

18 July 1966

RSIC-578

**AN EXPERIMENT ON THE QUANTITATIVE DESCRIPTION  
OF CLIMATIC ELEMENT FIELD BY ORTHOGONAL  
FUNCTIONS**

by  
Shih Yung-nien

Acta Meteorologica Sinica, 35, No. 3, 343-351 (1965)  
Translated from the Chinese

**DISTRIBUTION OF THIS DOCUMENT IS UNLIMITED**

Translation Branch  
Redstone Scientific Information Center  
Research and Development Directorate  
U. S. Army Missile Command  
Redstone Arsenal, Alabama 35809

## ABSTRACT

In this paper, the author first proposes the generalized problem of the quantitative description of climatic field by means of approximate analytic expression. It is submitted that the application of the linear combination of orthogonal functions in approximate expression has many advantages. A formula to measure the precision of the calculation is also proposed. Two calculated examples are given.

---

## I. INTRODUCTION

In the theory of climatology, for the study of the relations between the various climate-forming factors and the climatic element field, how to describe objectively and quantitatively the space time distribution of these factors and the elements is a very important basic problem.

Obviously, although the raw data and the contour maps from various stations are objective, they are not very convenient to handle theoretically, and therefore difficult to be applied directly. The average values or other indices obtained from the raw data or the contour maps frequently do not contain enough details to represent the characteristics of the distribution; some of them even lose all their representative values. Therefore, the most ideal method is to find an analytical expression represented by a mathematical function  $\hat{f}_n(x, y, z; t)$  to approximately describe quantitatively, according to our required accuracy, the climatic element field  $f(x, y, z; t)$ , the expression of which is not known but which exists objectively.

From the viewpoint of the statistical theory of climatology, such a problem is just the problem of finding the regression. However, if the method of solving a set of normal equations is used, it becomes very tedious even for finding the regression of one variable along a curve. Furthermore, if it is found that the calculated result is not satisfactory enough according to the required accuracy and terms have to be added, all the coefficients must be recalculated. As to the regression on a surface in a multidimensional space, it is of course a very tedious matter.

If the orthogonal functions in mathematics are used, we could avoid or lessen the defects and difficulties mentioned above. Also, a most advantageous choice of the set of orthogonal functions can be made (to simplify the equations and hasten the convergence) for each different problem. It is just because of this that there exist already many

examples in meteorology in which use is made of the linear combinations of orthogonal functions to describe quantitatively the element field, such as: use of trigonometric functions to perform harmonic analysis of the atmospheric temperature and the earth temperature<sup>1,2</sup> and use of equidistant point orthogonal polynomials to represent the longitudinal distribution<sup>4,5,6</sup> of the elements or climatic-forming factors. All these examples belong to the application of one-dimensional orthogonal functions to describe the time variation or the one-dimensional spatial distribution of climatic elements. Also, two-dimensional orthogonal functions such as the spherical functions<sup>7</sup>, the two-dimensional equidistant point orthogonal polynomials<sup>8,9,10,11,12</sup>, the mixed functions<sup>12</sup> of trigonometric functions and orthogonal polynomials have already been applied to describe the horizontal distribution of the element field or the climate-forming factors. In the series of papers by E. N. Blinova, spherical functions or the mixed functions<sup>13</sup> of the trigonometric functions and spherical functions are often used to describe the spatial distribution and the time variation of the climate elements and its formation factors.

## II. THE TENDENCY OF THE CLIMATIC VARIATION OF THE AVERAGE HIGHEST TEMPERATURES

According to the opinion of S. K. Pramanik et al.<sup>3</sup>, for the study of the tendency of climatic variation of temperature, it is best to obtain the separate equations for the variation curves of the highest and lowest temperatures. To confirm whether the variation from year to year is purely accidental or it may include some regular variation, the method of inflection point can first be used to perform random tests with respect to the series of the highest or the lowest temperatures. From the results of random tests by the inflection point method on the series of highest daily temperatures (averaged over many years) and of the lowest daily temperatures (averaged over many years) as recorded by the eight stations which are distributed over the entire country and which have records over long periods of time, only the continuous series of average highest temperatures of Shanghai (1904-1958, a total of 55 years) and of the average highest temperature of Shen-Yang (1906-1940, a total of 35 years) are not random. This is to say that although one can use mathematical methods coupled with the method of least square to obtain an equation for the tendency curves, these curves have no practical meaning since the rise and fall of the annual average of the highest or the lowest temperatures may be purely accidental. Therefore, we shall only obtain the tendency variation curve for the two series which are not random in nature.

Here, the climatic element field under consideration is only a one-dimensional function of time and the values of  $t$  taken are discrete and equidistant. Clearly, the best choice of the set of orthogonal functions shall be one-dimensional, equidistant point orthogonal polynomials.

According to R. A. Fisher's method<sup>15</sup>: let  $N$  be the number of equidistant points (the number of years for the series of temperatures). When  $N$  is odd, the year in the middle can be taken as the origin ( $t = 0$ ). With an increase or a decrease of one year,  $t$  also increases or decreases by 1. When  $N$  is even, the two middle years can be taken respectively as  $t = -1/2$  and  $t = +1/2$ ;  $t$  increases or decreases by 1 with the increase or decrease of one year. When the coordinate of  $t$  is chosen in this manner, the normalized, one-dimensional equidistant point orthogonal polynomials  $\Phi_\nu(t)$  can be expressed as

$$\Phi_\nu(t) = \frac{P_\nu(t)}{\sqrt{\sum_{t = \frac{1-N}{2}}^{\frac{N-1}{2}} P_\nu^2(t)}} \quad (1)$$

where

$$\left. \begin{aligned} P_0(t) &= 1, \\ P_1(t) &= t, \\ P_2(t) &= t^2 - \frac{N^2 - 1}{12}, \\ P_3(t) &= t^3 - \frac{3N^2 - 7}{20} t, \\ &\dots\dots\dots \end{aligned} \right\} \quad (2)$$

In general, there is the recursion formula:

$$P_{r+1}(t) = P_1(t) P_r(t) - \frac{r^2(N^2 - r^2)}{4 \times (4r^2 - 1)} P_{r-1}(t) \quad (3)$$

and the formulae:

$$\begin{aligned}
 & \sum_{t = \frac{1-N}{2}}^{\frac{N-1}{2}} P_0^2(t) = N, \\
 & \sum_{t = \frac{1-N}{2}}^{\frac{N-1}{2}} P_1^2(t) = \frac{N(N^2 - 1)}{12}, \\
 & \sum_{t = \frac{1-N}{2}}^{\frac{N-1}{2}} P_2^2(t) = \frac{N(N^2 - 1)(N^2 - 4)}{180}, \\
 & \sum_{t = \frac{1-N}{2}}^{\frac{N-1}{2}} P_3^2(t) = \frac{N(N^2 - 1)(N^2 - 4)(N^2 - 9)}{2800}, \\
 & \dots\dots\dots
 \end{aligned}
 \tag{4}$$

In general, one has

$$\sum_{t = \frac{1-N}{2}}^{\frac{N-1}{2}} P_r^2(t) = \frac{(N-1)^{(r)} (N+r)^{(r+1)}}{(2r+1) \binom{2r}{r}^2},
 \tag{5}$$

where

$$(N-1)^{(r)} = (N-1)(N-2)\dots(N-r+1)(N-r),$$

$$(N+r)^{(r+1)} = (N+r)(N+r-1)\dots(N+2)(N+1)N,$$

$$\binom{2r}{r}^2 = \left[ \frac{(2r)!}{r!r!} \right]^2.$$

The values of  $P_\nu(t)$  and  $\sum_t P_\nu^2(t)$  which vary with the values of  $N$ ,  $\nu$ ,  $t$  can be found from tables<sup>16</sup>. Therefore, it is very convenient to find the coefficient  $C_\nu$  ( $\nu = 0, 1, 2, \dots$ ):

$$C_\nu = \sum_{t = \frac{1-N}{2}}^{\frac{N-1}{2}} T_M(t) \phi_\nu(t) . \quad (6)$$

where  $T_M(t)$  denotes the annual average highest temperatures in the series.

When  $n$  is fixed,

$$\hat{T}_{Mn}(t) = \sum_{\nu=0}^n C_\nu \phi_\nu(t) . \quad (7)$$

which is the best quantitative description of the highest temperature series in the sense of least squares. It represents the parabolic tendency of the climatic variation of the highest temperatures.

The  $\rho_n$  defined below can be taken as the degree of accuracy when  $\hat{T}_{Mn}(t)$  is used to describe  $T_M(t)$ :

$$\rho_n^2 = \frac{\sum_{\nu=1}^n C_\nu^2}{N\sigma^2} \quad (8)$$

where  $\sigma^2$  is the squared difference of the  $T_M(t)$  series.

From the statistical point of view,  $\rho_n$  is actually the related index of  $T_M(t)$  relative to the tendency curve  $\hat{T}_{Mn}(t)$ . The advantages of adopting the related index  $\rho_n$  as degree of accuracy are that its meaning is clear and that it is convenient for calculation. Substituting the  $C_\nu$  ( $\nu = 1, 2, \dots, n$ ) already obtained into Equation (8), one can obtain  $\rho_n$  very quickly. When  $\hat{T}_{Mn}(t)$  and  $T_M(t)$  are completely the same,  $\rho_n = 1$ . The closer  $\hat{T}_{Mn}(t)$  is to  $T_M(t)$ , the closer is  $\rho_n$  to 1. On the other hand, if the required accuracy  $\rho_n$  is first given, then the  $C_1, C_2, \dots, C_n$  which are found by steps can be substituted into Equation (8) until the requirement is satisfied. Then,  $n$  is the most appropriate number of terms.

From  $\rho_n^2$  the standard deviation  $S$  can be found when  $\hat{T}_{Mn}(t)$  is used to describe  $T_M(t)$  quantitatively:

$$S = \sigma \sqrt{1 - \rho_n^2} \quad (9)$$

In addition, the method of the analysis of difference square can be used to test the distinguishability of the analytic expression which is obtained and used for quantitative description. Here, the difference square ratio  $F$  can be calculated with the formula below:

$$F = \frac{\frac{\rho_n^2}{n}}{\frac{1 - \rho_n^2}{N - n - 1}} \quad (10)$$

The degree of freedom of  $F$  is:  $(n, N - n - 1)$ .

Calculated results:

(1) Shen-yang (1906-1940)

The squared difference of the annual average highest temperature series:  $\sigma^2 = (0.67^\circ\text{C})^2$ .

Coefficient  $C_v$

$C_0$	$C_1$	$C_2$	$C_3$
81.0	1.95	-0.428	0.063

On substituting the  $C_v$  values from the above table and the  $\phi_v(t)$  of Equation (1) into Equation (7), and on combining terms of the same power, the tendency equation can be obtained:

$$\hat{T}_{M3}(t) = 13.8 + 0.0132t - 0.000795t^2 + 0.0000159t^3 \quad (11)$$

The related index  $\rho_n$  calculated according to Equation (8) can then be used to examine how close the tendency equation is to the original series:

$$\rho_3^2 = \frac{1.95^2 + 0.428^2 + 0.063^2}{35 \times 0.67^2} = 0.26 \quad .$$

i. e. :

$$\rho_3 = 0.51$$

The related index of the original series relative to the cubic parabola (11) is 0.51. It is clearly seen that  $C_1$  contributes most to the related index. If the tendency equation is taken to be:

$$\hat{T}_{M1}(t) = C_0 \phi_0(t) + C_1 \phi_1(t) = 13.7 + 0.0326t. \quad (12)$$

then the related index can also reach:

$$\rho_1 = \sqrt{\frac{1.95^2}{35 \times 0.67^2}} = 0.49 \quad .$$

According to Equation (19), when Equation (11) is used to describe the original series, the standard deviation can be calculated:

$$S = 0.67 \times \sqrt{1 - 0.26} = 0.576^\circ\text{C} \quad .$$

According to Equation (10), the difference square ratio is calculated to be:

$$F = \frac{\frac{0.26}{3}}{\frac{1 - 0.26}{35 - 3 - 1}} = 3.63 \quad .$$

If the distinguishability level is taken to be 5 percent, then the critical F value for the degree of freedom (3, 31) is:  ${}^{16}F^* = 2.91$ . Therefore, it is at least 95 percent sure that one can consider the agreement in Equation (11) as non-random.

## (2) Shanghai (1904-1958)

The squared difference of the annual average highest temperature series:  $\sigma^2 = (0.74^\circ\text{C})^2$ .



### Coefficient C

$C_0$	$C_1$	$C_2$	$C_3$
154.9	0.735	-3.32	1.89

On substituting  $C_v$  into Equation (7), the tendency equation can be obtained:

$$\hat{T}_{M3}(t) = 21.4 + 0.0511t - 0.00199t^2 - 0.0000979t^3 \quad (13)$$

The related index:

$$\rho_3 = \sqrt{\frac{0.735^2 + 3.32^2 + 1.89^2}{55 \times 0.74^2}} = 0.71 \quad .$$

Therefore, Equation (13) agrees even better with the original series than the corresponding case of Shen-yang. However, in the related index the main contributions come from the coefficients of the quadratic and cubic terms. Therefore, in the tendency equation for the climatic variation of highest temperatures of Shanghai, the quadratic and the cubic terms have to be considered. If only the linear term is considered, the related index is:

$$\rho_1 = \sqrt{\frac{0.735^2}{55 \times 0.74^2}} = 0.13 \quad .$$

If the consideration stops at the quadratic term, the related index is:

$$\rho_2 = \sqrt{\frac{0.735^2 + 3.32^2}{55 \times 0.74^2}} = 0.62 \quad .$$

The standard deviation of Equation (13) is:

$$S = 0.74 \times \sqrt{1 - 0.71^2} = 0.52^\circ\text{C}.$$

The ratio of the squared difference is:

$$F = \frac{\frac{0.71^2}{3}}{\frac{1 - 0.71^2}{55 - 3 - 1}} = 17.2$$

This F value greatly exceeds the critical<sup>16</sup> F\* value for a 0.1 percent distinguishability level and a degree of freedom of (3, 51). Therefore, it is more than 99.9 percent sure to consider the arrangement in the tendency Equation (13) as a non-random. In the figures, the broken lines represent the actual series of annual average highest temperatures of Shen-yang and Shanghai. From the figures, it can be seen that the tendency curve for Shen-yang is very close to being a straight line while the tendency curve for Shanghai obviously possesses the characteristics of a cubic parabola. From the calculations of the related indices we have already confirmed these facts.

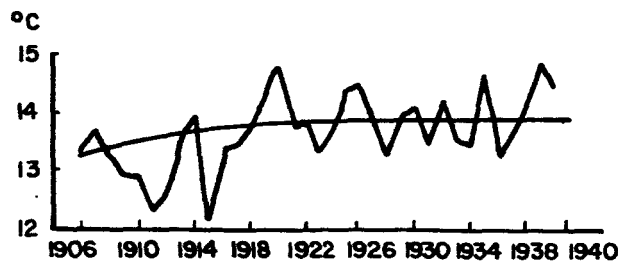


Figure 1. The Variation Tendency of the Annual Average Highest Temperatures of Shen-yang

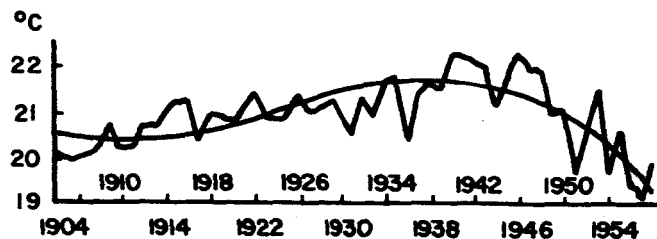


Figure 2. The Variation Tendency of the Annual Average Highest Temperatures of Shanghai.

Judging from these two curves, it is seen that, from the year 1905 to the year 1940, both Shen-yang and Shanghai have the temperature-rising tendency. From the tendency curve for Shanghai, it is seen that, beginning from the forties, there is a temperature falling tendency. The characteristics of these tendency curves are consistent with the conclusion obtained by Wang P'eng-fei<sup>17</sup>(3679 7720 7378) who used other methods to study the climatic variations of our country in the last hundred years.

### III. QUANTITATIVE DESCRIPTION OF THE TEMPERATURE FIELD ALONG THE COAST OF CHINA

In the equal-area projection map of Albers', the rectangular domain as shown in Figure 3 is chosen to be the object of description. The domain can be divided into  $14 \times 20$  squares by  $15 \times 21$  grid points. The coordinate of each grid point is  $(x, y)$ ,  $x$  taking on values from 0, 1, 2, ... to 14,  $y$  taking on values from 0, 1, 2, ... to 20. (See Figure 3.)

Based on data<sup>19</sup>, the temperature contour map for January and July of that district is made. At each grid point, the temperature  $T(x, y)$  of the corresponding month can be read off.

Let  $X_r(x)$  be the normalized, equidistant point orthogonal polynomial of degree  $r$  for 15 points,  $Y_s(y)$  be that for 21 points:

$$\left. \begin{aligned}
 X_r(x) &= \frac{\sum_{i=0}^r (-1)^i \binom{r}{i} \binom{r+i}{i} \frac{(x)^{(i)}}{(14)^{(i)}}}{\frac{(14+r+1)^{(r+1)}}{(2r+1)(14)^{(r)}}}, \\
 Y_s(y) &= \frac{\sum_{i=0}^s (-1)^i \binom{s}{i} \binom{s+i}{i} \frac{(y)^{(i)}}{(20)^{(i)}}}{\frac{(20+s+1)^{(s+1)}}{(2s+1)(20)^{(s)}}}
 \end{aligned} \right\} \cdot \quad (14)$$

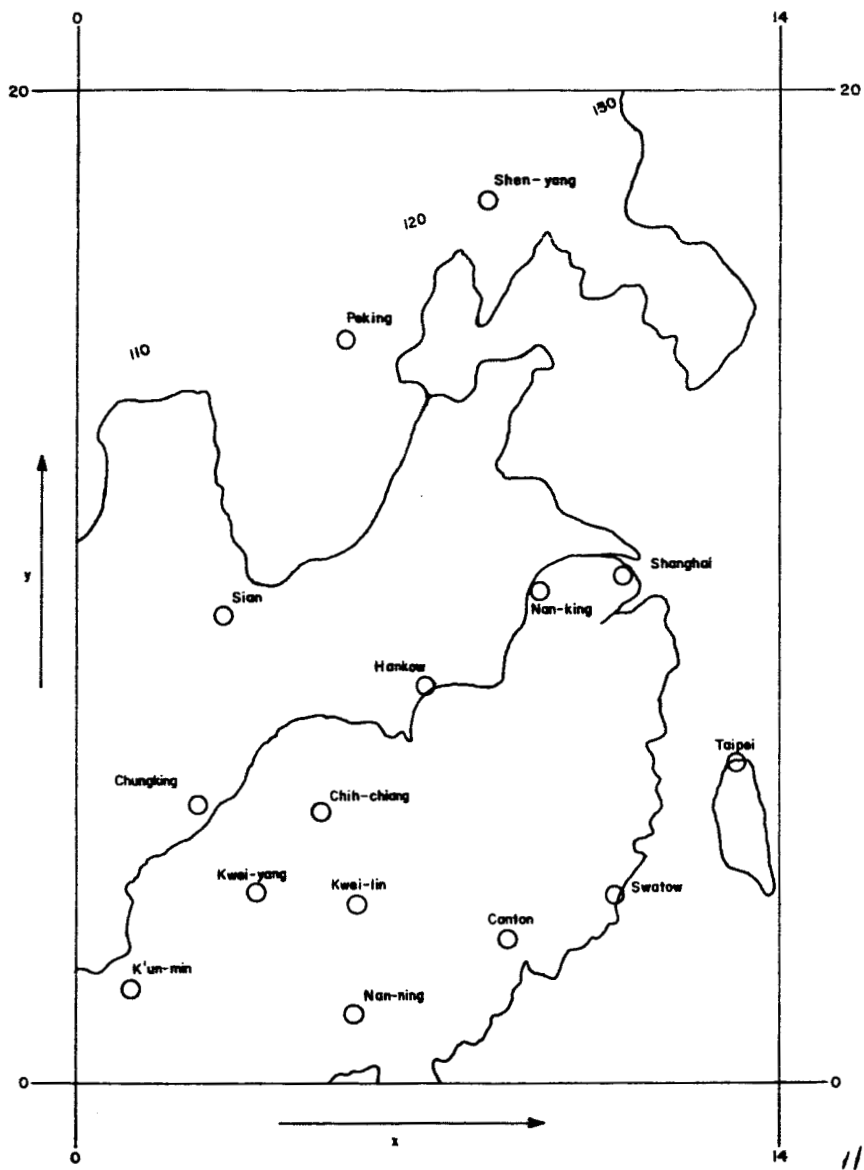


Figure 3. The Domain and the Coordinates of the Quantitatively Described Temperature Field.

where

$$(x)^{(i)} = x(x-1)\dots(x-i+1),$$

$$(14)^{(i)} = 14 \times 13 \times \dots \times (14-i+1),$$

$$(14+r+1)^{(r+1)} = (14+r+1)(14+r)\dots(14+1),$$

$$(14)^{(r)} = 14 \times 13 \times \dots \times (14-r+1).$$

Similarly for the rest. Their product  $X_r(x) Y_s(y)$  is then a normalized orthogonal polynomial of degree  $(r+s)$  which is orthogonal at  $15 \times 21$  grid points. From this, we can obtain the equation which describes quantitatively the temperature distribution of the corresponding month:

$$\hat{T}(x, y) = \sum_{r=0}^l \sum_{s=0}^m a_{rs} X_r(x) Y_s(y). \quad (15)$$

where the coefficient of each term is:

$$a_{rs} = \sum_{x=0}^{14} \sum_{y=0}^{20} T(x, y) X_r(x) Y_s(y). \quad (16)$$

The formula for calculating the related index  $\rho_n$  is now reduced to become:

$$\rho_n^2 = \frac{\sum_{r=0}^l \sum_{s=0}^m a_{rs}^2 - a_{00}^2}{\sum_{x=0}^{14} \sum_{y=0}^{20} T^2(x, y) - \frac{1}{15 \times 21} \left( \sum_{x=0}^{14} \sum_{y=0}^{20} T(x, y) \right)^2} \quad (17)$$

From the contour maps, the  $T(x, y)$  value at each grid point can be read off. According to Equation (16), and also by using the numerical table<sup>16</sup>, the  $a_{rs}$  value, the equation for quantitative description, the related index  $\rho_n$  of the raw data relative to the equation, the standard deviation  $S$  and the ratio of difference square can be obtained for January and July, respectively, as follows:

(1) January

$a_{rs}$  Value

$a_{00}$	$a_{10}$	$a_{01}$	$a_{20}$	$a_{11}$
31.08	-105.24	162.94	17.64	22.67
$a_{02}$	$a_{30}$	$a_{21}$	$a_{12}$	$a_{03}$
3.48	- 6.25	3.90	11.25	10.18

Equation for quantitative description:

$$\begin{aligned} \hat{T}(x, y) = & 1.94 + 0.17x - 0.14y - 0.000567x^2 + 0.000666xy \\ & + 0.0000114y^2 + 0.0000605x^3 - 0.0000024x^2y \\ & + 0.0000034xy^2 + 0.0000117y^3 . \end{aligned} \quad (18)$$

According to Equation (17), the related index of the raw data relative to Equation (18) is:

$$\rho_9 = \sqrt{\frac{105.24^2 + 162.94^2 + \dots + 10.18^2}{40925.76}} = 0.97$$

Standard deviation:

$$S = \sqrt{\frac{40925.76^2 \times (1 - 0.97^2)}{15 \times 21}} = 2.6^\circ\text{C} .$$

Ratio of difference square:

$$F = \frac{\frac{0.97^2}{9}}{\frac{1 - 0.97^2}{15 \times 21 - 9 - 1}} = 591.1 .$$

(2) July

$a_{rs}$  Value

$a_{00}$	$a_{10}$	$a_{01}$	$a_{20}$	$a_{11}$
456.75	-21.10	26.33	-20.95	-9.34
$a_{02}$	$a_{30}$	$a_{21}$	$a_{12}$	$a_{03}$
-20.17	- 7.96	-5.92	- 4.35	-1.87

Equation for quantitative description:

$$\begin{aligned} \hat{T}(x, y) = & 25.65 + 0.0529x - 0.0197y - 0.00251x^2 - 0.000390xy \\ & - 0.000256y^2 + 0.0000799x^3 + 0.00000392x^2y \\ & + 0.00000113xy^2 + 0.00000214y^3 \quad . \end{aligned} \quad (19)$$

The related index of raw data relative to Equation (19):

$$\rho_9 = \sqrt{\frac{21.10^2 + 26.33^2 + \dots + 1.87^2}{1938.80}} = 0.86 \quad .$$

Standard deviation:

$$S = \sqrt{\frac{1938.80 \times (1 - 0.86^2)}{15 \times 21}} = 1.54^\circ\text{C} \quad .$$

Ratio of difference square:

$$F = \frac{\frac{0.86^2}{9}}{\frac{1 - 0.86^2}{15 \times 21 - 9 - 1}} = 99.1 \quad .$$

By comparing the F value obtained above with the critical F\* value<sup>16</sup> for a 0.1 percent distinguishability level and a (9, 305) degree of freedom, it is found that in both January and July, the F value greatly exceeds F\*. Therefore, it may be considered that Equations (18) and (19) do not come about randomly.

In addition, from the  $a_{rs}$  value for January, it can be seen that the linear term is largely dominant. In fact, if only the linear term is considered:

$$\begin{aligned} \hat{T}(x, y) &= a_{00}X_0(x)Y_0(y) + a_{10}X_1(x)Y_0(y) + a_{01}X_0(x)Y_1(y) \\ &= 1.90 + 0.182x - 0.145y. \end{aligned} \quad (20)$$

Then the related index of the raw data relative to this descriptive Equation (20) is:

$$\rho_2 = \sqrt{\frac{105.24^2 + 162.94^2}{40925.76}} = 0.95$$

Hence the temperature distribution of January basically can be considered as a linear function of the horizontal coordinates (x, y).

However, with July it is another matter. From the  $a_{rs}$  value, it can be seen that the contribution of the quadratic term is of the same order as the contribution of the linear term. Even the cubic terms also make significant contribution. This demonstrates that in July, the temperature distribution along our coastal areas is much more complicated than that in January.

To confirm the correctness of the Equations (19) and (20) for quantitative description, the temperatures at various points were calculated according to the equations, and temperature contour maps were then made. The result thus obtained was very close to the original temperature contour maps.

Discussed above are just two examples in which the one-dimensional and two-dimensional equidistant point orthogonal polynomials are used for quantitative description.

For different purposes, the experiment of using various orthogonal sets of functions for quantitative description of the climatic element field is still being carried out, the results of which will be published later.

**Acknowledgements:** The stimulus and encouragement from my adviser, Professor Mo Chen-sheng (7803 2650 3932) enabled the author to complete the present work. Certain parts of the calculations in the



two practical examples were carried out, based on data in the theses of my fellow students Chiang Yen-hsia (5592 3601 7209) (1962) and Ts'ao Yung-hua (2580 3057 5478) (1963) in the Department. To all of them, the author wishes to express his thanks here.

## LITERATURE CITED

1. Mo Chen-sheng (7803 2650 3932), Ti-li Hsueh-pao (Acta Geographica Sinica) 18 (1944) 126-128.
2. Mo Chen-sheng (7803 2650 3932), Ch'i-hsiang Hsueh-pao (Acta Meteorologica Sinica) 21 (1950), 69-78.
3. Pramanik, S. K. and Jagannathan, P., Scientific Proceedings of the International Association of Meteorology, 1956, 86-138.
4. Dobryshman, E. M. Met i Gid. (Met. and Hyd.), 1956, 12, 18-25.
5. Rakipova, L. R., Trudy GGO (Works of Main Geophysical Observatory), No. 47 (103), (1953).
6. Rakipova, L. R., Teplovoi Rezhim Atmosferi (Thermal Regime Atmosphere) (1957).
7. Data Forecast Group, Scientific Research Division, Central Bureau of Meteorology, Ch'i-hsiang Hsueh-pao (Acta Meteorologica Sinica) 30 (1959), 405-413.
8. Chang Chia-ch'eng (1728 1367 6134), Chou Chia-pin (0719 1367 2430), Huang Wen-chieh (7806 2429 2638), Wu Wei-hua (3527 4850 5478), Ch'i-hsiang Hsueh-pao, 33 (1963), 231-243.
9. Bagrov, N. A., Trudy TsIPa (Work of Central Institute of Weather Forecasting), 64 (1957), 3-25.
10. Zverev, N. I., Trudy TsIPa, 85 (1959), 27-39.
11. Cihak, K., Arch. für Geophy. Met. und Biok., S. A., 12 (1960), 40-61.
12. Hare, F. K., Polar Atmosphere Symposium, Part 1. Meteorology Section (1958), 137-150.
13. Blinova, E. N., Trudy In-Ta Fiz Atm., AN SSSR, No. 2 (1958), 5-22.
14. Kendall, M. G., "Advanced Theory of Statistics," (II), Charles Griffin, 1946.
15. Fisher, R. A., "Statistical Methods for Research Workers," 11th ed., Oliver and Boyd, 1950.

16. Fisher, R. A. and Yates, F., "Statistical Tables for Bio., Agri. and Med. Research," 5th ed., Oliver and Boyd, 1957.
17. Wang P'eng-fei (3769 7720 7378), Tien-ch'i Yueh-k'an (Monthly Weather Journal), No. 3 (1958), 25-29.
18. "Climatic Atlas of Japan and Her Neighboring Countries," Tokyo, Gen. Met. Obs., 1943.

## DISTRIBUTION

	No. of Copies		No. of Copies
<u>EXTERNAL</u>			
Air University Library ATTN: AULST Maxwell Air Force Base, Alabama 36112	1	U. S. Atomic Energy Commission ATTN: Reports Library, Room G-017 Washington, D. C. 20545	1
U. S. Army Electronics Proving Ground ATTN: Technical Library Fort Huachuca, Arizona	1	U. S. Naval Research Laboratory ATTN: Code 2027 Washington, D. C. 20390	1
U. S. Naval Ordnance Test Station ATTN: Technical Library, Code 753 China Lake, California 93555	1	Weapons Systems Evaluation Group Washington, D. C. 20305	1
U. S. Naval Ordnance Laboratory ATTN: Library Corona, California 91720	1	John F. Kennedy Space Center, NASA ATTN: KSC Library, Documents Section Kennedy Space Center, Florida 32899	2
Lawrence Radiation Laboratory ATTN: Technical Information Division P. O. Box 808 Livermore, California	1	APGC (PGBPS-12) Eglin Air Force Base, Florida 32542	1
Sandia Corporation ATTN: Technical Library P. O. Box 969 Livermore, California 94551	1	U. S. Army CDC Infantry Agency Fort Benning, Georgia 31905	1
U. S. Naval Postgraduate School ATTN: Library Monterey, California 93940	1	Argonne National Laboratory ATTN: Report Section 9700 South Cass Avenue Argonne, Illinois 60440	1
Electronic Warfare Laboratory, USAECOM Post Office Box 205 Mountain View, California 94042	1	U. S. Army Weapons Command ATTN: AMSWE-RDR Rock Island, Illinois 61201	1
Jet Propulsion Laboratory ATTN: Library (TDS) 4800 Oak Grove Drive Pasadena, California 91103	2	Rock Island Arsenal ATTN: SWERI-RDI Rock Island, Illinois 61201	1
U. S. Naval Missile Center ATTN: Technical Library, Code N3022 Point Mugu, California	1	U. S. Army Cnd. & General Staff College ATTN: Acquisitions, Library Division Fort Leavenworth, Kansas 66027	1
U. S. Army Air Defense Command ATTN: ADSX Ent Air Force Base, Colorado 80912	1	Combined Arms Group, USACDC ATTN: Op. Res., P and P Div. Fort Leavenworth, Kansas 66027	1
Central Intelligence Agency ATTN: OCR/DD-Standard Distribution Washington, D. C. 20505	4	U. S. Army CDC Armor Agency Fort Knox, Kentucky 40121	1
Harry Diamond Laboratories ATTN: Library Washington, D. C. 20438	1	Michoud Assembly Facility, NASA ATTN: Library, I-MICH-OSD P. O. Box 29300 New Orleans, Louisiana 70129	1
Scientific & Tech. Information Div., NASA ATTN: ATS Washington, D. C. 20546	1	Aberdeen Proving Ground ATTN: Technical Library, Bldg. 313 Aberdeen Proving Ground, Maryland 21005	1
		NASA Sci. & Tech. Information Facility ATTN: Acquisitions Branch (S-AK/DL) P. O. Box 33 College Park, Maryland 20740	5
		U. S. Army Edgewood Arsenal ATTN: Librarian, Tech. Info. Div. Edgewood Arsenal, Maryland 21010	1

	No. of Copies		No. of Copies
National Security Agency ATTN: C3/TDL Fort Meade, Maryland 20755	1	Brookhaven National Laboratory Technical Information Division ATTN: Classified Documents Group Upton, Long Island, New York	1
Goddard Space Flight Center, NASA ATTN: Library, Documents Section Greenbelt, Maryland 20771	1	Watervliet Arsenal ATTN: SWEWV-RD Watervliet, New York 12189	1
U. S. Naval Propellant Plant ATTN: Technical Library Indian Head, Maryland 20640	1	U. S. Army Research Office (ARO-D) ATTN: CRD-AA-IP Box CM, Duke Station Durham, North Carolina	1
U. S. Naval Ordnance Laboratory ATTN: Librarian, Eva Liberman Silver Spring, Maryland 20910	1	Lewis Research Center, NASA ATTN: Library 21000 Brookpark Road Cleveland, Ohio 44135	1
Air Force Cambridge Research Labs. L. G. Hanscom Field ATTN: CRMCLR/Stop 29 Bedford, Massachusetts 01730	1	Systems Engineering Group (RTD) ATTN: SEPIR Wright-Patterson Air Force Base, Ohio 45433	1
Springfield Armory ATTN: SWESP-RE Springfield, Massachusetts 01101	1	U. S. Army Artillery & Missile School ATTN: Guided Missile Department Fort Sill, Oklahoma 73503	1
U. S. Army Materials Research Agency ATTN: AMCMR-ATL Watertown, Massachusetts 02172	1	U. S. Army CDC Artillery Agency ATTN: Library Fort Sill, Oklahoma 73504	1
Strategic Air Command (OAI) Offutt Air Force Base, Nebraska 68113	1	U. S. Army War College ATTN: Library Carlisle Barracks, Pennsylvania 17013	1
Picatinny Arsenal, USAMUCOM ATTN: SMUPA-VA6 Dover, New Jersey 07801	1	U. S. Naval Air Development Center ATTN: Technical Library Johnsville, Warminster, Pennsylvania 18974	1
U. S. Army Electronics Command ATTN: AMSEL-CB Fort Monmouth, New Jersey 07703	1	Frankford Arsenal ATTN: C-2500-Library Philadelphia, Pennsylvania 19137	1
Sandia Corporation ATTN: Technical Library P. O. Box 5800 Albuquerque, New Mexico 87115	1	Div. of Technical Information Ext., USAEC P. O. Box 62 Oak Ridge, Tennessee	1
ORA(RRRT) Holloman Air Force Base, New Mexico 88330	1	Oak Ridge National Laboratory ATTN: Central Files P. O. Box X Oak Ridge, Tennessee	1
Los Alamos Scientific Laboratory ATTN: Report Library P. O. Box 1663 Los Alamos, New Mexico 87544	1	Air Defense Agency, USACDC ATTN: Library Fort Bliss, Texas 79916	1
White Sands Missile Range ATTN: Technical Library White Sands, New Mexico 88002	1	U. S. Army Air Defense School ATTN: AKBAAS-DR-R Fort Bliss, Texas 79906	1
Rome Air Development Center (EMLAL-1) ATTN: Documents Library Griffiss Air Force Base, New York 13440	1		

	No. of Copies		No. of Copies
U. S. Army CDC Nuclear Group Fort Bliss, Texas 79916	1	<u>INTERNAL</u>	
Manned Spacecraft Center, NASA ATTN: Technical Library, Code RM6 Houston, Texas 77058	1	Headquarters U. S. Army Missile Command Redstone Arsenal, Alabama ATTN: AMSMI-D	1
Defense Documentation Center Cameron Station Alexandria, Virginia 22314	20	AMSMI-XE, Mr. Lowers	1
U. S. Army Research Office ATTN: STINFO Division 3045 Columbia Pike Arlington, Virginia 22204	1	AMSMI-XS, Dr. Carter	1
U. S. Naval Weapons Laboratory ATTN: Technical Library Dahlgren, Virginia 22448	1	AMSMI-Y	1
U. S. Army Engineer Res. & Dev. Labs. ATTN: Scientific & Technical Info. Br. Fort Belvoir, Virginia 22060	2	AMSMI-R, Mr. McDaniel	1
Langley Research Center, NASA ATTN: Library, MS-185 Hampton, Virginia 23365	1	AMSMI-RAP	1
Research Analysis Corporation ATTN: Library McLean, Virginia 22101	1	AMSMI-RBLD	10
U. S. Army Tank Automotive Center ATTN: SMTA-RIS.1 Warren, Michigan 48090	1	USACDC-LnO	1
Foreign Technology Division ATTN: Library Wright-Patterson Air Force Base, Ohio 45400	1	AMSMI-RBT	8
Clearinghouse for Federal Scientific and Technical Information U. S. Department of Commerce Springfield, Virginia 22151	1	AMSMI-RB, Mr. Croxton	1
Foreign Science & Technology Center, USAMC ATTN: Mr. Shapiro Washington, D. C. 20315	3	AMSMI-RRA, Dr. Essenwanger	1
		National Aeronautics & Space Administration Marshall Space Flight Center Huntsville, Alabama ATTN: MS-T, Mr. Wiggins	5

DOCUMENT CONTROL DATA - R&D		
<i>(Security classification of title, body of abstract and indexing annotation must be entered when the overall report is classified)</i>		
1. ORIGINATING ACTIVITY (Corporate author) Redstone Scientific Information Center Research and Development Directorate U. S. Army Missile Command Redstone Arsenal, Alabama 35809		2a. REPORT SECURITY CLASSIFICATION Unclassified
		2b. GROUP N/A
3. REPORT TITLE AN EXPERIMENT ON THE QUANTITATIVE DESCRIPTION OF CLIMATIC ELEMENT FIELD BY ORTHOGONAL FUNCTIONS Acta Meteorologica Sinica, 35, No. 3, 343-351 (1965)		
4. DESCRIPTIVE NOTES (Type of report and inclusive dates) Translated from the Chinese		
5. AUTHOR(S) (Last name, first name, initial)  Yung-nien, Shih		
6. REPORT DATE 18 July 1966	7a. TOTAL NO. OF PAGES 21	7b. NO. OF REFS 18
8a. CONTRACT OR GRANT NO. N/A b. PROJECT NO. N/A c. d.	9a. ORIGINATOR'S REPORT NUMBER(S)  RSIC-578	
9b. OTHER REPORT NO(S) (Any other numbers that may be assigned this report) AD _____		
10. AVAILABILITY/LIMITATION NOTICES Distribution of this document is unlimited.		
11. SUPPLEMENTARY NOTES  None	12. SPONSORING MILITARY ACTIVITY  Same as No. 1	
13. ABSTRACT In this paper, the author first proposes the generalized problem of the quantitative description of climatic field by means of approximate analytic expression. It is submitted that the application of the linear combination of orthogonal functions in approximate expression has many advantages. A formula to measure the precision of the calculation is also proposed. Two calculated examples are given.		

14. KEY WORDS	LINK A		LINK B		LINK C	
	ROLE	WT	ROLE	WT	ROLE	WT
Climatology Space time distribution Equidistant points Orthogonal polynomials ( )						

INSTRUCTIONS

1. **ORIGINATING ACTIVITY:** Enter the name and address of the contractor, subcontractor, grantee, Department of Defense activity or other organization (*corporate author*) issuing the report.

2a. **REPORT SECURITY CLASSIFICATION:** Enter the overall security classification of the report. Indicate whether "Restricted Data" is included. Marking is to be in accordance with appropriate security regulations.

2b. **GROUP:** Automatic downgrading is specified in DoD Directive 5200.10 and Armed Forces Industrial Manual. Enter the group number. Also, when applicable, show that optional markings have been used for Group 3 and Group 4 as authorized.

3. **REPORT TITLE:** Enter the complete report title in all capital letters. Titles in all cases should be unclassified. If a meaningful title cannot be selected without classification, show title classification in all capitals in parenthesis immediately following the title.

4. **DESCRIPTIVE NOTES:** If appropriate, enter the type of report, e.g., interim, progress, summary, annual, or final. Give the inclusive dates when a specific reporting period is covered.

5. **AUTHOR(S):** Enter the name(s) of author(s) as shown on or in the report. Enter last name, first name, middle initial. If military, show rank and branch of service. The name of the principal author is an absolute minimum requirement.

6. **REPORT DATE:** Enter the date of the report as day, month, year, or month, year. If more than one date appears on the report, use date of publication.

7a. **TOTAL NUMBER OF PAGES:** The total page count should follow normal pagination procedures, i.e., enter the number of pages containing information.

7b. **NUMBER OF REFERENCES:** Enter the total number of references cited in the report.

8a. **CONTRACT OR GRANT NUMBER:** If appropriate, enter the applicable number of the contract or grant under which the report was written.

8b, 8c, & 8d. **PROJECT NUMBER:** Enter the appropriate military department identification, such as project number, subproject number, system numbers, task number, etc.

9a. **ORIGINATOR'S REPORT NUMBER(S):** Enter the official report number by which the document will be identified and controlled by the originating activity. This number must be unique to this report.

9b. **OTHER REPORT NUMBER(S):** If the report has been assigned any other report numbers (*either by the originator or by the sponsor*), also enter this number(s).

10. **AVAILABILITY/LIMITATION NOTICES:** Enter any limitations on further dissemination of the report, other than those imposed by security classification, using standard statements such as:

- (1) "Qualified requesters may obtain copies of this report from DDC."
- (2) "Foreign announcement and dissemination of this report by DDC is not authorized."
- (3) "U. S. Government agencies may obtain copies of this report directly from DDC. Other qualified DDC users shall request through \_\_\_\_\_."
- (4) "U. S. military agencies may obtain copies of this report directly from DDC. Other qualified users shall request through \_\_\_\_\_."
- (5) "All distribution of this report is controlled. Qualified DDC users shall request through \_\_\_\_\_."

If the report has been furnished to the Office of Technical Services, Department of Commerce, for sale to the public, indicate this fact and enter the price, if known.

11. **SUPPLEMENTARY NOTES:** Use for additional explanatory notes.

12. **SPONSORING MILITARY ACTIVITY:** Enter the name of the departmental project office or laboratory sponsoring (*paying for*) the research and development. Include address.

13. **ABSTRACT:** Enter an abstract giving a brief and factual summary of the document indicative of the report, even though it may also appear elsewhere in the body of the technical report. If additional space is required, a continuation sheet shall be attached.

It is highly desirable that the abstract of classified reports be unclassified. Each paragraph of the abstract shall end with an indication of the military security classification of the information in the paragraph, represented as (TS), (S), (C), or (U).

There is no limitation on the length of the abstract. However, the suggested length is from 150 to 225 words.

14. **KEY WORDS:** Key words are technically meaningful terms or short phrases that characterize a report and may be used as index entries for cataloging the report. Key words must be selected so that no security classification is required. Identifiers, such as equipment model designation, trade name, military project code name, geographic location, may be used as key words but will be followed by an indication of technical context. The assignment of links, rules, and weights is optional.