS
C IOPT5=1 FINAL CASE WITH PLOTS
READ INPUT TAPE 5, 7, IOPT1, IOPT2, IOPT3, IOPT4, IOPT5, IOPT6, IOPT7, IOPT8
1, IOPT8
XM = IOPT1
XLD=IOPT4
READ INPUT TAPE 5, 2, ROW, COL, XH, XK
READ INPUT TAPE 5, 2, ZNU, THC, PHI, FF, RH
NROW=ROW
NCOL=COL
NCI=NCOL+1
NR1=NROW+1
ITOT=3*(NROW+6)
WRITE OUTPUT TAPE 6, 14, NROW, NCOL, XH, XK
WRITE OUTPUT TAPE 6, 15, ZNU, THC, PHI, FF, RH
DD = 1./ (12.*RH*RH)
IF (IOPT1) 23, 23, 22
22 READ INPUT TAPE 5, 4, (MM(I), I=1, NROW)
MM(NR1)=MM(NROW)
WRITE OUTPUT TAPE 6, 919
GO TO 25
23 DO 24 J=1, 30
24 MM(J)=0

```

```

25 IF (IOPT2) 31, 31, 26
26 YK(0)=PH1*FF
ZETA(1) = PH1*FF
X = ZETA(1) - XH/2.**MM(1)
YK(1)=X
ZETA(2)=X
NDIM=3*NROW
MO=0
GO TO 35
31 YK(1)=PH1*(1.+FF)/2.
X=YK(1)
ZETA (2)=X
NDIM=3*NROW-1
WRITE OUTPUT TAPE 6, 922
NCRV1=1
MO=1
35 WRITE OUTPUT TAPE 6, 920, (I, I=MO,NR1)
NR4=NR1+1-MO
DO 30 J=2, NROW
IF (MM(J)-MM(J-1)) 27, 27, 28
27 JM=MM(J)
GO TO 29
28 JM=MM(J-1)
29 X=X-XH/2.**JM
YK(J)=X
ZETA(J+1)=X
30 CONTINUE
YK(NR1)=PH1
ZETA (NR1+1)=PH1
WRITE OUTPUT TAPE 6, 921, (YK(I), I=MO, NR1)
NSM=NDIM-NROW
NSQ=72*NDIM
IF(IOPT4-1) 82, 106, 106
82 WRITE OUTPUT TAPE 6, 925
GO TO 84
106 READ INPUT TAPE 5, 2, TE, TI, TO, OC
WRITE OUTPUT TAPE 6, 951, TE, TI, TO, OC
TT1 = (TE + TI)/2. - TO
TT2 = (TE -TI)

```

```

SIP01130
SIP01140
SIP01150
SIP01160
SIP01170
SIP01180
SIP01190
SIP01200
SIP01210
SIP01220
SIP01230
SIP01240
SIP01250
SIP01260
SIP01270
SIP01280
SIP01290
SIP01300
SIP01310
SIP01320
SIP01330
SIP01340
SIP01350
SIP01360
SIP01370
SIP01380
SIP01390
SIP01400
SIP01410
SIP01420
SIP01430
SIP01440
SIP01450
SIP01460
SIP01470
SIP01480
SIP01490
SIP01500
SIP01510

```

```

TC = (1.+ ZNU)*OC*TT1
TD = (1.+ZNU)*OC*TT2
84 CONTINUE
79 READ INPUT TAPE 5, 4, (MM(I), I=31, 35)
CALL COEFZ
MFLAG=0
IF (KTIME) 81,81,400
81 CONTINUE
REWIND KTAPE
C COMPUTE L, M, N AND Z MATRICES OF FORWARD SWEEP
400 KTIME=KTIME+1
N1=NSM
N2=NSM
N3=NSM
I=1
GO TO 405
401 CALL WTAPE (XZTP,Z1,N1,1)
CALL RTAPE (XMTP,TMP, NSQ, 0)
CALL MTX (YK, I, 2)
IF (I-2) 405, 403, 402
402 CALL BACK (XNTP)
CALL ZERO (YL, NSQ)
CALL RTAPE (XMTP, TMP, NSQ,1)
CALL MTXS (TMP, YL, I, 1)
CALL RTAPE (XMTP, TMP, NSQ,0)
CALL ADDM (YK, YL, YK, -NSQ)
CALL RTAPE (XNTP, YL, NSQ, 0)
403 NI=NDIM
CALL RTAPE (XMTP, TMP, NSQ,1)
CALL MATM (YK, TMP, TMP,NDIM,N2, NDIM)
IF (I-2) 405, 405, 404
404 CALL RTAPE (XNTP, YL, NSQ, 1)
CALL MTXS (YL, TMP,I, 1)
405 CALL MTX (YL, I, 3)
IF (I-2) 408, 406, 406
406 CALL ADDM (YL, TMP, YL,-NSQ)
IF (I-NCOL) 407, 408, 408
407 CALL RTAPE (XNTP, TMP, NSQ,0)

```

| | | |
|-----|--|----------|
| 408 | CALL INVERT (YL, N1, ISING) | S1P01910 |
| | IF (I-1) 414, 414, 410 | S1P01920 |
| 410 | CALL MATM (YK, Z1, T2, NDIM, N2, 1) | S1P01930 |
| | IF (I-NCOL) 411, 421, 421 | S1P01940 |
| 411 | CALL RTAPE (XNTP, TMP, NSQ, 1) | S1P01950 |
| | CALL MATM (YK, TMP, TMP, NDIM, N2, NDIM) | S1P01960 |
| 414 | CALL MTX (YK, I, 4) | S1P01970 |
| | IF (I-2) 417, 416, 416 | S1P01980 |
| 416 | CALL ADDM (YK, TMP, YK, -NSQ) | S1P01990 |
| 417 | IF (I-NCOL+1) 418, 419, 419 | S1P02000 |
| 418 | CALL ZERO (TMP, NSQ) | S1P02010 |
| | CALL MTXS (YL, TMP, I, 5) | S1P02020 |
| | CALL WTAPE (XNTP, TMP, NSQ, 0) | S1P02030 |
| 419 | CALL MATM (YL, YK, YK, N1, N1, NDIM) | S1P02040 |
| | CALL WTAPE (XMTP, YK, NSQ, 0) | S1P02050 |
| | IF (I-NCOL+1) 420, 421, 421 | S1P02060 |
| 420 | CALL WTAPE (XNTP, TMP, NSQ, 1) | S1P02070 |
| | CALL BACK (XNTP) | S1P02080 |
| 421 | CALL CONS (T1, I) | S1P02090 |
| | IF (I-1) 426, 426, 422 | S1P02100 |
| 422 | CALL ADDM (T1, T2, T1, -NDIM) | S1P02110 |
| | IF (I-2) 426, 424, 423 | S1P02120 |
| 423 | CALL MTXS (Z2, T2, I, -1) | S1P02130 |
| 424 | DO 425 J=1, NDIM | S1P02140 |
| 425 | Z2(J)=Z1(J) | S1P02150 |
| | IF (I-NCOL) 426, 428, 428 | S1P02160 |
| 426 | CALL WTAPE (XMTP, YK, NSQ, 1) | S1P02170 |
| | CALL BACK (XMTP) | S1P02180 |
| | IF (I-2) 430, 429, 428 | S1P02190 |
| 428 | CALL ADDM (T1, T2, T1, -NDIM) | S1P02200 |
| | CALL BACK (XMTP) | S1P02210 |
| 430 | CALL MATM (YL, T1, Z1, N1, N1, 1) | S1P02220 |
| | CALL WTAPE (XZTP, Z1, N1, 0) | S1P02230 |
| | IF (I-NCOL) 431, 450, 450 | S1P02240 |
| 431 | IF (I-2) 434, 433, 432 | S1P02250 |
| 432 | N3=NDIM | S1P02260 |
| 433 | N2=NDIM | S1P02270 |
| 434 | I=I+1 | S1P02280 |
| | GO TO 401 | S1P02290 |

```

C      DECOMPOSITION COMPLETED • BEGIN BACKWARD SWEEP.
450  CALL WTAPE (XZTP, ZI, NI, I)
      CALL BACK (XZTP)
      CALL BACK (XNTP)
      N4= (NCOL+3)*(NROW+6)*3
      CALL ZERO (TMP, N4)
451  IF (I-NCOL) 452, 454, 454
452  DO 453 J=1, NDIM
      XX1(J)=XX(J)
453  XX(J)=ZI(J)
      CALL RTAPE (XMTP, YK, NSQ, I)
      CALL BACK (XMTP)
      IF (I-1) 454, 454, 4541
4541 CALL BACK (XMTP).
454  CALL RTAPE (XZTP, ZI, NI, 0)
      CALL RTAPE (XZTP, ZI, NI, 1)
      IF (I-1) 4543, 4543, 4542
4542 CALL BACK (XZTP)
4543 CALL BACK (XZTP)
      IF (I-NCOL+1) 456, 457, 462
456  CALL RTAPE (XNTP, YL, NSQ, 0)
457  CALL MATM( YK, XX, TI, NI, NDIM, 1)
      CALL ADDM (ZI, TI, ZI, -NDIM)
      IF (I-NCOL+1) 458, 462, 462
458  CALL RTAPE (XNTP, YL, NSQ, 1)
      IF (I-1) 4591, 4591, 459
459  CALL BACK (XNTP)
4591 CALL BACK (XNTP)
      CALL MATM (YL, XX1, TI, NI, NDIM, 1)
      CALL ADDM (ZI, TI, ZI, -NDIM)
460  IF (I-2) 463, 461, 462
461  NI=NSM
462  CALL RTAPE (XMTP, YK, NSQ, 0)
463  CALL STORE (ZI, I)
      IF (I-2) 500, 464, 464
464  I=I-1
      GO TO 452
500  MFLAG=1
      IF (IOPT2) 145, 145, 140

```

S1P02690
 S1P02700
 S1P02710
 S1P02720
 S1P02730
 S1P02740
 S1P02750
 S1P02760
 S1P02770
 S1P02780
 S1P02790
 S1P02800
 S1P02810
 S1P02820
 S1P02830
 S1P02840
 S1P02850
 S1P02860
 S1P02870
 S1P02880
 S1P02890
 S1P02900
 S1P02910
 S1P02920
 S1P02930
 S1P02940
 S1P02950
 S1P02960
 S1P02970
 S1P02980
 S1P02990
 S1P03000
 S1P03010
 S1P03020
 S1P03030
 S1P03040
 S1P03050
 S1P03060
 S1P03070

```

140 L0=6
    DO 141 L=1, NCOL
      TMP(L0)=TMP(L0+6)
141 L0=L0+ITOT
      L1=L0-ITOT
      L0=L0+ITOT
      TMP(L0)=TMP(L1)
145 L0=NCI*ITOT+12
    DO 147 J=1, NROW
      L1=L0-2*ITOT
      TMP(L0)=TMP(L1)
147 L0=L0+3
      L0=L0+3
      TMP(L0)=TMP(L1)
      L0=L0-ITOT
    DO 148 I=1, NCOL
      L0=L0-ITOT
      TMP(L0)=TMP(L1)
148 L1=L1-ITOT
      CALL BOUND
      IOUT=51
      NC2=NCOL+3
      IF (IOPT2) 501,501, 502
501 NR2=NROW+3
      GO TO 503
502 NR2=NROW+6
503 DO 520 I=1, NC2
      I3=I*(NROW+6)*3
      I2=I3-1
      I1=I2-1
      IF (IOUT+NR2-50) 505, 505, 504
504 WRITE OUTPUT TAPE 6, 1
      WRITE OUTPUT TAPE 6, 17
      IOUT=6
505 DO 515 JJ=1, NR2
      J=NROW-JJ+4
      IF (J-NR1) 506, 511, 510
506 IF (IOPT2) 507,507, 508
507 IF (J-1) 512, 512, 510
  
```


| | | |
|------|---|----------|
| 508 | IF (J) 510, 511, 510 | S1P03080 |
| 510 | WRITE OUTPUT TAPE 6, 930, I, J, TMP(I1), TMP(I2), TMP(I3) | S1P03090 |
| | GO TO 514 | S1P03100 |
| 511 | WRITE OUTPUT TAPE 6, 931, I, J, TMP(I1), TMP(I2), TMP(I3) | S1P03110 |
| | GO TO 514 | S1P03120 |
| 512 | WRITE OUTPUT TAPE 6, 932, I, J, TMP(I1), TMP(I2), TMP(I3) | S1P03130 |
| 514 | I1=I1-3 | S1P03140 |
| | I2=I2-3 | S1P03150 |
| | I3=I3-3 | S1P03160 |
| 515 | IOUT=IOUT+1 | S1P03170 |
| 520 | CONTINUE | S1P03180 |
| 521 | ISW3=1 | S1P03190 |
| | IOUT=50 | S1P03200 |
| | L=32 | S1P03210 |
| | K=0 | S1P03220 |
| | DO 540 J=M0, NR1 | S1P03230 |
| | IF (IOPT1) 537,537,536 | S1P03240 |
| 536 | CALL GRADE (J) | S1P03250 |
| 537 | IF (MM(31)) 5378, 5378, 5370 | S1P03260 |
| 5370 | IF (MM(L)-J) 5378, 5378, 5378 | S1P03270 |
| 5372 | IF (L-35) 5374, 5374, 5378 | S1P03280 |
| 5374 | L=L+1 | S1P03290 |
| | K=K+1 | S1P03300 |
| | K1=K | S1P03310 |
| | GO TO 5380 | S1P03320 |
| 5378 | K1=0 | S1P03330 |
| 5380 | DO 540 I=1, NC1 | S1P03340 |
| | IF (IOUT-41) 539, 538, 538 | S1P03350 |
| 538 | WRITE OUTPUT TAPE 6, 1, RECORD | S1P03360 |
| | IOUT=0 | S1P03370 |
| | IF (MFLAG) 532, 530, 531 | S1P03380 |
| 531 | WRITE OUTPUT TAPE 6, 20 | S1P03390 |
| | WRITE OUTPUT TAPE 6, 18 | S1P03400 |
| | GO TO 539 | S1P03410 |
| 530 | WRITE OUTPUT TAPE 6, 20 | S1P03420 |
| | WRITE OUTPUT TAPE 6, 962 | S1P03430 |
| | GO TO 539 | S1P03440 |
| 532 | WRITE OUTPUT TAPE 6, 939 | S1P03450 |
| | WRITE OUTPUT TAPE 6, 19 | S1P03460 |

```

539 IOUT=IOUT+1
    CALL STRESS (I,J,K1)
540 CONTINUE
    IF (MFLAG) 999, 544, 541
541 MFLAG=0
    GO TO 521
544 WRITE OUTPUT TAPE 6, 1, RECORD
    IO=0
    I1=1
    I2=4
    WRITE OUTPUT TAPE 6, 936
    I=1
    DO 560 JJ=1, NRI
      J=NR1+1-JJ
550 WRITE OUTPUT TAPE 6, 937, J, I, (YK(I3), I3=I1, I2)
      I1=I1+4
      I2=I1+3
      IF (I-NCOL) 551, 552, 560
551 I=I+1
      GO TO 550
552 I=NC1
      WRITE OUTPUT TAPE 6, 937, J, NC1, (YK(I3), I3=I1, I2)
      K1=8*(NC1+NR1)-3
      WRITE OUTPUT TAPE 6, 938, J, NC1, YK(K1)
      I1=I1+4
      I2=I1+3
      GO TO 550
560 CONTINUE
562 WRITE OUTPUT TAPE 6, 937, IO, NC1, (YK(I3), I3=I1, I2)
      K1=K1+4
      WRITE OUTPUT TAPE 6, 938, IO, NC1, YK(K1)
      I1=I1+4
      I2=I1+3
      IF (IOPT2) 566, 566, 564
564 CONTINUE
      DO 565 II=1, NC1
        I=NC1+1-II
        WRITE OUTPUT TAPE 6, 937, IO, I, (YK(I3), I3=I1, I2)

```

```

S1P03470
S1P03480
S1P03490
S1P03500
S1P03510
S1P03520
S1P03530
S1P03540
S1P03550
S1P03560
S1P03570
S1P03580
S1P03590
S1P03600
S1P03610
S1P03620
S1P03630
S1P03640
S1P03650
S1P03660
S1P03670
S1P03680
S1P03690
S1P03700
S1P03710
S1P03720
S1P03730
S1P03740
S1P03750
S1P03760
S1P03770
S1P03780
S1P03790
S1P03800
S1P03810
S1P03820
S1P03830
S1P03840
S1P03850

```

```

I1=I1+4
I2=I1+3
565 CONTINUE
566 IF(IOPT3) 999,999,545
545 MFLAG=-1
XM=0.
GO TO 521
999 CONTINUE
80 CALL CLOCK (TIM2)
TIME=TIM2-TIM1
TIM1=TIM2
PRINT 945, KTIME, TIME
WRITE OUTPUT TAPE 6, 945, KTIME, TIME
IF (MM(31)) 1000, 1000, 601
601 CALL CHAIN (2, 2)
1000 CALL RESET
GO TO 21
END
*
FORTRAN
SUBROUTINE ADDM (X, Y, Z, M)
DIMENSION X(3600), Y(3600), Z(3600)
IF (M) 20,1,1
1 DO 10 I=1,M
10 Z(I)= X(I)+Y(I)
11 GO TO 50
20 M=-M
DO 25 I=1,M
25 Z(I)= X(I)-Y(I)
50 RETURN
END
*
FORTRAN
SUBROUTINE BOUND
COMMON IOPT1, IOPT2, IOPT3, IOPT4, IOPT5, IOPT6, IOPT7, IOPT8
COMMON NCF
COMMON NDIM, NROW,NCOL,MM,I1,KM1,KM2,KP1,KP2,MFLAG,XM,XLD
COMMON ISW1, ISW2, ISW3
COMMON A, A1, A2, A3, A4, A5, A6, A7, A8, A9, A10, A11, A12
COMMON R, B1, B2, B3, B4, B5, B6, B7, B8, B9, B10
COMMON C, C1, C2, C3, C4, C5, C6, C7, C8,C9, C10,C11,C12,C13,C14,

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```

S1P03860
S1P03870
S1P03880
S1P03890
S1P03900
S1P03910
S1P03920
S1P03930
S1P03940
S1P03950
S1P03960
S1P03970
S1P03980
S1P03990
S1P04000
S1P04010
S1P04020
S1P04030
S1P04040
S1P04050
S1P04060
S1P04070
S1P04080
S1P04090
S1P04100
S1P04110
S1P04120
S1P04130
S1P04140
S1P04150
S1P04160
S1P04170
S1P04180
S1P04190
S1P04200
S1P04210
S1P04220
S1P04230
S1P04240

```

```

1 C15, C16, C17, C18, C19
COMMON FILL
COMMON TMP, YK, YL
DIMENSION FILL(1188)
DIMENSION TMP (5184), YK(5184), YL(5184)
DIMENSION MM(35)
DIMENSION NN(3)
I1=0
NRI=NROW+1
NCI=NCOL+1
L=0
ITOT=3*(NROW+6)
L1=ITOT
CALL GRADE(1)
LL=KP2
CALL GRADE(NROW)
LL2=KM2
DO 460 I=1, NCOL
TP=TMP(L+15)
TP2=TMP(L1-12)
N1=L1
DO 458 K=3,5
N=K+L
CALL EXTRA (TMP( N), TMP( N+3), TMP( N+6), TMP( N+9), TP)
CALL EXTRA (TMP(N1), TMP(N1-3), TMP(N1-6), TMP(N1-9), TP2)
N1=K+L1-8
TP =TMP(N+13)
TP2=TMP(N1-12)
IF (LL) 453, 454, 454
453 TP=(TP+TMP(N+10))*0.5
454 IF (LL2) 458, 458, 456
456 TP2=(TP2+TMP(N1-9))*0.5
458 CONTINUE
L=L+ITOT
L1=L1+ITOT
460 CONTINUE
NN(1)=NCI*ITOT+7
NN(2)=NN(1)+1
NN(3)=NN(2)+ITOT+1

```

```

S1P04250
S1P04260
S1P04270
S1P04280
S1P04290
S1P04300
S1P04310
S1P04320
S1P04330
S1P04340
S1P04350
S1P04360
S1P04370
S1P04380
S1P04390
S1P04400
S1P04410
S1P04420
S1P04430
S1P04440
S1P04450
S1P04460
S1P04470
S1P04480
S1P04490
S1P04500
S1P04510
S1P04520
S1P04530
S1P04540
S1P04550
S1P04560
S1P04570
S1P04580
S1P04590
S1P04600
S1P04610
S1P04620
S1P04630

```

```

DO 515 J=1, NROW
DO 510 K=1, 3
N=NN(K)+3*J
N1=N-ITOT
N2=N1-ITOT
N3=N2-ITOT
N4=N3-ITOT
CALL EXTRA (TMP(N), TMP(N1), TMP(N2), TMP(N3), TMP(N4))
510 CONTINUE
515 CONTINUE
L=NC1*ITOT
L1=L+4
LL=L1-2*ITOT
TMP(L1)=(TMP(LL)+TMP(L1+6))/2.
TMP(L1+1)=(TMP(LL+1)+TMP(L1+7))/2.
L1=L+ITOT-5
LL=L1-2*ITOT
TMP(L1)=(TMP(LL)+TMP(L1-6))/2.
TMP(L1+1)=(TMP(LL+1)+TMP(L1-5))/2.
RETURN
END
*
*
FORTRAN
LIST
SUBROUTINE CF(I, J, MF, K, AA, X)
COMMON IOPT1, IOPT2, IOPT3, IOPT4, IOPT5, IOPT6, IOPT7, IOPT8
COMMON NCF
COMMON NDIM, NROW, NCOL, MM, I1, KM1, KM2, KP1, KP2, MFLAG, XM, XLD
COMMON ISW1, ISW2, ISW3
COMMON A
COMMON TMP, YK, YL
DIMENSION MM(35)
DIMENSION A(1232)
DIMENSION AA(1)
DIMENSION X(72, 72)
DIMENSION TMP (5184), YK(5184), YL(5184)
C COMPUTE COEFFICIENT OF KTH UNKNOWN FOR MESH PT I,J.
I2=I
J2=J
M=MF

```

```

S1P04640
S1P04650
S1P04660
S1P04670
S1P04680
S1P04690
S1P04700
S1P04710
S1P04720
S1P04730
S1P04740
S1P04750
S1P04760
S1P04770
S1P04780
S1P04790
S1P04800
S1P04810
S1P04820
S1P04830
S1P04840
S1P04850
S1P04860
S1P04870
S1P04880
S1P04890
S1P04900
S1P04910
S1P04920
S1P04930
S1P04940
S1P04950
S1P04960
S1P04970
S1P04980
S1P04990
S1P05000
S1P05010
S1P05020

```

```

J4 = ISW1*NCF+1
NC1=NCOL+1
NR1=NROW+1
IF (ISW2) 107, 108, 106
106 J4=1
GO TO 108
107 FCTR=-1.
GO TO 109
108 FCTR=1.
109 IF (M) 110, 100, 120.
110 IF (M+1) 111, 112, 112
111 J2=J2-1
M=0
GO TO 100
112 FCTR=FCTR/2.
J5=J2-1
GO TO 101
120 IF (M-1) 122, 122, 121.
121 J2=J2+1
M=0
GO TO 100
122 FCTR=FCTR/2.
J5=J2+1
100 CONTINUE
101 IF (I2-1) 2, 4, 6
C COL I2 IS LEFT OF X-AXIS. REFLECT OVER SYMMETRY LINE. CHANGE SIGN
C IF K=2
2 I2=-I2+2
IF (K-2) 6, 3, 6
3 FCTR=-FCTR
GO TO 6
C COL I2 IS X-AXIS. OMIT COEFFICIENT IF K=2
4 IF (K-2) 6, 99, 6
6 IF (J2-NR1) 14, 99, 7
7 IF (J2-NR1-1) 8, 8, 11
8 IF (K-2) 11, 11, 9
9 IF (I2-NC1) 10, 99, 11
C COL J2 IS BEYOND THE BOUNDARY. K=3. SET J2=NROW-1

```

```

SIP05030
SIP05040
SIP05050
SIP05060
SIP05070
SIP05080
SIP05090
SIP05100
SIP05110
SIP05120
SIP05130
SIP05140
SIP05150
SIP05160
SIP05170
SIP05180
SIP05190
SIP05200
SIP05210
SIP05220
SIP05230
SIP05240
SIP05250
SIP05260
SIP05270
SIP05280
SIP05290
SIP05300
SIP05310
SIP05320
SIP05330
SIP05340
SIP05350
SIP05360
SIP05370
SIP05380
SIP05390
SIP05400

```

```

10 J2=J2-?
GO TO 50
11 J2=NR1
12 IF (I2-NC1) 80, 99, 13
13 I2=NC1
GO TO 80
14 IF (IOPT2) 15, 15, 19
15 IF (J2-1) 16, 18, 25
16 J2=-J2+2
IF (K-1) 17, 17, 25
17 FCTR=-FCTR
GO TO 25
18 IF (K-1) 99, 99, 25
19 IF (J2) 20, 99, 25
20 IF (J2+1) 24, 21, 21
21 IF (K-2) 24, 24, 22
22 IF (I2-NC1) 23, 99, 24
23 J2=1
GO TO 50
24 J2=0
GO TO 12
25 IF (I2-NC1) 50, 99, 26
26 IF (I2-NC1-1) 27, 27, 13
27 IF (K-2) 13, 13, 28
28 I2=I2-2
50 J1=INDEX(I2, J2, K)
IF (MFLAG) 51, 51, 52
51 X(I1, J1)=X(I1, J1)+AA(J4)*FCTR
125 IF (M) 130, 99, 130
52 YK(I1+2970)=YK(I1+2970)-AA(J4)*FCTR*TMP(J1)
GO TO 125
80 J1=INDEX(I2, J2, K)
J3=(J1+5-I1)*270+I1
YK(J3)=YK(J3)+AA(J4)*FCTR
IF (M) 135, 99, 135
99 RETURN
130 J2=J5
M=0
GO TO 50
135 J2=J5

```

```

S1P05410
S1P05420
S1P05430
S1P05440
S1P05450
S1P05460
S1P05470
S1P05480
S1P05490
S1P05500
S1P05510
S1P05520
S1P05530
S1P05540
S1P05550
S1P05560
S1P05570
S1P05580
S1P05590
S1P05600
S1P05610
S1P05620
S1P05630
S1P05640
S1P05650
S1P05660
S1P05670
S1P05680
S1P05690
S1P05700
S1P05710
S1P05720
S1P05730
S1P05740
S1P05750
S1P05760
S1P05770
S1P05780
S1P05790
S1P05800

```

```

M=0
GO TO 80
END
*
FORTRAN
FUNCTION CFZ( J, AA)
COMMON IOPT1, IOPT2, IOPT3, IOPT4, IOPT5, IOPT6, IOPT7, IOPT8
COMMON NCF
COMMON NDIM, NROW, NCOL, MM, MFLAG, XM,XLD
DIMENSION MM(40), AA(1)
J1 = J*NCF+1
CFZ=AA(J1)
RETURN
END
*
FORTRAN
SUBROUTINE COEFZ
COMMON IOPT1, IOPT2, IOPT3, IOPT4, IOPT5, IOPT6, IOPT7, IOPT8
COMMON NCF
COMMON NDIM, NROW, NCOL, MM, MFLAG, XM,XLD
COMMON ISW1, ISW2, ISW3
COMMON A, A1, A2, A3, A4, A5, A6, A7, A8, A9, A10, A11, A12
COMMON B, B1, B2, B3, B4, B5, B6, B7, B8, B9, B10
COMMON C, C1, C2, C3, C4, C5, C6, C7, C8, C9, C10, C11, C12, C13, C14,
1 C15, C16, C17, C18, C19
COMMON FILL
COMMON TMP, YK, YL
COMMON T1, T2, XX, XXI, Z, Z1, Z2
COMMON ZNU, THC, PHI, FF, RH, DD, XXH, XK
DIMENSION TMP (5184), YK(5184), YL(5184)
DIMENSION T1( 89), T2(89), XX(89), XXI(89), Z(89), Z1(89), Z2(89)
DIMENSION MM(40)
DIMENSION A(1)
DIMENSION FILL (1188)
NR1=NROW+1
D1 = (1.-ZNU)
D2 = (1. +ZNU)
D3 = (1.+DD)
D4 = (1.+4.*DD)
D5 = (2.-ZNU)
D6 = (3.-ZNU)

```

```

S1P05810
S1P05820
S1P05830
S1P05840
S1P05850
S1P05860
S1P05870
S1P05880
S1P05890
S1P05900
S1P05910
S1P05920
S1P05930
S1P05940
S1P05950
S1P05960
S1P05970
S1P05980
S1P05990
S1P06000
S1P06010
S1P06020
S1P06030
S1P06040
S1P06050
S1P06060
S1P06070
S1P06080
S1P06090
S1P06100
S1P06110
S1P06120
S1P06130
S1P06140
S1P06150
S1P06160
S1P06170
S1P06180
S1P06190

```


D7 = (3.-2.*ZNUJ)
YA5 = D2/2. + D5*DE
YA66 = D6/2. + D7*UD
YB10 = D2 -2.*D1*DD
DO 60 JJ = 0,NR1
J = NR1 -JJ
IF(J) 55,55, 54
54 XH = XXH/(2.**MM(J))
55 X = YK(J)
SX = SINF(X)
CX = COSF(X)
YA1 = D3 *SX
YA2 = D1*D4/(2.*SX)
YA3 = D3*CX
YA4 = -D3*(CX*CX + ZNU*SX*SX)/SX
YA6 = -YA66*CX/SX
YA7 = -DD*SX
YA8 = -D5*DD/SX
YA9 = -DD*CX
YA10 = D6*DD*CX/(SX*SX)
YA11 = (D2*SX - DD *YA4/D3)
YB3 = D1*D4*SX/2.
YB4 = D3/SX
YB5 = D1*D4*CX/2.
YB6 = YA2*(2.*SX*SX- 1.)
YB7 = -D5*DD
YB8 = -DD/(SX*SX)
YB9 = -DD*CX/SX
YC2 = D5/SX
YC3 = 2.*CX
YC4 = CX/(SX*SX)
YC5 = -((1.+ZNU*SX*SX)/SX + D2*SX/DD)
YC6 = (D1-D2/DD + 1.)/(SX*SX)*CX
YC8 = 1./(SX*SX)
YC9 = -CX/SX
YC10 = (2.*D1 -D2/DD+ YC8)
YC12 = -2./SX
YC13 = -YC8/SX
YC15 = 2.*CX*YC8

S1P06200
S1P06210
S1P06220
S1P06230
S1P06240
S1P06250
S1P06260
S1P06270
S1P06280
S1P06290
S1P06300
S1P06310
S1P06320
S1P06330
S1P06340
S1P06350
S1P06360
S1P06370
S1P06380
S1P06390
S1P06400
S1P06410
S1P06420
S1P06430
S1P06440
S1P06450
S1P06460
S1P06470
S1P06480
S1P06490
S1P06500
S1P06510
S1P06520
S1P06530
S1P06540
S1P06550
S1P06560
S1P06570
S1P06580

YC16 = (1.+ZNU*SX*SX)/SX
 YC17 = 4.*YC13 + D2/SX
 YC18 = -(D1+YC8)*CX
 YC19 = -2.*D2*SX/DD
 XHH = XH*XH
 XHHH = XHH*XH
 XHHHH = XHHH*XH
 XKK = XK*XK
 XKKK = XKK*XK
 XKKKK = XKKK*XK
 A1 = YA1/XHH + YA3/(2.*XH)
 A2 = YA1/XHH - YA3/(2.*XH)
 A3 = YA2/XKK
 A4 = -(A1 +A2)-2.*A3 + YA4
 A5 = YA5/(4.*XH*XK)
 A6 = YA6/(2.*XK)
 A7 = YA7/(2.*XHHH)
 A10 = YA10/XKK
 A11 = YA8/(2.*XH*XKK)
 A13 = YA9/XHH
 A14 = YA11/(2.*XH)
 A8 = -2.*A7 -2.*A11 + A13 + A14
 A9 = +2.*A7 +2.*A11 + A13 - A14
 A12 = -2.*A13 -2.*A10
 B1 = YA5/(4.*XH*XK)
 B2 = -YA6/(2.*XK)
 B3 = YB3/XHH + YB5/(2.*XH)
 B4 = YB3/XHH - YB5/(2.*XH)
 B5 = YR4/XKK
 B6 = -B3-B4-2.*B5 + YB6
 B7 = -YB7/(2.*XH*XK) -YB8/XKKK + YB10/(2.*XK)
 B8 = YB7/(2.*XH*XK) + YB9/(4.*XH*XK)
 B9=YB7/(2.*XH*XK)-YB9/(4.*XH*XK)
 B10 = YR8/(2.*XKKK)
 C1 = SX/(2.*XHHH)
 C4 = YC4/XKK
 C5 = YC2/(2.*XH*XKK)
 C10= YC8/(2.*XKKK)
 C13 = YC13/XKKK

SIP06590
 SIP06600
 SIP06610
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C2 = -2.*C1-2.*C5+YC3/XHH+YC5/(2.*XH)
C3 = +2.*C1+2.*C5+YC3/XHH-YC5/(2.*XH)
C6 = -2.*YC3/XHH -2.*C4+YC6
C7=-D5/(XHH*XK)-2.*C10+YC10/(2.*XK)
C8 = D5/(2.*XHH*XK) + YC9/(4.*XHH*XK)
C9 = D5/(2.*XHH*XK) - YC9/(4.*XHH*XK)
C11 = -SX/XHHHH - YC3/(2.*XHHH)
C12 = -SX/XHHHH + YC3/(2.*XHHH)
C14 = 4.*SX/XHHHH -2.*YC12/ (XHH*XKK) + YC3/XHHH-YC15/(XH*XKK)
1 + YC16/(XHH) + YC18/(2.*XH)
C15 = 4.*SX/XHHHH-2.YC12/(XHH*XKK) - YC3/XHHH + YC15/(XH*XKK)
1 + YC16/XHH -YC18/(2.*XH)
C16 = -2.*YC12/(XHH*XKK) -4.*YC13/XKKK + YC17/XKK
C17 = YC12/(XHH*XKK) + YC15/(2.*XHH*XKK)
C18 = YC12/(XHH*XKK) -YC15/(2.*XHH*XKK)
C19 = -6.*SX/XHHHH + 4.*YC12/(XHH*XKK) +6.*YC13/XKKK
1 -2.*YC16/XHH -2.*YC17 /XKK + YC19
A=1.
C=1.
CALL NORM(A1,A,12)
CALL NORM(B1,R,10)
CALL NORM(C1,C,19)
DO 58 L =1, NCF
L1 = J*NCF+L
58 A(L1)=A(L)
60 CONTINUE
RETURN
END
*
FORTRAN
SURROUTINE CONS (X, I)
COMMON IOPT1, IOPT2, IOPT3, IOPT4, IOPT5, IOPT6, IOPT7, IOPT8
COMMON NCF
COMMON NDIM, NROW, NCOL, MM, MFLAG, XM,XLD
COMMON ISW1, ISW2, ISW3
COMMON A, A1, A2, A3, A4, A5, A6, A7, A8, A9, A10, A11, A12
COMMON B, B1, B2, B3, B4, B5, B6, B7, B8, B9, B10
COMMON C, C1, C2, C3, C4, C5, C6, C7, C8, C9, C10, C11, C12, C13, C14,
1 C15, C16, C17, C18, C19
COMMON FILL
SIP06980
SIP06990
SIP07000
SIP07010
SIP07020
SIP07030
SIP07040
SIP07050
SIP07060
SIP07070
SIP07080
SIP07090
SIP07100
SIP07110
SIP07120
SIP07130
SIP07140
SIP07150
SIP07160
SIP07170
SIP07180
SIP07190
SIP07200
SIP07210
SIP07220
SIP07230
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SIP07260
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SIP07290
SIP07300
SIP07310
SIP07320
SIP07330
SIP07340
SIP07350
SIP07360

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COMMON TMP, YK, YL
COMMON T1, T2, XX, XX1, Z, Z1, Z2
COMMON ZNU, THC, PH1, FF, RH, DD, XH, XK
COMMON ZETA
COMMON TE, TI, TO, OC, TC, TD, DDLD
DIMENSION TMP (5184), YK(5184), YL(5184)
DIMENSION ZETA (30)
DIMENSION T1( 89), T2(89), XX(89), XX1(89), Z(89), Z1(89), Z2(89)
DIMENSION MM(40)
DIMENSION X(72), A(1), B(1), C(1)
DIMENSION FILL(1188)
3 DO 5 J=1, NDIM
5 X(J)=0.
IF (IOPT4-1) 6, 21, 21
6 DO 10 J=1, NROW
11=INDX (I, J, 3)
J4 = J*NCF+1
10 X(I1) = C(J4) * (ZNU**2-1.) * SINF(ZETA(J+1)) / DD
GO TO 99
21 CONTINUE

DO 31 J = 1, NROW
J4 = J*NCF+1
11 = INDX(I,J,3)
X(I1) = C(J4) * SINF(ZETA(J+1)) * TC / DD
31 CONTINUE
99 RETURN
END
*
FORTRAN
FUNCTION DEF (I1, JJ, KK, MF)
COMMON IOPT1, IOPT2, IOPT3, IOPT4, IOPT5, ICPT6, ICPT7, ICPT8
COMMON NCF
COMMON NDIM, NROW, NCOL, MM, MFLAG, XM, XLD
COMMON ISW1, ISW2, ISW3
COMMON A
COMMON TMP, YK, YL
DIMENSION MM(40)
DIMENSION A(1232)
DIMENSION TMP (5184), YK(5184), YL(5184)
N2=2*(NROW+6)

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SIP07370
SIP07380
SIP07390
SIP07400
SIP07410
SIP07420
SIP07430
SIP07440
SIP07450
SIP07460
SIP07470
SIP07480
SIP07490
SIP07500
SIP07510
SIP07520
SIP07530
SIP07540
SIP07550
SIP07560
SIP07570
SIP07580
SIP07590
SIP07600
SIP07610
SIP07620
SIP07630
SIP07640
SIP07650
SIP07660
SIP07670
SIP07680
SIP07690
SIP07700
SIP07710
SIP07720
SIP07730
SIP07740
SIP07750

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I=II
J=JJ
K=KK
M=MF
IF (M) 60, 50, 70
60 IF (M+1) 61, 62, 62
61 J=J-1
M=0
GO TO 50
62 J2=J-1
GO TO 50
70 IF (M-1) 72, 72, 71
71 J=J+1
M=0
GO TO 50
72 J2=J+1
50 SIGN=1.
IF (I-1) 1, 3, 3
1 I=2-I
IF (K-2) 3, 2, 3
2 SIGN=-1.
GO TO 5
3 IF (J-1) 4, 5, 5
4 IF (I OPT 2) 6, 6, 5
5 J=2-J
IF (K-1) 2, 2, 5
5 I2=(I-1)*N2+3*J+K+6
IF (M) 16, 13, 16
13 IF (SIGN) 14, 15, 15
14 DEF=-TMP(I2)
GO TO 99
15 DEF=TMP(I2)
GO TO 99
16 I3=(I-1)*N2+3*J2+K+6
DEF=SIGN*(TMP(I2)+TMP(I3))/2.
99 RETURN
END
FORTRAN
SUBROUTINE EQ1 (X, I1, I1, JJ, MX)

```

*

| | | |
|---|---|----------|
| C | COMPUTE COEFFICIENTS FOR EQUATION ONE FOR MESH PT I,J | S1P08150 |
| | COMMON IOPT1, IOPT2, IOPT3, IOPT4, IOPT5, IOPT6, IOPT7, IOPT8 | S1P08160 |
| | COMMON NCF | S1P08170 |
| | COMMON NDIM, NROW, NCOL, MM, KO, KM1, KM2, KP1, KP2, MFLAG, XM, XLD | S1P08180 |
| | COMMON ISW1, ISW2, ISW3 | S1P08190 |
| | COMMON A, A1, A2, A3, A4, A5, A6, A7, A8, A9, A10, A11, A12 | S1P08200 |
| | DIMENSION MM(35) | S1P08210 |
| | I1=I11 | S1P08220 |
| | I=I1 | S1P08230 |
| | J=JJ | S1P08240 |
| | M=MX | S1P08250 |
| | GO TO (30, 20, 30, 40, 50), M | S1P08260 |
| | 20 CONTINUE | S1P08270 |
| | MF=0 | S1P08280 |
| | ISW2=0 | S1P08290 |
| | CALL CF (I-1, J, MF, 1, A3, X) | S1P08300 |
| | CALLCF(I-1, J, MF, 3, A10, X) | S1P08310 |
| | ISW2=-1 | S1P08320 |
| | CALL CF (I-1, J, MF, 2, A6, X) | S1P08330 |
| | MF=KM1 | S1P08340 |
| | CALL CF (I-1, J-1, MF, 2, A5, X) | S1P08350 |
| | ISW2=0 | S1P08360 |
| | CALLCF(I-1, J-1, MF, 3, A11, X) | S1P08370 |
| | MF=KP1 | S1P08380 |
| | CALL CF (I-1, J+1, MF, 2, A5, X) | S1P08390 |
| | ISW2 = -1 | S1P08400 |
| | CALLCF(I-1, J+1, MF, 3, A11, X) | S1P08410 |
| | GO TO 50 | S1P08420 |
| | 30 CONTINUE | S1P08430 |
| | ISW2=0 | S1P08440 |
| | MF=0 | S1P08450 |
| | CALL CF (I, J, MF, 1, A4, X) | S1P08460 |
| | CALLCF(I, J, MF, 3, A12, X) | S1P08470 |
| | MF=KM1 | S1P08480 |
| | CALL CF (I, J-1, MF, 1, A1, X) | S1P08490 |
| | CALLCF(I, J-1, MF, 3, A8, X) | S1P08500 |
| | MF=KP1 | S1P08510 |
| | CALL CF (I, J+1, MF, 1, A2, X) | S1P08520 |
| | CALLCF(I, J+1, MF, 3, A9, X) | S1P08530 |

```

MF = KM2
CALLCF(I , J-2,MF,3,A7 ,X)
MF = KP2
ISW2=-1
CALLCF(I , J+2,MF,3,A7 ,X)
IF (MFLAG) 50, 50, 40
40 CONTINUE
MF=0
ISW2=0
CALL CF (I+1, J, MF, I, A3, X)
CALL CF (I+1, J, MF,2, A6,X)
CALLCF(I+1,J ,MF,3,A10,X)
MF=KM1
CALL CF (I+1, J-1, MF, 2, A5,X)
CALLCF(I+1,J-1,MF,3,A11,X)
MF=KP1
ISW2=-1
CALL CF (I+1, J+1, MF, 2, A5,X)
CALLCF(I+1,J+1,MF,3,A11,X)
ISW2 = 0
45 IF (I-1) 20, 20, 46
46 IF (MFLAG) 50, 50, 20
50 RETURN
END
*
FORTRAN
SURROUTINE FQ2 (X, I1, I1, JJ, MX)
C COMPUTE EQUATION TWO FOR MESH PT I, J.
COMMON IOPT1, IOPT2, IOPT3, IOPT4, IOPT5, IOPT6, IOPT7, IOPT8
COMMON NCF
COMMON NDIM, NROW,NCOL,MM,K0,KM1,KM2,KP1,KP2,MFLAG,XM,XLD
COMMON ISW1, ISW2, ISW3
COMMON A, A1, A2, A3, A4, A5, A6, A7, A8, A9, A10, A11, A12
COMMON R, R1, R2, R3, B4, B5, B6, B7, B8, B9, B10
DIMENSION MM(35)
I1=I11
I=I1
J=JJ
M=MX
GO TO (30, 20, 30, 40, 50), M

```

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S1P08540
S1P08550
S1P08560
S1P08570
S1P08580
S1P08590
S1P08600
S1P08610
S1P08620
S1P08630
S1P08640
S1P08650
S1P08660
S1P08670
S1P08680
S1P08690
S1P08700
S1P08710
S1P08720
S1P08730
S1P08740
S1P08750
S1P08760
S1P08770
S1P08780
S1P08790
S1P08800
S1P08810
S1P08820
S1P08830
S1P08840
S1P08850
S1P08860
S1P08870
S1P08880
S1P08890
S1P08900
S1P08910
S1P08920

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| | | |
|----|-----------------------------------|----------|
| 20 | CONTINUE | S1P08930 |
| | ISW2=0 | S1P08940 |
| | MF=0 | S1P08950 |
| | CALL CF (I-1, J, MF, 2, B5, X) | S1P08960 |
| | ISW2=-1 | S1P08970 |
| | CALL CF (I-1, J, MF, 1, B2, X) | S1P08980 |
| | CALL CF (I-1, J, MF, 3, B7, X) | S1P08990 |
| | MF=KM1 | S1P09000 |
| | CALL CF (I-1, J-1, MF, 1, B1, X) | S1P09010 |
| | CALL CF (I-1, J-1, MF, 3, B8, X) | S1P09020 |
| | MF=KP1 | S1P09030 |
| | CALL CF (I-1, J+1, MF, 3, B9, X) | S1P09040 |
| | ISW2=0 | S1P09050 |
| | CALL CF (I-1, J+1, MF, 1, B1, X) | S1P09060 |
| | GO TO 50 | S1P09070 |
| 30 | CONTINUE | S1P09080 |
| | ISW2=0 | S1P09090 |
| | MF=KM1 | S1P09100 |
| | CALL CF (I, J-1, MF, 2, B3, X) | S1P09110 |
| | MF=KP1 | S1P09120 |
| | CALL CF (I, J+1, MF, 2, R4, X) | S1P09130 |
| | MF=0 | S1P09140 |
| | CALL CF (I, J, MF, 2, B6, X) | S1P09150 |
| | 33 IF (MFLAG) 34, 34, 35 | S1P09160 |
| | 34 IF (I-2) 50, 35, 36 | S1P09170 |
| | 35 CONTINUE | S1P09180 |
| | ISW2=-1 | S1P09190 |
| | CALL CF (I-2, J, MF, 3, B10, X) | S1P09200 |
| | IF (MFLAG) 50, 50, 37 | S1P09210 |
| | 36 IF (I-NCOL) 50, 37, 37 | S1P09220 |
| | 37 CONTINUE | S1P09230 |
| | ISW2=0 | S1P09240 |
| | CALL CF (I+2, J, MF, 3, B10, X) | S1P09250 |
| | IF (MFLAG) 50, 50, 40 | S1P09260 |
| 40 | CONTINUE | S1P09270 |
| | ISW2=0 | S1P09280 |
| | MF=0 | S1P09290 |
| | CALL CF (I+1, J, MF, 1, B2, X) | S1P09300 |
| | CALL CF (I+1, J, MF, 2, B5, X) | S1P09310 |


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CALL CF ( I+1, J, MF, 3, B7, X)
MF=KMI
CALL CF ( I+1, J-1, MF, 1, B1, X)
CALL CF ( I+1, J-1, MF, 3, B8, X)
MF=KPI
CALL CF ( I+1, J+1, MF, 3, B9, X)
ISW2=-1
CALL CF ( I+1, J+1, MF, 1, B1, X)
45 IF (I-1) 20, 20, 46
46 IF (MFLAG) 50, 50, 20
50 RETURN
END
*
FORTRAN
SUBROUTINE EQ3 (X, I1, I1, II, JJ, MX)
COMPUTE EQUATION THREE FOR MESH PT I,J.
COMMON IOPT1, IOPT2, IOPT3, IOPT4, IOPT5, IOPT6, IOPT7, IOPT8
COMMON NCF
COMMON NDIM, NROW, NCOL, MM, K0, KM1, KM2, KP1, KP2, MFLAG, XM, XLD
COMMON ISW1, ISW2, ISW3
COMMON A, A1, A2, A3, A4, A5, A6, A7, A8, A9, A10, A11, A12
COMMON R, R1, R2, R3, R4, R5, R6, R7, R8, R9, R10
COMMON C, C1, C2, C3, C4, C5, C6, C7, C8, C9, C10, C11, C12, C13, C14,
1 C15, C16, C17, C18, C19
DIMENSION MM(35)
I1=I11
I=II
J=JJ
M=MX
GO TO (30, 20, 30, 40, 50), M
20 CONTINUE
ISW2=0
MF=0
CALL CF(I-1, J, MF, 1, C4, X)
CALL CF(I-1, J, MF, 3, C16, X)
ISW2=-1
CALL CF(I-1, J, MF, 2, C7, X)
MF=KPI
CALL CF(I-1, J+1, MF, 1, C5, X)
CALL CF(I-1, J+1, MF, 2, C9, X)

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S1P09320
S1P09330
S1P09340
S1P09350
S1P09360
S1P09370
S1P09380
S1P09390
S1P09400
S1P09410
S1P09420
S1P09430
S1P09440
S1P09450
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S1P09590
S1P09600
S1P09610
S1P09620
S1P09630
S1P09640
S1P09650
S1P09660
S1P09670
S1P09680
S1P09690
S1P09700

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| | |
|-----------------------------------|----------|
| ISW2=0 | S1P09710 |
| CALL CF(I-1,J+1,MF,3,C18,X) | S1P09720 |
| MF=KM1 | S1P09730 |
| CALL CF(I-1,J-1,MF,1,C5,X) | S1P09740 |
| CALL CF(I-1,J-1,MF,3,C17,X) | S1P09750 |
| ISW2 = -1 | S1P09760 |
| CALL CF(I-1,J-1,MF,2,C8,X) | S1P09770 |
| IF (I-1) 21, 21, 22 | S1P09780 |
| 21 ISW2=1 | S1P09790 |
| CX=CFZ(J, C10) | S1P09800 |
| CALL CF (I-1, J, 0,2, -4.*CX, X) | S1P09810 |
| GO TO 50 | S1P09820 |
| 22 IF (I-NCOL) 50, 24, 24 | S1P09830 |
| 24 ISW2=1 | S1P09840 |
| CX=CFZ(J, C10) | S1P09850 |
| CALL CF (I-1, J, 0, 2, 4.*CX, X) | S1P09860 |
| GO TO 50 | S1P09870 |
| 30 CONTINUE | S1P09880 |
| ISW2=0 | S1P09890 |
| MF=KM1 | S1P09900 |
| CALL CF(I, J-1,MF,1,C2,X) | S1P09910 |
| CALL CF(I, J-1,MF,3,C14,X) | S1P09920 |
| MF=KP1 | S1P09930 |
| CALL CF(I, J+1,MF,1,C3,X) | S1P09940 |
| CALL CF(I, J+1,MF,3,C15,X) | S1P09950 |
| MF=KM2 | S1P09960 |
| CALL CF(I, J-2,MF,3,C11,X) | S1P09970 |
| ISW2=0 | S1P09980 |
| MF=KP2 | S1P09990 |
| CALL CF(I, J+2,MF,3,C12,X) | S1P10000 |
| MF=0 | S1P10010 |
| CALL CF(I, J, MF,1,C6,X) | S1P10020 |
| CALL CF(I, J, MF,3,C19,X) | S1P10030 |
| IF (J-NROW) 32, 31, 31 | S1P10040 |
| 31 ISW2=1 | S1P10050 |
| CX=CFZ(J,C1) | S1P10060 |
| CALL CF(I, J+1, KP1, 1, -4.*CX,X) | S1P10070 |
| CALL CF (I, J, 0, 1, 6.*CX, X) | S1P10080 |
| CALL CF(I, J-1, KM1, 1, -4.*CX,X) | S1P10090 |

| | |
|--|----------|
| CALL CF (I, J-2, KM2, 1, 2.*CX, X) | SIP10100 |
| GO TO 36 | SIP10110 |
| 32 IF (J-1) 33, 33, 34 | SIP10120 |
| 33 ISW2=1 | SIP10130 |
| CX=CFZ(J,C1) | SIP10140 |
| CALL CF(I, J-1, KM1, 1, 4.*CX, X) | SIP10150 |
| CALL CF(I, J, 0, 1, -6.*CX, X) | SIP10160 |
| CALL CF(I, J+1, KP1, 1, 4.*CX, X) | SIP10170 |
| CALL CF(I, J+2, KP2, 1, -2.*CX, X) | SIP10180 |
| GO TO 36 | SIP10190 |
| 34 CONTINUE | SIP10200 |
| CALL CF (I, J-2, KM2, 1, C1, X) | SIP10210 |
| ISW2=-1 | SIP10220 |
| CALL CF (I, J+2, KP2, 1,C1, X) | SIP10230 |
| 36 IF (I-2) 360, 361, 362 | SIP10240 |
| 360 MP=MFLAG+1 | SIP10250 |
| GO TO 365 | SIP10260 |
| 361 MP=MFLAG+3 | SIP10270 |
| GO TO 365 | SIP10280 |
| 362 IF (I-NCOL) 363, 364, 364 | SIP10290 |
| 363 MP=MFLAG+5 | SIP10300 |
| GO TO 365 | SIP10310 |
| 364 MP=MFLAG+7 | SIP10320 |
| 365 GO TO (370, 366, 367, 366, 370, 366, 366, 366), MP | SIP10330 |
| 366 CONTINUE | SIP10340 |
| MF=0 | SIP10350 |
| ISW2 = 0 | SIP10360 |
| CALL CF(I+2,J ,MF,3,C13,X) | SIP10370 |
| IF (MFLAG) 370, 370, 367 | SIP10380 |
| 367 CONTINUE | SIP10390 |
| ISW2 = 0 | SIP10400 |
| CALL CF(I-2,J ,MF,3,C13,X) | SIP10410 |
| 370 GO TO (373, 372, 376, 375, 395, 375, 382, 380), MP | SIP10420 |
| 372 CONTINUE | SIP10430 |
| ISW2=1 | SIP10440 |
| CX=2.*CFZ(J, C10) | SIP10450 |
| CALL CF(I+2, J, 0, 2, CX, X) | SIP10460 |
| 373 CONTINUE | SIP10470 |
| ISW2=1 | SIP10480 |

| | |
|----------------------------------|----------|
| CX=CFZ(J, C10) | S1P10490 |
| CALL CF (I, J, 0, 2, 6.*CX, X) | S1P10500 |
| GO TO 395 | S1P10510 |
| 375 CONTINUE | S1P10520 |
| ISW2=0 | S1P10530 |
| CALL CF (I+2, J, 0, 2, C10, X) | S1P10540 |
| 376 CONTINUE | S1P10550 |
| ISW2=-1 | S1P10560 |
| CALL CF (I-2, J, 0, 2, C10, X) | S1P10570 |
| GO TO 395 | S1P10580 |
| 380 CONTINUE | S1P10590 |
| ISW2=1 | S1P10600 |
| CX=-2.*CFZ(J, C10) | S1P10610 |
| CALL CF (I-2, J, 0, 2, CX, X) | S1P10620 |
| 382 CONTINUE | S1P10630 |
| 390 ISW2=1 | S1P10640 |
| CX=CFZ(J, C10) | S1P10650 |
| CALL CF (I, J, 0, 2, -6.*CX, X) | S1P10660 |
| 395 CONTINUE | S1P10670 |
| IF (MFLAG) 50, 50, 40 | S1P10680 |
| 40 CONTINUE | S1P10690 |
| MF=0 | S1P10700 |
| ISW2=0 | S1P10710 |
| CALL CF(I+1, J, MF, 3, C16, X) | S1P10720 |
| CALL CF(I+1, J, -, MF, 2, C7, X) | S1P10730 |
| CALL CF(I+1, J, MF, 1, C4, X) | S1P10740 |
| MF=KM1 | S1P10750 |
| CALL CF(I+1, J-1, MF, 2, C8, X) | S1P10760 |
| CALL CF(I+1, J-1, MF, 1, C5, X) | S1P10770 |
| CALL CF(I+1, J-1, MF, 3, C17, X) | S1P10780 |
| MF=KPI | S1P10790 |
| ISW2 = -1 | S1P10800 |
| CALL CF(I+1, J+1, MF, 1, C5, X) | S1P10810 |
| ISW2 = 0 | S1P10820 |
| CALL CF(I+1, J+1, MF, 2, C9, X) | S1P10830 |
| CALL CF(I+1, J+1, MF, 3, C18, X) | S1P10840 |
| IF (I-NCOL) 42, 41, 41 | S1P10850 |
| 41 ISW2=1 | S1P10860 |
| CX=-4.*CFZ(J, C10) | S1P10870 |

```

GO TO 44
42 IF (I-1) 43,43, 45
43 ISW2=1
CX=4.*CFZ( J, C10)
44 CALL CF (I+1,J, 0, 2, CX, X)
45 IF (I-1) 20, 20, 46
46 IF (MFLAG) 50, 50, 20
50 RETURN
END
*
FORTRAN
SUBROUTINE EXTRA (X, X1, X2, X3, X4)
X=4.*X1-6.*X2+4.*X3-X4
RETURN
END
*
FORTRAN
SUBROUTINE GRADE (J)
COMMON IOPT1, IOPT2, IOPT3, IOPT4, IOPT5, IOPT6, IOPT7, IOPT8
COMMON NCF
COMMON NDIM, NROW,NCOL,MM,K0,KM1,KM2,KP1,KP2,MFLAG,XM,XLD
DIMENSION MM(35)
DO 2 I=37, 40
2 MM(I)=0
IF (J) 99, 99, 1
1 JM=MM(J)
JM1=MM(J-1)
JM2= MM(J-2)
JP1= MM(J+1)
JP2= MM(J+2)
IF (J-2) 10, 10, 4
4 IF (J-NROW+1) 5, 30, 30
5 IF (JP2-JM2) 10, 20, 30
C MESH SPACING INCREASING
10 IF (JP1-JM) 11, 12, 12
C DOUBLE MESH SPACING AFTER THIS ROW
11 KP1=-1
KP2=-2
IF (J-1) 40, 40, 99
12 IF (JP2-JP1) 14, 18, 18
14 KP2=-1

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S1P10880
S1P10890
S1P10900
S1P10910
S1P10920
S1P10930
S1P10940
S1P10950
S1P10960
S1P10970
S1P10980
S1P10990
S1P11000
S1P11010
S1P11020
S1P11030
S1P11040
S1P11050
S1P11060
S1P11070
S1P11080
S1P11090
S1P11100
S1P11110
S1P11120
S1P11130
S1P11140
S1P11150
S1P11160
S1P11170
S1P11180
S1P11190
S1P11200
S1P11210
S1P11220
S1P11230
S1P11240
S1P11250
S1P11260

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| | | |
|---|---|----------|
| | IF (J-2) 40, 15, 15 | S1P11270 |
| | 15 IF (JM-JM1) 16, 99, 99 | S1P11280 |
| C | MESH SPACING CHANGES IN BOTH DIRECTIONS | S1P11290 |
| | 16 KM2=-2 | S1P11300 |
| | GO TO 40 | S1P11310 |
| | 18 IF (J-2) 40, 20, 13 | S1P11320 |
| | 13 IF (JM-JM1) 19, 20, 20 | S1P11330 |
| C | DOUBLE THE MESH SPACING | S1P11340 |
| | 19 KM2=-2 | S1P11350 |
| | GO TO 40 | S1P11360 |
| | 20 GO TO 99 | S1P11370 |
| C | MESH SPACING IS DECREASING | S1P11380 |
| | 30 IF (JM-JM1) 32, 32, 31 | S1P11390 |
| C | CUT MESH SPACING IN HALF | S1P11400 |
| | 31 KM1=1 | S1P11410 |
| | KM2=2 | S1P11420 |
| | GO TO 40 | S1P11430 |
| | 32 IF (JM1-JM2) 37, 37, 33 | S1P11440 |
| | 33 IF (J-NROW+1) 35, 34, 34 | S1P11450 |
| C | MESH SPACING AT LAST ROW WAS CUT IN HALF | S1P11460 |
| | 34 KM2=1 | S1P11470 |
| | GO TO 99 | S1P11480 |
| | 35 IF (JP1-JM) 34, 34, 36 | S1P11490 |
| C | SPACING CHANGES IN BOTH DIRECTIONS | S1P11500 |
| | 36 KM2=1 | S1P11510 |
| | KP2=2 | S1P11520 |
| | GO TO 99 | S1P11530 |
| | 37 IF (J-NROW+1) 38, 20, 20 | S1P11540 |
| | 38 IF (JP1-JM) 20, 20, 39 | S1P11550 |
| C | MESH CUT IN HALF AFTER NEXT ROW | S1P11560 |
| | 39 KP2=2 | S1P11570 |
| | GO TO 99 | S1P11580 |
| | 40 CONTINUE | S1P11590 |
| | 99 RETURN | S1P11600 |
| | END | S1P11610 |
| * | FORTRAN | S1P11620 |
| | FUNCTION INDX(11, JJ, KK) | S1P11630 |
| | COMMON IOPT1, IOPT2, IOPT3, IOPT4, IOPT5, IOPT6, IOPT7, IOPT8 | S1P11640 |
| | COMMON NCF | S1P11650 |

COMMON NDIM, NROW, NCOL, MM, MFLAG, XM, XLD
 DIMENSION MM(40)
 I=I

S1P11660
 S1P11670
 S1P11680

J=JJ
 K=KK
 IF (MFLAG) 100, 100, 200

S1P11690
 S1P11700
 S1P11710

100 CONTINUE
 IF (IOPT2) 10, 10, 20

S1P11720
 S1P11730

10 IF (I-1) 1, 1, 5
 1 IF (K-1) 2, 2, 3
 2. INDX= (J-1)*2
 GO TO 50

S1P11740
 S1P11750
 S1P11760
 S1P11770

3 INDX= J*2-1
 GO TO 50
 5 INDX= 3*J+K-4

S1P11780
 S1P11790
 S1P11800

GO TO 50
 20 IF (I-1) 21, 21, 29
 21 IF (K-1) 22, 22, 24
 22 INDX=J*2-1
 GO TO 50
 24 INDX=J*2

S1P11810
 S1P11820
 S1P11830

GO TO 50
 29 INDX=3*J+K-3
 GO TO 50

S1P11840
 S1P11850
 S1P11860

GO TO 50
 GO TO 50
 200 IF (I-NCOL) 201, 201, 220
 201 IF (J-NROW) 202, 202, 210
 202 IF (J) 230, 230, 205

S1P11870
 S1P11880

205 INDX= (I-1)*(NROW+6)*3+3*J+K+6
 GO TO 50
 210 IF (IOPT2) 211, 211, 216
 211 INDX=3*(NROW+NCOL-I) +2+K
 212 IF (I-1) 214, 214, 50
 214 IF (K-3) 50, 215, 215

S1P11890
 S1P11900
 S1P11910
 S1P11920

215 INDX=INDX-1
 GO TO 50
 216 INDX=3*(NROW+NCOL+NCOL-I)+K+5
 GO TO 212
 220 INDX=3*J+K-4
 IF (IOPT2) 50, 50, 221

S1P11930
 S1P11940
 S1P11950

215 INDX=INDX-1
 GO TO 50
 216 INDX=3*(NROW+NCOL+NCOL-I)+K+5
 GO TO 212
 220 INDX=3*J+K-4
 IF (IOPT2) 50, 50, 221

S1P11960
 S1P11970
 S1P11980
 S1P11990

215 INDX=INDX-1
 GO TO 50
 216 INDX=3*(NROW+NCOL+NCOL-I)+K+5
 GO TO 212
 220 INDX=3*J+K-4
 IF (IOPT2) 50, 50, 221

S1P12000
 S1P12010
 S1P12020
 S1P12030
 S1P12040

```

221 INDX=INDX+3*NCOL+3
GO TO 50
230 INDX=3*I+K-4
IF (I-1) 231, 231, 50
231 IF (K-1) 232, 232, 50
232 INDX=INDX+1
50 RETURN
END
*
FORTRAN
SUBROUTINE MTX (X, I, M)
COMMON IOPT1, IOPT2, IOPT3, IOPT4, IOPT5, IOPT6, IOPT7, IOPT8
COMMON NCF
COMMON NDIM, NROW, NCOL, MM, I1, KM1, KM2, KP1, KP2, MFLAG, XM, XLD
COMMON ISW1, ISW2, ISW3
DIMENSION MM(35)
DIMENSION X(72, 72)
I1=0
DO 1 JI=1, NDIM
DO 1 JJ=1, NDIM
1 X(IJ, JJ)=0.
DO 100 J=1, NROW
ISW1=J
IF (XM) 50, 50, 7
7 CALL GRADE (J)
50 IF (J-1) 57, 57, 58
57 IF (IOPT2) 59, 59, 58
58 I1=I1+1
CALL EQ1 (X, I1, I, J, M)
59 IF (I-1) 61, 61, 60
60 I1=I1+1
CALL EQ2 (X, I1, I, J, M)
61 I1=I1+1
CALL EQ3 ( X, I1, I, J, M)
100 CONTINUE
RETURN
END
*
*
FORTRAN
LIST

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S1P12050
S1P12060
S1P12070
S1P12080
S1P12090
S1P12100
S1P12110
S1P12120
S1P12130
S1P12140
S1P12150
S1P12160
S1P12170
S1P12180
S1P12190
S1P12200
S1P12210
S1P12220
S1P12230
S1P12240
S1P12250
S1P12260
S1P12270
S1P12280
S1P12290
S1P12300
S1P12310
S1P12320
S1P12330
S1P12340
S1P12350
S1P12360
S1P12370
S1P12380
S1P12390
S1P12400
S1P12410
S1P12420

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SURROUTINE MTXS (X, Y, II, M)
COMMON IOPT1, IOPT2, IOPT3, IOPT4, IOPT5, IOPT6, IOPT7, IOPT8
COMMON NICE
COMMON NDIM, NROW, NCOL, MM, MFLAG, XM, XLD
COMMON ISW1, ISW2, ISW3
COMMON A, A1, A2, A3, A4, A5, A6, A7, A8, A9, A10, A11, A12
COMMON B, B1, B2, B3, B4, B5, B6, B7, B8, B9, B10
COMMON C, C1, C2, C3, C4, C5, C6, C7, C8, C9, C10, C11, C12, C13, C14,
1 C15, C16, C17, C18, C19
COMMON FILL
DIMENSION FILL(1188)
DIMENSION MM(40)
C MULTIPLICATION BY A SINGLE DIAGONAL
DIMENSION X(72, 72), Y(72, 72)
I=1
3 IF (M-1) 20, 100, 100
C CLEAR OUT Y
20 DO 23 J=1, NDIM
23 Y(J,1)=0.
L1=1
50 TO 2
100 L1=NDIM
IF (M-1) 2,2,50
C FORM A*X AND STORE IN Y
2 DO 5 J=1,NROW
6 CONTINUE
7 I1=INDEX (I, J, 2)
I2=I1+1
J1=INDEX (I-2, J, 3)
J2=J1-1
IF (I-3) 31, 31, 32
31 CC=0.
50 TO 33
32 IF(I-NCOL) 322,321, 321
321 CC= -2.*CFZ(J, C10)
50 TO 32
322 CC=-CFZ(J, C10)
33 BB=CFZ(J, B10)
CC2= CFZ (J, C13)
DO 4 K=1, L1

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S1P12430
S1P12440
S1P12450
S1P12460
S1P12470.
S1P12480
S1P12490
S1P12500
S1P12510
S1P12520
S1P12530
S1P12540
S1P12550
S1P12560
S1P12570
S1P12580
S1P12590
S1P12600
S1P12610
S1P12620
S1P12630
S1P12640
S1P12650
S1P12660
S1P12670
S1P12680
S1P12690
S1P17700
S1P12710
S1P12720
S1P12730
S1P12740
S1P12750
S1P12760
S1P12770
S1P12780
S1P12790
S1P12800
S1P12810
S1P12820

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```

Y(I1, K)=Y(I1, K)-X( J1, K)*BB
4 Y(I2, K)=Y(I2, K)+X (J2, K)*CC+X (J1, K)*CC2
5 CONTINUE
GO TO 99
C FORM X*E AND STORE IN Y
50 CONTINUE
DO 60 J=1, NROW
51 CONTINUE
52 IF (I-1) 49, 40, 48
49 CC=2.*CFZ(J, C13)
CC2=-2.*CFZ(J, C10)
BR=0.
GO TO 57
48 CC= CFZ (J, C13)
CC2=-CFZ(J, C10)
BR= CFZ (J, B10)
57 I2= INDX (I, J, 3)
I1=I2-1
J1= INDX(I+2, J, 2)
J2=J1+1
53 DO 54 K=1, L1
54 Y(K, J1)=Y(K, J1)-X(K, I2)*CC2
55 DO 58 K=1, L1
58 Y(K, J2)= Y(K, J2)+X(K, I1)*BR+X(K, I2)*CC
60 CONTINUE
99 RETURN
END
* FORTRAN
SUBROUTINE NORM (X, CONS, K)
DIMENSION X(19), Y(19)
DO 1 I=1,K
1 Y(I)=ABSF(X(I))
DO 10 I=2,K
IF (Y(1)-Y(I)) 2,10,10
2 TFMP=Y(1)
Y(I)=Y(I)
Y(I)=TEMP
10 CONTINUE
DO 20 I=1,K

```

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S1P12830
S1P12840
S1P12850
S1P12860
S1P12870
S1P12880
S1P12890
S1P12900
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S1P12930
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S1P12960
S1P12970
S1P12980
S1P12990
S1P13000
S1P13010
S1P13020
S1P13030
S1P13040
S1P13050
S1P13060
S1P13070
S1P13080
S1P13090
S1P13100
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S1P13120
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S1P13140
S1P13150
S1P13160
S1P13170
S1P13180
S1P13190
S1P13200
S1P13210

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20 X(I)=X(I)/Y
CONS=CONS/Y
RETURN
END
* FORTRAN
SUBROUTINE INVERT(A,IMAX,ISING)
SUBROUTINE TO INVERT A MATRIX
C DIMENSION A(72, 72), IN(72), TEMP(72)
ISING=0
N=IMAX
IMAXO=N-1
I1=1
1 I3=I1
IN(I1)=0
SUM=ABSF(A(I1,I1))
DO3I=I1,N
IF(SUM-ABSF(A(I,I1)))2,3,3
2 I3=I
IN(I1)=I
SUM=ABSF(A(I,I1))
3 CONTINUE
4 DO5J=1,N
SUM=A(I1,J)
A(I1,J)=A(I3,J)
5 A(I3,J)=SUM
6 I3=I1+1
IF(A(I1,I1))97,99,97
97 DO7I=I3,N
7 A(I,I1)=A(I,I1)/A(I1,I1)
J2=I1-1
IF(J2)8,11,8
8 DO9J=I3,N
9 A(I1,J)=A(I1,J)-DPSUM(A,I1,J,1,J2)
11 J2=I1
I1=I1+1
DO12I=I1,N
12 A(I,I1)=A(I,I1)-DPSUM(A,I,I1,1,J2)
IF(I1-N)1,14,1

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S1P13220
S1P13230
S1P13240
S1P13250
S1P13260
S1P13270
S1P13280
S1P13290
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S1P13610
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 S1P13940
 S1P13950
 S1P13960
 S1P13970
 S1P13980
 S1P13990

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14 D0600JP=1,N
   J=N+1-JP
   A(J,J)=1.0/A(J,J)
   IF(J-1)603,700,603
603 D0600IP=2,J
   I=J+1-IP
   IPO=I+1
   SUM=-DPSUM(A,I,J,IPO,J)
600 A(I,J)=SUM/A(I,I)
700 D0151J=1,IMAX0
   JPO=J+1
   D0151I=JPO,N
   IMO=I-1
   SUM=-DPSUM(A,I,J,J+1,IMO)
   SUM=SUM-A(I,J)
151 A(I,J)=SUM
   D0901I=1,N
   D0900J=1,N
   IF(I-J)897,897,898
897 TEMP(J)=DPSUM(A,I,J,J+1,N)
   TEMP(J)=TEMP(J)+A(I,J)
   GO TO 900
898 TEMP(J)=DPSUM(A,I,J,I,N)
900 CONTINUE
   D0901J=1,N
901 A(I,J)=TEMP(J)
   D0500I=2,N
   M=N+1-I
   IF(IN(M))502,500,502
502 ISS=IN(M)
   D0503L=1,N
   SUM=A(L,ISS)
   A(L,ISS)=A(L,M)
503 A(L,M)=SUM
500 CONTINUE
   GO TO 805
99 ISING=1
805 RETURN
   END
  
```

```

*      FORTRAN
SUBROUTINE STORE (X, II)
COMMON IOPT1, IOPT2, IOPT3, IOPT4, IOPT5, IOPT6, IOPT7, IOPT8
COMMON NCF
COMMON NDIM, NROW, NCOL, MM, MFLAG, XM, XLD
COMMON ISW1, ISW2, ISW3
COMMON A
COMMON TMP, YK, YL
DIMENSION TMP (5184), YK(5184), YL(5184)
DIMENSION A(1232)
DIMENSION X(59)
DIMENSION MM(40)
N2= (NROW+6)*3
NC1=NCOL+1
IF (MFLAG) 100, 100, 200
100 N1=(II-1)*N2+10
    I2=0
    DO 110 J=1, NROW
    IF (J-1) 101, 101, 103
101 IF (IOPT2) 104, 104, 103
103 I2=I2+1
    TMP(N1)=X(I2)
104 IF (II-1) 107, 107, 106
106 I2=I2+1
    TMP (N1+1)=X(I2)
107 I2=I2+1
    TMP (N1+2)=X(I2)
110 N1=N1+3
    GO TO 999
200 IF (IOPT2) 220, 220, 201
201 I2=11*270
    DO 210 I=1, NCOL
    N1= (I-1)*N2+1
    I2=I2+1
    TMP(N1+3)=YK(I2)
    IF (I-1) 208, 208, 204
204 I2=I2+1
    TMP(N1+4)=YK(I2)
208 I2=I2+1

```

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S1P14000
S1P14010
S1P14020
S1P14030
S1P14040
S1P14050
S1P14060
S1P14070
S1P14080
S1P14090
S1P14100
S1P14110
S1P14120
S1P14130
S1P14140
S1P14150
S1P14160
S1P14170
S1P14180
S1P14190
S1P14200
S1P14210
S1P14220
S1P14230
S1P14240
S1P14250
S1P14260
S1P14270
S1P14280
S1P14290
S1P14300
S1P14310
S1P14320
S1P14330
S1P14340
S1P14350
S1P14360
S1P14370
S1P14380

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```

TMP(N1+2)=YK(I2)
TMP(N1+5)=TMP(N1+11)
210 CONTINUE
N1=NC1*N2+4
TMP(N1)=YK(I2+1)
TMP(N1+1)=YK(I2+2)
TMP(N1+2)=YK(I2+3)
TMP(N1+6)=YK(I2+4)
I2=I2+4
GO TO 222
220 I2=I1*270
222 NO=NC1*N2+10
N1=N0+N2
NN=N0-N2-N2
TMP(N0+1)=YK(I2+1)
TMP(N1+2)=YK(I2+2)
I2=I2+2
TMP(N0+2)=TMP(NN+2)
230 DO 240 J=2, NROW
NO=N0+3
N1=N1+3
NN=NN+3
TMP(N0)=YK(I2+1)
TMP(N0+1)=YK(I2+2)
TMP(N0+2)=TMP(NN+2)
TMP(N1+2)=YK(I2+3)
240 I2=I2+3
NO=N0+6
TMP(N0)=YK(I2+1)
TMP(N0+1)=YK(I2+2)
TMP(N0+2)=YK(I2+3)
I2=I2+3
DO 250 I=1, NCOL
I1=NCOL+1-I
N1=I1*N2-5
I2=I2+1
TMP(N1)=YK(I2)
TMP(N1+2)=TMP(N1-4)
IF (I1-1) 252, 252, 251

```

```

S1P14390
S1P14400
S1P14410
S1P14420
S1P14430
S1P14440
S1P14450
S1P14460
S1P14470
S1P14480
S1P14490
S1P14500
S1P14510
S1P14520
S1P14530
S1P14540
S1P14550
S1P14560
S1P14570
S1P14580
S1P14590
S1P14600
S1P14610
S1P14620
S1P14630
S1P14640
S1P14650
S1P14660
S1P14670
S1P14680
S1P14690
S1P14700
S1P14710
S1P14720
S1P14730
S1P14740
S1P14750
S1P14760
S1P14770

```

```

251 I2=I2+1
    TMP(N1+1)=YK(I2)
252 I2=I2+1
    TMP(N1+5)=YK(I2)
250 CONTINUE
999 RETURN
END
*
FORTRAN
SUBROUTINE STRESS (I1,JJ,KK)
COMMON IOPT1, IOPT2, IOPT3, IOPT4, IOPT5, IOPT6, IOPT7, IOPT8
COMMON NCF
COMMON NDIM, NROW, NCOL, MM, I1, KM1, KM2, KP1, KP2, MFLAG, XM, XLD
COMMON ISW1, ISW2, ISW3
COMMON A
COMMON TMP, YK, YL
COMMON T1, T2, XX, XXI, Z, Z1, Z2
COMMON ZNU, THC, PHI, FF, RH, DO, XXH, XK
COMMON ZETA
COMMON TE, TI, TO, OC, TC, TD, DDL
DIMENSION A(1232)
DIMENSION MM(35)
DIMENSION T1( 89), T2(89), XX(89), XXI(89), Z(89), Z1(69), Z2(89)
DIMENSION TMP(5184), YK(4, 1296), YL(4,4,324)
DIMENSION ZETA (30)
101 FORMAT (I3, I4, I3, I3, 1P9E12.4)
    K = KK
    J=JJ
    NCI=NCOL+1
    NRI=NROW+1
    IF (XM) 1, 1, 5
1 XH=XXH
    GO TO 10
5 J1=XMAXOF (J, 1)
  J1=MM(J1)
  XH= XH/2.**J1
10 I=I1
    U = DEF (I, J, 1, 0)
    V = DEF (I, J, 2, 0)
    W = DEF (I, J, 3, 0)

```

```

S1P14780
S1P14790
S1P14800
S1P14810
S1P14820
S1P14830
S1P14840
S1P14850
S1P14860
S1P14870
S1P14880
S1P14890
S1P14900
S1P14910
S1P14920
S1P14930
S1P14940
S1P14950
S1P14960
S1P14970
S1P14980
S1P14990
S1P15000
S1P15010
S1P15020
S1P15030
S1P15040
S1P15050
S1P15060
S1P15070
S1P15080
S1P15090
S1P15100
S1P15110
S1P15120
S1P15130
S1P15140
S1P15150
S1P15160

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```

UX=(DEF(I,J-1,1,KM1)-DEF(I,J+1,1,KP1))/(2.*XH)
UT=(DEF(I+1,J,1,0)-DEF(I-1,J,1,0))/(2.*XK)
VX=(DEF(I,J-1,2,KM1)-DEF(I,J+1,2,KP1))/(2.*XH)
VT=(DEF(I+1,J,2,0)-DEF(I-1,J,2,0))/(2.*XK)
WX=(DEF(I,J-1,3,KM1)-DEF(I,J+1,3,KP1))/(2.*XH)
WT=(DEF(I+1,J,3,0)-DEF(I-1,J,3,0))/(2.*XK)
VXX=(DEF(I,J-1,2,KM1)-2.*DEF(I,J,2,0)+DEF(I,J+1,2,KP1))/(
1 XH*XH)
VXT=(DEF(I+1,J-1,2,KM1)-DEF(I+1,J+1,2,KP1)-DEF(I-1,J-1,2,KM1)
1 )+DEF(I-1,J+1,2,KP1))/(4.*XH*XK)
VTX=VXT
VIT=(DEF(I+1,J,2,0)-2.*DEF(I,J,2,0)+DEF(I-1,J,2,0))/XK**2
WXX=(DEF(I,J-1,3,KM1)-2.*DEF(I,J,3,0)+DEF(I,J+1,3,KP1))/XH**2
WXT=(DEF(I+1,J-1,3,KM1)-DEF(I+1,J+1,3,KP1)-DEF(I-1,J-1,3,KM1)+
1 DEF(I-1,J+1,3,KP1))/(4.*XH*XK)
WTX=WXT
WTT=(DEF(I+1,J,3,0)-2.*DEF(I,J,3,0)+DEF(I-1,J,3,0))/XK**2
WXXX=(DEF(I,J-2,3,KM2)-2.*DEF(I,J-1,3,KM1)+2.*DEF(I,J+1,3,KP1)
1 -DEF(I,J+2,3,KP2))/(2.*XH**3)
WXTT=(DEF(I+1,J-1,3,KM1)-2.*DEF(I,J-1,3,KM1)+2.*DEF(I,J+1,3,KP1)
1 )-DEF(I+1,J+1,3,KP1)+DEF(I-1,J-1,3,KM1)-DEF(I-1,J+1,3,KP1))/(2.*
2 XH*XK*XK)
WTTX=WXTT
WTTT=(DEF(I+2,J,3,0)-2.*DEF(I+1,J,3,0)+2.*DEF(I-1,J,3,0)-DEF(I-2,
1 J,3,0))/(2.*XK**3)
WXXT=(DEF(I+1,J-1,3,KM1)-2.*DEF(I+1,J,3,0)+2.*DEF(I-1,J,3,0)+
1 DEF(I+1,J+1,3,KP1)-DEF(I-1,J-1,3,KM1)-DEF(I-1,J+1,3,KP1))/(2.*
2 XH*XH*XK)
X=ZETA(J+1)
SI = SINF(X)
CO = COSF(X)
CSC = 1./SI
COT = CO *CSC
EPSX = UX+W
EPST = COT*U + CSC*VT + W
GAM = CSC*UT + VX - COT*V
XLX1 = UX - WXX
XLX2 = CSC*(VT - CSC*WTT + CO*(U-WX))
XLX12 = CSC*(CO *V + COT*WT - WXT - UT) + VX

```

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SIP15170
SIP15180
SIP15190
SIP15200
SIP15210
SIP15220
SIP15230
SIP15240
SIP15250
SIP15260
SIP15270
SIP15280
SIP15290
SIP15300
SIP15310
SIP15320
SIP15330
SIP15340
SIP15350
SIP15360
SIP15370
SIP15380
SIP15390
SIP15400
SIP15410
SIP15420
SIP15430
SIP15440
SIP15450
SIP15460
SIP15470
SIP15480
SIP15490
SIP15500
SIP15510
SIP15520
SIP15530
SIP15540
SIP15550

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```

XXX = UXX - WXXX
XXT = UXT - WXXT
XTX = CSC*(CO *(UX-WXX) + SI *(WX-U) - CSC*WTTX + VTX
1 - COT*(CO *(U-WX) - 2.*CSC*WTT + VTT)
XTT = CSC*(CO *(UT-WXT) - CSC*WTTT + VTT)
XXTX = CSC*(COT*WXT + CO *VX - SI *V - WXXT - UXT - CSC*CSC*(WT
1 - CO *(WXT + UT - COT*WT - CO *V)) + VXX
XXTT = VXT + CSC*(UTT - WXTT - CO *(VT - CSC*WTT))
IF (MFLAG) 20, 40, 40
20 CONTINUE
OMEGAX = U - WX
OMEGAT = V - CSC*WT
PHI = .5*(VX + CSC*(CO *V - UT))
WRITE OUTPUT TAPE 6, 101, J, I, EPSX, EPST, GAM, XLX1, XLX2, XLX12,
1 OMEGAX, OMEGAT, PHI
GO TO 99
40 CONTINUE
ANX = FPSX + ZNU*EPST - TC
ANT = EPST + ZNU*EPSX - TC
ANXT = GAM + 2.*DD*XLX12
ANTX = ANXT
AMX = XLX1 + ZNU*XLX2 - TD*RH
AMT = XLX2 + ZNU*XLX1 - TD*RH
AMXT = XLX12
AMTX = AMXT
AMXTT = XXTT
AMXTX = XXTX
AQX = XXX + ZNU*XTX + (1.-ZNU)*CSC*(XXTX + CO *(XLX1-XLX2))
AQT = XTT + ZNU*XXT + (1.-ZNU)*(2.*XLX12*COT + XXTX)
IF (K) 49, 49, 47
47 YL(1, K, I)=ANX
YL(2, K, I)=ANT
YL(3, K, I)=AMX
YL(4, K, I)=AMT
49 CONTINUE
IF (MFLAG) 45, 45, 46
45 WRITE OUTPUT TAPE 6, 101, J, I, AMX , AMT, AMXT, AGX , AQT
GO TO 48
46 WRITE OUTPUT TAPE 6, 101, J, I, ANX, ANT, ANXT, ANTX

```

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SIP15560
SIP15570
SIP15580
SIP15590
SIP15600
SIP15610
SIP15620
SIP15630
SIP15640
SIP15650
SIP15660
SIP15670
SIP15680
SIP15690
SIP15700
SIP15710
SIP15720
SIP15730
SIP15740
SIP15750
SIP15760
SIP15770
SIP15780
SIP15790
SIP15800
SIP15810
SIP15820
SIP15830
SIP15840
SIP15850
SIP15860
SIP15870
SIP15880
SIP15890
SIP15900
SIP15910
SIP15920
SIP15930
SIP15940

```

```

48 CONTINUE
IF (J) 60, 60, 51
51 IF (NR1-J) 70, 70, 52
52 IF (NC1-I) 80, 80, 99
C LOWER BOUNDARY
60 J3=NC1+NR1+2+NC1-I
YK(1,J3) = ANXT + 2.*DD*AMXT
YK(2,J3) = ANX
YK(3,J3) = AQX + CSC*(1.-ZNU)*AMXTT
YK(4,J3) = AMX
IF (I-NC1) 99, 69, 69
C SPECIAL POINT
69 K1=2*(NC1+NR1)+1
YK(1, K1)=-2.*AMXT
GO TO 80
C UPPER BOUNDARY
70 YK(1,I) = ANXT + 2.*DD*AMXT
YK(2,I) = ANX
YK(3,I) = -AQX - CSC*(1.-ZNU)*AMXTT
YK(4,I) = AMX
IF (I-NC1) 99, 79, 79
C SPECIAL CORNER POINT
79 K1=2*(NC1+NR1)
YK(1, K1)=+2.*AMXT
C RIGHT BOUNDARY
80 J3=NC1+NR1+1-J
YK(1,J3) = -ANTX - 2.*DD*AMXT
YK(2,J3) = ANT
YK(3,J3) = AQT + (1.-ZNU)*AMXTX
YK(4,J3) = AMT
99 RETURN
END
FORTRAN
SUBROUTINE ZERO (X,N)
DIMENSION X(8500)
DO I I=1,N
I X(I)=0.
RETURN
END

```

```

S1P15950
S1P15960
S1P15970
S1P15980
S1P15990
S1P16000
S1P16010
S1P16020
S1P16030
S1P16040
S1P16050
S1P16060
S1P16070
S1P16080
S1P16090
S1P16100
S1P16110
S1P16120
S1P16130
S1P16140
S1P16150
S1P16160
S1P16170
S1P16180
S1P16190
S1P16200
S1P16210
S1P16220
S1P16230
S1P16240
S1P16250
S1P16260
S1P16270
S1P16280
S1P16290
S1P16300
S1P16310
S1P16320
S1P16330

```


| | | | | |
|------|------|------------|-------|----------|
| SSM | ADD | AY | RWDIM | SIP16730 |
| ADD | AY | | | SIP16740 |
| ADD | ADD | RWDIM | | SIP16750 |
| ADD | ADD | =1 | | SIP16760 |
| STA | STA | YCOL | | SIP16770 |
| LXA | LXA | NR,1 | | SIP16780 |
| SXD | SXD | MT4,1 | | SIP16790 |
| AXT | AXT | 1,1 | | SIP16800 |
| LXA | LXA | NC,2 | | SIP16810 |
| YCOL | CLA | ** ,2 | | SIP16820 |
| STO | STO | TEM,2 | | SIP16830 |
| TIX | TIX | YCOL,2,1 | | SIP16840 |
| MT1 | SXA | I,1 | | SIP16850 |
| LDQ | LDQ | RWDIM | | SIP16860 |
| MPY | MPY | NC | | SIP16870 |
| XCA | XCA | ,4 | | SIP16880 |
| PAX | PAX | ,4 | | SIP16890 |
| CLA | CLA | RWDIM | | SIP16900 |
| ADD | ADD | AX | | SIP16910 |
| ADD | ADD | =1 | | SIP16920 |
| SUR | SUR | I | | SIP16930 |
| STA | STA | MT2 | | SIP16940 |
| STA | STA | AXIK | | SIP16950 |
| LXA | LXA | NC,2 | | SIP16960 |
| STZ | STZ | TEM | | SIP16970 |
| STZ | STZ | TEM+1 | | SIP16980 |
| PXA | PXA | 0,0 | | SIP16990 |
| MT2 | NZT | ** ,4 | | SIP17000 |
| TXI | TXI | MT3+1,2,-1 | | SIP17010 |
| LDQ | LDQ | ** ,4 | | SIP17020 |
| AYKJ | FMP | TEM,2 | | SIP17030 |
| DFAD | DFAD | TEM | | SIP17040 |
| DST | DST | TEM | | SIP17050 |
| TNX | TNX | *+2,2,1 | | SIP17060 |
| TIX | TIX | MT2,4,ROWD | | SIP17070 |
| STO | STO | ** ,1 | | SIP17080 |
| TXI | TXI | *+1,1,1 | | SIP17090 |
| TXL | TXL | MT1,1,** | | SIP17100 |
| CLA | CLA | J | | SIP17110 |

**=NR

| | | |
|--------|--------------|----------|
| STA | AIL | SIP17510 |
| CLA* | 2,4 | SIP17520 |
| ARS | 18 | SIP17530 |
| STA | I | SIP17540 |
| CLA* | 4,4 | SIP17550 |
| PDX | ,2 | SIP17560 |
| ARS | 18 | SIP17570 |
| SUB | =1 | SIP17580 |
| XCA | | SIP17590 |
| MPY | RDIM | SIP17600 |
| XCA | | SIP17610 |
| ADD | I | SIP17620 |
| PAX | ,1 | SIP17630 |
| CLA* | 3,4 | SIP17640 |
| ARS | 18 | SIP17650 |
| SUR | =1 | SIP17660 |
| XCA | | SIP17670 |
| MPY | RDIM | SIP17680 |
| XCA | | SIP17690 |
| SSM | | SIP17700 |
| ADD | AIL | SIP17710 |
| STA | ALJ | SIP17720 |
| STZ | SUM | SIP17730 |
| STZ | SUM+1 | SIP17740 |
| LDQ | **,1 | SIP17750 |
| FMP | **,2 | SIP17760 |
| DEAD | SUM | SIP17770 |
| DST | SUM | SIP17780 |
| TXI | *+1,1,ROWDIM | SIP17790 |
| TXI | *+1,2,1 | SIP17800 |
| TXL | AIL,2,** | SIP17810 |
| AXT | **,1 | SIP17820 |
| AXT | **,2 | SIP17830 |
| TRA | 6,4 | SIP17840 |
| COMMON | 1 | SIP17850 |
| FQU | R+203 | SIP17860 |
| PZE | | SIP17870 |
| ROWDIM | EQU | SIP17880 |
| RDIM | DEC | SIP17890 |

| | | |
|------|----------|----------|
| ADD | K | SIP18290 |
| SUB | K2 | SIP18300 |
| XCA | | SIP18310 |
| MPY | ROWD | SIP18320 |
| XCA | | SIP18330 |
| SUB | =1 | SIP18340 |
| ADD | K2 | SIP18350 |
| PAX | ,2 | SIP18360 |
| TRA | DPO | SIP18370 |
| AXT | 1,2 | SIP18380 |
| SXD | DP3,2 | SIP18390 |
| CLA | K | SIP18400 |
| ADD | K | SIP18410 |
| ADD | =1 | SIP18420 |
| XCA | | SIP18430 |
| MPY | ROWD | SIP18440 |
| XCA | | SIP18450 |
| ADD | K2 | SIP18460 |
| SUB | =1 | SIP18470 |
| PAX | ,2 | SIP18480 |
| CLA* | 5,4 | SIP18490 |
| ARS | 18 | SIP18500 |
| SUB | K2 | SIP18510 |
| ADD | =1 | SIP18520 |
| PAX | ,4 | SIP18530 |
| STZ | TEMP | SIP18540 |
| STZ | TEMP+1 | SIP18550 |
| LDQ | ** ,1 | SIP18560 |
| FMP | ** ,2 | SIP18570 |
| DFAD | TEMP | SIP18580 |
| DST | TEMP | SIP18590 |
| TXI | *+1,1,** | SIP18600 |
| TXI | *+1,2,** | SIP18610 |
| TIX | DP1,4,1 | SIP18620 |
| AXT | ** ,1 | SIP18630 |
| AXT | ** ,2 | SIP18640 |
| AXT | ** ,4 | SIP18650 |
| TRA | 6,4 | SIP18660 |
| DEC | 270 | SIP18670 |


```

K      DFC      5
I      PZE
K2     PZE
TEMP   BOOL     77774
      END
      FAP
      COUNT    150
      ENTRY   CLOCK
      ENTRY   WCKA
      ENTRY   WCKP
      SUBROUTINE   CLOCK
      *****
      * THIS SUBROUTINE PLACES THE CLOCK IN A GIVEN LOCATION SPECIFIED
      * BY THE CALL STATEMENT( THAT IS
      * CALL CLOCK(LOCATION TO E STORED IN FORTRAN OR
      * CALL CLOCK (FOR ABSOLUTE ASSEMBLIES USE TSX CLOCK
      * PZE (LOCATION TO BE STORED) IN FAP
      * OR
      * SVN (LOCATION TO BE STORED) GIVES THE CLOCK IN FLOATING POINT
      * PZE (LOCATION TO BE STORED) GIVES THE CLOCK IN BCD
      * IN FORTRAN THE CLOCK WILL ALWAYS BE GIVEN IN FLOATING POINT
      * THE CLOCK IS ALSO PRINTED ON-LINE
      * *****
      *
      * SPACE 3
      *
      * CLOCK BSS 0
      * WCKA BSS 0
      * WCKP BSS 0
      *
      * SXA CLOCK+55,1
      * SXA CLOCK+56,2
      * SXA CLOCK+57,4
      * RPRA
      * SPRA 10
      * RCHA CLOCK+105
      * TCOA *
      * STZ CLOCK+61
      * STZ CLOCK+62
      * CLA CLOCK+227
      * STO CLOCK+218
      * AXT 0,3

```

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SIP18680
SIP18690
SIP18700
SIP18710
SIP18720
SIP18730
SIP18740
SIP18750
SIP18760
SIP18770
SIP18780
*SIP18790
*SIP18800
*SIP18810
*SIP18820
*SIP18830
*SIP18840
*SIP18850
*SIP18860
*SIP18870
*SIP18880
*SIP18890
*SIP18900
SIP18910
SIP18920
SIP18930
SIP18940
SIP18950
SIP18960
SIP18970
SIP18980
SIP18990
SIP19000
SIP19010
SIP19020
SIP19030
SIP19040
SIP19050
SIP19060

```

| | | | |
|-----|-----------------|--|----------|
| AXT | 2,4 | | SIP19070 |
| LDQ | CLOCK+104,1 | | SIP19080 |
| PXD | 0,0 | | SIP19090 |
| CAQ | CLOCK+153,1 | | SIP19100 |
| CVR | CLOCK+217,6 | | SIP19110 |
| ORS | CLOCK+63,4 | | SIP19120 |
| TIX | *-4,4,1 | | SIP19130 |
| CLA | CLOCK+226,2 | | SIP19140 |
| STO | CLOCK+218 | | SIP19150 |
| TXT | *+1,2,1 | | SIP19160 |
| TXI | *+1,1,2 | | SIP19170 |
| TXL | CLOCK+12,1,17 | | SIP19180 |
| PXD | 0,0 | | SIP19190 |
| LDQ | CLOCK+61 | | SIP19200 |
| LGL | 30 | | SIP19210 |
| LDQ | CLOCK+62 | | SIP19220 |
| LGL | 18 | | SIP19230 |
| RQL | 6 | | SIP19240 |
| LGL | 12 | | SIP19250 |
| SLW | CLOCK+61 | | SIP19260 |
| LXA | CLOCK+57,4 | | SIP19270 |
| CAL | 1,4 | | SIP19280 |
| ARS | 18 | | SIP19290 |
| TZE | CLOCK+55 | | SIP19300 |
| PXD | 0,0 | | SIP19310 |
| LDQ | CLOCK+61 | | SIP19320 |
| CAQ | CLOCK+113,4 | | SIP19330 |
| STQ | CLOCK+61 | | SIP19340 |
| ARS | 18 | | SIP19350 |
| ADD | =02330000000000 | | SIP19360 |
| FAD | =02330000000000 | | SIP19370 |
| XCA | | | SIP19380 |
| FMP | =1,F2 | | SIP19390 |
| STO | CLOCK+87 | | SIP19400 |
| PXD | 0,0 | | SIP19410 |
| LDQ | CLOCK+61 | | SIP19420 |
| CAQ | CLOCK+133,2 | | SIP19430 |
| ARS | 18 | | SIP19440 |

| | | |
|-----|---|----------|
| PZE | *+3,,700 | SIP19850 |
| PZF | *+2,,800 | SIP19860 |
| PZE | *+1,,900 | SIP19870 |
| PZE | *+10 | SIP19880 |
| PZE | *+9,,10 | SIP19890 |
| PZE | *+8,,20 | SIP19900 |
| PZE | *+7,,30 | SIP19910 |
| PZE | *+6,,40 | SIP19920 |
| PZE | *+5,,50 | SIP19930 |
| PZE | *+4,,60 | SIP19940 |
| PZE | *+3,,70 | SIP19950 |
| PZE | *+2,,80 | SIP19960 |
| PZF | *+1,,900 | SIP19970 |
| PZE | | SIP19980 |
| PZE | ,,1 | SIP19990 |
| PZE | ,,2 | SIP20000 |
| PZE | ,,3 | SIP20010 |
| PZE | ,,4 | SIP20020 |
| PZE | ,,5 | SIP20030 |
| PZE | ,,6 | SIP20040 |
| PZE | ,,7 | SIP20050 |
| PZE | ,,8 | SIP20060 |
| PZE | ,,9 | SIP20070 |
| RCT | 8,0000000000001000010000001000000010000001000000100000110000111 | SIP20080 |
| RCT | 8,001000001111 | SIP20090 |
| RCT | 8,010000010001001001001001001001001001001001001001001001001001001001111 | SIP20100 |
| RCT | 8,011000011001001001001001001001001001001001001001001001001001001001111 | SIP20110 |
| RCT | 8,10000010000011000010100011000101000110001001001001001001001001001001111 | SIP20120 |
| RCT | 8,1010000101001101111 | SIP20130 |
| RCT | 8,1100001100011100011100010110010110010110010110010110010110010110111 | SIP20140 |
| RCT | 8,1110001100111001110101110101110101110101110101110101110101110111111 | SIP20150 |
| PZE | * | SIP20160 |
| PZE | *-1 | SIP20170 |
| PON | *-2,,4096 | SIP20180 |
| PON | *-3 | SIP20190 |
| PZE | *-4,,7*4096 | SIP20200 |
| PZE | *-5,,6*4096 | SIP20210 |
| PZE | *-6,,5*4096 | SIP20220 |
| PZE | *-7,,4*4096 | SIP20230 |

| | | | | |
|---------------|-------------------------------|---------|------------------------------------|----------|
| PZE | *-8,,3*4096 | | | S1P20240 |
| PZE | *-9,,2*4096 | | | S1P20250 |
| PZE | *-10,,1*4096 | | | S1P20260 |
| END | | | | S1P20270 |
| * FAP | | | | S1P20280 |
| | COUNT | 170 | | S1P20290 |
| * SUBROUTINES | RTAPE, WTAPE, BACK, AND RESET | | | S1P20300 |
| ENTRY | WTAPE | | | S1P20310 |
| ENTRY | RTAPE | | | S1P20320 |
| ENTRY | RFW | | | S1P20330 |
| ENTRY | BACK | | | S1P20340 |
| ENTRY | RESET | | | S1P20350 |
| WTAPE | CLA | WRS | | S1P20360 |
| STD | WRTP | | | S1P20370 |
| STZ | FLAG1 | | SET FLAG1 FOR WRITING | S1P20380 |
| TRA | BEGIN | | | S1P20390 |
| RTAPE | CLA | RDS | | S1P20400 |
| STD | WRTP | | READ, NOT WRITE | S1P20410 |
| STL | FLAG1 | | SET FOR READING | S1P20420 |
| REGIN | SXA | AXT,1 | | S1P20430 |
| | SXA | AXT+1,2 | | S1P20440 |
| STZ | FLAG | | FIRSTT TIME THROUGH | S1P20450 |
| CLA* | 1,4 | | | S1P20460 |
| STA | RSR | | | S1P20470 |
| ANA | MASK | | | S1P20480 |
| TZE | **3 | | | S1P20490 |
| STL | FLAG2 | | SET FLAG2 FOR CAANNEL A | S1P20500 |
| TRA | **2 | | | S1P20510 |
| STZ | FLAG2 | | SET FLAG2 FOR CHANNEL B | S1P20520 |
| NZT* | 4,4 | | IS THIS A CHECK | S1P20530 |
| TRA | WR | | GO AND START A READ OR WRITE | S1P20540 |
| CK | CKB | | CHECK FOR REDUNDANCY. | S1P20550 |
| CKA | * | | | S1P20560 |
| TRCA | ERR | | | S1P20570 |
| TRA | AXT | | | S1P20580 |
| TCOB | * | | | S1P20590 |
| TRCB | ERR | | | S1P20600 |
| TRA | AXT | | | S1P20610 |
| ZET | FLAG | | TAPE ERROR. IS THIS THE FIRST TIME | S1P20620 |

| | | | |
|-------|------|------------------|----------|
| TRA | BLNK | NO | S1P20630 |
| STL | FLAG | | S1P20640 |
| BSR | ** | | S1P20650 |
| WR | CLA* | 3,4 | S1P20660 |
| | STD | IOC | S1P20670 |
| | ARS | 18 | S1P20680 |
| | SSM | | S1P20690 |
| | ADD | 2,4 | S1P20700 |
| | ADD | =1 | S1P20710 |
| | STA | IOC | S1P20720 |
| | CLA* | 1,4 | S1P20730 |
| | STA | WRTP | S1P20740 |
| | ANA | TPNR | S1P20750 |
| | PAX | ,1 | S1P20760 |
| | CLA | TPCNT+1,1 | S1P20770 |
| | STA | LDI | S1P20780 |
| | STA | COMP | S1P20790 |
| | STA | STORE | S1P20800 |
| | PDX | ,2 | S1P20810 |
| LDJ | LDQ | ** ,2 | S1P20820 |
| | ZET | FLAG | S1P20830 |
| | TRA | RERUN | S1P20840 |
| | SSP | | S1P20850 |
| | ADD | ONE | S1P20860 |
| | PDX | ,2 | S1P20870 |
| | STD | TPCNT+1,1 | S1P20880 |
| | STA | TPCNT+1,1 | S1P20890 |
| | ZET | FLAG1 | S1P20900 |
| | TRA | WR1 | S1P20910 |
| | XCA | WRITE OPERATION. | S1P20920 |
| | ADD | ONE | S1P20930 |
| | ADD | =1 | S1P20940 |
| STORE | STO | ** ,2 | S1P20950 |
| | STO | IDENT | S1P20960 |
| WR1 | NZT | FLAG2 | S1P20970 |
| | TRA | TPB | S1P20980 |
| TPA | TCOA | * | S1P20990 |
| | TRCA | **+1 | S1P21000 |
| | XFC | WRTP | S1P21010 |

WORD COUNT

BOTTOM OF ARRAY IN AC

SET TAPE UNIT ADDRESS
PICK OUT LAST DIGIT
TAPE M. M TO XR 1

IF RERUN, DONT BUMP COUNTERS

NOT A BACKSPACE SO SIGN PLUS

IS IT, READ OR WRITE

READ OPERATION

WRITE OPERATION. MUST MAKE UP NEXT RECORD ID NR.

STORE NEXT RECORD ID WORD IN TABLE
FIRST WORD OF RECORD
CHANNEL A OR B

| | | | | | | |
|------|-----------|---------|---|--|--|----------|
| RCHA | ICID | | | | | S1P21020 |
| LCHA | IOC | | | | | S1P21030 |
| ZET | FLAG1 | | IF READING, GO CHECK RFCORD ID | | | S1P21040 |
| TRA | COMP | | | | | S1P21050 |
| ZET | FLAG | | IS THIS A RERUN | | | S1P21060 |
| TRA | CKA | YES. | GO AND CHECK FOR REDUNDANCY | | | S1P21070 |
| TRA | AXT | NO. | GO BACK AND COMPUTE SOME MORE | | | S1P21080 |
| TCOB | * | | | | | S1P21090 |
| TRCR | *+1 | | | | | S1P21100 |
| XEC | WRTP | | | | | S1P21110 |
| RCHR | ICID | | | | | S1P21120 |
| LCHR | IOC | | | | | S1P21130 |
| ZFT | FLAG1 | | | | | S1P21140 |
| TRA | COMP | | | | | S1P21150 |
| ZFT | FLAG | | | | | S1P21160 |
| TRA | CKR | | | | | S1P21170 |
| TRA | AXT | | | | | S1P21180 |
| CLA | **2 | | | | | S1P21190 |
| SUB | IDENT | | DOES FIRST WORD OF RECORD AGREE WITH ID | | | S1P21200 |
| TNZ | SHIFT | NO. | TRY ANOTHER RECORD | | | S1P21210 |
| STP | TPCNT+1,1 | | | | | S1P21220 |
| NZT | FLAG | YES. | IS THIS A RERUN | | | S1P21230 |
| TRA | AXT | IF NOT, | GO BACK | | | S1P21240 |
| CLA | FLAG2 | | | | | S1P21250 |
| TPA | CK | | | | | S1P21260 |
| ZFT | FLAG1 | | | | | S1P21270 |
| TRA | WR1 | | | | | S1P21280 |
| XCA | | | RESET ID WORD | | | S1P21290 |
| TRA | STORE+1 | | | | | S1P21300 |
| ZET | FLAG1 | | IS THIS A READ | | | S1P21310 |
| TRA | OUT | | IF SO GIVE UP | | | S1P21320 |
| XEC | BSR | | | | | S1P21330 |
| XFC | WRTP | | | | | S1P21340 |
| XEC | WRTP | | | | | S1P21350 |
| XEC | WRTP | | | | | S1P21360 |
| CLA | MAX | | | | | S1P21370 |
| SUR | =1 | | | | | S1P21380 |
| TMT | OUT | | QUIT AFTER MAX TIMES | | | S1P21390 |
| STO | MAX | | | | | S1P21400 |

| | | |
|-----------|---|----------|
| IDENT | STORE-1 | CLP21410 |
| MAX | | CLP21420 |
| =1 | | CLP21430 |
| OUT | | CLP21440 |
| MAX | | CLP21450 |
| TPCNT+1,1 | | CLP21460 |
| WRI | LAST ACTIVITY WAS READ OR WRITE SO GO AHEAD | CLP21470 |
| PSR | LAST ACTIVITY WAS BACKSPACE. MUST GO BACK | CLP21480 |
| PSR | | CLP21490 |
| WRI | LOOK FOR MISSING RECORD AGAIN | CLP21500 |
| **9,1 | | CLP21510 |
| **9,2 | | CLP21520 |
| 5,4 | | CLP21530 |
| DUMP | | CLP21540 |
| 1,4 | | CLP21550 |
| *+1 | | CLP21560 |
| ** | | CLP21570 |
| AX,1 | | CLP21580 |
| TPNR | | CLP21590 |
| ,1 | | CLP21600 |
| ,0 | | CLP21610 |
| TPCNT+1,1 | | CLP21620 |
| **9,1 | | CLP21630 |
| 2,4 | | CLP21640 |
| 1,4 | | CLP21650 |
| BSR | | CLP21660 |
| BSR | | CLP21670 |
| BX,1 | | CLP21680 |
| TPNR | | CLP21690 |
| ,1 | | CLP21700 |
| TPCNT+1,1 | | CLP21710 |
| ONE | | CLP21720 |
| ONE | | CLP21730 |
| ONE | | CLP21740 |
| TPCNT+1,1 | | CLP21750 |
| ,1 | | CLP21760 |
| 2,4 | | CLP21770 |
| | | CLP21780 |
| | | CLP21790 |


```

RESET PXA 0,0
      STD TPCNT-3
      STD TPCNT-2
      STD TPCNT-1
      STD TPCNT
      TPA 1,4
      ICST IDENT,1
      IORT 0,0
      WRS **
      WRS **
      RDS **
      PZE TRL4
      PZE TBL3
      PZE TBL2
      PZE TBL1
      TPCNT 7
      TPNR OCT 000000001000
      MASK OCT 40
      MAX DEC 1000000
      ONE OCT
      FLAG
      FLAG1
      FLAG2
      IDENT PZE
      TRL1 RES 80
      TRL2 RES 80
      TRL3 RES 80
      TRL4 RES 80
      END
      * CHAIN(2,2)
      * FORTPAN
      CSITWO CHAIN LINK 2 FOR SPHERE
      COMMON IOPT1, IOPT2, IOPT3, IOPT4, IOPT5, IOPT6, IOPT7, IOPT8
      COMMON NCF
      COMMON NDI4, NROW, NCOL, MM, MFLAG, XM, XLD
      COMMON ISW1, ISW2, ISW3
      COMMON A
      COMMON TMP, YK, YL
      COMMON T1, T2, XX, XXI, 7, Z1, Z2

```

```

SIP21800
SIP21810
SIP21820
SIP21830
SIP21840
SIP21850
SIP21860
SIP21870
SIP21880
SIP21890
SIP21900
SIP21910
SIP21920
SIP21930
SIP21940
SIP21950
SIP21960
SIP21970
SIP21980
SIP21990
SIP22000
SIP22010
SIP22020
SIP22030
SIP22040
SIP22050
SIP22060
SIP22070
SIP22080
SIP22090
SIP22100
SIP22110
SIP22120
SIP22130
SIP22140
SIP22150
SIP22160
SIP22170
SIP22180

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COMMON ZNU, THC, PH1, FF, RH, DD, XH, XK
COMMON ZETA
COMMON TE, TI, TO, OC, TC, TD, DDL
COMMON RECORD
DIMENSION A(1232)
DIMENSION MM(40)
DIMENSION T1( 89), T2(89), XX(89), XX1(89), Z(89), Z1(89), Z2(89)
DIMENSION TMP(5184), YK(5184), YL(4,4,324)
DIMENSION ZETA (30)
DIMENSION RECORD (12)
DIMENSION DISP(9), STRSS(9), ORDLBL(6,11), ABLBL(6), CILBL(6,4)
DIMENSION ARSC(80), AORD(25), POND(9)
DIMENSION CRLRL (6, 4)
DIMENSION AXLBL (6)
1 FORMAT (1H1, 12A6)
966 FORMAT (6A6)
B
KTAPF=15
MO=1-IOPT2
NR1=NR0W+1
NC1=NCOL+1
NR3=3*(NROW+6)
NR4=NR1+1-MO
51 READ INPUT TAPE 5, 966, ((CILBL(I, J), I=1, 6), J=1, 4)
NFND=0
NCRV=MM(31)
NCRV1=2-MO
NPTS=NCOL/26+1
NFLAG=1
CALL PLTLBL (DISP, STRSS, ORDLBL, ABLBL, POND, AXLBL)
TH=0.
COL=NCOL
DELH=1./COL
DO 52 I=1, NC1
ARSC(I)=TH
52 TH=TH+DELH
DO 53 J=1, NR1
JJ=NR1+2-J
53 AORD(J)=ZETA(JJ)
S1P222190
S1P222200
S1P222210
S1P222220
S1P222230
S1P222240
S1P222250
S1P222260
S1P222270
S1P222280
S1P222290
S1P222300
S1P222310
S1P222320
S1P222330
S1P222340
S1P222350
S1P222360
S1P222370
S1P222380
S1P222390
S1P222400
S1P222410
S1P222420
S1P222430
S1P222440
S1P222450
S1P222460
S1P222470
S1P222480
S1P222490
S1P222500
S1P222510
S1P222520
S1P222530
S1P222540
S1P222550
S1P222560
S1P222570

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AORD(NR1+1)=ZFTA(1)
601 DO 650 K=1, 2
WRITE TAPE KTAPE, RECORD
WRITE TAPE KTAPE, NCI, NCRV, NPTS, NEND, NFLAG
WRITE TAPE KTAPE, ABLBL, (ORDLBL(M,K),M=1,6), DISP
WRITE TAPE KTAPE, CILBL
DO 610 I=1, NCI
WRITE TAPE KTAPE, ARSC(I)
610 CONTINUE
L=32
L3=R1+MM(31)
DO 620 J=0, NR1
IF (MM(L)-J) 620, 611, 620
611 I1=3*(J+2)+K
DO 615 I=1, NCI
WRITE TAPE KTAPE, TMP(I1)
615 I1=I1+NR3
L=L+1
IF (L-L3) 620, 620, 650
620 CONTINUE
650 CONTINUE
DO 720 K=1, 4
K1=K+3
WRITE TAPE KTAPE, RECORD
WRITE TAPE KTAPE, NCI, NCRV, NPTS, NEND, NFLAG
WRITE TAPE KTAPE, ABLBL, (ORDLBL(M, K1), M=1, 6), STRSS
WRITE TAPE KTAPE, CILBL
DO 662 I=1, NCI
WRITE TAPE KTAPE, ARSC(I)
662 CONTINUE
DO 660 M=1, NCRV
DO 660 I=1, NCI
660 WRITE TAPE KTAPE, YL(K,M,I)
720 CONTINUE
DO 740 K1=1, 4
K=K1+7
NCRV=NCRV1
NCR=0
NCX=NC1

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S1P22580
S1P22590
S1P22600
S1P22610
S1P22620
S1P22630
S1P22640
S1P22650
S1P22660
S1P22670
S1P22680
S1P22690
S1P22700
S1P22710
S1P22720
S1P22730
S1P22740
S1P22750
S1P22760
S1P22770
S1P22780
S1P22790
S1P22800
S1P22810
S1P22820
S1P22830
S1P22840
S1P22850
S1P22860
S1P22870
S1P22880
S1P22890
S1P22900
S1P22910
S1P22920
S1P22930
S1P22940
S1P22950
S1P22960

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| | | |
|-----|---|------------|
| 725 | WRITE TAPE KTAPE, RECORD | SI P222970 |
| | WRITE TAPE KTAPE, NCX, NCRV, NPTS, NEND, NFLAG | SI P222980 |
| | IF (NCR) 723, 723, 724 | SI P222990 |
| 723 | CONTINUE | SI P23000 |
| | WRITE TAPE KTAPE, ABLBL, (ORDLBL(M,K), M=1, 6), BOND | SI P23010 |
| | GO TO 726 | SI P23020 |
| 724 | CONTINUE | SI P23030 |
| | WRITE TAPE KTAPE, AXLRL, (ORDLBL(M, K), M=1, 6), BOND | SI P23040 |
| 726 | CONTINUE | SI P23050 |
| | CALL PLBL (CBLRL, NCR) | SI P23060 |
| | WRITE TAPE KTAPE, CBLBL | SI P23070 |
| | IF (NCR) 727, 727, 729 | SI P23080 |
| 727 | DO 728 I=1, NCI | SI P23090 |
| 728 | WRITE TAPE KTAPE, ARSC(I) | SI P23100 |
| | I1=K1 | SI P23110 |
| | GO TO 731 | SI P23120 |
| 729 | DO 730 I=1, NR4 | SI P23130 |
| 730 | WRITE TAPE KTAPE, AORD(I) | SI P23140 |
| 731 | CONTINUE | SI P23150 |
| | KAD=4 | SI P23160 |
| | DO 735 M=1, NCRV | SI P23170 |
| | DO 732 L=1, NCX | SI P23180 |
| | WRITE TAPE KTAPE, YK(I1) | SI P23190 |
| 732 | I1=I1+KAD | SI P23200 |
| | I1=4*(NC1+NC1+NR1)+K1 | SI P23210 |
| 735 | KAD=-4 | SI P23220 |
| | IF (NCR) 736, 736, 740 | SI P23230 |
| 736 | NCR=1 | SI P23240 |
| | I1=4*NC1+K1 | SI P23250 |
| | KAD=4 | SI P23260 |
| | NCX=NR4 | SI P23270 |
| | NCRV=1 | SI P23280 |
| | IF (K1-4) 715, 714, 714 | SI P23290 |
| 714 | NEND=1 | SI P23300 |
| 715 | CONTINUE | SI P23310 |
| | GO TO 725 | SI P23320 |
| 740 | CONTINUE | SI P23330 |
| | WRITE TAPE KTAPE, XXN | SI P23340 |
| | BACKSPACE KTAPE | SI P23350 |

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IF (IOPT5) 1010, 1010, 1010, 1011
1010 CALL CHAIN (1, 2)
1011 CALL CHAIN (3,2)
END
* FAP
COUNT 80
*PLTLBL SUBROUTINE PLTLBL (DISP, STRSS, ORDLBL, ABLBL, BOND )
PLTLBL SXA AXT,1
SXA AXT+1,2
CLA 1,4
STA D1+1
AXT 9,1
AXT 0,2
D1 CLA DISP+9,1
STO **,2
TNX *+2,1,1
TXI D1,2,1
CLA 2,4
STA S1+1
AXT 9,1
AXT 0,2
S1 CLA STRSS+9,1
STO **,2
TNX *+2,1,1
TXI S1,2,1
CLA 3,4
STA 01+1
AXT 66,1
AXT 0,2
01 CLA ORDU+66,1
STO **,2
TNX *+2,1,1
TXI 01,2,1
CLA 4,4
STA A1+1
AXT 6,1
AXT 0,2
A1 CLA ARLBL+6,1
S1P23360
S1P23370
S1P23380
S1P23390
S1P23400
S1P23410
S1P23420
S1P23430
S1P23440
S1P23450
S1P23460
S1P23470
S1P23480
S1P23490
S1P23500
S1P23510
S1P23520
S1P23530
S1P23540
S1P23550
S1P23560
S1P23570
S1P23580
S1P23590
S1P23600
S1P23610
S1P23620
S1P23630
S1P23640
S1P23650
S1P23660
S1P23670
S1P23680
S1P23690
S1P23700
S1P23710
S1P23720
S1P23730
S1P23740

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| | | | | | | | |
|-------|-----------|----|--|--|--------|--------------------------------|----------|
| STO | **2 | | | | | | S1P23750 |
| TNX | *+2,1,1 | | | | | | S1P23760 |
| TXI | A1,2,1 | | | | | | S1P23770 |
| CLA | 5,4 | | | | | | S1P23780 |
| STA | B1+1 | | | | | | S1P23790 |
| AXT | 9,1 | | | | | | S1P23800 |
| AXT | 0,2 | | | | | | S1P23810 |
| CLA | BON+9,1 | | | | | | S1P23820 |
| STO | **2 | | | | | | S1P23830 |
| TNX | *+2,1,1 | | | | | | S1P23840 |
| TXI | P1,2,1 | | | | | | S1P23850 |
| CLA | 6,4 | | | | | | S1P23860 |
| STA | AX1+1 | | | | | | S1P23870 |
| AXT | 6,1 | | | | | | S1P23880 |
| AXT | 0,2 | | | | | | S1P23890 |
| CLA | AXLRL+6,1 | | | | | | S1P23900 |
| STO | **2 | | | | | | S1P23910 |
| TNX | *+2,1,1 | | | | | | S1P23920 |
| TXI | AX1,2,1 | | | | | | S1P23930 |
| AXT | **1 | | | | | | S1P23940 |
| AXT | **2 | | | | | | S1P23950 |
| TRA | 7,4 | | | | | | S1P23960 |
| ORDJ | BCI | 6, | | | U | | S1P23970 |
| ORDV | BCI | 6, | | | V | | S1P23980 |
| ORDW | BCI | 6, | | | W | | S1P23990 |
| ORDNX | BCI | 6, | | | NPHI | | S1P24000 |
| ORDNT | BCI | 6, | | | NTHETA | | S1P24010 |
| ORDMX | BCI | 6, | | | MPHI | | S1P24020 |
| ORDMT | BCI | 6, | | | MTHETA | | S1P24030 |
| ORDN | BCI | 6, | | | NTAN | | S1P24040 |
| ORDNB | BCI | 6, | | | NNORM | | S1P24050 |
| ORDQ | BCI | 6, | | | Q | | S1P24060 |
| ORDM | BCI | 6, | | | M | | S1P24070 |
| ARLRL | BCI | 6, | | | THETA | | S1P24080 |
| AXLRL | BCI | 6, | | | PHI | | S1P24090 |
| DTCD | BCI | 9, | | | FIG. | SPHERF DISPLACEMENT COMPONENTS | S1P24100 |
| STRSS | BCI | 9, | | | FIG. | SPHERE STRESS RESULTANTS | S1P24110 |
| BON | BCI | 9, | | | FIG. | BOUNDARY STRESS RESULTANTS | S1P24120 |
| | END | | | | | | S1P24130 |


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C AT WHICH IDENTIFYING SYMBOLS ARE TO BE PLACED
C IF NEND = 0, OTHER GRAPHS ARE TO FOLLOW
C IF NEND = 1, CURRENT GRAPH IS THE LAST
C IF NFLAG = 0, CONTROL WILL BE RETURNED TO CHAIN (1,3)
C IF NFLAG = 1, RUN WILL BE TERMINATED BY CALL EXIT
DIMENSION XP(200),YP(200,4),ABLRL(6),ORDLRL(6),GPHLRL(9),
1 CILRL(6,4),RECORD(12),YT(200)
EQUIVALENCE (KR,FR), (XXN, NFRR)
KP=15
REWIND KP
XXN=255151606060
NEND=0
20 READ TAPE KP, RECORD
READ TAPE KP, NXP, NCRVS, NPTS, NEND, NFLAG
READ TAPE KP, ABLRL, ORDLRL, GPHLRL
READ TAPE KP, CILRL
DO 32 KT = 1,NXP
32 READ TAPE KP, XP(KT)
DO 33 L = 1,NCRVS
DO 33 KT = 1,NXP
READ TAPE KP, YT(KT)
33 YP(KT,L) = YT(KT)
READ TAPE KP,FR
BACKSPACE KP
IF (KR-NERR) 61, 60, 61
60 NEND=1
61 CONTINUE
CALL PLOTS(NXP,NCRVS,NPTS,NEND,NFLAG,XP,YP,RECORD,AELBL,ORDLRL,
1 GPHLRL,CILRL)
IF(NEND)20,20,21
21 IF(NFLAG)40,40,41
40 CALL CHAIN (1,2)
41 CALL EXIT
END
*
FORTRAN
SUBROUTINE PLOTS(NXP,NCRVS,NPTS,NEND,NFLAG,X,Y,RECORD,ABLRL,
1 ORDLRL,GPHLRL,CILRL)
C SC 4020 ROUTINE FOR PLOTTING SEVERAL CURVES ON A SINGLE GRAPH
C INDEX (1280)

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S1P24530
S1P24540
S1P24550
S1P24560
S1P24570
S1P24580
S1P24590
S1P24600
S1P24610
S1P24620
S1P24630
S1P24640
S1P24650
S1P24660
S1P24670
S1P24680
S1P24690
S1P24700
S1P24710
S1P24720
S1P24730
S1P24740
S1P24750
S1P24760
S1P24770
S1P24780
S1P24790
S1P24800
S1P24810
S1P24820
S1P24830
S1P24840
S1P24850
S1P24860
S1P24870
S1P24880
S1P24890
S1P24900
S1P24910

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DIMENSION X(200),Y(200,4),ABLBL(6),ORDLBL(6),GPHLBL(6),RECORD(12)SIP24920
DIMENSION KX1(4),KY1(4),KX2(4),CILRL(6,4),CLBL(6),SIP24930
1 ORDL(6),GPHL(6),YP(200),MRK(4)SIP24940
WRITE OUTPUT TAPE 6,10SIP24950
10 FORMAT(15H0 PLOT CALLED )SIP24960
F TABLIVSIP24970
CALL CAMRAV(9)SIP24980
XL = X(1)SIP24990
XR = X(1)SIP25000
DO 20 I = 2,NXP
XL = MINIF(XL,X(I))SIP25010
20 XR = MAXIF(XR,X(I))SIP25020
DC = 20.0SIP25030
CALL DXDYV(1,XL,XR,DX,N,II,NX,DC,IERR)SIP25040
KX1(1) = 185SIP25050
KX1(2) = 185SIP25060
KX1(3) = 585SIP25070
KX1(4) = 585SIP25080
KY1(1) = 985SIP25090
KY1(2) = 955SIP25100
KY1(3) = 985SIP25110
KY1(4) = 955SIP25120
KX2(1) = 200SIP25130
KX2(2) = 200SIP25140
KX2(3) = 600SIP25150
KX2(4) = 600SIP25160
MRK(1) = 38SIP25170
MRK(2) = 55SIP25180
MRK(3) = 63SIP25190
MRK(4) = 53SIP25200
YB = 0.0SIP25210
YT = 0.0SIP25220
DO 40 J = 1,NCRVS
DO 40 I = 2,NXP
YR = MINIF(YR,Y(I,J))SIP25230
40 YT = MAXIF(YT,Y(I,J))SIP25240
YR = YR*.10SIP25250
YT = YT*.10SIP25260
L = 1SIP25270
SIP25280
SIP25290
SIP25300

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```

CALL DXDYV(2,YR,YT,DY,M,JJ,NY,DC,IERR1)
NX = + 3
NY=-2
II = -II
JJ = -JJ
CALL SETMIV(100,10,70,100)
CALL GRIDIV(L,XL,XR,YR,YT,DX,DY,N,M,II,JJ,NX,NY)
DO 60 K = 1,6
60 ORDL(K) = ORDLBL(K)
CALL CHS17V(2,2)
CALL RITSTV(12,18,TAPLIV)
CALL RITE2V(75,330,1023,180,1,36,1,OPDL,NLAST)
CALL RITE2V(330,57,1023,90,1,36,1,ARLBL,NLAST)
CALL PRINTV(72,RECORD,100,1015)
DO 61 K = 1,9
61 GPHL(K) = GPHLBL(K)
CALL CHSIZV(3,4)
CALL RITSTV(18,30,TARLIV)
CALL RITE2V(40,20,1023,90,2,54,1,GPHL,NLAST)
DO 70 J = 1,NCRVS
YP(I) = Y(I,J)
NX1 = NXV(X(I))
NY1 = NYV(YP(I))
DO 50 I = 1,NXP
YP(I) = Y(I,J)
NX2 = NXV(X(I))
NY2 = NYV(YP(I))
IF(NX2*NY2)45,50,45
45 CALL LINEV(NX1,NY1,NX2,NY2)
NX1 = NX2
NY1 = NY2
50 CONTINUE
MRKPT = MRK(J)
CALL APLQTV(NXP,X,YP,NPTS,NPTS,1,MRKPT,IERR)
KX = KX1(J)
KY = KY1(J)
NS = J
CALL POINTV(KX,KY,NS,ANY)
KXC = KX2(J)

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S1P25310
S1P25320
S1P25330
S1P25340
S1P25350
S1P25360
S1P25370
S1P25380
S1P25390
S1P25400
S1P25410
S1P25420
S1P25430
S1P25440
S1P25450
S1P25460
S1P25470
S1P25480
S1P25490
S1P25500
S1P25510
S1P25520
S1P25530
S1P25540
S1P25550
S1P25560
S1P25570
S1P25580
S1P25590
S1P25600
S1P25610
S1P25620
S1P25630
S1P25640
S1P25650
S1P25660
S1P25670
S1P25680
S1P25690

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S1P25700
S1P25710
S1P25720
S1P25730
S1P25740
S1P25750
S1P25760
S1P25770
S1P25780
S1P25790

```
DO 93 K = 1,6
93 CLRL(K) = CILBL(K,J)
92 CALL PRINTV(36,CLRL,KXC,KY)
70 CONTINUE
  IF(NEND)90,90,91
91 CALL FOFTV
  WRITE OUTPUT TAPE 6,80
80 FORMAT(22H0 PLOTTING COMPLETED )
90 RETURN
  END
```