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## FOREWORD

This report entitled "Thermal Analyzer Computer Program for the Solution of General Heat Transfer Problems," LR 18902, was prepared by the Lockheed-California Company under NASA Contract NAS 9-3349. Although originally developed by Lockheed in 1956 and continually updated over the past several years, the Thermal Analyzer Program was extensively modified for use under this contract.

Other reports prepared under this contract are:

- LR 18899 A Transient Heat Transfer and Thermodynamic Analysis of the Apollo Service Module Propulsion System - Final Report
  - Vol. I - Phase I Transient Thermal Analysis
  - Vol. II - Phase II Thermal Test Program
- LR 18900 A Transient Heat Transfer and Thermodynamic Analysis of the Apollo Service Module Propulsion System - Summary Report
- LR 18901 An Introduction to Spacecraft Thermal Control
- LR 18903 Thermal Analyzer Computer Program for the Solution of Fluid Storage and Pressurization Problems
- LR 18904 Computer Program for the Calculation of Incident Orbital Radiant Heat Flux
- LR 18905 Computer Program for the Calculation of Three-Dimensional Configuration Factors

This report was written by Mr. H. D. Schultz of Lockheed's Thermodynamics Department. The contributions of Messrs. R. B. David, F. R. Mastroly, and J. R. Gardner, also of the Lockheed-California Company, to this report are gratefully acknowledged. Mr. David was responsible for the programming and wrote Section VII and Appendices D and E of this report. Messrs. Mastroly and Gardner wrote computer manuals for two earlier versions of the Thermal Analyzer Program. Much of the content of the present report was adapted from the previous manuals.

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## TABLE OF CONTENTS

	Page
FOREWORD	i
LIST OF FIGURES	ix
LIST OF TABLES	xi
SUMMARY	xiii
I - INTRODUCTION	1-1
II - PROGRAM DESCRIPTION AND CAPABILITIES	2-1
III - PROBLEM SETUP	3-1
BASIC THERMAL SYSTEM AND ELECTRICAL ANALOG	3-1
PROBLEM LUMPING	3-2
Location of Lumps	3-2
Choice of Lump Size	3-7
METHOD OF SOLUTION	3-7
METHOD USED TO DETERMINE COMPUTING INTERVAL	3-10
CALCULATION OF CIRCUIT PARAMETERS	3-11
Resistor Values	3-12
Capacitor Values	3-20
Variable Resistors and Capacitors	3-20
Heat Inputs	3-21
IV - FUNCTIONS AND SPECIAL SUBROUTINES	4-1
DEFINITION OF TERMS	4-1
LIST OF ADDRESSABLE ELEMENTS	4-2
MATHEMATICAL OPERATIONS	4-4
CURVE INTERPOLATION	4-6
Linear Interpolation	4-6
Parabolic Interpolation	4-10
Bivariate Interpolation	4-14
RADIATION FUNCTIONS	4-17

## TABLE OF CONTENTS (Continued)

	Page
Radiation with Constant Factor	4-18
Radiation with Variable Factor	4-19
Radiation with Matrix	4-19
CONVERGENCE AND STEADY-STATE SUBROUTINES	4-23
MAXIMUM-MINIMUM SUBROUTINE	4-25
SAVE CURRENT DATA SUBROUTINE	4-27
TEMPERATURE CARD PUNCH SUBROUTINE	4-28
CURVE PLOTTING SUBROUTINE	4-29
AERODYNAMIC HEATING AND ABLATION SUBROUTINES	4-31
MISCELLANEOUS FORTRAN OPERATIONS	4-32
Variables	4-32
Statement Numbers	4-32
Comment Cards	4-33
GO TO Statements	4-33
Conditional Control and Logical Expressions	4-34
DO Statements	4-36
THERMAL PROPERTIES LIBRARY	4-37
Library Tape	4-37
Interpolation Routines	4-43
V - PROGRAM INPUT	5-1
SPECIAL DATA CARDS	5-2
DATA CARD FORMATS	5-3
BLOCK 1, INITIAL TEMPERATURES	5-4
BLOCK 2, RESISTORS	5-5
BLOCK 3, CAPACITORS	5-6
BLOCK 4, INPUT DATA	5-8

## TABLE OF CONTENTS (Continued)

	Page
BLOCK 5, TIME CONSTANTS	5-10
RESTART BLOCKS	5-11
FUNCT SUBROUTINE	5-14
PRINT SUBROUTINE	5-19
Standard Print Format	5-19
FORMAT Declarations	5-21
VI - EXAMPLE PROBLEMS	6-1
EXAMPLE #1	6-1
Problem Description	6-1
Conduction Resistors	6-3
Radiation Resistors	6-3
Capacitors	6-3
RC Products	6-4
Curves	6-5
Time Block	6-5
FUNCT Subroutine	6-7
PRINT Subroutine	6-7
Computer Input for Example #1	6-8
Computer Output	6-8
EXAMPLE #2	6-17
Problem Description	6-17
Conduction Resistors	6-18
Radiation Resistors	6-21
Capacitors	6-21
RC Products	6-22
Curves	6-23

## TABLE OF CONTENTS (Continued)

	Page
Time Block	6-24
Restart Block	6-25
FUNCT Subroutine	6-25
PRINT Subroutine	6-26
Computer Input	6-26
Computer Output	6-26
VII - GENERAL PROGRAM INFORMATION	7-1
INCORRECT DATA INPUT	7-1
Common Input Errors	7-1
Function Subroutine Errors	7-2
Data Diagnostic	7-3
Data Debugging Routine	7-4
PROGRAM CAPACITY	7-4
Version A (Short Problems)	7-4
Version B (Maximum Problems)	7-5
Version C (Pressurization)	7-5
MACHINE EXECUTION TIME	7-5
APPENDIX A - ECKERT AERODYNAMIC HEATING	A-1
ECKERT'S RECOMMENDED PROCEDURE	A-1
MODIFICATION OF ECKERT'S RELATIONS FOR DIGITAL COMPUTING USE	A-2
PROGRAM INPUT	A-4
Method 1	A-6
Method 2	A-6
LIMITATIONS OF ECKERT'S AERODYNAMIC HEATING METHOD	A-9

## TABLE OF CONTENTS (Continued)

	Page
EXAMPLE PROBLEM	A-10
Capacitors	A-11
Radiation Resistor	A-11
Conduction Resistor	A-11
Eckert K Factor	A-12
NOMENCLATURE FOR APPENDIX A	A-19
APPENDIX B - ABLATION	B-1
PROGRAM INPUT	B-2
EXAMPLE PROBLEM	B-5
APPENDIX C - DIGITAL COMPUTER SOLUTION FOR PASSAGE AIR AND WALL TEMPERATURES	C-1
APPENDIX D - COMPUTER OPERATION	D-1
ARRANGEMENT OF THE DECK	D-1
COMPUTATION SEQUENCE	D-10
DESCRIPTION OF PROGRAM DECKS	D-14
TAPE USAGE	D-17
NOTES ON COMPUTER OPERATION	D-18
APPENDIX E - DATA DIAGNOSTIC PROGRAM	E-1
PROGRAM OPERATION	E-1
PROGRAM SETUP	E-2
REFERENCES	R-1

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## LIST OF FIGURES

Figure		Page
3-1	Physical Geometry and Corresponding Thermal Network for a Re-entry Structure	3-3
3-2	Physical Geometry and Corresponding Thermal Network for an Electronic Equipment Rack	3-5
3-3	Physical Geometry and Corresponding Thermal Network for a Window Section	3-6
4-1	Correct and Incorrect Inputs for Curves Described by Parabolic Interpolation	4-12
6-1	Physical Geometry and Corresponding Thermal Network for Example Problem 1	6-2
6-2	Temperature History of Upper and Lower Surfaces	6-6
6-3	Physical Geometry and Corresponding Thermal Network for Example Problem 2	6-19
6-4	Temperature Plots for Example Problem 2	6-72
6-5	Temperature Plots for Example Problem 2 Restart	6-73
C-1	Physical Geometry and Corresponding Thermal Network for a Portion of an Air Passage	C-4
C-2	Function $f_3(\beta)$ Required for Passage Air Temperature Solution	C-15
C-3	Functions $f_1(\beta)$ and $f_2(\beta)$ Required for Passage Air Temperature Solution	C-16
D-1	Deck Setup for Thermal Analyzer Program	D-3
D-2	Program Linkage Arrangement - Version A	D-4
D-3	Program Linkage Arrangement - Version B	D-5
D-4	Simplified Flow Diagram of Computer Program	D-20
E-1	Source Program Deck Setup for Data Diagnostic Program	E-4

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## LIST OF TABLES

Table		Page
4-1	Thermal Properties Library Identification Codes	4-39
4-2	Data Classification Codes	4-44
5-1	Input Format for FUNCT Subroutine	5-15
5-2	Summary of Functions and Special Subroutines	5-17
5-3	Input Format for PRINT Subroutine	5-20
6-1	Input for Example 1	6-9
6-2	Computer Output for Example 1	6-12
6-3	Input for Example 2	6-28
6-4	Computer Output for Example 2	6-34
A-1	Input for Aerodynamic Heating Example Problem	A-14
B-1	Input for Ablation Example Problem	B-7
D-1	Program Capacity	D-1
D-2	Program Deck Order - Version A	D-6
D-3	Program Deck Order - Version B	D-8
D-4	Program Listing	D-21
E-1	Diagnostics	E-5
E-2	Data Diagnostic Program Listing	E-8

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## SUMMARY

This report discusses the application of the Thermal Analyzer Program, developed for the IBM 7040/7094 direct coupled digital computer or the IBM 7094 digital computer, to complex transient heat transfer problems. The report also discusses a separate data "debugging" program developed for the IBM 7040 digital computer, which allows examination of the program input data prior to submitting the problem for execution.

The transient heat transfer solution is obtained by converting the physical system into one consisting of lumped thermal capacities connected by thermal resistors, and then using the lumped parameter, or finite differences, approach to solve for the temperature history of the system. This solution, although discontinuous in space and time, can be obtained to any desired degree of accuracy by proper selection of lump size and computing interval within certain limitations as described herein.

The program affords direct solution of complex transient problems involving conduction, convection, radiation, heat storage, and ablation. In addition, by being able to specify any quantity as an arbitrary function of any other, it is possible to include such problems as change of state, variable thermodynamic properties, arbitrary variable boundary conditions, and other non-linear effects.

This report discusses the method used to transform the physical heat transfer problem into a resistance-capacitance (R-C) network (which is analogous to an electrical circuit), the numerical evaluation of the equivalent electrical elements, and the method of presentation (input format) required to input the problem into the computer. Several example problems illustrating most of the program features are included.

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## I - INTRODUCTION

Transient thermal phenomena may be studied experimentally, analyzed by graphical or relaxation methods such as the Schmidt plot, or calculated by direct solution of the appropriate differential equations or finite difference equations and approximations. Such methods are usually quite tedious and difficult even for relatively simple cases, and may be inaccurate if the problem is at all intricate.

With increasing aircraft speeds, and with space exploration a reality, the need for accurate transient heat transfer analyses of complex systems has become more acute. Detailed analyses are required for accurately predicting transient structural temperature distributions during high-speed flight, component and environmental temperatures in a space vehicle, the ablation requirements for a reentry body, and in many other cases where hand computations do not suffice. Conventional aircraft, which employ many thermal systems, also require detailed temperature analyses to assure proper system design and operation.

Because of the increased need for detailed thermal analyses, artificial methods are often substituted for the exact solutions of the proper differential equations as a means of obtaining a solution. The method selected for this program is one of many such methods in use and employs the electrical resistance capacitance analog. There are two reasons for this choice:

1. The equations describing any general heat transfer problem are of the same form as those describing an equivalent electrical R-C network. The electrical network equations are simple to set up in finite difference form, and consequently the heat transfer problem may be solved to any desired degree of accuracy.
2. The network setup is easy to visualize in relation to a schematic diagram of the physical problem.

To facilitate the solution of such an analogous network, the Lockheed-California Company has developed the Thermal Analyzer Program. The purpose

of this report is to enable a heat transfer engineer who is unfamiliar with the program to use it successfully in solving his problem. A basic familiarity with heat transfer laws is assumed, and hence primary emphasis is placed on the conversion of the physical problem into one that can be interpreted by the computer. Examples demonstrating the program features are included.

## II - PROGRAM DESCRIPTION AND CAPABILITIES

The Thermal Analyzer Program is written in FORTRAN IV for the IBM 7040/7094 direct coupled digital computer or the IBM 7094 digital computer. It computes transient temperature distributions in configurations of arbitrary complexity, using the electrical resistance-capacity analogy. Solutions are obtained by converting the physical system into one consisting of lumped thermal capacities connected by thermal resistors, and then using the lumped-parameter, or finite-differences approach to solve for the temperature history of a system.

The program permits direct solution of complex transient problems involving conduction, convection, radiation and heat storage. Furthermore, since it is possible to specify any quantity as an arbitrary function of any other, it is also possible to solve such problems as change of state, variable thermodynamic properties, arbitrary variable boundary conditions, and other nonlinear effects.

In developing the Thermal Analyzer Program, a primary objective has been to maximize input flexibility, and hence to keep the program as general as possible. Input format has not been restricted to any particular geometry, rather it is such that resistors and capacitors can be connected in the same manner as could the actual equipment components. Additions or other changes to the network can easily be made by adding or removing cards in the program input deck.

An outstanding feature of the program is its ability to accept various subroutines, or functions, as required by the particular problem. Currently available are various general-purpose and special functions which permit numerous mathematical operations beyond solution of the electrical network itself. These functions are discussed in Section IV.

Standard FORTRAN statements are accepted, allowing the user to add his own subroutines as required. More important, this flexibility in

handling subroutines allows new ones to be added without altering the basic program.

The program has the capability to run consecutively several cases which are basically similar, but differ in the value of certain parameters. An example of this is a parametric study of the effect of varying the surface emissivity and absorptivity of a space vehicle. A second restart feature is available in which several cases are run consecutively with the results of the first used as inputs to the second, and so on. The temperatures at the end of each case are recorded on tape and used as the initial temperatures for the subsequent case.

The program also allows the user to specify the format for printing the answers. In addition to the tabulated answers, an option provides for machine plotting of the results.

The steps required to solve a problem using the Thermal Analyzer Program are as follows:

1. The physical problem is set up and defined.
2. The physical problem is specified in terms of time, temperature, and a thermal network analogous to an electrical network consisting of resistances and capacities. This re-definition and re-description of the problem is known as lumping, and puts the problem in the only form which the computer is able to solve.
3. The network is described in detail in a form which allows it to be accepted by the computer program and solved. This involves writing up the program in a standard format.
4. This description of the network is transferred to punched cards which are then put into the computer.
5. The computer program solves the problem and provides the answers.
6. The program then provides for printing these answers in a format which can be prescribed by the user.
7. The answers thus printed are then interpreted by the user to provide the desired solution for the original problem.

Step 1 It is assumed that anyone using this program will be able to describe and specify his problem. The user must have a detailed knowledge of the

configuration, including conduction paths and surface properties if conduction and radiation are important heat transfer modes. In addition, it is assumed that boundary conditions, such as external heat inputs and adiabatic interfaces, are known.

Step 2 The most crucial and time-consuming step is the conversion of the physical problem into an equivalent resistance-capacitance network. The user must divide the physical geometry into sections called "lumps" and then calculate the resistance and capacity of these lumps. The capacity of each lump is the thermal capacity (mass times specific heat) of that portion of the physical problem which the lump represents. The use of the lumping process implies that a given portion of the actual structure is at a uniform average temperature. In lumping a problem there are many factors which influence the size, shape, and number of lumps to be used. Among these are the nature of the physical problem, the amount of detailed information desired, and the anticipated transient response rates and temperature gradients. Some of the considerations involved in problem lumping are discussed in Section III, where several examples are presented. Once the method of lumping has been established, each capacitor and resistor is assigned an integer designation number. Although the designation numbers are arbitrary, a systematic numbering scheme is usually employed for convenience. The user then computes the network resistor and capacitor values, following the general procedures outlined in Section III.

Step 3 After computing the network parameters, the problem must be described on input data sheets (General Purpose Data Sheets or FORTRAN Coding Sheets) in a prescribed manner. The input format is described in detail in Section V. The problem description is divided into five distinct blocks and two subroutines. The first three blocks define the network and give the initial values of the temperatures, resistors, and capacitors. The fourth block is a list of sub-blocks of data required for the problem solution. An example of the type of data that might appear here is the point-by-point description of a curve which is to be used by the functions (described below) for interpolation. Each data sub-block is assigned an

arbitrary designation number so that it may be referenced later in the program. The fifth block of data lists the printing interval, the final time of the case, and the initial time. The latter two times correspond to the real time of the physical problem.

The user must then prepare a standard FORTRAN subroutine (the FUNCT subroutine) in which he specifies the miscellaneous functions, or operations, which the program must perform. In general, the FUNCT subroutine specifies all operations necessary to solve the problem with the exception of the actual heat balance. An example of a function is the interpolation of a curve described in block 4, to perhaps specify the external heating rate to a portion of the network. The FUNCT subroutine may also be used to call in special subroutines such as aerodynamic heating, ablation, curve plotting, and several others. A complete list of the available functions and special subroutines is given in Section IV.

The last item which the user must code on input sheets is the PRINT subroutine, in which he specifies the quantities that are to be printed out at each printing time, and the desired output format. The program has been set up so that essentially every quantity of interest has an addressable storage location and may therefore be printed out. Section V describes the format used in writing the PRINT subroutine.

Although the FUNCT and PRINT subroutines are ordinary FORTRAN subroutines, standard input formats are presented in Section V, and the user need not have a knowledge of FORTRAN to prepare these routines.

Steps 4 and 5 The information on the input sheets is transferred to punched cards which are then input to the computer, and the problem is solved. The actual running of the program is described in Appendix D.

Step 6 The answers are printed on a line printer using the format prescribed by the user in the PRINT subroutine. As mentioned above, machine plotting of the results is optional.

Step 7 Interpretation of the answers to provide the desired solution for the original problem should present no difficulties.



## III - PROBLEM SETUP

BASIC THERMAL SYSTEM AND ELECTRICAL ANALOG

The Thermal Analyzer Program requires that the problem be described as an equivalent network using resistance, capacity, and temperature to define the heat transfer situation.

Thermal resistance refers to resistance to heat flow, analogous to electrical resistance which refers to resistance to current flow.

In any case involving heat transfer between two points, at temperatures  $T_i$  and  $T_k$ , the heat flow is given by an equation (analogous to Ohm's electrical law) as follows:

$$q = \frac{T_i - T_k}{R} \quad (3-1)$$

Some simple examples might be given here:

$$\text{For conduction, } q = kA \frac{\Delta T}{\Delta x} \Rightarrow R = \frac{\Delta x}{kA}$$

$$\text{For convection, } q = hA\Delta T \Rightarrow R = \frac{1}{hA}$$

If  $q$  is in Btu/hr or Btu/sec,  $R$  must be in hr. $^{\circ}$ F/Btu or sec. $^{\circ}$ F/Btu, respectively.

Transient analyses differ from steady-state analyses in that heat storage in a material undergoing a heating or cooling process is accounted for, thus causing a time lag in the temperature response of the material. The quantity of heat thus stored, and the description of the temperature response, will depend on the properties of the material itself. These properties determine the quantity called "thermal capacity," which

behaves in the thermal network in the same manner as electrical capacity behaves in an electrical network. Thermal capacity must be in the units of heat quantity per degree of temperature (e.g., Btu/°F) and is a function of the material's density, specific heat and volume. Physically, the thermal capacity of a material represents the amount of heat stored in a given volume for each degree of temperature rise experienced by the material.

For most materials, property values such as thermal conductivity, emissivity, and specific heat will be a function of temperature. In those cases where this variation is significant, it may be taken into consideration in the program through the use of curves as discussed in Section IV.

### PROBLEM LUMPING

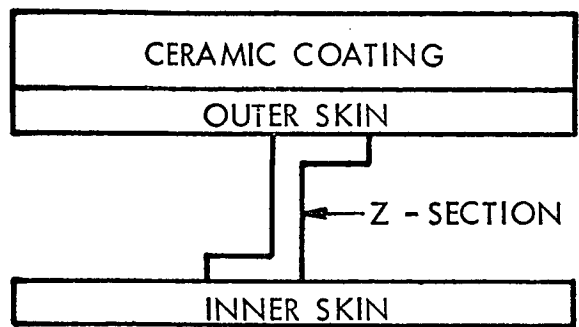
To transform the physical problem into a form suitable for the computer, it is necessary to convert it into an equivalent resistance-capacitance (R-C) network. This is accomplished by dividing the physical system into sections called "lumps" and calculating the resistance and capacity of these lumps. A "lump," then, is any portion of the physical problem which (though not necessarily physically disconnected) will not be connected to any other portion of the problem except by resistors. The discussions to follow outline some of the considerations involved in problem lumping.

### Location of Lumps

Although the lumps may take any size or shape, they should bear a simple relationship to the physical geometry. As a general rule, the nodes (the points where the lump capacities are assumed to be concentrated) should be located at those points where temperature data are desired, and these in turn are dictated by the nature of the problem itself. This is illustrated by the following examples. In each instance, the node locations are determined first and the lump boundaries located afterwards.

Example 1, Re-entry Structure - Figure 3-1 shows a re-entry structure consisting of an inner and outer skin separated by a z-section, with the outer skin protected by a ceramic coating. It is assumed that the section is not influenced by other such sections and that the problem is two-dimensional,

GEOMETRY



THERMAL NETWORK

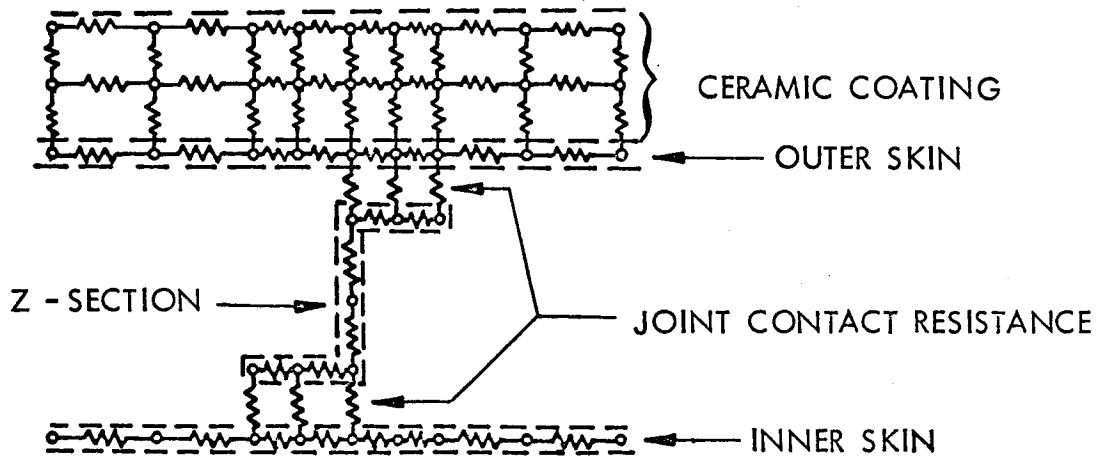


Figure 3-1. Physical Geometry and Corresponding Thermal Network for a Re-Entry Structure

i.e., no heat flow in and out of the plane of the drawing. However, it is a simple matter to connect many such sections into a complex three-dimensional problem. For this example, the temperature of the ceramic surface and the underlying structure is of primary importance. Also, it is assumed that large lateral temperature gradients exist near the z-section, with smaller gradients further out. With these points in mind, the resulting network is as shown in the lower sketch in Figure 3-1.

With regard to lump boundaries, the usual procedure is to place them so that the nodes are approximately in the center of the lumps except, of course, at the boundaries of the various layers. The problem of lump boundaries and the calculation of resistors and capacitors are discussed in detail in subsequent sections.

Example 2, Electronic Equipment Rack - Figure 3-2 shows an electronic equipment rack consisting of intersecting webs on which heat dissipating components are mounted. The corresponding thermal network is shown in the lower sketch. Since component temperatures are of primary interest here, the various capacities are assumed to be concentrated at points corresponding to equipment locations. However, this places the nodes inside the web boundaries as shown at the free ends of the two webs. At the juncture between the two webs, a string of zero capacitance nodes (designated by  $\otimes$  in Figure 3-2 and often referred to as "dummy" nodes) is required to effect a connection between webs. This technique is particularly useful in a complex network where many such interconnecting webs are involved, since it allows each web to be treated separately and then connected to other such webs at the various dummy nodes.

Example 3, Spacecraft Window - A section of a spacecraft window exposed to convection and radiation on both surfaces is shown in Figure 3-3. For this problem, one-dimensional heat flow is assumed. Three lumps have been arbitrarily assumed for the conduction network through the window, with nodes appearing at the boundaries to properly account for convection and radiation, both of which depend on the surface temperature.

The preceding illustrations are of but a few of the many lumping situations which arise. Probably the most important factor in problem lumping

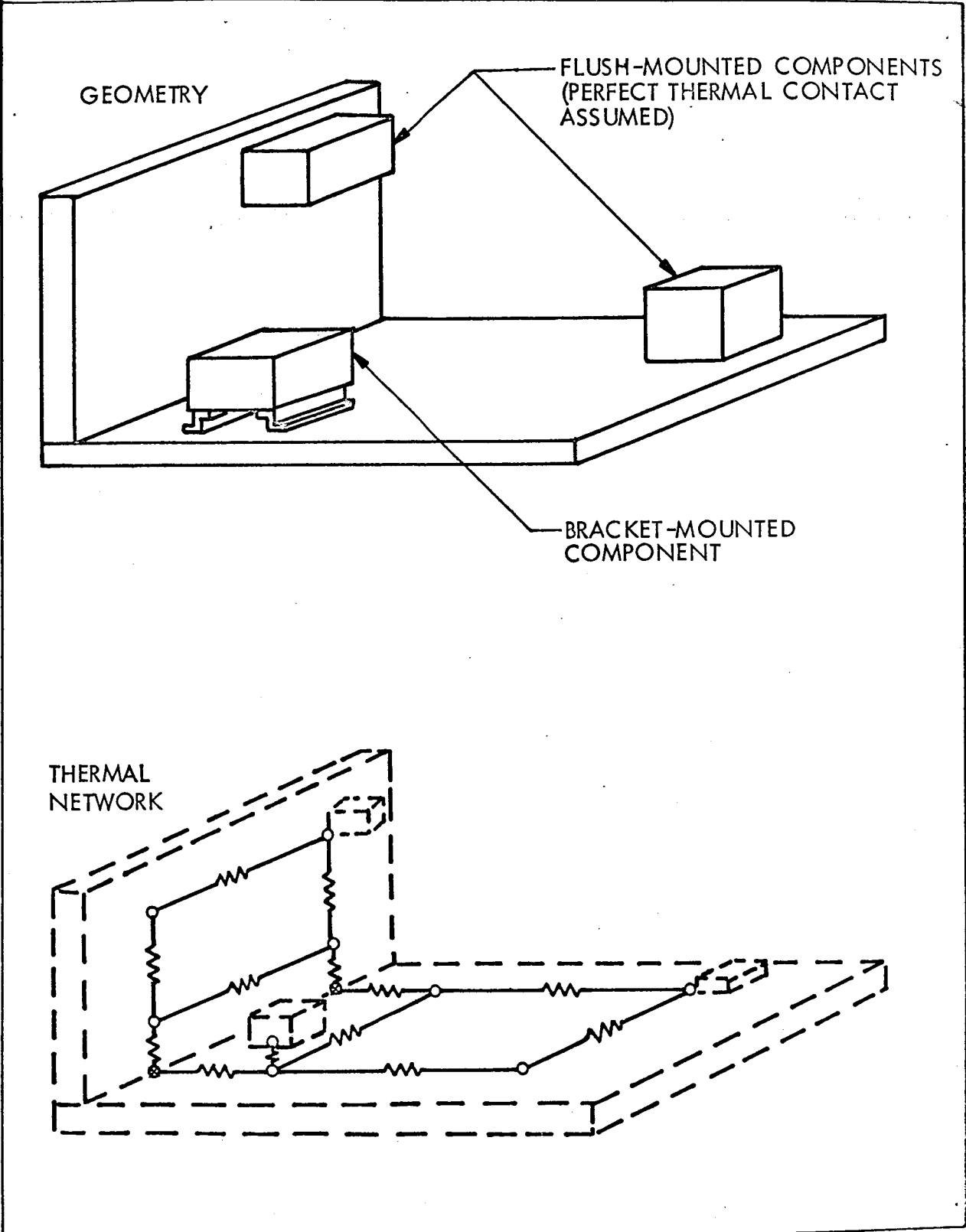


Figure 3-2. Physical Geometry and Corresponding Thermal Network for an Electronic Equipment Rack

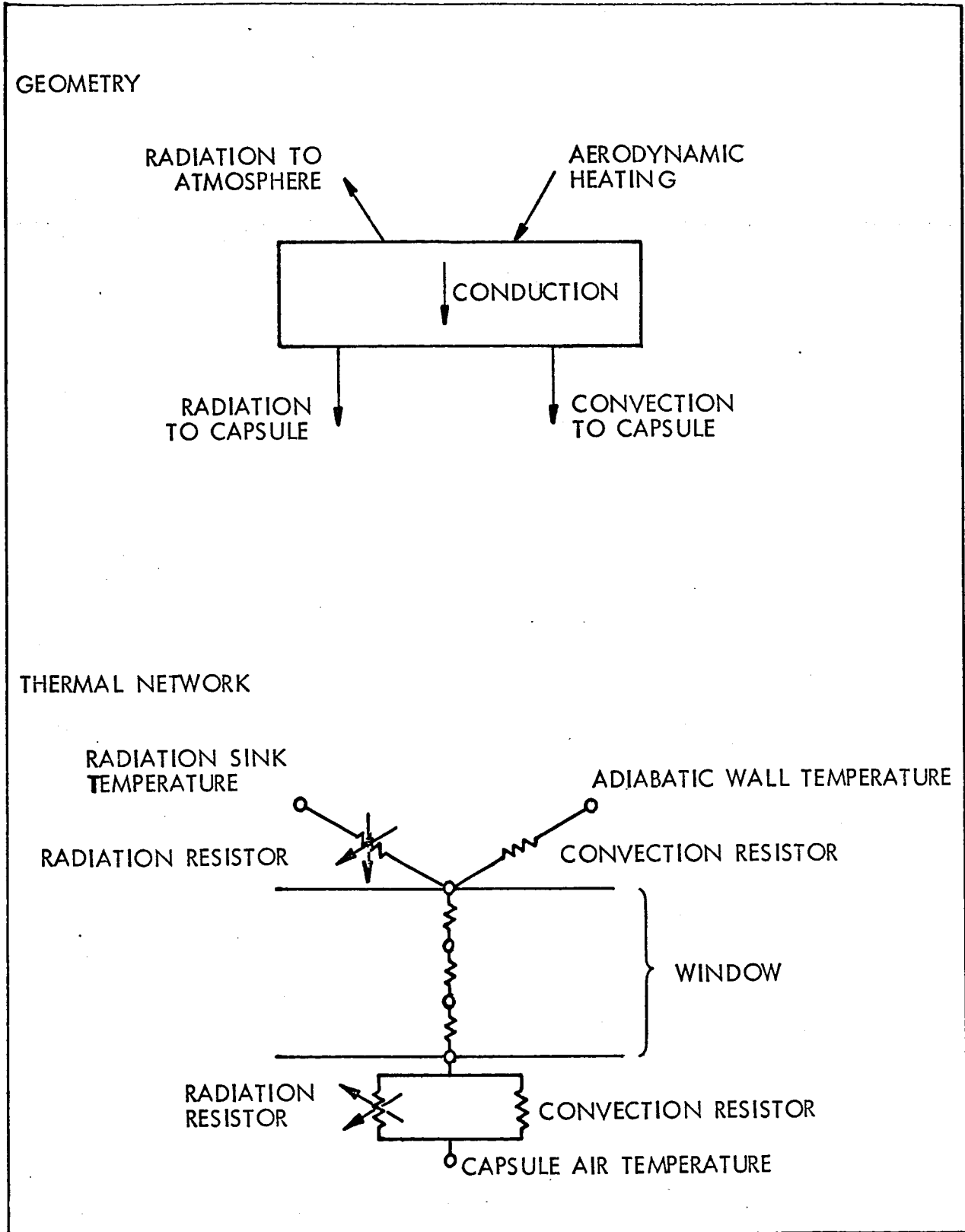


Figure 3-3. Physical Geometry and Corresponding Thermal Network for a Window Section

is experience, and this cannot be acquired merely by reading reports. Also, since no two situations are identical, it is impossible to cover all conceivable situations in a single report. It is hoped, however, that the examples presented here and in subsequent sections will provide some insight into the problems involved.

### Choice of Lump Size

In selecting the optimum lump size, recourse must be made to logic, and, most of all, experience. Here again, the nature of the physical problem will dictate to a great extent the final decisions. Generally, the choice of lump size will be based upon these factors:

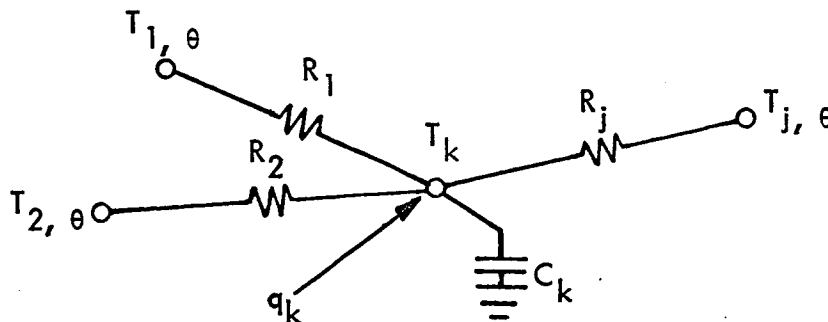
1. Consideration of inaccuracies introduced into the system resulting from the finite difference method of solution. These inaccuracies decrease (not necessarily linearly) as lump size decreases. About the only definite statement which can be made is that lump size should be as large as possible without causing excessive inaccuracies.
2. Anticipated temperature gradients and relative rates of transient response. Where it is suspected that large temperature gradients will occur, nodes should be placed closer together than those where these gradients are smaller. This is especially true when the thermal diffusivity of a particular layer is very small, with the resulting temperature gradients across it being highly nonlinear.
3. Convenience in visualizing the network and making calculations.
4. Program capacity. Ordinarily the capacity of the computer is not approached; on occasion, for extremely large and complex problems, this becomes an important consideration.
5. Consideration of machine time, which costs money. Not only do small lumps increase the number of nodes to be computed, but also they result in a smaller computing interval (difference in real time between successive steps), thus greatly increasing machine time.

### METHOD OF SOLUTION

As previously indicated, the Thermal Analyzer Program solves equations in finite difference form by means of an R-C electrical analog finite difference method. The comparable values in the two systems may be noted as follows:

<u>THERMAL</u>	<u>ELECTRICAL</u>
Temperature	Voltage
Heat Flux	Current
Resistance	Resistance
Capacity	Capacity

At a given node point k,



the solution is obtained by applying Kirchoff's Law at a point, or

$$\sum_j \frac{T_{j,\theta} - T_{k,\theta}}{R_j} + q_k = C_k \frac{dT_k}{d\theta} \quad (3-2)$$

where

- $T_{j,\theta}$  = Temperature at time  $\theta$  of any arbitrary node j connected to node k by a resistor  $R_j$
- $R_j$  = Resistor connecting nodes j and k
- $T_{k,\theta}$  = Temperature of node k at time  $\theta$
- $T_{k,\theta+\Delta\theta}$  = Temperature of node k after time increment  $\Delta\theta$
- $C_k$  = Capacity of node k
- $q_k$  = Arbitrary heat input into node k



By making the assumption that the surrounding temperatures,  $T_j$ , remain constant over a time interval  $\Delta\theta$ , it is possible to integrate equation 3-2 directly. However, as a result of a comparison study, it was found that better results were obtained by using the equation which results from assuming

$$\frac{dT_k}{d\theta} \approx \frac{T_{k,\theta + \Delta\theta} - T_{k,\theta}}{\Delta\theta} \quad (3-3)$$

and solving for  $T_{k,\theta + \Delta\theta}$  directly than by using the integrated equation. This comparison was made by running the same problem using both equations and varying the computing interval  $\Delta\theta$ . It was found that the linear equation, i.e., that obtained by using equation 3-3, was far less sensitive to  $\Delta\theta$ , and that the results obtained using the integrated equation approached the linear results as  $\Delta\theta \rightarrow 0$ . Although the integrated equation is "exact," it is suspected that the linear approximation, which "leads" the exact solution (it predicts higher temperatures in a warming system, lower temperatures in a cooling system), tends to anticipate the results. As a result, the equation used by the computer to solve the heat balance at a node was derived by combining equations 3-2 and 3-3 to obtain

$$T_{k,\theta + \Delta\theta} = \frac{\Delta\theta}{C_k} \left[ \sum_j \frac{T_{j,\theta} - T_{k,\theta}}{R_j} + q_k \right] + T_{k,\theta} \quad (3-4)$$

If the value of capacity  $C_k$  is zero, e.g., in a steady state problem,  $T_{k,\theta}$  in Equation 3-2 is replaced by  $T_{k,\theta + \Delta\theta}$  to give

$$T_{k,\theta + \Delta\theta} = \frac{\sum_j \frac{T_{j,\theta}}{R_j} + q_k}{\sum_j \frac{1}{R_j}} \quad (3-5)$$

If no capacitor is attached to node k, i.e.,  $C_k$  unspecified, no heat balance is computed at node k and  $T_k$  remains unchanged.

It is to be noted that the new temperature at a node is based upon the temperatures at the previous time point. To make the new temperatures independent of the order in which they are computed, each node is provided with two temperature storages, one for the "old" temperature,  $T_{k,\theta}$ , and one for the "new" temperature,  $T_{k,\theta+\Delta\theta}$ . At the beginning of each cycle, the values in the two storages are identical. During the heat balance, the temperatures in the "T at  $\theta$ " block are used to compute new values which go into the "T at  $(\theta + \Delta\theta)$ " block, the old temperature values remaining unchanged. At the end of the heat balance, the temperatures in the " $\theta$ " block are set equal to those in the " $(\theta + \Delta\theta)$ " block and the process repeated.

#### METHOD USED TO DETERMINE COMPUTING INTERVAL

In the section on lump size, it was stated that smaller lumps result in a smaller  $\Delta\theta$ . At each time point  $\theta$ , the machine computes the time constant, or RC product, of each node for which a non-zero capacitor is specified. This time constant is defined as the product of the capacity of the node times the equivalent resistance to that node. This equivalent resistance is defined as the parallel combination of all resistors connected to the node in question. Therefore,

$$(RC)_k = \frac{C_k}{\sum_j \frac{1}{R_j}} \quad (3-6)$$

where  $(RC)_k$  = time constant of node k ~ seconds (if R in sec<sup>o</sup>-F/Btu).

Since, for conduction,  $R = \delta/kA$ , and for capacity,  $C = \rho c A \delta$ , the RC product of a node is a function of the square of its thickness ( $\delta$ ) in the direction of the heat transfer, viz.

$$RC = \frac{C}{\sum_j \frac{1}{R_j}} = f \left[ \frac{\delta}{kA} \cdot \rho_c \delta A \right] = f \left[ \frac{\rho_c}{k} \cdot \delta^2 \right] \quad (3-7)$$

To obtain the computing interval,  $\Delta\theta$ , the computer searches the network to find the minimum RC product and compares this with the printing interval (the real-time increments for which the output is desired). The computer then takes whichever is smaller and multiplies it by a certain fraction to obtain  $\Delta\theta$ . Ordinarily this factor is 0.25, and unless changed by the user in the FUNCT subroutine, it remains so. However, there are times when a factor other than 0.25 is convenient, for example:

1. Increased  $\Delta\theta/RC$  (possibly as large as 0.9) can be used when only a small percentage of the nodes have small RC products compared with the others, and when a major reduction in machine time can be obtained at the cost of a small reduction in accuracy.
2. Reduced  $\Delta\theta/RC$  (as small as 0.1 or even smaller) should be used when it is desired to have the machine compute more frequently during certain portions of the program. In conjunction with the MMF function to be described subsequently, this procedure enables the computer to pick up the maximum and minimum temperatures of a particular node with a greater degree of accuracy. Since it is possible to make  $\Delta\theta/RC$  a variable, a reduced  $\Delta\theta/RC$  during one portion of the program can be offset, as far as machine time is concerned, by an increased  $\Delta\theta/RC$  during the other portions of the program.

#### CALCULATION OF CIRCUIT PARAMETERS

This section presents the general procedures employed to calculate capacitors and resistors, and the methods used to accommodate the various modes of heat transfer (conduction, convection, and radiation). The procedures required to transcribe the network parameters to data input sheets are described in Section V.

In the discussions which follow, it is assumed that ordinary engineering units will be used for program input. Specifically, the following units are assumed:

- a. Heat Flow, Btu/sec
- b. Temperature, °F
- c. Time, sec
- d. Resistance, sec °F/Btu
- e. Capacitors, Btu/°F

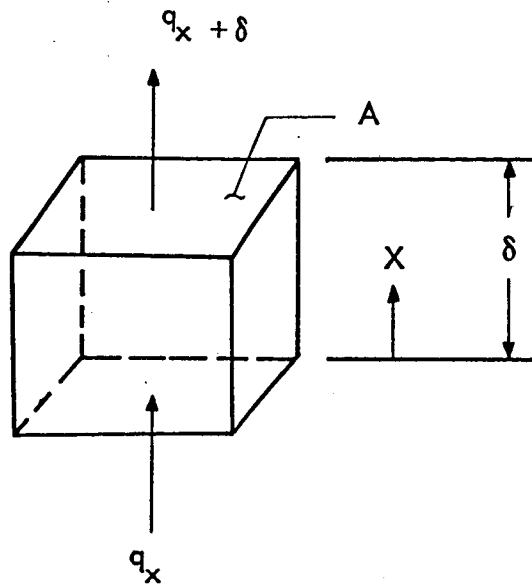
In cases not involving radiation, any consistent set of units may be employed for program input. Also in such cases, the time scale can be changed and all temperatures input as absolute (°R or °K) quantities. However, for radiation resistors the machine adds 460°F to the appropriate temperatures, and since a dimensional quantity, the Stefan-Boltzmann constant, is incorporated into the program as discussed later, it is not recommended that units other than those tabulated above be used for cases involving radiation.

#### Resistor Values

Resistors must be of the dimension time °F/Btu. For most practical engineering problems, particularly those involving materials with low RC products, the most convenient unit of time is seconds. Consequently, resistance is given in sec °F/Btu, and the heat flow is in Btu/sec. The form of the resistor depends on the particular mode of heat transfer involved.

Conduction Resistors - In all cases, conduction resistors are computed by the formula

$$R = 3600 \int_c^{\delta} \frac{dx}{kA}, \frac{\text{sec } ^\circ\text{F}}{\text{Btu}} \quad (3-8)$$



where:

- k = thermal conductivity, Btu/hr ft °F
- A = cross-sectional conductive heat transfer area, ft<sup>2</sup>
- x = distance along conductive path, ft
- R = resistance, sec- °F/Btu

For a rectangular parallelepiped or a cylinder with vertical sides, or for any configuration with constant cross-section, vertical sides, and parallel faces,

$$R = \frac{3600 \delta}{kA}, \frac{\text{sec } ^\circ\text{F}}{\text{Btu}} \quad (3-9)$$

Radiation Resistors - Since the radiation interchange from surface 1 to surface 2 is

$$q_{1-2} = \frac{T_1 - T_2}{R} = \frac{\epsilon_{12} A_1 F_{12} \sigma (\tau_1^4 - \tau_2^4)}{3600} \text{ Btu/sec,} \quad (3-10)$$

(where  $\tau_i$  = absolute temperature of node  $i \sim ^\circ R$ )

R will be of the form

$$R = \frac{3600}{\epsilon_{12} A_1 F_{12} \sigma (\tau_1^2 + \tau_2^2) (\tau_1 + \tau_2)} \quad (3-11)$$

where:

$\epsilon_{12}$  = emissivity factor

$A_1$  = area of radiating surface,  $ft^2$

$F_{12}$  = shape factor from surface 1 to surface 2

$\sigma$  = Stefan-Boltzmann Constant =  $0.1713 \times 10^{-8}$  Btu/hr  $ft^2$   $^\circ R^4$

The thermal analyzer program computes the radiation resistor

$$R = \frac{1.0}{\sigma K_{rad} \left[ (T_1 + 460)^2 + (T_2 + 460)^2 \right] \left[ (T_1 + 460) + (T_2 + 460) \right]} \quad (3-12)$$

given the value

$$K_{rad} = \frac{\epsilon_{12} A_1 F_{12}}{3600} \frac{ft^2 \text{ hr}}{sec} \quad (3-13)$$

The value for  $\sigma$  must not be included since it is built into the program. Note that since the program adds  $460^\circ F$  to each temperature, all temperatures must be in  $^\circ F$ .

In addition to the above, it is possible to have the computer evaluate its own value for  $K_{rad}$  as will be discussed in Section IV.

Convection Resistors, No Change in Fluid Temperature -

$$R = \frac{3600}{\int_0^A h d A_h} \frac{sec \text{ } ^\circ F}{Btu} \quad (3-14)$$

where:

R = resistance, sec-°F/Btu

h = heat transfer coefficient, Btu/hr-ft<sup>2</sup>-°F

A<sub>h</sub> = convective heat transfer area, ft<sup>2</sup>

For common sections when an average value of h can be used for the given area A<sub>h</sub>,

$$R = \frac{3600}{h A_h} \frac{\text{sec } ^\circ\text{F}}{\text{Btu}} \quad (3-15)$$

Convection Resistors, With Change in Fluid Temperature (Duct Temperature Drop) - The problem may be approached from two directions. The first assumes that the time for the fluid to pass a lump portion of the duct wall is very small compared with the time constant of the wall lump, i.e.,

$$\frac{\theta_L}{T_w} = \frac{L h P}{3600 \rho_w c_w A_w V} \ll 1$$

and that the thermal capacity of the fluid element is very small compared with the thermal capacity of the wall element, i.e.,

$$\frac{C_a}{C_w} = \frac{\rho_a c_v A_c}{\rho_w c_w A_w} \ll 1$$

where:

L = total passage length, ft

$\theta_L$  = time for fluid to flow through the passage, sec

T<sub>w</sub> = wall time constant, sec

h = heat transfer coefficient, Btu/hr-ft<sup>2</sup>-°F

P = perimeter of passage, ft

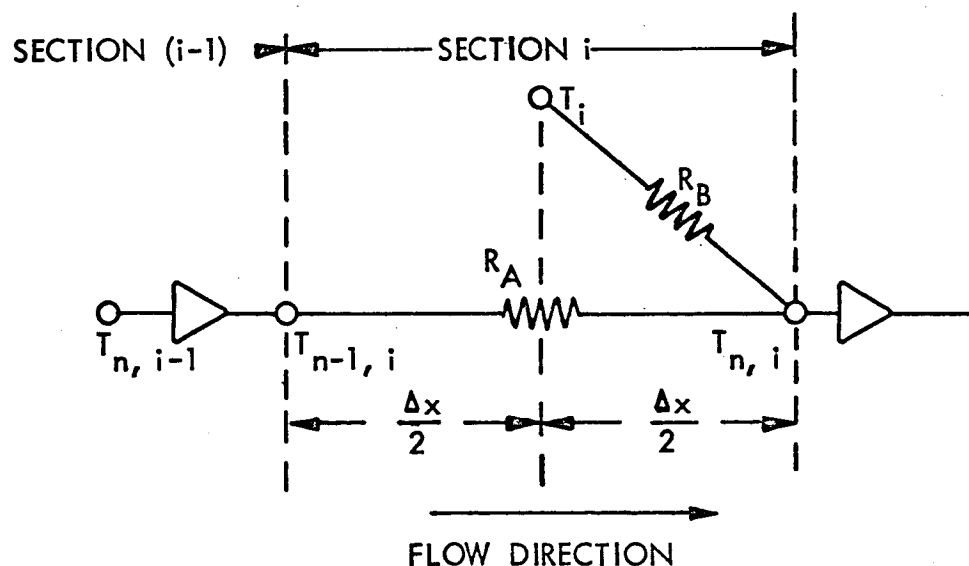
$\rho_w$  = density of wall material, lb/ft<sup>3</sup>

- $c_w$  = specific heat of wall material, Btu/lb °F
- $A_w$  = wall cross-section, ft<sup>2</sup>
- $C_a$  = thermal capacity of fluid, Btu/°F
- $C_w$  = thermal capacity of wall, Btu/°F
- $\rho_a$  = density of fluid, lb/ft<sup>3</sup>
- $c_v$  = fluid specific heat at constant volume, Btu/lb °F
- $A_c$  = passage cross-section area, ft<sup>2</sup>
- $V$  = velocity, ft/sec

This problem is treated as in methods 1 and 2, in the following paragraphs.

If these ratios are not very small, the problem must be treated as in method 3:

1. With uniform temperature in the passage walls in planes normal to the airflow direction,



$$R_A = \frac{3600}{W c_p}$$

$$R_B = \frac{3600}{W c_p (e^{\beta} - 1)}$$



where:

$$\beta = h A_h / W c_p$$

$h$  = heat transfer coefficient, Btu/hr-ft<sup>2</sup>-°F

$A_h$  = convective heat transfer area, ft<sup>2</sup>

$W$  = weight flow of fluid, lb/hr

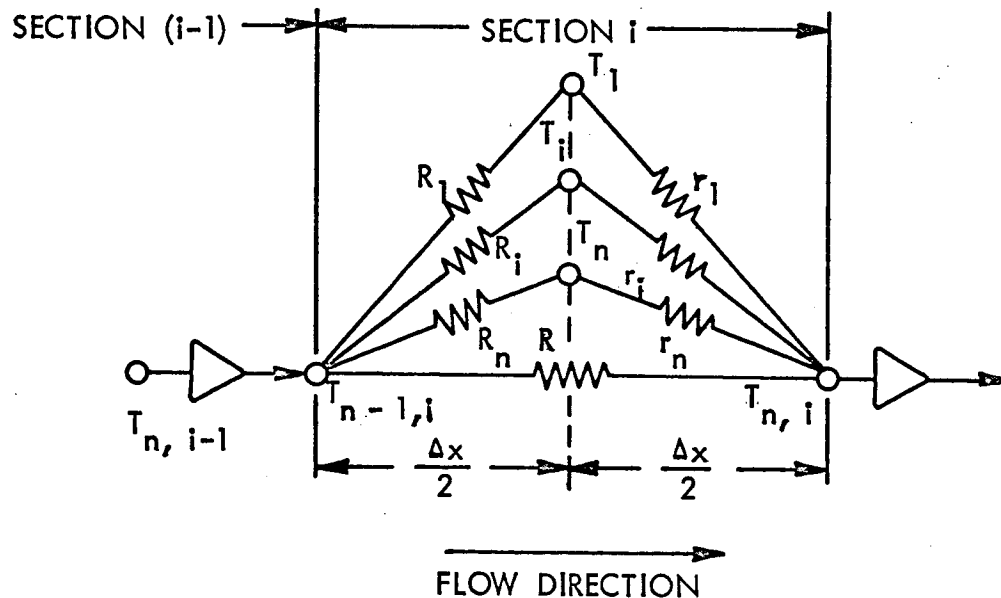
$c_p$  = fluid specific heat at constant pressure, Btu/lb-°F

$T_i$  = wall temperature, °F

$T_{n-1}$  = air temperature at inlet of the passage, °F

$T_n$  = air temperature at passage outlet, °F

2. With temperature gradients in the passage walls in planes normal to the flow direction as well as in the flow direction, the setup becomes somewhat more complicated.



at the inlet end

$$R_i = \frac{3600}{(h A)_i \left| \frac{1}{\beta} - e^{-\beta} (1 - e^{-\beta})^{-1} \right|}$$

and at the outlet end

$$r_i = \frac{3600}{(h A)_i \left| (1 - e^{-\beta})^{-1} - \frac{1}{\beta} \right|}$$

$$R = \frac{3600 (e^{\beta} - 1)}{a \left| (1 - e^{-\beta})^{-1} - \frac{1}{\beta} \right|}$$

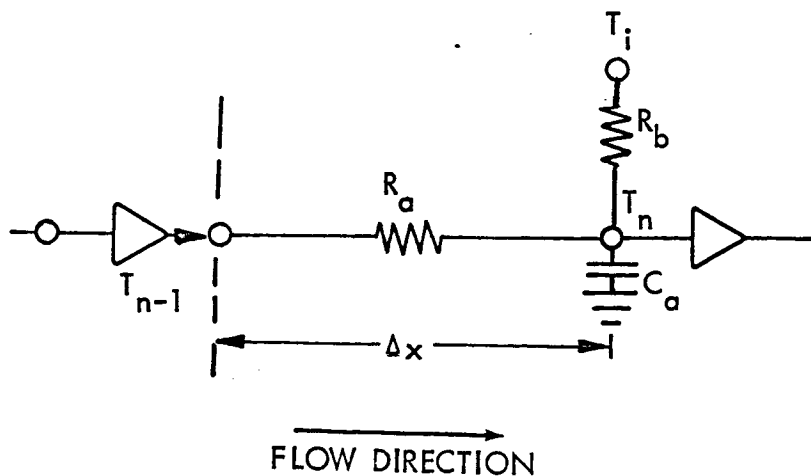
where

$$a = \sum_{i=1}^n (h A_h)_i$$

$$\beta = \sum_{i=1}^n \frac{(h A_h)_i}{W c_p}$$

and  $T_i$ ,  $T_{n-1}$  and  $T_n$  are defined as before.

3. If the conditions  $\theta_L/T_w \ll 1$  and  $C_a/C_w \ll 1$  are not met, the problem may be set up as follows:



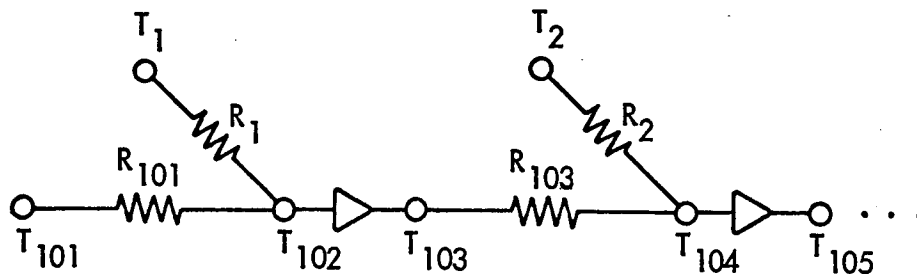
$$C_a = \rho c_v A_c \Delta x$$

$$R_a = \frac{3600}{W c_p}$$

$$R_b = \frac{3600}{h A_h}$$

This is a more general case; however, the conditions necessary for using Methods 1 or 2 are met in ordinary passage flow.

Derivations and plots of the equations presented above are given in Appendix C. The symbols  $\longrightarrow$  indicate that the inlet air temperature at section (i) is to be set equal to the outlet air temperature at section (i-1); i.e., to cause the temperatures to be influenced by upstream heat transfer but independent of downstream heat transfer. Failure to do this will cause the equations describing the network response to contain terms not present in the lumped parameter equations of the thermal system. For those cases where method 1 or 2 can be used, the computer is equipped to transfer the new temperature at the exit of one lump to the "new" temperature block of the inlet temperature of the next lump downstream. This transfer is made in the Function routine by the statement  $T(i) = T(i-1)$ . The statement  $TN(i) = TN(i-1)$  should also appear if it is desired to print out the temperatures since  $T(i)$  will be destroyed in the heat balance before printing occurs. As an example, consider the network:



In the FUNCT subroutine, the instructions

$$T(103) = T(102)$$

$$T(105) = T(104)$$

etc.

should appear. The capacitance of nodes 102, 104, etc. should be specified as zero. Nodes 103, 105, etc. should not be mentioned in the capacitor block.

In the event that method 3 is required, the same instructions must appear in the FUNCT subroutine, but the true capacitance must be specified for the fluid nodes. The dummy nodes ( $T_{n-1}$  in the figure on page 3-18) should not be mentioned in the capacitor block.

### Capacitor Values

The thermal capacity of a lump is calculated in all cases through the formula

$$C = A \delta \int_{T_1}^{T_2} \frac{\rho c}{T} dT + \int_0^{\delta} \rho c A dx \quad (3-16)$$

where:

$C$  = thermal capacity, Btu/°F

$\rho$  = density, lb/ft<sup>3</sup>

$c$  = specific heat, Btu/lb°F

In most cases of practical interest,  $\rho$  and  $c$  are constant over a large temperature range, and the above formula reduces to

$$C = \rho c \int_0^{\delta} A dx \quad (3-17)$$

where:

$$\int_0^{\delta} A dx = \text{volume of lump, ft}^3$$

### Variable Resistors and Capacitors

In many cases of practical interest, material properties, and hence resistor and capacitor values, are temperature dependent. To handle this problem the user can input the value as a function of temperature in curve form, or the machine can be given tables of the material properties and

directed to compute its own values of resistance and capacitance as described in Section V. To accomplish the latter, the Thermal Analyzer Program has a special library tape containing thermal properties of several commonly used structural materials, insulations, propellants, and pressurant gases. The data contained on this tape, and the functions required to call for it, are discussed in Section IV.

### Heat Inputs

Heat inputs to a particular node can be called out directly in the function subroutine as a constant or variable quantity, as described in Section IV. Many times, however, it is convenient to specify the heat input to a particular node in the form of a temperature through a resistor, where

$$R_k = \frac{T_i - T_k}{q_k}$$

If  $T_i \gg T_k$ , then  $q_k$  is essentially independent of  $T_k$ , and  $R_k$  can be computed by the relationship

$$R_k = \frac{T_i}{q_k}$$

As an example, to input 15 Btu/sec into a particular node set  $T_i = 15 \times 10^{10}$  (for 15 Btu/sec), and therefore

$$R_k = \frac{15 \times 10^{10}}{15} = 10^{10} \frac{\text{sec } ^\circ\text{F}}{\text{Btu}}$$

## IV - FUNCTIONS AND SPECIAL SUBROUTINES

The FUNCT subroutine is the most important and the most powerful section of the Thermal Analyzer Program. This subroutine contains a listing of all arithmetic operations, curve interpolations, and special functions including radiation, which are to be performed during program execution. The functions are executed at the start of each cycle (before the heat balance) in the order specified, a characteristic which becomes important when the execution of one function involves the result of another. This section presents a brief description of the functions and special subroutines available, what they are capable of, and where input errors are most likely to occur. The FUNCT subroutine input format is described in Section V.

DEFINITION OF TERMS

In the following discussion, several terms are used repeatedly to refer to the various elements of a given function callout. These terms are defined below:

1. Floating-Point Number - All numerical values are input in floating point, and as such must contain a decimal point. The number 30.6 is an example. For very large or very small numbers, such as  $10^{10}$  or  $10^{-10}$ , the capital letter E is used to signify a power of 10. For example, 1.30E6 means  $1.30 \times 10^6$  and 6.91E-4 means  $6.91 \times 10^{-4}$ .
2. Fixed-Point Number - Fixed point numbers are integers, either positive or negative, and as such are characterized by the absence of a decimal point. They are used to designate data sub-blocks and in numerous instructions to indicate the number of steps or items involved in the execution of that instruction.
3. Literal Numbers - These elements are characterized by a letter followed by a number in parentheses, such as T(6), R(14), etc. These are the addresses of the various items of numerical data, i.e., the location in the computer core where the data is stored. They tell the computer where to look for the numerical data required to perform a given instruction. As a result of this, they are referred to as "addressable elements."

In discussing the various functions the following notations are used:

1. When the variables of a function are arbitrary circuit elements, the independent variable is denoted by X and the dependent variable by Y.
2. N denotes the designation number of a data sub-block.
3. Unless otherwise specified, the letters A, B, C, D, E, F, G denote floating point constants whose values may appear explicitly in the function callout, or may be stored in an addressable element.
4. When the variables of a function are temperatures, Y refers to the temperature at time  $\theta + \Delta \theta$  and X refers to the temperature at time  $\theta$ .

#### LIST OF ADDRESSABLE ELEMENTS

Each item of numerical data of interest to the user is assigned an address which can then be used to refer to that item. A list of these addresses follows:

- |           |   |
|-----------|---|
| T(i)      | "Old" temperature of the i-th node (see below)  |
| TN(i)     | "New" temperature of the i-th node  |
| R(i)      | Resistor number i   |
| C(i)      | Capacitor number i  |
| RC(i)     | The RC product at C(i)  |
| Q(i)      | The arbitrary heat input into C(i)  |
| P(LN + i) | The i-th number in the data block whose designation number is N, and where LN = LOC(N) (see Section V). In determining the i-th number the designation number itself is not counted. Also, when specified in this manner, the PER in a periodic curve is not counted. |
| M(i)      | The i-th miscellaneous element, where   |
|           | M(1) Current time, $\theta$   |
|           | M(2) Initial time   |

- M(3) Final time
- M(4) Print interval
- M(5) Computing interval,  $\Delta\theta$
- M(6) Minimum RC product of the network
- M(7) The factor by which M(6) is multiplied to produce M(5). Unless changed by the variables, a factor of 0.25 is used.
- M(8) Print trigger, normally zero. If a variable puts any non-zero into this storage, a print-out of the output block will result at the end of that cycle.
- M(9) The number of that capacitor which produces the minimum RC product.
- M(11) The time of the next regular print
- M(12) The recovery temperature in the Eckert Aerodynamic Heating Subroutine (see Appendix A).
- M(14) The computing interval used during the previous cycle, ie.,  $\Delta\theta(\theta - \Delta\theta)$ .
- M(15) The product of M(6) and M(7). Ordinarily,  $M(15) = M(5)$ . However, M(5) may be reduced at a print time.
- M(16) The total number of computing cycles since the problem was begun.

The missing elements M(10) and M(13) were used in a former version of the Thermal Analyzer Program, written in machine language.

The temperature designated as T(i) is the "old" temperature of node i and is usually used as the independent variable when calculations involving temperature are performed, eg., heat balances. TN(i) is the "new" temperature of node i and is used in the functions as the dependent variable, or the new calculated temperature. At the end of each heat balance T(i) is set equal to TN(i).



MATHEMATICAL OPERATIONS

Any of the built-in subroutines (or functions) of the FORTRAN IV system may be used as an arithmetic statement in the FUNCT routine. Because of the many operations available, only a few will be mentioned here. For a more detailed listing, the user is referred to the FORTRAN reference manual.

The arithmetic operation symbols +, -, \*, /, \*\* denote addition, subtraction, multiplication, division, and exponentiation, respectively. Unless changed by the use of parentheses, the order of computation is understood to be as follows:

- |     |                             |           |
|-----|-----------------------------|-----------|
| (a) | exponentiation              | (**)      |
| (b) | multiplication and division | (* and /) |
| (c) | addition and subtraction    | (+ and -) |

For example, the expression

$$Y = A + B/C - D**E*F - G$$

will be taken to mean

$$Y = A + \frac{B}{C} - D^E F - G$$

Parentheses may be used to override the order in which the operations are to be computed. If parentheses appear, the expression within the innermost parentheses is computed first, following the order of computation given above. The computation then proceeds outward to the next parentheses, and so forth. As examples, the expression

$$Y = (A + B)/C - D**(E*F) - G$$

will be taken to mean

$$Y = \frac{A + B}{C} - D^{EF} - G$$

and the expression

$$Y = A + (B/(C - D))^{*(E*F - G)}$$

will be taken to mean

$$Y = A + \left( \frac{B}{C-D} \right)^{EF-G}$$

In addition to these arithmetic operations, the common mathematical functions such as logarithm, exponential, sine, cosine, square root, arctangent, and absolute value are available to the program user. Since their use is self-explanatory, they are listed below with only a brief explanation.

<u>Function</u>	<u>Description</u>
LOG	Logarithm to the base e
EXP	Powers of e or exponential
SIN	Sine of an angle whose measure is given in radians
COS	Cosine of an angle whose measure is given in radians
SQRT	Square root
ATAN	Arctangent or angle in radians of a given tangent value
ABS	Absolute value

As an example,

$$Y = A + \text{SQRT}(B^{**}C)$$

means

$$Y = A + \sqrt{B^C}$$

In the FORTRAN language it is also possible to have functions of functions. As an example

$$Y = \text{EXP}(\text{SQRT}((\text{COS}(2.*A)) **2. + B))$$

means

$$Y = e^{(\text{COS}^2 2A + B)^{1/2}}$$

### CURVE INTERPOLATION

One of the most commonly used functions involves some sort of curve interpolation, of which three types are available, viz., linear, parabolic, and linear bivariate. With curve interpolation, any addressable element listed above can be made a function of any other, or others, including itself. In addition to specifying simple interpolation, the instructions may be modified to provide for multiplying the curve value by some other number which can be either a fixed factor or some other variable.

A description of the various interpolation routines follows. The use of these routines will be further illustrated by the example problems of Section VI.

#### Linear Interpolation

This is the simplest and most commonly used interpolation routine. The callout is

$$Y = \text{LIN}(X, N)$$

where

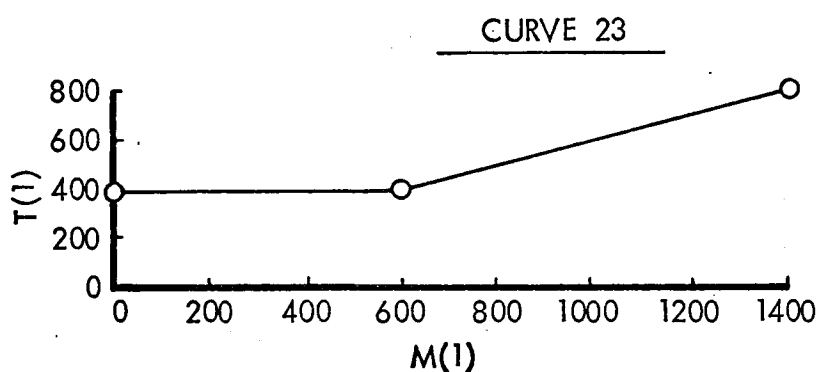
Y = linear function of X given by curve N

As an example, consider

$$T(1) = \text{LIN} (M(1), 23)$$

The temperature of node 1 is a linear function of time given by curve 23.

Curve 23 might appear as shown below:



The curve would be described on input data sheets as follows:

COLUMN

→	1	5	10	15	25	35	45	55	65	69	72
DEC			23								4001
DEC06				0.	400.	600.	400.	1400.	800.		4002
DEC01				0.							4003
DEC			-23								4004

The input format is described in detail in Section V. Briefly, a card containing DEC in columns 1, 2, and 3 and the curve designation number in columns 6 through 10 must precede the data, and a card containing DEC in columns 1, 2, and 3 and the negative of the curve designation number in columns 6 through 10 must terminate the curve. The curve designation numbers

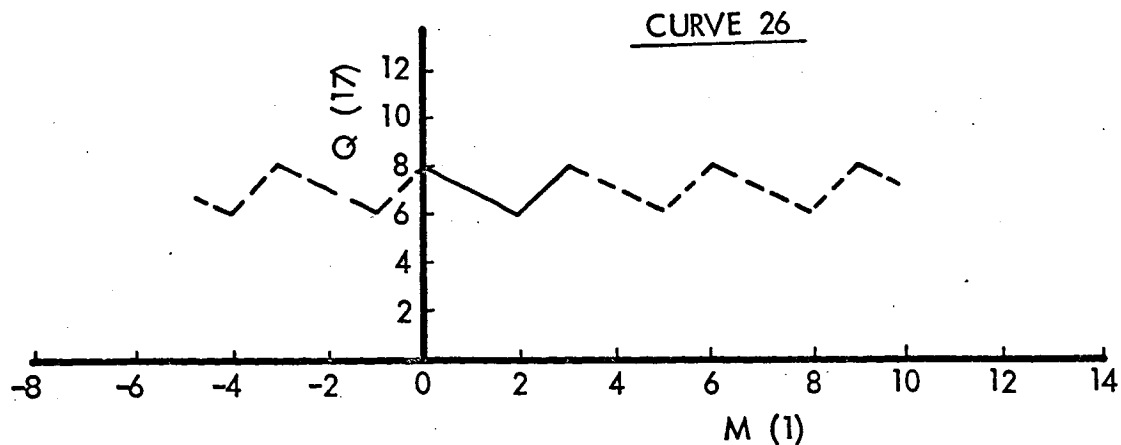
are arbitrary. The actual curve is described by listing the coordinates of the points circled on the plot. Each independent variable must immediately precede the corresponding dependent variable, and the independent variables are listed in increasing order. The integers in column 5 specify the number of floating point values on that card. The zero on the third card is a flag indicating the end of the data. Either a four- or five-digit card sequence number, at the user's discretion, is placed in columns 68 through 72.

In the above example, if current time,  $M(1)$ , lies between 0. and 600., interpolation for  $T(1)$  takes place along the straight line connecting these two points. If  $M(1)$  lies between 600. and 1400., interpolation takes place along the straight line connecting these two points. If  $M(1)$  is less than 0., or greater than 1400., the case is terminated.

As mentioned previously, it is also possible to have periodic functions. An example of a periodic curve is the external heat input to a shell node of an orbiting satellite. The fact that a curve is periodic does not alter the function specification; only the curve itself need be modified. Consider the example

$$Q(17) = \text{LIN}(M(1), 26)$$

where curve 26 is to be described by linear interpolation and is periodic. This curve is described to the program by the period (3 sec) followed by the curve itself as shown below.

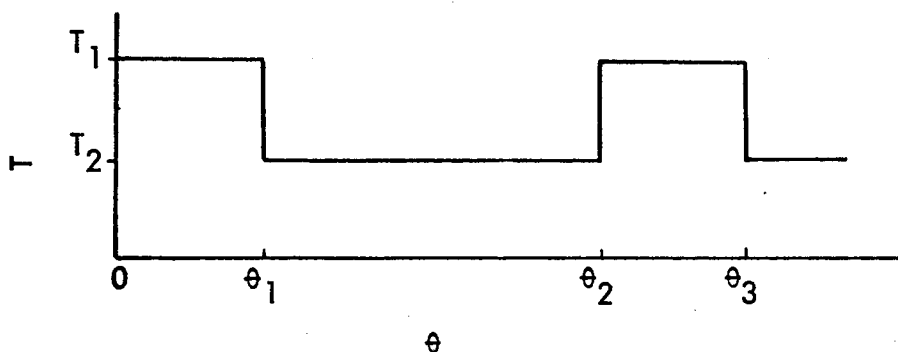


COLUMN

	1	5	10	15	25	35	45	55	65
DEC			26						
PER				3.					
DECO6				0.	8.	2.	6.	3.	8.
DECO1				0.					
DEC		-26							

The interpolation itself takes place exactly as in the linear interpolation described above, with the exception that the independent variable cannot lie outside the curve since the curve is understood to be indefinitely extended in both directions as indicated in the diagram.

When fitting a linear curve to a sharp discontinuity, such as a heating cycle,



the input specification for the curve should list the following coordinates:

0. ,  $T_1$   
 $\theta_1$  ,  $T_1$   
 $\theta_1$  ,  $T_2$   
 $\theta_2$  ,  $T_2$   
 $\theta_2$  ,  $T_1$   
 $\theta_3$  ,  $T_1$   
 $\theta_3$  ,  $T_2$   
 etc.

If the program finds itself computing at a time at which one of the discontinuities occurs, it will recognize the former value of the dependent variable. For example, if a computing point should occur at  $\theta_1$  or  $\theta_3$ ,  $T_1$  will be chosen as the proper temperature; if a computing point occurs at  $\theta_2$ ,  $T_2$  will be chosen. This problem will occur only if a computing time point occurs exactly at a point of discontinuity.

### Parabolic Interpolation

Where additional accuracy is desired, parabolic interpolation may be employed. However, it requires greater care in the selection of input points as discussed below. The callout is

$$Y = \text{PAR}(X, N)$$

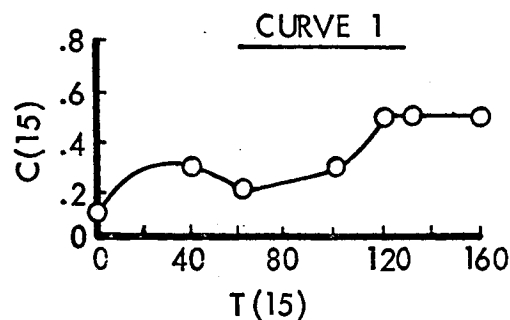
where

$$Y = \text{parabolic function of } X \text{ given by curve } N$$

As an example, consider

$$C(15) = \text{PAR}(T(15), 1)$$

The capacitance of node 15 is a function of the temperature of node 15 as given by curve 1. Curve 1 is to be described by parabolic interpolation. The curve and the data points input to the program are shown below:



COLUMN

	1	5	10	15	25	35	45	55	65
DEC			1						
DEC06			0.		0.	40.	.3	60.	.2
DEC06			100.		.3	120.	.5	125.	.5
DEC03			160.		.5	0.			
DEC			-1						

If the independent variable,  $T(15)$ , lies between 0. and 60., interpolation takes place by using that interpolating parabola which passes through the first 3 points and whose axis is parallel to the Y-axis. If  $T(15)$  lies between 60. and 120., the interpolating parabola is that parabola passing through the 3rd, 4th, and 5th points and parallel to the Y-axis. If  $T(15)$  lies between 120. and 160., the interpolating parabola is that parabola passing through the 5th, 6th, and 7th points and parallel to the Y-axis. If  $T(15)$  is off the curve (less than 0. or greater than 160.) the case is terminated.

These consecutive interpolating parabolas having only one point in common make it possible to describe discontinuous curves as well as curves which are made up of parabolic segments and linear segments (as curve 1). However, this manner of choosing parabolas always requires that an odd number of points be used in the curve description.

Since the parabolic curve-interpolation subroutine fits a curve to each successive series of three points, the choice of curve points is very critical. It must be emphasized that any sharp discontinuity should provide the end of one and the beginning of another set of three points. For example, Figure 4-1 shows the different interpretations of the same curve which would be given by different divisions. Note the extreme example of faulty interpolation which can occur in the case of a very steep curve.

When fitting a parabolic curve to a sharp discontinuity, such as the heating cycle described under Linear Interpretation in this section,



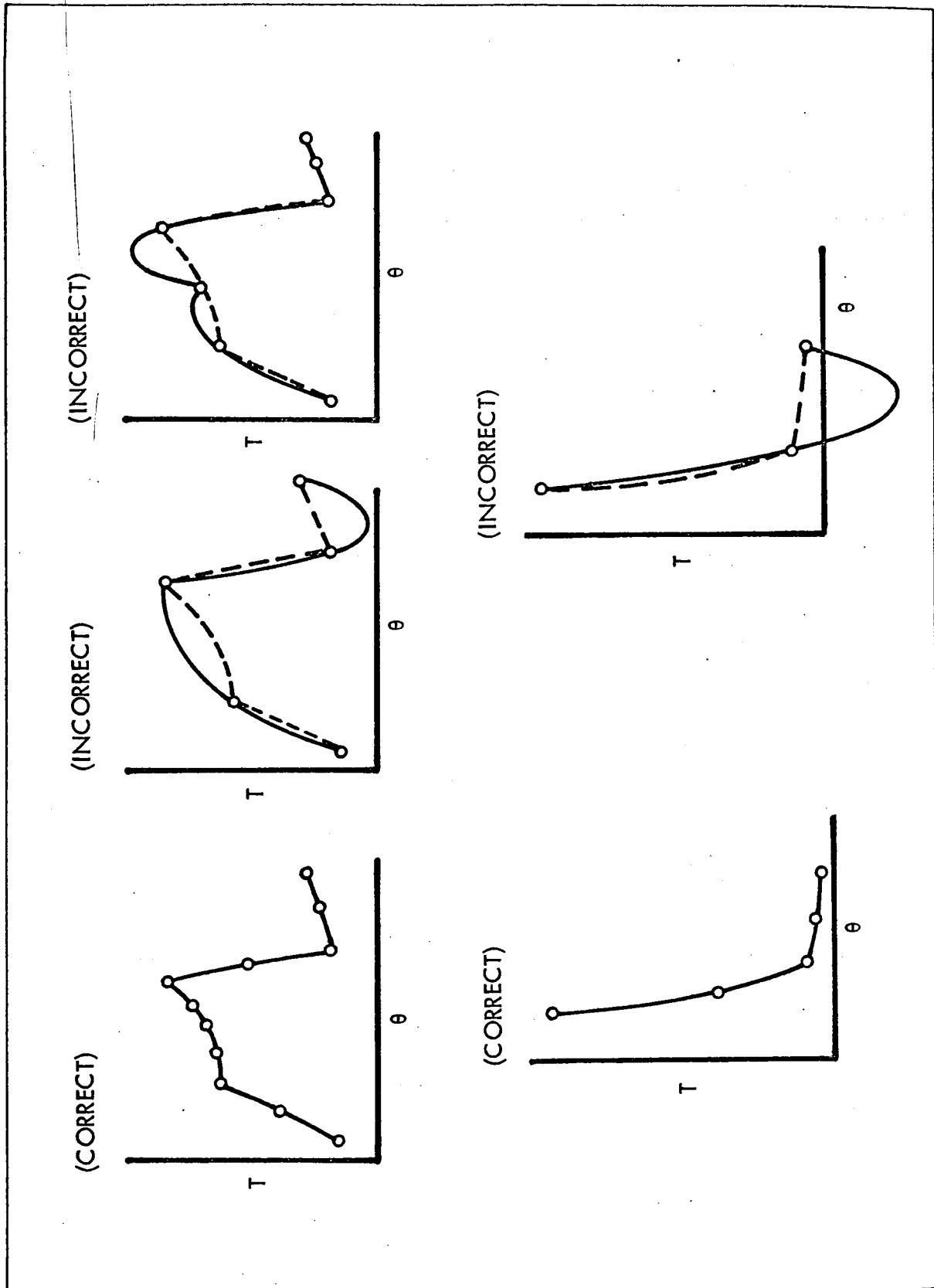
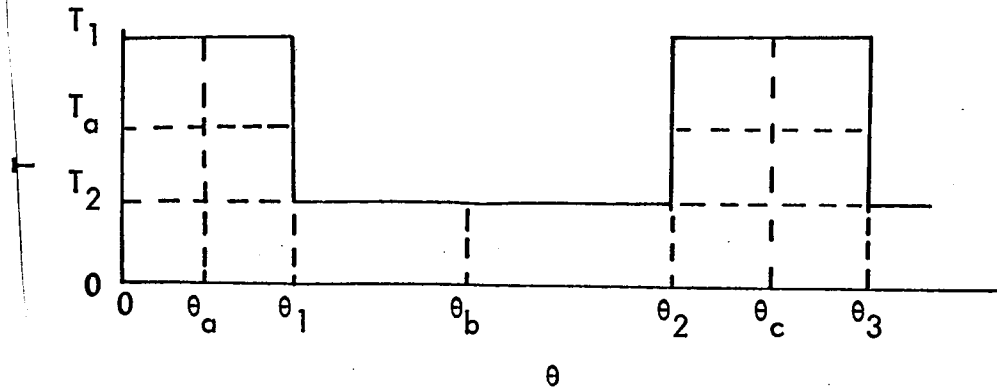


Figure 4-1. Correct and Incorrect Inputs for Curves Described by Parabolic Interpolation



$$T_2 < T_a < T_1$$

$$0 < \theta_a < \theta_1 < \theta_b < \theta_2, \quad \text{etc.}$$

the input specification for the curve should contain the following coordinates:

$$0, \quad T_1$$

$$\theta_a, \quad T_1$$

$$\theta_1, \quad T_1$$

$$\theta_1, \quad T_a$$

$$\theta_1, \quad T_2$$

$$\theta_b, \quad T_2$$

$$\theta_2, \quad T_2$$

$$\theta_2, \quad T_a$$

$$\theta_2, \quad T_1$$

$$\theta_c, \quad T_1$$

$$\theta_3, \quad T_1$$

etc.

If the program should find itself computing at a time which coincides with one of the discontinuities, it will recognize the previous value of the dependent variable. For example, for the above cyclic temperature, if the computing time point should occur at  $\theta_1$  or  $\theta_3$ ,  $T_1$  will be chosen as the proper temperature; if the program should be computing at time  $\theta_2$ ,  $T_2$  will be chosen.

### Bivariate Interpolation

Frequently, there are situations where a variable is a function of more than one independent variable. Examples of this are:

- (a) Internal losses in electronic components, which are commonly functions of current consumption and temperature.
- (b) Thermodynamic and transport property data, which are usually temperature and pressure dependent.

The Thermal Analyzer Program is equipped to handle such problems through use of the linear bivariate interpolation routine. The callout is

$$Y = BIV (X1, X2, N)$$

where

Y is a bivariate function of X1 and X2 given by Table N.

In setting up a table to be described by bivariate interpolation, the first word on the first line following the table designation number must be uuuvvv. where uuu is a three-digit number equal to the number of rows in the table and vvv is a three-digit number equal to the number of columns in the table. Do not count the row and column that uuuvvv appears in. Following the first word of the first line the values of the independent variable X2 are listed. For each of these values there is an entry below it corresponding to the value of the independent variable X1 appearing at the left. In other words, the data appear on the input sheet just as one might tabulate it on a sheet of paper, with the addition of the number uuuvvv. The table need not be terminated with a flag indicating the end of the data since the quantity of data is specified by the number uuuvvv.

As an example of the use of bivariate interpolation, consider the problem of the internal heat dissipation of a battery, where the losses are a function of both the battery temperature and the current consumption. In this example, the battery will be designated as node 3. It will be assumed that the current is a known function of time and is to be linearly interpolated from curve 1. The battery losses in watts are tabulated below:

LOSSES (WATTS) VS. LOAD (AMPS)

Current ~ amps →	0.	1.0	2.0	4.0	6.0
↓ Temperature ~ °F					
10.	0.	1.5	3.3	8.1	14.5
40.	0.	1.3	2.8	7.0	12.6
70.	0.	1.1	2.4	5.9	10.7
100.	0.	0.9	1.9	4.8	8.8
130.	0.	0.7	1.5	3.7	6.9

The bivariate curve will be designated as Table 8 and is described in the data block as follows:

COLUMN	1	5	10	15	25	35	45	55	65
→									
DEC		8							
DECO6		005005.			0.	1.0	2.0	4.0	6.0
DECO6			10.		0.	1.5	3.3	8.1	14.5
DECO6			40.		0.	1.3	2.8	7.0	12.6
DECO6			70.		0.	1.1	2.4	5.9	10.7
DECO6			100.		0.	0.9	1.9	4.8	8.8
DECO6			130.		0.	0.7	1.5	3.7	6.9
DEC		-8							

The function specification for this example is

$$Q(3) = BIV(T(3), LIN(M(1), 1), 8) * .000946$$

where the constant is the conversion factor from watts to Btu/sec. In the function callout the independent variables, current and temperature, must appear in the order listed because Table 8 is set-up with temperature values listed in the first column. Otherwise, the program would attempt to horizontally interpolate using T(3) as independent variable and would run off the curve since the values listed range only from 0 to 6.

If there are more than five values of the independent variable X2, the data cannot be listed on input sheets in the tabular arrangement shown above because each card is restricted to a maximum of six floating point entries. In that event, the elements of the table are listed on input sheets in consecutive order, reading from left to right on each row and down each column of the table. To illustrate, consider the addition of a sixth and seventh column to the tabulation of "Losses vs. Load" as shown below:

Current ~ amps →	0.	1.0	2.0	4.0	6.0	8.0	10.0
↓ Temperature ~ °F							
10.	0.	1.5	3.3	8.1	14.5	21.8	30.3
40.	0.	1.3	2.8	7.0	12.6	19.7	28.1
70.	0.	1.1	2.4	5.9	10.7	16.5	25.0
100.	0.	0.9	1.9	4.8	8.8	14.2	22.2
130.	0.	0.7	1.5	3.7	6.9	12.1	20.0

Table 8 might appear on the input sheet as follows:

COLUMN

→	1	5	10	15	25	35	45	55	65
DEC			8						
DECO6			005007.		0.	1.0	2.0	4.0	6.0
DECO2			8.0		10.0				
DECO6			10.0		0.	1.5	3.3	8.1	14.5
DECO2			21.8		30.3				
DECO6			40.0		0.	1.3	2.8	7.0	12.6

COLUMN	1	5	10	15	25	35	45	55	65
DECO2			19.7		28.1				
DECO6			70.0		0.	1.1	.2.4	5.9	10.7
DECO2			16.5		25.0				
DECO6			100.		0.	0.9	1.9	4.8	8.8
DECO2			14.2		22.2				
DECO6			130.		0.	0.7	1.5	3.7	6.9
DECO2			12.1		20.0				
DEC			-8						

Although six quantities may be listed on each card, the method shown above is preferred since the input is easier to read. The only requirement is that the table elements be listed in proper order.

#### RADIATION FUNCTIONS

As mentioned in Section III, "Calculation of Circuit Parameters," the machine is equipped to compute radiation resistors by the formula

$$R = \frac{1}{\sigma K_{\text{rad}} \left[ (T_1 + 460)^2 + (T_2 + 460)^2 \right] \left[ (T_1 + 460) + (T_2 + 460) \right]} \quad (4-1)$$

where the user computes and inputs to the program in the FUNCT subroutine the value

$$K_{\text{rad}} = \frac{\epsilon_{12} A_1 F_{12}}{3600} \quad \text{for } R \sim \frac{\text{sec } ^\circ\text{F}}{\text{Btu}} \quad (4-2)$$

Three radiation resistor functions are available as discussed in the following sections.

#### Radiation With Constant Factor

This is the simplest and most commonly used radiation function. It is used in those situations where a fixed  $K_{\text{rad}}$  is applicable. The basic callout is:

$$R(A) = \text{RAD} (B, C, K_{\text{rad}})$$

where A is the designation number of the resistor connecting nodes B and C.

As an example, consider the case of a one square foot plate with a surface emissivity of 0.8 radiating to outer space (shape factor  $F = 1.0$ ). For this case,

$$K_{\text{rad}} = \frac{(0.8)(1.0)(1.0)}{3600} = 2.22 \times 10^{-4}$$

If the resistor designation number is 106 and the plate and space are nodes 7 and 100, the function callout is

$$R(106) = \text{RAD}(7, 100, 2.22\text{E} - 4)$$

The order in which the two nodes are specified is immaterial since the program merely uses this information to solve for the resistor value using equation 4-1.

#### Radiation With Variable Factor

This is the same as the previous function except the value of  $K_{\text{rad}}$  is a variable. Examples of this are cases where the system geometry varies with time, or, more commonly, where the surface emissivity is temperature dependent. The callout is:

$$R(A) = \text{RAD}(B, C, X)$$

where the value of  $K_{\text{rad}}$  is stored in X, which may be either an addressable circuit element or a curve interpolation callout.

Two examples of the radiation with variable factor instruction are:

$$R(106) = \text{RAD}(7, 100, R(200))$$

$$R(106) = \text{RAD}(7, 100, (\text{LIN}(T(7), 13)))$$

In the first example, the value of  $K_{\text{rad}}$  has been temporarily stored in an unused resistor location. This procedure is often used when the value of  $K_{\text{rad}}$  is to be changed through a restart, as described in Section V. In the second example, the value of  $K_{\text{rad}}$  is linearly interpolated from curve 13 using the temperature of node 7 as independent variable. This instruction is convenient when the surface emissivity is temperature dependent.

#### Radiation With Matrix

In using the radiation functions described above, it is necessary to know  $K_{\text{rad}}$  in advance, and this in turn requires a knowledge of the geometric view factor  $F_{12}$  and the emissivity factor. Calculation of shape factors is beyond the scope of the program and is not covered here (see, however, references 1 and 2).

In most cases, the emissivity factor is computed by one of the following formulas:

#### infinite parallel plate

$$\epsilon_{12} = \frac{1}{\frac{1}{\epsilon_1} + \frac{1}{\epsilon_2} - 1}$$

#### concentric cylinder or sphere with $A_2 > A_1$

$$\epsilon_{12} = \frac{1}{\frac{1}{\epsilon_1} + \frac{A_1}{A_2} \left( \frac{1}{\epsilon_2} - 1 \right)}$$

#### two surfaces whose size is small compared with their distance apart

$$\epsilon_{12} = \epsilon_1 \epsilon_2$$

#### surface $A_1$ much smaller than, and completely enclosed by, surface $A_2$

$$\epsilon_{12} = \epsilon_1$$

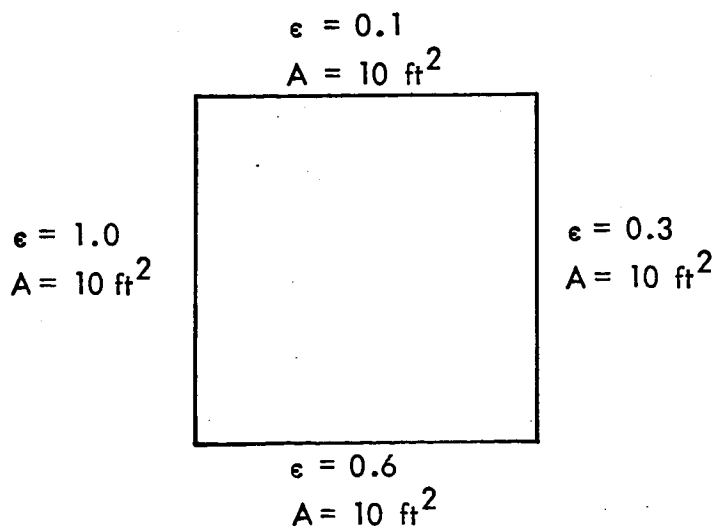


However, for those problems where several nonparallel surfaces are involved and the above formulas are not considered satisfactory, the program is equipped to compute the overall shape factor  $\bar{F}_{12}$  in contrast to the geometrical shape factor  $F_{12}$ . The method used is discussed in detail in several heat transfer texts, such as McAdams (Reference 3), and will not be covered here. The method basically is to set up the radiation energy interchange equations and solve them through use of determinants. It is to be noted that the machine performs the calculation of  $K_{\text{rad}}$  only once, and hence the various quantities such as emissivity must all be assumed to be constants.

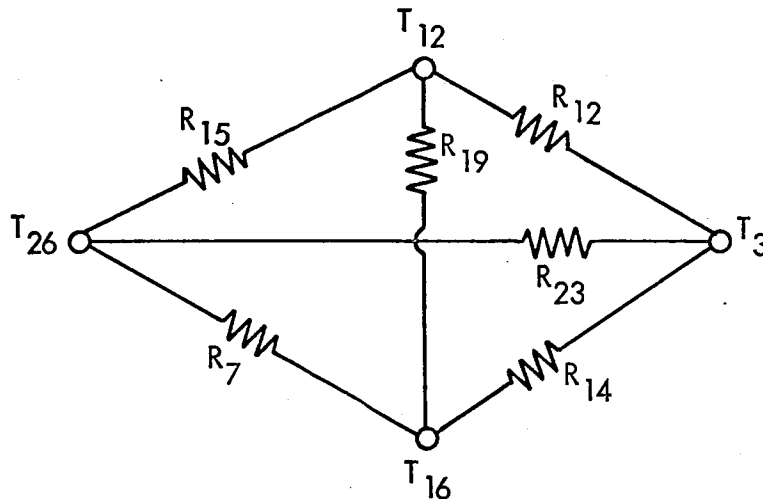
The Radiation with Matrix callout is

$$R(A) = \text{RRM}(B, C, N)$$

where A is the designation number of the resistor connecting nodes B and C, and N is the designation number of the table containing the data used to compute  $K_{\text{rad}}$ . Since this routine is used where several surfaces are involved, table N will appear in several resistor callouts. Also, it is possible to have more than one such system in a given network, and to have the same surface appear in more than one matrix. Consider the case of four walls arranged in a square pattern:



The shape factors have been computed to be 0.4 between opposite walls, and 0.3 between adjacent walls. The corresponding circuit is shown below. The node and resistor number assignments are completely arbitrary.



The RRM callouts for the above network are:

$$R(15) = \text{RRM}(12, 26, 6)$$

$$R(19) = \text{RRM}(12, 16, 6)$$

$$R(12) = \text{RRM}(12, 3, 6)$$

$$R(23) = \text{RRM}(26, 3, 6)$$

$$R(7) = \text{RRM}(16, 26, 6)$$

$$R(14) = \text{RRM}(16, 3, 6)$$

Table 6 contains the following information:

- the order of matrix of configuration factors, which in this example is 4.
- the matrix of configuration factors (row order)
- each node number and the area, emissivity, and reflectivity of each of these nodes.

For a 4th order matrix, the input would be as shown below. The subscripts refer to the order in which the nodes are listed, and are not necessarily the node or resistor designation numbers.

$$\begin{matrix}
 (A_1 F_{11} - A_1 / \rho_1) & A_1 F_{12} & A_1 F_{13} & A_1 F_{14} \\
 A_2 F_{21} & (A_2 F_{22} - A_2 / \rho_2) & A_2 F_{23} & A_2 F_{24} \\
 A_3 F_{31} & A_3 F_{32} & (A_3 F_{33} - A_3 / \rho_3) & A_3 F_{34} \\
 A_4 F_{41} & A_4 F_{42} & A_4 F_{43} & (A_4 F_{44} - A_4 / \rho_4)
 \end{matrix}$$

$$\left. \begin{matrix}
 N_1, A_1, \epsilon_1, \rho_1 \\
 N_2, A_2, \epsilon_2, \rho_2 \\
 N_3, A_3, \epsilon_3, \rho_3 \\
 N_4, A_4, \epsilon_4, \rho_4
 \end{matrix} \right\}$$

the order in which the nodes are listed must correspond to the order of matrix rows.

where  $N_i$  = node number i  
 $A_i$  = area of node i  
 $\epsilon_i$  = emissivity of node i  
 $\rho_i$  = reflectivity of node i, usually equal to  $(1 - \epsilon_i)$

The input for this particular example is shown below. (The reflectivity of node 26 has been taken as 0.01 to avoid division by zero).

COLUMN	1	5	10	15	25	35	45
DEC			6				
DECO4				4.			
DECO4			-11.1		3.0	4.0	3.0
DECO4			3.0		-14.3	3.0	4.0
DECO4			4.0		3.0	-25.0	3.0
DECO4			3.0		4.0	3.0	-1000.

COLUMN	1	5	10	15	25	35	.45
DECO4			12.		10.	.10	.90
DECO4			3.		10.	.30	.70
DECO4			16.		10.	.60	.40
DECO4			26.		10.	.99	.01
DEC		-6					

Note that, with the exception of the curve designation numbers, all values in the table are input as floating point numbers.

The machine computes the radiation K factor by the formula

$$(K_{\text{rad}})_{ij} = \frac{1}{3600} \frac{\epsilon_i \epsilon_j}{\rho_i \rho_j} A_i A_j \left| \frac{D_{ij}}{D} \right|$$

where:

D is the determinant of the matrix

$D_{i,j}$  is the minor of the element  $(i,j)$ , i.e., the determinant of the matrix formed by removing the  $i$ -th row and the  $j$ -th column.

The absolute value sign around the ratio  $D_{ij}/D$  comes about because as the equations were written, the machine could compute a negative K-factor, whereas the direct solution of the simultaneous equations involved results in positive K-factors.

#### CONVERGENCE AND STEADY-STATE SUBROUTINES

Since most problems to be solved by the Thermal Analyzer involve transient analysis, the initial values chosen for resistance, capacity, and temperature assume some importance. If it is desired to begin a transient problem at some steady-state condition and then apply variable boundary conditions (as would often occur in aerodynamic heating problems), it is very important that the initial conditions approximate the true steady-state conditions as nearly as possible before the transient conditions are applied. In many cases, the starting temperatures are uniform throughout the network and thus present no problem. However, many problems, such as

the transient heating of a reentry vehicle, involve nonuniform starting temperatures. To handle this problem, the converge (CVG) function is used, the callout being

CALL CVG(A, N, M)

where

$|T_{i,\Delta\theta} - T_i| \leq$  A = degree of convergence (defined below).

N = maximum number of iterations to be executed in the convergence attempt.

M = number of iterations between prints of the output block.

When this function is encountered in the FUNCT routine, the heat balance and list of functions are evaluated repeatedly with time held constant (although with a finite computing interval) until the temperatures reach the required convergence, i.e., until the largest temperature difference of any node on consecutive passes is less than A (usually input as 0.005). When the temperatures have converged, the convergence function is removed from the function list, the regular output block is printed with "time" set to the number of iterations required for convergence and with " $\Delta\theta$ " set to the designation number of the last node to converge. The case is then executed in the normal matter. If the temperatures fail to converge after N iterations, the case is discontinued, with a print of the regular output block with "time" set to N.

When using the CVG function, it should be remembered that the degree of convergence, A, is not necessarily the maximum deviation from the true converged temperatures, but merely the maximum temperature change of any node between two successive cycles. Consequently, it is quite possible that the deviation from the converged temperature could be several orders of magnitude greater than A and could amount to several degrees. For this reason, a small value of A, such as 0.005, should be used.

As input above, the CVG uses the capacitor values as input. To speed the convergence process, an optional form of the input can be used, namely

## CALL CVG(A, N, - M)

where the negative sign on M is a flag which causes the convergence iteration to be executed with all capacitors set to zero. However, some care must be exercised when using zero capacitors in those cases which involve radiation resistors. Because radiation resistors vary inversely as the cube of the corresponding temperatures, they are very sensitive to small temperature changes. If the converged temperatures are very much different from the initial guesses, oscillations could be set up which will prevent convergence. In most cases, however, a reasonable set of initial temperatures should converge even if the zero capacitor option is used in cases involving radiation.

When the CVG function is used to solve purely steady-state cases, it is necessary to specify some non-zero final time in the time block to guarantee that the CVG function is executed properly. The value used should be of the order of the minimum RC product of the network to guarantee that a few "normal" cycles, i.e., with progressive time, are computed.

In addition to the CVG routine, a similar function (STS) is available which operates on the heat balance only and does not execute the function list during each iteration. Therefore, if there are radiation resistors or heat inputs called out in the functions, it is generally preferable to use the CVG subroutine. The steady-state function callout

## CALL STS (A)

assigns zeros to all capacitors, and causes iteration through the circuit to proceed until the largest temperature difference of any node on consecutive passes is less than A. The original values of the capacitors are then restored, a flag is set to ignore the steady-state function in ensuing passes, and the case continued.

MAXIMUM-MINIMUM SUBROUTINE

In addition to the temperature-time history of the various nodes, it is often desired to know also the maximum and minimum temperatures of these nodes, and to be able to obtain them without having to search through

the normal output data. This is especially true in large programs where several hundred temperatures may be involved.

This problem is handled by use of the maximum-minimum function (MMF), the callout being

```
CALL MMF(  $\theta_i$ ,  $\theta_f$ , N, S)
```

where  $\theta_i$  and  $\theta_f$  are explicit (floating point) numbers, or addressable elements. During the time interval  $\theta_i < \theta < \theta_f$ , the maximum-minimum function records all local maximum and minimum temperatures of all nodes whose designation numbers are listed in data table N. The value S indicates the frequency with which the program is to search the output to determine the maximum and minimum temperatures, e.g., a 1 requires a search every cycle, a 2 requires a search every second cycle, etc. The node designation numbers appear in table N as floating point numbers. This table is terminated by a zero flag. To illustrate the use of the MMF function, assume that over the time interval 0-100 sec, the program is to conduct a search every other computing cycle to determine the maximum and minimum temperatures of nodes 7, 15, 83, and 94, which will be listed in Table 3. The table appears as follows:

DEC	3					
DEC05		7.	15.	83.	94.	0.
DEC	-3					

The instruction in the FUNCT subroutine is

```
CALL MMF(0., 100., 3, 2)
```

Generally, the search is required for the entire time span of the case and the following instruction would be used:

```
CALL MMF (M(2), M(3), 3, 2)
```

M(2) and M(3) are the initial and final times for the case, respectively.

The maximum and minimum temperatures are automatically printed following the regular time history print. This maximum-minimum output contains the range of the function (since there can be more than one MMF in a case), followed by a table with five non-zero columns. The first column is the designation number of the nodes (in the same order as given in the input table N), the second column is the list of the local maximums, the third column is the list of local minimums, the fourth column contains the times of the local maximums, and the fifth column contains the times of the local minimums. The MMF subroutine is illustrated in Example #2 of Section VI.

Only distinct local maximums and minimums are recorded. Therefore, if the rate of temperature change with time for a node does not change sign during the range of the MMF function, no maximum or minimum is recorded for that node. On the other hand, if the temperature of a node, after increasing for a while, remains constant for a time, and then decreases, a maximum would be recorded at the last time point for which the temperature was constant.

As a result of the manner in which the computer handles MMF data, there is a limitation on the amount of such data which can be obtained from a single case. Specifically, there must be less than 6000 maximums and minimums (representing 3000 cycles) in order for all of them to be printed. (A case with 200 nodes undergoing 20 temperature cycles would total  $2 \times 200 \times 20 = 8000$  and this exceeds this limit). If the total exceeds 6000, only the first (chronologically speaking) 6000 will be printed and all subsequent max-min data will be lost. This limitation can be overcome by dividing the case into two or more segments, with the additional cases run as restarts using the SAV function described below.

#### SAVE CURRENT DATA SUBROUTINE

This function makes it possible to use the output of one case as input to another in conjunction with the restart feature. An example of its use would be a full-life analysis of a recoverable satellite, with separate cases being run for ascent, orbit and recovery.



Ordinarily a restart case uses as its basis the data which existed at the start of the previous case. The Save Current Data (SAV) function provides the means whereby the answers of one case may be used as input into the next. The callout is

```
CALL SAV (A, B)
```

At the first time point for which A is greater than or equal to B, the data currently in core, i.e., the current values of temperature, resistance, and capacitance, are stored on tape to be used in the subsequent case. In nearly all cases A will be current time, M(1). The value of B may appear explicitly (floating point) or it may be an addressable element, e.g., final time, M(3). As an example,

```
CALL SAV (M(1), M(3))
```

will save the data in core at the end of each case, to be used as the initial conditions for the subsequent case.

#### TEMPERATURE CARD PUNCH SUBROUTINE

This subroutine is frequently used in complex cases as an alternate restart feature. It provides for the automatic recording of all temperatures on punched cards in proper format for the initial temperature block. The function specification is

```
CALL PUNCHT( $\theta$ , A, B)
```

where  $\theta$  is the time at which the temperatures are to be saved, and cards are required for nodes A through B.  $\theta$  may be an explicit (floating point) number or an addressable element. A and B are listed in fixed-point notation. If the function is specified as CALL PUNCHT( $\theta$ , 0, 0) the program will interpret the zeros as a special code requiring the punching of temperature cards for all nodes.

The advantage of this subroutine is that once the temperatures are recorded, the case may be removed from the computer and resumed later when machine time becomes available. Also, in complex cases requiring several hours of computer time, it is customary to call for punched cards at various times throughout the run. Then, if an error occurs, the case may be re-run starting at the last time for which valid temperature cards were obtained.

To help identify the punched cards, the information in columns 6 through 14 of the case identification card (Section V) and the time  $\theta$  are automatically punched on each card. Thus, if this subroutine is used, it is desirable that the information on the case identification card begin with some code, for example, CASE B-2.

#### CURVE PLOTTING SUBROUTINE

In many problems it is desirable to obtain the results in curve form in addition to the tabulated output. To accomplish this, the Thermal Analyzer Program has a subroutine to write a plot tape which controls a machine plotter. The function specification for the plotting routine is

CALL TPLOT(N)

where N is the designation number of the table containing the information to write the tape. Table N must contain the following items, in the order listed:

- (a) the initial time of the plot.
- (b) the final time of the plot.
- (c) the time interval between successive plots (discussed below).
- (d) all nodes whose temperatures are to be plotted.
- (e) a zero flag terminating the table.

All of these entries must be floating point. The plotting routine does not automatically plot the temperatures at each computing cycle, the frequency

of the plot being specified by the user. The program subtracts the final time from the initial, and divides that quantity by the specified frequency (item C above) to determine how often the temperatures are to be plotted. If these times do not coincide with computing times, the machine will plot the temperatures for each subsequent computing time. For example, if the initial and final times are 0 and 100 sec, the time interval between plots specified at 10 sec, and the computing interval set at 3 sec, the temperatures would be plotted at 0 sec, 12 sec, 21 sec, 30 seconds, etc. If the user desires a plot every computing cycle, the third storage location of table N must be set equal to the computing interval  $M(5)$  by the following function specifications:

```
LN = LOC(N)
P(LN + 3) = M(5)
CALL TPLOT(N)
```

Although this routine will only plot temperatures, in practice any addressable quantity can be plotted simply by storing that quantity in an unused temperature location. For example, to plot  $R(4)$ , one could set  $TN(200) = R(4)$  and plot  $T(200)$ . Note that at the end of the heat balance,  $T(200)$  is set equal to  $TN(200)$ , so it is necessary to store  $R(4)$  in the "new" temperature location.

This routine is currently set up to plot a maximum of 5 temperatures per curve. If, for example, 8 nodes are specified in table N, the first 5 will be plotted on one curve and the remaining 3 on a separate curve. A maximum of 20 nodes may be listed per table and a maximum of 20 tables may be used.

As an example of the input for the plotting routine, suppose that it is desired to plot the first and last 100 sec of a case that runs continuously from 0 to 500 sec. The temperatures of nodes 24, 68, 72, and 93 are to be plotted at 10-sec intervals. For this case two tables could be set up as follows:

COLUMN  
→

	1	5	10	15	25	35	45	55	65
DEC		20							
DECO6			0.	100.	10.	24.	68.	72.	
DECO2			93	0.					
DEC		-20							
DEC		21							
DECO6			400.	500.	10.	24.	68.	72.	
DECO2			93.	0.					
DEC		-21							

The function specifications are

CALL TPIOT (20)

CALL TPIOT (21)

In Section VI, plots have been obtained for 5 nodes in Example Problem #2 to illustrate the use of the function and the quality of the curves. Note that the information on the case identification card (see Section V) is automatically printed at the top of each curve.

#### AERODYNAMIC HEATING AND ABLATION SUBROUTINES

The Eckert Aerodynamic Heating subroutine computes the surface convective heat transfer by the reference temperature method. The primary advantage of this method is that it allows incompressible skin friction relations to be employed in evaluating high-velocity-flow heat transfer. This is accomplished by evaluating the air properties at a suitably defined reference temperature, which depends only on the wall, local inviscid flow, and recovery temperatures.

The Ablation subroutine computes the amount of material that is ablated (if the temperature is above the ablation temperature) as a function of time as part of the heat balance. This solution is applicable to one-dimensional heat transfer to a pure subliming (non-charring) surface.

These specialized subroutines are discussed in detail in Appendices A and B. Example problems are set up and written on data input sheets to demonstrate the use of each subroutine.

MISCELLANEOUS FORTRAN OPERATIONS

Although a knowledge of FORTRAN is not required to use the Thermal Analyzer Program, an understanding of a few basic FORTRAN operations is highly desirable. The following is a brief discussion of some of the most commonly used operations, along with some general information useful in writing the FUNCT subroutine. The topics include the use of fixed- and floating-point variables, statement numbers, comment cards, and control statements. The treatment of each topic is brief, and the reader is referred to the FORTRAN reference manual for more detailed information.

Variables

A variable is a symbol or name which refers to a place in memory where the number or value represented by that name is stored. The name of any variable consists of one or more alphabetic or numerical characters, the first of which must be alphabetic (A through Z). The maximum number of characters permitted in the name is 6 for the 7094 processor. Names beginning with the letters I, J, K, L, M, or N are variable names for fixed-point numbers. All other names represent floating-point values. For example, K15 and NEXT are valid integer variables and A50 and VALUE are valid floating-point variables. In general, fixed- and floating-point variables cannot be mixed. As examples:

$B = A * I$  is not permitted since B and A are floating-point numbers and I is a fixed-point number.

$B = A + 2$  is not permitted since B and A are floating-point numbers and 2 (without decimal) is fixed-point.

$B = A + 2.$  is permitted since A, B, and 2. (with decimal) are all fixed-point numbers.

Statement Numbers

It is frequently desirable to identify a statement by name or number. This is accomplished by a numerical statement number (any integer from 1 to 32767) placed in columns 1 through 5 of the data input sheet.

The only other restriction is that a statement number must not be repeated in any subroutine. The use of statement numbers will become more apparent in the following sections.

#### Comment Cards

Occasionally the user may wish to have comments printed out in the `FUNCT` and `PRINT` subroutines. This is accomplished by placing the letter `C` in column 1 of the data input sheet and the desired comments in columns 7 through 72. The comment card is then ignored by the FORTRAN processor, and serves merely to furnish commentary information in the program listing.

#### GO TO Statements

Unconditional transfer statements which begin with the words `GO TO` permit the user to alter arbitrarily the sequence in which the program statements are to be executed. A frequent use of the `GO TO` statement is to skip an inapplicable instruction as shown by the first example in the following section.

To illustrate an unconditional transfer statement, the instruction

```
GO TO 17
```

means that the next statement to be executed is the one labeled 17. Statement 17 may either precede or follow the `GO TO` statement. All statements in between will be skipped and, once statement 17 is executed, the computer will execute those which follow, in the order in which they appear.

Computed `GO TO` statements are used as a switch for branching to one of several places in the program, depending on the integer value of a test location. To illustrate, the statement

```
GO TO (7, 4, 28, 9), K
```

transfers control to the statement labeled 7, 4, 28, or 9 when the current value of `K` is 1, 2, 3, or 4, respectively.

## Conditional Control and Logical Expressions

Frequently it is desirable to execute a particular function, or set of functions, only under certain specified conditions. This is accomplished by the IF statement which directs control to one of three different statements, depending on the value of an arithmetic expression. The statement

```
IF(X) A, B, C
```

will direct the computer to immediately execute statement A if the value of (X) is negative, to execute statement B if (X) is zero, and to execute statement C if (X) is positive. Any statements between the IF statement and the next executed statement (A, B, or C) will be skipped. The expression (X) may be any legal FORTRAN arithmetic expression discussed in the preceding sections.

To illustrate the use of the conditional control statement, consider a lunar spacecraft which is slowly rotating about one axis. The solar heating rate to shell node 10 is to be linearly interpolated from curve 10. At 45,000 sec, however, the vehicle stops rolling and the heating rate to node 10 is a constant value, say 0.085 Btu/sec. The appropriate functions might appear as follows:

```
IF (M(1) - 45000.) 2, 3, 3
2  Q(10) = LIN (M(1), 10)
   GO TO 4
3  Q(10) = 0.085
```

If current time is less than 45,000 sec, statement 2 is executed. Statement 3 is then skipped by the insertion of a GO TO statement which directs control to statement 4. The latter is not shown but would presumably follow statement 3. If current time is equal to or greater than 45,000 sec, the IF statement directs control to statement 3, after which statement 4 and succeeding functions are executed in a normal manner.

A logical IF statement has been added to the FORTRAN IV language so that decisions can be based directly on the true or false value of a quantity which is logical rather than arithmetic in nature. The statement

IF(Y)F

means that if the logical expression (Y) is true, execute the statement F and then proceed to the statement following F; otherwise (if Y is false), do not execute F, but simply proceed to the following statement. F may be any single executable statement except another logical IF statement or a DO statement.

Comparisons can be made by means of the logical operators .OR., .AND., or .NOT., or by any of the following relational operators:

<u>Symbol</u>	<u>Meaning</u>
.EQ.	Equal to
.NE.	Not equal to
.LT.	Less than
.LE.	Less than or equal to
.GT.	Greater than
.GE.	Greater than or equal to

Two examples of the use of logical IF statements are given below:

IF (M(6).EQ.80..OR.T(26).GE.500.) GO TO 5

means that if the minimum RC product equals 80 or if the temperature of node 26 is greater than or equal to 500, proceed immediately to statement 5.

IF (M(1).GE.35..AND.M(1).LE.70.) T(30) = 1100.

means that if current time is between 35 and 70, set the temperature of node 30 equal to 1100.



With the logical IF statement it is possible to simplify the functions required for the lunar spacecraft example given above. To illustrate, the two statements

$$Q(10) = 0.085$$

$$\text{IF } (M(1).LT. 45000.) \text{ } Q(10) = \text{LIN } (M(1),10)$$

are equivalent to the four statements listed previously. The second function merely overrides the first if current time is less than 45,000 sec.

#### DO Statements

Most computer programs involve a group of steps which are to be executed in a repetitive fashion. The iteration or DO statement greatly facilitates the definition and control of these repetitive steps. The statement

$$\text{DO A I} = \text{B, C, N}$$

controls the repetition of all succeeding statements down through and including the statement labeled A. Repetition of these statements is controlled by varying the index called I, from an initial value of B to a terminal value of C in increments of N. If the integer N does not appear the increment is understood to be 1. For example, the statements

$$\text{DO 13 I} = 1, 3$$

$$Q(I) = 0.25$$

$$R(I + 100) = \text{RAD } (I, 100, .3E - 5)$$

$$13 \text{ CONTINUE}$$

will cause the following operations to be performed:

```
Q(1) = 0.25
Q(2) = 0.25
Q(3) = 0.25
R(101) = RAD(1, 100, 0.3E - 5)
R(102) = RAD(2, 100, 0.3E - 5)
R(103) = RAD(3, 100, 0.3E - 5)
```

The terminating statement need not always be a CONTINUE card as shown in the above example. However, the last statement in an iteration loop cannot be a transfer statement, conditional or unconditional, or another iteration statement. The termination of a DO loop with a CONTINUE card is always acceptable and is recommended as a means to avoid the above difficulties. Another restriction on the use of DO loops is that control must never be transferred from outside to any card within the iteration loop with the exception of the first, or DO statement, card.

#### THERMAL PROPERTIES LIBRARY

The thermal properties library contains tables of physical properties of a number of propellants, pressurants, simulated propellants, structural materials, and insulations. Special data search and interpolation routines are incorporated into the Thermal Analyzer Program to utilize the library data.

#### Library Tape

The thermal properties and library tape are discussed in detail and completely listed in Reference 2. The property tables contain data on density, specific heat, and thermal conductivity vs. temperature for liquids and solids; vapor pressure, viscosity, heat of vaporization, and surface tension vs. temperature for liquids; and specific heat, thermal conductivity, and compressibility factor vs. temperature and pressure for gases. The properties data are given in the following units:

Density, lb/ft<sup>3</sup>  
 Specific heat, Btu/lb °F  
 Thermal conductivity, Btu/hr ft °F  
 Vapor pressure, psia  
 Viscosity, lb/ft sec  
 Heat of vaporization, Btu/lb  
 Surface tension, lb/ft

The library itself is contained on a reserved tape. Each curve is uniquely identified by a six-character code consisting of both a material and a property identification. Table 4-1 is a complete listing of the identification codes and titles of every library table. The use of the library tape is described below.

A flag in the data-block of the Thermal Analyzer will cause the compiler to search the data tape for the specific table called for by the flag. That table will then be stored in place of the flag. There must be an exact correspondence between the identification of the tables stored on tape and the flags used to call the tables to be used in the program. The flag consists of six alphameric characters in columns 6-11, preceded by the mnemonic code "TAP" in columns 1-3. (See Table 4-1.) The data entry and flag are as follows:

COLUMN		
→ 1	DEC	401
	TAP	NTO-13
	DEC	-401
		Table No.
		I.D. of table stored on tape
		End-of-table flag

This entry means that the material properties data table identified as Table "NIO-13" (Thermal Conductivity of Liquid Nitrogen Tetroxide) is to be stored as Table 401 within the Thermal Analyzer input data block.

In all cases where data are available, the tables are accurate for linear interpolation within  $\pm 5\%$  over the appropriate temperature range. To construct a useful data library, it was necessary to extend

TABLE 4-1

## THERMAL PROPERTIES LIBRARY IDENTIFICATION CODES

TAP NTO-11	DENSITY OF LIQUID NITROGEN TETROXIDE	101012266
TAP NTO-12	SPECIFIC HEAT OF LIQUID NITROGEN TETROXIDE	102012266
TAP NTO-13	THERMAL CONDUCTIVITY OF LIQUID NITROGEN TETROXIDE	103012266
TAP NTO-14	VAPOR PRESSURE OF LIQUID NITROGEN TETROXIDE	104012266
TAP NTO-15	VISCOSITY OF LIQUID NITROGEN TETROXIDE	105012266
TAP NTO-16	HEAT OF VAPORIZATION OF LIQUID NITROGEN TETROXIDE	106012266
TAP NTO-17	SURFACE TENSION OF LIQUID NITROGEN TETROXIDE	107012266
TAP NTO-22	SPECIFIC HEAT OF GASEOUS NITROGEN TETROXIDE	108012266
TAP NTO-23	THERMAL CONDUCTIVITY OF GASEOUS NITROGEN TETROXIDE	109012266
TAP NTO-28	COMPRESSIBILITY FACTOR OF GASEOUS NITROGEN TETROXIDE	110012266
TAP OXY-11	DENSITY OF LIQUID OXYGEN	111012266
TAP OXY-12	SPECIFIC HEAT OF LIQUID OXYGEN	112012266
TAP OXY-13	THERMAL CONDUCTIVITY OF LIQUID OXYGEN	113012266
TAP OXY-14	VAPOR PRESSURE OF LIQUID OXYGEN	114012266
TAP OXY-15	VISCOSITY OF LIQUID OXYGEN	115012266
TAP OXY-16	HEAT OF VAPORIZATION OF LIQUID OXYGEN	116012266
TAP OXY-17	SURFACE TENSION OF LIQUID OXYGEN	117012266
TAP OXY-22	SPECIFIC HEAT OF GASEOUS OXYGEN	118012266
TAP OXY-23	THERMAL CONDUCTIVITY OF GASEOUS OXYGEN	119012266
TAP OXY-28	COMPRESSIBILITY FACTOR OF GASEOUS OXYGEN	120012266
TAP FLU-11	DENSITY OF LIQUID FLUORINE	121012266
TAP FLU-12	SPECIFIC HEAT OF LIQUID FLUORINE	122012266
TAP FLU-13	THERMAL CONDUCTIVITY OF LIQUID FLUORINE	123012266
TAP FLU-14	VAPOR PRESSURE OF LIQUID FLUORINE	124012266
TAP FLU-15	VISCOSITY OF LIQUID FLUORINE	125012266
TAP FLU-16	HEAT OF VAPORIZATION OF LIQUID FLUORINE	126012266
TAP FLU-17	SURFACE TENSION OF LIQUID FLUORINE	127012266
TAP FLU-22	SPECIFIC HEAT OF GASEOUS FLUORINE	128012266
TAP FLU-23	THERMAL CONDUCTIVITY OF GASEOUS FLUORINE	129012266
TAP FLU-28	COMPRESSIBILITY FACTOR OF GASEOUS FLUORINE	130012266
TAP ODF-11	DENSITY OF LIQUID OXYGEN DIFLUORIDE	131012266
TAP ODF-12	SPECIFIC HEAT OF LIQUID OXYGEN DIFLUORIDE	132012266
TAP ODF-13	THERMAL CONDUCTIVITY OF LIQUID OXYGEN DIFLUORIDE	133012266
TAP ODF-14	VAPOR PRESSURE OF LIQUID OXYGEN DIFLUORIDE	134012266
TAP ODF-15	VISCOSITY OF LIQUID OXYGEN DIFLUORIDE	135012266
TAP ODF-16	HEAT OF VAPORIZATION OF LIQUID OXYGEN DIFLUORIDE	136012266
TAP ODF-22	SPECIFIC HEAT OF GASEOUS OXYGEN DIFLUORIDE	138012266
TAP ODF-28	COMPRESSIBILITY FACTOR OF LIQUID OXYGEN DIFLUORIDE	140012266
TAP CTF-11	DENSITY OF LIQUID CHLORINE TRIFLUORIDE	141012266
TAP CTF-12	SPECIFIC HEAT OF LIQUID CHLORINE TRIFLUORIDE	142012266
TAP CTF-13	THERMAL CONDUCTIVITY OF LIQUID CHLORINE TRIFLUORIDE	143012266
TAP CTF-14	VAPOR PRESSURE OF LIQUID CHLORINE TRIFLUORIDE	144012266
TAP CTF-15	VISCOSITY OF LIQUID CHLORINE TRIFLUORIDE	145012266
TAP CTF-16	HEAT OF VAPORIZATION OF LIQUID CHLORINE TRIFLUORIDE	146012266
TAP CTF-17	SURFACE TENSION OF LIQUID CHLORINE TRIFLUORIDE	147012266
TAP CTF-22	SPECIFIC HEAT OF GASEOUS CHLORINE TRIFLUORIDE	148012266
TAP CTF-28	COMPRESSIBILITY FACTOR, GASEOUS CHLORINE TRIFLUORIDE	150012266
TAP AER-11	DENSITY OF LIQUID AEROZINE 50	151012266
TAP AER-12	SPECIFIC HEAT OF LIQUID AEROZINE 50	152012266
TAP AER-13	THERMAL CONDUCTIVITY OF LIQUID AEROZINE 50	153012266
TAP AER-14	VAPOR PRESSURE OF LIQUID AEROZINE 50	154012266
TAP AER-15	VISCOSITY OF LIQUID AEROZINE 50	155012266
TAP AER-16	HEAT OF VAPORIZATION OF LIQUID AEROZINE 50	156012266
TAP AER-17	SURFACE TENSION OF LIQUID AEROZINE 50	157012266
TAP AER-22	SPECIFIC HEAT OF GASEOUS AEROZINE 50	158012266
TAP AER-23	THERMAL CONDUCTIVITY OF GASEOUS AEROZINE 50	159012266
TAP AER-28	COMPRESSIBILITY FACTOR OF GASEOUS AEROZINE 50	160012266
TAP MMH-11	DENSITY OF LIQUID MONOMETHYL HYDRAZINE	161012266
TAP MMH-12	SPECIFIC HEAT OF LIQUID MONOMETHYL HYDRAZINE	162012266
TAP MMH-13	THERMAL CONDUCTIVITY OF LIQUID MONOMETHYL HYDRAZINE	163012266
TAP MMH-14	VAPOR PRESSURE OF LIQUID MONOMETHYL HYDRAZINE	164012266

TABLE 4-1

(Continued)

TAP	MMH-15	VISCOSITY OF LIQUID MONOMETHYL HYDRAZINE	165012266
TAP	MMH-16	HEAT OF VAPORIZATION OF LIQUID MONOMETHYL HYDRAZINE	166012266
TAP	MMH-17	SURFACE TENSION OF LIQUID MONOMETHYL HYDRAZINE	167012266
TAP	MMH-22	SPECIFIC HEAT OF GASEOUS MONOMETHYL HYDRAZINE	168012266
TAP	MMH-23	THERMAL CONDUCTIVITY, GASEOUS MONOMETHYL HYDRAZINE	169012266
TAP	MMH-28	COMPRESSIBILITY FACTOR, GASEOUS MONOMETHYL HYDRAZINE	170012266
TAP	DIB-11	DENSITY OF LIQUID DIBORANE	171012266
TAP	DIB-12	SPECIFIC HEAT OF LIQUID DIBORANE	172012266
TAP	DIB-13	THERMAL CONDUCTIVITY OF LIQUID DIBORANE	173012266
TAP	DIB-14	VAPOR PRESSURE OF LIQUID DIBORANE	174012266
TAP	DIB-15	VISCOSITY OF LIQUID DIBORANE	175012266
TAP	DIB-16	HEAT OF VAPORIZATION OF LIQUID DIBORANE	176012266
TAP	DIB-22	SPECIFIC HEAT OF GASEOUS DIBORANE	178012266
TAP	DIB-28	COMPRESSIBILITY FACTOR OF GASEOUS DIBORANE	180012266
TAP	HYD-11	DENSITY OF LIQUID HYDROGEN	181012266
TAP	HYD-12	SPECIFIC HEAT OF LIQUID HYDROGEN	182012266
TAP	HYD-13	THERMAL CONDUCTIVITY OF LIQUID HYDROGEN	183012266
TAP	HYD-14	VAPOR PRESSURE OF LIQUID HYDROGEN	184012266
TAP	HYD-15	VISCOSITY OF LIQUID HYDROGEN	185012266
TAP	HYD-16	HEAT OF VAPORIZATION OF LIQUID HYDROGEN	186012266
TAP	HYD-17	SURFACE TENSION OF LIQUID HYDROGEN	187012266
TAP	HYD-22	SPECIFIC HEAT OF GASEOUS NORMAL HYDROGEN	188012266
TAP	HYD-23	THERMAL CONDUCTIVITY OF GASEOUS PARA HYDROGEN	189012266
TAP	HYD-28	COMPRESSIBILITY FACTOR OF GASEOUS PARA HYDROGEN	190012266
TAP	HA5-11	DENSITY OF LIQUID HYBALINE A5	191012266
TAP	HA5-12	SPECIFIC HEAT OF LIQUID HYBALINE A5	192012266
TAP	HA5-13	THERMAL CONDUCTIVITY OF LIQUID HYBALINE A5	193012266
TAP	HA5-14	VAPOR PRESSURE OF LIQUID HYBALINE A5	194012266
TAP	HA5-15	VISCOSITY OF LIQUID HYBALINE A5	195012266
TAP	HA5-22	SPECIFIC HEAT OF GASEOUS HYBALINE A5	198012266
TAP	HA5-23	THERMAL CONDUCTIVITY OF GASEOUS HYBALINE A5	199012266
TAP	HA5-28	COMPRESSIBILITY FACTOR OF GASEOUS HYBALINE A5	200012266
TAP	NIT-11	DENSITY OF LIQUID NITROGEN	201012266
TAP	NIT-12	SPECIFIC HEAT OF LIQUID NITROGEN	202012266
TAP	NIT-13	THERMAL CONDUCTIVITY OF LIQUID NITROGEN	203012266
TAP	NIT-14	VAPOR PRESSURE OF LIQUID NITROGEN	204012266
TAP	NIT-15	VISCOSITY OF LIQUID NITROGEN	205012266
TAP	NIT-16	HEAT OF VAPORIZATION OF LIQUID NITROGEN	206012266
TAP	NIT-17	SURFACE TENSION OF LIQUID NITROGEN	207012266
TAP	NIT-22	SPECIFIC HEAT OF GASEOUS NITROGEN	208012266
TAP	NIT-23	THERMAL CONDUCTIVITY OF GASEOUS NITROGEN	209012266
TAP	NIT-28	COMPRESSIBILITY FACTOR OF GASEOUS NITROGEN	210012266
TAP	HEL-22	SPECIFIC HEAT OF GASEOUS HELIUM	218012266
TAP	HEL-23	THERMAL CONDUCTIVITY OF GASEOUS HELIUM	219012266
TAP	HEL-28	COMPRESSIBILITY FACTOR OF GASEOUS HELIUM	220012266
TAP	G60-11	DENSITY OF LIQUID .6 ETHYLENE GLYCOL	221012266
TAP	G60-12	SPECIFIC HEAT OF LIQUID .6 ETHYLENE GLYCOL	222012266
TAP	G60-13	THERMAL CONDUCTIVITY OF LIQUID .6 ETHYLENE GLYCOL	223012266
TAP	G60-14	VAPOR PRESSURE OF LIQUID .6 ETHYLENE GLYCOL	224012266
TAP	G60-15	VISCOSITY OF LIQUID .6 ETHYLENE GLYCOL	225012266
TAP	G60-22	SPECIFIC HEAT OF GASEOUS .6 ETHYLENE GLYCOL	228012266
TAP	G60-23	THERMAL CONDUCTIVITY OF GASEOUS .6 ETHYLENE GLYCOL	229012266
TAP	G60-28	COMPRESSIBILITY FACTOR, GASEOUS .6 ETHYLENE GLYCOL	230012266
TAP	F11-11	DENSITY OF LIQUID FREON 11	231012266
TAP	F11-12	SPECIFIC HEAT OF LIQUID FREON 11	232012266
TAP	F11-13	THERMAL CONDUCTIVITY OF LIQUID FREON 11	233012266
TAP	F11-14	VAPOR PRESSURE OF LIQUID FREON 11	234012266
TAP	F11-15	VISCOSITY OF LIQUID FREON 11	235012266
TAP	F11-16	HEAT OF VAPORIZATION OF LIQUID FREON 11	236012266
TAP	F11-17	SURFACE TENSION OF LIQUID FREON 11	237012266
TAP	F11-22	SPECIFIC HEAT OF GASEOUS FREON 11	238012266

TABLE 4-1  
(Continued)

TAP L92A-3	THERMAL CONDUCTIVITY OF LINDE SI-92 (80 LAYERS/INCH)	483012266
TAP L92B-1	DENSITY OF LINDE SI-92 (100 LAYERS/INCH)	491012266
TAP L92B-2	SPECIFIC HEAT OF LINDE SI-92	492012266
TAP L92B-3	THERMAL CONDUCTIVITY OF LINDE SI-92 (100 LAYERS/INCH)	493012266
TAP L92C-1	DENSITY OF LINDE SI-92 (120 LAYERS/INCH)	501012266
TAP L92C-2	SPECIFIC HEAT OF LINDE SI-92	502012266
TAP L92C-3	THERMAL CONDUCTIVITY OF LINDE SI-92 (120 LAYERS/INCH)	503012266
TAP L92D-1	DENSITY OF LINDE SI-92 (160 LAYERS/INCH)	511012266
TAP L92D-2	SPECIFIC HEAT OF LINDE SI-92	512012266
TAP L92D-3	THERMAL CONDUCTIVITY OF LINDE SI-92 (160 LAYERS/INCH)	513012266
TAP LFWA-1	DENSITY OF LINDE FT WT (40 LAYERS/INCH)	521012266
TAP LFWA-2	SPECIFIC HEAT OF LINDE FLT WT	522012266
TAP LFWA-3	THERMAL CONDUCTIVITY OF LINDE FLT WT (40 LAYERS/INCH)	523012266
TAP LFWB-1	DENSITY OF LINDE FT WT (50 LAYERS/INCH)	531012266
TAP LFWB-2	SPECIFIC HEAT OF LINDE FLT WT	532012266
TAP LFWB-3	THERMAL CONDUCTIVITY OF LINDE FLT WT (50 LAYERS/INCH)	533012266
TAP LFWC-1	DENSITY OF LINDE FT WT (60 LAYERS/INCH)	541012266
TAP LFWC-2	SPECIFIC HEAT OF LINDE FLT WT	542012266
TAP LFWC-3	THERMAL CONDUCTIVITY OF LINDE FLT WT (60 LAYERS/INCH)	543012266
TAP LFWD-1	DENSITY OF LINDE FT WT (80 LAYERS/INCH)	551012266
TAP LFWD-2	SPECIFIC HEAT OF LINDE FLT WT	552012266
TAP LFWD-3	THERMAL CONDUCTIVITY OF LINDE FLT WT (80 LAYERS/INCH)	553012266
TAP LHTA-1	DENSITY OF LINDE HIGH TEMP (60 LAYERS/INCH)	561012266
TAP LHTA-2	SPECIFIC HEAT OF LINDE HIGH TEMP	562012266
TAP LHTA-3	THERMAL CONDUCTIVITY OF LINDE HI TEMP (60 LAYERS/INCH)	563012266
TAP LHTB-1	DENSITY OF LINDE HIGH TEMP (120 LAYERS/INCH)	571012266
TAP LHTB-2	SPECIFIC HEAT OF LINDE HIGH TEMP	572012266
TAP LHTB-3	THERMAL CONDUCTIVITY OF LINDE HI TEMP (120 LAYER/INCH)	573012266
TAP LHTC-1	DENSITY OF LINDE HIGH TEMP (180 LAYERS/INCH)	581012266
TAP LHTC-2	SPECIFIC HEAT OF LINDE HIGH TEMP	582012266
TAP LHTC-3	THERMAL CONDUCTIVITY OF LINDE HI TEMP (180 LAYER/INCH)	583012266
TAP NRCA-1	DENSITY OF NRC-2 (40 LAYERS/INCH)	601012266
TAP NRCA-2	SPECIFIC HEAT OF NRC-2	602012266
TAP NRCA-3	THERMAL CONDUCTIVITY OF NRC-2 (40 LAYERS/INCH)	603012266
TAP NRCB-1	DENSITY OF NRC-2 (100 LAYERS/INCH)	611012266
TAP NRCB-2	SPECIFIC HEAT OF NRC-2	612012266
TAP NRCB-3	THERMAL CONDUCTIVITY OF NRC-2 (100 LAYERS/INCH)	613012266
TAP NRCC-1	DENSITY OF NRC-2 (160 LAYERS/INCH)	621012266
TAP NRCC-2	SPECIFIC HEAT OF NRC-2	622012266
TAP NRCC-3	THERMAL CONDUCTIVITY OF NRC-2 (160 LAYERS/INCH)	623012266
TAP FGLS-1	DENSITY OF FIBERGLASS	701012266
TAP FGLS-2	SPECIFIC HEAT OF FIBERGLASS	702012266
TAP FGLS-3	THERMAL CONDUCTIVITY OF FIBERGLASS	703012266
TAP MQTZ-1	DENSITY OF MICRO QUARTZ	751012266
TAP MQTZ-2	SPECIFIC HEAT OF MICRO QUARTZ	752012266
TAP MQTZ-3	THERMAL CONDUCTIVITY OF MICRO QUARTZ	753012266

TABLE 4-1  
(Continued)

TAP F11-23	THERMAL CONDUCTIVITY OF GASEOUS FREON 11	239012266
TAP F11-28	COMPRESSIBILITY FACTOR OF GASEOUS FREON 11	240012266
TAP BERL-1	DENSITY OF BERYLLIUM	291012266
TAP BERL-2	SPECIFIC HEAT OF BERYLLIUM	292012266
TAP BERL-3	THERMAL CONDUCTIVITY OF BERYLLIUM	293012266
TAP AL22-1	DENSITY OF ALUMINUM 2219-T87	301012266
TAP AL22-2	SPECIFIC HEAT OF ALUMINUM 2219-T87	302012266
TAP AL22-3	THERMAL CONDUCTIVITY OF ALUMINUM 2219-T87	303012266
TAP AL70-1	DENSITY OF ALUMINUM 7075-T6	311012266
TAP AL70-2	SPECIFIC HEAT OF ALUMINUM 7075-T6	312012266
TAP AL70-3	THERMAL CONDUCTIVITY OF ALUMINUM 7075-T6, AS RECEIVED	313012266
TAP AL70-4	THERMAL CONDUCTIVITY OF ALUMINUM 7075-T6, ANNEALED	314012266
TAP MGA3-1	DENSITY OF MAGNESIUM AZ31B-H24	321012266
TAP MGA3-2	SPECIFIC HEAT OF MAGNESIUM AZ31B-H24	322012266
TAP MGA3-3	THERMAL CONDUCTIVITY OF MAGNESIUM AZ31B-H24	323012266
TAP T6AL-1	DENSITY OF TITANIUM 6AL4V	331012266
TAP T6AL-2	SPECIFIC HEAT OF TITANIUM 6AL4V	332012266
TAP T6AL-3	THERMAL CONDUCTIVITY OF TITANIUM 6AL4V	333012266
TAP T110-1	DENSITY OF TITANIUM A110AT	341012266
TAP T110-2	SPECIFIC HEAT OF TITANIUM A110AT	342012266
TAP T110-3	THERMAL CONDUCTIVITY OF TITANIUM A110AT	343012266
TAP C103-1	DENSITY OF COLUMBIUM C-103	351012266
TAP C103-2	SPECIFIC HEAT OF COLUMBIUM C-103	352012266
TAP C103-3	THERMAL CONDUCTIVITY OF COLUMBIUM C-103	353012266
TAP S321-1	DENSITY OF STAINLESS STEEL 321	361012266
TAP S321-2	SPECIFIC HEAT OF STAINLESS STEEL 321	362012266
TAP S321-3	THERMAL CONDUCTIVITY OF STAINLESS STEEL 321	363012266
TAP INCX-1	DENSITY OF INCONEL X	371012266
TAP INCX-2	SPECIFIC HEAT OF INCONEL X	372012266
TAP INCX-3	THERMAL CONDUCTIVITY OF INCONEL X	373012266
TAP INCX-4	THERMAL CONDUCTIVITY OF INCONEL X, SOLUTION TREATED	374012266
TAP RE41-1	DENSITY OF RENE 41	381012266
TAP RE41-2	SPECIFIC HEAT OF RENE 41	382012266
TAP RE41-3	THERMAL CONDUCTIVITY OF RENE 41, 2HR SOLN TREATED	383012266
TAP RE41-4	THERMAL CONDUCTIVITY OF RENE 41, 4HR SOLN TREATED	384012266
TAP L12A-1	DENSITY OF LINDE SI-12 (8 LAYERS/INCH)	401012266
TAP L12A-2	SPECIFIC HEAT OF LINDE SI-12	402012266
TAP L12A-3	THERMAL CONDUCTIVITY OF LINDE SI-12 (8 LAYERS/INCH)	403012266
TAP L12B-1	DENSITY OF LINDE SI-12 (10 LAYERS/INCH)	411012266
TAP L12B-2	SPECIFIC HEAT OF LINDE SI-12	412012266
TAP L12B-3	THERMAL CONDUCTIVITY OF LINDE SI-12 (10 LAYERS/INCH)	413012266
TAP L12C-1	DENSITY OF LINDE SI-12 (12 LAYERS/INCH)	421012266
TAP L12C-2	SPECIFIC HEAT OF LINDE SI-12	422012266
TAP L12C-3	THERMAL CONDUCTIVITY OF LINDE SI-12 (12 LAYERS/INCH)	423012266
TAP L12D-1	DENSITY OF LINDE SI-12 (14 LAYERS/INCH)	431012266
TAP L12D-2	SPECIFIC HEAT OF LINDE SI-12	432012266
TAP L12D-3	THERMAL CONDUCTIVITY OF LINDE SI-12 (14 LAYERS/INCH)	433012266
TAP L62A-1	DENSITY OF LINDE SI-62 (40 LAYERS/INCH)	441012266
TAP L62A-2	SPECIFIC HEAT OF LINDE SI-62	442012266
TAP L62A-3	THERMAL CONDUCTIVITY OF LINDE SI-62 (40 LAYERS/INCH)	443012266
TAP L62B-1	DENSITY OF LINDE SI-62 (60 LAYERS/INCH)	451012266
TAP L62B-2	SPECIFIC HEAT OF LINDE SI-62	452012266
TAP L62B-3	THERMAL CONDUCTIVITY OF LINDE SI-62 (60 LAYERS/INCH)	453012266
TAP L62C-1	DENSITY OF LINDE SI-62 (80 LAYERS/INCH)	461012266
TAP L62C-2	SPECIFIC HEAT OF LINDE SI-62	462012266
TAP L62C-3	THERMAL CONDUCTIVITY OF LINDE SI-62 (80 LAYERS/INCH)	463012266
TAP L62D-1	DENSITY OF LINDE SI-62 (100 LAYERS/INCH)	471012266
TAP L62D-2	SPECIFIC HEAT OF LINDE SI-62	472012266
TAP L62D-3	THERMAL CONDUCTIVITY OF LINDE SI-62 (100 LAYERS/INCH)	473012266
TAP L92A-1	DENSITY OF LINDE SI-92 (80 LAYERS/INCH)	481012266
TAP L92A-2	SPECIFIC HEAT OF LINDE SI-92	482012266

some properties data by means of extrapolation and/or estimation into regions where data were unavailable. All such "extended" data are flagged and interpolations based on these data are automatically noted by the interpolation routines, and suitable explanations are printed out. These "extended" data are not necessarily accurate to within  $\pm 5\%$  but are included as a convenience.

### Interpolation Routines

Once the required tables are stored in the data block, the properties may be called for in the FUNCT subroutine, using either the linear or bivariate interpolation routines discussed previously, or the linear interpolation with integration routine discussed below. Linear interpolation should be used for the solid and liquid properties data, except for the conductivity of insulations which requires the special integration feature. For gases, the bivariate interpolation routine is required since the properties are temperature and pressure dependent. The tables are interpolated horizontally with temperature as independent variable and vertically with pressure as independent variable. As a result, the function specification must be of the form

$$Y = BIV (\text{pressure, temperature, table number})$$

An integer code has been added at the beginning of each table to indicate the special nature of the table and the method of acquiring the data, if applicable. The absence of the code or a code "0" indicates that no special procedures (such as extrapolation) were required to obtain the data, and that interpolation is to take place in a normal fashion. The data classification codes and their explanations are given in Table 4-2.

Since the actual property values in such tables are always positive, the absolute magnitude of the value is used during interpolation. "Extended" data are entered as negative numbers, thus allowing the interpolation routine to recognize when such values have been used, and to print a comment that this has occurred. Note, however, that if the code is zero or does not appear, negative values are treated as negative.



TABLE 4-2  
DATA CLASSIFICATION CODES

Code	Explanation
0	Normal curve
1	Extrapolated data
2	Fitted parabola
3	Estimated values
4	"Dummy" values
5	Values for 1 atmosphere pressure
6	Values for saturation line
7	Special bivariate interpolation routine, used in vicinity of saturation line
15	1 plus 5
16	1 plus 6
71	7 plus 1
73	7 plus 3

A special situation exists for interpolation on incomplete bivariate curves indicated by code "7." The properties of gases involve the saturation line, beyond which data are meaningless. In the neighborhood of the saturation line, interpolation will be attempted with only one, two, or three meaningful points. This difficulty is surmounted by entering all points beyond the saturation line as zeros. The routine then recognizes the situation, and shifts its base points until it has four meaningful values. It then extrapolates to the required point. Note, again, that this will occur only if a non-zero code is entered in the table. (See Reference 2.) If the code is zero or does not appear, normal linear bivariate interpolation will occur, and any zero or negative value is treated as zero or negative.

A special linear interpolation and integration subroutine, XLIN, has been included which determines the area under a specified curve, N, from X1 to X2 divided by X2 - X1:

$$\text{XLIN}(X1, X2, N) = \frac{1}{X2 - X1} \int_{X1}^{X2} F_N(X) dX \quad (4-3)$$

This routine is intended specifically to compute temperature-dependent conductivity of insulation. The routine integrates by the trapezoidal rule from the left end of the curve to X1, from the left end of the curve to X2, and then divides the difference by X2 - X1. Equation (4-3) above then becomes:

$$\text{XLIN}(X1, X2, N) = \frac{1}{X2 - X1} * \left( \int_{-460}^{X2} F_N(X) dX - \int_{-460}^{X1} F_N(X) dX \right) \quad (4-4)$$

XLIN is a variation of function LIN, and uses identical coding in evaluating the curve at first X1, then X2. It integrates the preceding part of the curve as it locates the interval in which it interpolates. Having integrated and interpolated for X1, the answers are saved, and a second pass is made to evaluate the same functions for X2. Then the difference between the integrals is taken, divided by (X2 - X1), and that value is returned as the value of function XLIN.

The curve, data block N, is required to be monotonically increasing in the independent variable, but following the last value of the dependent variable there must be a flag less than the last value of the independent variable. This is the same rule that applies to function LIN.

An example of the function specification is

$$K = \text{XLIN} (T(14), T(15), 28)$$

where the conductivity for the resistor connecting nodes 14 and 15 is to be obtained by integrating curve 28.

## V - PROGRAM INPUT

This section describes how to transcribe the sketch of the electrical analog network to data cards. It also describes how to prepare the subroutines which contain the functions and the print format.

The problem description for each case is divided into five distinct blocks and two subroutines. The first three blocks define the network and give the initial values of the temperatures, resistors, and capacitors. The fourth block is a list of sub-blocks of data required by the functions and subroutines. The fifth block lists the print interval, and the initial and final times of the case. The functions and subroutines used in the case are listed in FORTRAN statements in the FUNCT subroutine. The PRINT subroutine contains the list of quantities to be printed at each specified printing interval, plus the desired output format.

A scheme whereby all circuit elements may be referenced between blocks is completed by the user as he describes the circuit. In block 1, each node is assigned an integer which is the designation number of that node throughout the blocks following. Likewise, in block 2, each resistor is assigned a designation number. Each set of data in block 4 is also assigned a designation number. Moreover, the program automatically assigns designation numbers to certain computed and input quantities which are thereby available to the user. A complete list of these addressable quantities was given in Section IV.

The problem description is written on input data sheets or FORTRAN coding sheets of a standard form. Each line of data (blocks 1 through 5) will become a card with columns 1, 2, and 3 containing a three-lettered mnemonic code, columns 4 and 5 either containing a numerical value or left blank, and columns 6 through N containing the data. Columns N + 1 through 72 are then available for user's comments and a card sequence number, if desired.

SPECIAL DATA CARDS

The three-lettered mnemonic code in columns 1, 2, and 3 will take one of the following seven forms:

1. Case Identification Card (CID). This is a card placed at the beginning of each case to identify the output. The letters CID appear in columns 1, 2, and 3, followed by user's comments in columns 6 through 72. If the user desires, these comments may be printed out at the top of each page of output belonging to that case (see "FORMAT Declarations" discussed later in this section).
2. DEC Card. The letters DEC in columns 1, 2, and 3, and a numerical value greater than zero in columns 4 and 5 indicate that the data on that card are not to be handled in any special way, but merely to be entered into consecutive storage. The integers in columns 4 and 5 represent the number of values or sets of values on that card, as discussed in the following sections.
3. Increment Card (INC). This card is used to abbreviate a repetitive list of data. It can only be used in the initial temperature, resistor, and capacitor blocks, and in the data block. It is best explained by an example:

DEC01	a	b.	
INC	2	-3.0	4

means that card DEC01 a b is to be repeated 4 times, each time incrementing the first number on the card by 2 and the second number by -3. Thus the 2 cards above are equivalent to the following 5 cards:

DEC01	a	b.
DEC01	a+2	b-3.0
DEC01	a+4	b-6.0
DEC01	a+6	b-9.0
DEC01	a+8	b-12.0

Note that fixed- and floating-point numbers must be incremented by fixed- and floating-point numbers, respectively. The number of times the card is to be incremented (4 in the above example) is given in fixed point as shown. As a further example, suppose that the following cards are to be incremented:

DEC01	4	5	50	0.
DEC01	5	6	50	0.
DEC01	6	7	50	0.
DEC01	7	8	50	0.
DEC01	8	9	50	0.

The proper instructions are as follows:

DEC01	4	5	50	0.
INC	1	1	0	0. 4

4. Periodic Data Card (PER). The letters PER in columns 1, 2, and 3, with columns 4 and 5 left blank indicate a periodic curve. The period of the curve is given in floating-point notation in columns 6 through 15. When a periodic curve is specified, the PER card follows the DEC card which contains the curve designation number.
5. End of Block Card (NBK). Each of the first five blocks is terminated by a card having NBK in columns 1, 2, and 3.
6. Geometric Resistor Card (RES). This card is used to specify a resistor whose value is automatically computed by the Thermal Analyzer, given the resistor geometry and the designation number of the curve describing the material conductivity vs temperature. See page 5-6 for details.
7. Geometric Capacitor Card (CAP). This card is used to specify a capacitor whose value is automatically computed by the Thermal Analyzer, given the capacitor geometry and the designation numbers of the curves describing the material specific heat and density vs temperature. See page 5-8 for details.

#### DATA CARD FORMATS

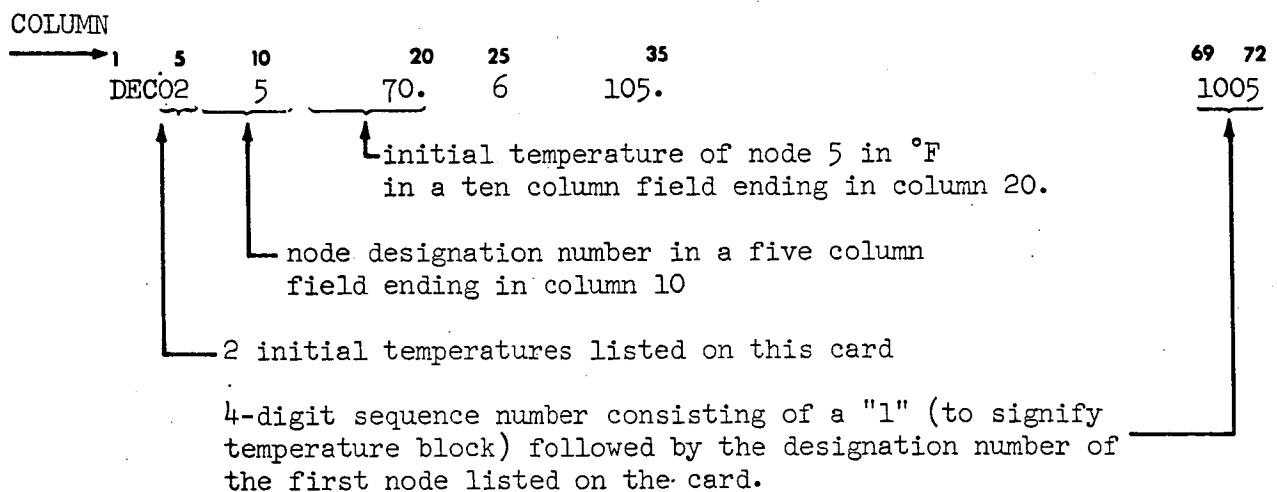
All CID, INC, PER, and NBK cards have columns 4 and 5 blank. RES and CAP cards always contain a zero (or a blank) in column 4 and a 1 in column 5. DEC cards have columns 4 and 5 blank only when the information contained on the card is the designation number of a curve or table or when the card is a flag in the restart block. In other words, a DEC card will have columns 4 and 5 blank if and only if the card does not contain a floating-point number. Otherwise, a zero (or blank) is placed in column 4 and an integer equal to the number of floating-point numbers contained on the card is placed in column 5.

The numerical data are contained in columns 6 through 65. The first field always begins in column 6. Fixed-point numbers have a field width of 5 columns and must end in the last column of the field in which they appear. Floating-point numbers have a field width of 10 columns and do not have to end in the last column of the field except when the E format (indicating a power of 10) is used to input the value. It is recommended, however, that all values end in the last column of the field to facilitate checking of the input data.

Any column to the right of the last field containing numerical data can be used for comments. However, certain of these comment columns should be reserved for a card sequence number. Ordinarily a 4-digit number starting in column 69, or a 5-digit number starting in column 68 is sufficient. The choice and use of sequence numbers is purely arbitrary, and is at the discretion of the user. As a general rule, however, a systematic scheme, such as that shown in the examples which follow, should be employed to facilitate subsequent changes in the deck and to allow for machine sorting of the cards. Five-digit sequence numbers are useful in cases where a large number of curves are required. A commonly used and convenient procedure is to let the first three digits of the sequence number represent the curve number, and the last two digits represent the card number of that curve. This system is used by the Orbital Radiation Program (Ref. 4) which has an output option to supply the external heating rate history in the form of curves punched in proper format for the Thermal Analyzer Program.

#### BLOCK 1, INITIAL TEMPERATURES

In block 1, each node is listed by a designation number (fixed-point) by which the node will be referenced in later blocks, followed by the initial value of the temperature at that node (floating-point number). Up to 4 nodes and their initial temperatures may be listed on each card. An example of a temperature input listing two nodes on a card is shown below.



Note that fixed-point numbers are listed in 5-column fields, and floating-point numbers are listed in 10-column fields. No columns may be skipped between fields.

Since in many practical cases a uniform initial temperature applies to a large portion of the network, the computer is programmed automatically to increment initial temperatures. For example:

DECO1	1	70.
DECO1	50	100.
DECO1	80	20.

would be interpreted as

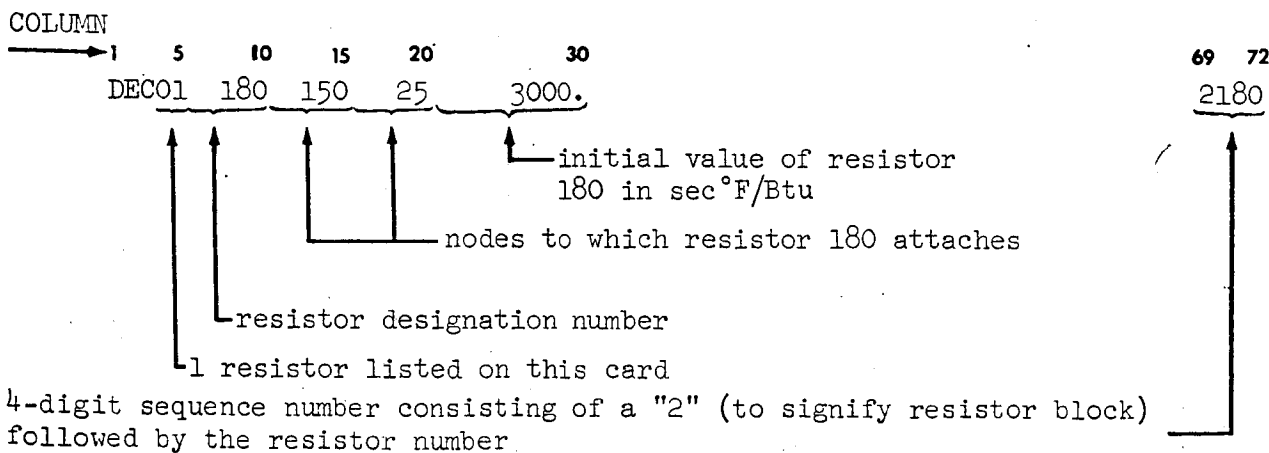
T(1) through T(49) have an initial temperature of 70°F.  
 T(50) through T(79) have an initial temperature of 100°F.  
 T(80) has an initial temperature of 20°F.

Note that storage is reserved for nodes 1 through 80 whether they are used or not. Thus, these locations may be used for storing miscellaneous floating-point data.

The initial temperature block, as well as the resistor, capacitor, data, and time blocks, must be terminated with an NBK card.

BLOCK 2, RESISTORS

Each resistor is listed by the designation number of the resistor, followed by the designation numbers of the two nodes which the resistor connects, followed by the initial value of the resistor. In those cases where all values of a resistor are to be computed by a function, a dummy initial value (as zero) must be given. All resistors must be given in this block even though they may be described later (for instance, radiation resistors). Up to 2 resistors may be listed on a card. An example of a resistor input is shown below.



An input option provides for the program to compute its own resistor values, given the resistor geometry and a curve of the material conductivity as a function of temperature. The resistor is computed by the formula

$$R = \frac{\delta}{kwd} \sim \frac{\text{sec}^\circ\text{F}}{\text{Btu}}$$

where

- $\delta$  = the distance along conductive path
- k = the thermal conductivity
- w,d = the width and depth of the cross-sectional conductive heat transfer area

The resistor is automatically computed if described in block 2 as follows:

COLUMN	1	5	10	15	20	30	40	50	55
→	RES01	A	B	C	$\delta$	w	d	N	

where

- A = the resistor designation number
- B,C = the nodes which resistor A connects
- $\delta$ ,w,d = the length, width, and depth of the resistor
- N = the designation number of the curve containing the material conductivity as a function of temperature

Any consistent set of units may be employed. A, B, C, and N are listed in fixed-point notation in 5-column fields.  $\delta$ ,w, and d are given in floating-point in 10-column fields. The program updates the resistor value each computing cycle, after interpolating for the conductivity as a function of the temperature of node B.

This option is applicable only when the resistor cross-section is uniform. The conductivity curve can be described in the data block, or may be called in from the thermal properties library.



BLOCK 3, CAPACITORS

Each node at which there is a capacitor is listed by that node's designation number (already assigned in block 1), followed by the value of the capacitor. If the capacity is to be computed by a function, a dummy initial value must be given.

At each node for which a capacitor is specified, i.e., appears explicitly in the capacitor block, a new temperature is computed for that node. If, however, no capacitor is specified for a given node, no heat balance is computed, and the temperature of that node remains unchanged, unless changed by a function statement.

Up to four capacitor values can be listed on a card. An example of a capacitor input is shown below:

COLUMN	1	5	10	20	69	72
→	DECO1	25	.117		3025	

↑ value of capacitor 25 in Btu/°F  
 ↑ capacitor (node) designation number  
 ↑ number of capacitors listed on this card

4-digit sequence number consisting of "3" (to signify capacitor block) followed by the capacitor designation number.

An input option provides for the program to compute its own capacitor values, given the node geometry and curves of density and specific heat as a function of temperature. The capacitor is computed by the formula

$$C = \delta w d \rho c \quad \frac{\text{Btu}}{^\circ\text{F}}$$

where

$\delta, w, d$  = the length, width, and depth of the node

$\rho$  = the material density

$c$  = the material specific heat

The capacitor is automatically computed if described in block 3 as follows:

COLUMN	1	5	10	20	30	40	45	50
→	1	5	10	20	30	40	45	50
	CAPO1	A	$\delta$	w	d	$N_1$	$N_2$	

where

A = the capacitor designation number

$N_1$  = the designation number of the curve containing the material specific heat vs temperature

$N_2$  = the designation number of the curve containing the material density vs temperature

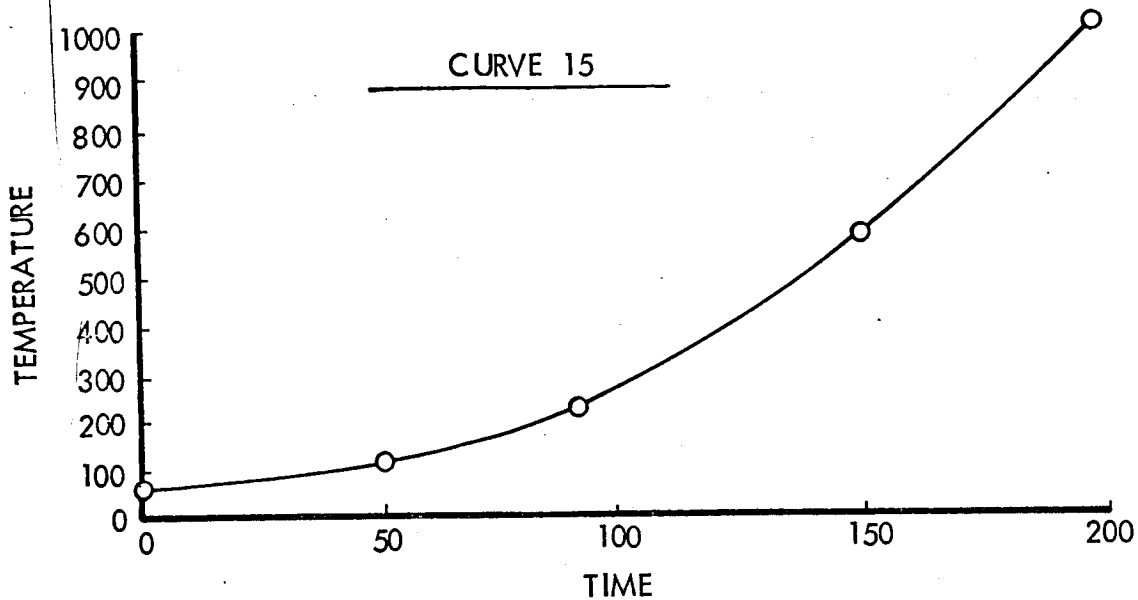
Any consistent set of units may be employed. A,  $N_1$  and  $N_2$  are given in fixed-point notation in 5-column fields, and  $\delta$ , w, and d are given in floating-point notation in 10-column fields. The capacitance of node A is updated each computing cycle, after the program interpolates curves  $N_1$  and  $N_2$  for the specific heat and density.

#### BLOCK 4, INPUT DATA

Block 4 consists of individual sub-blocks of input data which are used by the functions. The function which uses the data determines the nature of the numbers in the sub-block. For instance, the data might be the point by point description of a curve which the function will use for interpolation. Also, the data block is very convenient as a storage for data constants used for special calculations, or as temporary storage to be used as required during various portions of the program.

Each sub-block of data is identified by a fixed-point number called the designation number of the sub-block. The designation numbers are arbitrary, but can be used only once. A DEC card with the designation number listed in columns 6 through 10 must precede the sub-block, and a DEC card with the negative of the designation number listed in columns 6 through 10 must terminate the sub-block.

To illustrate, suppose that the curve plotted below is to be described in the data block.



Curve 15 would appear on the input data sheet as follows:

COLUMN	1	5	10	15	25	35	45	55	65	69	72
DEC			15								4001
DEC06				0.	60.	50.	110.	90.	220.		4002
DEC05			150.		570.	200.	1000.	0.			4003
DEC		-15									4004

In block 4, the sequence numbers are often assigned as consecutive integers starting with 4001. In the above example, card 4001 contains the curve designating number, and card 4004 contains the negative of the curve designation number. The actual curve is described on cards 4002 and 4003 by listing the coordinates of the points circled on the plotted curve. Each independent variable must immediately precede the corresponding dependent variable, and the independent variables must be listed in increasing order. The number of points needed to describe a curve depends on the accuracy required, and the type of interpolation routine employed. The machine as yet does not know whether the variables are time, temperature, or something else;

this information being given in the FUNCT subroutine. The zero on card 4003 is a flag indicating the end of the curve. This flag can be any number as long as it is less than the preceding value of the independent variable, which in this example is 200. This point is important, for if all values of the independent variable were negative, then the zero would not be correct. If, for example, the last value of the independent variable were -50., the end-of-curve flag would have to be something like -51.

The designation number of a sub-block may be used in the FUNCT and PRINT subroutines to refer to a particular element in the sub-block. Before such a reference can be made, however, a locating statement must be made in the subroutine in which the reference is made. For example, to refer to a value in curve 15 above, the statement

$$L15 = LOC(15)$$

is first necessary. Then the sixth number in curve 15 (in this case the value 220.) would be referred to as

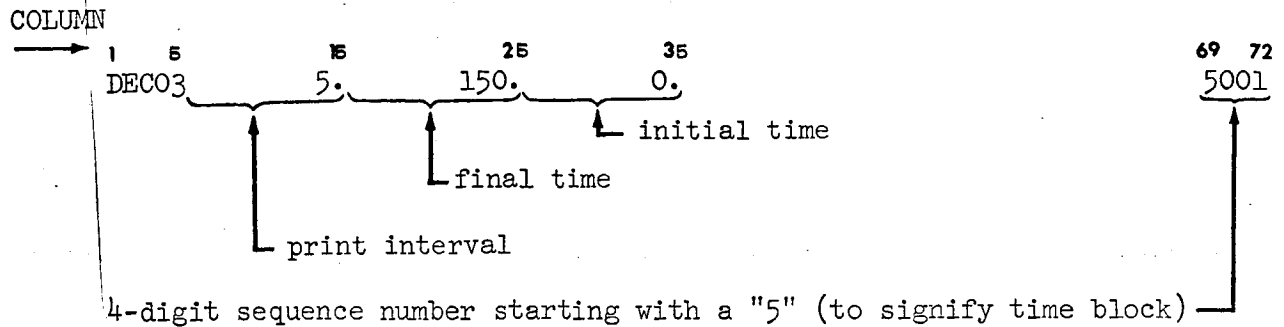
$$P(L15 + 6)$$

In determining the sixth number note that the table designation number itself is not counted. Also, if this had been a periodic curve, the value given for the period would not be counted.

As stated previously, the data block must be terminated with an NBK card. Occasionally, a thermal analyzer problem will be run in which block 4 is not required. In this case two consecutive NBK cards must appear at the end of the capacitor block.

#### BLOCK 5, TIME CONSTANTS

Block 5 contains the printing interval, the final time of the case, and the initial time of the case. These are the only three quantities to appear in block 5, and they must be given in the order listed above. The unit of time must be consistent with that used throughout the problem, normally seconds. A sample time block is shown on the following page.



These items can, of course, be listed on separate cards, thus allowing room for comments following the numbers.

### RESTART BLOCKS

Many times it is desired to run several cases which are basically similar, differing only in the values of certain parameters. An example of this is a parametric study of the insulation thickness required for a given application where only resistor and capacitor values are changed between cases. Another example is an Earth-orbiting vehicle, where solar inputs can vary depending upon the angle between the Earth-sun line and the orbit plane. The restart can also be used to string several transient cases together, with the final temperatures of one case being used as the initial temperatures for the case which follows.

To use the restart feature, one or more restart blocks (each one constituting a separate case) can be added, with each restart block causing the preceding case to be re-run as a new case with certain changes as indicated in the restart block. A restart block can change any or all of the data sub-blocks, but if a data sub-block, e.g., a curve, is changed, it must be restarted in its entirety together with the same designation number used in the original case and it must contain the same or fewer numbers than the data sub-block being replaced. If the curve is periodic, the PER card must be included in the restart. Also, a restart block can change the time block, but if the time block is changed, it must be restarted in its entirety. If more than one restart block follows a case, each succeeding restart block is interpreted to be changes to the immediately preceding case, and not changes to the original case.

Since each restart is a separate case, a CID card is inserted ahead of each restart to identify the output. This card is not mandatory, but its use is recommended. The next card is a flag indicating to which block the cards following the flag refer. The flags are as follows (note absence of decimal point):

COLUMN		IO	
→ 1			
DEC	1		New initial temperatures
DEC	2		New resistors
DEC	3		New capacitances
DEC	4		New time block
DEC	5		New data sub-blocks

Immediately following each of the initial value change flags (1, 2, or 3) are the change cards. Each of these change cards contains two items, the first being the designation number of the item to be changed and the second being the new initial value of that item. A DEC 0 card ends each set of change cards pertaining to a particular class of quantities, e.g., resistors. If the time block is to be changed, a DEC 4 card followed by the complete time block, i.e., print interval, final time and initial time, plus a DEC 0 at the end is required. A DEC 5 card precedes the new data sub-blocks, with a DEC 0 card after the last new sub-block. Each restart block, i.e., all the changes required for a given case, is terminated with an NBK card.

As an example of a restart, the following changes are to be made in a case:

- (a)  $T(17) = 50.$
- (b)  $R(15) = 6000.$
- (c)  $C(11) = 0.031$
- (d) New linear curve 40, where,

$$y = 17. \text{ at } x = 0.$$

$$y = 53. \text{ at } x = 100.$$

- (e) New time block, where,

$$M(4) = 10.$$

$$M(3) = 500.$$

$$M(2) = 150.$$

The input is shown on the following page. The order in which the various blocks are changed is arbitrary.

COLUMN	1	10	15	20	25
	CID	RESTART	EXAMPLE		
	DEC	2			Change resistors
	DECO1	15	6000.		
	DEC	0			
	DEC	1			Change temperatures
	DECO1	17	50.		
	DEC	0			
	DEC	4			Change time block
	DECO1		10.		New print interval
	DECO1		500.		New final time
	DECO1		150.		New initial time
	DEC	0			
	DEC	3			Change capacitors
	DECO1	11	.031		
	DEC	0			
	DEC	5			Change data block
	DEC	40			New curve 40
	DECO2		0.	17.	
	DECO2		100.	53.	
	DECO1		0.		End curve 40
	DEC	-40			
	DEC	0			End curve changes
	NBK				End restart block

One very useful application of the restart feature is in the analysis of an Earth-orbiting vehicle for which several sets of solar inputs may be applicable depending upon the orientation of the orbit plane with respect to the Earth-sun line. For this case the basic deck incorporates only the storage required to accommodate the solar data. To prevent the basic deck from running, the initial and final times should be input as zero. The correct time block can then be included in the various restart decks which load the particular solar inputs for each orbit orientation.

The following points should be kept in mind when using restarts:

- A restart block can only change values which had been given in the original case.
- A restart cannot change the structure of the network, i.e., the way the various resistors and capacitors are connected.
- A restart cannot add or delete data sub-blocks, but merely change the data contained in these sub-blocks.
- A restart block cannot change the FUNCT or the PRINT subroutines.
- The data within a restart block can be incremented, but those increment cards used in the original case are no longer applicable and must be repeated if the restart data is to be incremented.

FUNCT SUBROUTINE

The FUNCT subroutine is an ordinary FORTRAN subroutine in which the user lists all curve interpolations, arithmetic operations, and special functions to be performed during program execution. These functions are executed at the beginning of each computing cycle, before the heat balance is performed. A standard input format is described below so that the user need not have a knowledge of FORTRAN to prepare this routine. If the user is familiar with FORTRAN he should still learn to fill out the forms as described, but then should not hesitate to employ his knowledge to supplement the capabilities of the prepared program.

The input form for the FUNCT subroutine is illustrated in Table 5-1. All of the information shown must appear in the subroutine and, with the exception of the functions, these are generally the only items which must appear. With the exception of the first card, the information begins in column 7. A four-digit sequence number is placed in columns 77 through 80 of each card as a convenience in sorting or making changes to the deck.

The statement \$IBFTC FUNCT on the first card identifies the function subroutine and must be input as shown. The statement NODECK, NOREF will delete from the output the internal reference listing for the subroutine and will eliminate the punching of a binary deck. If either of these items is desired, replace NODECK (or NOREF) with DECK (or REF), leaving no blank spaces; e.g., DECK, REF.

The statement SUBROUTINE FUNCT sets up the linkage between the FUNCT subroutine and the calling program, and must be input as shown.

The variables listed in the COMMON declaration are assigned locations in a reserved section of core so they will not be destroyed by overlay operations. Card 6003 must also appear as shown.

The DIMENSION declaration tells the processor how much space in memory must be allocated or reserved for each collection of elements. Each variable which appears in the program in subscripted form must appear in a DIMENSION statement, and the statement must precede the first appearance of the variable. For example, on card 6004, 16 storages are reserved for the collection of elements called M, which are defined in Section IV. The DIMENSION declaration should be filled out exactly as shown. If the user wishes to add another



TABLE 5-1  
INPUT FORMAT FOR FUNCT SUBROUTINE

GENERAL PURPOSE DATA SHEET				LOCKHEED-CALIFORNIA COMPANY A DIVISION OF LOCKHEED AIRCRAFT CORPORATION		PAGE	OF
PREPARED	NAME	DATE	TITLE	WO	EWA	JOB NO.	GROUP
CHECKED							
ID							
77	80	1					
6001	IBFTC	FUNCT	NODECK, NOREF				
6002			SUBROUTINE FUNCT				
6003			COMMON P, M				
6004			DIMENSION P(16000), M(16), TN(1), T(1), R(1), C(1), Q(1), RC(1)				
6005			EQUIVALENCE (P(1), TN(1)),				
1							
6006			1 (P				
6007			2 (P				
6008			3 (P				
6009			4 (P				
6010			5 (P				
1							
6011			REAL M, LIN				
6998			RETURN				
6999			END				
1							
70	72	73	76				

FORM D4 7924-1



subscripted variable to the subroutine, storage may be reserved by including on card 6004 the name of the variable followed in parentheses by the number of quantities requiring storage space. Alternately, a second DIMENSION card could be added to accomplish the same purpose.

From the user's standpoint the EQUIVALENCE declaration is required so that he may refer to the temperatures, resistors, capacitors and heating rates in terms which are meaningful to him. As an example, it allows the user to refer to a particular temperature by a T followed in parentheses by the node designation number. The user must fill in the blank spaces within the parentheses on cards 6006 through 6010 with the five integers defined below:

<u>CARD</u>	<u>INTEGER</u>
6006	$j=1 + \text{greatest temperature designation number}$
6007	$k=j + \text{greatest temperature designation number}$
6008	$m=k + \text{greatest resistor designation number}$
6009	$n=m + \text{greatest capacitor designation number}$
6010	$p=n + \text{greatest capacitor designation number}$

Since columns 7 through 72 are all available for data input, the EQUIVALENCE declaration could actually be written on two cards, instead of six as shown. The integers in column 6 are codes indicating that the information on that card is a continuation of the information on the previous card.

The REAL statement defines the variables M and LIN as floating-point values, since ordinarily these variable names are reserved for fixed-point values.

Next, all functions which the program is required to execute are listed, in the order of their execution. The order of execution is generally unimportant except when the execution of one function involves the result of another. For the user's convenience, the functions discussed in Section IV are summarized in Table 5-2.

The FUNCT subroutine is always terminated with the RETURN statement and the END declaration. The RETURN statement marks the completion of the intended task, and returns control to the calling program. The END declaration merely signals the processor that there are no more cards to be translated for that program.

TABLE 5-2.  
SUMMARY OF FUNCTIONS AND SPECIAL SUBROUTINES

FUNCTION	EXAMPLE	MEANING
LINEAR INTERPOLATION	Y=LIN(X,N)	Y is a linear function of X given by curve N
PARABOLIC INTERPOLATION	Y=PAR(X,N)	Y is a parabolic function of X given by curve N
BIVARIATE INTERPOLATION	Y=BIV(X1,X2,N)	Y is a bivariate function of X1 and X2 given by table N
LINEAR INTERPOLATION WITH INTEGRATION	K=XLIN(X1,X2,N)	K (thermal conductivity of insulating material) is $\frac{1}{X2-X1} \int_{X1}^{X2} F_N(X) dx,$ <p>where X1 and X2 are the temperatures of the nodes on each side of the insulation</p>
RADIATION WITH CONSTANT FACTOR	R(A)=RAD(B,C,K)	Resistor A connects nodes B and C and the K factor is a fixed constant.
RADIATION WITH VARIABLE FACTOR	R(A)=RAD(B,C,X)	Resistor A connects nodes B and C and the K factor is stored in the circuit element X.
RADIATION WITH MATRIX	R(A)=RRM(B,C,N)	Resistor A connects nodes B and C and table N contains the data used to compute the K factors.
CONVERGENCE	CALL CVG(A,N,M)	The heat balance and list of functions are evaluated repeatedly until the temperatures reach the required convergence, A. A maximum of N iterations are to be performed, and a print is required every M-th iteration. If M is negative, convergence will be attempted with all capacitors set to zero.

TABLE 5-2 (Cont)

FUNCTION	EXAMPLE	MEANING
STEADY STATE	CALL STS(A)	All capacitors are set to zero, the function list is ignored, and the heat balance evaluated repeatedly until the required convergence, A, is obtained.
MAXIMUM-MINIMUM	CALL MMF( $\theta_i$ , $\theta_f$ , N,S)	The program searches the output every S-th computing cycle between times $\theta_i$ and $\theta_f$ to determine the maximum and the minimum temperatures of the nodes listed in table N.
SAVE CURRENT DATA	CALL SAV(A,B)	If A (usually current time) is greater than B, the data currently in core are stored on tape and used as initial conditions in the subsequent case.
INITIAL TEMPERATURE CARD PUNCH	CALL PUNCHT ( $\theta$ ,A,B)	The temperatures A through B at time $\theta$ are recorded on punched cards in proper format for the initial temperature block.
CURVE PLOTTING	CALL TPLOTT(N)	The temperatures of all nodes listed in table N are to be machine plotted.
AERODYNAMIC HEATING	CALL EAH i(j,K, $H, \alpha_o, F$ )	The aerodynamic heating to node j is to be computed by the reference temperature method. K is the Eckert K factor, H is the location where the calculated heat transfer coefficient is to be stored, $\alpha_o$ is the surface angle of attack, and F is a code indicating whether node j is located on an upper or lower surface. H, $\alpha_o$ , and F are optional inputs.
ABLATION	CALL ABL(i,N)	The surface (ablating) node number is i and table N contains the ablator properties used to calculate the network parameters.

PRINT SUBROUTINE

The PRINT subroutine is an ordinary FORTRAN subroutine in which the user specifies the quantities that are to be printed out at each printing interval, and the desired output format. Like the FUNCT subroutine, no knowledge of FORTRAN is necessary to prepare this routine. However, to take advantage of the ability to specify the output format, the user is encouraged to learn the basic rules in writing format statements. In the discussion which follows, emphasis is placed on the input for a "standard" print format which will be acceptable to the user in most cases. This format lists the data in six full columns, with the corresponding time appearing by itself to the left of the first row of output. None of the quantities are labeled, but this is of little consequence unless a very large number of quantities are being printed. The advantages of this format are its simplicity and the fact that it requires no knowledge of format statements by the user. Following the explanation of this "standard" format, some of the general rules pertaining to the writing of format statements are reviewed for those who wish to label their output.

Standard Print Format

The input form for the PRINT subroutine is illustrated in Table 5-3. The first eleven cards contain essentially the same information as the corresponding cards in the FUNCT subroutine (Table 5-1). The blank spaces in the EQUIVALENCE declaration must be filled in with the integers j, k, m, n, and p defined in the preceding section. The REAL statement in the PRINT subroutine does not declare LIN to be a real, or floating-point, value since the variable LIN will not ordinarily appear in this subroutine.

The WRITE statement specifies the quantities to be printed and references the statement number of the FORMAT declaration which specifies the arrangement of the output data. The general form of the WRITE statement is

WRITE (6,N) A,B,C,....

where 6 is the designation number of the system output tape, N is the number of the corresponding FORMAT declaration, and the quantities A, B, C, etc.,

TABLE 5-3  
INPUT FORMAT FOR PRINT SUBROUTINE

GENERAL PURPOSE DATA SHEET				LOCKHEED-CALIFORNIA COMPANY A DIVISION OF LOCKHEED AIRCRAFT CORPORATION		PAGE	OF
PREPARED	NAME	DATE	TITLE		JOB NO.		
CHECKED			WO	EWA	GROUP		
77	80	1	70	72	73	76	
7001	#IBFTC PRINT	NODECK, NOREF					
7002	SUBROUTINE PRINT						
7003	COMMON P, M						
7004	DIMENSION P(16000), M(16), TN(1), T(1), R(1), C(1), Q(1), RC(1)						
7005	EQUIVALENCE (P(1), TN(1)),						
7006	1	( P )					
7007	2	( P )					
7008	3	( P )					
7009	4	( P )					
7010	5	( P )					
7011	REAL M						
7012	WRITE (6, 10) M(1),						
7013	1						
7014	2						
7015	3						
7016	4						
7017	5						
7018	6						
7019	7						
7020	8						
7021	9						
7022	A						
7023	10	FORMAT (1H0, 7E18.8/(19X, 6E18.8))					
7024	RETURN						
7025	END						

FORM DX 7924.1

are to be printed in that order. On card 7012, for example, the statement

```
WRITE (6,10) M(1),
```

will cause the value of current time to be printed first. The user should then list the remaining items of interest, separated by commas, in the order in which they are to be printed. Any addressable element may be printed out. Although not required by the program, if the standard six-column format is used, these elements should be listed six to a card for convenience in identifying the output. There is no limit to the number of items that may be printed. Any character other than 0 (zero) or a blank may be used in column 6 as a continuation flag. However, the maximum number of continuation cards in any statement is 19. If more than 20 lines are required, the remaining items are listed on additional WRITE statements, all of which begin

```
WRITE (6,10)
```

When the designation numbers to be listed in a WRITE statement are consecutive, they can be abbreviated. To illustrate, if the temperatures of nodes 20 through 85 are to be printed consecutively, an acceptable WRITE statement is

```
WRITE (6,10) (T(I), I=20,85)
```

The FORMAT statement shown in Table 5-3 calls for the values to be printed out using the E format (for powers of 10), with seven quantities listed on the first line, and six on each remaining line.

The PRINT subroutine must be terminated with the RETURN and END cards.

The output format described above is illustrated in Example #1 of Section VI. The following section describes the FORMAT declaration in more detail for those who wish to take advantage of the opportunity to specify the output format.

#### FORMAT Declarations

When the results are to be printed on one or more lines of paper, the computer must know how the information is to be distributed among the columns on each printed line. The information to be printed on a particular line may be thought of as a unit output record. Some line printers for the IBM 1401

and 1410 computers can accept unit output records containing 100 characters while other printers, such as the 1401 with special features, provide 132 printer columns. The following discussion pertaining to output will assume the use of a line printer which can accept records containing 132 characters. Regardless of the printer used, the first character of each record is actually not printed. Instead, it is interpreted by the printer as a special code for control of paper movement just prior to printing the record. As a result, only 131 characters are available to the user to become printed information on 131 columns of the printed line.

Each unit output record is made up of one or more fields, a field being a group of one or more columns whose contents can or must be described separately. Each field is described by a format code which specifies the form, size, and location of each field from left to right within each of one or more records. The purpose of the FORMAT declaration is to make this code available to the computer during execution of the WRITE statement. The remainder of this section is concerned with the definition, description, and use of format codes.

Field Specification Codes - Numerical output will take one of the following three forms:

1. Integers (I-fields) - Integers are printed out without decimal point; for example,

$$\pm XXX$$

2. Floating Point With Exponent (E-fields) - When using this form, the decimal point is printed immediately to the left of the leading significant digit; for example,

$$\pm 0.X_1 X_2 X_3 X_4 E \pm n_1 n_2$$

applies to a request for 4 decimal places.

3. Floating Point Without Exponentiation (F-fields) - An example of this form applicable to a request for 5 decimal places is

$$\pm X_1 X_2 X_3 . X_4 X_5 X_6 X_7 X_8$$



In all three examples, the negative sign will appear if the quantity is negative, but the + sign will never appear.

A field specification for an I-, E-, or F-field consists of one of the letters I, E, or F followed by an integer which specifies the size of the field, i.e., the number of available columns to be used. If the E or F field is specified, an additional code is required to denote the location of the decimal point. For example, I6 specifies a six-column integer field, and F10.5 specifies a ten column F-field with five numbers following the decimal point. Caution should be exercised in specifying the field width of E-fields since accuracy to one significant digit only requires an E-field of eight columns, i.e.,

$$\pm 0.X_1 E \pm m_1 n_1$$

As examples of the general output appearance of E and F fields, consider the number -13.175492. The output appearance for several different field specification codes are shown below:

<u>Code</u>	<u>Output Appearance</u>
F10.6	-13.175492
F10.3	-13.175
F10.0	-13.
E10.3	-0.132E 02
E10.4	0.1318E 02 (invalid)

Note that E-field specifications must provide at least 7 columns in excess of the number of decimal places required. Regardless of the format code, the last digit always appears in the last column of the field.

Format Declarations for Records Containing Numerical Data Only - The general form of the FORMAT declaration is simply a statement number followed by the word FORMAT followed by the format code in parentheses; i.e.,

NN FORMAT (format code)

Its use is best explained by examples. Suppose that we wish to print the variables M(5), T(6), R(18), C(26), J1, and KLOD in that order. The first

four are floating point variables, and the latter two are fixed point. If the WRITE statement were

```
WRITE(6,35) M(5), T(6), R(18), C(26), J1, KLOD
```

the FORMAT declaration might appear as

```
35 FORMAT (F10.4, F10.4, F10.4, F10.4, I5, I5)
```

or

```
35 FORMAT (4F10.4, 2I5)
```

Both formats would result in identical outputs consisting of a 10-column F-field for the floating point numbers, and a 5 column integer field for the fixed point numbers. The printed line might appear as follows (note that the first column is always skipped):

COLUMN							
→	2	10	20	30	40	45	50
	50.0000	-31.7183	8267.9526	1.8913	6	-83	

Parentheses may be used within the format code to indicate repetition of the format description within the parentheses for all succeeding lines. For example, the WRITE statement

```
WRITE (6,10)(T(I), I=1,50)
```

and corresponding FORMAT declaration

```
10 FORMAT (6E15.4/(7F15.2))
```

will cause the first six temperatures to be printed on the first line using the E-field format. Then, the remaining 44 temperatures will be listed, seven per line using the F-field format. The slash (/) indicates the end of a record, i.e., the end of a printed line, as explained in the next section.

Printer Carriage Control - In order to print an output record, the line printer must first be told on which line that record should be printed. With this information, the printer can then move the carriage which holds the paper the desired amount just prior to the printing of a line. The printer receives the desired carriage control information in the form of a one character code placed at the first of the output record being readied for printing. The first position of the record, therefore, is never printed and is always assumed to be a carriage control code. It is therefore imperative that each output record be format coded to provide a carriage control code in the first column.

Single line spacing means that the paper is advanced one line before printing. The code for single line spacing is a blank ( $\square$ ). With some risk of error, a blank is ensured if the first field is an I-, E-, or F-field which has been provided with more than enough columns to print the given number. A much safer approach is to force a blank in the first character of the output record by making the first field a skip field. This is accomplished by incorporating in the format code the specification mnX, where mn is an integer representing the number of columns to be skipped. Some examples are given below.

In the last example of the preceding section

```
FORMAT (6E15.4/(7F15.2))
```

was assumed to be a suitable FORMAT declaration. A much preferred form, in which we are certain to have a blank as the leading character of each record, is

```
FORMAT (1X,6E15.4/(1X,7F15.2))
```

When this form is used, each new record described begins with a 1X field. The first line has the format 1X,6E15.4 and all succeeding lines are described as 1X,7F15.2.

Line spacing is accomplished by use of a slash (/) or multiple slashes ahead of or following any record description. The above example is now repeated several times to illustrate this technique:

Example 1

```
FORMAT (1X,6E15.4//(1X,7F15.2))
```

The double slash causes an extra blank line to appear after the first line is printed. The first slash marks the end of the first line and the second slash marks the end of the second line.

Example 2

```
FORMAT (1X,6E15.4////(1X,7F15.2))
```

By the same reasoning quadruple slashes cause three extra blank lines. In general, N slashes appearing at the end of a record description will produce N-1 extra lines after that record.

Example 3

```
FORMAT (1X,6E15.4/(1X,7F15.2)/)
```

The slash before the final right parentheses does not cause an extra line. The combination "/" has the same effect as the final parentheses ")" by itself.

Example 4

```
FORMAT (1X,6E15.4/(1X,7F15.2)//)
```

The double slash causes one extra blank line after each record coded (1X,7F15.2).

Example 5

```
FORMAT (//1X,6E15.4/(1X,7F15.2))
```

The double slash causes two blank lines before the first record is printed, so the printing begins on the third line. In general, if N slashes appear at the very beginning of the format code, N extra blank lines will result.

Hollerith Fields - The use of a Hollerith or H-field enables the user to provide for the printing of alphameric words or phrases in the form of comments, titles, headings, etc., to explain the numerical results being printed. Use of H-fields, while frequently desirable, is optional. An H-field is of the form

sssHccc...ccc

where

sss is a space count which may be any integer up to 132.

H is the symbol identifying the Hollerith field.

ccc...ccc denotes the contents of the sss spaces following immediately after the letter H; ccc...ccc includes all blanks and special characters, i.e., all blank spaces indicated by the symbol  $\square$  must be included in the space count.

Hollerith fields are especially useful to print messages, titles, and headings without calling for the value of variables. Also, they can be used for line-printer carriage control. Since the use of a line printer requires that the first position of any output record be a carriage control character it is convenient to introduce a one space Hollerith field as the first field of every output record, as shown below.

<u>Desired Paper Movement Upward</u>	<u>Required Carriage Control Code</u>	<u>Simplest Way of Coding</u>
one line	$\square$ (a blank)	1 H $\square$
two lines	0 (zero)	1 H 0
skip to top of next page	1	1 H 1

To illustrate, the format used as an example above

```
FORMAT (1X,6E15.4/(1X,7F15.2))
```

could be written

```
FORMAT (1H $\square$ 6E15.4/(1H $\square$ 7F15.2))
```

and in each case the output would appear the same, i.e., single-spaced. If we wished to start printing at the top of the page, the appropriate format code is

```
FORMAT (1H16E15.4/(1H $\square$ 7F15.2))
```

To further illustrate the use of Hollerith fields assume that it is desired to list the current time M(1), print interval M(15), minimum RC product M(6), and the node at which the minimum RC product appears M(9).

Furthermore, this information is to be printed on one line and labeled as follows:

```
TIME=XXXXXXX. ^ SECONDS ^^^^^ COMP. ^ INTERVAL=XXXX.XXX ^ SECONDS ^^^^^ (RC)MIN=XXXX.XXX ^
SECONDS ^ AT ^ NODEXXXXXX.
```

The carets (^) indicate that a blank space is to be provided. If a paper movement of two lines (double space) is desired before writing this line, the appropriate WRITE statement and FORMAT declarations appear as follows:

```
WRITE (6,837) M(1), M(15), M(6), M(9)
```

```
837 FORMAT (6H0 TIME=,F8.0,8H0 SECONDS,5X,15HCOMP.0 INTERVAL=F8.3,8H0 SECONDS,
1 5X,8H(RC)MIN=,F8.3,16H0 SECONDS0 AT0 NODE,F6.0)
```

The following remarks pertaining to the above FORMAT declaration are applicable:

1. The zero in the first Hollerith field serves as carriage control, moving the paper upward two lines.
2. Any character lying within the Hollerith field, i.e., any character found within the sss spaces following the H, will be printed exactly as it appears in the format code. These spaces within the H-field must be counted carefully to ensure that the correct space count is used. An error in the space count will usually render the format code invalid.
3. It is not necessary to separate by a comma an H-field from any characters which follow it on the right. Thus, in

```
8H(RC)MIN=,F8.3....
```

the comma could be optionally omitted after the equal sign. The comma in

```
F8.3,16H0 SECONDS.....
```

is required. The reason is that commas are required to mark the end of one field code and the beginning of another when the computer has no other means of determining this demarcation. Due to space count, an H-field, unlike other field codes, provides sufficient information for the computer to determine where it ends.

4. The integer 1 on the second line of the FORMAT declaration is a continuation code, and appears in column 6.

The reader should now be in a position to interpret the "standard" Format code given in the Section "Standard Print Format", i.e.,

```
FORMAT (1H0,7E18.8/(19X,6E18.8))
```

After the paper is advanced 2 lines, the first 7 numerical quantities are listed, using an 18 column E-field format. On each succeeding line the first 19 spaces are skipped, followed by 6 numerical quantities again using the E-field format.

Alphameric Fields - Alphameric or "BCD" information may be stored internally in the computer and printed out when desired using the A-field code. This code has the following form:

Axx

where xx is the field width or the number of columns allocated for the field, and A is the code letter for this type of field.

The use of A-fields will not be discussed in detail except for explaining the procedure to have the information on the CID card printed in the output. To accomplish this, the COMMON card in the PRINT subroutine must appear as

```
COMMON P,M,MISCEL(23),CID(12)
```

Then, assuming the FORMAT declaration is statement number 101 and it is desired to skip to the top of the next page, the WRITE statement and FORMAT declarations appear as follows:

```
WRITE (6,101)(CID(I),I=1,12)
```

```
101 FORMAT (1H1///33X,12A6)
```

The triple slash will cause the top two lines to be skipped. Thirty-three spaces are skipped to approximately center the CID information on the top of the page. The line skipping and centering are, of course, optional.

## VI - EXAMPLE PROBLEMS

Two examples demonstrating the various program features are presented in this section. These problems are worked in detail to show the complete process involved in converting the physical system into an equivalent RC network and the transcription of this network onto the data sheets from which the data cards are punched. The computer output is shown for both problems.

EXAMPLE #1 - Temperature response of an equipment-mounting plate during sub-orbital test flight of a lifting re-entry vehicle.

Problem Description

A number of heat-dissipating electronic components are mounted on a 0.10-in. aluminum plate in the equipment bay of an unmanned lifting re-entry test vehicle. The plate and equipment radiate on both sides to quartz fiber insulation attached to the internal surfaces of the upper and lower skins. The skin temperatures are known functions of time from a separate ascent and re-entry heating analysis. Assuming a mean heat dissipation of 100-w/sq ft ( $0.095 \text{ Btu/sec-ft}^2$ ) and an equipment density of 25 psf, the problem is to determine the temperature rise of the aluminum plate and equipment during the suborbital flight. The physical picture and corresponding thermal network are shown in Figure 6-1.

The insulation is divided into lumps either 1.0 in. or 0.5 in. thick, with nodes appearing on the interior boundaries where radiation to the equipment plate occurs. Although node and resistor designation numbers are completely arbitrary a systematic scheme is employed for convenience. The following material properties are assumed.



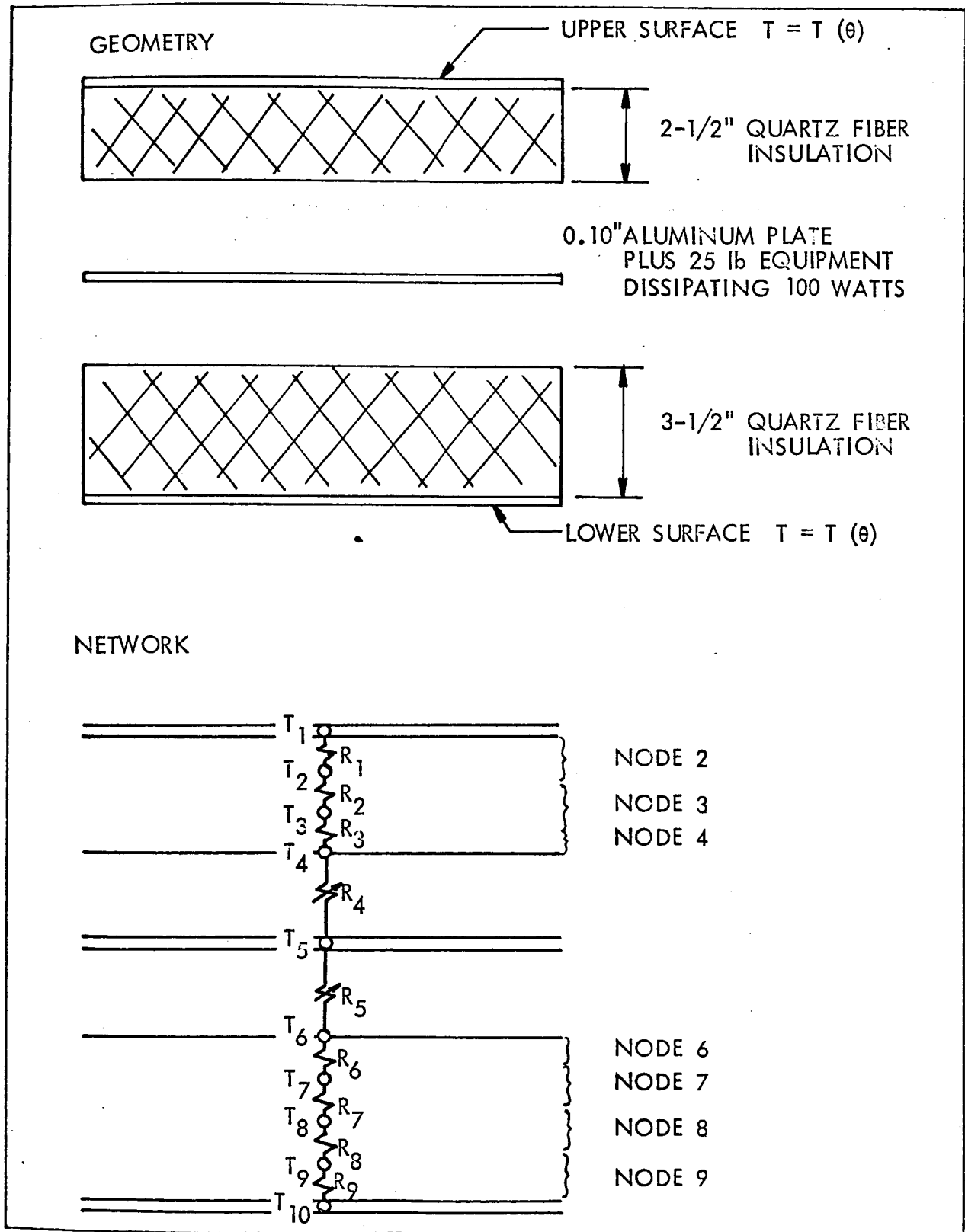


Figure 6-1. Physical Geometry and Corresponding Thermal Network for Example Problem 1

<u>Property</u>	<u>Insulation</u>	<u>Aluminum</u>
k = thermal conductivity (Btu/hr ft°F)	0.06	NR
c = specific heat (Btu/lb°F)	0.25	0.20
ρ = density (lb/ft <sup>3</sup> )	3.0	175
ε = surface emissivity	0.8	0.1

### Conduction Resistors

$$R_2 = R_3 = R_6 = R_7 = R_8 = \frac{3600 \delta}{kA} = \frac{(3600) \left( \frac{1}{12} \right)}{(0.06)(1)} = 5000 \frac{\text{sec}^\circ\text{F}}{\text{Btu}}$$

$$R_1 = R_9 = \frac{3600 \delta}{kA} = \frac{3600 \frac{0.5}{12}}{(0.06)(1)} = 2500 \frac{\text{sec}^\circ\text{F}}{\text{Btu}}$$

The resistance through the external skins is neglected, since it is negligible compared with that through the insulation.

### Radiation Resistors

The radiation K factors are computed using the effective emissivity factor given by the infinite parallel plate formula, and a view factor of unity.

$$\epsilon_{12} = \frac{1}{\frac{1}{\epsilon_1} + \frac{1}{\epsilon_2} - 1} = \frac{1}{\frac{1}{0.1} + \frac{1}{0.8} - 1} = 0.0975$$

$$K_4 = K_5 = \frac{\epsilon_{12} FA}{3600} = \frac{(0.0975)(1.0)(1.0)}{3600} = 2.71 \times 10^{-5}$$

### Capacitors

For the insulation nodes:

$$C_2 = C_3 = C_7 = C_8 = C_9 = \rho c \delta A = (3.0)(0.25) \left( \frac{1}{12} \right) (1) = 0.0625 \frac{\text{Btu}}{^\circ\text{F}}$$

$$C_4 = C_6 = \rho c \delta A = (3.0)(0.25) \left( \frac{0.5}{12} \right) (1) = 0.0313 \frac{\text{Btu}}{^\circ\text{F}}$$

For the equipment and mounting plate, assuming an average specific heat of 0.15 for the electronic components:

$$C5 = 25(0.15) + \rho c \delta A = 3.75 + 175(0.2) \left( \frac{0.1}{12} \right) (1) = 4.04 \frac{\text{Btu}}{^\circ\text{F}}$$

No capacitors are required for nodes 1 and 10 since their temperatures are specified by a curve.

### RC Products

Although not required by the computer, the user should be familiar with the computation of RC products. To illustrate the procedure, the RC products are computed for this example.

Nodes 2 and 9:

$$(RC)_2 = (RC)_9 = \frac{C2}{\frac{1}{R1} + \frac{1}{R2}} = \frac{0.0625}{\frac{1}{2500} + \frac{1}{5000}} = 104 \text{ sec}$$

Nodes 3, 7, and 8:

$$(RC)_3 = (RC)_7 = (RC)_8 = \frac{C3}{\frac{1}{R2} + \frac{1}{R3}} = \frac{0.0625}{\frac{1}{5000}} = 313 \text{ sec}$$

The RC products of nodes 4, 5, and 6 depend on the value of the radiation resistors 4 and 5, which are temperature dependent. Assuming all three nodes are at 150°F:

$$R4 = R5 = \frac{1.0}{\sigma K_4 [(T_4 + 460)^2 + (T_5 + 460)^2] [(T_4 + 460) + (T_5 + 460)]}$$

$$= \frac{1}{(0.1713 \times 10^{-8})(2.71 \times 10^{-5})(4)(610)^3} = 23700 \frac{\text{sec } ^\circ\text{F}}{\text{Btu}}$$

Nodes 4 and 6:

$$(RC)_4 = (RC)_6 = \frac{C4}{\frac{1}{R3} + \frac{1}{R4}} = \frac{0.0313}{\frac{1}{5000} + \frac{1}{23700}} = 129 \text{ sec}$$

Node 5:

$$(RC)_5 = \frac{C5}{\frac{1}{R4} + \frac{1}{R5}} = \frac{4.04}{\frac{1}{23700} + \frac{1}{23700}} = 47900 \text{ sec}$$

Initially, nodes 2 and 9 have the lowest RC products, but if the temperatures of nodes 4, 5, or 6 become quite large, resistors 4 and 5 decrease and it is possible that later in the problem  $(RC)_{\min}$  would appear at either node 4 or 6. If several nodes all have the same RC product, the one with the lowest designation number is used to determine the computing interval. In this example, however, the initial  $(RC)_{\min}$  is greater than the specified 100-sec printing interval and therefore

$$\Delta\theta = (0.25)(100) = 25 \text{ sec}$$

Later in the problem, if  $(RC)_{\min}$  becomes less than 100 sec, the computing interval will be  $0.25 (RC)_{\min}$ .

### Curves

Two curves are required, namely the variation of  $T(1)$  and  $T(10)$  with time. These temperature histories are assumed to be known and are input as curves 1 and 10, respectively. These curves are shown in Figure 6-2.

### Time Block

The following times are assumed:

Print interval = 100 sec

Final time = 2300 sec

Initial time = 0 sec

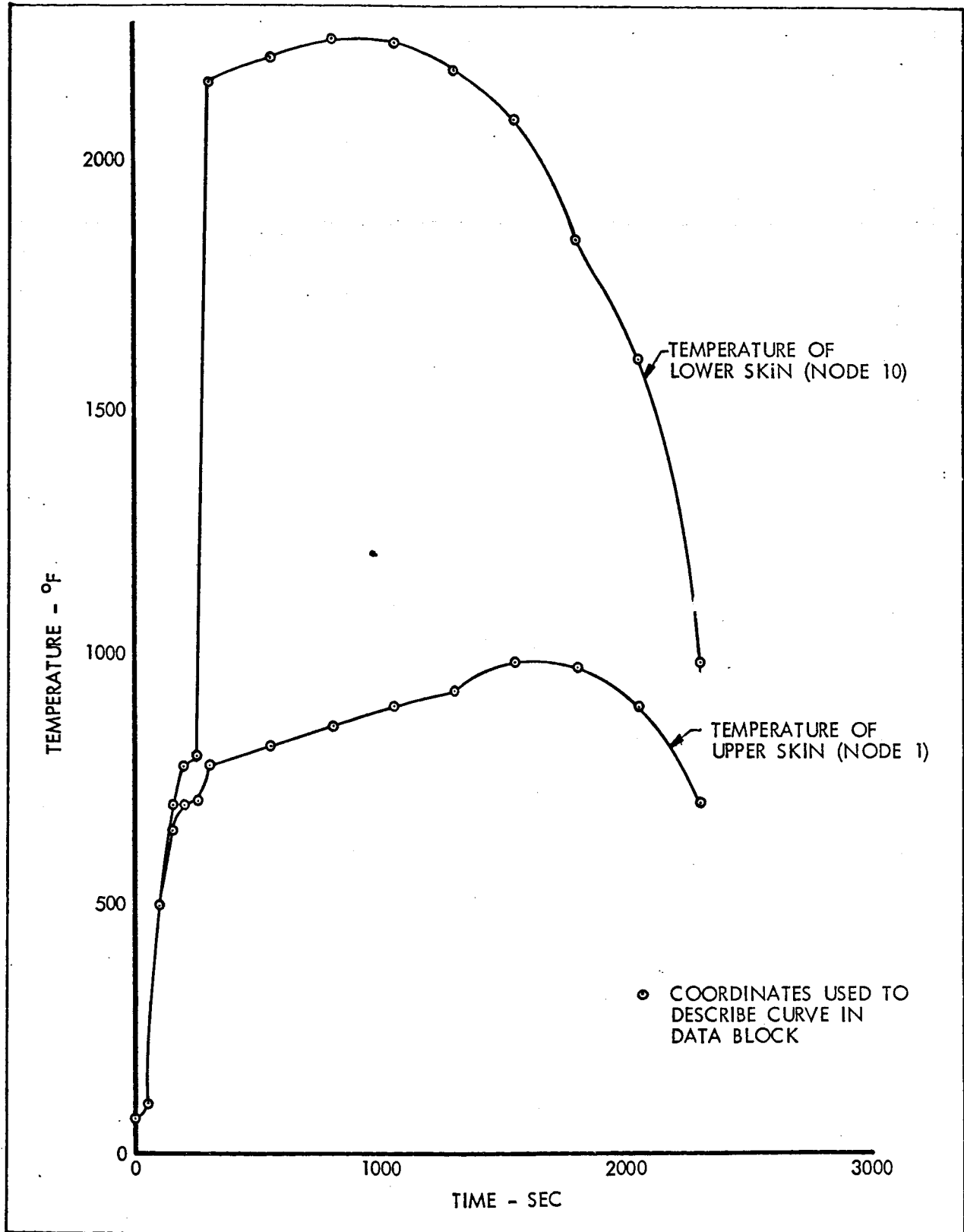


Figure 6-2. Temperature History of Upper and Lower Surfaces

FUNCT Subroutine

The five constants required for the EQUIVALENCE declaration are as follows:

$$\begin{aligned} j &= 1 + \text{greatest temperature designation number} = 1 + 10 = 11 \\ k &= j + \text{greatest temperature designation number} = 11 + 10 = 21 \\ m &= k + \text{greatest resistor designation number} = 21 + 9 = 30 \\ n &= m + \text{greatest capacitor designation number} = 30 + 9 = 39 \\ p &= n + \text{greatest capacitor designation number} = 39 + 9 = 48 \end{aligned}$$

The following function callouts are required:

- (a) Variation of T(1) and T(10) with time

$$\begin{aligned} T(1) &= \text{LIN}(M(1), 1) \\ T(10) &= \text{LIN}(M(1), 10) \end{aligned}$$

- (b) Radiation with constant K factor

$$\begin{aligned} R(4) &= \text{RAD}(4, 5, 2.71E-5) \\ R(5) &= \text{RAD}(5, 6, 2.71E-5) \end{aligned}$$

- (c) Heat input to node 5

$$Q(5) = 0.095$$

Two additional instructions  $TN(1) = T(1)$  and  $TN(10) = T(10)$  are necessary only if it is desired to print the temperatures of nodes 1 and 10 in the output. The reason is that, unless otherwise specified, the "new" temperatures of these nodes never change from their initial value of 70°F (since no capacitors are specified and hence no heat balance is performed). Then, at the end of each computing cycle, T(i) is set equal to TN(i) and the temperatures interpolated from curves 1 and 10 are replaced by the value 70°F, which is then printed in the output. Note that the heat balance on the nodes with capacitors is properly executed whether these additional instructions are added or not since the independent variable used in the heat balance is T(i), not TN(i).

PRINT Subroutine

The print format is set up to list the data in six full columns, with the corresponding time appearing by itself to the left of the first

row of output. This is the standard output format described in Section V. The output specification includes all temperatures, radiation resistors 4 and 5, the minimum RC product, and the node at which  $(RC)_{\min}$  appears.

#### Computer Input for Example #1

The input for Example #1 is shown on data input sheets in Table 6-1. In addition to the previous instructions the following remarks are applicable:

1. The order in which nodes, resistors, capacitors, and curves are input is arbitrary.
2. The user's name and phone number should appear on the first temperature card to identify the output.
3. A liberal use of the space available for comments will help identify various information for future reference.

#### Computer Output

The computer output for Example #1 is shown in Table 6-2. The first two pages list the FUNCT subroutine and the PRINT subroutine. The third page lists the initial temperature, resistor, capacitor, data, and time blocks just as they appear on the input sheets (Table 6-1). The number 2266 added to the sequence number during keypunch is the Lockheed-California Company designation number for the Thermal Analyzer Program.

The answers are printed on the fourth and fifth pages of Table 6-2. As an example of how the output is read, the temperatures, etc., existing at 1500 sec are tabulated below.

Current time = 1500 sec

T(1)	=	979.0°F
T(2)	=	844.7°F
T(3)	=	631.8°F
T(4)	=	469.0°F
T(5)	=	117.2°F
T(6)	=	630.1°F
T(7)	=	958.9°F
T(8)	=	1383.4°F

TABLE 6-1  
INPUT FOR EXAMPLE 1 (1 of 3)

GENERAL PURPOSE DATA SHEET										LOCKHEED-CALIFORNIA COMPANY A DIVISION OF LOCKHEED AIRCRAFT CORPORATION		PAGE	OF									
PREPARED	NAME	DATE	TITLE							JOB NO.												
CHECKED					WO	EWA				GROUP												
SEQ.	ID	77	80	1	5	10	15	20	25	30	35	40	45	50	55	60	65	70	72	73	76	
CID																						
DECO1	1																					1000
DECO1	10																					1001
NBK																						1002
DECO1	1																					1999
1	5																					2001
DECO2	2																					2002
DECO2	4																					2003
DECO2	6																					2004
DECO2	8																					2005
NBK																						2999
1	5																					3001
DECO1	2																					3002
DECO4	3																					3003
DECO2	8																					3999
NBK																						4001
1	5																					4002
DECO6																						4003
																						4004
																						4005
DECO6																						4006
1	5																					4007
DECO1																						4008
DEC	-1																					4009
DEC	10																					4010
DECO6																						500.
DECO6																						800.

FORM DX 7924-1





TABLE 6-1  
INPUT FOR EXAMPLE 1 (2 of 3)

GENERAL PURPOSE DATA SHEET										LOCKHEED-CALIFORNIA COMPANY A DIVISION OF LOCKHEED AIRCRAFT CORPORATION										PAGE OF	
PREPARED		NAME		DATE		TITLE						JOB NO.									
CHECKED						WO EWA						GROUP									
SEQ.	ID	77	80	1	5	10	15	20	25	30	35	40	45	50	55	60	65	70	72	73	76
DECO6						300.		2150.		550.		2200.		800.		2240.		4012			
DECO6						1050.		2230.		1300.		2180.		1550.		2080.		4013			
DECO6						1800.		1840.		2050.		1600.		2300.		990.		4014			
DECO1						0.												4015			
DEC						-10												4016			
NBK																		4999			
DECO1						100.												5001			
DECO1						2300.												5002			
DECO1						0.												5003			
NBK																		5999			
0001	#IBFTC																				
0002																					
0003																					
0004																					
0005																					
0006																					
0007																					
0008																					
0009																					
0010																					
0011																					
0012																					
0013																					
0014																					
0015																					



TABLE 6-1  
INPUT FOR EXAMPLE 1 (3 of 3)

GENERAL PURPOSE DATA SHEET				LOCKHEED-CALIFORNIA COMPANY A DIVISION OF LOCKHEED AIRCRAFT CORPORATION		PAGE	OF
PREPARED	NAME	DATE	TITLE	WO	EWA	JOB NO.	GROUP
CHECKED							
77	80	1					
0016	END						
0101	BIBFC PRINT	NODECK, NØREF					
0102	SUBROUTINE PRINT						
0103	COMMON P, M						
0104	DIMENSION P(16000), M(16)	TN(1), T(1), R(1), C(1), Q(1), RC(1)					
0105	EQUIVALENCE (P(1), TN(1)), (P(11), T(11)), (P(21), R(11)), (P(30), C(1))						
0106	1 (P(39), Q(1)), (P(48), RC(1))						
0107	REAL M						
0108	WRITE (6, 10) M(1), T(1), T(2), T(3), T(4), T(5), T(6),						
0109	1 T(7), T(8), T(9), T(10), R(4), R(5),						
0110	2 M(6), M(9)						
0111	10 FORMAT (1H0, 7E18.8 / (19X, 6E18.8))						
0112	RETURN						
0113	END						

FORM DX 7924-1



TABLE 6-2. COMPUTER OUTPUT FOR EXAMPLE 1

EXTERNAL FORMULA NUMBER	SOURCE STATEMENT	INTERNAL FORMULA NUMFR(S)
	02/11/65	
	FUNCT	
	END	
	SUBROUTINE FUNCT	
	COMMON P,M	22660002
	DIMENSION P(16000),M(16),TN(1),T(1),R(1),C(1),Q(1),RC(1)	22660003
	EQUIVALENCE (P(1),TN(1)),(P(11),T(1)),(P(21),R(1)),(P(30),C(1)),	22660004
	I (P(39),Q(1)),(P(48),RC(1))	22660005
	REAL M,LIN	22660006
	T(1)=LIN(M(1),1)	22660007
	T(10)=LIN(M(1),10)	22660008
	R(4)=RAD(4.5,2.71E-5)	22660009
	R(5)=RAD(5.6,2.71E-5)	22660010
	Q(5)=.095	22660011
	TN(1)=T(1)	22660012
	TN(10)=T(10)	22660013
	RETURN	22660014
	END	22660015
		22660016
		.1
		.2
		.3
		.4
		.5
		.6
		.7
		.8
		.9

TABLE 6-2. (CONTINUED)

PRINT EXTERNAL FORMULA NUMBER	SOURCE STATEMENT	INTERNAL FORMULA NUMBER(S)
		02/11/65
		INTERNAL FORMULA NUMBER(S)
SUBROUTINE PRINT		22660102
COMMON P, M		22660103
DIMENSION P(16000), M(16), TN(1), T(1), R(1), C(1), Q(1), RC(1)		22660104
EQUIVALENCE (P(1), TN(1)), (P(11), T(1)), (P(21), R(1)), (P(30), C(1)),		22660105
1 (P(39), Q(1)), (P(48), RC(1))		22660106
REAL M		22660107
WRITE (6,10) M(1), T(1), T(2), T(3), T(4), T(5), T(6),		22660108
1 T(7), T(8), T(9), T(10), R(4), R(5),		22660109
2 M(6), M(9)		22660110
10 FORMAT (1H0, 7E18.8 / (19X, 6E18.8))		22660111
RETURN		22660112
END		22660113

TABLE 6-2. (CONTINUED)

THERMAL ANALYZER		EXAMPLE PROBLEM ONE		NAME, PHONE NO.		DATE			
DEC 1	1	1	2	2500.	3	4	5000.	10002266	
DEC 1	10	2	3	5000.	5	6	0.	10012266	
NBK 0		4	5	0.	7	8	5000.	10022266	
DEC 1	1	6	7	5000.	9	10	2500.	19992266	
DEC 2	2	8	9	5000.				20012266	
DEC 2	4							20022266	
DEC 2	6							20032266	
DEC 2	8							20042266	
NBK 0								20052266	
DEC 1	2	0.0625	4	0.0313	6	0.0313	7	29992266	
DEC 4	3	0.0625	9	0.0625	5	4.04		30012266	
DEC 3	8							30022266	
NBK 0								30032266	
DEC 0	1	TEMPERATURE OF UPPER SURFACE VS TIME							39992266
DEC 0	6	0.	70.	50.	100.	100.	500.	40012266	
DEC 6	6	150.	650.	200.	700.	250.	710.	40022266	
DEC 6	6	300.	780.	550.	820.	800.	860.	40032266	
DEC 6	6	1050.	900.	1300.	930.	1550.	990.	40042266	
DEC 6	6	1800.	980.	2050.	900.	2300.	710.	40052266	
DEC 1	0.							40062266	
DEC 0	-1							40072266	
DEC 0	10	TEMPERATURE OF LOWER SURFACE VS TIME							40082266
DEC 0	6	0.	70.	50.	100.	100.	500.	40092266	
DEC 6	6	150.	700.	200.	770.	250.	800.	40102266	
DEC 6	6	300.	2150.	550.	2200.	800.	2240.	40112266	
DEC 6	6	1050.	2230.	1300.	2180.	1550.	2080.	40122266	
DEC 6	6	1800.	1840.	2050.	1600.	2300.	990.	40132266	
DEC 1	0.							40142266	
DEC 0	-10							40152266	
NBK 0								40162266	
DEC 1	100.	PRINT INTERVAL							49992266
DEC 1	2300.	FINAL TIME							50012266
DEC 1	0.	INITIAL TIME							50022266
NBK 0								50032266	
								59992266	





TABLE 6-2. (CONTINUED)

0.1300000E 04	0.9300000E 03 0.8791711E 03 0.09999999E 03	0.80582423E 03 0.13229030E 04 0.	0.59851721E 03 0.18873320E 04	0.44638080E 03 0.21799999E 04	0.10842127E 03 0.12899929E 05	0.58393256E 03 0.96338193E 04
0.1399999E 04	0.9540000E 03 0.92334776E 03 0.09999999E 03	0.82426919E 03 0.13579357E 04 0.	0.61561422E 03 0.18831363E 04	0.45840325E 03 0.21399999E 04	0.11273802E 03 0.12452172E 05	0.60982078E 03 0.90417093E 04
0.1500000E 04	0.9780000E 03 0.95898052E 03 0.98548014E 02	0.84476697E 03 0.13834853E 04 0.59999999E 01	0.63188629E 03 0.18707935E 04	0.46904038E 03 0.20999999E 04	0.11721960E 03 0.11973185E 05	0.630167C7E 03 0.850255568E 04
0.1600000E 04	0.9880000E 03 0.98677257E 03 0.97171213E 02	0.86272401E 03 0.14004283E 04 0.59999999E 01	0.64769918E 03 0.18477961E 04	0.47901399E 03 0.20320000E 04	0.12184091E 03 0.11630581E 05	0.64589774E 03 0.81892129E 04
0.1699999E 04	0.9840000E 03 0.10027228E 04 0.96069537E 02	0.87081108E 03 0.14064947E 04 0.59999999E 01	0.66133881E 03 0.18015420E 04	0.48824015E 03 0.19360000E 04	0.12657857E 03 0.11315288E 05	0.65775389E 03 0.79487673E 04
0.1800000E 04	0.9800000E 03 0.10202923E 04 0.95216984E 02	0.87445297E 03 0.14008209E 04 0.59999999E 01	0.67177222E 03 0.17438259E 04	0.49600982E 03 0.18400000E 04	0.13140851E 03 0.11042460E 05	0.66609942E 03 0.77686273E 04
0.1900000E 04	0.9480000E 03 0.10259638E 04 0.94604029E 02	0.86732227E 03 0.13852209E 04 0.59999999E 01	0.67864677E 03 0.16797774E 04	0.50202907E 03 0.17439999E 04	0.13630372E 03 0.10816120E 05	0.67109285E 03 0.76421797E 04
0.2000000E 04	0.9160000E 03 0.10248831E 04 0.94214528E 02	0.85182516E 03 0.13615756E 04 0.59999999E 01	0.68050308E 03 0.16115524E 04	0.50578301E 03 0.16480000E 04	0.14123559E 03 0.10644735E 05	0.67298458E 03 0.75631223E 04
0.2099999E 04	0.8620000E 03 0.10178459E 04 0.94025739E 02	0.82781392E 03 0.13308184E 04 0.59999999E 01	0.67755535E 03 0.15248423E 04	0.50694314E 03 0.14780000E 04	0.14617427E 03 0.10533698E 05	0.7211336E 03 0.75251579E 04
0.2200000E 04	0.7860000E 03 0.10047156E 04 0.94019347E 02	0.78578499E 03 0.12847551E 04 0.59999999E 01	0.66791797E 03 0.13827737E 04	0.50523114E 03 0.12340000E 04	0.15109108E 03 0.10486240E 05	0.66872783E 03 0.75238769E 04
0.2300000E 04	0.7100000E 03 0.98326895E 03 0.94229066E 02	0.73511326E 03 0.12188146E 04 0.59999999E 01	0.65068914E 03 0.12148283E 04	0.49975958E 03 0.99000000E 03	0.15599522E 03 0.10521859E 05	0.66234028E 03 0.75660551E 04

$$\begin{aligned}
 T(9) &= 1870.7^{\circ}\text{F} \\
 T(10) &= 2100.0^{\circ}\text{F} \\
 R(4) &= 11973.\text{sec}^{\circ}\text{F}/\text{Btu} \\
 R(5) &= 8502.\text{sec}^{\circ}\text{F}/\text{Btu} \\
 (RC)_{\min} &= 98.5 \text{ sec} \\
 (RC)_{\min} &\text{ occurs at node 6}
 \end{aligned}$$

Prior to 1500 sec  $(RC)_{\min}$  is greater than 100 sec so the computing interval is based on the specified 100-sec print interval. As a result, the program prints 100. for  $(RC)_{\min}$  and 0. for the node number.

EXAMPLE #2 - Temperature response of a satellite equipment bay from launch through the first orbit.

#### Problem Description

The electronic equipment rack of an earth-orbiting satellite is shown in Figure 6-3. A thermal analysis of this bay is to be performed for the time from launch through the first orbit, assuming an adiabatic interface with the rest of the vehicle. The bay consists of two intersecting aluminum webs on which three electronic components are mounted, and an aluminum outer shell. The heat dissipation of two of these components is constant, while that of the third is periodic with time.

Two sets of external heating curves are required: (1) a curve showing the ascent heating up to the time of orbit insertion, and (2) six periodic curves showing the incident orbital radiation. The ascent heating pulse is estimated in this example. The orbital heating curves were obtained from the Orbital Radiation Program (Ref. 4) for an earth-oriented horizontal cylinder in a 115-mile circular orbit. A noon launch at an inclination angle of 32.5 degrees and a zenith angle of 180 degrees at the center of the equipment bay are assumed.

The initial values of surface emissivity and solar absorptivity will be changed in a restart. In addition, certain items will be plotted to demonstrate the plotting routine and a max-min search will be conducted for some of the more important nodes.



The physical geometry and equivalent thermal network are shown in Figure 6-3.

Since component temperatures are of primary interest here, the various capacities are assumed to be concentrated at points corresponding to equipment locations. The capacitance of the flush-mounted equipment is lumped with that of the adjacent web. The bracket-mounted equipment is represented by a separate node connected by a conduction resistor to the adjacent web. At the juncture between the two webs, a string of zero capacitance nodes (designated by  $\otimes$  and often referred to as "dummy" nodes) are used to effect a connection between webs. Perfect thermal contact at the web juncture, and at the web-shell intersection is assumed in this example. Also, the placement of shell nodes at the web-shell intersection implies that the external heating (or cooling) rates are much greater than heat losses by conduction to the vehicle interior.

The following material properties are assumed:

	<u>Property</u>	<u>Aluminum</u>
k =	thermal conductivity, Btu/hr ft °F	70.
c =	specific heat, Btu/lb°F	.020
$\rho$ =	density, lb/ft <sup>3</sup>	175.

### Conduction Resistors

On the webs

$$R_{14} = R_{17} = R_{24} = R_{27} = \frac{3600 \delta}{kA} = \frac{3600 \left( \frac{9}{12} \right)}{(70) \left( \frac{0.10}{12} \right) \left( \frac{12}{12} \right)} = 4620 \frac{\text{sec}^\circ\text{F}}{\text{Btu}}$$

$$R_{13} = R_{15} = R_{16} = R_{18} = R_{23} = R_{25} = R_{26} = R_{28} = \frac{R_{14}}{2} = 2310 \frac{\text{sec}^\circ\text{F}}{\text{Btu}}$$

$$R_{104} = R_{105} = R_{106} = R_{107} = \frac{3600 \delta}{kA} = \frac{3600 \left( \frac{12}{12} \right)}{(70) \left( \frac{0.10}{12} \right) \left( \frac{9}{12} \right)} = 8240 \frac{\text{sec}^\circ\text{F}}{\text{Btu}}$$

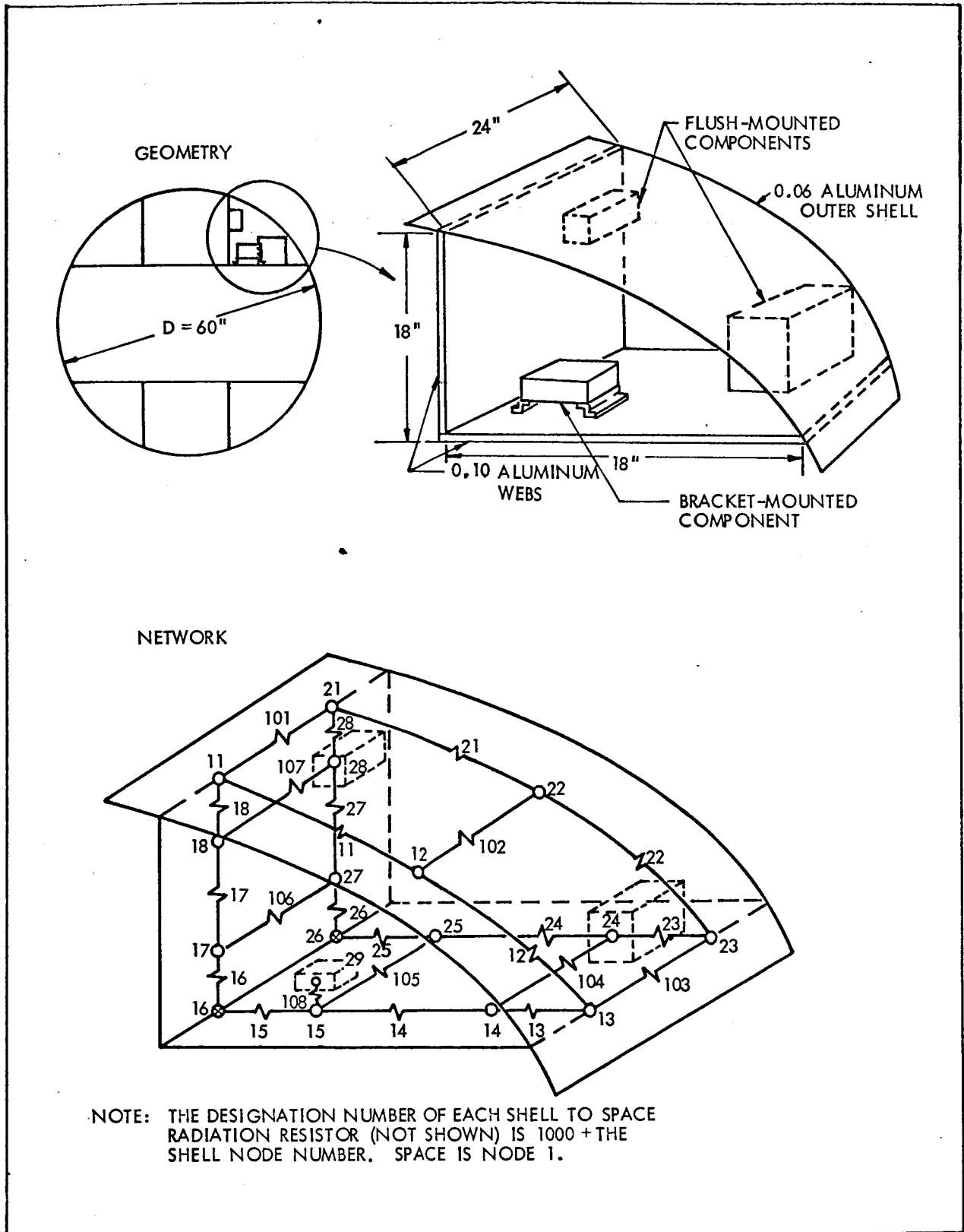


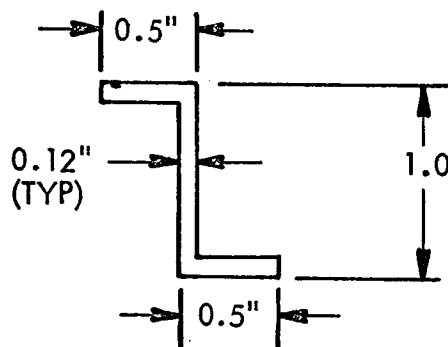
Figure 6-3. Physical Geometry and Corresponding Thermal Network for Example Problem 2

On the shell

$$R_{11} = R_{12} = R_{21} = R_{22} = \frac{3600\delta}{kA} = \frac{3600 \left(\frac{13}{12}\right)}{(70) \left(\frac{0.06}{12}\right) \left(\frac{12}{12}\right)} = 11100 \frac{\text{sec}^\circ\text{F}}{\text{Btu}}$$

$$R_{101} = R_{102} = R_{103} = \frac{3600\delta}{kA} = \frac{3600 \frac{12}{12}}{(70) \left(\frac{0.06}{12}\right) \left(\frac{13}{12}\right)} = 9500 \frac{\text{sec}^\circ\text{F}}{\text{Btu}}$$

To compute  $R_{108}$ , assume that each aluminum Z section is 5 in. in length with a cross-section as follows:



Ignore the resistance through each flange but assume a contact conductance of 500 Btu/hr ft<sup>2</sup> °F between the lower flange and the web, and between the upper flange and the equipment.

$$R_{\text{CONTACT}} = \frac{3600}{kA} = \frac{3600}{(500) \left(\frac{0.5}{12}\right) \left(\frac{5}{12}\right)} = 415 \frac{\text{sec}^\circ\text{F}}{\text{Btu}}$$

The resistance through the web of the Z section is

$$R_{\text{WEB}} = \frac{3600\delta}{kA} = \frac{3600 \left(\frac{1.0}{12}\right)}{70 \left(\frac{0.12}{12}\right) \left(\frac{5}{12}\right)} = 1030 \frac{\text{sec}^\circ\text{F}}{\text{Btu}}$$

The total resistance through one Z section is

$$R = 2R_{\text{CONTACT}} + R_{\text{WEB}} = 2(415) + 1030 = 1860 \frac{\text{sec}^\circ\text{F}}{\text{Btu}}$$

Since there are two of these in parallel

$$R_{108} = \frac{R}{2} = 930 \frac{\text{sec}^\circ\text{F}}{\text{Btu}}$$

### Radiation Resistors

Internal radiation is ignored in this example; however, each shell node must have a radiation resistor to space. In the basic deck assume  $\alpha_s = 0.8$  and  $\epsilon = 0.8$ . In the restart assume  $\alpha_s = 0.4$  and  $\epsilon = 0.7$ .

Basic deck

$$K_{11} = K_{12} = K_{13} = K_{21} = K_{22} = K_{23} = \frac{\epsilon FA}{3600} = \frac{(0.8)(1) \left( \frac{13 \times 12}{144} \right)}{3600} = 2.40 \times 10^{-4}$$

Restart

$$K_{11} = K_{12} = K_{13} = K_{21} = K_{22} = K_{23} = \frac{(0.7)(1) \left( \frac{13 \times 12}{144} \right)}{3600} = 2.10 \times 10^{-4}$$

Since both  $\alpha_s$  and  $\epsilon$  are required in the shell heating functions (see below) these values, as well as the value of the radiation k factor, are stored in Table 103. The appropriate changes are made to Table 103 in the restart.

### Capacitors

For the webs, excluding the capacitance of the electronic components

$$C_{14} = C_{15} = C_{17} = C_{18} = C_{24} = C_{25} = C_{27} = C_{28}$$

$$= \rho c \delta A = (175)(0.2) \left( \frac{0.06 \times 12 \times 9}{1728} \right) = 0.131 \frac{\text{Btu}}{^\circ\text{F}}$$

For the shell

$$C_{11} = C_{12} = C_{13} = C_{21} = C_{22} = C_{23}$$

$$= \rho c \delta A = (175) (0.2) \left( \frac{0.10 \times 12 \times 13}{1728} \right) = 0.316 \frac{\text{Btu}}{^\circ\text{F}}$$

$$C_{16} = C_{26} = 0.$$

Assume that each of the three electronic components has a capacitance of 1.5 Btu/°F (including the mounting bracket for node 29). Therefore,

$$C_{29} = 1.5 \text{ Btu/}^\circ\text{F}$$

$$C_{24} = 1.5 + 0.131 = 1.63 \text{ Btu/}^\circ\text{F}$$

$$C_{28} = 1.5 + 0.131 = 1.63 \text{ Btu/}^\circ\text{F}$$

#### RC Products

The RC products for web node 15 and shell node 21 are computed to estimate the computing interval for this problem. On the web

$$(RC)_{15} = \frac{C_{15}}{\frac{1}{R_{105}} + \frac{1}{R_{14}} + \frac{1}{R_{15}} + \frac{1}{R_{108}}} = \frac{0.131}{\frac{1}{8240} + \frac{1}{4620} + \frac{1}{2310} + \frac{1}{930}} = 71 \text{ sec}$$

Since the network for node 15 is similar to that of the other web nodes with the addition of the small resistor, R108, it appears that the minimum RC product for the webs occurs at node 15.

Because shell node 21 has a radiation resistor attached to it, its RC product is temperature dependent. If, for example,  $T(21) = 250^\circ\text{F}$ ,

$$\begin{aligned} R(1021) &= \frac{1}{\sigma K_{21}^4 [T(21) + 460.]^3} \\ &= \frac{1}{(0.1713 \times 10^{-8}) (2.4 \times 10^{-4})(4)(710)^3} = 1700 \frac{\text{sec}^\circ\text{F}}{\text{Btu}} \end{aligned}$$

and

$$(RC)_{21} = \frac{C(21)}{\frac{1}{R_{21}} + \frac{1}{R_{101}} + \frac{1}{R_{28}} + \frac{1}{R_{1021}}} = \frac{0.316}{\frac{1}{11100} + \frac{1}{9500} + \frac{1}{2310} + \frac{1}{1700}} = 260 \text{ sec}$$

If  $T(21) = -100^\circ\text{F}$ 

$$R(1021) = \frac{1}{(0.1713 \times 10^{-8})(2.4 \times 10^{-4})(4)(360)^3} = 13000 \frac{\text{sec}^\circ\text{F}}{\text{Btu}}$$

and

$$(RC)_{21} = \frac{0.316}{\frac{1}{11100} + \frac{1}{9500} + \frac{1}{2310} + \frac{1}{13000}} = 448 \text{ sec}$$

It appears, therefore, that the minimum RC product will occur at node 15, and will have a value of about 71 sec. In this example problem  $M(7)$  is set at 0.6, causing a computing interval of about 43 sec. During ascent, however, the specified print interval is less than 43 seconds. Hence, during this time the computing interval is determined by the print interval rather than the (RC) min.

### Curves

The following curves are required:

#### CURVE NO.

#### DESCRIPTION

- |     |  |
|-----|--|
| 101 | Shell ascent heating (including radiation) from liftoff to the time of orbit insertion (700 sec). This one curve will be assumed applicable to all six shell nodes. The value of the heating rate for times equal to or greater than 700 sec is set at zero so this curve has no effect on the orbital analysis. |
| 102 | Print interval $M(4)$ vs time.   |

<u>CURVE NO.</u>	<u>DESCRIPTION</u>
103	A table storing the constants $\alpha_s$ , $\epsilon$ , and the shell radiation K factor.
104	A table listing the nodes (11, 12, 24, 28, and 29) for the maximum-minimum search.
105	A table listing the nodes (11, 12, 24, 28 and 29) and time intervals for the plotting function.
106	A periodic curve showing the heat dissipation of the component at node 24.
111	A periodic curve showing the solar spectrum radiation to shell nodes 11 and 21.
211	A periodic curve showing the infra-red radiation to shell nodes 11 and 21.
112	A periodic curve showing the solar spectrum radiation to shell nodes 12 and 22.
212	A periodic curve showing the infra-red radiation to shell nodes 12 and 22.
113	A periodic curve showing the solar spectrum radiation to shell nodes 13 and 23.
213	A periodic curve showing the infra-red radiation to shell nodes 13 and 23.

#### Time Block

The following times are assumed:

Print interval = 5 sec for  $0. \leq M(1) \leq 150.$ ,  
 10 sec for  $150. < M(1) \leq 200.$ , and  
 300 sec for  $M(1) > 200.$

Final time = 6200 sec

Initial time = 0 sec

Restart Block

The only changes required are the values of  $\alpha_s$ ,  $\epsilon$ , and  $K_{RAD}$  which are stored in Table 3. Note that this table must be changed in its entirety, including the table designation number.

FUNCT Subroutine

The following functions are required:

- (a) An instruction to set  $M(7) = 0.6$ .
- (b) An instruction to change the temperature of the shell radiation sink, node 1, from its value of  $50^\circ\text{F}$  applicable to ascent, to a value of  $-460^\circ\text{F}$ , appropriate for the orbital phase. Only a slight inaccuracy results if this change is made instantaneously at 150 sec since the shell temperature is sufficiently large that the choice of sink temperature is relatively insignificant.
- (c) Callouts for the ascent heating and radiation functions for the external shell. These instructions are combined in a DO loop. Since the radiation K factor is obtained from storage Table 103 a locating statement  $L103 = LOC(103)$  precedes the radiation callout.
- (d) Callouts for the shell orbital heat inputs. A logical IF statement will precede these instructions so that they are skipped if time is less than 700 sec, the assumed orbit insertion time. The instructions will appear as

$$Q(11) = Q(11) + \text{Area} * \text{Absorptivity} * \text{LIN}(M(1), 111) \\ + \text{Area} * \text{Emissivity} * \text{LIN}(M(1), 211) \\ \text{etc.}$$

The term  $Q(11)$  on the right side of the equation is required when more than one heat input is called out for a particular node, and it is desired that they be summed. Otherwise, each successive callout would merely replace the previous value. In this example problem, the term is actually not required since the first callout (item (c) above) specifies that  $Q(11) = 0$ . for  $M(1) > 700$  sec.

- (e) Callouts for the heat dissipation of nodes 24, 28, and 29.
- (f) An instruction to obtain the print interval,  $M(4)$ , from curve 102.
- (g) The plotting function callout for nodes 11, 12, 24, 28, and 29.
- (h) The max-min function callout for nodes 11, 12, 24, 28, and 29.



The five constants required for the EQUIVALENCE statement are:

$$j = 1 + 29 = 30$$

$$k = 30 + 29 = 59$$

$$m = 59 + 1023 = 1082$$

$$n = 1082 + 29 = 1111$$

$$p = 1111 + 29 = 1140$$

### PRINT Subroutine

The output specification for this case consists of all temperatures, and the heat rejection at nodes 24, 28, and 29. Each of these items is given an appropriate label to illustrate the flexibility of the FORTRAN language in writing Format statements. The first line of output lists the current time, computing interval, minimum RC product, and the node at which the (RC) min appears.

Four prints are specified on each page of output. To accomplish this, the variable BLOCK is used to sum the number of prints and when BLOCK = 5., the program is instructed to eject, print the information contained on the CID card, and then set BLOCK = 1. to indicate the first print on that page. The remaining WRITE statements are then executed in a normal manner.

### Computer Input

The input data for Example #2 is shown in Table 6-3. Note that curves 111, 211, 112, 212, 113, and 213 are missing since they are obtained directly as punched cards from the Orbital Radiation Program.

### Computer Output

The computer output for Example #2 is shown in Table 6-4. The first two pages list the FUNCT and PRINT subroutines. The next five pages list the initial temperature, resistor, capacitor, and data blocks exactly as they appear on the input sheets (Table 6-3), with the addition of the heating rate curves obtained from the Orbital Radiation Program.

The answers for the basic case are printed on the next 14 pages. During the time that a 5 or 10 sec print interval is requested, the computing interval is six-tenths of the print interval. When a 300-sec print interval is requested, the computing interval is six-tenths of the  $(RC)_{\min}$  which, as anticipated, appears at node 15 and has a value of about 71 sec. The Maximum-Minimum output appears immediately following the answers. Zeros are printed for the maximum and minimum temperatures of nodes 28 and 29 since the temperatures increase monotonically. Four distinct maximums and minimums were recorded for shell nodes 11 and 12.

The new data required for the restart are printed following the Max-Min output, exactly as it appears on the input sheet. The succeeding pages show the answers for the restart and the Maximum-Minimum output. It appears that the changes in surface radiation properties has little effect on the temperatures of the electronic components.

The machine plotted temperatures are shown in Figures 6-4 and 6-5 for the basic case and restart, respectively. The information on the CID card is automatically printed on the top of each figure. The format used to identify the node numbers and symbols is also standard. The scales are selected by the program according to the overall range of temperatures and time.



TABLE 6-3  
INPUT FOR EXAMPLE 2 (2 of 6)

GENERAL PURPOSE DATA SHEET		LOCKHEED-CALIFORNIA COMPANY A DIVISION OF LOCKHEED AIRCRAFT CORPORATION										PAGE	OF	
PREPARED	NAME	DATE	TITLE										JOB NO.	
CHECKED			NO										GROUP	
ID			70	72	73	76								
DEC04	14	0.131	15	17	18	18	0.131	3003						
DEC03	21	0.316	22	23	23	23	0.316	3004						
DEC04	24	1.63	25	27	28	28	0.131	3005						
DEC03	29	1.5	16	26	0.	0.	0.	3006						
NBK								3999						
DEC	101	SHELL HEATING DURING ASCENT												
DEC06	0.	0.	35	40	40	40	0.	10101						
DEC06	60.	1.4	75	85	85	85	1.4	2						
DEC06	115.	27	130.	.023	700.	700.	.023	3						
DEC05	700.	0.	7000.	0.	0.	0.	0.	4						
DEC	-101	VARIABLE PRINT INTERVAL												
DEC	102	0.	5.	145.	5.	145.	10.	10106						
DEC06	190.	10.	190.	300.	7000.	7000.	300.	10201						
DEC01	0.							2						
DEC	-102	SHELL SOLAR ABSORPTIVITY, EMISSIVITY, AND RAD.K-FACTOR												
DEC	103	.8	2.4E-4					10205						
DEC03								10301						
DEC	-103	NODES FOR MAX-MIN FUNCTION												
DEC	104	24.	28.	29.	11	12.	0.	10302						
DEC06								10303						
DEC	-104	NODES TO BE PLOTTED												
DEC	105	0.	6200.	150.	24.	28.	29.	10401						
DEC06								10402						
DEC03								10403						
								10501						
								10502						
								10503						



TABLE 6-3  
INPUT FOR EXAMPLE 2 (3 of 6)

GENERAL PURPOSE DATA SHEET										LOCKHEED-CALIFORNIA COMPANY		PAGE OF		
PREPARED		NAME		DATE		TITLE				JOB NO.				
CHECKED						WO				EWA				
ID										GROUP				
77	60	1												
DEC	-105													
DEC	106													
PER														
DEC06														
DEC06														
DEC01														
DEC	-106													
NBK														
DEC03														
NBK														
CID														
DEC														
DEC	103													
DEC03														
DEC	-103													
DEC														
NBK														
1	5													



TABLE 6-3  
INPUT FOR EXAMPLE 2 (4 of 6)

GENERAL PURPOSE DATA SHEET				LOCKHEED-CALIFORNIA COMPANY A DIVISION OF LOCKHEED AIRCRAFT CORPORATION		PAGE	OF
PREPARED	NAME	DATE	TITLE	WO	EWA	JOB NO.	GROUP
CHECKED							
27	80	1				70	7273-70
0001	#IBFTC FUNCT	NODECK, NØREF					
0002		SUBROUTINE FUNCT					
0003		COMMON P, M					
0004		DIMENSION P(16000), M(16), TN(1), T(1), R(1), C(1), Q(1), RC(1)					
0005		EQUIVALENCE (P(1), TN(1)), (P(30), T(1)), (P(59), R(1)), (P(1082), C(1)),					
0006		I (P(1111), Q(1)), (P(1140), RC(1))					
0007		REAL M, LIN					
0008		M(7) = 0.6					
0009		IF (M(1).EQ.150.) T(1) = -460.					
0010		L103 = LOC(103)					
0011		DØ 1 I = 1, 3					
0012		Q (I+10) = LIN(M(1), 101)					
0013		Q (I+20) = Q (I+10)					
0014		R (I+1010) = RAD(10+I, 1), P(L103+3)					
0015		R (I+1020) = RAD(20+I, 1), P(L103+3)					
0016		CONTINUE					
0017		IF (M(1).LT.700.) GØ TØ 3					
0018		DØ 2 I = 1, 3					
0019		Q (I+10) = Q (I+10) + 1.08 * P(L103+1) * LIN(M(1), 110+I) + 1.08 * P(L103+2) *					
0020		I LIN(M(1), 210+I)					
0021		Q (I+20) = Q (I+10)					
0022		CONTINUE					
0023		Q (24) = LIN(M(1), 106)					
0024		Q (28) = 0.03					
0025		Q (29) = 0.04					

FORM DX 7824-1



TABLE 6-3  
INPUT FOR EXAMPLE 2 (5 of 6)

GENERAL PURPOSE DATA SHEET		LOCKHEED-CALIFORNIA COMPANY A DIVISION OF LOCKHEED AIRCRAFT CORPORATION		PAGE	OF
PREPARED	NAME	DATE	TITLE	JOB NO.	
CHECKED					
ID			WO	EWA	GROUP
77	80	1			
0026					
0027					
0028					
0029					
0030					
0031					
0101					
0102					
0103					
0104					
0105					
0106					
0107					
0108					
0109					
0110					
0111					
0112					
0113					
0114					
0115					

FORM DX 7924-1



TABLE 6-3  
INPUT FOR EXAMPLE 2 (6 of 6)

GENERAL PURPOSE DATA SHEET				LOCKHEED-CALIFORNIA COMPANY A DIVISION OF LOCKHEED AIRCRAFT CORPORATION		PAGE	OF
PREPARED	NAME	DATE	TITLE	WO	EWA	JOB NO.	GROUP
CHECKED							
77	80	1					
0116		5	WRITE (6, 1103) T(24), T(28), T(29), Q(24), Q(28), Q(29)	70	72	73	76
0117	100		FORMAT (11H//11H, 12A6)				
0118	101		FORMAT (//6H TIME=, F8.0, 8H SECONDS, 5X, 20H COMPUTING INTERVAL=, 1 F8.3, 8H SECONDS, 5X, 8H(RC) MIN=, F8.3, 16H SECONDS AT NODE, F6.0)				
0119							
0120	102		FORMAT (53H TEMPERATURE OF EXTERNAL SHELL NODES				
		1	3X, 53H TEMPERATURE OF INTERNAL WEB NODES				
0121		2	127H NODE				
0122		3	14				
0123		4	8/8H TEMP. , 6F7.0, 7X, 10F7.0)				
0124		5	FORMAT (53H EQUIPMENT TEMPERATURES AND HEATING RATES				
0125	103						
		1	53H NODE				
0126		2	11H TEMP. , 3F10.0/				
0127		3	11H Q(BTU/SEC), 3F10.4)				
0128							
0129			RETURN				
0130			END				





TABLE 6-4

## COMPUTER OUTPUT FOR EXAMPLE 2

FUNCT	EXTERNAL FORMULA NUMBER	SOURCE STATEMENT	INTERNAL FORMULA NUMBER(S)
SUBROUTINE FUNCT			22660002
COMMON P,M			22660003
DIMENSION P(16000),M(16),TN(1),T(1),R(1),C(1),Q(1),RC(1)			22660004
EQUIVALENCE (P(1),TN(1)),(P(30),T(1)),(P(59),R(1)),(P(1082),C(1)),			22660005
1 (P(1111),Q(1)),(P(1140),RC(1))			22660006
REAL M,LIN			22660007
M(7)=7.6			22660008
IF (M(1).EQ.150.) T(1)=-460.			22660009
L103=LQC(103)			22660010
DO 1 I=1,3			22660011
Q(I+10)=LIN(M(1),101)			22660012
Q(I+20)=Q(I+10)			22660013
R(I+100)=RAD(10+I,1,P(L103+3))			22660014
R(I+120)=RAD(20+I,1,P(L103+3))			22660015
1 CONTINUE			22660016
IF (M(1).LT.700.) GO TO 3			22660017
DO 2 I=1,3			22660018
Q(I+10)=Q(I+10)+1.08*P(L103+1)*LIN(M(1),110+I)+1.08*P(L103+2)*			22660019
1 LIN(M(1),210+I)			22660020
Q(I+20)=Q(I+10)			22660021
2 CONTINUE			22660022
3 Q(24)=LIN(M(1),106)			22660023
Q(28)=0.03			22660024
Q(29)=0.04			22660025
M(4)=LIN(M(1),102)			22660026
CALL TPL0T(105)			22660027
CALL MMF(M(2),M(3),104,1)			22660028
TN(1)=T(1)			22660029
RETURN			22660030
END			22660031

TABLE 6-4 (Continued)

PRINT	EXTERNAL FORMULA NUMBER	SOURCE STATEMENT	INTERNAL FORMULA NUMBER(S)
			06/15/65
			22660102
		SUBROUTINE PRINT	22660103
		COMMON P,M,MISCFL(23),CID(12)	22660104
		DIMENSION P(16000),M(16),TN(1),T(1),R(1),C(1),Q(1),RC(1)	22660105
		EQUIVALENCE (P(1),TN(1)),(P(30),T(1)),(P(59),R(1)),(P(1082),C(1))	22660106
		1 (P(1111),Q(1)),(P(1140),RC(1))	22660107
		REAL M	22660108
		IF (M(1),EQ.0.) BLOCK=4.	,1 ,2 ,3
		BLOCK=BLOCK+1.	,4
		IF (BLOCK.EQ.5.) WRITE (6,100) (CID(I),I=1,12)	,5 ,6 ,7 ,8 ,9 ,10
			,11
		IF (BLOCK.EQ.5.) BLOCK=1.	,12 ,13 ,14
		WRITE (6,101) M(1),M(15),M(6),M(9)	,15 ,16 ,17
		WRITE (6,102)	
		1 T(11),T(12),T(13),T(21),T(22),T(23),	
		2 T(14),T(15),T(16),T(17),T(18),T(24),T(25),T(26),T(27),T(28)	
		WRITE (6,103) T(24),T(29),T(29),Q(24),Q(29),Q(29)	,18 ,19 ,20
			,21 ,22 ,23
100		FORMAT (1H1///1H ,12A6)	22660117
101		FORMAT (///6H TIME=,F8.0,9H SECONDS,5X,20H COMPUTING INTERVAL=,	22660118
		1 F8.3,9H SECONDS,5X,9H(RC)MIN=,F8.3,16H SECONDS AT NODE,F6.0)	22660119
102		FORMAT (53H TEMPERATURE OF EXTERNAL SHELL NODES	, 22660120
		1 3X,53H TEMPERATURE OF INTERNAL WEB NODES	/ 22660121
		2 127H NODE 11 12 13 21 22 23	22660122
		3 14 15 16 17 18 24 25 26 27	22660123
		49/9H TEMP. ,6F7.0,7X,10F7.0)	22660124
103		FORMAT (53H EQUIPMENT TEMPERATURES AND HEATING RATES	/ 22660125
		1 53H NODE 24 28 29	/ 22660126
		2 11H TEMP. ,3F10.0/	22660127
		3 11H Q(RTU/SFC),3F10.4)	22660128
		RETURN	22660129 ,24
		END	22660130 ,25



TABLE 6-4 (Continued)

THERMAL ANALYZER EXAMPLE PROBLEM TWO										
DEC										
					NAME, PHONE NUMBER					
					DATE					
DEC 1	1									10002266
DEC 2	11									10012266
NBK 0										10022266
DEC 1	11	11	12	11100.						19992266
DEC 2	12	12	13	11100.	13	13	14	2310.		20012266
DEC 2	14	14	15	4620.	15	15	16	2310.		20022266
DEC 2	16	16	17	2310.	17	17	18	4620.		20032266
DEC 2	18	19	11	2310.	21	21	22	11100.		20042266
DEC 2	22	22	23	11100.	23	23	24	2310.		20052266
DEC 2	24	24	25	4620.	25	25	26	2310.		20062266
DEC 2	26	26	27	2310.	27	27	28	4620.		20072266
DEC 1	28	28	21	2310.						20082266
DEC 1	101	11	21	9500.						20092266
INC 0	1	1	1	0.	2					20102266
DEC 1	104	14	24	8240.						20112266
INC 0	1	1	1	0.	3					20122266
DEC 1	1011	11	1	0.						20132266
INC 0	1	1	0	0.	2					20142266
DEC 1	1021	21	1	0.						20152266
INC 0	1	1	0	0.	2					20162266
DEC 1	108	15	29	930.						20172266
NBK 0										20182266
DEC 1	11	0.316								29992266
INC 0	1	0.	2							30012266
DEC 4	14	0.131	15	0.131	17	0.131	18	0.131		30022266
DEC 3	21	0.316	22	0.316	23	0.316				30032266
DEC 4	24	1.63	25	0.131	27	0.131	28	1.63		30042266
DEC 3	29	1.5	16	0.	26	0.				30052266
NBK 0										30062266
DEC 0	101	SHELL HEATING DURING ASCENT								39992266
DEC 6		0.	0.	35.	0.	40.		.05		101012266
DEC 6		50.	1.4	75.	1.5	85.		1.4		101022266
DEC 6		115.	.27	130.	.023	700.		.023		101032266
DEC 6		700.	0.	7000.	0.	0.				101042266
DEC 0	-101									101052266
DEC 0	102	VARIABLE PRINT INTERVAL								101062266
DEC 6		0.	5.	145.	5.	145.		10.		102012266
DEC 6		190.	10.	190.	300.	7000.		300.		102022266
DEC 1		0.								102032266
DEC 0	-102									102042266
DEC 0	103	SHELL SOLAR ABSORPTIVITY, EMISSIVITY, AND RAD. K-FACTOR								102052266
DEC 3		.8	.8	2.4E-4						103012266
DEC 0	-103									103022266
DEC 0	104	NODES FOR MAX-MIN FUNCTION								103032266
DEC 6		24.	28.	29.	11.	12.		0.		104012266
DEC 0	-104									104022266
DEC 0	105	NODES TO BE PLOTTED								104032266
DEC 6		0.	6200.	150.	24.	28.		29.		105012266
DEC 3		11.	12.	0.						105022266
DEC 0	-105									105032266
DEC 0	106	NODE 24 HEAT DISSIPATION								105042266
PER 0		5200.								106012266
DEC 6		0.	0.	1700.	0.	1700.		.085		106022266
DEC 6		3700.	.085	3700.	0.	5290.		0.		106032266
DEC 1		0.								106042266
DEC 0	-106									106052266
DEC 0	111	SOLAR SPEC								106062266
PER 1	5299.7793									11101
DEC 2	0.	0.0202								11102
										11103

TABLE 6-4 (Continued)

THERMAL ANALYZER EXAMPLE PROBLEM TWO			1C002266
DEC 2	220.4074	0.0139	11104
DEC 2	440.8149	0.0265	11105
DEC 2	661.2223	0.0024	11106
DEC 2	837.5482	0.0270	11107
DEC 2	952.2421	0.	11108
DEC 2	981.6299	0.	11109
DEC 2	1102.0372	0.	11110
DEC 2	1322.4447	0.	11111
DEC 2	1542.8521	0.	11112
DEC 2	1763.2595	0.	11113
DEC 2	1983.6670	0.	11114
DEC 2	2204.0744	0.	11115
DEC 2	2424.4819	0.	11116
DEC 2	2644.8895	0.	11117
DEC 2	2865.2968	0.	11118
DEC 2	3085.7042	0.	11119
DEC 2	3085.7042	0.	11120
DEC 2	3100.3978	0.0267	11121
DEC 2	3306.1117	0.0009	11122
DEC 2	3526.5191	0.0097	11123
DEC 2	3746.9265	0.0186	11124
DEC 2	3967.3338	0.0272	11125
DEC 2	4187.7412	0.0382	11126
DEC 2	4408.1497	0.0305	11127
DEC 2	4628.5561	0.0273	11128
DEC 2	4848.9635	0.0262	11129
DEC 2	5069.3700	0.0246	11130
DEC 2	5289.7783	0.0202	11131
DEC 2	0.	0.	11132
DEC 0	111		11133
DEC 0	211		21101
PER 1	5289.7783		21102
DEC 2	0.	0.0202	21103
DEC 2	220.4074	0.0203	21104
DEC 2	440.8149	0.0205	21105
DEC 2	661.2223	0.0205	21106
DEC 2	837.5482	0.0203	21107
DEC 2	952.2421	0.0203	21108
DEC 2	981.6299	0.0203	21109
DEC 2	1102.0372	0.0196	21110
DEC 2	1322.4447	0.0200	21111
DEC 2	1542.8521	0.0201	21112
DEC 2	1763.2595	0.0201	21113
DEC 2	1983.6670	0.0197	21114
DEC 2	2204.0744	0.0196	21115
DEC 2	2424.4819	0.0191	21116
DEC 2	2644.8895	0.0190	21117
DEC 2	2865.2968	0.0191	21118
DEC 2	3085.7042	0.0197	21119
DEC 2	3085.7042	0.0197	21120
DEC 2	3100.3978	0.0197	21121
DEC 2	3306.1117	0.0197	21122
DEC 2	3526.5191	0.0201	21123
DEC 2	3746.9265	0.0201	21124
DEC 2	3967.3338	0.0197	21125
DEC 2	4187.7412	0.0198	21126
DEC 2	4408.1497	0.0203	21127
DEC 2	4628.5561	0.0205	21128
DEC 2	4848.9635	0.0205	21129

INFRA-RED

TABLE 6-4 (Continued)

THERMAL ANALYZER EXAMPLE PROBLEM TWO			10002266
DEC 2	5069.3709	0.0203	21130
DEC 2	5299.7793	0.0202	21131
DEC 2	0.	0.	21132
DEC 0-	211		21133
DEC 0	112		11201
PER 1	5299.7793		11202
DEC 2	0.	0.0197	11203
DEC 2	220.4074	0.0136	11204
DEC 2	440.8149	0.0064	11205
DEC 2	661.2223	0.0001	11206
DEC 2	937.5492	0.0232	11207
DEC 2	952.2421	0.	11208
DEC 2	891.6299	0.	11209
DEC 2	1102.0372	0.	11210
DEC 2	1322.4447	0.	11211
DEC 2	1542.8521	0.	11212
DEC 2	1763.2595	0.	11213
DEC 2	1983.6670	0.	11214
DEC 2	2204.0744	0.	11215
DEC 2	2424.4819	0.	11216
DEC 2	2544.8895	0.	11217
DEC 2	2865.2958	0.	11218
DEC 2	3085.7042	0.	11219
DEC 2	3085.7042	0.	11220
DEC 2	3100.3978	0.0229	11221
DEC 2	3306.1117	0.0008	11222
DEC 2	3526.5191	0.0094	11223
DEC 2	3746.9265	0.0181	11224
DEC 2	3967.3338	0.0266	11225
DEC 2	4187.7412	0.0310	11226
DEC 2	4408.1487	0.0296	11227
DEC 2	4628.5561	0.0264	11228
DEC 2	4848.9635	0.0256	11229
DEC 2	5069.3709	0.0241	11230
DEC 2	5299.7793	0.0197	11231
DEC 2	0.	0.	11232
DEC 0-	112		11233
DEC 0	212		21201
PER 1	5299.7793		21202
DEC 2	0.	0.0197	21203
DEC 2	220.4074	0.0197	21204
DEC 2	440.8149	0.0200	21205
DEC 2	661.2223	0.0200	21206
DEC 2	937.5492	0.0198	21207
DEC 2	952.2421	0.0198	21208
DEC 2	891.6299	0.0198	21209
DEC 2	1102.0372	0.0192	21210
DEC 2	1322.4447	0.0194	21211
DEC 2	1542.8521	0.0196	21212
DEC 2	1763.2595	0.0196	21213
DEC 2	1983.6670	0.0192	21214
DEC 2	2204.0744	0.0192	21215
DEC 2	2424.4819	0.0187	21216
DEC 2	2544.8895	0.0186	21217
DEC 2	2865.2958	0.0187	21218
DEC 2	3085.7042	0.0192	21219
DEC 2	3085.7042	0.0192	21220
DEC 2	3100.3978	0.0192	21221
DEC 2	3306.1117	0.0193	21222

SOLAR SPEC

INFRA-RED

TABLE 6-4 (Continued)

THERMAL ANALYZER EXAMPLE PROBLEM TWO			10002266
DEC 2	3526.5191	0.0196	21223
DEC 2	3746.9265	0.0195	21224
DEC 2	3967.3338	0.0192	21225
DEC 2	4187.7412	0.0193	21226
DEC 2	4408.1487	0.0198	21227
DEC 2	4628.5561	0.0200	21228
DEC 2	4848.9635	0.0200	21229
DEC 2	5069.3709	0.0197	21230
DEC 2	5289.7783	0.0197	21231
DEC 2	0.	0.	21232
DEC 0-	212		21233
DEC 0	113		11301
PER 1	5289.7783		11302
DEC 2	0.	0.0184	11303
DEC 2	220.4074	0.0127	11304
DEC 2	440.8149	0.0059	11305
DEC 2	661.2223	0.0001	11306
DEC 2	837.5482	0.0182	11307
DEC 2	852.2421	0.	11308
DEC 2	881.6298	0.	11309
DEC 2	1102.0372	0.	11310
DEC 2	1322.4447	0.	11311
DEC 2	1542.8521	0.	11312
DEC 2	1763.2595	0.	11313
DEC 2	1983.6670	0.	11314
DEC 2	2204.0744	0.	11315
DEC 2	2424.4819	0.	11316
DEC 2	2644.8895	0.	11317
DEC 2	2865.2968	0.	11318
DEC 2	3085.7042	0.	11319
DEC 2	3085.7042	0.	11320
DEC 2	3100.3978	0.0180	11321
DEC 2	3306.1117	0.0007	11322
DEC 2	3526.5191	0.0087	11323
DEC 2	3746.9265	0.0168	11324
DEC 2	3967.3338	0.0248	11325
DEC 2	4187.7412	0.0285	11326
DEC 2	4408.1487	0.0275	11327
DEC 2	4628.5561	0.0245	11328
DEC 2	4848.9635	0.0239	11329
DEC 2	5069.3709	0.0226	11330
DEC 2	5289.7783	0.0184	11331
DEC 2	0.	0.	11332
DEC 0-	113		11333
DEC 0	213		21301
PER 1	5289.7783		21302
DEC 2	0.	0.0183	21303
DEC 2	220.4074	0.0184	21304
DEC 2	440.8149	0.0186	21305
DEC 2	661.2223	0.0186	21306
DEC 2	837.5482	0.0185	21307
DEC 2	852.2421	0.0185	21308
DEC 2	881.6298	0.0185	21309
DEC 2	1102.0372	0.0179	21310
DEC 2	1322.4447	0.0181	21311
DEC 2	1542.8521	0.0182	21312
DEC 2	1763.2595	0.0183	21313
DEC 2	1983.6670	0.0179	21314
DEC 2	2204.0744	0.0179	21315

SOLAR SPEC

INFRA-RED

TABLE 6-4 (Continued)

THERMAL ANALYZER EXAMPLE PROBLEM TWO				10002266
DEC 2	2424.4919		0.0174	21316
DEC 2	2644.8895		0.0173	21317
DEC 2	2865.2968		0.0174	21318
DEC 2	3085.7042		0.0179	21319
DEC 2	3085.7042		0.0179	21320
DEC 2	3100.3978		0.0179	21321
DEC 2	3306.1117		0.0179	21322
DEC 2	3526.5191		0.0183	21323
DEC 2	3746.9265		0.0182	21324
DEC 2	3967.3338		0.0178	21325
DEC 2	4187.7412		0.0180	21326
DEC 2	4408.1497		0.0185	21327
DEC 2	4628.5561		0.0186	21328
DEC 2	4848.9635		0.0186	21329
DEC 2	5069.3709		0.0184	21330
DEC 2	5289.7783		0.0183	21331
DEC 2	0.		0.	21332
DEC 0-	213			21333
NBK 0				49992266
DEC 3	5.	6200.	0.	50012266
NBK 0				59992266
			0.	TIME BLOCK

TABLE 6-4. (CONTINUED)

10002266

THERMAL ANALYZER EXAMPLE PROBLEM TWO

TIME= 0. SECONDS COMPUTING INTERVAL= 0. SECONDS (RC)MIN= 5.000 SECONDS AT NODE 0.  
 TEMPERATURE OF EXTERNAL SHELL NODES  
 NODE 11 12 13 21 22 23 24 25 26 27 28  
 TEMP. 70. 70. 70. 70. 70. 70. 70. 70. 70. 70. 70.

EQUIPMENT TEMPERATURES AND HEATING RATES  
 NODE 24 28 29  
 TEMP. 70. 70. 70.  
 Q(BTU/SEC) 0. 0.0300 0.0400

TIME= 5. SECONDS COMPUTING INTERVAL= 3.000 SECONDS (RC)MIN= 5.000 SECONDS AT NODE 0.  
 TEMPERATURE OF EXTERNAL SHELL NODES  
 NODE 11 12 13 21 22 23 24 25 26 27 28  
 TEMP. 70. 70. 70. 70. 70. 70. 70. 70. 70. 70. 70.

EQUIPMENT TEMPERATURES AND HEATING RATES  
 NODE 24 28 29  
 TEMP. 70. 70. 70.  
 Q(BTU/SEC) 0. 0.0300 0.0400

TIME= 10. SECONDS COMPUTING INTERVAL= 3.000 SECONDS (RC)MIN= 5.000 SECONDS AT NODE 0.  
 TEMPERATURE OF EXTERNAL SHELL NODES  
 NODE 11 12 13 21 22 23 24 25 26 27 28  
 TEMP. 70. 70. 70. 70. 70. 70. 70. 70. 70. 70. 70.

EQUIPMENT TEMPERATURES AND HEATING RATES  
 NODE 24 28 29  
 TEMP. 70. 70. 70.  
 Q(BTU/SEC) 0. 0.0300 0.0400

TIME= 15. SECONDS COMPUTING INTERVAL= 3.000 SECONDS (RC)MIN= 5.000 SECONDS AT NODE 0.  
 TEMPERATURE OF EXTERNAL SHELL NODES  
 NODE 11 12 13 21 22 23 24 25 26 27 28  
 TEMP. 70. 70. 70. 70. 70. 70. 70. 70. 70. 70. 70.

EQUIPMENT TEMPERATURES AND HEATING RATES  
 NODE 24 28 29  
 TEMP. 70. 70. 70.  
 Q(BTU/SEC) 0. 0.0300 0.0400



TABLE 6-4. (CONTINUED)

10002266

THERMAL ANALYZER EXAMPLE PROBLEM TWO

TIME=	20. SECONDS	COMPUTING INTERVAL=	3.000 SECONDS	(RC)MIN=	5.000 SECONDS AT NODE	0.
TEMPERATURE OF EXTERNAL SHELL NODES						
NODE	11	12	13	21	22	23
TEMP.	70.	70.	70.	70.	70.	70.
TEMPERATURE OF INTERNAL WEB NODES						
NODE	14	15	16	17	18	24
TEMP.	70.	70.	70.	70.	70.	70.
EQUIPMENT TEMPERATURES AND HEATING RATES						
NODE	24	28	29			
TEMP.	70.	70.	71.			
Q(BTU/SEC)	0.	0.0300	0.0400			
TIME=	25. SECONDS	COMPUTING INTERVAL=	3.000 SECONDS	(RC)MIN=	5.000 SECONDS AT NODE	0.
TEMPERATURE OF EXTERNAL SHELL NODES						
NODE	11	12	13	21	22	23
TEMP.	70.	70.	70.	70.	70.	70.
TEMPERATURE OF INTERNAL WEB NODES						
NODE	14	15	16	17	18	24
TEMP.	70.	70.	70.	70.	70.	70.
EQUIPMENT TEMPERATURES AND HEATING RATES						
NODE	24	28	29			
TEMP.	70.	70.	71.			
Q(BTU/SEC)	0.	0.0300	0.0400			
TIME=	30. SECONDS	COMPUTING INTERVAL=	3.000 SECONDS	(RC)MIN=	5.000 SECONDS AT NODE	0.
TEMPERATURE OF EXTERNAL SHELL NODES						
NODE	11	12	13	21	22	23
TEMP.	70.	70.	70.	70.	70.	70.
TEMPERATURE OF INTERNAL WEB NODES						
NODE	14	15	16	17	18	24
TEMP.	70.	70.	70.	70.	70.	70.
EQUIPMENT TEMPERATURES AND HEATING RATES						
NODE	24	28	29			
TEMP.	70.	71.	71.			
Q(BTU/SEC)	0.	0.0300	0.0400			
TIME=	35. SECONDS	COMPUTING INTERVAL=	3.000 SECONDS	(RC)MIN=	5.000 SECONDS AT NODE	0.
TEMPERATURE OF EXTERNAL SHELL NODES						
NODE	11	12	13	21	22	23
TEMP.	70.	69.	70.	70.	69.	70.
TEMPERATURE OF INTERNAL WEB NODES						
NODE	14	15	16	17	18	24
TEMP.	70.	70.	70.	70.	70.	70.
EQUIPMENT TEMPERATURES AND HEATING RATES						
NODE	24	28	29			
TEMP.	70.	71.	71.			
Q(BTU/SEC)	0.	0.0300	0.0400			

TABLE 6-4. (CONTINUED)

10002266

THERMAL ANALYZER EXAMPLE PROBLEM TWO

TIME= 40. SECONDS COMPUTING INTERVAL= 3.000 SECONDS (RC)MIN= 5.000 SECONDS AT NODE 0.

TEMPERATURE OF EXTERNAL SHELL NODES

NODE	11	12	13	21	22	23	24	25	26	27	28
TEMP.	70.	70.	70.	70.	70.	70.	70.	70.	70.	70.	71.

EQUIPMENT TEMPERATURES AND HEATING RATES

NODE	24	28	29
TEMP.	70.	71.	71.
Q(BTU/SEC)	0.	0.0300	0.0400

TIME= 45. SECONDS COMPUTING INTERVAL= 3.000 SECONDS (RC)MIN= 5.000 SECONDS AT NODE 0.

TEMPERATURE OF EXTERNAL SHELL NODES

NODE	11	12	13	21	22	23	24	25	26	27	28
TEMP.	75.	75.	75.	75.	75.	75.	70.	70.	70.	70.	71.

EQUIPMENT TEMPERATURES AND HEATING RATES

NODE	24	28	29
TEMP.	70.	71.	71.
Q(BTU/SEC)	0.	0.0300	0.0400

TIME= 50. SECONDS COMPUTING INTERVAL= 3.000 SECONDS (RC)MIN= 5.000 SECONDS AT NODE 0.

TEMPERATURE OF EXTERNAL SHELL NODES

NODE	11	12	13	21	22	23	24	25	26	27	28
TEMP.	85.	85.	85.	85.	85.	85.	70.	70.	70.	70.	71.

EQUIPMENT TEMPERATURES AND HEATING RATES

NODE	24	28	29
TEMP.	70.	71.	71.
Q(BTU/SEC)	0.	0.0300	0.0400

TIME= 55. SECONDS COMPUTING INTERVAL= 3.000 SECONDS (RC)MIN= 5.000 SECONDS AT NODE 0.

TEMPERATURE OF EXTERNAL SHELL NODES

NODE	11	12	13	21	22	23	24	25	26	27	28
TEMP.	100.	100.	100.	100.	100.	100.	70.	70.	70.	70.	71.

EQUIPMENT TEMPERATURES AND HEATING RATES

NODE	24	28	29
TEMP.	70.	71.	71.
Q(BTU/SEC)	0.	0.0300	0.0400

TABLE 6-4. (CONTINUED)

10002266

THERMAL ANALYZER EXAMPLE PROBLEM TWO

TIME=	60. SECONDS	COMPUTING INTERVAL=	3.000 SECONDS	(RC)MIN=	5.000 SECONDS AT NODE	0.
TEMPERATURE OF EXTERNAL SHELL NODES						
NODE	11	12	13	21	22	23
TEMP.	121.	121.	121.	121.	121.	121.
TEMPERATURE OF INTERNAL WEB NODES						
NODE	14	15	16	17	18	24
TEMP.	70.	70.	70.	70.	71.	70.
EQUIPMENT TEMPERATURES AND HEATING RATES						
NODE	24	28	29			
TEMP.	70.	71.	72.			
Q(BTU/SEC)	0.	0.0300	0.0400			
TIME=	65. SECONDS	COMPUTING INTERVAL=	3.000 SECONDS	(RC)MIN=	5.000 SECONDS AT NODE	0.
TEMPERATURE OF EXTERNAL SHELL NODES						
NODE	11	12	13	21	22	23
TEMP.	142.	143.	142.	143.	142.	142.
TEMPERATURE OF INTERNAL WEB NODES						
NODE	14	15	16	17	18	24
TEMP.	70.	70.	70.	70.	72.	70.
EQUIPMENT TEMPERATURES AND HEATING RATES						
NODE	24	28	29			
TEMP.	70.	71.	72.			
Q(BTU/SEC)	0.	0.0300	0.0400			
TIME=	70. SECONDS	COMPUTING INTERVAL=	3.000 SECONDS	(RC)MIN=	5.000 SECONDS AT NODE	0.
TEMPERATURE OF EXTERNAL SHELL NODES						
NODE	11	12	13	21	22	23
TEMP.	164.	166.	164.	165.	166.	164.
TEMPERATURE OF INTERNAL WEB NODES						
NODE	14	15	16	17	18	24
TEMP.	73.	70.	70.	70.	73.	70.
EQUIPMENT TEMPERATURES AND HEATING RATES						
NODE	24	28	29			
TEMP.	70.	72.	72.			
Q(BTU/SEC)	0.	0.0300	0.0400			
TIME=	75. SECONDS	COMPUTING INTERVAL=	3.000 SECONDS	(RC)MIN=	5.000 SECONDS AT NODE	0.
TEMPERATURE OF EXTERNAL SHELL NODES						
NODE	11	12	13	21	22	23
TEMP.	147.	149.	187.	187.	189.	187.
TEMPERATURE OF INTERNAL WEB NODES						
NODE	14	15	16	17	18	24
TEMP.	75.	71.	70.	70.	75.	70.
EQUIPMENT TEMPERATURES AND HEATING RATES						
NODE	24	28	29			
TEMP.	70.	72.	72.			
Q(BTU/SEC)	0.	0.0300	0.0400			

TABLE 6-4. (CONTINUED)

10002266

THERMAL ANALYZER EXAMPLE PROBLEM TWO

TIME= 80. SECONDS COMPUTING INTERVAL= 3.000 SECONDS (RCJMIN= 5.000 SECONDS AT NODE 0.  
 TEMPERATURE OF EXTERNAL SHELL NODES  
 NODE 11 12 13 21 22 23 14 15 16 17 18 24 25 26 27 28  
 TEMP. 208. 211. 208. 211. 208. 77. 71. 70. 70. 77. 71. 70. 70. 70. 70. 70. 72.  
 EQUIPMENT TEMPERATURES AND HEATING RATES  
 NODE 24 28 29  
 TEMP. 71. 72. 72.  
 Q(BTU/SEC) 0. 0.0300 0.0400

TIME= 85. SECONDS COMPUTING INTERVAL= 3.000 SECONDS (RCJMIN= 5.000 SECONDS AT NODE 0.  
 TEMPERATURE OF EXTERNAL SHELL NODES  
 NODE 11 12 13 21 22 23 14 15 16 17 18 24 25 26 27 28  
 TEMP. 229. 233. 229. 229. 233. 229. 79. 71. 70. 70. 79. 71. 70. 70. 70. 70. 72.  
 EQUIPMENT TEMPERATURES AND HEATING RATES  
 NODE 24 28 29  
 TEMP. 71. 72. 72.  
 Q(BTU/SEC) 0. 0.0300 0.0400

TIME= 90. SECONDS COMPUTING INTERVAL= 3.000 SECONDS (RCJMIN= 5.000 SECONDS AT NODE 0.  
 TEMPERATURE OF EXTERNAL SHELL NODES  
 NODE 11 12 13 21 22 23 14 15 16 17 18 24 25 26 27 28  
 TEMP. 247. 251. 247. 247. 251. 247. 81. 71. 70. 70. 81. 71. 70. 70. 70. 70. 73.  
 EQUIPMENT TEMPERATURES AND HEATING RATES  
 NODE 24 28 29  
 TEMP. 71. 73. 72.  
 Q(BTU/SEC) 0. 0.0300 0.0400

TIME= 95. SECONDS COMPUTING INTERVAL= 3.000 SECONDS (RCJMIN= 5.000 SECONDS AT NODE 0.  
 TEMPERATURE OF EXTERNAL SHELL NODES  
 NODE 11 12 13 21 22 23 14 15 16 17 18 24 25 26 27 28  
 TEMP. 261. 267. 261. 261. 267. 261. 84. 71. 71. 70. 84. 71. 70. 70. 70. 70. 73.  
 EQUIPMENT TEMPERATURES AND HEATING RATES  
 NODE 24 28 29  
 TEMP. 71. 73. 72.  
 Q(BTU/SEC) 0. 0.0300 0.0400

TABLE 6-4. (CONTINUED)

THERMAL ANALYZER EXAMPLE PROBLEM TWO

10002266

TIME= 100. SECONDS COMPUTING INTERVAL= 3.000 SECONDS (RCIMIN= 5.000 SECONDS AT NODE 0.  
 TEMPERATURE OF EXTERNAL SHELL NODES  
 NODE 11 12 13 21 22 23  
 TEMP. 273. 279. 273. 272. 279. 272.  
 TEMPERATURE OF INTERNAL WEB NODES  
 14 15 16 17 18  
 87. 71. 71. 70. 87.  
 EQUIPMENT TEMPERATURES AND HEATING RATES  
 NODE 24 28 29  
 TEMP. 71. 73. 73.  
 Q(BTU/SEC) 0. 0.0300 0.0400

TIME= 105. SECONDS COMPUTING INTERVAL= 3.000 SECONDS (RCIMIN= 5.000 SECONDS AT NODE 0.  
 TEMPERATURE OF EXTERNAL SHELL NODES  
 NODE 11 12 13 21 22 23  
 TEMP. 281. 289. 281. 281. 289. 280.  
 TEMPERATURE OF INTERNAL WEB NODES  
 14 15 16 17 18  
 89. 71. 71. 71. 90.  
 EQUIPMENT TEMPERATURES AND HEATING RATES  
 NODE 24 28 29  
 TEMP. 72. 74. 73.  
 Q(BTU/SEC) 0. 0.0300 0.0400

TIME= 110. SECONDS COMPUTING INTERVAL= 3.000 SECONDS (RCIMIN= 5.000 SECONDS AT NODE 0.  
 TEMPERATURE OF EXTERNAL SHELL NODES  
 NODE 11 12 13 21 22 23  
 TEMP. 286. 295. 286. 286. 295. 285.  
 TEMPERATURE OF INTERNAL WEB NODES  
 14 15 16 17 18  
 92. 72. 71. 71. 93.  
 EQUIPMENT TEMPERATURES AND HEATING RATES  
 NODE 24 28 29  
 TEMP. 72. 74. 73.  
 Q(BTU/SEC) 0. 0.0300 0.0400

TIME= 115. SECONDS COMPUTING INTERVAL= 3.000 SECONDS (RCIMIN= 5.000 SECONDS AT NODE 0.  
 TEMPERATURE OF EXTERNAL SHELL NODES  
 NODE 11 12 13 21 22 23  
 TEMP. 288. 298. 288. 288. 298. 287.  
 TEMPERATURE OF INTERNAL WEB NODES  
 14 15 16 17 18  
 95. 72. 71. 71. 96.  
 EQUIPMENT TEMPERATURES AND HEATING RATES  
 NODE 24 28 29  
 TEMP. 72. 74. 73.  
 Q(BTU/SEC) 0. 0.0300 0.0400



TABLE 6-4. (CONTINUED)

10002266

THERMAL ANALYZER EXAMPLE PROBLEM TWO

TIME= 120. SECONDS COMPUTING INTERVAL= 3.000 SECONDS (RCJMIN= 5.000 SECONDS AT NODE 0.  
 TEMPERATURE OF EXTERNAL SHELL NODES  
 NODE 11 12 13 21 22 23 14 15 16 17 18 24 25 26 27 28  
 TEMP. 288. 300. 288. 288. 300. 288. 98. 72. 71. 71. 99. 73. 70. 70. 70. 75.  
 EQUIPMENT TEMPERATURES AND HEATING RATES  
 NODE 24 28 29  
 TEMP. 73. 75. 73.  
 Q(BTU/SEC) 0. 0.0300 0.0400

TIME= 125. SECONDS COMPUTING INTERVAL= 3.000 SECONDS (RCJMIN= 5.000 SECONDS AT NODE 0.  
 TEMPERATURE OF EXTERNAL SHELL NODES  
 NODE 11 12 13 21 22 23 14 15 16 17 18 24 25 26 27 28  
 TEMP. 289. 300. 288. 287. 300. 287. 101. 72. 72. 71. 102. 73. 70. 70. 70. 75.  
 EQUIPMENT TEMPERATURES AND HEATING RATES  
 NODE 24 28 29  
 TEMP. 73. 75. 73.  
 Q(BTU/SEC) 0. 0.0300 0.0400

TIME= 130. SECONDS COMPUTING INTERVAL= 3.000 SECONDS (RCJMIN= 5.000 SECONDS AT NODE 0.  
 TEMPERATURE OF EXTERNAL SHELL NODES  
 NODE 11 12 13 21 22 23 14 15 16 17 18 24 25 26 27 28  
 TEMP. 295. 299. 285. 284. 299. 284. 104. 72. 72. 72. 104. 73. 70. 70. 70. 75.  
 EQUIPMENT TEMPERATURES AND HEATING RATES  
 NODE 24 28 29  
 TEMP. 73. 75. 73.  
 Q(BTU/SEC) 0. 0.0300 0.0400

TIME= 135. SECONDS COMPUTING INTERVAL= 3.000 SECONDS (RCJMIN= 5.000 SECONDS AT NODE 0.  
 TEMPERATURE OF EXTERNAL SHELL NODES  
 NODE 11 12 13 21 22 23 14 15 16 17 18 24 25 26 27 28  
 TEMP. 283. 298. 283. 282. 298. 282. 106. 73. 72. 72. 107. 73. 70. 71. 70. 76.  
 EQUIPMENT TEMPERATURES AND HEATING RATES  
 NODE 24 28 29  
 TEMP. 73. 76. 73.  
 Q(BTU/SEC) 0. 0.0300 0.0400



TABLE 6-4. (CONTINUED)

10002266

THERMAL ANALYZER EXAMPLE PROBLEM TWO

TIME=	145. SECONDS	COMPUTING INTERVAL=	3.000 SECONDS	(RC)MIN=	5.000 SECONDS AT NODE	0.
TEMPERATURE OF EXTERNAL SHELL NODES				TEMPERATURE OF INTERNAL WEB NODES		
NODE	11 12 13 21 22 23			14 15 16 17 18	24 25 26 27 28	
TEMP.	281. 296. 281. 279. 296. 279.			109. 72. 72. 110.	74. 70. 71. 70. 76.	
EQUIPMENT TEMPERATURES AND HEATING RATES						
NODE	24 28 29					
TEMP.	74. 76. 74.					
Q(BTU/SEC)	0. 0.0300 0.0400					
TIME=	145. SECONDS	COMPUTING INTERVAL=	3.000 SECONDS	(RC)MIN=	5.000 SECONDS AT NODE	0.
TEMPERATURE OF EXTERNAL SHELL NODES				TEMPERATURE OF INTERNAL WEB NODES		
NODE	11 12 13 21 22 23			14 15 16 17 18	24 25 26 27 28	
TEMP.	279. 295. 276. 277. 295. 277.			111. 73. 73. 112.	74. 70. 71. 71. 77.	
EQUIPMENT TEMPERATURES AND HEATING RATES						
NODE	24 29					
TEMP.	74. 77. 74.					
Q(BTU/SEC)	0. 0.0300 0.0400					
TIME=	150. SECONDS	COMPUTING INTERVAL=	6.000 SECONDS	(RC)MIN=	10.000 SECONDS AT NODE	0.
TEMPERATURE OF EXTERNAL SHELL NODES				TEMPERATURE OF INTERNAL WEB NODES		
NODE	11 12 13 21 22 23			14 15 16 17 18	24 25 26 27 28	
TEMP.	276. 293. 276. 274. 293. 274.			113. 74. 73. 115.	74. 70. 71. 71. 77.	
EQUIPMENT TEMPERATURES AND HEATING RATES						
NODE	24 28 29					
TEMP.	74. 77. 74.					
Q(BTU/SEC)	0. 0.0300 0.0400					
TIME=	160. SECONDS	COMPUTING INTERVAL=	6.000 SECONDS	(RC)MIN=	10.000 SECONDS AT NODE	0.
TEMPERATURE OF EXTERNAL SHELL NODES				TEMPERATURE OF INTERNAL WEB NODES		
NODE	11 12 13 21 22 23			14 15 16 17 18	24 25 26 27 28	
TEMP.	271. 290. 271. 269. 290. 268.			118. 74. 73. 119.	75. 71. 71. 71. 76.	
EQUIPMENT TEMPERATURES AND HEATING RATES						
NODE	24 28 29					
TEMP.	75. 78. 74.					
Q(BTU/SEC)	0. 0.0300 0.0400					

TABLE 6-4. (CONTINUED)

10002266

THERMAL ANALYZER EXAMPLE PROBLEM TWO

TIME= 170. SECONDS COMPUTING INTERVAL= 6.000 SECONDS (RCJMIN= 10.000 SECONDS AT NODE 0.  
 TEMPERATURE OF EXTERNAL SHELL NODES  
 NODE 11 12 13 21 22 23 24 25 26 27 28  
 TEMP. 266. 286. 266. 263. 286. 263. 121. 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28  
 EQUIPMENT TEMPERATURES AND HEATING RATES  
 NODE 24 28 29  
 TEMP. 75. 78. 74.  
 Q(BTU/SEC) 0. 0.0300 0.0400

TIME= 180. SECONDS COMPUTING INTERVAL= 6.000 SECONDS (RCJMIN= 10.000 SECONDS AT NODE 0.  
 TEMPERATURE OF EXTERNAL SHELL NODES  
 NODE 11 12 13 21 22 23 24 25 26 27 28  
 TEMP. 261. 283. 261. 258. 283. 258. 125. 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28  
 EQUIPMENT TEMPERATURES AND HEATING RATES  
 NODE 24 28 29  
 TEMP. 76. 79. 75.  
 Q(BTU/SEC) 0. 0.0300 0.0400

TIME= 190. SECONDS COMPUTING INTERVAL= 6.000 SECONDS (RCJMIN= 10.000 SECONDS AT NODE 0.  
 TEMPERATURE OF EXTERNAL SHELL NODES  
 NODE 11 12 13 21 22 23 24 25 26 27 28  
 TEMP. 257. 280. 256. 253. 280. 253. 128. 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28  
 EQUIPMENT TEMPERATURES AND HEATING RATES  
 NODE 24 28 29  
 TEMP. 76. 80. 75.  
 Q(BTU/SEC) 0. 0.0300 0.0400

TIME= 200. SECONDS COMPUTING INTERVAL= 42.579 SECONDS (RCJMIN= 70.965 SECONDS AT NODE 15.  
 TEMPERATURE OF EXTERNAL SHELL NODES  
 NODE 11 12 13 21 22 23 24 25 26 27 28  
 TEMP. 257. 276. 252. 248. 276. 248. 131. 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28  
 EQUIPMENT TEMPERATURES AND HEATING RATES  
 NODE 24 28 29  
 TEMP. 77. 80. 75.  
 Q(BTU/SEC) 0. 0.0300 0.0400





TABLE 6-4. (CONTINUED)

THERMAL ANALYZER EXAMPLE PROBLEM TWO

10002266

TIME= 500. SECONDS COMPUTING INTERVAL= 42.579 SECONDS (RC)MIN= 70.965 SECONDS AT NODE 15.  
 TEMPERATURE OF EXTERNAL SHELL NODES TEMPERATURE OF INTERNAL WEB NODES  
 NODE 11 12 13 21 22 23 14 15 16 17 18 24 25 26 27 28  
 TEMP. 172. 199. 170. 153. 198. 152. 146. 91. 94. 100. 158. 87. 78. 81. 80. 94.  
 EQUIPMENT TEMPERATURES AND HEATING RATES  
 NODE 24 28 29  
 TEMP. 87. 94. 84.  
 Q( BTU/SEC) 0. 0.0300 0.0400

TIME= 800. SECONDS COMPUTING INTERVAL= 42.579 SECONDS (RC)MIN= 70.965 SECONDS AT NODE 15.  
 TEMPERATURE OF EXTERNAL SHELL NODES TEMPERATURE OF INTERNAL WEB NODES  
 NODE 11 12 13 21 22 23 14 15 16 17 18 24 25 26 27 28  
 TEMP. 139. 154. 132. 120. 151. 114. 126. 97. 101. 109. 140. 92. 87. 90. 91. 102.  
 EQUIPMENT TEMPERATURES AND HEATING RATES  
 NODE 24 28 29  
 TEMP. 92. 102. 94.  
 Q( BTU/SEC) 0. 0.0300 0.0400

TIME= 1100. SECONDS COMPUTING INTERVAL= 42.579 SECONDS (RC)MIN= 70.965 SECONDS AT NODE 15.  
 TEMPERATURE OF EXTERNAL SHELL NODES TEMPERATURE OF INTERNAL WEB NODES  
 NODE 11 12 13 21 22 23 14 15 16 17 18 24 25 26 27 28  
 TEMP. 113. 119. 104. 99. 115. 91. 110. 102. 105. 110. 123. 93. 93. 97. 99. 108.  
 EQUIPMENT TEMPERATURES AND HEATING RATES  
 NODE 24 28 29  
 TEMP. 93. 108. 102.  
 Q( BTU/SEC) 0. 0.0300 0.0400

TIME= 1400. SECONDS COMPUTING INTERVAL= 42.579 SECONDS (RC)MIN= 70.965 SECONDS AT NODE 15.  
 TEMPERATURE OF EXTERNAL SHELL NODES TEMPERATURE OF INTERNAL WEB NODES  
 NODE 11 12 13 21 22 23 14 15 16 17 18 24 25 26 27 28  
 TEMP. 94. 93. 85. 87. 90. 78. 98. 106. 106. 107. 108. 93. 97. 101. 103. 112.  
 EQUIPMENT TEMPERATURES AND HEATING RATES  
 NODE 24 28 29  
 TEMP. 93. 112. 110.  
 Q( BTU/SEC) 0. 0.0300 0.0400

TABLE 6-4. (CONTINUED)

10002266

THERMAL ANALYZER EXAMPLE PROBLEM TWO

TIME= 1700. SECONDS COMPUTING INTERVAL= 42.579 SECONDS (RCJMIN= 70.965 SECONDS AT NODE 15.  
 TEMPERATURE OF EXTERNAL SHELL NODES  
 NODE 11 12 13 21 22 23 24 25 26 27 28  
 TEMP. 81. 74. 73. 81. 72. 70. 90. 109. 106. 105. 95. 91. 100. 103. 105. 105. 115.  
 EQUIPMENT TEMPERATURES AND HEATING RATES  
 NODE 24 28 29  
 TEMP. 91. 115. 116.  
 Q(BTU/SEC) 0. 0.0300 0.0400

TIME= 2000. SECONDS COMPUTING INTERVAL= 42.579 SECONDS (RCJMIN= 70.965 SECONDS AT NODE 15.  
 TEMPERATURE OF EXTERNAL SHELL NODES  
 NODE 11 12 13 21 22 23 24 25 26 27 28  
 TEMP. 71. 61. 65. 78. 60. 66. 86. 112. 107. 102. 86. 105. 103. 105. 107. 107. 117.  
 EQUIPMENT TEMPERATURES AND HEATING RATES  
 NODE 24 28 29  
 TEMP. 103. 117. 123.  
 Q(BTU/SEC) 0.0850 0.0300 0.0400

TIME= 2300. SECONDS COMPUTING INTERVAL= 42.579 SECONDS (RCJMIN= 70.965 SECONDS AT NODE 15.  
 TEMPERATURE OF EXTERNAL SHELL NODES  
 NODE 11 12 13 21 22 23 24 25 26 27 28  
 TEMP. 63. 50. 60. 76. 51. 67. 84. 116. 108. 101. 80. 116. 109. 109. 109. 109. 119.  
 EQUIPMENT TEMPERATURES AND HEATING RATES  
 NODE 24 28 29  
 TEMP. 116. 119. 128.  
 Q(BTU/SEC) 0.0850 0.0300 0.0400

TIME= 2600. SECONDS COMPUTING INTERVAL= 42.579 SECONDS (RCJMIN= 70.965 SECONDS AT NODE 15.  
 TEMPERATURE OF EXTERNAL SHELL NODES  
 NODE 11 12 13 21 22 23 24 25 26 27 28  
 TEMP. 57. 42. 57. 74. 44. 70. 85. 120. 110. 100. 75. 126. 114. 112. 111. 111. 120.  
 EQUIPMENT TEMPERATURES AND HEATING RATES  
 NODE 24 28 29  
 TEMP. 126. 120. 134.  
 Q(BTU/SEC) 0.0850 0.0300 0.0400



TABLE 6-4. (CONTINUED)

10002266

THERMAL ANALYZER EXAMPLE PROBLEM TWO

TIME= 2900. SECONDS COMPUTING INTERVAL= 42.579 SECONDS (RC)MIN= 70.965 SECONDS AT NODE 15.  
 TEMPERATURE OF EXTERNAL SHELL NODES  
 NODE 11 12 13 21 22 23 TEMPERATURE OF INTERNAL WEB NODES 14 15 16 17 18 24 25 26 27 28  
 TEMP. 53. 36. 56. 73. 40. 73. 86. 124. 113. 101. 71. 136. 120. 116. 113. 122.  
 EQUIPMENT TEMPERATURES AND HEATING RATES  
 NODE 24 28 29  
 TEMP. 136. 122. 139.  
 Q(RTU/SEC) 0.0850 0.0300 0.0400

TIME= 3200. SECONDS COMPUTING INTERVAL= 42.579 SECONDS (RC)MIN= 70.965 SECONDS AT NODE 15.  
 TEMPERATURE OF EXTERNAL SHELL NODES  
 NODE 11 12 13 21 22 23 TEMPERATURE OF INTERNAL WEB NODES 14 15 16 17 18 24 25 26 27 28  
 TEMP. 57. 38. 60. 79. 43. 82. 89. 128. 115. 101. 70. 145. 125. 120. 116. 123.  
 EQUIPMENT TEMPERATURES AND HEATING RATES  
 NODE 24 28 29  
 TEMP. 145. 123. 143.  
 Q(RTU/SEC) 0.0850 0.0300 0.0400

TIME= 3500. SECONDS COMPUTING INTERVAL= 42.579 SECONDS (RC)MIN= 70.965 SECONDS AT NODE 15.  
 TEMPERATURE OF EXTERNAL SHELL NODES  
 NODE 11 12 13 21 22 23 TEMPERATURE OF INTERNAL WEB NODES 14 15 16 17 18 24 25 26 27 28  
 TEMP. 56. 38. 63. 89. 44. 87. 94. 132. 119. 104. 71. 153. 130. 124. 119. 125.  
 EQUIPMENT TEMPERATURES AND HEATING RATES  
 NODE 24 28 29  
 TEMP. 153. 125. 148.  
 Q(RTU/SEC) 0.0850 0.0300 0.0400

TIME= 3800. SECONDS COMPUTING INTERVAL= 42.579 SECONDS (RC)MIN= 70.965 SECONDS AT NODE 15.  
 TEMPERATURE OF EXTERNAL SHELL NODES  
 NODE 11 12 13 21 22 23 TEMPERATURE OF INTERNAL WEB NODES 14 15 16 17 18 24 25 26 27 28  
 TEMP. 64. 47. 72. 88. 53. 98. 100. 137. 122. 107. 74. 154. 135. 128. 122. 127.  
 EQUIPMENT TEMPERATURES AND HEATING RATES  
 NODE 24 28 29  
 TEMP. 154. 127. 153.  
 Q(RTU/SEC) 0. 0.0300 0.0400

TABLE 6-4. (CONTINUED)

THERMAL ANALYZER EXAMPLE PROBLEM TWO

10002266

TIME= 4100. SECONDS COMPUTING INTERVAL= 42.579 SECONDS (RC)MIN= 70.965 SECONDS AT NODE 15.  
 TEMPERATURE OF EXTERNAL SHELL NODES  
 NODE 11 12 13 21 22 23 14 15 16 17 18 24 25 26 27 28  
 TEMP. 76. 61. 85. 99. 68. 108. 107. 142. 127. 111. 81. 149. 137. 130. 125. 129.

EQUIPMENT TEMPERATURES AND HEATING RATES  
 NODE 24 28 29  
 TEMP. 149. 129. 157.  
 Q(BTU/SEC) 0. 0.0300 0.0400

TIME= 4400. SECONDS COMPUTING INTERVAL= 42.579 SECONDS (RC)MIN= 70.965 SECONDS AT NODE 15.  
 TEMPERATURE OF EXTERNAL SHELL NODES  
 NODE 11 12 13 21 22 23 14 15 16 17 18 24 25 26 27 28  
 TEMP. 87. 75. 95. 108. 82. 114. 114. 146. 131. 116. 91. 145. 137. 132. 128. 132.

EQUIPMENT TEMPERATURES AND HEATING RATES  
 NODE 24 28 29  
 TEMP. 145. 132. 162.  
 Q(BTU/SEC) 0. 0.0300 0.0400

TIME= 4700. SECONDS COMPUTING INTERVAL= 42.579 SECONDS (RC)MIN= 70.965 SECONDS AT NODE 15.  
 TEMPERATURE OF EXTERNAL SHELL NODES  
 NODE 11 12 13 21 22 23 14 15 16 17 18 24 25 26 27 28  
 TEMP. 94. 84. 101. 113. 90. 115. 119. 151. 136. 121. 99. 142. 138. 135. 131. 136.

EQUIPMENT TEMPERATURES AND HEATING RATES  
 NODE 24 28 29  
 TEMP. 142. 136. 167.  
 Q(BTU/SEC) 0. 0.0300 0.0400

TIME= 5000. SECONDS COMPUTING INTERVAL= 42.579 SECONDS (RC)MIN= 70.965 SECONDS AT NODE 15.  
 TEMPERATURE OF EXTERNAL SHELL NODES  
 NODE 11 12 13 21 22 23 14 15 16 17 18 24 25 26 27 28  
 TEMP. 98. 89. 104. 115. 94. 114. 123. 155. 140. 126. 105. 139. 140. 137. 134. 139.

EQUIPMENT TEMPERATURES AND HEATING RATES  
 NODE 24 28 29  
 TEMP. 139. 139. 171.  
 Q(BTU/SEC) 0. 0.0300 0.0400

TABLE 6-4. (CONTINUED)

THERMAL ANALYZER EXAMPLE PROBLEM TWO

10002266

TIME= 5300. SECONDS COMPUTING INTERVAL= 42.579 SECONDS (RCJMIN= 70.965 SECONDS AT NODE 15.  
 TEMPERATURE OF EXTERNAL SHELL NODES TEMPERATURE OF INTERNAL WEB NODES  
 NODE 11 12 13 21 22 23 14 15 16 17 18 24 25 26 27 28  
 TEMP. 99. 90. 104. 115. 94. 112. 124. 159. 144. 131. 108. 137. 141. 140. 137. 143.  
 EQUIPMENT TEMPERATURES AND HEATING RATES  
 NODE 24 28 29  
 TEMP. 137. 143. 176.  
 Q(BTU/SEC) 0. 0.0300 0.0400

TIME= 5600. SECONDS COMPUTING INTERVAL= 42.579 SECONDS (RCJMIN= 70.965 SECONDS AT NODE 15.  
 TEMPERATURE OF EXTERNAL SHELL NODES TEMPERATURE OF INTERNAL WEB NODES  
 NODE 11 12 13 21 22 23 14 15 16 17 18 24 25 26 27 28  
 TEMP. 95. 86. 100. 111. 89. 106. 124. 162. 147. 134. 109. 135. 142. 142. 140. 145.  
 EQUIPMENT TEMPERATURES AND HEATING RATES  
 NODE 24 28 29  
 TEMP. 135. 145. 180.  
 Q(BTU/SEC) 0. 0.0300 0.0400

TIME= 5900. SECONDS COMPUTING INTERVAL= 42.579 SECONDS (RCJMIN= 70.965 SECONDS AT NODE 15.  
 TEMPERATURE OF EXTERNAL SHELL NODES TEMPERATURE OF INTERNAL WEB NODES  
 NODE 11 12 13 21 22 23 14 15 16 17 18 24 25 26 27 28  
 TEMP. 89. 75. 92. 104. 79. 97. 121. 165. 150. 136. 107. 132. 143. 144. 142. 148.  
 EQUIPMENT TEMPERATURES AND HEATING RATES  
 NODE 24 28 29  
 TEMP. 132. 148. 184.  
 Q(BTU/SEC) 0. 0.0300 0.0400

TIME= 6200. SECONDS COMPUTING INTERVAL= 42.579 SECONDS (RCJMIN= 70.965 SECONDS AT NODE 15.  
 TEMPERATURE OF EXTERNAL SHELL NODES TEMPERATURE OF INTERNAL WEB NODES  
 NODE 11 12 13 21 22 23 14 15 16 17 18 24 25 26 27 28  
 TEMP. 85. 69. 87. 103. 73. 93. 118. 168. 151. 136. 104. 130. 144. 145. 144. 149.  
 EQUIPMENT TEMPERATURES AND HEATING RATES  
 NODE 24 28 29  
 TEMP. 130. 149. 188.  
 Q(BTU/SEC) 0. 0.0300 0.0400



TABLE 6-4. (CONTINUED)

RANGE OF MINIMUM-MAXIMUM						
η.	0.6200000E 04					
MODE NO.	MAX T	MIN T	TIME OF MAX	TIME OF MIN		
24	0.92973553E 02 0.15754692E 03	0.69997304E 02 0.91462558E 02	0.11851580E 04 0.36703160E 04	0.4000000E 02 0.16999999E 04		
28	0.	0.	0.	0.		
29	0.	0.	0.	0.		
11	0.28848826E 03 0.56979638E 02 0.99294759E 02 0.88702224E 02	0.69505806E 02 0.51479299E 02 0.55820698E 02 0.86379537E 02	0.12000000E 03 0.32425790E 04 0.52128948E 04 0.61128948E 04	0.34999999E 02 0.30703159E 04 0.34128950E 04 0.59851579E 04		
12	0.30027721E 03 0.38503425E 02 0.90621306E 02 0.72856805E 02	0.69495180E 02 0.33908306E 02 0.37677485E 02 0.71894490E 02	0.12300000E 03 0.32425790E 04 0.52128948E 04 0.61128948E 04	0.34999999E 02 0.30703159E 04 0.33703160E 04 0.60277369E 04		

TABLE 6-4. (CONTINUED)

DEC 0	5	RESTART FOR EXAMPLE PROBLEM TWO	60012266
DEC 0	103	NEW DATA	60022266
DEC 3		CHANGE TABLE 3	60032266
DEC 0	-103	.4	60042266
DEC 0	0	.7	60052266
NRK 0	0	2.1E-4	60062266
		END RESTART	60072266

TABLE 6-4. (CONTINUED)

60012266

RESTART FOR EXAMPLE PROBLEM TWO

TIME= 3. SECONDS COMPUTING INTERVAL= 0. SECONDS (RC)MIN= 5.000 SECONDS AT NODE 0.  
 TEMPERATURE OF EXTERNAL SHELL NODES  
 NODE 11 12 13 21 22 23 24 25 26 27 28  
 TEMP. 70. 70. 70. 70. 70. 70. 70. 70. 70. 70. 70.

EQUIPMENT TEMPERATURES AND HEATING RATES  
 NODE 24 28 29  
 TEMP. 70. 70. 70.  
 Q(BTU/SEC) 0. 0.0300 0.0400

TIME= 5. SECONDS COMPUTING INTERVAL= 3.000 SECONDS (RC)MIN= 5.000 SECONDS AT NODE 0.  
 TEMPERATURE OF EXTERNAL SHELL NODES  
 NODE 11 12 13 21 22 23 24 25 26 27 28  
 TEMP. 70. 70. 70. 70. 70. 70. 70. 70. 70. 70. 70.

EQUIPMENT TEMPERATURES AND HEATING RATES  
 NODE 24 28 29  
 TEMP. 70. 70. 70.  
 Q(BTU/SEC) 0. 0.0300 0.0400

TIME= 10. SECONDS COMPUTING INTERVAL= 3.000 SECONDS (RC)MIN= 5.000 SECONDS AT NODE 0.  
 TEMPERATURE OF EXTERNAL SHELL NODES  
 NODE 11 12 13 21 22 23 24 25 26 27 28  
 TEMP. 70. 70. 70. 70. 70. 70. 70. 70. 70. 70. 70.

EQUIPMENT TEMPERATURES AND HEATING RATES  
 NODE 24 28 29  
 TEMP. 70. 70. 70.  
 Q(BTU/SEC) 0. 0.0300 0.0400

TIME= 15. SECONDS COMPUTING INTERVAL= 3.000 SECONDS (RC)MIN= 5.000 SECONDS AT NODE 0.  
 TEMPERATURE OF EXTERNAL SHELL NODES  
 NODE 11 12 13 21 22 23 24 25 26 27 28  
 TEMP. 70. 70. 70. 70. 70. 70. 70. 70. 70. 70. 70.

EQUIPMENT TEMPERATURES AND HEATING RATES  
 NODE 24 28 29  
 TEMP. 70. 70. 70.  
 Q(BTU/SEC) 0. 0.0300 0.0400



TABLE 6-4. (CONTINUED)

60012266

RESTART FOR EXAMPLE PROBLEM TWO

TIME=	20. SECONDS	COMPUTING INTERVAL=	3.000 SECONDS	(RCJMIN=	5.000 SECONDS AT NODE	0.
TEMPERATURE OF EXTERNAL SHELL NODES				TEMPERATURE OF INTERNAL WEB NODES		
NODE	11 12 13 21	22	23	14 15 16 17 18	24	25
TEMP.	70. 70. 70. 70.	70.	70.	70. 70. 70. 70. 70.	70.	70.
EQUIPMENT TEMPERATURES AND HEATING RATES						
NODE	24 28 29					
TEMP.	70. 70. 71.					
Q(BTU/SEC)	0. 0.0300 0.0400					
TIME=	25. SECONDS	COMPUTING INTERVAL=	3.000 SECONDS	(RCJMIN=	5.000 SECONDS AT NODE	0.
TEMPERATURE OF EXTERNAL SHELL NODES				TEMPERATURE OF INTERNAL WEB NODES		
NODE	11 12 13 21	22	23	14 15 16 17 18	24	25
TEMP.	70. 70. 70. 70.	70.	70.	70. 70. 70. 70. 70.	70.	70.
EQUIPMENT TEMPERATURES AND HEATING RATES						
NODE	24 28 29					
TEMP.	70. 70. 71.					
Q(BTU/SEC)	0. 0.0300 0.0400					
TIME=	30. SECONDS	COMPUTING INTERVAL=	3.000 SECONDS	(RCJMIN=	5.000 SECONDS AT NODE	0.
TEMPERATURE OF EXTERNAL SHELL NODES				TEMPERATURE OF INTERNAL WEB NODES		
NODE	11 12 13 21	22	23	14 15 16 17 18	24	25
TEMP.	70. 70. 70. 70.	70.	70.	70. 70. 70. 70. 70.	70.	70.
EQUIPMENT TEMPERATURES AND HEATING RATES						
NODE	24 28 29					
TEMP.	70. 70. 71.					
Q(BTU/SEC)	0. 0.0300 0.0400					
TIME=	35. SECONDS	COMPUTING INTERVAL=	3.000 SECONDS	(RCJMIN=	5.000 SECONDS AT NODE	0.
TEMPERATURE OF EXTERNAL SHELL NODES				TEMPERATURE OF INTERNAL WEB NODES		
NODE	11 12 13 21	22	23	14 15 16 17 18	24	25
TEMP.	70. 70. 70. 70.	70.	70.	70. 70. 70. 70. 70.	70.	70.
EQUIPMENT TEMPERATURES AND HEATING RATES						
NODE	24 28 29					
TEMP.	70. 70. 71.					
Q(BTU/SEC)	0. 0.0300 0.0400					

TABLE 6-4. (CONTINUED)

RESTART FOR EXAMPLE PROBLEM TWO

60012266

TIME= 40. SECONDS COMPUTING INTERVAL= 3.000 SECONDS (RC)MIN= 5.000 SECONDS AT NODE 0.  
 TEMPERATURE OF EXTERNAL SHELL NODES  
 NODE 11 12 13 21 22 23 24 25 26 27 28  
 TEMP. 70. 70. 70. 70. 70. 70. 70. 70. 70. 70. 70. 71.  
 EQUIPMENT TEMPERATURES AND HEATING RATES  
 NODE 24 28 29  
 TEMP. 70. 71. 71.  
 Q(BTU/SEC) 0. 0.0300 0.0400

TIME= 45. SECONDS COMPUTING INTERVAL= 3.000 SECONDS (RC)MIN= 5.000 SECONDS AT NODE 0.  
 TEMPERATURE OF EXTERNAL SHELL NODES  
 NODE 11 12 13 21 22 23 24 25 26 27 28  
 TEMP. 75. 75. 75. 75. 75. 75. 70. 70. 70. 70. 70. 71.  
 EQUIPMENT TEMPERATURES AND HEATING RATES  
 NODE 24 28 29  
 TEMP. 70. 71. 71.  
 Q(BTU/SEC) 0. 0.0300 0.0400

TIME= 50. SECONDS COMPUTING INTERVAL= 3.000 SECONDS (RC)MIN= 5.000 SECONDS AT NODE 0.  
 TEMPERATURE OF EXTERNAL SHELL NODES  
 NODE 11 12 13 21 22 23 24 25 26 27 28  
 TEMP. 85. 85. 85. 85. 85. 85. 70. 70. 70. 70. 70. 71.  
 EQUIPMENT TEMPERATURES AND HEATING RATES  
 NODE 24 28 29  
 TEMP. 70. 71. 71.  
 Q(BTU/SEC) 0. 0.0300 0.0400

TIME= 55. SECONDS COMPUTING INTERVAL= 3.000 SECONDS (RC)MIN= 5.000 SECONDS AT NODE 0.  
 TEMPERATURE OF EXTERNAL SHELL NODES  
 NODE 11 12 13 21 22 23 24 25 26 27 28  
 TEMP. 100. 100. 100. 100. 100. 100. 70. 70. 70. 70. 70. 71.  
 EQUIPMENT TEMPERATURES AND HEATING RATES  
 NODE 24 28 29  
 TEMP. 70. 71. 71.  
 Q(BTU/SEC) 0. 0.0300 0.0400

TABLE 6-4. (CONTINUED)

RESTART FOR EXAMPLE PROBLEM TWO

60012266

TIME= 60. SECONDS COMPUTING INTERVAL= 3.000 SECONDS (RC)MIN= 5.000 SECONDS AT NODE 0.  
 TEMPERATURE OF EXTERNAL SHELL NODES  
 NODE 11 12 13 21 22 23 TEMPERATURE OF INTERNAL WEB NODES  
 TEMP. 121. 121. 121. 121. 121. 121. 14. 15 16 17 18 24 25 26 27 28  
 EQUIPMENT TEMPERATURES AND HEATING RATES  
 NODE 24 28 29  
 TEMP. 70. 71. 72.  
 Q(RTU/SEC) 0. 0.0300 0.0400

TIME= 65. SECONDS COMPUTING INTERVAL= 3.000 SECONDS (RC)MIN= 5.000 SECONDS AT NODE 0.  
 TEMPERATURE OF EXTERNAL SHELL NODES  
 NODE 11 12 13 21 22 23 TEMPERATURE OF INTERNAL WEB NODES  
 TEMP. 143. 143. 143. 143. 143. 143. 72. 70. 70. 70. 72. 24 25 26 27 28  
 EQUIPMENT TEMPERATURES AND HEATING RATES  
 NODE 24 28 29  
 TEMP. 70. 71. 72.  
 Q(RTU/SEC) 0. 0.0300 0.0400

TIME= 70. SECONDS COMPUTING INTERVAL= 3.000 SECONDS (RC)MIN= 5.000 SECONDS AT NODE 0.  
 TEMPERATURE OF EXTERNAL SHELL NODES  
 NODE 11 12 13 21 22 23 TEMPERATURE OF INTERNAL WEB NODES  
 TEMP. 165. 166. 165. 165. 166. 165. 73. 70. 70. 70. 73. 24 25 26 27 28  
 EQUIPMENT TEMPERATURES AND HEATING RATES  
 NODE 24 28 29  
 TEMP. 70. 72. 72.  
 Q(RTU/SEC) 0. 0.0300 0.0400

TIME= 75. SECONDS COMPUTING INTERVAL= 3.000 SECONDS (RC)MIN= 5.000 SECONDS AT NODE 0.  
 TEMPERATURE OF EXTERNAL SHELL NODES  
 NODE 11 12 13 21 22 23 TEMPERATURE OF INTERNAL WEB NODES  
 TEMP. 187. 189. 187. 187. 189. 187. 75. 71. 70. 70. 75. 24 25 26 27 28  
 EQUIPMENT TEMPERATURES AND HEATING RATES  
 NODE 24 28 29  
 TEMP. 70. 72. 72.  
 Q(RTU/SEC) 0. 0.0300 0.0400

TABLE 6-4. (CONTINUED)

60012266

RESTART FOR EXAMPLE PROBLEM TWO

TIME= 87. SECONDS COMPUTING INTERVAL= 3.000 SECONDS (RC)MIN= 5.000 SECONDS AT NODE 0.  
 TEMPERATURE OF EXTERNAL SHELL NODES  
 NODE 11 12 13 21 22 23 24 25 26 27 28  
 TEMP. 209. 212. 209. 209. 212. 209. 77. 71. 70. 70. 77. 18 17 18 24 25 70. 70. 26 27 70. 72.  
 EQUIPMENT TEMPERATURES AND HEATING RATES  
 NODE 24 28 29  
 TEMP. 71. 72. 72.  
 Q(BTU/SEC) 0. 0.0300 0.0400

TIME= 85. SECONDS COMPUTING INTERVAL= 3.000 SECONDS (RC)MIN= 5.000 SECONDS AT NODE 0.  
 TEMPERATURE OF EXTERNAL SHELL NODES  
 NODE 11 12 13 21 22 23 24 25 26 27 28  
 TEMP. 229. 233. 229. 229. 233. 229. 79. 71. 70. 70. 79. 18 17 18 24 25 70. 70. 26 27 70. 72.  
 EQUIPMENT TEMPERATURES AND HEATING RATES  
 NODE 24 28 29  
 TEMP. 71. 72. 72.  
 Q(BTU/SEC) 0. 0.0300 0.0400

TIME= 90. SECONDS COMPUTING INTERVAL= 3.000 SECONDS (RC)MIN= 5.000 SECONDS AT NODE 0.  
 TEMPERATURE OF EXTERNAL SHELL NODES  
 NODE 11 12 13 21 22 23 24 25 26 27 28  
 TEMP. 247. 252. 247. 247. 252. 247. 81. 71. 70. 70. 81. 18 17 18 24 25 70. 70. 26 27 70. 73.  
 EQUIPMENT TEMPERATURES AND HEATING RATES  
 NODE 24 28 29  
 TEMP. 71. 73. 72.  
 Q(BTU/SEC) 0. 0.0300 0.0400

TIME= 95. SECONDS COMPUTING INTERVAL= 3.000 SECONDS (RC)MIN= 5.000 SECONDS AT NODE 0.  
 TEMPERATURE OF EXTERNAL SHELL NODES  
 NODE 11 12 13 21 22 23 24 25 26 27 28  
 TEMP. 262. 268. 267. 262. 268. 262. 84. 71. 71. 70. 84. 18 17 18 24 25 70. 70. 26 27 70. 73.  
 EQUIPMENT TEMPERATURES AND HEATING RATES  
 NODE 24 28 29  
 TEMP. 71. 73. 72.  
 Q(BTU/SEC) 0. 0.0300 0.0400



TABLE 6-4. (CONTINUED)

60012266

RESTART FOR EXAMPLE PROBLEM TWO

TIME= 100. SECONDS COMPUTING INTERVAL= 3.000 SECONDS (RCIMIN= 5.000 SECONDS AT NODE 0.  
 TEMPERATURE OF EXTERNAL SHELL NODES  
 NODE 11 12 13 21 22 23 14 15 16 17 18 24 25 26 27 28  
 TEMP. 274. 280. 274. 273. 280. 273. 87. 71. 71. 70. 87. 71. 70. 70. 70. 70. 73.  
 EQUIPMENT TEMPERATURES AND HEATING RATES  
 NODE 24 28 29  
 TEMP. 71. 73. 73.  
 Q(BTU/SEC) 0. 0.0300 0.0400

TIME= 105. SECONDS COMPUTING INTERVAL= 3.000 SECONDS (RCIMIN= 5.000 SECONDS AT NODE 0.  
 TEMPERATURE OF EXTERNAL SHELL NODES  
 NODE 11 12 13 21 22 23 14 15 16 17 18 24 25 26 27 28  
 TEMP. 282. 290. 282. 282. 290. 282. 90. 71. 71. 71. 90. 72. 70. 70. 70. 74.  
 EQUIPMENT TEMPERATURES AND HEATING RATES  
 NODE 24 28 29  
 TEMP. 72. 74. 73.  
 Q(BTU/SEC) 0. 0.0300 0.0400

TIME= 110. SECONDS COMPUTING INTERVAL= 3.000 SECONDS (RCIMIN= 5.000 SECONDS AT NODE 0.  
 TEMPERATURE OF EXTERNAL SHELL NODES  
 NODE 11 12 13 21 22 23 14 15 16 17 18 24 25 26 27 28  
 TEMP. 287. 297. 287. 287. 297. 287. 92. 72. 71. 71. 93. 72. 70. 70. 70. 74.  
 EQUIPMENT TEMPERATURES AND HEATING RATES  
 NODE 24 28 29  
 TEMP. 72. 74. 73.  
 Q(BTU/SEC) 0. 0.0300 0.0400

TIME= 115. SECONDS COMPUTING INTERVAL= 3.000 SECONDS (RCIMIN= 5.000 SECONDS AT NODE 0.  
 TEMPERATURE OF EXTERNAL SHELL NODES  
 NODE 11 12 13 21 22 23 14 15 16 17 18 24 25 26 27 28  
 TEMP. 290. 300. 290. 289. 300. 289. 95. 72. 71. 71. 96. 72. 70. 70. 70. 74.  
 EQUIPMENT TEMPERATURES AND HEATING RATES  
 NODE 24 28 29  
 TEMP. 72. 74. 73.  
 Q(BTU/SEC) 0. 0.0300 0.0400

TABLE 6-4. (CONTINUED)

60012266

RESTART FOR EXAMPLE PROBLEM TWO

TIME=	127. SECONDS	COMPUTING INTERVAL=	3.000 SECONDS	(RC)MIN=	5.000 SECONDS AT NODE	0.
TEMPERATURE OF EXTERNAL SHELL NODES						
NODE	11 12 13 21	22 23	24 25	26 27 28		
TEMP.	290. 302. 290. 289.	302. 289.	98. 72. 71. 71.	99. 73. 70. 70.	26 27 28	75.
EQUIPMENT TEMPERATURES AND HEATING RATES						
NODE	24 28 29					
TEMP.	73. 75. 73.					
Q(BTU/SEC)	0. 0.0300 0.0400					
TIME=	125. SECONDS	COMPUTING INTERVAL=	3.000 SECONDS	(RC)MIN=	5.000 SECONDS AT NODE	0.
TEMPERATURE OF EXTERNAL SHELL NODES						
NODE	11 17 13 21	22 23	24 25	26 27 28		
TEMP.	289. 302. 289. 289.	302. 288.	101. 72. 72. 71.	102. 73. 70. 70.	26 27 28	75.
EQUIPMENT TEMPERATURES AND HEATING RATES						
NODE	24 28 29					
TEMP.	73. 75. 73.					
Q(BTU/SEC)	0. 0.0300 0.0400					
TIME=	130. SECONDS	COMPUTING INTERVAL=	3.000 SECONDS	(RC)MIN=	5.000 SECONDS AT NODE	0.
TEMPERATURE OF EXTERNAL SHELL NODES						
NODE	11 12 13 21	22 23	24 25	26 27 28		
TEMP.	287. 301. 287. 286.	301. 286.	104. 72. 72. 72.	105. 73. 70. 70.	26 27 28	75.
EQUIPMENT TEMPERATURES AND HEATING RATES						
NODE	24 28 29					
TEMP.	73. 75. 73.					
Q(BTU/SEC)	0. 0.0300 0.0400					
TIME=	135. SECONDS	COMPUTING INTERVAL=	3.000 SECONDS	(RC)MIN=	5.000 SECONDS AT NODE	0.
TEMPERATURE OF EXTERNAL SHELL NODES						
NODE	11 12 13 21	22 23	24 25	26 27 28		
TEMP.	285. 300. 285. 284.	300. 284.	106. 73. 72. 72.	107. 73. 70. 70.	26 27 28	76.
EQUIPMENT TEMPERATURES AND HEATING RATES						
NODE	24 28 29					
TEMP.	73. 76. 74.					
Q(BTU/SEC)	0. 0.0300 0.0400					

TABLE 6-4. (CONTINUED)

RESTART FOR EXAMPLE PROBLEM TWO

60012266

TIME=	140. SECONDS	COMPUTING INTERVAL=	3.000 SECONDS	(RC)MIN=	5.000 SECONDS AT NODE	0.
TEMPERATURE OF EXTERNAL SHELL NODES						
NODE	11 12 13 21 22 23	TEMPERATURE OF INTERNAL WEB NODES				
TEMP.	283. 299. 283. 282. 299. 281.	14 15 16 17 18	24 25	26 27	28	76.
		109. 73. 72. 72. 110. 74.	70. 70.	71. 70.	71. 76.	
EQUIPMENT TEMPERATURES AND HEATING RATES						
NODE	24 28 29					
TEMP.	74. 76. 74.					
Q(RTU/SEC)	0. 0.0300 0.0400					
TIME=	145. SECONDS	COMPUTING INTERVAL=	3.000 SECONDS	(RC)MIN=	5.000 SECONDS AT NODE	0.
TEMPERATURE OF EXTERNAL SHELL NODES						
NODE	11 12 13 21 22 23	TEMPERATURE OF INTERNAL WEB NODES				
TEMP.	281. 298. 281. 279. 298. 279.	14 15 16 17 18	24 25	26 27	28	77.
		111. 73. 73. 73. 112. 74.	70. 70.	71. 71.	71. 77.	
EQUIPMENT TEMPERATURES AND HEATING RATES						
NODE	24 28 29					
TEMP.	74. 77. 74.					
Q(RTU/SEC)	0. 0.0300 0.0400					
TIME=	150. SECONDS	COMPUTING INTERVAL=	6.000 SECONDS	(RC)MIN=	10.000 SECONDS AT NODE	0.
TEMPERATURE OF EXTERNAL SHELL NODES						
NODE	11 12 13 21 22 23	TEMPERATURE OF INTERNAL WEB NODES				
TEMP.	279. 296. 279. 277. 296. 277.	14 15 16 17 18	24 25	26 27	28	77.
		114. 74. 73. 73. 115. 74.	70. 70.	71. 71.	71. 77.	
EQUIPMENT TEMPERATURES AND HEATING RATES						
NODE	24 28 29					
TEMP.	74. 77. 74.					
Q(RTU/SEC)	0. 0.0300 0.0400					
TIME=	160. SECONDS	COMPUTING INTERVAL=	6.000 SECONDS	(RC)MIN=	10.000 SECONDS AT NODE	0.
TEMPERATURE OF EXTERNAL SHELL NODES						
NODE	11 12 13 21 22 23	TEMPERATURE OF INTERNAL WEB NODES				
TEMP.	274. 293. 274. 272. 293. 271.	14 15 16 17 18	24 25	26 27	28	78.
		118. 74. 73. 74. 119. 75.	71. 71.	71. 71.	71. 78.	
EQUIPMENT TEMPERATURES AND HEATING RATES						
NODE	24 28 29					
TEMP.	75. 78. 76.					
Q(RTU/SEC)	0. 0.0300 0.0400					



TABLE 6-4. (CONTINUED)

60012266

RESTART FOR EXAMPLE PROBLEM TWO

TIME=	170. SECONDS	COMPUTING INTERVAL=	6.000 SECONDS	(RC)MIN=	10.000 SECONDS AT NODE	0.
TEMPERATURE OF EXTERNAL SHELL NODES						
NODE	11 12 13 21	22 23	TEMPERATURE OF INTERNAL WEB NODES			
TEMP.	269. 290. 269. 266.	290. 266.	14 15 16 17 18	74. 74. 74. 74. 74.	124. 75. 71. 71.	26 27 28
EQUIPMENT TEMPERATURES AND HEATING RATES						
NODE	24 28 29					
TEMP.	75. 78. 74.					
Q(RTU/SEC)	0. 0.0300 0.0400					
TIME=	180. SECONDS	COMPUTING INTERVAL=	6.000 SECONDS	(RC)MIN=	10.000 SECONDS AT NODE	0.
TEMPERATURE OF EXTERNAL SHELL NODES						
NODE	11 12 13 21	22 23	TEMPERATURE OF INTERNAL WEB NODES			
TEMP.	265. 287. 265. 262.	287. 261.	14 15 16 17 18	76. 75. 75. 75. 75.	128. 76. 71. 71.	26 27 28
EQUIPMENT TEMPERATURES AND HEATING RATES						
NODE	24 28 29					
TEMP.	76. 79. 75.					
Q(RTU/SEC)	0. 0.0300 0.0400					
TIME=	190. SECONDS	COMPUTING INTERVAL=	6.000 SECONDS	(RC)MIN=	10.000 SECONDS AT NODE	0.
TEMPERATURE OF EXTERNAL SHELL NODES						
NODE	11 12 13 21	22 23	TEMPERATURE OF INTERNAL WEB NODES			
TEMP.	261. 284. 261. 257.	284. 256.	14 15 16 17 18	76. 75. 76. 76. 76.	131. 77. 71. 71.	26 27 28
EQUIPMENT TEMPERATURES AND HEATING RATES						
NODE	24 28 29					
TEMP.	77. 80. 75.					
Q(RTU/SEC)	0. 0.0300 0.0400					
TIME=	200. SECONDS	COMPUTING INTERVAL=	42.579 SECONDS	(RC)MIN=	70.965 SECONDS AT NODE	15.
TEMPERATURE OF EXTERNAL SHELL NODES						
NODE	11 12 13 21	22 23	TEMPERATURE OF INTERNAL WEB NODES			
TEMP.	257. 281. 256. 252.	281. 252.	14 15 16 17 18	77. 76. 77. 77. 77.	135. 77. 71. 71.	26 27 28
EQUIPMENT TEMPERATURES AND HEATING RATES						
NODE	24 28 29					
TEMP.	77. 80. 75.					
Q(RTU/SEC)	0. 0.0300 0.0400					



TABLE 6-4. (CONTINUED)

RESTART FOR EXAMPLE PROBLEM TMD

60012266

TIME= 500. SECONDS COMPUTING INTERVAL= 42.579 SECONDS (RC)MIN= 70.965 SECONDS AT NODE 15.  
 TEMPERATURE OF EXTERNAL SHELL NODES  
 NODE 11 12 13 21 22 23 TEMPERATURE OF INTERNAL WEB NODES 24 25 26 27 28  
 TEMP. 192. 212. 179. 162. 210. 160. 150. 94. 91. 101. 163. 88. 79. 81. 81. 95.

EQUIPMENT TEMPERATURES AND HEATING RATES  
 NODE 24 28 29  
 TEMP. 89. 95. 84.  
 Q(RTU/SEC) 0. 0.0300 0.0400

TIME= 800. SECONDS COMPUTING INTERVAL= 42.579 SECONDS (RC)MIN= 70.965 SECONDS AT NODE 15.  
 TEMPERATURE OF EXTERNAL SHELL NODES  
 NODE 11 12 13 21 22 23 TEMPERATURE OF INTERNAL WEB NODES 24 25 26 27 28  
 TEMP. 147. 166. 141. 126. 163. 121. 131. 98. 103. 111. 147. 93. 88. 91. 92. 103.

EQUIPMENT TEMPERATURES AND HEATING RATES  
 NODE 24 28 29  
 TEMP. 93. 103. 94.  
 Q(RTU/SEC) 0. 0.0300 0.0400

TIME= 1100. SECONDS COMPUTING INTERVAL= 42.579 SECONDS (RC)MIN= 70.965 SECONDS AT NODE 15.  
 TEMPERATURE OF EXTERNAL SHELL NODES  
 NODE 11 12 13 21 22 23 TEMPERATURE OF INTERNAL WEB NODES 24 25 26 27 28  
 TEMP. 121. 130. 112. 104. 126. 97. 115. 103. 107. 112. 129. 95. 95. 95. 95. 100.

EQUIPMENT TEMPERATURES AND HEATING RATES  
 NODE 24 28 29  
 TEMP. 95. 109. 102.  
 Q(RTU/SEC) 0. 0.0300 0.0400

TIME= 1400. SECONDS COMPUTING INTERVAL= 42.579 SECONDS (RC)MIN= 70.965 SECONDS AT NODE 15.  
 TEMPERATURE OF EXTERNAL SHELL NODES  
 NODE 11 12 13 21 22 23 TEMPERATURE OF INTERNAL WEB NODES 24 25 26 27 28  
 TEMP. 102. 104. 93. 93. 100. 84. 103. 107. 108. 110. 114. 95. 99. 103. 105. 113.

EQUIPMENT TEMPERATURES AND HEATING RATES  
 NODE 24 28 29  
 TEMP. 95. 113. 110.  
 Q(RTU/SEC) 0. 0.0300 0.0400

TABLE 6-4. (CONTINUED)

60012266

RESTART FOR EXAMPLE PROBLEM TWO

TIME=	1700. SECONDS	COMPUTING INTERVAL=	42.579 SECONDS	(RC)MIN=	70.965 SECONDS AT NODE	15.
TEMPERATURE OF EXTERNAL SHELL NODES						
NODE	11 12 13 21 22	23	24	25	26	27 28
TEMP.	88. 85. 81. 87. 82.	76.	95. 111. 109. 108. 102.	94. 102.	105. 107. 117.	
TEMPERATURE OF INTERNAL WEB NODES						
NODE	14 15 16 17 18	19	20	21	22	23
TEMP.	95. 111. 109. 108. 102.	94.	102.	105.	107. 117.	
EQUIPMENT TEMPERATURES AND HEATING RATES						
NODE	24 28 29					
TEMP.	94. 117. 117.					
Q(HTU/SEC)	0. 0.0300 0.0400					
TIME=	2000. SECONDS	COMPUTING INTERVAL=	42.579 SECONDS	(RC)MIN=	70.965 SECONDS AT NODE	15.
TEMPERATURE OF EXTERNAL SHELL NODES						
NODE	11 12 13 21 22	23	24	25	26	27 28
TEMP.	78. 70. 72. 84. 69.	72.	91. 114. 110. 106. 95.	107. 105.	108. 109. 119.	
TEMPERATURE OF INTERNAL WEB NODES						
NODE	14 15 16 17 18	19	20	21	22	23
TEMP.	91. 114. 110. 106. 95.	107.	105.	108.	109. 119.	
EQUIPMENT TEMPERATURES AND HEATING RATES						
NODE	24 28 29					
TEMP.	107. 119. 124.					
Q(HTU/SEC)	0.0850 0.0300 0.0400					
TIME=	2300. SECONDS	COMPUTING INTERVAL=	42.579 SECONDS	(RC)MIN=	70.965 SECONDS AT NODE	15.
TEMPERATURE OF EXTERNAL SHELL NODES						
NODE	11 12 13 21 22	23	24	25	26	27 28
TEMP.	70. 59. 66. 81. 59.	73.	89. 118. 111. 104. 86.	119. 111.	111. 111. 121.	
TEMPERATURE OF INTERNAL WEB NODES						
NODE	14 15 16 17 18	19	20	21	22	23
TEMP.	89. 118. 111. 104. 86.	119.	111.	111.	111. 121.	
EQUIPMENT TEMPERATURES AND HEATING RATES						
NODE	24 28 29					
TEMP.	119. 121. 129.					
Q(HTU/SEC)	0.0850 0.0300 0.0400					
TIME=	2600. SECONDS	COMPUTING INTERVAL=	42.579 SECONDS	(RC)MIN=	70.965 SECONDS AT NODE	15.
TEMPERATURE OF EXTERNAL SHELL NODES						
NODE	11 12 13 21 22	23	24	25	26	27 28
TEMP.	64. 50. 63. 80. 52.	76.	90. 122. 113. 104. 81.	130. 117.	115. 114. 123.	
TEMPERATURE OF INTERNAL WEB NODES						
NODE	14 15 16 17 18	19	20	21	22	23
TEMP.	90. 122. 113. 104. 81.	130.	117.	115.	114. 123.	
EQUIPMENT TEMPERATURES AND HEATING RATES						
NODE	24 28 29					
TEMP.	130. 123. 135.					
Q(HTU/SEC)	0.0850 0.0300 0.0400					

TABLE 6-4. (CONTINUED)

RESTART FOR EXAMPLE PROBLEM TWO

60012266

TIME= 2900. SECONDS COMPUTING INTERVAL= 42.579 SECONDS (RC)MIN= 70.965 SECONDS AT NODE 15.  
 TEMPERATURE OF EXTERNAL SHELL NODES  
 NODE 11 12 13 21 22 23 24 25 26 27 28  
 TEMP. 60. 44. 62. 79. 47. 79. 91. 126. 116. 104. 77. 139. 122. 119. 116. 125.

EQUIPMENT TEMPERATURES AND HEATING RATES  
 NODE 24 28 29  
 TEMP. 139. 125. 140.  
 Q(BTU/SEC) 0.0850 0.0300 0.0400

TIME= 3200. SECONDS COMPUTING INTERVAL= 42.579 SECONDS (RC)MIN= 70.965 SECONDS AT NODE 15.  
 TEMPERATURE OF EXTERNAL SHELL NODES  
 NODE 11 12 13 21 22 23 24 25 26 27 28  
 TEMP. 60. 43. 64. 82. 47. 86. 94. 131. 118. 105. 75. 148. 128. 123. 119. 126.

EQUIPMENT TEMPERATURES AND HEATING RATES  
 NODE 24 28 29  
 TEMP. 148. 126. 145.  
 Q(BTU/SEC) 0.0850 0.0300 0.0400

TIME= 3500. SECONDS COMPUTING INTERVAL= 42.579 SECONDS (RC)MIN= 70.965 SECONDS AT NODE 15.  
 TEMPERATURE OF EXTERNAL SHELL NODES  
 NODE 11 12 13 21 22 23 24 25 26 27 28  
 TEMP. 59. 41. 66. 82. 47. 90. 97. 135. 122. 107. 75. 157. 133. 127. 122. 128.

EQUIPMENT TEMPERATURES AND HEATING RATES  
 NODE 24 28 29  
 TEMP. 157. 128. 150.  
 Q(BTU/SEC) 0.0850 0.0300 0.0400

TIME= 3800. SECONDS COMPUTING INTERVAL= 42.579 SECONDS (RC)MIN= 70.965 SECONDS AT NODE 15.  
 TEMPERATURE OF EXTERNAL SHELL NODES  
 NODE 11 12 13 21 22 23 24 25 26 27 28  
 TEMP. 62. 44. 71. 86. 50. 98. 102. 139. 125. 110. 76. 158. 138. 131. 125. 130.

EQUIPMENT TEMPERATURES AND HEATING RATES  
 NODE 24 28 29  
 TEMP. 159. 130. 155.  
 Q(BTU/SEC) 0. 0.0300 0.0400

TABLE 6-4. (CONTINUED)

RESTART FOR EXAMPLE PROBLEM TWO

60012266

TIME= 4100. SECONDS COMPUTING INTERVAL= 42.579 SECONDS (RCJMIN= 70.965 SECONDS AT NODE 15.  
 TEMPERATURE OF EXTERNAL SHELL NODES  
 NODE 11 12 13 21 22 23 14 15 16 17 18 24 25 26 27 28  
 TEMP. 68. 51. 79. 92. 58. 103. 106. 143. 129. 113. 80. 152. 139. 135. 128. 132.

EQUIPMENT TEMPERATURES AND HEATING RATES  
 NODE 24 28 29  
 TEMP. 152. 132. 159.  
 Q(BTU/SEC) 0. 0.0300 0.0400

TIME= 4400. SECONDS COMPUTING INTERVAL= 42.579 SECONDS (RCJMIN= 70.965 SECONDS AT NODE 15.  
 TEMPERATURE OF EXTERNAL SHELL NODES  
 NODE 11 12 13 21 22 23 14 15 16 17 18 24 25 26 27 28  
 TEMP. 74. 58. 85. 97. 65. 106. 110. 147. 132. 116. 84. 147. 140. 135. 130. 134.

EQUIPMENT TEMPERATURES AND HEATING RATES  
 NODE 24 28 29  
 TEMP. 147. 134. 164.  
 Q(BTU/SEC) 0. 0.0300 0.0400

TIME= 4700. SECONDS COMPUTING INTERVAL= 42.579 SECONDS (RCJMIN= 70.965 SECONDS AT NODE 15.  
 TEMPERATURE OF EXTERNAL SHELL NODES  
 NODE 11 12 13 21 22 23 14 15 16 17 18 24 25 26 27 28  
 TEMP. 77. 63. 88. 100. 69. 105. 113. 151. 136. 120. 89. 143. 140. 136. 132. 137.

EQUIPMENT TEMPERATURES AND HEATING RATES  
 NODE 24 28 29  
 TEMP. 143. 137. 168.  
 Q(BTU/SEC) 0. 0.0300 0.0400

TIME= 5000. SECONDS COMPUTING INTERVAL= 42.579 SECONDS (RCJMIN= 70.965 SECONDS AT NODE 15.  
 TEMPERATURE OF EXTERNAL SHELL NODES  
 NODE 11 12 13 21 22 23 14 15 16 17 18 24 25 26 27 28  
 TEMP. 80. 66. 90. 102. 72. 104. 115. 155. 139. 123. 92. 139. 140. 138. 134. 139.

EQUIPMENT TEMPERATURES AND HEATING RATES  
 NODE 24 28 29  
 TEMP. 139. 139. 173.  
 Q(BTU/SEC) 0. 0.0300 0.0400

TABLE 6-4. (CONTINUED)

60012266

RESTART FOR EXAMPLE PROBLEM TWO

TIME=	5300. SECONDS	COMPUTING INTERVAL=	42.579 SECONDS	(RC)MIN=	70.965 SECONDS AT NODE	15.
TEMPERATURE OF EXTERNAL SHELL NODES						
NODE	11	12	13	21	22	23
TEMP.	81.	67.	90.	102.	72.	102.
TEMPERATURE OF INTERNAL WEB NODES						
NODE	14	15	16	17	18	24
TEMP.	116.	158.	142.	126.	95.	136.
EQUIPMENT TEMPERATURES AND HEATING RATES						
NODE	24	28	29			
TEMP.	136.	141.	177.			
Q(18TU/SEC)	0.	0.0300	0.0400			
TIME=	5600. SECONDS	COMPUTING INTERVAL=	42.579 SECONDS	(RC)MIN=	70.965 SECONDS AT NODE	15.
TEMPERATURE OF EXTERNAL SHELL NODES						
NODE	11	12	13	21	22	23
TEMP.	80.	65.	88.	101.	70.	98.
TEMPERATURE OF INTERNAL WEB NODES						
NODE	14	15	16	17	18	24
TEMP.	116.	161.	144.	128.	96.	133.
EQUIPMENT TEMPERATURES AND HEATING RATES						
NODE	24	28	29			
TEMP.	133.	143.	181.			
Q(18TU/SEC)	0.	0.0300	0.0400			
TIME=	5900. SECONDS	COMPUTING INTERVAL=	42.579 SECONDS	(RC)MIN=	70.965 SECONDS AT NODE	15.
TEMPERATURE OF EXTERNAL SHELL NODES						
NODE	11	12	13	21	22	23
TEMP.	76.	60.	84.	98.	65.	92.
TEMPERATURE OF INTERNAL WEB NODES						
NODE	14	15	16	17	18	24
TEMP.	115.	164.	146.	130.	95.	130.
EQUIPMENT TEMPERATURES AND HEATING RATES						
NODE	24	28	29			
TEMP.	130.	145.	184.			
Q(18TU/SEC)	0.	0.0300	0.0400			
TIME=	6200. SECONDS	COMPUTING INTERVAL=	42.579 SECONDS	(RC)MIN=	70.965 SECONDS AT NODE	15.
TEMPERATURE OF EXTERNAL SHELL NODES						
NODE	11	12	13	21	22	23
TEMP.	75.	56.	81.	98.	61.	89.
TEMPERATURE OF INTERNAL WEB NODES						
NODE	14	15	16	17	18	24
TEMP.	113.	166.	148.	131.	94.	127.
EQUIPMENT TEMPERATURES AND HEATING RATES						
NODE	24	28	29			
TEMP.	127.	147.	188.			
Q(18TU/SEC)	0.	0.0300	0.0400			

TABLE 6-4. (CONTINUED)

RANGE OF MINIMUM-MAXIMUM		0.6200000E 04			
NODE NO.	MAX T	MIN T	TIME OF MAX	TIME OF MIN	
24	0.94971831E 02 0.16111676E 03	0.69997656E 02 0.93935698E 02	0.12703160E 04 0.36703160E 04	0.40000000E 02 0.16999999E 04	
28	0.	0.	0.	0.	
29	0.	0.	0.	0.	
11	0.29009773E 03 0.60110962E 02 0.80980001E 02 0.76623477E 02	0.69566916E 02 0.58092370E 02 0.58823948E 02 0.75392339E 02	0.12000000E 03 0.31999999E 04 0.52999999E 04 0.61128948E 04	0.34999999E 02 0.30703159E 04 0.34554740E 04 0.59851579E 04	
12	0.30216596E 03 0.42506868E 02 0.66655913E 02 0.58164551E 02	0.69557594E 02 0.41300423E 02 0.40919013E 02 0.57733718E 02	0.12500000E 03 0.31999999E 04 0.52554738E 04 0.61128948E 04	0.34999999E 02 0.30703159E 04 0.34554740E 04 0.60277369E 04	

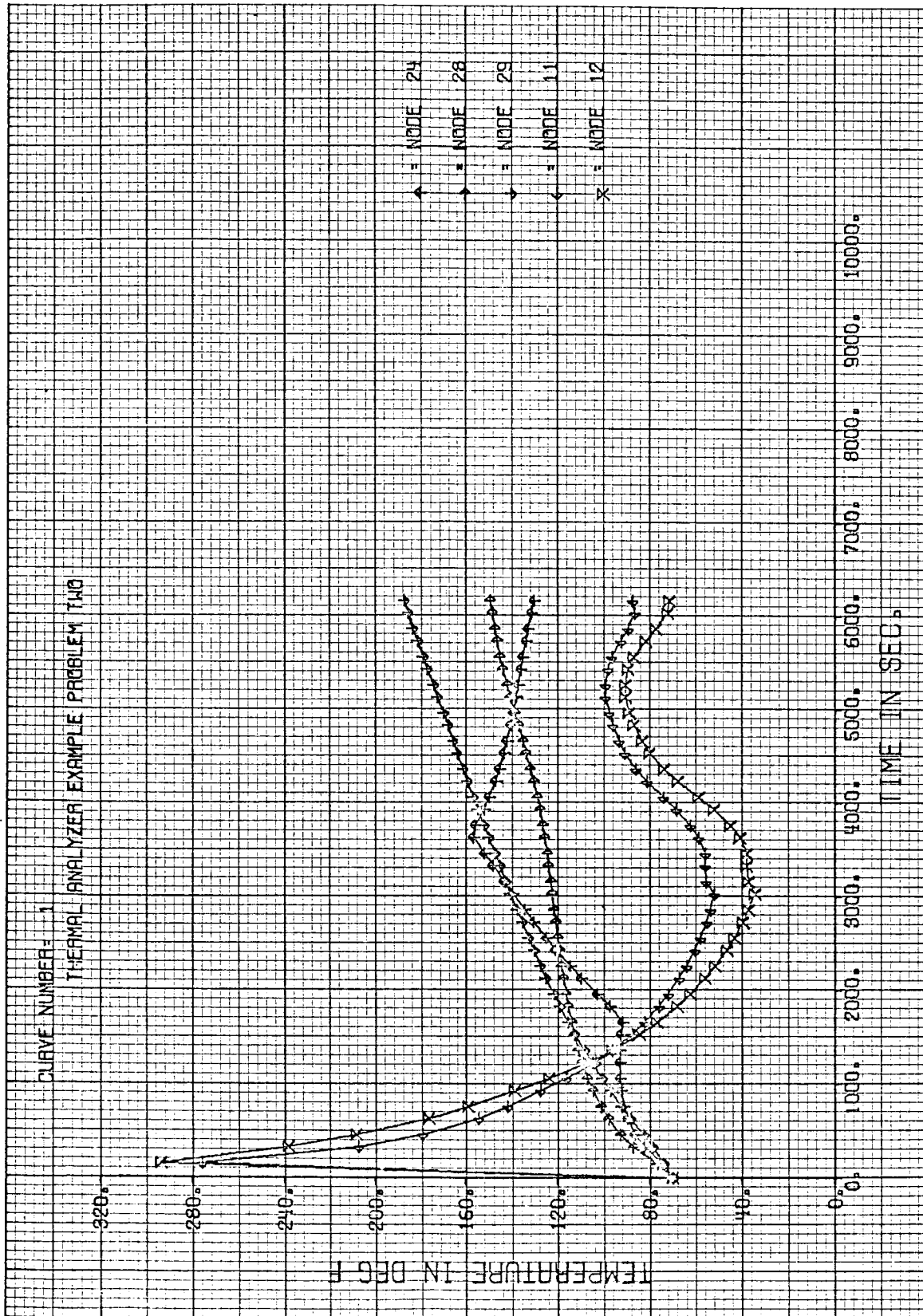


Figure 6-4. Temperature Plots for Example Problem 2

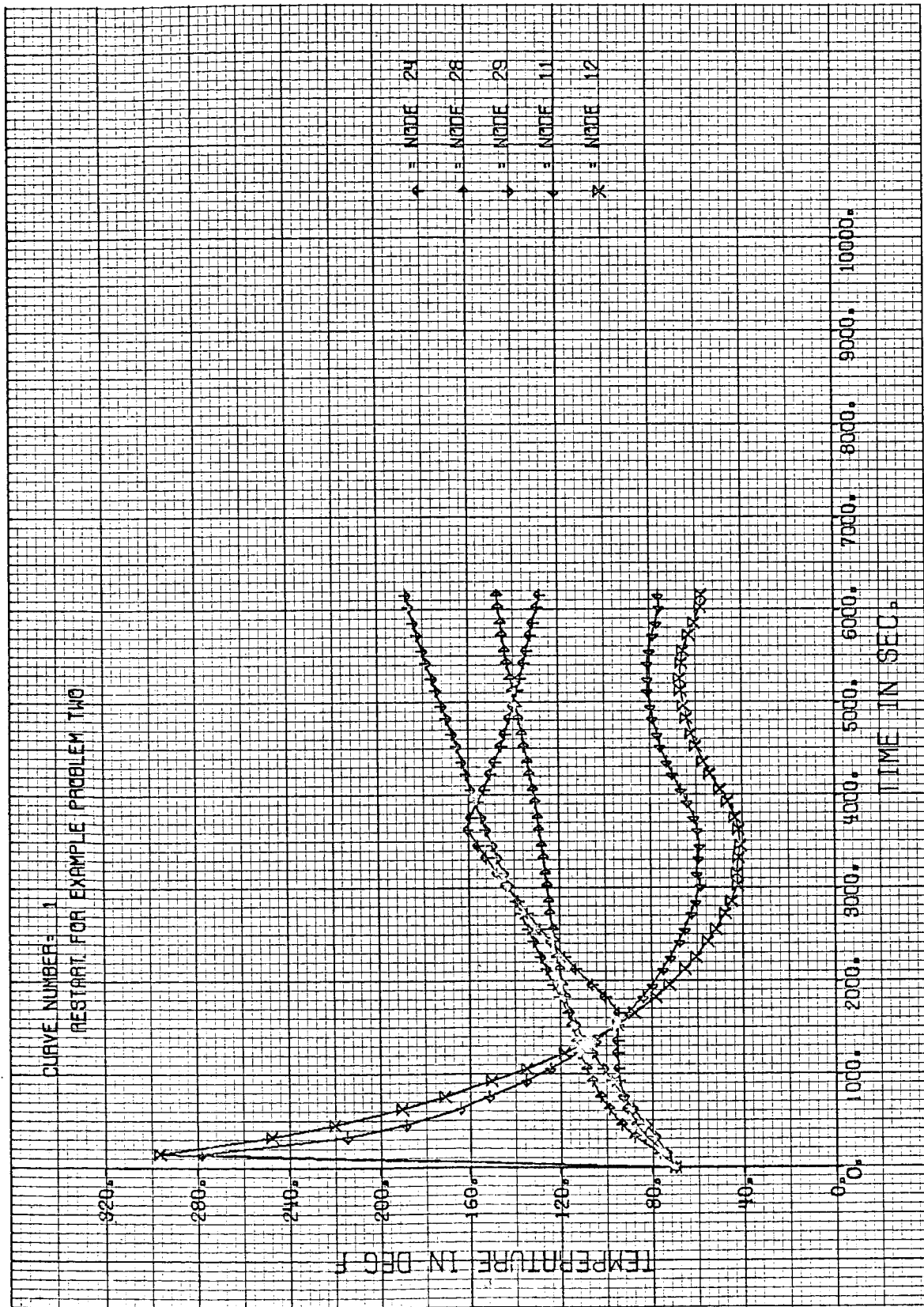


Figure 6-5. Temperature Plots for Example Problem 2 Restart



## VII - GENERAL PROGRAM INFORMATION

INCORRECT DATA INPUTCommon Input Errors

In a program as complex as the Thermal Analyzer, a wide variety of input errors can occur. Some of the most frequent are:

1. Number of items on a DEC card does not match the number in columns 4 & 5. This usually occurs in the data block and results in the input data on that card being truncated after the number of items specified in columns 4 & 5 have been stored. However, if more items are asked for than exist, blank fields are read, and zeros are inserted into the data at that point.
2. Floating-point number is punched without a decimal point. Depending on the position of the number in the field, this results in a multiplication by a power of ten.
3. Integer number is not right-adjusted (blanks left at the right end of the field). This error results in a multiplication by a power of ten. Usually, the integers are either node or resistor numbers, and a multiplication by ten changes the entire circuit, and often results in values being stored into the wrong block or even completely out of the data area.
4. A capacitor is specified for a node whose temperature is to remain constant or is to be supplied by the FUNCT subroutine. Any capacitor listed in the capacitor block causes a heat balance to be performed at that node and the computed temperature to be stored, thus destroying the value assigned. This is true for zero-valued capacitors as well as positive capacitors.

Most other errors in input are checked by the program. However, the foregoing errors are impossible to detect as the current program makes use of the FORTRAN system library routines to read and convert the data.

### Function Subroutine Errors

Certain errors occur fairly often in the FUNCT subroutine. These too, cannot be checked in the current program, because the Function subroutine (FUNCT) is compiled by FORTRAN.

One of the more common Function errors is incorrect use of the "old" and the "new" temperature blocks. For each listed capacitor, a new temperature is computed as a function of the capacitance, time step, its old temperature, the old temperatures of neighboring nodes, and any arbitrary heat inputs. In the special case of a zero-valued capacitor, the new temperature is a function only of the old temperatures of its neighboring nodes, and any other heat inputs. The new temperatures are computed during the heat balance. Then all temperatures in the new temperature block are moved into the old temperature block in preparation for the next cycle. Therefore, any value stored into the "old" temperature block will have an effect on the heat balances performed on itself and on its neighbors, but it will be replaced by its "new" value immediately thereafter. If it has no capacity, its new value will be its initial input value.

Another frequent Function subroutine error is misuse of the time step,  $\Delta \theta$ . Three values of time step are provided in the miscellaneous block, M(I). M(5) contains the actual time step used to arrive at the current time. Usually, at the time of a print, a short time step is needed to arrive at the print time, and M(5), if printed, gives a false indication of step size. Therefore the time step that would have been used, had this not been a print cycle, is provided in M(15). For cycles other than print cycles, M(5) = M(15). For certain purposes it is necessary to know the time step used in the previous heat balance. This quantity is provided in M(14).

Control of the printing interval by means of a value interpolated from a time-dependent curve is often a convenient device, but care must be taken in the choice of points for the curve. If, at time =  $\theta$ , it is desired to change the printing interval from  $PI_1$  to  $PI_2$ , one may use a step-function curve of the form:

$$\theta_{\text{initial}}, PI_1$$

$$\theta - PI_1, PI_1$$

$$\theta - PI_1, PI_2$$

$$\theta_{\text{final}}, PI_2$$

The print interval must be changed at or before one print interval before the time at which the new interval is to take effect, since the next time to print is decided at the time of printing, but before the function subroutine is entered.

### Data Diagnostic

A large amount of data diagnostic is included in the program. The diagnostic routines always print a comment describing the type of error found. For example, if one of the node numbers mentioned in the resistor block is greater than the highest numbered node mentioned in the temperature block, the program sets an error flag to prevent execution of the program, and prints the comment:

```
RESISTOR^NNN^CONNECTS^NODES^MMM,^LLL^GREATER^THAN^MAX^TEMP.NO.=^JJJ
```

If the input data overflows the data storage region, P, the program sets an error flag to prevent execution, and prints the comment:

```
MMM^DATA^STORAGE^EXCEEDED.^TOTAL^OF^NNN
```

In these examples, the three-letter symbols, MMM, NNN, LLL, and JJJ represent numbers that appear in the diagnostic comment.

Unfortunately, not all errors can be checked by the program. For example, if a resistor is connected to a wrong node, but the node number is legitimate, the problem is still a legal problem, but not the problem that the user wants to solve. Note, again, that some errors cause the FORTRAN system to reject the problem, and this situation can mean that not all of the data has been examined. For example, an error in the Function or Print routines that

deletes compilation means that no data has been read at all. A decimal point or other non-integer character in an integer field means that the data inspection is terminated at that point and the data following has not been examined. Any error that is illegal to FORTRAN will delete the problem at that point.

Some diagnostic has also been provided in the execution phase. This includes such errors as a zero or negative time step, attempted division by zero in certain situations, interpolation requested outside the range of the curve, and a number of other more specific errors which are checked in specific subroutines. Undoubtedly there are errors in this phase that could be but have not been diagnosed. But the diagnostic continually becomes more complete as new errors are encountered.

#### Data Debugging Routine

A short version of the compiler portion of the program has been devised, for the purpose of checking data only. This program, described in Appendix E, includes the same diagnostic included in the main program, excepting the error checks during execution.

#### PROGRAM CAPACITY

Currently there are three versions of the program. Two versions have 16000 storage locations available for data, but do not include the fluid storage and pressurization subroutines. One of these, Version A, has been set up to run short problems with minimum overlay. The other, Version B, has been set up with maximum overlay to allow inclusion of the largest possible function and print routines. Version C, including fluid storage and pressurization, has 13000 storage locations available for data.

#### Version A (Short Problems)

There are 16000 storage locations available for data. This is sufficient to handle the largest problem encountered to date, although some of the largest have had to be revised somewhat to fit into the available storage. This allows approximately 1000 temperatures and capacitors, 2500 resistors, and approximately 3500 words in the data blocks. Approximately 2700 storage

locations are available for the FUNCT and PRINT subroutines. This means that the degree of sophistication allowable is strictly limited.

#### Version B (Maximum Problems)

The data storage available is the same as for version A, above. The linkage has been changed to allow maximum storage for the function and print routines. There are about 4800 storage locations available for these routines in version B. Additional space can be gained in two ways:

1. By eliminating unused subroutines, such as linear, parabolic and/or bivariate interpolation, or by eliminating the larger unused routines in dependent links, such as the radiation resistor matrix. Note that the largest routine actually used limits the possible saving.
2. By breaking the Function and/or Print routines into several functions, with unique names for each, and adding \$INCLUDE cards at the proper places.

#### Version C (Pressurization)

13000 storage locations are available for standard input data in version C. (The dimension size is 14000, but approximately 1000 locations are used for special fluid storage and pressurization program storage.) For further details of version C, see Reference 9.

#### MACHINE EXECUTION TIME

The execution time for the Thermal Analyzer is almost wholly dependent on the particular problem to be solved. Small problems (depending also on the particular functions used) will often run faster than 0.01 min/cycle, where a cycle is defined as one full pass through the program. On the other end of the scale, the largest problems to date take about 0.25 min/cycle. The time required is a function of the number and type of arithmetic operations, the size of the network, the subroutine functions used, and the amount of overlaying required. The number of cycles required to complete execution is the time range,  $M(3) - M(2)$ , divided by the computing interval,  $\Delta \theta$ . Generally,  $\Delta \theta$  is a variable and is computed as the product of the network  $(RC)_{\min}$  and the factor stored in  $M(7)$ . Unless changed by the user in the FUNCT subroutine,

$M(7) = 0.25$ . If the printing interval is less than the  $(RC)_{\min}$ , the computing interval is determined as the product of the printing interval and  $M(7)$ .

A quick estimate of  $\Delta \theta$  may be obtained by multiplying  $M(7)$  by the smallest of the following three quantities:

1. The print interval.
2. The smallest capacitor times its smallest connecting resistor.
3. The smallest resistor times its smallest connecting capacitor.

This method is far from fool-proof, since in particular, radiation resistors are variable inversely with the cube of the temperatures of connected nodes. Also, computations 2 and 3 above, may not give the minimum RC value. In anticipation of a long run, perhaps the best method of getting a time estimate is to run the program for a very short time history and print out the time step or the number of cycles used.

## APPENDIX A

## ECKERT AERODYNAMIC HEATING

The Eckert Aerodynamic Heating subroutine is a valuable tool in performing convective heat transfer calculations for high-velocity flows. The program computes the aerodynamic heating rate when given trajectory, flow field, and air property data in a prescribed manner. Eckert's calculation procedure, or the reference temperature method, as it is commonly called, eliminates the dependence of skin friction, and hence wall heating rate, on variable fluid properties associated with high-velocity flow. This allows heat transfer calculations to be accomplished as with incompressible flow where property variations across the boundary layer are negligible.

ECKERT'S RECOMMENDED PROCEDURE

The recommended heating equations follow. Additional explanation can be found in Reference 5. The symbols used are defined in the table of nomenclature given at the end of this section.

For two-dimensional laminar flow over an isothermal and isobaric surface

$$St = 0.332 (Re^*)^{-0.5} (Pr^*)^{-0.667} \quad (A-1)$$

$$q_w = h (T_R - T_w) \quad (A-2)$$

where the asterisk denotes property values to be evaluated at a reference temperature given by

$$T^* = 0.28 T_e + 0.22 T_R + 0.50 T_w \quad (A-3)$$

For two-dimensional turbulent flow over an isothermal and isobaric surface

$$St^* = 0.0296 (Re^*)^{-0.2} (Pr^*)^{-0.667} \quad (A-4)$$

The wall heat transfer is calculated from equation A-2. The reference temperature given by equation A-3 is assumed valid for both laminar and turbulent flows.

MODIFICATION OF ECKERT'S RELATIONS FOR DIGITAL COMPUTING USE

In the form given in the previous section the equations do not lend themselves to computer calculation; therefore, they are modified as explained here:

For turbulent flow, from equation A-4:

$$h_T = 0.0296 \frac{k^*}{X} (Re^*)^{0.8} (Pr^*)^{0.333} \quad (A-5)$$

Combining equation A-5 with equation A-2 results in

$$q_{wT} = \frac{0.0296}{X^{0.2}} \left[ \frac{Re^*}{X} \frac{M_\infty}{M_\infty} \right]^{0.8} (Pr^*)^{0.333} k^* (T_R - T_w) \quad (A-6)$$

Using the Mach number definition

$$M = \frac{u}{c}$$

and the perfect gas relation

$$\frac{c}{c_\infty} = \left( \frac{T}{T_\infty} \right)^{0.5}$$

the Reynolds number term in equation A-6 is modified, resulting in the following expression:



$$\frac{Re^*}{X} = \left[ \frac{Re_\infty}{X} \left( \frac{M_e}{M_\infty} \right) \left( \frac{T_e}{T_\infty} \right)^{0.5} \left( \frac{\rho_e}{\rho_\infty} \right) \right] \left( \frac{\rho^*}{\rho_e} \right) \left( \frac{\mu_\infty}{\mu_e} \right) \left( \frac{\mu_e}{\mu^*} \right) \quad (A-7)$$

Next, the viscosity relation

$$\frac{\mu_e}{\mu^*} = \left( \frac{T_\infty}{T_e} \right)^{0.69}$$

and perfect gas law

$$\frac{\rho^*}{\rho_e} = \frac{T_e}{T^*}$$

are used to modify equation A-7 to the following form:

$$\frac{Re^*}{X} = \left[ \frac{Re_\infty}{X} \left( \frac{M_e}{M_\infty} \right) \left( \frac{\rho_e}{\rho_\infty} \right) \left( \frac{T_e}{T_\infty} \right)^{-0.2} \right] \left( \frac{T_e}{T^*} \right)^{1.69} \quad (A-8)$$

Defining the Reynolds number ratio as

$$\frac{Re_e}{Re_\infty} = \left( \frac{M_e}{M_\infty} \right) \left( \frac{\rho_e}{\rho_\infty} \right) \left( \frac{T_e}{T_\infty} \right)^{-0.2}$$

the expression for  $q_w$  becomes

$$q_{wT} = \frac{0.0296}{X^{0.2}} \left[ \left( \frac{Re_\infty}{XM_\infty} \right) M_\infty \left( \frac{Re_e}{Re_\infty} \right) \left( \frac{T_e}{T^*} \right)^{1.69} \right]^{0.8} (Pr^*)^{0.333} \quad (A-9)$$

$$k^* (T_R - T_w)$$

By a similar process the expression for laminar flow becomes

$$q_{wL} = \frac{0.332}{X^{0.5}} \left[ \left( \frac{Re_{\infty}}{XM_{\infty}} \right) M_{\infty} \left( \frac{Re_e}{Re_{\infty}} \right) \left( \frac{T_e}{T^*} \right)^{1.69} \right]^{0.5} (Pr^*)^{0.333} k^* (T_R - T_w) \quad (A-10)$$

Equations A-9 and A-10 are combined to give the programmed form

$$q_w = K \beta \left[ \left( \frac{Re_{\infty}}{XM_{\infty}} \right) M_{\infty} \left( \frac{Re_e}{Re_{\infty}} \right) \left( \frac{T_e}{T^*} \right)^{1.69} \right]^a (Pr^*)^{0.333} k^* M_{\infty}^b (T_R - T_w) \quad (A-11)$$

where the factor  $\beta$  has been included as an angle of attack modifier. Its use is optional and  $\beta$  will have a value of unity unless changed by the user as described below. The term  $M_{\infty}^b$  is included to give the Eckert equation the same form as that used by another aerodynamic heating method, which is no longer being used. The recovery temperature is computed from the following:

$$T_R = T_e \left[ 1 + Pr^e \left( \frac{\gamma - 1}{2} \right) M_e^2 \right] \quad (A-12)$$

where  $Pr^e$  is the temperature recovery factor. A constant value of  $Pr = 0.71$  is used in the program.

#### PROGRAM INPUT

Several tables must always be provided in the data block when the Eckert heating routine is used. The designation numbers of these tables are permanently reserved and linear interpolation of the data is understood. The user must always provide tables 1, 3, 4, 5, 6, 8, 11, 12, and 13. If the angle of attack multiplier  $\beta$  is not understood to be unity, tables 2 and 7 must also be provided. The following list shows the composition of each table.

<u>TABLE DESIGNATION NUMBER</u>	<u>INDEPENDENT VARIABLE</u>	<u>DEPENDENT VARIABLE</u>
1	$\theta$	H
3	H	$\log_{10} \left( \frac{Re_{\infty}}{XM_{\infty}} \right)$
4	$T^*$	$\log_{10} \left( Pr^{0.333} k \right)$
5	$M_{\infty}$	$\frac{Re_e}{Re_{\infty}}$
6	$M_{\infty}$	$\frac{T_e}{T_{\infty}}$
8	Constants a, b, e, $\gamma$ in that order	
11	$\theta$	$M_{\infty}$
12	H	$T_{\infty}$
13	$M_{\infty}$	$\frac{M_e}{M_{\infty}}$
2	$\theta$	$\alpha_R$
7	$\alpha$	$\beta$ or constants $K_w$ and $K_L$

Note that tables 3 and 12 contain only atmospheric data and as such are standard, reusable tables. This is also true of table 4, which contains thermodynamic and transport properties data. The trajectory is defined in tables 1 and 11, and the local flow field in tables 5, 6, and 13. Table 8 lists the constants a, b, e, and  $\gamma$  from equations 11 and 12. Using the Blasius expressions for skin friction (equations 1 and 4) and assuming the fluid is air with  $\gamma = 1.4$ , these constants are:

BOUNDARY LAYER	a	b	e	$\gamma$
laminar	0.5	0	0.5	1.4
turbulent	0.8	0	0.333	1.4

The angle of attack multiplier  $\beta$  is optional. Two possible methods exist for its use.

#### Method 1

In this method the angle of attack multiplier is input in table 7 as

$$\beta = f(\alpha)$$

where the angle of attack is obtained from

$$\text{For the top surface, } F = 0 \quad \alpha = -(\alpha_R - \alpha_o)$$

$$\text{For the bottom surface, } F = 1 \quad \alpha = (\alpha_R - \alpha_o)$$

Both  $F$  and  $\alpha_o$  are input as part of the function callout as described below. The vehicle angle of attack  $\alpha_R$  is given in table 2 as a function of time.

#### Method 2

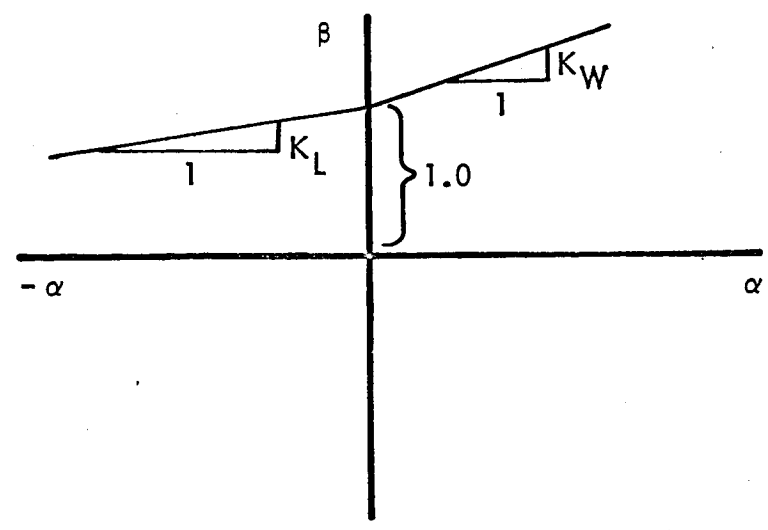
This method consists of inputting two slopes,  $K_w$  and  $K_L$ , in table 7, and having the machine compute the angle-of-attack multiplier by one of the following equations:

$$\alpha > 0 \text{ (a windward surface)} \quad \beta = 1 + K_w \alpha$$

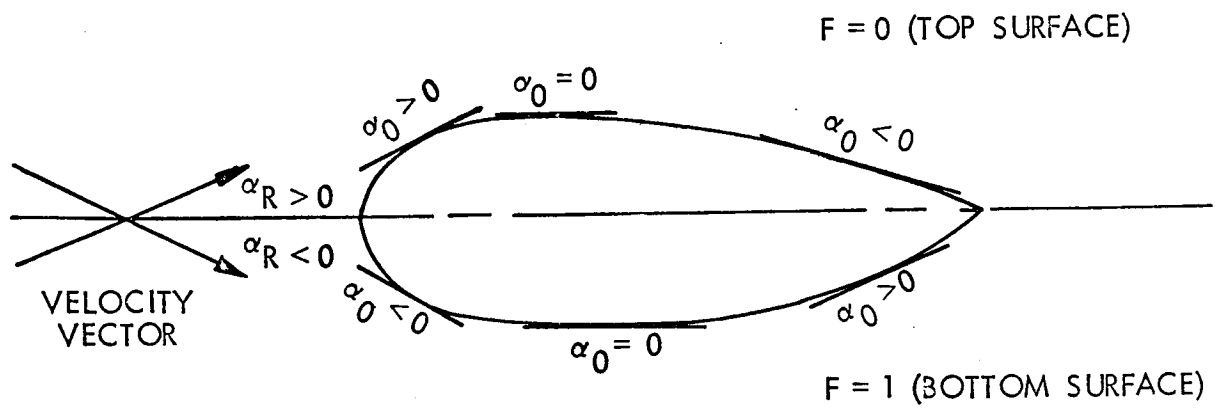
$$\alpha < 0 \text{ (a leeward surface)} \quad \beta = 1 + K_L \alpha$$

The vehicle angle of attack  $\alpha_R$  is again given in table 2 as a function of time.

Shown below is a sketch of the  $\beta - \alpha$  relation used in Method 2.



The sign convention used to determine  $\alpha_R$  and  $\alpha_0$  is indicated below.



One additional quantity is required as data input to the computer when using the Eckert Aerodynamic heating routine. This is the K factor in equation A-11 which, as can be seen by comparing equations A-9, A-10, and A-11, is given by the following:

$$\text{Laminar flow} \quad K = \frac{0.332A}{X^{0.5}} \quad (\text{A-13})$$

$$\text{Turbulent flow} \quad K = \frac{0.0296A}{X^{0.2}} \quad (\text{A-14})$$

The subroutine callout takes one of the following forms:

CALL EAH4 (j, K, H,  $\alpha_0$ , F)

CALL EAH3 (j, K,  $\alpha_0$ , F)

CALL EAH2 (j, K, H)

CALL EAH1 (j, K)

where

- j is the node number for which q is computed.
- K is the floating point constant K, or the location where K is stored.
- H is the location where the value of the heat transfer coefficient is to be stored, if desired.
- $\alpha_0$  is the vehicle surface angle in radians. If not specified, the angle-of-attack multiplier  $\beta$  is understood to be unity.
- F is a flag which is 0 for an upper surface and 1 for a lower surface. F is vacant if  $\alpha_0$  is vacant.

Several example callouts are:

1. CALL EAH1 (16,0.02)

Means compute the aerodynamic heating to node 16 with  $K = 0.02$  and  $\beta$  is understood to be 1.

2. CALL EAH1 (16,P(L + 3))

Means compute the aerodynamic heating to node 16, and find the value of the K factor in the third storage location of the table whose designation number corresponds to L.

This arrangement allows K to be a variable expressed by some other function.

3. CALL EAH2 (16, 0.02, P(L20 + 2))

Means the same as (1) except that the value of the heat transfer coefficient is to be stored in the second storage location of the table whose designation number corresponds to L20. This arrangement allows h to be called out in the print block.

4. CALL EAH3 (16, 0.02, 0.2, 0)

Means the same as (1) except that the angle of attack multiplier  $\beta$  is computed by Method I above with  $\alpha_0 = 0.2$  radians, and the node is located on the upper surface.

5. CALL EAH4 (16, P(L + 3), P(L20 + 2), 0.02, 1)

Means compute the aerodynamic heating to node 16, find the K factor in the third storage location of the table whose designation number corresponds to L, and store the value of the heat transfer coefficient in the second storage location of the table whose designation number corresponds to L20. The angle of attack multiplier  $\beta$  is computed by Method I with  $\alpha_0 = 0.2$  radians, and the node is located on a bottom surface.

The recovery temperature in  $^{\circ}\text{F}$  is automatically stored in the addressable element M(12).

#### LIMITATIONS OF ECKERT'S AERODYNAMIC HEATING METHOD

The aerodynamic heating subroutine described herein is strictly valid within certain limitations. These are summarized below:

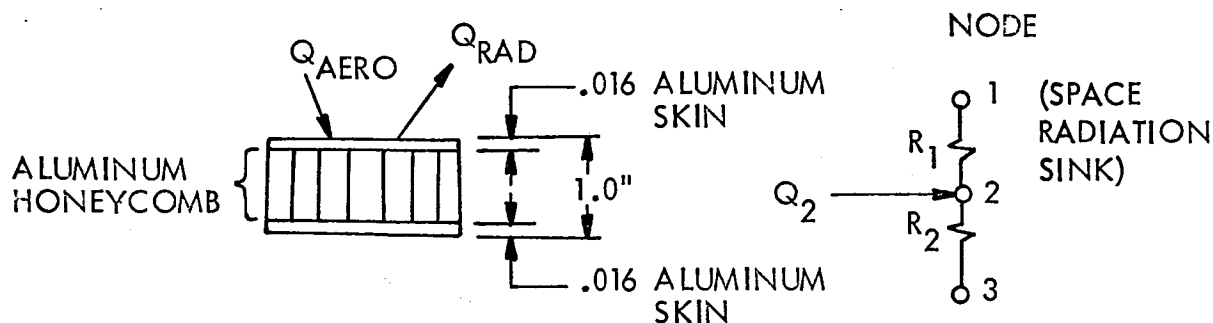
1. In deriving Eckert's relations for digital computing the reference temperature form was used, rather than reference enthalpy. This assumes constant specific heat and Prandtl number.

2. Effects of dissociation and ionization are neglected in the heating relations. This limits the velocity range for which the equations are valid. For example, dissociation of the air molecules behind a normal shock begins at approximately Mach 6, for an altitude of 200,000 ft.
3. Near continuum flow is required, i.e.,  $H \leq 200,000$  ft.
4. Two-dimensional flow along a constant pressure and temperature surface is assumed.
5. Steady, or slowly accelerating, flow is required.

The above assumptions probably limit the accuracy of the method to something like  $\pm 10\%$  for a typical ascent trajectory.

#### EXAMPLE PROBLEM

To illustrate the procedure in using the Eckert heating subroutine, a simple ascent heating problem is set up. Suppose it is desired to calculate the transient temperature response of an aluminum honeycomb skin located at a distance of 45 ft from the nose of the vehicle. The vehicle trajectory (altitude and Mach number vs time) and local flow field parameters are assumed known. A sketch of a unit surface area of the skin and the corresponding thermal network are given below.



The following assumptions are made:

1. The boundary layer is turbulent for the first 135 sec after launch, at which time transition to laminar flow occurs instantaneously.



2. The external skin (node 2) radiates to a free space sink of 50°F.
3. The skin rear face is perfectly insulated.
4. The aluminum properties are:

$$\rho = 0.1 \text{ lb/in}^3$$

$$c_p = 0.2 \text{ Btu/lb}^\circ\text{F}$$

$$\epsilon = 0.55$$

$$k_{\text{HONEYCOMB}} = 8 \frac{\text{Btu in.}}{\text{hr ft}^2\text{ }^\circ\text{F}}$$

$$C_{\text{HONEYCOMB}} = 0.03 \frac{\text{Btu}}{^\circ\text{F ft}^2}$$

#### Capacitors

Lump each skin with half of the honeycomb core

$$C_2 = C_3 = \rho V c_p + \frac{.03}{2}$$

$$= 0.1 \frac{\text{lb}}{\text{in}^3} \times .016 (144) \text{ in}^3 \times 0.2 \frac{\text{Btu}}{\text{lb } ^\circ\text{F}} + 0.015 = 0.0611 \frac{\text{Btu}}{^\circ\text{F}}$$

#### Radiation Resistor

$$K_1 = \frac{\epsilon FA}{3600} = \frac{0.55 (1) (1)}{3600} = 1.53 \times 10^{-4}$$

#### Conduction Resistor

$$R_2 = \frac{l}{kA} = \frac{0.968 \text{ in} \times 3600 \frac{\text{sec}}{\text{hr}}}{8 \frac{\text{Btu in.}}{\text{hr ft}^2\text{ }^\circ\text{F}} \times 1 \text{ ft}^2} = 436 \frac{\text{sec } ^\circ\text{F}}{\text{Btu}}$$

Eckert K Factor

$$K^2_{\text{turbulent}} = \frac{0.0296A}{X^{0.2}} = \frac{0.0296(1)}{(45)^{0.2}} = 0.0138$$

$$K^2_{\text{laminar}} = \frac{0.332A}{X^{0.5}} = \frac{0.332(1)}{(45)^{0.5}} = 0.0496$$

The program input is shown in Figure A-1. The value of the turbulent K factor is stored in the location T(4). Tables 1 and 11 contain, respectively, the vehicle altitude and Mach number vs time. These are assumed values and are typical of large liquid fuel boosters. Tables 3 and 11 contain  $\log_{10} (Re_{\infty}/XM_{\infty})$  and freestream temperature vs altitude for Patrick Air Force Base, Florida. These tables were constructed from the measured data published in Reference 6. Table 4 contains  $\log_{10} (Pr^{0.333} k)$  vs temperature, using the data of Reference 7. Thus, tables 3, 4, and 11 contain real properties data, applicable to any Cape Kennedy launch. Actually, the difference between the Patrick Air Force Base Standard Atmosphere and the 1962 U.S. Standard Atmosphere (Reference 8) is so slight that the data in these tables may be used with considerable confidence regardless of the launch site. Tables 5, 6, and 13 list assumed values for the flow field parameters ( $Re_e/Re_{\infty}$ ,  $T_e/T_{\infty}$ , and  $M_e/M_{\infty}$ ) as a function of freestream Mach number. These values depend primarily on the vehicle geometry. The constants a, b, e, and  $\gamma$  applicable to a turbulent boundary layer are stored in Table 8. In the time block the initial and final times are set at 0 and 160 sec, with a print interval of 5 sec. For a typical ascent heating problem, the computing interval should not exceed 5 sec to prevent temperature oscillations.

The FUNCT subroutine should be self-explanatory. Card 6008 contains the radiation function and, if current time does not equal 140., all other functions are ignored with the exception of the Eckert Heating routine. The K factor is obtained from TN(4). If current time equals 140., the turbulent K factor stored in TN(4) is replaced by the laminar K factor (with a value 0.0496). Also, the constants a and e of table 8 are replaced by their laminar values.

Note that these changes are made at 140 sec, rather than at 135 sec when transition is assumed to occur. This is a result of the finite difference solution which, with a computing interval of  $\Delta\theta$  sec, assumes that the value of each independent variable remains constant during the time  $\theta - \Delta\theta$ . Thus, if the exponent  $e$  stored in table 8 is changed at 140 sec, the new value is used by the EAH subroutine during the interval 135-140 sec.

The PRINT subroutine is set up to list the current time, node 2 temperature, node 3 temperature, recovery temperature, and aerodynamic heating rate on a single line of output. The first 4 items will appear in the F-field format, and the heating rate in the E-field format.

TABLE A-1  
INPUT FOR AERODYNAMIC HEATING EXAMPLE PROBLEM (1 of 5)

GENERAL PURPOSE DATA SHEET										LOCKHEED-CALIFORNIA COMPANY A DIVISION OF LOCKHEED AIRCRAFT CORPORATION		PAGE	OF					
PREPARED	NAME	DATE	TITLE							JOB NO.	GROUP							
CHECKED	WO							EWA										
ID																		
77	80	1	10	15	20	25	30	35	40	45	50	55	60	65	70	72	73	76
CID	ECKERT AERODYNAMIC HEATING EXAMPLE PROBLEM																	
DECO4	1	50.	2	70.	4	0.0138	TEMPERATURES										1000	
NBK																		
DECO2	1	1	2	0.	2	3	436. RESISTORS										2001	
NBK																		
DECO2	2	0.0611	3	0.0611	CAPACITORS										3001			
NBK																		
DEC	1	ALTITUDE VS TIME															40101	
DECO6	0.	0.	20.	2000.	40.	8500.											2	
DECO6	60.	24000.	70.	35000.	80.	48500.											3	
DECO6	90.	63000.	100.	80000.	110.	100000.											4	
DECO6	120.	123000.	130.	150000.	140.	181000.											5	
DECO5	150.	212000.	160.	247000.	0.											6		
DEC	-1																40107	
DEC	3	LOG(RE/XM) VS ALTITUDE FOR PATRICK AFB															40301	
DECO6	0.	6.832	5000.	6.775	10000.	6.712											02	
DECO6	15000.	6.646	20000.	6.582	25000.	6.517											03	
DECO6	30000.	6.453	35000.	6.382	40000.	6.310											04	
DECO6	45000.	6.230	50000.	6.134	55000.	6.024											05	
DECO6	60000.	5.910	65000.	5.790	70000.	5.672											06	
DECO6	75000.	5.561	80000.	5.447	85000.	5.342											07	
DECO6	90000.	5.241	95000.	5.127	100000.	5.029											08	
DECO6	105000.	4.922	110000.	4.815	115000.	4.708											09	
DECO6	120000.	4.603	125000.	4.507	130000.	4.410											10	
DECO6	135000.	4.305	140000.	4.216	145000.	4.125											11	

FORM DX 7924-1



TABLE A-1  
 INPUT FOR AERODYNAMIC HEATING EXAMPLE PROBLEM (2 of 5)

GENERAL PURPOSE DATA SHEET										LOCKHEED-CALIFORNIA COMPANY A DIVISION OF LOCKHEED AIRCRAFT CORPORATION		PAGE	OF								
PREPARED	NAME	DATE	TITLE							JOB NO.	GROUP										
CHECKED								#	EWA												
SEC.	ID	77	80	1	15	20	25	30	35	40	45	50	55	60	65	70	72	73	76		
DEC06	150000.				4.038			156000.			3.927			175000.					3.628	40312	
DEC06	190000.				3.424			200000.			3.280			210000.					3.129	40313	
DEC06	220000.				2.969			230000.			2.800			240000.					2.621	40314	
DEC06	250000.				2.429			263000.			2.156			280000.					1.704	40315	
DEC03	300000.				1.198			0.												40316	
DEC	-3																			40317	
DEC	4				LOG(PR** .333 K) VS TEMPERATURE (IN DEG. RANKINE)																
DEC06	250.				-5.75			332.			-5.6198			500.					-5.4495	40401	
DEC06	700.				-5.3388			900.			-5.2691			1000.					-5.2253	40402	
DEC06	1100.				-5.1981			2300.			-5.0177			5400.					-4.8016	40403	
DEC06	7200.				-4.7205			9000.			-4.6743			10000.					-4.6476	40404	
DEC	0.																			40405	
DEC	-4																			40406	
DEC	5				REYNOLDS NUMBER RATIO VS MACH NUMBER																
DEC06	0.				1.000			1.0			1.000			1.5					0.925	40501	
DEC06	2.0				0.772			2.5			0.621			3.0					0.480	40502	
DEC06	3.5				0.390			4.0			0.320			4.5					0.267	40503	
DEC06	5.0				0.216			5.8			0.165			6.5					0.129	40504	
DEC05	7.5				0.095			10.0			0.070			0.						40505	
DEC	-5																			40506	
DEC	6				TEMPERATURE RATIO VS MACH NUMBER																
DEC06	0.				1.00			1.0			1.00			1.3					1.02	40601	
DEC06	2.0				1.07			2.5			1.19			3.0					1.30	40602	
DEC06	4.0				1.70			4.5			1.90			5.0					2.15	40603	
DEC06	5.8				2.51			6.5			2.92			7.5					3.48	40604	

FORM DX 7924-1



TABLE A-1  
INPUT FOR AERODYNAMIC HEATING EXAMPLE PROBLEM (3 of 5)

GENERAL PURPOSE DATA SHEET		LOCKHEED-CALIFORNIA COMPANY A DIVISION OF LOCKHEED AIRCRAFT CORPORATION		PAGE	OF		
PREPARED	NAME	DATE	TITLE	JOB NO.			
CHECKED			NO	EWA	GROUP		
77	DEC03	10	110.	20	5.00	70	40606
	DEC	-6				72	40607
	DEC	8	CONSTANTS A, B, E, AND GAMMA			73	40801
	DEC04	-8	0.8	0.333	1.4	74	40802
	DEC					75	40803
	DEC	11	FREESTREAM MACH NUMBER VS TIME			76	41101
	DEC06		0.	0.01	0.21	77	41102
	DEC06		60.	0.94	1.32	78	41103
	DEC06		90.	2.28	2.83	79	41104
	DEC06		120.	4.47	4.93	80	41105
	DEC05		150.	7.72	8.92	81	41106
	DEC	-11				82	41107
	DEC	12	TEMPERATURE VS ALTITUDE FOR PATRICK AFB			83	41201
	DEC06		0.	534.	471.	84	41202
	DEC06		45000.	377.	369.	85	41203
	DEC06		60000.	370.	397.	86	41204
	DEC06		110000.	430.	484.	87	41205
	DEC06		175000.	509.	473.	88	41206
	DEC06		220000.	400.	352.	89	41207
	DEC05		280000.	298.	298.	90	41208
	DEC	-12				91	41209
	DEC	13	MACH NUMBER RATIO VS MACH NUMBER			92	41301
	DEC06		0.	1.00	1.00	93	41302
	DEC06		2.0	0.93	0.85	94	41303
	DEC06		3.5	0.73	0.68	95	41304



TABLE A-1  
INPUT FOR AERODYNAMIC HEATING EXAMPLE PROBLEM (4 of 5)

GENERAL PURPOSE DATA SHEET				LOCKHEED-CALIFORNIA COMPANY A DIVISION OF LOCKHEED AIRCRAFT CORPORATION				PAGE	OF	
PREPARED	NAME	DATE	TITLE	WO				EWA	GROUP	
CHECKED										
SEQ.	ID									
77	80	1	DECOG	5.0	0.60	5.8	0.55	6.5	0.52	41305
			DECO5	7.5	0.47	10.0	0.40	0		41306
			DEC	-13						41307
			NBK							49999
			DECO3	5.	160.	0.			TIME BLOCK	5001
			NBK							5999
6001			IBFTC FUNCT							
6002										
6003			SUBROUTINE FUNCT							
			COMMON P, M							
6004										
6005			DIMENSION P(16000), M(16), TN(1), T(1), R(1), Q(1), RC(1)							
6006			EQUIVALENCE (P(1), TN(1)), (P(5), T(1)), (P(9), R(1)), (P(11), C(1)),							
6007			1 (P(14), Q(1)), (P(17), RC(1))							
6008			REAL M, LIN							
			R(1) = RAD(1, 2, 1.53E-4)							
6009			IF (M(1).EQ.140.) GO TO 1							
6010			GO TO 2							
6011			TN(4) = 0.0496							
6012			L8 = LFC(8)							
6013			P(L8+1) = 0.5							
6014			P(L8+3) = 0.5							
6015			CALL EAH1(2, TN(4))							
6016			RETURN							
6017			END							

FORM DX 7924-1



TABLE A-1  
INPUT FOR AERODYNAMIC HEATING EXAMPLE PROBLEM (5 of 5)

GENERAL PURPOSE DATA SHEET				LOCKHEED-CALIFORNIA COMPANY A DIVISION OF LOCKHEED AIRCRAFT CORPORATION		PAGE	OF
PREPARED	NAME	DATE	TITLE	WO	EWA	JOB NO.	GROUP
CHECKED							
SEQ.	ID						
27	601	70	7273	76			
7001	#IBFTC PRINT	15	NODECK, NOREF				
7002	SUBROUTINE PRINT	20					
7003	COMMON P, M	25					
7004	DIMENSION P(16000)	30	M(16), T(1), R(1), C(1), Q(1), RC(1)				
7005	EQUIVALENCE (P(1), T(1)), (P(5), T(1)), (P(9), R(1)), (P(11), C(1)),	35					
7006	1 (P(14), Q(1)), (P(17), RC(1))	40					
7007	REAL M	45					
7008	WRITE (6, 10) M(1), T(2), T(3), M(12), Q(2)	50					
7009	10 FORMAT (1H0, A18.0, 1E18.8)	55					
7010	RETURN	60					
7011	END	65					





## NOMENCLATURE FOR APPENDIX A

a	Exponent in equation A-11
A	Heated surface area, $\text{ft}^2$
b	Mach number exponent in equation A-11
c	Speed of sound, $\text{ft}/\text{sec}$
$c_p$	Specific heat, $\text{Btu}/\text{lb}^\circ\text{F}$
C	Thermal capacitance, $\text{Btu}/^\circ\text{F}$
e	Prandtl number exponent in equation A-12
h	Heat transfer coefficient, $\text{Btu}/\text{ft}^2 \text{ sec}^\circ\text{F}$
H	Altitude, $\text{ft}$
k	Thermal conductivity, $\text{Btu}/\text{ft sec}^\circ\text{F}$
K	Eckert K factor defined by equations A-13 and A-14
$K_w, K_L$	Surface slopes
Pr	Prandtl number
q	Surface heat flux, $\text{Btu}/\text{ft}^2 \text{ sec}$
Q	Surface heat flux, $\text{Btu}/\text{sec}$
R	Thermal resistor, $\text{sec}^\circ\text{F}/\text{Btu}$
Re	Reynolds number
St	Stanton number
T	Temperature, $^\circ\text{R}$
u	Velocity, $\text{ft}/\text{sec}$

## NOMENCLATURE FOR APPENDIX A (Continued)

V	Volume of lump, in <sup>3</sup>
X	Equivalent boundary layer length, ft
$\alpha$	Local angle of attack, radians
$\alpha_R$	Vehicle body axis angle of attack, radians
$\alpha_0$	Vehicle surface angle, radians
$\beta$	Angle of attack multiplier
$\mu$	Viscosity, lb/ft sec
$\gamma$	Ratio of specific heats
$\epsilon$	Emissivity
$\theta$	Time, sec
$\rho$	Density, lb/ft <sup>3</sup>

Subscripts

e	Boundary layer edge
R	Recovery
w	Wall
$\infty$	Freestream

Superscripts

*	Evaluated at the reference temperature given by equation A-3
---	--

## APPENDIX B

## ABLATION

The ablation subroutine is an extension of the Thermal Analyzer Program to solve problems involving transient and steady-state ablation. The function calculates the amount of material that is ablated (if the temperature is above the ablation temperature) as a function of time as part of the heat balance using the finite difference technique. The amount of material that is ablated is then removed from the network by a switching arrangement, while the normal transient temperature distribution is calculated for the remaining ablation material and back-up structure. The ablation function, like most other functions, must have entries in the data block and FUNCT subroutine with the data block being a table of information that the function needs to perform the ablation process.

The ablation function will only ablate a network that has the nodes at the boundaries of the lumps. The nodes and their information must be put into the table and listed in the capacitor block in the order in which they will ablate, but the node numbers need not be assigned consecutively. The machine calculates the resistors and capacitors in the ablating layer at each cycle, allowing for material removal. All material properties, e.g., thermal conductivity, heat ablation, etc., may be made a function of any variable. The three limitations of the program are:

1. Only ablation from a solid to a gas without a char layer may be considered.
2. Only one-dimensional heat transfer can be handled in the ablation material.
3. Ablation network resistors and capacitors may not be input by the geometric methods discussed on pages 5-6 and 5-8.

Some of the items that make the program very flexible are:

1. Heat of ablation and temperature of ablation may be made a function of temperature, heating rate, enthalpy, or time.

2. The ablating system may be stopped and started an infinite number of times.
3. It can handle the case of any number of layers of different ablation materials.
4. Many ablating systems can be handled at one time, either separately or linked together at a nonablating node.
5.  $\rho$ ,  $c_p$ , and  $k$  may be a function of any variable.
6. Radiation from the ablating node with emissivity as a variable can be handled by the program.

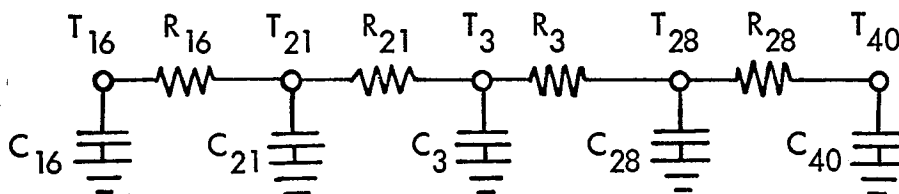
### PROGRAM INPUT

The ablation subroutine callout is

CALL ABL(i,N)

where  $i$  is the first (surface) ablating node number and  $N$  is the designation number of the table which contains the ablator properties used for the calculation of the capacitors and resistors in the ablating network.

To illustrate the use of this function, consider the example of a 4-link ablating chain sketched below.



(NOTE the correspondence between node and resistor numbers. This is an absolute necessity when using the ablation function.)

Node 16 is the first ablating node; i.e., the material is ablated from left to right in the figure. The network to the left of  $C_{16}$  is normally a description of the heat input (which would include radiation outward) to the outermost ablating material. The network to the right of  $C_{28}$  (starting with node 40) would be the structure to which the ablating material is attached.

The ablation table contains the list of capacitor-resistor links in the same order that ablation will take place. Note that although the ablation table would be a sufficient description of the ablation network, this ablation network must have been described in the resistor block and capacitor block just as any part of the network was described. However, the initial values assigned to the ablation resistors and capacitors will be replaced by those found by computation using the tabular properties and hence can be input as zero.

The leading line of the table must be entered as 10 zeros, the two trailing columns (columns 9 and 10) must be entered as zeros, and the final line consists of one zero. These bordering zeros result in a convenient matrix reference scheme for the user of the ablation function as well as providing necessary storage for the ablation program. The first 8 entries on the intermediate lines contain, in order, the following information:

1. Node and corresponding resistor designation numbers
2. Ablator thermal conductivity - Btu/hr ft °F
3. Ablator density - lb/ft<sup>3</sup>
4. Ablator specific heat - Btu/lb °F
5. Cross-sectional area normal to heat flow - ft<sup>2</sup>
6. Initial resistor length - in.
7. Ablation temperature - °F
8. Heat of ablation - Btu/lb

The ablation table (designated as Table 4 in this example) is entered as

0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
16.	$K_{16}$	$\rho_{16}$	$C_{16}$	$A_{16}$	$x_{16}$	$T_{16,a}$	$H_{16,a}$	0.	0.
21.	$K_{21}$	$\rho_{21}$	$C_{21}$	$A_{21}$	$x_{21}$	$T_{21,a}$	$H_{21,a}$	0.	0.
3.	$K_3$	$\rho_3$	$C_3$	$A_3$	$x_3$	$T_{3,a}$	$H_{3,a}$	0.	0.
28.	$K_{28}$	$\rho_{28}$	$C_{28}$	$A_{28}$	$x_{28}$	$T_{28,a}$	$H_{28,a}$	0.	0.
0.									

where the various quantities may be identified by reference to the above list. Each entry must be in floating point. During execution, the ninth column will be updated as ablation progresses and will contain the accumulative amount of material (in in.) ablated at that particular node. Consequently, in the PRINT subroutine, a WRITE statement listing the addresses

$$P(I4+19), P(I4+29), P(I4+39), P(I4+49)$$

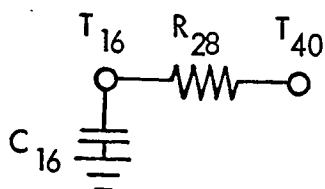
where

$$I4 = LOC(4)$$

will cause to be printed the total material ablated at each node as a function of time. To aid in data reduction, each time a new link begins to ablate, and each time a node stops ablating, the regular output block is automatically printed.

There is no restriction on the number of ablating links in an ablating chain or on the number of separate ablating chains in a particular case. Further, there is no restriction on the number of resistors going into the left-most capacitor (in this case  $C_{16}$ ). However, each interior ablating node must have exactly one resistor to the left and one resistor to the right. If the terminal ablating node is only "half ablating" (input by setting  $T_{28,a}$  equal to a fictitiously large number), there is no restriction on the number of resistors attached to the terminal ablating node.

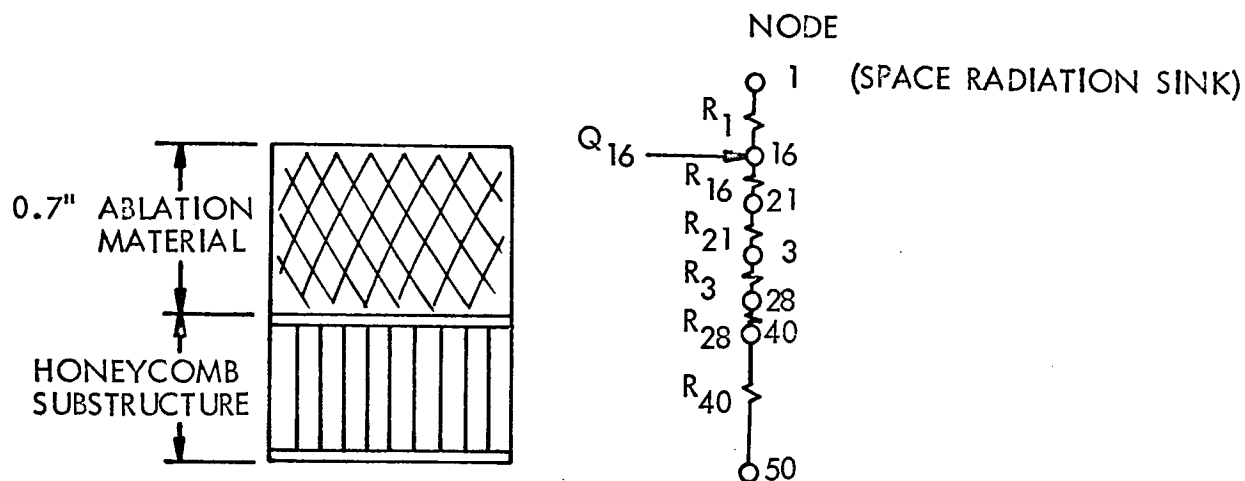
As the material ablates from left to right, the outer boundary is considered to move to the right. Thus, in the example capacitor number 16 continually moves; and if all nodes are completely ablated away, node numbers 21, 3, and 28 and resistor numbers 16, 21, and 3 will vanish from the circuit. Then the circuit will consist merely of



Again we have assumed that the right-hand part of the original  $C_{28}$  was non-ablating material so that the ablation stops at this point.

#### EXAMPLE PROBLEM

To illustrate the procedure in using the ablation subroutine, the following simple problem is set up. Consider the application of a low temperature subliming ablator near the nose region of a highly accelerating solid fuel rocket. The ascent heating pulse is assumed known. A sketch of a unit surface area of the skin and the corresponding thermal network are shown below.



A 4-link ablating chain is set up using the node and resistor designation numbers of the example discussed in the preceding section. The following assumptions are made:

1. The outermost surface of the ablator (node 16) radiates to a free space sink of  $50^{\circ}\text{F}$ . The surface emissivity is 0.8 resulting in a radiation K factor of  $2.22 \times 10^{-4}$ .
2. Conduction resistor 40 connects the substructure skin nodes 40 and 50.  $R(40)$  has a value of  $2000 \text{ sec } ^{\circ}\text{F}/\text{Btu}$ , and each skin node has a capacitance of  $0.10 \text{ Btu}/^{\circ}\text{F}$ .
3. The ablator properties and dimensions are:

$$\text{Thermal conductivity} = 0.08 \text{ Btu/hr ft } ^{\circ}\text{F at } 0^{\circ}\text{F}$$

$$= 0.12 \text{ Btu/hr ft } ^{\circ}\text{F at } 600^{\circ}\text{F}$$

Density .	=	66 lb/ft <sup>3</sup>
Specific heat	=	0.35 Btu/lb °F
Cross-sectional area	=	1.0 ft <sup>2</sup>
Initial lump thickness	=	0.2 in. for resistors 16, 21, and 3
	=	0.1 in. for resistor 28
Ablation temperature	=	535°F
Heat of Ablation	=	600 Btu/lb

The program input is shown in Table B-1. Dummy values are entered for the ablation material resistors and capacitors since these are computed each cycle by the ABL subroutine. The assumed aerodynamic heat pulse is shown as curve 1 of the data block. The ablation table 4 is entered using the assumed properties listed above. The ablator conductivity is shown in curve 5. The initial and final times are set at 0 and 100 seconds, with a print interval of 2.5 sec.

In the FUNCT subroutine, card 6008 calls for linear interpolation of curve 1 to obtain the aerodynamic heating to node 16. On cards 6010-6013, the values of thermal conductivity listed in table 4 are updated each cycle by interpolating curve 5, using as independent variable the average temperature of the nodes to which the particular resistor is attached. Card 6014 calls in the Ablation subroutine, and card 6015 specifies the space radiation function. The radiation flux is computed and stored in the variable QRAD16 by subtracting the space sink temperature from the wall temperature, and dividing by the space radiation resistor.

The PRINT subroutine calls for the output to be listed in six columns, with the corresponding time appearing by itself to the left of the first line of output. The first line will consist of the temperatures of nodes 16, 21, 3, 28, 40 and 50, in that order. The second line will list the accumulated amount of material ablated at nodes 16, 21, 3, and 28; the aerodynamic heating rate; and the radiation loss to space.



TABLE B-1  
INPUT FOR ABLATION EXAMPLE PROBLEM (1 of 3)

GENERAL PURPOSE DATA SHEET			LOCKHEED-CALIFORNIA COMPANY A DIVISION OF LOCKHEED AIRCRAFT CORPORATION												PAGE	OF		
PREPARED	NAME	DATE	TITLE													JOB NO.		
CHECKED			WO	EWA													GROUP	
ID					70	72	73	76										
77	80	1																
	CID			ABLATION EXAMPLE PROBLEM														
	DECO1	1		50.														1000
	DECO2	2		70.	50	70.												1001
	NBK																	1002
	DECO2	1		16	0.	16	21	0.										1999
	DECO2	21	21	3	0.	3	28	0.										2001
	DECO2	28	28	40	0.	40	50	2000.										2002
	NBK																	2003
	DECO3	16		0.	21	0.	3	0.										2999
	DECO3	28		0.	40	.1	50	.1										3001
	NBK																	3002
	DECO3	1																3999
	DEC	1																4001
	DECO6			0.	0.	15.	0.	25.										4002
	DECO6			35.	12.	40.	16.	50.										4003
	DECO6			60.	16.	75.	4.	90.										4004
	DECO3	-1		100.	0.	0.												4005
	DEC	4																4006
	DEC																	4007
	DECO6			0.	0.	0.	0.	0.										4008
	DECO6			0.	0.	0.	0.	16.										4009
	DECO6			66.	0.35	11.	0.1	535.										600.
	DECO6			0.	0.	21.	0.08	66.										0.35
	DECO6			1.	0.2	535.	600.	0.										0.
	DECO6			2.	0.08	66.	0.35	1.										0.2
	DECO6			60.	60.	0.	0.	28.										0.08
	DECO6			60.	60.	0.	0.	28.										4014

FORM DX 7924.1



TABLE B-1  
INPUT FOR ABLATION EXAMPLE PROBLEM (2 of 3)

GENERAL PURPOSE DATA SHEET										LOCKHEED-CALIFORNIA COMPANY A DIVISION OF LOCKHEED AIRCRAFT CORPORATION		PAGE	OF							
PREPARED	NAME	DATE	TITLE		JOB NO.					GROUP										
CHECKED										WO	EWA									
SEQ.	ID	77	80	1	5	10	15	20	25	30	35	40	45	50	55	60	65	70	7273	76
DEC06					66.			0.35		11.		0.2		535.		600.		4015		
DEC03					0.			0.		0.								4016		
DEC				-4														4017		
DEC				5				CONDUCTIVITY VS TEMPERATURE										4018		
DEC05					0.			0.08		600.		0.12		0.				4019		
DEC																		4020		
NBK																		4999		
DEC03								100.		0.								5001		
NBK																		5999		
6001																				
6002																				
6003																				
6004																				
6005																				
6006																				
6007																				
6008																				
6009																				
6010																				
6011																				
6012																				
6013																				
6014																				
6015																				



TABLE B-1  
INPUT FOR ABLATION EXAMPLE PROBLEM (3 of 3)

GENERAL PURPOSE DATA SHEET				LOCKHEED-CALIFORNIA COMPANY A DIVISION OF LOCKHEED AIRCRAFT CORPORATION		PAGE	OF
PREPARED	NAME	DATE	TITLE		GROUP	JOB NO.	
CHECKED			WO	EWA			
ID							
77	80	1					
6016							
6017							
6018							
7001							
7002							
7003							
7004							
7005							
7006							
7007							
7008							
7009							
7010							
7011							
7012							
7013							

FORM DX 7824-1



## APPENDIX C

## DIGITAL COMPUTER SOLUTION FOR PASSAGE AIR AND WALL TEMPERATURES

The basic approach in the computation of passage air and wall temperatures is the lumped parameter technique widely employed in the electrical analog solution of problems involving partial differential equations. The network for convection at a surface where there is no appreciable variation of the fluid temperature in the flow direction is simply a resistance,  $R_c$ , connecting each of the node points representing the surface temperatures of the solid to a node point representing the fluid bulk temperature, where

$$R_c = \frac{1}{h A_c}$$

$h$  = heat transfer coefficient

$A_c$  = area for convective heat transfer  
per surface temperature node

Such is not the case for the network for convection from a gas to a surface where the convective heat transfer gives rise to appreciable variations of the gas temperature in the flow direction, and the analysis of this situation is therefore presented in somewhat greater detail here. The partial differential equation describing the variation of fluid bulk temperature,  $T$ , with distance in the flow direction,  $X$ , and time,  $\theta$ , is

$$\left( \frac{\rho c_v A_c}{p} \right) \left( \frac{\partial T}{\partial \theta} \right) + \left( \frac{W c_p}{p} \right) \left( \frac{\partial T}{\partial X} \right) + h (T - T_i) = 0$$

where

$T_i$  = passage wall temperature

$V$  = fluid mean velocity

$W$  = fluid flow rate

$c_p$  = fluid specific heat at constant pressure

- $c_v$  = fluid specific heat at constant volume  
 $h$  = heat transfer coefficient  
 $p$  = perimeter of cross-section for heat transfer  
 $A_c$  = cross-sectional area of passage

The rates of change of flow work and kinetic energy of the fluid are neglected in the preceding equation as these terms are small compared with the rate of change of the internal energy of the fluid and the heat transfer rates as represented by the first and second, and the third terms, respectively.

The straightforward application of the lumped parameter technique entails the substitution of the equivalent difference for the distance derivative,  $\left(\frac{\partial T}{\partial X}\right)$ , viz.

$$\left(\frac{\partial T}{\partial X}\right) \approx \frac{T_n - T_{n-1}}{(\delta X)}$$

in the equation above to yield

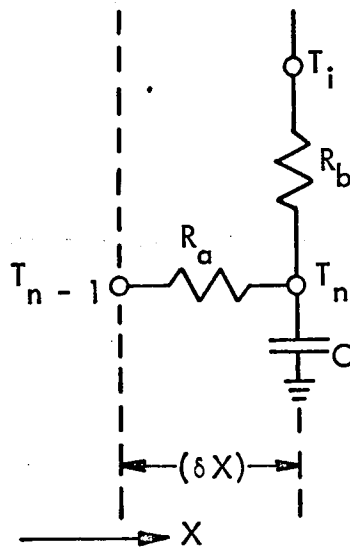
$$\left\{ \rho c_v A_c (\delta X) \right\} \left( \frac{d T_n}{d \theta} \right) + (W c_p) (T_n - T_{n-1}) + \left\{ hp (\delta X) \right\} (T_n - T_i) = 0$$

The network representation for this equation is as shown below, where

$$C = \rho c_v A_c (\delta X)$$

$$R_a = \frac{1}{W c_p}$$

$$R_b = \frac{1}{hp (\delta X)}$$



Application of this lumped parameter network to the air passage of the problem at hand (and to heat exchanger passages in general where the fluid is a gas) necessitates the use of a very large number of node points for a moderate accuracy in the problem solution. It is shown below from a consideration of a simplified network for a typical element of the complete representation that the capacitor shown in the circuit above may be removed from the circuit without significantly affecting the accuracy of the solution. This in itself does not relieve the requirement for a large number of node points; however, it does permit the term in the original partial differential equation corresponding to this capacitance,  $(\rho c_v A_c/p) (\partial T/\partial \theta)$ , to be removed. Once this term is removed a more refined approximation than that employed above may be substituted for the second term,  $(W c_p/p) (\partial T/\partial X)$ ; whence, a smaller number of node points will produce an equivalent accuracy.

A slice of thickness  $(\delta X)$  of the portion of an air passage included between planes of symmetry is illustrated in Figure C-1. Also illustrated is the equivalent network considering variations of the wall temperature in the direction of airflow only. The triangular symbol schematically indicates a cathode follower (functionally a vacuum tube amplifier with unity gain). The purpose of this component is to reproduce the potential (temperature) of a given node point at a second node point without drawing any appreciable current (heat flux) from the first. If cathode followers are not inserted as

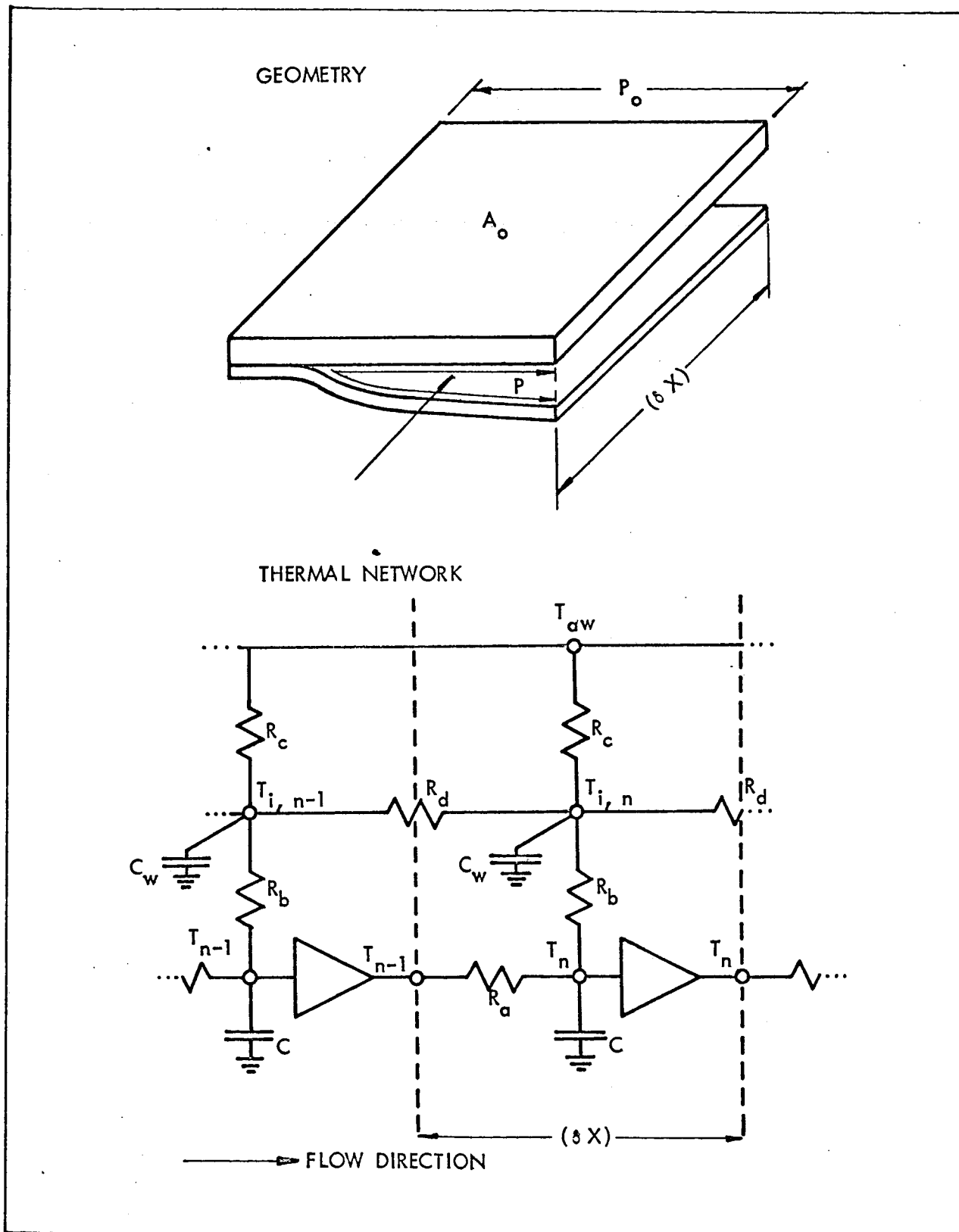


Figure C-1. Physical Geometry and Corresponding Thermal Network for a Portion of an Air Passage

indicated, the equations describing the network response will contain terms not present in the lumped parameter equations of the thermal system. The presence of cathode followers is rationalized on a physical basis by noting that cathode followers isolate air node point temperatures from any effects of convective heat transfer at downstream nodes but not from upstream nodes in accordance with the physical facts.

$R_a$ ,  $R_b$ , and  $C$  are computed as indicated previously and

$T_{aw}$  = adiabatic wall temperature

$h_o$  = external heat transfer coefficient

$A_w$  = shaded area of the figure above

$A_o$  =  $p_o (\delta X)$  = external area for heat transfer

$c_w$  = specific heat of wall

$\rho_w$  = density of wall

$k_w$  = thermal conductivity of wall

$R_c$  =  $\frac{1}{h_o A_o}$

$C_w$  =  $\rho_w c_w A_w (\delta X)$

If the removal of the capacitances representing the rate of change of internal thermal energy of the passage air with respect to time is not to have a significant effect on the solution, an obvious requirement is that these capacitances be very small compared with other capacitances of the system (the passage wall capacitances), i.e.

$$\frac{C}{C_w} = \frac{\rho c_v A_c}{\rho_w c_w A_w} \ll 1$$

An additional consideration is involved as a result of the fact that the effect of changes of passage inlet temperatures are not reflected immediately at downstream points due to the finite time required for the air to traverse the passage. The electrical capacitors representing the thermal capacity of the air,  $C$ , the resistances,  $R_a$ , and the cathode followers, form an electrical



circuit which may be described as a delay line. The delays in this case represent the time required for an air particle to pass from the inlet of the passage to downstream node points. Removal of the capacitors representing the thermal capacity of the air eliminates the delays and is thus tantamount to assuming air particles traverse the passage in zero time. This is justified if the actual time of traverse,  $\theta_L$ , is very small compared to a suitable measure of the time required for a significant change of the wall temperatures. Such a measure is the time constant,  $\tau$ , (resistance-capacitance product) of a wall temperature node point for changes of the air temperature. (The term, time constant, is employed in the usual sense here, i.e., the time required for a node point potential to respond within  $1/e$  or 37% of the final steady-state value resulting from a step change of an adjacent node point potential.)

$$\tau = R_b C_w = \frac{\rho_w c_w A_w}{hp}$$

$$\theta_L = \frac{L}{V}$$

where

$L$  = total passage length

The second condition that must be satisfied is then

$$\frac{\theta_L}{\tau} = \frac{L hp}{\rho_w c_w A_w V} \ll 1$$

The partial differential equation describing the variation of fluid bulk temperature,  $T$ , with distance in the flow direction,  $X$  and time,  $\theta$ , then reduces to

$$\left(\frac{\partial T}{\partial X}\right) + \left(\frac{hp}{w c_p}\right) (T - T_i) = 0$$

Since time does not appear explicitly in this equation it may be treated in the same manner as the ordinary differential equation

$$\left(\frac{dT}{dX}\right) + \left(\frac{hp}{W c_p}\right) (T - T_i) = 0$$

insofar as obtaining a solution is concerned with the understanding that instantaneous values of the wall temperature,  $T_i$ , will be employed in the solution. Assuming that the wall temperature may be considered uniform over a segment of the passage of length  $(\delta X)$  and noting the boundary condition

$$(T)_{x=0} = T_{n-1}$$

where

$T_{n-1}$  = air temperature at the inlet of the segment

the solution becomes

$$T = T_i + (T_{n-1} - T_i) e^{-\frac{hp X}{W c_p}}$$

Setting  $X = (\delta X)$  yields the segment outlet air temperature,  $T_n$

$$T_n = T_i + (T_{n-1} - T_i) e^{-\beta}$$

where

$$\beta = \frac{\Delta h A}{W c_p}$$

$A = p (\delta X)$  = effective area of the segment  
for convective heat transfer

Integrating the heat transfer rate to the wall per unit length over the length of the segment yields the heat transfer rate to the wall segment,  $Q_i$ ,

$$Q_i = \int_0^{(\delta X)} q \, dX = \int_0^{(\delta X)} h_p (T - T_i) \, dX$$

$$Q_i = \int_0^{(\delta X)} h_p (T_{n-1} - T_i) e^{-\frac{\beta X}{(\delta X)}} \, dX$$

$$Q_i = \frac{(hA)}{\beta} (T_{n-1} - T_i)(1 - e^{-\beta})$$

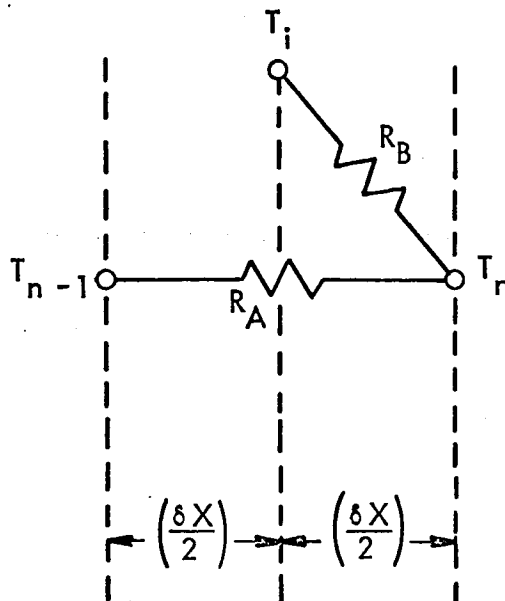
Eliminating the segment inlet temperature,  $T_{n-1}$ , between this expression and the expression for the segment outlet temperature yields

$$Q_i = (W c_p) (e^{\beta} - 1) (T_n - T_i)$$

and eliminating the wall temperature,  $T_i$ , between the same two expressions yields

$$Q_i = (W c_p) (T_{n-1} - T_n)$$

The simplest network satisfying these relationships is shown in the following sketch. (As indicated previously, cathode followers are inserted between this passage segment network and the identical network for the adjacent segments.) Comparison of this network with that previously obtained indicates that, in addition to the absence of a capacitor representing the rate of change of the internal thermal energy of the air, the following differences exist: the wall temperature node location is midway between rather than adjacent to air temperature nodes; and the resistance connecting the segment air outlet temperature node,  $T_n$ , to the wall temperature node,  $T_i$ , is smaller by the ratio  $\beta/(e^{\beta} - 1)$ . Note that as  $(\delta X)$  and hence  $\beta$  approach zero this ratio approaches unity, and that the resistances connecting the segment air inlet and outlet temperature nodes are identical.



$$R_A = \frac{1}{W c_p}$$

$$R_B = \frac{1}{W c_p (e^\beta - 1)}$$

Since significant temperature gradients may exist in the passage walls in planes normal to as well as in the direction of the airflow, the analysis is extended here to include convection to (N) wall temperature nodes around the periphery of each segment. The partial differential equation becomes

$$\left(\frac{\partial T}{\partial X}\right) + \frac{1}{(W c_p)} \sum_{i=1}^N (hp)_i (T - T_i) = 0$$

and the boundary condition is as before

$$(T)_{x=0} = T_{n-1}$$

The solution is then

$$T = \frac{1}{\alpha} \left( 1 - e^{-\frac{\beta X}{(\delta X)}} \right) \sum_{i=1}^N (hA)_i T_i + T_{n-1} e^{-\frac{\beta X}{(\delta X)}}$$

where

$$a \triangleq \sum_{i=1}^N (hA)_i$$

$$\beta \triangleq \frac{a}{W c_p}$$

Setting  $X = (\delta X)$  yields the segment outlet air temperature,  $T_n$ ,

$$T_n = \frac{1}{a} (1 - e^{-\beta}) \sum_{i=1}^N (hA)_i T_i + T_{n-1} e^{-\beta}$$

and integrating the heat transfer rate per unit length over the length of the passage yields the following expression for the heat flux to each wall node point.

$$q_i = (hp)_i \int_0^{(\delta X)} (T - T_i) dX$$

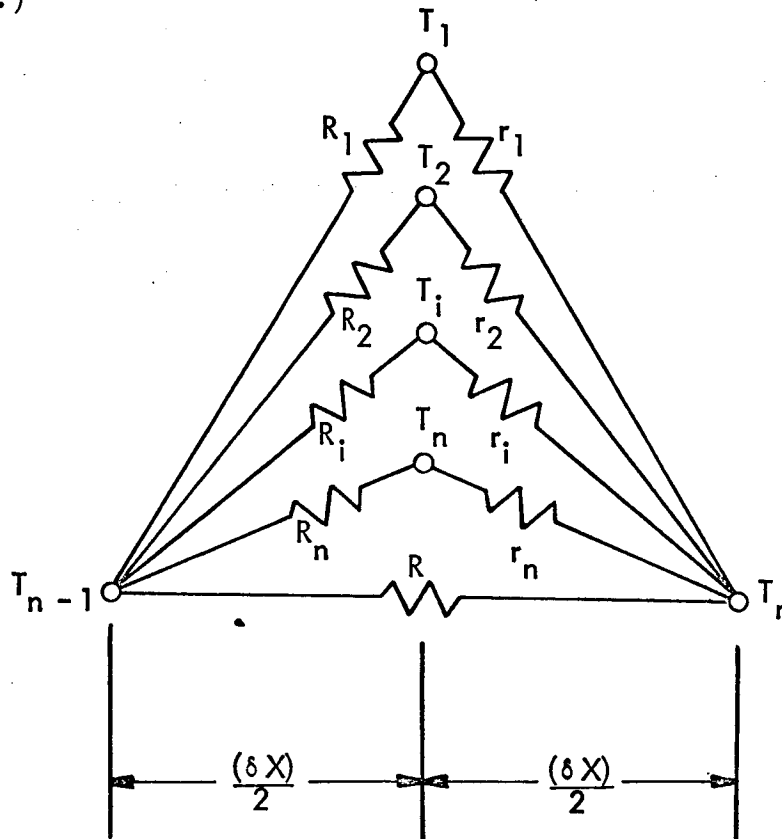
$$q_i = (hA)_i \left\{ \frac{1}{a} \left( 1 + \frac{e^{-\beta}}{\beta} - \frac{1}{\beta} \right) \sum_{i=1}^N (hA)_i T_i + \frac{1}{\beta} (1 - e^{-\beta}) T_{n-1} - T_i \right\}$$

Eliminating the term involving the summation between this expression and the expression for the passage segment air outlet temperature

$$q_i = (hA)_i \left\{ \left( 1 - e^{-\beta} \right)^{-1} - \frac{1}{\beta} \right\} (T_n - T_i) + (hA)_i \left\{ \frac{1}{\beta} - e^{-\beta} (1 - e^{-\beta})^{-1} \right\} (T_{n-1} - T_i)$$

The simplest network satisfying these relationships is illustrated below.

(Again, cathode followers must be inserted between this network and the adjoining networks.)

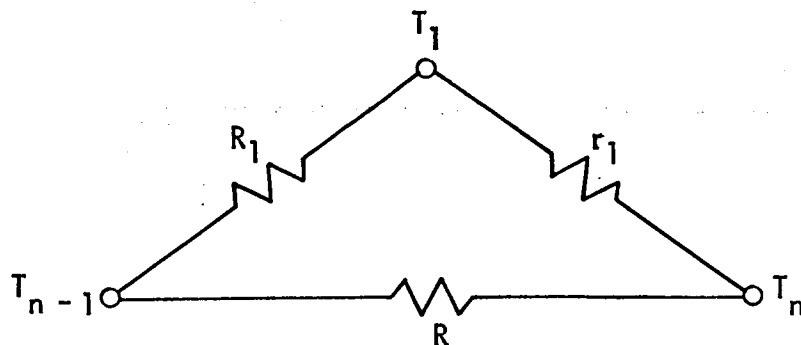


$$R_i = \frac{1}{(hA)_i \left\{ \frac{1}{\beta} - e^{-\beta} (1 - e^{-\beta})^{-1} \right\}} = \frac{f_1(\beta)}{(hA)_i}$$

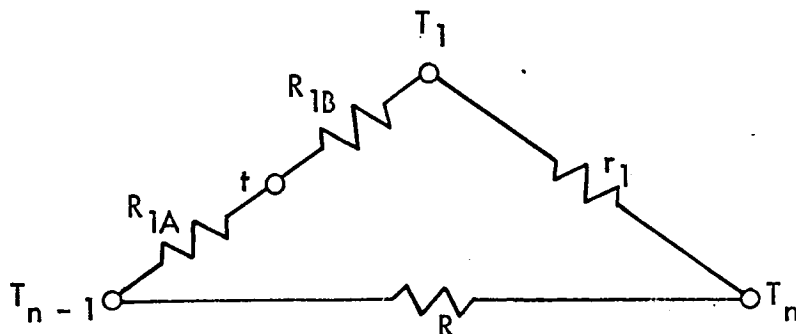
$$r_i = \frac{1}{(hA)_i \left\{ (1 - e^{-\beta})^{-1} - \frac{1}{\beta} \right\}} = \frac{f_2(\beta)}{(hA)_i}$$

$$R = \frac{1}{a \left\{ (1 - e^{-\beta})^{-1} - \frac{1}{\beta} \right\}} = \frac{f_3(\beta)}{a}$$

It is not immediately apparent that for  $N = 1$  the network above reduces to the network previously presented for a single wall temperature node, and this is therefore demonstrated here. For  $N = 1$  the circuit becomes



The resistor,  $R_1$ , will be replaced with two series connected resistors whose series resistance equals that of  $R_1$  and whose ratio is equal to  $r_1/R$  as illustrated.



$$R_{1A} + R_{1B} = R_1$$

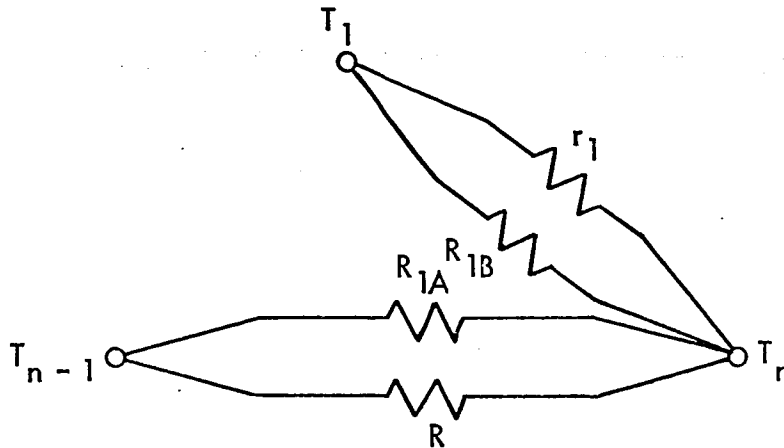
$$\frac{R_{1B}}{R_{1A}} = \frac{r_1}{R}$$

Solving for  $R_{1A}$  and  $R_{1B}$

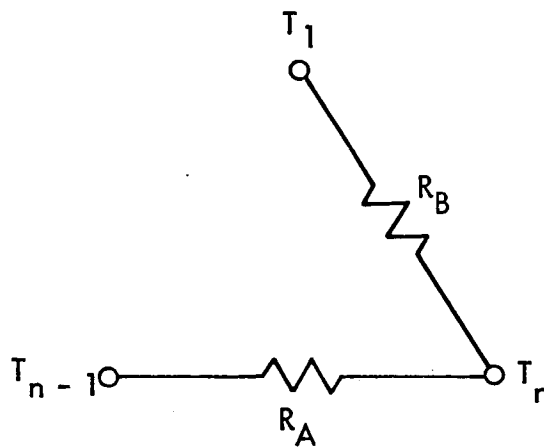
$$R_{1A} = \frac{R_1}{\frac{r_1}{R} + 1}$$

$$R_{1B} = \frac{R_1}{1 + \frac{R}{r_1}}$$

Since there is no current drawn from either node  $t$  or node  $T_n$  and since  $R_{1B}/R_{1A} = r_1/R$ , the potentials  $t$  and  $T_n$  are equal. Hence, the node points  $t$  and  $T_n$  may be connected to one another without affecting the circuit operation. Thus, the circuit becomes



The resistances  $R$  and  $R_{1A}$  may now be combined into a single resistance,  $R_A$ ; and  $r_1$  and  $R_{1B}$  may be combined into a single resistance,  $R_B$ .



$$R_A = \frac{1}{\frac{1}{R} + \frac{1}{R_{1A}}} = \frac{R R_{1A}}{R_{1A} + R}$$

$$R_B = \frac{1}{\frac{1}{r_1} + \frac{1}{R_{1B}}} = \frac{r_1 R_{1B}}{R_{1B} + r_1}$$



Substituting the expressions for  $R_1$ ,  $r_1$  and  $R_1$  yields values of  $R_A$  and  $R_B$  identical to those obtained in the one wall temperature node analysis, viz.

$$R_A = \frac{1}{W c_p}$$

$$R_B = \frac{1}{W c_p (e^\beta - 1)}$$

Since calculation of the factors  $f_1(\beta)$ ,  $f_2(\beta)$  and  $f_3(\beta)$

$$\left( \frac{1}{\left\{ \frac{1}{\beta} - e^{-\beta} (1 - e^{-\beta})^{-1} \right\}} , \frac{1}{\left\{ (1 - e^{-\beta})^{-1} - \frac{1}{\beta} \right\}} \text{ and } \frac{e^\beta - 1}{\left\{ (1 - e^{-\beta})^{-1} - \frac{1}{\beta} \right\}} \right)$$

is quite tedious, and may be inaccurate for small values of  $\beta$ , these functions are shown in Figures C-2 and C-3.

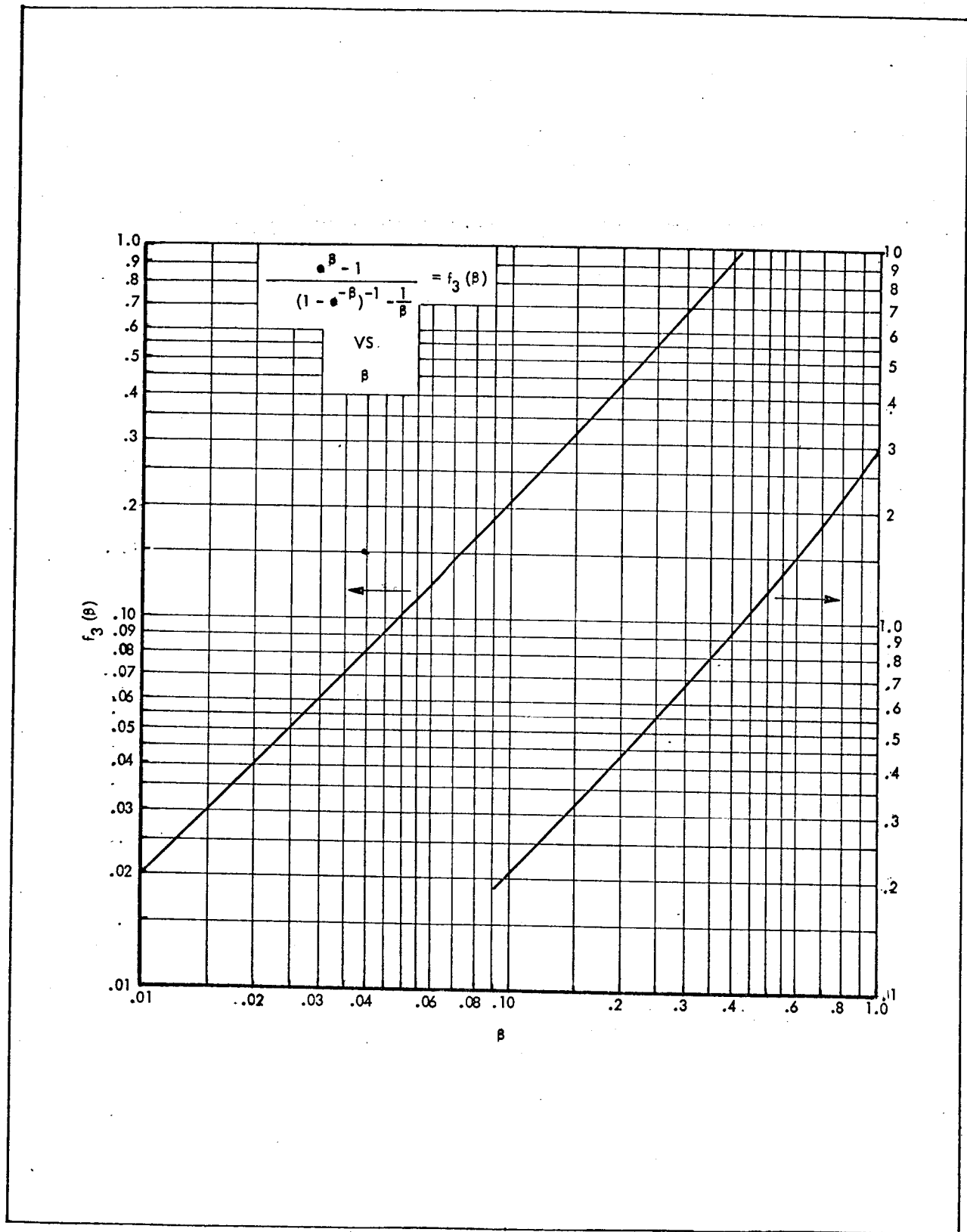


Figure C-2. Function  $f_3(\beta)$  Required for Passage Air Temperature Solution

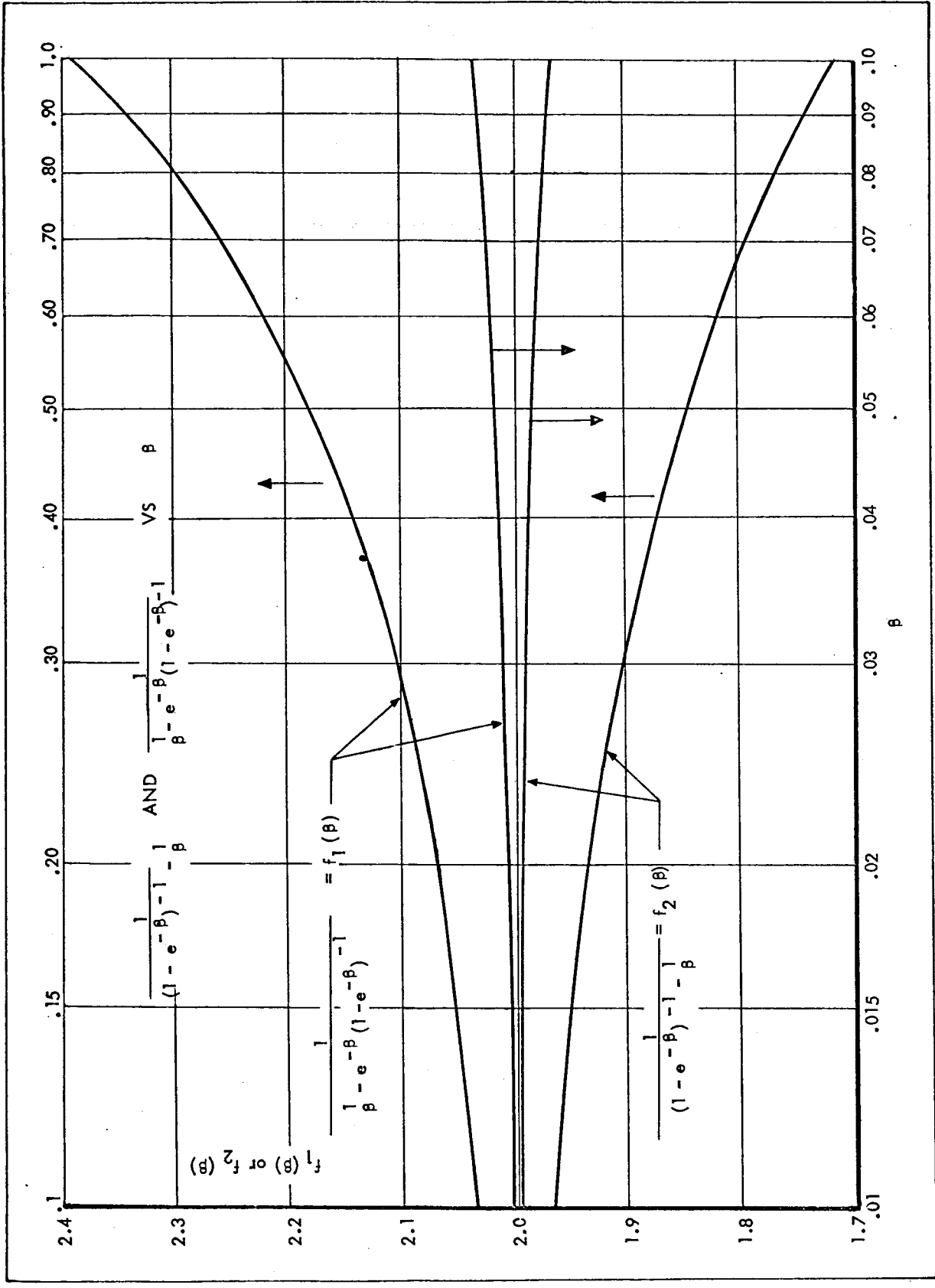


Figure C-3. Functions  $f_1(\beta)$  and  $f_2(\beta)$  Required for Passage Air Temperature Solution

## APPENDIX D

## COMPUTER OPERATION

The Thermal Analyzer Program exists in three versions: Version A for regular problems, Version B for maximum-sized problems, and Version C for fluid storage and pressurization problems. Table D-1 summarizes the capacity of the three versions of the program.

TABLE D-1  
PROGRAM CAPACITY

Version	"A" (Regular)	"B" (Maximum)	"C" (Pressurization)
Overall Data Storage	16,000	16,000	13,000
Temperatures	~ 1000	~ 1000	300
Resistors	~ 2500	~ 2500	700
Data Block	~ 3500	~ 3500	10,000
FUNCT and PRINT	~ 2700	~ 4800	1100

This appendix describes the arrangement of the program deck, computation sequence, and tape usage for Versions A and B. It also contains a brief description of the program decks and a complete listing of the basic program and subroutines. Version C, which is applicable to fluid storage and pressurization problems, is described in detail in Reference 9.

#### ARRANGEMENT OF THE DECK

The program deck is arranged as follows. The two subroutines, PRINT and FUNCT, are inserted in the program deck between the two cards:

\$IEDIT SYSIN1

and

\$ENTRY MAN6

The input data - temperatures, resistors, etc. - are inserted between the next two cards:

\$DATA

END

Figure D-1 is a representation of the deck setup.

The \$IEDIT SYSLB3 card sets up the system to read the required subroutines from a reserved program library tape: Unit A8 on the Stand-Alone 7094, and unit SYSLB3 on the 7040/7094 D.C. Provision is made for the operator to mount the required tape by a \$PAUSE card on the Stand-Along 7094, and by a \$SETUP card for the 7040/7094 D.C. The required linkage is set up as the programs are read and loaded. Figures D-2 and D-3 show the overlay linkage arrangement for Versions A and B. Both versions use the same basic program and subroutines - the only difference is the way the various subroutines or functions are combined into links. While it is possible to combine the subroutines in a variety of ways, these two versions should cover most situations that may arise. Tables D-2 and D-3 show the order of the program deck for each version. Each subroutine is represented in these tables by its initial card. Version A should be used wherever possible as Version B obtains its additional capacity at considerable expense in execution time.

Additional capacity can be obtained, if necessary, by eliminating certain of the subroutines that are not used in a particular problem. The following subroutines are referenced only by the FUNCT and/or PRINT subroutines, and if not used there, they may be eliminated for a given run.

<u>Subroutine or Function</u>	<u>Deck Name</u>
LIN	LIN6
BIV	BIV6
PAR	PAR6, ATR6*
TANKA	TNK6
RAD	RAD6
SAV	SAV6

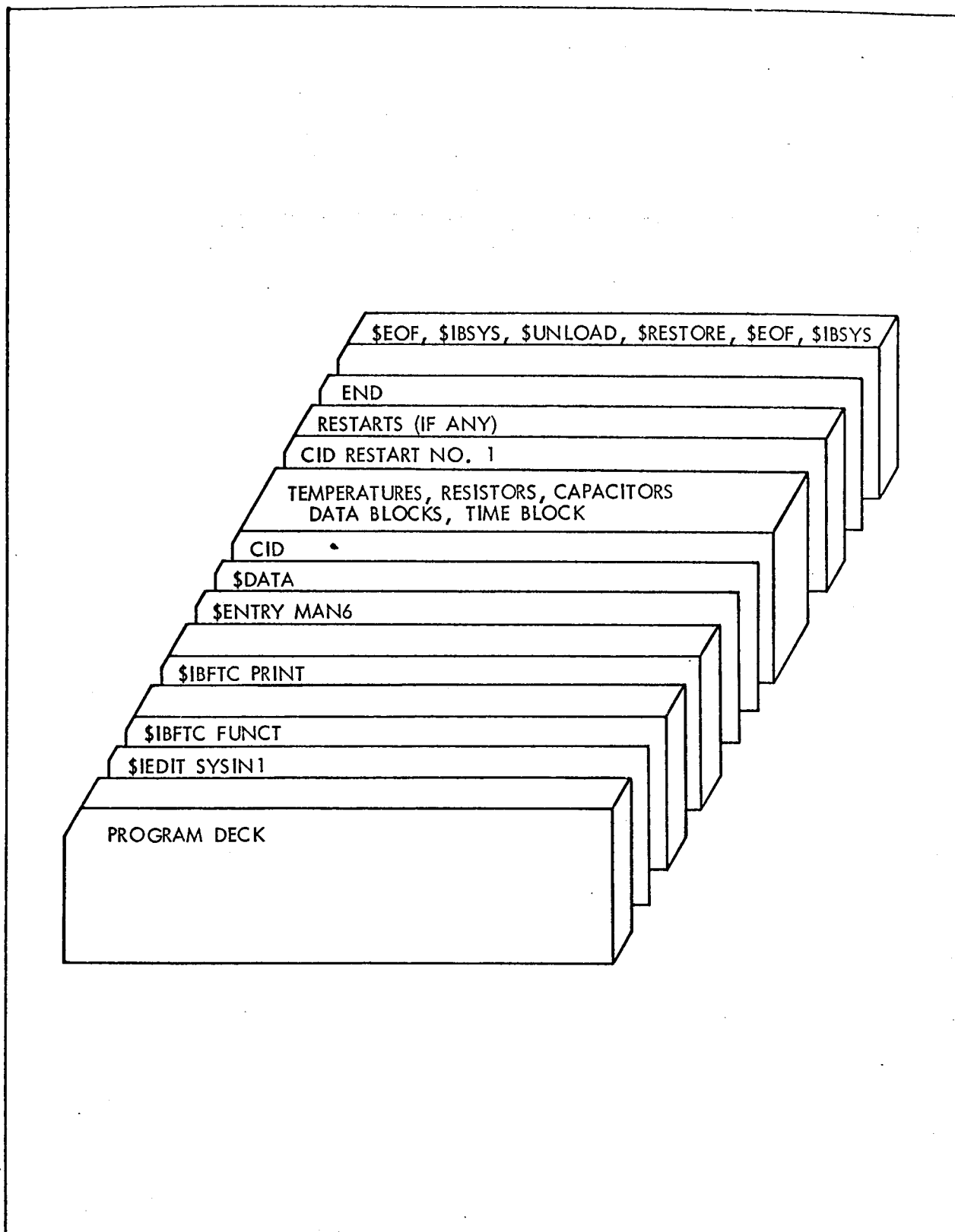


Figure D-1. Deck Setup for Thermal Analyzer Program

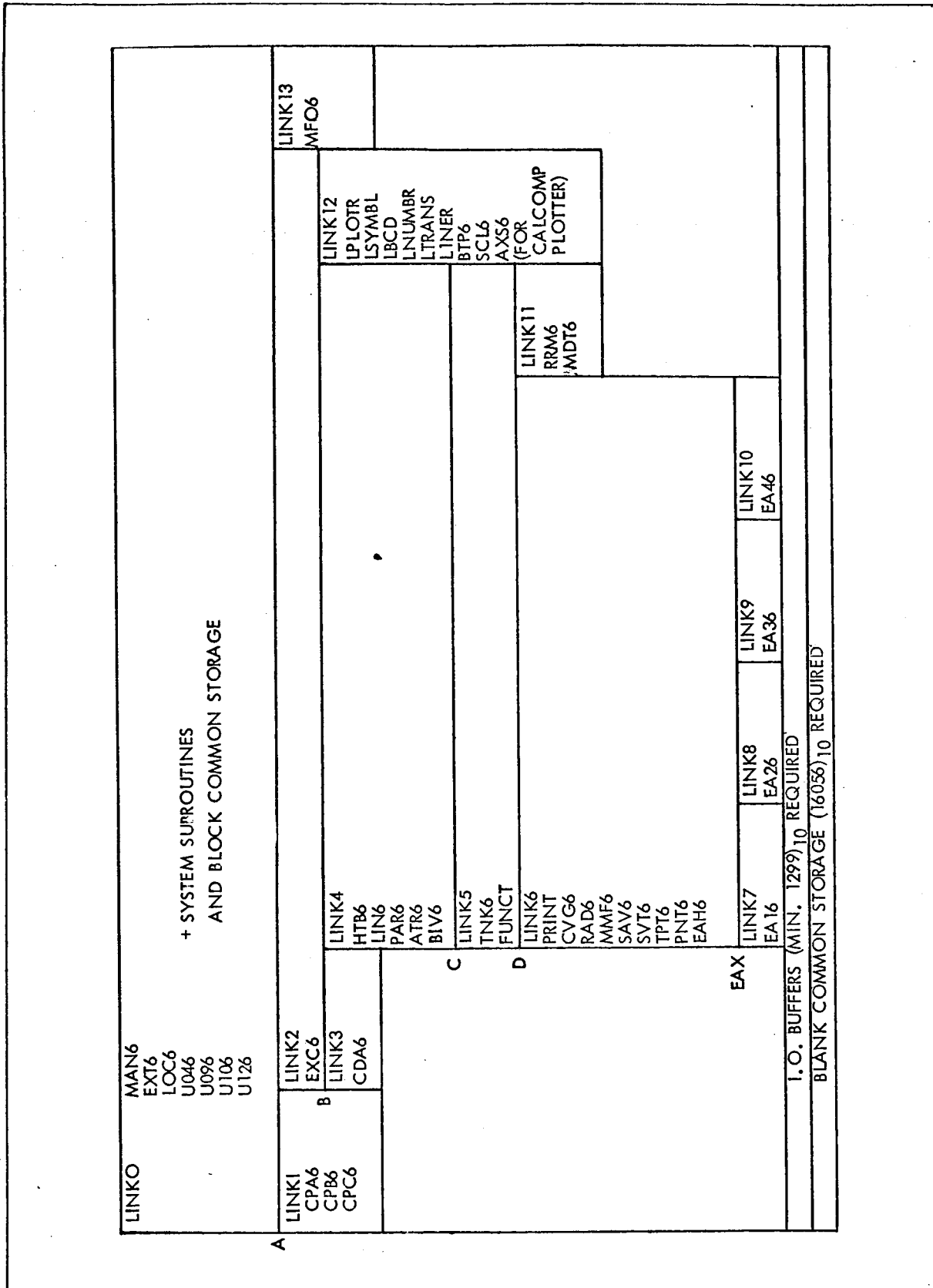


Figure D-2. Program Linkage Arrangement - Version A

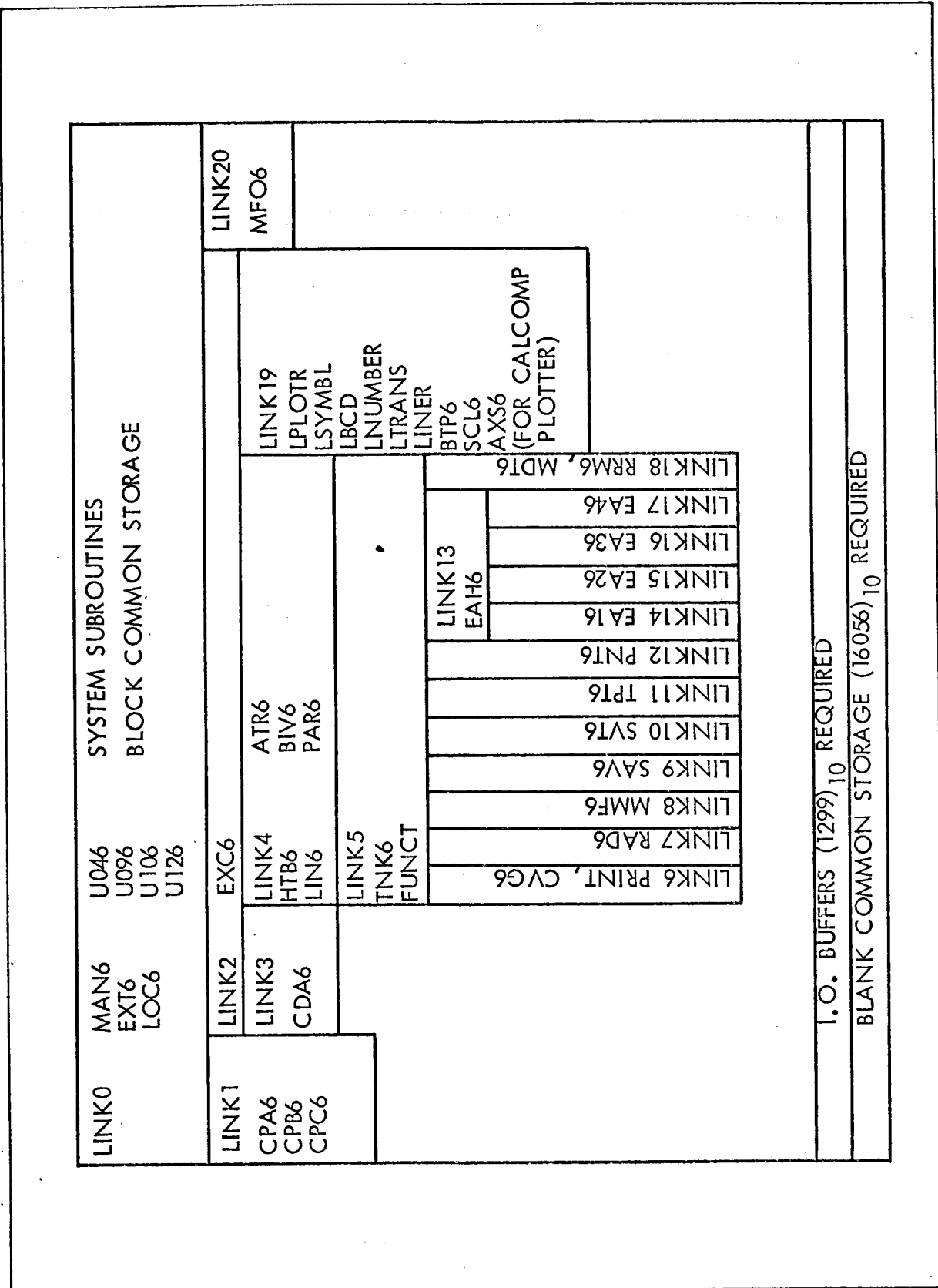


Figure D-3. Program Linkage Arrangement - Version B



TABLE D-2  
PROGRAM DECK ORDER - VERSION A

\$JOB	7,15,10000	5174833780	012266A 43233 DAVID	2266
\$ID	JOB 2266A	DAVID	THERMAL ANALYSER - FORTRAN, SHORT JOBS	0001
\$ID	7,15,10000	5174833780	012266A 43233 DAVID	2266
\$PAUSE	PLEASE MOUNT RESERVE TAPE 290 ON UNIT A8, START			
\$ATEND	0,77777			
\$SETUP	L83	T290,DISK,,,1		0003
\$ASSIGN	SYSLB3			0004
\$ASSIGN	SYSLB2			0005
\$ATTACH	B2			0006
\$AS	SYSLB2			0007
\$ATTACH	A8			
\$AS	SYSLB3			0009
\$EXECUTE	IBJOB			0010
\$IBJOB	NOMAP			
\$FILE	'UNIT16',A(2),READY,NOLIST,INOUT,HIGH,BIN,BLK=457			
\$EDIT	SYSLB3,SRCH1			0012
\$IBLDR	MAN6			0013
\$IBLDR	EXT6			0014
\$IBLDR	LOC6			0015
\$IBLDR	U046			0016
\$IBLDR	U096			0017
\$IBLDR	U106			0018
\$IBLDR	U126			0019
\$ORIGIN	A,SYSLB2			0020
\$IBLDR	CPA6			0021
\$IBLDR	CPB6			0023
\$IBLDR	CPC6			0024
\$ORIGIN	A,SYSLB2			0028
\$IBLDR	EXC6			0029
\$ORIGIN	C,SYSLB2			0030
\$IBLDR	CDA6			0031
\$ORIGIN	C,SYSLB2			0032
\$IBLDR	HTB6			0033
\$IBLDR	LIN6			0035
\$IBLDR	PAR6			0036
\$IBLDR	ATR6			0037
\$IBLDR	BIV6			
\$ORIGIN	D,SYSLB2			0039
\$IBLDR	TNK6			0040
\$INCLUDE	FUNCT			0041
\$ORIGIN	E,SYSLB2,REW			0043
\$INCLUDE	PRINT			0042
\$IBLDR	CVG6			0050
\$IBLDR	RAD6			0044
\$IBLDR	MMF6			0047
\$IBLDR	SAV6			0048
\$IBLDR	SVT6			0049
\$IBLDR	TPT6			0051
\$IBLDR	PNT6			A0051
\$IBLDR	EAH6			0057
\$ORIGIN	EAX,SYSLB2,REW			
\$IBLDR	EA16			0053
\$ORIGIN	EAX,SYSLB2,REW			
\$IBLDR	EA26			0054
\$ORIGIN	EAX,SYSLB2,REW			
\$IBLDR	EA36			0055
\$ORIGIN	EAX,SYSLB2,REW			
\$IBLDR	EA46			0056
\$ORIGIN	E,SYSLB2,REW			0052
\$IBLDR	RRM6			0045
\$IBLDR	MDT6			0046

TABLE D-2  
(CONTINUED)

\$ORIGIN	C,SYSLB2,REW	0079
\$INCLUDE	LPLOTR,LSYMBL,LBCD,LNUMBR,LTRANS,LINER	0081
\$IBLDR BTP6		0080
\$IBLDR SCL6		
\$IBLDR AXS6		
\$ORIGIN	A,SYSLB2,REW	0082
\$IBLDR MF06		0083
\$EDIT	SYSIN1	0084
C		
C	INSERT FUNCT AND PRINT ROUTINES HERE	
C		
\$DATA		
C	INSERT INPUT DATA HERE, FOLLOWED BY ANY RESTARTS	
C		
END		
\$EOF		0086
\$IBSYS		0087
\$UNLOAD	SYSLB3	
\$PAUSE	PLEASE REMOVE TAPE 290 FROM UNIT A8, SAVE IT, START	
\$RESTORE		0089
\$EOF		0090
\$IBSYS		0091



## TABLE D-3

## PROGRAM DECK ORDER - VERSION B

\$JOB	7,15,10000	5174833780	012266B 43233 DAVID	2266
\$ID	JOB 2266B	DAVID	THERMAL ANALYSER - FORTRAN, LONG JOBS	
\$ID	7,15,10000	5174833780	012266B 43233 DAVID	2266
\$PAUSE	PLEASE MOUNT RESERVE TAPE 290 ON UNIT A8, START			
\$ATEND	0,77777			
\$\$SETUP LB3	T290,DISK,,,1			0003
\$ASSIGN	SYSLB3			0004
\$ASSIGN	SYSLB2			0005
\$ATTACH	B2			0006
\$AS	SYSLB2			0007
\$ATTACH	A8			
\$AS	SYSLB3			0009
\$EXECUTE	IBJOB			0010
\$IBJOB	MAP,LOGIC			0011
\$FILE	'UNIT16',A(2),READY,NOLIST,INOUT,HIGH,BIN,BLK=457			
\$IEDIT	SYSLB3,SRCH1			0012
\$IBLDR MAN6				0013
\$IBLDR EXT6				0014
\$IBLDR LOC6				0015
\$IBLDR U046				0016
\$IBLDR U096				0017
\$IBLDR U106				0018
\$IBLDR U126				0019
\$ORIGIN	A,SYSLB2			0020
\$IBLDR CPA6				0021
\$IBLDR CPB6				0023
\$IBLDR CPC6				0024
\$ORIGIN	A,SYSLB2			0028
\$IBLDR EXC6				0029
\$ORIGIN	C,SYSLB2			0030
\$IBLDR CDA6				0031
\$ORIGIN	C,SYSLB2			0032
\$IBLDR HTB6				0033
\$IBLDR LIN6				0035
\$IBLDR PAR6				0036
\$IBLDR ATR6				0037
\$IBLDR BIV6				
\$ORIGIN	D,SYSLB2			0039
\$IBLDR TNK6				0040
\$INCLUDE	FUNCT			0041
\$ORIGIN	E,SYSLB2,REW			0043
\$INCLUDE	PRINT			0042
\$IBLDR CVG6				0050
\$ORIGIN	E,SYSLB2,REW			
\$IBLDR RAD6				0044
\$ORIGIN	E,SYSLB2,REW			
\$IBLDR MMF6				0047
\$ORIGIN	E,SYSLB2,REW			
\$IBLDR SAV6				0048
\$ORIGIN	E,SYSLB2,REW			
\$IBLDR SVT6				0049
\$ORIGIN	E,SYSLB2,REW			
\$IBLDR TPT6				0051
\$ORIGIN	E,SYSLB2,REW			
\$IBLDR PNT6				A0051
\$ORIGIN	E,SYSLB2,REW			
\$IBLDR EAH6				0057
\$ORIGIN	EAX,SYSLB2,REW			
\$IBLDR EA16				0053
\$ORIGIN	EAX,SYSLB2,REW			
\$IBLDR EA26				0054

TABLE D-3  
(CONTINUED)

\$ORIGIN	EAX,SYSLB2,REW	
\$IBLDR EA36		0055
\$ORIGIN	EAX,SYSLB2,REW	
\$IBLDR EA46		0056
\$ORIGIN	E,SYSLB2,REW	0052
\$IBLDR RRM6		0045
\$IBLDR MDT6		0046
\$ORIGIN	C,SYSLB2,REW	0079
\$INCLUDE	LPLOTR,LSYMBL,LBCD,LNUMBR,LTRANS,LINER	0081
\$IBLDR BTP6		0080
\$IBLDR SCL6		
\$IBLDR AXS6		
\$ORIGIN	A,SYSLB2,REW	0082
\$IBLDR MFO6		0083
\$IEDIT	SYSIN1	0084
C		
C	INSERT FUNCT AND PRINT ROUTINES HERE	
C		
\$DATA		
C	INSERT INPUT DATA HERE, FOLLOWED BY ANY RESTARTS	
C		
END		
\$EOF		0086
\$IBSYS		0087
\$UNLOAD	SYSLB3	
\$PAUSE	PLEASE REMOVE TAPE 290 FROM UNIT A8, SAVE IT, START	
\$RESTORE		0089
\$EOF		0090
\$IBSYS		0091

<u>Subroutine or Function</u>	<u>Deck Name</u>
PUNCHT	PNT6
EAH1	EA16
EAH2	EA26
EAH3	EA36
EAH4	EA46
RRM	RRM6, MDT6*
CVG	CVG6***

\*Where two subroutines are listed, the second is called if and only if the first is called

\*\*EAH is called if and only if any one of EAH1, EAH2, EAH3, or EAH4 is called.

\*\*\*CVG6 (CALL CVG) executes a PRINT, and must therefore be in the same link or a link dependent from PRINT.

To remove a given subroutine it is necessary simply to remove the \$IBLDR SUBR. card from the deck, and to remove the \$ORIGIN card just ahead of it if and only if the \$IBLDR card removed was the only one in that link. That is, two \$ORIGIN cards must not appear together.

#### COMPUTATION SEQUENCE

The \$IEDIT SYSIN1 card transfers loading to the standard input tape, and subroutines FUNCT and PRINT are read from it. The system then loads Link 0 into core and transfers control to it. Link 1, the compile phase link, is entered to read and compile the data in the following order:

1. Initial temperatures
2. NBK card
3. Initial resistors and connections
4. NBK card
5. Initial capacitors
6. NBK card
7. Data Blocks

8. NBK card
9. Print Interval, Final Time, Initial Time
10. NBK card

Two passes through the data are made. The first determines the kind of data and the number of items on a card. All cards are read, printed, and stored on tape 4. The second pass converts the data from BCD to the required (floating-point or integer) binary and stores it on the compiled data tape, tape 3.

The execution phase is then loaded, the compiled data is read from tape 3 into core, and control passes to subroutine HTBAL (deck name HTB6) which is the controlling subroutine during execution of the time-history. HTBAL calls the FUNCT subroutine, which in turn calls any subroutines there needed. On the return from FUNCT, HTBAL executes a heat balance for each node listed in the capacitor block, according to one of the two following formulas:

$$T_{k,\theta + \Delta\theta} = \frac{\Delta\theta}{C_k} \left( \sum_j \frac{T_{j,\theta}}{R_j} - T_{k,\theta} \sum_j \frac{1}{R_j} + q_k \right) + T_{k,\theta}$$

where

- $T_{k,\theta + \Delta\theta}$  = The temperature of node k at time  $\theta + \Delta\theta$
- $T_{k,\theta}$  = The temperature of node k at time  $\theta$ .
- $T_{j,\theta}$  = The temperature of node j at time  $\theta$ .
- $R_j$  = The value of resistor j, connecting nodes j and k.
- $\sum_j$  = Sum including all nodes connected to node k by a resistor.
- $C_k$  = The value of the capacitor at node k.
- $q_k$  = The value of the arbitrary heat input to node k.

If the value of the capacitor,  $C_k$ , is zero,

$$T_{k, \theta + \Delta\theta} = \frac{\sum_j \frac{T_{j, \theta}}{R_j} + q_k}{\sum_j \frac{1}{R_j}}$$

At the same time, the R-C product of each node having a non-zero capacitor is computed

$$(RC)_k = C_k / \sum_j \frac{1}{R_j}$$

The smallest RC product in the network or the printing interval, whichever is smaller, become the "minimum R-C product," and the time step for the following cycle,  $\Delta\theta$ , is some fraction (normally, 0.25) of this  $(RC)_{\min}$ .

At this point, the program calls those subroutines requiring both "old" and "new" temperatures: Convergence (CVG), Minimum and Maximum Temperatures (MMF), and Save Current Data (SAV). These routines are used only if they have been called for in the FUNCT routine.

All temperatures in the  $T_{\theta + \Delta\theta}$  (new) temperature block are then moved into the  $T_{\theta}$  (old) temperature block, thus destroying the old temperatures and making the two blocks identical. Note that this operation specifically includes temperatures not mentioned in the capacitor block, so-called "fixed temperatures." To change the value of a "fixed temperature," it is necessary to change the value on the  $T_{\theta + \Delta\theta}$  (new) block. If the old value is changed, that value will be used for that cycle only in the heat balance (as one of  $T_{j, \theta}$ ) and then will be destroyed by the original value left unchanged in the  $T_{\theta + \Delta\theta}$  (new) block.  $T_{j, \theta + \Delta\theta}$  is stored in  $P(i)$ , and  $T_{j, \theta}$  is stored in  $(P(\max T + i))$ . That is, the new temperature block comes first in the P data storage region.

The program then calls the PRINT routine and computes the next time to print if it has reached print time. It then computes the current time for the next cycle, calls the plot routine if plotting has been called for, and then returns control to the Function routine for the next cycle. When, in computing the current time for the next cycle, the current time is greater than the final time (specified in the time block),  $\Delta\theta$  is chosen so that the current time is equal to the final time for the next cycle, and at the end of the next cycle, control is returned to the executive program in link 0. From there, if plotting has been called for (CALL TPLOT) the plotting routines are called in and executed. Then, if maximum and minimum temperature monitoring has been called for (CALL MMF), the max-min output routine (MFOUT) is called in and executed.

Thereafter, control passes back to the compilation phase, and any restarts are compiled. A restart consists of only one block of input data, followed by an NBK card. However any value that was compiled in the initial case may be changed. There are five flags, each one telling the program that the items following it are to be changed in the initial case. Flag 1 indicates that the cards following are temperature cards. Similarly, resistor and capacitor values are changed by cards following Flags 2 and 3, respectively. Flag 4 indicates a new time block, which must be changed in its entirety. Flag 5 is used to indicate changes to the data block. Note that each sub-block of data (a curve or table) must be changed in its entirety, the restart containing all identifications, values, and if in the original curve, the period. When a data block is changed, the new values are stored starting at the beginning of that data block. Care must be taken not to exceed the storage allotted to that data block in the initial case. If that allotment is exceeded, the remainder will be stored in the next following data block or blocks, thus destroying some information. Each restart may include any or all of the above changes, and each must end with an NBK card. There is no theoretical limit to the number of restarts for a given run, but practical considerations, such as the size of deck, the machine time used, etc., will limit the number.

Following all of the restarts, the last card read by the program should be the "END" card. This card signals the program to exit and avoids an "End of file reading..." diagnostic. It also enables the program to complete plotting and minimum-maximum output before exiting.



The cards following the "end" card are system instructions to restore the system tapes used and allow removal of reserved and special output tapes, as required. Figure D-4 is a simplified flow diagram of the program. It applies to both Versions A and B. Table D-4 is a complete listing of the basic program and subroutines.

#### DESCRIPTION OF PROGRAM DECKS

A brief description of the function and operation of each of the program decks follows. The subroutines called for in the FUNCT and PRINT routines are discussed in more detail in Section IV.

MAN6	Initiates program and exits to system.
EXT6	Controls the program flow between compile, execution, and post-processing phases; contains block-common storage for information that must not be destroyed between phases.
U046	Defines tape unit 4 as BCD
U096	Defines tape unit 9 as BCD
U106	Defines tape unit 10 as BCD
U126	Defines tapeunit 12 as BCD
LOC6	Locates the beginning point of a data block. Let $L = LOC(N)$ , where $N$ is a data block designation number, then $P(L+1)$ is the first point in the data block.
CPA6	Performs first-pass compilation of input data and stores it on unit 4.
CPB6	Performs second-pass compilation of input data, reading unit 4 and writing unit 3.
CPC6	Performs compilation and posting of changes specified in restart blocks, writes revised data on unit 3.
EXC6	Initiates execution phase; contains block common storage for those items that may not be destroyed during the execution phase.
CDA6	Reads compiled data from unit 3 into core storage.
HTB6	Controls execution of the time history of the required problem; performs the basic heat balance on each node; updates



the temperature blocks each cycle; controls the time variables and selects printing cycles.

- FUNCT** Controls the execution of each cycle except for heat balance and time calculations. Calls such routines as it needs to perform the required operations; performs user's miscellaneous calculations and circuit value changes.
- PRINT** Writes the required output on the system output tape according to the format(s) specified.
- LIN6** Performs linear interpolation for the independent variable and data block specified as  $Y = \text{LIN}(X,N)$
- BIV6** Performs bivariate linear interpolation for the independent variables and the data block specified as  $Y = \text{BIV}(X1,X2,N)$  where  $X1$  is the vertical independent variable, and  $X2$  is the horizontal independent variable.
- PAR6** Performs parabolic interpolation for the independent variable and the data block specified as  $Y = \text{PAR}(X,N)$ . Data block  $N$  must have an odd number of point pairs.
- ATR6** Called by **PAR6** to assist in parabolic interpolation.
- TNK6** Initiates pressurization program, and stores data block numbers for use in pressurization. CALL TANK A (K) results in a diagnostic in versions A and B.
- CVG6** Iterates through the whole program, but holds time constant until the temperatures have achieved steady state. CALL CVG (A,N,M), where  $A$  is the greatest allowable temperature difference between cycles,  $N$  is the upper limit on the number of cycles to be used,  $M$  is a print flag signaling to print every  $M$  cycle. If  $M$  is negative, all capacitors are treated as if zero valued.
- RAD6** Calculates the value of a radiation resistor. The function specification  $R(A) = \text{RAD}(B,C,K_{\text{rad}})$  will cause resistor  $A$  to be computed according to the equation

$$R(A) = 1. / \left\{ .1713 * 10^{-8} K_{\text{rad}} \left[ (T_B + 460)^2 + (T_C + 460)^2 \right] \right. \\ \left. \left[ T_B + T_C + 920 \right] \right\}$$

- MMF6** Finds local maxima and minima for the temperatures listed in data block  $N$ . CALL MMF ( $\theta_i, \theta_f, N, S$ ), where  $\theta_i$  and  $\theta_f$  give

the time range desired, N is the data block containing the temperature numbers, and S means perform this test every Sth cycle.

- SAV6 Initiates a call from HTB6 to SVT6 when the first argument, A, is greater than or equal to the second, B. CALL SAV (A,B).
- SVT6 Writes the current condition of the data onto tape 3, the compiled data tape. This allows a restart to continue from the point at which the previous case stopped, or to rerun a portion of case with new parameters.
- TPT6 Writes time and the values of the temperatures listed in data block N onto tape 11 to be post-processed by BTP6 for the plotter. CALL TPLOT (N).
- PNT6 Punches cards giving the temperature numbers and values suitable for use as an initial temperature block. CALL PUNCHT ( $\theta$ ,A,B) where  $\theta$  is the time at which temperatures are to be punched, and A and B are the smallest and highest temperature numbers punched. If A = B = 0 all temperatures will be punched.
- EA16 Sets up a call to EAH6 with two arguments, node number j and constant K, i.e., CALL EAH1(j,K)
- EA26 Sets up a call to EAH6 with three arguments, H to be stored CALL EAH2(j,K,H)
- EA36 Sets up a call to EAH6 with four arguments, adding  $\alpha_o$  and surface flag to EAH1 arguments in place of H. CALL EAH3(j,K, $\alpha_o$ ,F)
- EA46 Sets up a call to EAH6 with five arguments, adding the location for storing H. CALL EAH4(j,K,H, $\alpha_o$ ,F)
- EAH6 Computes the aerodynamic heating to node j, given K,  $\alpha_o$ , and a flag telling whether the node is upper or lower surface. Eckert's aerodynamic heating equation is used. EAH6 is called from EA16, EA26, EA36, or EA46.
- RRM6 Computes radiation resistors by the same formula as RAD6, except that  $K_{rad}$  is computed from a radiation matrix given in data block N, and is dependent on all the temperatures in the matrix network. MDT6 is called from RRM6.  $R(A) = RRM(B,C,N)$  where B and C are the nodes directly connected to resistor A, and N is the data block number.
- MDT6 Matrix inversion routine used by RRM6. Maximum matrix size is 15 x 15.

BTP6 Plot post-processor routine reads the information stored by TPT6, sorts it and, for the Calcomp plotter, writes it on a tape for off-line processing. For the S-C 2040 plotter, it displays directly on the CRT.

AXS6 Routine for drawing axes for the Calcomp plotter, called by BTP6.

SCI6 Routine for selecting scales and scaling information for the Calcomp plotter called by BTP6.

MFO6 Minimum-maximum temperature post-processor reads information stored on tape by MMF6, sorts it and prints it.

#### TAPE USAGE

The following list gives the tapes used during compilation and execution of a program, depending in some cases on the requests made in the FUNCT subroutine.

#### COMPILE PHASE TAPE USAGE

<u>Tape No.</u>	<u>Use</u>
2	Contains program overlay links .
3	Store compiled data
4	Store semi-compiled data
5	System standard input
6	System standard output
8	Not used
9	Used by pressurization program
10	Used by pressurization program
11	Not used
12	Materials Library tape (Reserved)
16	Not used

## EXECUTION PHASE TAPE USAGE

<u>Tape No.</u>	<u>Use</u>
2	Contains program overlay links.
3	Read compiled data. Rewrite if SAV is called.
4	Not used
5	Not used
6	System Standard Output
8	Specified temperatures for off-line use, Reserve.
9	Min-max intermediate output.
10	Min-max intermediate output.
11	Plot intermediate output
12	Not used
16	Plot output (Calcomp Plotter)

NOTES ON COMPUTER OPERATION

Some general observations regarding computer operation, and some difficulties which frequently arise are discussed in the following paragraphs.

1. When running on the IBM 7094 Stand Alone machine, difficulty has been encountered due to dirty tape heads. In particular, the overlay tape (B-3) is used so heavily on the largest jobs, that within a couple of hours a tape read check is almost certain to occur. This happens when the overlay communication region is trying to reach the next link, which is still on tape, but cannot due to the dirty tape head. Overlay communication remains in a two-instruction loop until operator action intervenes.
2. Versions A and B have a built-in indicator using sense lights to indicate the degree of completion of the time history. The sense lights are used as binary indicators showing 16ths of the time history completed. This enables the operator to determine that the job appears to be progressing properly.
3. On the 7040/7094 D.C. it has been found that not more than one tape may be set up to be deblocked from disk to tape. Therefore, if more than one tape is to be processed off-line or by a later job, all but one such tape must be assigned to a physical tape.

4. Backspacing a simulated (disk) tape is a complicated and time-consuming operation. Therefore, after each link is loaded, the thermal analyzer calls for a rewind of the overlay tape. It might prove more efficient to make the overlay tape physically a tape, but this has not been tested.



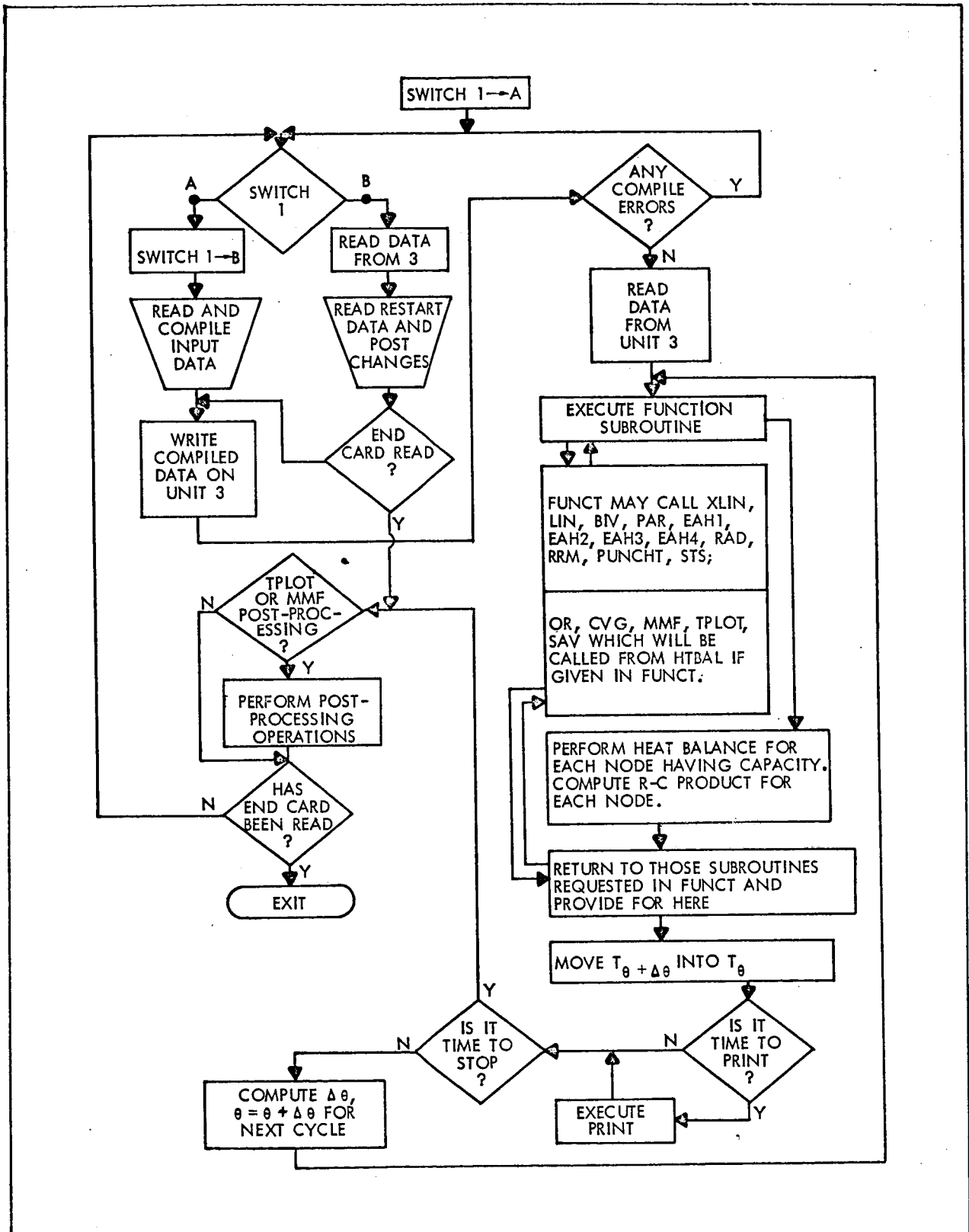


Figure D-4. Simplified Flow Diagram of Computer Program

## TABLE D-4. PROGRAM LISTING

SIBFTC MAN6	MAN6000
C AS OF 12/4/64	MAN6001
NLAG = 1	MAN6002
CALL EXETIV (NLAG)	MAN6003
CALL EXIT	MAN6004
STOP	MAN6005
END	MAN6006

SIBFTC EXT6	EXT6000
SUBROUTINE EXETIV (NLAG)	EXT6001
C AS OF 5/25/65	EXT6002
COMMON P(16000),M(16),MAXT,MAXR,MAXC,KSP,KST,KURV7,NCVG,NSTS,NFAB	EXT6003
COMMON NABL(10),NKSP,LMMF,NRMF,NREAD,CC(12)	EXT6004
COMMON NR,MAXP,MAXK,MAXS,MAXM	EXT6005
COMMON /CP2/ ERROR,MAXMUM	EXT6006
COMMON /CPITM/ ITIMO	EXT6007
COMMON /CPPLT/NPLT,NEND,KSKIP	EXT6020
COMMON /EXFLG/NTFLG,NSAV,NFLG	EXT6021
COMMON /EXPLT/ NLFLG	EXT6022
MAXMUM=16000	EXT6025
ITIMO = 1	EXT6026
NEND=0	EXT6027
NPLT=1	EXT6028
ERROR=0.	EXT6029
NTYPE=0	EXT6030
NTFLG=0	EXT6031
IR=1	EXT6032
8 CALL COMPIL(IR)	EXT6033
IF (ERROR.EQ.0..AND.NEND.EQ.0) CALL EXCUT(NLAG)	EXT6035
IF (ERROR.NE.0.) WRITE (6,100)	EXT6036
100 FORMAT(44HOERROR HAS OCCURRED SOMEWHERE IN ABOVE CASE.)	EXT6037
IF (LMMF.GT.2) CALL MFOUT	EXT6038
IF (NPLT.GT.1) NBIT=1	EXT6039
IF (NBIT.GT.0) CALL BITAP	EXT6040
IF (NEND.GT.0) RETURN	EXT6041
IR=2	EXT6042
GO TO 8	EXT6043
END	EXT6045



TABLE D-4. (Continued)

SIBFTC LOC6		
	FUNCTION LOC (KT)	LOC6000
C	AS OF 04/27/65	LOC6001
C		LOC6002
C	LOC ROUTINE FINDS FIRST LOCATION AHEAD OF LOCATION STARTING TABLE	LOC6003
C		KTLOC6004
	COMMON P, M, MAXT, MAXR, MAXC, KSP, KST	LOC6005
	COMMON /EXADR/ LCTN,LCTO,LCR,LCC,LQG,LCRC,LCPS,LCK,LCKA	LOC6006
	COMMON /CP2/ ERROR	LOC6007
	DIMENSION P(16000), M(16), NSTRT(1)	LOC6008
	EQUIVALENCE (P(1), NSTRT(1))	LOC6009
	REAL M	LOC6010
	IF (KT.LF.0) GO TO 13	LOC6011
10	J=LCKA	LOC6012
11	J1=NSTRT(J)/2**18	LOC6013
	J2=MOD(NSTRT(J),2**18)	LOC6014
	IF (J1.EQ.KT) GO TO 12	LOC6015
	IF (J1.EQ.0) GO TO 13	LOC6016
	J=J+1	LOC6017
	GO TO 11	LOC6018
12	IF (P(J2).NE.32767.) J2=J2-1	LOC6019
	LOC=J2	LOC6020
	RETURN	LOC6021
13	WRITE (6,21) KT	LOC6022
21	FORMAT (10HOCURVE NO.15,25H IS NOT IN ADDRESS TABLE.)	LOC6023
	ERROR =1.	LOC6024
	RETURN	LOC6025
	END	LOC6026
		LOC6027
SIRMAP	U046	
	ENTRY	.UN04.
.UN04.	PZF	UNIT04
UNIT04	FILE	,UT4,READY,INOUT,BLK=22,BCD,NOLIST
	END	
		U046
		U 46
		U 46
		U 46
		U 46
SIRMAP	U096	
	ENTRY	.UN09.
.UN09.	PZE	UNIT09
UNIT09	FILE	,B(3),READY,INOUT,BLK=22,BCD,NOLIST
	END	
		U096
		U 96
		U 96
		U 96
		U 96
SIRMAP	U106	
	ENTRY	.UN10.
.UN10.	PZF	UNIT10
UNIT10	FILE	,A(3),READY,INOUT,BLK=22,BCD,NOLIST
	END	
		U106
		U 06
		U 06
		U 06
		U 06
SIRMAP	U126	
	ENTRY	.UN12.
.UN12.	PZE	UNIT12
UNIT12	FILE	,B(2),READY,INPUT,BLK=22,BCD,NOLIST
	END	
		U126
		U 26
		U 26
		U 26
		U 26

TABLE D-4. (Continued)

	SIBFTC CPA6	CPA6000
	SUBROUTINE COMPIL (IR)	CPA6001
C	AS OF 04/27/65	CPA6002
C	8/21/64	CPA6003
	CHANGED TO INCLUDE MINMAX	CPA6004
	COMMON P, M, MAXT, MAXR, MAXC, KSP, KST, KURV 7, NCVG, NSTS, NFAB	CPA6005
	COMMON NABL,NKSP,LMMF,NRMF,NREAD,CC	CPA6006
	COMMON NRECD, NRPD, NWCT, NWST, NWTM	CPA6007
	COMMON /CP2/ERROR,MAXMUM	CPA6008
	COMMON /CPPLT/ NPLT,NEND	CPA6009
	COMMON /EXPLT/ NLFLG	CPA6010
	DIMENSION CZ(6),CY(6)	CPA6011
	DIMENSION A(12), I 1(12), I 2(12), I 3(12), NABL(10), CC(12)	CPA6012
	DIMENSION P(16000), IRLINE(1), KPSD(1), NSTRT(1), M(16), KDAT(1)	CPA6013
	EQUIVALENCE (P(4000), IRLINE(1)), (P(8000), KPSD(1)), (P(13000),	CPA6014
	I NSTRT(1)), (P(1), KDAT(1))	CPA6015
	REAL M, INC, NBK,NET	CPA6016
	INTEGER CP	CPA6017
	DATA ENDF/6H -1 /	CPA6018
	DATA NET/6HNET /	CPA6019
	DATA DEC/6HDEC /	CPA6020
	DATA INC/6HINC /	CPA6021
	DATA PER/6HPER /	CPA6022
	DATA NBK/6HNRK /	CPA6023
	DATA CID/6HCID /	CPA6024
	DATA TAP/6HTAP /	CPA6025
	DATA RES/6HRES /	CPA6026
	DATA CAP/6HCAP /	CPA6027
	DATA COD/6HCOD /	CPA6028
	DATA ZERO/6H000000/	CPA6029
	DATA (CZ(I),I=1,6)/2H01,2H02,2H03,2H04,2H05,2H06/,BLANK/1H /	CPA6030
	DATA (CY(I),I=1,6)/2H 1,2H 2,2H 3,2H 4,2H 5,2H 6/,ZERZ/2H00/	CPA6031
	DATA ZERY/2H 0/	CPA6039
209	FORMAT (A3,A2,12A6)	CPA6040
210	FORMAT (5X,12A6)	CPA6041
211	FORMAT (5X, A3,I2,12A6)	CPA6042
212	FORMAT (1H1,9X,12A6)	CPA6043
215	FORMAT (40H0 KOUNT IS NOT CORRECT IN COMPIL ROUTINE )	CPA6044
218	FORMAT (I 3, 3X, I 2)	CPA6046
223	FORMAT (7HOCODE= A6,12H IS ILLEGAL.)	CPA6050
224	FORMAT (25HOCANNOT FIND CURVE NAMED A6,17H ON LIBRARY TAPE.)	CPA6051
232	FORMAT (53HOCODE= NET IS ILLEGAL IN THIS VERSION. USE VERSION C.)	CPA6053
233	FORMAT (5H ** ,A3,A2,12A6,23H ** THIS CARD IGNORED.)	CPA6054
	NCVG = 1	CPA6055
	NSTS = 1	CPA6056
	MATLIB =1	CPA6057
	NSW2=1	CPA6058
	NPLT=1	CPA6059
	NLFLG=1	CPA6061
	NFAB = 1	CPA6062
	NSW2=1	CPA6063
	LINE = 1	CPA6064
	LMMF=1	CPA6065
	NRMF=0	CPA6066
	NREAD=0	CPA6067
	DO 101 I = 1, 10	CPA6068
	NABL(I) = 0	CPA6069
101	CONTINUE	CPA6070
	GO TO (105, 149, 149), IR	CPA6071
105	REWIND 4	CPA6072
	DO 107 I = 1, MAXMUM	CPA6073
	P(I) = 0.	

TABLE D-4. (Continued)

107	CONTINUE	CPA6074
	KOUNT = 1	CPA6075
110	CP=-1	CPA6076
	IF (MATLIB.EQ.1) READ (5,209) CM,CX,(A(I),I=1,12)	CPA6079
	IF (MATLIB.EQ.2) READ (12,209) CM,CX,(A(I),I=1,12)	CPA6080
1101	DO 1102 I=1,6	CPA6081
1102	IF (CX.EQ.CY(I).OR.CX.EQ.CZ(I)) CP=1	CPA6082
	IF (CX.EQ.BLANK.OR.CX.EQ.ZERZ.OR.CX.EQ.ZERY) CP=0	CPA6083
	IF (CP.GF.0) GO TO 1103	CPA6084
	CP=0	CPA6085
	ERROR=1.	CPA6086
	WRITE (6,215)	CPA6087
1103	IF (LINE.LT.60) GO TO 111	CPA6088
109	WRITE (6,212) (CC(I),I=1,12)	CPA6089
	LINE = 1	CPA6090
111	IF (CM.EQ.CID) GO TO 117	CPA6091
	IF (CM.EQ.TAP) GO TO 150	CPA6092
	WRITE (6,211) CM,CP,(A(I),I=1,12)	CPA6093
	LINE=LINE+1	CPA6094
	IF (CM .EQ. DEC) GO TO 116	CPA6095
	IF (CM .EQ. INC) GO TO 118	CPA6096
	IF (CM .EQ. PER) GO TO 119	CPA6097
	IF (CM .EQ. NBK) GO TO 120	CPA6098
	IF (CM.EQ.RES) GO TO 123	CPA6099
	IF (CM.EQ.CAP) GO TO 124	CPA6100
	IF (CM.EQ.NET) GO TO 170	CPA6101
	IF (CM.EQ.COD) GO TO 112	CPA6102
115	WRITE (6,223) CM	CPA6103
	ERROR=1.	CPA6104
	GO TO 110	CPA6105
112	KOD = 9	CPA6106
	GO TO 125	CPA6107
116	KOD = 1	CPA6108
	GO TO 125	CPA6109
117	CMID=CM	CPA6110
	ICP=CP	CPA6111
	DO 1171 I=1,12	CPA6112
	CC(I)=A(I)	CPA6113
1171	CONTINUE	CPA6114
	LINE =1	CPA6115
	WRITE (6,212) (CC(I),I=1,12)	CPA6116
	GO TO 110	CPA6117
118	KOD = 3	CPA6118
	GO TO 125	CPA6119
119	KOD = 4	CPA6120
	GO TO 125	CPA6121
120	KOD = 5	CPA6122
	KOUNT = KOUNT + 1	CPA6123
	IF (KOUNT - 6) 125, 171, 122	CPA6124
121	KOD = 6	CPA6125
	GO TO 125	CPA6126
122	WRITE (6, 215)	CPA6127
	ERROR =2.	CPA6128
	RETURN	CPA6129
123	KOD=7	CPA6130
	GO TO 125	CPA6131
124	KOD=8	CPA6132
	GO TO 125	CPA6133
150	IF (MATLIB.EQ.2) GO TO 160	CPA6134
	MATLIB=2	CPA6135
	FIRST=0.	CPA6136

TABLE D-4. (Continued)

	WRITE (6,211) CM,CP,(A(I),I=1,12)	CPA6137
	LINE=LINE+1	CPA6138
151	READ ( 12 ,209) Z1,MZ2,Z3	CPA6139
	IF (Z1.NE.TAP) GO TO 151	CPA6140
	IF (Z3.EQ.A(1)) GO TO 110	CPA6141
	IF (Z3.NE.ZERO) GO TO 151	CPA6142
	REWIND 12	CPA6143
	FIRST=FIRST+1.	CPA6144
	IF (FIRST.EQ.1.) GO TO 151	CPA6145
	WRITE (6,224) A(1)	CPA6146
	ERROR=1.	CPA6147
160	MATLIB=1	CPA6148
	GO TO 110	CPA6149
170	WRITE (6,232) CM	CPA6150
	ERROR=1.	CPA6151
175	READ (5,209) CM,CX,(A(J),J=1,12)	CPA6152
	IF (CM.EQ.DEC.OR.CM.EQ.CID.OR.CM.EQ.NBK) GO TO 1101	CPA6153
	WRITE (6,233) CM,CX,(A(J),J=1,12)	CPA6154
	GO TO 175	CPA6155
125	WRITE (4,218) KOD,CP	CPA6163
	WRITE (4, 210) (A(I), I = 1, 12)	CPA6164
	IF (KOUNT - 6) 110, 130, 122	CPA6165
130	END FILE 4	CPA6166
	REWIND 4	CPA6167
	REWIND 3	CPA6168
	CALL COMP2	CPA6169
	RETURN	CPA6170
149	CALL RESTRT	CPA6171
	RETURN	CPA6172
	END	CPA6173

TABLE D-4. (Continued)

SIBFTC CPB6	CPB6000
SUBROUTINE COMP2	CPB6001
C  AS OF 06/02/65	CPB6002
COMMON P, M, MAXT, MAXR, MAXC, KSP, KST, KURV 7, NCVG, NSTS, NFAB	CPB6003
COMMON NABL,NKSP,LMMF,NRMF,NREAD,CC	CPB6004
COMMON NRECD, NRPD, NWCT, NWST, NWTM	CPB6005
COMMON /CP2/ERROR,MAXMUM	CPB6006
DIMENSION BCDR(5)	CPB6007
DIMENSION A(12), I 1(12), I 2(12), I 3(12), NABL(10), CC(12)	CPB6008
DIMENSION P(16000), IRLINE(1), KPSD(1), NSTRT(1), M(16), KDAT(1)	CPB6010
EQUIVALENCE (P(4000), IRLINE(1)), (P(8000), KPSD(1)), (P(13000),	CPB6011
1 NSTRT(1)), (P(1), KDAT(1))	CPB6012
REAL M, INC, NBK,NET	CPB6013
INTEGER CP	CPB6014
DATA (BCDB(1),I=1,5)/6HTEMP.,6HRESIS.,6HCPAC.,6HCURVE ,6HMISC. /	CPB6015
200  FORMAT (5X, 4(I 5, E 10.2))	CPB6016
201  FORMAT (5X, I 5, E 10.2, I 5)	CPB6017
202  FORMAT (5X, 2(3I 5, E 10.2))	CPB6018
203  FORMAT (5X, 3I 5, E 10.2, I 5)	CPB6019
204  FORMAT (5X, I 5)	CPB6020
205  FORMAT (5X, 6E 10.2)	CPB6021
206  FORMAT (5X,E10.2,I5)	CPB6022
218  FORMAT (I 3, 3X, I 2)	CPB6031
219  FORMAT (15HOKOD MUST NOT =15,8H IN THE A6,7H BLOCK.)	CPB6032
220  FORMAT (26HOTALB NO. = 0 IS ILLEGAL.)	CPB6033
222  FORMAT (30H0 TOO MANY WORDS IN DAT BLOCK )	CPB6034
223  FORMAT (7HOCODE= A6,12H IS ILLEGAL.)	CPB6035
224  FORMAT (25HOCANNOT FIND CURVE NAMED A6,17H ON LIBRARY TAPE.)	CPB6036
230  FORMAT (28HOSOMETHING WRONG AFTER TABLE16,17H AND BEFORE TABLE16)	CPB6037
231  FORMAT (25HOSOMETHING WRONG IN TABLE 16)	CPB6038
232  FORMAT (7HOERROR,I5,E15.5,22H NEGATIVE NODE NUMBER.)	CPB6039
233  FORMAT (7HOERROR,3I5,E15.5,26H NEGATIVE RESISTOR NUMBER.)	CPB6040
235  FORMAT (14HOCAPACITOR NO.I5,22H IS GREATER THAN MAXT=15)	CPB6041
236  FORMAT (5HONODE I5,20H HAS NO CONNECTIONS.)	CPB6042
234  FORMAT (9HORESISTORI5,15H CONNECTS NODESI5,1H,I5,27H GREATER THAN	CPB6043
IMAX TEMP.NO.=15)	CPB6044
240  FORMAT (5X,3I5,3E10.0,I5)	CPB6045
241  FORMAT (5X,3I5,3E10.0,2I5)	CPB6046
242  FORMAT (5X,I5,3E10.0,2I5)	CPB6047
243  FORMAT (5X,I5,3E10.0,3I5)	CPB6048
244  FORMAT (1H0,I6,33H DATA STORAGE EXCEEDED. TOTAL OF I6,	CPB6049
1 12H DATA ITEMS.)	CPB6050
250  FORMAT (14H1P STORAGE MAP /14H0 TEMPERATURES,9X,I6,8X,6HTOTAL I6)	CPB6051
251  FORMAT (23H  TEMPERATURES                  I6,8X,6HTOTAL I6)	CPB6052
252  FORMAT (23H  RESISTORS                      I6,8X,6HTOTAL I6)	CPB6053
253  FORMAT (23H  CAPACITORS                    I6,8X,6HTOTAL I6)	CPB6054
254  FORMAT (23H  CURRENTS (Q)                  I6,8X,6HTOTAL I6)	CPB6055
255  FORMAT (23H  R-C PRODUCTS                  I6,8X,6HTOTAL I6)	CPB6056
256  FORMAT (23H  PSEUDO-SEQUENCE              I6,8X,6HTOTAL I6)	CPB6057
257  FORMAT (23H  DATA BLOCKS (CURVES) I6,8X,6HTOTAL I6)	CPB6058
258  FORMAT (23H  DATA BLOCK ADDRESSES I6,8X,6HTOTAL I6)	CPB6059
NSW2=1	CPB6060
NGRC=1	CPB6061
NGRC1=1	CPB6062
KGRC=1	CPB6063
KOUNT = 1	CPB6064
MAXT = 0	CPB6065
MAXR = 0	CPB6066
MAXC = 0	CPB6067
MAXP = 0	CPB6068
L = 0	CPB6069

TABLE D-4. (Continued)

	DO 131 I=1,5000	CPB6070
	KDAT(I)=10	CPB6071
131	CONTINUE	CPB6072
	IK = 1	CPB6073
	MAXS=1	CPB6074
132	READ (4, 218) KOD, KOD 1	CPB6075
	IF (NGRC.EQ.2.AND.NGRCL.EQ.2) NGRC=1	CPB6076
	IF (NGRC.EQ.2) NGRC1=2	CPB6077
	GO TO (134, 135, 136, 137, 138, 139), KOUNT	CPB6078
C		CPB6079
C	READ IN INITIAL TEMPERATURES OF ALL NODES	CPB6080
C		CPB6081
134	GO TO (3,13,9,13,14,13,13,13) ,KOD	CPB6082
3	READ (4, 200) (I 1(I), A(I), I = 1, KOD 1)	CPB6083
	DO 7 I = 1, KOD 1	CPB6084
	J = I 1(I)	CPB6085
	IF (J - MAXT) 5, 5, 4	CPB6086
4	MAXT = J	CPB6087
5	IF (J.EQ.0) WRITE (6,232) J,A(I)	CPB6088
	IF (J.EQ.0) ERROR=1.	CPB6089
6	P(J) = A(I)	CPB6090
	ITEM = J	CPB6091
	ATEM = A(I)	CPB6092
7	CONTINUE	CPB6093
	GO TO 132	CPB6094
9	READ (4, 201) N 1, A 1, N 2	CPB6095
	J = ITEM	CPB6096
	AA = ATEM	CPB6097
	DO 12 I = 1, N 2	CPB6098
	J = J + N 1	CPB6099
	AA = AA + A 1	CPB6100
	IF (J.GT.MAXT) MAXT=J	CPB6101
11	P(J) = AA	CPB6102
	ITEM = J	CPB6103
	ATEM = AA	CPB6104
12	CONTINUE	CPB6105
	GO TO 132	CPB6106
13	WRITE (6,219) KOD,BCDB(KOUNT)	CPB6107
	ERROR =2.	CPB6108
	RETURN	CPB6109
14	KOUNT = KOUNT + 1	CPB6110
	TEMPX=0.	CPB6111
	DO 141 I=1,MAXT	CPB6112
	IF (KDAT(I).EQ.10) P(I)=TEMPX	CPB6113
	IF (KDAT(I).NE.10) TEMPX=P(I)	CPB6114
141	CONTINUE	CPB6115
	READ (4, 200) I 1(1)	CPB6116
	WRITE (3) MAXT, NCVG, NSTS	CPB6117
	WRITE (3) (P(I), I = 1, MAXT)	CPB6118
	WRITE (3) MAXT, NCVG, NSTS	CPB6119
	WRITE (3) (P(I), I = 1, MAXT)	CPB6120
	DO 15 I = 1, 5000	CPB6121
	P(I) = 0.	CPB6122
15	CONTINUE	CPB6123
	WRITE (6,250) MAXT,MAXT	CPB6124
	MAXIM=MAXT+MAXT	CPB6125
	WRITE (6,251) MAXT,MAXIM	CPB6126
	GO TO 132	CPB6127
C		CPB6128
C	READ IN RESISTERS	CPB6129
C		CPB6130

TABLE D-4. (Continued)

135	GO TO (17,13,24,13,30,13,29,13),KOD	CPB6131
17	READ (4, 202) (I 1(I), I 2(I), I 3(I), A(I), I = 1, KOD 1)	CPB6132
18	DO 22 I=1,KOD1	CPB6133
	J = I 1(I)	CPB6134
	IF (J.GT.MAXR) MAXR=J	CPB6135
19	IF(J.LE.0) WRITE (6,233) I1(I),I2(I),I3(I),A(I)	CPB6136
	IF(J.LE.0) ERROR=1.	CPB6137
20	P(J) = A(I)	CPB6138
	L = L + 1	CPB6139
	IRLINE(L) = I 3(I) + 4096*(I 2(I) + 4096*J)	CPB6140
	IF (J.GE.2048) IRLINE(L)=-IRLINE(L)	CPB6141
	ITEM = J	CPB6142
	ITEM 2 = I 2(I)	CPB6143
	ITEM 3 = I 3(I)	CPB6144
	AEM = A(I)	CPB6145
	IF (ITEM2.LE.MAXT.AND.ITEM3.LE.MAXT) GO TO 22	CPB6146
	WRITE (6,234) ITEM,ITEM2,ITEM3,MAXT	CPB6147
	ERROR=1.	CPB6148
22	CONTINUE	CPB6149
	GO TO 132	CPB6150
25	READ (4,241) I1(1),I2(1),I3(1),X,Y,Z,KRVC,N2	CPB6151
	J=ITEM	CPB6152
	DO 2501 I=1,N2	CPB6153
	J=J+I1(1)	CPB6154
	ITEM2=ITEM2+I2(1)	CPB6155
	ITEM3=ITEM3+I3(1)	CPB6156
	X1=X1+X	CPB6157
	Y1=Y1+Y	CPB6158
	Z1=Z1+Z	CPB6159
	KKRV=KKRV+KCRV	CPB6160
	IF (J.GT.MAXR) MAXR=J	CPB6161
	P(J)=X1/(Y1*Z1)	CPB6162
	L=L+1	CPB6163
	IRLINE(L)=ITEM3+4096*(ITEM2+4096*J)	CPB6164
	IF (J.GE.2048) IRLINE(L)=-IRLINE(L)	CPB6165
	ITEM=J	CPB6166
	NSTR(KGRC)=J+4096*KKRV	CPB6167
	KGRC=KGRC+1	CPB6168
	IF (ITEM2.LE.MAXT.AND.ITEM3.LE.MAXT) GO TO 2501	CPB6169
	WRITE (6,234) ITEM,ITEM2,ITEM3,MAXT	CPB6170
	ERROR=1.	CPB6171
2501	CONTINUE	CPB6172
24	GO TO (2401,25),NGRC	CPB6173
2401	READ (4,203) I1(1),I2(1),I3(1),A(1),N2	CPB6174
	J = ITEM	CPB6175
	DO 28 I = 1, N 2	CPB6176
	J = J + I 1(1)	CPB6177
	ITEM 2 = ITEM 2 + I 2(1)	CPB6178
	ITEM 3 = ITEM 3 + I 3(1)	CPB6179
	AEM = AEM + A(1)	CPB6180
	IF (J.GT.MAXR) MAXR=J	CPB6181
26	P(J) = AEM	CPB6182
	L = L + 1	CPB6183
	IRLINE(L) = ITEM 3 + 4096*(ITEM 2 + 4096*J)	CPB6184
	IF (J.GE.2048) IRLINE(L)=-IRLINE(L)	CPB6185
	ITEM = J	CPB6186
	IF (ITEM2.LE.MAXT.AND.ITEM3.LE.MAXT) GO TO 28	CPB6187
	WRITE (6,234) ITEM,ITEM2,ITEM3,MAXT	CPB6188
	ERROR=1.	CPB6189
28	CONTINUE	CPB6190
	GO TO 132	CPB6191

TABLE D-4. (Continued)

29	READ (4,240) I1(1),I2(1),I3(1),X,Y,Z,KCRV	CPB6192
	A(1)=X/(Y*Z)	CPB6193
	NGRC=2	CPB6194
	X1=X	CPB6195
	Y1=Y	CPB6196
	Z1=Z	CPB6197
	NSTRT(KGRC)=I1(1)+4096*KCRV	CPB6198
	KGRC=KGRC+1	CPB6199
	KKRV=KCRV	CPB6200
	GO TO 18	CPB6201
30	KOUNT = KOUNT + 1	CPB6202
	READ (4, 202) I 1(1)	CPB6203
	WRITE (3) MAXR, NCVG, NSTS	CPB6204
	WRITE (3) (P(I), I = 1, MAXR)	CPB6205
	DO 31 I = 1, MAXR	CPB6206
	P(I) = 0.	CPB6207
31	CONTINUE	CPB6208
	MAXIM=MAXIM+MAXR	CPB6209
	WRITE (6,252) MAXR,MAXIM	CPB6210
	GO TO 132	CPB6211
C		CPB6212
C	READ IN CAPACITORS	CPB6213
C		CPB6214
136	GO TO (33,13,46,13,52,13,13,43),KOD	CPB6215
33	READ (4, 200) (I 1(I), A(I), I = 1, KOD 1)	CPB6216
	NOP = 0	CPB6217
39	DO 42 I = 1, KOD 1	CPB6218
	J = I 1(I)	CPB6219
	IF (J.GT.MAXT) WRITE (6,235) J,MAXT	CPB6220
	IF (J.GT.MAXT) ERROR=1.	CPB6221
	IF (J.GT.MAXC) MAXC=J	CPB6222
35	IF (J.LE.0) WRITE (6,232) J,A(I)	CPB6223
	IF (J.LE.0) ERROR=1.	CPB6224
36	P(J) = A(I)	CPB6225
	ITEM = J	CPB6226
	ATFM = A(I)	CPB6227
	KPSD(IK)=I1(I)+4096*(KKRV+4096*KKRV1)	CPB6228
	KPSD(IK)=-KPSD(IK)	CPB6229
	MAXP = MAXP + 1	CPB6230
	NODCON=0	CPB6231
	IK = IK + 1	CPB6232
	DO 41 K = 1, L	CPB6233
	IDAT 1 = IRLINE(K)/16777216	CPB6234
	IF (IRLINE(K).LT.0) IDAT1=IABS(IDAT1)+2048	CPB6235
	IDAT 2 = MOD(IRLINE(K)/4096, 4096)	CPB6236
	IDAT 3 = MOD(IRLINE(K), 4096)	CPB6237
	IF (IRLINE(K).LT.0) IDAT2=IABS(IDAT2)	CPB6238
	IF (IRLINE(K).LT.0) IDAT3=IABS(IDAT3)	CPB6239
	IF (I 1(I) - IDAT 2) 38, 37, 38	CPB6240
37	DO 3601 I9=1,KGRC	CPB6241
	KGR=MOD(NSTRT(I9),4096)	CPB6242
	KGK=MOD(NSTRT(I9)/4096,4096)	CPB6243
	IF (KGR.EQ.IDAT1) GO TO 3602	CPB6244
3601	CONTINUE	CPB6245
	KGK=0	CPB6246
3602	KPSD(IK)=IDAT3+4096*(IDAT1+4096*KGK)	CPB6247
	IF (KGR.EQ.IDAT1) NSTRT(I9)=0	CPB6248
	MAXP = MAXP + 1	CPB6249
	NODCON=1	CPB6250
	IK = IK + 1	CPB6251
38	IF (I 1(I) - IDAT 3) 41, 40, 41	CPB6252



TABLE D-4. (Continued)

40	DO 4001 I9=1,KGRC	CPB6253
	KGR=MOD(NSTRT(I9),4096)	CPB6254
	KGK=MOD(NSTRT(I9)/4096,4096)	CPB6255
	IF (KGR.EQ.IDAT1) GO TO 4002	CPB6256
4001	CONTINUE	CPB6257
	KGK=0	CPB6258
4002	KPSD(IK)=IDAT2+4096*(IDAT1+4096*KGK)	CPB6259
	IF (KGR.EQ.IDAT1) NSTRT(I9)=0	CPB6260
	MAXP = MAXP + 1	CPB6261
	NODCON=1	CPB6262
	IK = IK + 1	CPB6263
41	CONTINUE	CPB6264
	IF (NODCON.EQ.1) GO TO 42	CPB6265
	ERROR=1.	CPB6266
	WRITE (6,236) I1(I)	CPB6267
42	CONTINUE	CPB6268
	IF (NOP) 132, 132, 48	CPB6269
43	READ (4,242) I1(I),X,Y,Z,KKRV,KKRV1	CPB6270
	A(1)=X*Y*Z	CPB6271
	NGRC=2	CPB6272
	GO TO 39	CPB6273
46	GO TO (47,4701),NGRC	CPB6274
47	READ (4,201) N1,A1,N2	CPB6275
	NOP = NOP + 1	CPB6276
	KOD 1 = 1	CPB6277
	GO TO 50	CPB6278
4701	READ (4,243) N1,X1,Y1,Z1,IK1,IK2,N2	CPB6279
	KOD1=1	CPB6280
	GO TO 49	CPB6281
4702	I1(1)=ITEM+N1	CPB6282
	X=X+X1	CPB6283
	Y=Y+Y1	CPB6284
	Z=Z+Z1	CPB6285
	A(1)=X*Y*Z	CPB6286
	KKRV=KKRV+IK1	CPB6287
	KKRV1=KKRV1+IK2	CPB6288
	GO TO 39	CPB6289
48	IF (NOP - N 2) 49, 132, 132	CPB6290
49	NOP = NOP + 1	CPB6291
	GO TO (50,4702),NGRC	CPB6292
50	I 1(1) = ITEM + N 1	CPB6293
	A(1) = ATEM + A 1	CPB6294
	GO TO 39	CPB6295
52	KOUNT = KOUNT + 1	CPB6296
	MAXP = MAXP + 1	CPB6297
	KPSD(MAXP) = 0	CPB6298
	READ (4, 200) I 1(1)	CPB6299
	WRITE (3) MAXC, NCVG, NSTS	CPB6300
	WRITE (3) (P(I), I = 1, MAXC)	CPB6301
	DO 53 I = 1, MAXC	CPB6302
	P(I) = 0.	CPB6303
53	CONTINUE	CPB6304
	WRITE (3) MAXC, NCVG, NSTS	CPB6305
	WRITE (3) (P(I), I = 1, MAXC)	CPB6306
	WRITE (3) MAXC, NCVG, NSTS	CPB6307
	WRITE (3) (P(I), I = 1, MAXC)	CPB6308
	WRITE (3) MAXP, NCVG, NSTS	CPB6309
	WRITE (3) (KPSD(I), I = 1, MAXP)	CPB6310
	NWPD = MAXP	CPB6311
	NRECD = 7	CPB6312
	KSP = 2*MAXT + MAXR + 3*MAXC + 1	CPB6313

TABLE D-4. (Continued)

KST = KSP + MAXP	CPB6314
KST 1 = KST	CPB6315
NKSP = KST - 1	CPB6316
JJ = 0	CPB6317
N2=0	CPB6318
MAXIM=MAXIM+MAXC	CPB6319
WRITE (6,253) MAXC,MAXIM	CPB6320
MAXIM=MAXIM+MAXC	CPB6321
WRITE (6,254) MAXC,MAXIM	CPB6322
MAXIM=MAXIM+MAXC	CPB6323
WRITE (6,255) MAXC,MAXIM	CPB6324
MAXIM=MAXIM+MAXP	CPB6325
WRITE (6,256) MAXP,MAXIM	CPB6326
GO TO 132	CPB6327
C	CPB6328
C READ IN DATA SUB-BLOCKS	CPB6329
C	CPB6330
137 GO TO (56,13,66,67,68,13,13,13,691) ,KOD	CPB6331
56 IF (KOD 1) 57, 57, 64	CPB6332
57 READ (4, 204) NTAB	CPB6333
IF (NTAB) 62, 58, 59	CPB6334
58 WRITE (6, 220)	CPB6335
GO TO 132	CPB6336
59 IF (NSW2.EQ.1) GO TO 591	CPB6337
WRITE (6,230) NTABO,NTAB	CPB6338
ERROR=1.	CPB6339
NSW2=1	CPB6340
KST=KST1+JJ	CPB6341
591 NSTRT(MAXS)=KST+2**18*NTAB	CPB6342
NSW2=2	CPB6343
NTABO=NTAR	CPB6344
MAXS=MAXS+1	CPB6345
GO TO 132	CPB6346
62 IF (NSW2.EQ.2) GO TO 621	CPB6347
WRITE (6,231) NTABO	CPB6348
ERROR=1.	CPB6349
621 NSW2=1	CPB6350
IF (NTAB+7) 63,61,63	CPB6351
61 KURV 7 = KST 1 + JJ - KST	CPB6352
63 KST = KST 1 + JJ	CPB6353
GO TO 132	CPB6354
64 READ (4, 205) (A(I), I = 1, KOD 1)	CPB6355
641 DC 65 I = 1, KOD 1	CPB6356
JJ = JJ + 1	CPB6357
P(JJ) = A(I)	CPB6358
65 CONTINUE	CPB6359
IF (N2.GT.0) GO TO 661	CPB6360
GO TO 132	CPB6361
66 READ (4,206) AINC,N2	CPB6362
A(1)=P(JJ)	CPB6363
KOD1=1	CPB6364
661 A(1)=A(1)+AINC	CPB6365
N2=N2-1	CPB6366
GO TO 641	CPB6367
67 READ (4, 205) A(1)	CPB6368
P(JJ + 1) = 32767.	CPB6369
P(JJ + 2) = A(1)	CPB6370
JJ = JJ + 2	CPB6371
GO TO 132	CPB6372
68 KOUNT = KOUNT + 1	CPB6373
KST = KST - 1	CPB6374

TABLE D-4. (Continued)

	NWCT = JJ	CPB6375
	WRITE (3) NWCT, NCVG, NSTS	CPB6376
	WRITE (3) (P(I), I = 1, NWCT)	CPB6377
	NRECD = NRECD + 2	CPB6378
	READ (4, 205) A(1)	CPB6379
	WRITE (3) MAXS, NCVG, NSTS	CPB6380
	WRITE (3) (NSTRT(I), I = 1, MAXS)	CPB6381
	NWST = MAXS	CPB6382
	JJ = 0	CPB6383
	DO 69 I=1,40	CPB6384
	P(I)=0.	CPB6385
69	CONTINUE	CPB6386
	MAXIM=MAXIM+NWCT	CPB6387
	WRITE (6,257) NWCT,MAXIM	CPB6388
	MAXIM=MAXIM+MAXS	CPB6389
	WRITE (6,258) MAXS,MAXIM	CPB6390
	IF (MAXIM.LT.MAXMUM) GO TO 132	CPB6391
	ERROR=1.	CPB6392
	WRITE (6,244) MAXMUM,MAXIM	CPB6393
	GO TO 132	CPB6394
691	READ (4,204) ICOD	CPB6395
	KDAT(JJ+1) = 32765	CPB6396
	KDAT(JJ+2) = ICOD	CPB6397
	JJ = JJ+2	CPB6398
	GO TO 132	CPB6399
138	GO TO (70, 13, 13, 13, 72, 72), KOD	CPB6400
C70	READ (4, 200) (I1(I),A(I),I=1,KOD1)	CPB6401
70	READ (4, 205) ( A(I),I=1,KOD1)	CPB6402
	DO 71 I = 1, KOD 1	CPB6403
C	JJ = I1(I)	CPB6404
	JJ = JJ+1	CPB6405
	P(JJ+20)=A(I)	CPB6406
71	CONTINUE	CPB6407
	GO TO 132	CPB6408
72	KOUNT = KOUNT + 1	CPB6409
C	THE FOLLOWING 5 CARDS GO WITH THE NON-C CARDS ABOVE	CPB6410
	P(1)=P(23)	CPB6411
	P(2)=P(23)	CPB6412
	P(3)=P(22)	CPB6413
	P(4)=P(21)	CPB6414
	IF (P(24).NE.0.) P(7)=P(24)	CPB6415
	P(11)=P(2)	CPB6416
	JJ=16	CPB6417
	WRITE (3) JJ, NCVG, NSTS	CPB6418
	WRITE (3) (P(I), I = 1, JJ)	CPB6419
	NWTM = JJ	CPB6420
	END FILE 3	CPB6421
	NRECD=9	CPB6422
	REWIND 4	CPB6423
139	REWIND 3	CPB6424
	RETURN	CPB6425
	END	CPB6426



TABLE D-4. (Continued)

\$IBFTC CPC6		
	SUBROUTINE RESTR	CPC6000
C	AS OF 04/27/65	CPC6001
	COMMON P, M, MAXT, MAXR, MAXC, KSP, KST, KURV 7, NCVG, NSTS, NFAB	CPC6002
	COMMON NABL, NKSP, LMMF, NRMF, NREAD, CC	CPC6003
	COMMON NRECD, NRPD, NWCT, NWST, NWTM	CPC6004
	COMMON /CP2/ERROR, MAXMUM	CPC6005
	COMMON /CPPLT/NPLT, NEND	CPC6006
	DIMENSION A(12), I 1(12), I 2(12), I 3(12), NABL(10), CC(12)	CPC6007
	DIMENSION A1(6)	CPC6008
	DIMENSION CZ(6), CY(6)	CPC6009
	DIMENSION P(16000), IRLINE(1), KPSD(1), NSTRT(1), M(16), KDAT(1)	CPC6010
	EQUIVALENCE (P(4000), IRLINE(1)), (P(8000), KPSD(1)), (P(13000),	CPC6011
	I NSTRT(1)), (P(1), KDAT(1))	CPC6012
	REAL M, INC, NBK, NET	CPC6013
	INTEGER CP	CPC6014
	DATA ENDF/6H -1 /	CPC6015
	DATA NET/6HNFT /	CPC6016
	DATA DEC/6HDEC /	CPC6017
	DATA INC/6HINC /	CPC6018
	DATA PER/6HPER /	CPC6019
	DATA NBK/6HNBK /	CPC6020
	DATA CID/6HCID /	CPC6021
	DATA TAP/6HTAP /	CPC6022
	DATA COD/6HCOD /	CPC6023
	DATA ZERO/6H000000 /	CPC6024
	DATA END /6HEND /	CPC6025
	DATA (CY(I), I=1,6)/2H 1,2H 2,2H 3,2H 4,2H 5,2H 6/,ZERZ/2H00/	CPC6026
	DATA (CZ(I), I=1,6)/2H01,2H02,2H03,2H04,2H05,2H06/,BLANK/1H /	CPC6027
	DATA ZERY/2H 0/	CPC6028
200	FORMAT (5X, 4(I 5, E 10.2))	CPC6029
201	FORMAT (5X, I 5, E 10.2, I 5)	CPC6030
204	FORMAT (5X, I 5)	CPC6031
205	FORMAT (5X, 6E 10.2)	CPC6034
209	FORMAT (A3,A2,12A6)	CPC6035
210	FORMAT (5X,12A6)	CPC6037
211	FORMAT (5X, A3,12,12A6)	CPC6038
212	FORMAT (1H1,9X,12A6)	CPC6039
215	FORMAT (4CHO KOUNT IS NOT CORRECT IN RESTR ROUTINE )	CPC6040
218	FORMAT (I 3, 3X, I 2)	CPC6042
222	FORMAT (30HO TOO MANY WORDS IN DAT BLOCK )	CPC6044
223	FORMAT (7HOCODE= A6,12H IS ILLEGAL.)	CPC6047
224	FORMAT (25HOCANNOT FIND CURVE NAMED A6,17H ON LIBRARY TAPE.)	CPC6048
236	FORMAT (15HOBLOCK NUMBER =I6,29H IS ILLEGAL. RESTART DELETED. )	CPC6049
237	FORMAT (14HIEND OF CASES.)	CPC6052
241	FORMAT (5X,E10.0,I5)	CPC6053
242	FORMAT (5X,2E10.0,I5)	CPC6054
243	FORMAT (5X,3E10.0,I5)	CPC6055
244	FORMAT (5X,4E10.0,I5)	CPC6056
245	FORMAT (5X,5E10.0,I5)	CPC6057
246	FORMAT (5X,6E10.0,I5)	CPC6058
	NRECD=9	CPC6059
	MATLIB =1	CPC6060
	LINE=1	CPC6061
149	REWIND 4	CPC6062
139	REWIND 3	CPC6063
	DO 310 I = 1, 16	CPC6064
	M(I) = 0.0	CPC6065
310	CONTINUE	CPC6066
	M(7) = 0.25	CPC6067
	MAXP = 0	CPC6068
		CPC6069

TABLE D-4. (Continued)

	JJ = 1	CPC6070
	DO 75 I = 1, NRECD	CPC6071
	READ (3) N 1	CPC6072
	MAXP = MAXP + N 1	CPC6073
	READ (3) (P(J), J = JJ, MAXP)	CPC6074
	JJ = MAXP + 1	CPC6075
75	CONTINUE	CPC6076
	READ (3) N 1	CPC6077
	READ (3) (M(I), I=1, N1)	CPC6078
	MAXP = MAXP + N 1	CPC6079
	REWIND 3	CPC6080
	IF (MAXP - MAXMUM) 701, 701, 81	CPC6081
81	WRITE (6, 222)	CPC6082
100	ERROR=2.	CPC6083
701	IF (MATLIB.EQ.1) READ (5, 209) CM, CX, (A(I), I=1, 12)	CPC6084
	IF (MATLIB.EQ.2) READ ( 12 , 209) CM, CX, (A(I), I=1, 12)	CPC6085
	CP=-1	CPC6086
1101	DO 1102 I=1, 6	CPC6087
1102	IF (CX.EQ.CY(I).OR.CX.EQ.CZ(I)) CP=1	CPC6088
	IF (CX.EQ.BLANK.OR.CX.EQ.ZERZ.OR.CX.EQ.ZERY) CP=0	CPC6089
	IF (CP.GE.0) GO TO 1103	CPC6090
	WRITE (6, 215)	CPC6091
	ERROR=1.	CPC6092
	CP=0	CPC6093
1103	IF (CM.EQ.END) GO TO 900	CPC6094
	IF (CM.EQ.TAP) GO TO 150	CPC6095
	IF (LINE.LT.60) GO TO 7011	CPC6096
	WRITE (6, 212) (CC(I), I=1, 12)	CPC6097
	LINE = 1	CPC6098
7011	IF (CM.EQ.CID) GO TO 117	CPC6099
	WRITE (6, 211) CM, CP, (A(I), I=1, 12)	CPC6100
	LINE = LINE+1	CPC6101
	IF (CM .EQ. DEC) GO TO 702	CPC6102
	IF (CM .EQ. INC) GO TO 703	CPC6103
	IF (CM.EQ.COD) GO TO 707	CPC6104
	IF (CM .EQ. PER) GO TO 704	CPC6105
	IF (CM .EQ. NBK) GO TO 705	CPC6106
	WRITE (6, 223) CM	CPC6107
	ERROR=1.	CPC6108
	GO TO 701	CPC6109
117	CMID=CM	CPC6110
	ICP=CP	CPC6111
	DO 1171 I=1, 12	CPC6112
	CC(I)=A(I)	CPC6113
1171	CONTINUE	CPC6114
	LINE=1	CPC6115
	WRITE (6, 212) (CC(I), I=1, 12)	CPC6116
	GO TO 701	CPC6117
150	IF (MATLIB.EQ.2) GO TO 160	CPC6118
	MATLIB=2	CPC6119
	FIRST = 0.	CPC6120
	WRITE (6, 211) CM, CP, (A(I), I=1, 12)	CPC6121
	LINE = LINE+1	CPC6122
151	READ ( 12 , 209) Z1, Z2, Z3	CPC6123
	IF (Z1.NE.TAP) GO TO 151	CPC6124
	IF (Z3.EQ.A(1)) GO TO 701	CPC6125
	IF (Z3.NE.ZERO) GO TO 151	CPC6126
	REWIND 12	CPC6127
	FIRST = FIRST+1.	CPC6128
	IF (FIRST.EQ.1.) GO TO 151	CPC6129
	WRITE (6, 224) A(1)	CPC6130

TABLE D-4. (Continued)

160	ERROR =1. MATLIB=1 GO TO 701	CPC6131 CPC6132 CPC6133
702	KOD=1 GO TO 706	CPC6134 CPC6135
703	KOD = 2 GO TO 706	CPC6136 CPC6137
704	KOD = 3 GO TO 706	CPC6138 CPC6139
707	KOD = 5 GO TO 706	CPC6140 CPC6141
705	KOD = 4	CPC6142
706	WRITE (4,218) KOD,CP WRITE (4, 210) (A(I), I = 1, 12) IF (KOD.LT.4) GO TO 701 IF (KOD.EQ.4) GO TO 708 WRITE (6,215) ERROR=1.	CPC6143 CPC6144 CPC6145 CPC6146 CPC6147 CPC6148
708	END FILE 4 REWIND 4	CPC6149 CPC6150
714	READ (4, 218) KOD, KOD 1 GO TO (717, 122, 122, 719), KOD	CPC6151 CPC6152
717	IF (KOD 1) 718, 718, 716	CPC6153
716	WRITE (6, 250)	CPC6154
250	FORMAT (34H KOD1 IS NOT ZERO IN RESTART BLOCK ) ERROR=1. GO TO 714	CPC6155 CPC6156 CPC6157
122	WRITE (6,215) ERROR=1. GO TO 719	CPC6158 CPC6159 CPC6160
719	REWIND 4 REWIND 3 MAXP = 0 M(1)=M(2) M(11)=M(2) JJ = 1 DO 800 I = 1, NRECD GO TO (780, 780, 782, 784, 784, 784, 786, 788, 790), I	CPC6161 CPC6162 CPC6163 CPC6164 CPC6165 CPC6166 CPC6167 CPC6168
780	N 1 = MAXT GO TO 798	CPC6169 CPC6170
782	N 1 = MAXR GO TO 798	CPC6171 CPC6172
784	N 1 = MAXC GO TO 798	CPC6173 CPC6174
786	N 1 = NWPD GO TO 798	CPC6175 CPC6176
788	N 1 = NWCT GO TO 798	CPC6177 CPC6178
790	N 1 = NWST	CPC6179
798	WRITE (3) N 1, NCVG, NSTS MAXP = MAXP + N 1 WRITE (3) (P(J), J = JJ, MAXP) JJ = MAXP + 1	GPC6180 CPC6181 CPC6182 CPC6183
800	CONTINUE N 1 = 16 WRITE (3) N 1, NCVG, NSTS WRITE (3) (M(I), I=1,N1) END FILE 3 REWIND 3 RETURN	CPC6184 CPC6185 CPC6186 CPC6187 CPC6188 CPC6189
718	READ (4, 204) NBLK	CPC6190 CPC6191

TABLE D-4. (Continued)

	IF (NBLK.EQ.11) GO TO 714	CPC6192
	IF (NBLK.GE.1.AND.NBLK.LE.5) GO TO (720,730,740,750,760),NBLK	CPC6193
	WRITE (6,236) NBLK	CPC6194
	ERROR=1.	CPC6195
	NBLK =1	CPC6196
	GO TO 714	CPC6197
720	READ (4, 218) KOD, KOD 1	CPC6198
	GO TO (722, 725, 122, 719), KOD	CPC6199
722	IF (KOD 1) 721, 721, 723	CPC6200
721	READ (4, 204) I	CPC6201
	GO TO 714	CPC6202
723	READ (4, 200) (I 1(I), A(I), I = 1, KOD 1)	CPC6203
	DO 724 I = 1, KOD 1	CPC6204
	J = I 1(I)	CPC6205
	JJ = J + MAXT	CPC6206
	P(JJ) = A(I)	CPC6207
	P(J) = A(I)	CPC6208
	ITEM = I 1(I)	CPC6209
	ATEM = A(I)	CPC6210
724	CONTINUE	CPC6211
	GO TO 720	CPC6212
725	READ (4, 201) N 1, A 1, N 2	CPC6213
	J = ITEM	CPC6214
	AA = ATEM	CPC6215
	DO 726 I = 1, N 2	CPC6216
	J = J + N 1	CPC6217
	JJ = J + MAXT	CPC6218
	AA = AA + A 1	CPC6219
	P(J) = AA	CPC6220
	P(JJ) = AA	CPC6221
	ITEM = J	CPC6222
	ATEM = AA	CPC6223
726	CONTINUE	CPC6224
	GO TO 720	CPC6225
730	READ (4, 218) KOD, KOD 1	CPC6226
	GO TO (731, 734, 122, 719), KOD	CPC6227
731	IF (KOD 1) 721, 721, 732	CPC6228
732	READ (4, 200) (I 1(I), A(I), I = 1, KOD 1)	CPC6229
	DO 733 I = 1, KOD 1	CPC6230
	J = I 1(I) + 2*MAXT	CPC6231
	P(J) = A(I)	CPC6232
	ITEM = I 1(I)	CPC6233
	ATEM = A(I)	CPC6234
733	CONTINUE	CPC6235
	GO TO 730	CPC6236
734	READ (4, 201) N 1, A 1, N 2	CPC6237
	J = ITEM	CPC6238
	AA = ATEM	CPC6239
	DO 736 I = 1, N 2	CPC6240
	J = J + N 1	CPC6241
	JJ = J + 2*MAXT	CPC6242
	AA = AA + A 1	CPC6243
	P(JJ) = AA	CPC6244
	ITEM = J	CPC6245
	ATEM = AA	CPC6246
736	CONTINUE	CPC6247
	GO TO 730	CPC6248
740	READ (4, 218) KOD, KOD 1	CPC6249
	GO TO (741, 744, 122, 719), KOD	CPC6250
741	IF (KOD 1) 721, 721, 742	CPC6251
742	READ (4, 200) (I 1(I), A(I), I = 1, KOD 1)	CPC6252

TABLE D-4. (Continued)

	DO 743 I = 1, KOD 1	CPC6253
	J = I 1(I) + 2*MAXT + MAXR	CPC6254
	P(J) = A(I)	CPC6255
	ITEM = I 1(I)	CPC6256
	ATEM = A(I)	CPC6257
743	CONTINUE	CPC6258
	GO TO 740	CPC6259
744	READ (4, 201) N 1, A 1, N 2	CPC6260
	J = ITEM	CPC6261
	AA = ATEM	CPC6262
	DO 746 I = 1, N 2	CPC6263
	J = J + N 1	CPC6264
	JJ = J + 2*MAXT + MAXR	CPC6265
	AA = AA + A 1	CPC6266
	P(JJ) = AA	CPC6267
	ITEM = J	CPC6268
	ATEM = AA	CPC6269
746	CONTINUE	CPC6270
	GO TO 740	CPC6271
750	JJ = 5	CPC6272
751	READ (4, 218) KOD, KOD 1	CPC6273
	GO TO (752, 122, 122, 719), KOD	CPC6274
752	IF (KOD 1) 721, 721, 753	CPC6275
753	READ (4, 205) ( A(I), I=1, KOD1)	CPC6276
	DO 754 I = 1, KOD 1	CPC6277
	JJ = JJ-1	CPC6278
	IF (JJ.EQ.1) M(7)=A(7)	CPC6279
	IF (JJ.EQ.1) GO TO 754	CPC6280
	M(JJ) = A(I)	CPC6281
754	CONTINUE	CPC6282
	GO TO 751	CPC6283
760	READ (4, 218) KOD, KOD 1	CPC6284
	IF (KOD.EQ.4) GO TO 719	CPC6285
759	READ (4, 204) NTAB	CPC6286
	IF (NTAB) 760, 714, 761	CPC6287
761	L = LOC (NTAB)	CPC6288
762	READ (4, 218) KOD, KOD 1	CPC6289
	GO TO (764, 770, 763, 719, 773), KOD	CPC6290
763	L = L + 1	CPC6291
	READ (4, 205) A(1)	CPC6292
	P(L) = A(1)	CPC6293
	GO TO 762	CPC6294
764	IF (KOD 1) 759, 759, 766	CPC6295
766	READ (4, 205) (A(I), I = 1, KOD 1)	CPC6296
	KOD2=KOD1	CPC6297
	DO 769 I = 1, KOD 1	CPC6298
	L = L + 1	CPC6299
	P(L) = A(I)	CPC6300
769	CONTINUE	CPC6301
	GO TO 762	CPC6302
770	IF (KOD1.LE.0) KOD1=KOD2	CPC6303
	GO TO (7701, 7702, 7703, 7704, 7705, 7706), KOD1	CPC6304
7701	READ (4, 241) (A1(I), I=1, KOD1), INCR	CPC6305
	GO TO 771	CPC6306
7702	READ (4, 242) (A1(I), I=1, KOD1), INCR	CPC6307
	GO TO 771	CPC6308
7703	READ (4, 243) (A1(I), I=1, KOD1), INCR	CPC6309
	GO TO 771	CPC6310
7704	READ (4, 244) (A1(I), I=1, KOD1), INCR	CPC6311
	GO TO 771	CPC6312
7705	READ (4, 245) (A1(I), I=1, KOD1), INCR	CPC6313



TABLE D-4. (Continued)

7706	GO TO 771	CPC6314
	READ (4,246) (A1(I),I=1,KOD1),INCR	CPC6315
	GO TO 771	CPC6316
771	DO 772 I=1,KOD1	CPC6317
	A(I)=A(I)+A1(I)	CPC6318
	L=L+1	CPC6319
	P(L)=A(I)	CPC6320
772	CONTINUE	CPC6321
	INCR=INCR-1	CPC6322
	IF (INCR.GT.0) GO TO 771	CPC6323
	GO TO 762	CPC6324
773	READ (4,204) ICOD	CPC6325
	KDAT (L+1) = 32765	CPC6326
	KDAT (L+2) = ICOD	CPC6327
	L=L+2	CPC6328
	GO TO 762	CPC6329
900	REWIND 3	CPC6330
	REWIND 4	CPC6331
	WRITE (6,237)	CPC6332
	NEND=1	CPC6333
	RETURN	CPC6334
	END	CPC6335

\$IBFTC	EXC6	EXC6000
	SUBROUTINE EXCUT(NLAG)	EXC6001
C	AS OF 05/19/65	EXC6002
	COMMON P(16000),M(16),MAXT,MAXR,MAXC,KSP,KST,KURV7,NCVG	EXC6003
	COMMON NSTS,NFAB,NABL(10),NKSP	EXC6004
	DIMENSION KP(1)	EXC6005
	EQUIVALENCE (P(1),KP(1))	EXC6006
	COMMON /CP2/ERROR	EXC6007
	COMMON /EXADR/LCTN,LCTO,LCR,LCC,LCQ,LCRC,LCPS,LCK,LCKA	EXC6008
	COMMON /EXPLT/ NLFLG	EXC6009
	COMMON /EXFLG/NTFLG,NSAV,NFLG	EXC6010
	COMMON /EXSTA/ NC,NCUR1,NCURV(20)	EXC6011
	COMMON /EXCVG/ NFLAG,ITMAX,ITER,NODE,PM1,PM,DTO,ATEM,NTEM,MTEM	EXC6012
	NFLG=0	EXC6013
	NSAV=0	EXC6014
	NLFLG=0	EXC6015
	REWIND 11	EXC6016
	CALL CDATA	EXC6017
	CALL HTBAL(NLAG)	EXC6018
	RETURN	EXC6019
	END	EXC6020

TABLE D-4. (Continued)

5IBFTC CDA6	CDA6000
SUBROUTINE CDATA	CDA6001
C  AS OF 04/27/65	CDA6002
COMMON P(16000),M(16),MAXT,MAXR,MAXC,KSP,KST,KURV7,NCVG,	CDA6003
1 NSTS,NFAB,NABL(10),NKSP,LMMF,NRMF,NREAD,CC(12)	CDA6004
COMMON NR,MAXP,NWCT,MAXS,MAXM	CDA6005
COMMON /CP2/ERROR	CDA6006
COMMON /EXADR/ LCTN,LCTO,LCR,LCC,LCQ,LCRC,LCPS,LCK,LCKA	CDA6007
REAL M	CDA6008
LCTN=1	CDA6009
READ(3) MAXT	CDA6010
LCTO=LCTN+MAXT	CDA6011
L=LCTO-1	CDA6012
READ(3) (P(I),I=LCTN,L)	CDA6013
READ(3) MAXT	CDA6014
LCR=LCTO+MAXT	CDA6015
L=LCR-1	CDA6016
READ(3) (P(I),I=LCTO,L)	CDA6017
READ(3) MAXR	CDA6018
LCC=LCR+MAXR	CDA6019
L=LCC-1	CDA6020
READ(3) (P(I),I=LCR,L)	CDA6021
READ(3) MAXC	CDA6022
LCQ=LCC+MAXC	CDA6023
L=LCQ-1	CDA6024
READ(3) (P(I),I=LCC,L)	CDA6025
READ(3) MAXC	CDA6026
LCRC=LCQ+MAXC	CDA6027
L=LCRC-1	CDA6028
READ(3) (P(I),I=LCQ,L)	CDA6029
READ(3) MAXC	CDA6030
LCPS=LCRC+MAXC	CDA6031
L=LCPS-1	CDA6032
READ(3) (P(I),I=LCRC,L)	CDA6033
READ(3) MAXP	CDA6034
LCK=LCPS+MAXP	CDA6035
L=LCK-1	CDA6036
READ(3) (P(I),I=LCPS,L)	CDA6037
READ(3) NWCT	CDA6038
LCKA=LCK+NWCT	CDA6039
L=LCKA-1	CDA6040
READ(3) (P(I),I=LCK,L)	CDA6041
READ(3) MAXS	CDA6042
L=LCKA+MAXS-1	CDA6043
READ(3) (P(I),I=LCKA,L)	CDA6044
READ(3) MAXM	CDA6045
READ(3) (M(I),I=1,MAXM)	CDA6046
IF (M(7).LE.0.) M(7)=.25	CDA6047
RETURN	CDA6048
END	CDA6049

TABLE D-4. (Continued)

SIBFTC	HTB6		HTB6000
	SUBROUTINE HTBAL (NLAG)		HTB6001
C	AS OF 06/12/65		HTB6002
	COMMON P, M, MAXT, MAXR, MAXC, KSP, KST, KURV 7, NCVG, NSTS, NFAB		HTB6003
	COMMON NABL, NKSP, LMMF, NRMF, NREAD		HTB6004
	COMMON /EXFLG/NTFLG,NSAV,NFLG		HTB6005
	COMMON / CP2/ ERROR		HTB6006
	COMMON / EXPLT/ NLFLG		HTB6007
	COMMON /CPITM/ ITIMO		HTB6008
	DIMENSION P(16000), M(16), KPSD(1), NABL(10)		HTB6009
	EQUIVALENCE (P(1), KPSD(1)).		HTB6010
	REAL M,LIN		HTB6011
	ITIME = ITIMO		HTB6012
24	IR=1		HTB6013
	T16TH = (M(3)-M(2))/16.		HTB6014
	T16TS = T16TH+M(2)		HTB6015
	CALL SLITE (0)		HTB6016
	IF (M(16).LE.0.) M(16)=0.		HTB6017
	IF (M(16).GT.0.) GO TO 29		HTB6018
	DO 28 I=KSP,NKSP		HTB6019
	IF (KPSD(I)) 25,29,26		HTB6020
25	NN=-KPSD(I)		HTB6021
	ND= MOD(NN,4096)		HTB6022
	K1= NN/2**24		HTB6023
	K2= MOD(NN/2**12,4096)		HTB6024
	IF (K1.EQ.0.OR.K2.EQ.0) GO TO 28		HTB6025
	RHO = LIN(P(ND),K1)		HTB6026
	CP = LIN(P(ND),K2)		HTB6027
	NC = ND+2*MAXT+MAXR		HTB6028
	P(NC) = P(NC)*CP*RHO		HTB6029
	GO TO 28		HTB6030
26	ND = MOD(KPSD(I),4096)		HTB6031
	NR = MOD(KPSD(I)/4096,4096)		HTB6032
	K3 = KPSD(I)/2**24		HTB6033
	IF (K3.EQ.0) GO TO 28		HTB6034
	J = NR+2*MAXT		HTB6035
	FACT=LIN(P(ND),K3)		HTB6036
	P(J)=P(J)/FACT		HTB6037
28	CONTINUE		HTB6038
29	CONTINUE		HTB6039
40	GO TO (1, 4, 4), NSTS		HTB6040
1	NPRINT = 1		HTB6041
2	I 1 = 0		HTB6042
	I 2 = MAXT		HTB6043
	I 3 = I 2 + MAXT		HTB6044
	I 4 = I 3 + MAXR		HTB6045
	I 5 = I 4 + MAXC		HTB6046
	I 6 = I 5 + MAXC		HTB6047
	SUM 1 = 0.		HTB6048
	SUM 2 = 0.		HTB6049
	SUM 3 = 0.		HTB6050
3	CALL FUNCT		HTB6051
	IF (ERROR.GT.0.) GO TO 770		HTB6052
	IF (NSTS.EQ.2) IR=2		HTB6053
	IF (NCVG.EQ.2) IR=2		HTB6054
4	NFLAG = 1		HTB6055
	IF (M(1).LT.T16TS) GO TO 203		HTB6056
	T16TS=T16TS+T16TH		HTB6057
	DO 202 J=1,4		HTB6058
	I=5-J		HTB6059
	CALL SLITET (I,LIT)		HTB6060

TABLE D-4. (Continued)

201	GO TO (202,201),LIT	HTB6061
	CONTINUE	HTB6062
	CALL SLITE (I)	HTB6063
	GO TO 203	HTB6064
202	CONTINUE	HTB6065
203	CONTINUE	HTB6066
	RCM = M(4)	HTB6067
	M(9) = 0.	HTB6068
	J = KSP	HTB6069
44	NN = MOD(KPSD(J),4096)	HTB6070
	NN = ISIGN(NN,KPSD(J))	HTB6071
	IF (NN.EQ.0) GO TO 50	HTB6072
	GO TO 14	HTB6073
5	NN = MOD(KPSD(J),4096)	HTB6074
	NN = ISIGN(NN,KPSD(J))	HTB6075
	IF (NN) 6, 7, 19	HTB6076
6	IF (J.LT.NKSP) GO TO 8	HTB6077
7	NFLAG = 2	HTB6078
8	P(NRC) = ABS(P(NC))/SUM2*SIGN(1.,P(NRC))	HTB6079
	IF (SUM2.EQ.0.) WRITE (6,2003) N2	HTB6080
	IF (SUM2.EQ.0.) ERROR=2.	HTB6081
2003	FORMAT (23H0SUM(1./R)=0. FOR NODE I5)	HTB6082
	IF (M(16).LE.0. ) P(NRC)=ABS(P(NRC))	HTB6083
	IF (IR.EQ.2) GO TO 10	HTB6084
	IF (P(NC).NE.0.) GO TO 11	HTB6085
10	P(NTNK) = (SUM 1 + P(NQ))/SUM 2	HTB6086
	GO TO 13	HTB6087
11	P(NTNK)=M(5)/ABS(P(NC))*(SUM1-SUM 3 + P(NQ)) + P(NTOK)	HTB6088
	IF (P(NRC).NE.0.) GO TO 132	HTB6089
2001	FORMAT (23H0 R-C PRODUCT FOR NODE I 4, 6H IS E 20.8)	HTB6090
130	WRITE (6, 2001) N 2, P(NRC)	HTB6091
	ERROR=2.	HTB6092
	GO TO 13	HTB6093
132	IF (ABS(P(NRC)).GE.RCM) GO TO 13	HTB6094
12	M(9) = N 2	HTB6095
	RCM = ABS(P(NRC))	HTB6096
13	SUM 1 = 0.	HTB6097
	SUM 2 = 0.	HTB6098
	SUM 3 = 0.	HTB6099
	GO TO (14, 72, 99), NFLAG	HTB6100
14	N 2 = - NN	HTB6101
	NTNK = N 2 + I 1	HTB6102
	NC = N 2 + I 4	HTB6103
	NTOK = N 2 + I 2	HTB6104
	NQ = N 2 + I 5	HTB6105
	NRC = N 2 + I 6	HTB6106
	J = J + 1	HTB6107
19	NN = MOD(KPSD(J)/4096,4096)	HTB6108
	IDAT = MOD(KPSD(J), 4096)	HTB6109
	NR = NN + I 3	HTB6110
	NTOM = IDAT + I 2	HTB6111
	J = J + 1	HTB6112
22	SUM 1 = SUM 1 + P(NTOM)/P(NR)	HTB6113
	SUM 2 = SUM 2 + 1./P(NR)	HTB6114
	SUM 3 = SUM 3 + P(NTOK)/P(NR)	HTB6115
	GO TO 5	HTB6116
50	WRITE (6, 52)	HTB6117
52	FORMAT (35H SOMETHING ROTTEN IN HTBAL ROUTINE )	HTB6118
	GO TO 770	HTB6119
72	M(6) = RCM	HTB6120
	M(16)=M(16)+1.0	HTB6121

TABLE D-4. (Continued)

	M(14)=M(5)	HTB6122
	DO 724 I=KSP,NKSP	HTB6123
	IF (KPSD(I)) 721,725,722	HTB6124
721	NN =-KPSD(I)	HTB6125
	ND = MOD(NN,4096)	HTB6126
	K1 = NN/2**24	HTB6127
	K2 = MOD(NN/2**12,4096)	HTB6128
	IF (K1.EQ.0.OR.K2.EQ.0) GO TO 724	HTB6129
	RHO = LIN(P(ND),K1)	HTB6130
	CP = LIN(P(ND),K2)	HTB6131
	J = ND+MAXT	HTB6132
	RHO1 = LIN(P(J),K1)	HTB6133
	CP1 = LIN(P(J),K2)	HTB6134
	NC = ND+2*MAXT+MAXR	HTB6135
	P(NC) = P(NC)*CP/CP1*RHO/RHO1	HTB6136
	GO TO 724	HTB6137
722	ND = MOD(KPSD(I),4096)	HTB6138
	NR = MOD(KPSD(I)/4096,4096)	HTB6139
	K3 = KPSD(I)/2**24	HTB6140
	IF (K3.EQ.0) GO TO 724	HTB6141
	J = NR+2*MAXT	HTB6142
	J1 = ND+MAXT	HTB6143
	FACT=LIN(P(ND),K3)	HTB6144
	FACT1=LIN(P(J1),K3)	HTB6145
	P(J)=P(J)*FACT/FACT1	HTB6146
724	CONTINUE	HTB6147
725	CONTINUE	HTB6148
	IF (NSAV.NE.0) CALL SAVT3	HTB6149
	ITIME = ITIME	HTB6151
	GO TO (56, 99, 56), NSTS	HTB6152
56	GO TO (108,60,60,108),NCVG	HTB6153
108	GO TO (73,109,111,109),LMMF	HTB6154
109	LMMF=3	HTB6155
	CALL MMF(0.,0.,1,1)	HTB6156
	LMMF=4	HTB6157
	GO TO 73	HTB6158
60	GO TO (115,112,111,115),LMMF	HTB6159
111	WRITE (6,2005) LMMF	HTB6160
2005	FORMAT(7H LMMF=I5,4X,36H WRONG VALUE AT THIS POINT IN HTBAL )	HTB6161
	GO TO 770	HTB6162
112	LMMF=4	HTB6163
115	CALL CVG(-1.,1,1)	HTB6164
	M(5) = M(7)*M(6)	HTB6165
	M(15) = M(5)	HTB6166
	GO TO (50, 3, 3, 76), NCVG	HTB6167
73	J = MAXT + 1	HTB6168
	DO 74 I = 1, MAXT	HTB6169
	P(J) = P(I)	HTB6170
	J = J + 1	HTB6171
74	CONTINUE	HTB6172
	IF (M(8)) 79, 75, 79	HTB6173
75	IF (NPRINT) 78, 77, 77	HTB6174
79	M(8) = 0.	HTB6175
77	CALL PRINT	HTB6176
	IF (NPRINT) 78, 97, 76	HTB6177
76	M(11) = M(11) + M(4)	HTB6178
78	M(5) = M(7)*M(6)	HTB6179
	IF (M(5).GT.0.) GO TO 80	HTB6180
	WRITE(6,2002) M(5)	HTB6181
	GO TO 770	HTB6182
2002	FORMAT (16H1 DELTA THETA = E15.6,24H MUST BE GREATER THAN 0.)	HTB6183

TABLE D-4. (Continued)

80	M(15) = M(5)	HTB6184
	PM 1 = M(1)	HTB6185
	IF (NLFLG.GT.1) CALL TPLOT(-1)	HTB6186
	M(1) = M(1) + M(5)	HTB6187
	IF (M(11) - M(3)) 83, 82, 82	HTB6188
82	M(11) = M(3)	HTB6189
	LPT = 2	HTB6190
	GO TO 84	HTB6191
83	LPT = 1	HTB6192
84	IF (M(1) - M(11)) 85, 90, 87	HTB6193
85	NPRINT = - 1	HTB6194
	GO TO 3	HTB6195
87	M(5) = M(11) - PM 1	HTB6196
	M(1) = M(11)	HTB6197
90	GO TO (92, 93), LPT	HTB6198
92	NPRINT = 1	HTB6199
	GO TO 3	HTB6200
93	NPRINT = 0	HTB6201
	GO TO 3	HTB6202
770	ERROR=2.	HTB6203
	WRITE (6,2004) ERROR	HTB6204
2004	FORMAT (36HOERROR HAS OCCURRED. JOB TERMINATED. 6H LEVELF4.1/ 1 28HOLAST TIME POINT CALCULATED.)	HTB6205
	CALL PRINT	HTB6206
	NLAG=2	HTB6207
	RETURN	HTB6208
97	IF (NLFLG.GT.1) CALL TPLOT(-1)	HTB6209
	GO TO (96,111,111,94),LMMF	HTB6210
94	NLAG=3	HTB6211
	GO TO 91	HTB6212
96	NLAG=2	HTB6213
91	GO TO (95,98,98),NFAB	HTB6214
95	GO TO (99,50,98),NSTS	HTB6215
98	GO TO 99	HTB6216
99	RETURN	HTB6217
	END	HTB6218
		HTB6219

TABLE D-4. (Continued)

	\$IBFTC BIV6	BIV6000
	FUNCTION BIV (XV,XH,K,ERR )	BIV6001
C	AS OF 06/12/65	BIV6002
	COMMON P(16000),M(16)	BIV6003
	COMMON /CP2/ERROR	BIV6004
	DIMENSION KP(1)	BIV6005
	EQUIVALENCE (P(1),KP(1))	BIV6006
	REAL M	BIV6006
	L=LOC(K)+1	BIV6007
	KFLL=0	BIV6008
	KOD=32765	BIV6009
	IF (KOD.EQ.KP(L)) KOD=KP(L+1)	BIV6010
	IF (KOD.NE.32765) L=L+2	BIV6011
	LV = P(L)/1000.+1	BIV6012
	LH = AMOD(P(L),1000.)+1	BIV6013
	IF (P(L+1).GT.P(L+2)) GO TO 20	BIV6014
	IF (XH.LT.P(L+1)) GO TO 50	BIV6015
	DO 15 J=2,LH	BIV6016
	L1=L+J-1	BIV6017
	IF(P(L1).GT.P(L1+1)) GO TO 50	BIV6018
	IF (XH.LE.P(L1+1)) GO TO 30	BIV6019
15	CONTINUE	BIV6020
50	ERROR=2.	BIV6021
	WRITE (6,90) K,XV,XH	BIV6022
	RETURN	BIV6023
20	IF (XH.GT.P(L+1)) GO TO 50	BIV6024
	DO 25 J=2,LH	BIV6025
	L1=L+J-1	BIV6026
	IF (P(L1).LT.P(L1+1)) GO TO 50	BIV6027
	IF (XH.GE.P(L1+1)) GO TO 30	BIV6028
25	CONTINUE	BIV6029
	GO TO 50	BIV6030
30	L2=L+LH+1	BIV6031
	L3=L2+LH+1	BIV6032
	IF (P(L2).GT. P(L3)) GO TO 40	BIV6033
	IF (XV.LT.P(L2)) GO TO 50	BIV6034
	DO 35 I=1,LV	BIV6035
	L2= L+I*(LH+1)	BIV6036
	L3= L2+LH+1	BIV6037
	IF (P(L2).GT.P(L3)) GO TO 50	BIV6038
	IF (XV.LE.P(L3)) GO TO 60	BIV6039
35	CONTINUE	BIV6040
	GO TO 50	BIV6041
40	IF (XV.GT.P(L2)) GO TO 50	BIV6042
	DO 45 I=1,LV	BIV6043
	L2= L+I*(LH+1)	BIV6044
	L3= L2+LH+1	BIV6045
	IF (P(L2).LT.P(L3)) GO TO 50	BIV6046
	IF (XV.GE.P(L3)) GO TO 60	BIV6047
45	CONTINUE	BIV6048
	GO TO 50	BIV6049
60	J1=L2+L1-L	BIV6050
	J2=J1+1	BIV6051
	J3=L3+L1-L	BIV6052
	J4=J3+1	BIV6053
	IF (KOD.EQ.32765.OR.KOD.EQ.0) GO TO 80	BIV6054
61	KFLG=0	BIV6055
	IF (P(J1).EQ.0.)KFLG=KFLG+1	BIV6056
	IF (P(J2).EQ.0.)KFLG=KFLG+2	BIV6057
	IF (P(J3).EQ.0.)KFLG=KFLG+4	BIV6058
	IF (P(J4).EQ.0.)KFLG=KFLG+8	BIV6059

TABLE D-4. (Continued)

	IF (KFLG.EQ.0) GO TO 70	BIV6060
	KFLL=KFLG	BIV6061
	GO TO (62,64,66,62,62,50,62,64,50,64,64,68,62,64,50),KFLG	BIV6062
62	J1=J1+1	BIV6063
	J2=J2+1	BIV6064
	J3=J3+1	BIV6065
	J4=J4+1	BIV6066
	L1=L1+1	BIV6067
	GO TO 61	BIV6068
64	J1=J1-1	BIV6069
	J2=J2-1	BIV6070
	J3=J3-1	BIV6071
	J4=J4-1	BIV6072
	L1=L1-1	BIV6073
	GO TO 61	BIV6074
66	J1=J1+LH+1	BIV6075
	J2=J2+LH+1	BIV6076
	J3=J3+LH+1	BIV6077
	J4=J4+LH+1	BIV6078
	L3=L3+LH+1	BIV6079
	GO TO 61	BIV6080
68	J1=J1-(LH+1)	BIV6081
	J2=J2-(LH+1)	BIV6082
	J3=J3-(LH+1)	BIV6083
	J4=J4-(LH+1)	BIV6084
	L3=L3-(LH+1)	BIV6085
	GO TO 61	BIV6086
70	Z1=ABS(P(J1))+(ABS(P(J2))-ABS(P(J1)))/(P(L1+1)-P(L1))	BIV6087
	1 *(XH-P(L1 ))	BIV6088
	Z2=ABS(P(J3))+(ABS(P(J4))-ABS(P(J3)))/(P(L1+1)-P(L1))	BIV6089
	1 *(XH-P(L1 ))	BIV6090
75	L4=L3-LH-1	BIV6091
	BIV= Z1+(Z2-Z1)/(P(L3)-P(L4)) *(XV-P(L4))	BIV6092
	IF (KOD.EQ.0.OR.KOD.EQ.32765) GO TO 79	BIV6093
	IF (TIME.EQ.M(1)) GO TO 76	BIV60931
	IF (TIME1.EQ.M(11)) GO TO 79	BIV60932
	TIME=M(1)	BIV60933
76	IF (TIME1.NE.M(11)) WRITE (6,92)	BIV60934
	TIME1=M(11)	BIV60935
	WRITE (6,93) K,KOD,XH,XV,BIV	BIV60936
	IF (KFLL.NE.0) WRITE (6,91) K,KOD ,XV,XH,BIV	BIV60937
79	RETURN	BIV6094
80	Z1= (P(J1))+( (P(J2))- (P(J1)))/(P(L1+1)-P(L1))	BIV6095
	1 *(XH-P(L1 ))	BIV6096
	Z2= (P(J3))+( (P(J4))- (P(J3)))/(P(L1+1)-P(L1))	BIV6097
	1 *(XH-P(L1 ))	BIV6098
	GO TO 75	BIV6099
90	FORMAT (24HOEFF BIVARIATE CURVE NO. 15,16H. VERTICAL I.V.=E12.4,	BIV6100
	1 18H, HORIZONTAL I.V.=E12.4,1H.)	BIV6101
91	FORMAT (29HOEXTRAPOLATION USED FOR CURVE 15, 7H, FLAG=I3,	BIV6102
	1 16H. VERTICAL I.V.=E12.4,18H, HORIZONTAL I.V.=E12.4,	BIV6103
	2 11H, DEP.VAR.=E12.4)	BIV6104
92	FORMAT (47HODERIVED VALUES USED IN THE FOLLOWING CURVES... )	BIV6106
93	FORMAT (20H BIVARIATE CURVE NO. 16,8H COD = I6,	BIV6107
	1 11H X(HOR) = E12.4,12H X(VERT) = E12.4,12H Y VALUE =E12.4)	BIV6108
	END	BIV6109



TABLE D-4. (Continued)

SIBFTC	LIN6	LIN6000
	REAL FUNCTION LIN (X, N)	LIN6001
C	AS OF 5/25/65	LIN6002
C		LIN6003
C	Y=LINEAR FUNCTION OF X GIVEN BY CURVE N	LIN6004
C		LIN6005
	COMMON P, M	LIN6006
	COMMON /CP2/ ERROR	LIN6007
	DIMENSION P(16000), M(16), KP(1)	LIN6008
	EQUIVALENCE (P(1), KP(1))	LIN6009
	REAL M	LIN6010
	KOD=32765	LIN6011
	PER = 32767.	LIN6012
	LL = LOC(N)	LIN6013
	LL = LL + 1	LIN6014
	NFLAG = 1	LIN6015
	IF (KP(LL), .NE. KOD) GO TO 1	LIN6016
	KOD=KP(LL+1)	LIN6017
	LL=LL+2	LIN6018
1	IF (P(LL-1).NE.PER) GO TO 3	LIN6019
2	PER = P(LL)	LIN6020
	LL = LL + 1	LIN6021
	NFLAG = 2	LIN6022
3	LU = LL	LIN6023
	J = LL	LIN6024
5	LU = LU + 2	LIN6025
	IF (P(LU) - P(J)) 7, 6, 6	LIN6026
6	J = LU	LIN6027
	GO TO 5	LIN6028
7	LU = LU - 1	LIN6029
	LV=LU+2	LIN6030
8	IF (X - P(LL)) 9, 10, 10	LIN6031
9	PERX=-PER	LIN6032
	GO TO (40, 18), NFLAG	LIN6033
10	IF (P(LU - 1) - X) 12, 25, 25	LIN6034
12	PERX= PER	LIN6035
	GO TO (40, 18), NFLAG	LIN6036
18	IF (ABS((P(LU-1)-P(LL))/PER-1.).GT.PER*1.E-6) GO TO 40	LIN6037
	DO 20 J = LL, LV, 2	LIN6038
	P(J) = P(J) + PERX	LIN6039
20	CONTINUE	LIN6040
	GO TO 8	LIN6041
25	LL = LL + 2	LIN6042
	DO 28 J = LL, LU, 2	LIN6043
	IF (X - P(J)) 27, 27, 28	LIN6044
27	IF (KOD.NE.32765) GO TO 272	LIN6045
271	LIN=(P(J+1)-P(J-1))/(P(J)-P(J-2))*(X-P(J-2))+P(J-1)	LIN6046
	GO TO 50	LIN6047
272	LIN=(ABS(P(J+1))-ABS(P(J-1)))/(P(J)-P(J-2))*(X-P(J-2))+ABS(P(J-1))	LIN6048
	IF (KOD.EQ.0) GO TO 50	LIN6049
76	FORMAT (47HODERIVED VALUES USED IN THE FOLLOWING CURVES... )	LIN6050
	IF (TIME.EQ.M(1)) GO TO 80	LIN6051
	IF (TIME1.EQ.M(11)) GO TO 50	LIN60511
	TIME=M(1)	LIN6052
80	IF (TIME1.NE.M(11)) WRITE (6,76)	LIN60521
	TIME1=M(11)	LIN60522
	WRITE (6,77) N,KOD,X,LIN	LIN6053
77	FORMAT (11H CURVE NO.= 16, 8H COD = 15,25H INDEPENDENT VARIABLE	LIN6054
	1E = E12.4,23H DEPENDENT VARIABLE = E12.4)	LIN6055
	GO TO 50	LIN6056
28	CONTINUE	LIN6057

TABLE D-4. (Continued)

```

LL = LL - 2
40 WRITE (6, 42) X, N
WRITE (6, 73) (P(I), I = LL, LU)
73 FORMAT(29HOCURVE POINT PAIRS FOLLOW.... /(1X,3(2E18.8,4X)))
42 FORMAT (27H0INDEP VAR FOR LIN INTERP.= E 20.8, 7H CURVE= I 4 ,
1 16H OFF CURVE )
IF (ERROR.EQ.0.) WRITE (6, 75)
75 FORMAT (30H0 LAST TIME POINT CALCULATED )
M(8)=1.
IF (ERROR.EQ.0.) ERROR=2.
50 RETURN
END

```

```

LIN6058
LIN6059
LIN6060
LIN6061
LIN6062
LIN6063
LIN6064
LIN6065
LIN6066
LIN6067
LIN6068
LIN6069

```

```

$IBFTC ATR6
FUNCTION ATRP 1 (C, X)
C AS OF 12/4/64
DIMENSION C(1)
I = 5
IF (C(1) - X) 3, 3, 1
1 IF (C(I + 2) - C(I)) 16, 17, 17
17 I = I + 4
GO TO 1
16 J = I + 3
ATRP 1 = C(J)
18 WRITE (6, 101) X, (C(K), K = 1, J)
101 FORMAT (13H OFF CURVE X= E 16.8/(1H 2E 16.8))
RETURN
3 IF (X - C(I)) 4, 4, 5
4 TELA = (C(I - 1) - C(I - 3))/(C(I - 2) - C(I - 4))
TELB = (C(I + 1) - C(I - 1))/(C(I) - C(I - 2))
ATRP 1 = C(I - 3) + (X - C(I - 4))*TELA + (X - C(I - 4))*(X - C(I
1 - 2))*(TELB - TELA)/(C(I) - C(I - 4))
RETURN
5 IF (C(I + 2) - C(I)) 6, 6, 7
6 ATRP 1 = C(I + 1)
J = I + 2
GO TO 18
7 I = I + 4
GO TO 3
END

```

TABLE D-4. (Continued)

```

SIRFTC PAR6
      FUNCTION PAR (X, N)
C      AS OF 04/27/65
C
C      Y=PARABOLIC FUNCTION OF X GIVEN BY CURVE N
C
      COMMON P, M
      DIMENSION P(16000), M(16), C(8)
      REAL M
      PER = 32767.
      LL = LOC(N)
      LL = LL + 1
      NFLAG = 1
2      IF (P(LL - 1) - PER) 3, 2, 3
      PER = P(LL)
      LL = LL + 1
      NFLAG = 2
3      LU = LL
      J = LL
5      LU = LU + 2
      IF (P(LU) - P(J)) 7, 6, 6
6      J = LU
      GO TO 5
7      LU = LU - 1
8      IF (X - P(LL)) 9, 10, 10
9      GO TO (40, 14), NFLAG
10     IF (P(LU - 1) - X) 12, 25, 25
12     GO TO (40, 18), NFLAG
14     DO 15 J = LL, LU, 2
      P(J) = P(J) - PER
15     CONTINUE
      GO TO 8
18     DO 20 J = LL, LU, 2
      P(J) = P(J) + PER
20     CONTINUE
      GO TO 8
25     LL = LL + 4
      DO 28 J = LL, LU, 4
      IF (X - P(J)) 27, 27, 28
27     LL = J - 4
      GO TO 44
28     CONTINUE
      LL = LL - 4
40     WRITE (6, 42) X, N
42     FORMAT (27HOINDEP VAR FOR PAR INTERP.= E 20.8, 7H CURVE= I 4 ,
1 16H OFF CURVE )
      WRITE (6, 43) (P(I), I = LL, LU)
43     FORMAT (16HOCURVE POINTS = 4E 18.8)
      CALL PRINT
      CALL EXIT
      STOP
44     LU = LL + 5
      I = 0
      DO 45 J = LL, LU
      I = I + 1
      C(I) = P(J)
45     CONTINUE
      C(I + 1) = 0.
      PAR = ATRP 1(C, X)
      RETURN
      END

```

TABLE D-4. (Continued)

SIRFTC	MMF6	MMF6000
	SUBROUTINE MMF (T1,T2,NN,MM)	MMF6001
C	AS OF 04/27/65	MMF6002
	COMMON P,M,MAXT,MAXR,MAXC,KSP,KST,KURV7,NCVG,NSTS,NFAB	MMF6003
	COMMON NABL,NKSP,LMMF,NRMF,NREAD	MMF6004
	DIMENSION P(16000),M(16),NABL(10),KNOD(1)	MMF6005
	EQUIVALENCE (P(1),KNOD(1))	MMF6006
	REAL M	MMF6007
301	FORMAT (7012)	MMF6008
	GO TO (1,2,3,770),LMMF	MMF6009
1	NRMF=0	MMF6010
	REWIND 10	MMF6011
	REWIND 9	MMF6012
	NP=0	MMF6013
	NREAD=0	MMF6014
	KCY=0	MMF6015
	LMMF=2	MMF6016
2	NRMF=NRMF+1	MMF6017
	WRITE (10,301) T1,T2,NN,MM	MMF6018
	L=LOC(NN)	MMF6019
100	L=L+1	MMF6020
	NDN=P(L)	MMF6021
	IF (NDN) 770,770,101	MMF6022
101	KNOD(L)=KCY+4096*(NP+4096*NDN)	MMF6023
	NDN=KNOD(L)/16777216	MMF6024
	NP=MOD(KNOD(L)/4096,4096)	MMF6025
	KCY=MOD(KNOD(L),4096)	MMF6026
	GO TO 100	MMF6027
3	REWIND 10	MMF6028
	DO 60 I=1,NRMF	MMF6029
	READ (10,301) TO,TF,NT,MC	MMF6030
	IF (M(1)-TF) 4,5,60	MMF6031
4	IF (M(1)-TO) 60,5,5	MMF6032
5	L=LOC(NT)	MMF6033
11	L=L+1	MMF6034
	NDN=KNOD(L)/16777216	MMF6035
	NP=MOD(KNOD(L)/4096,4096)	MMF6036
	KCY=MOD(KNOD(L),4096)	MMF6037
	IF (NDN) 60,60,21	MMF6038
21	KCY=KCY+1	MMF6039
	IF (KCY-MC) 50,6,6	MMF6040
6	KCY=0	MMF6041
	NDO=MAXT+NDN	MMF6042
	IF (NP) 22,22,30	MMF6043
22	IF (P(NDN)-P(NDO)) 25,50,24	MMF6044
24	NP=1	MMF6045
	GO TO 50	MMF6046
25	NP=2	MMF6047
	GO TO 50	MMF6048
30	IF (P(NDN)-P(NDO)) 33,50,31	MMF6049
31	GO TO (50,32),NP	MMF6050
32	NPP=1	MMF6051
	GO TO 40	MMF6052
33	GO TO (34,50),NP	MMF6053
34	NPP=2	MMF6054
40	PM1=M(1)-M(5)	MMF6055
	NREAD=NREAD+1	MMF6056
	WRITE (9,301) TO,TF,NT,NP,NDN,P(NDO),PM1	MMF6057
	NP=NPP	MMF6058
50	KNOD(L)=KCY+4096*(NP+4096*NDN)	MMF6059
	GO TO 11	MMF6060

TABLE D-4. (Continued)

60	CONTINUE	MMF6061
	REWIND 10	MMF6062
770	RETURN	MMF6063
	END	MMF6064
\$IBFTC	RAD6	RAD6000
	FUNCTION RAD (N 1, N 2, CV)	RAD6001
C	AS OF 04/27/65	RAD6002
C		RAD6003
C	RADIATION WITH CONSTANT OR VARIABLE FACTOR CV	RAD6004
C		RAD6005
	COMMON P, M, MAXT	RAD6006
	DIMENSION P(16000), M(16)	RAD6007
	REAL M	RAD6008
	SIGK = CV*.1713 E - 8	RAD6009
	J = MAXT + N 1	RAD6010
	T 1 = P(J) + 459.6	RAD6011
	J = MAXT + N 2	RAD6012
	T 2 = P(J) + 459.6	RAD6013
	RAD = 1./(SIGK*(T 1*T 1 + T 2*T 2)*(T 1 + T 2))	RAD6014
	RETURN	RAD6015
	END	RAD6016
\$IBFTC	SAV6	SAV6000
	SUBROUTINE SAV(X,Y)	SAV6001
C	AS OF 04/27/65	SAV6002
	COMMON P(16000),M(16),MAXT,MAXR,MAXC	SAV6003
	COMMON /EXFLG/NTFLG,NSAV,NFLG	SAV6004
	REAL M	SAV6005
	NSAV=0	SAV6006
	IF (X.LT.Y.OR.NFLG.GT.0) GO TO 20	SAV6007
	NFLG=1	SAV6008
	NSAV=1	SAV6009
20	RETURN	SAV6010
	END	SAV6011
\$IBFTC	EA16	EA16000
	SUBROUTINE EAH1 (NODE,QK)	EA16001
C	AS OF 05/07/65	EA16002
	COMMON P,M,MAXT,MAXR,MAXC,KSP,KST	EA16003
	DIMENSION P(16000),M(16)	EA16004
	REAL M	EA16005
	K=2*MAXT+MAXR+MAXC+NODE	EA16006
	KOD=1	EA16007
	ALPHO=0.	EA16008
	MF=0	EA16009
	CALL ECHERT (KOD,NODE,ALPHO,MF,HJ,TER)	EA16010
	P(K)= HJ*QK*TER	EA16011
	RETURN	EA16012
	END	EA16013

TABLE D-4. (Continued)

\$IBFTC EA26	EA26000
SUBROUTINE EAH 2 (NODE, QK, VAR)	EA26001
AS OF 04/27/65	EA26002
C  COMMON P, M, MAXT, MAXR, MAXC, KSP, KST	EA26003
DIMENSION P(16000), M(16)	EA26004
REAL M	EA26005
K = 2*MAXT + MAXR + MAXC + NODE	EA26006
KOD = 1	EA26007
ALPHO = 0.	EA26008
MF = 0	EA26009
CALL ECHERT (KOD, NODE, ALPHO, MF, HJ, TER)	EA26010
P(K) = HJ*QK*TER	EA26011
VAR = HJ	EA26012
RETURN	EA26013
END	EA26014
\$IBFTC EA36	EA36000
SUBROUTINE EAH 3 (NODE, QK, ALPHO, MF)	EA36001
AS OF 04/27/65	EA36002
C  COMMON P, M, MAXT, MAXR, MAXC, KSP, KST	EA36003
DIMENSION P(16000), M(16)	EA36004
REAL M	EA36005
KOD = 2	EA36006
CALL ECHERT (KOD, NODE, ALPHO, MF, HJ, TER)	EA36007
K = 2*MAXT + MAXR + MAXC + NODE	EA36008
P(K) = HJ*QK*TER	EA36009
RETURN	EA36010
END	EA36011
\$IBFTC EA46	EA46000
SUBROUTINE EAH 4 (NODE, QK, VAR, ALPHO, MF)	EA46001
AS OF 04/27/65	EA46002
C  COMMON P, M, MAXT, MAXR, MAXC, KSP, KST	EA46003
DIMENSION P(16000), M(16)	EA46004
REAL M	EA46005
K = 2*MAXT + MAXR + MAXC + NODE	EA46006
KOD = 2	EA46007
CALL ECHERT (KOD, NODE, ALPHO, MF, HJ, TER)	EA46008
P(K) = HJ*QK*TER	EA46009
VAR = HJ	EA46010
RETURN	EA46011
END	EA46012

TABLE D-4. (Continued)

SIBFTC EAH6	EAH6000
SUBROUTINE ECHERT (KOD, NODE, ALPHO, K, HJ, TER)	EAH6001
AS OF 04/27/65	EAH6002
C	EAH6003
C	EAH6004
C	EAH6005
AERODYNAMIC HEATING USING ECHERT FORMULA	EAH6006
COMMON P, M, MAXT, MAXR, MAXC, KSP, KST, KURV 7	EAH6007
DIMENSION P(16000), M(16)	EAH6008
REAL M, LIN	EAH6009
GO TO (1, 2), KOD	EAH6010
1  BETHA = 1.	EAH6011
GO TO 15	EAH6012
2  ALPHR = LIN(M(1), 2)	EAH6013
IF (K) 3, 3, 4	EAH6014
3  ALPHA = ALPHO - ALPHR	EAH6015
GO TO 5	EAH6016
4  ALPHA = ALPHR - ALPHO	EAH6017
5  IF (KURV 7 - 3) 7, 7, 6	EAH6018
6  BETHA = LIN(ALPHA, 7)	EAH6019
GO TO 15	EAH6020
7  J = LOC(7)	EAH6021
IF (ALPHA) 8, 8, 10	EAH6022
8  BETHA = P(J + 2)*ALPHA + 1.	EAH6023
GO TO 15	EAH6024
10  BETHA = P(J + 1)*ALPHA + 1.	EAH6025
15  QMAX = LIN(M(1), 11)	EAH6026
S = LIN(QMAX, 5)	EAH6027
H = LIN(M(1), 1)	EAH6028
ALRDXM = LIN(H, 3)	EAH6029
TLDTM = LIN(QMAX, 6)	EAH6030
TMAX = LIN(H, 12)	EAH6031
TL = TLDTM*TMAX	EAH6032
QMLDMM = LIN(QMAX, 13)	EAH6033
QML = QMLDMM*QMAX	EAH6034
J = LOC(8)	EAH6035
A = P(J + 1)	EAH6036
B = P(J + 2)	EAH6037
QL = P(J + 3)	EAH6038
GAMMA = P(J + 4)	EAH6039
QN = 0.71**QL*((GAMMA - 1.)/2.)*QML**2	EAH6040
J = MAXT + NODE	EAH6041
TLPDTL = 0.5*(1. + (P(J) + 459.6)/TL) + 0.22*QN	EAH6042
TLP = TLPDTL*TL	EAH6043
TR = TL*(1. + QN)	EAH6044
M(12) = TR	EAH6045
ALPRK = LIN(TLP, 4)	EAH6046
PRK = 10.0**ALPRK	EAH6047
RLDXM = 10.0**ALRDXM	EAH6048
HJ = BETHA*(S*RLDXM*QMAX/TLPDTL**1.69)**A*QMAX**B*PRK	EAH6049
TER = TR - P(J) - 459.6	EAH6050
RETURN	EAH6051
END	

TABLE D-4. (Continued)

SIBFTC	CVG6	CVG6000
	SUBROUTINE CVG (A, N, M 2)	CVG6001
C	AS OF 04/26/65	CVG6002
C		CVG6003
C	CONVERGE ROUTINE FINDS EQUILIBRIUM STARTING TEMPERATURES	CVG6004
C		CVG6005
	COMMON P, M, MAXT, MAXR, MAXC, KSP, KST, KURV 7, NCVG, NSTS, NFAB	CVG6006
	COMMON NABL, NKSP	CVG6007
	DIMENSION P(16000), M(16), NABL(10), KPSD(1)	CVG6008
	EQUIVALENCE (P(1), KPSD(1))	CVG6009
	COMMON /EXCVG/ NFLAG, ITMAX, ITER, NODE, PM1, PM, DTO, ATEM, NTEM, MTEM	CVG6010
	COMMON /CP2/ ERROR	CVG6011
	REAL M	CVG6012
1	GO TO (2, 8, 8, 6), NCVG	CVG6013
2	ITMAX = 0	CVG6014
	ITER = 0	CVG6015
	NODE = 0	CVG6016
	NFLAG = 1	CVG6017
	PM 1 = M(1)	CVG6018
	PM2=M(6)	CVG6019
	PM3=M(9)	CVG6020
	DTO = 0.	CVG6021
	ATEM = A	CVG6022
	NTEM = N	CVG6023
7	MTEM = M 2	CVG6024
	IF (MTEM) 4, 3, 5	CVG6025
3	WRITE (6, 50)	CVG6026
50	FORMAT (49H0 NO. OF ITERATIONS BETWEEN PRINTS IS ZERO IN CVG )	CVG6027
51	ERROR = 2.	CVG6028
	RETURN	CVG6029
4	NCVG = 2	CVG6030
	MTEM = IABS(MTEM)	CVG6031
61	M(1)=PM1	CVG6032
	M(6)=PM2	CVG6033
	M(9)=PM3	CVG6034
6	RETURN	CVG6035
5	NCVG = 3	CVG6036
	GO TO 61	CVG6037
8	IF (A) 9, 9, 7	CVG6038
9	DIFM = 0.	CVG6039
20	ITER = ITER + 1	CVG6040
	ITMAX = ITMAX + 1	CVG6041
	JJ = NKSP - 1	CVG6042
	DO 11 I = KSP, JJ	CVG6043
	IF (KPSD(I)) 10, 11, 11	CVG6044
10	JN=MOD(KPSD(I),4096)	CVG6045
	JN=IABS(JN)	CVG6046
	J = MAXT + JN	CVG6047
	DIF = ABS(P(JN) - P(J))	CVG6048
	IF (DIF.LT.DTO) GO TO 303	CVG6049
300	DTMX=0.1*(P(J)+460.)	CVG6050
	IF (DTMX.LT.0.) DTMX=0.	CVG6051
	IF (DIF.LE.DTMX) GO TO 302	CVG6052
	DIF=SIGN(DTMX,(P(JN)-P(J)))	CVG6053
	P(JN)=P(J)+DIF	CVG6054
	GO TO 303	CVG6055
302	P(JN)=(P(JN)+P(J))/2.	CVG6056
303	DIF=ABS(DIF)	CVG6057
	IF (DIF.LE.DIFM) GO TO 11	CVG6058
	DIFM=DIF	CVG6059
	NODE=JN	CVG6060



TABLE D-4. (Continued)

11	CONTINUE	CVG6061
	DTO = DIFM	CVG6062
	J = MAXT + 1	CVG6063
307	DO 308 I = 1, MAXT	CVG6064
	P(J) = P(I)	CVG6065
	J = J + 1	CVG6066
308	CONTINUE	CVG6067
	IF (NFLAG.EQ.1) GO TO 55	CVG6068
	IF (DIFM.GE.ATEM) GO TO 14	CVG6069
13	NCVG = 4	CVG6070
55	ITER = 0	CVG6071
	M(1) = ITMAX	CVG6072
	M(9)=NODE	CVG6073
	M(6)=DTO	CVG6074
56	CALL PRINT	CVG6075
	NFLAG = 2	CVG6076
	GO TO 6	CVG6077
14	IF (ITMAX - NTEM) 15, 16, 16	CVG6078
15	IF (ITER - MTEM) 6, 55, 55	CVG6079
16	M(1) = NTEM	CVG6080
	CALL PRINT	CVG6081
	WRITE (6,60) ITMAX,DTO,NODE	CVG6082
60	FORMAT (33H0TEMPERATURES DID NOT CONVERGE IN I7,12H ITERATIONS.	CVG6083
	1 8H MAX-DT= E12.4, 8H AT NODE I5)	CVG6084
	GO TO 51	CVG6085
	END	CVG6086
	\$IBFTC STS6	STS6000
	SUBROUTINE STS (GK)	STS6001
	AS OF 04/27/65	STS6002
C		STS6003
C		STS6004
C	STEADY STATE FINDS EQUIL. STARTING TEMPS. WITH HEAT BALANCE EQ.	STS6005
C		STS6006
	COMMON P, M, MAXT, MAXR, MAXC, KSP, KST, KURV 7, NCVG, NSTS	STS6007
	DIMENSION P(16000), M(16)	STS6008
	REAL M	STS6009
1	GO TO (2, 10, 10), NSTS	STS6010
2	NSTS = 2	STS6011
	NLAG = 1	STS6012
4	CALL HTBAL (NLAG)	STS6013
	DIFM = 0.	STS6014
	J = MAXT + 1	STS6015
	DO 6 I = 1, MAXT	STS6016
	DIF = ABS(P(I) - P(J))	STS6017
	J = J + 1	STS6018
	IF (DIFM - DIF) 5, 6, 6	STS6019
5	DIFM = DIF	STS6020
6	CONTINUE	STS6021
	J = MAXT + 1	STS6022
	DO 8 I = 1, MAXT	STS6023
	P(J) = P(I)	STS6024
	J = J + 1	STS6025
8	CONTINUE	STS6026
	IF (DIFM - QK) 9, 4, 4	STS6027
9	NSTS = 3	STS6028
10	RETURN	STS6029
	END	

TABLE D-4. (Continued)

	SIBFTC RRM6	RRM6000
	FUNCTION RRM (N 1, N 2, N)	RRM6001
C	AS OF 06/12/65	RRM6002
	COMMON P, M, MAXT	RRM6003
	COMMON /CP2/ERROR	RRM6003
	DIMENSION P(16000), M(16), A(15, 15)	RRM6004
	REAL M	RRM6005
	L = LOC(N)	RRM6006
	KORD = P(L + 1)	RRM6007
	IF (KORD.GT.15) GO TO 60	RRM60071
	L = L + 2	RRM6008
	K = L + KORD*KORD	RRM6009
	NSB 1 = 0	RRM6010
	NSB 2 = 0	RRM6011
	KOUNT = 0	RRM6012
	K 2 = K + 4*KORD - 1	RRM6013
	J = 0	RRM6014
	DO 18 I = K, K 2, 4	RRM6015
	J = J + 1	RRM6016
	NODE = P(I)	RRM6017
	IF (NODE - N 1) 4, 4, 5	RRM6018
4	A 1 = P(I + 1)	RRM6019
	E 1 = P(I + 2)	RRM6020
	RHO 1 = P(I + 3)	RRM6021
	NSB 1 = J	RRM6022
	GO TO 17	RRM6023
5	IF (NODE - N 2) 18, 6, 18	RRM6024
6	A 2 = P(I + 1)	RRM6025
	E 2 = P(I + 2)	RRM6026
	RHO 2 = P(I + 3)	RRM6027
	NSB 2 = J	RRM6028
17	KOUNT = KOUNT + 1	RRM6029
	IF (KOUNT - 2) 18, 20, 19	RRM6030
18	CONTINUE	RRM6031
19	WRITE (6, 70) N 1, N 2, N	RRM6032
70	FORMAT (7H0 NODE 1 4, 3HOR 1 4, 24HDOES NOT APPEAR IN TABLE 16)	RRM6033
	GO TO 80	RRM6035
20	A 1 = A 1*A 2	RRM6037
	E 1 = E 1*E 2	RRM6038
	RHO 1 = RHO 1*RHO 2	RRM6039
	LTEM = L	RRM6040
	K = 0	RRM6041
	K 2 = 0	RRM6042
	DO 42 I = 1, KORD	RRM6043
	IF (I - NSB 1) 21, 21, 22	RRM6044
21	L = L + KORD	RRM6045
	GO TO 42	RRM6046
22	K = K + 1	RRM6047
	DO 40 J = 1, KORD	RRM6048
	IF (J - NSB 2) 23, 39, 24	RRM6049
24	K 2 = K 2 + 1	RRM6050
	A(K, K 2) = P(L)	RRM6051
39	L = L + 1	RRM6052
40	CONTINUE	RRM6053
	K 2 = 0	RRM6054
42	CONTINUE	RRM6055
	NN = KORD - 1	RRM6056
	CALL MDETR (NN, A)	RRM6057
	DIJ = C	RRM6058
	L = LTEM	RRM6059
	DO 50 I = 1, KORD	RRM6060

TABLE D-4. (Continued)

	DO 50 J = 1, KORD	RRM6061
	A(I, J) = P(L)	RRM6062
	L = L + 1	RRM6063
50	CONTINUE	RRM6064
	CALL MDETR (KORD, C, A)	RRM6065
	QK = (0.4811 E - 12 * E 1 * A 1) / (0.1713 E - 8 * RHO 1) * ABS(DIJ / C)	RRM6066
	JN1 = MAXT + N1	RRM6067
	JN2 = MAXT + N2	RRM6068
	T1 = P(JN1) + 460.	RRM6069
	T2 = P(JN2) + 460.	RRM6070
	RRM = 1. / (0.1713 E - 8 * QK * (T1 * T1 + T2 * T2) * (T1 + T2))	RRM6071
	RETURN	RRM6072
60	WRITE (6, 61) N, KORD	RRM6073
61	FORMAT (10H OTABLE NO. I6, 17H HAS MATRIX ORDER I6, 1 30H, MAXIMUM IS 15. CASE DELETED. )	RRM6074
80	ERROR = 2.	RRM6075
	RETURN	RRM6076
	END	RRM6077

	\$IBFTC MDT6	MDT6000
	SUBROUTINE MDETR (N, C, A)	MDT6001
C	AS OF 12/4/64	MDT6002
	DIMENSION A(15, 15), B(16)	MDT6003
	LN = N - 1	MDT6004
	DO 18 I = 1, LN	MDT6005
	MI = I + 1	MDT6006
	DO 18 K = MI, N	MDT6007
	IF (A(I, I)) 19, 3, 19	MDT6008
3	K 1 = I + 1	MDT6009
	DO 6 K 2 = K 1, N	MDT6010
	IF (A(I, K 2)) 4, 6, 4	MDT6011
4	DO 5 JJ = 1, N	MDT6012
	B(JJ) = A(JJ, K 2)	MDT6013
	A(JJ, K 2) = A(JJ, I)	MDT6014
	A(JJ, I) = - B(JJ)	MDT6015
5	CONTINUE	MDT6016
	GO TO 19	MDT6017
6	CONTINUE	MDT6018
	C = 0.0	MDT6019
	GO TO 100	MDT6020
19	AA = A(K, I) / A(I, I)	MDT6021
	DO 18 J = I, N	MDT6022
17	A(K, J) = A(K, J) - AA * A(I, J)	MDT6023
18	CONTINUE	MDT6024
	B(1) = 1.0	MDT6025
	DO 32 L = 1, N	MDT6026
	B(L + 1) = B(L) * A(L, L)	MDT6027
32	CONTINUE	MDT6028
	C = B(N + 1)	MDT6029
100	RETURN	MDT6030
	END	MDT6031

TABLE D-4. (Continued)

SIBFTC	SVT6	SVT6000
	SUBROUTINE SAVT3	SVT6001
C	AS OF 06/04/65	SVT6002
	COMMON P(16000),M(16),MAXT,MAXR,MAXC,NDUMY(20),DUMMY(12),NR,	SVT6003
	1 MAXP,MAXK,MAXS,MAXM	SVT6004
	COMMON /EXFLG/NTFLG,NSAV,NFLG	SVT6005
	DIMENSION LX(9)	SVT6006
	REAL M	SVT6007
	NSAV=0	SVT6008
	REWIND 3	SVT6009
	LX(1)=MAXT	SVT6010
	LX(2)=MAXT	SVT6011
	LX(3)=MAXR	SVT6012
	LX(4)=MAXC	SVT6013
	LX(5)=MAXC	SVT6014
	LX(6)=MAXC	SVT6015
	LX(7)=MAXP	SVT6016
	LX(8)=MAXK	SVT6017
	LX(9)=MAXS	SVT6018
	L2=0	SVT6019
	DO 10 I=1,9	SVT6020
	L1=L2+1	SVT6021
	L2=L2+LX(I)	SVT6022
	WRITE (3) LX(I),L1,L2	SVT6023
	WRITE (3) (P(J),J=L1,L2)	SVT6024
10	CONTINUE	SVT6025
	L1=1	SVT6026
	L2=MAXM	SVT6027
	WRITE (3) MAXM,L1,L2	SVT6028
	WRITE (3) (M(I),I=L1,L2)	SVT6029
	END FILE 3	SVT6030
	REWIND 3	SVT6031
	RETURN	SVT6032
	END	SVT6033

TABLE D-4. (Continued)

SIBFTC TPT6	TPT6000
SUBROUTINE TPL0T(NMB)	TPT6001
C    AS OF 06/05/65	TPT6002
C    FOR THERMAL ANALYSER ROUTINE	TPT6003
C    THIS ROUTINE PUTS ALL POINTS OF CURVE WITH RESPECT TO TIME RANGE,	TPT6004
C    AND NMB ON BINARY TAPE	TPT6005
C    ROUTINE WILL ONLY HANDLE 20 CURVES WITH 20 NODES PER CURVE	TPT6006
COMMON /CPPLT/NPLT,NEND	TPT6007
COMMON /EXSTA/ NC,NCUR1,NCURV	TPT6008
COMMON / EXPLT/ NLFLG	TPT6009
COMMON P,M,MAXT,MAXR,MAXC	TPT6010
DIMENSION P(16000),M(16) ,T(20) ,NCURV(20),NODE(20)	TPT6011
REAL M	TPT6012
C    NMB = CURVE NUMBER	TPT6013
C    K = NUMBER OF TEMPERATURE CURVES TO BE PLOTTED PER CURVE NMB.	TPT6014
C    P(L+1) = INTIAL TIME--THETA I	TPT6015
C    P(L+2) = FINAL TIME --THETA F	TPT6016
C    P(L+3) = TIME INCREMENT--DELTA THETA	TPT6017
IF (NLFLG.LE.1) NLFLG=1	TPT6018
NPLT=2	TPT6019
GO TO (1 , 2 , 5 ) , NLFLG	TPT6020
1    IF (NMB .LE. 0) GO TO 30	TPT6021
NCUR1 = NMB	TPT6022
NLFLG = 2	TPT6023
NC = 1	TPT6024
IF (NC.LE.20) GO TO 2	TPT6025
WRITE (6,102) NC	TPT6026
102  FORMAT ( 1H0,I5,26H IS TOO MANY PLOT CURVES.)	TPT6027
GO TO 30	TPT6028
3    NCURV(NC) = NMB	TPT6029
GO TO 30	TPT6030
2    IF (NMB .LE. 0) GO TO 4	TPT6031
IF (NCUR1 .EQ. NMB) GO TO 4	TPT6032
NC = NC + 1	TPT6033
NCURV(NC) = NMB	TPT6034
GO TO 30	TPT6035
4    NLFLG = 3	TPT6036
5    IF (NMB .GT. 0) GO TO 30	TPT6037
TIME = M(1)	TPT6038
DO 28 I1 = 1 , NC	TPT6039
NTAB= NCURV(I1)	TPT6040
K = 0	TPT6041
L = LOC(NTAB)	TPT6042
N = L+4	TPT6043
13  IF (TIME.LT.P(L+1).OR .TIME.GT.P(L+2)) GO TO 28	TPT6044
15  J = P(N)	TPT6045
IF (J.EQ.0) GO TO 17	TPT6046
N = N+1	TPT6047
K = K+1	TPT6048
IF (K.LE.20) GO TO 16	TPT6049
WRITE (6,101) NTAB	TPT6050
P(N-1)=0.	TPT6051
GO TO 17	TPT6052
101  FORMAT (15H0PLOT CURVE NO. I5,25H HAS MORE THAN 20 POINTS.)	TPT6053
16  NODE(K) = J	TPT6054
NN = J + MAXT	TPT6055
T(K) = P(NN)	TPT6056
GO TO 15	TPT6057
17  IF (K.LT.1) GO TO 28	TPT6058
25  WRITE (11)NTAB,K,(NODE(I),I=1,K),P(L+1),P(L+2),P(L+3),M(1),	TPT6059
1 (T(I),I=1,K)	TPT6060

TABLE D-4. (Continued)

	P(L+1) = P(L+1)+P(L+3)	
28	CONTINUE	TPT6061
30	RETURN	TPT6062
	END	TPT6063
		TPT6064
SIBFTC	PNT6	PNT6000
	SUBROUTINE PUNCH(TIME,N1,N2)	PNT6001
C	AS OF 04/27/65	PNT6002
	COMMON P(16000),M(16),MAXT,NDUM(22),CC(12)	PNT6003
	REAL M	PNT6004
	IF (M(1),NF.TIME) RETURN	PNT6005
	NA=N1+MAXT	PNT6006
	IF (N1.EQ.0) NA=1+MAXT	PNT6007
	NB=N2+MAXT	PNT6008
	IF (N2.EQ.0) NB=MAXT+MAXT	PNT6009
	DO 10 I=NA,NB	PNT6010
	IF (I.EQ.NA.OR.I.EQ.NB) GO TO 9	PNT6011
	IF (P(I).EQ.P(I-1)) GO TO 10	PNT6012
9	IX=I-MAXT	PNT6013
	ISEQ=IX+10000	PNT6014
	PUNCH 11,IX,P(I),CC(1),CC(2),TIME,ISEQ	PNT6015
10	CONTINUE	PNT6016
	RETURN	PNT6017
11	FORMAT (5HDEC01,I5,F10.2, 7X,A6,A3,5H - ATF7.0,8H SECONDS,	PNT6018
	1 11X,I5,8X)	PNT6019
	END	PNT6020
SIBFTC	TNK6	TNK6001
	SUBROUTINE TANKA(N)	TNK6002
	WRITE (6,10)	TNK6003
	RETURN	TNK6004
10	FORMAT (42HOCALL TO TANKA IS ILLEGAL IN THIS VERSION.)	TNK6005
	END	TNK6006

TABLE D-4. (Continued)

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$IBFTC BTP6                                BTP6000
SUBROUTINE BITAP                            BTP6001
C AS OF 05/07/65                            BTP6002
C ROUTINE FOR CAL-COMP PLOTTER              BTP6003
C FOR THERMAL ANALYSER                     BTP6004
COMMON /CPPLT/NPLT,NEND,KSKIP              BTP6005
COMMON P,M,NX(23),CC(12)                  BTP6006
DIMENSION P(16000),M(16),XP(1),YP(1),TEMP(20),KURV(20),BTP6007
1 XS(2),YS(2),TITLE(3),XTITLE(3),YTITLE(4),BCD(10), BTP6008
2 TNODE(20),KNOD(20),TITLEN(2),BUFFER(914) BTP6009
EQUIVALENCE (P(10000),XP(1)),(P(11000),YP(1)) BTP6010
REAL M                                      BTP6011
KSKIP = 1                                  BTP6012
NOK=5                                       BTP6013
HT = .14                                    BTP6014
ERR = 0.0                                   BTP6015
NRECD = 0                                   BTP6016
NTRECD = 0                                  BTP6017
IDONE = 8888                               BTP6018
WRITE (11) IDONE,KSKIP,(P(I),I=1,6)        BTP6019
C NTAB = TABLE (CURVE) NUMBER              BTP6020
C NC = NUMBER OF DIFFERENT CURVES WITH POINTS BTP6021
C NT = NUMBER OF TEMPERATURE POINTS PER CURVE NUMBER BTP6022
C TIMI = INITIAL TIME                      BTP6023
C TIMF = FINAL TIME                        BTP6024
C DTIM = DELTA TIME                        BTP6025
C TIM = CURRENT TIME                       BTP6026
C TEMP(I)...I=1,NT.. = TEMPERATURES        BTP6027
DATA (TITLE(I),I=1,3) /6HCURVE,6HNUMBER,6H= / BTP6028
DATA (XTITLE(I),I=1,3) /6HTIME,6HSEC.,6H / BTP6029
DATA (YTITLE(I),I=1,4) /6HTEMPER,6HATURE,6HIN DEG,6HREES F/ BTP6030
DATA (TITLEN(I),I=1,2) /6H = NC, 6HDE / BTP6031
DATA (BCD(I),I=1,10) /0150000000000,0160000000000,0170000000000, BTP6032
1032000000000,0350000000000,0360000000000,0370000000000,0360000000000, BTP6033
2000,0120000000000,0330000000000/
H = .42
C
PNO = 0.0                                  BTP6035
REWIND 11                                   BTP6036
IEND = 7777                                 BTP6037
YRANGE = 8.0                               BTP6038
XRANGE = 10.0                              BTP6039
1 NTRECD = NTRECD + NRECD + 1              BTP6040
IF (IEND .EQ. IDONE) GO TO 93              BTP6041
NRECD = 1                                   BTP6042
M2 = 200                                    BTP6043
NC = 1                                       BTP6044
KC = 0                                       BTP6045
DO 2 I = 1, NTRECD                         BTP6046
2 READ (11) NTAB                            BTP6047
KURV(NC) = NTAB                            BTP6048
IF (NTAB .EQ. IEND .OR. NTAB .EQ. IDONE) GO TO 93 BTP6049
6 READ (11) NTAB                            BTP6050
IF (NTAB .EQ. IDONE) IEND = 8888          BTP6051
IF (NTAB .EQ. IEND) GO TO 11              BTP6052
NRECD = NRECD + 1                          BTP6053
DO 8 I = 1, NC                             BTP6054
8 IF (KURV(I) .EQ. NTAB) GO TO 6          BTP6055
CONTINUE                                    BTP6056
NC = NC + 1                                 BTP6057
KURV(NC) = NTAB                            BTP6058
BTP6059
BTP6060

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TABLE D-4. (Continued)

11	GO TO 6	BTP6061
	REWIND 11	BTP6062
	KC = KC + 1	BTP6063
	IF (KC .GT. NC) GO TO 1	BTP6064
	YS(2) = 0.	BTP6065
	YS(1) = 1.E16	BTP6066
	N = 0	BTP6067
	NFLAG = 1	BTP6068
	K = 0	BTP6069
	DO 3 I = 1 , NTRECD	BTP6070
3	READ (11) NTAB	BTP6071
	BACKSPACE 11	BTP6072
	DO 16 KK = 1 , NRECD	BTP6073
	READ (11) NTAB,NT,(KNOD(I),I=1,NT),TIMI,TIMF,DTIM,TIM,	BTP6074
	1 (TEMP(I),I=1,NT)	BTP6075
	IF (KURV(KC) .NE. NTAB) GO TO 16	BTP6076
	GO TO (12,13) , NFLAG	BTP6077
12	XS(2) = TIMF	BTP6078
	XS(1) = TIMI.	BTP6079
	DO 15 I=1,NT	BTP6080
15	TNODE(I) = KNOD(I)	BTP6081
	NFLAG = 2	BTP6082
	NODES = NT	BTP6083
13	K = K + 1	BTP6084
	P(K) = TIM	BTP6085
	N = N + M2 + K	BTP6086
	DO 14 I = 1 , NT	BTP6087
	P(N) = TEMP(I)	BTP6088
	IF (TEMP(I) .GT. YS(2)) YS(2) = TEMP(I)	BTP6089
	IF (TEMP(I) .LT. YS(1)) YS(1) = TEMP(I)	BTP6090
	N = N + M2	BTP6091
14	CONTINUE	BTP6092
	N = 0	BTP6093
16	CONTINUE	BTP6094
	IF (YS(1).NE.YS(2)) GO TO 17	BTP6095
	YS(1)=YS(1)-1.	BTP6096
	YS(2)=YS(2)+1.	BTP6097
17	YS(1)=YS(1)-(YS(2)-YS(1))/10.	BTP6098
	YS(2)=YS(2)+(YS(2)-YS(1))/10.	BTP6099
	REWIND 11	BTP6100
	NPTS = K	BTP6101
	MM = 0	BTP6102
	N = 0	BTP6103
	IF (KSKIP .GT. 1) GO TO 20	BTP6104
C	DETERMINE SCALE AND DRAW AXIS	BTP6105
	CALL PLOTS (BUFFER,914)	BTP6106
	KSKIP = 2	BTP6107
20	CALLASCALE (XS,2,XRANGE,XMIN,DX,1,ERX)	BTP6108
	CALLASCALE (YS,2,YRANGE,YMIN,DY,1,ERY)	BTP6109
	L=2.3 -(ERX-XMIN)/10.	BTP6110
	IF (L.LT.0) L=0	BTP6111
24	CALL XYAXIS(1.,1.,XRANGE,1.,XMIN,DX,L,5.,3.,21,0.,XTITLE,18,0.)	BTP6112
	L=2.3 -(ERY-YMIN)/10.	BTP6113
	IF (L.LT.0) L=0	BTP6114
	CALL XYAXIS(1.,1.,YRANGE,1.,YMIN,DY,L,.1,3.,21,90.,YTITLE,18,90.)	BTP6115
	YN = 6.0	BTP6116
	PNO = PNO + 1.	BTP6117
	KX = 0	BTP6118
25	KX = KX + 1	BTP6119
	N = N + M2	BTP6120
	B = BCD(KX)	BTP6121



TABLE D-4. (Continued)

	MM = MM + 1	BTP6122
	DO 30 I = 1 , NPTS	BTP6123
	K = N + 1	BTP6124
	X = ( P(I) - XMIN) /DX + 1.0	BTP6125
	Y = (P(K) - YMIN) /DY +1.0	BTP6126
	XP(I) = X	BTP6127
	YP(I) = Y	BTP6128
	CALL SYMBL4 (X,Y,H,B,0.0,1)	BTP6129
30	CONTINUE	BTP6130
	CALL LINE (XP,YP,NPTS,1)	BTP6131
	X = XRRANGE + 1.5	BTP6132
	YN = YN - .5	BTP6133
	CALL SYMBL4 (X,YN,H,B,0.0,1)	BTP6134
	CALL SYMBL4 (X,YN,HT,TITLEN,0.0,12)	BTP6135
	X = X + 1.2	BTP6136
	Y = TNODE(MM)	BTP6137
	CALL NUMBER (X,YN,HT,Y,0.0,-1)	BTP6138
	IF (NODES .GT. MM .AND. KX .LT. NOK)GO TO 25	BTP6139
	Y = 9.5	BTP6140
	X = XRRANGE/2. - 3.	BTP6141
	Z = X + 1.8	BTP6142
	CALL SYMBL4 (X,Y,HT,TITLE,0.0,18)	BTP6143
	CALL NUMBER (Z,Y,HT, PNO ,0.0,-1)	BTP6144
	CALL SYMBL4(X,Y-0.3,HT, CC ,0.,61)	BTP6145
	XSPACE = XRRANGE + 7.0	BTP6146
	CALL PLOT (XSPACE,0.0,-3)	BTP6147
	IF (NODES .EQ. MM) GO TO 11	BTP6148
	GO TO 24	BTP6149
93	IF (KSKIP .LE. 1) GO TO 95	BTP6150
	IF (NEND.EQ.0) GO TO 95	BTP6151
94	PRINT 222,PNO	BTP6152
222	FORMAT(37H0 REMOVE PLOT TAPE AND MARK AS HAVING F5.0 ,8H PLOTS )	BTP6153
	CALL TRWEND	BTP6154
	PAUSE 55555	BTP6155
	WRITE(6,222) PNO	BTP6156
95	REWIND 11	BTP6157
	RETURN	BTP6158
	END	BTP6159

TABLE D-4. (Continued)

\$IBFTC	SCL6	SCL6000
	SUBROUTINE ASCALE (X, N, S, YMIN, DY, K, YMAX)	SCL6001
C		SCL6002
C	X - THE GIVEN ARRAY OF VALUES TO BE SCALED, AND THE OUTPUT	SCL6003
C	SCALED VALUES	SCL6004
C	N - NO. OF X VALUES	SCL6005
C	S - NO. OF INCREMENTS	SCL6006
C	YMIN - GENERATED MINIMUM X VALUE, ROUNDED DOWN	SCL6007
C	DY - GENERATED INCREMENT	SCL6008
C	K - SPACING BETWEEN X VALUE STORAGES	SCL6009
C	YMAX = GENERATED MAXIMUM X VALUE, NOT ROUNDED	SCL6010
C		SCL6011
	DIMENSION X(2)	SCL6012
	YMAX = X(1)	SCL6013
	YMIN = X(1)	SCL6014
	NP = N*K	SCL6015
	DO 6 I = K, NP, K	SCL6016
	IF (YMAX .LT. X(I)) YMAX = X(I)	SCL6017
	IF (YMIN .GT. X(I)) YMIN = X(I)	SCL6018
6	CONTINUE	SCL6019
	IF (YMIN .NE. YMAX) GO TO 20	SCL6020
	DX = 1.0	SCL6021
	YMIN = YMIN - (S/2.0)*DX	SCL6022
	GO TO 36	SCL6023
20	DX = (YMAX - YMIN)/S	SCL6024
	NA = 0	SCL6025
	IF (DX - 1.) 25, 36, 30	SCL6026
25	DX = DX*10.	SCL6027
	NA = NA + 1	SCL6028
	IF (DX .LT. 1. .OR. DX .GE. 10.) GO TO 25	SCL6029
	GO TO 35	SCL6030
30	IF (DX .GE. 1. .AND. DX .LT. 10.) GO TO 35	SCL6031
	DX = DX/10.	SCL6032
	NA = NA + 1	SCL6033
	GO TO 30	SCL6034
35	IF (DX .GT. 4.) DY = 10.**(NA + 1)	SCL6035
	IF (DX .LE. 4.) DY = 4.*10.**NA	SCL6036
	IF (DX .LE. 2.) DY = 2.*10.**NA	SCL6037
36	RNDFTR = -0.9	SCL6038
	IYMIN = YMIN/DY + RNDFTR	SCL6039
	YMIN = FLOAT(IYMIN)*DY	SCL6040
	DO 40 I = 1, NP, K	SCL6041
	X(I) = (X(I)-YMIN)/DY	SCL6042
40	CONTINUE	SCL6043
	RETURN	SCL6044
	END	SCL6045

TABLE D-4. (Continued)

SIBFTC	AXS6	AXS6000
	SUBROUTINE XYAXIS(XORG,YORG,ALNGTH,SCDT,AMIN,DA,N,XLAB,	AXS6001
	1 YLAB,HLAB,ALAB,HEAD,NC,AXANG)	AXS6002
C		AXS6003
C	XORG - X COORDINATE OF FIRST POINT ON AXIS	AXS6004
C	YORG - Y COORDINATE OF FIRST POINT ON AXIS	AXS6005
C	ALNGTH-LENGTH OF AXIS IN INCHES - TOTAL	AXS6006
C	SCDT -LENGTH IN INCHES BETWEEN TICK MARKS	AXS6007
C	AMIN -LABEL VALUE OF FIRST POINT ON AXIS	AXS6008
C	DA -SCALE VALUE PER INCH OF LABEL VALUES	AXS6009
C	N -NUMBER OF DECIMAL PLACES FOR AXIS LABEL VALUES	AXS6010
C	XLAB -X COORDINATE OF AXIS LABEL	AXS6011
C	YLAB -Y COORDINATE OF AXIS LABEL	AXS6012
C	HLAB -HEIGHT OF AXIS LABEL	AXS6013
C	ALAB -ANGLE OF AXIS LABEL	AXS6014
C	HEAD -AXIS LABEL	AXS6015
C	NC -NUMBER OF CHARACTERS IN AXIS LABEL	AXS6016
C	AXANG -ANGLE OF AXIS	AXS6017
C		AXS6018
	DIMENSION HEAD(3)	AXS6019
	DATA DATK, HNUM/0.07, 0.14/	AXS6020
	DATA PLUG/0.5E-07/	AXS6021
	XCON = 1.0	AXS6022
	YCON = HNUM/2.0	AXS6023
	IF ( AXANG .NE. 0.0 ) GO TO 50	AXS6024
	XCON = 2.0	AXS6025
	YCON = 0.25	AXS6026
50	RLAB = AXANG * 0.01745329	AXS6027
	DELNUM = DA*SCDT	AXS6028
	SRSCDT = SIN(RLAB)*SCDT	AXS6029
	CRSCDT = COS(RLAB)*SCDT	AXS6030
	CR = COS(RLAB)	AXS6031
	SR = SIN(RLAB)	AXS6032
	WNUM = HNUM*6.0/7.0	AXS6033
	ICNT = 0	AXS6034
	ANUM = AMIN	AXS6035
100	NA = N + 3	AXS6036
	IF ( ANUM .EQ. 0.0) ANUM = 0.0	AXS6037
	IF (ANUM .LT. 0.0) NA = NA + 1	AXS6038
	I = 0	AXS6039
105	I = I + 1	AXS6040
	IF (ABS(ANUM) .LT. 10.0**I) GO TO 115	AXS6041
	NA = NA + 1	AXS6042
	GO TO 105	AXS6043
115	ADIST = FLOAT(ICNT)*SCDT	AXS6044
	IF (ADIST .GT. ALNGTH) GO TO 200	AXS6045
	XC = XORG + ADIST*CR - FLOAT(NA)*WNUM/XCON + 0.05	AXS6046
	YC = YORG + ADIST*SR - YCON	AXS6047
	IF (YC .GT. YLAB .AND. YLAB .GT. (YC - SRSCDT) .OR. XC .GT. XLAB	AXS6048
	1 .AND. XLAB .GT. (XC - CRSCDT)) CALL SYMBL 4 (XLAB, YLAB, HLAB,	AXS6049
	2 HEAD, ALAB, NC)	AXS6050
	XNUM = ANUM + PLUG	AXS6051
	CALL NUMBER (XC,YC,HNUM,XNUM,0.0,N)	AXS6052
	ICNT = ICNT + 1	AXS6053
	ANUM = ANUM + DELNUM	AXS6054
	GO TO 100	AXS6055
200	IF (YLAB .GE. (YORG+ALNGTH)) CALL SYMBL4(XLAB,YLAB,HLAB,HEAD ,	AXS6056
	1 ALAB,NC)	AXS6057
	I = 3	AXS6058
205	XC = XORG + FLOAT(ICNT - 1)*CRSCDT	AXS6059
	YC = YORG + FLOAT(ICNT - 1)*SRSCDT	AXS6060

TABLE D-4. (Continued)

CALL PLOT (XC, YC, I)	AXS6061
I = I - 1	AXS6062
IF (I .LT. 1) I = 1	AXS6063
XC = XC - SR*DATK	AXS6064
YC = YC - CR*DATK	AXS6065
CALL PLOT (XC, YC, I)	AXS6066
XC = XC + SR*DATK	AXS6067
YC = YC + CR*DATK	AXS6068
CALL PLOT (XC, YC, I)	AXS6069
ICNT = ICNT - 1	AXS6070
IF (ICNT .LE. 0) RETURN	AXS6071
GO TO 205	AXS6072
END	AXS6073

TABLE D-4. (Continued)

\$IBFTC	MFO6	MFO6000
	SUBROUTINE MFOUT	MFO6001
C	AS OF 04/27/65	MFO6002
	COMMON P,M,MAXT,MAXR,MAXC,KSP,KST,KURV7,NCVG,NSTS,NFAB	MFO6003
	COMMON NABL,NKSP,LMMF,NRMF,NREAD	MFO6004
	DIMENSION P(16000),M(16),NABL(10),TEML(1),TIML(1),TEMS(1),TIMS(1)	MFO6005
	DIMENSION NLNO(1500),KNOD(1)	MFO6006
	EQUIVALENCE (P(1),KNOD(1),TEML(1)),(P(3000),TIML(1)),(P(6000),	MFO6007
	1 TEMS(1)),(P(9000),TIMS(1))	MFO6008
	REAL M	MFO6009
301	FORMAT (7012)	MFO6010
	REWIND 10	MFO6011
	REWIND 9	MFO6012
	IF (NREAD) 1,1,2	MFO6013
1	WRITE (6,204)	MFO6014
	GO TO 770	MFO6015
2	KK=0	MFO6016
	DO 102 I=1,NRMF	MFO6017
	READ (10,301) TO,TF,NT,MC	MFO6018
	L=LOC (NT)	MFO6019
99	L=L+1	MFO6020
	KK=KK+1	MFO6021
	NDN=KNOD(L)/16777216	MFO6022
	IF (NDN) 101,101,100	MFO6023
100	NLNO(KK)=NDN	MFO6024
	GO TO 99	MFO6025
101	NLNO(KK)=0	MFO6026
102	CONTINUE	MFO6027
	REWIND 10	MFO6028
	L=0	MFO6029
	DO 40 I=1,NRMF	MFO6030
	READ (10,301) TO,TF,NT,MC	MFO6031
	WRITE (6,200) TO,TF	MFO6032
	WRITE (6,205)	MFO6033
205	FORMAT (1H0,5X,8HNODE NO.,6X,5HMAX T,13X,5HMIN T,11X,	MFO6034
	1 11HTIME OF MAX,7X,11HTIME OF MIN )	MFO6035
3	L=L+1	MFO6036
	JJ=1	MFO6037
	KK=1	MFO6038
	ND1=NLNO(L)	MFO6039
	IF (ND1) 40,40,4	MFO6040
4	DO 30 J=1,NREAD	MFO6041
	READ (9,301) T1,T2,NT2,MMT,ND2,TEM,TIME	MFO6042
	IF (NT-NT2) 30,10,30	MFO6043
10	IF (ND1-ND2) 30,11,30	MFO6044
11	GO TO (13,16),MMT	MFO6045
13	TEML(JJ)=TEM	MFO6046
	TIML(JJ)=TIME	MFO6047
	JJ=JJ+1	MFO6048
	GO TO 30	MFO6049
16	TEMS(KK)=TEM	MFO6050
	TIMS(KK)=TIME	MFO6051
	KK=KK+1	MFO6052
30	CONTINUE	MFO6053
	TEML(JJ)=0.	MFO6054
	TIML(JJ)=0.	MFO6055
	TEMS(KK)=0.	MFO6056
	TIMS(KK)=0.	MFO6057
	IF (JJ-KK) 31,32,32	MFO6058
31	JJ=KK-1	MFO6059
	GO TO 34	MFO6060

TABLE D-4. (Continued)

32	JJ=JJ-1		MF06061
34	WRITE (6,202) ND1,(TEML(K),TEMS(K),TIML(K),TIMS(K),K=1, JJ)		MF06062
	REWIND 9		MF06063
	GO TO 3		MF06064
40	CONTINUE		MF06065
200	FORMAT (28H1 RANGE OF MINIMUM-MAXIMUM //4X,2E18.8 )		MF06066
202	FORMAT (4H0 I10,4E18.8/(14X,4E18.8))		MF06067
204	FORMAT (43H NO MAXIMUMS AND MINIMUMS WERE RECORDED )		MF06068
	REWIND 10		MF06069
770	RETURN		MF06070
	END		MF06071

TABLE D-4. (Continued)

\$IBFTC XLN6		XLN6000
FUNCTION XLIN(X1,X2,N)		XLN6001
C AS OF 6/17/65		XLN6002
C		XLN6003
C XLIN = AREA UNDER CURVE N FROM X1 TO X2		XLN6004
C		XLN6005
COMMON P, M		XLN6006
COMMON /CP2/ ERROR		XLN6007
DIMENSION P(16000), M(16), KP(1)		XLN6008
EQUIVALENCE (P(1),KP(1))		XLN6009
REAL M		XLN6010
KOD=32765		XLN6011
PER = 32767.		XLN6012
SUM=0.		XLN60121
NJC=1		XLN60121
X=X1		XLN60121
LL = LOC(N)		XLN6013
LL = LL + 1		XLN6014
NFLAG = 1		XLN6015
IF (KP(LL).NE.KOD) GO TO 1		XLN6016
KOD=KP(LL+1)		XLN6017
LL=LL+2		XLN6018
1 IF (P(LL-1).NE.PER) GO TO 3		XLN6019
2 PER = P(LL)		XLN6020
LL = LL + 1		XLN6021
NFLAG = 2		XLN6022
3 LU = LL		XLN6023
J = LL		XLN6024
5 LU = LU + 2		XLN6025
IF (P(LU) - P(J)) 7, 6, 6		XLN6026
6 J = LU		XLN6027
GO TO 5		XLN6028
7 LU = LU - 1		XLN6029
LV=LU+2		XLN6030
8 IF (X - P(LL)) 9, 10, 10		XLN6031
9 PERX=-PER		XLN6032
GO TO (40, 18), NFLAG		XLN6033
10 IF (P(LU - 1) - X) 12, 25, 25		XLN6034
12 PERX= PER		XLN6035
GO TO (40, 18), NFLAG		XLN6036
18 IF (ABS((P(LU-1)-P(LL))/PER-1.).GT.PER*1.E-6) GO TO 40		XLN6037
DO 20 J = LL, LV, 2		XLN6038
P(J) = P(J) + PERX		XLN6039
20 CONTINUE		XLN6040
GO TO 8		XLN6041
25 LL = LL + 2		XLN6042
26 DO 30 J = LL, LU, 2		XLN6043
IF (X - P(J)) 27, 27, 28		XLN6044
27 IF (KOD.NE.32765) GO TO 272		XLN6045
271 XLN=(P(J+1)-P(J-1))/(P(J)-P(J-2))*(X-P(J-2))+P(J-1)		XLN6046
GO TO 50		XLN6047
272 XLN=(ABS(P(J+1))-ABS(P(J-1)))/(P(J)-P(J-2))*(X-P(J-2))+ABS(P(J-1))		XLN6048
IF (KOD.EQ.0) GO TO 50		XLN6049
76 FORMAT (47HODERIVED VALUES USED IN THE FOLLOWING CURVES... )		XLN6050
IF (TIME.EQ.M(1)) GO TO 80		XLN6051
IF (TIME1.EQ.M(11)) GO TO 50		XLN60511
TIME=M(1)		XLN6052
80 IF (TIME1.NE.M(11)) WRITE (6,76)		XLN60521
TIME1=M(11)		XLN60522
WRITE (6,77) N,KOD,X,LIN		XLN6053
77 FORMAT (11H CURVE NO.= 16, 8H COD = 15,25H INDEPENDENT VARIABLE XLN6054		XLN6054

TABLE D-4. (Continued)

	1E = E12.4,23H DEPENDENT VARIABLE = E12.4)	
	GO TO 50	XLN6055
28	SUM=SUM+(P(J)-P(J-2))*(P(J-1)+P(J+1))/2.	XLN6056
30	CONTINUE	XLN60561
	LL = LL - 2	XLN6057
40	WRITE (6, 42) X, N	XLN6058
	WRITE (6, 73) (P(I), I = LL, LU)	XLN6059
73	FORMAT(29HOCURVE POINT PAIRS FOLLOW.... /(1X,3(2E18.8,4X)))	XLN6060
42	FORMAT (27H0INDEP VAR FOR LIN INTERP.= E 20.8, 7H CURVE= I 4 ,	XLN6061
	1 16H OFF CURVE )	XLN6062
	IF (ERROR.EQ.0.) WRITE (6, 75)	XLN6063
75	FORMAT (30H0 LAST TIME POINT CALCULATED )	XLN6064
	M(8)=1.	XLN6065
	IF (ERROR.EQ.0.) ERROR=2.	XLN6066
	RETURN	XLN6067
50	IF (NJC.EQ.2) GO TO 85	XLN6068
	NJC=2	XLN6069
	SUM1=SUM+(X-P(J-2))*(P(J-1)+XLN)/2.	XLN6070
	X=X2	XLN6071
	SUM=0.	XLN6072
	GO TO 26	XLN6073
85	SUM2=SUM+(X-P(J-2))*(P(J-1)+XLN)/2.	XLN6074
	XLIN=(SUM2-SUM1)/(X2-X1)	XLN6075
	RETURN	XLN6076
	END	XLN6077
		XLN6078



APPENDIX E  
DATA DIAGNOSTIC PROGRAM

A special program has been written, based extensively on the compile phase of the Thermal Analyzer Program, which scans input data and notes any errors that it finds. The purpose of this program is to allow a short diagnostic run for a large data deck before submitting it to execute.

PROGRAM OPERATION

The program actually compiles the data, printing notes on any errors it finds as it goes along. A much more rigorous examination is made in this routine than in the regular Thermal Analyzer compile phase.

In the Thermal Analyzer several errors can cause the program to terminate before completing its error check. The coding covering most of these errors has been changed in this program to allow the error check to continue. In particular, optional error exits have been selected so that bad data that would cause termination of the run under normal circumstances will simply be noted and the program will continue execution.

To simplify the program set-up on the computer, the special tapes used for the Thermal Analyzer have been eliminated from this job. All the program decks are contained in the card deck submitted to the computer. Therefore the program library tape used with the Thermal Analyzer is not used with this program. Any curves which are requested from the material properties library tape will merely be noted. The tape is not searched, and therefore is not needed. However, the program cannot make sure that the requested curve actually is on the tape; if it is not, a diagnostic will result later from the Thermal Analyzer run.

Since the problem is not executed, those diagnostics peculiar to the execution phase of the Thermal Analyzer do not appear in this program. For

example, a condition producing a time step of zero can be detected only in the execution phase. An independent variable that goes beyond the range of the independent variable specified in a curve for interpolation can only be detected in the execution phase. Such errors will not be noted in the diagnostic program.

Since the Thermal Analyzer has versions with different storage allocations, some of the errors do not apply to all versions. For example, if the data exceeds 14000 storages but not 16000, it cannot be run on version C, but may be run on versions A or B. Where such restrictions apply, the diagnostic will so state.

#### PROGRAM SET-UP

Figure E-1 shows the deck set-up for the diagnostic program, and Table E-1 is a list of the diagnostic comments that could occur.

The input data is set-up just as for the Thermal Analyzer:

1. Temperature block cards
2. NBK card
3. Resistor block cards
4. NBK card
5. Capacitor block cards
6. NBK card
7. Data Sub-block cards
8. NBK card
9. Time block cards
10. NBK card
11. Restart        }
12. NBK card        }     Repeat as often as needed.
13. END

When the data deck is ready, it is inserted into the diagnostic program deck following the \$DATA card; it is input data for this program, too. Following the last data card, which is the "END" card, are the required program termination cards to return control to IB monitor system, \$EOF and \$IBSYS.

Table E-2 is a complete listing of the eleven data diagnostic program subroutines.



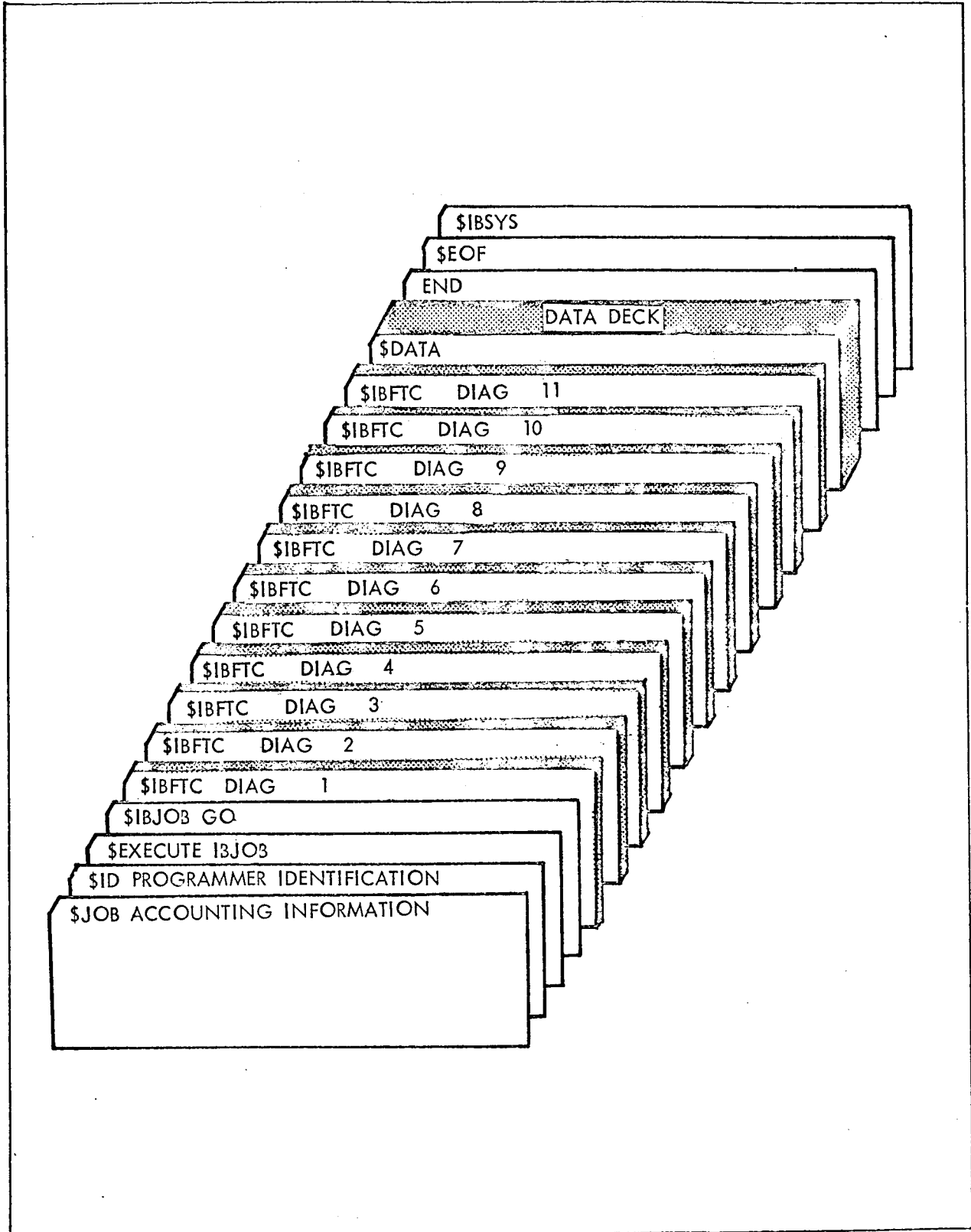


Figure E-1 Source Program Deck Setup For Data Diagnostic Program

TABLE E-1  
DIAGNOSTICS

DECK NAME: DIAG  
SUBROUTINE: COMPIL

215 FORMAT ( 66H0 COUNT IN COLS. 4 AND 5 IS NOT AN INTEGER LESS THAN OCOMP025  
1R EQUAL TO 6 ) COMP0251  
223 FORMAT (7H0CODE= A6,12H IS ILLEGAL.) COMP021  
214 FORMAT (56H0 BLOCK COUNT IN COMPIL ROUTINE IS AN UNREASONABLE VALUCOMP024  
1E ) COMP0241

DECK NAME: DIAG  
SUBROUTINE: SREAD

210 FORMAT (1H0 71H AN ILLEGAL CHARACTER HAS BEEN REPLACED BY A ZERO I2266277  
IN THE FOLLOWING CARD /1H 24I3) 2266278  
211 FORMAT (1H0100H AN ILLEGAL CHARACTER HAS BEEN REPLACED BY A ZERO I2266279  
IN THE FOLLOWING PRESSURIZATION PROGRAM INPUT CARD /1H 7F10.2) 2266280  
201 FORMAT (10H0NTYPE OF I5,12H IS ILLEGAL.) 2266270  
202 FORMAT ( 9H0NRAD OF I5,12H IS ILLEGAL.) 2266271  
203 FORMAT ( 9H0NCIR OF I5,12H IS ILLEGAL.) 2266272  
204 FORMAT (10H0NSECT OF I5,12H IS ILLEGAL.) 2266273  
205 FORMAT ( 9H0NTNK OF I5,12H IS ILLEGAL.) 2266274  
206 FORMAT ( 8H0IGC OF I5,12H IS ILLEGAL.) 2266275  
207 FORMAT (11H0IPRESS OF I5,12H IS ILLEGAL.) 2266276

DECK NAME: DIAG  
SUBROUTINE: LOC

21 FORMAT (10H0CURVE NO.15,25H IS NOT IN ADDRESS TABLE.) LOC 535



TABLE E-1 DIAGNOSTICS (Continued)

DECK NAME:	DIAGN	COMPO30
SUBROUTINE:	RESTRT	COMP025
222	FORMAT (30H0 TOO MANY WORDS IN DAT BLOCK )	COMP021
215	FORMAT (40H0 KOUNT IS NOT CORRECT IN RESTRT ROUTINE )	22660221
223	FORMAT (7H0CODE= A6,12H IS ILLEGAL.)	COMP356
280	FORMAT (1H0 44H FOLLOWING CARD OUT OF PLACE IN THIS RESTART)	22660223
250	FORMAT (43H KOUNT HAS BEEN INCLUDED ON BLOCK FLAG CARD )	22660224
252	FORMAT (1H0 70H AN ILLEGAL CHARACTER HAS BEEN REPLACED BY ZERO IN 1 THE FOLLOWING CARD /5X,5HDEC I5)	REST021
236	FORMAT (15H0BLOCK NUMBER =16,29H IS ILLEGAL. RESTART DELETED. )	PRE22660225
253	FORMAT (1H0 64H FOLLOWING CARD ILLEGAL IN TEMPERATURE BLOCK OF PREVIOUS RESTART)	22660226
254	FORMAT (1H0 88H TERMINATING CARD OF ONE OF THE BLOCKS IN PREVIOUS RESTART CONTAINS AN ILLEGAL CHARACTER)	22660227
255	FORMAT (1H0113H AN ILLEGAL CHARACTER HAS BEEN REPLACED BY A ZERO IN THE FOLLOWING CARD OF THE TEMP BLOCK OF THE PREVIOUS RESTART)	22660228
257	FORMAT (1H0 61H FOLLOWING CARD ILLEGAL IN RESISTOR BLOCK OF PREVIOUS RESTART)	22660229
259	FORMAT (1H0116HAN ILLEGAL CHARACTER HAS BEEN REPLACED BY A ZERO IN THE FOLLOWING CARD OF THE RESISTOR BLOCK OF THE PREVIOUS RESTART)	22660230
260	FORMAT (1H0 62H FOLLOWING CARD ILLEGAL IN CAPACITOR BLOCK OF PREVIOUS RESTART)	22660231
261	FORMAT (1H0112H AN ILLEGAL CHARACTER HAS BEEN REPLACED BY A ZERO IN THE FOLLOWING CARD OF THE CAP BLOCK OF THE PREVIOUS RESTART)	22660232
262	FORMAT (1H0 57H FOLLOWING CARD ILLEGAL IN TIME BLOCK OF PREVIOUS RESTART)	22660233
263	FORMAT (1H0113H AN ILLEGAL CHARACTER HAS BEEN REPLACED BY A ZERO IN THE FOLLOWING CARD OF THE TIME BLOCK OF THE PREVIOUS RESTART)	22660234
264	FORMAT (1H0115H AN ILLEGAL CHARACTER HAS BEEN REPLACED BY A ZERO IN THE FOLLOWING CARD IN A DATA SUB-BLOCK OF THE PREVIOUS RESTART)	22660235

## TABLE E-2

## DATA DIAGNOSTIC PROGRAM LISTING

\$IBFTC DIAG1	
C AS OF 12/4/64	
NLAG = 1	2088M003
CALL EXETIV (NLAG)	2088M004
CALL EXIT	2088M005
STOP	2088M006
END	2088M007

\$IBMAP DIAG2	
ENTRY .UN04.	
.UN04. PZE UNIT04	
UNIT04 FILE ,UT4,READY,INOUT,BLK=22,BCD,NOLIST	
END	
\$IBMAP DIAG4	
ENTRY .UN09.	
.UN09. PZE UNIT09	
UNIT09 FILE ,B(3),READY,INOUT,BLK=22,BCD,NOLIST	
END	
\$IBMAP DIAG3	
ENTRY .UN10.	
.UN10. PZE UNIT10	
UNIT10 FILE ,A(3),READY,INOUT,BLK=22,BCD,NOLIST	
END	



TABLE E-2. (Continued)

```

SIBFTC DIAG5
SUBROUTINE EXETIV (NLAG)
C AS OF 5/25/65
COMMON P(14000),M(16),MAXT,MAXR,MAXC,KSP,KST,KURV7,NCVG,NSTS,NFAB
COMMON NABL(10),NKSP,LMMF,NRMF,NREAD,CC(12)
COMMON NR,MAXP,MAXK,MAXS,MAXM
COMMON /CP2/ ERROR,MAXMUM
COMMON /CPITM/ ITIMO
COMMON /CPNET/NTYPE,TKRAD,TKLEN,TEMPZ,NRAD,NCIR,NSECT,NTNK,
1 TKTHK(5),TKWAL1,TKWAL2,INNOD,KOUT,
2 FMCO,FMNO,FMOLC,VGAS,IGC,IPRESS,FMOLN,FMIN,FMAX,PMIN,
3 PMAX,FMOLX,TSAT,ANGLE,TX,PR,TANKV,
4 MM(50), NUMTAB(100), NEXW(50),
5 RADI(4),NSEX(50),HELBI(14) ,LLFLOW,HELT,HELP,HELW
6 ,TSTRAT,SAREA,IOPISX(5)
COMMON /CONTR/ TLIQ,SCLIQ,TGAS,SCGAS,SCALL,TLMAX,SCINT,TSGAS,
1 COMUN(5),DMCC,TLMAX,TALL,FML0,GAVITY,FKG,FKL,ZC,PC,ZN,FMLU,FMLA,
2 ZX,CPX,TLA,GAMMA,RHOL,RHOG,CPL,CPG,RLAM,MCNT,PN,FMC,FMN,R
COMMON /CHP/SMCV,SMCA,SMNV,SMNA,SDMCC,SMLAS,SMLUS,SUMEX,HELWS,GOLD,
1 ANGOLD,FMG,FXL,TS,DELTS,DELVS,FMGAS
COMMON /CPPLT/NPLT,NEND,KSKIP
COMMON /EXFLG/NTFLG,NSAV,NFLG
COMMON /EXPLT/ NLFLG
DIMENSION VS(100),FLA(25)
EQUIVALENCE (P(13651),VS),(P(13751),FLA)
MAXMUM = 13650
ITIMO = 1
NEND=0
NPLT=1
ERROR=0.
NTYPE=0
NTFLG=0
5 IR=NLAG
8 CALL COMPIL(IR)
NLAG=IR
NLAG=2
IF (NEND.GT.0) RETURN
IF (ERROR.GT.1.) ERROR=0.
IF (1.EQ.1) GO TO 5
RETURN
END

```

EXETV002

EXETV010

EXETV020

EXET 020

EXET021

EXET006

HTB 006

DIAG007

EXET0069

FXFT 025

EXET 025

EXET 026

EXETV030

EXETV060

EXETV070

EXET0772

EXET0773

EXET078

EXET079

EXET099

TABLE E-2 (Continued)

\$IBFTC DIAG6		
SUBROUTINE COMPIL (IR)		COMP003
C AS OF 04/27/65		
C 8/21/64 CHANGED TO INCLUDE MINMAX		COMP004
COMMON P, M, MAXT, MAXR, MAXC, KSP, KST, KURV 7, NCVG, NSTS, NFAB		COMP004
COMMON NABL, NKSP, LMMF, NRMF, NREAD, CC		COMP005
COMMON NRECD, NRPD, NWCT, NWST, NWTM		COMP006
COMMON /CP2/ERROR, MAXMUM		COMP006
COMMON /CPPLT/ NPLT, NEND		COMP006
COMMON /EXPLT/ NLFLG		COMP006
DIMENSION CZ(6), CY(6)		COMP007
DIMENSION A(12), I 1(12), I 2(12), I 3(12), NABL(10), CC(12)		COMP007
DIMENSION P(14000), IRLINE(1), KPSD(1), NSTRT(1), M(16), KDAT(1)		COMP008
EQUIVALENCE (P(4000), IRLINE(1)), (P(8000), KPSD(1)), (P(13000),		COMP009
1 NSTRT(1)), (P(1), KDAT(1))		COMP010
REAL M, INC, NBK, NET		COMP0
INTEGER CP		COMP011
DATA ENDF/6H -1 /		COMP011
DATA NET/6HNFT /		COMP011
DATA DEC/6HDEC /		COMP011
DATA INC/6HINC /		COMP011
DATA PER/6HPER /		COMP011
DATA NBK/6HNBK /		COMP011
DATA CID/6HCID /		COMP011
DATA TAP/6HTAP /		COMP011
DATA RES/6HRES /		COMP011
DATA CAP/6HCAP /		COMP011
DATA COD/6HCOD /		COMP011
DATA ZERO/6H000000/		COMP011
DATA (CZ(I), I=1,6)/2H01,2H02,2H03,2H04,2H05,2H06/, BLANK/1H /		COMP011
DATA (CY(I), I=1,6)/2H 1,2H 2,2H 3,2H 4,2H 5,2H 6/, ZERZ/2H00/		COMP011
DATA ZERY/2H 0/		COMP011
200 FORMAT (5X, 4(I 5, E 10.2))		COMP015
201 FORMAT (5X, I 5, E 10.2, I 5)		COMP016
202 FORMAT (5X, 2(3I 5, E 10.2))		COMP017
203 FORMAT (5X, 3I 5, E 10.2, I 5)		COMP018
204 FORMAT (5X, I 5)		COMP019
205 FORYAT (5X, 6E 10.2)		COMP020
208 FORMAT (1H1, A3, I2, 12A6)		COMP021
209 FORMAT (A3, A2, 12A6)		COMP021
210 FORYAT (5X, 12A6)		COMP021
211 FORMAT (5X, A3, I2, 12A6)		COMP022
212 FORMAT (1H1, 9X, 12A6)		COMP023
214 FORMAT (56H0 BLOCK COUNT IN COMPIL ROUTINE IS AN UNREASONABLE VALU		COMP024
1E )		COMP0241
215 FORMAT ( 66H0 COUNT IN COLS. 4 AND 5 IS NOT AN INTEGER LESS THAN		COMP025
1R EQUAL TO 6 )		COMP0251
216 FORMAT (I 3, A 6)		COMP026
218 FORMAT (I 3, 3X, I 2)		COMP027
219 FORMAT (38H0 KOD IS NOT CORRECT IN COMPIL ROUTINE )		COMP028
220 FORMAT (26H0TABLE NO. = 0 IS ILLEGAL.)		COMP029
222 FORMAT (30H0 TOO MANY WORDS IN DAT BLOCK )		COMP030
223 FORMAT (7H0CODE= A6,12H IS ILLEGAL.)		COMP021
224 FORMAT (25H0CANNOT FIND CURVE NAMED A6,17H ON LIBRARY TAPE.)		COMP021
230 FORMAT (28H0SOMETHING WRONG AFTER TABLE16,17H AND BEFORE TABLE16)		COMP021
231 FORMAT (25H0SOMETHING WRONG IN TABLE 16)		COMP021
232 FORMAT (5X,3H***,5X,6H CURVE A5,36H FROM LIBRARY TAPE WILL APPEAR		COMP022
HERE.)		
NCVG = 1		COMP031
NSTS = 1		COMP032
MATLIB = 1		COMP032

TABLE E-2 -(Continued)

NSW2=1	2266032
NPLT=1	2266032
NLFLG=1	2266032
NETSW=0	COMP032
NFAB = 1	COMP033
NSW2=1	COMP034
LINE = 1	COMP034
LMMF=1	COMP034
NRMF=0	COMP034
NREAD=0	COMP034
DO 101 I = 1, 10	COMP035
NABL(I) = 0	COMP036
101 CONTINUE	COMP037
GO TO (105, 149, 149), IR	COMP038
105 REWIND 4	COMP039
DO 107 I = 1, MAXVUM	COMP040
P(I) = 0.	COMP0401
107 CONTINUE	COMP0402
KOUNT = 1	COMP042
110 CP=-1	COMP043
IF (KOUNT.EQ.2.AND.NETSW.EQ.2) GO TO 180	COMP0431
IF (KOUNT.EQ.3.AND.NETSW.EQ.1) GO TO 190	COMP0431
IF (MATLIB.EQ.1) READ (5,209) CM,CX,(A(I),I=1,12)	COMP044
1101 DO 1102 I=1,6	COMP045
1102 IF (CX.EQ.CY(I).OR.CX.EQ.CZ(I)) CP=1	COMP0451
IF (CX.EQ.BLANK.OR.CX.EQ.ZERZ.OR.CX.EQ.ZERY) CP=0	COMP046
IF (CP.GE.0) GO TO 1103	COMP0461
CP=0	COMP0462
ERROR=1.	COMP0462
WRITE (6,215) CX	COMP0462
1103 IF (LINE.LT.60) GO TO 111	COMP0463
109 WRITE (6,212) (CC(I),I=1,12)	COMP047
LINE = 1	COMP048
111 IF (CM.EQ.CID) GO TO 117	COMP049
IF (CM.EQ.TAP) GO TO 150	COMP0491
WRITE (6,211) CM,CP,(A(I),I=1,12)	COMP0492
LINE=LINE+1	COMP0492
IF (CM.EQ.DEC) GO TO 116	COMP050
IF (CM.EQ.INC) GO TO 118	COMP051
IF (CM.EQ.PER) GO TO 119	COMP052
IF (CM.EQ.NBK) GO TO 120	COMP053
IF (CM.EQ.RES) GO TO 123	COMP050
IF (CM.EQ.CAP) GO TO 124	COMP050
IF (CM.EQ.NET) GO TO 170	COMP053
IF (CM.EQ.COD) GO TO 112	COMP050
115 WRITE (6,223) CM	COMP054
ERROR=1.	COMP054
GO TO 110	COMP055
112 KOD = 9	COMP0551
GO TO 125	COMP0552
116 KOD = 1	COMP056
GO TO 125	COMP057
117 CMID=CM	COMP057
ICP=CP	COMP0571
DO 1171 I=1,12	COMP0572
CC(I)=A(I)	COMP0573
1171 CONTINUE	COMP0574
LINE = 1	COMP0575
WRITE (6,212) (CC(I),I=1,12)	COMP0575
GO TO 110	COMP0576
118 KOD = 3	COMP058
GO TO 125	COMP058

TABLE E-2 (Continued)

119	KOD = 4 GO TO 125	COMP060
120	KOD = 5 KOUNT = KOUNT + 1 IF (KOUNT - 6) 125, 121, 122	COMP061 COMP062 COMP063 COMP064
121	KOD = 6 GO TO 125	COMP065
122	WRITE (6,214) ERROR = 2. RETURN	COMP066 COMP067 COMP068 COMP069
123	KOD=7 GO TO 125	COMP0691
124	KOD=8 GO TO 125	COMP0692 COMP0693 COMP0694
150	WRITE (6,211) CM,CP,(A(I),I=1,12) WRITE (6,232) A(1) LINE = LINE + 2 GO TO 110	DIAG0702 DIAG0703 DIAG0704 COMP0710
170	NETSW=2 CALL INSIDE GO TO 110	COMP0711 COMP0712 COMP0712
180	READ (10,209) CM,CX,(A(I),I=1,12) IF (A(1).NE.ENDF) GO TO 1101 NETSW=1 REWIND 10 GO TO 110	COMP0713 COMP0714 COMP0715 COMP0715 COMP0716
190	READ ( 9,209) CM,CX,(A(I),I=1,12) IF (A(1).NE.ENDF) GO TO 1101 NETSW=0 REWIND 9 GO TO 110	COMP0717 COMP0718 COMP0719 COMP0719 COMP0720
125	WRITE (4,218) KOD,CP WRITE (4, 210) (A(I), I = 1, 12) IF (KOUNT - 6) 110, 130, 122	COMP0721 COMP073 COMP074 COMP075
130	END FILE 4 REWIND 4 REWIND 3 CALL COMP2 RETURN	COMP076 COMP077 078 079
149	CALL RESTRT RETURN END	080

TABLE E-2 (Continued)

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SIBFTC DIAG7
SUBROUTINE INSIDE
C AS OF 6/30/65
COMMON P(14000)
COMMON /CPNET/NTYPE,TKRAD,TKLEN,TEMPZ,NRAD,NCIR,NSECT,NTNK,
1 TKTHK(5),TKWAL1,TKWAL2,INNOD,KOUT,
2 FMCO,FMNO,FMOLC,VGAS,IGC,IPRESS,FMOLN,FMIN,FMAX,PMIN,
3 PMAX,FMOLX,TSAT,ANGLE,TX,PR,TANKV,
5 RADI(4),HEL8(14),LLFLOW,HELT,HELP,HELW
6 ,ISTRAT,SAREA,IPTSX(5),FMULTF(5),STRINP(20)
7 ,GSOLD(2),TTCPBL(2),DLIQ ,NLSURF,ICALL
EQUIVALENCE (FMULTF(1), FLT),(FMULTF(2),FLKL)
DIMENSION VS(250),DUMMY(500)
1 ,NUMTAB(100),NEXW(125),NSEX(125),MM(125)
DIMENSION LNO(250),NLNNS(125),NGNNS(125)
EQUIVALENCE (P(13251),VS),(P(13501),DUMMY)
1,(P(12526),NUMTAB),(P(12626),NEXW),(P(12751),NSEX),(P(12876),MM)
EQUIVALENCE(P(12276),LNO),(P(12151),NLNNS),(P(12026),NGNNS)
REAL LEN
PI = 3.14159265
V=0.
FLA=0.
CALL SREAD
INODE=INNOD
REWIND 9
REWIND 10
C TANKV = VOLUME OF TANK
VOLX=PI*TKRAD**2
IF (NTYPE.EQ.2) TANKV=1.33333*VOLX*TKRAD
IF (NTYPE.EQ.1) TANKV=VOLX*(1.33333*TKRAD+TKLEN)
ITIM= 1
SUM =0.0
DO 10 I=1,NTNK
SUM =SUM+ TKTHK(I)
10 CONTINUE
FNRAD =NRAD
FNCIR =NCIR
FNSECT= NSECT
KEYNOD= -1
C IF CYLINDER NTYPE=1 ,IF SPHERE NTYPE=2
PI2= 3.14159265*2.0
NRES =0
C COMPUTE RADIAL RESISTORS FOR HEMISPHERE
15 KK = NRAD/4
M = 0
K1 = (NCIR+NTNK +1)
JJ = NRAD
J1 = NCIR + NTNK +1
II = NCIR +NTNK
DO 50 KI= 1,KK
K = KI-1
DO 40 JI= 1,JJ
J=JI -1
DO 30 I= 1,II,1
M = M+1
NODE = M-1 +INODE
29 NRES =NRES+1
NODE1= NODE+1
WRITE(10,8002) NRES,NODE,NODE1,FLA
8002 FORMAT(5HDEC01,3I5,E10.3,50X)
30 CONTINUE
1911002
1911007
1911004
INSD
INSD
1911005
INSD007
INSD0071
INSD0072
1911008
1911009
1911010
1911011
1911012
1911013
1911014
1911015
1911016
1911017
1911018
1911019
1911021
1911022
1911023
1911024
1911025
1911026
1911027
1911028
1911029
1911030
1911031
1911032
1911033
1911034
1911056
1911057
1911058
INSD059
1911060

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TABLE E-2 (Continued)

	M = M+1	1911061
40	CONTINUE	1911062
50	CONTINUE	1911063
	M = 0	1911064
	II = II+1	1911065
	DO 80 KI = 1, KK	1911066
	K = KI-1	1911067
	DO 70 JI = 1, JJ	1911068
	J = JI-1	1911069
	DO 60 I = 1, II	1911070
	M = M + 1	1911071
	NODE = M + INODE - 1	1911072
	NODE1 = NODE + NCIR + NTK + 1	1911073
	IF (JI .EQ. JJ) NODE1 = NODE - (NRAD-1) * (NCIR + NTK + 1)	1911074
	IF (I .LE. NCIR + 1) GO TO 59	INSD075
	IF (I .NE. II) GO TO 60	INSD085
59	NRES = NRES + 1	1911089
	WRITE(10,8002) NRES, NODE, NODE1, FLA	1911090
60	CONTINUE	1911091
70	CONTINUE	1911092
80	CONTINUE	1911093
	M = 0	1911094
	KK = KK-1	1911095
	IF (KK * JJ * II .EQ. 0) GO TO 115	
	DO 110 KI = 1, KK	1911096
	K = KI-1	1911097
	DO 100 JI = 1, JJ	1911098
	J = JI-1	1911099
	DO 90 I = 1, II	1911100
	M = M+1	
	NODE = M-1 + INODE	1911101
	NODE1 = NODE + (NRAD) * (NCIR + NTK + 1)	1911102
	IF (I .LE. NCIR + 1) GO TO 89	INSD103
	IF (I .NE. II) GO TO 90	INSD112
89	NRES = NRES + 1	1911116
	WRITE(10,8002) NRES, NODE, NODE1, FLA	1911117
90	CONTINUE	1911118
100	CONTINUE	1911119
110	CONTINUE	1911120
C	CALCULATE CONDENSOR BLOCK LIST FOR SPHERE	1911121
115	CONTINUE	
	M = 0	1911122
	KK = NRAD/4	1911123
	JJ = NRAD	1911124
	II = NCIR + NTK + 1	1911125
	DO 140 KI = 1, KK	1911126
	K = KI-1	1911127
	CON = -SIN(FLOAT(K)*PI2/FNRAD) + SIN(FLOAT(K+1)*PI2/FNRAD)	1911128
	DO 130 JI = 1, JJ	1911129
	J = JI-1	19111291
	DO 120 I = 1, II	1911130
	M = M+1	1911131
	NODE = M - 1 + INODE	1911132
119	WRITE(9,8003) NODE, V	1911147
8003	FORMAT(5HDEC01, I5, E10.3, 60X)	INSD148
120	CONTINUE	1911149
130	CONTINUE	1911150
140	CONTINUE	1911151
C	TEST KEYNODE	1911152
C		1911153
C		1911154

TABLE E-2 (Continued)

C	IF ( KEYNOD.EQ.-1)GO TO 200	1911155
	JJ = NRAD	1911156
	II = NCIR +NTNK + 1	1911157
	M = 0	1911158
C	CALCULATE CONNECTING RESISTORS SPHERE TO SPHERE AND SPHERE TO	1911159
C	CYLINDER	1911160
	DO 170 JI =1,JJ	1911161
	J = JI-1	1911162
	DO 160 I =1,II	1911163
	M = M+1	1911164
	NODE = M-1 +KEYNOD	1911165
	NODE1 = M-1 +INODE	1911166
	IF (1.LE.NCIR+1) GO TO 149	1911168
	IF (1.NE.III) GO TO 160	INSD169
149	NRES=NRES+1	INSD178
	WRITE (10,8002) NRES,NODE,NODE1,FLA	INSD183
160	CONTINUE	1911184
170	CONTINUE	1911185
190	NEND =-1	1911186
	WRITE ( 9,8002) NEND	1911187
	WRITE (10,8002) NEND	1911188
	END FILE 9	1911189
	END FILE 10	1911190
	REWIND 9	1911191
	REWIND 10	INSD1911
	RETURN	INSD1911
200	IF (NTYPE.EQ.1) GO TO 201	1911192
	KEYNOD= INODE	1911193
	INODE = (NCIR + NTK+1)*NRAD**2/4 +INODE	1911194
	GO TO 15	1911195
201	KEYNOD = INODE	1911196
	INODE = (NCIR + NTK+1)*NRAD**2/4 + INODE	1911197
C	CALCULATE RESISTORS AND CONDENSORS OF CYLINDER BODY	1911198
	M = 0	1911199
	II = -NCIR +NTNK	191200
	JJ = NRAD	191201
	KK = NSECT	191202
	DO 230 KI =1,KK	191203
	K = KI-1	191204
	DO 220 JI =1,JJ	191205
	J = JI-1	191206
	DO 210 I =1,II	191207
	M = M +1	191208
	NODE = M-1 +INODE	191209
	NODE1= NODE +1	191210
209	NRES = NRES + 1	191211
	WRITE (10,8002) NRES,NODE,NODE1,FLA	191233
210	CONTINUE	191234
	M = M+1	191235
220	CONTINUE	191236
230	CONTINUE	191237
	II = II+1	191238
	M = 0	191239
	DO 270 KI =1,KK	191240
	K = KI-1	191241
	DO 260 JI =1,JJ	191242
	J = JI-1	191243
	DO 250 I =1,II	191244
	M = M+1	191245
	NODE = M-1 +INODE	191246
	NODE1= NODE +NCIR +NTNK + 1	191247
		191248

TABLE E-2 (Continued)

249	IF (JI.EQ.JJ) NODE1 = NODE1 -NRAD*(NCIR + NTKK+1)	1911264
	NRES =NRES +1	1911265
	WRITE(10,8002) NRES,NODE,NODE1,FLA	1911266
250	CONTINUE	1911267
260	CONTINUE	1911268
270	CONTINUE	1911269
	KK = KK-1	1911270
	LEN =TKLEN /FNSECT	1911271
	M =0	1911272
	IF (KK*JJ*II.EQ.0) GO TO 305	
	DO 300 KI =1,KK	1911273
	K = KI-1	1911274
	DO 290 JI =1,JJ	1911275
	J=JI-1	1911276
	DO 280 I =1,II	1911277
	M=M+1	
	NODE = M-1 +INODE	1911278
	NODE1 = NODE +(NRAD )*(NCIR+NTNK+1)	1911279
	IF (I.LE.NCIR+1) GO TO 279	INSD280
	IF (I.NE.II) GO TO 280	INSD287
279	NRES = NRES +1	1911291
	WRITE(10,8002) NRES,NODE,NODE1,FLA	1911292
280	CONTINUE	1911293
290	CONTINUE	1911294
300	CONTINUE	1911295
C	CALCULATE CONDENSORS FOR CYLINDER	1911296
305	CONTINUE	
	KK =KK+1	1911297
	M = 0	1911298
	DO 330 KI=1,KK	1911299
	K = KI-1	1911300
	DO 320 JI=1,JJ	1911301
	J = JI-1	1911302
	DO 310 I =1,II	1911303
	M =M+1	1911304
	NODE = M -1 +INODE	1911305
309	WRITE( 9,8003) NODE,V	1911319
310	CONTINUE	1911320
320	CONTINUE	1911321
330	CONTINUE	1911322
	II = NCIR + NTKK +1	1911323
	JJ = NRAD	1911324
	M = 0	1911325
	DO 350 JI =1,JJ	1911326
	J = JI-1	1911327
	DO 340 I =1,II	1911328
	M = M+1	1911329
	NODE = M-1 +KEYNOD	1911330
	NODE1 = M-1 +INODE	1911331
	IF (I.LE.NCIR+1) GO TO 349	INSD332
	IF (I.NE.II) GO TO 340	INSD340
349	NRES=NRES+1	INSD344
	WRITE(10,8002) NRES ,NODE, NODE1,FLA	1911345
340	CONTINUE	1911346
350	CONTINUE	1911347
	KEYNOD= INODE +(NCIR+NTNK+1)*NRAD *(NSECT-1)	1911348
	INODE = INODE +(NCIR+NTNK+1)*NRAD *NSECT	1911349
	GO TO 15	1911350
	END	1911352



TABLE E-2 (Continued)

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SIBFTC DIAGS
SUBROUTINE SREAD
C AS OF 05/18/65
C IF KOUT=1 --SOME AUXILIARY PRINT
C IF KOUT=2 --ALL AUXILIARY PRINT
COMMON P(14000)
COMMON /CPNET/NTYPE,TKRAD,TKLEN,TEMPZ,NRAD,NCIR,NSECT,NTNK,
1 TKTHK(5),TKWAL1,TKWAL2,INNOD,KOUT,
2 FMCO,FMNO,FMOLC,VGAS,IGC,IPRESS,FMOLN,FMIN,FMAX,PMIN,
3 PMAX,FMOLX,TSAT,ANGLE,TX,PR,TANKV,
4 MM(50), NUMTAB(100), NEXW(50),
5 RADI(4),NSEX(50),HELB(14) ,LLFLOW,HELT,HELP,HELW 2266005
6 ,ISTRAT,SAREA,IOPTSX(5)
DIMENSION VS(100),FLA(250)
EQUIVALENCE (P(13651),VS),(P(13751),FLA)
EQUIVALENCE (IOPTSX(1),IRSTRT),(IOPTSX(2),IPTLIQ),
1 (IOPTSX(3),LIBTAP),(IOPTSX(4),MTIME )
2 (IOPTSX(5),KUT )
C MTIME = MACHINE TIME FOR THIS SEGMENT (MINUTES) IF RUN IN SEGMENTS
C KUT = TIME (IN SECONDS) AT WHICH CURRENT SEGMENT IS TO BE CUT
DIMENSION STRINP(7),FMULTF(5)
DIMENSION IERROR(1) 2266200
DATA IERROR(1)/32/, NERROR/1/ 2266201
CALL FXPPT (IERROR,NERROR) 2266205
CALL FSWTON(3,32,33,45)
CALL FXNPRT(1,32)
READ(5,10) NTYPE,NRAD,NCIR,NSECT,NTNK,INNOD,IGC,IPRESS,KOUT
1 (IOPTSX(1),I=1,4),KUT1,KUT2,KUT3
IF (IERROR(1).GT.0) GO TO 1 2266203
WRITE (6,210) NTYPE,NRAD,NCIR,NSECT,NTNK,INNOD,IGC,IPRESS,KOUT 2266204
1 (IOPTSX(1),I=1,4),KUT1,KUT2,KUT3 2266205
IERROR(1) = IABS(IERROR(1)) 2266206
1 CONTINUE 2266207
MTIME = MTIME *60
KUT = 1000000*KUT1 + 1000*KUT2 + KUT3
IF (NTYPE.LT.1.OR.NTYPE.GT.2) GO TO 101
2 IF (NRAD.LE.0.OR.MOD(NRAD,4).NE.0) GO TO 102 2266208
3 IF (NCIR.LT.1) GO TO 103 2266209
4 IF (NSECT.LT.1) GO TO 104 2266210
5 IF (NTNK.LT.0. OR.NTNK.GT.5) GO TO 105 2266211
6 IF (IGC.LT.1.OR.IGC.GT.2) GO TO 106 2266212
7 IF (IPRESS.LT.1.OR.IPRESS.GT.2) GO TO 107 2266213
8 READ (5,20) TKRAD,TKLEN,TEMPZ,TKWAL1,TKWAL2 22662131
IF (IERROR(1).GT.0) GO TO 11 2266214
WRITE (6,211) TKRAD,TKLEN,TEMPZ,TKWAL1,TKWAL2 2266215
IERROR(1) = IABS(IERROR(1)) 2266216
11 CONTINUE 2266217
READ (5,20) (TKTHK(I),I=1,5)
IF (IERROR(1).GT.0) GO TO 12 2266218
WRITE (6,211) (TKTHK(I),I=1,5) 2266219
IERROR(1) = IABS (IERROR(1)) 2266220
12 CONTINUE 2266221
READ (5, 20) PR,VGAS,TSAT,FMOLC,FMOLN,FMOLX,TX
IF (IERROR(1).GT.0) GO TO 13 2266222
WRITE (6,211) PR,VGAS,TSAT,FMOLC,FMOLN,FMOLX,TX 2266223
IERROR(1) = IABS(IERROR(1)) 2266224
13 CONTINUE 2266225
READ (5, 20) FMIN,FMAX,PMIN,PMAX
IF (IERROR(1).GT.0) GO TO 14 2266226
WRITE (6,211) FMIN,FMAX,PMIN,PMAX 2266227
IERROR(1) = IABS(IERROR(1)) 2266228

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TABLE E-2 (Continued)

14	CONTINUE READ (5,20) (RADI(I),I=1,4) IF (IERROR(1).GT.0) GO TO 15 WRITE (6,211) (RADI(I),I=1,4) IERROR(1) = IABS(IERROR(1))	2266220 2266230 2266231 2266232
15	CONTINUE READ (5,20) (HELBI(I),I=1, 8) IF (IERROR(1).GT.0) GO TO 16 WRITE (6,211) (HELBI(I),I=1,8) IERROR(1) = IABS(IERROR(1))	2266233 2266001 2266234 2266235 2266236
16	CONTINUE READ (5,20) (STRINP(I),I=1,7) IF (IERROR(1).GT.0) GO TO 17 WRITE (6,211) (STRINP(I),I=1,7) IERROR(1) = IABS(IERROR(1))	2266237
17	CONTINUE READ (5,20) (FMULTF(I),I=1,5) IF (IERROR(1).GT.0) GO TO 18 WRITE (6,211) (FMULTF(I),I=1,5) IERROR(1) = IABS(IERROR(1))	
18	CONTINUE WRITE (6,601) 1 NTYPE, NRAD, NCIR, NSECT, NTK, INNOD, IGC, IPRESS, 2 TKRAD, TKLEN, TEMPZ, TKWAL1, TKWAL2, (TKTHK(I), I=1,5), 3 PR, VGAS, TSAT, FMOLC, FMOLN, FMOLX, TX, 4 FMIN, FMAX, PMIN, PMAX, (RADI(I), I=1,4), 5 (HELBI(I), I=1, 8) HELBI(5) = HELBI(5)+460. HELI = HELBI(5) HELP = HELBI(7) HELBI(11) = HELI HELBI(13) = (NCIR+NTK)*(NRAD*(2+NSECT))+ 1*(NCIR+NTK+1)*(NRAD*(3+2*NSECT)+2*(NRAD*(NRAD/4-1))) HELBI(12) = (NCIR+NTK+1)*(NRAD*(NSECT+2*NRAD/4))	2266002 2266004
601	FORMAT(29H) PRESSURIZATION PROGRAM INPUT // 1 80H NTYPE NRAD NCIR NSECT NTK INODE IG 2C IPRESS /1H ,13,7110/ 50HOTKRAD TKLEN TEMPZ T 3KWAL 1 TKWAL 2 /XF7.3,4F10.3/23H0INSULATION THICKNESSES/ 4XF7.3,4F10.3/, 5 70H0 PR V GAS T SAT MOL C MOL N MOL X 6T X /XF7.3,6F10.3/35H0F MIN F MAX P MIN P MAX 7/XF7.3,3F10.3/, 8 40HORADI F RADI S RADI E1 RADI E2 A /X F7.3, E11.3, 2F10.3/ 9 20H0HELIUM BOTTLE INPUT / XF7.1,6F10.3/ F7.3/1H1) TSAT = TSAT+460. TEMPZ = TEMPZ+460. TX = TX+460. LLFLOW = 0 RETURN	
10	FORMAT(24I3)	
20	FORMAT(7F10.0)	
101	WRITE (6,201) NTYPE GO TO 2	2266250
102	WRITE (6,202) NRAD GO TO 3	2266252
103	WRITE (6,203) NCIR GO TO 4	2266254
104	WRITE (6,204) NSECT GO TO 5	2266256
105	WRITE (6,205) NTK	

TABLE E-2 (Continued)

	GO TO 6	2266259
106	WRITE (6,206) IGC ...	
	GO TO 7	2266260
107	WRITE (6,207) IPRESS	
	GO TO 8	2266262
201	FORMAT (10HONTYPE OF I5,12H IS ILLEGAL.)	2266270
202	FORMAT ( 9HONRAD OF I5,12H IS ILLEGAL.)	2266271
203	FORMAT ( 9HONCIR OF I5,12H IS ILLEGAL.)	2266272
204	FORMAT (10HONSECT OF I5,12H IS ILLEGAL.)	2266273
205	FORMAT ( 9HONTNK OF I5,12H IS ILLEGAL.)	2266274
206	FORMAT ( 8H0IGC OF I5,12H IS ILLEGAL.)	2266275
207	FORMAT (11H0IPRESS OF I5,12H IS ILLEGAL.)	2266276
210	FORMAT (1H0 71H AN ILLEGAL CHARACTER HAS BEEN REPLACED BY A ZERO	2266277
	IN THE FOLLOWING CARD /1H 2413)	2266278
211	FORMAT (1H0100H AN ILLEGAL CHARACTER HAS BEEN REPLACED BY A ZERO	2266279
	IN THE FOLLOWING PRESSURIZATION PROGRAM INPUT CARD /1H 7F10.2)	2266280
	END	

	SIBFTC DIAG9	
	FUNCTION LOC (KT)	LOC 002
C	AS OF 04727/65	
C		LOC 003
C	LOC ROUTINE FINDS FIRST LOCATION AHEAD OF LOCATION STARTING TABLE KT	LOC 004
C		LOC 005
	COMMON P, M, MAXT, MAXR, MAXC, KSP, KST	LOC 006
	COMMON /EXADR/ LCTN,LCTO,LCR,LCC,LCQ,LCRC,LCPS,LCK,LCKA	LOC 5207
	COMMON /CP2/ ERROR	LOC 5207
	DIMENSION P(14000), M(16), NSTRT(1)	LOC 007
	EQUIVALENCE (P(1), NSTRT(1))	LOC 008
	REAL M	LOC 009
	IF (KT.LE.0) GO TO 13	LOC 523
10	J=LCKA	LOC 524
11	J1=NSTRT(J)/2**18	LOC 5241
	J2=MOD(NSTRT(J),2**18)	LOC 525
	IF (J1.EQ.KT) GO TO 12	LOC 527
	IF (J1.EQ.0) GO TO 13	LOC 528
	J=J+1	LOC 529
	GO TO 11	LOC 530
12	IF (P(J2).NE.32767.) J2=J2-1	LOC 531
	LOC=J2	LOC 532
	RETURN	LOC 533
13	WRITE (6,21) KT	LOC 534
21	FORMAT (10HOCURVE NO.I5,25H IS NOT IN ADDRESS TABLE.)	LOC 535
	ERROR =1.	LOC 536
	RETURN	LOC 537
	END	LOC 538

TABLE E-2 (Continued)

SIBFTC DIAG10		
	SUBROUTINE COMP2	COM2002
C	AS OF 06/02/65	
	COMMON P, M, MAXT, MAXR, MAXC, KSP, KST, KURV 7, NCVG, NSTS, NFAB	COMP004
	COMMON NABL, NKSP, LMMF, NRMF, NREAD, CC	COMP005
	COMMON NRECD, NRPD, NWCT, NWST, NWTM	COMP006
	COMMON /CP2/ERROR, MAXMUM	COMP006
	DIMENSION BCDB(5)	COMP007
	DIMENSION A(I2), I 1(12), I 2(12), I 3(12), NABL(10), CC(12)	COMP007
	DIMENSION P(14000), IRLINE(1), KPSD(1), NSTRT(1), M(16), KDAT(1)	COMP008
	EQUIVALENCE (P(4000), IRLINE(1)), (P(8000), KPSD(1)), (P(13000),	COMP009
	I NSTRT(1)), (P(1), KDAT(1))	COMP010
	REAL M, INC, NBK, NET	COMP0
	INTEGER CP	COMP011
	DATA (BCDB(I), I=1,5)/6HTEMP, .6HRESIS, .6HCAPAC, .6HCURVE, .6HMISC.	COMP011
200	FORMAT (5X, 4(I 5, E 10.2))	COMP015
201	FORMAT (5X, I 5, E 10.2, I 5)	COMP016
202	FORMAT (5X, 2(I 5, E 10.2))	COMP017
203	FORMAT (5X, 3I 5, E 10.2, I 5)	COMP018
204	FORMAT (5X, I 5)	COMP019
205	FORMAT (5X, 6E 10.2)	COMP020
206	FORMAT (5X, E10.2, I5)	COMP021
208	FORMAT (1H1, A3, I2, 12A6)	COMP021
209	FORMAT (A3, I2, 12A6)	COMP021
210	FORMAT (5X, 12A6)	COMP021
211	FORMAT (5X, A3, I2, 12A6)	COMP021
212	FORMAT (5H1 12A 6)	COMP022
214	FORMAT (29H0 INPUT MUST BE BAD, QUIT JOB )	COMP023
215	FORMAT (40H0 KOUNT IS NOT CORRECT IN COM2 ROUTINE )	COMP024
216	FORMAT (I 3, A 6)	COMP025
218	FORMAT (I 3, 3X, I 2)	COMP026
219	FORMAT (15H0KOD MUST NOT =15,8H IN THE A6,7H BLOCK.)	COMP027
220	FORMAT (26H0TABLE NO. = 0 IS ILLEGAL.)	COMP028
222	FORMAT (30H0 TOO MANY WORDS IN DAT BLOCK )	COMP029
223	FORMAT (7H0CODE= A6,12H IS ILLEGAL.)	COMP030
224	FORMAT (25H0CANNOT FIND CURVE NAMED A6,17H ON LIBRARY TAPE.)	COMP021
230	FORMAT (28H0SOMETHING WRONG AFTER TABLE16,17H AND BEFORE TABLE16)	COMP021
231	FORMAT (25H0SOMETHING WRONG IN TABLE 16)	COMP021
232	FORMAT (7HCERROR,15,E15.5,22H NEGATIVE NODE NUMBER.)	COMP030
233	FORMAT (7HCERROR,315,E15.5,26H NEGATIVE RESISTOR NUMBER.)	COMP030
234	FORMAT (9HCRESISTOR15,15H CONNECTS NODES15,1H,15,27H GREATER THAN	COMP20301
	1MAX TEMP.NO.=15)	COMP20302
235	FORMAT (14H0CAPACITOR NO.15,22H IS GREATER THAN MAXT=15)	COMP2030
236	FORMAT (5H0NOCDE 15,20H HAS NO CONNECTIONS.)	COMP030
240	FORMAT (5X,3I5,3E10.0,I5)	COMP2031
241	FORMAT (5X,3I5,3E10.0,2I5)	COMP2031
242	FORMAT (5X,I5,3E10.0,2I5)	COMP2031
243	FORMAT (5X,I5,3E10.0,3I5)	COMP2031
244	FORMAT (1H0,I6,33H DATA STORAGE EXCEEDED. TOTAL OF 16,	COMP20311
	1 12H DATA ITEMS.)	COMP20312
245	FORMAT (30H0DATA WILL FIT VERSION A OR B.)	DIAG0312
250	FORMAT (14H1P STORAGE MAP /14H0 TEMPERATURES,9X,I6,8X,6HTOTAL I6)	COMP20313
251	FORMAT (23H TEMPERATURES 16,8X,6HTOTAL I6)	COMP20313
252	FORMAT (23H RESISTORS 16,8X,6HTOTAL I6)	COMP20313
253	FORMAT (23H CAPACITORS 16,8X,6HTOTAL I6)	COMP20313
254	FORMAT (23H CURRENTS (Q) 16,8X,6HTOTAL I6)	COMP20313
255	FORMAT (23H R-C PRODUCTS 16,8X,6HTOTAL I6)	COMP20313
256	FORMAT (23H PSEUDO-SEQUENCE 16,8X,6HTOTAL I6)	COMP20313
257	FORMAT (23H DATA BLOCKS (CURVES) 16,8X,6HTOTAL I6)	COMP20313
258	FORMAT (23H DATA BLOCK ADDRESSES 16,8X,6HTOTAL I6)	COMP20313
350	FORMAT (1H030H ILLEGAL CHARACTER IN ONE OF THE FOLLOWING NODE NOS.	COMP2032

TABLE E-2 (Continued)

	1 OR TEMPS. REPLACED BY ZERO./5X,15,F10.2,15,F10.2,15,F10.2,15,F10.	COM2033
	22)	COM20331
351	FORMAT (1H087H ILLEGAL CHARACTER HAS BEEN REPLACED BY 0 IN THE FOLC	COM2034
	LOWING INC CARD, TEMPERATURE BLOCK./1H 5HINC 15,E10.2,15)	COM2035
352	FORMAT (1H045H FOLLOWING CARD ILLEGAL IN TEMPERATURE BLOCK /5XA3,	COM2036
	112,12A6)	COM2037
353	FORMAT (1H042H FOLLOWING CARD ILLEGAL IN RESISTOR BLOCK /5XA3,12,	COM2038
	112A6)	COM2039
2551	FORMAT (1H087H AN ILLEGAL CHARACTER HAS BEEN REPLACED BY A ZERO INCOM	COM2040
	1 THE FOLLOWING CARD, RESISTOR BLOCK)	COM2041
354	FORMAT (1H A3,12,315,F10.2,315,F10.2)	COM2042
356	FORMAT (1H A5,315,3F10.2,215)	COM2043
357	FORMAT (1H A5,315,E10.2,15)	COM2044
358	FORMAT (1H043H FOLLOWING CARD ILLEGAL IN CAPACITOR BLOCK /5XA3,12,	COM2045
	112A6)	COM2046
259	FORMAT (1H0 88H AN ILLEGAL CHARACTER HAS BEEN REPLACED BY A ZERO ICOM	COM2047
	IN THE FOLLOWING CARD, CAPACITOR BLOCK)	COM2048
260	FORMAT (1H A3,12,15,F10.2,15,F10.2,15,F10.2,15,F10.2)	COM2049
261	FORMAT (1H A5,4F10.2,215)	COM2050
262	FORMAT (1H 5HINC 15,F10.2,15)	COM2051
263	FORMAT (1H 5HINC 15,3F10.2,315)	COM2052
264	FORMAT (1H043H FOLLOWING CARD ILLEGAL IN DATA SUB-BLOCKS /5XA3,12,	COM2053
	112A6)	COM2054
265	FORMAT (1H0 87H AN ILLEGAL CHARACTER HAS BEEN REPLACED BY A ZERO ICOM	COM2055
	IN THE FOLLOWING CARD, DATA SUB-BLOCK)	COM2056
266	FORMAT (1H 5HDEC 15)	COM2057
267	FORMAT (1H A3,12,F10.2,F10.2,F10.2,F10.2,F10.2,F10.2)	COM2058
268	FORMAT (1H A5,F10.2,15)	COM2059
269	FORMAT (1H0 37H FOLLOWING CARD ILLEGAL IN TIME BLOCK /1H A3,12,12A	COM2060
	15)	COM2061
270	FORMAT (1H0 83H AN ILLEGAL CHARACTER HAS BEEN REPLACED BY A ZERO ICOM	COM2062
	IN THE FOLLOWING CARD, TIME BLOCK /1H A3,12,F10.2,F10.2,F10.2,F10.	COM2063
	22,F10.2,F10.2)	COM2064
	DIMENSION CODE(8)	COM2071
	DATA CODE /6HDEC ,6H ,6HINC ,6HPER ,6HNBK ,6HNBK ,6COM2072	
	1HRES ,6HCAP /	COM2073
	DIMENSION IERROR(1)	COM2074
	DATA IERROR(1)/32/,NERROR/1/	COM2075
	CALL FXPPT(IERROR,NERROR)	COM2076
	CALL FSWTON(3,32,33,45)	
	CALL FXNPRT(1,32)	
	MAXAE = 16000	DIAG0761
	NSW2=1	COMP077
	NGRC=1	COMP078
	NGRC1=1	COMP078
	KGRC=1	COMP078
	KOUNT = 1	COMP078
	MAXT = 0	COMP079
	MAXR = 0	COMP080
	MAXC = 0	COMP081
	MAXP = 0	COMP082
	L = 0	COMP083
	DO 131 I=1,5000	22660831
	KDAT(I)=10	22660832
131	CONTINUE	22660833
	IK = 1	COMP084
	MAXS=1	COMP085
132	READ (4, 218) KOD, KOD 1	COMP086
	IERROR(1)=IABS(IERROR(1))	
	IF (NGRC.EQ.2.AND.NGRC1.EQ.2) NGRC=1	COM20861
	IF (NGRC.EQ.2) NGRC1=2	COM20862
	GO TO (134, 135, 136, 137, 138, 139), KOUNT	COMP087

TABLE E-2 (Continued)

C	READ IN INITIAL TEMPERATURES OF ALL NODES	COMP088
C		COMP089
134	GO TO (3,13,9,13,14,13,13,13),KOD	COMP090
3	READ (4, 200) (I 1(I), A(I), I = 1, KOD 1)	COM2091
	IF ( IERROR(1).GT.0) GO TO 500	COMP092
	WRITE (6, 350) ( I1(I), A(I), I=1, KOD1)	COM20921
	IERROR(1) =IABS(IERROR(1))	COM20922
500	CONTINUE	COM20923
	DO 7 I = 1, KOD 1	COM20924
	J = I 1(I)	COMP093
	IF (J - MAXT) 5, 5, 4	COMP094
4	MAXT = J	COMP095
5	IF (J.EQ.0) WRITE (6,232) J,A(I)	COMP096
	IF (J.EQ.0) ERROR=1.	COMP097
6	P(J) = A(I)	COMP0971
	ITEM = J	COMP098
	ATEM = A(I)	COMP099
7	CONTINUE	COMP100
	GO TO 132	COMP101
9	READ (4, 201) N 1, A 1, N 2	COMP102
	IF (IERROR(1).GT.0) GO TO 501	COMP103
	WRITE (6,351) N1,A1,N2	COM21031
	IERROR(1) =IABS(IERROR(1))	COM21032
501	CONTINUE	COM21033
	J = ITEM	COM21034
	AA = ATEM	COMP104
	DO 12 I = 1, N 2	COMP105
	J = J + N 1	COMP106
	AA = AA + A 1	COMP107
	IF (J.GT.MAXT) MAXT=J	COMP108
11	P(J) = AA	COMP109
	ITEM = J	COMP111
	ATEM = AA	COMP112
12	CONTINUE	COMP113
	GO TO 132	COMP114
13	READ (4,210) (A(I), I=1,12)	COMP115
	WRITE (6,352) CODE(KOD),KOD1, (A(I),I=1,12)	COM21160
	ERROR = 2.	COM21161
	IERROR(1)=IABS(IERROR(1))	COM21162
	GO TO 132	COM21163
14	KOUNT = KOUNT + 1	COM21164
	TEMPX=0.	COMP118
	DO 141 I=1,MAXT	22661181
	IF (KDAT(I).EQ.10) P(I)=TEMPX	22661182
	IF (KDAT(I).NE.10) TEMPX=P(I)	22661183
141	CONTINUE	22661184
	READ (4, 200) I 1(I)	22661185
	IERROR(1) =IABS(IERROR(1))	COMP119
	WRITE (3) MAXT, NCVG, NSTS	COM21191
	WRITE (3) (P(I), I = 1, MAXT)	COMP120
	WRITE (3) MAXT, NCVG, NSTS	COMP121
	WRITE (3) (P(I), I = 1, MAXT)	COMP122
	DO 15 I = 1, 5000	COMP123
	P(I) = 0.	COMP124
15	CONTINUE	COMP125
	WRITE (6,250) MAXT,MAXT	COMP126
	MAXIM=MAXT+MAXT	COM21261
	WRITE (6,251) MAXT,MAXIM	COM21262
	GO TO 132	COM21263
C		COMP127
C	READ IN RESISTERS	COMP128
C		COMP129
135	GO TO (17,16,24,16,30,16,29,16), KOD	COMP130
16	READ (4,210) (A(I),I=1,12)	COM21310
		22661311

TABLE E-2 (Continued)

WRITE (6,353) CODE(KOD),KOD1, (A(I),I=1,12)	COM21312
IERROR(1) = IABS(IERROR(1))	COM21313
GO TO 132	COM21314
17 READ (4, 202) (I 1(I), I 2(I), I 3(I), A(I), I = 1, KOD 1)	COMP132
IF (IERROR(1).GT.0) GO TO 175	COM21321
WRITE (6,2531)	COM21322
WRITE (6,354) CODE(KOD), KOD1,(I1(I),I2(I),I3(I),A(I),I=1,KOD1)	COM21323
IERROR(1) = IABS(IERROR(1))	COM21324
175 CONTINUE	COM21325
18 DO 22 I=1,KOD1	COM2133
J = I 1(I)	COMP134
IF (J.GT.MAXR) MAXR=J	COMP135
19 IF (J.LE.0) WRITE (6,233) I1(I),I2(I),I3(I),A(I)	COMP137
IF (J.LE.0) ERROR=1.	COMP1371
20 P(J) = A(I)	COMP138
L = L + 1	COMP139
IRLINE(L) = I 3(I) + 4096*(I 2(I) + 4096*J)	COMP140
IF (J.GE.2048) IRLINE(L)=-IRLINE(L)	COM21401
ITEM = J	COMP141
ITEM 2 = I 2(I)	COMP142
ITEM 3 = I 3(I)	COMP143
ATEM = A(I)	COMP144
IF (ITEM2.LE.MAXT.AND.ITEM3.LE.MAXT) GO TO 22	COM21441
WRITE (6,234) ITEM,ITEM2,ITEM3,MAXT	COM21442
ERROR=1.	COM21443
22 CONTINUE	COMP145
GO TO 132	COMP146
25 READ (4,241) I1(1),I2(1),I3(1),X,Y,Z,KRVC,N2	COM21461
IF (IERROR(1).GT.0) GO TO 2502	COM21462
WRITE (6,2531)	COM21463
WRITE (6,356) CODE(3),I1(1),I2(1),I3(1),X,Y,Z,KRVC,N2	COM21464
IERROR(1) = IABS(IERROR(1))	COM21465
2502 CONTINUE	COM21466
J=ITEM	COM21462
DO 2501 I=1,N2	COM21463
J=J+I1(1)	COM21464
ITEM2=ITEM2+I2(1)	COM21464
ITEM3=ITEM3+I3(1)	COM21464
X1=X1+X	COM21464
Y1=Y1+Y	COM21464
Z1=Z1+Z	COM21464
KKRV=KKRV+KCRV	COM21464
IF (J.GT.MAXR) MAXR=J	COM21465
P(J)=X1/(Y1*Z1)	COM21465
L=L+1	COM21465
IRLINE(L)=ITEM3+4096*(ITEM2+4096*J)	COM21466
IF (J.GE.2048) IRLINE(L)=-IRLINE(L)	COM21467
ITEM=J	COM21467
NGRC(KGRC)=J+4096*KKRV	COM21467
KGRC=KGRC+1	COM21468
IF (ITEM2.LE.MAXT.AND.ITEM3.LE.MAXT) GO TO 2501	COM21469
WRITE (6,234) ITEM,ITEM2,ITEM3,MAXT	COM2147
ERROR=1.	COM21471
CONTINUE	COM21472
GO TO (2401,25),NGRC	COM21472
2401 READ (4,203) I1(1),I2(1),I3(1),A(1),N2	COM21478
IF (IERROR(1).GT.0) GO TO 2402	COM21479
WRITE (6,2531)	COM21480
WRITE (6,357) CODE(3),I1(1),I2(1),I3(1),A(1),N2	COM21481
IERROR(1) = IABS(IERROR(1))	COM21482
CONTINUE	COM21483

TABLE E-2 (Continued)

	J = ITEM	
	DO 28 I = 1, N 2	COM21484
	J = J + I 1(1)	COMP149
	ITEM 2 = ITEM 2 + I 2(1)	COMP150
	ITEM 3 = ITEM 3 + I 3(1)	COMP151
	AITEM = AITEM + A(1)	COMP152
	IF (J.GT.MAXR) MAXR=J	COMP153
26	P(J) = AITEM	COM2154
	L = L + 1	COMP156
	IRLINE(L) = ITEM 3 + 4096*(ITEM 2 + 4096*J)	COMP157
	IF (J.GE.2048) IRLINE(L)=-IRLINE(L)	COMP158
	ITEM = J	COM21581
	IF (ITEM2.LE.MAXT.AND.ITEM3.LE.MAXT) GO TO 28	COMP159
	WRITE (6,234) ITEM,ITEM2,ITEM3,MAXT	COM21591
	ERROR=1.	COM21592
28	CONTINUE	COM21593
	GO TO 132	COMP160
29	READ (4,240) I1(1),I2(1),I3(1),X,Y,Z,KCRV	COMP161
	IF (IERROR(1).GT.0) GO TO 2901	COM21161
	WRITE (6,2531)	COM21611
	WRITE (6,356) CODE(7),I1(1),I2(1),I3(1),X,Y,Z,KCRV	COM21612
	IERROR(1) = IABS(IERROR(1))	COM21613
2901	CONTINUE	COM21614
	A(1)=X/(Y*Z)	COM21615
	NGRC=2	COM21162
	X1=X	COM21162
	Y1=Y	COM21162
	Z1=Z	COM21162
	NSTR(KGRC)=I1(1)+4096*KCRV	COM21162
	KGRC=KGRC+1	COM21163
	KKRV=KCRV	COM21164
	GO TO 18	COM21164
30	KOUNT = KOUNT + 1	COM21165
	READ (4, 202) I 1(1)	COMP162
	IERROR(1) = IABS(IERROR(1))	COMP163
	WRITE (3) MAXR, NCVG, NSTS	COM21631
	WRITE (3) (P(I), I = 1, MAXR)	COMP164
	DO 31 I = 1, MAXR	COMP165
	P(I) = 0.	COMP166
31	CONTINUE	COMP167
	MAXIM=MAXIM+MAXR	COMP168
	WRITE (6,252) MAXR,MAXIM	COM21681
	GO TO 132	COM21682
C		COMP169
C	READ IN CAPACITORS	COMP170
C		COMP171
136	GO TO (33,32,46,32,52,32,32,43), KOD	COMP172
32	READ (4,210) (A(I),I=1,12)	COM2174
	WRITE (6,358) CODE(KOD),KOD1, (A(I),I=1,12)	COM21741
	IERROR(1) = IABS(IERROR(1))	COM21742
	GO TO 132	COM21743
33	READ (4, 200) (I 1(I), A(I), I = 1, KOD 1)	COM21744
	IF (IERROR(1).GT.0) GO TO 3301	COMP174
	WRITE (6,259)	COM21745
	WRITE (6,260) CODE(KOD), KOD1, (I1(I),A(I),I=1,KOD1)	COM21746
	IERROR(1) = IABS(IERROR(1))	COM21747
3301	CONTINUE	COM21748
	NOP = 0	COM21749
39	DO 42 I = 1, KOD 1	COMP175
	J = I 1(I)	COMP176
	IF (J.GT.MAXT) WRITE (6,235) J,MAXT	COMP177
		COM2178



TABLE E-2 (Continued)

	IF (J.GT.MAXI) ERROR=1.	COMP2178
	IF (J.GT.MAXC) MAXC=J	COMP178
35	IF (J.LE.0) WRITE (6,232) J,A(I)	COMP180
	IF (J.LE.0) ERROR=1.	COMP1801
36	P(J) = A(I)	COMP181
	ITEM = J	COMP182
	ATEM = A(I)	COMP183
	KPSD(IK)=I1(I)+4096*(KKRV+4096*KKRV1)	COMP2184
	KPSD(IK)=-KPSD(IK)	COMP21841
	MAXP = MAXP + 1	COMP185
	NODCON=0	
	IK = IK + 1	COMP186
	DO 41 K = 1, L	COMP187
	IDAT 1 = IRLINE(K)/16777216	COMP188
	IF (IRLINE(K).LT.0) IDAT1=IABS(IDAT1)+2048	COMP21881
	IDAT 2 = MOD(IRLINE(K)/4096, 4096)	COMP189
	IDAT 3 = MOD(IRLINE(K), 4096)	COMP190
	IF (IRLINE(K).LT.0) IDAT2=IABS(IDAT2)	COMP21901
	IF (IRLINE(K).LT.0) IDAT3=IABS(IDAT3)	COMP21901
	IF (I 1(I) - IDAT 2) 38, 37, 38	COMP191
37	DO 3601 I9=1,KGRC	COMP2192
	KGR=MOD(NSRT(I9),4096)	COMP21921
	KGK=MOD(NSRT(I9)/4096,4096)	COMP21921
	IF (KGR.EQ.IDAT1) GO TO 3602	COMP21922
3601	CONTINUE	COMP21923
	KGK=0	COMP21924
3602	KPSD(IK)=IDAT3+4096*(IDAT1+4096*KGK)	COMP21925
	IF (KGR.EQ.IDAT1) NSRT(I9)=0	COMP21926
	MAXP = MAXP + 1	COMP193
	NODCON=1	
	IK = IK + 1	COMP194
38	IF (I 1(I) - IDAT 3) 41, 40, 41	COMP195
40	DO 4001 I9=1,KGRC	COMP2196
	KGR=MOD(NSRT(I9),4096)	COMP21961
	KGK=MOD(NSRT(I9)/4096,4096)	COMP21961
	IF (KGR.EQ.IDAT1) GO TO 4002	COMP21962
4001	CONTINUE	COMP21963
	KGK=0	COMP21964
4002	KPSD(IK)=IDAT2+4096*(IDAT1+4096*KGK)	COMP21965
	IF (KGR.EQ.IDAT1) NSRT(I9)=0	COMP21966
	MAXP = MAXP + 1	COMP197
	NODCON=1	
	IK = IK + 1	COMP198
41	CONTINUE	COMP199
	IF (NODCON.EQ.1) GO TO 42	
	ERROR=1.	COMP1991
	WRITE (6,236) I1(I)	COMP1992
42	CONTINUE	COMP200
	IF (NOP) 132, 132, 48	COMP201
43	READ (4,242) I1(I),X,Y,Z,KKRV,KKRV1	COMP22011
	IF (IERROR(1).GT.0) GO TO 4201	COMP22011
	WRITE (6,259)	COMP22012
	WRITE (6,261) CODE(KOD),I1(I),X,Y,Z,KKRV,KKRV1	COMP22013
	IERROR(1) = IABS(IERROR(1))	COMP22014
4201	CONTINUE	COMP22015
	A(I)=X*Y*Z	COMP22012
	NGRC=2	COMP22013
	GO TO 39	COMP22014
46	GO TO (47,4701),NGRC	COMP2202
47	READ (4,201) N1,A1,N2	COMP22021
	IF (IERROR(1).GT.0) GO TO 471	COMP22022
	WRITE (6,358)	COMP22023

TABLE E-2 (Continued)

	WRITE (6,262) N1,A2,N2	COM22024
	IERROR(1) = IABS(IERROR(1))	COM22025
471	CONTINUE	COM22026
	NOP = NOP + 1	COMP203
	KOD 1 = 1	COMP204
	GO TO 50	COMP205
4701	READ (4,243) N1,X1,Y1,Z1,IK1,IK2,N2	COM22051
	IF (IERROR(1).GT.0) GO TO 4705	COM22052
	WRITE (6,358)	COM22053
	WRITE (6,263) N1,X1,Y1,Z1,IK1,IK2,N2	COM22054
	IERROR(1) = IABS(IERROR(1))	COM22055
4705	CONTINUE	COM22056
	KOD1=1	COM22052
	GO TO 49	COM22053
4702	I1(1)=ITEM+N1	COM22054
	X=X+X1	COM22055
	Y=Y+Y1	COM22055
	Z=Z+Z1	COM22055
	A(I)=X*Y*Z	COM22056
	KKRV=KKRV+IK1	COM22056
	KKRV1=KKRV1+IK2	COM22056
	GO TO 39	COM22057
48	IF (NOP - N 2) 49, 132, 132	COMP206
49	NOP = NOP + 1	COMP207
	GO TO (50,4702),NGRC	COM22071
50	I 1(1) = ITEM + N 1	COMP208
	A(1) = ATEM + A 1	COMP209
	GO TO 39	COMP210
52	KOUNT = KOUNT + 1	COMP211
	MAXP = MAXP + 1	COMP212
	KPSD(MAXP) = 0	COMP213
	READ (4, 200) I 1(1)	COMP214
	IERROR(1) = IABS(IERROR(1))	COM22141
	WRITE (3) MAXC, NCVG, NSTS	COMP215
	WRITE (3) (P(I), I = 1, MAXC)	COMP216
	DO 53 I = 1, MAXC	COMP217
	P(I) = 0.	COMP218
53	CONTINUE	COMP219
	WRITE (3) MAXC, NCVG, NSTS	COMP220
	WRITE (3) (P(I), I = 1, MAXC)	COMP221
	WRITE (3) MAXC, NCVG, NSTS	COMP222
	WRITE (3) (P(I), I = 1, MAXC)	COMP223
	WRITE (3) MAXP, NCVG, NSTS	COMP224
	WRITE (3) (KPSD(I), I = 1, MAXP)	COMP225
	NWPD = MAXP	COMP226
	NRECD = 7	COMP227
	KSP = 2*MAXT + MAXR + 3*MAXC + 1	COMP228
	KST = KSP + MAXP	COMP229
	KST 1 = KST	COMP230
	NKSP = KST - 1	COMP231
	JJ = 0.	COMP232
	N2=0	COMP2321
	MAXIM=MAXIM+MAXC	COM22322
	WRITE (6,253) MAXC,MAXIM	COM22323
	MAXIM=MAXIM+MAXC	COM22324
	WRITE (6,254) MAXC,MAXIM	COM22325
	MAXIM=MAXIM+MAXC	COM22326
	WRITE (6,255) MAXC,MAXIM	COM22327
	MAXIM=MAXIM+MAXP	COM22328
	WRITE (6,256) MAXP,MAXIM	COM22329
	GO TO 132	COMP233
C	READ IN DATA SUB-BLOCKS	COMP234
C		COMP235
C		COMP236
	137 GO TO (56,55,66,67,68,55,55,55,691) ,KOD	COM2237

TABLE E-2 (Continued)

55	READ (4,210) (A(I),I=1,12)	COM22371
	WRITE (6,264) CODE(KOD), KOD1, (A(I),I=1,12)	COM22372
	IERROR(1) = IABS(IERROR(1))	COM22373
	GO TO 132	COM22374
56	IF (KOD 1) 57, 57, 64	COMP238
57	READ (4, 204) NTAB	COMP239
	IF (IERROR(1).GT.0) GO TO 5701	COM22391
	WRITE (6,265)	COM22392
	WRITE (6,266) NTAB	COM22393
	IERROR(1) = IABS(IERROR(1))	COM22394
5701	CONTINUE	COM22395
	IF (NTAB) 62, 58, 59	COMP240
58	WRITE (6, 220)	COMP241
	GO TO 132	COMP242
59	IF (NSW2.EQ.1) GO TO 591	COMP243
	WRITE (6,230) NTABO,NTAB	COMP2431
	ERROR=1.	COMP2432
	NSW2=1	COMP2433
	KST=KST1+JJ	COMP2434
591	NSTRT(MAXS)=KST+2**18*NTAB	COM22435
	NSW2=2	COMP2436
	NTABO=NTAB	COMP2437
	MAXS=MAXS+1	COMP244
	GO TO 132	COMP246
62	IF (NSW2.EQ.2) GO TO 621	COMP247
	WRITE (6,231) NTABO	COMP2471
	ERROR=1.	COMP2472
621	NSW2=1	COMP2473
	IF (NTAB+7) 63,61,63	COMP2474
61	KURV 7 = KST 1 + JJ - KST	COMP248
63	KST = KST 1 + JJ	COMP249
	GO TO 132	COMP250
64	READ (4, 205) (A(I), I = 1, KOD 1)	COMP251
	IF (IERROR(1).GT.0) GO TO 6401	COM22511
	WRITE (6,265)	COM22512
	WRITE (6,267) CODE(KOD),KOD1,(A(I),I=1,KOD1)	COM22513
	IERROR(1) = IABS(IERROR(1))	COM22514
6401	CONTINUE	COM22515
641	DO 65 I = 1, KOD 1	COM2252
	JJ = JJ + 1	COMP253
	P(JJ) = A(I)	COMP254
65	CONTINUE	COMP255
	IF (N2.GT.0) GO TO 661	COM22551
	GO TO 132	COMP256
66	READ (4,206) AINC,N2	COM22561
	IF (IERROR(1).GT.0) GO TO 6601	COM22562
	WRITE (6,265)	COM22563
	WRITE (6,268) CODE(KOD),AINC,N2	COM22564
	IERROR(1) = IABS(IERROR(1))	COM22565
6601	CONTINUE	COM22566
	A(1)=P(JJ)	COM22562
	KOD1=1	COM22562
661	A(1)=A(1)+AINC	COM22563
	N2=N2-1	COM22564
	GO TO 641	COM22565
67	READ (4, 205) A(1)	COMP257
	IF (IERROR(1).GT.0) GO TO 6701	COM22571
	WRITE (6,265)	COM22572
	WRITE (6,268) CODE(KOD),A(1)	COM22573
	IERROR(1) = IABS(IERROR(1))	COM22574
6701	CONTINUE	COM22575

TABLE E-2 (Continued)

	P(JJ + 1) = 32767.	COMP258
	P(JJ + 2) = A(1)	COMP259
	JJ = JJ + 2	COMP260
	GO TO 132	COMP261
68	KOUNT = KOUNT + 1	COMP262
	KST = KST - 1	COMP263
	NWCT = JJ	COMP264
	WRITE (3) NWCT, NCVG, NSTS	COMP265
	WRITE (3) (P(I), I = 1, NWCT)	COMP266
	NRECD = NRECD + 2	COMP267
	READ (4, 205) A(1)	COMP268
	IERROR(1) = IABS(IERROR(1))	COM22681
	WRITE (3) MAXS, NCVG, NSTS	COMP269
	WRITE (3) (NSTRI(I), I = 1, MAXS)	COMP270
	NWST = MAXS	COMP271
	JJ = 0	COMP272
	DO 69 I=1,40	COM22721
	P(I)=0.	COM22722
69	CONTINUE	COM22723
	MAXIM=MAXIM+NWCT	COM22724
	WRITE (6,257) NWCT,MAXIM	COM22725
	MAXIM=MAXIM+MAXS	COM22726
	WRITE (6,258) MAXS,MAXIM,MAXIM	COM22727
	IF (MAXIM.LT.MAXMUM) GO TO 132	COM22731
	ERROR=1.	COM22732
	WRITE (6,244) MAXMUM,MAXIM	COM22733
	IF (MAXIM.LE.16000) WRITE (6,245)	DIAG2733
	IF (MAXIM.GT.16000) WRITE (6,244) MAXAB,MAXIM	DIAG2734
	GO TO 132	COM22734
691	READ (4,204) ICOD	COM22731
	KDAT(JJ+1) = 32765	COM22732
	KDAT(JJ+2) = ICOD	COM22733
	JJ = JJ+2	COM22734
	GO TO 132	COM22735
138	GO TO (70,73,73,73,72,72) ,KOD	COM2274
73	READ (4,210) (A(I), I=1,12)	COM22741
	WRITE (6,269) CODE(KOD),KOD1,(A(I),I=1,12)	COM22742
	IERROR(1) = IABS(IERROR(1))	COM22743
	GO TO 132	COM22744
C70	READ (4, 200) (I1(I),A(I),I=1,KOD1)	COM2275
70	READ (4, 205) (A(I),I=1,KOD1)	COM2275
	IF (IERROR(1).GT.0) GO TO 7001	COM22751
	WRITE (6,270) CODE(KOD), KOD1, (A(I),I=1,KOD1)	COM22752
	IERROR(1) = IABS(IERROR(1))	COM22753
7001	CONTINUE	COM22754
	DO 71 I = 1, KOD 1	COMP276
	JJ = I1(I)	COMP277
	JJ = JJ+1	COMP277
	P(JJ+20)=A(I)	COMP278
71	CONTINUE	COMP279
	GO TO 132	COMP280
72	KOUNT = KOUNT + 1	COMP281
C	THE FOLLOWING 5 CARDS GO WITH THE NON-C CARDS ABOVE	
	P(1)=P(23)	COM22810
	P(2)=P(23)	COM22810
	P(3)=P(22)	COM22810
	P(4)=P(21)	COM22810
	IF (P(24).NE.0.) P(7)=P(24)	COM22810
	P(11)=P(2)	COM22810
	JJ=16	COM22811
	WRITE (3) JJ, NCVG, NSTS	COMP282
	WRITE (3) (P(I), I = 1, JJ)	COMP283
	NWTM = JJ	COMP284
	END FILE 3	COMP285
	NRECD=9	COM22851
	REWIND 4	COMP286
139	REWIND 3	COMP287
	RETURN	COMP288
	END	

TABLE E-2 (Continued)

5IBFTC DIAG11	
SUBROUTINE RESTR	REST0002
AS OF 04/27/65	
COMMON P, M, MAXT, MAXR, MAXC, KSP, KST, KURV 7, NCVG, NSTS, NFAB	COMP004
COMMON NABL, NKSP, LMMF, NRMF, NREAD, CC	COMP005
COMMON NRECD, NRPD, NWCT, NWST, NWTM	COMP006
COMMON /CP2/ERROR, MAXMUM	REST006
COMMON /CPPLT/NPLT, NEND	
DIMENSION A(12), I 1(12), I 2(12), I 3(12), NABL(10), CC(12)	COMP007
DIMENSION A1(6)	REST007
DIMENSION CZ(6), CY(6)	REST007
DIMENSION P(14000), IRLINE(1), KPSD(1), NSTRT(1), M(16), KDAT(1)	COMP008
EQUIVALENCE (P(4000), IRLINE(1)), (P(8000), KPSD(1)), (P(13000),	COMP009
1 NSTRT(1)), (P(1), KDAT(1))	COMP010
REAL M, INC, NBK, NET	COMP0
INTEGER CP	COMP011
DATA ENDF/6H -1 /	COMP011
DATA NET/6HNET /	COMP011
DATA DEC/6HDEC /	COMP011
DATA INC/6HINC /	COMP011
DATA PER/6HPER /	COMP011
DATA NBK/6HNBK /	COMP011
DATA CID/6HCID /	COMP011
DATA TAP/6HTAP /	COMP011
DATA COD/6HCOD /	REST011
DATA ZERO/6H000000/	COMP011
DATA END /6HEND /	REST011
DATA (CY(I), I=1,6)/2H 1,2H 2,2H 3,2H 4,2H 5,2H 6/,ZERZ/2H00/	REST011
DATA (CZ(I), I=1,6)/2H01,2H02,2H03,2H04,2H05,2H06/,BLANK/1H /	REST011
DATA ZERY/2H 0/	REST011
DIMENSION CODE(4)	22660111
DATA CODE/6HDEC ,6HINC ,6HPER ,6HNBK /	22660112
200 FORMAT (5X, 4(I 5, E 10.2))	COMP015
201 FORMAT (5X, I 5, E 10.2, I 5)	COMP016
202 FORMAT (5X, 2(3I 5, E 10.2))	COMP017
203 FORMAT (5X, 3I 5, E 10.2, I 5)	COMP018
204 FORMAT (5X, I 5)	COMP019
205 FORMAT (5X, 6E 10.2)	COMP020
208 FORMAT (1H1,A3,I2,12A6)	COMP021
209 FORMAT (A3,A2,12A6)	REST021
210 FORMAT (5X,12A6)	COMP021
211 FORMAT (5X, A3,I2,12A6)	COMP022
212 FORMAT (1H1,9X,12A6)	REST023
214 FORMAT (29HO INPUT MUST BE BAD, QUIT JOB )	COMP024
215 FORMAT (40HO KOUNT IS NOT CORRECT IN RESTRT ROUTINE )	COMP025
216 FORMAT (I 3, A 6)	COMP026
218 FORMAT (I 3, 3X, I 2)	COMP027
219 FORMAT (38HO KOD IS NOT CORRECT IN RESTRT ROUTINE )	COMP028
220 FORMAT (26HOTABLE NO. = 0 IS ILLEGAL.)	COMP029
222 FORMAT (30HO TOO MANY WORDS IN DAT BLOCK )	COMP030
223 FORMAT (7HOCODE= A6,12H IS ILLEGAL.)	COMP021
224 FORMAT (25HOCANNOT FIND CURVE NAMED A6,17H ON LIBRARY TAPE.)	COMP021
230 FORMAT (28HOSOMETHING WRONG AFTER TABLE16,17H AND BEFORE TABLE16)	COMP021
231 FORMAT (25HOSOMETHING WRONG IN TABLE I6)	COMP021
236 FORMAT (15HOBLOCK NUMBER =I6,29H IS ILLEGAL. RESTART DELETED. )	REST021
237 FORMAT (14H1END OF CASES.)	REST021
241 FORMAT (5X,E10.0,I5)	REST021
242 FORMAT (5X,2E10.0,I5)	REST021
243 FORMAT (5X,3E10.0,I5)	REST021
244 FORMAT (5X,4E10.0,I5)	REST021
245 FORMAT (5X,5E10.0,I5)	REST021

TABLE E-2 (Continued)

246	FORMAT (5X,6E10.0,I5)	
280	FORMAT (1H0 44H FOLLOWING CARD OUT OF PLACE IN THIS RESTART)	REST021
251	FORMAT (1H A3,I2,I2A6)	22660221
252	FORMAT (1H0 70H AN ILLEGAL CHARACTER HAS BEEN REPLACED BY ZERO IN THE FOLLOWING CARD /5X,5HDEC I5)	22660222
253	FORMAT (1H0 64H FOLLOWING CARD ILLEGAL IN TEMPERATURE BLOCK OF PREVIOUS RESTART)	22660223
254	FORMAT (1H0 88H TERMINATING CARD OF ONE OF THE BLOCKS IN PREVIOUS RESTART CONTAINS AN ILLEGAL CHARACTER)	22660226
255	FORMAT (1H0113H AN ILLEGAL CHARACTER HAS BEEN REPLACED BY A ZERO IN THE FOLLOWING CARD OF THE TEMP BLOCK OF THE PREVIOUS RESTART)	22660228
256	FORMAT (1H 5X,A3,I2,I5,F10.2,I5)	22660229
257	FORMAT (1H0 61H FOLLOWING CARD ILLEGAL IN RESISTOR BLOCK OF PREVIOUS RESTART)	2266023
258	FORMAT (1H A3,I2,6F10.2)	22660231
259	FORMAT (1H0116HAN ILLEGAL CHARACTER HAS BEEN REPLACED BY A ZERO IN THE FOLLOWING CARD OF THE RESISTOR BLOCK OF THE PREVIOUS RESTART)	22660233
260	FORMAT (1H0 62H FOLLOWING CARD ILLEGAL IN CAPACITOR BLOCK OF PREVIOUS RESTART)	22660234
261	FORMAT (1H0112H AN ILLEGAL CHARACTER HAS BEEN REPLACED BY A ZERO IN THE FOLLOWING CARD OF THE CAP BLOCK OF THE PREVIOUS RESTART)	22660235
262	FORMAT (1H0 57H FOLLOWING CARD ILLEGAL IN TIME BLOCK OF PREVIOUS RESTART)	22660237
263	FORMAT (1H0113H AN ILLEGAL CHARACTER HAS BEEN REPLACED BY A ZERO IN THE FOLLOWING CARD OF THE TIME BLOCK OF THE PREVIOUS RESTART)	22660238
264	FORMAT (1H0115H AN ILLEGAL CHARACTER HAS BEEN REPLACED BY A ZERO IN THE FOLLOWING CARD IN A DATA SUB-BLOCK OF THE PREVIOUS RESTART)	22660239
265	FORMAT (1H A3,I2,F10.2,I5)	22660240
266	FORMAT (1H A3,I2,2F10.2,I5)	22660241
267	FORMAT (1H A3,I2,3F10.2,I5)	22660242
268	FORMAT (1H A3,I2,4F10.2,I5)	22660243
269	FORMAT (1H A3,I2,5F10.2,I5)	22660244
270	FORMAT (1H A3,I2,5F10.2,I5)	22660245
271	FORMAT (5X,3H***,5X,6HCURVE A6,36H FROM LIBRARY TAPE WILL APPEAR HERE.)	22660246
	DIMENSION IERROR(1)	22660247
	DATA IERROR(1) /32/,NERROR/1/	22660248
	CALL FXPPT (IERROR,NERROR)	22660249
	CALL FSXTON(3,32,33,45)	22660250
	CALL FXNPRT(1,32)	22660251
	NRECD=9	22660252
	MATLIB =1	CEST032
	LINE=1	COMP032
149	REWIND 4	COMP032
139	REWIND 3	COMP288
	DO 310 I = 1, 16	COMP301
	M(I) = 0.0	COMP302
310	CONTINUE	COMP303
	M(7) = 0.25	COMP304
	MAXP = 0	COMP305
	JJ = 1	COMP306
	DO 75 I = 1, NRECD	COMP307
	READ (3) N 1	COMP308
	MAXP = MAXP + N 1	COMP309
	READ (3) (P(J), J = JJ, MAXP)	COMP310
	JJ = MAXP + 1	COMP311
75	CONTINUE	COMP312
	READ (3) N 1	COMP313
	READ (3) (M(I), I=1,N1)	COMP314
	REWIND 3	REST315
	IF (MAXP -MAXMUM) 701,701,81	COMP317
81	WRITE (6, 222)	COMP318
		COMP322

TABLE E-2 (Continued)

100	ERROR=2.	COMP323
701	IF (MATLIB.EQ.1) READ (5,209) CM,CX,(A(I),I=1,12) CP=-1	REST325
1101	DO 1102 I=1,6	REST3251
1102	IF (CX.EQ.CY(I).OR.CX.EQ.CZ(I)) CP=1 IF (CX.EQ.BLANK.OR.CX.EQ.ZERZ.OR.CX.EQ.ZERY) CP=0 IF (CP.GE.0) GO TO 1103 WRITE (6,215) ERROR=1. CP=0	REST3251 REST3251 REST3251 REST3251 REST3251 REST3251 REST3251
1103	IF (CM.EQ.END) GO TO 900 IF (CM.EQ.TAP) GO TO 150 IF (LINE.LT.60) GO TO 7011 WRITE (6,212) (CC(I),I=1,12) LINE = 1	REST3251 REST3251 REST3251 REST3252 REST3253 REST3254 REST3255 REST3256
7011	IF (CM.EQ.CTD) GO TO 117 WRITE (6,211) CM,CP,(A(I),I=1,12) LINE = LINE+1 IF (CM.EQ.DEC) GO TO 702 IF (CM.EQ.INC) GO TO 703 IF (CM.EQ.COD) GO TO 707 IF (CM.EQ.PER) GO TO 704 IF (CM.EQ.NRK) GO TO 705 WRITE (6,223) CM ERROR=1. GO TO 701	REST3257 COMP332 COMP333 REST333 COMP334 COMP335 REST336 REST3361 REST3362 REST3363 REST3364 REST3365 REST3366 REST3367 REST3367 REST3368 REST3369 DIAG3372 DIAG3373 DIAG3374 REST338 REST3381 REST3382
117	CMID=CM ICP=CP DO 1171 I=1,12 CC(I)=A(I)	COMP332 COMP333 REST333 COMP334 COMP335 REST336 REST3361 REST3362 REST3363 REST3364 REST3365 REST3366 REST3367 REST3367 REST3368 REST3369 DIAG3372 DIAG3373 DIAG3374 REST338 REST3381 REST3382
1171	CONTINUE LINE=1 WRITE (6,212) (CC(I),I=1,12) GO TO 701	REST3367 REST3367 REST3368 REST3369 DIAG3372 DIAG3373 DIAG3374 REST338 REST3381 REST3382
150	WRITE (6,211) CM,CP,(A(I),I=1,12) WRITE (6,271) A(1) LINE = LINE + 2 GO TO 701	REST3382 COMP339 COMP340 COMP341 COMP342 REST3421 REST3422 COMP343 REST347 COMP348 REST349 REST3491 REST3492 REST3493
702	KOD=1 GO TO 706	COMP343 REST347 COMP348 REST349 REST3491 REST3492 REST3493
703	KOD = 2 GO TO 706	COMP343 REST347 COMP348 REST349 REST3491 REST3492 REST3493
704	KOD = 3 GO TO 706	COMP343 REST347 COMP348 REST349 REST3491 REST3492 REST3493
707	KOD = 5 GO TO 706	COMP343 REST347 COMP348 REST349 REST3491 REST3492 REST3493
705	KOD = 4	COMP343 REST347 COMP348 REST349 REST3491 REST3492 REST3493
706	WRITE (4,218) KOD,CP WRITE (4, 210) (A(I), I = 1, 12) IF (KOD.LT.4) GO TO 701 IF (KOD.EQ.4) GO TO 708 WRITE (6,215) ERROR=1.	COMP343 REST347 COMP348 REST349 REST3491 REST3492 REST3493
708	END FILE 4 REWIND 4	COMP343 REST347 COMP348 REST349 REST3491 REST3492 REST3493
714	READ (4, 218) KOD, KOD 1 IERROR(1) = IABS(IERROR(1)) GO TO (717,1221,1221,719),KOD	COMP343 REST347 COMP348 REST349 REST3491 REST3492 REST3493
1221	READ (4,210) (A(I),I=1,12) WRITE (6,280) WRITE (6,251) CODE(KOD),KOD1,(A(I),I=1,12) IERROR(1) = IABS(IERROR(1)) GO TO 714	COMP343 REST347 COMP348 REST349 REST3491 REST3492 REST3493
717	IF (KOD 1) 718, 718, 716	COMP343 REST347 COMP348 REST349 REST3491 REST3492 REST3493
716	WRITE (6, 250)	COMP343 REST347 COMP348 REST349 REST3491 REST3492 REST3493

TABLE E-2 (Continued)

250	FORMAT (43H KOUNT HAS BEEN INCLUDED ON BLOCK FLAG CARD )	COMP356
	ERROR=1.	REST357
	GO TO 714	REST3571
719	REWIND 4	COMP358
	REWIND 3	COMP359
	MAXP = 0	COMP360
	M(1)=M(2)	REST360
	M(11)=M(2)	REST360
	JJ = 1	COMP361
	DO 800 I = 1, NRECD	COMP362
	GO TO (780, 780, 782, 784, 784, 784, 786, 788, 790), I	COMP363
780	N 1 = MAXT	COMP364
	GO TO 798	COMP365
782	N 1 = MAXR	COMP366
	GO TO 798	COMP367
784	N 1 = MAXC	COMP368
	GO TO 798	COMP369
786	N 1 = NWPD	COMP370
	GO TO 798	COMP371
788	N 1 = NWCT	COMP372
	GO TO 798	COMP373
790	N 1 = NWST	COMP374
798	WRITE (3) N 1, NCVG, NSTS	COMP375
	MAXP = MAXP + N 1	COMP376
	WRITE (3) (P(J), J = JJ, MAXP)	COMP377
	JJ = MAXP + 1	COMP378
800	CONTINUE	COMP379
	N 1 = 16	COMP380
	WRITE (3) N 1, NCVG, NSTS	COMP381
	WRITE (3) (M(I), I=1, N1)	COMP382
	END FILE 3	COMP383
	REWIND 3	COMP384
	RETURN	COMP385
718	READ (4, 204) NBLK	COMP387
	IF (IERROR(1).GT.0) GO TO 7181	22663871
	WRITE (6,252) NBLK	22663872
	IERROR(1) = IABS(IERROR(1))	22663873
7181	CONTINUE	22663874
	IF (NBLK.EQ.11) GO TO 714	22663875
	IF (NBLK.GE.1.AND.NBLK.LE.5) GO TO (720,730,740,750,760),NBLK	REST388
	WRITE (6,236) NBLK	REST3881
	ERROR=1.	REST3882
	NBLK = 1	REST3883
	GO TO 714	REST3884
720	READ (4, 218) KOD, KOD 1	COMP389
	IERROR(1) = IABS(IERROR(1))	22663891
	GO TO (722,725,7201,719), KOD	2266390
7201	READ (4,210) (A(I), I=1,12)	22663901
	WRITE (6,253)	22663902
	WRITE (6,251) CODE(KOD), KOD1, (A(I), I=1,12)	22663903
	GO TO 720	22663904
722	IF (KOD 1) 721, 721, 723	COMP391
721	READ (4, 204) I	COMP392
	IF (IERROR(1).GT.0) GO TO 7211	22663921
	WRITE (6,254)	22663922
	IERROR(1) = IABS(IERROR(1))	22663923
7211	CONTINUE	22663924
	GO TO 714	COMP393
723	READ (4, 200) (I 1(I), A(I), I = 1, KOD 1)	COMP394
	IF (IERROR(1).GT.0) GO TO 7231	22663941
	WRITE (6,255)	22663942
	WRITE (6,258) CODE(KOD), KOD1, (A(I), I=1, KOD1)	22663943



TABLE E-2 (Continued)

	IERROR(1) = IABS(IERROR(1))	22663944
7231	CONTINUE	22663945
	DO 724 I = 1, KOD 1	COMP395
	J = I 1(I)	COMP396
	JJ = J + MAXT	COMP397
	P(JJ) = A(I)	COMP398
	P(J) = A(I)	COMP399
	ITEM = I 1(I)	COMP400
	ATEM = A(I)	COMP401
724	CONTINUE	COMP402
	GO TO 720	COMP403
725	READ (4, 201) N 1, A 1, N 2	COMP404
	IF (IERROR(1).GT.0) GO TO 7251	22664041
	WRITE (6,255)	22664042
	WRITE (6,256) CODE(KOD), KOD1, N1, A1,N2	22664043
	IERROR(1) = IABS(IERROR(1))	22664044
7251	CONTINUE	22664045
	J = ITEM	COMP405
	AA = ATEM	COMP406
	DO 726 I = 1, N 2	COMP407
	J = J + N 1	COMP408
	JJ = J + MAXT	COMP409
	AA = AA + A 1	COMP410
	P(J) = AA	COMP411
	P(JJ) = AA	COMP412
	ITEM = J	COMP413
	ATEM = AA	COMP414
726	CONTINUE	COMP415
	GO TO 720	COMP416
730	READ (4, 218) KOD, KOD 1	COMP417
	IERROR(1) = IABS(IERROR(1))	22664171
	GO TO (731, 734,7301,719), KOD	2266418
7301	READ (4,210)	22664181
	WRITE (6,257)	22664182
	WRITE (6,251) CODE(KOD), KOD1, (A(I),I=1,12)	22664183
	IERROR(1) = IABS(IERROR(1))	22664184
	GO TO 730	
731	IF (KOD 1) 721, 721, 732	COMP419
732	READ (4, 200) (I 1(I), A(I), I = 1, KOD 1)	COMP420
	IF (IERROR(1).GT.0) GO TO 7321	22664201
	WRITE (6,259)	22664202
	WRITE (6,258) CODE(KOD), KOD1, (A(I),I=1,KOD1)	22664203
	IERROR(1) = IABS(IERROR(1))	22664204
7321	CONTINUE	22664205
	DO 733 I = 1, KOD 1	COMP421
	J = I 1(I) + 2*MAXT	COMP422
	P(J) = A(I)	COMP423
	ITEM = I 1(I)	COMP424
	ATEM = A(I)	COMP425
733	CONTINUE	COMP426
	GO TO 730	COMP427
734	READ (4, 201) N 1, A 1, N 2	COMP428
	IF (IERROR(1).GT.0) GO TO 7341	22664281
	WRITE (6,259)	22664282
	WRITE (6,256) CODE(KOD), KOD1, N1,A1,N2	22664283
	IERROR(1) = IABS(IERROR(1))	22664284
7341	CONTINUE	22664285
	J = ITEM	COMP429
	AA = ATEM	COMP430
	DO 736 I = 1, N 2	COMP431
	J = J + N 1	COMP432
	JJ = J + 2*MAXT	COMP433
	AA = AA + A 1	COMP434
	P(JJ) = AA	COMP435
	ITEM = J	COMP436

TABLE E-2 (Continued)

	ATEM = AA	
736	CONTINUE	COMP437
	GO TO 730	COMP438
740	READ (4, 218) KOD, KOD 1	COMP439
	IERROR(1)=IABS(IERROR(1))	COMP440
	GO TO (741,744,7401,719), KOD	22664401
7401	READ (4,210) (A(I),I=1,12)	2266441
	WRITE (6,260)	22664411
	WRITE (6,251) CODE(KOD), KOD1, (A(I),I=1,12)	22664412
	IERROR(1) = IABS(IERROR(1))	22664413
	GO TO 740	22664414
741	IF (KOD 1) 721, 721, 742	22664415
742	READ (4, 200) (I 1(I), A(I), I = 1, KOD 1)	COMP442
	IF (IERROR(1).GT.0) GO TO 7411	COMP443
	WRITE (6,261)	22664431
	WRITE (6,258) CODE(KOD), KOD1, (A(I),I=1,KOD1)	22664432
	IERROR(1) = IABS(IERROR(1))	22664433
7411	CONTINUE	22664434
	DO 743 I = 1, KOD 1	22664435
	J = I 1(I) + 2*MAXT + MAXR	COMP444
	P(J) = A(I)	COMP445
	ITEM = I 1(I)	COMP446
	ATEM = A(I)	COMP447
743	CONTINUE	COMP448
	GO TO 740	COMP449
744	READ (4, 201) N 1, A 1, N 2	COMP450
	IF (IERROR(1).GT.0) GO TO 7441	COMP451
	WRITE (6,261)	22664511
	WRITE (6,256) CODE(KOD),KOD1,N1,A1,N2	22664512
	IERROR(1) = IABS(IERROR(1))	22664513
7441	CONTINUE	22664514
	J = ITEM	22664515
	AA = ATEM	COMP452
	DO 746 I = 1, N 2	COMP453
	J = J + N 1	COMP454
	JJ = J + 2*MAXT + MAXR	COMP455
	AA = AA + A 1	COMP456
	P(JJ) = AA	COMP457
	ITEM = J	COMP458
	ATEM = AA	COMP459
746	CONTINUE	COMP460
	GO TO 740	COMP461
750	JJ = 5	COMP462
751	READ (4, 218) KOD, KOD 1	COMP463
	IERROR(1) = IABS(IERROR(1))	COMP464
	GO TO (752,7511,7511,719), KOD	22664641
7511	READ (4,210) (A(I),I=1,12)	2266465
	WRITE (6,262)	22664651
	WRITE (6,251) CODE(KOD), KOD1,(A(I),I=1,KOD1)	22664652
	IERROR(1) = IABS(IERROR(1))	22664653
	GO TO 750	22664654
752	IF (KOD 1) 721, 721, 753	22664655
753	READ (4, 205) ( A(I),I=1,KOD1)	COMP466
	IF (IERROR(1).GT.0) GO TO 7531	REST467
	WRITE (6,263)	22664671
	WRITE (6,258) CODE(KOD), KOD1, (A(I),I=1,KOD1)	22664672
	IERROR(1) = IABS(IERROR(1))	22664673
7531	CONTINUE	22664674
	DO 754 I = 1, KOD 1	22664675
	JJ = JJ-1	COMP468
	IF (JJ.EQ.1) M(7)=A(I)	REST469
		REST4691

TABLE E-2 (Continued)

IF (JJ.EQ.1) GO TO 754	REST4692
M(JJ) = A(I)	COMP470
754 CONTINUE	COMP471
GO TO 751	COMP472
760 READ (4, 218) KOD, KOD 1	COMP473
IERROR(1) = IABS(IERROR(1))	22664731
IF (KOD.EQ.4) GO TO 719	22664732
759 READ (4, 204) NTAB	COMP474
IF (IERROR(1).GT.0) GO TO 7591	22664741
WRITE (6,264)	22664742
WRITE (6,256) CODE(KOD), KOD1, NTAB	22664743
IERROR(1) = IABS(IERROR(1))	22664744
7591 CONTINUE	22664745
IF (NTAB) 760, 714, 761	COMP475
761 L = LOC (NTAB)	REST476
762 READ (4, 218) KOD, KOD 1	COMP477
IERROR(1) = IABS(IERROR(1))	22664771
GO TO (764,770,763,719,773) ,KOD	REST478
763 L = L + 1	COMP479
READ (4, 205) A(1)	COMP480
IF (IERROR(1).GT.0) GO TO 7631	22664801
WRITE (6,264)	22664802
WRITE (6,258) CODE(KOD),KOD1, A(1)	22664803
IERROR(1) = IABS(IERROR(1))	22664804
7631 CONTINUE	22664805
P(L) = A(1)	COMP481
GO TO 762	COMP482
764 IF (KOD 1) 759, 759, 766	COMP483
766 READ (4, 205) (A(I), I = 1, KOD 1)	COMP484
IF (IERROR(1).GT.0) GO TO 7661	22664841
WRITE (6,264)	22664842
WRITE (6,258) CODE(KOD),KOD1, (A(I),I=1,KOD1)	22664843
IERROR(1) = IABS(IERROR(1))	22664844
7661 CONTINUE	22664845
KOD2 = KOD1	22664846
DO 769 I = 1, KOD 1	COMP485
L = L + 1	COMP486
P(L) = A(I)	COMP487
769 CONTINUE	COMP488
GO TO 762	COMP489
770 IF (KOD1.LE.0) KOD1=KOD2	REST4890
GO TO (7701,7702,7703,7704,7705,7706),KOD1	
7701 READ (4,241) (A(I),I=1,KOD1),INCR	
IF (IERROR(1).GT.0) GO TO 771	2266500
WRITE (6,264)	22665001
WRITE (6,265) CODE(KOD), KOD1, (A(I),I=1,KOD1),INCR	22665002
GO TO 7707	22665003
7702 READ (4,242) (A(I),I=1,KOD1),INCR	
IF (IERROR(1).GT.0) GO TO 771	22665011
WRITE (6,264)	22665012
WRITE (6,266) CODE (KOD), KOD1, (A(I),I=1,KOD1),INCR	22665013
GO TO 7707	22665014
7703 READ (4,243) (A(I),I=1,KOD1),INCR	
IF (IERROR(1).GT.0) GO TO 771	2266502
WRITE (6,264)	22665021
WRITE (6,267) CODE(KOD),KOD1,(A(I),I=1,KOD1),INCR	22665022
GO TO 7707	22665023
7704 READ (4,244) (A(I),I=1,KOD1),INCR	
IF (IERROR(1).GT.0) GO TO 771	2266502
WRITE (6,264)	22665021
WRITE (6,268) CODE(KOD),KOD1,(A(I),I=1,KOD1),INCR	22665022

TABLE E-2 (Continued)

GO TO 7707	
7705 READ (4,245) (A1(I),I=1,KOD1),INCR	22665023
IF (IERROR(1).GT.0) GO TO 771	
WRITE (6,264)	2266503
WRITE (6,269) CODE(KOD),KOD1,(A(I),I=1,KOD1),INCR	22665031
GO TO 7707	22665032
7706 READ (4,246) (A1(I),I=1,KOD1),INCR	22665033
IF (IERROR(1).GT.0) GO TO 771	
WRITE (6,264)	2266504
WRITE (6,270) CODE(KOD),KOD1,(A(I),I=1,KOD1),INCR	22665041
GO TO 7707	22665042
7707 IERROR(1) = IABS(IERROR(1))	22665043
771 DO 772 I=1,KOD1	2266505
A(I)=A(I)+A1(I)	REST4893
L=L+1	REST4894
P(L)=A(I)	REST4894
772 CONTINUE	REST4895
INCR=INCR-1	REST4896
IF (INCR.GT.0) GO TO 771	REST4897
GO TO 762	REST4898
773 READ (4,204) ICOD	REST4899
KDAT (L+1) = 32765	REST490
KDAT (L+2) = ICOD	REST4901
L=L+2	REST4902
GO TO 762	REST4903
900 REWIND 3	REST4904
REWIND 4	REST4905
WRITE (6,237)	REST491
NEND=1	REST4911
RETURN	
END	REST494



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