

NASA CR 65863

LIBRARY COPY

NOV 24 1967

MANNED SPACECRAFT CENTER  
HOUSTON, TEXAS

SID 67-498

STUDY OF APOLLO WATER IMPACT  
FINAL REPORT

VOLUME 11

USER'S MANUAL FOR UNSYMMETRIC SHELL OF  
REVOLUTION ANALYSIS

(Contract NAS9-4552, G.O. 5264)

May 1967



Prepared by

E. Carrión  
S. C. Furuike  
T. Nishimoto  
(Authors)

GPO PRICE \$ \_\_\_\_\_

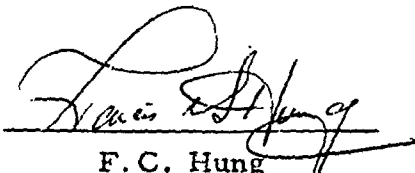
CFSTI PRICE(S) \$ \_\_\_\_\_


Hard copy (HC) \_\_\_\_\_

Microfiche (MF) \_\_\_\_\_

Approved by

FF 853 July 65

  
F. C. Hung  
Program Manager  
Structures and Materials

  
L. A. Harris  
Assistant Manager  
Science and Technology

NORTH AMERICAN AVIATION, INC.

SPACE DIVISION

602(D)	<b>N68-11939</b>	
	(ACCESSION NUMBER)	(THRU)
	326 (PAGES)	1 (CODE)
	CR-65863 (NASA CR OR TCR AD NUMBER)	32 (CATEGORY)



PRECEDING PAGE BLANK NOT FILMED.

## FOREWORD

This report was prepared by North American Aviation, Inc., Space Division, under NASA Contract NAS9-4552, for the National Aeronautics and Space Administration, Manned Space Flight Center, Houston, Texas, with Dr. F. C. Hung, Program Manager and Mr. P. P. Radkowski, Assistant Program Manager. This work was administered under the direction of Structural Mechanics Division, MSC, Houston, Texas with Dr. F. Stebbins as the technical monitor.

This report is presented in eleven volumes for convenience in handling and distribution. All volumes are unclassified.

The objective of the study was to develop methods and Fortran IV computer programs to determine by the techniques described below, the hydro-elastic response of representation of the structure of the Apollo Command Module immediately following impact on the water. The development of theory, methods and computer programs is presented as Task I Hydrodynamic Pressures, Task II Structural Response and Task III Hydroelastic Response Analysis.

Under Task I - Computing program to extend flexible sphere using the Spencer and Shiffman approach has been developed. Analytical formulation by Dr. Li using nonlinear hydrodynamic theory on structural portion is formulated. In order to cover a wide range of impact conditions, future extensions are necessary in the following items:

- a. Using linear hydrodynamic theory to include horizontal velocity and rotation.
- b. Nonlinear hydrodynamic theory to develop computing program on spherical portion and to develop nonlinear theory on toroidal and conic sections.

Under Task II - Computing program and User's Manual were developed for nonsymmetrical loading on unsymmetrical elastic shells. To fully develop the theory and methods to cover realistic Apollo configuration the following extensions are recommended:

- a. Modes of vibration and modal analysis.
- b. Extension to nonsymmetric short time impulses.

~~PRECEDING PAGE BLANK NOT FILMED~~

c. Linear buckling and elasto-plastic analysis

These technical extensions will not only be useful for Apollo and future Apollo growth configurations, but they will also be of value to other aeronautical and spacecraft programs.

The hydroelastic response of the flexible shell is obtained by the numerical solution of the combined hydrodynamic and shell equations. The results obtained herein are compared numerically with those derived by neglecting the interaction and applying rigid body pressures to the same elastic shell. The numerical results show that for an axially symmetric impact of the particular shell studied, the interaction between the shell and the fluid produces appreciable differences in the overall acceleration of the center of gravity of the shell, and in the distribution of the pressures and responses. However the maximum responses are within 15% of those produced when the interaction between the fluid and the shell is neglected. A brief summary of results is shown in the abstracts of individual volumes.

The volume number and authors are listed on the following page.

The contractor's designation for this report is SID 67-498.



## INDEX FOR FINAL REPORT

### "Apollo Water Impact"

<u>Volume No.</u>	<u>Volume Title</u>	<u>Authors</u>
1	Hydrodynamic Analysis of Apollo Water Impact	T. Li and T. Sugimura
2	Dynamic Response of Shells of Revolution During Vertical Impact Into Water - No Interaction	A. P. Cappelli, and J. P. D. Wilkinson
3	Dynamic Response of Shells of Revolution During Vertical Impact Into Water - Hydroelastic Interaction	J. P. D. Wilkinson, A. P. Cappelli, and R. N. Salzman
4	Comparison With Experiments	J. P. D. Wilkinson
5	User's Manual - No Interaction	J. P. D. Wilkinson
6	User's Manual - Interaction	J. P. D. Wilkinson and R. N. Salzman
7	Modification of Shell of Revolution Analysis	A. P. Cappelli and S. C. Furuike
8	Unsymmetric Shell of Revolution Analysis	A. P. Cappelli, T. Nishimoto, P. P. Radkowski and K. E. Pauley
9	Mode Shapes and Natural Frequencies Analysis	A. P. Cappelli
10	User's Manual for Modification of Shell of Revolution Analysis	A. P. Cappelli and S. C. Furuike
11	User's Manual for Unsymmetric Shell of Revolution Analysis	E. Carrión, S. C. Furuike and T. Nishimoto



PRECEDING PAGE BLANK NOT FILMED.

Volume 11

User's Manual  
For the Unsymmetric Shell of Revolution Computer  
Programs Static and Dynamic

ABSTRACT

The unsymmetric shell of revolution programs described in this volume were developed as a basic tool in the static and dynamic analysis of shells of revolution having arbitrary distribution of stiffness subjected to arbitrary loads and temperature.

The analytical basis for the two computer programs, static and dynamic, is presented. The analysis is restricted to linear-elastic thin shell theory. The basic equations include the effect of shear distortion. The analysis utilizes a Fourier series technique to separate the circumferential variation. The resulting set of equations are reduced to an algebraic set by the use of finite difference forms for variations of the other variables. These algebraic equations are then solved numerically by a direct matrix elimination procedure.

The computer programs were written in FORTRAN IV. In order to keep input data at a minimum extensive use of call function subroutines have been used. Call functions are subroutines which are coded and compiled by the user. This eliminates the necessity of large tabular inputs.

Solutions obtained from the Dynamic Unsymmetric Shell program are the displacement and rotation time histories. Also included in the output are the histories of internal forces and moments.

The solutions obtained from the Static Unsymmetric Shell program include displacements, rotations, internal force and moment resultants, and stresses. This output is presented in tabular form. The users of these programs should be forewarned that the programs are only a tool and insight must be used in relating results to an actual physical problem.

This volume is intended to supply the information necessary for the use of both the Dynamic Unsymmetric Shell program and the Static Unsymmetric Shell program. Detailed descriptions have been included in this volume to aid the user in performing extensions and modifications of these programs.

(ACCESSION NUMBER) 320	(THRU)
(PAGES) 1-48	(CODE)
(NASA CR OR TMX OR AD NUMBER) 44-65863	(CATEGORY)

vii -



PRECEDING PAGE BLANK NOT FILMED.

CONTENTS

Section	Page
FOREWORD . . . . .	iii
ABSTRACT . . . . .	vii
I. THEORY . . . . .	1
1.1 Introduction . . . . .	1
1.2 Nomenclature . . . . .	1
1.3 Scope and Limitations . . . . .	3
1.4 Shell Coordinate System . . . . .	4
1.5 Equations of Motion . . . . .	5
1.6 Formulation into Solution Variables . . . . .	8
1.7 Circumferential Variable Separation . . . . .	13
1.8 Finite Difference Formulation in the Meridional Variable . . . . .	26
1.9 Finite Difference Formulation in the Time Variable . . . . .	28
1.10 Matrix Solution of the Difference Equations . . . . .	30
1.11 Static Analysis . . . . .	32
1.12 References . . . . .	33
1.13 Appendix . . . . .	33
1.13.1 Modification of Sanders' Equations . . . . .	33
1.13.2 Series Product Expansion . . . . .	36
1.13.3 Coefficients . . . . .	36
II. GENERAL DESCRIPTION OF THE COMPUTER PROGRAMS . . . . .	45
2.1 Introduction . . . . .	45
2.2 Program Capabilities and Limitations . . . . .	45
2.3 Sign Conventions and Dimensions . . . . .	46
2.4 Reference, Inner and Outer Surfaces . . . . .	46
2.5 Geometry . . . . .	47
2.5.1 Cone-Cylinder . . . . .	47
2.5.2 Sphere-Toroid . . . . .	48
2.5.3 Discrete Point . . . . .	49
2.6 Function Subroutine Parameters . . . . .	50
2.6.1 Stiffness Properties . . . . .	50
2.6.2 Thermal Loads . . . . .	51

Section	Page
2.6.3 Elastic Foundations . . . . .	51
2.6.4 External Damping . . . . .	51
2.6.5 Mass Parameter . . . . .	51
2.6.6 Pressure Loads . . . . .	51
2.6.7 Parameters for Stresses . . . . .	52
2.7 Stations . . . . .	52
2.8 Boundary Conditions . . . . .	53
2.9 Reference Quantities . . . . .	53
2.10 Output Indicators . . . . .	54
III. DETAILED USE OF THE PROGRAMS . . . . .	55
3.1 Introduction . . . . .	55
3.2 Deck Set-Up . . . . .	56
3.3 Data Deck Set-Up . . . . .	59
3.3.1 Title Cards . . . . .	60
3.3.2 General Shell Data, GDA . . . . .	60
3.3.3 Geometry Data, GMDA . . . . .	62
3.4 Function Subprograms . . . . .	64
3.5 Utility Subroutines . . . . .	69
3.5.1 DECRD . . . . .	69
3.5.2 MAD, MSU, MMY, INVMS . . . . .	72
3.5.3 DINTRP, ENTERP . . . . .	83
3.5.4 CODIMA . . . . .	86
3.5.5 FILE . . . . .	90
3.6 Sample Problem Number 1 . . . . .	95
3.6.1 Problem Description and Set-Up . . . . .	95
3.6.2 Data Sheets . . . . .	96
3.6.3 Function Subprograms Used . . . . .	98
3.6.4 Output . . . . .	102
3.7 Sample Problem Number 2 . . . . .	114
3.7.1 Problem Description and Set-Up . . . . .	114
3.7.2 Data Sheets . . . . .	116
3.7.3 Function Subprograms Used . . . . .	119
3.8 Sample Problem Number 3 . . . . .	115
3.8.1 Problem Description and Set-Up . . . . .	125
3.8.2 Data Sheets . . . . .	126
3.8.3 Function Subprograms Used . . . . .	128
3.8.4 Output . . . . .	131
3.9 Sample Problem Number 4 . . . . .	167
3.9.1 Problem Description and Set-Up . . . . .	167
3.9.2 Data Sheets . . . . .	169
3.9.3 Function Subprograms Used . . . . .	171

Section	Page
3.10 Error Indications, Pitfalls, Recommendations . . .	176
3.11 Program Listings for Static Version . . . . .	177
3.12 Program Listings for Dynamic Version; Load Map . . . . .	230
3.13 Nomenclature . . . . .	298





PRECEDING PAGE BLANK NOT FILMED.

ILLUSTRATIONS

Figure		Page
1.1	Geometry and Coordinates . . . . .	4
1.2	Sign Convention . . . . .	7
1.3	Stiffness Profile . . . . .	15
2.1	Cone-Cylinder Geometry. . . . .	48
2.2	Sphere-Toroid Geometry. . . . .	48
2.3	Discrete Point Geometry. . . . .	50

## 1.0 THEORY

### 1.1 INTRODUCTION

This section presents the analytical basis of the computer programs. The dynamic response problem is presented and the specialization for the static analysis is made.

The analysis is based on a modified form of the general first order linear shell theory of Sanders. These equations have been modified to include transverse shear distortion, see Appendix 1.13.1 The modified equilibrium equations are extended to include time dependence by D'Alembert's principle. Fourier analysis is used to separate variables in the circumferential direction and a system of finite difference approximations are used to reduce the partial differential equations to an algebraic set. This set is solved by using a direct matrix elimination procedure.

The material presented in this section is an extension and parallels of the work of Sanders<sup>1</sup>, Budiansky and Radkowski<sup>2</sup>, and Johnson and Greif<sup>3</sup>. The notation used is identical to that of Reference 2 except where noted.

### 1.2 NOMENCLATURE

#### Fourier Coefficients

$u_n, v_n, w_n, \phi_{\xi n}, \phi_{\theta n}$	= displacements and rotations
$P_{\xi n}, P_{\theta n}, P_n$	= loads
$t_{\xi n}^T, t_{\theta n}^T, m_{\xi n}^T, m_{\theta n}^T$	= temperature induced force terms
$t_{\xi}^n, t_{\theta}^n, t_{\xi\theta}^n, t_{\theta\xi}^n, q_{\xi}^n$ $q_{\theta}^n, m_{\xi}^n, m_{\theta}^n, m_{\xi\theta}^n$	} = force resultants, modified and effective
$b_{mj}, d_{mj}, g_{mj}, g_{13j}$	
$k_{mj}, c_{mj}, m_{mj}$	= elastic foundation, damping, mass

$f_{5k+1, 5j+1} \cdot \cdot \cdot \cdot f_{5k+5, 5j+5}$	} = elements of F, G, H, K, $\alpha$ , $\beta$ , p, $\ell$ R, S, and a
$g_{5k+1, 5j+1} \cdot \cdot \cdot \cdot g_{5k+5, 5j+5}$	
$h_{5k+1, 5j+1} \cdot \cdot \cdot \cdot h_{5k+5, 5j+5}$	
$k_{5k+1, 5j+1} \cdot \cdot \cdot \cdot k_{5k+5, 5j+5}$	
$\alpha_{5k+1, 5j+1} \cdot \cdot \cdot \cdot \alpha_{5k+5, 5j+5}$	
$\beta_{5k+1, 5j+1} \cdot \cdot \cdot \cdot \beta_{5k+5, 5j+5}$	
$p_{5k+1} \cdot \cdot \cdot \cdot p_{5k+5, \ell_1^k \cdot \cdot \cdot \ell_5^k}$	
$r_{5k+1, 5j+1} \cdot \cdot \cdot \cdot r_{5k+5, 5j+5}$	
$s_{5k+1, 5j+1} \cdot \cdot \cdot \cdot s_{5k+5, 5j+5}$	
$a_{5k+1} \cdot \cdot \cdot \cdot \cdot \cdot \cdot a_{5k+5}$	

Coordinates and Constants

$\xi, \theta, \zeta$	= coordinates
r	= normal distance from shell axis
s	= meridional shell coordinate
a, $h_0, \sigma_0, E_0$	= reference constants
$\omega_\theta, \omega_\xi$	= nondimensional curvatures
u, v, w, $\phi_\xi, \phi_\theta$	= displacements and rotations
$\sigma_\xi, \sigma_\theta, \tau_{\xi\theta}, \tau_{\xi\zeta}, \tau_{\theta\zeta}$	= stresses
$\epsilon_\xi, \epsilon_\theta, \epsilon_{\xi\theta}, k_\xi, k_\theta$	} = strains
$k_{\xi\theta}, \gamma_{\xi\zeta}, \gamma_{\theta\zeta}$	
$B_i, C_i, D_i, G_i, K_i, M_i$	= isotropic stiffness functions
E, $\nu, \alpha$	= material properties
$q_\xi, q_\theta, q$	= loads
T	= temperature change

$$\left. \begin{array}{l} N_{\xi}, N_{\theta}, \bar{N}_{\xi\theta}, M_{\xi}, M_{\theta}, \bar{M}_{\xi\theta}, Q_{\xi} \\ Q_{\theta}, \hat{N}_{\xi\theta}, N_{\xi}^T, N_{\theta}^T, M_{\xi}^T, M_{\theta}^T \end{array} \right\} = \text{force resultants, modified, effective,} \\ \text{and temperature induced}$$

### Matrices

$$F, G, H, K, \alpha, \beta, \Omega, \Lambda, R, S = 5K \times 5K \text{ order}$$

$$p, l, x = 5K \times 1 \text{ order}$$

### Indices

$$i, j, n = \text{Dummy}$$

$$k = k^{\text{th}} \text{ Fourier component}$$

## 1.3 SCOPE AND LIMITATIONS

The shell theory on which these programs are based is restricted to linear, elastic, thin shell theory.

- (a) The thickness of the shell at any point is small compared to the other dimensions.
- (b) Deformations of the shell are small compared to the smallest radius of curvature.
- (c) All material points of the shell deform elastically, obeying Hooke's law for transverse isotropic materials.
- (d) The shell is "complete," i.e., its only boundaries are at meridian ends and inner and outer surfaces.
- (e) The class of shells considered has a surface of revolution reference surface which is within or in close proximity of the shell walls such that  $\int E \xi d\xi = 0$ .
- (f) The parameters of stiffness, e.g., in-plane stiffnesses are permitted to vary in both the meridional and circumferential directions. Implied is that parameters such as thickness, Young's modulus, etc., are permitted to vary in both the meridional and circumferential directions. The stiffness parameter's variation in the circumferential direction is restricted to those with a plane of symmetry.
- (g) Arbitrary loads and temperature distributions are permissible. Excluded are problems with thermal distributions such that limitation (e) is not satisfied.

- (h) The effects of transverse shear is included.
- (i) Instability is not considered.
- (j) Distributed mass, elastic foundation, and external damping is included. These distributions have the same symmetry conditions as the stiffness parameters (f).

#### 1.4 SHELL COORDINATE SYSTEM

The geometry of a shell is defined entirely by specifying the form of the reference surface and the thickness of the shell at each point. For convenience, the shell coordinate system and geometrical relations used in Reference 2 will be adopted here. The reference surface is assumed to be a surface of revolution and is selected at a convenient location, within or in proximity to the shell walls. The first fundamental form of the reference surface is defined by

$$d\bar{s}^2 = ds^2 + r^2 d\theta^2 \quad (1.1)$$

where  $d\bar{s}$  is a line element on the surface and  $s$  and  $\theta$  denote orthogonal coordinates selected along lines of principal curvature.

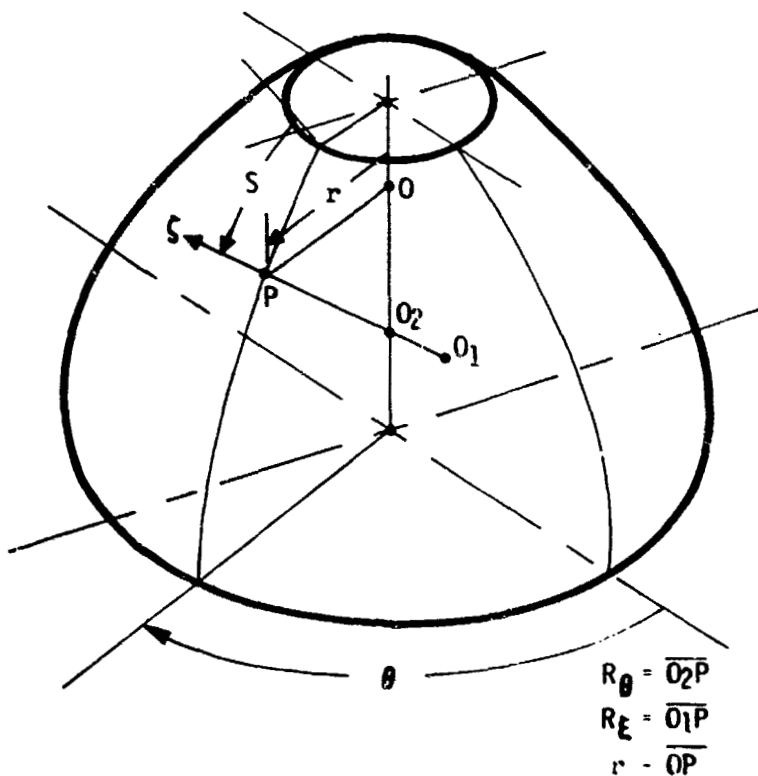


Figure 1.1. Geometry and Coordinates

The generator on the reference surface is defined by  $r(s)$  where  $r$  is the distance from the axis of revolution. The coordinate  $s$  is a measure of the meridional distance along an axisymmetric reference surface, and  $\theta$  is a circumferential angle, as shown in Figure 1.1. The coordinate,  $\zeta$ , is selected as a measure of the normal outward distance from the reference surface ( $\zeta = 0$ ). The principal radii of curvature are

$$R_s = - \left[ 1 - \left( \frac{dr}{ds} \right)^2 \right]^{1/2} / \frac{d^2r}{ds^2} \quad R_\theta = r \left[ 1 - \left( \frac{dr}{ds} \right)^2 \right]^{-1/2} \quad (1.2)$$

Introduce the nondimensional meridional coordinate  $\xi = s/a$ , where  $a$  is a reference length; then, with  $\rho = r/a$ , the nondimensional curvatures  $\omega_\xi = a/R_s$  and  $\omega_\theta = a/R_\theta$  can be found from the formulas

$$\omega_\xi = - (\gamma' + \gamma^2) / \omega_\theta \quad \omega_\theta = \left[ 1 - (\rho')^2 \right]^{1/2} / \rho \quad (1.3)$$

where

$$\gamma = \rho' / \rho$$

In these equations, and henceforth,  $( )' = \frac{\partial( )}{\partial \xi}$

Finally from the Codazzi relation we obtain

$$\omega_\theta' = \gamma (\omega_\xi - \omega_\theta) \quad (1.4)$$

and the relation

$$\frac{\rho''}{\rho} = - \omega_\xi \omega_\theta \quad (1.5)$$

## 1.5 EQUATIONS OF MOTION

The general equilibrium equations for an arbitrary shell based on the first-order linear shell theory of Sanders are given in Reference 1. These equations are modified to include the effect of transverse shear distortion by the procedure suggested by Sanders.\* These equilibrium equations are extended to equations of motion by use of D'Alembert's principle. These equations specialized for a shell whose reference surface is a surface of revolution are given as,

---

\*See Appendix

$$a \left[ \frac{\partial \rho}{\partial \xi} N_{\xi} + \rho \frac{\partial N_{\xi}}{\partial \xi} + \frac{\partial \bar{N}_{\xi\theta}}{\partial \theta} - \frac{\partial \rho}{\partial \xi} N_{\theta} \right] + \quad (1.6.1)$$

$$a \rho \omega_{\xi} Q_{\xi} + \frac{1}{2} (\omega_{\xi} - \omega_{\theta}) \frac{\partial \bar{M}_{\xi\theta}}{\partial \theta} + a^2 \rho q_{\xi} = a^2 \rho \left[ M \frac{\partial^2 U_{\xi}}{\partial t^2} + C_{\xi} \frac{\partial U_{\xi}}{\partial t} + K_{\xi} U_{\xi} \right]$$

$$a \left[ \frac{\partial N_{\theta}}{\partial \theta} + 2 \frac{\partial \rho}{\partial \xi} \bar{N}_{\xi\theta} + \rho \frac{\partial \bar{N}_{\xi\theta}}{\partial \xi} \right] + a \rho \omega_{\theta} Q_{\theta} + \quad (1.6.2)$$

$$\frac{\rho}{2} \frac{\partial}{\partial \xi} [(\omega_{\theta} - \omega_{\xi}) \bar{M}_{\xi\theta}] + a^2 \rho q_{\theta} = a^2 \rho \left[ M \frac{\partial^2 U_{\theta}}{\partial t^2} + C_{\theta} \frac{\partial U_{\theta}}{\partial t} + K_{\theta} U_{\theta} \right]$$

$$a \left[ \frac{\partial \rho}{\partial \xi} Q_{\xi} + \rho \frac{\partial Q_{\xi}}{\partial \xi} + \frac{\partial Q_{\theta}}{\partial \theta} - \quad (1.6.3)$$

$$\rho (\omega_{\xi} N_{\xi} + \omega_{\theta} N_{\theta}) \right] + a^2 \rho q_{\zeta} = a^2 \rho \left[ M \frac{\partial^2 W}{\partial t^2} + C_{\zeta} \frac{\partial W}{\partial t} + K_{\zeta} W \right]$$

$$\frac{\partial \rho}{\partial \xi} M_{\xi} + \rho \frac{\partial M_{\xi}}{\partial \xi} + \quad (1.6.4)$$

$$\frac{\partial \bar{M}_{\xi\theta}}{\partial \theta} - \frac{\partial \rho}{\partial \xi} M_{\theta} - a \rho Q_{\xi} = a \rho \left[ M^* \frac{\partial^2 \Phi_{\xi}}{\partial t^2} + C_{\xi}^* \frac{\partial \Phi_{\xi}}{\partial t} + K_{\xi}^* \Phi_{\xi} \right]$$

$$\frac{\partial M_{\theta}}{\partial \theta} + 2 \frac{\partial \rho}{\partial \xi} \bar{M}_{\xi\theta} + \quad (1.6.5)$$

$$\rho \frac{\partial M_{\xi\theta}}{\partial \xi} - a \rho Q_{\theta} = a \rho \left[ M_{\theta}^* \frac{\partial^2 \Phi_{\theta}}{\partial t^2} + C_{\theta}^* \frac{\partial \Phi_{\theta}}{\partial t} + K_{\theta}^* \Phi_{\theta} \right]$$

where

$$M(\xi, \theta) = \rho(\xi, \theta) h(\xi, \theta) \text{ (mass/unit area of shell)}$$

$$M(\xi, \theta)^* = \frac{\rho(\xi, \theta) h^3(\xi, \theta)}{12} \text{ (mass moment/unit area of shell)}$$

$$C_{(\ )}(\xi, \theta) = \text{external damping coefficient}$$

$$K_{(\ )}(\xi, \theta) = \text{spring constants}$$

Where the components of membrane force, transverse force and moment (about the reference surface) per unit length, and load per unit area (assumed to be applied at the reference surface) are shown in Figure 1-2.

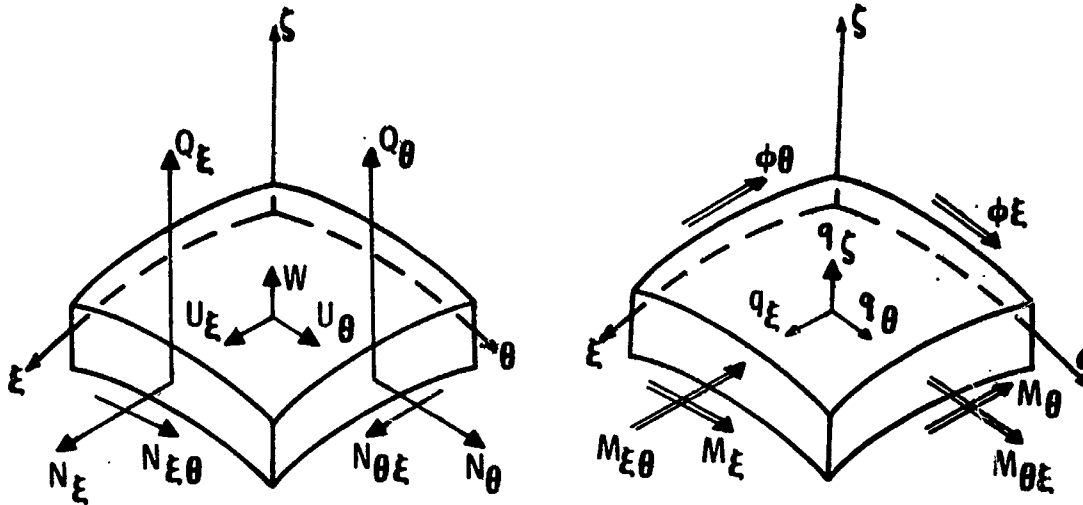


Figure 1-2. Sign Convention and Coordinates, Moments, Forces, Loads, Displacements, and Rotations

In the Sanders' first-order theory the inplane shearing forces  $N_{\xi\theta}$  and  $N_{\theta\xi}$  as well as twisting moments  $M_{\xi\theta}$  and  $M_{\theta\xi}$  are not handled separately, but instead are combined to form modified variables

$$\bar{N}_{\xi\theta} = \frac{1}{2} (N_{\xi\theta} + N_{\theta\xi}) \quad (1.7)$$

$$\bar{M}_{\xi\theta} = \frac{1}{2} (M_{\xi\theta} + M_{\theta\xi}) \quad (1.8)$$

and

$$\bar{k}_{\xi\theta} = \frac{1}{2} (k_{\xi\theta} + k_{\theta\xi}) \quad (1.9)$$

It is necessary when including the effects of transverse shear distortion to consider five equilibrium equations. Recall in Reference 2 that when shear deformation is neglected the shear forces are eliminated and resulting equilibrium equations are reduced to the consideration of three equations. The neglecting of transverse shear strains implies that normals to middle surface of the shell remain normal after deformation. The degree of error introduced by this assumption naturally depends on the magnitude of transverse shearing forces and shear rigidity of the shell. For discontinuous loads and shells having low shear rigidity, shear deformations may be comparable to bending and axial deformations and cannot be ignored.



### 1.6 FORMULATION INTO SOLUTION VARIABLES

The equations of motion are now expressed in terms of the solution variables, displacements and rotations.

The force and moment expressions in the equations of motion are determined by evaluating the following integrals through the thickness

$$\begin{aligned}
 N_{\xi} &= \int \sigma_{\xi} d\zeta & M_{\xi} &= \int \sigma_{\xi} \zeta d\zeta \\
 N_{\theta} &= \int \sigma_{\theta} d\zeta & M_{\theta} &= \int \sigma_{\theta} \zeta d\zeta \\
 \bar{N}_{\xi\theta} &= \int \tau_{\xi\theta} d\zeta & \bar{M}_{\xi\theta} &= \int \tau_{\xi\theta} \zeta d\zeta \\
 Q_{\xi} &= \int \tau_{\xi\zeta} d\zeta & Q_{\theta} &= \int \tau_{\theta\zeta} d\zeta
 \end{aligned} \tag{1.10}$$

where in the above integrals we have neglected terms of order  $\zeta/R$ ,  $R$  is the minimum radius of curvature. The stresses used above are defined as:

$\sigma_{\xi}, \sigma_{\theta}$	are normal stresses, acting on the faces
$\tau_{\xi\theta}$	is an in-plane shear stress acting parallel to the reference surface
$\tau_{\xi\zeta}, \tau_{\theta\zeta}$	are transverse shear stresses acting normal to the reference surface

By assuming that plane sections before remain plane after deformation, the strains at a distance  $\zeta$  from the reference surface can be expressed in terms of the reference surface strains as follows:

$$\begin{aligned}
 \epsilon_{\xi}(\zeta) &= \epsilon_{\xi} + \zeta k_{\xi} \\
 \epsilon_{\theta}(\zeta) &= \epsilon_{\theta} + \zeta k_{\theta} \\
 \epsilon_{\xi\theta}(\zeta) &= \epsilon_{\xi\theta} + \zeta \bar{k}_{\xi\theta}
 \end{aligned} \tag{1.11}$$

where  $\epsilon_{\xi}$ ,  $\epsilon_{\theta}$  and  $\epsilon_{\xi\theta}$  are the strains of the reference surface and  $\epsilon_{\xi\theta}(\zeta)$  is one-half the usual engineering strain.

are The stress-strain-temperature relations for an isotropic material

$$\sigma_{\xi} = \frac{E}{1 - \nu^2} \left\{ \epsilon_{\xi} + \nu \epsilon_{\theta} + \zeta (k_{\xi} + \nu k_{\theta}) - \alpha (1 + \nu) T \right\}$$

$$\sigma_{\theta} = \frac{E}{1 - \nu^2} \left\{ \epsilon_{\theta} + \nu \epsilon_{\xi} + \zeta (k_{\theta} + \nu k_{\xi}) - \alpha (1 + \nu) T \right\}$$

(1.12)

$$\tau_{\xi\theta} = G (\epsilon_{\xi\theta} + \zeta \bar{k}_{\xi\theta})$$

$$\tau_{\xi\zeta} = G (\gamma_{\xi\zeta})$$

$$\tau_{\theta\zeta} = G (\gamma_{\theta\zeta})$$

where

$$G = \frac{E}{2(1 + \nu)}$$

Substituting these equations into Eqs. 1.10 and employing appropriate integrations through the thickness yield the following stress/resultants-strain relationships.

$$N_{\xi} = B_1 \epsilon_{\xi} + B_3 \epsilon_{\theta} + C_1 k_{\xi} + C_3 k_{\theta} - N_{\xi}^T$$

$$N_{\theta} = B_3 \epsilon_{\xi} + B_2 \epsilon_{\theta} + C_3 k_{\xi} + C_2 k_{\theta} - N_{\theta}^T$$

$$\bar{N}_{\xi\theta} = G_1 \epsilon_{\xi\theta} + G_{12} k_{\xi\theta}$$

$$Q_{\xi} = G_2 \gamma_{\xi\zeta}$$

(1.13)

$$M_{\xi} = C_1 \epsilon_{\xi} + C_3 \epsilon_{\theta} + D_1 k_{\xi} + D_3 k_{\theta} - M_{\xi}^T$$

$$M_{\theta} = C_3 \epsilon_{\xi} + C_2 \epsilon_{\theta} + D_3 k_{\xi} + D_2 k_{\theta} - M_{\theta}^T$$

$$\bar{M}_{\xi\theta} = G_{12} \epsilon_{\xi\theta} + G_{13} k_{\xi\theta}$$

$$Q_{\theta} = G_3 \gamma_{\theta\zeta}$$

where in the above equations the shell stiffnesses are given by

$$\begin{aligned}
 B_1 = B_2 &= \int \frac{E}{1-\nu^2} d\zeta, \quad B_3 = \int \frac{\nu E}{1-\nu^2} d\zeta, \quad C_1 = C_2 = \int \frac{E\zeta}{1-\nu^2} d\zeta, \quad C_3 = \int \frac{\nu E\zeta}{1-\nu^2} d\zeta \\
 D_1 = D_2 &= \int \frac{E}{1-\nu^2} \zeta^2 d\zeta, \quad D_3 = \int \frac{\nu E\zeta^2}{1-\nu^2} d\zeta \\
 G_1 = G_2 = G_3 &= \int G d\zeta \\
 G_{12} &= \int G\zeta d\zeta \\
 G_{13} &= \int G\zeta^2 d\zeta
 \end{aligned} \tag{1.14}$$

and thermal loads are

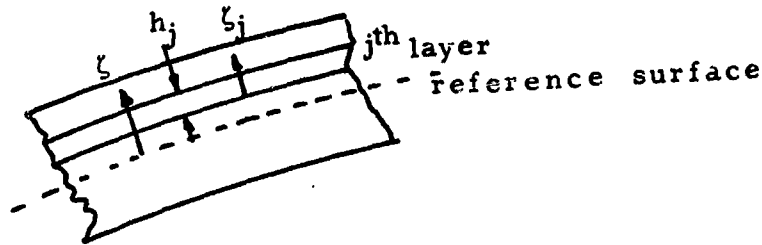
$$\begin{aligned}
 N_{\xi}^T = N_{\theta}^T &= \int \frac{\alpha(1+\nu)}{1-\nu^2} ET\zeta d\zeta \\
 M_{\xi}^T = M_{\theta}^T &= \int \frac{\alpha(1+\nu)}{1-\nu^2} ET\zeta^2 d\zeta
 \end{aligned} \tag{1.15}$$

For the case of discontinuous material properties through the thickness the integration is taken piece-wise through the thickness. An additional assumption of constant Poisson's ratios through the thickness is made. Therefore the isotropic nature of the layers are retained in the stiffness parameters. The shell stiffness and thermal loads take the form,

$$\begin{aligned}
 B_1 = B_2 = \frac{B_3}{\nu} &= \frac{1}{1-\nu^2} \int E d\zeta, \quad D_1 = D_2 = \frac{D_3}{\nu} = \frac{1}{1-\nu^2} \int E\zeta^2 d\zeta \\
 C_1 = C_2 = \frac{C_3}{\nu} &= \frac{1}{1-\nu^2} \int E\zeta d\zeta, \quad G_1 = G_2 = G_3 = B_1 \frac{(1-\nu)}{2} \\
 G_{12} &= C_1 \frac{(1-\nu)}{2}, \quad G_{13} = D_1 \frac{(1-\nu)}{2}
 \end{aligned} \tag{1.16}$$

It follows that because of the reference surface choice, namely that the condition  $\int E \zeta d\zeta = 0$  is satisfied, the integration takes the form

$$A = \int F(\zeta) d\zeta = \sum_j \int_0^{h_j} F_j(\zeta_j) d\zeta_j \quad (1.17)$$



The reference surface strains and bending distortion terms may be defined in terms of displacements and rotations by the following expressions. The membrane strains of the reference surface are given by

$$\begin{aligned} \epsilon_\xi &= \frac{1}{a} \left[ \frac{\partial U_\xi}{\partial \xi} + \omega_\xi W \right] \\ \epsilon_\theta &= \frac{1}{a} \left[ \frac{1}{\rho} \frac{\partial U_\theta}{\partial \theta} + \gamma U_\xi + \omega_\theta W \right] \\ \epsilon_{\xi\theta} &= \frac{1}{2a} \left[ \frac{1}{\rho} \frac{\partial U_\xi}{\partial \theta} + \frac{\partial U_\theta}{\partial \xi} - \gamma U_\theta \right] \end{aligned} \quad (1.18)$$

where  $U$ ,  $V$ ,  $W$  are displacements in the  $\xi$ ,  $\theta$  and  $\zeta$  directions respectively. Transverse shear strains are given by

$$\begin{aligned} \gamma_{\xi\zeta} &= \Phi_\xi - \frac{1}{a} \left[ \omega_\xi U_\xi - \frac{\partial W}{\partial \xi} \right] \\ \gamma_{\theta\zeta} &= \Phi_\theta - \frac{1}{a} \left[ \omega_\theta U_\theta - \frac{1}{\rho} \frac{\partial W}{\partial \theta} \right] \end{aligned} \quad (1.19)$$

where  $\Phi_\xi$ ,  $\Phi_\theta$  are rotations.

The bending distortion terms are given by

$$\begin{aligned}
 k_{\xi} &= \frac{1}{a} \frac{\partial \Phi_{\xi}}{\partial \xi} \\
 k_{\theta} &= \frac{1}{a} \left[ \frac{1}{\rho} \frac{\partial \Phi_{\theta}}{\partial \theta} + \gamma \Phi_{\xi} \right] \\
 \bar{k}_{\xi\theta} &= \frac{1}{2a} \left[ \frac{1}{\rho} \frac{\partial \Phi_{\xi}}{\partial \theta} + \frac{\partial \Phi_{\theta}}{\partial \xi} - \gamma \Phi_{\theta} + \frac{1}{2a} (\omega_{\xi} - \omega_{\theta}) \left( \frac{1}{\rho} \frac{\partial U_{\xi}}{\partial \theta} - \frac{\partial U_{\theta}}{\partial \xi} - \gamma U_{\theta} \right) \right]
 \end{aligned} \tag{1.20}$$

Substituting equations (1.18, 1.19, 1.20) into equation 1.13 the force terms in the equations of motion can be expressed in terms of the displacements

$$\begin{aligned}
 N_{\xi} &= \frac{1}{a} \left\{ B_1 \frac{\partial U_{\xi}}{\partial \xi} + B_3 \gamma U_{\xi} + B_3 \left( \frac{1}{\rho} \right) \frac{\partial U_{\theta}}{\partial \theta} + (B_1 \omega_{\xi} + B_2 \omega_{\theta}) W \right\} - N^T \\
 N_{\theta} &= \frac{1}{a} \left\{ B_3 \frac{\partial U_{\xi}}{\partial \xi} + B_2 \gamma U_{\xi} + B_2 \left( \frac{1}{\rho} \right) \frac{\partial U_{\theta}}{\partial \theta} + (B_3 \omega_{\xi} + B_2 \omega_{\theta}) W \right\} - N^T \\
 N_{\xi\theta} &= \frac{1}{2a} \left\{ \frac{1}{\rho} G_1 \frac{\partial U_{\xi}}{\partial \theta} + G_1 \frac{\partial U_{\theta}}{\partial \xi} - \gamma G_1 U_{\theta} \right\} \\
 Q_{\xi} &= G_2 \left\{ -\frac{1}{a} \omega_{\xi} U_{\xi} + \frac{1}{a} \frac{\partial W}{\partial \xi} + \Phi_{\xi} \right\} \\
 M_{\xi} &= \frac{1}{a} \left\{ D_1 \frac{\partial \Phi_{\xi}}{\partial \xi} + D_3 \gamma \Phi_{\xi} + D_3 \frac{1}{\rho} \frac{\partial \Phi_{\theta}}{\partial \theta} \right\} - M^T \\
 M_{\theta} &= \frac{1}{a} \left\{ D_3 \frac{\partial \Phi_{\xi}}{\partial \xi} + D_2 \gamma \Phi_{\xi} + D_2 \frac{1}{\rho} \frac{\partial \Phi_{\theta}}{\partial \theta} \right\} - M^T \\
 \bar{M}_{\xi\theta} &= \frac{1}{2a} \left\{ \frac{1}{2a} G_{13} (\omega_{\xi} - \omega_{\theta}) \left( \frac{1}{\rho} \frac{\partial U_{\xi}}{\partial \theta} - \frac{\partial U_{\theta}}{\partial \xi} - \gamma U_{\theta} \right) + G_{13} \left( \frac{1}{\rho} \frac{\partial \Phi_{\xi}}{\partial \theta} + \frac{\partial \Phi_{\theta}}{\partial \xi} - \gamma \Phi_{\theta} \right) \right\} \\
 Q_{\theta} &= G_3 \left\{ -\frac{1}{a} \omega_{\theta} U_{\theta} + \frac{1}{a\rho} \frac{\partial W}{\partial \theta} + \Phi_{\theta} \right\}
 \end{aligned} \tag{1.21}$$

By employing the relations, equations 1.21 the equations of motion can be expressed in terms of the dependent variables, displacements and rotations.

## 1.7 CIRCUMFERENTIAL VARIABLE SEPARATION

The analysis utilizes a Fourier approach which will permit separation of variables and yield a more tractable set of shell equations. The procedure involves expanding of the pertinent variables in Fourier series with appropriate normalization to provide nondimensional Fourier coefficients of roughly comparable magnitudes for different variables. Letting  $\sigma_0$ ,  $E_0$ ,  $h_0$  be a reference stress level, Young's modulus, and thickness, respectively, solutions for the field equations are sought in the form

$$\begin{aligned}
 U_\xi &= \frac{a\sigma_0}{E_0} \sum_{n=0}^{\infty} u_n(\xi, t) \cos n\theta \\
 U_\theta &= \frac{a\sigma_0}{E_0} \sum_{n=1}^{\infty} v_n(\xi, t) \sin n\theta \\
 W &= \frac{a\sigma_0}{E_0} \sum_{n=0}^{\infty} w_n(\xi, t) \cos n\theta \\
 \Phi_\xi &= \frac{\sigma_0}{E_0} \sum_{n=0}^{\infty} \phi_{\xi n}(\xi, t) \cos n\theta \\
 \Phi_\theta &= \frac{\sigma_0}{E_0} \sum_{n=1}^{\infty} \phi_{\theta n}(\xi, t) \sin n\theta
 \end{aligned} \tag{1.22}$$

These Fourier expansions are consistent with loadings in the form

$$\begin{aligned}
 q_\xi &= \frac{\sigma_0 h_0}{a} \sum_{n=0}^{\infty} p_{\xi n}(\xi, t) \cos n\theta \\
 q_\theta &= \frac{\sigma_0 h_0}{a} \sum_{n=1}^{\infty} p_{\theta n}(\xi, t) \sin n\theta \\
 q_\zeta &= \frac{\sigma_0 h_0}{a} \sum_{n=0}^{\infty} p_{\zeta n}(\xi, t) \cos n\theta
 \end{aligned} \tag{1.23}$$

The above Fourier expansions are not the most general form. The expansions  $q_r$ ,  $q_t$  are symmetrical expansions about  $\theta = 0$ . For full generality, they must be augmented by additional sine series expansions. The form  $q_\theta$  in turn would be supplemented by cosine series. Consistently, the series expansions for displacements and rotations must be augmented for the general case.

Expansions for the temperature distributions may be described in a similar manner; however, since the thermal coefficients and Young's modulus can vary in the circumferential direction, it will be more convenient to expand the thermal load in Fourier series as follows

$$N^T = \sigma_o h_o \sum_{n=0}^{\infty} t_n^T \text{Cos } n\theta \quad (1.24)$$

$$M^T = \frac{\sigma_o h_o^3}{a} \sum_{n=0}^{\infty} m_n^T \text{Cos } n\theta$$

Where the Fourier components  $t_n^T$  and  $m_n^T$  are given by

$$t_n^T = \frac{2}{\pi} \int_0^{\pi} \frac{N^T}{\sigma_o h_o} \text{Cos } n\theta \, d\theta$$

$$m_n^T = \frac{2}{\pi} \int_0^{\pi} \frac{aM^T}{\sigma_o h_o^3} \text{Cos } n\theta \, d\theta$$

Since the stiffness mass, external damping and elastic foundation parameters are variable in the circumferential directions, these will also be expanded in a Fourier series. For example, the expansion for the extensional stiffness parameter is of the form

$$B = \sum_{j=0}^{\infty} b_j \text{Cos } j\theta + \sum_{j=1}^{\infty} b_j \text{Sin } j\theta \quad (1.25)$$

In many problems, there exists a plane of symmetry with respect to planform geometry. See Figure 1-3.

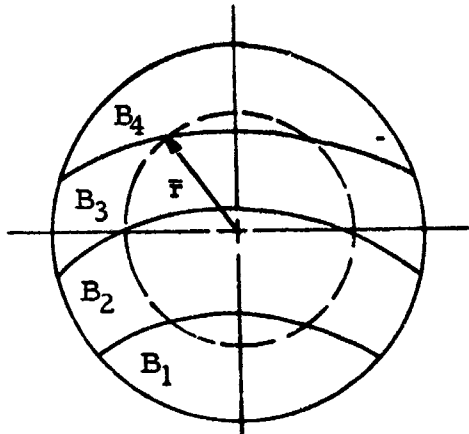


Figure 1.3. Stiffness Profile

A plane of symmetry is assumed here. The coefficients of B, viz.,  $b_j$  are found by integrations of the form

$$b_j = \frac{2}{\pi} \int_0^{\pi} B(\xi, \theta) \cos j\theta d\theta \quad (1.26)$$

The Fourier expansions of the shell stiffness parameters (Eqs. 1.14), consistent with previous formulation are given by

$$\begin{aligned} B_m &= E_o h_o \sum_{j=0}^{\infty} b_{mj}(\xi) \cos j\theta && \text{Inplane Stiffness} \\ D_m &= E_o h_o^3 \sum_{j=0}^{\infty} d_{mj}(\xi) \cos j\theta && \text{Bending Stiffness} \\ C_m &= \sum_{j=0}^{\infty} c_{mj}(\xi) \cos j\theta && \text{External Damping} \end{aligned} \quad (1.27)$$



$$\begin{aligned}
K_m &= \sum_{j=0}^{\infty} k_{mj}(\xi) \cos j\theta && \text{Elastic Foundation} \\
M_m &= \sum_{j=0}^{\infty} m_{mj}(\xi) \cos j\theta && \text{Mass Property}
\end{aligned} \tag{1.27}$$

Substitution of the displacement and rotation series expansions (Eqs. 1.22) and the above stiffness expansions into Eqs. (1.21) and employing the proper trigonometric identities yields the following series expressions relating forces (moments) in terms of the Fourier coefficients of the displacement variables and stiffness parameters:

$$\begin{aligned}
N_{\xi} &= \sigma_o h_o \sum_{k=0}^{\infty} \left[ \sum_{j=0}^{\infty} \left\{ B_1^{kj} \left( \frac{\partial u_j}{\partial \xi} + \omega_{\xi} w_j \right) + B_3^{kj} \left( \gamma u_j + \frac{k}{\rho} v_j + \omega_{\xi} w_j \right) \right\} - \right. \\
&\quad \left. t_k^T \right] \cos k\theta \\
N_{\theta} &= \sigma_o h_o \sum_{k=0}^{\infty} \left[ \sum_{j=0}^{\infty} \left\{ B_3^{kj} \left( \frac{\partial u_j}{\partial \xi} + \omega_{\xi} w_j \right) + B_2^{kj} \left( \gamma u_j + \frac{k}{\rho} v_j + \omega_{\theta} w_j \right) \right\} - \right. \\
&\quad \left. t_k^T \right] \cos k\theta \\
\bar{N}_{\xi\theta} &= \sigma_o h_o \sum_{k=1}^{\infty} \left[ \sum_{j=0}^{\infty} \frac{G_1^{kj}}{2} \left( \frac{\partial v_j}{\partial \xi} - \frac{k}{\rho} u_j - \gamma v_j \right) \right] \sin k\theta \\
Q_{\xi} &= \sigma_o h_o \sum_{k=0}^{\infty} \left[ \sum_{j=0}^{\infty} G_2^{kj} \left( -\omega_{\xi} u_j + \frac{\partial w_j}{\partial \xi} + \phi_{\xi j} \right) \right] \cos k\theta \\
M_{\xi} &= \frac{\sigma_o h_o^3}{a} \sum_{k=0}^{\infty} \left[ \sum_{j=0}^{\infty} \left\{ D_1^{kj} \frac{\partial \phi_{\xi j}}{\partial \xi} + D_3^{kj} \left( \gamma \phi_{\xi j} + \frac{k}{\rho} \phi_{0j} \right) \right\} - m^T \right] \cos k\theta \\
M_{\theta} &= \frac{\sigma_o h_o^3}{a} \sum_{k=0}^{\infty} \left[ \sum_{j=0}^{\infty} \left\{ D_3^{kj} \frac{\partial \phi_{\xi j}}{\partial \xi} + D_2^{kj} \left( \gamma \phi_{\xi j} + \frac{k}{\rho} \phi_{0j} \right) \right\} - m^T \right] \cos k\theta
\end{aligned} \tag{1.28}$$

$$\begin{aligned}
\bar{M}_{\xi\theta} &= \frac{\sigma_0 h_0^3}{a} \sum_{k=1}^{\infty} \left[ \sum_{j=0}^{\infty} \frac{G_{13}^{kj}}{2} \left( -\frac{k}{\rho} \phi_{\xi j} + \frac{\partial \phi_{\theta j}}{\partial \xi} - \gamma \phi_{\theta j} + \frac{1}{2} (\omega_{\xi} - \omega_{\theta}) \right) \right. \\
&\quad \left. \left( -\frac{k}{\rho} u_j - \frac{\partial v_j}{\partial \xi} - \gamma v_j \right) \right] \sin k\theta \\
Q_{\theta} &= \sigma_0 h_0 \sum_{n=1}^{\infty} \left[ \sum_{j=0}^{\infty} \left\{ C_3^{kj} \left( -\omega_{\theta} v_j - \frac{k}{\rho} w_j + \phi_{\theta j} \right) \right\} \right] \sin k\theta
\end{aligned} \tag{1.28}$$

The translational inertial force terms are expressed as

$$\begin{aligned}
M_{\xi} \ddot{U} &= \sum_{k=0}^{\infty} \left[ \sum_{j=0}^{\infty} M_1^{kj} \ddot{u}_j \right] \cos k\theta \\
M_{\theta} \ddot{V} &= \sum_{k=1}^{\infty} \left[ \sum_{j=0}^{\infty} M_2^{kj} \ddot{v}_j \right] \sin k\theta \\
M_{\zeta} \ddot{W} &= \sum_{k=0}^{\infty} \left[ \sum_{j=0}^{\infty} M_3^{kj} \ddot{w}_j \right] \cos k\theta
\end{aligned} \tag{1.29}$$

The translational damping force is expressible as

$$\begin{aligned}
C_{D_{\xi}} \dot{U} &= \sum_{k=0}^{\infty} \left( \sum_{j=0}^{\infty} C_1^{kj} \dot{u}_j \right) \cos k\theta \\
C_{D_{\theta}} \dot{V} &= \sum_{k=1}^{\infty} \left( \sum_{j=0}^{\infty} C_2^{kj} \dot{v}_j \right) \sin k\theta \\
C_{D_{\zeta}} \dot{W} &= \sum_{k=0}^{\infty} \left( \sum_{j=0}^{\infty} C_3^{kj} \dot{w}_j \right) \cos k\theta
\end{aligned} \tag{1.30}$$

The translational elastic foundation force is expressible as

$$\begin{aligned}
 K_{\xi} U &= \sum_{k=0}^{\infty} \left( \sum_{j=0}^{\infty} k_1^{kj} u_j \right) \cos k\theta \\
 K_{\theta} V &= \sum_{k=1}^{\infty} \left( \sum_{j=0}^{\infty} k_2^{kj} v_j \right) \sin k\theta \\
 K_{\zeta} W &= \sum_{k=0}^{\infty} \left( \sum_{j=0}^{\infty} k_3^{kj} w_j \right) \cos k\theta
 \end{aligned} \tag{1.31}$$

The stiffness recursion relationships above are described in the form

$$\begin{aligned}
 A^{kj} &= \frac{1}{2} \left\{ a_{(k+j)} + \left[ 1 - \delta^2 (j - n) + \delta (k) \right] a_{|k-j|} \right\} \\
 \bar{A}^{kj} &= \frac{1}{2} \left\{ -\bar{a}_{(k+j)} + \left[ 1 - \delta^2 (j - k) + \delta (k) \right] \bar{a}_{|k-j|} \right\}
 \end{aligned} \tag{1.32}$$

where the specific coefficients of interest (dropping  $k_j$  superscript) are given by

$$\begin{aligned}
 A &= \left\{ B_1, B_2, B_3, D_1, D_2, D_3, g_2, M_1, M_3, C_1, C_3, K_1, K_3 \right\} \\
 a &= \left\{ b_1, b_2, b_3, d_1, d_2, d_3, g_2, m_1, m_3, c_1, c_3, k_1, k_3 \right\}
 \end{aligned}$$

and

$$\begin{aligned}
 \bar{A} &= \left\{ G_1, G_3, G_{13}, M_2, C_2, K_2 \right\} \\
 \bar{a} &= \left\{ g_1, g_3, g_{13}, m_2, c_2, k_2 \right\}
 \end{aligned}$$

In the above expressions  $\delta (m)$  is defined as

$$\delta (m) = \begin{cases} -1, & m < 0 \\ 0, & m = 0 \\ +1, & m > 0 \end{cases}$$

(\*See Appendix 1.2 (multiplication of series expressions) for a more detailed description of  $A^{kj}$  and  $\bar{A}^{kj}$ .)

Substitution of the stress resultant expressions and dynamic force resultants (Eqs. 1.28 - 1.31) into the shell equilibrium equations (Eqs. 1.6) yields five finite series expressions in the circumferential coordinate relating the Fourier coefficients  $u_j$ ,  $v_j$ ,  $w_j$ ,  $\phi_{\xi j}$  and  $\phi_{\theta j}$  of the displacement and rotation variables. For practical considerations we truncate the series solution of the dependent variables to  $K$  terms in the Fourier component. Employing the appropriate orthogonality relationships of Fourier series to these equilibrium expressions yields a system of  $5K$  ordinary differential equations relating the  $5K$  unknown Fourier coefficients. These equations are presented in a form amenable for computer programming and are given as follows:

$$\sum_{j=0}^{K-1} \left[ f_{5k+l, 5j+1} u_j'' + f_{5k+l, 5j+2} v_j'' + f_{5k+l, 5j+3} w_j'' + f_{5k+l, 5j+4} \phi_{\xi j}'' + f_{5k+l, 5j+5} \phi_{\theta j}'' + g_{5k+l, 5j+1} u_j' + \dots + g_{5k+l, 5j+5} \phi_{\theta j}' + h_{5k+l, 5j+1} u_j + \dots + h_{5k+l, 5j+5} \phi_{\theta j} \right] \quad (1.33)$$

$$k_{5k+l, 5j+1} u_j + \dots + k_{5k+l, 5j+5} \phi_{\theta j} = \alpha_{5k+l, 5j+1} \ddot{u}_j + \dots + \alpha_{5k+l, 5j+5} \ddot{\phi}_{\theta j} + \beta_{5k+l, 5j+1} \dot{u}_j + \dots + \beta_{5k+l, 5j+5} \dot{\phi}_{\theta j} + p_{5k+l}$$

where

$$l = 1, 2, 3, 4, 5$$

$$k, j = 0, \dots, K - 1$$

where the  $f$ ,  $g$ ,  $h$ ,  $k$ ,  $\alpha$  and  $\beta$  coefficients are described in Appendix 1-B. (It should be noted that the form of the above equations is more complicated than was obtained in Reference 2 for analysis of shells of revolution. This complexity arises from the fact that the equilibrium equations cannot be decoupled for each Fourier component of displacement variables for the case of unsymmetric shell.)

The above equation can be conveniently written in matrix form as follows:

$$Fz'' + Gz' + (H + K)z = \alpha z + \beta \dot{z} + p \quad (1.34)$$

where  $F$ ,  $G$ ,  $H$ ,  $K$ ,  $\alpha$ ,  $\beta$  are square arrays and  $z$ ,  $p$  are column arrays. These arrays are defined as,

$$F = \begin{bmatrix} f_{11} & f_{12} & \cdot & \cdot & f_{1,5k} \\ f_{21} & \cdot & \cdot & \cdot & \cdot \\ \cdot & \cdot & \cdot & \cdot & \cdot \\ \cdot & \cdot & \cdot & \cdot & \cdot \\ f_{5k,1} & \cdot & \cdot & \cdot & f_{5k,5k} \end{bmatrix} \quad G = \begin{bmatrix} g_{11} & g_{12} & \cdot & \cdot & \cdot \\ g_{21} & \cdot & \cdot & \cdot & \cdot \\ \cdot & \cdot & \cdot & \cdot & \cdot \\ \cdot & \cdot & \cdot & \cdot & \cdot \\ \cdot & \cdot & \cdot & \cdot & \cdot \end{bmatrix}$$

$$H = \begin{bmatrix} h_{11} & h_{12} & \cdot & \cdot & \cdot \\ h_{21} & \cdot & \cdot & \cdot & \cdot \\ \cdot & \cdot & \cdot & \cdot & \cdot \\ \cdot & \cdot & \cdot & \cdot & \cdot \\ \cdot & \cdot & \cdot & \cdot & \cdot \end{bmatrix} \quad K = \begin{bmatrix} k_{11} & k_{12} & \cdot & \cdot & \cdot \\ k_{21} & \cdot & \cdot & \cdot & \cdot \\ \cdot & \cdot & \cdot & \cdot & \cdot \\ \cdot & \cdot & \cdot & \cdot & \cdot \\ k_{5k,1} & \cdot & \cdot & \cdot & \cdot \end{bmatrix}$$

$$\alpha = \begin{bmatrix} \alpha_{11} & \alpha_{12} & \cdot & \cdot & \cdot \\ \alpha_{21} & \cdot & \cdot & \cdot & \cdot \\ \cdot & \cdot & \cdot & \cdot & \cdot \\ \cdot & \cdot & \cdot & \cdot & \cdot \\ \cdot & \cdot & \cdot & \cdot & \cdot \end{bmatrix} \quad \beta = \begin{bmatrix} \beta_{11} & \beta_{12} & \cdot & \cdot & \cdot \\ \beta_{21} & \cdot & \cdot & \cdot & \cdot \\ \cdot & \cdot & \cdot & \cdot & \cdot \\ \cdot & \cdot & \cdot & \cdot & \cdot \\ \cdot & \cdot & \cdot & \cdot & \cdot \end{bmatrix}$$

$$z = \begin{bmatrix} z_1 \\ z_2 \\ z_3 \\ \cdot \\ z_k \end{bmatrix} \quad z_i = \begin{bmatrix} u_i \\ v_i \\ w_i \\ \phi_{\xi i} \\ \phi_{\theta i} \end{bmatrix} \quad p = \begin{bmatrix} p_1 \\ p_2 \\ \cdot \\ \cdot \\ p_k \end{bmatrix} \quad p_i = \begin{bmatrix} p_1^i \\ p_2^i \\ p_3^i \\ p_4^i \\ p_5^i \end{bmatrix}$$

The elements of the F, G and H, K,  $\alpha$ ,  $\beta$ , and p matrices are given in Appendix 1.13.1 and are presented there in a format which is designed to ease computer programming. The coefficients of P are the Fourier components of the applied external load and are known quantities for a specific loading case.

The more general case of shells having arbitrary distribution of stiffness, loads, damping, and elastic foundation can be considered in the same manner as the case of plane of symmetry of stiffness and loads. In this case the total Fourier series representation of all the variables, displacements, rotations, stiffness and loads, must be carried in the analysis. The analysis will follow the same format of the special case formulated previously.

### Boundary Conditions

Consistent with Sanders' equilibrium equations, the boundary conditions for the specification of the forces or displacements, or constraint between them are described below. On the edge where  $\xi = \text{constant}$  (i. e.,  $\xi = 0$ , and  $\xi = \bar{s}$ )

$$\begin{aligned} N_{\xi} & \text{ or } U_{\xi} \\ \hat{N}_{\xi\theta} & \text{ or } U_{\theta} \\ Q_{\xi} & \text{ or } W \\ M_{\xi} & \text{ or } \Phi_{\xi} \\ \bar{M}_{\xi\theta} & \text{ or } \Phi_{\theta} \end{aligned} \tag{1.35}$$

where

$$\hat{N}_{\xi\theta} = \bar{N}_{\xi\theta} + \frac{1}{2a} (\omega_0 - \omega_{\xi}) \bar{M}_{\xi\theta}$$

These conditions can be expressed in matrix form by,

$$\bar{\Omega}\bar{y} + \bar{\Lambda}\bar{z} = \bar{l} \quad (1.36)$$

where  $\bar{y}$ ,  $\bar{l}$ ,  $\bar{z}$  are column matrices and  $\bar{\Omega}$ ,  $\bar{\Lambda}$  are appropriate diagonal matrices

$$\bar{y} = \begin{bmatrix} N_{\xi} \\ \hat{N}_{\xi\theta} \\ Q_{\xi} \\ M_{\xi} \\ M_{\xi\theta} \end{bmatrix} \quad \bar{z} = \begin{bmatrix} U_{\xi} \\ U_{\theta} \\ W \\ \Phi_{\xi} \\ \Phi_{\theta} \end{bmatrix} \quad \bar{l} = \begin{bmatrix} l_1 \\ l_2 \\ l_3 \\ l_4 \\ l_5 \end{bmatrix}$$

$$\bar{\Omega} = \begin{bmatrix} \omega_1 & & & & \\ & \omega_2 & & & \\ & & \omega_3 & & \\ & & & \omega_4 & \\ & & & & \omega_5 \end{bmatrix} \quad \bar{\Lambda} = \begin{bmatrix} \lambda_1 & & & & \\ & \lambda_2 & & & \\ & & \lambda_3 & & \\ & & & \lambda_4 & \\ & & & & \lambda_5 \end{bmatrix}$$

The logic which connects  $\bar{\Omega}$ ,  $\bar{\Lambda}$ ,  $\bar{l}$  and the conditions desired are given in the following table:

Matrix Elements				
Condition at Boundary	$\omega_i$	$\lambda_i$	$l_i$	
Displacement Prescribed	0	1	$C_1$	$C_1 =$ value of displacement
Force Prescribed	1	0	$C_2$	$C_2 =$ value of force
Constraint Condition	1	$C_3$	0	$C_3 =$ constant relating force and displacement

For example, if  $\Phi_{\xi}$  is given as a boundary condition then  $\lambda_4 = 1$ ,  $\omega_4 = 0$  and  $l_4$  is the prescribed value of  $\Phi_{\xi}$ . Note  $C_i$  is nondimensionalized with the appropriate reference constants.

It will be convenient to expand forces and moments in Fourier series in manner consistent with the previous developments. Letting

$$\begin{aligned}
 N_{\xi} &= \sum t_{\xi}^n \text{Cos } n\theta \\
 \hat{N}_{\xi\theta} &= \sum \hat{t}_{\xi\theta}^n \text{Sin } n\theta \\
 Q_{\xi} &= \sum q_{\xi}^n \text{Cos } n\theta \\
 M_{\xi} &= \sum m_{\xi}^n \text{Cos } n\theta \\
 \bar{M}_{\xi\theta} &= \sum m_{\xi\theta}^n \text{Sin } n\theta
 \end{aligned}
 \tag{1.37}$$

and

$$\begin{aligned}
 l_1 &= \sum l_1^n \text{Cos } n\theta \\
 l_2 &= \sum l_2^n \text{Sin } n\theta \\
 l_3 &= \sum l_3^n \text{Cos } n\theta \\
 l_4 &= \sum l_4^n \text{Cos } n\theta \\
 l_5 &= \sum l_5^n \text{Sin } n\theta
 \end{aligned}$$

The above series expressions together with Eqs. (1.21) are substituted into Eq. (1.36) and the circumferential variation separated, yielding the following matrix form for the relationship of the Fourier coefficients.

$$\Omega y + \Lambda z = l \tag{1.38}$$

where

$$y = \begin{bmatrix} y_1 \\ y_2 \\ \cdot \\ \cdot \\ y_k \end{bmatrix} \quad y_i = \begin{bmatrix} t_{\xi}^i \\ \hat{t}_{\xi\theta}^i \\ q_{\xi}^i \\ m_{\xi}^i \\ m_{\xi\theta}^i \end{bmatrix} \quad z = \begin{bmatrix} z_1 \\ z_2 \\ \cdot \\ \cdot \\ z_k \end{bmatrix} \quad z_i = \begin{bmatrix} u_i \\ v_i \\ w_i \\ \phi_{\xi_i} \\ \phi_{\theta_i} \end{bmatrix}$$



$$\Omega = \begin{bmatrix} \bar{\Omega} & & & & \\ & \bar{\Omega} & & & \\ & & \cdot & & 0 \\ & & & C & \cdot \\ & & & & \bar{\Omega}_k \end{bmatrix} \quad \Lambda = \begin{bmatrix} \bar{\Lambda} & & & & \\ & \bar{\Lambda} & & 0 & \\ & & \cdot & & \\ & & & 0 & \cdot \\ & & & & \bar{\Lambda}_k \end{bmatrix}$$

$$\ell = \begin{bmatrix} \bar{\ell}_1 \\ \bar{\ell}_2 \\ \cdot \\ \cdot \\ \bar{\ell}_k \end{bmatrix} \quad \ell_i = \begin{bmatrix} \ell_{1i} \\ \ell_{2i} \\ \ell_{3i} \\ \cdot \\ \ell_{4i} \\ \ell_{5i} \end{bmatrix}$$

It will be desirable to express boundary conditions in terms of  $z$ . The substitution of Eqs. (1.37) in Eq. (1.27) with appropriate orthogonality operations yields a set of recursion expressions relating Fourier coefficients of forces and moments to the displacement and stiffness coefficients. These relationships are given by

$$t_{\xi}^k = \sum_{j=0}^{K-1} \left[ r_{5k+1, 5j+1} u_j' + r_{5k+1, 5j+4} \phi_{\xi j}' + s_{5k+1, 5j+1} u_j + s_{5k+1, 5j+2} v_j + s_{5k+1, 5j+3} w_j + s_{5k+1, 5j+4} \phi_{\xi j} + s_{5k+1, 5j+5} \phi_{0j} \right] + a_{5k+1} \quad (1.39)$$

$$t_{\xi 0}^k = \sum_{j=0}^{K-1} \left[ r_{5k+2, 5j+2} v_j' + r_{5k+2, 5j+5} \phi_{0j}' + s_{5k+2, 5j+1} u_j + s_{5k+2, 5j+2} v_j + s_{5k+2, 5j+4} \phi_{\xi j} + s_{5k+2, 5j+5} \phi_{0j} \right]$$

$$q_{\xi}^k = \sum_{j=0}^{K-1} \left[ r_{5k+3, 5j+2} w'_j + s_{5k+3, 5j+1} u_j + s_{5k+3, 5j+4} \phi_{\xi j} \right]$$

$$m_{\xi}^k = \sum_{j=0}^{K-1} \left[ r_{5k+4, 5j+1} u'_j + r_{5k+4, 5j+4} \phi'_{\xi j} + s_{5k+4, 5j+1} u_j \right. \\ \left. + s_{5k+4, 5j+2} v_j + s_{5k+4, 5j+3} w_j + s_{5k+4, 5j+4} \phi_{\xi j} \right. \\ \left. + s_{5k+4, 5j+5} \phi_{\theta j} \right] + a_{\pi 5k+4}$$

$$m_{\xi\theta}^k = \sum_{j=0}^{K-1} \left[ r_{5k+5, 5j+2} v'_j + r_{5k+5, 5j+5} \phi'_{\theta j} + s_{5k+5, 5j+1} u_j \right. \\ \left. + s_{5k+5, 5j+2} v_j + s_{5k+5, 5j+4} \phi_{\xi j} + s_{5k+5, 5j+5} \phi_{\theta j} \right]$$

where

$$k = 0, 1, 2, \dots, K-1$$

Coefficients are given in Appendix 1-3.

Equation 1.39 can be written in matrix notation as

$$y = Rz' + Sz + a \quad (1.40)$$

Hence, the boundary conditions (1.38) become

$$\Omega Rz' + (\Lambda + \Omega s) z = \ell - \Omega a \quad (1.41)$$

The form of Eq. (1.41) is modified if the shell has a pole (i.e.,  $r = 0$ ) because the coefficients of the differential equations become singular for this case. Following a similar limiting process as described by Greenbaum (Reference 5) the conditions supplied at the pole are:

For Fourier index = 0

$$u_0 = v_0 = \phi_{\xi 0} = \phi_{\theta 0} = q_{\xi 0} = 0 \quad (1.42)$$

For Fourier index = 1

$$u_1 + v_1 = w_1 = \phi_{\xi_1} + \phi_{\theta_1} = t_{\xi_1} - \hat{t}_{\xi\theta_1} = m_{\xi_1} - m_{\xi\theta_1} = 0 \quad (1.42)$$

For Fourier index  $\geq 2$

$$u_i = v_i = w_i = \phi_{\xi_i} = \phi_{\theta} = 0$$

### 1.8 FINITE DIFFERENCE FORMULATION IN THE MERIDIONAL VARIABLE

In a manner similar to that described in Reference 2 the partial differential equation in the matrix form (Equation 1.34) is reduced by a system of finite difference approximations. The variation in the meridional coordinate of the Fourier coefficients are described point-wise in Eq. (1.34). The following are finite difference forms for the partial differentials in the meridional coordinate at interior points.

$$\begin{aligned} \frac{\partial^2 f}{\partial \xi^2} &= \frac{1}{\Delta^2} (f_{i+1} - 2f_i + f_{i-1}) \\ \frac{\partial f}{\partial \xi} &= \frac{1}{2\Delta} (f_{i+1} - f_{i-1}) \end{aligned} \quad (1.43)$$

where  $\Delta$  is the increment along  $\xi$  and subscripts denote the discrete value of the function taken.

The forms at boundary points (initial)

$$\left( \frac{\partial f}{\partial \xi} \right)_1 = \frac{1}{2\Delta} (3f_1 - 4f_2 + f_3) \quad (1.44)$$

terminal

$$\left( \frac{\partial f}{\partial \xi} \right)_N = \frac{1}{2\Delta} (-f_{N-2} + 4f_{N-1} - 3f_N) \quad (1.45)$$

The result of the application of the various finite difference forms can be stated compactly as the following set of equations:

$$\begin{aligned}
A_0 z_2 + B_0 z_1 + C_0 z_0 &= g_0 \\
A_i z_{i+1} + B_i z_i + C_i z_{i-1} &= g_i + 2\Delta (\alpha_i \ddot{z}_i + \beta_i \dot{z}_i)
\end{aligned} \tag{1.46}$$

$$A_N z_N + B_N z_{N-1} + C_N z_{N-2} = g_N$$

Where

$$A_0 = -\Omega_0 R_0$$

$$B_0 = 2 \frac{\Omega_0}{\Delta} R_0$$

$$C_0 = \Lambda_0 + \Omega_0 S_0 - 3 \frac{\Omega_0}{2\Delta} R_0$$

$$g_0 = l_0 - \Omega_0 a_0$$

the subscript (o) refers to the conditions at  $s = 0$ .

For  $i \neq 0, N$

$$\begin{aligned}
A_i &= \frac{2F_i}{\Delta} + G_i \\
B_i &= \frac{4F_i}{\Delta} + 2\Delta (H_i + K_i) \\
C_i &= \frac{2F_i}{\Delta} - G_i
\end{aligned} \tag{1.47}$$

$$g_i = 2\Delta p_i$$

Finally for  $i = N$  or conditions at  $s = \bar{s}$

$$\begin{aligned}
A_N &= \Lambda_N + \Omega_N S_N + 3 \frac{\Omega_N}{2\Delta} R_N \\
B_N &= -2 \frac{\Omega_N}{\Delta} R_N \\
C_N &= \frac{\Omega_N}{2\Delta} R_N
\end{aligned} \tag{1.48}$$

$$g_N = l_N - \Omega_N a_N$$

### 1.9 FINITE DIFFERENCE FORMULATION IN THE TIME VARIABLE

By the use of difference equations the above differential equation in matrix form may be transformed into a set of algebraic equations involving the variable  $z_i$  at successive values of time.

The most commonly used are the central difference forms; however, from a numerical stability aspect, the difference forms of Houbolt 3, 4 are used. These forms are

$$\ddot{z} = \frac{2z_j - 5z_{j-1} + 4z_{j-2} - z_{j-3}}{\delta^2} \quad (1.49)$$

$$\dot{z} = \frac{11z_j - 18z_{j-1} + 9z_{j-2} - 2z_{j-3}}{6\delta} \quad (1.50)$$

Where the subscript  $j$  refers to the time interval  $j = 0, 1, 2, \dots$  and  $\delta$  is the time increment.

Introducing these expressions in Eq. 1.46 results in the following set of algebraic equations for the shell response problem.

$$\begin{aligned} A_0 z_{2,j} + B_0 z_{1,j} + C_0 z_{0,j} &= g_0 \\ A_i^* z_{i+1,j} + B_{i,j}^* z_{i,j} + C_i^* z_{i-1,j} &= g_{i,j} \\ A_N z_{N,j} + B_N z_{N-1,j} + C_N z_{N-2,j} &= g_N \end{aligned} \quad (1.51)$$

where

$$\begin{aligned} A_i^* &= \delta A_i \\ B_{i,j}^* &= \delta B_i + 4 \frac{\Delta}{\delta} \alpha_i + \frac{11}{3} \Delta \beta_i \\ C_i^* &= \delta C_i \\ g_{i,j}^* &= \delta g_i + L_i z_{i,j-1} + M_i z_{i,j-2} + N_i z_{i,j-3} \end{aligned}$$

and

$$\begin{aligned} L_i &= 10 \frac{\Delta}{\delta} \alpha_i + 6 \Delta \beta_i \\ M_i &= -8 \frac{\Delta}{\delta} \alpha_i - 3 \Delta \beta_i \\ N_i &= 2 \frac{\Delta}{\delta} \alpha_i + \frac{2}{3} \Delta \beta_i \end{aligned}$$

In the real problem no values of  $z_i$  exists for less than zero. The assumption that  $z_i$  does exist before  $t = 0$  is a means of allowing the recurrence from Eq. (1.51) to apply at the origin as well as later values of time. Furthermore, no violation is made as long as the initial conditions of  $t = 0$  are satisfied.

To obtain values for fictitious terms  $j = -1, -2$  a procedure similar to that described by Houbolt is used. The procedure will require a modification of  $B_{i,j}^*$ ,  $g_{i,j}^*$  for  $j = 1, 2$ .

The difference equations for the first and second derivatives at the third increment of four successive increments are given by

$$\begin{aligned}\ddot{z}_{i,j} &= \frac{1}{\delta^2} (z_{i,j+1} - 2z_{i,j} + z_{i,j-1}) \\ \dot{z}_{i,j} &= \frac{1}{6\delta} (2z_{i,j+1} + 3z_{i,j} - 6z_{i,j-1} + z_{i,j-2})\end{aligned}\tag{1.52}$$

Applying the equations at  $t = 0$ , i.e.,  $j = 0$

$$\begin{aligned}\ddot{z}_{i,0} &= \frac{1}{\delta^2} (z_{i,1} - 2z_{i,0} + z_{i,-1}) \\ \dot{z}_{i,0} &= \frac{1}{6\delta} (2z_{i,1} + 3z_{i,0} - 6z_{i,-1} + z_{i,-2})\end{aligned}\tag{1.53}$$

The initial conditions are that the displacements and velocities are prescribed at  $t = 0$ . By application of Newton's second law, a secondary initial condition can be established, i.e., acceleration immediately following application of the initial forces. These conditions are

$$\begin{aligned}z_{i,0} &= d_{i,0} \\ \dot{z}_{i,0} &= v_{i,0} \\ \ddot{z}_{i,0} &= a_{i,0}\end{aligned}\tag{1.54}$$

Where  $d_{i,0}$ ,  $v_{i,0}$ ,  $a_{i,0}$  are column  $n$  matrices formed of the respective coefficients of the Fourier expansions on  $\theta$  of the initial displacements, velocities, and accelerations at the meridional location  $i$ .

Substitution of these values into Eq. (1.53) yields the following relations

$$\begin{aligned}
 z_{i,0} &= d_{i,0} \\
 z_{i,-1} &= \delta^2 a_{i,0} + 2d_{i,0} - z_{i,1} \\
 z_{i,-2} &= 6\delta^2 a_{i,0} + 6\delta v_{i,0} + ad_{i,0} - 8z_{i,1}
 \end{aligned} \tag{1.55}$$

Substitution of these relations in Eq. (1.50) for  $j = 1$  yields the following change in the definitions of Eq. (1.52)

$$\begin{aligned}
 B_{i,1}^* &= \delta B_i + 12 \frac{\Delta}{\delta} \alpha_i + 6\Delta\beta_i \\
 g_{i,1}^* &= \delta g_i + \left( 12 \frac{\Delta}{\delta} \alpha_i + 6\Delta\beta_i \right) d_{i,0} + \left( 4\Delta\delta\alpha_i - \frac{7}{3} \delta^2 \Delta\beta_i \right) a_{i,0} + \\
 &\quad (12\Delta\alpha_i + 4\Delta\delta\beta_i) v_{i,0}
 \end{aligned} \tag{1.56}$$

Substitution of definitions Eq. (1.50) for  $j = 2$  yields the following change in definitions of Eq. (1.52)

$$\begin{aligned}
 g_{i,2}^* &= \delta g_i + \left( 8 \frac{\Delta}{\delta} \alpha_i + \frac{16}{3} \beta_i \right) z_{i,1} + \left( -4 \frac{\Delta}{\delta} \alpha_i - \frac{5}{3} \Delta\beta_i \right) d_{i,0} + \\
 &\quad \left( 2 \frac{\Delta}{\delta} \alpha_i + \frac{2}{3} \Delta\beta_i \right) \delta^2 a_{i,0}
 \end{aligned} \tag{1.57}$$

The set of Eq. (1.52) and the additional definitions at the first two time intervals Eqs. (1.56, 1.57) is now the algebraic statement of the dynamic response problem.

#### 1.10 MATRIX SOLUTION OF THE DIFFERENCE EQUATIONS

The set of matrix equations defined in Eqs. 1.51, 1.56, 1.57 will be solved by the same procedure described in Reference 2. This procedure is essentially a Gaussian elimination performed on the partitioned arrays. A slight modification of the elimination procedure described in Reference 6 is used here. Considering the first and second equations of Eq. (1.52) at the  $j^{\text{th}}$  time interval

$$\begin{aligned}
 A_0 z_{2,j} + B_0 z_{1,j} + C_0 z_{0,j} &= g_0 \\
 A_1 z_{2,j} + B_1^* z_{1,j} + C_1 z_{0,j} &= g_{1,j}^*
 \end{aligned} \tag{1.58}$$

PAGE <sup>31</sup>~~30~~ AND <sup>32</sup>~~31~~ ARE MISSING FROM ORIGINAL DOCUMENT.



~~RESEARCH PAGE BLANK NOT FILMED.~~

The matrix solution of these difference equations are solved by the procedure described in Section 1.10. By defining the starred quantities, ( )\*, without the star the numerical procedure for the static analysis is completely defined.

## 1.12 REFERENCES

1. Sanders, J. Lyell, Jr., "An Improved First-Approximation Theory for Thin Shells," NASA TR R-24, 1959.
2. Budiansky and Radkowski, "Numerical Analysis of Unsymmetrical Bending of Shells of Revolution," AIAA Journal, Vol. 1, No. 8, August 1963.
3. Johnson, D. E., and Greif, R., "Dynamic Response of a Cylindrical Shell; Two Numerical Methods," AIAA J. 4, 486-494 (1966).
4. Houbolt, J. C., "A Recurrence Matrix Solution for the Dynamic Response of Aircraft in Gusts," NASA TN 2060, January 1950.
5. Greenbaum, G. A., "Comments on 'Numerical Analysis of Unsymmetrical Bending of Shells of Revolution,'" AIAA Journal, Vol. 2, No. 3 (March 1964), pp 590, 591.
6. Potters, M. L. "A Matrix Method for the Solution of a Second Order Difference Equation in Two Variables," Mathematisch Centrum, Amsterdam, Holland, Report MR 19 (1955).

## 1.13 APPENDIX

### 1.13.1 Modification of Sander's Equations

Virtual change in the strain energy within C

$$\delta \bar{U} = \iint (N_{11} \delta \epsilon_{11} + N_{12} \delta \epsilon_{12} + N_{21} \delta \epsilon_{21} + N_{22} \delta \epsilon_{22} + M_{11} \delta k_{11} + M_{12} \delta k_{12} + M_{21} \delta k_{21} + M_{22} \delta k_{22} + Q_1 \delta \gamma_1 + Q_2 \delta \gamma_2) ds \quad (1)$$

$$\epsilon_{12} = \epsilon_{21} \quad (2)$$

$$k_{12} - k_{21} = \left( \frac{1}{R_2} - \frac{1}{R_1} \right) \epsilon_{12} + \frac{1}{\alpha_1 \alpha_2} \frac{\partial \alpha_2 \gamma_2}{\partial \xi_1} - \frac{1}{\alpha_1 \alpha_2} \frac{\partial \alpha_1 \gamma_1}{\partial \xi_2} \quad (3)$$

~~RESEARCH PAGE BLANK NOT FILMED.~~

Substituting (2) → (1)

$$\begin{aligned}
 &= \iint \left[ N_{11} \delta \epsilon_{11} + (N_{12} + N_{21}) \delta \epsilon_{12} + N_{22} \delta \epsilon_{22} + M_{11} \delta k_{11} + \right. \\
 &\quad \left. \frac{1}{2} M_{12} \delta k_{12} + \frac{1}{2} M_{12} \delta k_{12} + \frac{1}{2} M_{21} \delta k_{21} + \frac{1}{2} M_{21} \delta k_{21} + \right. \\
 &\quad \left. \frac{1}{2} M_{21} \delta k_{12} - \frac{1}{2} M_{21} \delta k_{12} + \frac{1}{2} M_{12} \delta k_{21} - \frac{1}{2} M_{12} \delta k_{21} + \right. \\
 &\quad \left. M_{22} \delta k_{22} + Q_1 \delta \gamma_1 + Q_2 \delta \gamma_2 \right] \alpha_1 \alpha_2 d\xi_1 d\xi_2
 \end{aligned} \tag{4}$$

Rearrange

$$\begin{aligned}
 &= \iint \left[ N_{11} \delta \epsilon_{11} + (N_{12} + N_{21}) \delta \epsilon_{12} + N_{22} \delta \epsilon_{22} + M_{11} \delta k_{11} + \right. \\
 &\quad \left. \frac{1}{2} (M_{12} - M_{21}) \delta (k_{12} - k_{21}) + \frac{1}{2} (M_{12} + M_{21}) \delta k_{21} + \right. \\
 &\quad \left. \frac{1}{2} (M_{12} + M_{21}) \delta k_{12} + M_{22} \delta k_{22} + Q_1 \delta \gamma_1 + Q_2 \delta \gamma_2 \right] \alpha_1 \alpha_2 d\xi_1 d\xi_2
 \end{aligned} \tag{5}$$

Substitute 3 → 5.

$$\begin{aligned}
 &\iint \left[ N_{11} \delta \epsilon_{11} + (N_{12} + N_{21}) \delta \epsilon_{12} + N_{22} \delta \epsilon_{22} + M_{11} \delta k_{11} + \right. \\
 &\quad \left. \frac{1}{2} (M_{12} - M_{21}) \delta \left( \left( \frac{1}{R_2} - \frac{1}{R_1} \right) \epsilon_{12} + \frac{1}{\alpha_1 \alpha_2} \frac{\partial \alpha_2 \gamma_2}{\partial \xi_1} - \right. \right. \\
 &\quad \left. \left. \frac{1}{\alpha_1 \alpha_2} \frac{\partial \alpha_1 \gamma_1}{\partial \xi_2} \right) + \frac{1}{2} (M_{21} + M_{12}) \delta (k_{12} + k_{21}) + M_{22} \delta k_{22} + \right. \\
 &\quad \left. Q_1 \delta \gamma_1 + Q_2 \delta \gamma_2 \right] \alpha_1 \alpha_2 d\xi_1 d\xi_2
 \end{aligned}$$

Group.

$$\iint \left\{ N_{11} \delta \epsilon_{11} + 2 \left( \frac{1}{2} (N_{12} + N_{21}) + \frac{1}{4} \left( \frac{1}{R_2} - \frac{1}{R_1} \right) (M_{12} - M_{21}) \right) \delta \epsilon_{12} + \right. \\ \left. N_{22} \delta \epsilon_{22} + M_{11} \delta k_{11} + \frac{1}{2 \alpha_1 \alpha_2} (M_{12} - M_{21}) \delta \left( \frac{\partial \alpha_2 \gamma_2}{\partial \xi_1} - \frac{\partial \alpha_1 \gamma_1}{\partial \xi_2} \right) + \right. \\ \left. \frac{1}{2} (M_{21} + M_{12}) \delta (k_{12} + k_{21}) + M_{22} \delta k_{22} + Q_1 \delta \gamma_1 + Q_2 \delta \gamma_2 \right\} \alpha_1 \alpha_2 d\xi_1 d\xi_2$$

Expanding  $\delta \frac{\partial}{\partial \xi} (\alpha \gamma)$

$$\delta \left( \frac{\partial \alpha_2 \gamma_2}{\partial \xi_1} - \frac{\partial \alpha_1 \gamma_1}{\partial \xi_2} \right) = \delta \left( \gamma_2 \frac{\partial \alpha_2}{\partial \xi_1} + \alpha_2 \frac{\partial \gamma_2}{\partial \xi_1} - \gamma_1 \frac{\partial \alpha_1}{\partial \xi_2} - \alpha_1 \frac{\partial \gamma_1}{\partial \xi_2} \right)$$

Substitute and Group.

$$\iint \left\{ N_{11} \delta \epsilon_{11} + 2 \left[ \frac{1}{2} (N_{12} + N_{21}) + \frac{1}{4} \left( \frac{1}{R_2} - \frac{1}{R_1} \right) (M_{12} - M_{21}) \right] \delta \epsilon_{12} + \right. \\ \left. N_{22} \delta \epsilon_{22} + M_{11} \delta k_{11} + \frac{1}{2} (M_{21} + M_{12}) \delta (k_{12} + k_{21}) + M_{22} \delta k_{22} + \right. \\ \left. \left[ Q_1 - \frac{1}{2 \alpha_1 \alpha_2} \frac{\partial \alpha_1}{\partial \xi_2} (M_{12} - M_{21}) \right] \delta \gamma_1 + \left[ Q_2 + \frac{1}{2 \alpha_1 \alpha_2} \frac{\partial \alpha_2}{\partial \xi_1} (M_{12} - M_{21}) \right] \right. \\ \left. \delta \gamma_2 + \frac{1}{2} (M_{12} - M_{21}) \delta \left( \frac{1}{\alpha_1} \frac{\partial \gamma_2}{\partial \xi_1} - \frac{1}{\alpha_2} \frac{\partial \gamma_1}{\partial \xi_2} \right) \right\} \alpha_1 \alpha_2 d\xi_1 d\xi_2$$

Assumption

$$M_{12} - M_{21} \rightarrow 0, \quad \frac{\delta \partial \gamma_i}{\partial \xi_j} \ll \delta (\epsilon, k)$$

$$\iint \left\{ N_{11} \delta \epsilon_{11} + 2 \bar{N}_{12} \delta \epsilon_{12} + N_{22} \delta \epsilon_{22} + M_{11} \delta k_{11} + M_{22} \delta k_{22} + \right. \\ \left. 2 \bar{M}_{12} \delta \bar{k}_{12} + Q_1 \delta \gamma_1 + Q_2 \delta \gamma_2 \right\} \alpha_1 \alpha_2 d\xi_1 d\xi_2$$

$$\bar{N}_{12} = \frac{1}{2} (N_{12} + N_{21})$$

$$\bar{M}_{12} = \frac{1}{2} (M_{12} + M_{21})$$

$$\bar{K}_{12} = \frac{1}{2} (k_{12} + k_{21})$$

### 1.132 Multiplication of Series Expansions

The relationships  $A^{nj}$  and  $\bar{A}^{nj}$  used in the text are found by multiplying term by term the series expansions of stiffness and strain and noting a recurring sequence of the resulting expressions

$$\begin{aligned} \text{e. g., } \left( \sum_{j=0}^{K-1} b_j \cos j\theta \right) \left( \sum_{n=0}^{K-1} \epsilon_{\xi n} \cos n\theta \right) &= \sum_{n=0}^{K-1} \left( \sum_{j=0}^{K-1} A^{nj} \epsilon_{\xi j} \right) \cos n\theta \\ &= \sum_{n=0}^{K-1} \left\{ \sum_{j=0}^{K-1} \frac{1}{2} \left[ b^{(n+j)} + \left| 1 - \delta^2 (j-k) + \delta(k) \right| b^{|n-j|} \right] \epsilon_{\xi j} \right\} \cos n\theta \\ \left( \sum_{j=0}^{K-1} b_j \cos j\theta \right) \left( \sum_{n=1}^{K-1} \bar{\epsilon}_{\xi n} \sin n\theta \right) &= \sum_{n=1}^{K-1} \left( \sum_{j=0}^{K-1} \bar{A}^{nj} \bar{\epsilon}_{\xi j} \right) \sin n\theta \\ &= \sum_{n=1}^{K-1} \left\{ \sum_{j=0}^{K-1} \frac{1}{2} \left[ -b^{(n+j)} + \left| 1 - \delta^2 (j-k) + \delta(k) \right| b^{|n-j|} \right] \bar{\epsilon}_{\xi j} \right\} \sin n\theta \end{aligned}$$

where

$$\delta(m) = \begin{cases} -1 & m < 0 \\ 0 & m = 0 \\ +1 & m > 0 \end{cases}$$

### 1.133 Coefficients

Stiffness parameters related in an isotropic manner

$$B_1 = B_2 = \frac{B_3}{\nu}$$

$$D_1 = D_2 = \frac{D_3}{\nu}$$

$$G_1 = G_2 = G_3 = \frac{B_1 (1 - \nu)}{2}$$

$$G_{13} = \frac{D_1 (1 - \nu)}{2}$$

$$f_{5k+1, 5j+1} = B_1^{kj}$$

$$f_{5k+1, 5j+4} = 0$$

$$f_{5k+2, 5j+2} = \frac{G_1^{kj}}{2} + \frac{\lambda^2}{8} (\omega_\theta - \omega_\xi)^2 G_{13}^{kj}$$

$$f_{5k+2, 5j+5} = \frac{\lambda^2}{4} (\omega_\theta - \omega_\xi) G_{13}^{kj}$$

$$f_{5k+3, 5j+3} = G_2^{kj}$$

$$f_{5k+4, 5j+1} = 0$$

$$f_{5k+4, 5j+4} = \lambda^2 D_1^{kj}$$

$$f_{5k+5, 5j+2} = \frac{\lambda^2}{4} (\omega_\theta - \omega_\xi) G_{13}^{kj}$$

$$f_{5k+5, 5j+5} = \frac{\lambda^2}{2} G_{13}^{kj}$$

$$g_{5k+1, 5j+1} = B_1^{kj'} + \gamma B_1^{kj}$$

$$g_{5k+1, 5j+2} = \frac{k}{\rho} B_3^{kj} + \frac{k}{2\rho} G_1^{kj} - \frac{\lambda^2 k}{8\rho} (\omega_\theta - \omega_\xi)^2 G_{13}^{kj}$$

$$g_{5k+1, 5j+3} = \omega_\xi B_1^{kj} + \omega_\theta B_3^{kj} + \omega_\xi G_2^{kj}$$

$$g_{5k+1, 5j+4} = 0$$

$$g_{5k+1, 5j+5} = + \frac{\lambda^2 k}{4\rho} (\omega_\xi - \omega_\theta) G_{13}^{kj}$$

$$g_{5k+2, 5j+1} = -\frac{k}{2\rho} G_1^{kj} + \frac{\lambda^2 k}{8\rho} (\omega_\theta - \omega_\xi)^2 G_{13}^{kj} - \frac{k}{\rho} B_3^{kj}$$

$$g_{5k+2, 5j+2} = \frac{G_1^{kj'}}{2} + \frac{\gamma}{2} G_1^{kj} + \frac{\lambda^2}{8} (\omega_\theta - \omega_\xi)^2 G_{13}^{kj'} - \frac{\lambda^2}{8} (\gamma (\omega_\theta - \omega_\xi)^2 + 2\omega'_\xi (\omega_\theta - \omega_\xi)) G_{13}^{kj}$$

$$g_{5k+2, 5j+4} = -\frac{\lambda^2 k}{4\rho} (\omega_\theta - \omega_\xi) G_{13}^{kj}$$

$$g_{5k+2, 5j+5} = + \frac{\lambda^2}{4} (\omega_\theta - \omega_\xi) G_{13}^{kj'} + \frac{\lambda^2}{4} (2\gamma (\omega_\xi - \omega_\theta) - \omega'_\xi) G_{13}^{kj}$$

$$g_{5k+3, 5j+1} = -\omega_\xi G_2^{kj} - \omega_\xi B_1^{kj} - \omega_\theta B_3^{kj}$$

$$g_{5k+3, 5j+3} = G_2^{kj'} + \gamma G_2^{kj}$$

$$g_{5k+3, 5j+4} = G_2^{kj}$$

$$g_{5k+4, 5j+1} = 0$$

$$g_{5k+4, 5j+2} = + \frac{\lambda^2 k}{4\rho} (\omega_\theta - \omega_\xi) G_{13}^{kj}$$

$$g_{5k+4, 5j+3} = -G_2^{kj}$$

$$g_{5k+4, 5j+4} = \lambda^2 D_1^{kj'} + \gamma \lambda^2 D_1^{kj}$$

$$\begin{aligned}
g_{5k+4, 5j+5} &= \lambda^2 \frac{k}{\rho} D_3^{kj} + \frac{\lambda^2}{2} \frac{k}{\rho} G_{13}^{kj} \\
g_{5k+5, 5j+1} &= \frac{\lambda^2}{2} \frac{k}{\rho} (\omega_\theta - \omega_\xi) G_1^{kj} \\
g_{5k+5, 5j+2} &= +\frac{\lambda^2}{4} (\omega_\theta - \omega_\xi) G_{13}^{kj'} + \frac{\lambda^2}{4} (2\gamma (\omega_\theta - \omega_\xi) - \omega'_\xi) G_{13}^{kj} \\
g_{5k+5, 5j+4} &= -\frac{\lambda^2}{2} \frac{k}{\rho} G_{13}^{kj} - \lambda^2 \frac{k}{\rho} D_3^{kj} \\
g_{5k+5, 5j+5} &= \frac{\lambda^2}{2} G_{13}^{kj'} + \frac{\lambda^2}{2} \gamma G_{13}^{kj} \\
h_{5k+1, 5j+1} &= \gamma B_3^{kj'} - \omega_\xi \omega_\theta B_3^{kj} - \gamma^2 B_2^{kj} - \frac{k^2}{2\rho^2} G_1^{kj} - \frac{\lambda^2}{8} \frac{k^2}{\rho^2} (\omega_\theta - \omega_\xi)^2 G_{13}^{kj} - \\
&\quad \omega_\xi^2 G_2^{kj} \\
h_{5k+1, 5j+2} &= \frac{k}{\rho} B_3^{kj'} - \frac{k}{\rho} B_2^{kj} - \frac{\gamma}{2} \frac{k}{\rho} G_1^{kj} - (\omega_\xi - \omega_\theta)^2 \frac{\gamma \lambda^2}{8} \frac{k}{\rho} G_{13}^{kj} \\
h_{5k+1, 5j+3} &= \omega_\xi B_1^{kj'} + \omega_\theta B_3^{kj'} + (\omega'_\xi + \gamma \omega_\xi) B_1^{kj} - \gamma \omega_\theta B_2^{kj} \\
h_{5k+1, 5j+4} &= +\omega_\xi G_2^{kj} + \frac{\lambda^2}{4} \frac{k^2}{\rho^2} (\omega_\theta - \omega_\xi) G_{13}^{kj} \\
h_{5k+1, 5j+5} &= +\frac{\lambda^2 \gamma}{4} \frac{k}{\rho} (\omega_\theta - \omega_\xi) G_{13}^{kj} \\
h_{5k+2, 5j+1} &= -\frac{k}{2\rho} G_1^{kj'} - \frac{\gamma k}{2\rho} G_1^{kj} - \frac{k}{\rho} \gamma B_2^{kj} + \frac{\lambda^2}{8} \frac{k}{\rho} (\omega_\theta - \omega_\xi)^2 G_{13}^{kj'} - \\
&\quad \frac{\lambda^2}{8} \frac{k}{\rho} (\omega_\theta - \omega_\xi) (3\gamma (\omega_\theta - \omega_\xi) - 2\omega'_\xi) G_{13}^{kj}
\end{aligned}$$

$$h_{5k+2, 5j+2} = \frac{1}{2} (\omega_\xi \omega_\theta - \gamma^2) G_1^{kj} - \frac{\gamma}{2} G_1^{kj'} - \frac{k^2}{\rho^2} B_2^{kj} - \omega_\theta^2 G_{13}^{kj} + \quad \checkmark$$

$$\frac{\lambda^2 \gamma}{8} (\omega_\theta - \omega_\xi)^2 G_{13}^{kj'} - \frac{\lambda^2}{8} ((\omega_\theta - \omega_\xi)^2 (\omega_\xi \omega_\theta + 3\gamma^2) -$$

$$(\omega_\xi - \omega_\theta) 2\gamma \omega'_\xi) G_{13}^{kj}$$

$$h_{5k+2, 5j+3} = -\frac{k}{\rho} \omega_\xi B_3^{kj} - \frac{k}{\rho} \omega_\theta B_2^{kj} - \omega_\theta \frac{k}{\rho} G_3^{kj}$$

$$h_{5k+2, 5j+4} = +\frac{\lambda^2 k}{4 \rho} \gamma (2(\omega_\theta - \omega_\xi) + \omega'_\xi) G_{13}^{kj} - \frac{\lambda^2}{4} \frac{k}{\rho} (\omega_\theta - \omega_\xi) G_{13}^{kj'}$$

$$h_{5k+2, 5j+5} = +\omega_\theta G_3^{kj} - \frac{\lambda^2 \gamma}{4} (\omega_\theta - \omega_\xi) G_{13}^{kj'} + \frac{\lambda^2}{4} (\omega_\theta - \omega_\xi) (\omega_\xi \omega_\theta + 2\gamma^2) G_{13}^{kj} +$$

$$\frac{\lambda^2 \gamma}{4} \omega'_\xi G_{13}^{kj}$$

$$h_{5k+3, 5j+1} = -(\omega'_\xi + \gamma \omega_\xi) G_2^{kj} - \omega_\xi \gamma B_3^{kj} - \omega_\theta \gamma B_2^{kj} - \omega_\xi G_2^{kj'}$$

$$h_{5k+3, 5j+2} = -\frac{k}{\rho} \omega_\xi B_3^{kj} - \frac{k}{\rho} \omega_\theta B_2^{kj} - \omega_\theta \frac{k}{\rho} G_3^{kj}$$

$$h_{5k+3, 5j+3} = -\frac{k^2}{\rho^2} G_3^{kj} - \omega_\xi^2 B_1^{kj} - 2\omega_\theta \omega_\xi B_3^{kj} - \omega_\theta^2 B_2^{kj}$$

$$h_{5k+3, 5j+4} = G_2^{kj'} + \gamma G_2^{kj}$$

$$h_{5k+3, 5j+5} = \frac{k}{\rho} G_3^{kj}$$

$$h_{5k+4, 5j+1} = +\frac{k^2}{4\rho^2} \lambda^2 (\omega_\theta - \omega_\xi) G_{13}^{kj} + \omega_\xi G_2^{kj}$$

$$h_{5k+4, 5j+2} = +\frac{\lambda^2 k}{4} \frac{k}{\rho} \gamma (\omega_\theta - \omega_\xi) G_{13}^{kj}$$



$$\begin{aligned}
h_{5k+4, 5j+3} &= 0 \\
h_{5k+4, 5j+4} &= -\lambda^2 \omega_\xi \omega_\theta D_3^{kj} + \lambda^2 \gamma D_3^{kj'} - \frac{\lambda^2 k^2}{2\rho^2} G_{13}^{kj} - \gamma^2 \lambda^2 D_2^{kj} - G_2^{kj} \\
h_{5k+4, 5j+5} &= \lambda^2 \frac{k}{\rho} D_3^{kj'} - \frac{\lambda^2 \gamma k}{2\rho} G_{13}^{kj} - \lambda^2 \gamma \frac{k}{\rho} D_2^{kj} \\
h_{5k+5, 5j+1} &= +\frac{\lambda^2 k}{4\rho} (\omega_\theta - \omega_\xi) G_{13}^{kj'} - \frac{\lambda^2 k}{4\rho} \omega'_\xi G_{13}^{kj} \\
h_{5k+5, 5j+2} &= +\frac{\lambda^2 \gamma}{4} (\omega_\theta - \omega_\xi) G_{13}^{kj'} - \frac{\lambda^2}{4} (\gamma \omega'_\xi + \omega_\xi \omega_\theta (\omega_\theta - \omega_\xi)) G_{13}^{kj} + \\
&\quad \omega_\theta G_3^{kj} \\
h_{5k+5, 5j+3} &= +\frac{k}{\rho} G_3^{kj} \\
h_{5k+5, 5j+4} &= -\frac{\lambda^2 k}{2\rho} G_{13}^{kj'} - \lambda^2 \frac{k}{\rho} \gamma D_2^{kj} - \frac{\lambda^2 k}{2\rho} \gamma G_{13}^{kj} \\
h_{5k+5, 5j+5} &= -\frac{\lambda^2 \gamma}{2} G_{13}^{kj'} - \lambda^2 \frac{k^2}{\rho^2} D_2^{kj} - G_3^{kj} + \frac{\lambda^2}{2} (\omega_\xi \omega_\theta - \gamma^2) G_{13}^{kj} \\
p_{5k+1} &= -p_\xi^k + t_{\xi T}^{k'} + \gamma (t_{\xi T}^k - t_{\theta T}^k) \\
p_{5k+2} &= -p_\theta^k - \frac{k}{\rho} t_{\theta T}^k \\
p_{5k+3} &= -p^k - \omega_\xi t_{\xi T}^k - \omega_\theta t_{\theta T}^k \\
p_{5k+4} &= \lambda^2 m_{\xi T}^{k'} + \lambda^2 \gamma m_{\xi T}^k - \lambda^2 \gamma m_{\theta T}^k \\
p_{5k+5} &= -\frac{k}{\rho} \lambda^2 m_{\theta T}^k
\end{aligned}$$

$$r_{5k+1, 5j+1} = B_1^{kj}$$

$$r_{5k+1, 5j+4} = 0$$

$$r_{5k+2, 5j+2} = \frac{1}{2} G_1^{kj} + \frac{\lambda^2}{8} (\omega_\theta - \omega_\xi)^2 G_{13}^{kj}$$

$$r_{5k+2, 5j+5} = + \frac{\lambda^2}{4} (\omega_\theta - \omega_\xi) G_{13}^{kj}$$

$$r_{5k+3, 5j+3} = G_2^{kj}$$

$$r_{5k+4, 5j+1} = 0$$

$$r_{5k+4, 5j+4} = D_1^{kj}$$

$$r_{5k+5, 5j+2} = + \left( \frac{\omega_\theta - \omega_\xi}{4} \right) G_{13}^{kj}$$

$$r_{5k+5, 5j+5} = \frac{1}{2} G_{13}^{kj}$$

$$s_{5k+1, 5j+1} = \gamma B_3^{kj}$$

$$s_{5k+1, 5j+2} = \frac{k}{\rho} B_3^{kj}$$

$$s_{5k+1, 5j+3} = \omega_\xi B_1^{kj} + \omega_\theta B_3^{kj}$$

$$s_{5k+1, 5j+4} = 0$$

$$s_{5k+1, 5j+5} = 0$$

$$s_{5k+2, 5j+1} = - \frac{k}{2\rho} G_1^{kj} + \frac{\lambda^2}{8} \frac{k}{\rho} (\omega_\theta - \omega_\xi)^2 G_{13}^{kj}$$

$$\begin{aligned}
s_{5k+2, 5j+2} &= -\frac{\gamma}{2} G_1^{kj} + \frac{\lambda^2}{8} \gamma (\omega_\theta - \omega_\xi)^2 G_{13}^{kj} \\
s_{5k+2, 5j+4} &= -\frac{\lambda^2 k}{4 \rho} (\omega_\theta - \omega_\xi) G_{13}^{kj} \\
s_{5k+2, 5j+5} &= -\frac{\gamma \lambda^2}{4} (\omega_\theta - \omega_\xi) G_{13}^{kj} \\
s_{5k+3, 5j+4} &= -\omega_\xi G_2^{kj} \\
s_{5k+3, 5j+4} &= G_2^{kj} \\
s_{5k+4, 5j+1} &= 0 \\
s_{5k+4, 5j+2} &= 0 \\
s_{5k+4, 5j+3} &= 0 \\
s_{5k+4, 5j+4} &= \gamma D_3^{kj} \\
s_{5k+4, 5j+5} &= \frac{k}{\rho} D_3^{kj} \\
s_{5k+5, 5j+1} &= +\frac{k}{4\rho} (\omega_\theta - \omega_\xi) G_{13}^{kj} \\
s_{5k+5, 5j+2} &= +\frac{\gamma}{4} (\omega_\theta - \omega_\xi) G_{13}^{kj} \\
s_{5k+5, 5j+4} &= -\frac{k}{2\rho} G_{13}^{kj} \\
s_{5k+5, 5j+5} &= -\frac{\gamma}{2} G_{13}^{kj}
\end{aligned}$$

$$a_{5k+1} = -t_{\xi T}^k$$

$$a_{5k+4} = -m_{\xi T}^k$$

All other  $r, s, a$  are equal to zero.

## 2.0 GENERAL DESCRIPTION OF COMPUTER PROGRAMS

### 2.1 INTRODUCTION

Both the Static and Dynamic analysis described in Section 1.0 are programmed for solution on the IBM 7094 digital computer using the IBM FORTRAN IV code. This section will give a general description of the two computer programs. The scope and limitations of the computer programs are outlined. The necessary quantities in selecting a mathematical model for the best utilization of the programs are described. The detailed description, the machine program, input instructions, flow diagram, sample data sheets, etc., are given in Section 3.0.

### 2.2 PROGRAM CAPABILITIES AND LIMITATIONS

Before describing some of the general program characteristics, it will perhaps be worthwhile to list some of the capabilities which are not generally present in other shell analysis programs. Also included in this list are limitations in the program that have resulted due to theoretical restrictions, computer storage capacity, economic considerations, etc.

- a. Shells having meridional and circumferential variation in the stiffness properties can be analyzed. The circumferential variation must have a property of symmetry about some plane,  $\theta = \text{constant}$  ( $\text{constant} = 0$ ).
- b. Static shells can be subjected to loads and temperatures which may vary meridionally and circumferentially with the limitation that these distributions must exhibit the same property of symmetry as the stiffness. The time dependent loadings for the dynamic response of shells must have the same conditions on the special distributions and also can vary arbitrarily in time.
- c. For static shells, elastic foundations can be considered. The distribution of these parameters are subject to the same condition of symmetry described for stiffness. For the dynamic response, both elastic foundations and external dampings are considered. These are also subject to the same symmetry conditions imposed on the stiffness parameters.

- d. Shells analyzed must have a surface of revolution reference surface. The middle surface of the shell has been taken as the reference surface for these computer programs, i. e., the section properties must be symmetric about the reference surface ( $\int E \zeta d\zeta = 0$ ).
- e. User compiled call functions are used in place of tables to input data of a 2 and 3 variable nature.
- f. As many as 100 spacial integration intervals can be considered.
- g. The Fourier expansions can be taken to 10 terms.

### 2.3 SIGN CONVENTIONS AND DIMENSIONS

The sign conventions used in the programs are illustrated in Figures (1.2, 1.3) in Section 1.0. To augment briefly the stresses  $\sigma_\xi$ ,  $\sigma_\theta$  and membrane forces  $N_\xi$ ,  $N_\theta$  are positive when they tend to produce tension and negative when they are in compression. The moments  $M_\xi$ ,  $M_\theta$  are positive in sign when they tend to produce tensile stresses in the inner surfaces and compressive stresses in the outer surface (see Section 2.4). The extensional displacement  $u$ , transverse deflection  $w$ , and meridional rotation  $\Phi_\xi$ , are positive when the  $\xi$  and  $\zeta$  coordinates are increased respectively.

In using the program, all data specified must be dimensionally consistent.

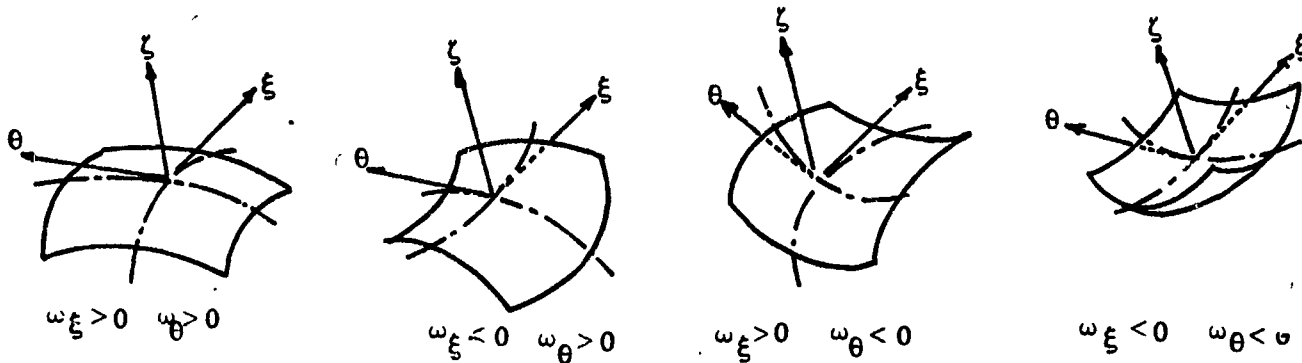
### 2.4 REFERENCE, INNER, AND OUTER SURFACES

The reference surface  $\zeta = 0$  is chosen such that the requirements of limitation (d) above be satisfied. The cross sectional properties are then evaluated based upon this reference surface. As discussed in 1.15, a substantial simplification is obtained when specifying key geometric functions (e. g.,  $\rho$ ,  $\gamma$ ), if the reference surface is chosen according to convenience anywhere within the shell wall. However, the shell stiffness parameter should be evaluated systematically along the lines discussed in Section 1.6 Eq. 1.17.

It will be convenient to refer to inner and outer surfaces of the shell. One can keep the inner and outer surface definitions clear by remembering that in direction of increasing value of  $\xi$  the outer surface is on the left and inner surface is on the right when the geometry is drawn with axial distance increasing from top to bottom and radial distance from left to right as shown in Figure 1.1.

## 2.5 GEOMETRY (GIN)

Geometric parameters must be defined at each station location. The sign convention for the curvature parameters,  $\omega_\xi$ ,  $\omega_\theta$  are defined in the figures below.



In order to assist the analyst in defining the set of geometry parameters with a minimum number of input parameters, several options for specific classes of geometries are made available. The options are described below with their identifying code number (GIN).

### 2.5.1 Cone-Cylinder Option (GIN) = 1.0

This geometry option may be specified for a complete range of regional configurations generated by a straight line, e. g., circular plates, divergent cones, cylinders and convergent cones. A minimum of 3 input parameters are required. The input parameters required are defined as follows:

1. RA1 - Radial distance from axis of revolution to the first station ( $i = 1$ ) of the region.
2. AXL - meridional length of shell.
3. ANX - angle the generator makes with the axis of revolution.

Figure 2.3 illustrates the geometric parameters used in describing the cone cylinder option.

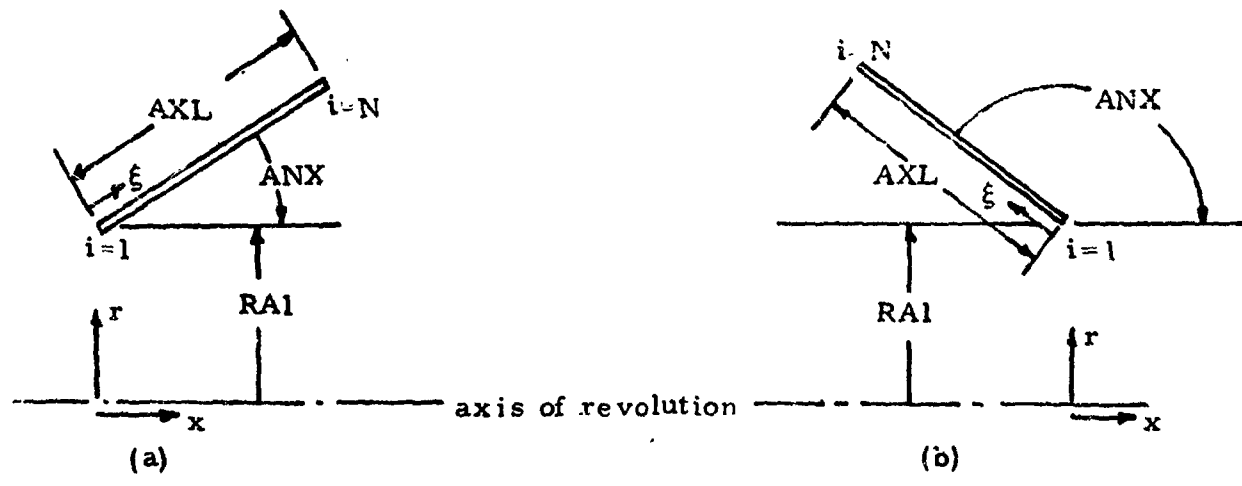


Figure 2.1 Cone Cylinder Geometry

Both RAI and AXL are positive quantities. The parameter ANX is given in degrees and is positive clockwise measured from the generator to the positive X axis as shown in Figure 2. 1.

2. 5. 2 Sphere-Toroid (GIN = 2. 0)

This option may be specified for a complete range of regional configuration generated by a circular curve. Four input parameters are necessary for defining a sphere-toroid as shown in Figure 2. 4.

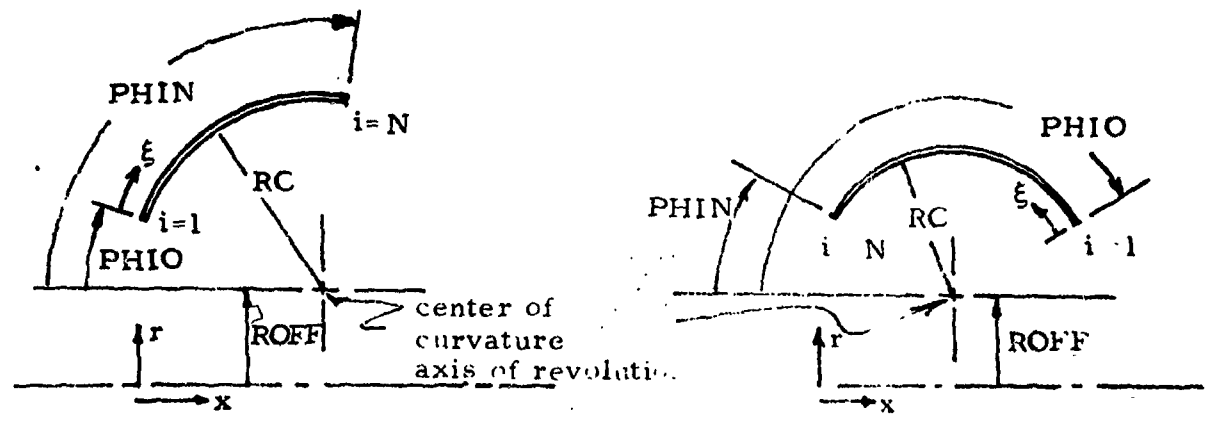


Figure 2.2 Sphere Toroid Geometry



The input parameters are:

1. RC - Radius of curvature of the generator
2. ROFF - Offset distance measured from axis of revolution to the center of meridional curvature.
3. PHIO - Angular position in degrees of the beginning of a region measured clockwise positive about the center of curvature from an axis parallel to the axis of revolution.
4. PHIN - Angular position of the end of the region.

#### 2.5.3 Discrete Point Option (GIN = ±4.0)

This option was developed for use on regions where the generator cannot be described by one of the other options or where a curved generator is given by a set of discrete points. As a consequence of various possible ways the geometry may be supplied to the analyst, several variations of input data format can be accommodated.

On a positive indicator (GIN = +4.0), the program will set up the necessary geometric parameter from the input data which describes the generator by discrete radial and axial distances. The input quantities to the program are EM (number of points given), RIPT (radial distance from axis of revolution at input points), XIPT (axial coordinates of the input points). The set of RIPT and XIPT must include the first and last points of the region. XIPT must be given in ascending magnitudes. On a negative indicator (GIN = -4.0), the coordinates of the discrete points are given in radial and surface or arc length, the surface length coordinate is input directly in the XIPT locations.

An interpolation routine is used to obtain appropriate geometric parameters at station points from the original input values. The parameters such as curvatures are computed using finite difference forms of the station set. A least squares method is used to minimize the scatter of these computations. To hold the errors in curvatures to less than 10 percent, the number of points described by RIPT and XIPT should be at least as great as the number of stations. For some situations such as locations of major changes in the generator curve, it will be necessary to input a denser population of RIPT and XIPT. (See Figure 2.3.) Because of the difficulty involved in the least squares and interpolation routines, extreme care must be exercised in the use of this option in order to obtain an adequate description of shell geometry. A significant improvement in results is obtained if the additional recommendations described are adhered to.

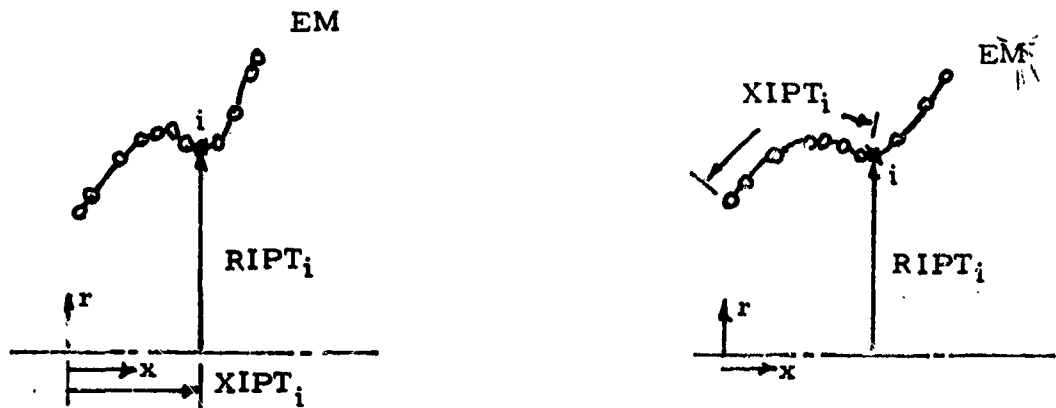


Figure 2.3

When the meridional and circumferential radii of curvatures are available, they can be input at discrete points and curve-fit to give a better description of the curvatures. If possible, it is strongly recommended that this capability be used since the errors in curvatures are reduced considerably to better control curvatures and less input points of the generator are required. This data is input in the location RCURV and RCURZ for radius of curvatures  $R_{\xi}$  and  $R_{\theta}$ , respectively (Section 1.3). RCURV and RCURZ values must correspond with the points described by RIPT and XIPT. This is an optional input to both  $GIN = +4.0$  and  $GIN = -4.0$ . When no values are input at RCURV and RCURZ locations, the curvatures will be computed from the discrete point set of RIPT and XIPT.

## 2.6 CALL FUNCTION PARAMETERS

Input data of a multivariable nature are defined to the computer programs by the use of call function subroutines. These parameters are described functional in terms of the meridional and circumferential variables (PEL, ZTA). The time variable (TU) is available for describing the loading history. Call function subroutines are to be coded and compiled by the user. Specific instructions for the coding of these subroutines are given in Section 3. Data that will be input in this manner are described in the following sections.

### 2.6.1 Stiffness Properties

The stiffness parameters are described in Section 1.6, Equations 1.16. It is sufficient to describe the inplane stiffness  $B_1$ , and the bending stiffness  $D_1$  and Poisson's ratio in order to define all the necessary parameters. The

function (BFCN, Static, DBBDD, Dynamics) will be written to define these parameters over the reference surface of the shell.

$$B_1 = B_1 (\xi, \theta)$$

$$D_1 = D_1 (\xi, \theta)$$

#### 2.6.2 Thermal Loads

The thermal load terms are described in Section 1.6, Equation 1.15. The call function (TFCN, Static, DTMP, Dynamics) will be written to define these parameters over the reference surface of the shell.

$$N_{\xi}^T = N_{\xi}^T (\xi, \theta)$$

$$M_{\xi}^T = M_{\xi}^T (\xi, \theta)$$

#### 2.6.3 Elastic Foundations

The elastic foundation parameters are defined in Section 1.6, Equation 1.6. For the static program these parameters will be defined in function subroutine KFCN. For the dynamic program these parameters will be defined in DKMP.

#### 2.6.4 External Damping

The external damping parameters are defined in Section 1.6, Equation 1.6. In the Dynamics program this function subroutine, DKMP will define both the elastic foundation terms and the external damping parameters.

#### 2.6.5 Mass Properties

The mass properties for the Dynamic program defined in Section 1.6, Equation 1.6 are defined to the computer program in the subroutine DMASS.

#### 2.6.6 Pressure Loads

The pressure loading for the static case is defined to the program in the subroutine PFCN. For the dynamic case the time dependent loading is defined to the computer program in the subroutine PRSS. Positive pressure yields positive displacement.

### 2.6.7 Parameters for Stresses

For the static program, the parameters necessary for the computation of stresses are defined to the computer program by the following subroutines, STR1FN, STR2FN, TTF1, TTF2. These subroutines define the following parameters:

STR1FN, for the first stress print layer, EI1, Young's Modulus, DN1, distance from the reference surface to the stress print locations and POIS1, Poisson's ratio.

STR2FN, these are parameters necessary for stresses at a second layer. The definitions of EI2, DN2, POIS2 correspond to the first stress print parameters.

TTF1, this subroutine defines the temperature TMP1 and thermal expansion coefficient ALF1 at the first stress print location.

TTF2, these parameters are for the second stress print and the TMP2, ALF2 have definitions corresponding to TTF1.

### 2.7 STATIONS IN REGIONS: (EN)

The machine program achieves a shell solution by integration of finite difference equations along the meridian or arc length distance of the shell. The number of integration points (called stations) located in the region under consideration is assigned the EN code value. The stations are equally spaced with the initial point located on the reference surface at the beginning of the region designated station 1 ( $i = 1$  or  $s = 0$ ) and the last or EN-th station at the end of the region called station N ( $i = N$  or  $s = \bar{s}$ ). The numbering of stations proceeds in direction of positive meridional coordinate assigned to the respective region. The maximum number of stations permissible in a region is 100 (minimum 5). The regional input data are specified at stations on the reference surface of each region.

The length of the finite difference "lump" of shell is computed internal to the program from the length or wrap distance and the number of stations (EN) in the region. This finite difference increment of integration is defined as DEL in the program and printout.

The machine running time increases with the number of integration steps considered per region. The type of shell problem considered should dictate the size of the grid mesh or number of stations considered. This comes with experience and how the results are to be used. As a general rule, it is recommended that more integration intervals be used where rapid change in variables occurs along the length of the shell.

### 3.0 DETAILED USE OF PROGRAMS

#### 3.1 INTRODUCTION

The Unsymmetric Shell Computer Program is written in the FORTRAN IV language and makes use of the overlay feature and the ALTIO option of that language. ALTIO sacrifices speed of execution in favor of providing an additional 1900 core locations. (It does not make use of buffered input-output.) If the programs are to be compiled for use without the ALTIO option it will be necessary to add an additional BACKSPACE command at each location where the backspace moved the tape over an END OF FILE. These have been noted in the listings.

The program has been checked out in NAASYS, the NAA adaption of the IBM 7090/7094 IBSYS/IBJOB system and used the NAASYS library routines shown in the load map, Section 3.12m.

The NAASYS input tape is 'UNIT05'; the output tape is 'UNIT06'. In addition to these files, the program uses units 3, 7, 8, 9, 10, 11, 12 and 13 as scratch tapes or for overlay storage during execution. NAASYS itself, is stored on 'UNIT01'.

The program is made up of an executive program and eleven links, four of which are called by the executive program, three by the DATLNK subroutine and four by the PANDX subroutine. The name of the main program in each link and a description of its use, follows.

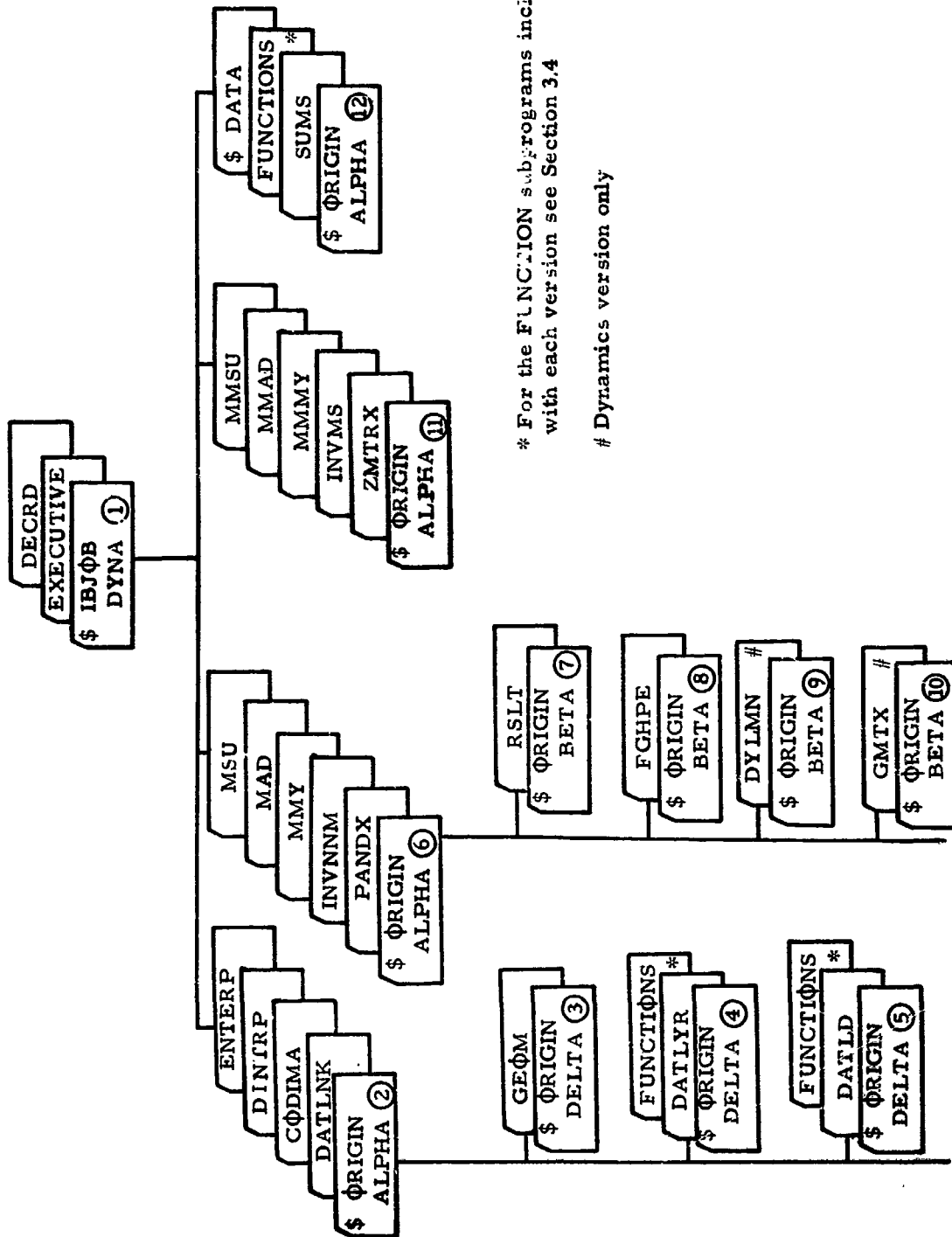
Link No.	Name	Purpose
0	Executive	Reads the title cards and general data; sets up tape numbers and rewinds all tapes; controls the flow of execution of other links.
1	DATLNK	Acts as a sub-executive program to control GEOM, DATLYR and DATLD so that these three subroutines may share common auxiliary routines CODIMA, ENTERP and DINTRP.
2	GEOM	Reads geometry parameters, GMDA. Sets up top and bottom boundary matrices. Calculates DEL, R, XSI, WTIX, WFEX, GAMA, RHIOX, WFEPX and stores the latter 5 arrays on tape. Prints general data, boundary matrices and pertinent geometry data on indicator.

Link No.	Name	Purpose
3	DATLYR	Sets up stiffness and temperature coefficients by function subprograms. These are stored on tape.
4	DATLD	This is the Fourier Load coefficients generator. Pressures, PFE, PTH and PN are supplied by function subprograms. These coefficients are preserved on tape.
5	PANDX	A sub-executive program which, together with the subroutines it controls--RSLT, FGHPE, DYLMN, GMTX--generates the recursion terms and the 'P' and 'X' matrices of equations 1.60 Section 1.10.
6	RSLT	Sets up the boundary matrices needed in computing 'P' and 'X' at the top and bottom of the shell. (See Section 1.10.)
7	FGHPE	Sets up the F, G, and H matrices in equilibrium equations 1.34 of Section 1.7.
8	DYLMN*	Sets up the L, M, and N matrices for the dynamic response equations of Section 1.9. These are written on tape 13.
9	GMTX*	Forms the PE matrix of equation 1.34 of Section 1.7. Computes 'G**', 'B**', 'P' and 'X' matrices.
10	ZMTRX	Computes 'Z', the solution matrix.
11	SUMS	Sums the Fourier components and computes internal loads, i.e., bending moments, transverse shear forces, and membrane forces. (In the static version, stresses may also be computed in this link with the parameters defined by function subprograms.)

\*Dynamics version only

### 3.2 DECK SET-UP

In Figure 3A of this section we have shown the set-up of the column-binary program deck with the necessary control cards for each link. A list of the deck names corresponding to the subprogram names is given in the table at the end of the section.



\* For the FUNCTION subprograms included with each version see Section 3.4

# Dynamics version only

Figure 3A.

TABLE OF SUBROUTINE NAMES AND DECK NAMES

Subroutine Name	Static Deck	Dynamics Deck
DATLNK	DLNK	DLKDY
GEOM	GMTRY	GMVD
DATLYR	STIFF	STFDY
DATLD	LOAD	LLDY
PANDX	PEANDX	PXDYN
RSLT	BNDRY	BNDD
FGHPE	FGMTX	FGHDY
DYLMN		LMNDY
GMTX		GDYN
ZMTRX	SOLTN	SLND
SUMS	SUSM	SUMD



The \$IBJOB, \$ORIGIN and \$DATA cards are single control cards. The circled number found on the first two mentioned control cards, indicate the order in which they, plus the associated decks of that link, should be stacked. For example, those second level subroutines preceded by a \$ORIGIN DELTA card - GEOM, DATLYR and DATLD will be found in the deck before the first level subroutine, PANDX, because they are executed in this order.

It is imperative that the utility subroutines be kept with each deck as shown. Since only one link of the same level may occupy core at a given time, the utility subprograms CODIMA, ENTERP and DINTRP are stored with the DATLNK link so that they may be shared by GEOM, DATLYR and DATLD.

Additional control cards preceding the \$IBJOB card are likely to vary somewhat with the installation. An IBM systems handbook should be consulted. The cards used at Space and Information Systems Division are shown in Figure 3B, below.

```
9 020020 0 $JOB   IBJOB   055705055945 32 192120BB04702FURU IKE
9 020021 0 $IBJOB PLASTIC
9 020323 0 $IBSYS
```

Figure 3B

### 3.3 DATA DECK SET-UP

Data decks should be stacked as follows:

1. Three cards (72 columns each) of title data.
2. GDA, general shell data, read by the EXECUTIVE program.
3. GMDA, geometry data, read by the GEOM subroutine.

All other parameters such as stiffnesses, springs, damping, mass, temperature and pressure loadings, and section properties used in stress computations are defined by function subprograms. These subprograms will be written by the user and compiled for each particular run. A discussion of how to write the various function subprograms is found in Section 3.4.

With the exception of the three title cards, each group of data listed above should have a minus sign in column 1 of the last card, since this data is read by the DECRD subroutine. See Section 3.5.1. In the instructions below, the DECRD index of each input quantity is given.

### 3.3.1 Title Cards

Three title cards form the first three cards of any data deck for each case. These cards are useful in identifying the run at a later date. They may include a brief problem description, the date of the run, a reference, etc.

These cards may not be omitted, but they may be blank, if desired. If the cards are forgotten, the error indication from DECRD may occur for a multiple case run in which title cards are present for the second case, or the job may terminate with an EXECUTION ENDED designation (as explained in Section 3.5.1). A more serious situation occurs when the data from subsequent subroutines are read out of turn and the program is placed in an endless loop.

### 3.3.2 GDA, General Shell Data

All input data must be dimensionally consistent. It should be noted that all nondimensionalization is done internal to the program, thus all inputs must be supplied with appropriate dimensions (e.g., transverse load PN is input with dimensions  $P/L^2$ ).

DECRD Index	Name	Description and Comments
1	A0	Reference length (a)
2	H0	Reference thickness ( $h_0$ )
3	E0	Reference Young's modulus ( $E_0$ )
4	SIG0	Reference stress ( $\sigma_0$ )
5	P0I	Poisson's ratio ( $\nu$ )
6	ENF	The number of Fourier components (10 maximum)

DECRD Index	Name	Description and Comments
7	BCIT	<p>Boundary condition indicator at first station.</p> <ul style="list-style-type: none"> <li>= 1. closed apex</li> <li>= 2. pinned</li> <li>= 3. clamped</li> <li>= 4. free</li> <li>= 5. roller w</li> <li>= 6. roller u</li> <li>= 10. special boundary matrices read in with geometry data. Must use 10 whenever non-zero values are prescribed in boundary matrices <math>l_0</math> or <math>l_n</math>.</li> </ul>
8	BCIB	<p>Boundary condition indicator at last station. (As BCIT)</p>
9	PFLAG	<p>Print indicator for input data.</p> <ul style="list-style-type: none"> <li>= 0. prints general data and boundary matrices</li> <li>= 1. prints above information and input data for the particular geometry configuration selected by GIN and the computed values for <math>r</math>, <math>x</math>, <math>\omega_\theta</math>, <math>\omega_\phi</math>, <math>\rho</math> and <math>\gamma</math>.</li> <li>= -1. prints all of above information and stiffness coefficients, elastic coefficients, thermal load and moment and pressure loads.</li> </ul>
10	CEXT	Number of time cycles
11	DELT	Time increment in seconds

DECRD Index	Name	Description and Comments
12	THT	Circumferential angle $\theta$ (degrees). Five values of THETA may be chosen. The deflections, rotations, internal loads and stresses will be printed at these values.
18	FPRNT	Fourier component print values. Three prints are permitted. Two intermediate prints of the Fourier summing are possible for checking convergence. The last FPRNT value given should be the same as the value given for ENF in the general data, i. e., GDA (6).

Note: If THT and FPRNT are not entered, the program will set THT (1) = 0.0 and FPRNT (1) = ENF.

The last card of GDA data should have a minus (-) in column 1.

### 3.3.3 GMDA, Geometry Data

The GMDA data array is zeroed before the data is read. This means that any data with a value = 0. need not be entered.

DECRD Index	Name	Description and Comments
1	GIN	Geometry indicator = 1. cone-cylinder = 2. sphere-toroid = ±4. discrete points
2	EN	Number of meridional stations (100 maximum)
3	ENLAY	Number of layers
4	RA1	Radial distance from axis of revolution to station 1. (L)*

When GIN = 1.0; see Section 2.5.1

\*L - unit of length

DECRD Index	Name	Description and Comments
5	AXL	Meridional length of shell (L)
6	ANY	Angle the generator makes with the axis of revolution (degrees)

When GIN = 2.0; see Section 2.5.2

4	RC	Radius of curvature of the generator (L)
5	RØFF	Offset distance measured from axis of revolution to center of meridional curvature (L)
6	PHI0	Initial opening angle from the vertical axis (degrees)
7	PHIN	Final opening angle from the vertical axis (degrees)

When GIN = 4.0; see Section 2.5.3

8	EM	Number of RIPT's given (12 minimum, 100 maximum)
9	RIPT	Discrete radial distances
109	XIPT	Discrete axial or vertical distances (or arc lengths)
209	RCURV	Meridional radii of curvature
309	RCURZ	Circumferential radii of curvature

Boundary matrices, when not set by indicator: only the elements which might possibly be non-zero are included in the arrays. The explanation below assumes the user is familiar with Section 2.8, Boundary Conditions.

409	BNDTX (1) = $\Omega(1,1)$	Elements of force boundary matrix ( $\Omega_0$ ) at station 1
410	$\Omega(1,2)$	
411	$\Omega(2,2)$	
412	$\Omega(3,3)$	

DECRD Index	Name	Description and Comments
413	$\Omega(4, 4)$	
414	$\Omega(5, 4)$	
415	$\Omega(5, 5)$	
416	BNDTX (8) = $\Lambda(1, 1)$	Elements of displacement boundary matrix ( $\Lambda_0$ ) at station 1
417	$\Lambda(2, 2)$	
418	$\Lambda(3, 3)$	
419	$\Lambda(4, 4)$	
420	$\Lambda(5, 5)$	
421	BNDTX (13) = $\ell_1$	Column boundary matrix ( $\ell$ ) at station 1. The five elements are in consecutive locations.
426	BNDTB (1) = $\Omega(1, 1)$	Elements of force boundary matrix ( $\Omega_N$ ) at station N, stored in the same manner as $\Omega_0$ above.
433	BNDTB (8) = $\Lambda(1, 1)$	Elements of displacement boundary matrix ( $\Lambda_N$ ) at station N; diagonal elements only.
438	BNDTB (13) = $\ell_1$	Matrix ( $\ell$ ) for the last station

The last card of GMDA data should have a minus (-) in column 1.

### 3.4 FUNCTIONAL SUBPROGRAMS

The FUNCTION subprogram is an independently written and compiled program that is executed wherever its name appears in an arithmetic statement in another routine. The object (binary) or source (FORTRAN) deck must be included in the job deck even though the FUNCTION value equals zero; otherwise, the program that references the FUNCTION will not be executed.

## "REPRODUCIBILITY OF THE ORIGINAL PAGE IS POOR;"

Since a FUNCTION is a separately compiled subprogram, the variables and statement numbers within it do not relate to any other component of the program. Communication between the FUNCTION and its calling program takes place at execution time. The value of the FUNCTION is always returned to the calling program; values may also be returned via the FUNCTION arguments and/or variables assigned to a common region.

### General Form:

```
FUNCTION      name (a, b, ... n)
.
.
.
name = ...
.
.
.
RETURN
.
.
.
END
```

Name is a subprogram name (1-6 alphanumeric characters, the first of which is alphabetic). FUNCTION names used in this program are listed at the end of this section.

a, b, --n are unsubscripted variable or array names used to transfer values between the FUNCTION subprogram and the program that references it. There must be at least one argument.

### Basic Description:

The FUNCTION statement must be the first statement in the subprogram definition. (Comments cards excluded.) The name must not be the same as a library or built-in function unless the name is included in an EXTERNAL statement which precedes the first use of the FUNCTION by the calling program.

The FUNCTION subprogram may contain any FORTRAN statement except another FUNCTION statement, a SUBROUTINE statement, or a BLOCK DATA subprogram.

A variable in a COMMON block may be referenced if the rules for use of COMMON are followed.

## "REPRODUCIBILITY OF THE ORIGINAL PAGE IS POOR."

The name of the FUNCTION must be assigned a value at least once within the subprogram. This value may be assigned by the appearance of the function name on the left side of an arithmetic statement (e. g. SOMEF = X/Y), or by its appearance in the list of a READ statement within the subprogram.

### Arguments:

The relationship between variable names used as arguments in the calling program and the variables used as arguments in the FUNCTION subprogram is illustrated in the following example.

#### Calling Program

```
.  
.   
.   
A = SOMEF (B, C)   
.   
.   
.
```

#### Subprogram

```
FUNCTION SOMEF (X, Y)   
50 SOMEF = X/Y   
55 RETURN   
END
```

The value of the variable B of the calling program will be used as the value of the subprogram variable X; and C for Y. Thus, if B = 10.0 and C = 5.0, then A = 2.0.

The arguments used in the unsymmetrical shell of revolution program are PEL, ZTA and TU, where PEL is the meridional distance to a station, ZTA is the circumferential distance and TU is the elapsed time. If additional values are necessary to define a FUNCTION it will be necessary to include a READ statement in the subprogram and to supply the required data cards to satisfy the READ at execution time.

### RETURN and END Statements:

A FUNCTION subprogram must contain an END statement and at least one RETURN statement. The END statement specifies the physical end of the subprogram for the compiler. The RETURN statement signifies a logical conclusion of the computation and returns any computed value and control to the calling program.



## Multiple Entries:

The normal entry into a FUNCTION subprogram is made by a function reference in an arithmetic expression. Entry is made at the first executable statement following the FUNCTION statement. It is also possible to enter a FUNCTION by means of a reference to an ENTRY statement in the FUNCTION.

### General Form

ENTRY     name (a, b, ... n)

name is the name of an entry point. It must follow all the rules given for the FUNCTION name.

a, b, ... n are the dummy arguments corresponding to actual arguments supplied by a function reference.

The ENTRY statement is not executable. When inserted in a series of statements, the ENTRY statement has no effect on the logical flow of the subprogram. Entry to the subprogram is made at the first executable statement following the ENTRY statement, so it is easy to start using a subprogram at any desired point.

Within a FUNCTION subprogram, only the FUNCTION name may be used as the variable to carry a result back to the calling program. The ENTRY name may not be used for this purpose. The following example illustrates this rule.

### Calling Program

```
.  
.   
.   
A = ONEF (B, C)   
.   
.   
F = TWOF (D, E)   
.   
.   
.
```

### Subprogram

```
FUNCTION ONEF (X, Y)   
5 ONEF = X * Y   
10 RETURN
```

```

      ENTRY TWOF (X, Y)
  → ONEF = X + Y
20 RETURN
   END

```

Note the use of the primary function name to return the function value to the calling program, even when the reference was to an ENTRY name.

Additional examples showing the use of FUNCTION subprograms with multiple ENTRY statements may be found in Sections 3.6, 3.7, 3.8 and 3.9.

Following is a table which gives the FUNCTION names, ENTRY names, calling program names and the assigned deck names (\$IBFTC manes) for the static and dynamic versions of the Unsymmetrical Shell of Revolution Program. For their definitions see Program Nomenclature, Section 3.13.

	STATIC	DYNAMIC
Calling Program DATLYR		
FUNCTION BBB (PEL, ZTA) ENTRY DDD (ZTA)	BFCN	DBBDD
FUNCTION ENTT (PEL, ZTA) ENTRY EMTT (PEL, ZTA)	TFCN	DTMP
FUNCTION *DKK1 (PEL, ZTA) ENTRY *DKK2 (PEL, ZTA) ENTRY DKK3 (PEL, ZTA) ENTRY DMP1 (PEL, ZTA) ENTRY DMP2 (PEL, ZTA) ENTRY DMP3 (PEL, ZTA)	KFCN	DKDMP
FUNCTION DMM1 (PEL, ZTA) ENTRY DMM4 (PEL, ZTA)		
Calling Program DATLD		
FUNCTION PPPN (PEL, ZTA) ENTRY PPPH (PEL, ZTA) ENTRY PPPF (PEL, ZTA)	PFCN	

\*Deleted in the static deck because of core storage problems, therefore DKK3 becomes the FUNCTION name.

	STATIC	DYNAMIC
FUNCTION PPPN (PEL, ZTA, TU)		
ENTRY PPPH (PEL, ZTA, TU)		DPRSS
ENTRY PPPF (PEL, ZTA, TU)		

Calling Program SUMS

FUNCTION EI1 (PEL, ZTA)	
ENTRY DN1 (PEL, ZTA)	STR1FN
ENTRY POIS1 (PEL, ZTA)	
FUNCTION EI2 (PEL, ZTA)	
ENTRY DN2 (PEL, ZTA)	STR2FN
ENTRY POIS2 (PEL, ZTA)	
FUNCTION TMP1 (PEL, ZTA)	
ENTRY ALF1 (PEL, ZTA)	TTF1
FUNCTION TMP2 (PEL, ZTA)	
ENTRY ALF2 (PEL, ZTA)	TTF2

### 3.5 UTILITY SUBROUTINES

#### 3.5.1 DECRD Subroutine

All data, with the exception of the three title cards, is read by means of the DECRD subroutine, included with the symbolic decks.

This routine provides the facility for reading a variable number of pieces of floating point data into specified elements of an array; these elements may be either in sequential or in nonconsecutive locations. Only the information specified is actually read into storage.

		16	
4.6			
0.			
1.	+ 17		
3.3	- 2		24

The fixed point number (index) in the first field on each card defines the position of the first piece of data on the card. If the index is 1, the first piece of data will be stored in the first location reserved for the array; if it is 16, the first word will be placed in the 16th position, etc. The remaining fields on each card contain information for the successive locations of the array. If one or more fields are left blank, no information is read into the locations corresponding to these fields; the information already in these locations is unaltered.

The sample data sheets shown in Section 3.6.2 have 6 fields of 12 card columns each, and an identification field of 8 columns for sorting purposes.

- a. The index must be written to the extreme right of the first field; it may not be zero or blank. (No decimal point)
- b. The programmer should keep in mind the way in which FORTRAN stores arrays having double or triple subscripts, e. g., A(1, 1), A(2, 1), A(3, 1), A(1, 2), A(2, 2), etc.
- c. The floating point (REAL) data should be entered with a decimal point (anywhere in the field) and an exponent, when necessary, written to the extreme right of the field and preceded by a '+' or '-'.
- d. Reading data is concluded by placing a negative sign in column 1 of the last card to be read.
- e. Zero should always be entered as '0.'. A'-0.' or '.0' will be recognized as a blank.

ERROR indication: If the index is zero or blank, the comment "\*\*\*\*BAD INDEX ON DECRD CARD=" will be printed, followed by a print-out of the columns 1-80 of the defective card. The job will be terminated.

If the data for the array in the CALL statement has been completely read, and no negative sign has been encountered in column 1 of the last card sent, data intended for subsequent CALL's will be read into the incorrect array. When there are no data cards to satisfy the appetite of a CALL DECRD statement, the job will terminate with an EXECUTION ENDED designation.

If this occurs before all expected results have been printed, check the last card of each data block for the negative sign in column 1.

In order to use the DECRD routine in conjunction with the ALTIO option, it is necessary to physically load a copy of the routine with the program deck. ALTIO will not cause the proper adjustments to DECRD from the library tape at load time, so drop-in decks must be used.

"REPRODUCIBILITY OF THE ORIGINAL PAGE IS POOR;"

DECRD000  
DECRD005  
DECRD010  
DECRD015  
DECRD020  
DECRD025  
DECRD030  
DECRD035  
DECRD040  
DECRD045  
DECRD050  
DECRD055  
DECRD060  
DECRD065  
DECRD070  
DECRD075  
DECRD080  
DECRD085  
DECRD090

```
$IRFIC DECRD
SURROUTINE DECRD(D)
DIMENSION FLT(5), ID(2), D(1)
10 READ (5,100) LOC, FLT, ID
100 FORMAT (I12, 5F12.0, 1A6, 1A2)
IF (LOC.EQ. 0) GO TO 500
15 K = IABS(LOC) - 1
DO 20 I = 1,5
IF (SIGN(1.0,FLT(I)).LT.0.0 .AND. FLT(I) .EQ. 0.0) GO TO 20
J = K + I
D(J) = FLT(I)
20 CONTINUE
IF (LOC.LT. 0) GO TO 1000
GO TO 10
500 WRITE (6,200) ID
200 FORMAT(10HORAD DATA 1A6,1A2)
1000 CALL EXIT
RETURN
END
```

### 3.5.2 MAD, MSU, MMY, INVMS

These four subroutines perform matrix addition, subtraction, multiplication and inversion, respectively. They are extremely simple in their approach and must be recompiled to change dimensions for use in other decks. There are no error indications given in the 1st three routines other than the usual NAASYS trapping information for underflows, overflows and divide checks. When data has been entered correctly, these subroutines will present no problems.

The inversion routine has an error indicator, IX, which is set at 0 or -1 for a singular matrix. This is returned to the calling program through the argument list and may be tested after return. The Unsymmetrical Shell of Revolution Program makes such a test, prints the comment "SINGULAR MATRIX I = XX" and terminates the job. When this error occurs, check the data—especially any special boundary matrices entered, and the FUNCTION subprograms.

The Dynamics version of the program uses a MAP (machine language coded) copy of the INVMS subroutine. The FORTRAN language routine causes the GDYN link to exceed core storage. Listings for both versions are included.

```

$TRFC MADD
C MATRIX ADD SUBROUTINE
C
C ARGUMENTS
C L NO. OF ROWS
C M NO. OF COLS
C A(I,J) MRA
C B(I,J) MAD
C C(I,J) MSR
C SUBROUTINE MAD(L,M,A,R,C)
C DIMENSION A(50,50), R(50,50), C( ,50)
C DO 30 I=1,L
C DO 30 J=1,M
C C(I,J)=A(I,J)+R(I,J)
C RETURN
C END

```

DECK NO. 8K-903

```

00000400
00000410
00000420
00000430
00000440
00000450
00000460
00000470
00000480
00000490
00000500
00000510
00000520
00000530

```

"REPRODUCIBILITY OF THE ORIGINAL PAGE IS POOR"

DECK NO. 8K-904  
00000400  
00000410  
00000420  
00000430  
00000440  
00000450  
00000460  
00000470  
00000480  
00000490  
00000500  
00000510  
00000520  
00000530

```
$IBFTC MSUB  
C MATRIX SURTRACT SUBROUTINE  
C  
C ARGUMENTS  
C L NO. OF ROWS  
C M. NO. OF COLS  
C A(I,J) MRA  
C B(I,J) MSU  
C C(I,J) MSR  
C SUBROUTINE MSU(L,M,A,B,C)  
C DIMENSION A(50,50), B(50,50), C(50,50)  
C DO 30 I=1,L  
C DO 30 J=1,M  
C 30 C(I,J)=A(I,J)-B(I,J)  
C RETURN  
C END
```



```

C $I,ETC MMDY
C MATRIX MULTIPLY SUBROUTINE
C ARGUMENTS
C L NO. OF ROWS X MATRIX
C M NO. OF COLS X MATRIX
C N NO. OF COLS Y MATRIX
C X(I,K) MRA
C Y(K,J) NMY
C Z(I,J) MSP
C SUBROUTINE MMY(L,M,N,X,Y,Z)
C DIMENSION X(50,50), Y(50,50), Z(50,50)
C DO 30 I=1,L
C DO 30 J=1,N
C Z(I,J)=0.0
C DO 30 K=1,M
C Z(I,J)=Z(I,J)+X(I,K)*Y(K,J)
C RETURN
C END

```

DECK NO. 8K-901

```

0000010
0000020
0000030
0000040
0000050
0000060
0000070
0000080
0000090
0000100
0000110
0000120
0000130
0000140
0000150
0000160
0000170

```

```

INVS0000
C *** 7094 FORTRAN IV SINGLE PRECISION GENERAL DIMENSION FIND INVERSE INVS0001
C OF MATRIX USING SINGLE PRECISION OPERATIONS INVS0002
C INVS0003
C ARGUMENTS INVS0004
C A ORIGINAL MATRIX DIMENSIONED N X N INVS0005
C N ROW DIMENSION OF A AND AI AS GIVEN BY DIMENSION STATEMENT INVS0006
C M1 NUMBER OF ROWS USED BY A AND AI M1 MUST BE LESS THAN OR EQUAL TO N INVS0007
C IX ERROR INDICATOR INVS0008
C D WORKING ARRAY MUST BE SINGLE PRECISION AND DIMENSIONED M1 X M1 INVS0009
C INVS0010
C SUBROUTINE INVMS (A,N,M1,IX,D,AI) INVS0011
C INVS0012
C DIMENSION A(N,1), D(M1,1), IKOL(50), AI(N) INVS0020
C REAL MULT INVS0030
C EQUIVALENCE (I1,I4,I7 ), (I2,I5,J,K), (I3,L), INVS0040
C 1 (PROD,MULT,AMX) INVS0050
C INVS0059
C M = M1 INVS0060
C DO 3 I=1,M INVS0070
C DO 3 J=1,M INVS0080
C D(I,J) = A(I,J) INVS0090
C DO 1000 I=1,M INVS0099
C I1 = I INVS0100
C DO 5 J=1,M INVS0110
C AI(J) = ARS(D(I,J)) INVS0120
C IF (I1 - 1) 6,11,6 INVS0130
C DO 10 I2=2,I1 INVS0140
C I3 = IKOL(I2-1) INVS0150
C AI(I3) = 0. INVS0160
C INVS0170
C 10 CONTINUE INVS0180
C AMX = AI(1) INVS0190
C I4 = 1 INVS0200
C DO 15 I5=2,M INVS0210
C IF(AI(I5) .LE. AMX) GO TO 15 INVS0220
C AMX = AI(I5) INVS0230
C I4 = I5 INVS0240
C CONTINUE INVS0250
C IKOL(I) = I4 INVS0260
C PROD = D(I,I4) INVS0270
C AT = 1. INVS0280
C IF (AI(I4) .EQ. 0.) GO TO 17 INVS0290

```

```

17 AT = ABS(PROD / A(I,I4))
   IF (I.EQ.1) AMN = 1.
   AMN = AMINI (AT,AMN)
   D(I,I4) = 1.
   IF (PROD) 20,2000,20
   DO 30 K=1,M
   D(I,K) = D(I,K) / PROD
   DO 40 L=1,M
   IF (L.EQ.1) GO TO 40
   MULT = D(L,I4)
   D(L,I4) = 0.
   DO 35 K=1,M
   D(L,K) = D(L,K) - MULT * D(I,K)
35 CONTINUE
40 CONTINUE
1000 C
DO 1015 I=1,M
17 = IKOL(I)
DO 1010 J=1,M
18 = IKOL(J)
1010 A(I7,J) = D(I,I8)
1015 CONTINUE
C
IX = 1
AMN = ALOG10 (1./AMN)
IF (AMN.GT.6.) IX = -1
1030 D(1,1) = AMN
2000 RETURN
   IX = 0
   GO TO 1030
   END

```

```

INVS0300
INVS0310
INVS0320
INVS0330
INVS0340
INVS0350
INVS0360
INVS0370
INVS0380
INVS0390
INVS0400
INVS0410
INVS0420
INVS0430
INVS0440
INVS0449
INVS0450
INVS0460
INVS0470
INVS0480
INVS0490
INVS0500
INVS0509
INVS0510
INVS0520
INVS0530
INVS0540
INVS0550
INVS0560
INVS0570
INVS0580

```

\$IBMAP	INVMS	INVMS*	307I0000
LNVS	LRL	5,4	307I0010
	CLA*	EX1,1	307I0020
	SXA	EX2,2	307I0030
	SXA	EX3,3	307I0040
	SXA		307I0050
	STA	N1	307I0060
	STA	N3	307I0070
	STA	N4	307I0080
	STA	N6	307I0090
	STA	N7	307I0100
	STA	N10	307I0110
	STA	N13	307I0120
	STA	N14	307I0130
	STA	FIN	307I0140
	PAC	1	307I0150
	SCD	N12,1	307I0160
	SXD	MN,1	307I0170
	ADD	ROWTA	307I0180
	STA	51	307I0190
	STA	R2	307I0200
	STA	R3	307I0210
	STA	R4	307I0220
	CLA*	4,4	307I0230
	STO	N	307I0240
	PAX	1	307I0250
	SXD	N2,1	307I0260
	SXD	N5,1	307I0270
	SXD	N8,1	307I0280
	SXD	N9,1	307I0290
	SXD	N11,1	307I0300
	LDQ*	5,4	307I0310
	MPY	N	307I0320
	XCA		307I0330
	SUB		307I0340
	SUB	=1	307I0350
	ADD	3,4	307I0360
	STA	MX1	307I0370
	STA	MX2	307I0380
	STA	MX3	307I0390
	STA	MX4	307I0400
	STA	MX5	307I0410
	STA	MX6	307I0420

(MX+N\*2-N-1)

114

SEARCH	3,4	30710430
CLA	H+1	30710440
STA	=1	30710450
SUB	ST1	30710460
STA	1,2	30710470
AXC	X1,2	30710480
SXD	S2,2	30710490
SXD	ROWNI+1,2	30710500
TXI	**1,2,-1	30710510
SXD	ROWNI+2,2	30710520
TXI	**1,2,1	30710530
AXT	**3	30710540
CLA	**2	30710550
SLW	**3	30710560
TXI	**1,2,**	30710570
TIX	MX1,3,1	30710580
AXC	1,3	30710590
TXH	**2,3,** (-M-1)	30710600
TRA	N3	30710610
CLA	COLNOS-1,3	30710620
PAX	*2	30710630
STZ	**2	30710640
TIX	X1,3,1	30710650
AXT	**3	30710660
SXA	J,3	30710670
CLA	**3	30710680
TIX	R4,3,1	30710690
TRA	X5	30710700
CAS	**3	30710710
TRA	X3	30710720
TRA	X3	30710730
SXA	J,3	30710740
TRA	R3	30710750
LXD	X1,3	30710760
TXI	**1,3,-1	30710770
SXD	X1,3	30710780
CLA	J	30710790
STO	COLNOS-2,3	30710800
AXT	**2	30710810
LDQ	J	30710820
MPY	N	30710830
XCA	N	30710840
SUB	N	30710850

SUB	=1	30710860
ADD	3,4	30710870
STA	J1	30710880
STA	J2	30710890
STA	J3	30710900
STA	J4	30710910
CLA	**2	30710920
TZE	SING	30710930
STO	PROD	30710940
CLA	=1	30710950
STO	**2	30710960
AXT	**3	30710970
NULL		30710980
CLA	**2	30710990
FDP	PROD	30711000
NULL		30711010
STQ	**2	30711020
TXI	**1,2,**	30711030
TIX	ROWI,3,1	30711040
AXC	**1	30711050
SXA	S1,1	30711060
TXH	**2,1,**	30711070
TXH	S1+1,1,**	30711080
CLA	**1	30711090
STO	MULT	30711100
STZ	**1	30711110
AXT	**3	30711120
XEC	S2	30711130
LDQ	**2	30711140
FMP	MULT	30711150
STO	TEMP	30711160
CLA	**1	30711170
FSB	TEMP	30711180
STO	**1	30711190
TXI	**1,2,**	30711200
TXI	**1,1,**	30711210
TIX	MX4,3,1	30711220
AXY	**1	30711230
TXH	**2,1,-2	30711240
TXI	ROWNI,1,1	30711250
XEC	S2	30711260
TXL	FIN,2,**	30711270
TIX	SFARCH,2,1	30711280

(-N)

三六

FIN	AXC	**1	30711290
ST2	SXA	SAV1,1	30711300
	CLA	COLNOS-1,1	30711310
	PAC	2	30711320
	AXT	**3	30711330
N10	CLA	**1	30711340
ST1	STO	TOL-1,2	30711350
DUM1	TIX	**1,1,**	30711360
N11	TIX	**1,2,**	30711370
N12	TIX	ST1,3,1	30711380
SAV1	AXT	**1	30711390
	TXH	**2,1,-2	30711400
	TXI	ST2,1,1	30711410
N13	AXC	**1	30711420
H2	SXA	H1,1	30711430
	LDQ	COLNOS-1,1	30711440
	MPY*	5,4	30711450
	XCA		30711460
	SUB*	5,4	30711470
	PAC	2	30711480
	PAC	1	30711490
	XCA		30711500
	MPY	N	30711510
	XCA		30711520
	SUB	N	30711530
	PAC	1	30711540
N14	AXT	**3	30711550
H	CLA	TOL,2	30711560
	STO	**1	30711570
	TXI	**1,1,-1	30711580
	TXI	**1,2,-1	30711590
	TIX	H,3,1	30711600
H1	AXT	**1	30711610
	TXH	**2,1,-2	30711620
	TXI	H2,1,1	30711630
	CLA	=1	30711640
IXSTO	STO*	6,4	30711650
EX1	AXT	**1	30711660
EX2	AXT	**2	30711670
EX3	AXT	**3	30711680
	TRA	1,4	30711690
SING	STZ*	6,4	30711700
	TRA	EX1	30711710

MX-1  
DUMY-1  
N  
N  
RESTORE (-1)

(-J)

N  
DUMY  
MX

RESTORE (-1)

"REPRODUCIBILITY OF THE ORIGINAL PAGE IS POOR."

N	REM	STORAGE	1	30711720
J	PZE		1	30711730
TOL	FQU			30711740
COLNOS	BLK1			30711750
DUMY	BLK2			30711760
TEMP	TOL			30711770
MULT	DUMY+2	N**2		30711780
ROWTAB	DUMY+3			30711790
PROD	DUMY+4			30711800
ROWTA	MULT		1	30711810
FND	ROWTAB			30711820
				30711830



### 3.5.3 DINTRP, ENTERP

These subroutines perform linear double and single interpolation. DINTRP makes use of ENTERP in interpolation for values along a particular curve. They are included for use by FUNCTION subprograms called by DATLYR or DATLD.

In DINTRP when the first argument is not bounded by the given table (curves) the statement

"ARGUMENT EXCEEDS EXTENT OF TABLE IN DINTRP." is printed, followed by

```
ARGUMENT = (1 PE 12.4)
TABLE VALUES (printed 6/line)
```

and the job is terminated.

When the argument in the single interpolation subroutine, ENTERP, exceeds the limits of the table, the routine selects the value at either end of the table and continues after printing.

```
"LIMITS OF TABLE EXCEEDED BY ARGUMENT = (1 PE 12.4)
(1 PE 12.4) = VALUE USED FROM TABLE"
```

Values entered in the tables should always be given in increasing algebraic order, both in terms of the numbers used to designate each curve of the family, and the values assigned to the points along the curve.

```

SIBFTC ENTP
C LINEAR INTERPOLATION SUBROUTINE **ENTERP** 6J-997 00000001
C 00000002
C SELECTS THE VALUE AT FITHER END OF TABLE WHEN ARGUMENT EXCEEDS
C LIMIT, THEN CONTINUES 00000003
C 00000004
C 00000005
C SUBROUTINE ARGUMENTS 00000006
C X VALUE TO LOOK UP IN TABLE 00000007
C TAB(1) NO. OF PAIRS OF ARGUMENTS AND VALUES IN TABLE 00000008
C TAB(2),ETC ARGUMENTS AND FUNCTIONS INTERLACED 00000009
C 00000019
C FUNCTION ENTERP (X,TAB) 00000020
C 00000024
C 00000025
C 00000030
C DIMENSION TAB(101)
C IF (TAB) 9,9,8
9 ENTERP = - TAB 00000035
C RETURN 00000040
8 N = TAB 00000045
C DO 5 I=1,N 00000050
1 IF (TAB(2*I)-X) 5,4,3 00000055
3 IF (I-1) 6,6,7 00000060
7 ENTERP = TAB(2*I-1) + (X-TAB(2*I-2)) * (TAB(2*I+1) - TAB(2*I-1)) 00000065
V / (TAB(2*I) - TAB(2*I-2)) 00000070
C RETURN 00000080
4 ENTERP = TAB(2*I+1) 00000085
C RETURN 00000090
5 CONTINUE 00000095
M = 2*N+1 0000100
K = M 0000101
105 WRITE ( 6,10) X, TAB(K) 0000105
10 FORMAT (// 10X, 39HLIMITS OF TABLE EXCEEDED BY ARGUMENT = 1PE12.4 0000110
1 / 10X, E12.4, 24H = VALUE USED FROM TABLE. 0000111
ENTERP = TAB(K) 0000115
C RETURN 0000120
6 M = 2*N+1 0000130
K = 3 0000140
GO TO 105 0000150
END 0000160

```

```

$IBFTC DNTP
C DOUBLE INTERPOLATION FUNCTION SUBROUTINE
C ARGUMENTS
C X USED TO DETERMINE WHICH TABLE TO USE (WHICH CURVE OF FAMILY)
C Y ARGUMENT USED AS X COORDINATE OF POINTS ON CURVE
C TAB(1) NO. OF TABLES (NO. OF CURVES IN FAMILY)
C TAB(2) NO. TO REPRESENT FIRST CURVE. MUST BE ITS LOWEST VALUE
C TAB(3) NO. OF ARGUMENTS IN FIRST TABLE (POINTS ALONG CURVE)
C TAB(4),ETC. X AND Y VALUES ALONG CURVE (INTERLACED)
C TAB(2*TAB(3)+4) LIKE TAB(2) FOR 2ND CURVE. THIS IS FOLLOWED
C BY ITS NO. OF PTS., VALUES, AND REPEATED THE NO. OF TIMES NCFCS-
C SARY BASED ON THE NO. OF TABLES LISTED IN TAB(1)
C
C FUNCTION DINTRP(X,Y,TAB)
C DIMENSION TAB(1)
C N = TAB + .5
C J = 0
C K = 0
C DO 50 I=1,N
C M SELECTS ONE OF FAMILY OF CURVES EQUAL TO OR ABOVE X VALUE
C M = I+J
C MU REPRESENTS NEXT LOWEST CURVE IN FAMILY
C MU = I+K-1
C IF(TAB(M+1)-X) 20,10,4
C 4 IF(I-1) 5,5,7
C 10 DINTRP=ENTERP(Y,TAB(M+2))
C RETURN
C 7 Z2 = ENTERP(Y,TAB(M+2))
C Z1 = ENTERP(Y,TAB(MU+2))
C DINTRP = Z1 + (X - TAB(MU+1)) * (Z2 - Z1) / (TAB(M+1) - TAB(MU+1))
C RETURN
C 20 K = J
C 50 J = INT (TAB(M+2) + .5) * 2 + 1 + J
C 5 MP1 = M + 1
C 6 WRITE (6, 30) X, (TAB(L), L=1,MP1)
C 30 FORMAT(/5X, 43HARGUMENT EXCEEDS EXTENT OF TABLE IN DINTRP. /10X,
C 1 10HARGUMENT =,1P6E12.4 /10X, 12HTABLE VALUES, 5X,1P6E12.4 /
C 2 (27X, 6E12.4)
C CALL EXIT
C STOP
C END

```

J.L. FICK

\$\*

#### 3.5.4 CODIMA

CODIMA is a curve fitting subroutine which has the following properties:

1. To the straight portions of any curve defined by three points on a straight line, a straight line will be fitted.
2. To the smooth portion of any curve, a smooth curve will be fitted.
3. The method maintains continuous first derivative except at the ends of a straight segment.
4. The method will fit curves with "corners" or "sharp turns" without the large deviation usually found in other methods.

An interpolation method is developed such that some of the considerations taken when an engineer fits a curve with a french curve are formulated. This is the CODIM (controlled deviation interpolation method) concept.

The method will interpolate in a more engineering manner in the sense that:

1. The first derivative is continuous except at the ends of straight segments defined by three points on a straight line.
2. No large deviation will be found when slope changes are large.
3. Ability to change value and slope rapidly.
4. Ability to fit straight lines on straight line portions of the curve and fit smooth arcs through the smooth portions of the curve.

The method fits a polynomial through an interval with information given by "previous points" (points to the left) and another polynomial through the interval with information given by "subsequent points" (points to the right). These two polynomials are then compared for compatibility. If they differ, a weighted average of the polynomials is taken in a way such that the polynomial that deviates less from the straight line connecting the points defining the interval is given more weight. For simplicity, parabolae are used over higher degree polynomials, in the CODIMA version.

```

CODIM000
CODIM001
CODIM009
CODIM010
CODIM011
CODIM012
CODIM013
CODIM014
CODIM015
CODIM016
CODIM017
CODIM018
CODIM019
CODIM020
CODIM025
CODIM029
CODIM030
CODIM040
CODIM049
CODIM050
CODIM059
CODIM060
CODIM070
CODIM080
CODIM089
CODIM090
CODIM100
CODIM109
CODIM110
CODIM120
CODIM130
CODIM140
CODIM149
CODIM150
CODIM160
CODIM170
CODIM180
CODIM190
CODIM199
CODIM200
CODIM210
CODIM220
CODIM230

$IBFTC CODS
C PARABOLIC CURVE FITTING SUBROUTINE (THREE POINTS)
C
C SUBROUTINE CODIMA (N1, X, Y, XI, YI, N2, SHAPE)
C
C ARGUMENTS
C N1 NO. OF POINTS TO ITERPOLATE
C X LOCATION OF POINTS TO BE INTERPOLATED
C Y ANSWERS
C XI INDEPENDENT ARGUMENT
C YI DEPENDENT ARGUMENT
C N2 NO. OF ARGUMENTS
C SHAPE 0 = FITS END WITH STRAIGHT LINE 1 = CURVE, LAST 3 PTS.
C
C DIMENSION X(1),Y(1),XI(1),YI(1),D(2),A(2),B(2),C(2)
C
C 100 IN = 0
C XK = SHAPE
C
C DO 800 N = 1,N1
C
C IF (N2-2) 110,115,120
C 110 Y(N) = YI(N2)
C GO TO 800
C
C 115 Y(N) = (YI(2)-YI(1))/(XI(2)-XI(1))* (X(N)-XI(1))+YI(1)
C GO TO 800
C
C 120 J = 1
C 125 IF(XI(J)-X(N)) 130,140,150
C 140 Y(N) = YI(J)
C GO TO 800
C
C 130 J = J+1
C IF(J-N2) 125,125,145
C 145 Y(N) = (YI(N2)-YI(N2-1))/(XI(N2)-XI(N2-1))*(X(N)-XI(N2-1))
C + YI(N2 - 1)
C GO TO 800
C
C 150 IF(J-2) 115,155,160
C 155 K = 3
C JJ = 1
C GO TO 185

```

```

CODIM240
CODIM250
CODIM260
CODIM270
CODIM280
CODIM290
CODIM300
CODIM309
CODIM310
CODIM320
CODIM330
CODIM340
CODIM350
CODIM360
CODIM370
CODIM380
CODIM390
CODIM400
CODIM410
CODIM420
CODIM430
CODIM440
CODIM450
CODIM460
CODIM470
CODIM480
CODIM490
CODIM500
CODIM509
CODIM510
CODIM520
CODIM530
CODIM540
CODIM550
CODIM560
CODIM570
CODIM580
CODIM590
CODIM599
CODIM600
CODIM610
CODIM620
CODIM630

160 IF(J-N2) 170,165,145
165 K = N2-1
    JJ = 2
    GO TO 185
170 IF(J-IN) 180,300,180
180 JJ = 3
    K = J
C
185 DO 200 M = 1,2
    X1 = XI(K-1)-XI(K)
    X2 = XI(K)-XI(K-2)
    X3 = XI(K-2)-XI(K-1)
    Y1 = YI(K-1)-YI(K)
    Y2 = YI(K)-YI(K-2)
    Y3 = YI(K-2)-YI(K-1)
    XX1 = XI(K-2)**2
    XX2 = XI(K-1)**2
    XX3 = XI(K)**2
    D(M) = XX1*X1 + XX2*X2 + XX3*X3
    A(M) = (YI(K-2)*X1 + YI(K-1)*X2 + YI(K)*X3)/D(M)
    B(M) = (XX1*Y1 + XX2*Y2 + XX3*Y3)/D(M)
    C(M) = YI(K-2) - A(M)*XX1 - B(M)*XI(K-2)
    200 K = K+1
    300 P1 = X(N)*(A(1)*X(N)+B(1)) + C(1)
    P2 = X(N)*(A(2)*X(N)+B(2)) + C(2)
    AL = (X(N)-XI(J-1))/(XI(J)-XI(J-1))
    S = YI(J)*AL + YI(J-1)*(1.0-AL)
    GO TO (320,330,350),JJ
C
320 P2 = P1
    AL = (X(N)-XI(1))/(XI(2)-XI(1))
    S = AL*YI(2) + (1.0-AL)*YI(1)
    IF (SHAPE) 321,322, 322
    321 XM1 = ABS (YI(2) - YI(1)) / (XI(2) - XI(1))
    XM2 = ABS (YI(3) - YI(2)) / (XI(3) - XI(2))
    XK = 1. - ABS (XM1 - XM2) / (XM1 + XM2)
    322 P1 = S + XK *(P2-S)
    GO TO 350
C
330 P1 = P2
    AL = (X(N)-XI(N2-1))/(X(N2)-XI(N2-1))
    S = AL*YI(N2) + (1.0-AL)*YI(N2-1)
    IF (SHAPE) 331,332, 332

```

```
331 XM1 = ABS (YI(N2 - 1) - YI(N2)) / (XI(N2 - 1) - XI(N2))
    XM2 = ABS (YI(N2 - 2) - YI(N2 - 1)) / (XI(N2 - 2) - XI(N2 - 1))
    XK = 1. - ABS (XM1 - XM2) / (XM1 + XM2)
332 P2 = S + XK*(P1-S)
C
350 E1 = ABS (P1-S)
    E2 = ABS (P2-S)
    IN = J
    IF (E1+E2) 700,700-750
700 Y(N) = S
    GO TO 800
750 YNUM = E1 * AL * P2 + (1. - AL) * E2 * P1
    YDEN = E1 * AL + (1. - AL) * E2
    Y(N) = YNUM / YDEN
800 CONTINUE
C
900 RETURN
    END
```

```
CODIM640
CODIM650
CODIM660
CODIM670
CODIM679
CODIM680
CODIM690
CODIM700
CODIM710
CODIM720
CODIM730
CODIM740
CODIM750
CODIM760
CODIM770
CODIM779
CODIM780
CODIM790
```

### 3.5.5 FILE

FILE is a function subprogram by which any number of files (or end of file marks) on a tape may be skipped, as specified by the programmer. Alternatively, the tape may be backspaced any number of files. The tape is positioned at the beginning of the desired file ready to read or write the first record. (Extent: 45 locations.)

Availability: On the FORTRAN library tape.

Use: The specified tape can be positioned as indicated by means of the statement:

A = FILE(I, J)

- |   |  |
|---|--|
| A | Used to make the statement format consistent with FORTRAN rules.   |
| I | FORTRAN tape number of one of the available tapes; must be a positive fixed point constant or variable.  |
| J | The number of files to be skipped or backspaced, <u>including the file in which the tape is positioned.</u> It must be a fixed point FORTRAN expression.<br>J > 0, skip<br>J < 0, backspace<br><u>J should never be zero.</u> If a zero argument is used, one file will be skipped either forward or backward depending on the sign of zero. |

#### Examples:

- Tape 4 is positioned within or at the end of file 2 and we wish to get to file 5. Then J = 3.  
A = FILE(4, 3)
- Tape 4 is positioned at the beginning of file 12 and file 16 is desired. Then J = 4.  
A = FILE(4, 4)
- Tape 4 is positioned anywhere within file 7 and file 4 is desired. Then J = -4.  
A = FILE(4, -4)
- Tape 4 is positioned anywhere within file 7 and the beginning of file 7 is desired. Then J = -1.  
A = FILE(4, -1)

Even if the tape is at the beginning of a file, you must count that file in computing the value of J. In the last example, if tape 4 is at the beginning of file 7 and a J of -1 is given, the next file to be read or written would still be file 7.



```

SIRMAP  FILE,Q      N5250000
TITLF   LRL        N5250010
*****          N5250020
*****          N5250030
*****          N5250040
*        ROUTINE TO POSITION A FORTRAN TAPE AT THE BEGINNING OF A FILE. N5250050
*        CALL      FILF(UNIT,COUNT) N5250060
*        UNIT      = FORTRAN TAPE NUMBER. (INTEGER) N5250070
*        UNIT      UNIT MUST BE A 729 TAPE. N5250080
*        UNIT      UNIT MUST BE A SCRATCH OR RESERVE TAPE. N5250090
*        COUNT     = NUMBER OF FILES TO BE SKIPPED OR BACKSPACED, N5250100
*        COUNT     INCLUDING THE CURRENT FILE. (INTEGER) N5250110
*        COUNT     COUNT GT 0 MEANS SKIP. N5250120
*        COUNT     COUNT LT 0 MEANS BACKSPACE. N5250130
*        COUNT     COUNT EQ 0 MEANS NO OPERATION. N5250140
*        ORIGINAL PROGRAMMING BY E. LESTER, 892 G.O., 7/10/63 N5250150
*        REVISED BY H. HARNED, I.B.M. N5250160
*        REWRITTEN BY D. H. ADAMS, 200-312 S.I.D., 8/13/65 N5250170
*        ***** N5250180
*        ***** N5250190
*        ***** N5250200
*        ***** N5250210
*        ***** N5250220
*        ***** N5250230
*        ***** N5250240
*        ***** N5250250
*        ***** N5250260
*        ***** N5250270
*        ***** N5250280
*        ***** N5250290
*        ***** N5250300
*        ***** N5250310
*        ***** N5250320
*        ***** N5250330
*        ***** N5250340
*        ***** N5250350
*        ***** N5250360
*        ***** N5250370
*        ***** N5250380
*        ***** N5250390
*        ***** N5250400
*        ***** N5250410
*        ***** N5250420

*****
PARAMETER DEFINITIONS
UNIT  SET 1+2 (ARG) FORTRAN UNIT
COUNT SET 2+2 (ARG) FILE COUNT (+ OR -)
UCW3  SET 2 UCB WORD 3
FCW3  SET 2 FCB WORD 3
FCW4  SET 3 FCB WORD 4
FCW6  SET 5 FCB WORD 6
FCW10 SET 9 FCB WORD 10
BSF   SET 6 BACKSPACE FILE
LENGTH SET 12 FCB LENGTH
SPACE
UCB   SET 4 (XR) UNIT CONTROL BLOCK
FCB   SET 1 (XR) FILE CONTROL BLOCK
NFILFS SET 1 (XR) FILE COUNT
LFR   SET 4 (XR) LENGTH OF FILE BLOCK
%SPACF
MONUN: LROOL 200000 MONITOR UNIT
INT     L900L 400000 INTERNAL FILE
    
```

NON729	1 500L	600000	DEVICE NOT 729 TAPE	N5250430
	SPACE			N5250440
	EGU	•CL5FO	AVOID IOCS FOR ALTIO	N5250450
	SPACE			N5250460
	OCT	140	SYSTEM UNIT TABLE ORIGIN	N5250470
	TTL	INITIALIZATION		N5250480
	SAVE	1+1		N5250490
	NZT#	COUNT*4	=FILE COUNT	N5250500
	RETURN	FILE	RETURN IF ZERO	N5250510
	CLA*	UNIT*4	=FORTRAN UNIT	N5250520
	TSX	•DFCVA*4	CONVERT TO BCD	N5250530
	XCL			N5250540
	ANA	=07777	MODULO 100	N5250550
	SLW	NUMBER	STORE FOR COMPARE	N5250560
	CAL	•LFRL		N5250570
	PAC	•FCB	=FILE BLOCK ORIGIN	N5250580
	PDX	•LFB	=FILE BLOCK LENGTH	N5250590
			SFARCH FCBS FOR UNIT	N5250600
			=FILE NAME, 'UNIT**'	N5250610
			EXTRACT **	N5250620
			COMPARE WITH UNIT	N5250630
				N5250640
				N5250650
				N5250660
				N5250670
				N5250680
				N5250690
				N5250700
				N5250710
				N5250720
				N5250730
				N5250740
				N5250750
				N5250760
				N5250770
				N5250780
				N5250790
				N5250800
				N5250810
				N5250820
				N5250830
				N5250840
				N5250850

SEARCH CAL	FCW10*FCB		
ANA	=07777		
LAS	NUMBER		
TRA	**2		
TRA	FOUND		
TNX	NOFILE,LFB,LENGTH		IS THERE ANOTHER FILE
TXI	SEARCH,FCB,-LENGTH		YFS, EXAMINE IT
FOUND	SCA	CLOSF*FCB	STORF LOC(FILE)
	SCA	NDSEL*FCB	
	PCA	*FCB	
	SUB	SYSUNI	DECEIVE •LXSEL
	STA	LXSEL	
	TTL	HOUSEKEEPING	
	TSX	•CLOSE*4	CLOSE FILE
	MON	**	
	SPACE		
	LDI	FCW3*FCB	IS UNIT
	BFT	MONUNI	MONITOR CONTROLLED
	TRA	ERROR	YES
	SPACE		
	LDI	FCW4*FCB	IS FILE
	BFT	INT	INTERNAL
	TRA	ERROR	YFS
	SPACE		

LDI	FCW6,FCB	15 UNIT	N5250860
RFT	NON729	A 729 TAPE	N5250870
TRA	ERROR	NO	N5250880
SPACF			N5250890
LXA	LK,DR,4		N5250900
CLA*	COUNT,4	=FILE COUNT	N5250910
PAX	*NFILES		N5250920
TPL	SKIP	FORWARD IF PLUS, ELSE ...	N5250930
TTL	PERFORM REQUESTED ACTION		N5250940
TSX	*NDSFL,4	BACKSPACE 1 FILE	N5250950
PZE	**,*BSF		N5250960
TIX	*-?,NFILES,1	COUNT DOWN	N5250970
SPACE			N5250980
CLA*	NDSSEL	EXAMINE TAPE POSITION --	N5250990
PAC	*UCR	IF NOT AT LOAD POINT	N5251000
NZT	UCW3,UCR	THEN READ PAST EOF	N5251010
RETURN	FILE	ELSE RETURN	N5251020
SPACE			N5251030
CALL	*LXSEL(LXSEL)	SKIP 1 FILE	N5251040
TIX	SKIP,NFILES,1	COUNT DOWN	N5251050
RETURN	FILE		N5251060
SPACE	4		N5251070
LXSEL	**,*+1		N5251080
PON	**0		N5251090
IORPN	**1		N5251100
TCH			N5251110
TTL	ERROR HANDLING	FILE SEARCH FAILED	N5251120
NOFILE	*FXEM,(CODEXX)		N5251130
CALL	FILE		N5251140
RETURN	FILE		N5251150
CODEXX	DEC 151		N5251160
IOCD	FAIL,4		N5251170
IOCD	IGNORF,3		N5251180
SPACF			N5251190
ERROR	FCW10,FCB	=FILE NAME	N5251200
CAL	NAME	ILLEGAL FILE	N5251210
SLW	*FXEM,(CODEYY)		N5251220
CALL	FILE		N5251230
RETURN	FILE		N5251240
CODEYY	DEC 152		N5251250
IOCD	BAD,5		N5251260
IOCD	IGNORE,3		N5251270
SPACF			N5251280
BCI	1,0UNIT	UNIT (BCD)	
BCI	1,*****		
BCI	2, UNDEFINED		

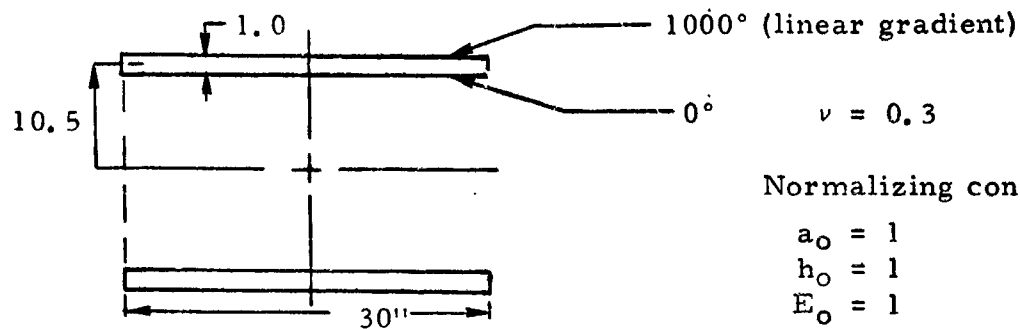
"REPRODUCIBILITY OF THE ORIGINAL PAGE IS POOR."

BAD	BCI	4.0 FILE SKIP ILLEGAL FOR	N5251290
NAME	BCI	1.*****	N5251300
IGNORE	BCI	3.0RFQUEST IGNORED.	N5251310
	TTL		N5251320
LK. DR	LDIR		N5251330
	END		N5251340

### 3.6 SAMPLE PROBLEM 1

#### 3.6.1 Problem Description and Set-Up

A free cylinder under thermal loading is considered. The geometry and loading is shown in the following figure



Normalizing constants

$$a_0 = 1$$

$$h_0 = 1$$

$$E_0 = 1$$

$$\sigma_0 = 1$$

FREE ENDS

No pressure load

Axisymmetric NF = 0

Stiffness Parameters

$$BBB = 2.4725 \times 10^7 \text{ (in plane)}$$

$$DDD = 1.8887 \times 10^6 \text{ (bending)}$$

Thermal Load

$$ENTT = 9.375 \times 10^4 \text{ (in plane)}$$

$$EMTT = 1.0045 \times 10^4 \text{ (bending)}$$

Stress Output Parameters

$$EI1 = 3 \times 10^7$$

$$EI2 = 1.5 \times 10^7$$

$$DN1 = -0.4167$$

$$DN2 = 0.5833$$

$$POIS1 = 0.3$$

$$POIS2 = 0.3$$



DECK NUMBER	PERIOD	DESCRIPTION	DATE	BY
1	6	ENF		
4		BCIT (free)		
10		BCIB (special; axisymmetric complete)		
1		PFLAG		
11		GIN (cone-cylinder)		
21		EN (21 stations)		
105		RAI (radius)		
15		20 A x L (length)		
429		$\Omega(3,3)$		
21		$\Lambda(1,1)$		
433		$\Lambda(2,2)$		
1		$\Lambda(4,4)$		
22				

GMDA, Geometry Data

3.6.3 Functional Subprogram Used

```
00000001
00000009 STIFFNESS FUNCTION
00000019
00000020
00000021
00000100
00000110
00000119
00000120
00000200
00000210
00000999
```

```
$IBFTC BFCN
C
C
FUNCTION BRR( PFL,ZTA )
BRR = 2.4725274F7
RETURN
C
ENTRY DDD ( ZTA )
BRR = 1.8887362F6
RETURN
END
```

```
00000001
00000009 TEMPERATURE FUNCTION
00000019
00000020
00000021
00000100
00000110
00000119
00000120
00000200
00000210
00000999
```

```
$IBFTC TFCN
C
C
FUNCTION ENT( PFL,ZTA )
ENT = 9.375E+4
RETURN
C
ENTRY ENT( PFL,ZTA )
ENT = 1.0045F4
RETURN
END
```



```
00000001
00000009
00000019
00000020
00000021
00000100
00000110
00000119
00000999

$IBFTC PFCN          SPRING FUNCTION
C
C
C      FUNCTION DKR4( PFL,ZTA )
C      DKR4 = 0.0
C      RETURN
C      END
```

```
00000001
00000009
00000019
00000020
00000021
00000100
00000110
00000119
00000120
00000200
00000210
00000219
00000220
00000300
00000310
00000999

$IBFTC PFCN          PRESSURE FUNCTION
C
C
C      FUNCTION PPPN( PFL,ZTA )
C      PPPN = 0.
C      RETURN
C      ENTRY   PPPH( PEL,ZTA )
C      PPPN = 0.
C      RETURN
C      ENTRY   PPPF( PFL,ZTA )
C      PPPN = 0.
C      RETURN
C      END
```

```

$IBFTC STR1FN      00000001
C      1ST SURFACE ** ELASTIC MODULUS, DISTANCE, POISSON'S RATIO
C      00000009
C      00000019
C      FUNCTION E11 ( PEL,ZTA )
C      00000020
C      00000021
C      E11 = 3.0E+7
C      RETURN
C      00000100
C      00000110
C      00000119
C      00000120
C      ENTRY DN1 ( PEL,ZTA )
C      E11 = -0.41666667
C      RETURN
C      00000210
C      00000219
C      00000220
C      ENTRY POIS1( PEL,ZTA )
C      E11 = 0.3
C      RETURN
C      00000310
C      00000999
C      END
    
```

```

$IBFTC STR2FN      00000001
C      2ND SURFACE ** ELASTIC MODULUS, DISTANCE, POISSON'S RATIO
C      00000009
C      00000019
C      00000020
C      00000021
C      00000100
C      00000110
C      00000119
C      00000120
C      00000200
C      00000210
C      00000219
C      00000220
C      00000300
C      00000310
C      00000999
C      END
    
```

```
$IBFIC TTF1
C 1ST SURFACE ** COEF. OF THERMAL EXPANSION, TEMPERATURE
C 00000001
C 00000009
C 00000019
C 00000020
C 00000021
C 00000100
C 00000110
C 00000119
C 00000120
C 00000200
C 00000210
C 00000999
C
C ENTRY ALF1( PEL,ZTA )
C TMP1 = 10.0E-6
C RETURN
C
C FND
```

```
$IBFIC TTF2
C 2ND SURFACE ** COEF. OF THERMAL EXPANSION, TEMPERATURE
C 00000001
C 00000009
C 00000019
C 00000020
C 00000021
C 00000100
C 00000110
C 00000119
C 00000120
C 00000200
C 00000210
C 00000999
C
C ENTRY ALF2( PEL, A )
C TMP2 = 5.0E-6
C RETURN
C
C END
```

3.6.4 Output

CYLINDER UNDER THERMAL LOAD  
ARS JOURNAL, JANUARY 1962  
RADKOWSKI, DAVIS, BOLDRUC

GENERAL DATA

AO = 1.0000E 00 HO = 1.0000E 00 FO = 1.0000E 00 SIGO = 1.0000E 00  
 POI = 3.0000E-01 ENF = 1.0000E 00 BCIT = 4.0000E 00 BCIB = 1.0000E 01  
 PFLAG = -1.0000E 00

PRINT ANGLES (THY) -  
 0.0000E-39 -1.0000E 10 -1.0000E 10 -1.0000E 10 -1.0000E 10 -1.0000E 10

FOURIER HARMONIC PRINTS (FPRINT) -  
 1.0000E 00 -1.0000E 10 -1.0000E 10 -1.0000E 10

BOUNDARY MATRICES

TOP BOUNDARY \*\*

OMEGA  
 1.0000000E 00 0.0000000E-39 0.0000000E-39 0.0000000E-39 0.0000000E-39  
 0.0000000E-39 1.0000000E 00 0.0000000E-39 0.0000000E-39 0.0000000E-39  
 0.0000000E-39 0.0000000E-39 1.0000000E 00 0.0000000E-39 0.0000000E-39  
 0.0000000E-39 0.0000000E-39 0.0000000E-39 1.0000000E 00 0.0000000E-39  
 0.0000000E-39 0.0000000E-39 0.0000000E-39 0.0000000E-39 1.0000000E 00

LAMBDA

0.0000000E-39 0.0000000E-39 0.0000000E-39 0.0000000E-39 0.0000000E-39  
 0.0000000E-39 0.0000000E-39 0.0000000E-39 0.0000000E-39 0.0000000E-39  
 0.0000000E-39 0.0000000E-39 0.0000000E-39 0.0000000E-39 0.0000000E-39  
 0.0000000E-39 0.0000000E-39 0.0000000E-39 0.0000000E-39 0.0000000E-39  
 0.0000000E-39 0.0000000E-39 0.0000000E-39 0.0000000E-39 0.0000000E-39

L -

0.0000000E-39 0.0000000E-39 0.0000000E-39 0.0000000E-39 0.0000000E-39

BOTTOM BOUNDARY \*\*

OMEGA			
0.0000000E-39	0.0000000E-39	0.0000000E-39	0.0000000E-39
0.0000000E-39	0.0000000E-39	0.0000000E-39	0.0000000E-39
0.0000000E-39	0.0000000E-39	0.0000000E-39	0.0000000E-39
0.0000000E-39	0.0000000E-39	0.0000000E-39	0.0000000E-39
0.0000000E-39	0.0000000E-39	0.0000000E-39	0.0000000E-39

L.A. DA			
1.0000000E-00	0.0000000E-39	0.0000000E-39	0.0000000E-39
0.0000000E-39	1.0000000E-00	0.0000000E-39	0.0000000E-39
0.0000000E-39	0.0000000E-39	0.0000000E-39	0.0000000E-39
0.0000000E-39	0.0000000E-39	1.0000000E-00	0.0000000E-39
0.0000000E-39	0.0000000E-39	0.0000000E-39	1.0000000E-00

L -			
0.0000000E-39	0.0000000E-39	0.0000000E-39	0.0000000E-39

GEOMETRY DATA FOR CONE - CYLINDER

NUMBER OF STATIONS - 21

I	R(I)	XI(I)	W(THETA)	W(XI)	RHOX(I)	GAMA(I)
1	1.050000E 01	0.000000E-39	9.5238095E-02	0.000000E-39	1.050000E 01	0.000000E-39
2	1.050000E 01	7.500000E-01	9.5238095E-02	0.000000E-39	1.050000E 01	0.000000E-39
3	1.050000E 01	1.500000E 00	9.5238095E-02	0.000000E-39	1.050000E 01	0.000000E-39
4	1.050000E 01	2.250000E 00	9.5238095E-02	0.000000E-39	1.050000E 01	0.000000E-39
5	1.050000E 01	3.000000E 00	9.5238095E-02	0.000000E-39	1.050000E 01	0.000000E-39
6	1.050000E 01	3.750000E 00	9.5238095E-02	0.000000E-39	1.050000E 01	0.000000E-39
7	1.050000E 01	4.500000E 00	9.5238095E-02	0.000000E-39	1.050000E 01	0.000000E-39
8	1.050000E 01	5.250000E 00	9.5238095E-02	0.000000E-39	1.050000E 01	0.000000E-39
9	1.050000E 01	6.000000E 00	9.5238095E-02	0.000000E-39	1.050000E 01	0.000000E-39
10	1.050000E 01	6.750000E 00	9.5238095E-02	0.000000E-39	1.050000E 01	0.000000E-39
11	1.050000E 01	7.500000E 00	9.5238095E-02	0.000000E-39	1.050000E 01	0.000000E-39
12	1.050000E 01	8.250000E 00	9.5238095E-02	0.000000E-39	1.050000E 01	0.000000E-39
13	1.050000E 01	9.000000E 00	9.5238095E-02	0.000000E-39	1.050000E 01	0.000000E-39
14	1.050000E 01	9.750000E 00	9.5238095E-02	0.000000E-39	1.050000E 01	0.000000E-39
15	1.050000E 01	1.050000E 01	9.5238095E-02	0.000000E-39	1.050000E 01	0.000000E-39
16	1.050000E 01	1.125000E 01	9.5238095E-02	0.000000E-39	1.050000E 01	0.000000E-39
17	1.050000E 01	1.200000E 01	9.5238095E-02	0.000000E-39	1.050000E 01	0.000000E-39
18	1.050000E 01	1.275000E 01	9.5238095E-02	0.000000E-39	1.050000E 01	0.000000E-39
19	1.050000E 01	1.350000E 01	9.5238095E-02	0.000000E-39	1.050000E 01	0.000000E-39
20	1.050000E 01	1.425000E 01	9.5238095E-02	0.000000E-39	1.050000E 01	0.000000E-39
21	1.050000E 01	1.500000E 01	9.5238095E-02	0.000000E-39	1.050000E 01	0.000000E-39

CHECKPRINT OF COEFC BLOCKS STORED IN GROUPS OF (2\*ENF) PER MERIDIONAL STATION. THE COEFFICIENTS  
 PRINTED ARE SCB1, SC01, SCNTSI, SCMTSI, DCK3 (IN THAT ORDER) AND ARE SEPARATED FROM EACH OTHER BY THE  
 THREE ..... FIELDS.

FOR STATION 1 THROUGH STATION 21

2.4725267E 07	-4.7055554E 00	2.4725267E 07	-4.7055554E 00	2.4725267E 07	-4.7055554E 00
2.4725267E 07	-4.7055554E 00	2.4725267E 07	-4.7055554E 00	2.4725267E 07	-4.7055554E 00
2.4725267E 07	-4.7055554E 00	2.4725267E 07	-4.7055554E 00	2.4725267E 07	-4.7055554E 00
2.4725267E 07	-4.7055554E 00	2.4725267E 07	-4.7055554E 00	2.4725267E 07	-4.7055554E 00
2.4725267E 07	-4.7055554E 00	2.4725267E 07	-4.7055554E 00	2.4725267E 07	-4.7055554E 00
2.4725267E 07	-4.7055554E 00	2.4725267E 07	-4.7055554E 00	2.4725267E 07	-4.7055554E 00
.....	.....	.....	.....	.....	.....
-2.9236110E-01	1.8887359E 06	-2.9236110E-01	1.8887359E 06	-2.9236110E-01	1.8887359E 06
-2.9236110E-01	1.8887359E 06	-2.9236110E-01	1.8887359E 06	-2.9236110E-01	1.8887359E 06
-2.9236110E-01	1.8887359E 06	-2.9236110E-01	1.8887359E 06	-2.9236110E-01	1.8887359E 06
-2.9236110E-01	1.8887359E 06	-2.9236110E-01	1.8887359E 06	-2.9236110E-01	1.8887359E 06
-2.9236110E-01	1.8887359E 06	-2.9236110E-01	1.8887359E 06	-2.9236110E-01	1.8887359E 06
-2.9236110E-01	1.8887359E 06	-2.9236110E-01	1.8887359E 06	-2.9236110E-01	1.8887359E 06
.....	.....	.....	.....	.....	.....
9.3749997E 04	-1.8120659E-02	9.3749997E 04	-1.8120659E-02	9.3749997E 04	-1.8120659E-02
9.3749997E 04	-1.8120659E-02	9.3749997E 04	-1.8120659E-02	9.3749997E 04	-1.8120659E-02
9.3749997E 04	-1.8120659E-02	9.3749997E 04	-1.8120659E-02	9.3749997E 04	-1.8120659E-02
9.3749997E 04	-1.8120659E-02	9.3749997E 04	-1.8120659E-02	9.3749997E 04	-1.8120659E-02
9.3749997E 04	-1.8120659E-02	9.3749997E 04	-1.8120659E-02	9.3749997E 04	-1.8120659E-02
9.3749997E 04	-1.8120659E-02	9.3749997E 04	-1.8120659E-02	9.3749997E 04	-1.8120659E-02
.....	.....	.....	.....	.....	.....
-2.0589192E-03	1.0045000E 04	-2.0589192E-03	1.0045000E 04	-2.0589192E-03	1.0045000E 04
-2.0589192E-03	1.0045000E 04	-2.0589192E-03	1.0045000E 04	-2.0589192E-03	1.0045000E 04
-2.0589192E-03	1.0045000E 04	-2.0589192E-03	1.0045000E 04	-2.0589192E-03	1.0045000E 04
-2.0589192E-03	1.0045000E 04	-2.0589192E-03	1.0045000E 04	-2.0589192E-03	1.0045000E 04
-2.0589192E-03	1.0045000E 04	-2.0589192E-03	1.0045000E 04	-2.0589192E-03	1.0045000E 04
-2.0589192E-03	1.0045000E 04	-2.0589192E-03	1.0045000E 04	-2.0589192E-03	1.0045000E 04
.....	.....	.....	.....	.....	.....
0.0000000E-39	-0.0000000E-39	0.0000000E-39	-0.0000000E-39	0.0000000E-39	-0.0000000E-39
0.0000000E-39	-0.0000000E-39	0.0000000E-39	-0.0000000E-39	0.0000000E-39	-0.0000000E-39
0.0000000E-39	-0.0000000E-39	0.0000000E-39	-0.0000000E-39	0.0000000E-39	-0.0000000E-39
0.0000000E-39	-0.0000000E-39	0.0000000E-39	-0.0000000E-39	0.0000000E-39	-0.0000000E-39



CHECKPRINT OF LOAD COEF. STORED IN GROUPS OF ALL ENF PER MERIDIONAL STATION. THE COEFFICIENTS ARE PFE, PTH, PN (IN THAT ORDER) AND ARE SEPARATED FROM EACH OTHER BY \*\*\*\*\* FIELDS.

FOR STATION 1 THROUGH STATION 21

0.000000E-39	0.000000E-39	0.000000E-39	0.000000E-39	0.000000E-39	0.000000E-39	0.000000E-39	0.000000E-39	0.000000E-39	0.000000E-39
0.000000E-39	0.000000E-39	0.000000E-39	0.000000E-39	0.000000E-39	0.000000E-39	0.000000E-39	0.000000E-39	0.000000E-39	0.000000E-39
0.000000E-39	0.000000E-39	0.000000E-39	0.000000E-39	0.000000E-39	0.000000E-39	0.000000E-39	0.000000E-39	0.000000E-39	0.000000E-39
0.000000E-39	0.000000E-39	0.000000E-39	0.000000E-39	0.000000E-39	0.000000E-39	0.000000E-39	0.000000E-39	0.000000E-39	0.000000E-39
0.000000E-39	0.000000E-39	0.000000E-39	0.000000E-39	0.000000E-39	0.000000E-39	0.000000E-39	0.000000E-39	0.000000E-39	0.000000E-39
0.000000E-39	0.000000E-39	0.000000E-39	0.000000E-39	0.000000E-39	0.000000E-39	0.000000E-39	0.000000E-39	0.000000E-39	0.000000E-39
0.000000E-39	0.000000E-39	0.000000E-39	0.000000E-39	0.000000E-39	0.000000E-39	0.000000E-39	0.000000E-39	0.000000E-39	0.000000E-39
0.000000E-39	0.000000E-39	0.000000E-39	0.000000E-39	0.000000E-39	0.000000E-39	0.000000E-39	0.000000E-39	0.000000E-39	0.000000E-39
0.000000E-39	0.000000E-39	0.000000E-39	0.000000E-39	0.000000E-39	0.000000E-39	0.000000E-39	0.000000E-39	0.000000E-39	0.000000E-39
0.000000E-39	0.000000E-39	0.000000E-39	0.000000E-39	0.000000E-39	0.000000E-39	0.000000E-39	0.000000E-39	0.000000E-39	0.000000E-39
0.000000E-39	0.000000E-39	0.000000E-39	0.000000E-39	0.000000E-39	0.000000E-39	0.000000E-39	0.000000E-39	0.000000E-39	0.000000E-39

\*Z\* MATRIX FOR STATION 21  
0.000000E-39 0.000000E-39 3.0273973E-02 2.9521609E-10 0.0000000E-39

\*Z\* MATRIX FOR STATION 20  
-2.2108287E-03 0.0000000E-39 3.0281600E-02 2.2427470E-05 0.0000000E-39

\*Z\* MATRIX FOR STATION 19  
-4.4213307E-03 0.0000000E-39 3.0304480E-02 5.0239731E-05 0.0000000E-39

\*Z\* MATRIX FOR STATION 18  
-6.6311037E-03 0.0000000E-39 3.0349646E-02 9.0617861E-05 0.0000000E-39

\*Z\* MATRIX FOR STATION 17  
-8.8395379E-03 0.0000000E-39 3.0429458E-02 1.4980632E-04 0.0000000E-39

\*Z\* MATRIX FOR STATION 16  
-1.1045710E-02 0.0000000E-39 3.0560775E-02 2.3272686E-04 0.0000000E-39

\*Z\* MATRIX FOR STATION 15  
-1.3248305E-02 0.0000000E-39 3.0763433E-02 3.3978652E-04 0.0000000E-39

\*Z\* MATRIX FOR STATION 14  
.  
.  
.  
.  
.  
.

\*Z\* MATRIX FOR STATION 6

-3.2645028E-02    0.0000000E-39    3.4107951E-02    -1.5989654E-03    0.0000000E-39

\*Z\* MATRIX FOR STATION 5

-3.4790510E-02    0.0000000E-39    3.2547584E-07    -3.3380269E-03    0.0000000E-39

\*Z\* MATRIX FOR STATION 4

-3.6985673E-02    0.0000000E-39    2.9471267E-02    -5.7134319E-03    0.0000000E-39

\*Z\* MATRIX FOR STATION 3

-3.9268604E-02    0.0000000E-39    2.4355890E-02    -8.7390917E-03    0.0000000E-39

\*Z\* MATRIX FOR STATION 2

-4.1688553E-02    -0.0000000E-39    1.6683303E-02    -1.2315728E-02    -0.0000000E-39

\*Z\* MATRIX FOR STATION 1

-4.4304717E-02    0.0000000E-39    6.0422107E-03    -1.6167123E-02    -0.0000000E-39

STATION 21

THETA = 0.00

ENF = 0.0

U	V	W	PHI(XI)	PHI(THETA)
0.000000E-39	0.000000E-39	3.0273973E-02	2.9521609E-10	0.000000E-39

STATION 20

THETA = 0.00

ENF = 0.0

U	V	W	PHI(XI)	PHI(THETA)
-2.2108287E-03	0.000000E-39	3.0281600E-02	2.2427470E-05	0.000000E-19

STATION 19

THETA = 0.00

ENF = 0.0

U	V	W	PHI(XI)	PHI(THETA)
-4.4213307E-03	0.000000E-39	3.0304480E-02	5.0239731E-05	0.000000E-39

THETA = 0.00  
ENF = 0.0  
U V W  
-3.9268604E-02 0.0000000E-39 2.4355830E-02 -8.7390917E-03 PHI(XI) PHI(THETA)  
0.0000000E-39

STATION 2  
THETA = 0.00  
ENF = 0.0  
U V W  
-4.1688553E-02 -0.0000000E-39 1.6683303E-02 -1.2315728E-02 PHI(XI) PHI(THETA)  
-0.0000000E-39

STATION 1  
THETA = 0.00  
ENF = 0.0  
U V W  
-4.4304717E-02 0.0000000E-39 6.0422107E-03 -1.6167123E-02 PHI(XI) PHI(THETA)  
-0.0000000E-39

STATION 21  
 N(XI) N(THETA) M(XI,THETA) Q(XI)  
 5.264589E 02 -5.9428223E 02 0.000000E-39 -1.4750057E-03

M(XI) M(THETA) M(XI,THETA) Q(THETA)  
 -1.0094696E 04 -1.0059907E 04 0.000000E-39 -0.000000E-39

STRESSES FOR LAYER 1

SIG(XI) SIG(THETA) SIG(XI,THETA) SIG(XI,ETA) SIG(THETA,ETA)  
 1.2606342E 05 1.2431609E 05 -0.000000E-39 -1.9666753E-03 -0.000000E-39

STRESSES FOR LAYER 2

SIG(XI) SIG(THETA) SIG(XI,THETA) SIG(XI,ETA) SIG(THETA,ETA)  
 -4.4544874E 04 -4.5114929E 04 0.000000E-39 -9.8333765E-04 -0.000000E-39

STATION 20  
 N(XI) N(THETA) M(XI,THETA) Q(XI)  
 5.210742E 02 -5.7955566E 02 0.000000E-39 1.8084047E 01

M(XI) M(THETA) M(XI,THETA) Q(THETA)  
 -1.0108257E 04 -1.0063975E 04 0.000000E-39 -0.000000E-39

STRESSES FOR LAYER 1

SIG(XI) SIG(THETA) SIG(XI,THETA) SIG(XI,ETA) SIG(THETA,ETA)  
 1.2615487E 05 1.2436532E 05 -0.000000E-39 2.4112076E 01 -0.000000E-39

STATION 2  
 N(XI) N(THETA) M(XI, THETA) Q(XI)  
 1.0485137E 03 -2.9560514E 04 0.0000000E-19 -9.2257202E 02

M(XI) M(THETA) M(XI, THETA) Q(THETA)  
 -6.9193945E 02 -7.2390801E 03 0.0000000E-39 0.0000000E-39

STRESSES FOR LAYER 1  
 SIG(XI) SIG(THETA) SIG(XI, THETA) SIG(XI, ETA) SIG(THETA, ETA)  
 5.8375792E 04 6.5179318E 04 -0.0000000E-39 -1.2300967E 03 0.0000000E-39

STRESSES FOR LAYER 2  
 SIG(XI) SIG(THETA) SIG(XI, THETA) SIG(XI, ETA) SIG(THETA, ETA)  
 3.6717552E 03 -5.0065183E 04 0.0000000E-39 -6.1504833E 02 0.0000000E-39

STATION 1  
 N(XI) N(THETA) M(XI, THETA) Q(XI)  
 -7.6171875E-02 -5.2677420E 04 0.0000000E-39 3.6267831E-02

M(XI) M(THETA) M(XI, THETA) Q(THETA)  
 -1.1962891E-02 -7.0315019E 03 0.0000000E-39 -0.0000000E-39

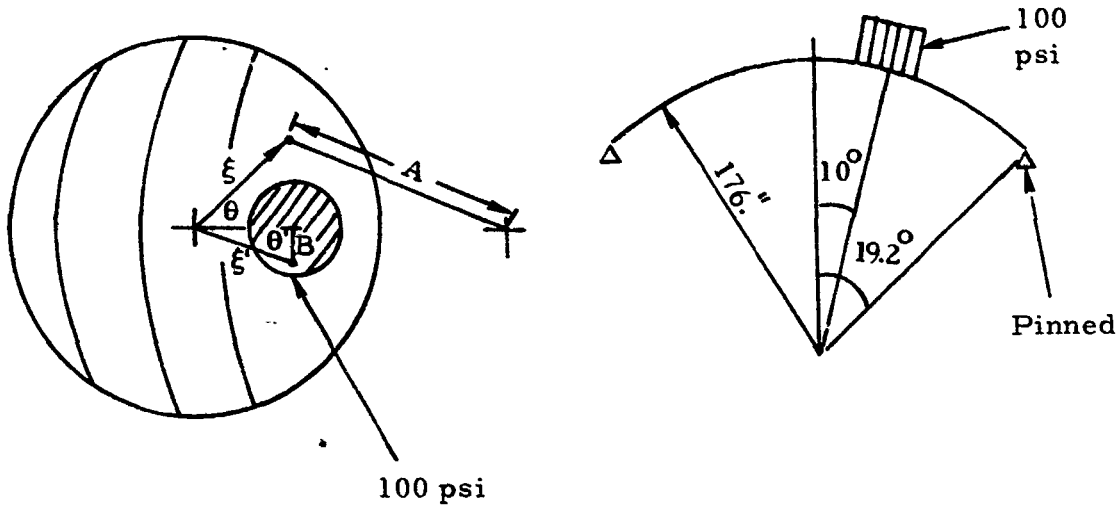
STRESSES FOR LAYER 1  
 SIG(XI) SIG(THETA) SIG(XI, THETA) SIG(XI, ETA) SIG(THETA, ETA)  
 5.1945470E 04 3.2847100E 04 -0.0000000E-39 4.8357133E-02 -0.0000000E-39

STRESSES FOR LAYER 2  
 SIG(XI) SIG(THETA) SIG(XI, THETA) SIG(XI, ETA) SIG(THETA, ETA)  
 6.4952361E 03 -6.4419699E 04 0.0000000E-39 2.4178567E-02 -0.0000000E-39

### 3.7 SAMPLE PROBLEM 2

#### 3.7.1 Problem Description

An Apollo-like shell pinned at the edge is considered.



Normalizing constants

$$\begin{aligned} a_0 &= 1 \\ h_0 &= 1 \\ E_0 &= 1 \\ \sigma_0 &= 1 \end{aligned}$$

No Thermal Loads

Stiffness Parameter

$$A = \xi^2 \left[ 5625 - 2(75)\xi, \cos \theta \right]$$

$$\begin{aligned} \text{if } A < 4425, & \quad BBB = 3.296 \times 10^6 \\ & \quad DDD = 3.296 \times 10^6 \end{aligned}$$

$$\begin{aligned} \text{if } 4425 < A < 7225, & \quad BBB = 1.9779 \times 10^6 \\ & \quad DDD = 1.9779 \times 10^6 \end{aligned}$$

$$\begin{aligned} \text{if } 7225 < A < 11025, & \quad BBB = 1.386 \times 10^6 \\ & \quad DDD = 1.386 \times 10^6 \end{aligned}$$

$$\begin{aligned} \text{if } A > 11025, & \quad BBB = 0.79116 \times 10^6 \\ & \quad DDD = 0.79116 \times 10^6 \end{aligned}$$



### Pressure parameters

#### Normal pressure definition

$$B = \xi^2 + (30.492)^2 - 2(30.492)\xi \cos \theta$$

$$\text{if } B < 400 \quad \text{PPPN} = 100.0$$

$$\text{if } B \geq 400 \quad \text{PPPN} = 0.0$$

also circumferential and meridional pressures definition

$$\text{PPPH} = \text{PPPF} = 0.0$$

#### Stress output parameters

$$EI1 = EI2 = 29.5 \times 10^6 \text{ Young's Modulus of stress output location}$$

#### Distance to neutral surface

$$A = \xi^2 + 5625. - 2(75)\xi \cos \theta$$

$$\text{if } A < 4425 \quad \text{DN1} = -1.025, \text{ DN2} = +1.025$$

$$\text{if } 4425 < A < 7225, \quad \text{DN1} = -1.005, \text{ DN2} = +1.005$$

$$\text{if } 7225 < A < 11025, \quad \text{DN1} = -0.995, \text{ DN2} = +0.995$$

$$\text{if } A > 11025, \quad \text{DN1} = -0.987, \text{ DN2} = +0.987$$





DECK NO.	PROGRAMMER	DATE	PAGE	OF	JOB NO.
NUMBER	IDENTIFICATION	DESCRIPTION	DO NOT KEY PUNCH		
6		PHIO			
19.2		PHIN			
	73				
	21				
	8				
	73				
	73				

FORM 114 C-17 REV. 7 55.

3.7.3 Function Subprograms Used

```

$IRFTC 67CN
APOLLO SHELL
C
FUNCTION RRR (PFL,ZTA)
C
A = PFL * PFL + 5625. - 150. * PFL * COS( ZTA )
C
IF (A .LE. 4225.) GO TO 20
IF (A .LE. 7225.) GO TO 30
IF (A .LE. 11025.) GO TO 35
C
K = 1
10 RRR = 0.79116F6
GO TO 100
C
20 K = 2
25 RRR = 3.296F6
GO TO 100
C
30 K = 3
RRR = 1.9779F6
GO TO 100
C
35 K = 4
40 RRR = 1.386F6
GO TO 100
C
ENTRY DDD (ZTA)
C
IF (K - 2) 10, 25, 50
C
50 IF (K .GT. 3) GO TO 40
C
RRR = 1.9779F6
100 RETURN
C
END
    
```

```

$IBFTC TFCN          00000001
C                    00000009
C                    00000019
C                    00000020
C                    00000021
C                    00000100
C                    00000110
C                    00000119
C                    00000120
C                    00000200
C                    00000210
C                    00000999

TEMPERATURE FUNCTION
FUNCTION ENT1( PFL,ZTA )
ENT1 = 0.
RETURN
ENTRY   EM11( PEL,ZTA )
ENT1 = 0.
RETURN
END

```

```

$IBFTC KFCN          00000001
C                    00000009
C                    00000019
C                    00000020
C                    00000021
C                    00000100
C                    00000110
C                    00000119
C                    00000999

SPRINGS FUNCTION
FUNCTION DKR3( PEL,ZTA )
DKR3 = 0.0
RETURN
END

```

```

$IBFTC PFCN
C
HELL LOAD
00000001
00000010
00000019
00000020
00000021
00000030
00000039
00000040
00000050
00000060
00000070
00000080
00000090
00000100
00000110
00000120
00000129
00000130
00000140
00000150
00000190
00000200
END

```

FUNCTION PFCN (PFL,ZTA)

A = PFL\*PFL + 30.402\*30.402 - 2.0 \* 30.497 \* PFL \* COS( 7TA )

PPPN = 0.0  
IF(A .LE. 400.0) PPPN = 100.0  
RETURN

ENTRY PPPH (PFL,ZTA)  
PPPN = 0.0  
RETURN

ENTRY PPPF (PEL,ZTA)  
PPPN = 0.0  
RETURN

3/1

```

SIBFC STRIEN
C 1ST SURFACE ** ELASTIC MODULUS, DISTANCE, POISSON'S RATIO
C APOLLO SHELL
C
C FUNCTION EII ( PEL,ZTA )
C EII = 29.5F6
C RETURN
C
C ENTRY DNI ( PEL,ZTA )
C
C A = PEL * PEL + 5625. - 150. * PEL * COS( ZTA )
C
C IF (A .LE. 4225.) GO TO 20
C IF (A .LE. 7225.) GO TO 30
C IF (A .LE. 11025.) GO TO 40
C
C EII = -.987
C GO TO 100
C
C 20 EII = -1.025
C GO TO 100
C
C 30 EII = -1.005
C GO TO 100
C
C 40 EII = -.995
C 100 RETURN
C
C ENTRY POIS( PEL,ZTA )
C EII = 0.4
C RETURN
C END
    
```

000001  
0000009  
0000010  
0000019  
0000020  
0000021  
0000150  
0000110  
0000119  
0000120  
0000121  
0000125  
0000129  
0000130  
0000132  
0000134  
0000139  
0000140  
0000145  
0000149  
0000150  
0000155  
0000159  
0000160  
0000165  
0000169  
0000170  
0000210  
0000219  
0000220  
0000230  
0000310  
0000999



```

STARFC STR2FN          00000001
C 2ND SURFACE ** PLASTIC MODULUS, DISTANCE, POISSON'S RATIO 00000006
C                                APOLLO. SHELL
C
C FUNCTION F12 ( PFL,ZTA )
C E12 = 29.5F6
C RETURN
C
C ENTRY DN2 ( PFL,ZTA )
C A = PFL * PFL + 5625. - 150. * PFL * COS( ZTA )
C IF ( A .LE. 4225. ) GO TO 20
C IF ( A .LE. 7225. ) GO TO 30
C IF ( A .LE. 11025. ) GO TO 40
C
C E12 = .987
C GO TO 100
C
C 20 E12 = 1.025
C GO TO 100
C
C 30 E12 = 1.005
C GO TO 100
C
C 40 E12 = .995
C 100 RETURN
C ENTRY POIS2( PFL,ZTA )
C E12 = 0.3
C RETURN
C END

```

```

$IBFTC ITF1
C 1ST SURFACE ** COEFF. OF THERMAL EXPANSION, TEMPERATURE
C
C
C
C
FUNCTION TMP1( PFL,ZTA )
C
C
C
ENTRY ALF1( PFL,ZTA )
TMP1 = 0.0
RETURN
END

```

```

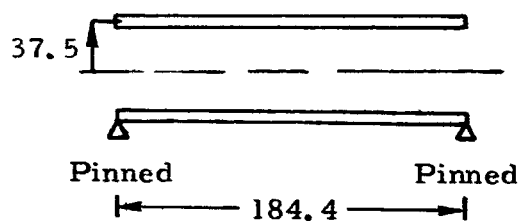
$IBFTC ITF2
C 2ND SURFACE ** COEFF. OF THERMAL EXPANSION, TEMPERATURE
C
C
C
C
FUNCTION TMP2( PFL,ZTA )
C
C
C
ENTRY ALF2( PFL,ZTA )
TMP2 = 0.0
RETURN
END

```

### 3.8 SAMPLE PROBLEM 3

#### 3.8.1 Problem Description

A uniform cylinder under semisinusoidal time dependent loading is considered.



$$\begin{aligned} \nu &= 1/6 \\ a_0 &= 1 \\ h_0 &= 1 \\ E_0 &= 1 \\ \sigma_0 &= 1 \end{aligned}$$

#### Stiffness Parameters

$$BBB = 12.0925 \times 10^6$$

$$DDD = 16.56 \times 10^4$$

Mass properties  $DMM1 = 3.49 \times 10^{-3}$

No thermal loading

No elastic foundation

No external damping

Pressure loading

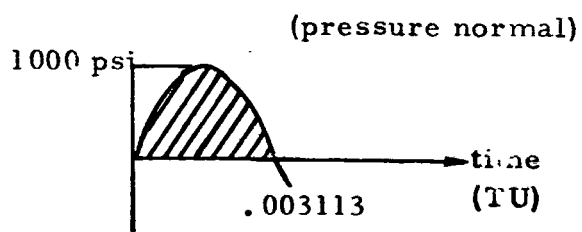
if  $TU < .003113$

$$PPPN = 1000 \sin(1003 TU)$$

if  $TU \geq .003113$

$$PPPN = 0.0$$

$$PPPH = PPPF = 0.0$$





NUMBER	IDENTIFICATION	DESCRIPTION	DO NOT KEY PUNCH
6			
1		ENF	
2		BCIT	
2		BCIB	
- 1	73	PFLAG	
3	1 1	CEXT	
1 1			
5	- 4	DELT	
	73		
	1 2		
			GMDA, Geometry Data
1		GIN (cylinder)	
1 1		EN	
3 7	73	RAI	
5			
1 8 4	2 0	AXL	ANX = 0.
4			
	73		
	80		

### 3.8.3. Function Subprograms Used

```
$IRFTC DRBDD
C
C STIFFNESS FUNCTION
C
C FUNCTION BRRT (PFL,ZTA )
C
C BRB = 12.0925E+6
C RETURN
C
C ENTRY DDD ( ZTA )
C BRB = 16.56E+4
C RETURN
C END
```

```
$IRFTC DTMP
C
C TEMPERATURE FUNCTION
C
C FUNCTION FMTT (PFL,ZTA )
C
C ENTRY EMTT ( PFL,ZTA )
C FMTT = 0.
C RETURN
C END
```

```

$IBFIC DKDMP          00000011
C          00000019
C          00000319
C          00000520
C          00000021
C          00000120
C          00000219
C          00000220
C          00000319
C          00000320
C          00000419
C          00000420
C          00000519
C          00000520
C          00000610
C          00000999

```

SPRING AND DAMPING FUNCTION

```

FUNCTION DKK1( PEL,ZTA )
ENTRY DKK2( PEL,ZTA )
ENTRY DKK3( PEL,ZTA )
ENTRY DMP1( PEL,ZTA )
ENTRY DMP2( PEL,ZTA )
ENTRY DMP3( PEL,ZTA )
DKK1 = 0.
RETURN
END

```

```

$IBFIC DMASS          00000001
C          00000019
C          00000020
C          00000021
C          00000100
C          00000110
C          00000119
C          00000120
C          00000200
C          00000210
C          00000900

```

MASS FUNCTION

```

FUNCTION DMM1( PEL,ZTA )
DMM1 = 3.4900886E-3
RETURN
ENTRY DMM4( PEL,ZTA )
DMM1 = 0.
RETURN
END

```

\$IBFTC DPRSS	00000001
C	00000019
C	00000020
C	00000021
	00000030
	00000040
	00000050
	00000100
	00000110
	00000119
	00000120
	00000200
	00000210
	00000219
	00000220
	00000300
	00000310
	00000999

PRESSURE FUNCTION

```

FUNCTION PPPN( PEL,ZTA,TU)
IF(TU.LT. 3.113E-3) GO TO 5
PPPN = 0.
GO TO 10
5 PPPN = 1000. * SIN(1003. * TU)
10 RETURN
C
ENTRY PPPH( PEL,ZTA,TU )
PPPN = 0.
RETURN
C
ENTRY PPPF( PEL,ZTA,TU )
PPPN = 0.
RETURN
END

```



3.8.4 Output

TRANSIENT RESPONSE OF SIMPLY SUPPORTED CYLINDER TO UNIFORM

\* \* \* SHENG

SINUSOIDAL PULSE

\* \* \*

GENERAL DATA

AN = 1.0000E 00    MO = 1.0000E 00    EO = 1.0000E 00    SIGN = 1.0000E 00  
 PDI = 1.6670E-01    ENF = 1.0000E 00    BCIV = 2.0000E 00    BCIB = 2.0000E 00  
 PFLAG = -1.0000E 00    CEXT = 3.0000E 00    DELT = 5.0000E-04

PRINT ANGLES (TTT) -

0.0000E-39 -1.0000E 10 -1.0000E 10 -1.0000E 10 -1.0000E 10 -1.0000E 10

FOURIER HARMONIC PRINTS (FPRINT) -

1.0000E 00 -1.0000E 10 -1.0000E 10 -1.0000E 10

BOUNDARY MATRICES

TOP BOUNDARY \*\*

OMEGA  
 0.0000000E-39    0.0000000E-39    0.0000000E-39    0.0000000E-39  
 0.0000000E-39    0.0000000E-39    0.0000000E-39    0.0000000E-39  
 0.0000000E-39    0.0000000E-39    0.0000000E-39    0.0000000E-39  
 0.0000000E-39    0.0000000E-39    1.0000000E 00    0.0000000E-39  
 0.0000000E-39    0.0000000E-39    0.0000000E-39    1.0000000E 00

LAMBDA  
 1.0000000E 00    0.0000000E-39    0.0000000E-39    0.0000000E-39  
 0.0000000E-39    1.0000000E 00    0.0000000E-39    0.0000000E-39  
 0.0000000E-39    0.0000000E-39    1.0000000E 00    0.0000000E-39  
 0.0000000E-39    0.0000000E-39    0.0000000E-39    1.0000000E-39

L -  
 0.0000000E-39    0.0000000E-39    0.0000000E-39    0.0000000E-39

BOTTOM BOUNDARY \*\*

OMEGA

0.000000E-39	0.000000E-39	0.000000E-39	0.000000E-39	0.000000E-39
0.000000E-39	0.000000E-39	0.000000E-39	0.000000E-39	0.000000E-39
0.000000E-39	0.000000E-39	0.000000E-39	0.000000E-39	0.000000E-39
0.000000E-39	0.000000E-39	0.000000E-39	0.000000E-39	0.000000E-39
0.000000E-39	0.000000E-39	0.000000E-39	0.000000E-39	0.000000E-39

LAMSDA

0.000000E-39	0.000000E-39	0.000000E-39	0.000000E-39	0.000000E-39
0.000000E-39	0.000000E-39	0.000000E-39	0.000000E-39	0.000000E-39
0.000000E-39	0.000000E-39	0.000000E-39	0.000000E-39	0.000000E-39
0.000000E-39	0.000000E-39	0.000000E-39	0.000000E-39	0.000000E-39
0.000000E-39	0.000000E-39	0.000000E-39	0.000000E-39	0.000000E-39

L -

0.000000E-39	0.000000E-39	0.000000E-39	0.000000E-39	0.000000E-39
--------------	--------------	--------------	--------------	--------------

"REPRODUCIBILITY OF THE ORIGINAL PAGE IS POOR."

GEOMETRY DATA FOR CONE - CYLINDER

NUMBER OF STATIONS - 11

RAI = 3.7500E 01    AXL = 1.8440E 02    ANX = 0.0000E-39

DEL = 1.8440E 01

I	R(I)	XI(I)	W(THETA)	W(XI)	RHOX(I)	GAMA(I)
1	3.750000E 01	0.000000E-39	2.6666667E-02	0.000000E-39	3.750000E 01	0.000000E-39
2	3.750000E 01	1.844000E 01	2.6666667E-02	0.000000E-39	3.750000E 01	0.000000E-39
3	3.750000E 01	3.688000E 01	2.6666667E-02	0.000000E-39	3.750000E 01	0.000000E-39
4	3.750000E 01	5.5319999E 01	2.6666667E-02	0.000000E-39	3.750000E 01	0.000000E-39
5	3.750000E 01	7.3759998E 01	2.6666667E-02	0.000000E-39	3.750000E 01	0.000000E-39
6	3.750000E 01	9.2199998E 01	2.6666667E-02	0.000000E-39	3.750000E 01	0.000000E-39
7	3.750000E 01	1.106400E 02	2.6666667E-02	0.000000E-39	3.750000E 01	0.000000E-39
8	3.750000E 01	1.290800E 02	2.6666667E-02	0.000000E-39	3.750000E 01	0.000000E-39
9	3.750000E 01	1.4751999E 02	2.6666667E-02	0.000000E-39	3.750000E 01	0.000000E-39
10	3.750000E 01	1.6595999E 02	2.6666667E-02	0.000000E-39	3.750000E 01	0.000000E-39
11	3.750000E 01	1.8439999E 02	2.6666667E-02	0.000000E-39	3.750000E 01	0.000000E-39





CHECKPRINT OF LOAD COEFF. STORED IN GROUPS OF ALL ENF PER MERIDIONAL STATION. THE COEFFICIENTS ARE PFF, PTH, PN (IN THAT ORDER) AND ARE SEPARATED FROM EACH OTHER BY ..... FIELDS.

FOR STATION 1 THROUGH STATION 11

0.0000000E-39	0.0000000E-39	0.0000000E-39	0.0000000E-39	0.0000000E-39	0.0000000E-39
0.0000000E-39	0.0000000E-39	0.0000000E-39	0.0000000E-39	0.0000000E-39	0.0000000E-39
.....	.....	.....	.....	.....	.....
0.0000000E-39	0.0000000E-39	0.0000000E-39	0.0000000E-39	0.0000000E-39	0.0000000E-39
4.8074125E 02	4.8074125E 02	4.8074125E 02	4.8074125E 02	4.8074125E 02	4.8074125E 02
4.8074125E 02	4.8074125E 02	4.8074125E 02	4.8074125E 02	4.8074125E 02	4.8074125E 02

\*Z\* MATRIX FOR STATION 11

0.000000E-39 0.000000E-39 0.000000E-39 1.8837273E-04 0.000000E-39

\*Z\* MATRIX FOR STATION 10

-5.4071139E-05 -0.000000E-39 4.7842581E-03 1.4433218E-04 -0.000000E-39

\*Z\* MATRIX FOR STATION 9

-1.7326856E-05 -0.000000E-39 5.3232849E-03 1.2210523E-05 -0.000000E-39

\*Z\* MATRIX FOR STATION 8

-2.9512694E-06 -0.000000E-39 5.2341661E-03 -3.2122134E-06 -0.000000E-39

\*Z\* MATRIX FOR STATION 7

-3.8498865E-07 -0.000000E-39 5.2047550E-03 -8.4332169E-07 -0.000000E-39

\*Z\* MATRIX FOR STATION 6

-9.0949470E-13 -0.000000E-39 5.2030697E-03 -1.8189894E-12 -0.000000E-39

\*Z\* MATRIX FOR STATION 5

3.8498592E-07 -0.000000E-39 5.2047549E-03 8.4332896E-07 -0.000000E-39



\*Z\* MATRIX FOR STATION 4

2.9512657E-04 -0.0000000E-39 5.2341662E-03 3.2122225E-06 -0.0000000E-39

\*Z\* MATRIX FOR STATION 3

1.7326853E-05 -0.0000000E-39 5.3232850E-03 -1.2210519E-05 -0.0000000E-39

\*Z\* MATRIX FOR STATION 2

5.4073140E-05 -0.0000000E-39 4.7842582E-03 -1.4433218E-04 -0.0000000E-39

\*Z\* MATRIX FOR STATION 1

-8.5192534E-05 -0.0000000E-39 -6.9652297E-06 1.7655379E-03 0.0000000E-39

STATION 11

THETA = 0.00

ENF = 0.0

0.000000E-39      U      0.000000E-39      V      0.000000E-39      W      0.000000E-39      PHI(XI)      1.8837273E-04      PHI(THETA)      0.000000E-39

STATION 10

THETA = 0.00

ENF = 0.0

-5.4073139E-05      U      -0.000000E-39      V      4.7842581E-03      W      0.000000E-39      PHI(XI)      1.4433218E-04      PHI(THETA)      -0.000000E-39

STATION 9

THETA = 0.00

ENF = 0.0

0.000000E-39      U      0.000000E-39      V      0.000000E-39      W      0.000000E-39      PHI(XI)      0.000000E-39      PHI(THETA)      0.000000E-39

-1.7326856E-05    -0.0000000E-39    5.3232849E-03    1.2210523E-05    -0.0000000E-39

STATION = 8

THETA = 0.00

ENF = 0.0

-2.9512694E-06    U    -0.0000000E-39    V    5.2341661E-03    W    5.2341661E-03    PHI(XI)    PHI(THETA)    -3.2122134E-06    -0.0000000E-39

STATION = 7

THETA = 0.00

ENF = 0.0

-3.8498865E-07    U    -0.0000000E-39    V    5.2047550E-03    W    5.2047550E-03    PHI(XI)    PHI(THETA)    -8.4332169E-07    -0.0000000E-39

STATION = 6

THETA = 0.00

ENF = 0.0

U V W PHI(XI) PHI(THETA)  
-9.0949470E-13 -0.0000000E-39 5.2030697E-03 -1.8189894E-12 -0.0000000E-39

STATION 5

THETA = 0.00

ENF = 0.0

U V W PHI(XI) PHI(THETA)  
3.8498592E-07 -0.0000000E-39 5.2047549E-03 8.4332896E-07 -0.0000000E-39

STATION 4

THETA = 0.00

ENF = 0.0

U V W PHI(XI) PHI(THETA)  
2.9512657E-06 -0.0000000E-39 5.2341662E-03 3.2122225E-06 -0.0000000E-39

STATION 3

THETA = 0.00

ENF = 0.0

U 1.7326853E-05 V -0.0000000E-39 W 5.3232850E-03 PHI(XI) -1.2210519E-05 PHI(THETA) -0.0000000E-39

STATION 2

THETA = 0.00

ENF = 0.0

U 5.4073140E-05 V -0.0000000E-39 W 4.7842582E-03 PHI(XI) -1.433218E-04 PHI(THETA) -0.0000000E-39

STATION 1

THETA = 0.00

ENF = 0.0

U -8.5192534E-05 V -0.0000000E-39 W -6.9652297E-06 PHI(XI) 1.7655379E-03 PHI(THETA) 0.0000000E-39

STATION 11

N(XI) N(THETA) Q(XI) Q(THETA)  
 6.5276389E 01 1.0875239E 01 -9.3807093E 02  
 M(XI) M(THETA) M(XI, THETA) M(XI, THETA)  
 -8.1676997E -08 -1.3615547E -08 0.0000000E -39 0.0000000E -39

STATION 10

N(XI) N(THETA) Q(XI) Q(THETA)  
 2.6285587E 02 1.5437102E 03 -4.2890719E -02  
 M(XI) M(THETA) M(XI, THETA) M(XI, THETA)  
 7.9101014E -01 1.3186140E -01 0.0000000E -39 0.0000000E -39

STATION 9

N(XI) N(THETA) Q(XI) Q(THETA)  
 2.6939186E 02 1.7137870E 03 5.6839940E -02  
 M(XI) M(THETA) M(XI, THETA) M(XI, THETA)  
 6.6250940E -01 1.1044032E -01 0.0000000E -39 0.0000000E -39

STATION 8

N(XI) N(THETA) Q(XI) Q(THETA)  
 2.7587846E 02 1.6869174E 03 8.6695042E -03  
 M(XI) M(THETA) M(XI, THETA) M(XI, THETA)

5.8614855E-02 9.7710979E-03 0.0000000E-39 0.0000000E-39

STATION 7

N(XI) N(THETA) Q(XI) Q(THETA)  
2.7818148E 02 1.6781980E 03 0.0000000E-39 -7.2527718E-04  
M(XI) M(THETA) Q(XI) Q(THETA)  
-1.4423594E-02 -2.4044130E-03 0.0000000E-39 0.0000000E-39

STATION 6

N(XI) N(THETA) Q(XI) Q(THETA)  
2.7943943E 02 1.6777718E 03 0.0000000E-39 6.739327E-06  
M(XI) M(THETA) Q(XI) Q(THETA)  
-7.5734623E-03 -1.2624962E-03 0.0000000E-39 0.0000000E-39

STATION 5

N(XI) N(THETA) Q(XI) Q(THETA)  
2.7818148E 02 1.6781980E 03 0.0000000E-39 7.5393842E-04  
M(XI) M(THETA) Q(XI) Q(THETA)  
-1.4423651E-02 -2.4044226E-03 0.0000000E-39 0.0000000E-39

STATION 4

N(XI) N(THETA) Q(XI) Q(THETA)  
2.7580848E 02 1.6869174E 03 0.0000000E-39 -8.6554708E-03

M(XI) M(THETA) M(XI,THETA) Q(THETA)  
5.8614882E-02 9.7711007E-03 0.0000000E-39 0.0000000E-39

STATION 3

N(XI) N(THETA) N(XI,THETA) Q(XI)  
2.6935936E 02 1.7136088E 03 0.0000000E-39 -5.6823896E-02

M(XI) M(THETA) M(XI,THETA) Q(THETA)  
6.6250543E-01 1.1044032E-01 0.0000000E-39 0.0000000E-39

STATION 2

N(XI) N(THETA) N(XI,THETA) Q(XI)  
2.9079345E 02 1.5483667E 03 0.0000000E-39 9.9445981E-01

M(XI) M(THETA) M(XI,THETA) Q(THETA)  
-7.9825127E 00 -1.3306849E 00 0.0000000E-39 0.0000000E-39

STATION 1

N(XI) N(THETA) N(XI,THETA) Q(XI)  
1.4866468E 02 2.2598750E 01 0.0000000E-39 1.0785388E 04

M(XI) M(THETA) M(XI,THETA) Q(THETA)  
-2.6320569E 01 -4.3876387E 00 -0.0000000E-39 0.0000000E-39



CHECKPRINT OF LOAD COEF. STORED IN GROUPS OF ALL ENF PER MERIDIONAL STATION. THE COEFFICIENTS ARE PFE, PTH, PN (IN THAT ORDER) AND ARE SEPARATED FROM EACH OTHER BY ..... FIELDS.

FOR STATION 1 THROUGH STATION 11

0.000000E-39	0.000000E-39	0.000000E-39	0.000000E-39	0.000000E-39	0.000000E-39
0.000000E-39	0.000000E-39	0.000000E-39	0.000000E-39	0.000000E-39	0.000000E-39
.....	.....	.....	.....	.....	.....
0.000000E-39	0.000000E-39	0.000000E-39	0.000000E-39	0.000000E-39	0.000000E-39
0.000000E-39	0.000000E-39	0.000000E-39	0.000000E-39	0.000000E-39	0.000000E-39
8.4308790E 02	8.4308790E 02	8.4308790E 02	8.4308790E 02	8.4308790E 02	8.4308790E 02
8.4308790E 02	8.4308790E 02	8.4308790E 02	8.4308790E 02	8.4308790E 02	8.4308790E 02

\*7\* MATRIX FOR STATION 11

0.000000E-39 0.000000E-39 0.000000E-39 1.1038860E-03 0.000000E-39

\*Z\* MATRIX FOR STATION 10

-6.3454623E-04 0.000000E-39 2.5893420E-02 8.6705199E-04 0.000000E-39

\*Z\* MATRIX FOR STATION 9

-3.7170339E-04 0.000000E-39 3.1978566E-02 1.5654976E-04 0.000000E-39

\*Z\* MATRIX FOR STATION 8

-1.3692552E-04 0.000000E-39 3.1565081E-02 -2.2956723E-05 0.000000E-39

\*Z\* MATRIX FOR STATION 7

-3.9743107E-05 0.000000E-39 3.1131263E-02 -1.7755876E-05 0.000000E-39

\*Z\* MATRIX FOR STATION 6

-0.000000E-39 0.000000E-39 3.1010200E-02 2.1877873E-11 0.000000E-39

\*Z\* MATRIX FOR STATION 5

3.9743143E-05 0.000000E-39 3.1131264E-02 1.7755898E-05 0.000000E-39

\*Z\* MATRIX FOR STATION 4  
1.3692557E-04 0.0000000E-39 3.1665081E-02 7.2956723E-05 0.0000000E-39

\*Z\* MATRIX FOR STATION 3  
3.7170340E-04 0.0000000E-39 3.1978566E-02 -1.5654974E-04 0.0000000E-39

\*Z\* MATRIX FOR STATION 2  
6.3454624E-04 -0.0000000E-39 2.5893420E-02 -8.6705197E-04 -0.0000000E-39

\*Z\* MATRIX FOR STATION 1  
-2.1984192E-11 0.0000000E-39 1.1268639E-09 -1.1038859E-03 -0.0000000E-39

STATION 11

THETA = 0.00

ENF = 0.0

0.000000E-39      U      V      W      PHI(XI)      PHI(THETA)

0.000000E-39

0.000000E-39

0.000000E-39

1.1038860E-03

0.000000E-39

STATION 10

THETA = 0.00

ENF = 0.0

-6.3454623E-04      U      V      W      PHI(XI)      PHI(THETA)

0.000000E-39

0.000000E-39

2.5893420E-02

8.6705199E-04

0.000000E-39

STATION 9

THETA = 0.00

ENF = 0.0

U      V      W      PHI(XI)      PHI(THETA)

-3.7170339E-04    0.0000000E-39    3.1978566E-02    1.5654976E-04    0.0000000E-39

STATION    8

THETA = 0.00  
ENF = 0.0  
U    V    W    PHI(XI)    PHI(THETA)  
-1.3692552E-04    0.0000000E-39    3.1665081E-02    -2.2956723E-05    0.0000000E-39

STATION    7

THETA = 0.00  
ENF = 0.0  
U    V    W    PHI(XI)    PHI(THETA)  
-3.9743107E-05    0.0000000E-39    3.1131263E-02    -1.775876E-05    0.0000000E-39

STATION    6

THETA = 0.00  
ENF = 0.0

U -0.0000000E-39 V 0.0000000E-39 W 3.1710200E-02 PHI(XI) 2.1827873E-11 PHI(THETA) 0.0000000E-39

STATION 5

THETA = 0.00  
ENF = 0.0

U 3.9743143E-05 V 0.0000000E-39 W 3.1131264E-02 PHI(XI) 1.7755898E-05 PHI(THETA) 0.0000000E-39

STATION 4

THETA = 0.00  
ENF = 0.0

U 1.3692557E-04 V 0.0000000E-39 W 3.1665081E-02 PHI(XI) 2.2956723E-05 PHI(THETA) 0.0000000E-39

STATION 3

THETA = 0.00  
ENF = 0.0

U 3.7170340E-04 V 0.0000000E-39 W 3.1978566E-02 PHI(XI) -1.5654974E-04 PHI(THETA) 0.0000000E-39

STATION 2

THETA = 0.00

ENF = 0.0

U 6.3454624E-04 V -0.0000000E-39 W 2.5893420E-02 PHI(XI) -8.6705197E-04 PHI(THETA) -0.0000000E-39

STATION 1

THETA = 0.00

ENF = 0.0

U -2.1984192E-11 V 0.0000000E-39 W 1.1268639E-09 PHI(XI) -1.1038859E-03 PHI(THETA) -0.0000000E-39

## STATION 11

N(XI)	N(THETA)	N(XI, THETA)	O(XI)
7.1036246E 02	1.1841742E 02	0.000000E-39	-4.2191703E 03
M(XI)	M(THETA)	M(XI, THETA)	O(THETA)
-5.5540324E-07	-9.2585720E-08	0.000000E-39	-0.000000E-39

## STATION 10

N(XI)	N(THETA)	N(XI, THETA)	O(XI)
1.5137821E 03	8.3700780E 03	0.000000E-39	-2.3069341E-01
M(XI)	M(THETA)	M(XI, THETA)	O(THETA)
4.2537650E 00	7.0910262E-01	0.000000E-39	-0.000000E-39

## STATION 9

N(XI)	N(THETA)	N(XI, THETA)	O(XI)
1.5558496E 03	1.0784818E 04	0.000000E-39	2.5867319E-01
M(XI)	M(THETA)	M(XI, THETA)	O(THETA)
3.9963506E 00	6.6619164E-01	0.000000E-39	-0.000000E-39

## STATION 8

N(XI)	N(THETA)	N(XI, THETA)	O(XI)
1.5933162E 03	1.0192784E 04	0.000000E-39	8.9983445E-02
M(XI)	M(THETA)	M(XI, THETA)	O(THETA)



7.8267372E-01 1.3047171F-01 0.0000000E-39 -0.0000000E-39

STATION 7

N(XI) N(THETA) M(XI,THETA) O(XI)  
1.6285702F 03 1.0031306E 04 0.0000000F-39 6.1373189E-03  
M(XI) M(THETA) M(XI,THETA) O(THETA)  
-1.0308124E-01 -1.7183643E-02 0.0000000F-39 -0.0000000F-39

STATION 6

N(XI) N(THETA) M(XI,THETA) O(XI)  
1.6408960E 03 9.9954070E 03 0.0000000E-39 6.6360177E-05  
M(XI) M(THETA) M(XI,THETA) O(THETA)  
-1.5945630E-01 -2.6581365E-02 0.0000000F-39 -0.0000000E-39

STATION 5

N(XI) N(THETA) M(XI,THETA) O(XI)  
1.6285702E 03 1.0031307E 04 0.0000000E-39 -6.023427E-03  
M(XI) M(THETA) M(XI,THETA) O(THETA)  
-1.0308104E-01 -1.7183610E-02 0.0000000E-39 -0.0000000E-39

STATION 4

N(XI) N(THETA) M(XI,THETA) O(XI)  
1.5933164E 03 1.0192785E 04 0.0000000E-39 -8.9919292E-02

M(XI) M(THETA) Q(THETA)  
7.8267372E-01 1.3047171E-01 0.0000000E-39

STATION 3

N(XI) N(THETA) Q(XI)  
1.5556607E 03 1.0283748E 04 0.0000000E-39

M(XI) M(THETA) Q(THETA)  
3.9963505E 00 6.6619163E-01 0.0000000E-39

STATION 2

N(XI) N(THETA) Q(XI)  
1.5137822E 03 8.3700781E 03 2.3058344E-01

M(XI) M(THETA) Q(THETA)  
4.2537646E 00 7.0910256E-01 0.0000000E-39

STATION 1

N(XI) N(THETA) Q(XI)  
7.1036217E 02 1.184174E 02 4.2191705E 03

M(XI) M(THETA) Q(THETA)  
-1.4375143E-06 -2.3963362E-07 0.0000000E-39

CHECKPRINT OF LOAD COEF. STORED IN GROUPS OF ALL ENF PER MERIDIONAL STATION. THE COEFFICIENTS ARE PFE, PTH, PN (IN THAT ORDER) AND ARE SEPARATED FROM EACH OTHER BY ..... FIELDS.

FOR STATION 1 THROUGH STATION 11

0.0000000E-39	0.0000000E-39	0.0000000E-39	0.0000000E-39	0.0000000E-39
0.0000000E-39	0.0000000E-39	0.0000000E-39	0.0000000E-39	0.0000000E-39
.....	.....	.....	.....	.....
0.0000000E-39	0.0000000E-39	0.0000000E-39	0.0000000E-39	0.0000000E-39
0.0000000E-39	0.0000000E-39	0.0000000E-39	0.0000000E-39	0.0000000E-39
9.9780282E 02	9.9780282E 02	9.9780282E 02	9.9780282E 02	9.9780282E 02
9.9780282E 02	9.9780282E 02	9.9780282E 02	9.9780282E 02	9.9780282E 02

\*Z\* MATRIX FOR STATION 11  
0.000000E-39 0.000000E-39 0.000000E-39 2.7384748E-03 0.000000E-39

\*Z\* MATRIX FOR STATION 10  
-2.180071E-03 0.000000E-39 6.0952131E-02 2.1914625E-03 0.000000E-39

\*Z\* MATRIX FOR STATION 9  
-1.5983047E-03 0.000000E-39 8.0825035E-02 5.5042525E-04 0.000000E-39

\*Z\* MATRIX FOR STATION 8  
-7.3723757E-04 0.000000E-39 8.1248075E-02 -4.1839783E-05 0.000000E-39

\*Z\* MATRIX FOR STATION 7  
-2.5419031E-04 0.000000E-39 7.9279975E-02 -7.0573849E-05 0.000000E-39

\*Z\* MATRIX FOR STATION 6  
-0.000000E-39 0.000000E-39 7.8644956E-02 1.1641532E-10 0.000000E-39

\*Z\* MATRIX FOR STATION 5  
2.5419041E-04 0.000000E-39 7.9279978E-02 7.0573937E-05 0.000000E-39

-----  
Z MATRIX FOR STATION 4

7.3723778E-04    0.0000000E-39    8.1248075E-02    4.1839696E-05    0.0000000E-39

-----  
Z MATRIX FOR STATION 3

1.5983048E-03    0.0000000E-39    8.0825035E-02    -5.5042517E-04    0.0000000E-39

-----  
Z MATRIX FOR STATION 2

2.1800072E-03    -0.0000000E-39    6.0952132E-02    -2.1914624E-03    -0.0000000E-39

-----  
Z MATRIX FOR STATION 1

-4.993643E-11    0.0000000E-39    4.3257842E-09    -2.7384744E-03    -0.0000000E-39

-----  
-----  
-----  
-----

STATION 11

THETA = 0.00

ENF = 0.0

U 0.0000000E-39 V 0.0000000E-39 W 0.0000000E-39 PHI(XI) 2.7384748E-03 PHI(THETA) 0.0000000E-39

STATION 10

THETA = 0.00

ENF = 0.0

U -2.1800071E-03 V 0.0000000E-39 W 6.0952131E-02 PHI(XI) 2.1914625E-03 PHI(THETA) 0.0000000E-39

STATION 9

THETA = 0.00

ENF = 0.0

U PHI(XI) PHI(THETA)

-1.5983047E-03    0.0000000E-39    8.0825035E-02    5.5042525E-04    0.0000000E-39

STATION    8

THETA = 0.00

ENF = 0.0

-7.3723757E-04    U    0.0000000E-39    V    8.1248075E-02    W    -4.1839783E-05    PHI(XI)    PHI(THETA)    0.0000000E-39

STATION    7

THETA = 0.00

ENF = 0.0

-2.5419031E-04    U    0.0000000E-39    V    7.9279975E-02    W    -7.0573849E-05    PHI(XI)    PHI(THETA)    0.0000000E-39

STATION    6

THETA = 0.00

ENF = 0.0

U -0.000000E-39 V 0.000000E-39 W 7.8644956E-02 PHI(XI) 1.1641532E-10 PHI(THETA) 0.000000E-39

STATION 5

THETA = 0.00  
ENF = 0.0

U 2.5419041E-04 V 0.000000E-39 W 7.9279978E-02 PHI(XI) 7.0573937E-05 PHI(THETA) 0.000000E-39

STATION 4

THETA = 0.00  
ENF = 0.0

U 7.3723778E-04 V 0.000000E-39 W 8.1248075E-02 PHI(XI) 4.1839696E-05 PHI(THETA) 0.000000E-39

STATION 3

THETA = 0.00  
ENF = 0.0



U 1.5993048E-03 V 0.0000000E-39 W 8.0825035E-02 PHI(XI) -5.5042517E-04 PHI(THETA) 0.0000000E-39

STATION 2

THETA = 0.00  
ENF = 0.0

U 2.180072E-03 V -0.0000000E-39 W 6.0952132E-02 PHI(XI) -2.1914624E-03 PHI(THETA) -0.0000000E-39

STATION 1

THETA = 0.00  
ENF = 0.0

U -4.9936943E-11 V 0.0000000E-39 W 4.3257842E-09 PHI(XI) -2.7384744E-03 PHI(THETA) -0.0000000E-39

STATION 11

N(XI) 2.3351250E 03 N(THETA) 3.8926534E 02 Q(XI) -8.4685251E 03  
 M(XI) -1.6335390E -06 M(THETA) -2.7231094E -07 M(XI,THETA) 0.0000000E -39

M(XI) -1.6335390E -06 M(THETA) -2.7231094E -07 Q(THETA) -0.0000000E -39

STATION 10

N(XI) 3.8005566E 03 N(THETA) 1.9742384E 04 Q(XI) -5.3272472E -01  
 M(XI) 9.8248624E 00 M(THETA) 1.6378045E 00 M(XI,THETA) 0.0000000E -39

M(XI) 9.8248624E 00 M(THETA) 1.6378045E 00 Q(THETA) -0.0000000E -39

STATION 9

N(XI) 3.8716973E 03 N(THETA) 2.5984509E 04 Q(XI) 5.1087612E -01  
 M(XI) 1.0028058E 01 M(THETA) 1.5716772E 00 M(XI,THETA) 0.0000000E -39

M(XI) 1.0028058E 01 M(THETA) 1.5716772E 00 Q(THETA) -0.0000000E -39

STATION 8

N(XI) 3.9250056E 03 N(THETA) 2.6126317E 04 Q(XI) 2.7448915E -01  
 M(XI) M(THETA) M(XI,THETA) Q(THETA)

2.7884335E 00 4.6493187E-01 -0.0000000E-39

STATION 7

N(XI) N(THETA) Q(XI)  
 4.0199776E 03 2.5524842E 04 4.8591152E-02

M(XI) M(THETA) Q(THETA)  
 -1.8787109E-01 -3.1318111E-02 -0.0000000E-39

STATION 6

N(XI) N(THETA) Q(XI)  
 4.060813E 03 2.5332579E 04 2.0484360E-04

M(XI) M(THETA) Q(THETA)  
 -6.3378710E-01 -1.0565231E-01 -0.0000000E-39

STATION 5

N(XI) N(THETA) Q(XI)  
 4.0199776E 03 2.5524843E 04 -4.8151247E-02

M(XI) M(THETA) Q(THETA)  
 -1.8786965E-01 -3.1317871E-02 -0.0000000E-39

STATION 4

N(XI) N(THETA) Q(XI)  
 3.9267862E 03 2.6126318E 04 -2.7442041E-01

M(XI) M(THETA) M(XI,THETA) Q(THETA)  
 2.7884336E 00 4.6483188E-01 0.0000000E-39 -0.0000000E-39

STATION 3

N(XI) N(THETA) N(XI,THETA) Q(XI)  
 3.8712259E 03 2.5981806E 04 0.0000000E-39 -5.1056799E-01

M(XI) M(THETA) M(XI,THETA) Q(THETA)  
 1.0028057E 01 1.6716771E 00 0.0000000E-39 -0.0000000E-39

STATION 2

N(XI) N(THETA) N(XI,THETA) Q(XI)  
 3.8005567E 03 1.9742384E 04 0.0000000E-39 5.3257809E-01

M(XI) M(THETA) M(XI,THETA) Q(THETA)  
 9.8248610E 00 1.6378043E 00 0.0000000E-39 0.0000000E-39

STATION 1

N(XI) N(THETA) N(XI,THETA) Q(XI)  
 2.3351237E 03 3.8926515E 02 0.0000000E-39 8.4685262E 03

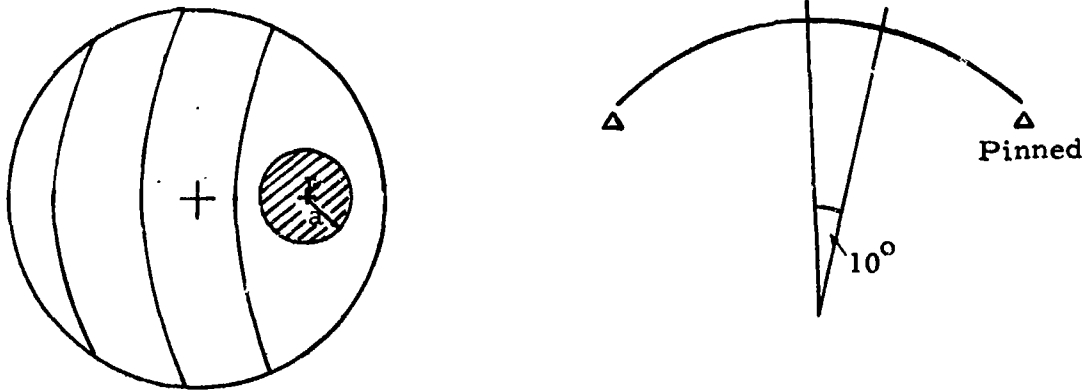
M(XI) M(THETA) M(XI,THETA) Q(THETA)  
 -4.7045922E-06 -7.8425551E-07 0.0000000E-39 -0.0000000E-39

END EXECUTION 37  
 D06961FURUKI R302517-11 980 00-09-20 03/03/77  
 JOB TOTALS= \*\*PRINTING= 228 LINES \*\*PUNCHING= 7 CARDS \*\*CRT= 00000-35MM 00000-9INCH

### 3.9 SAMPLE PROBLEM 4

#### 3.9.1 Problem Description

The Apollo-like shell of sample problem 1, Section 3.7 is now subjected to hydrodynamic pressures compacted from a rigid shell solution.



All the input parameters are the same as sample problem 1 except for the subroutine describing pressures.

$V_o = 360 \text{ in./s}$	Initial impact velocity
$R_c = 175.6 \text{ in.}$	Radius of curvature
$\rho_w = 62.5/17280 \text{ \#/in.}^3$	Fluid density
$W_T = 10,000$	Weight of body

inside wetted region

$$PPPN = \frac{\sqrt{2} \rho_w V_o^{3/2} R_c^{1/2} \left[ 1 - \gamma (2 - 3r^2/a^2) \right]}{\pi t^{1/2} (1 - r^2/a^2)^{1/2} (1 + \gamma)^2}$$

where

$$t = \frac{1}{R_c V_o} \left( \frac{3W_T}{4\sqrt{2} \rho_w} \right)^{2/3}, \quad \gamma = \frac{8\sqrt{2} \rho_w (R_c V_o t)^{3/2}}{3W_T}$$

outside wetted region

$$PPPN = 0.0$$

also

$$PPPH = PPPF = 0.0$$

The mass properties of the Apollo-like shell.

$$DMM1 = 1.4648 \times 10^{-3}(t_f) + 4.7443 \times 10^{-5}$$

where

$$A = \xi^2 + 5625 - 2(75)\xi \cos \theta$$

$$A < 4225 \quad t_f = 0.05$$

$$4225 < A < 7225 \quad t_f = 0.03$$

$$7225 < A < 11025 \quad t_f = 0.02$$

$$A > 11025 \quad t_f = 0.012$$



DECK NO.	PROGRAMMER	IDENTIFICATION	DATE	PAGE 2 of 2	JOB NO.
NUMBER			DESCRIPTION	DO NOT KEY PUNCH	
6			ENF (No. of Fourier harmonics)	GDA, continued	
1			BCIT (Closed apex)		
1			BCIB (Pinned)		
2			PFLAG		
- 1			CEXT (No. of time cycles)		
6		1 1			
1 1			DELT (Time increment)		
5		- 4			
			THT & FPRNT are set by the program.	GMDA, Geometry Data	
1		1 2			
2			GIN (Sphere)		
2 6			EN (No. of stations)		
1 7 6			RC		
			RFF		
1 9 . 2			PHIN	(PHIO = 0.0)	



3.9.3 Function Subprogram Used

```

$IBFTC DRGDD 00000001
C 00000010 APOLLO SHELL
C 00000011
C 00000015
C 00000019
C 00000020
C 00000029
C 00000030
C 00000040
C 00000050
C 00000059
C 00000060
C 00000070
C 00000080
C 00000089
C 00000090
C 00000100
C 00000110
C 00000119
C 00000120
C 00000130
C 00000140
C 00000149
C 00000150
C 00000160
C 00000170
C 00000179
C 00000180
C 00000189
C 00000190
C 00000199
C 00000200
C 00000209
C 00000210
C 00000999
C 00001009
C 00001010

FUNCTION BRB (PFL,ZTA)
A = PFL * PFL + 5625. - 150. * PFL * COS( ZTA )
IF (A .LE. 4225.) GO TO 20
IF (A .LF. 7225.) GO TO 30
IF (A .LF. 11025.) GO TO 35
K = 1
10 BRB = 0.79116E6
GO TO 100
C
20 K = 2
25 BRB = 3.296E6
GO TO 100
C
30 K = 3
BRB = 1.9779E6
GO TO 100
C
35 K = 4
40 BRB = 1.386E6
GO TO 100
C
ENTRY DDD (ZTA)
IF (K - 2) 10, 25, 50
50 IF (K .GT. 3) GO TO 40
BRB = 1.9779E6
100 RETURN
C
END
    
```

```

$IRFTC DTMP          00000001
C          TEMPERATURE FUNCTION 00000000
C          FUNCTION FNTT( PEL,ZTA ) 00000019
C          00000020 00000021
C          00000119 00000120
C          ENTRY EMTT( PEL,ZTA ) 00000200
          FNTT = 0.
          RETURN
          END

```

```

$IRFTC DKDMP          00000001
C          SPRING AND DAMPING FUNCTION 00000000
C          00000019 00000020
C          FUNCTION DKKI( PEL,ZTA ) 00000021
C          ENTRY DKK1( PEL,ZTA ) 00000120
C          00000219 00000220
C          ENTRY DKK3( PEL,ZTA ) 00000319
C          00000320 00000419
C          ENTRY DMP1( PEL,ZTA ) 00000420
C          00000519 00000520
C          ENTRY DMP3( PEL,ZTA )
          DKK1 = 0.
          RETURN
          END

```

```

$IRFTC DMOSS             00000001
C                         MASS FUNCTION
C                         APOLLO SHELL
C                         00000010
C                         00000019
C                         00000020
C                         00000021
C                         00000125
C                         00000129
C                         00000130
C                         00000132
C                         00000134
C                         00000139
C                         00000140
C                         00000145
C                         00000149
C                         00000150
C                         00000155
C                         00000159
C                         00000160
C                         00000165
C                         00000169
C                         00000170
C                         00000180
C                         00000210
C                         00000219
C                         00000220
C                         00000300
C                         00000310
C                         00000999

FUNCTION DMM1( PFL,ZTA )
A = PFL * PEL + 5625. - 150. * PEL * COS( ZTA )

IF (A .LF. 4225.) GO TO 20
IF (A .LF. 7225.) GO TO 30
IF (A .LF. 11025.) GO TO 40

TF = .012
GO TO 100

C
20 TF = .05
GO TO 100

C
30 TF = .03
GO TO 100

C
40 TF = .02
100 DMM1 = 1.4648033E-3 * TF + 4.7443145E-5
RETURN
C
ENTRY DMM4( PFL,ZTA )
DMM1 = 0.
RETURN
END
    
```

```

00000005
C PRESSURE FUNCTION ** RIGID BODY HYDRODYNAMICS PRESSURE ** 00000010
C 0000014
C FUNCTION PPPN (PFL,ZTA,TU) 00000015
C 00000016
C COMMON GDA(25), DFL 00000020
C 00000021
C UNSYMMETRIC PRESSURE CASE * 10 DEGREE OFFSET * 00000022
C 00000023
C CONSTANTS SFT TO APOLLO IMPACT CASE 00000024
C 00000020
C VIN INITIAL IMPACT VELOCITY, IN /SEC 00000030
C VIN = 360.0 00000034
C R RADIUS OF CURVATURE 00000035
C R = 175.6 00000039
C RHO FLUID DENSITY, LBS /CU IN 00000040
C RHO = 62.5 /178.0 00000044
C WT WEIGHT OF BODY, LBS 00000045
C 00000045
C 00000099
C RMAX = SQRT (2.0 * TU * R * VIN) 00000100
C A3 = 1.3333 * RHO * RMAX **3 /WT 00000110
C BAF = A3 + 1.0 00000120
C A1 = 2.0 * R * VIN **2 * RHO / (3.1415927 * RMAX * 386.4 *RAF**2) 00000130
C A = 2.0 * RHO * RMAX **3 /WT 00000140
C B = A1 * RMAX * (1.0 - 4.0 * A /3.0) 00000150
C SII = RMAX - DFL 00000160
C SI = SQRT (DFL **2 + 929.762 - 60.984 * PFL * COS(ZTA)) 00000170
C ROC = SI /RMAX 00000180
C 00000189
C IF(SI.GT. RMAX) GO TO 40 00000190
C 00000199
C IF(SI.LT. RMAX .AND. SI.GT. SII) GO TO 30 0000200
C 0000209
C 20 PPPN = -A1 * (1.0 - A1 * (2.0 - 3.0 * ROC **2)) /SQRT(1.0 - ROC**2) 0000210
C GO TO 50 0000220
C 0000227
C WETTED BOUNDARY, PRESSURE AVERAGED OVER DEL 0000228
C 0000229
C 30 RORM = SII /RMAX 0000230
C PPPN = -B * ((1.0 + A) * 3.1415927 /2.0 - ((1.0 + A) * ARSIN 0000240
C 1 (RORM) - A * RORM * SQRT(1.0 - RORM **2))) /DFL 0000241
C GO TO 50 0000250
C 0000259

```

"REPRODUCIBILITY OF THE ORIGINAL PAGE IS POOR;"

40	PPPN = 0.0	00000260
		00000269
50	RETURN	00000270
		00000279
		00000280
		00000290
		00000300
		00000309
		00000310
		00000320
		00000330
		00000500

	ENTRY PPPH (PFL,ZTA,TU)	
	PPPN = 0.0	
	RETURN	

	ENTRY PPF (PFL,ZTA,TU)	
	PPPN = 0.0	
	RETURN	
	FND	

### 3.10 ERROR INDICATIONS, PITFALLS, RECOMMENDATIONS

Several of the error indications resulting from improper data input have already been discussed. To reiterate, they were:

1. A bad index on a DECRD card (Section 3.5.1)
2. Omission of the negative sign on the last card of a data array (Section 3.5.1)
3. Omission of some or all of the title cards (Section 3.3.1).

One should be very careful to check the output from the program to see that it corresponds to the input that he entered. Better yet, an independent check of input data may prevent a wasted run on the digital computer.

The amount of data entered by the DECRD routine is relatively small but such things as sign convention, angle measurements, and compatibility of units are common pitfalls.

Many of the needed parameters are supplied to the program by use of FUNCTION subprograms. Before writing such subprograms, Section 3.4, 3.6.3, 3.7.3, 3.8.3 and 3.9.3 should be studied. A check list is given below.

1. Are the FUNCTION and ENTRY names spelled the same as those given in the table of Section 3.4?
2. Does the number of arguments agree with the number in the calling program? Note that ENTRY DDD has just one argument, (ZTA), and the pressure functions for the Dynamics version require the added argument TU.
3. Has the FUNCTION name been used to return the function value to the calling program even when reference was made to an ENTRY name?
4. Does the FUNCTION subprogram contain at least one RETURN statement and an END statement?
5. If additional data were needed to define the function have the data cards been included with the data deck?

3.11 PROGRAM LISTINGS FOR STATIC VERSION

3.11a Main Program

```

00000017
00000020
00000030
00000040
00000050
00000060
00000070
00000080
00000090
00000100
00000110
00000120
00000130
00000140
00000150
00000160
00000170
00000180
00000183
00000184
00000185
00000186
00000187
00000195
00000200
00000221
00000222
00000223
00000224
00000225
00000226
00000227
00000230
00000231
00000239
00000240
00000250
00000260
00000270
00000271
00000290
00000299
00000300

SIBFC MAIN
APULLO WATER IMPACT ANALYSIS
**
REFERENCES ** AIAA JOURNAL, VOL. 1, NO. 8, AUG. 1963, PG.1833FF AND
VOL. 2, NO. 3, MARCH 1964, PG. 590FF
** SID 65-1633 REPORT, APULLO WATER IMPACT ANALYSIS, NOV.
23, 1965, PG. 81FF

NOMENCLATURE
AO REFERENCE LENGTH (IN)
HO REFERENCE THICKNESS (IN)
EO REFERENCE YOUNG MODULUS (PSI)
SIGO REFERENCE STRESS (PSI)
POI POISSON RATIO
ENF NO. OF FOURIER COMPONENTS
BCIT TOP BOUNDARY CONDITION FLAG
BCIB BOTTOM BOUNDARY CONDITION FLAG
= 1.0 CLOSED APFX
= 2.0 PINNED
= 3.0 CLAMPED
= 4.0 FREL
= 5.0 ROLLER W
= 6.0 ROLLER U
= 10.0 SPECIAL BOUNDARY READ WITH GEOMETRY DATA

PFLAG DATA PRINT INDICATOR
= 0.0 PRINTS GENERAL DATA AND BND. MATRICES
= 1.0 PRINTS ABOVE INFORMATION AND INPUT DATA
FOR A PARTICULAR GEOMETRY, AND THE PARA-
METERS COMPUTED IN GEOM.
=-1.0 PRINTS ALL OF THE ABOVE INFORMATION AND
STIFFNESS COEFFICIENTS, ELASTIC COEFF.,
THERMAL LOAD AND MOMENT AND PRESSURES

THT CIRCUMFERENTIAL ANGLE THETA (DEGREES) 5 MAX
FPRNT FOURIER COMPONENT PRINT VALUES. 3 PERMITTED

TAPE USAGE -
TAPE 3 - THREE FILES.
FIRST FILE - FOURIER COEFFICIENTS FOR LOAD.
SECOND FILE - INITIAL BOUNDARY MATRICES
GENERATED IN 'RSLT'.
THIRD FILE - MATRICES FROM STATION NO. 1.

TAPE 4 - TWO FILES.
    
```

```

C FIRST FILE - A RECORD OF EACH REGION STUDIED TO 000317
C IN 'GEOMETRY'. 00003311
C A LAST RECORD CONTAINING A 'P' 00000330
C AND AN 'X' GENERATED FOR 00000331
C STATION (N-2). THIS RECORD IS 00000332
C WRITTEN IN FORNIX AND BACKSPACED. 00000333
C SECOND FILE - A 'Z' MATRIX FOR EACH STATION. 00000360
C 00000369
C TAPE 9 - ONE FILE. 00000370
C STIFFNESS COEFFICIENTS GENERATED 00000380
C IN 'DAILYR'. 00000390
C 00000399
C TAPE 10 - ONE FILE. 00000400
C EACH RECORD CONTAINS 'P', AND 'X', 00000410
C FOR EACH STATION. LAST RECORD 00000411
C CONTAINS ONLY R, S, AA0, AND 00000412
C L1 FOR LAST STATION. 00000413
C 00000420
C 00000430
C 00000450
C EQUIVALENCE (GDA( 1), A0), (GDA( 2), HU),
C (GDA( 3), EU), (GDA( 4), SIGO),
C (GDA( 5), POI), (GDA( 6), ENF),
C (GDA( 7), BCIT), (GDA( 8), BCIB),
C (GDA( 9), PFLAG), (GDA(12), TH1),
C (GDA(18), FPRNT)
C COMMON GDA(25), DEL, N, MNF, NTH,
C 1 BMTX(160)
C 5 REWIND 3
C REWIND 10
C REWIND 4
C REWIND 9
C READ AND PRINT 3 CARDS OF TITLE DATA
C READ (5,7) BCD
C 7 FORMAT( 12A6 )
C WRITE (6,8) BCD
C 8 FORMAT(1H1 / (18X, 12A6 //) )
C DO 10 L = 1,11
C GDA(L+11) = -1.*F+10

```



```

C      IO GDA(L) = 0.0
C      READ GENERAL DATA
C      20 CALL DECRO (GDA)
C      IF (THI(1) .EQ. -1.E+10) THI(1) = 0.0
C      IF (FPRNT(1) .EQ. -1.E+10) FPRNT(1) = ENF
C      DATA LINK
C      CALL DATLNK
C      FORM P, AND IX, MATRICES
C      CALL PANDX
C      REWIND 9
C      CALL ZMTRX
C      SOLUTIONS
C      CALL SUMS
C      SUMS AND INTERNAL LOADS
C      GO TO 5
C      END

```

0.000580  
0.000590  
0.000599  
0.000600  
0.000612  
0.000613  
0.000619  
0.000620  
0.000680  
0.000689  
0.000690  
0.000710  
0.000719  
0.000720  
0.000730  
0.000739  
0.000740  
0.000750  
0.000760  
0.000999  
0.001000

3.11b DATLNK Subroutine (DLNK)

```

$IFTC DLNK          00000001
C SUB-EXECUTIVE ROUTINE FOR GEOM, DATLYR AND DATLD TO PERMIT ONE 00000010
C COPY OF CUDIVA, ENTERP AND DINTRP IN THE DECK SET-UP 00000011
C SUBROUTINE DATLNK 00000019
C 00000020
C 00000099
C COMMON GDA(25), DEL, N, NNF, NTH, BMTX(160) 00000100
C 00000198
C SET UP R, RHOX, GAMA, WTH, WFL, XSI 00000199
C 00000200
C 00000205
C 00000218
C SET UP MATERIAL PROPERTIES 00000219
C 00000220
C 00000225
C 00000238
C SET UP FOURIER LOAD COEFF. 00000239
C 00000240
C 00000999
C RETURN 00001000
C 00001009
C END 00001010
    
```



```

EQUIVALENCE (BMTX( 1), OMGN( 1)) 00000440
(BMTX( 51), ALM( 1)) 00000450
(BMTX(101), OMG1( 1)) 00000460
(BMTX(151), LL( 1)) 00000470
00000479
00000480
EQUIVALENCE (GDA( 2), H( 1)) 00000490
(GDA( 4), SIG( 1)) 00000500
(GDA( 6), ENF( 1)) 00000510
(GDA( 8), H( 1)) 00000511
(GDA(12), THT( 1)) 00000512
00000513
00000520
EQUIVALENCE (GMDA( 1), GIN( 1)) 00000530
(GMDA( 3), PLANK( 1)) 00000540
(GMDA( 5), AXL,ROFF( 1)) 00000550
(GMDA( 7), PHIN( 1)) 00000560
(GMDA( 9), RIPT( 1)) 00000570
(GMDA(209), RCURV( 1)) 00000580
(GMDA(409), HNDTX( 1)) 00000590
00000600
00000610
00000620
00000630
00000640
00000650
00000660
00000670
00000680
00000690
00000700
00000710
00000720
00000730
00000740
00000750
00000760
00000770
00000780
00000790
00000800
00000810
00000820
DO 2 J = 1,442
2 GMDA(I) = 0.0
CALL DECRD (GMDA)
DO 3 I = 1,160
3 BMTX(I) = 0.0
IF (RCIT .NE. 1.0) GO TO 5
CLOSED AREA
OMG0(3,3) = 1.0
OMG1(1,1) = 1.0
OMG1(1,2) = -1.0
OMG1(5,4) = -1.0
OMG1(5,5) = 1.0
ALM0(1,1) = 1.0
ALM0(2,2) = 1.0
ALM0(4,4) = 1.0
ALM0(5,5) = 1.0
ALM1(2,1) = 1.0
ALM1(2,2) = 1.0
ALM1(3,3) = 1.0

```

```

ALM1(4,4) = 1.0
ALM1(4,5) = 1.0
GO TO 21
C
5 IF (RCIT .NF. 10.) GO TO 10
SPECIAL BOUNDARY
OMG0(1,1) = BNDTX( 1)
OMG0(1,2) = BNDTX( 2)
OMG0(2,2) = BNDTX( 3)
OMG0(3,3) = BNDTX( 4)
OMG0(4,4) = BNDTX( 5)
OMG0(5,4) = BNDTX( 6)
OMG0(5,5) = BNDTX( 7)
ALM0(1,1) = BNDTX( 8)
ALM0(2,2) = BNDTX( 9)
ALM0(3,3) = BNDTX(10)
ALM0(4,4) = BNDTX(11)
ALM0(5,5) = BNDTX(12)
DO 8 IJ = 1,5
8 LL(IJ) = BNDTX(IJ+1?)
GO TO 21
C
10 IBMX = RCIT
I0 = 1
IL = 51
CHOOSE BOUNDARY
11 GO TO (21,12,13,14,15,16), IRMX
PINNED
12 BMTX(10 + 18) = 1.
BMTX(10 + 24) = 1.
BMTX(11) = 1.
BMTX(11 + 6) = 1.
BMTX(11 + 12) = 1.
GO TO 20
CLAMPED
13 BMTX(11) = 1.
BMTX(11 + 6) = 1.
BMTX(11 + 12) = 1.
BMTX(11 + 18) = 1.
BMTX(11 + 24) = 1.
GO TO 20
FREE
14 BMTX(10) = 1.

```

	BMTX(10 + 6) = 1.	00001250
	BMTX(10 + 12) = 1.	00001260
	BMTX(10 + 18) = 1.	00001270
	BMTX(10 + 24) = 1.	00001280
	GO TO 20	00001290
C		00001300
	ROLLER W	
	15 BMTX(10 + 12) = 1.	00001310
	BMTX(10 + 18) = 1.	00001320
	BMTX(10 + 24) = 1.	00001330
	BMTX(11) = 1.	00001340
	BMTX(11 + 6) = 1.	00001350
	GO TO 20	00001360
C		00001370
	ROLLER U	
	16 BMTX(10) = 1.	00001380
	BMTX(10 + 18) = 1.	00001390
	BMTX(10 + 24) = 1.	00001400
	BMTX(11 + 6) = 1.	00001410
	BMTX(11 + 12) = 1.	00001420
C		00001429
	20 IF(10 .NE. 1) GO TO 28	00001430
C		00001439
	21 IF (RCIR .NE. 1.0) GO TO 23	00001440
C		00001449
	CLOSED APEX	
	OMGN(1,1) = 1.0	00001450
	OMG1(1,1) = 1.0	00001460
	OMG1(1,2) = -1.0	00001470
	OMG1(5,4) = 1.0	00001480
	OMG1(5,5) = 1.0	00001490
	ALMN(1,1) = 1.0	00001500
	ALMN(2,2) = 1.0	00001510
	ALMN(4,4) = 1.0	00001520
	ALMN(5,5) = 1.0	00001530
	ALM1(2,1) = 1.0	00001540
	ALM1(2,2) = 1.0	00001550
	ALM1(3,3) = 1.0	00001560
	ALM1(4,4) = 1.0	00001570
	ALM1(4,5) = 1.0	00001580
	GO TO 28	00001590
C		00001599
	23 IF (RCIR .NE. 1.0) GO TO 25	00001600
C		00001609
	SPECIAL BOUNDARY	
	OMGN(1,1) = BNDIS( 1)	00001610
	OMGN(1,2) = BNDIS( 2)	00001620

```

OMGN(2,2) = BNDTB( 3)
OMGN(3,4) = BNDTB( 4)
OMGN(4,4) = BNDTB( 5)
OMGN(5,4) = BNDTB( 6)
OMGN(5,5) = BNDTB(7)
ALMN(1,1) = BNDTB(8)
ALMN(2,2) = BNDTB( 9)
ALMN(3,3) = BNDTB(10)
ALMN(4,4) = BNDTB(11)
ALMN(5,5) = BNDTB(12)
DO 24 IJ = 1,5
24 LLL(IJ) = BNDT( IJ+12)
GO TO 28
C
25 IRLX = IRLS
IC = 26
IL = 76
GO TO 11
C
28 WRITE (6,1065) A , H, F, J, G, POI, FNF, HCII, RCIR, PFLAG,
1 THY, FORNT,
2 OMGN, ALMO, LLL, OMGN, ALMN, LLLN
N = EN
GMI = ABS(GINI)
NN = N - 1
IF (GMI - 2.0) 30, 35, 50
C
C CONE - CYLINDER
C
30 IF (PFLAG.NE.0.0) WRITE(6,31) N, IRLX, AXL, NIX
C
31 FORMAT (1H1,30A,33HGEOMETRY DATA FOR CONE - CYLINDER /73DX,22060, 33H, 31,2)
1ER OF STATIONS = 914/76X,7HRA1 =91P13.4,7X,7HAXL =9E13.4,7X,7HAXL
2 THAX =9F13.4)
C
DEL = AXL/(FN - 1.0)
SINFI = SIND(ANX)
COSFI = COSD(ANX)
XSI(1) = 0.0
WIX(1) = A0 * COSFI/RAI
WFX(1) = 0.0
PHOX(1) = RAI/AD

```

```

R(I) = RA1
DO 32 I = 2, N
  R(I) = R(I-1) + DEL * SINFI
  XSI(I) = XSI(I-1) + DEL * COSFI
  WTX(I) = A0 * COSFI/R(I)
  WFEX(I) = 0.0
  32 R-OX(I) = R(I)/A0
    (GO TO 95
C
C          SPHERE - TOROID
C          **
C          35 IF (PFLAG .NE. 0.0) WRITE (6,37) N, RC, ROFF, PHIO, PHIN
C          37 FORMAT (1H1,35X,33HGEOMETRY DATA FOR SPHERE - TOROID 775X,22HNUMB
  IER OF STATIONS = ,I4//6X,7HRC = ,E13.4,7X,7HROFF = ,E13.4,7X,7H
  2 7HPHIO = ,E13.4,7X,7HPHIN = ,E13.4 )
C
  ANGSP = PHIN - PHIO
  DEL = ANGSP/LEN - 1.0)
  AM = 1.0
  AMU = SIGN(A0,JFL)
  XSI(1) = 0.0
  BPHI = PHIO
  BSINP = SIND(PHIO)
  BCOSP = COSD(PHIO)
  R(1) = RC * BSINP + ROFF
  DO 40 I = 1, NN
    APMI = MPMI + DEL
    ASINP = SIND(APMI)
    ACOSP = COSD(APMI)
    R(I+1) = R(I) + RC * (ASINP - BSINP)
    XSI(I+1) = XSI(I) + A0 * (DCOSP - ACOSP)
    WFEX(I) = A0/RC * A0
    IF (ROFF .EQ. 0.0) GO TO 38
    WTX(I) = A0 * BSINP/R(I)
    (GO TO 39
  38 WTX(I) = WFEX(I)
  39 R-OX(I) = R(I)/A0
  40 CONTINUE
C

```



```

DEF = ABS(DEL)
WFFX(N) = AO/RC*AMB)
IF (ROFF .EQ. 0.0) GO TO 45
WTHX(N) = AO * F5(INP /R(N)
GO TO 46
45 WTHX(N) = WFFX(N)
46 RHOX(N) = R(N)/AU
GO TO 48
47 RHOX(N) = 0.0
48 /FL = DFL * RC * 0.01745329
) TO 95
C
50 IF (GMT .GT. 3.0) GO TO 60
C
WRITE (6,55)
55 FORMAT (1H1,42HARBITRARY FUNCTIONS CANNOT BE MANIPLED, YFF. )
GO TO 140
C
GENERAL DISCRETE POINTS
C
60 M = EM
MM = M - 1
MM2 = M - 2
C
IF (PFLAG .NE. 0.0) WRITE(6,62) N, (RIP(I), XIPT(I)), I = 1,M)C,002720
62 FORMAT (1H1,30X,31H)LOM(CRY DATA = DISCR) IN POSITIVE //35X,22H)NUMBER C,002730
1 OF STATIONS = ,14//16),1HR,16X,2HX)1//13X,1P/2EQ.0/) )
C
SARH(1) = 0.0
IF (GIN .LT. 0.0) GO TO 77
DO /5 1L = 1,MM
SURR = 0.0
DLT = XIPT(IL+1) - XIPT(IL)
K = 10
AK = K
DDL = DLT/AK
KPI = K + 1
DO 65 JI = 1,KPI
AJI = JI - 1
XJ(JI) = XIPT(JI) + AJI * DDL

```

```

00002467
0000247
00002480
00002490
00002500
00002510
00002520
00002530
00002540
00002550
00002560
00002570
00002580
00002590
00002600
00002610
00002620
00002630
00002640
00002650
00002660
00002670
00002680
00002690
00002700
00002710
00002720
00002730
00002740
00002750
00002760
00002770
00002780
00002790
00002800
00002810
00002820
00002830
00002840
00002850
00002860
00002870
00002880

```

```

65 CONTINUE
CALL CODIMA (KPI,XJ, RKJ, XIPI, RIPI, M, 1.0)
DO 69 I = 2,K
69 RJ(I) = (RRJ(I-1) + RRJ(I) + RRJ(I+1))/3.0
RJ(I) = RRJ(I)
RJ(KPI) = RRJ(KPI)

DO 70 JR = 1,K
DLR(JR) = RJ(JR+1) - RJ(JR)
DLS = SORT(DLR(JR)**2 + DDL**2)
70 SURB = SURB + DLS
SARB(IL+1) = SARB(IL) + SURB
75 CONTINUE
GO TO 80
77 DO 78 I = 1,M
78 SARB(I) = XIPI(I)
80 DEL = SARB(M)/(EN - 1.0)
SURF(1) = 0.0
DO 82 I = 1,NN
82 SURF(I+1) = SURF(I) + DLL
CALL CODIMA(N, SURF,RCRV, SARB, RCURV, M, 1.0)
CALL CODIMA(N,SURF,RCRZ, SARB, RCRZ, M, 1.0)
CALL CODIMA (N,SURF, R, SARB, RIPI, M, 1.0)

CALL CODIMA (N, SURF, XSI, SARB, XIPI, M, -1.0)
MLN = N - 2
NSM = 1
84 DO 85 I = 3,MLN
RR(I) = (-3.*R(I-2) + 12.*R(I-1) + 17.*R(I) + 12.*R(I+1) - 3. *
R(I+2))/35.0
85 CONTINUE
R(NN) = R(NN)
RR(2) = R(2)
RR(N) = R(N)
RR(1) = R(1)
IF (NSM.EQ. 25) GO TO 88
NSM = NSM + 1
DO 87 I = 1,N
87 R(I) = RR(I)
GO TO 84

```

```

00002800
000029
00002910
00002920
00002930
00002940
00002950
00002965
00002970
00002980
00002990
00003000
00003010
00003020
00003030
00003040
00003050
00003060
00003070
00003080
00003090
00003100
00003120
00003130
00003140
00003150
00003150
00003170
00003180
00003190
00003200
00003210
00003220
00003230
00003240
00003250
00003260
00003270
00003280
00003290
00003300
00003310
00003320

```

```

88 RHOX(I) = RR(I)/A0
DEL50 = DFL * DFL
DO 89 I = 1,N
  89 PHOX(I+1) = RR(I+1) /A0
  GO TO 110
C
C
C      COMPUTE GAMA
**
95 DEL = DEL/ A0
DEL50 = DEL * DEL
DO 105 I = 1,N
  DENM = 12. * RHOX(I) * DEL
  DENMP = 2. * RHOX(I) * DFL
  IF (RHOX(I) .EQ. 0.) GO TO 97
  IF (I .NE. 1) GO TO 98
  IF (RCIR .EQ. 1.0) GO TO 103
  GAMA(I) = (3. * (RHOX(I+1) - RHOX(I)) + RHOX(I+1) - RHOX(I+2)) / DENMP
  GO TO 105
97 GAMA(I) = 0.0
  GO TO 105
98 IF (I .EQ. N) GO TO 100
  IF (I .EQ. 2) GO TO 99
  IF (I .EQ. N-1) GO TO 99
  GAMA(I) = (RHOX(I-2) - 8. * (RHOX(I-1) -
  1) / DENM
  GO TO 105
99 GAMA(I) = (RHOX(I+1) - RHOX(I-1)) / DENMP
  GO TO 105
100 IF (RCIR .EQ. 1.0) GO TO 103
  GAMA(I) = (3. * (RHOX(I) - RHOX(I-1)) + RHOX(I-2) - RHOX(I-1)) / DENMP
  GO TO 105
103 GAMA(I) = 0.
105 CONTINUE
  GO TO 123
C
110 DO 115 I = 1,N
  WFE(I) = A0 / RCRV(I)
  WTH(I) = A0 / RCRZ(I)
  IF (FMOX(I) .EQ. 0.0) GO TO 113
  PRO = (RHOX(I) * WTH(I)) ** 2
  IF (PRO .GT. 1.0) GO TO 114
  GAMA(I) = SORT(1.-PRO) / RHOX(I)
  GO TO 115

```

```

113 GAMMA(I) = 0.0
GO TO 115
114 GAMMA(I) = 0.0
115 CONTINUE
C
123 DO 127 I = 1,N
WFDNM = 2. * DFL
IF (T.NE.1) GO TO 124
WFEPI(I) = (4. * WFEI(I+1) - 3. * WFEI(I) - WFEI(I+2)) / WFDNM
GO TO 127
124 IF (I.EQ.N) GO TO 126
WFEPI(I) = (WFEI(I+1) - WFEI(I-1)) / WFDNM
GO TO 127
126 WFEPI(I) = (WFEI(I-2) + 3. * WFEI(I) - 4. * WFEI(I-1)) / WFDNM
127 CONTINUE
C
WRITE (4) I,HX, WFEI, GAMMA, RHOX, WFEPI
C
129 IF (PELAG.EQ.0.0) GO TO 140
WRITE (6,130) DEL, (I, R(I), XSI(I), ATX(I), WFEI(I), RHOX(I),
1 GAMMA(I), I = 1,N)
C
130 FORMAT (1H-, 5X, 7HDEL =,1PF13.4 //
3X,1H,9X,4HR(I),12X,5HX(1)),1 X,9H(1HETA),11X,
2 5HW(X),11X,7HRHOX(I),1 X,7HGAMA(I) //114, 1P6(17.7) )
C
140 RETURN
C
1000 FORVAL(1H,4/,12HGENERAL DATA// 3X,7HATX =,1PF13.4, 8X,7HHC
1 =,5F13.4, 8X,7HFO =,5F13.4, 8X,7HIG =,5F13.4// 3X,7HPOI =,
2 5F13.4, 8X,7HFN =,5F13.4, 8X,7HBCI =,5F13.4, 8X,7HHCIN =,
3 5F13.4//3X,7HDEL =, 5F13.4 //
4 //6X,20HPRINT ANGLES (TH) - // 24X,6E13.4 //6X,33HFOURIFR HCC004124
5 HARMONIC PRINTS (FPRNT) - // 24X, 4E13.4
6
7Y MATRICES /6X,15HTOP BOUNDAR) **// 6X,5HUMEGA /5(5E17.7)// 6X,
8 6HLAMRDA /5(5E17.7)// 6X,3HL -// 5F17.7 //6X,18HROTTON BOUNDARY C0004128
9** // 6X,5HUMEGA /5(5E17.7)// 6X,6HLAMRDA /5(5E17.7)// 6X,3HL -// 5F17.7
X 5F17.7 )
END

```

3. 11d DATLYR Subroutine (STIFF)

```

$IRFTC STIFF          00000010
C                    00000020
C                    00000030
C                    00000040
C                    00000110
C *** STIFFNESS COEFF. ARE STORED IN SECTIONS OF ALL FOURIER
C COMPONENTS /MERIDIONAL STATION, UP TO BLOCKS OF 200
C                    00000112
C                    00000120
C                    00000130
C DIMENSION SCB1(200), SCB2(200), SCB3(200), SCG1(200), SCG2(200),
C                    00000140
C                    00000141
C                    00000142
C SCNTSI(200), SCNTH(200), SCMSI(200), SCMTH(200), DCK3(200)
C                    00000179
C                    00000180
C                    00000190
C                    00000200
C                    00000210
C                    00000220
C                    00000230
C                    00000240
C                    00000250
C                    00000251
C                    00000252
C                    00000253
C                    00000260
C                    00000299
C EQUIVALENCE (COFFC 1), SCB1),
C                    (COFFC 401), SCB3),
C                    (COFFC 801), SCG2),
C                    (COFFC(1201), SC01), (COFFC(1401), SC02), (COFFC(1601), SC03), (COFFC(1801), SCG13), (COFFC(2001), SCN151), (COFFC(2201), SCN11H), (COFFC(2401), SCM151), (COFFC(2601), SCM11H), (COFFC(2801), DCK3)
C                    00000329
C                    00000331
C                    00000332
C                    00000333
C                    00000334
C                    00000335
C                    00000390
C                    00000390
C                    00000400
C                    00000410
C                    00000420

FOURIER STIFFNESS COEFFICIENTS GENERATOR * *
SUBROUTINE DAILYR
*** STIFFNESS COEFF. ARE STORED IN SECTIONS OF ALL FOURIER
COMPONENTS /MERIDIONAL STATION, UP TO BLOCKS OF 200
DIMENSION COFFC(3000)
DIMENSION SCB1(200), SCB2(200), SCB3(200), SCG1(200), SCG2(200),
1 SCG3( 200), SCD1(200), SCD2(200), SCD3(200), SCG13(200),
2 SCNTSI(200), SCNTH(200), SCMSI(200), SCMTH(200), DCK3(200)
COMMON GDA(2), DEL, N, NMF, NTH,
1 6MTX(160)
C
C EQUIVALENCE (GDA( 1), A0),
C                    (GDA( 3), E0),
C                    (GDA( 4), SIG),
C                    (GDA( 5), P01),
C                    (GDA( 7), BC1),
C                    (GDA( 9), PFLAG),
C                    (GDA(12), THT),
C                    (GDA(18), FPRNT)
C
EQUIVALENCE (COFFC 1), SCB1),
C                    (COFFC 401), SCB3),
C                    (COFFC 801), SCG2),
C                    (COFFC(1201), SC01), (COFFC(1401), SC02), (COFFC(1601), SC03), (COFFC(1801), SCG13), (COFFC(2001), SCN151), (COFFC(2201), SCN11H), (COFFC(2401), SCM151), (COFFC(2601), SCM11H), (COFFC(2801), DCK3)
C                    00000329
C                    00000331
C                    00000332
C                    00000333
C                    00000334
C                    00000335
C                    00000390
C                    00000390
C                    00000400
C                    00000410
C                    00000420

IF(PFLAG .LT. 0.) WRITE(6,1)
10 FORMAT(1H1/6X, 96HCHECKPRINT OF COFFC BLOCKS STORED IN GROUPS OF
12*ENF) PER MERIDIONAL STATION. THE COEFFICIENTS /10TH PRINTED ARE
2 SCB1, SCD1, SCN151, SCMSI, DCK3 (IN THAT ORDER) AND ARE SEPARATE
30 FROM EACH OTHER BY THE / 21H THREE ..... FIELDS. / / / )
ENTH = 90.
H02 = H0 # HU
SS3 = 2.73.1615927
NTH = ENTH

```

```

NNF = ENF
NNF2 = 2 * NMF
IN = 1

C C DETERMINE SIZE OF BLOCK **
C C
C C LN = N
C C GO TO 60
C C 60 F (MNF .LT. 400) GO TO 55
C C LN = 200/NNF2
C C GO TO 78
C C
C C 65 LN = 10 / NMF2
C C 8 LN = IN + LN - 1
C C 60 DELTH = 3.1415927 / ENTH
C C
C C 63 DO 95 I = 1, LN
C C 64 COEFF(I) = 0.0
C C
C C 70 DO 100 J = 1, LN
C C FT = I - 1
C C DEL = FT * DEL
C C
C C K1 = NMF2 * (I - 1)
C C DO 100 NN = 1, NMF2
C C K2 = K1 + NN
C C FNU = NN - 1
C C
C C 75 DO 95 J = 1, LN
C C FJ = J - 1
C C ZTA = FJ * DELTH + DELTH * 0.5
C C IF (NN .EQ. 1) GO TO 90

```

```

1.0000440
0.0000450
0.0000470
0.0000470
0.0000480
0.0000490
0.0000500
0.0000510
0.0000519
0.0000520
0.0000530
0.0000540
0.0000549
0.0000550
0.0000560
0.0000570
0.0000579
0.0000580
0.0000590
0.0000600
0.0000610
0.0000620
0.0000630
0.0000640
0.0000650
0.0000650
0.0000660
0.0000670
0.0000680
0.0000689
0.0000700
0.0000710
0.0000720
0.0000730
0.0000740
0.0000750
0.0000750
0.0000780
0.0000790
0.0000800
0.0000810
0.0000820
0.0000830

```

LESS THAN ONE BLOCK MORE

AT LEAST 2 FULL BLOCKS MORE

GREATER THAN ONE BLOCK, LESS THAN TWO  
AVOID HAVING ONLY TWO STATIONS IN A BLOCK.

ZERO COEFFICIENT AREA

ESTABLISH MERIDIONAL DISTANCE

```

C      80 SCB1(K2) = SCB1(K2) + DBH1PEL,ZTA)
      SCNTS1(K2) = SCNTS1(K2) + FNT1PEL,ZTA) * COS(TENN * ZTA)
      SCNTS1(K2) = SCNTS1(K2) + FNT1PEL,ZTA) * COS(FNN * ZTA)
      SCD1(K2) = SCD1(K2) + DDD1ZTA) * COS(FNN * ZTA)
      DCK3(K2) = DCK3(K2) + DKK3PEL,ZTA) * COS(TENN * ZTA)
      GO TO 95
C
C      90 SCB1(K2) = SCB1(K2) + RBH1PEL,ZTA) / 2.0
      SCNTS1(K2) = SCNTS1(K2) + ENT1PEL,ZTA) / 2.0
      SCNTS1(K2) = SCNTS1(K2) + ENT1PEL,ZTA) / 2.0
      SCD1(K2) = SCD1(K2) + DDD1ZTA) / 2.0
      DCK3(K2) = DCK3(K2) + DKK3PEL,ZTA) / 2.0
      95 CONTINUE
C
C      S3 = S53/(EO * H0)
      SCB1(K2) = S3 * DELTH * SCB1(K2)
      S4 = S3 * A0*A0
      DCK3(K2) = S4 * DELTH * DCK3(K2)
      S3 = S53 / (SIG0 * H0)
      SCNTS1(K2) = S3 * DELTH * SCNTS1(K2)
      S3 = S53 * AU / (SIG0 * H02 * H0)
      SCNTS1(K2) = S3 * DELTH * SCNTS1(K2)
      S3 = S53/(EO * H02 * H0)
      SCD1(K2) = S3 * DELTH * SCD1(K2)
C
C      98 S52 = (1. - PO1) / 2.
      SCG1(K2) = S52 * SCD1(K2)
      SCG1(K2) = S52 * SCD1(K2)
      SCB2(K2) = SCB1(K2)
      SCB3(K2) = PO1 * SCB1(K2)
      SCG2(K2) = S52 * SCB1(K2)
      SCG3(K2) = SCG1(K2)
      SCD2(K2) = SCD1(K2)
      SCD3(K2) = PO1 * SCD1(K2)
      100 CONTINUE
C
      WRITE ( 9) LN, IN, COFFC
      NX = (LN - IN + 1) * NWF2
      XX = GDA(25)
      IF (PFLAG * LT. 0.)
      XWRITE (6,105) IN, LN, (SCB1(I), I=1,NX), XX, XX, XX, (SCD1(I),

```

```

00000839
00000840
00000850
00000855
00000860
00000866
00000870
00000879
00000880
00000883
00000886
00000890
00000895
00000900
00000910
00000919
00000920
00000930
00000931
00000934
00000935
00000940
00000945
00000950
00000955
00000960
00000970
00000980
00000985
00000990
0001010
0001020
0001030
0001040
0001050
0001060
0001120
0001130
0001140
0001145
0001146
0001149
0001150

```

NORMALIZE

FIRST FOURIER COMPONENT

OTHER FOURIER COMPONENTS

```

1 I=1,200) XA, XX, AX, (CCN13)I(1), I=1,200) XZ, XZ, AX, (CCN1 I(1), I=1,200)
2 I=1,200) XX, XX, VX, (DCP3)I(1), I=1,200)
105 FORMAT(10A,11HFOR STATION, 13,16) THRU (H, 10) ION, 14//
1 ( 1P6F17.7) )
C
IF (LN.EQ. N) GO TO 110
IN = LN + 1
NCN = N - LN
MNF = NCN * MNF?
GO TO 40
110 RETURN
C
LND

```



3.11e DATLD Subroutine (LOAD)

```

C          SIRFTC LOAD          00000010
C          FOURIER LOAD COEFFICIENTS GENERATOR BY FUNCTIONS ONLY 00000020
C          SUBROUTINE DATLD      00000030
C          DIMENSION PFF(10,50), PTH(10,5,1), PN(1,5,1) 00000040
C          * FNIVALFNCE (GDA( 1), AU), (GDA( 2), HU), 00000040
C          1 (GDA( 3), EU), (GDA( 4), SIG), 00000041
C          2 (GDA( 5), PO), (GDA( 6), FNF), 00000042
C          3 (GDA( 7), BCIT), (GDA( 8), BCIB), 00000043
C          4 (GDA( 9), PFLAG), (GDA(12), THF), 00000044
C          5 (GDA(10), PPRNT) 00000045
C          6 (GDA(18), PPRNT) 00000046
C          COMMON GDA(25), DEL, N, NNF, NTH, 00000049
C          1 HMTX(160) 00000050
C          * INITIALIZE * * * * * 00000051
C          NAR = 0 00000053
C          SSR = 2. / 3.1415927 00000054
C          SA = SSR * AU / (SIG * HU) 00000056
C          DO 20 I = 1,50 00000058
C          DO 20 K = 1,10 00000059
C          PFF(K,I) = 0.0 00000600
C          PTH(K,I) = 0.0 00000610
C          PN(K,I) = 0.0 00000630
C          20 CONTINUE 00000650
C          IF (PFLAG .LT. 0.) WRITE(6,31) 00000670
C          30 FORMAT(1H1/6X, 98HCHECKPRINT OF LOAD COEFF. STORED IN GROUPS OF ALL0000730
C          1 ENF PER MERIDIONAL STATION. THE COEFFICIENTS ARE / 81H PFF, PTH,0000741
C          2, PN (IN THAT ORDER) AND ARE SEPARATED FROM EACH OTHER BY ***** F00000742
C          3IELDS. /) 00000743
C          NT = N 00000770
C          50 FT = 0.0 00000790
C          N11 = 1 00000810
C          N12 = N 00000820
C          SPECIAL FUNCTIONS 00000830

```

```

0000084
0000085
0000086
0000087
0000088
0000089
0000090
0000091
0000092
0000093
0000094
0000095
0000096
0000097
0000098
0000099
0000100
0000101
0000102
0000103
0000104
0000105
0000106
0000107
0000108
0000109
0000110
0000111
0000112
0000113
0000114
0000115
0000116
0000117
0000118
0000119
0000120
0000121
0000122
0000123
0000124
0000125
0000126
0000127
0000128
0000129
0000130
0000131
0000132
0000133
0000134
0000135
0000136
0000137
0000138
0000139
0000140
0000141
0000142
0000143
0000144
0000145
0000146
0000147
0000148
0000149
0000150
0000151
0000152
0000153
0000154
0000155
0000156
0000157
0000158
0000159
0000160
0000161
0000162
0000163
0000164
0000165
0000166
0000167
0000168
0000169
0000170
0000171
0000172
0000173
0000174
0000175
0000176
0000177
0000178
0000179
0000180
0000181
0000182
0000183
0000184
0000185
0000186
0000187
0000188
0000189
0000190
0000191
0000192
0000193
0000194
0000195
0000196
0000197
0000198
0000199
0000200

```

ENTH = NIH  
 DELTH = 3.1415927 / FNTH  
 EACH BLOCK OF LOADS CANNOT CONTAIN MORE THAN 50 STAS.  
 IF (NI .GT. 50) NI = 50  
 DO 100 I = 1, NI  
 FI = FI + 1.0  
 PEL = (FI - 1.0) \* DFL  
 DO 100 NN = 1, NNF  
 FNN = NN - 1  
 DO 95 J = 1, NTH  
 EJ = J - 1  
 ZTA = EJ \* DELTH + DELTH \* 0.5  
 IF (NTH .EQ. 1) GO TO 90  
 PTH(NN, I) = PTH(NN, I) + PPPH(PEL, ZTA) \* IN(FNN \* (ZTA - 1.5707963))  
 PFF(NN, I) = PFF(NN, I) + PPPF(PEL, ZTA) \* COS(FNN \* ZTA)  
 PN(NN, I) = PN(NN, I) + PPN(PEL, ZTA) \* COS(FNN \* ZTA)  
 GO TO 95  
 90 PTH(NN, I) = PTH(NN, I) + PPPH(PEL, ZTA) / 2.  
 PFF(NN, I) = PFF(NN, I) + PPPF(PEL, ZTA) / 2.  
 PN(NN, I) = PN(NN, I) + PPN(PEL, ZTA) / 2.  
 95 CONTINUE  
 PTH(NN, I) = 53 \* DELTH \* PTH(NN, I)  
 PFF(NN, I) = 53 \* DELTH \* PFF(NN, I)  
 PN(NN, I) = 53 \* DELTH \* PN(NN, I)  
 100 CONTINUE  
 2PIIF ( 2) PFF, PTH, PN  
 107 XX = GOA(25)  
 IF (N .GT. 50 .AND. NAF .EQ. 0) NI2 = 50  
 IF (PELAG .LT. 0)  
 2PIIF ( 4, 103) NI1, NI2, ((PFF(NN, I), NN=1, NNF), I=1, NI1), AX, XX,  
 100 ((PTH(NN, I), NN=1, NNF), I=1, NI1), AX, XX, ((PN(NN, I), NN=1, NNF), I=1, NI1)  
 2PIIF ( 1) NI1  
 108 FORMAT (10X, 11HFOR STATION, I3.16H THROUGH STATION, I4.//  
 1 ( 1P6517.7) )

```

NAR = NAR + NI
IF (NAR .EQ. NI) GO TO 600
C
C
C
MORE THAN 50 STATIONS TO STORE
*
NI = N - NI
NI1 = 51
NI2 = N
DO 115 I = 1,50
DO 110 J = 1,10
PTH(J,I) = 0.0
PFE(J,I) = 0.0
110 PNI(J,I) = 0.0
115 CONTINUE
C
C
GO TO 70
C
600 FND FILE 3
PFWIND 3
C
RETURN
620 FORMAT (1H-// (10X, 1P5F17.7))
FND
00001239
00001240
00001250
00001260
00001270
00001280
00001281
00001282
00001290
00001300
00001310
00001320
00001330
00001340
00001350
00001360
00003000
00003010
00003020
00003030
00003040
00003050
00003060

```

3.11f PANDX Subroutine (PEANDX)

```

00000010
00000020
00000030
00000040
00000050
00000060
00000070
00000080
00000090
00000100
00000110
00000120
00000130
00000140
00000150
00000160
00000170
00000180
00000190
00000200
00000210
00000220
00000230
00000240
00000250
00000260
00000270
00000280
00000290
00000300
00000310
00000320
00000330
00000340
00000350
00000360
00000370
00000379
00000380
00000390
00000400
00000410
00000411

SIBFTC PEANDX
C GENERATES THE 'P' AND 'X' MATRICES
C NOTE RECURSION TERMS ARE ALSO GENERATED
C SUBROUTINE PANDX
C
C AD REFERENCE LENGTH (IN)
C HO REFERENCE THICKNESS (IN)
C EO REFERENCE YOUNGS MODULUS (PSI)
C SIGO REFERENCE STRESS (PSI)
C MNF NO. OF TERMS IN THE FOURIER EXPANSION.
C LAM LAMBDA = HO / AO
C WFE OMEGA (XI)
C WTH OMEGA (THETA)
C ARRAYS USED
C COFFC - CONTAINS STIFF. COEFF. FROM DATLYR
C P1SCB1 - TEMPORARY STORAGE
C P2SCB1 - FOR STIFFNESS COEFF. (B1)
C PANDX FLAGS
C IRTE .NE. 1 FIRST STATION - NOT FIRST BLOCK
C IRTE .EQ. 1 LAST STATION - PREVIOUS BLOCK
C IFGFG = 10 F, G, H, PE HAVE NOT BEEN COMPUTED, YET.
C IFGFG = 0 P AND X HAVE BEEN COMPUTED FOR IRTE = 1.
C IFGFG = 1 P AND X COMPUTED. INCREMENT STA. INDEX.
C IRSFG = 10 R, S, LT. HAVE NOT BEEN COMPUTED.
C IRSFG = 1 INITIAL BOUNDARY COMPUTED.
C IRSFG = 0 TERMINAL BOUNDARY COMPUTED.
C COUNTERS -
C *M - ABSOLUTE STATION NUMBER. *
C I - STATION NO. WITHIN EACH BLOCK OF STIFF. COEFF.
C *MMN - STATION NO. WITHIN BLOCK OF LOADS.
C IFLG - STIFF. COEFF. BLOCK. *
C
C EQUIVALENCE (BMIX( 1), OMG0), (BMIX( 26), OMGN),
1 (BMIX( 51), ALM0), (BMIX( 76), ALMN),
2 (BMIX(101), OMG1), (BMIX(126), ALM1),
3 (BMIX(151), LL0), (BMIX(156), LLLN)
C
C EQUIVALENCE (GDA( 1), AO), (GDA( 2), HO),
1 (GDA( 3), EO), (GDA( 4), SIGO),
2 (GDA( 5), POI), (GDA( 6), ENF),
3 (GDA( 7), BCIT), (GDA( 8), BCIB),
4 (GDA( 9), PFLAG),
C

```

```

5          (GDA(18), PRNT)          (GDA(12), THT),          00000412
6          (GDA(18), PRNT)          (GDA(12), THT),          00000413
          (GDA(18), PRNT)          (GDA(12), THT),          00000419
EQUIVALENCE (COEFC( 1), SCB1), (COEFC( 201), SCB2), 00000420
              (COEFC( 401), SCB3), (COEFC( 601), SCG1), 00000421
              (COEFC( 801), SCG2), (COEFC(1001), SCG3), 00000422
3 (COEFC(1201), SCD1), (COEFC(1401), SCD2), (COEFC(1601), SCD3), 00000423
4 (COEFC(1801), SCG13), (COEFC(2001), SCNTSI), (COEFC(2201), SCMTTH), 00000424
5 (COEFC(2401), SCMTSI), (COEFC(2601), SCMTTH), (COEFC(2801), DCK3) 00000425
          00000500
          00000510
DIMENSION WTHX(100), WFEX(100), RHGX(100), GAMAX(100), WFEPX(100) 00000510
DIMENSION ALMO(5,5), ALMN(5,5), OMGU(5,5), OMGN(5,5) 00000520
DIMENSION ALM1(5,5), OMG1(5,5) 00000530
REAL LLO(5), LLLN(5), MFE(10), MTP(10) 00000540
DIMENSION P1SCB1(20), P2SCB1(20), P1SCD1(20), P2SCD1(20) 00000550
1 TFE(10), P1SG1(20), P2SG1(20), P1ENT(20), P2ENT(20), 00000560
2 TTP(10), P1SCG1(20), P2SCG1(20), P1EMT(20), P2EMT(20), 00000570
3 P2DCK3(20), PFE50(10), PTH50(10), PN50(10) 00000571
DIMENSION PFE(10, 50), PTH(10, 50), PN(10, 50) 00000580
DIMENSION P(50,50), X(50) 00000600
          00000610
          00000620
DIMENSION COEFC(3000) 00000630
DIMENSION SCB1(200), SCB2(200), SCB3(200), SCG1(200), SCG2(200), 00000631
1 SCG3( 200), SCD1(200), SCD2(200), SCD3(200), SCG13(200), 00000632
2 SCMTSI(200), SCMTTH(200), SCMTSI(200), SCMTTH(200), DCK3(200) 00000670
COMMON GDA(25), DEL, N, NNF, NTH, 00000680
1 RMTX(160) 00000690
          00000700
          00000710
REAL LAM, LAM02, LAM202, LAM204, LAM208, LAM2, KORO, KOR02, 00000719
1 MFFTK, MTHTK, MFETP, LLI 00000720
COMMON /PXCMM/ MM, LLN, I, IFLG, LN, IRSFG, IFGFG, 00000721
1 RR1KJ, RR2KJ, RR3KJ, GG1KJ, GG2KJ, GG3KJ, DD1KJ, DD2KJ, DD3KJ, 00000722
2 GG13KJ, TFE1K, TFE2K, MFE1K, MFE2K, MTH1K, MTH2K, BB1P, BB2P, 00000723
3 DD1P, DD2P, GG13P, TFE1P, TFE2P, MFETP, OMG(5,5), ALM(5,5), LLI(5), 00000724
4 WTH, WFE, GAM, RHO, WFEP, LAM, LAM2, LAM02, LAM202, LAM204, 00000725
5 LAM208, GAM2, WTMWF, WTMWF2, WFWT, PTHK, PNK, PFEK, P, X, 00000726
6 DCK1KJ, DCK2KJ, DCK3KJ 00000789
COMMON /BLOCK1/ EMM2(50,50) 00000790
COMMON /BLOCK2/ EMM3(50) 00000800
          00000810

```

```

00000819
00000820
00000828
00000829
00000830
00000850
00000860
00000865
00000870
00000880
00000888
00000889
00000890
00000895
00000896
00000897
00000896
00000896
00000899
00000900
00000909
00000910
00000920
00000930
00000940
00000950
00000960
00000970
00000980
00000990
00001000
00001010
00001020
00001022
00001024
00001026
00001028
00001030
00001040
00001050
00001059
00001060
00001070
00001080

C      IF(IPFLAG .EQ. -1.E+10) WRITE (6,340)
C      READ GEOMETRY PARAMETERS FROM TAPE 4, FIRST FILE. (100)
C      THIS TAPE IS WRITTEN IN GEOM AND BACKSPACED IN DATLNK
C      READ ( 4) WTHX, WFEX, GAMA, RHOX, WFEPIX
C
C      INITIALIZE * * * *
C      N2 = 2 * NNF
C      NMM = 0
C      IFLG = 0
C
C      READ PRESSURES (10,50) FROM TAPE 3, FIRST FILE.
C      TAPE 3 WRITTEN AND REWOUND IN DATLD SUBROUTINE
C      READ ( 3) PFE, PTH, PN
C
C      READ STIFFNESS COEFF (200) FROM TAPE 9. THIS TAPE IS
C      WRITTEN IN DATLYR AND REWOUND IN DATLNK AND MAIN
C      IN - INITIAL STATION IN BLOCK
C      LN - LAST STATION IN BLOCK
C      10 READ ( 9) LN, IN, COE.C
C
C      IRTE = 1
C      MM = IN - 1
C      IFLG = IFLG + 1
C      LLN = LN - IN + 1
C      I = 0
C      KK = NNF
C      DEL2 = 2. * DEL
C
C      20 I = 1 + 1
C      MM = MM + 1
C      NMM = NMM + 1
C      IF (MM .NE. 51) GO TO 23
C      DO 21 IX = 1, KK
C      PFE50(IX) = PFE(IX,50)
C      PTH50(IX) = PTH(IX,50)
C      PN50(IX) = PN(IX,50)
C      21 READ ( 3) PFE, PTH, PN
C      NMM = 1
C      REWIND 3
C
C      23 DO 9998 J = 1, KK
C
C      FSTABLISH BOUNDARY CONDITIONS ARRAY. *

```

```

C
IF (MM .NE. 1) GO TO 33
IF (J .EQ. 1) GO TO 31
IF (BCIB .NE. 1.0) GO TO 31
IF (J .GT. 2) GO TO 29
C
27 DO 28 KN = 1,5
LLI(KN) = 0.0
DO 28 JJ = 1,5
OMG(KN, JJ) = OMGI(KN, JJ)
28 ALM(KN, JJ) = ALMI(KN, JJ)
GO TO 37
C
29 DO 30 KN = 1,5
DO 30 JJ = 1,5
OMG(KN, JJ) = 0.0
ALM(KN, JJ) = 0.0
IF (KN .EQ. JJ) ALM(KN, JJ) = 1.0
30 LLI(KN) = 0.0
GO TO 37
C
31 DO 32 KN = 1,5
LLI(KN) = LLI(KN)
DO 32 JJ = 1,5
OMG(KN, JJ) = OMGO(KN, JJ)
32 ALM(KN, JJ) = ALMO(KN, JJ)
GO TO 37
C
33 IF (MM .NE. N) GO TO 37
IF (J .EQ. 1) GO TO 34
IF (BCIB .NE. 1.0) GO TO 34
IF (J .GT. 2) GO TO 29
GO TO 27
34 DO 35 KN = 1,5
LLI(KN) = LLI(KN)
DO 35 JJ = 1,5
OMG(KN, JJ) = OMGN(KN, JJ)
35 ALM(KN, JJ) = ALMN(KN, JJ)
C
37 DO 9998 K = 1, KK
IF (I .NE. 1) GO TO 85
IF (IFLG .NE. 1) GO TO 98
C
00001090
00001100
00001110
00001120
00001130
00001139
00001140
00001145
00001150
00001160
00001170
00001190
00001195
00001200
00001210
00001230
00001240
00001250
00001260
00001270
00001279
00001280
00001285
00001290
00001300
00001310
00001330
00001339
00001340
00001350
00001360
00001370
00001380
00001390
00001395
00001400
00001410
00001420
00001439
00001440
00001450
00001460
00001470

```

CLOSED APEX, 2ND HARMONIC

CLOSED APEX, .GT. 2ND HARMONIC

1ST FOURIER COMPONENT, 1ST STA.

```

00001480
00001490
00001500
00001510
00001520
00001530
00001540
00001550
00001560
00001570
00001580
00001582
00001590
00001600
00001610
00001620
00001630
00001640
00001650
00001660
00001670
00001680
00001690
00001700
00001710
00001720
00001730
00001732
00001733
00001734
00001735
00001736
00001740
00001750
00001770
00001780
00001800
00001810
00001820
00001840
00001850
00001870
00001880

C          RECURSION FORMS          *          *          *
C
38 JMK = J - K
   KMJA = 1 + IARS(K - J)
   KPJ = K + J - 1
   TERM1 = 1.0
   IF (JMK .EQ. 0) TERM1 = 0.0
   TERM2 = 1.0
   IF (K .EQ. 1) TERM2 = 0.0
   FCTR = 1. - TERM1 + TERM2
   FCTR2 = 1. - 2. * TERM2
   IF (K+J .GT. 10) FCTR2 = 0.

C
   K1 = N2 * I + KPJ
   K2 = N2 * (I-1) + KPJ
   K3 = N2 * (I+1) + KPJ
   K4 = N2 * I + KMJA
   K5 = N2 * (I-1) + KMJA
   K6 = N2 * (I+1) + KMJA
   K7 = N2 * (I-2) + KPJ
   K8 = N2 * (I-2) + KMJA
   K9 = N2 * (I-3) + KPJ
   K10 = N2 * (I-3) + KMJA

C
   IF (IMM .NE. 1) GO TO 55

C          FORWARD DIFFERENCE FOR FIRST STATION.          *
C
   IF (J .NE. 1) GO TO 39
   FDP(V) = (4. * SCNTSI(K1) - 3. * SCNTSI(K2) - SCNTSI(K3)) / DEL2
   WTP(K) = (4. * SCMTSI(K1) - 3. * SCMTSI(K2) - SCMTSI(K3)) / DEL2
   TFE(K) = SCNTSI(K2)
   WFE(K) = SCMTSI(K2)

C
39 BPIKPJ = (4. * SCBI(K1) - 3. * SCBI(K2) - SCBI(K3)) / DEL2
   DPIKPJ = (4. * SCDI(K1) - 3. * SCDI(K2) - SCDI(K3)) / DEL2
   GIPKPJ = (4. * SCGI(K1) - 3. * SCGI(K2) - SCGI(K3)) / DEL2
   GPIKPJ = (4. * SCGI(K2) - SCGI(K3)) / DEL2

C
   BPIKMJ = (4. * SCBI(K4) - 3. * SCBI(K5) - SCBI(K6)) / DEL2
   DPIKMJ = (4. * SCDI(K4) - 3. * SCDI(K5) - SCDI(K6)) / DEL2
   GIPKMJ = (4. * SCGI(K4) - 3. * SCGI(K5) - SCGI(K6)) / DEL2
   GIPKMJ = (4. * SCGI(K4) - 3. * SCGI(K5) - SCGI(K6)) / DEL2

C

```



```

C C DERIVATIVE OF STIFFNESS RECURSIONS. *
C C
C C 40 RB1P = 0.5 * (RP1KPJ + FCTR * BP1KMJ)
C C DD1P = 0.5 * (DP1KPJ + FCTR * DP1KMJ)
C C GG13P = 0.5 * (FCR * G13KMJ + FCTR * G13KPJ)
C C GG1P = 0.5 * (FCR * GP1KMJ + FCTR * GP1KPJ)
C C
C C STIFFNESS RECURSION *
C C
C C 50 PA1KJ = 0.5 * (SCB1(K2) + FCTR * SCB1(K5))
C C DD1KJ = 0.5 * (SCD1(K2) + FCTR * SCD1(K5))
C C GG13KJ = 0.5 * (FCR * SCG13(K5) + FCTR * SCG13(K2))
C C GG1KJ = 0.5 * (FCR * SCG1(K5) + FCTR * SCG1(K2))
C C DCK3KJ = 0.5 * (DCK3(K2) + FCTR * DCK3(K5))
C C GO TO 150
C C
C C 55 IF (MM.EQ. N) GO TO 65
C C IF (J.NE. 1) GO TO 57
C C TP(K) = (SCNTSI(K1) - SCNTSI(K7)) / DEL2
C C MP(K) = (SCMTSI(K1) - SCMTSI(K7)) / DEL2
C C TFE(K) = SCNTSI(K2)
C C MFE(K) = SCMTSI(K2)
C C 5: BP1KPJ = (SCB1(K1) - SCB1(K7)) / DEL2
C C DP1KPJ = (SCD1(K1) - SCD1(K7)) / DEL2
C C G13KPJ = (SCG13(K1) - SCG13(K7)) / DEL2
C C GP1KPJ = (SCG1(K1) - SCG1(K7)) / DEL2
C C
C C 60 BP1KMJ = (SCB1(K4) - SCB1(K8)) / DEL2
C C DP1KMJ = (SCD1(K4) - SCD1(K8)) / DEL2
C C G13KMJ = (SCG13(K4) - SCG13(K8)) / DEL2
C C GP1KMJ = (SCG1(K4) - SCG1(K8)) / DEL2
C C GO TO 40
C C
C C BACKWARD DIFFERENCE FOR LAST STATION. *
C C 65 IF (J.NE. 1) GO TO 70
C C TP(K) = (SCNTSI(K9) + 3. * SCNTSI(K2) - 4. * SCNTSI(K7)) / DEL2
C C MP(K) = (SCMTSI(K9) + 3. * SCMTSI(K2) - 4. * SCMTSI(K7)) / DEL2
C C TFE(K) = SCNTSI(K2)
C C MFE(K) = SCMTSI(K2)
C C
C C 70 BP1KPJ = (SCB1(K9) + 3. * SCB1(K2) - 4. * SCB1(K7)) / DEL2
C C DP1KPJ = (SCD1(K9) + 3. * SCD1(K2) - 4. * SCD1(K7)) / DEL2
C C
00001890
00001900
00001910
00001920
00001930
00001940
00001950
00001960
00001970
00001980
00001990
00002000
00002010
00002016
00002020
00002030
00002040
00002042
00002043
00002044
00002045
00002046
00002050
00002060
00002070
00002080
00002090
00002100
00002110
00002120
00002130
00002140
00002150
00002160
00002170
00002172
00002173
00002174
00002175
00002176
00002180
00002190
00002200

```

00002210  
 00002220  
 00002230  
 00002240  
 00002250  
 00002260  
 00002270  
 00002280  
 00002290  
 00002300  
 00002310  
 00002320  
 00002330  
 00002340  
 00002350  
 00002360  
 00002370  
 00002380  
 00002390  
 00002400  
 00002410  
 00002420  
 00002423  
 00002426  
 00002430  
 00002440  
 00002450  
 00002460  
 00002470  
 00002480  
 00002490  
 00002496  
 00002500  
 00002503  
 00002506  
 00002510  
 00002519  
 00002520  
 00002529  
 00002530  
 00002540  
 00002550  
 00002560

G13KPJ = (SCG13(K9) + 3. \* SCG13(K2) - 4. \* SCG13(K7)) / DEL2  
 GPIKPJ = (SCG1(K9) + 3. \* SCG1(K2) - 4. \* SCG1(K7)) / DEL2  
 RPIKMJ = (SCB1(K10) + 3. \* SCB1(K5) - 4. \* SCB1(K8)) / DEL2  
 DPIKMJ = (SCD1(K10) + 3. \* SCD1(K5) - 4. \* SCD1(K8)) / DEL2  
 G13KMJ = (SCG13(K10) + 3. \* SCG13(K5) - 4. \* SCG13(K8)) / DEL2  
 GPIKMJ = (SCG1(K10) + 3. \* SCG1(K5) - 4. \* SCG1(K8)) / DEL2  
 GO TO 40

85 IF (LN .EQ. N) GO TO 38  
 IF (I .NE. 3) GO TO 91

AT ARBITRARY STATION 3  
 SAVE COEFF. OF LAST TWO STAS. OF THIS BLOCK. TO BE  
 USED TO COMPUTE DERIVATIVES ON NEXT BLOCK. \*

KK2 = 2 \* KK  
 K11 = N2 \* (LLN-2)  
 K12 = N2 \* (LLN-1)  
 DO 90 JK = 1, KK2  
 K13 = K11 + JK  
 K14 = K12 + JK  
 P1ENT(IK) = SCNTSI(K13)  
 P2ENT(IK) = SCNTSI(K14)  
 P1SCB1(IK) = SCB1(K13)  
 P2SCB1(IK) = SCB1(K14)  
 P1SCD1(IK) = SCD1(K13)  
 P2SCD1(IK) = SCD1(K14)  
 P1SG13(IK) = SCG13(K13)  
 P2SG13(IK) = SCG13(K14)  
 P1SCG1(IK) = SCG1(K13)  
 P2CK3(IK) = DCK3(K14)  
 P2SCG1(IK) = SCG1(K14)  
 P1EMT(IK) = SCMTSI(K13)  
 P2EMT(IK) = SCMTSI(K14)

90 CONTINUE

IS COEFF BLOCK COMPLETED

91 IF (I .EQ. LLN) GO TO 10

NO

GO TO 38

98 JMK = J - K

```

KMJA = I + IABS(K - J)
KPJ = K + J - 1
TERM1 = 1.0
IF (JMK .EQ. 0) TERM1 = 0.0
TERM2 = 1.0
IF (K .EQ. 1) TERM2 = 0.0
FCTR = 1. - TERM1 + TERM2
FCTR2 = 1. - 2. * TERM2
IF(K+J .GT. 10) FCTR2 = 0.

C
K1 = N2 * I + KPJ
K2 = N2 * (I-1) + KPJ
K4 = N2 * I + KMJA
K5 = N2 * (I-1) + KMJA

C
IRTF .NF. 1 - FIRST STATION IN A SECTION (NOT REGION).
IRTE .EQ. 1 - LAST STATION IN PREVIOUS SECTION.

C
100 IF (IRTE .NF. 1) GO TO 110

C
LAST STATION - PREVIOUS BLOCK
IF (K .NE. 1 .OR. J .NE. 1) GO TO 102
MM = MM - 1
MMN = MMN - 1
102 IF (J .NF. 1) GO TO 103
TPI(K) = (SCMTSI(K2) - PIEMT(KPJ)) /DEL2
MPI(K) = (SCMTSI(K2) - PIEMT(KPJ)) /DEL2
TFE(K) = PZEMT(KPJ)
MFE(K) = PZEMT(KPJ)
103 BPIKPJ = (SCB1(K2) - P1SCB1(KPJ)) /DEL2
DPIKMJ = (SCD1(K2) - P1SCD1(KPJ)) /DEL2
G13KPJ = (SCG13(K2) - P1SG13(KPJ)) /DEL2
GP1KPJ = (SCG1(K2) - P1SCG1(KPJ)) /DEL2

C
105 BPIKMJ = (SCB1(K5) - P2SCB1(KMJA)) /DEL2
DPIKMJ = (SCD1(K5) - P2SCD1(KMJA)) /DFL2
G13KMJ = (SCG13(K5) - P2SG13(KMJA)) /DEL2
GPIKMJ = (SCG1(K5) - P2SCG1(KMJA)) /DEL2
GO TO 120

C
FIRST STATION - NOT FIRST BLOCK
110 IF (K .NF. 1 .OR. J .NF. 1) GO TO 111
MM = MM + 1

```

```

00002570
00002580
00002590
00002600
00002610
00002620
00002630
00002640
00002645
00002650
00002660
00002670
00002680
00002690
00002700
00002701
00002702
00002703
00002710
00002719
00002720
00002730
00002740
00002750
00002752
00002753
00002754
00002755
00002756
00002760
00002770
00002780
00002790
00002800
00002810
00002820
00002830
00002840
00002850
00002860
00002900
00002910
00002920

```

```

MMN = MMN + 1
111 IF (.NE. 1) GO TO 112
TTP(K) = (SCNTSI(K1) - P2EMT(KPJ)) / DEL2
MTP(K) = (SCNTSI(K1) - P2EMT(KPJ)) / DEL2
TFE(K) = SCNTSI(K2)
MFE(K) = SCNTSI(K2)
112 BPIKPJ = (SCBI(K1) - P2SCBI(KPJ)) / DFL2
DPIKPJ = (SCDI(K1) - P2SCDI(KPJ)) / DEL2
G13KPJ = (SCG1(K1) - P2SG1(KPJ)) / DEL2
GPIKPJ = (SCG1(K1) - P2SCG1(KPJ)) / DEL2
C
BPIKMJ = (SCBI(K4) - P2SCBI(KMJA)) / DEL2
DPIKMJ = (SCDI(K4) - P2SCDI(KMJA)) / DEL2
G13KMJ = (SCG1(K4) - P2SG1(KMJA)) / DEL2
GPIKMJ = (SCG1(K4) - P2SCG1(KMJA)) / DEL2
C
120 BB1P = 0.5 * (BPIKPJ + FCTR * BPIKMJ)
DD1P = 0.5 * (DPIKPJ + FCTR * DPIKMJ)
GG13P = 0.5 * (FCTR * G13KMJ + FCTR2 * G13KPJ)
GG1P = 0.5 * (FCTR * GPIKMJ + FCTR2 * GPIKPJ)
C
125 IF (.NOT. 1) GO TO 135
TFRM11 = P2SCBI(KPJ)
TFRM21 = P2SCDI(KPJ)
AB1KJ = 0.5 * (TFRM11 + FCTR * P2SCBI(KMJA))
DD1KJ = 0.5 * (TFRM21 + FCTR * P2SCDI(KMJA))
GG13KJ = 0.5 * (FCTR * P2SG1(KMJA) + FCTR2 * P2SG1(KPJ))
GG1KJ = 0.5 * (FCTR * P2SCG1(KMJA) + FCTR2 * P2SCG1(KPJ))
DCK3KJ = 0.5 * (P2DCK3(KPJ) + FCTR * P2DCK3(KMJA))
GO TO 150
C
135 BARIKJ = 0.5 * (SCBI(K2) + FCTR * SCBI(K5))
DD1KJ = 0.5 * (SCDI(K2) + FCTR * SCDI(K5))
GG13KJ = 0.5 * (FCTR * SCG1(K5) + FCTR2 * SCG1(K2))
GG1KJ = 0.5 * (FCTR * SCG1(K5) + FCTR2 * SCG1(K2))
DCK3KJ = 0.5 * (DCK3(K2) + FCTR * DCK3(K5))
C
150 AARIKJ = AARIKJ
BARIKJ = POI * AB1KJ
SS2 = (1. - POI) / 2.
GG2KJ = SS2 * AARIKJ
GG3KJ = GG1KJ
BARIKJ = POI * BB1P

```

```

00002930
00002932
00002933
00002934
00002935
00002936
00002940
00002950
00002960
00002970
00002980
00002990
00003000
00003010
00003020
00003030
00003040
00003050
00003060
00003070
00003080
00003090
00003100
00003120
00003130
00003140
00003150
00003160
00003166
00003170
00003180
00003190
00003200
00003210
00003220
00003226
00003230
00003250
00003260
00003270
00003280
00003290
00003300

```

00003310  
 00003320  
 00003400  
 00003410  
 00003420  
 00003422  
 00003424  
 00003430  
 00003440  
 00003450  
 00003460  
 00003470  
 00003480  
 00003482  
 00003490  
 00003500  
 00003510  
 00003511  
 00003512  
 00003513  
 00003514  
 00003515  
 00003520  
 00003530  
 00003540  
 00003550  
 00003560  
 00003570  
 00003580  
 00003590  
 00003600  
 00003610  
 00003620  
 00003630  
 00003640  
 00003650  
 00003660  
 00003670  
 00003680  
 00003690  
 00003700  
 00003710  
 00003720

GG3P = GGIP  
 GG2P = SS2 \* RRIP  
 DD2KJ = DD1KJ  
 DD3KJ = POI \* DD1KJ  
 DD3P = POI \* DD1P  
 DCK1KJ = 0.  
 DCK2KJ = 0.  
 TFEK = TFE(K)  
 TTHK = TFE(K)  
 MFEK = MFE(K)  
 MTHK = MFE(K)  
 TFEIP = TTP(K)  
 MFEIP = MTP(K)  
 IF(MMN .EQ. 0) GO TO 153  
 PFEK = PFE(K,MMN)  
 PTHK = PTH(K,MMN)  
 PNK = PN(K,MMN)  
 GO TO 154

C 153 PFEK = PFE50(K)  
 PTHK = PTH50(K)  
 PNK = PN50(K)

C  
 C  
 C  
 C

P AND X FORMULATION

C 154 WTH = WTHX(MM)  
 WFE = WFEX(MM)  
 GAM = GAMA(MM)  
 RHO = RHOX(MM)  
 WFEP = WFEPX(MM)  
 LAM = HO /AO  
 LAM2 = LAM \* LAM  
 LAM02 = LAM /2.  
 LAM202 = LAM \* LAM02  
 LAM204 = LAM02 \* LAM02  
 LAM208 = LAM204 /2.  
 GAM2 = GAM \*\*2  
 WTMWF = WTH - WFE  
 WTMWF2 = WTMWF \*\*2  
 WFWT = WFE \* WTH

C IF (IFLG .NF. 1) GO TO 235

\*\*

```

C      IF ( I .NE. 1) GO TO 235
C
C      195 CALL RSLT (J,K,KK)
C      IF (IRSFG .GT. 1) GO TO 9998
C      IF (IRSFG .EQ. 1) GO TO 20
C      RETURN
C
C      295 IF ( I .NE. LLN) GO TO 237
C      IF (LN .EQ. N) GO TO 155
C
C      237 CALL FGHPE (J,K,KK,IRTE)
C      IF (IFGFG .GT. 1) GO TO 9998
C      IF (IFGFG .EQ. 1) GO TO 20
C      GO TO 23
C      9998 CONTINUE
C
C      340 FORMAT(1H--,14HENTERED PANDX. )
C      RETURN
C      FND

```

SET UP BOUNDARY MATRICES

SET UP MATRICES IN EQUILIBRIUM EQ.

```

00003730
00003740
00003749
00003750
00003760
00003770
00003780
00003790
00003800
00003810
00003818
00003819
00003820
00003830
00003840
00003850
00003880
00003890
00003900
00003910
00003920

```

3.11g RSLT Subroutine (BNDRY)

```

SUBFC BNDRY
SUBROUTINE RSLT (J,K,KN)
C
C COMPUTES THE BOUNDARY MATRICES FOR IP AND X MATRICES.
C
DIMENSION R(50,50), AA(50,50), S(50,50), LI(50)
DIMENSION STAG(5,5), X(10), ZX(50)
C
COMMON GDA(25), DEL, N, NNF, NIB,
1 BMTX(16)
C
COMMON /PXCMT/
2 BRKJ, HR2KJ, GR2KJ, GR2KJ, GR2KJ, GR2KJ, GR2KJ, GR2KJ,
3 GG13KJ, TFEK, THIK, WFEK, WFEK, WFEK, WFEK, WFEK, WFEK,
4 DDIP, DDIP, GG13P, TFEIP, WFEIP, WFEIP, WFEIP, WFEIP,
5 WIM, WEL, GAM, KMG, WFP, LAM, LAM2, LAM2, LAM2, LAM2,
6 LAM208, GAM2, WIMW, WIMW2, WIM, WIM, WIM, WIM,
7 DCKIKJ, DCF2KJ, DCK3KJ
C
COMMON /HLOCK1/ FMM2(50,50)
COMMON /HLOCK2/ FMM3(50)
C
EQUIVALENCE (GDA( 1), A(1),
1 (GDA( 3), L(1),
2 (GDA( 5), P(1),
3 (GDA( 7), BC(1),
4 (GDA( 9), PFLA(1),
5 (GDA(11), THT),
6 (GDA(12), THT))
C
REAL LAM, LAM2, LAM208, LAM208, LAM208, LAM208, LAM208,
1 TFEK, THIK, WFEK, WFEK, WFEK, WFEK, WFEK, WFEK,
C
R, S, LT MATRICES IN BOUNDARY EQUATIONS (44, 42) S(1) S(1) 164
C
KK5 = 5 * NNF
KCRO = 0
IF (J .NE. 1) GO TO 164
IF (J .NE. 1) GO TO 164
C
ZERO ARRAYS FOR ALL MATRICES.
C
DO 161 KN = 1,KN

```

L1(0,0) = 0.0  
 D0 162 JJ = 1.0K  
 S(K0,0) = 0.0  
 R(KV,0) = 0.0  
 162 CONTINUE  
 163 CONTINUE  
 C  
 164 IF(RHO.EQ.0.) GO TO 165  
 KORO = FLOAT(K-1) / RHO  
 .165 KORO = KORO \* KORO  
 R(5\*K-4,5\*J-4) = RB(KJ) \* 0.45(1,1)  
 R(5\*K-3,5\*J-3) = GG(KJ) / 2. + LA\*208 \* W(1) \* J \* 0.13KJ  
 R(5\*K-2,5\*J-2) = LA\*204 \* W(1) \* J \* 0.13KJ  
 R(5\*K-1,5\*J-1) = GG(KJ)  
 R(5\*K,5\*J) = ((GG(KJ) \* W(1) / 2.) + KORO) \* 0.70(5,5)  
 R(5\*K,5\*J) = GG(KJ) \* 0.5 \* K \* GG(0,0)  
 R(5\*K-4,5\*J-3) = K(1) \* K(1) \* J \* 0.16(1,2)  
 R(5\*K-4,5\*J) = R(5\*K-3,5\*J) \* 0.16(1,2)  
 R(5\*K-3,5\*J-1) = R(5\*K-1,5\*J-1) \* 0.16(5,6)  
 C  
 S(5\*K-4,5\*J-4) = (GA) \* 0.35KJ  
 S(5\*K-4,5\*J-3) = KORO \* 0.35KJ  
 S(5\*K-4,5\*J-2) = W(1) \* 0.35KJ + W(1) \* 0.16(5,6)  
 S(5\*K-3,5\*J-4) = LA\*208 \* 0.16(5,6) \* 0.13KJ + 0.13KJ / 2.  
 S(5\*K-3,5\*J-3) = CA \* S(5\*K-2,5\*J-4)  
 S(5\*K-3,5\*J) = -GA \* 0.35KJ  
 S(5\*K-2,5\*J-4) = KORO \* S(5\*K-1,5\*J-4)  
 S(5\*K-2,5\*J-3) = -KORO \* S(5\*K-1,5\*J)  
 S(5\*K-2,5\*J-2) = W(1) \* 0.2KJ \* 0.16(3,4)  
 S(5\*K-2,5\*J-1) = 0.2KJ \* 0.16(3,4)  
 S(5\*K-1,5\*J-1) = (GA) \* 0.35KJ  
 S(5\*K,5\*J) = 0.35KJ  
 S(5\*K,5\*J-1) = (GA) \* 0.35KJ \* 0.16(7,8)  
 S(5\*K,5\*J-2) = (GA) \* 0.35KJ \* 0.16(7,8)  
 S(5\*K,5\*J-3) = KORO \* S(5\*K,5\*J-4)  
 S(5\*K,5\*J-4) = KORO \* S(5\*K,5\*J-4)  
 S(5\*K,5\*J-1) = -GA \* 0.35KJ / 2.  
 S(5\*K,5\*J-2) = -GA \* 0.35KJ / 2.  
 R(5\*K-4,5\*J-3) = R(5\*K-1,5\*J-1) \* 0.16(2,3)  
 R(5\*K-3,5\*J) = R(5\*K-3,5\*J) \* 0.16(2,3)  
 R(5\*K-1,5\*J-1) = R(5\*K-1,5\*J-1) \* 0.16(4,5)  
 S(5\*K-4,5\*J-4) = S(5\*K-4,5\*J-4) \* S(5\*K(1,1) + 0.16(3,4) \* 0.16(5,6)



```

1 OMG(1,2) 20000870
S(5*K-4,5*J-3) = S(5*K-4,5*J-3) * OMG(1,1) + S(5*K-3,5*J-2) *
1 OMG(1,2) 00000880
S(5*K-4,5*J-2) = S(5*K-4,5*J-2) * OMG(1,1) 00000890
S(5*K-4,5*J-1) = S(5*K-3,5*J-1) * OMG(1,2) 00000900
S(5*K-4,5*J) = S(5*K-3,5*J) * OMG(1,2) 00000910
S(5*K-3,5*J-3) = S(5*K-3,5*J-3) * OMG(2,2) 00000920
S(5*K-3,5*J-2) = S(5*K-3,5*J-2) * OMG(2,2) 00000930
S(5*K-3,5*J-1) = S(5*K-3,5*J-1) * OMG(2,2) 00000940
S(5*K-3,5*J) = S(5*K-3,5*J) * OMG(2,2) 00000950
S(5*K-3,5*J-4) = S(5*K-3,5*J-4) * OMG(2,2) 00000960
S(5*K-3,5*J-1) = S(5*K-3,5*J-1) * OMG(2,2) 00000970
S(5*K-3,5*J) = S(5*K-3,5*J) * OMG(2,2) 00000980
S(5*K-3,5*J-4) = S(5*K-3,5*J-4) * OMG(2,2) 00000990
S(5*K-3,5*J-3) = S(5*K-3,5*J-3) * OMG(2,2) 00001000
S(5*K-3,5*J-2) = S(5*K-3,5*J-2) * OMG(2,2) 00001010
S(5*K-3,5*J-1) = S(5*K-3,5*J-1) * OMG(2,2) 00001020
S(5*K-3,5*J) = S(5*K-3,5*J) * OMG(2,2) 00001030
S(5*K-3,5*J-4) = S(5*K-3,5*J-4) * OMG(2,2) 00001040
S(5*K-3,5*J-3) = S(5*K-3,5*J-3) * OMG(2,2) 00001050
S(5*K-3,5*J-2) = S(5*K-3,5*J-2) * OMG(2,2) 00001060
S(5*K-3,5*J-1) = S(5*K-3,5*J-1) * OMG(2,2) 00001070
S(5*K-3,5*J) = S(5*K-3,5*J) * OMG(2,2) 00001080
S(5*K-1,5*J-1) = S(5*K-1,5*J-1) * OMG(4,4) 00001090
S(5*K-1,5*J) = S(5*K-1,5*J) * OMG(4,4) + S(5*K-1,5*J) * OMG(5,4) 00001100
S(5*K-1,5*J-2) = S(5*K-1,5*J-2) * OMG(4,4) 00001110
S(5*K-1,5*J-1) = S(5*K-1,5*J-1) * OMG(4,4) 00001120
S(5*K-1,5*J) = S(5*K-1,5*J) * OMG(4,4) 00001130
S(5*K-1,5*J-2) = S(5*K-1,5*J-2) * OMG(4,4) + LLI(4) 00001140
S(5*K-1,5*J-1) = S(5*K-1,5*J-1) * OMG(4,4) + LLI(4) 00001150
S(5*K-1,5*J) = S(5*K-1,5*J) * OMG(4,4) + LLI(4) 00001160
S(5*K-1,5*J-2) = S(5*K-1,5*J-2) * OMG(4,4) + LLI(4) 00001170
S(5*K-1,5*J-1) = S(5*K-1,5*J-1) * OMG(4,4) + LLI(4) 00001180
S(5*K-1,5*J) = S(5*K-1,5*J) * OMG(4,4) + LLI(4) 00001190
S(5*K-2,5*J-2) = ALM(3,3) 00001200
S(5*K-4,5*J-4) = S(5*K-4,5*J-4) + ALM(1,1) 00001210
S(5*K-3,5*J-3) = S(5*K-3,5*J-3) + ALM(2,2) 00001220
S(5*K-3,5*J-4) = S(5*K-3,5*J-4) + ALM(2,2) 00001230
S(5*K-1,5*J-1) = S(5*K-1,5*J-1) + ALM(4,4) 00001240
S(5*K-1,5*J) = S(5*K-1,5*J) + ALM(4,4) 00001250
S(5*K-5*J) = S(5*K-5*J) + ALM(4,5) 00001260
S(5*K-5*J) = S(5*K-5*J) + ALM(4,5) 00001270
166 IF (K .NE. JJ) GO TO 167 00001280
IF (J .EQ. KK) GO TO 164 00001290
167 IRSFG = 10 00001300
RETURN 00001310
169 IF (IFLG .GT. 1) GO TO 305 00001320
IF (I .GT. 1) GO TO 305 00001330
A = FILE(3,1) 00001340
INITIAL BOUNDARY * * * 00001350
C 00001360
C 00001370

```





162	CONTINUE		0.0000417
163	CONTINUE		0.0000420
			0.0000429
			0.0000430
			0.0000440
			0.0000449
			0.0000450
			0.0000451
			0.0000460
			0.0000480
			0.0000500
			0.0000510
			0.0000520
			0.0000530
			0.0000539
			0.000054
			0.0000550
			0.000056
			0.0000570
			0.0000580
			0.0000610
			0.0000620
			0.0000621
			0.0000650
			0.0000670
			0.0000671
			0.000069
			0.000070
			0.0000710
			0.0000720
			0.000074
			0.0000750
			0.0000760
			0.0000770
			0.0000780
			0.0000781
			0.0000800
			0.0000810
			0.0000818
			0.0000820
			0.0000821
			0.0000822

1	H(5**K-4.5**J-3) = KORO * ( BB3P - GAM * BB2KJ - GAM / 2. * GG1KJ - GAM * WTMWF2 * LAM208 * GG13KJ )	00000850
	H(5**K-4.5**J-2) = WFE * BB1P + WTH * ( BB3P - GAM * BB2KJ )	00000851
1	1 + BB1KJ * ( WFFP + GAM * WFF )	00000880
184	H(5**K-4.5**J-1) = WFE * GG2KJ + KOR02 * LAM204 * WTMWF * GG13KJ	00000900
	H(5**K-4.5**J) = KORO * GAM * LAM204 * WTMWF * GG13KJ	00000930
1	H(5**K-3.5**J-4) = KORO * ( LAM208 * ( WTMWF2 * GG13P - WTMWF * GG13KJ * ( 3. * GAM * WTMWF - 2. * WFFP ) ) - GG1P / 2. + GAM	00000951
2	* ( -GG1KJ / 2. - HR2KJ )	00000952
	H(5**K-3.5**J-3) = ( WFT - GAM / 2. * GG1KJ - GAM / 2. * GG1P	00000980
1	- KOR02 * BB2KJ - WTH * *2 * GG1P + LAM208 * ( GAM * WTMWF2 * GG13P - GG13KJ * ( WTMWF2 * ( WFT + 3. * GAM ) + 2. * WTMWF	00000981
2	* GAM * WFFP ) - DCK2KJ	00000982
3	* GAM * WFFP ) - DCK2KJ	00000983
190	H(5**K-3.5**J-2) = KORO * ( WFF * BB3KJ + WTH * ( BB2KJ + GG1KJ ) )	00001020
	H(5**K-3.5**J-1) = KORO * ( LAM204 * ( GAM * ( 2. * WTMWF + WFFP ) * GG13KJ - WTMWF * GG13P ) )	00001030
1	GG13KJ - WTMWF * GG13P )	00001040
	H(5**K-3.5**J) = WTH * GG3KJ + LAM204 * WTMWF * GG13P + GAM * LAM204	00001060
2	( GG13KJ * ( WFT + 2. * GAM2 ) - GAM * GG13P ) + GAM * LAM204	00001080
3	* WFFP * GG13KJ	00001090
199	H(5**K-2.5**J-4) = GG2KJ * ( WFFP + GAM * WFF ) - WFF * ( GAM * BB3KJ + GG2P ) - WTH * GAM * BB2KJ	00001100
	H(5**K-2.5**J-3) = H(5**K-3.5**J-2)	00001110
	H(5**K-2.5**J-2) = KORO * GG3KJ - WFE * *2 * BB1KJ - WTH * ( 2. * WTMWF	00001120
1	WFE * BB3KJ + WTH * BB2KJ ) - DCK3KJ	00001130
	H(5**K-2.5**J-1) = GG2P + GAM * GG2KJ	00001140
	H(5**K-2.5**J) = KORO * GG3KJ	00001150
	H(5**K-1.5**J-4) = H(5**K-4.5**J-1)	00001170
	H(5**K-1.5**J-3) = KORO * LAM204 * GAM * WTMWF * GG13KJ	00001190
195	H(5**K-1.5**J-1) = LAM2 * ( GAM * DD3P - WFT * DD3KJ - KOR02 / 2. * GG13KJ - GAM2 * DD2KJ ) - GG2KJ	00001200
1	H(5**K-1.5**J) = LAM2 * KORO * ( DD3P - GAM * ( GG13KJ / 2. + DD2KJ ) )	00001250
	H(5**K.5**J-4) = KORO * LAM204 * ( WTMWF * GG13P - WFFP * GG13KJ )	00001260
	H(5**K.5**J-3) = LAM204 * ( GAM * WTMWF * GG13P - GG13KJ * ( GAM * WFFP + WFT * WTMWF ) ) + WTH * GG3KJ	00001280
1	H(5**K.5**J-2) = H(5**K-2.5**J)	00001290
198	H(5**K.5**J-1) = KORO * ( LAM202 * ( GG13P + GAM * GG13KJ ) + LAM2 * GAM * DD2KJ )	00001310
	H(5**K.5**J) = LAM202 * ( ( WFT - GAM2 ) * GG13KJ - GAM * GG13P )	00001311
1	- KOR02 * LAM2 * DD2KJ - GG3KJ	00001340
	PE(5**K-4) = - PFEK + TFETP + GAM * ( TFETK - TTHK )	00001350
	PE(5**K-3) = - PTHK - TTHK * KORO	00001360
		00001370
		00001380
		00001390
		00001400

```

PE(5*K-2) = - PAK - AEG * DEL * WIM * THIK
PE(5*K-1) = LAM2 * TAPETP + GAR * (OFFT - THIK)
PE(5*K) = - KOR * LAM2 * MHTA
C
IF (K * NF * KK) GO TO 203
IF (J * EQ * KK) GO TO 208
203 IFGFG = 10
GO TO 261
C
C
C
C
FORM MATRICES A, B, C, D, E
C
208 DO 210 K=1, KK5
DO 210 J=1, KK5
210 F(K,J) = (2./DEL) * F(K,J)
CALL MAD (KK5, KK5, F, G, EMM2)
CALL MSU (KK5, KK5, F, G, G)
DO 212 K=1, KK5
PE(K) = 2. * DEL * PE(K)
DO 212 J=1, KK5
H(K,J) = 2. * DEL * H(K,J)
212 F(K,J) = - 2. * F(K,J)
CALL MAD (KK5, KK5, F, H, H)
DO 214 K=1, KK5
DO 214 J=1, KK5
214 F(K,J) = FM2(K,J)
C
C
C
C
COMPUTE P AND X
IF (MM * NF * 2) GO TO 240
CALL INVMN (C, 5J, KK5, IERK)
IF (IERR * LF * 0) GO TO 320
C
C
C
C
WRITE ON TAPE - TO BE USED WHEN FORMING Z(1)
ORDER - A, B, C, G
C
C
C
C
WRITE (3) F, H, G, PE
BACKSPACE 3
BACKSPACE 3
C
C
C
STATION NO. 2 - TOP BOUNDARY *
C
C

```

BACKSPACE 3 WHEN NOT USING AIRIO

C	READ MATRICES GENERATED IN 'RSLT'	*	00001840
C			00001850
C			00001860
C	READ G0 *	*	00001870
C			00001880
C			00001890
C	READ ( 3 ) LT		00001900
C	BACKSPACE 3		00001910
C	BACKSPACE 3		00001920
C	READ C0 *	*	00001930
C			00001940
C			00001950
C	READ ( 3 ) S		00001960
C	CALL MMY (KK5, KK5, KK5, S, G, EMM2 )		00001970
C	CALL MMY (KK5, KK5, KK5, EMM2, F, G )		00001980
C	BACKSPACE 3		00001990
C	BACKSPACE 3		00002000
C	READ A0 *	*	00002010
C			00002020
C			00002030
C	READ ( 3 ) S		00002040
C	CALL MSU (KK5, KK5, S, G, F )		00002050
C	CALL MMY (KK5, KK5, 1, EMM2, PF, EMM3 )		00002060
C	BACKSPACE 3		00002070
C	BACKSPACE 3		00002080
C	READ B0 *	*	00002090
C			00002100
C			00002110
C	READ ( 3 ) S		00002120
C	CALL MSU (KK5, KK5, S, G, S )		00002130
C	CALL MMY (KK5, KK5, 1, EMM2, PF, EMM3 )		00002140
C	CALL MSU (KK5, 1, LI, EMM3, LI )		00002150
C	CALL INVNM (S, 50, KK5, TERR )		00002160
C	IF (IFERR .LE. 0) GO TO 320		00002170
C			00002180
C	CALL MMY (KK5, KK5, KK5, S, F, P )		00002190
C	CALL MMY (KK5, KK5, 1, S, LI, X )		00002200
C	BACKSPACE 3		00002210
C	BACKSPACE 3		00002220
C			00002230
C	225 WRITE (10) I, P, X		00002240
C	290 IFGFG = 1		00002250
C	GO TO 261		00002260
C			00002270

\*BACKSPACE 3 WHEN NOT USING ALIAS





3. 11i ZMTRX Subroutine (SOLTN)

```

SIBFTC SOLTN          00000010
C SOLUTION MATRICES  00000020
C                   00000029
C                   00000036
C                   00000040
C                   00000050
C DIMENSION PX(50,50), XX(50), ZX(50), AA11(50,50), BB11(50,50),
I CC11(50,50), GG11(50), Z(50)
C DIMENSION ZX2(50), BHC(50,50), GGU(50)
C                   00000099
C                   00000110
C                   00000119
C EQUIVALENCE (GDAI 9), PFLAG)
C
C COMMON /BLK1/ EMM2(50,50)
C COMMON /BLK2/ EMM3(50)
C COMMON GDAI(25), DEL, N, NNF, NIH,
I RMTX(160)
C                   00000160
C                   00000170
C                   00000180
C DO 15 I = 1,50
C 15 Z(I) = 0.0
C
C READ MATRICES P AND X FOR STA. (N-2)
C
C READ (4) BR0, GGO
C END FILE 4
C
C KK5 = 5 * NNF
C DO 100 NN = 1,N
C MN = N - NN + 1
C IF (NN.EQ. 1) GO TO 20
C
C READ MATRICES P AND X FOR STA. (N-1).
C
C READ (10) I, PX, XX
C
C READ MATRICES A, B, C, E(PE) GENERATED FOR STA. (N)
C
C READ (10) AA11, BB11, CC11, GG11
C CALL MMY(KK5, KK5, AA11, BR0, EMM2 )
C CALL MMSU(KK5, KK5, EMM2, BB11, BB11 )
C CALL MMY(KK5, KK5, I, AA11, GGU, EMM3 )
C CALL MMSU(KK5, I, GG11, EMM3, GG11 )

```

```

CALL MMY(KK5, KK5, 1, BB11, XX, LMM3 )
CALL MMAD(KK5, 1, GG11, LMM3, GG11 )
CALL MMY(KK5, KK5, KK5, BB11, PX, FMM2 )
CALL MMAD(KK5, KK5, CC11, FMM2, CC11 )
CALL INMS (CC11, 50, KK5, IERR )
IF (IERR .NE. 0) GO TO 120
CALL MMY(KK5, KK5, 1, CC11, GG11, ZX )
C
WRITE ( 4) MN, ZX
C
WRITE (6, 130) MN, (ZX(IX), IX=1, KK5)
GO TO 100
C
20 IF (NN .EQ. N) GO TO 40
BACKSPACE 10
BACKSPACE 10
READ (10) I, PX, XX
C
CALL MMY (KK5, KK5, 1, PX, ZX, Z )
CALL MMSU (KK5, 1, XX, Z, Z )
C
IF (MN .NE. N-2) GO TO 30
DO 25 K = 1, KK5
25 ZX(K) = Z(K)
30 DO 35 K = 1, KK5
35 ZX(K) = Z(K)
C
WRITE ( 4) MN, ZX
C
WRITE (6, 140) MN, (ZX(IX), IX=1, KK5)
GO TO 100
C
READ MATRICES A, B, C, E(PE) GENERATED FOR STA. (2)
C
40 READ ( 3) AA11, BB11, CC11, GG11
CALL MMY(KK5, KK5, 1, BB11, ZX, PX )
CALL MMY(KK5, KK5, 1, AA11, ZX, ZX )
CALL MMSU(KK5, 1, GG11, ZX, GG11 )
CALL MMSU(KK5, 1, GG11, PX, GG11 )
CALL MMY(KK5, KK5, 1, CC11, GG11, Z )
C
WRITE (6, 140) MN, (Z(IX), IX=1, KK5)

```

```

C      WRITE ( 4) MN, Z      00000819
100 CONTINUE                00000820
C                             00000830
C                             00000840
      IF (PFLAG .EQ. -1.E+10) WRITE(6,109)
109 FORMAT (1H-, 10HLEFT SOLTN )
110 RETURN                  00000842
C                             00000843
C                             00000850
C                             00000859
120 WRITE (6,125)           00000860
      CALL EXIT              00000870
      STOP                   00000880
125 FORMAT (1H-,10X,45HERROR - INVERSION OF SINGULAR MATRIX IN 'Z', 100000890
C                             00000900
130 FORMAT (1H1,10X,24H'Z', MATRIX FOR STATION , 14// (12X,1P5E17.7)) 00000910
140 FORMAT (/// 10X,24H'Z', MATRIX FOR STATION , 14// (12X,1P5E17.7)) 00000915
C                             00000920
C                             00000930
      END

```

\$IBFTC SUSM	SOLUTION SUMMATION	W/ STRESSES	**	00000010
C				00000020
C				00000030
C	SUBROUTINE SUMS			00000040
C				00000041
C				00000042
C	NOMENCLATURE			00000043
C	THT	HORIZONTAL ANGLES (DEGREES) 5 MAXIMUM		00000044
C	FPRNT	FOURIER COMPONENT PRINT VALUES OF DEFLECTIONS AND		00000045
C		ROTATIONS (3 POSSIBLE)		00000050
C				00000060
C	DIMENSION	Z(50), THT( 6), FPRNT( 3)		00000070
C	DIMENSION	ULZ(100,5), VLZ(100,5), WLZ(100,5), PHS LZ(100,5),		00000080
C	1	PHTLZ(100,5), UL(100,5), VL(100,5), WL(100,5),		00000090
C	2	PHSL(100,5), PHIL(100,5), WFFX(100), WTHX(100),		00000100
C	3	GAMA(100), RHOX(100), WFFPX(100)		00000110
C				00000150
C	DIMENSION	R1(100,5), B2(100,5), B3(100,5), D1(100,5), D2(100,5),		00000151
C	1	D3(100,5), G1(100,5), G2(100,5), G3(100,5), G13(100,5),		00000152
C	2	ENTSI(100,5), ENITH(100,5), EMTSI(100,5), EMITH(100,5)		00000160
C				00000170
C	DIMENSION	ENFE( 5), FNTH( 5), ENFT( 5), OFE( 5), EMFE( 5),		00000180
C	1	EMTH( 5), EMFT( 5), QTH( 5)		00000190
C				00000200
C	DIMENSION	SIGSI1(5), SIGTH1(5), TAUST1(5), TAUSG1(5),		00000210
C	1	TAUTG1(5), SIGSI2(5), SIGTH2(5), TAUSI2(5), TAUSG2(5),		00000220
C	2	TAUTG2(5)		00000230
C				00000240
C	DIMENSION	COFFC(3000)		00000250
C	DIMENSION	SCB1(200), SCB2(200), SCB3(200), SCG1(200), SCG2(200),		00000260
C	1	SCG3( 200), SCD1(200), SCD2(200), SCD3(200), SCG13(200),		00000270
C	2	SCNTSI(200), SCNITH(200), SCMISI(200), SCMIIH(200)		00000390
C				00000400
C	EQUIVALENCE	(GDA( 1), A0),	(GDA( 2), H01),	00000410
C	1	(GDA( 3), E0),	(GDA( 4), SIG0),	00000420
C	2	(GDA( 5), P01),	(GDA( 6), ENF),	00000430
C	3	(GDA( 7), RCIT),	(GDA( 8), BCIB),	00000431
C	4	(GDA( 9), PFLAG),	(GDA(12), THT),	00000432
C	5			00000433
C	6	(GDA(18), FPRNT)		00000440
C				00000450
C	EQUIVALENCE	(COEFC( 1), SCB1),	(COEFC( 201), SCR2),	00000460
C	1	(COEFC( 401), SCB3),	(COEFC( 601), SCG1),	00000470
C	2	(COEFC( 801), SCG2),	(COEFC(1001), SCG3),	

```

3 (COEFC(1201), SCD1), (COEFC(1401), SCD2), (COEFC(1601), SCD3), 00002480
4 (COEFC(1801), SCG13), (COEFC(2001), SCNTS1), (COEFC(2201), SCNTTH), 00000490
5 (COEFC(2401), SCMTS1), (COEFC(2601), SCMTTH) 00000500
C 00000510
C 00000520
C 00000530
C 00000540
C 00000560
C 00000610
C 00000620
C 00000630
C 00000639
C 00000640
C 00000645
C 00000650
C 00000660
C 00000670
C 00000680
C 00000690
C 00000700
C 00000710
C 00000720
C 00000722
C 00000724
C 00000726
C 00000730
C 00000740
C 00000750
C 00000760
C 00000770
C 00000780
C 00000790
C 00000800
C 00000810
C 00000820
C 00000830
C 00000840
C 00000850
C 00000860
C 00000870
C 00000880
C 00000890
C 00000900

COMMON GDA(25), DEL, N, NNF, NTH, BMTX(160)

REWIND 4

A = FILF (4,1)
SS1 = SIGN/FO
SS2 = SS1 * A0

DO 200 I = 1, N
IF (I .EQ. 1) WRITE ( 6, 246)
II = N - I + 1

READ ( 4) MN, Z

WRITE (6, 290) II

DO 35 IT = 1, 5
B1(I, IT) = 0.0
D1(I, IT) = 0.0
ENTSI(I, IT) = 0.0
EMTSI(I, IT) = 0.0
ULZ(I, IT) = 0.0
VLZ(I, IT) = 0.0
WLZ(I, IT) = 0.0
PHSLZ(I, IT) = 0.0
35 PHTLZ(I, IT) = 0.0

C
IT = 1
50 U = 0.0
V = 0.0
W = 0.0
PHS = 0.0
PHT = 0.0
IX = 1
THETA = THT(IT)

C
DO 150 NF = 1, NNF
ANF = NF - 1
NT = (NF - 1) * 5

```

```

0000910
0000920
0000930
0000940
0000950
0000960
0000970
0000980
0000990
0001000
0001010
0001020
0001030
0001040
0001050
0001060
0001070
0001080
0001089
0001090
0001100
0001110
0001120
0001130
0001140
0001150
0001160
0001170
0001180
0001190
0001200
0001210
0001229
0001230
0001240
0001250
0001260
0001270
0001280
0001290
0001300
0001310
0001320

NU = NT + 1
NV = NT + 2
NW = NU + 2
NFS = NV + 2
NFT = NW + 2
FCT = COSD (ANF * THETA)
FCT2 = FCT * SS2
FCT1 = FCT * SS1
FCT3 = SIND (ANF * THETA)
FCT4 = SS2 * FCT3
FCT5 = SS1 * FCT3

C
U = U + Z(NU) * FCT2
V = V + Z(NV) * FCT4
W = W + Z(NW) * FCT2
PHS = PHS + Z(NFS) * FCT1
PHT = PHT + Z(NFT) * FCT5

C
C
DERIVATIVES WITH RESPECT TO THETA
ULZ(I,IT) = ULZ(I,IT) - Z(NU) * FCT4 * ANF
VLZ(I,IT) = VLZ(I,IT) + Z(NV) * FCT2 * ANF
WLZ(I,IT) = WLZ(I,IT) - Z(NW) * FCT4 * ANF
PHSLZ(I,IT) = PHSLZ(I,IT) - Z(NFS) * FCT5 * ANF
PHTLZ(I,IT) = PHTLZ(I,IT) + Z(NFT) * FCT1 * ANF

C
BNF = ANF + 1.
IF (BNF .NE. FPRNT(IX)) GO TO 150

WRITE (6,300) THETA, ANF, U, V, W, PHS, PHT
IX = IX + 1
150 CONTINUE

C
DISPLACEMENTS
UL(I,IT) = U
VL(I,IT) = V
WL(I,IT) = W
PHSL(I,IT) = PHS
PHTL(I,IT) = PHT

C
IF (THT(IT+1) .LT. 0.0) GO TO 200
IT = IT + 1
GO TO 50
200 CONTINUE

```

```

C
REWIND 4
IIT = IT
S1 = FO * HO
S2 = S1 * HO * HO
S3 = (1. - POI)/2.
S4 = SIGO * HO
S5 = AO / (S4 * HO **2)
II = 0
NF2 = 2 * NNF

C
210 READ ( 9) LN, IN, COEFC
LLN = LN - IN + 1
DO 240 I = 1, LLN
II = II + 1
K1 = NF2 * (I-1)

C
DO 230 IT = 1, IIT
THETA = THJ/IT)
DO 225 NF = 1, NF2
ANF = NF - 1
K2 = K1 + NF
B1(II,IT) = B1(II,IT) + SCB1(K2) * COSD(ANF * THETA) * S1
D1(II,IT) = D1(II,IT) + SCD1(K2) * COSD(ANF * THETA) * S2
EMTSI(II,IT) = EMTSI(II,IT) + SCNTSI(K2) * THETA * S4
EMTSI(II,IT) = EMTSI(II,IT) + SCMTSI(K2) * THETA * S5

225 CONTINUE
B11 = B1(II,IT)
D11 = D1(II,IT)
B2(II,IT) = B11
B3(II,IT) = POI * B11
D2(II,IT) = D11
D3(II,IT) = POI * D11
G1(II,IT) = S3 * B11
G2(II,IT) = S3 * R11
G3(II,IT) = B11 * S3
G13(II,IT) = S3 * D11
EMTH(II,IT) = EMTSI(II,IT)
EMTTH(II,IT) = EMTSI(II,IT)

230 CONTINUE
240 CONTINUE

C
IF (LN .EQ. N) GO TO 245

```

00001330  
00001340  
00001350  
00001360  
00001370  
00001380  
00001383  
00001386  
00001390  
00001400  
00001410  
00001420  
00001430  
00001440  
00001450  
00001460  
00001470  
00001480  
00001490  
00001500  
00001510  
00001520  
00001530  
00001540  
00001543  
00001546  
00001550  
00001560  
00001570  
00001580  
00001590  
00001630  
00001640  
00001650  
00001660  
00001670  
00001690  
00001710  
00001730  
00001740  
00001750  
00001760  
00001770

```

C      GO TO 210
C      245 READ ( 4 ) WTHX, WFFX, GAMA, RHOX, WFFPX
C
C      K1 = 1
C      K2 = 2
C      DNM = -2. * DFL
C
C      DO 275 I = 1,N
C      IF (I.EQ. 1) WRITE( 6,246)
C      246 FORMAT( IH1 )
C      L = N - I + 1
C      H = L
C      PEL = (H - 1.) * DEL
C      WFF = WFFX(L)
C      WTH = WTHX(L)
C      GAM = GAMA(L)
C      RHO = RHOX(L)
C      DRHO = 0.
C      IF(RHO.NE. 0.) DRHO = 1. /RHO
C      DAO = 1./AO
C
C      DO 265 IT = 1,IT1
C      THETA = THT(IT)
C      ZIA = THETA * .017453293
C
C      DERIVATIVES WITH RESPECT TO PSI
C
C      IF (I.NE. 1) GO TO 250
C
C      LAST STATION
C      ULP = (4. * UL(I,IT) - 3. * UL(I+1,IT) - UL(I+2,IT)) / DNM
C      VLP = (4. * VL(I,IT) - 3. * VL(I+1,IT) - VL(I+2,IT)) / DNM
C      WLP = (4. * WL(I+1,IT) - 3. * WL(I,IT) - WL(I+2,IT)) / DNM
C      PHSLP = (4. * PHSL(I+1,IT) - 3. * PHSL(I,IT) - PHSL(I+2,IT)) / DNM
C      PHTLP = (4. * PHTL(I+1,IT) - 3. * PHTL(I,IT) - PHTL(I+2,IT)) / DNM
C      GO TO 260
C      250 IF (I.EQ. N) GO TO 255
C
C      (NOTE - 'I' IS COUNTING BACKWARDS)
C      ULP = (UL(I+1,IT) - UL(I-1,IT)) / DNM
C      VLP = (VL(I+1,IT) - VL(I-1,IT)) / DNM
C      WLP = (WL(I+1,IT) - WL(I-1,IT)) / DNM
C      PHSLP = (PHSL(I+1,IT) - PHSL(I-1,IT)) / DNM
C      PHTLP = (PHTL(I+1,IT) - PHTL(I-1,IT)) / DNM
C      GO TO 260
C
C      FIRST STATION
C

```

00001750  
00001790  
00001800  
00001810  
00001820  
00001821  
00001840  
00001860  
00001870  
00001872  
00001874  
00001880  
00001890  
00001895  
00001900  
00001910  
00001920  
00001930  
00001940  
00001941  
00001950  
00001959  
00001960  
00001970  
00001972  
00001979  
00001980  
00001989  
00001990  
00002000  
00002010  
00002020  
00002030  
00002040  
00002050  
00002059  
00002060  
00002070  
00002080  
00002090  
00002100  
00002110  
00002119



```

255 ULP = (UL(I-2,IT) + 3. * UL(I,IT) - 4. * UL(I-1,IT)) /DNM
VLP = (VL(I-2,IT) + 3. * VL(I,IT) - 4. * VL(I-1,IT)) /DNM
WLP = (WL(I-2,IT) + 3. * WL(I,IT) - 4. * WL(I-1,IT)) /DNM
PHSLP = (PHSL(I-2,IT) + 3. * PHSL(I,IT) - 4. * PHSL(I-1,IT)) /DNM
PHTLP = (PHTL(I-2,IT) + 3. * PHTL(I,IT) - 4. * PHTL(I-1,IT)) /DNM
C
C
C
      COMPUTATION OF STRAINS ** (STR 139, PG.17) **
260 FSI = DAO * (ULP + WFF * WL(I,IT))
ETH = DAO * (DRHO * VLZ(I,IT) + GAM * UL(I,IT) + WTH * WL(I,IT))
ESTH = DAO/2. * (DRHO * ULZ(I,IT) + VLP - GAM * VL(I,IT))
GSI = PHSL(I,IT) - DAO * (WFF * UL(I,IT) - WLP)
GTH = PHTL(I,IT) - DAO * (WTH * VL(I,IT) - DRHO * WLZ(I,IT))
EKSI = DAO * PHSLP
EKTH = DAO * (DRHO * PHTLZ(I,IT) + GAM * PHSL(I,IT))
EKSTH = DAO/2. * (DRHO * PHSLZ(I,IT) + PHTLP - GAM * PHTL(I,IT) +
1 DAO/2. * (WFF-WTH)*(DRHO*ULZ(I,IT) - VLP-GAM*VL(I,IT)))
IF(PFLAG.EQ.-10.) WRITE(6,261) I., THETA, SI, ETH, ESTH, GSI,
1 GTH, EKSI, EKTH, EKSTH
261 FORMAT(/// 10X, 14HCHECKPRINT OF STRAINS AT STATION ,I4, 5X,
1 7THETA ,1PE12.4// 8F13.4 )
C
C
C
      COMPUTATION OF INTERNAL FORCES ** (STR 139, PG.12) **
ENFE(IT) = B1(L,IT) * ESI + B3(L,IT) * ETH - ENTSI(L,IT)
ENTH(IT) = B3(L,IT) * FSI + B2(L,IT) * ETH - ENTTH(L,IT)
ENFT(IT) = G1(L,IT) * ESTH
QFE(IT) = G2(L,IT) * GSI
EMFE(IT) = D1(L,IT) * EKSI + D3(L,IT) * EKTH - EMFSI(L,IT)
EMTH(IT) = D3(L,IT) * EKSI + D2(L,IT) * EKTH - EMTH(L,IT)
EMFT(IT) = G13(L,IT) * EKSTH
QTH(IT) = G3(L,IT) * GTH
C
C
C
      COMPUTATION OF STRESSES ** (STR 139, PG.11) **
OPE = E11 (PEL,ZTA)
IF (OPE.EQ.0.) GO TO 265
OPD = DN1 (PEL,ZTA)
OPA = ALF1(PEL,ZTA)
OPTT = TMP1(PEL,ZTA)
POI1 = POIS1 (PEL, ZTA)
FTR = OPF / (1.-POI1*POI1)
C
C
C
      INNER SURFACE
00002120
00002130
00002140
00002150
00002160
00002170
00002180
00002190
00002200
00002210
00002220
00002230
00002240
00002250
00002260
00002270
00002271
00002280
00002281
00002285
00002286
00002290
00002300
00002310
00002320
00002350
00002360
00002370
00002380
00002400
00002420
00002430
00002440
00002450
00002460
00002469
00002470
00002471
00002472
0002474
00002476
00002478
00002510

```

```

C      TERM = (OPA + POI1 * OPA) * OPTI
      TER = OPE/(2.*(1.+POI1))
00002520
00002530
00002539
00002540
00002550
00002560
00002570
00002580
      SFLECTED SURFACE
00002589
00002590
00002592
00002594
00002596
00002598
00002630
00002640
00002650
00002659
00002660
00002670
00002680
00002690
00002700
00002710
00002720
00002730
00002740
00002745
00002750
00002760
00002770
00002780
00002790
00002800
00002810
00002820
00002830
00002840
00002849
00002850
00002860
00002870
00002880

```

262 SIGSI1(IIT) = FTR \* (ESI + POI1\*ETH + OPD\*(EKSI+POI1\*EKTH) - TERM) - TERM)  
SIGTH1(IIT) = FTR \* (FTH + POI1\*ESI + OPD\*(EKTH+POI1\*EKSI) - TERM)  
TAUST1(IIT) = TER \* (FSTH + OPD \* FKSTH)  
TAUSG1(IIT) = TER \* GSI  
TAUTG1(IIT) = TER \* GTH

C OPD = DN2 (PEL,ZTA)  
OPE = E12 (PEL,ZTA)  
OPA = ALF2(PEL,ZTA)  
OPTT = TMP2(PEL,ZTA)  
POI2 = POIS2 (PFL, ZTA)  
FTR = OPE/(1.-POI2\*POI2)  
TERM = (OPA + POI2 \* OPA) \* OPTT  
TER = OPE/(2.\*(1.+POI2) )

C 264 SIGSI2(IIT) = FTR \* (ESI + POI2\*ETH + OPD\*(FKSI+POI2\*EKTH) - TERM)  
SIGTH2(IIT) = FTR \* (FTH + POI2\*ESI + OPD\*(EKTH+POI2\*EKSI) - TERM)  
TAUST2(IIT) = TER \* (ESTH + OPD \* FKSTH)  
TAUSG2(IIT) = TER \* GSI  
TAUTG2(IIT) = TER \* GTH

C 265 CONTINUE

C WRITE (6,268) L, (EMFE(J), ENTH(J), ENFT(J), GFE(J), J = 1,IIT)  
WRITE (6,270) (EMFE(J), EMTH(J), EMFT(J), OTH(J), J = 1,IIT)  
IF (OPE .EQ. 0.) GO TO 275  
WRITE (6,272) K1, (SIGSI1(J), SIGTH1(J), TAUST1(J), TAUSG1(J),  
1 TAUTG1(J), J = 1,IIT)  
WRITE (6,272) K2, (SIGSI2(J), SIGTH2(J), TAUST2(J), TAUSG2(J),  
1 TAUTG2(J), J = 1,IIT)

C 268 FORMAT (1H-/11X,9HSTATION ,14// 19X, 5HN(XI),11X, 8HN(THETA), 7X,00002800  
1 11HN(XI,THETA),10X, 5HQ(XI) / (12X, 1P4E17.7) )

C 270 FORMAT (1H-/18X, 5HM(XI),11X, 8HM(THETA), 7X,11HM(XI,THETA), 8X,  
1 8HO(THETA) / (12X, 1P4E17.7) )

C 272 FORMAT (1H-/16X,18HSTRESSES FOR LAYER ,14// 19X, 7HSIG(XI), 8X,  
1 10HSIG(THETA),6X,13HSIG(XI,THETA),5X,11HSIG(XI,ETA),5X,  
2 14HSIG(THETA,ETA) / (12X, 1P5E17.7) )

C

```

C 275 CONTINUE                                00002890
      IF (PFLAG .EQ. -1.E+10) WRITE(6,280)    00002900
      280 FORMAT (1H--, 9HLEFT SUMS )         00002902
      RETURN                                  00002904
C                                             00002910
      290 FORMAT (////10X, 9HSTATION ,I4)    00002919
      300 FORMAT (//// 10X, 9HTHFTA = ,F7.2//11X, 9HENF = ,F5.1//21X, 1HW, 00002930
      1 16X, 1HV, 16X, 1HW, 12X, 7HPH(X1), 9X, 10HPH(TIMETA) / (112X, 1P5E17, 7) 00002940
C                                             00002950
      END                                     00002960

```

### 3.12 PROGRAM LISTINGS FOR DYNAMICS VERSION

#### 3.12a Executive Program

```

SIDFTC EXEC
C APOLLO WATER IMPACT ANALYSIS
C
C REFERENCES ** AIAA JOURNAL, VOL. 1, NO. 8, AUG. 1963, PG.1833FF AND
C VOL. 2, NO. 3, MARCH 1964, PG. 590FF
C ** SID 65-1631 REPORT, APOLLO WATER IMPACT ANALYSIS, NOV.
C 23, 1965, PG. 81FF
C
C NOMENCLATURE
C AO REFERENCE LENGTH (IN)
C HO REFERENCE THICKNESS (IN)
C EO REFERENCE YOUNG MODULUS (PSI)
C SIGO REFERENCE STRESS (PSI)
C POI POISSON RATIO
C ENF NO. OF FOURIER COMPONENTS
C BCIT TOP BOUNDARY CONDITION FLAG
C BCIB BOTTOM BOUNDARY CONDITION FLAG.
C = 1.0 CLOSED APEX
C = 2.0 PINNED
C = 3.0 CLAMPED
C = 4.0 FREE
C = 5.0 ROLLER W
C = 6.0 ROLLER U
C = 10.0 SPECIAL BOUNDARY READ WITH GEOMETRY DATA
C
C DELT TIME INCREMENT
C CEXT NUMBER OF TIME CYCLES
C PFLAG DATA PRINT INDICATOR
C = 0.0 PRINTS GENERAL DATA AND BND. MATRICES
C = 1.0 PRINTS ABOVE INFORMATION AND INPUT DATA
C FOR A PARTICULAR GEOMETRY, AND THE PARA-
C METERS COMPUTED IN GEOM
C = -1.0 PRINTS ALL OF THE ABOVE INFORMATION AND
C STIFFNESS COEFFICIENTS, ELASTIC COEF.,
C THERMAL LOAD AND MOMENT AND PRESSURES
C
C THT CIRCUMFERENTIAL ANGLE THETA (DEGREES) 5 MAX
C FPRNT FOURIER COMPONENT PRINT VALUES. 3 PERMITTED
C
C DIMENSION BCD(36), THT(6), FPRNT(3)
C
C EQUIVALENCE (GDAI 1), AO),
C 1 (GDAI 3), EO),
C 2 (GDAI 5), POI),
C (GDAI 2), HO),
C (GDAI 4), SIGO),
C (GDAI 6), ENF),
C
00000010
00000020
00000030
00000040
00000050
00000060
00000070
00000080
00000090
00000100
00000110
00000120
00000130
00000140
00000150
00000160
00000181
00000182
00000183
00000184
00000185
00000186
00000187
00000195
00000200
00000210
00000220
00000221
00000222
00000223
00000224
00000225
00000226
00000227
00000230
00000231
00000239
00000520
00000525
00000529
00000530
00000531
00000532

```

```

3      (GDA( 7), BCIT),          (GDA( 8), BCIB),          00000533
4      (GDA( 9), PFLAG),        (GDA(10), CEXT),          00000534
5      (GDA(11), DELT),         (GDA(12), THT),          00000535
6      (GDA(13), FPRNT)
C
COMMON GDA(25), DEL, N, NNF, NTH,
1 RMTX(160), TCTR, KZTW, KPTR, KPTW, KPTR
C
5 READ (5,7) BCD
7 FORMAT( 12A6 )
WRITE (6,8) BCD
8 FORMAT(1H1 / (10X, 12A6 //) )
C
DO 10 L = 1,11
GDA(L+11) = -1.E+10
10 GDA(L) = 0.0
KZTR = 8
KZTW = 11
KPTR = 10
KPTW = 12
C
CALL DECRD (GDA)
C
TEXT = CEXT
IF(THT(1) .EQ. -1.E+10) THT(1) = 0.0
IF(FPRNT(1) .EQ. -1.E+10) FPRNT(1) = ENF
C
DO 100 I = 1,TEXT
REWIND 3
REWIND 4
REWIND 8
REWIND 9
REWIND 10
REWIND 11
REWIND 12
REWIND 13
C
TCTR = 1
CALL DATLNK (1)
C
SET TIME COUNTER
DATA LINK
FORM 'P' AND 'X' MATRICES

```

CALL PANDX	00000920
END FILE 3	00000920
REWINO 3	00000940
IF (YCTR .EQ. 2.0) BACKSPACE 10	00000950
	00000960
CALL ZMTRX	00000970
	00000980
CALL SUMS	00000982
	00000989
100 CONTINUE	00000990
	00001000
GO TO 5	00001010
END	00001030

SOLUTIONS

SUMS AND INTERNAL LOADS

3.12b DATLNK Subroutine (DLKDY)

```

$IBFTC DLKDY
C SUB-EXECUTIVE ROUTINE FOR GEOM, DATLYR AND DATLD TO PERMIT ONE
C COPY OF CODIMA, ENTERP AND DINTRP IN THE DECK SET-UP
C
C SUBROUTINE DATLNK (1)
C
C COMMON GDA(25), DEL, N, NNF, NIH,
C 1 BMTX(160), TCTR, KZTW, KZTR, KPTW, KPTR
C
C IF (1 .NE. 1) GO TO 50
C CALL GFOM
C
C SET UP MATERIAL PROPERTIES
C
C CALL DATLYR
C REWIND 9
C
C SET UP FOURIER LOAD COEFF.
C
C 50 CALL DATLD
C
C RETURN
C
C END
    
```

3. 12c GEOM Subroutine (GMYD)

```

$IRFTC GMYD
C ** POLLO WATER IMPACT STUDY ** * GEOMETRY COMPUTATION **
C
C SUBROUTINE GEOM
C
C GMI = GEOMETRY INDICATOR
C = 1.0 - CONE - CYLINDER
C = 2.0 - SPHERE - TOROID
C = 3.0 - ARBITRARY FUNCTIONS
C = 4.0 - GENERAL DISCRETE POINTS
C **
C INPUTS - GMI = 1.0
C RAI = RADIUS AT STATION 1
C AXL = AXIAL SURFACE LENGTH
C ANX = ANGLE - GENERATOR AND AXIS OF REVOLUTION
C **
C RC = RADIUS OF CURVATURE
C ROFF = OFFSET DISTANCE TO CENTER OF CURVATURE
C PHIO = INITIAL OPENING ANGLE FROM VERTICAL AXIS
C PHIN = FINAL ANGLE
C **
C GMI = 4.0 (- 4.0 DISCRETE ARCLENGTHS )
C EM = NUMBER OF RIPTS GIVEN
C RIPT = DISCRETE RADII
C XIPT = DISCRETE XI'S (OR ARCLENGTHS)
C RCURV = MERIDIONAL RADII OF CURVATURE
C RCURZ = CIRCUMFERENTIAL RADII OF CURVATURE
C **
C
C DIMENSION WFW(16), WFP(4), STAP(4), SJAW(16), RRJ(12), RCRV(100),
1RCURZ(100), RCURV(100), RR(100), RIPT(100), XIPT(100), SARR(100),
2SURF(100), XJ(11), RJ(11), DLR(10), R(100), XSI(100), WTHX(100),
3WFPX(100), RHOX(100), GAMA(100), WFFPX(100), RCRZ(100), GMDA(442)
C
C DIMENSION BNDTX(17), RNDTB(17), THT(6), FPRNT(4)
C DIMENSION OMG0(5,5), OMGN(5,5), ALM0(5,5), ALMN(5,5)
C DIMENSION ALM1(5,5), OMG1(5,5)
C REAL LLO(5), LLLN(5)
C
C COMMON GDA(25), DEL, N, NNF, NTH,
1 AMTX(160), TCTR, KZTW, KZTR, KPTW, KPTR
C
C

```



1	EQUIVALENCE	(RMTX( 1), OMGO),	(RMTX( 26), OMGN),	00000440
2		(RMTX( 5), ALMO),	(RMTX( 76), ALMN),	00000450
3		(RMTX(10), OMG1),	(RMTX(126), ALM1),	00000460
		(RMTX(15), LLL),	(RMTX(156), LLLN),	00000470
C				00000479
1	EQUIVALENCE	(GDA( 1), AO),	(GDA( 2), HO),	00000480
2		(GDA( 3), FO),	(GDA( 4), SIGO),	00000490
3		(GDA( 5), PO),	(GDA( 6), FNF),	00000500
4		(GDA( 7), RCIT),	(GDA( 8), BCIB),	00000510
5		(GDA( 9), PFLAG),	(GDA(10), CEXT),	00000511
6		(GDA(11), DFLT),	(GDA(12), THT),	00000512
		(GDA(18), FPRNT),		00000513
C				00000520
1	EQUIVALENCE	(GMDA( 1),	(GMDA( 2),	00000530
2		(GMDA( 3),	(GMDA( 4),	00000540
3		(GMDA( 5),	(GMDA( 6),	00000550
4		(GMDA( 7),	(GMDA( 8),	00000560
5		(GMDA( 9),	(GMDA(10),	00000570
6		(GMDA(20),	(GMDA(30),	00000580
		(GMDA(40),	(GMDA(42),	00000590
C				00000600
DO 2	I = 1,442			00000610
2	GMDA(1) = 0,0			00000620
C				00000630
	CALL DECRD (GMDA)			00000640
C				00000650
DO 3	I = 1,160			00000660
3	BMTX(1) = 0,0			00000670
C				00000680
	IF (RCIT *NF, 1,0) GO TO 5			00000690
C				00000700
	OMGO(3,3) = 1,0			00000710
	OMG1(1,1) = 1,0			00000720
	OMG1(1,2) = -1,0			00000730
	OMG1(5,4) = -1,0			00000740
	OMG1(5,5) = 1,0			00000750
	ALMO(1,1) = 1,0			00000760
	ALMO(2,2) = 1,0			00000770
	ALMO(4,4) = 1,0			00000780
	ALMO(5,5) = 1,0			00000790
	ALM1(2,1) = 1,0			00000800
	ALM1(2,2) = 1,0			00000810
	ALM1(3,3) = 1,0			00000820

	ALM1(4,4) = 1.0	00000830
	ALM1(4,5) = 1.0	00000840
	GO TO 21	00000850
C		00000860
		00000870
		00000880
C	5 IF (RCIT .NF. 10.) GO TO 10	00000890
		00000900
	OMGO(1,1) = RNDTX( 1)	00000910
	OMGO(1,2) = BNDTX( 2)	00000920
	OMGO(3,3) = RNDTX( 4)	00000930
	OMGO(4,4) = RNDTX( 5)	00000940
	OMGO(5,4) = RNDTX( 6)	00000950
	OMGO(5,5) = RNDTX( 7)	00000960
	ALMO(1,1) = BNDTX( 8)	00000970
	ALMO(2,2) = BNDTX( 9)	00000980
	ALMO(3,3) = BNDTX(10)	00000990
	ALMO(4,4) = BNDTX(11)	00001000
	ALMO(5,5) = BNDTX(12)	00001010
	DO 8 IJ = 1,5	00001020
	A LL(IJ) = RNDTX(IJ+12)	00001030
	GO TO 21	00001040
C	10 IBMX = BCIT	00001050
	IO = 1	00001060
	IL = 51	00001070
C		00001080
	11 GO TO (21,12,13,14,15,16), IRMX	00001090
		00001100
C		00001110
	12 BMTX(IO + 18) = 1.	00001120
	BMTX(IO + 24) = 1.	00001130
	BMTX(IL) = 1.	00001140
	BMTX(IL + 6) = 1.	00001150
	BMTX(IL + 12) = 1.	00001160
	GO TO 20	00001170
C		00001180
	13 BMTX(IL) = 1.	00001190
	BMTX(IL + 6) = 1.	00001200
	BMTX(IL + 12) = 1.	00001210
	BMTX(IL + 18) = 1.	00001220
	BMTX(IL + 24) = 1.	00001230
	GO TO 20	00001240
C		00001250
	14 BMTX(IO) = 1.	00001260

	BMTX(10 + 6) = 1.	00001270
	BMTX(10 + 12) = 1.	00001280
	BMTX(10 + 18) = 1.	00001290
	BMTX(10 + 24) = 1.	00001300
	GO TO 20	00001310
C		00001320
	15 ROLLER W	00001330
	BMTX(10 + 12) = 1.	00001340
	BMTX(10 + 18) = 1.	00001350
	BMTX(10 + 24) = 1.	00001360
	BMTX(1L) = 1.	00001370
	BMTX(1L + 6) = 1.	00001380
	GO TO 20	00001390
C		00001400
	16 ROLLER U	00001410
	BMTX(10 + 18) = 1.	00001420
	BMTX(10 + 24) = 1.	00001430
	BMTX(1L + 6) = 1.	00001440
	BMTX(1L + 12) = 1.	00001450
C		00001460
	20 IF(10 .NE. 1) GO TO 28	00001470
C		00001480
	21 IF (RCIR .NF. 1.0) GO TO 23	00001490
C		00001500
	CLOSED APEX	00001510
	OMGN(1,2) = 1.0	00001520
	OMG1 (1,1) = 1.0	00001530
	OMG1 (1,2) = -1.0	00001540
	OMG1 (5,4) = -1.0	00001550
	OMG1 (5,5) = 1.0	00001560
	ALMN(1,1) = 1.0	00001570
	ALMN(2,2) = 1.0	00001580
	ALMN(4,4) = 1.0	00001590
	ALMN(5,5) = 1.0	00001600
	ALM1 (2,1) = 1.0	00001610
	ALM1 (2,2) = 1.0	00001620
	ALM1 (3,3) = 1.0	00001630
	ALM1(4,4) = 1.0	00001640
	ALM1 (4,5) = 1.0	00001650
C		00001660
	GO TO 28	00001670
	23 IF (RCIR .NF. 10.) GO TO 25	00001680
C		00001690
	SPECIAL BOUNDARY	00001700
	OMGN(1,1) = BNDT5( 1)	00001710
	OMGN(1,2) = BNDTR( 2)	00001720

```

OMGN(2,2) = BNDTR( 3) 00001700
OMGN(3,3) = BNDTR( 4) 00001710
OMGN(4,4) = BNDTR( 5) 00001720
OMGN(5,4) = BNDTR( 6) 00001730
OMGN(5,5) = BNDTR(7) 00001740
ALMN(1,1) = BNDTR(8) 00001750
ALMN(2,2) = BNDTR( 9) 00001760
ALMN(3,3) = BNDTR(10) 00001770
ALMN(4,4) = BNDTR(11) 00001780
ALMN(5,5) = BNDTR(12) 00001790
DO 24 IJ = 1,5 00001800
24 LLLN(IJ) = BNDTR(IJ+12) 00001810
GO TO 28 00001820
C 00001830
25 IRMX = RCIR 00001840
IO = 26 00001850
IL = 76 00001860
GO TO 11 00001870
C 00001880
28 WRITE (6,1000) AO, HO, FO, SIGO, POI, FNF, RCIT, RCIR, PFLAG, 00001890
1 CEXT, DELT, THT, FPRNT, 00001891
2 OMGO, ALMG, LLO, OMGN, ALMN, LLLN 00001902
C 00001910
N = EN 00001920
GMI = ABS(GIN) 00001930
NN = N - 1 00001940
IF (GMI - 2.0) 30, 35, 50 00001950
C 00001960
C CONE - CYLINDER 00001971
C ** 00001980
30 IF (PFLAG.NE.0.0) WRITE(6,31) N, RAI, AXL, ANX 00001990
C 00002000
31 FORMAT (1H1,19X,34HGEOMETRY DATA FOR CONE - CYLINDER /,15X,22HNUMB0002010 00002010
1ER OF STATIONS - ,16//5X,7HRA1 =,1PE13.4,7X,7HAXL =,E13.4,7X,00002020
2 7HANX =,E13.4) 00002030
C 00002040
DEL = AXL/EN - 1.0) 00002050
SINFI = 5INDTANX) 00002060
COSFI = COSDIANX) 00002070
KSI(1) = 0.0 00002080
WTHX(1) = AO * COSFI/RAI 00002090
WFEX(1) = 0.0 00002100
RHOX(1) = RAI/AO 00002110

```

```

R(I) = RA1
DO 37 I = 2,N
  R(I) = R(I-1) + DEL * SINFI
  XSI(I) = XSI(I-1) + DEL * COSFI
  WTHX(I) = AD * COSFI/R(I)
  WFFX(I) = 0.0
37 RHOX(I) = R(I)/AD
GO TO 95

C
C      SPHERE - TOROID      **
C
35 IF (PFLAG .NE. 0.0) WRITE (6,37) N, RC, ROFF, PHI0, PHIN
C
37 FORMAT (I11,3X,31HGEOMETRY DATA FOR SPHERE - TOROID //35X,22HNUMBER00002250
1FR OF STATIONS - ,14//6X,7HRC =,1PF13.4,7X,7HROFF =,F13.4,7X,00002260
2 7HPHI0 =,F13.4,7X,7HPHIN =,F13.4 )
C
ANGSP = PHIN - PHI0
DEL = ANGSP/(FN - 1.0)
AM = 1.0
AMU = SIGN(AM,DEL)
XSI(1) = 0.0
RPHI = PHIN
BSINP = SIN(PHI0)
RCOSP = COSD(PHI0)
R(1) = RC * BSINP + ROFF
DO 40 I = 1,NN
  APhi = RPHI + DEL
  ASINP = SIND(APhi)
  ACOSP = COSD(APhi)
  R(I+1) = R(I) + RC * (ASINP - BSINP)
  XSI(I+1) = XSI(I) + RC * (RCOSP - ACOSP)
  WFFX(I) = AD/RC * AMU
  IF (ROFF .EQ. 0.0) GO TO 38
  WTHX(I) = AD * BSINP/R(I)
  GO TO 39
38 WTHX(I) = WFFX(I)
39 RHOX(I) = R(I)/AD
  RPHI = APhi
  ASINP = ASINP
  RCOSP = ACOSP
40 CONTINUE
C

```

```

DFL = ABS(DFL)
WFFX(N) = A07R7*AMJ
IF (ROFF.EQ.0.0) GO TO 45
WTHX(N) = A0 * RSINP /R(N)
GO TO 46
45 WTHX(N) = WFEX(N)
IF (RCIR.EQ.1.0) GO TO 47
46 RHOX(N) = R(N)/A0
GO TO 48
47 RHOX(N) = 0.0
48 DFL = DFL * RC * 0.01745329
GO TO 45
C
49 IF (GMT.GT.3.0) GO TO 60
C
WRITE (6,55)
55 FORMAT (1H),43ARBITRARY FUNCTIONS CANNOT BE HANDLED. YFT. )
C
GO TO 140
C
GENERAL DISCRETE POINTS
**
C
60 M = EM
MM = M - 1
MH2 = M - 2
C
IF (PFLAG.NE.0.0) WRITE(6,62) N, (XIPT(I), XIPT(I), I = 1,M)0002810
C
62 FORMAT (1H),39X,11HGOMETRY DATA - DISCRETE POINTS //15X,22HNUMBER0002810
1 OF STATIONS - ,14//16X,1HR,16X,2HXI//13X,1P2E20.7) 1
C
SARB(I) = 0.0
IF (GIN.LT.0.) GO TO 77
DO 75 IL = 1,MM
SURB = 0.0
DLT = XIPT(IL+1) - XIPT(IL)
K = 10
AK = K
DDL = DLT/AK
KPI = K + 1
DO 65 JI = 1,KPI
AJI = JI - 1
XJ(JI) = XIPT(IL) + AJI * DDL

```

```

00002550
00002560
00002570
00002580
00002590
00002600
00002610
00002620
00002630
00002640
00002650
00002660
00002670
00002680
00002690
00002700
00002710
00002720
00002730
00002740
00002750
00002760
00002770
00002780
00002790
00002800
00002810
00002820
00002830
00002840
00002850
00002860
00002870
00002880
00002890
00002900
00002910
00002920
00002930
00002940
00002950
00002960
00002970

```

```

65 CONTINUE
C
CALL CODIMA (KP1,XJ, RRJ, XIPT, RIPT, M, 1.0)
DO 69 I = 2,K
00002980
00002990
00003000
00003010
00003020
00003030
00003040
00003050
RJJ(I) = (RRJ(I-1) + RRJ(I) + RRJ(I+1)) / 3.0
RJ(KP1) = RRJ(KP1)
C
DO 70 JR = 1,K
00003060
00003070
DLR(JR) = RJ(JR+1) - RJ(JR)
DLS = SORT(DLR(JR)**2 + DDL**2)
00003080
00003090
70 SURB = SURB + DLS
SARB(IL+1) = SARB(IL) + SURB
00003100
00003110
75 CONTINUE
GO TO 80
00003120
00003130
77 DO 78 I = 1,M
00003140
78 SARB(I) = XIPT(I)
00003150
80 DEL = SARB(M) / (FN - 1.0)
00003160
00003170
C
SURF(1) = 0.0
00003180
DO 82 I = 1,NN
00003190
82 SURF(I+1) = SURF(I) + DEL
00003200
00003210
CALL CODIMA(N, SURF, RCRV, SARB, RCURV, M, 1.0)
CALL (ONTMAIN,SURF, RCRZ, SARB, RCURZ, M, 1.0)
00003220
00003230
C
CALL CODIMA (N,SURF, R, SARB, RIPT, M, 1.0)
00003240
00003250
C
CALL CODIMA (N, SURF, XSI, SARB, XIPT, M, -1.0)
00003260
00003270
MLN = N - 2
00003280
NSM = 1
00003290
84 DO 85 I = 3,MLN
00003300
RR(I) = (-3.*R(I-2) + 12.*R(I-1) + 17.*R(I) + 12.*R(I+1) - 3. *
00003310
1 R(I+2)) / 35.0
00003320
85 CONTINUE
00003330
RR(NN) = R(NN)
00003340
RR(2) = R(2)
00003350
RR(N) = R(N)
00003360
RR(1) = R(1)
00003370
IF (NSM .EQ. 25) GO TO 88
00003380
NSM = NSM + 1
00003390
DO 87 I = 1,N
00003400
87 R(I) = RR(I)
00003410
GO TO 84

```

```

88 RHOX(I) = RR(I)/A0
DELSQ = DEL * DEL
DO 89 I = 1,N
89 RHOX(I+1) = RR(I+1) /A0
GO TO 110
C
C
C      **
C      COMPUTE GAMA
95 DFL = DEL / A0
DELSQ = DEL * DEL
DO 105 I = 1,N
DENM = 12. * RHOX(I) * DEL
DENM = 2. * RHOX(I) * DEL
IF(RHOX(I) .EQ. 0.) GO TO 97
IF (I .NE. 1) GO TO 98
IF (RC(I) .EQ. 1.0) GO TO 103
GAMA(I) = (3.*(RHOX(I+1) - RHOX(I)) + RHOX(I+1) - RHOX(I+2))/DENM
GO TO 105
97 GAMA(I) = 0.0
GO TO 105
98 IF (I .EQ. N) GO TO 100
IF (I .EQ. 2) GO TO 99
IF (I .EQ. N-1) GO TO 99
GAMA(I) = (RHOX(I-2) - 8. * (RHOX(I-1) -
1) /DENM
GO TO 105
99 GAMA(I) = (RHOX(I+1) - RHOX(I-1)) /DFNMP
GO TO 105
100 IF (RC(I) .EQ. 1.0) GO TO 103
GAMA(I) = (3.*(RHOX(I)-RHOX(I-1)) + RHOX(I-2) - RHOX(I-1)) /DENM
GO TO 105
103 GAMA(I) = 0.
105 CONTINUE
GO TO 123
C
110 DO 115 I = 1,N
WFEX(I) = A0/RCRV(I)
WTHX(I) = A0/RCRZ(I)
IF (RHOX(I) .EQ. 0.0) GO TO 113
PRO = (RHOX(I) * WTHX(I))**2
IF (PRO .GT. 1.0) GO TO 114
GAMA(I) = SORT(1.-PRO)/RHOX(I)
GO TO 115

```

```

00003420
00003430
00003440
00003450
00003460
00003470
00003480
00003490
00003500
00003510
00003520
00003530
00003540
00003550
00003560
00003570
00003580
00003590
00003600
00003610
00003620
00003630
00003640
00003650
00003660
00003670
00003680
00003690
00003700
00003710
00003720
00003730
00003740
00003750
00003760
00003770
00003780
00003790
00003800
00003810
00003820
00003830
00003840

```



```

113 GAMA(I) = 0.0
GO TO 115
114 GAMA(I) = 0.0
115 CONTINUE
C
123 DO 127 I = 1,N
WFDNM = 2. * DFL
IF (I.NE. 1) GO TO 124
WFEX(I) = (4. * WFEX(I+1) - 3. * WFEX(I) - WFEX(I+2)) /WFDNM
GO TO 127
124 IF (I.EQ. N) GO TO 126
WFEX(I) = (WFEX(I+1) - WFEX(I-1)) /WFDNM
GO TO 127
126 WFEX(I) = (WFEX(I-2) + 3. * WFEX(I) - 4. * WFEX(I-1)) /WFDNM
127 CONTINUE
C
WRITE (3) WTHX, WFEX, GAMA, RHOX, WFEX
C
C
129 IF (PFLAG.EQ. 0.0) GO TO 140
WRITE (6,130) DEL, (I, R(I), XSI(I), WTHX(I), WFEX(I), RHOX(I),
1 GAMA(I), I = 1,N)
C
130 FORMAT (1H-, 5X, 7HDFL =,1PE13.4 //
3X,1HI,9X,4HR(I),12X,5HXI(I),10X,8HW(THETA),11X,
2 5HW(XI),11X,7HRHOX(I),10X,7HGAMA(I) //(I4, 1P6E17.7) )
C
140 RETURN
C
1000 FORMAT(1H1,47X,12HGENERAL DATA:// 3X,7HA0 =,1PE13.4, 8X,7HH0
1 =,E13.4, 8X,7HFO =,E13.4, 8X,7HSIG0 =,E13.4// 3X,7HPOI =,
2 F13.4, 8X,7HFN0 =,F13.4, 8X,7HRCIT =,F13.4, 8X,7HRCIR =,
3 E13.4//3X,7HPFLAG =,F13.4, 8X,7HCEXT =,F13.4, 8X,7HDFLT =,
4 E13.4//6X,20HPRINT ANGLES (THI) - // 24X,6E13.4 //6X,33HFOURIER H00004124
5 HARMONIC PRINTS (FPRNT) - // 24X, 4E13.4
6 //1H-,45X,17HBOUNDAR00004126
7Y MATRICES /6X,15HTOP BOUNDARY **// 6X,5HOMEGA /5(5E17.7)// 6X, 00004127
8 6HLAMBDA /5(5E17.7)// 6X,3HL -/ 5E17.7///6X,18HBOTTOM BOUNDARY 00004128
9** // 6X,5HOMEGA /5(5E17.7)// 6X,6HLAMUDA /5(5E17.7)// 6X,3HL -/00004129
X 5E17.7 )
END
00009999

```

3. 12d DATLYR Subroutine (STFDY)

```

00000010
00000020
00000030
00000040
00000050
00000060
00000061
00000120
00000130
00000150
00000160
00000170
00000180
00000190
00000199
00000200
00000210
00000220
00000230
00000240
00000250
00000260
00000270
00000280
00000281
00000282
00000309
00000310
00000320
00000330
00000340
00000350
00000360
00000370
00000380
00000390
00000400
00000420
00000430
00000431
00000432
00000433
00000434
00000435

SUBROUTINE DATLYR
*** STIFFNESS COEFF. ARE STORED IN SECTIONS OF ALL FOURIER
COMPONENTS /MERIDIONAL STATION, UP TO BLOCKS OF 100
DIMENSION COEFFC(2200)
DIMENSION SCB1(100), SCR2(100), SCR3(100), SCG1(100), SCG2(100),
1 SCG3(100), SCD1(100), SCD2(100), SCD3(100), SCG13(100),
2 SCNTS1(100), SCNTH1(100), SCMTS1(100), SCMTH(100), DCM1(100),
3 DCM4(100), DCC1(100), DCC2(100), DCC3(100), DCK1(100), DCK2(100),
4 DCK3(100)
COMMON GDA(25), DEL, N, NNF, NTH,
1 RMTX(160), TCTR, KZTW, KZTR, KPIW, KPTR
EQUIVALENCE (GDA( 1), A0), (GDA( 2), H0),
1 (GDA( 3), E0), (GDA( 4), SIG0),
2 (GDA( 5), P0I), (GDA( 6), ENF),
3 (GDA( 7), BC1I), (GDA( 8), BC1R),
4 (GDA( 9), PFLAG), (GDA(10), CE1T),
5 (GDA(11), DELT), (GDA(12), TH1),
6 (GDA(18), FPRNT)
EQUIVALENCE (COEFC( 1), SCB1), (COEFC(101), SCR2), (COEFC(101), SCNTH), (COEFC(101), SCNTS1),
1 (COEFC( 2), SCB1), (COEFC( 3), SCG1), (COEFC( 3), SCD1), (COEFC( 3), DCM1), (COEFC( 3), DCC1), (COEFC( 3), DCK1),
2 (COEFC( 4), SCG2), (COEFC( 5), SCG3), (COEFC( 5), SCD2), (COEFC( 5), DCM2), (COEFC( 5), DCC2), (COEFC( 5), DCK2),
3 (COEFC( 6), SCD1), (COEFC( 8), SCD3), (COEFC( 8), SCNTS1), (COEFC( 8), SCNTH), (COEFC( 8), DCM1), (COEFC( 8), DCC1), (COEFC( 8), DCK1),
4 (COEFC( 9), SCD1), (COEFC(13), SCNTS1), (COEFC(13), SCNTH), (COEFC(13), DCM1), (COEFC(13), DCC1), (COEFC(13), DCK1),
5 (COEFC(12), SCNTS1), (COEFC(12), SCNTH), (COEFC(12), DCM1), (COEFC(12), DCC1), (COEFC(12), DCK1), (COEFC(12), DCC2), (COEFC(12), DCC3),
6 (COEFC(15), DCM4), (COEFC(16), DCC1), (COEFC(17), DCC2), (COEFC(18), DCC3), (COEFC(18), DCK1), (COEFC(18), DCC2), (COEFC(18), DCC3),
7 (COEFC(18), DCC3), (COEFC(19), DCK1), (COEFC(19), DCC1), (COEFC(19), DCC2), (COEFC(19), DCK2), (COEFC(19), DCC3),
8 (COEFC(21), DCC3)
IF (PFLAG .LT. 0.) WRITE(6,10)
10 FORMAT(1H1/6X, 96MCHECKPRINT OF COEFC BLOCKS STORED IN GROUPS OF 100,00432
12*ENF) PER MERIDIONAL STATION. THE COEFFICIENTS /103H PRINTED ARE 00000434
2 SCB1, SCD1, SCNTS1, SCNTH, DCM1, DCM4, DCC1, DCC2, DCC3, DCK1, DCC2, DCC3, DCK1, DCC2, DCC3, DCK1, DCC2, DCC3, DCK1

```

3CK2, DCK3 (IN THAT ORDER) / 62H AND ARE SEPARATED FROM EACH OTHER 000007435  
 4BY THE THREE ..... FIELDS. /// 00000436  
 ENTH = 90. 00000440  
 HD2 = HO \* HO 00000450  
 SS3 = 2.73.1415927 00000460  
 NTH = ENTH 00000470  
 ENNF2 = ENF + ENF 00000480  
 NNF = FRF 00000490  
 NNF2 = 2 \* NNF 00000500  
 TN = I 00000510  
 \*\*  
 DETERMINE SIZE OF BLOCK 00000518  
 00000519  
 MNF = N \* NNF2 00000520  
 00000530  
 40 IF (MNF .GT. 100) GO TO 50 00000539  
 LESS THAN ONE BLOCK MORE  
 LN = N 00000540  
 GO TO 60 00000550  
 50 IF (MNF .LT. 200) GO TO 55 00000560  
 AT LEAST 2 FULL BLOCKS MORE  
 LN = 100/NNF2 00000569  
 GO TO 58 00000570  
 00000580  
 00000584  
 00000585  
 00000586  
 00000587  
 00000590  
 55 LN = 50/NNF2 00000600  
 58 LN = LN + LN - 1 00000620  
 00000630  
 00000640  
 60 DFLTH = 3.1415927/ ENTH 00000649  
 ZERO COEFFICIENT AREA  
 63 DO 65 I = 1,200 00000650  
 65 COFFC(I) = 0.0 00000660  
 00000670  
 00000680  
 70 DO 100 J = 1N, LN 00000689  
 ESTABLISH MERIDIONAL DISTANCE  
 EI = I - 1 00000690  
 PEL = EI \* DEL 00000700  
 K1 = NNF2 \* (I - IN) 00000710  
 00000719  
 DO 100 NN = 1,NNF2 00000720  
 K2 = K1 + NN 00000730  
 EMN = NN - 1 00000740  
 00000740

C	75	DO	95	J = 1,NTH	00000770
				EJ = J - 1	00000780
				ZTA = EJ * DELTH + DELTH * 0.5	00000790
				IF (NN * EQ. 1) GO TO 90	00000800
C					00000810
C					00000820
				OTHER FOURIER COMPONENTS	00000830
	80	SCB1(K2) = SCB1(K2) +	BBB1(PEL,ZTA)	* COS(FNN * ZTA)	00000840
		SCD1(K2) = SCD1(K2) +	DDD1(ZTA)	* COS(ENN * ZTA)	00000845
		SCNTS1(K2) = SCNTS1(K2) +	EMT1(PEL,ZTA)	* COS(ENN * ZTA)	00000850
		SCMIS1(K2) = SCMIS1(K2) +	FMT1(PFL,ZTA)	* COS(ENN * ZTA)	00000855
		DCM1(K2) = DCM1(K2) +	DMM1(PFL,ZTA)	* COS(FNN * ZTA)	00000860
		DCM4(K2) = DCM4(K2) +	DMM4(PEL,ZTA)	* COS(FNN * ZTA)	00000870
		DCK1(K2) = DCK1(K2) +	DKK1(PEL,ZTA)	* COS(ENN * ZTA)	00000880
		DCC1(K2) = DCC1(K2) +	DMP1(PFL,ZTA)	* COS(ENN * ZTA)	00000885
		DCC2(K2) = DCC2(K2) +	DKK2(PEL,ZTA)	* COS(ENN * ZTA)	00000890
		DCC3(K2) = DCC3(K2) +	DMP2(PEL,ZTA)	* COS(FNN * ZTA)	00000895
		DCK3(K2) = DCK3(K2) +	DKK3(PEL,ZTA)	* COS(ENN * ZTA)	00000900
		DCC3(K2) = DCC3(K2) +	DMP3(PEL,ZTA)	* COS(ENN * ZTA)	00000905
		GO TO 95			00000910
C				FIRST FOURIER COMPONENT	00000919
	90	SCB1(K2) = SCB1(K2) +	HRR1(PEL,ZTA)	/ 2.0	00000920
		SCD1(K2) = SCD1(K2) +	DDD1(ZTA)	/ 2.0	00000925
		SCNTS1(K2) = SCNTS1(K2) +	EMT1(PEL,ZTA)	/ 2.0	00000930
		SCMIS1(K2) = SCMIS1(K2) +	FMT1(PEL,ZTA)	/ 2.0	00000935
		DCM1(K2) = DCM1(K2) +	DMM1(PEL,ZTA)	/ 2.0	00000940
		DCM4(K2) = DCM4(K2) +	DMM4(PEL,ZTA)	/ 2.0	00000950
		DCK1(K2) = DCK1(K2) +	DKK1(PEL,ZTA)	/ 2.0	00000960
		DCC1(K2) = DCC1(K2) +	DMP1(PEL,ZTA)	/ 2.0	00000965
		DCK2(K2) = DCK2(K2) +	DKK2(PEL,ZTA)	/ 2.0	00000970
		DCC2(K2) = DCC2(K2) +	DMP2(PEL,ZTA)	/ 2.0	00000975
		DCK3(K2) = DCK3(K2) +	DKK3(PEL,ZTA)	/ 2.0	00000980
		DCC3(K2) = DCC3(K2) +	DMP3(PEL,ZTA)	/ 2.0	00000985
		95 CONTINUE			00000990
C				NORMALIZE	00001000
C					00001009
		S3 = SS3/1E0 * H0			00001010
		SCB1(K2) = S3 * DELTH * SCB1(K2)			00001020
		S4 = S3 * A0 * A0			00001030
		DCM1(K2) = S4 * DELTH * DCM1(K2)			00001040
		DCM4(K2) = S3 * DELTH * DCM4(K2)			00001050
		DCK1(K2) = S4 * DELTH * DCK1(K2)			00001060
		DCC1(K2) = S4 * DELTH * DCC1(K2)			00001065

```

DCK2(K2) = S4 * DELTH * DCK2(K2)      00001070
DCC2(K2) = S4 * DELTH * DCC2(K2)      00001075
DCK3(K2) = S4 * DELTH * DCK3(K2)      00001080
DCC3(K2) = S4 * DELTH * DCC3(K2)      00001083
S3 = S53 / (SIGO * H0)                 00001085
SCNTS1(K2) = S3 * DELTH * SCNTS1(K2)   00001090
S3 = S53 * A0 / (SIGO * H02 * H0)      00001093
SCMYS1(K2) = S3 * DELTH * SCMYS1(K2)   00001096
S3 = S53 / (EO * H02 * H0)             00001100
SCD1(K2) = S3 * DELTH * SCD1(K2)       00001110
C                                         00001120
98 S52 = (1. - P01) / 2.                00001130
SCG13(K2) = S52 * SCB1(K2)             00001140
SCG1(K2) = S52 * SCB1(K2)             07001150
SCB2(K2) = SCB1(K2)                    00001160
SCB3(K2) = P01 * SCB1(K2)              00001170
SCG2(K2) = S52 * SCB1(K2)              00001180
SCG3(K2) = SCG1(K2)                    00001190
SCD2(K2) = SCD1(K2)                    00001200
SCD3(K2) = P01 * SCD1(K2)              00001210
100 CONTINUE                             00001280
C                                         00001290
WRITE ( 9) LN, IN, COEFC                00001300
NX = (LN - IN + 1) * NMF2              00001305
XX = GDA(25)                             00001306
IF (PFLAG .LT. 0.)                      00001309
XWRITE (6,105) IN, LN, (SCB1(I), I=1,NX), XX, XX, XX, (SCD1(I), 00001310
1 I=1,NX), XX, XX, XX, (SCMYS1(I), I=1,NX), XX, XX, XX, (SCMYS1(I),00001311
2 I=1,NX), XX, XX, XX, (DCM1(I), I=1,NX), XX, XX, XX, (DCM4(I), I 00001312
3 = 1,NX), XX, XX, XX, (DCC1(I), I=1,NX), XX, XX, XX, (DCC2(I), I 00001313
4 = 1,NX), XX, XX, XX, (DCC3(I), I=1,NX), XX, XX, XX, (DCK1(I), I 00001314
5 = 1,NX), XX, XX, XX, (DCK2(I), I=1,NX), XX, XX, XX, (DCK3(I), I 00001315
6 = 1,NX)                                00001316
105 FORMAT(10X,11HFOR STATION, 13,16H THROUGH STATION, 14/// 00001320
1 ( 1P6F17.7) )                          00001321
C                                         00001330
IF (LN .EQ. N) GO TO 110                 00001340
IN = LN + 1                              00001350
NCN = N - LN                             00001360
NMF = NCN * NMF2                          00001370
GO TO 40                                  00001380
110 RETURN                                00001390
C                                         00001400
END                                         00001410

```

3.12e DATLD Subroutine (DLDY)

```

STARTC DLDY      00000010
C                FOURTER LOAD COEFFICIENTS GENERATOR BY FUNCTIONS ONLY 00000020
C                00000030
C                00000040
C                00000050
C                00000060
C                00000340
C                00000440
C                00000450
C                00000460
C                00000470
C                00000480
C                00000481
C                00000482
C                00000490
C                00000500
C                00000510
C                00000520
C                00000525
C                00000530
C                00000550
C                00000560
C                00000570
C                00000580
C                00000590
C                00000600
C                00000610
C                00000620
C                00000630
C                00000650
C                00000670
C                00000690
C                00000720
C                00000730
C                00000740
C                00000741
C                00000742
C                00000743
C                00000770
C                00000790
C                00000795
C                00000800
C                00000810

SUBROUTINE DATLD
DIMENSION PFE(10,50), PTH(10,50), PN(10,50)
FOURTER LOAD COEFFICIENTS GENERATOR BY FUNCTIONS ONLY
1  (GDA( 1), AO), (GDA( 2), HO),
2  (GDA( 3), EO), (GDA( 4), SIGO),
3  (GDA( 5), PO), (GDA( 6), ENF),
4  (GDA( 7), BCIT), (GDA( 8), BCIT),
5  (GDA( 9), PFLAG), (GDA(10), CEXT),
6  (GDA(11), DELT), (GDA(12), THT),
   (GDA(18), FPRN)

COMMON GDA(25), DEL, N, NNF, NTH,
1 RMTX(160), TCTR, KZTW, KZTR, KP1W, KP1R

C                INITIALIZE * * * * *
NAB = 0
SS3 = 2. / 3. * 1415927
S3 = SS3 * AU / (SIGO * HO)
NUN = 2
IF (N .GT. 50) NUN = 3
IF (TCTR .GT. 1.0) AF = FILE (9,NUN)

DO 20 I = 1,50
DO 20 K = 1,10
PFE(K,I) = 0.0
PTH(K,I) = 0.0
PN(K,I) = 0.0
20 CONTINUE

IF (PFLAG .LT. 0.) WRITE(6,30)
30 FORMAT(1H1/6X, 9#CHECKPRINT OF LOAD COEF. STORED IN GROUPS OF ALL 00000740
1 ENF PER MERIDIONAL STATION. THE COEFFICIENTS ARE / 81# PFE, PTH 00000741
2) PN (IN THAT ORDER) AND ARE SEPARATED FROM EACH OTHER BY 00000742
3 FIELDS. / 777)
NI = N

C                SPECIAL FUNCTIONS
C                00000770
C                00000790
C                00000795
C                00000800
C                00000810
    
```

```

N11 = 1
N12 = N
FNTH = NTH
DELTH = 3.1415927 / ENTH
C
C      EACH BLOCK OF LOADS CANNOT CONTAIN MORE THAN 50 STAS.
C
IF (N1 .GT. 50) N1 = 50
70 DO 100 I = 1,N1
EI = EI + 1.0
PEL = (EI - 1.0) * DEL
C
DO 100 NN = 1,NNF
ENN = NN - 1
TU = DELT * TCTR
C
DO 95 J = 1,NTH
EJ = J - 1
ZTA = EJ * DELTH + DELTH * 0.5
IF (NN .EQ. 1) GO TO 90
C
PTH(NN,I) = PTH(NN,I) + PPH(PEL,ZTA,TU) * SIN(ENN * (ZTA - 1.5707963))
PFE(NN,I) = PFE(NN,I) + PPF(PEL,ZTA,TU) * COS(ENN * ZTA)
PN(NN,I) = PN(NN,I) + PPN(PEL,ZTA,TU) * COS(ENN * ZTA)
GO TO 95
C
90 PTH(NN,I) = PTH(NN,I) + PPH(PEL,A,TU) / 2.
PFE(NN,I) = PFE(NN,I) + PPF(PEL,ZTA,TU) / 2.
PN(NN,I) = PN(NN,I) + PPN(PEL,ZTA,TU) / 2.0
95 CONTINUE
C
PTH(NN,I) = S3 * DELTH * PTH(NN,I)
PFE(NN,I) = S1 * DELTH * PFE(NN,I)
PN(NN,I) = S3 * DELTH * PN(NN,I)
100 CONTINUE
C
IF (ICTR .EQ. 1.0) GO TO 105
WRITE ( 9) PFE, PTH, PN
GO TO 107
105 WRITE ( 3) PFE, PTH, PN
107 XX = GDA(25)
IF (N .GT. 50 .AND. NAR.EQ. 0) N12 = 50
IF (PFLAG .LT. 0.)

```

```

00000820
00000830
00000840
00000850
00000870
00000873
00000876
00000880
00000890
00000900
00000910
00000919
00000920
00000930
00000940
00000960
00000970
00000980
00000990
0001000
0001010
0001030
0001040
0001050
0001060
0001069
0001080
0001090
0001100
0001110
0001120
0001130
0001140
0001150
0001160
0001170
0001180
0001190
0001200
0001210
0001220
0001222
0001229

```

```

WRITE (6,108) NI1, NI2, (PFE(NN,1), NN=1,NNF), I=1,NI1, XX, XX, XC, XC, NI230
IX, (PTH(NN,1), NN=1,NNF), I=1,NI1, XX, XX, XX, (PNT(NN,1), NN=1,NNF)I231
2NNF), I=1,NI1)
108 FORMAT(10X,11HFOR STATION, 13,16H THROUGH STATION, 14777
1 ( 1P6E17.7) )
C
NAB = NAB + NI
IF (NAB .EQ. N) GO TO 600
C
C MORE THAN 50 STATIONS TO STORE *
C
NI = N - NI
NI1 = 51
NI2 = N
DO 115 I = 1,50
DO 110 J = 1,10
PTH(J,I) = 0.0
PFE(J,I) = 0.0
110 PHT(J,I) = 0.0
115 CONTINUE
C
GO TO 70
C
600 IF (TR .NE. 1.0) GO TO 610
REWIND 3
RETURN
C
610 IF (N .GT. 50) BACKSPACE 9
BACKSPACE 9
RETURN
C
END

```



3. 12f PA1DX Subroutine (PXDYN)

```

00000010
00000020
00000030
00000040
00000050
00000060
00000070
00000080
00000090
00000100
00000110
00000120
00000130
00000140
00000150
00000160
00000170
00000171
00000171
00000190
00000196
00000197
00000198
00000199
00000200
00000210
00000220
00000230
00000240
00000250
00000260
00000270
00000280
00000290
00000300
00000310
00000312
00000313
00000314
00000315
00000316
00000320
00000330
00000340

**
**

SUBROUTINE PANDX
  AO REFERENCE LENGTH (IN)
  HO REFERENCE THICKNESS (IN)
  EO REFERENCE YOUNGS MODULUS (PSI)
  SIGO REFERENCE STRESS (PSI)
  NPIF NO. OF TERMS IN THE FOURIER EXPANSION.
  LAM LAMBDA = HO /AO
  WFE OMEGA (XI)
  WTH OMEGA (THETA)

  ARRAYS USED
  COEFC - CONTAINS STIFFNESS COEFF CALCULATED IN DATLYR
  P1SCB1 - TEMP STORAGE FOR STIFFNESS COEFF AT LAST TWO
  P2SCB1 - STATIONS OF THE BLOCK

  PANDX FLAGS
  JPATH = 0 PATH IND. THRU ENF LOOP WHEN F, G, H INCOMPLETE.
  KPATH = 1 PATH IND. THRU ENF LOOP TO SKIP FGMPE AND BND.
  KPATH = 0 PATH IND. THRU ENF LOOP WHEN L, M, N INCOMPLETE
  KPATH = 1 PATH IND. THRU ENF LOOP TO SKIP DYLMM AND BND.
  IRTE .NE. 1 FIRST STATION - NOT FIRST BLOCK
  IRTE .EQ. 1 LAST STATION - PREVIOUS BLOCK
  IFGFG = 10 F, G, H, PE HAVE NOT BEEN COMPLETED, YET.
  IFGFG = 0 P AND X HAVE BEEN COMPUTED FOR IRTE = 1.
  IFGFG = 1 P AND X COMPUTED. INCREMENT STA. INDEX.
  IRSFG = 10 R, S, LI, HAVE NOT BEEN COMPLETED.
  IRSFG = 1 INITIAL BOUNDARY COMPUTED.
  IFDYN = 10 AL, AM, AN HAVE NOT BEEN COMPLETED.
  IFDYN = 1 AK, AM, AN COMPUTED.
  IFMX = 10 PE NOT COMPUTED.
  IFMX = 1 PE COMPUTED.

  COUNTERS
  MM - ABSOLUTE STATION NUMBER.
  I - STATION NO. WITHIN EACH BLOCK OF STIFF. COEFF.
  MMN - STATION NO. WITHIN BLOCK OF LOADS.
  IFLG - STIFF. COEFF. BLOCK.

  EQUIVALENCE (BMTX( 1), OMGO), (BMTX( 26), OMGN),
  (BMTX( 51), ALMO), (BMTX( 76), ALMN),
  1

```

```

2 (BMTX(101), OMG1), (BMTX(126), ALM1), 0000350
3 (BMTX(151), LLO), (BMTX(156), LLLN) 0000360
0000370
EQUIVALENCE (GDA( 1), AU), (GDA( 2), HO), 0000380
(GDA( 3), ED), (GDA( 4), SIGO), 0000390
(GDA( 5), POI), (GDA( 6), ENF), 0000400
(GDA( 7), BCIT), (GDA( 8), BCIB), 0000410
(GDA( 9), PFLAG), (GDA(10), CEXT), 0000420
(GDA(11), DELT), (GDA(12), THT), 0000421
(GDA(18), FPRNT) 0000422
0000440
0000450
0000460
0000470
0000480
0000490
0000491
0000492
0000493
0000494
0000540
0000570
0000580
0000590
0000600
0000610
0000620
0000630
0000640
0000649
0000650
0000660
0000670
0000680
0000690
0000700
0000710
0000720
0000730
0000740
0000760
0000770
0000780

C
DIMENSION WTX(100), WFX(100), RHOX(100), GAMA(100), WFEPX(100)
DIMENSION ALMO(5,5), ALMN(5,5), OMGU(5,5), OMGN(5,5)
DIMENSION ALM1(5,5), OMG1(5,5)
REAL LLO(5), LLLN(5), MFE(10), MTP(10)
DIMENSION P1SCB1(20), P2SCB1(20), P1SCD1(20), P2SCD1(20),
1 TFE(10), P1SG13(20), P2SG13(20), P1ENT1(20), P2ENT1(20), PN50(10),
2 TTP(10), P1SCG1(20), P2SCG1(20), P1FMT1(20), P2FMT1(20),
3 P2DCK1(20), P2DCK2(20), P2DCK3(20), P2DCM1(20), P2DCM4(20),
4 P2DCC1(20), P2DCC2(20), P2DCC3(20), PFE50(10), PTH50(10)
DIMENSION PFE(10, 50), PTH(10, 50), PN(10, 50)
DIMENSION P(50,50), X(50)

C
DIMENSION COEFC(2200)
DIMENSION SCB1(100), SCB2(100), SCB3(100), SCG1(100), SCG2(100),
1 SCG3(100), SCD1(100), SCD2(100), SCD3(100), SCNTTH(100),
2 SCNTSI(100), SCNTTH(100), SCMTSI(100), SCMTTH(100), DCM1(100),
3 DCM4(100), DCC1(100), DCC2(100), DCC3(100), DCK1(100), DCK2(100),
4 DCK3(100)

EQUIVALENCE (COEFC( 1), SCB1), (COEFC(101), SCB2),
1 (COEFC( 20), SCB3), (COEFC( 30), SCG1),
2 (COEFC( 40), SCG2), (COEFC( 50), SCG3),
3 (COEFC( 60), SCD1), (COEFC( 70), SCD2),
4 (COEFC( 80), SCD3), (COEFC(101), SCNTTH),
5 (COEFC( 90), SCG13), (COEFC(101), SCNTSI), (COEFC(110), SCNTTH),
6 (COEFC(120), SCMTSI), (COEFC(130), SCMTTH), (COEFC(140), DCM1),
7 (COEFC(150), DCM4), (COEFC(160), DCC1), (COEFC(170), DCC2),
8 (COEFC(180), DCC3), (COEFC(190), DCK1), (COEFC(200), DCK2),
9 (COEFC(210), DCK3)

C
COMMON GDA(25), DEL, N, NNF, NTH,
1 BMTX(160), TCTR, KZTW, KZTR, KPTH, KPTR

```

```

C      00000789
C      00000790
C      00000800
C      00000809
C      00000810
C      00000811
C      00000812
C      00000813
C      00000814
C      00000815
C      00000816
C      00000817
C      00000900
C      00000910
C      00000920
C      00000930
C      00000939
C      00000940
C      00000950
C      00000960
C      00000970
C      00000980
C      00000990
C      00000999
C      00001000
C      00001010
C      00001019
C      00001020
C      00001030
C      00001040
C      00001048
C      00001049
C      00001050
C      00001056
C      00001057
C      00001058
C      00001059
C      00001060
C      00001069
C      00001070
C      00001080
C      00001090
C      00001100

1 REAL LAM, LAM02, LAM202, LAM204, LAM208, LAM2, KORO, KORO2,
   MFETK, MTHTK, MFETP, LLI
C
COMMON /PXCMM/ MM, LLN, I, IFLG, LN, IRSFG, IFGFG,
1 BB1KJ, BB2KJ, BB3KJ, GG1KJ, GG2KJ, GG3KJ, DD1KJ, DD2KJ, DD3KJ,
2 GG13KJ, TFETK, TTHTK, MFETK, MTHTK, BB1P, BB3P, GG1P, GG2P,
3 DD1P, DD3P, GG13P, TFETP, MFETP, OMG(5,5), ALM(5,5), LLI(5),
4 WTH, WFE, GAM, RHO, WFEP, LAM, LAM2, LAM02, LAM202, LAM204,
5 LAM208, GAM2, WTMWF, WTMWF2, WFT, THK, PNK, PFEK, P, X,
6 DCM1KJ, DCM2KJ, DCM3KJ, DCM4KJ, DCM5KJ, DCC1KJ, DCC2KJ, DCC3KJ,
7 DCN1KJ, DCK2KJ, DCK3KJ
COMMON /BLOCK1/ EMM2 (50,50)
COMMON /BLOCK2/ EMM3 (50)
C
IF(PFLAG.EQ.-1.E+10) WRITE (6,340)
C
READ ( 3) WTHX, WFEX, GAMA, RHOX, WFEPX READ GEOMETRY PARAMETERS (100)
N2 = 2 * NNF
C
IN = 1
MMN = 0
IFLG = 0
C
IF (TCTR.EQ.1.0) GO TO 8
READ ( 9) PFE, PTH, PN READ PRESSURES (10, 50)
C
REWIND 9
AF = FILE (9,1)
GO TO 15
C
8 READ ( 3) PFE, PTH, PN READ PRESSURES (10,50) TIME CYCLE 1
C
C
C
C
C
10 READ ( 9) LN, IN, COEFC READ STIFFNESS COEFF (100)
C
15 IRTE = 1 IN - INITIAL STATION IN BLOCK
MM = IN - 1 LN - LAST STATION IN BLOCK
IFLG = IFLG + 1
LLN = LN - IN + 1

```

```

00001110
00001120
00001130
00001140
00001150
00001160
00001170
00001180
00001190
00001200
00001210
00001230
00001232
00001234
00001236
00001238
00001240
00001250
00001260
00001270
00001280
00001290
00001300
00001310
00001320
00001329
00001330
00001340
00001350
00001360
00001365
00001366
00001367
00001370
00001380
00001390
00001400
00001409
00001410
00001420
00001430
00001440
00001450

C
I = 0
KK = NNF
DEL2 = 2. * DEL

20 I = I + 1
MM = MM + 1
MMN = MMN + 1
IF (TCTR.GT. 1.0 .AND. MM.EQ. 1) GO TO 20
IF (TCTR.GT. 1.0 .AND. MM.EQ. N) RETURN
JPATH = 0
KPATH = 0
IF (MM.NE. 51) GO TO 23
DO 19 IX = 1, KK
PFE50(IX) = PFE(IX, 50)
PTH50(IX) = PTH(IX, 50)
19 PNE50(IX) = PN(IX, 50)
IF (TCTR.EQ. 1.0) GO TO 21
AF = FILE(9, 2)
READ ( 9) PFE, PTH, PN
READ ( 9) PFE, PTH, PN
REWIND 9
AF = FILE(9, 2)
GO TO 22
21 READ ( 3) PFE, PTH, PN
22 MMN = 1

C
23 DO 9998 J = 1, KK
IF (TCTR.GT. 1.0) GO TO 37
IF (JPATH.EQ. 1) GO TO 37
IF (KPATH.EQ. 1) GO TO 37
ESTABLISH BOUNDARY CONDITIONS ARRAY.
IF (MM.NE. 1) GO TO 33
IF (J.EQ. 1) GO TO 31
IF (BCIT.NE. 1.0) GO TO 31
IF (J.GT. 2) GO TO 29
CLOSED APEX, 2ND HARMONIC
27 DO 28 KN = 1, 5
DO 28 JJ = 1, 5
OMG(KN, JJ) = OMG1(KN, JJ)
ALM(KN, JJ) = ALM1(KN, JJ)
28 LL1(KN) = 0.0

```

```

C          GO TO 37
29 DO 30 KN = 1.5
DO 30 JJ = 1.5
OMG(KN,JJ) = 0.0
ALM(KN,JJ) = 0.0
IF (KN.EQ. JJ) ALM(KN,JJ) = 1.0
30 LLI(KN) = 0.0
GO TO 37

C          1ST FOURIER COMPONENT, 1ST STA.
31 DO 32 KN = 1.5
DO 32 JJ = 1.5
OMG(KN,JJ) = OMGO(KN,JJ)
ALM(KN,JJ) = ALMO(KN,JJ)
32 LLI(KN) = LLO(KN)
GO TO 37

C          LAST STATION
33 IF (MM.NE. N) GO TO 37
C          IF (J.EQ. 1) GO TO 34
IF (RCIB.NE. 1.0) GO TO 34
IF (J.GT. 2) GO TO 28
GO TO 27

C          1ST FOURIER COMPONENT, NTH STA.
34 DO 35 KN = 1.5
DO 35 JJ = 1.5
OMG(KN,JJ) = OMGN(KN,JJ)
ALM(KN,JJ) = ALMN(KN,JJ)
35 LLI(KN) = LLLN(KN)

C          DO 998 K = 1, KK
37 DO 998 K = 1, KK
IF (YCTR.GT. 1.0) GO TO 152
IF (KPATH.EQ. 1) GO TO 152
IF (I.NE. 1) GO TO 85
IF (IFLG.NE. 1) GO TO 98

C          RECURSION FORMS
C          * *
C          * *
38 JMK = J - K
KMJA = 1 + IABS(K - J)
KPJ = K + J - 1
TERM1 = 1.0
IF (JMK.EQ. 0) TERM1 = 0.0

```

```

00001460
00001469
00001470
00001480
00001490
00001500
00001510
00001520
00001530
00001539
00001540
00001550
00001560
00001570
00001580
00001590
00001599
00001600
00001609
00001610
00001620
00001630
00001640
00001649
00001650
00001660
00001670
00001680
00001690
00001699
00001700
00001710
00001720
00001730
00001740
00001750
00001751
00001752
00001760
00001770
00001780
00001790
00001800

```

```

TERM2 = 1.0
IF (K.EQ. 1) TERM2 = 0.0
FCTR = 1. - TERM1 + TERM2
FCTR2 = 1. - 2. * TERM2

K2 = N2 * (I-1) + KPJ
K5 = N2 * (I-1) + KMJA
IF (.JPATH.EQ. 1) GO TO 50
K1 = N2 * I + KPJ
K3 = N2 * (I+1) + KPJ
K4 = N2 * I + KMJA
K6 = N2 * (I+1) + KMJA
K7 = N2 * (I-2) + KPJ
K8 = N2 * (I-2) + KMJA
K9 = N2 * (I-3) + KPJ
K10 = N2 * (I-3) + KMJA

IF (MM.NE. 1) GO TO 55
C
C
C
FORWARD DIFFERENCE FOR FIRST STATION.
IF (.NE. 1) GO TO 39
TTP(K) = (4. * SCNTSI(K1) - 3. * SCNTSI(K2) - SCNTSI(K3)) / DEL2
MTP(K) = (4. * SCNTSI(K1) - 3. * SCNTSI(K2) - SCNTSI(K3)) / DEL2
TFE(K) = SCNTSI(K2)
MFE(K) = SCNTSI(K2)

39 BPIKPJ = (4. * SCB1(K1) - 3. * SCB1(K2) - SCB1(K3)) / DEL2
DPIKPJ = (4. * SCD1(K1) - 3. * SCD1(K2) - SCD1(K3)) / DEL2
G13KPJ = (4. * SCG13(K1) - 3. * SCG13(K2) - SCG13(K3)) / DEL2
GPIKPJ = (4. * SCG1(K1) - 3. * SCG1(K2) - SCG1(K3)) / DEL2

C
C
BPIKMJ = (4. * SCB1(K4) - 3. * SCB1(K5) - SCB1(K6)) / DEL2
DPIKMJ = (4. * SCD1(K4) - 3. * SCD1(K5) - SCD1(K6)) / DEL2
G13KMJ = (4. * SCG13(K4) - 3. * SCG13(K5) - SCG13(K6)) / DEL2
GPIKMJ = (4. * SCG1(K4) - 3. * SCG1(K5) - SCG1(K6)) / DEL2

C
C
DERIVATIVE OF STIFFNESS RECURSIONS.
C
40 BB1P = 0.5 * (BPIKPJ + FCTR * BPIKMJ)
DD1P = 0.5 * (DPIKPJ + FCTR * DPIKMJ)
GG13P = 0.5 * (G13KPJ + FCTR * G13KMJ + FCTR2 * G13KPJ)
GG1P = 0.5 * (GPIKPJ + FCTR * GPIKMJ + FCTR2 * GPIKPJ)

C
C
C

```

```

00001810
00001820
00001830
00001840
00001850
00001860
00001870
00001880
00001890
00001900
00001910
00001920
00001930
00001940
00001950
00001960
00001970
00001980
00001988
00001989
00001990
00001991
00001992
00001993
00001994
00001995
00002000
00002010
00002020
00002040
00002050
00002060
00002080
00002090
00002110
00002120
00002121
00002122
00002130
00002140
00002150
00002160
00002170

```

```

C          STIFFNESS RECURSION      *
C
50  BB1KJ = 0.5 * (SCB1(K2) + FCTR * SCB1(K5))
    DD1KJ = 0.5 * (SCD1(K2) + FCTR * SCD1(K5))
    DCM1KJ = 0.5 * (DCM1(K2) + FCTR * DCM1(K5))
    DCM2KJ = 0.5 * ( FCTR * DCM1(K5) + FCTR2 * DCM1(K2))
    DCM4KJ = 0.5 * ( DCM4(K2) + FCTR * DCM4(K5))
    DCM5KJ = 0.5 * ( FCTR * DCM4(K5) + FCTR2 * DCM4(K2))
    DCK1KJ = 0.5 * (DCK1(K2) + FCTR * DCK1(K5))
    DCK2KJ = 0.5 * ( FCTR * DCK2(K5) + FCTR2 * DCK2(K2))
    DCK3KJ = 0.5 * (DCK3(K2) + FCTR * DCK3(K5))
    GGI3KJ = 0.5 * (FCTR * SCG13(K5) + FCTR2 * SCG13(K2))
    GG1KJ = 0.5 * (FCTR * SCG1(K5) + FCTR2 * SCG1(K2))
GO TO 150

C          IF (MM.EG. N) GO TO 65
    IF (J.NE. 1) GO TO 57
    TTP(K) = (SCNTSI(K1) - SCNTSI(K7)) /DEL2
    MTP(K) = (SCMTSI(K1) - SCMTSI(K7)) /DEL2
    TFE(K) = SCNTSI(K2)
    MFE(K) = SCMTSI(K2)

57  BPIKPJ = (SCB1(K1) - SCB1(K7)) /DEL2
    DPIKPJ = (SCD1(K1) - SCD1(K7)) /DEL2
    G13KPJ = (SCG13(K1) - SCG13(K7)) /DEL2
    GPIKPJ = (SCG1(K1) - SCG1(K7)) /DEL2

C          BPIKMJ = (SCB1(K4) - SCB1(K8)) /DEL2
    DPIKMJ = (SCD1(K4) - SCD1(K8)) /DEL2
    G13KMJ = (SCG13(K4) - SCG13(K8)) /DEL2
    GPIKMJ = (SCG1(K4) - SCG1(K8)) /DEL2
GO TO 40

C          BACKWARD DIFFERENCE FOR LAST STATION.
C          IF (J.NE. 1) GO TO 70
    TTP(K) = (SCNTSI(K9) + 3. * SCNTSI(K2) - 4. * SCNTSI(K7)) /DEL2
    MTP(K) = (SCMTSI(K9) + 3. * SCMTSI(K2) - 4. * SCMTSI(K7)) /DEL2
    TFE(K) = SCNTSI(K2)
    MFE(K) = SCMTSI(K2)

C          BPIKPJ = (SCB1(K9) + 3. * SCB1(K2) - 4. * SCB1(K7)) /DEL2
    DPIKPJ = (SCD1(K9) + 3. * SCD1(K2) - 4. * SCD1(K7)) /DEL2
    G13KPJ = (SCG13(K9) + 3. * SCG13(K2) - 4. * SCG13(K7)) /DEL2
    GPIKPJ = (SCG1(K9) + 3. * SCG1(K2) - 4. * SCG1(K7)) /DEL2

```

```

00002171
00002172
00002180
00002190
00002200
00002210
00002220
00002230
00002240
00002250
00002260
00002270
00002280
00002290
00002300
00002310
00002311
00002312
00002313
00002314
00002315
00002316
00002330
00002340
00002350
00002370
00002380
00002390
00002400
00002410
00002420
00002430
00002431
00002432
00002433
00002434
00002435
00002436
00002437
00002440
00002450
00002460
00002470

```

```

C      00002480
      00002490
      00002500
      00002510
      00002520
      00002530
      00002540
      00002550
      00002560
      00002570
      00002577
      00002578
      00002579
      00002580
      00002590
      00002600
      00002610
      00002620
      00002630
      00002640
      00002650
      00002660
      00002670
      00002680
      00002690
      00002700
      00002710
      00002720
      00002730
      00002740
      00002750
      00002760
      00002770
      00002772
      00002774
      00002776
      00002778
      00002780
      00002789
      00002790
      00002799
      00002800
      00002810

      BPIKMJ = (SCB1(K10) + 3. * SCB1(K5) - 4. * SCB1(K8)) /DEL2
      DPIKMJ = (SCD1(K10) + 3. * SCD1(K5) - 4. * SCD1(K8)) /DEL2
      G13KMJ = (SCG13(K10) + 3. * SCG13(K5) - 4. * SCG13(K8)) /DEL2
      GPIKMJ = (SCG1(K10) + 3. * SCG1(K5) - 4. * SCG1(K8)) /DEL2
      GO TO 40

C
C
C      85 IF (LN .EQ. N) GO TO 38
      IF (I .NE. 3) GO TO 93

      AT ARBITRARY STATION 3
      SAVE COEFF. OF LAST TWO STAS. OF THIS BLOCK. TO BE
      USED TO COMPUTE DERIVATIVES ON NEXT BLOCK. *

      KK2 = 2 * KK
      K11 = N2 * (LLN-2)
      K12 = N2 * (LLN-1)
      DO 90 IK = 1, KK2
      K13 = K11 + IK
      K14 = K12 + IK
      P1SCB1(IK) = SCB1(K13)
      P2SCB1(IK) = SCB1(K14)
      P1SCD1(IK) = SCD1(K13)
      P2SCD1(IK) = SCD1(K14)
      P1SG13(IK) = SCG13(K13)
      P2SG13(IK) = SCG13(K14)
      P1SCG1(IK) = SCG1(K13)
      P2SCG1(IK) = SCG1(K14)
      P2DCM1(IK) = DCM1(K14)
      P2DCM4(IK) = DCM4(K14)
      P2DCK1(IK) = DCK1(K14)
      P2DCK2(IK) = DCK2(K14)
      P2DCK3(IK) = DCK3(K14)
      P1ENT(IK) = SCNTSI(K13)
      P2ENT(IK) = SCNTSI(K14)
      P1MT(IK) = SCMTSI(K13)
      P2MT(IK) = SCMTSI(K14)
      90 CONTINUE

      IS COEFF BLOCK COMPLETED
      NO

C      93 IF (I .EQ. LLN) GO TO 10
      GO TO 38

C
C

```



```

C      98 JMK = J - K
      KMJA = 1 + IABS(K - J)
      KPJ = K + J - 1
      TERM1 = 1.0
      IF (JMK .EQ. 0) TFRM1 = 0.0
      TERM2 = 1.0
      IF (K .EQ. 1) TERM2 = 0.0
      FCTR = 1. - TERM1 + TERM2
      FCTR2 = 1. - 2. * TERM2

C      K1 = N2 * I + KPJ
      K2 = N2 * (I-1) + KPJ
      K4 = N2 * I + KMJA
      K5 = N2 * (I-1) + KMJA

C      IF (JPATH .EQ. 1) GO TO 125

C      IRTE .NE. 1 - FIRST STATION IN A SECTION (NOT REGION).
C      IRTE .EQ. 1 - LAST STATION IN PREVIOUS SECTION.
C      100 IF (IRTE .NE. 1) GO TO 110
C      LAST STATION - PREVIOUS BLOCK
C      IF (K .NE. 1 .OR. J .NE. 1) GO TO 102
C      MM = MM - 1
C      MMN = MMN - 1
C      102 IF (J .NE. 1) GO TO 103
C      TTP(K) = (SCNTSI(K2) - PIENT(KPJ)) /DEL2
C      MTP(K) = (SCMTSI(K2) - PIEMT(KPJ)) /DEL2
C      TFE(K) = PZENT(KPJ)
C      MFE(K) = PZEMT(KPJ)
C      103 BP1KPJ = (SCP1(K2) - P1SCB1(KPJ)) /DEL2
C      DP1KPJ = (SCD1(K2) - P1SCD1(KPJ)) /DEL2
C      G13KPJ = (SCG13(K2) - P1SG13(KPJ)) /DEL2
C      GP1KPJ = (SCG1(K2) - P1SCG1(KPJ)) /DEL2

C      105 BP1KMJ = (SCB1(K5) - P2SCB1(KMJA)) /DEL2
C      DP1KMJ = (SCD1(K5) - P2SCD1(KMJA)) /DEL2
C      G13KMJ = (SCG13(K5) - P2SG13(KMJA)) /DFL2
C      GP1KMJ = (SCG1(K5) - P2SCG1(KMJA)) /DEL2
C      GO TO 120

C      110 IF (K .NE. 1 .OR. J .NE. 1) GO TO 111
      FIRST STATION - NOT FIRST BLOCK

```

00002820  
00002830  
00002840  
00002850  
00002860  
00002870  
00002880  
00002890  
00002900  
00002910  
00002920  
00002930  
00002940  
00002950  
00002960  
00002970  
00002980  
00002986  
00002987  
00002988  
00002989  
00002990  
00003000  
00003010  
00003020  
00003030  
00003031  
00003032  
00003033  
00003034  
00003035  
00003040  
00003050  
00003060  
00003070  
00003080  
00003090  
00003100  
00003120  
00003130  
00003140  
00003190  
00003200

```

MM = MM + 1
MMN = MMN + 1
111 IF (J.NE. 1) GO TO 112
      TPI(K) = (SCNTSI(K1) - P2ENT(KPJ)) / DEL2
      MTP(K) = (SCMTSI(K1) - P2EMT(KPJ)) / DEL2
      TFE(K) = SCNTSI(K2)
      MFE(K) = SCNTSI(K2)
112 BPIKPJ = (SCB1(K1) - P2SCB1(KPJ)) / DEL2
      DPIKPJ = (SCD1(K1) - P2SCD1(KPJ)) / DEL2
      G13KPJ = (SCG13(K1) - P2SG13(KPJ)) / DEL2
      GPIKPJ = (SCG1(K1) - P2SCG1(KPJ)) / DEL2
C
      BPIKMJ = (SCB1(K4) - P2SCB1(KMJA)) / DEL2
      DPIKMJ = (SCD1(K4) - P2SCD1(KMJA)) / DEL2
      G13KMJ = (SCG13(K4) - P2SG13(KMJA)) / DEL2
      GPIKMJ = (SCG1(K4) - P2SCG1(KMJA)) / DEL2
C
      BB1P = 0.5 * (BPIKPJ + FCTR * BPIKMJ)
      DD1P = 0.5 * (DPIKPJ + FCTR * DPIKMJ)
      GG13P = 0.5 * (FCTR * G13KMJ + FCTR2 * G13KPJ)
      GG1P = 0.5 * (FCTR * GPIKMJ + FCTR2 * GPIKPJ)
C
125 IF (IRTE.NE. 1) GO TO 135
      TERM11 = P2SCB1(KPJ)
      TERM21 = P2SCD1(KPJ)
130 BB1KJ = 0.5 * (TERM11 + FCTR * P2SCB1(KMJA))
      DD1KJ = 0.5 * (TERM21 + FCTR * P2SCD1(KMJA))
      DCM1FJ = 0.5 * (P2DCM1(KPJ) + FCTR * P2DCM1(KMJA))
      DCM2KJ = 0.5 * (FCTR * P2DCM1(KMJA) + FCTR2 * P2DCM1(KPJ))
      DCM4KJ = 0.5 * (P2DCM4(KPJ) + FCTR * P2DCM4(KMJA))
      DCM5KJ = 0.5 * (FCTR * P2DCM4(KMJA) + FCTR2 * P2DCM4(KPJ))
      DCK1KJ = 0.5 * (P2DCK1(KPJ) + FCTR * P2DCK1(KMJA))
      DCK2KJ = 0.5 * (FCTR * P2DCK2(KMJA) + FCTR2 * P2DCK2(KPJ))
      DCK3KJ = 0.5 * (P2DCK3(KPJ) + FCTR * P2DCK3(KMJA))
      GG13KJ = 0.5 * (FCTR * P2SG13(KMJA) + FCTR2 * P2SG13(KPJ))
      GG1KJ = 0.5 * (FCTR * P2SCG1(KMJA) + FCTR2 * P2SCG1(KPJ))
      GO TO 150
C
135 BB1KJ = 0.5 * (SCB1(K2) + FCTR * SCE1(K5))
      DD1KJ = 0.5 * (SCD1(K2) + FCTR * SCD1(K5))
      DCM1KJ = 0.5 * (DCM1(K2) + FCTR * DCM1(K5))
      DCM2KJ = 0.5 * (FCTR * DCM1(K5) + FCTR2 * DCM1(K2))
      DCM4KJ = 0.5 * (DCM4(K2) + FCTR * DCM4(K5))

```

```

00003210
00003220
00003221
00003222
00003223
00003224
00003225
00003230
00003240
00003250
00003260
00003270
00003280
00003290
00003300
00003310
00003320
00003330
00003340
00003350
00003360
00003370
00003380
00003390
00003400
00003410
00003420
00003430
00003440
00003450
00003460
00003470
00003480
00003490
00003500
00003510
00003520
00003530
00003540
00003550
00003560
00003570
00003580

```

DCM5KJ = 0.5 \* ( FCTR \* DCM4(K5) + FCTR2 \* DCM4(K2) )  
 DCK1KJ = 0.5 \* ( DCK1(K2) + FCTR \* DCK1(K5) )  
 DCK2KJ = 0.5 \* ( FCTR \* DCK2(K5) + FCTR2 \* DCK2(K2) )  
 DCK3KJ = 0.5 \* ( DCK3(K7) + FCTR \* DCK3(K5) )  
 GG13KJ = 0.5 \* ( FCTR \* SCG13(K5) + FCTR2 \* SCG13(K2) )  
 GG1KJ = 0.5 \* ( FCTR \* SCG1(K5) + FCTR2 \* SCG1(K2) )

C 150 BB2KJ = BB1KJ  
 BB3KJ = POI \* BB1KJ  
 SS2 = (1. - POI) / 2.  
 GG2KJ = SS2 \* BB1KJ  
 GG3KJ = GG1KJ  
 BB3P = POI \* BB1P  
 GG3P = GG1P  
 GG2P = SS2 \* BB1P  
 DD2KJ = DD1KJ  
 DD3KJ = POI \* DD1KJ  
 DD3F = POI \* DD1P  
 152 TFETK = TFE(K)  
 THTK = TFE(K)  
 MFETK = MFE(K)  
 MHTK = MFE(K)  
 TFETP = TTP(K)  
 MFETP = MTP(K)  
 IF(MMN, EQ, 0) GO TO 153  
 PF EK = PFE(K,MMN)  
 PTHK = PTH(K,MMN)  
 PNK = PN(K,MMN)  
 GO TO 154  
 C 153 PF EK = PFE50(K)  
 PTHK = PTH50(K)  
 PNK = PN50(K)  
 C P AND X FORMULATION  
 C  
 C  
 C 150 WTH = WTHX(MM)  
 WFE = WFEX(MM)  
 GAM = GAMA(MM)  
 RMO = RMOX(MM)  
 WFEP = WFEPX(MM)  
 LAM = HO /AO

00003590  
 00003600  
 00003610  
 00003620  
 00003630  
 00003640  
 00003650  
 00003670  
 00003680  
 00003690  
 00003700  
 00003710  
 00003720  
 00003730  
 00003740  
 00003750  
 00003760  
 00003770  
 00003780  
 00003790  
 00003800  
 00003810  
 00003820  
 00003830  
 00003832  
 00003840  
 00003850  
 00003860  
 00003861  
 00003862  
 00003863  
 00003864  
 00003865  
 00003870  
 00003880  
 00003890  
 00003900  
 00003910  
 00003920  
 00003930  
 00003940  
 00003950  
 00003960

```

LAM2 = LAM * LAM
IF (TCTR .GT. 1.0) GO TO 450
IF (KPATH .EQ. 1) GO TO 450
LAM02 = LAM / 2.
LAM202 = LAM * LAM02
LAM204 = LAM02 * LAM02
LAM208 = LAM204 / 2.
GAM2 = GAM ** 2
WTMWF = WTH - WFE
WTMWF2 = WTMWF ** 2
WFWT = WFE * WTH
C
IF (JPATH .EQ. 1) GO TO 400
IF (IFLG .NE. 1) GO TO 235
IF (I .NE. 1) GO TO 235
C
C
195 CALL RSLT (J,K,KK)
IF (IRSFG .GT. 1) GO TO 9998
IF (IRSFG .EQ. 1) GO TO 20
RETURN
C
235 IF (I .NE. LLN) GO TO 237
IF (LN .EQ. N) GO TO 155
C
C
237 CALL FGHPE (J,K,KK,IRTE)
IF (IFGFG .GT. 1) GO TO 9998
JPATH = 1
GO TO 23
C
C
400 CALL DYLMM (J,K,KK,IFDYN)
IF (IFDYN .GT. 1) GO TO 9998
KPATH = 1
GO TO 23
C
C
450 CALL GMTX (J,K,KK,IFMX)
IF (IFMX .GT. 1) GO TO 9998
IF (TCTR .GT. 1.0) GO TO 20
IF (IFGFG .EQ. 1) GO TO 20
IRTE = 0
JPATH = 0
KPATH = 0
GO TO 23
9998 CONTINUE
C
140 FORMAT (1H--14HENTERFD PANDX. )
RETURN
END

```

```

00003970
00003980
00003990
00004000
00004010
00004020
00004030
00004050
00004060
00004070
00004080
00004090
00004100
00004110
00004120
00004130
00004139
00004140
00004150
00004160
00004170
00004180
00004190
00004200
00004208
00004209
00004210
00004220
00004230
00004240
00004268
00004269
00004270
00004280
00004290
00004300
00004308
00004309
00004310
00004320
00004330
00004340
00004350
00004360
00004370
00004380
00004390
00004400
00004410
00004420
00004430

```

SET UP BOUNDARY MATRICES

SET UP MATRICES IN EQUILIBRIUM EQ.

SET UP L, M, N MATRICES USED IN G\*\*

FORM G\*\*, D\*\*, P AND X MATRICES

3.12g RSLT Subroutine (BNDD)

```

$IHFTC BNDD
C
SURROUTINE RSLT (J,K,KK)
C
C COMPUTES THE BOUNDARY MATRICES FOR IP AND XI MATRICES.
C
DIMENSION R(50,50), AA(5,50), J(50,50), L1(50)
DIMENSION P(5,5), X(5), ZX(5)
C
COMMON GDA(25), DEL, N, NNF, NTH,
1 RMTX(160), ICTR, K/T, K/TP, K/PL, K/PR
C
COMMON /PXC/MV, MN, LLN, L, JF1, LN, JP, EG, JF,FG,
1 RRTKJ, RR3KJ, RR4KJ, CC3KJ, CC2KJ, RR2KJ, RR1KJ, RR3KJ,
2 GG1KJ, TFFK, LTHK, MFFK, MTHK, MHP, RR3P, GG1P, GG2P,
3 DD1P, DD3P, GG1P, TFFP, MFFP, MHP, OMG(5,5), LL1(5),
4 WTH, WFF, GAM, RHO, WFFP, LAM, LAM2, LAM202, LAM204,
5 LAM208, GAM2, WTMWF, WTMWF2, WFR1, PIHK, PNK, PFFK, P, X,
6 DCM1KJ, DCM2KJ, DCM3KJ, DCM4KJ, DCM5KJ, DCC1KJ, DCC2KJ, DCC3KJ,
7 DCK1KJ, DCK2KJ, DCK3KJ
C
COMMON /BLOCK1/ EMM2 (50,50)
COMMON /BLOCK2/ EMM3 (50)
C
EQUIVALENCE (GDA1 1), AU1, (GDA1 2), HU1,
1 (GDA1 3), FO1, (GDA1 4), SIG1,
2 (GDA1 5), PO1, (GDA1 6), ENF1,
3 (GDA1 7), RC11, (GDA1 8), RC1B1,
4 (GDA1 9), PFLAG1, (GDA11), CEXT1,
5 (GDA111), DFLT1, (GDA112), TH1,
6 (GDA118), FPRN1)
C
REAL LAM, LAM02, LAM202, LAM204, LAM208, LAM2, KURO, KUR02,
1 MFFK, MTHK, MFFP, L1, LL1
C R, S, LT MATRICES IN BOUNDARY EQUATIONS (44, 45) JID, 65-1633
C
KK5 = 5 * NNF
IF (K.NE.1) GO TO 164
IF (J.NE.1) GO TO 164
C
DO 163 KN = 1, KK5
LT(KN) = 0.0
DO 162 JJ = 1, KK5

```

S(KN,JJ) = 0.0  
 R(KN,JJ) = 0.0  
 162 CONTINUE  
 163 CONTINUE  
 C  
 164 KORO = FLOAT(K-1) / RHO  
 KORO2 = KORO \* KORO  
 R(5\*K-4,5\*J-4) = RR1KJ \* OMG(1,1)  
 R(5\*K-3,5\*J-3) = GG1KJ / 2. + LAM208 \* WTMWF2 \* GG13KJ  
 R(5\*K-2,5\*J-2) = LAM204 \* WTMWF \* GG13KJ  
 R(5\*K-1,5\*J-1) = DD1KJ \* OMG(3,3)  
 R(5\*K, 5\*J) = ((GG13KJ \* WTMWF / 2.) \* U.5) \* OMG(5,5)  
 R(5\*K,5\*J) = GG13KJ \* 0.5 \* OMG(5,5)  
 R(5\*K-4,5\*J-3) = R(5\*K-3,5\*J-3) \* OMG(1,2)  
 R(5\*K-4,5\*J) = R(5\*K-3,5\*J) \* OMG(1,2)  
 R(5\*K,5\*J-1) = R(5\*K-1,5\*J-1) \* OMG(5,4)  
 C  
 S(5\*K-4,5\*J-4) = GAM \* RR3KJ  
 S(5\*K-4,5\*J-3) = KORO \* BB3KJ  
 S(5\*K-4,5\*J-2) = WFE \* BB1KJ + WTH \* BB3KJ  
 S(5\*K-3,5\*J-4) = LAM208 \* WTMWF2 \* GG13KJ - GG1KJ / 2.  
 S(5\*K-3,5\*J-3) = GAM \* S(5\*K-3,5\*J-4)  
 S(5\*K-3,5\*J) = -GAM \* R(5\*K-3,5\*J)  
 S(5\*K-3,5\*J-4) = KORO \* S(5\*K-3,5\*J-4)  
 S(5\*K-3,5\*J-1) = -KORO \* R(5\*K-3,5\*J)  
 S(5\*K-2,5\*J-4) = -WFE \* GG2KJ \* OMG(3,3)  
 S(5\*K-2,5\*J-1) = GG2KJ \* OMG(3,3)  
 S(5\*K-1,5\*J-1) = GAM \* DD3KJ  
 S(5\*K-1,5\*J) = KORO \* DD3KJ  
 S(5\*K, 5\*J-4) = GG13KJ \* WTMWF / 4.  
 S(5\*K,5\*J-3) = GAM \* S(5\*K, 5\*J-4)  
 S(5\*K,5\*J-4) = KORO \* S(5\*K,5\*J-4)  
 S(5\*K,5\*J-1) = -KORO \* GG13KJ / 2.  
 S(5\*K,5\*J) = -GAM \* GG13KJ / 2.  
 R(5\*K-3,5\*J-3) = R(5\*K-3,5\*J-3) \* OMG(2,2)  
 R(5\*K-3,5\*J) = R(5\*K-3,5\*J) \* OMG(2,2)  
 R(5\*K-1,5\*J-1) = R(5\*K-1,5\*J-1) \* OMG(4,4)  
 C  
 S(5\*K-4,5\*J-4) = S(5\*K-4,5\*J-4) \* OMG(1,1) + S(5\*K-3,5\*J-4) \*  
 1 OMG(1,2)  
 S(5\*K-4,5\*J-3) = S(5\*K-4,5\*J-3) \* OMG(1,1) + S(5\*K-3,5\*J-3) \*  
 1 OMG(1,2)

```

S(5*K-4.5*J-2) = S(5*K-4.5*J-2) * O/G(1.1)
S(5*K-4.5*J-1) = S(5*K-4.5*J-1) * O/G(1.2)
S(5*K-4.5*J) = S(5*K-4.5*J) * O/G(1.2)
S(5*K-3.5*J-2) = S(5*K-3.5*J-2) * O/G(2.2)
S(5*K-3.5*J-1) = S(5*K-3.5*J-1) * O/G(2.2)
S(5*K-3.5*J) = S(5*K-3.5*J) * O/G(2.2)
S(5*K-2.5*J-4) = S(5*K-2.5*J-4) * O/G(2.2)
S(5*K-2.5*J-3) = S(5*K-2.5*J-3) * O/G(2.2)
S(5*K-2.5*J-2) = S(5*K-2.5*J-2) * O/G(2.2)
S(5*K-2.5*J-1) = S(5*K-2.5*J-1) * O/G(2.2)
S(5*K-2.5*J) = S(5*K-2.5*J) * O/G(2.2)
S(5*K-1.5*J-4) = S(5*K-1.5*J-4) * O/G(5.5)
S(5*K-1.5*J-3) = S(5*K-1.5*J-3) * O/G(5.5)
S(5*K-1.5*J-2) = S(5*K-1.5*J-2) * O/G(5.5)
S(5*K-1.5*J-1) = S(5*K-1.5*J-1) * O/G(5.5)
S(5*K-1.5*J) = S(5*K-1.5*J) * O/G(5.5)
O/G(5.4)
S(5*K-1.5*J-1) = S(5*K-1.5*J-1) * O/G(4.4)
S(5*K-1.5*J) = S(5*K-1.5*J) * O/G(4.4)
S(5*K-1.5*J) = S(5*K-1.5*J) * O/G(4.4)
C
LT(5*K-4) = IF(5*K * O/G(1.1) + LL(1))
LT(5*K-3) = LL(2)
LT(5*K-2) = LL(3)
LT(5*K-1) = MFFIK * O/G(4.4) + LL(4)
LT(5*K) = LL(5)
C
IF (K .NE. J) GO TO 166
S(5*K-2.5*J-2) = ALM(2.2)
S(5*K-4.5*J-4) = S(5*K-4.5*J-4) + ALM(1.1)
S(5*K-3.5*J-3) = S(5*K-3.5*J-3) + ALM(2.2)
S(5*K-3.5*J-4) = S(5*K-3.5*J-4) + ALM(2.1)
S(5*K-1.5*J-1) = S(5*K-1.5*J-1) + ALM(4.4)
S(5*K-1.5*J) = S(5*K-1.5*J) + ALM(4.5)
S(5*K-1.5*J) = S(5*K-1.5*J) + ALM(5.5)
C
165 IF (K .NE. K) GO TO 167.
167 IF (J .EQ. K) GO TO 169.
IRSG = 10
GO TO 180
C
160 IF (IFLG .GT. 1) GO TO 305
IF (I .GT. 1) GO TO 3.5
C
DO 175 K = 1,KK5
DC 175 J = 1,KK5
175 R(K,J) = (20/DEL) * R(K,J)
C
INITIAL BOUNDARY
SAVE IS0

```

```

WRITE (11) R
DO 176 K = 1, KK5
DO 176 J = 1, KK5
176 AAO(K,J) = .25 * R(K,J)
C
WRITE (11) AAO
DO 177 K = 1, KK5
DO 177 J = 1, KK5
177 FMM2(K,J) = 3. * AAO(K,J)
CALL MAD (KK5, KK5, S, FMM2, S)
C
WRITE (11) S
C
WRITE (11) LT
END FILE 11
IRSG = 1
180 IF (PFLAG .EQ. -1.5+10) WRITE (6,310)
RETURN
C
305 DO 306 K = 1, KK5
DO 306 J = 1, KK5
306 R(K,J) = (3.7/12.*DEL1) * R(K,J)
CALL MAD (KK5, KK5, S, R, AAO)
DO 307 K = 1, KK5
DO 307 J = 1, KK5
R(K,J) = R(K,J) / 3.
307 S(K,J) = -4. * R(K,J)
C
WRITE (11) R, S, AAO, LI
HACKSPACE 10
C
IRSG = 0
REWIND 13
END FILE 9
REWIND 11
C
MOVE R, A, C, G, FROM IP 11 TO 3
BY SEPARATE RECORDS
C
READ (11) P
WRITE (3) P
READ (11) P

```

```

0001490
0001491
0001492
0001493
0001494
0001495
0001496
0001497
0001498
0001499
0001500
0001501
0001502
0001503
0001504
0001505
0001506
0001507
0001508
0001509
0001510
0001511
0001512
0001513
0001514
0001515
0001516
0001517
0001518
0001519
0001520
0001521
0001522
0001523
0001524
0001525
0001526
0001527
0001528
0001529
0001530
0001531
0001532
0001533
0001534
0001535
0001536
0001537
0001538
0001539
0001540
0001541
0001542
0001543
0001544
0001545
0001546
0001547
0001548
0001549
0001550
0001551
0001552
0001553
0001554
0001555
0001556
0001557
0001558
0001559
0001560
0001561
0001562
0001563
0001564
0001565
0001566
0001567
0001568
0001569
0001570
0001571
0001572
0001573
0001574
0001575
0001576
0001577
0001578
0001579
0001580
0001581
0001582
0001583
0001584
0001585
0001586
0001587
0001588
0001589
0001590
0001591
0001592
0001593
0001594
0001595
0001596
0001597
0001598
0001599
0001600
0001601
0001602
0001603
0001604
0001605
0001606
0001607
0001608
0001609
0001610
0001611
0001612
0001613
0001614
0001615
0001616
0001617
0001618
0001619
0001620
0001621
0001622
0001623
0001624
0001625
0001626
0001627
0001628
0001629
0001630
0001631
0001632
0001633
0001634
0001635
0001636
0001637
0001638
0001639
0001640
0001641
0001642
0001643
0001644
0001645
0001646
0001647
0001648
0001649
0001650
0001651
0001652
0001653
0001654
0001655
0001656
0001657
0001658
0001659
0001660
0001661
0001662
0001663
0001664
0001665
0001666
0001667
0001668
0001669
0001670
0001671
0001672
0001673
0001674
0001675
0001676
0001677
0001678
0001679
0001680
0001681
0001682
0001683
0001684
0001685
0001686
0001687
0001688
0001689
0001690
0001691
0001692
0001693
0001694
0001695
0001696
0001697
0001698
0001699
0001700
0001701
0001702
0001703
0001704
0001705
0001706
0001707
0001708
0001709
0001710
0001711
0001712
0001713
0001714
0001715
0001716
0001717
0001718
0001719
0001720
0001721
0001722
0001723
0001724
0001725
0001726
0001727
0001728
0001729
0001730
0001731
0001732
0001733
0001734
0001735
0001736
0001737
0001738
0001739
0001740
0001741
0001742
0001743
0001744
0001745
0001746
0001747
0001748
0001749
0001750
0001751
0001752
0001753
0001754
0001755
0001756
0001757
0001758
0001759
0001760
0001761
0001762
0001763
0001764
0001765
0001766
0001767
0001768
0001769
0001770
0001771
0001772
0001773
0001774
0001775
0001776
0001777
0001778
0001779
0001780
0001781
0001782
0001783
0001784
0001785
0001786
0001787
0001788
0001789
0001790
0001791
0001792
0001793
0001794
0001795
0001796
0001797
0001798
0001799
0001800
0001801
0001802
0001803
0001804
0001805
0001806
0001807
0001808
0001809
0001810
0001811
0001812
0001813
0001814
0001815
0001816
0001817
0001818
0001819
0001820
0001821
0001822
0001823
0001824
0001825
0001826
0001827
0001828
0001829
0001830
0001831
0001832
0001833
0001834
0001835
0001836
0001837
0001838
0001839
0001840
0001841
0001842
0001843
0001844
0001845
0001846
0001847
0001848
0001849
0001850
0001851
0001852
0001853
0001854
0001855
0001856
0001857
0001858
0001859
0001860
0001861
0001862
0001863
0001864
0001865
0001866
0001867
0001868
0001869
0001870
0001871
0001872
0001873
0001874
0001875
0001876
0001877
0001878
0001879
0001880
0001881
0001882
0001883
0001884
0001885
0001886
0001887
0001888
0001889
0001890
0001891
0001892
0001893
0001894
0001895
0001896
0001897
0001898
0001899
0001900
0001901
0001902
0001903
0001904
0001905
0001906
0001907
0001908
0001909
0001910
0001911
0001912
0001913
0001914
0001915
0001916
0001917
0001918
0001919
0001920
0001921
0001922
0001923
0001924
0001925
0001926
0001927
0001928
0001929
0001930
0001931
0001932
0001933
0001934
0001935
0001936
0001937
0001938
0001939
0001940
0001941
0001942
0001943
0001944
0001945
0001946
0001947
0001948
0001949
0001950
0001951
0001952
0001953
0001954
0001955
0001956
0001957
0001958
0001959
0001960
0001961
0001962
0001963
0001964
0001965
0001966
0001967
0001968
0001969
0001970
0001971
0001972
0001973
0001974
0001975
0001976
0001977
0001978
0001979
0001980
0001981
0001982
0001983
0001984
0001985
0001986
0001987
0001988
0001989
0001990
0001991
0001992
0001993
0001994
0001995
0001996
0001997
0001998
0001999
0002000

```



```

WRITE ( 3 ) P
READ ( 1 ) P
WRITE ( 3 ) P
READ ( 1 ) X
WRITE ( 3 ) X
AF = FILE ( 1 , 1 )
END FILE 3
C
MOVE CN, HN, AN, GN FROM TAPE 1 TO 3
READ ( 1 ) P, FMM2, AAD, X
WRITE ( 3 ) P, EMM2, AAU, X
C
READ ( 1 ) P, FMM2, AAD, X
WRITE ( 3 ) P, EMM2, AAU, X
BACKSPACE 10
AF = FILE ( 1 , 1 )
C
READ ( 1 ) P, X
WRITE ( 3 ) P, X
C
MOVE L, M, N - TP 13 TO 9 ( 2 FILES POSSIBLE )
NM2 = ( N - 2 ) * 3
DO 170 I = 1, NM2
IF ( I .EQ. 147 ) END FILE 9
READ ( 1 ) P
WRITE ( 9 ) P
170 CONTINUE
END FILE 9
GO TO 180
180 FORMAT ( 1H-, 11HLEFT HANDRY. )
END
0001760
0001770
0001780
0001790
0001800
0001810
0001820
0001830
0001840
0001850
0001860
0001870
0001880
0001890
0001900
0001910
0001920
0001930
0001937
0001938
0001939
0001940
0001950
0001960
0001970
0001980
0001990
0002000
0002010
0002020
0002030

```

3. 12h FGHPE Subroutine (FGHDY)

```

SUBROUTINE FGHPE (J,K,KF,IRIF)
DIMENSION P(50,50), F(5,5), F1(5,5), G(5,5), H(5,5)
COMMON GDA(25), DEL, H, NNF, NTH,
1 RMTX(160), ICTR, K21, K2IR, PPI, PPIR
COMMON /PXCMM/ MM, LLN, I, IFLG, LN, IFFG, IFGG,
1 RRJK, RRJK, RRJK, GGJK, GGJK, GGJK, DDJK, DDJK, DDJK,
2 GGJK, ITHK, MTHK, MTHK, RRJK, RRJK, RRJK, GGJK, GGJK,
3 DDJK, DDJK, GGJK, IFFJK, IFFJK, IFFJK, IFFJK, IFFJK, IFFJK,
4 NTH, WFF, GAM, RHO, WFF, LAM, LAM, LAM, LAM, LAM, LAM,
5 LAM, GAM, WFF, WFF, WFF, WFF, WFF, WFF, WFF, WFF,
6 DCMJK, DCMJK, DCMJK, DCMJK, DCMJK, DCMJK, DCMJK, DCMJK,
7 DCMJK, DCMJK, DCMJK
COMMON /BLOCK1/ EMM2 (50,50)
COMMON /BLOCK2/ FMM3 (50)
EQUIVALENCE (GDA(1), A0),
1 (GDA(3), F0),
2 (GDA(5), POL),
3 (GDA(7), ACIT),
4 (GDA(9), PLAG),
5 (GDA(11), DELT),
6 (GDA(18), FPRNT)
PEAL LAM, LAM, LAM, LAM, LAM, LAM, LAM, LAM, LAM, LAM,
1 WFFK, WTHK, WFFK, I(50), LI
C F, G, H, P, MATRICES IN EQUILIBRIUM EQUATIONS (13) SID 65-163
KK5 = 5 * NNF
IF (K.NE.1) GO TO 164
IF (J.NE.1) GO TO 164
DO 163 KN = 1, KK5
DO 162 JJ = 1, KK5
F(KN, JJ) = 0.0
G(KN, JJ) = 0.0
ZERO MATRIX ARRAYS

```

```

HIKN,JJ) = 0.0
162 CONTINUE
163 CONTINUE
164 KOR0 = FLOATIK-1) /RHO
168 KOR02 = KOR0 * KOR0
C
F,G,H,PE MATRICES IN EQUILIBRIUM EQUATIONS. (33) SID 65-1633
C
DFLT2 = DFLT * DFLT
F(5*K-4,5*J-4) = RB1KJ
F(5*K-3,5*J-3) = GG1KJ/2. + LAM208 * WTMWF2 * GG13KJ
F(5*K-3,5*J) = LAM204 * WTMWF * GG13KJ
F(5*K-2,5*J-2) = GG2KJ
F(5*K-1,5*J-1) = LAM2 * DD1KJ
F(5*K,5*J-3) = F(5*K-3,5*J)
F(5*K,5*J) = LAM202 * GG13KJ
C
G(5*K-4,5*J-4) = RB1P + GAM * RB1KJ
G(5*K-4,5*J-3) = KOR0 * ( RB1KJ + GG1KJ /2. - LAM208 *
1 WTMWF2 * GG13KJ )
G(5*K-4,5*J-2) = WFE * ( RB1KJ + GG2KJ ) + WTH * RB1KJ
G(5*K-4,5*J) = -KOR0 * LAM204 * WTMWF * GG13KJ
G(5*K-3,5*J-4) = -G(5*K-4,5*J-3)
G(5*K-3,5*J-3) = GG1P/2. + LAM208 * ( WTMWF2 * GG13P - GG13KJ
2 * ( WTMWF2 * GAM + 2. * WFFP * WTMWF ) ) + GG1KJ * GAM /2.
G(5*K-3,5*J-2) = -KOR0 * LAM204 * WTMWF * GG13KJ
G(5*K-3,5*J) = LAM204 *
1) GG13P * WTMWF - GG13KJ * ( 2. * GAM * WTMWF + WFFP )
G(5*K-2,5*J-4) = -G(5*K-4,5*J-2)
G(5*K-2,5*J-2) = GG2P + GAM * GG2KJ
G(5*K-2,5*J-1) = GG2KJ
G(5*K-1,5*J-3) = -G(5*K-3,5*J-1)
G(5*K-1,5*J-2) = -G(5*K-2,5*J-1)
G(5*K-1,5*J-1) = LAM2 * ( DD1P + GAM * DD1KJ )
G(5*K-1,5*J) = KOR0 * ( LAM2 * DD1KJ + LAM202 * GG13KJ )
G(5*K,5*J-4) = -G(5*K-4,5*J)
G(5*K,5*J-3) = LAM204 *
1 GG13P * WTMWF + GG13KJ * ( 2. * GAM * WTMWF - WFFP )
G(5*K,5*J-1) = -G(5*K-1,5*J)
183 G(5*K,5*J) = LAM202 * ( GG13P + GAM * GG13KJ )
C
H(5*K-4,5*J-4) = GAM * PR1P - WFM1 * RB1KJ - GAM2 * RB2KJ - KOR02 *

```

1 GG1KJ/2.0 + LAM208\* WTMWF2\*GG13KJ) -WFF\*\*2 \* GG2KJ - DCK1KJ -00000767  
 2 2.0 \* DCM1KJ / DELT2 - 11.0 \* DCC1KJ / ( 6.0 \* DELT ) 00000767  
 H15K-4.5\*J-2) = KORO \* ( BR2P - GAM \* BR2KJ - GAM /2. \* 00000777  
 1 GG1KJ - GAM \* WTMWF2 \* LAM208 \* GG13KJ ) 00000780  
 H15K-4.5\*J-2) = WFF \* BR1P + WTH \* ( BR2P - GAM \* BR2KJ ) 00000790  
 1 + BR1KJ \* ( WFFP + GAM \* WFF ) 00000800  
 H15K-4.5\*J-1) = WFF \* GG2KJ + KORO \* ( LAM204 \* WTMWF \* GG13KJ ) 00000810  
 H15K-4.5\*J-1) = KORO \* GAM \* LAM204 \* WTMWF \* GG13KJ 00000820  
 H15K-3.5\*J-4) = KORO \* ( LAM208 \* ( WTMWF2 \* GG13P - WTMWF \* 00000830  
 1 GG13KJ \* ( 2. \* GAM \* WTMWF - 2. \* WFF ) - GG1P /2. + GAM 00000840  
 2 \* (-GG1KJ/2. - BR2KJ ) ) 00000850  
 H15K-3.5\*J-3) = (WFT - GAM2) /2. \* GG1KJ - GAM/2. \* GG1P - KORO \* 00000860  
 1 BR2KJ - WTH \*\*2 \* GG2KJ + LAM208 \* ( GAM \* WTMWF2 \* GG13P - GG13KJ 00000870  
 2 \* ( WTMWF2 \* (WFT + 2. \* GAM2) + 2. \* WTMWF \* GAM \* WFF ) - DCK2KJ 00000880  
 3 - 2.0 \* DCM2KJ / DELT2 - 11.0 \* DCC2KJ / ( 6.0 \* DELT ) 00000890  
 100 H15K-3.5\*J-2) = KORO \* ( WFF \* BR2KJ + WTH \* ( BR2KJ + GG2KJ ) ) 00000900  
 H15K-3.5\*J-1) = KORO \* ( LAM204 \* ( GAM \* ( 2. \* WTMWF + WFF ) \* 00000910  
 1 GG13KJ - WTMWF \* GG13P ) ) 00000920  
 H15K-3.5\*J-1) = WTH \* GG2KJ + LAM204 \* WTMWF \* 00000930  
 2 ( GG13KJ \* ( WFT + 2. \* GAM2 ) - GAM \* GG13P ) + GAM \* LAM204 00000940  
 3 \* WFFP \* GG13KJ 00000950  
 100 H15K-2.5\*J-4) = GG2KJ \* ( WFFP + GAM \* WFF ) - WFF \* ( GAM \* 00000960  
 1 BR2KJ + GG2P ) - WTH \* GAM \* BR2KJ 00000970  
 H15K-2.5\*J-2) = H15K-2.5\*J-2) 00000980  
 H15K-2.5\*J-2) = KORO \* GG2KJ - WFF\*\*2 \* BR1KJ - WTH ( 2. \* WFF \* 00000990  
 1 BR2KJ + WTH \* BR2KJ ) - DCK3KJ - 2.0 \* DCM1KJ / DELT2 - 11.0 00001000  
 2 \* DCC3KJ / ( 6.0 \* DELT ) 00001010  
 H15K-2.5\*J-1) = GG2P + GAM \* GG2KJ 00001020  
 H15K-2.5\*J) = KORO \* GG3KJ 00001030  
 H15K-1.5\*J-4) = H15K-4.5\*J-1) 00001040  
 H15K-1.5\*J-3) = KORO \* LAM204 \* GAM \* WTMWF \* GG13KJ 00001050  
 100 H15K-1.5\*J-1) = LAM2 \* (GAM \* DD3P - WFT) \* DCK3KJ - KORO/2. \* GG13KJ - 00001060  
 1 GAM2 \* DD2KJ - GG2KJ -2.0 \* DCM2KJ / DELT2 00001070  
 H15K-1.5\*J) = LAM2 \* KORO \* ( DD3P - GAM \* ( GG13KJ /2. + 00001090  
 1 DD2KJ ) ) 00001100  
 H15K-5\*J-4) = KORO \* ( LAM204 \* ( WTMWF \* GG13P - WFFP \* GG13KJ 00001110  
 1 ) ) 00001120  
 H15K-5\*J-3) = LAM204 \* (GAM \* WTMWF \* GG13P - GG13KJ \* (GAM \* WFFP 00001130  
 1 + WFT \* WTMWF ) ) + WTH \* GG3KJ 00001140  
 H15K-5\*J-2) = H15K-2.5\*J) 00001150  
 100 H15K-5\*J-1) = KORO \* ( LAM202 \* ( GG13P + GAM \* GG13KJ ) + LAM2 00001160  
 1 \* GAM \* DD2KJ ) 00001170  
 H15K-5\*J) = LAM202 \* ( (WFT - GAM2) \* GG13KJ - GAM \* GG13P ) 00001180

```

1 -L-2002 * LAMBDA INDKJ - GCRJ
C
C
IF (K.NE.KK) GO TO 203
IF (J.EQ.KF) GO TO 208
203 IFGEG = 10
GO TO 251
C
C
208 DO 210 K=1,KK5
DO 210 J = 1,KK5
F(K,J) = (2./DEL) * F(K,J) * DELT
G(K,J) = DELT * G(K,J)
210 H(K,J) = DELT * H(K,J)
CALL MAD (KK5,KK5, F, G, FMM2 )
CALL MSU (KK5,KK5, F, G, G )
DO 212 K = 1,KK5
DO 212 J = 1,KK5
H(K,J) = 2. * DELT * H(K,J)
212 F(K,J) = - 2. * F(K,J)
CALL MAD (KK5,KK5, F, H, H )
DO 214 K = 1,KK5
DO 214 J = 1,KK5
214 F(K,J) = FMM2(K,J)
C
C
IF (MM.NE.2) GO TO 260
CALL INVMNM (G, 5, KK5, IFRR )
IF (IFRR.LE.0) GO TO 320
SAVE A1, R1, C1 - TO BE USED IN FORMING Z(O)
WRITE (11) F, H, G
BACKSPACE 11
WRITE (12) F, H, G
250 IFGEG = 1
251 IFIPFLAG.EQ.-1.F+10) WRITE(6,252)
252 FORMAT (1H--11HLFFI FGTX. )
RETURN
C

```

```

-20 * GCRJ / FILE
DE FORMATS IN GCRJ
00001270
00001271
00001272
00001273
00001274
00001275
00001276
00001277
00001278
00001279
00001280
00001281
00001282
00001283
00001284
00001285
00001286
00001287
00001288
00001289
00001290
00001291
00001292
00001293
00001294
00001295
00001296
00001297
00001298
00001299
00001300
00001301
00001302
00001303
00001304
00001305
00001306
00001307
00001308
00001309
00001310
00001311
00001312
00001313
00001314
00001315
00001316
00001317
00001318
00001319
00001320
00001321
00001322
00001323
00001324
00001325
00001326
00001327
00001328
00001329
00001330
00001331
00001332
00001333
00001334
00001335
00001336
00001337
00001338
00001339
00001340
00001341
00001342
00001343
00001344
00001345
00001346
00001347
00001348
00001349
00001350
00001351
00001352
00001353
00001354
00001355
00001356
00001357
00001358
00001359
00001360

```

REPRODUCIBILITY OF THE DATA

```
260 WRITE (12) F, H, G  
IF (I.NE. 1) GO TO 250  
IF (IRTE.NE. 1) GO TO 250  
IFGG = 0  
GO TO 251  
270 WRITE (16,25) I  
280 FORMAT (1H-9X,16H5 INGH AR MATRIX,9X,6H1 = ,14)  
CALL EXIT  
STOP  
END
```

000163  
000164  
000165  
000166  
000167  
000168  
000169  
000170  
000171

3.12i DYLMN Subroutine (LMNDY)

```

$IFTC LMNDY
C
C
SUBROUTINE DYLMN(J,K,KO,IFUN)
C
C
DIMENSION AL(50,50), A(10,50), AN(5,50)
DIMENSION PR(5,5), Y(5,1)
EQUIVALENCE (A(1,1), A(1)), (A(1,50), A(1)),
1 (GDA(1), GDA(1)), (A(1,1), A(1)),
2 (GDA(5), GDA(5)), (A(1,1), A(1)),
3 (GDA(7), GDA(7)), (A(1,1), A(1)),
4 (GDA(9), GDA(9)), (A(1,1), A(1)),
5 (GDA(11), GDA(11)), (A(1,1), A(1)),
6 (GDA(13), GDA(13)), (A(1,1), A(1)),
7 (GDA(15), GDA(15)), (A(1,1), A(1))
C
COMMON GDA(25), GEL, S, NNF, Y(10)
1 RMIX(160), ICR
C
COMMON /PXCMP/ MN, ILN, I, IFLG, LN, IPRG, IPRG,
1 BRKJ, BR2KJ, BR3KJ, GGKJ, GG2KJ, GG3KJ, DD1KJ, DD2KJ, DD3KJ,
2 GG1KJ, TFFK, ITHK, MFFK, MTHK, RH3P, RH3P, GG2P,
3 DD1P, DD3P, GULP, TFFP, MFFP, MTHP, XG(15,5), ALM(5,5), LL(5),
4 WTH, WFP, GAM, RHO, WFER, LAM, LAM2, LAM2, LAM204,
5 LAM208, GAM2, WTW, WTW, WTW, WTW, WTW, WTW, WTW, WTW, WTW, WTW,
6 DCMKJ, DCM2KJ, DCM3KJ, DCM4KJ, DCM5KJ, DCM6KJ, DCM7KJ, DCM8KJ, DCM9KJ,
7 DCK1KJ, DCK2KJ, DCK3KJ
C
COMMON /BLOCK1/ EMM2 (50,50)
COMMON /BLOCK2/ EMM3 (50)
C
REAL LAM, LAM2, LAM202, LAM204, LAM208, LAM2, KORO, KURO2,
1 MFFK, MTHK, WFER, WTW
C
KFS = 5 + NNF
IF (Y(NF,1) GO TO 164
IF (J(NF,1) GO TO 164
C
DO 163 KN = 1,KK5
DO 162 JJ = 1,KK5
AI(KN, JJ) = 0.0
AM(KN, JJ) = 0.0

```

```

163 CONTINUE
163 CONTINUE
C
164 DFLD = DFL/DELT
AL(5*K-4.5*J-4) = -10. * DFLD * DCM1KJ - 7.0*DFL*DCC1KJ
AL(5*K-3.5*J-3) = -10.*DFLD * DCM2KJ - 6.0*DFL*DCC2KJ
AL(5*K-2.5*J-2) = -10.0 * DFLD * DCM3KJ - 5.0 * DFL * DCC3KJ
AL(5*K-1.5*J-1) = -10.0 * DFLD * DCM4KJ - 6.0 * DFL * DCC4KJ
AL(5*K.5*J) = -10. * DFLD * DCM5KJ

C
AM(5*K-4.5*J-4) = 8.0* DELD * DCM1KJ + 3.0 * DEL*DCC1KJ
AM(5*K-3.5*J-3) = 8.0*DELD * DCM2KJ + 3.0* DEL*DCC2KJ
AM(5*K-2.5*J-2) = 8.0 * DELD * DCM3KJ + 3.0 * DEL * DCC3KJ
AM(5*K-1.5*J-1) = 8.0 * DELD * DCM4KJ
AM(5*K.5*J) = 8.0* DELD * DCM5KJ

C
AN(5*K-4.5*J-4) = -2.0* DFLD * DCM1KJ - 2.0/3.0*DFL*DCC1KJ
AN(5*K-3.5*J-3) = -2.0 * DELD * DCM2KJ - 2.0/3.0 * DEL * DCC2KJ
AN(5*K-2.5*J-2) = -2.0 * DELD * DCM3KJ - 2.0 / 3.0 * DEL * DCC3KJ
AN(5*K-1.5*J-1) = -2.0 * DELD * DCM4KJ
AN(5*K.5*J) = -2.0 * DELD * DCM5KJ

C
IF (K .NE. KK) GO TO 225
IF (J .FU. KK) GO TO 235
225 IFDYN = 10
GO TO 249

C
MATRICES ARE COMPLETE - SAVE ON TP 13
C
C
C
235 IFDYN = 1
WRITE (13) AL
WRITE (13) AM
WRITE (13) AN
BACKSPACE 13
BACKSPACE 13
BACKSPACE 13
240 TP(FLAG .FO. -1.F+10) WRITE(6.250)
250 FORMAT (1H-, 9HLEFT L*NO. )
RETURN
END

```





```

00000390
00000392
00000394
00000396
00000399
00000400
00000401
00000402
00000403
00000404
00000405
00000408
00000410
00000420
00000430
00000440
00000450
00000460
00000470
00000480
00000490
00000500
00000510
00000520
00000530
00000540
00000550
00000560
00000570
00000590
00000610
00000620
00000640
00000650
00000658
00000660
00000670
00000680
00000690
00000698
00000700
00000710

15 CONTINUE
20 IF (ICTR .EQ. 1) GO TO 22
   READ (4) TMP1, TMP2, TMP3, TMP4, TMP5
   GO TO 28
C
22 KORO = FLOAT(K-1) / RHO
   TMP1 = TFETP + GAM *(TFETK - TTHTK)
   TMP2 = TTHTK * KORO
   TMP3 = WFE * TFETK + WTH * TTHTK
   TMP4 = LAM2 *(MFETP + GAM *(MFETK - MTHTK) )
   TMP5 = KORO * LAM2 * MTHTK
   WRITE (4) TMP1, TMP2, TMP3, TMP4, TMP5
C
C
C
   PE MATRIX
28 PE(5*K-4) = - PFEK + TMP1
   PE(5*K-3) = - PTHK - TMP2
   PE(5*K-2) = - PNK - TMP3
   PE(5*K-1) = TMP4
   PE(5*K) = - TMP5
30 IF (K .NE. KK) GO TO 35
   IF (J .EQ. KK) GO TO 40
35 IFMX = 10
   GO TO 519
C
40 DO 50 KN = 1, KK5
   PE(KN) = 2. * DEL * DELT * PE(KN)
50 CONTINUE
C
   IF (ICTR .GT. 1) .AND. MM .EQ. 2) GO TO 70
   IF (ICTR .GT. 1) GO TO 60
   DO 55 KN = 1, 150
   COND1(KN) = 0.0
   WRITE ( 8) ZP, ZPP, ZPPP
   GO TO 85
C
60 IF (KZTR .EQ. 8) GO TO 66
   BACKSPACE 11
   BACKSPACE 11
   GO TO 80
C
66 BACKSPACE 8
   BACKSPACE 8

```

```

C      GO TO 80
70 AF = FILE (KZTR, 1)
   IF (KZTR.EQ. 8) GO TO 76
   BACKSPACF = 11
   GO TO 80
C
76 BACKSPACE 8
C
80 READ (KZTR) ZP, ZPP, ZPPP
C
85 DELT2 = DELT * DELT
   IF (TCTR - 2.0) 90, 217, 215
90 DO 95 K = 1, KK5
   EMM3(K) = 2. * ZP(K)
   EMM4(K) = DELT2 * ZPP(K)
   ZPP(K) = EMM3(K) + EMM4(K)
   EMM4(K) = 6. * EMM4(K)
   ZPPP(K) = 6. * DELT * ZPPP(K)
   EMM3(K) = 9. * ZP(K)
   ZPPP(K) = EMM4(K) + ZPPP(K) + EMM3(K)
95 CONTINUE
C
150 READ (13) AL
   CALL MMY (KK5, F.5, 1, AL, ZP, EMM3)
C
   READ (13) EMM2
   CALL MMY (KK5, KK5, 1, EMM2, ZPP, EMM4)
   CALL MAD (KK5, 1, EMM4, EMM3, EMM3)
C
DO 170 K = 1, KK5
DO 170 J = 1, KK5
EMM2(K, J) = U.33333333 * EMM2(K, J)
AL(K, J) = AL(K, J) / 6.
170 CONTINUE
   CALL MAD (KK5, KK5, AL, EMM2, AL)
C
180 READ (13) EMM2
   CALL MMY (KK5, KK5, 1, EMM2, ZPPP, EMM4)
DO 190 K = 1, KK5
EMM3(K) = EMM3(K) + EMM4(K)
PE(K) = PE(K) + EMM3(K)

```

READ L MATRIX

READ M MATRIX

READ N MATRIX

```

00000720
00000728
00000730
00000740
00000750
00000760
00000768
00000770
00000778
00000780
00000790
00000810
00000820
00000830
00000840
00000850
00000860
00000870
00000880
00000890
00000900
00000910
00000920
00000928
00000930
00000940
00000948
00000950
00000960
00000970
00000980
00000990
00010000
00001010
00001020
00001030
00001040
00001048
00001050
00001060
00001070
00001080
00001090

```

```

C 190 CONTINUE
C 208 BACKSPACE 17
209 DO 210 K = 1, KK5
DO 210 J = 1, KK5
210 EMM2(K,J) = 3.5 * EMM2(K,J)
CALL MSU (KK5, KK5, EMM2, AL, AL)
GO TO 225
C
C 212 DO 213 K = 1, KK5
ZPPP(K) = DELT2 * ZPPP(K)
EMM3(K) = 2. * ZPP(K)
ZP(K) = 8. * ZP(K)
ZPPP(K) = ZPPP(K) + EMM3(K) + ZP(K)
ZPP(K) = ZPP(K) + ZP(K) / 3.0
ZP(K) = ZP(K) / 6.0
213 CONTINUE
C
215 READ ( 9) AL
CALL MMY (KK5, KK5, 1, AL, ZP, EMM3)
READ ( 9) EMM2
CALL MMY (KK5, KK5, 1, EMM2, ZPP, EMM4)
CALL MAD (KK5, 1, EMM4, EMM3, EMM3)
READ ( 9) EMM2
CALL MMY (KK5, KK5, 1, EMM2, ZPPP, EMM4)
DO 220 K = 1, KK5
EMM3(K) = EMM3(K) + EMM4(K)
PE(K) = PE(K) + EMM3(K)
220 CONTINUE
C
C G DBLSTAR HAS BEEN GENERATED AND STORED IN PE
C
C 225 IF (ICTR .LE. 2.0) GO TO 230
READ (13) A, B, C
GO TO 250
C
230 READ (12) A, B, C
C COMPUTE B**
C IF (ICTR .GT. 1.0) GO TO 250
CALL MAD (KK5, KK5, B, AL, B)
C

```

```

00001160
00001108
00001110
00001120
00001130
00001140
00001150
00001160
00001170
00001180
00001190
00001200
00001210
00001230
00001240
00001250
00001260
00001270
00001280
00001290
00001300
00001310
00001320
00001330
00001340
00001350
00001360
00001370
00001380
00001390
00001400
00001410
00001420
00001430
00001440
00001450
00001460
00001468
00001470
00001488
00001490
00001500
00001510

```

```

C 250 IF (MM .NE. 2) GO TO 400
C
C STATION NO. 2 - TOP BOUNDARY
IF (TCR - 2.0) 265,260,300
BACKSPACE 3
READ (3) EMM4
BACKSPACE 3
BACKSPACE 3
READ (3) AL
BACKSPACE 3
BACKSPACE 3
C
CALL MMY (KK5, KK5, AL, C, EMM2)
CALL MMY (KK5, KK5, KK5, EMM2, A, AL)
C
READ (3) P
BACKSPACE 3
BACKSPACE 3
CALL MSU (KK5, KK5, P, AL, AL)
CALL MMY (KK5, KK5, KK5, EMM2, B, P)
C
READ (3) B
CALL MSU (KK5, KK5, B, P, B)
CALL MMY (KK5, KK5, 1, EMM2, PE, EMM3)
CALL MSU (KK5, 1, EMM4, EMM3, EMM4)
CALL INVNM (B, 50, KK5, IERR)
IF (IERR .LE. 0) GO TO 320
C
C INVERSE REPLACES B ON TAPE
WRITE (13) A, B, C
C
CALL MMY (KK5, KK5, KK5, B, AL, P)
CALL MMY (KK5, KK5, 1, B, EMM4, X)
GO TO 500
C
C 265 READ (11) EMM4
BACKSPACE 11
BACKSPACE 11
READ GO
C
C READ (11) AL
BACKSPACE 11
BACKSPACE 11
READ CO
C

```

```

00001528
00001530
00001540
00001548
00001550
00001560
00001570
00001580
00001590
00001600
00001610
00001620
00001630
00001640
00001650
00001660
00001668
00001670
00001680
00001690
00001700
00001710
00001720
00001730
00001740
00001750
00001760
00001770
00001780
00001798
00001800
00001810
00001820
00001830
00001840
00001850
00001858
00001860
00001870
00001880
00001888
00001890

```

```

*BACKSPACE 3 WHEN NOT USING ALTRID
**265 BACKSPACE 11 - REMOVE STATEMENT NO. 265 FROM CARD 1860

```

```

BACKSPACE 11
BACKSPACE 11
CALL MMY (KK5, KK5, KK5, AL, C, EMM2)
CALL MMY (KK5, KK5, KK5, EMM2, A, C)

C
READ (11) AL
BACKSPACE 11
BACKSPACE 11
CALL MSU (KK5, KK5, AL, C, A)
CALL MMY (KK5, KK5, KK5, EMM2, B, C)

C
READ (11) AL
270 CALL MSU (KK5, KK5, AL, C, AL)
CALL MMY (KK5, KK5, 1, EMM2, PE, EMM3)
CALL MSU (KK5, 1, EMM4, EMM3, EMM4)
CALL INVNM (AL, 50, KK5, IERR)
IF (IERR .LE. 0) GO TO 320
275 CALL MMY (KK5, KK5, KK5, AL, A, P)
CALL MMY (KK5, KK5, 1, AL, EMM4, X)
GO TO 500

C
300 READ (KPTR) MM, P, X
C
AF = FILE (3,2)
BACKSPACE 3
READ ( 3) EMM4
BACKSPACE 3
BACKSPACE 3
READ ( 3) AL
BACKSPACE 3
BACKSPACE 3

C
CALL MMY (KK5, KK5, KK5, AL, C, EMM2)
CALL MMY (KK5, KK5, 1, EMM2, PE, EMM3)
CALL MSU (KK5, 1, EMM4, EMM3, EMM4)
CALL MMY (KK5, KK5, 1, B, EMM4, X)
GO TO 500

C
400 IF (TCTR .GT. 2.0) GO TO 450
CALL MMY (KK5, KK5, KK5, C, P, EMM2)
CALL MSU (KK5, KK5, B, EMM2, B)

C
C
C
* * COMPUTE P AND X **
00001900
00001910
00001920
00001930
00001938
00001940
00001950
00001960
00001970
00001980
00001988
00001990
00002000
00002010
00002020
00002030
00002040
00002050
00002060
00002070
00002080
00002090
00002098
00002100*
00002110
00002120
00002130
00002140
00002150
00002160
00002170
00002180
00002190
00002210
00002220
00002240
00002250
00002260
00002270
00002280
00002290
00002300
00002310

```

\*BACKSPACE 3 WHEN NOT USING ALRTIØ

```

C      CALL INVNM (B, 50, KK5, IERR)
      IF (IERR .LE. 0) GO TO 320
      IF (ICTR .EQ. 1.0) GO TO 450
      WRITE (13) A, B, C
450    CALL MMY(KK5, KK5, 1, C, X, EMM3)
      IF (ICTR .LE. 2.0) GO TO 460
      READ (KPTR) MM, P, X
460    CALL MSU (KK5, 1, PE, EMM3, PE)
      CALL MMY (KK5, KK5, 1, B, PE, X)
C
C      IF (ICTR .GT. 2.0) GO TO 480
      CALL MMY (KK5, KK5, B, A, P)
C
480    IF (MM .NE. N-2) GO TO 500
      IF (ICTR .GT. 1.0) GO TO 500
      WRITE (11) P, X
      GO TO 510
C
500    IF (MM .NE. 2) GO TO 510
      IF (ICTR .GT. 1.0) GO TO 504
      AF = FILE(11,1)
      READ (11) A, B, C
      BACKSPACE 11
      WRITE (11) A, B, C, PE
      END FILE 11
      GO TO 510
C
504    AF = FILE (3,1)
      READ ( 3) A, B, C, EMM3
      READ ( 3) A, B, C, EMM3
      BACKSPACE 3
      WRITE ( 3) A, B, C, PE
C
510    IF (ICTR .GT. 2.0) GO TO 514
      WRITE (10) MM, P, X
      GO TO 515
C
514    WRITE (KPTN) MM, P, X
      IF (MM .EQ. N-1) GO TO 540
515    IFMX = 1
519    IF (PFLAG .EQ. -1.E+10) WRITE(16,520)
520    FORMAT (1H-10HLEFT GOYD. )

```

```

00002320
00002330
00002340
00002350
00002360
00002370
00002380
00002390
00002400
00002410
00002420
00002430
00002440
00002450
00002460
00002470
00002480
00002490
00002498
00002500
00002510
00002520
00002530
00002540
00002550
00002560
00002570
00002578
00002580
00002590
00002600
00002610
00002620
00002628
00002630
00002640
00002650
00002652
00002660
00002670
00002680
00002690
00002700

```

00002715  
00002716  
00002720  
00002730  
00002740  
00002750  
00002759  
00002760  
00002770  
00002780  
00002789  
00002790  
00002800  
00002805  
00002806  
00002820  
00002830

```
C      RETURN  
C      540 IF (KPTM .EQ. 12) GO TO 550  
C      BACKSPACE 10  
C      BACKSPACE 10  
C      GO TO 515  
C      550 BACKSPACE 12  
C      BACKSPACE 12  
C      GO TO 515  
C      320 WRITE (6,325) MM  
C      325 FORMAT (1M,9X,16HSINGULAR MATRIX,9X,4HMM= ,14)  
C      CALL EXIT  
C      STOP  
C      END
```





```

10  KX5 - 5 * X51
C
DO 100 NN = 1, N
NN = N - NN + 1
C
IF (NN .NE. 1) GO TO 20
C
11  (ICTR .GT. 20) GO TO 12
C
READ (10) I, PX, XX
GO TO 13
C
12  READ (KPI) I, PX, XX
C
13  IF (ICTR .GT. 1) GO TO 14
READ (10) A11, B11, C11, G11
GO TO 16
C
14  READ (3) A11, B11, C11, G11
AF = FILE (A,1)
C
16  CALL NMMY (KK5, KK5, KK5, A11, B11, FM2)
CALL NMSU (KK5, KK5, EMM2, B11, B11)
CALL NMMY (KK5, KK5, 1, A11, G1, FMM3)
CALL NMSU (KK5, 1, G11, EMM3, G11)
CALL NMMY (KK5, KK5, 1, B11, XX, EMM3)
CALL NMSU (KK5, 1, G11, EMM3, G11)
CALL NMSU (KK5, KK5, KX5, B11, PX, EMM2)
CALL NMSU (KK5, PX5, C11, FM2, C11)
CALL NMMY (CC11, 5, KK5, IFRR)
IF (IFRR .LE. 0) GO TO 120
CALL NMMY (KK5, KK5, 1, CC11, G11, ZX)
C
WRITE (3) NN, ZX
C
WRITE (6,130) NN, (ZX(KP), KP=1, KK5)
GO TO 100
C
20  IF (NN .EQ. N) GO TO 40
IF (ICTR .GT. 20) GO TO 22
IF (ICTR .EQ. 20 .AND. NN .EQ. 2) GO TO 21
BACKSPACE 10
BACKSPACE 10
21

```

LAST STATION

00000493  
00000494  
00000495  
00000496  
00000497  
00000498  
00000499  
00000500  
00000501  
00000502  
00000503  
00000504  
00000505  
00000506  
00000507  
00000508  
00000509  
00000510  
00000511  
00000512  
00000513  
00000514  
00000515  
00000516  
00000517  
00000518  
00000519  
00000520  
00000521  
00000522  
00000523  
00000524  
00000525  
00000526  
00000527  
00000528  
00000529  
00000530  
00000531  
00000532  
00000533  
00000534  
00000535  
00000536  
00000537  
00000538  
00000539  
00000540  
00000541  
00000542  
00000543  
00000544  
00000545  
00000546  
00000547  
00000548  
00000549  
00000550  
00000551  
00000552  
00000553  
00000554  
00000555  
00000556  
00000557  
00000558  
00000559  
00000560  
00000561  
00000562  
00000563  
00000564  
00000565  
00000566  
00000567  
00000568  
00000569  
00000570  
00000571  
00000572  
00000573

C	READ (10) 1, PX, XX	00000748
C		00000749
C	GO TO 25	00000750
C		00000751
C	22 IF (KPTW * 10 * 10) GO TO 23	00000752
C	IF (INN * NF * 2) BACKSPACE 12	00000753
C	BACKSPACE 12	00000754
C	GO TO 24	00000755
C		00000756
C	23 IF (INN * NF * 2) BACKSPACE 10	00000757
C	BACKSPACE 10	00000758
C	24 READ (KPTW) 1, PX, XX	00000759
C	25 READ (K2IR) ZP, ZPP, ZPPP	00000760
C		00000761
C	IF (ICTO * NF * 10) GO TO 27	00000762
C	IF (K2IR * FO * 8) GO TO 26	00000763
C	BACKSPACE 11	00000764
C	BACKSPACE 11	00000765
C	GO TO 27	00000766
C		00000767
C	26 BACKSPACE 8	00000768
C	BACKSPACE 8	00000769
C	27 CALL MMSU (KK5, KK5, 1, PX, ZY, Z)	00000770
C	CALL MMSU (KK5, 1, XX, Z, Z)	00000771
C		00000772
C	IF (INN * NF * N-2) GO TO 30	00000773
C	DO 28 K = 1, KK5	00000774
C	28 ZX(K) = Z(K)	00000775
C		00000776
C	30 DO 35 K = 1, KK5	00000777
C	35 ZX(K) = Z(K)	00000778
C		00000779
C	WRITE (K2TW) ZX, ZP, ZPP	00000780
C		00000781
C	WRITE (3) MN, ZX	00000782
C	WRITE (6, 14) MN, (ZX(TX), TX=1, KK5)	00000783
C		00000784
C	GO TO 100	00000785
C		00000786
C	40 END FILE 3	00000787
C	REWIND 3	00000788

FIRST STATION

```

AF = FILE (3,2)
READ ( 3) AA11, BB11, CC11, GG11
C
READ ( 3) AA11, BB11, CC11, GG11
AF = FILE (3,2)
C
CALL MMY(KK5, KK5, 1, RR1), ZX, PY)
CALL MMY(KK5, KK5, 1, AA11, ZX, ZX)
CALL MMSU(KK5, 1, GG11, ZX, GG11)
CALL MMSU(KK5, 1, GG11, PX, GG11)
CALL MMY(KK5, KK5, 1, CC11, GG11, )
C
WRITE (6, 14) MN, (Z(IK), IK=1, KK5)
C
WRITE ( 3) MN, Z
100 CONTINUE
C
C
DO 102 I = 1, 10
W(I) = 0.0
C
REWIND 3
REWIND KZIR
REWIND KZTW
DELT2 = DELT * DELT
C
DO 108 I = 1, N
IF (1.0 - FG, 1.0 - OR, 1.0 - FQ, N) GO TO 108
C
READ (KZTW) ZP, ZPP, ZPPP
C
DO 104 NF = 1, NNF
NT = (NF - 1) * 5
NW = NT + 3
IF (1.0 - TR * NF, 1.0) GO TO 103
DO = ZPP(NW)
ZM1 = ZPPP(NW) * DELT2 + 2.0 * ZPP(NW) - ZP(NW)
W(NF) = (3.0 * ZP(NW) - 4.0 * DO + 2.0 * W1) / (2.0 * DELT)
GO TO 104
103 W(NF) = (3.0 * ZP(NW) - 4.0 * ZPP(NW) + ZPPP(NW)) / (2.0 * DELT)
104 CONTINUE
C
106 WRITE (KZTR) W

```

0000119

0000120

0000121

0000122

0000123

0000124

0000125

0000126

0000127

0000128

0000129

0000130

0000131

0000132

0000133

0000134

0000135

0000136

0000137

0000138

0000139

0000140

0000141

0000142

0000143

0000144

0000145

0000146

0000147

0000148

0000149

0000150

COMPUTE VELOCITIES

ZJ IN FILE BY ITSELF

```

C FOR CONTINUF 00001638
C 00001660
C 00001668
C 00001670
C 00001678
C 00001680
C 00001690
C 00001500
C 00001510
C 00001520
C 00001530
C 00001532
C 00001533
C 00001538
C 00001540
C 00001548
C 00001550
C 00001560
C 00001562
C 00001570
C 00001580
C 00001590
C 00001595
C 00001600
C 00001610
C 00001615

```

END FILE KZTW  
 S1 = KZTR  
 KZTR = KZTW  
 KZTW = S1  
 S1 = KPTR  
 KPTR = KPTW  
 KPTW = S1  
 IF(PFLAG.EQ.-1.F+10) WRITE(6,109)  
 109 FORMAT (1H-' SOLUTION ')  
 110 RETURN  
 120 WRITE (6,125)  
 CALL EXIT  
 STOP  
 125 FORMAT (1H-'SINGULAR MATRIX IN 'Z', 10X,45HERROR - INVERSION OF SINGULAR MATRIX IN 'Z', 10X,45HERROR - INVERSION OF SINGULAR MATRIX FOR STATION , 14// (12X,1P5E17.7))  
 140 FORMAT (/// 10X,24H'Z' MATRIX FOR STATION , 14// (12X,1P5E17.7))  
 140 FORMAT (/// 10X,24H'Z' MATRIX FOR STATION , 14// (12X,1P5E17.7))  
 END

3. 121 SUMS Subroutine (SUMD)

SIBFTC SUMD SOLUTION SUMMATION W/O STRESSES \*\*

C C

C SURROUTINE Sums

C Nomenclature

C THT HORIZONTAL ANGLES (DEGREES) 5 MAXIMUM

C FPRINT FOURIER COMPONENT PRINT VALUES OF DEFLECTIONS AND

C ROTATIONS (3 POSSIBLE)

C DIMENSION Z(50), THT( 6), FPRINT( 3)

C DIMENSION ULZ(100,5), VLZ(100,5), WLZ(100,5), PHS LZ(100,5),

1 PHTLZ(100,5), UL(100,5), VL(100,5), WL(100,5),

2 PHS L(100,5), PHTL(100,5), WFEX(100), WTHX(100),

3 GAMA(100), RHOX(100), WFEPX(100)

C DIMENSION B1(100,5), B2(100,5), B3(100,5), D1(100,5), D2(100,5),

1 D3(100,5), G1(100,5), G2(100,5), G3(100,5), G13(100,5), 000 0151

2 ENTSl(100,5), ENTTH(100,5), EMTSI(100,5), EMTTH(100,5)

C DIMENSION ENFE( 5), ENTH( 5), ENFT( 5), QFE( 5), EMFE( 5),

1 ENTH( 5), EMFT( 5), QTH( 5)

C DIMENSION COEFC(2200)

C DIMENSION SCB1(100), SCB2(100), SCB3(100), SCG1(100), SCG2(100),

1 SCG3(100), SCD1(100), SCD2(100), SCD3(100), SCG13(100),

2 SCNTSI(100), SCNTTH(100), SCMTS1(100), SCMTTH(100), DCM1(100),

3 DCM4(100), DCC1(100), DCC2(100), DCC3(100), DCK1(100), DCK2(100),

4 DCK3(100)

C EQUIVALENCE (COEFC( 1), SCB1), (COEFC(101), SCB2),

1 (COEFC( 20), SCB3), (COEFC( 30), SCG1), (COEFC(301),

2 (COEFC( 40), SCG2), (COEFC( 50), SCG3), (COEFC(501),

3 (COEFC( 60), SCD1), (COEFC( 70), SCD2),

4 (COEFC( 80), SCD3), (COEFC(110), SCNTTH), (COEFC(1101),

5 (COEFC( 90), SCG13), (COEFC(1301), SCNTSI), (COEFC(1301), SCNTTH),

6 (COEFC(1201), SCMTS1), (COEFC(1301), SCMTTH), (COEFC(1401), DCM1),

7 (COEFC(1501), DCM4), (COEFC(1601), DCC1), (COEFC(1701), DCC2),

8 (COEFC(1801), DCC3), (COEFC(1901), DCK1), (COEFC(2001), DCK2),

9 (COEFC(2101), DCK3)

C EQUIVALENCE (GDA( 1), A0), (GDA( 2), M0),

1 (GDA( 3), E0), (GDA( 4), SIG0),

```

2      (GDA( 5), POI),
3      (GDA( 7), BCIT),
4      (GDA( 9), PFLAG),
5      (GDA(11), DELT),
6      (GDA(18), FPRNT)
C
COMMON GDA(25), DEL, N, MNF, NTH,
1 BMTX(160), TCTR, KZTR, KZTR, KPTR, KPTR
C
REWIND 9
C
AF = FILE (3,3)
SS1 = SIGO/EO
SS2 = SS1 * A0
C
DO 200 I = 1,N
IF(I .EQ. 1) WRITE( 6,246)
II = N - I + 1
IF (II .EQ. N) AF = FILE (3,1)
C
READ ( 3) MN, Z
C
WRITE (6,290) II
C
DO 35 IT = 1,5
BI(II,IT) = 0.0
DI(II,IT) = 0.0
EMTSI(II,IT) = 0.0
EMTSII(II,IT) = 0.0
VLZ(II,IT) = 0.0
VLZI(II,IT) = 0.0
WLSZ(II,IT) = 0.0
WLSZI(II,IT) = 0.0
35 ATLSZ(II,IT) = 0.0
C
IT = 1
50 U = 0.0
V = 0.0
W = 0.0
PMS = 0.0
PMT = 0.0
IX = 1
THETA = TMT(IT)
00000420
00000430
00000431
00000432
00000433
00000510
00000520
00000521
00000530
00000540
00000600
00000610
00000620
00000630
00000639
00000640
00000645
00000650
00000655
00000660
00000670
00000679
00000690
00000700
00000710
00000720
00000722
00000724
00000726
00000730
00000740
00000750
00000760
00000770
00000780
00000790
00000800
00000810
00000820
00000830
00000840
00000850
00000860

```

00000870  
00000880  
00000890  
00000900  
00000910  
00000920  
00000930  
00000940  
00000950  
00000960  
00000970  
00000980  
00000990  
00001000  
00001010  
00001020  
00001030  
00001040  
00001050  
00001060  
00001070  
00001080  
00001089  
00001090  
00001100  
00001110  
00001120  
00001130  
00001140  
00001150  
00001160  
00001170  
00001180  
00001190  
00001200  
00001210  
00001229  
00001230  
00001240  
00001250  
00001260  
00001270  
00001280

```
C      DO 150 NF = 1, NNF  
      ANF = NF - 1  
      NT = (NF - 1) * 5  
      NU = NT + 1  
      NV = NT + 2  
      NW = NU + 2  
      NFS = NV + 2  
      NFT = NW + 2  
      FCT = COSD (ANF * THETA)  
      FCT2 = FCT * SS2  
      FCT1 = FCT * SS1  
      FCT3 = SIND (ANF * THETA)  
      FCT4 = SS2 * FCT3  
      FCT5 = SS1 * FCT3  
C      U = U + Z(NU) * FCT2  
      V = V + Z(NV) * FCT4  
      W = W + Z(NW) * FCT2  
      PHS = PHS + Z(NFS) * FCT1  
      PHT = PHT + Z(NFT) * FCT5  
C      UHZ(I,IT) = UHZ(I,IT) - Z(NU) * FCT4 * ANF  
      VLZ(I,IT) = VLZ(I,IT) + Z(NV) * FCT2 * ANF  
      WLZ(I,IT) = WLZ(I,IT) - Z(NW) * FCT4 * ANF  
      PHSLZ(I,IT) = PHSLZ(I,IT) - Z(NFS) * FCT5 * ANF  
      PHTLZ(I,IT) = PHTLZ(I,IT) + Z(NFT) * FCT1 * ANF  
C      BNF = ANF + 1  
      IF (BNF .NE. FPRNT(IX)) GO TO 150  
C      WRITE (6,300) THETA, ANF, U, V, W, PHS, PHT  
      IX = IX + 1  
      150 CONTINUE  
C      U(I,IT) = U  
      VL(I,IT) = V  
      WL(I,IT) = W  
      PHS(I,IT) = PHS  
      PHTL(I,IT) = PHT  
C      DISPLACEMENTS
```



```

IF (THT(I1+1) .LT. 0.0) GO TO 200
I1 = I1 + 1
GO TO 50
200 CONTINUE

```

C

```

REMIIND 3
I11 = I1
S1 = E0 * H0
S2 = S1 * H0 * H0
S3 = (1. - POI)/2.
S4 = SIGO * H0
S5 = A0 / (S4 * H0 **2)
I1 = 0
NF2 = 2 * NNF

```

C

```

210 READ ( 9) LN, IN, COEFC
LLN = LN - IN + 1
DO 240 I = 1,LLN
  I1 = I1 + 1
  K1 = NF2 * (I-1)

```

C

```

DO 230 IT = 1,I11
  THETA = THT(IT)
  DO 225 NF = 1,NF2
    ANF = NF - 1
    K2 = K1 + NF
    B1(I1,IT) = B1(I1,IT) + SCB1(K2) * COSD(ANF * THETA) * S1
    D1(I1,IT) = D1(I1,IT) + SCD1(K2) * COSD(ANF * THETA) * S2
    EMTSI(I1,IT) = EMTSI(I1,IT) + SCNTSI(K2) * COSD(ANF * THETA) * S4
    EMTSI(I1,IT) = EMTSI(I1,IT) + SCMTSI(K2) * COSD(ANF * THETA) * S5
  225 CONTINUE

```

225

```

  B11 = B1(I1,IT)
  D11 = D1(I1,IT)
  B2(I1,IT) = B11
  B3(I1,IT) = POI * B11
  D2(I1,IT) = D11
  D3(I1,IT) = POI * D11
  G1(I1,IT) = S3 * B11
  G2(I1,IT) = S3 * B11
  G3(I1,IT) = B11 * S3
  G13(I1,IT) = S3 * D11
  ENTTH(I1,IT) = EMTSI(I1,IT)
  EMTTH(I1,IT) = EMTSI(I1,IT)

```

```

00001290
00001300
00001310
00001320
00001330
00001340
00001350
00001360
00001370
00001380
00001383
00001386
00001390
00001400
00001410
00001420
00001430
00001440
00001450
00001460
00001470
00001480
00001490
00001500
00001510
00001520
00001530
00001540
00001543
00001546
00001550
00001560
00001570
00001580
00001590
00001630
00001640
00001650
00001660
00001670
00001690
00001710
00001730

```

00001758  
00001759  
00001760  
00001761  
00001762  
00001763  
00001764  
00001765  
00001766  
00001767  
00001768  
00001769  
00001770  
00001771  
00001772  
00001773  
00001774  
00001775  
00001776  
00001777  
00001778  
00001779  
00001780  
00001781  
00001782  
00001783  
00001784  
00001785  
00001786  
00001787  
00001788  
00001789  
00001790  
00001791  
00001792  
00001793  
00001794  
00001795  
00001796  
00001797  
00001798  
00001799  
00001800  
00001801  
00001802  
00001803  
00001804  
00001805  
00001806  
00001807  
00001808  
00001809  
00001810  
00001811  
00001812  
00001813  
00001814  
00001815  
00001816  
00001817  
00001818  
00001819  
00001820  
00001821  
00001822  
00001823  
00001824  
00001825  
00001826  
00001827  
00001828  
00001829  
00001830  
00001831  
00001832  
00001833  
00001834  
00001835  
00001836  
00001837  
00001838  
00001839  
00001840  
00001841  
00001842  
00001843  
00001844  
00001845  
00001846  
00001847  
00001848  
00001849  
00001850  
00001851  
00001852  
00001853  
00001854  
00001855  
00001856  
00001857  
00001858  
00001859  
00001860  
00001861  
00001862  
00001863  
00001864  
00001865  
00001866  
00001867  
00001868  
00001869  
00001870  
00001871  
00001872  
00001873  
00001874  
00001875  
00001876  
00001877  
00001878  
00001879  
00001880  
00001881  
00001882  
00001883  
00001884  
00001885  
00001886  
00001887  
00001888  
00001889  
00001890  
00001891  
00001892  
00001893  
00001894  
00001895  
00001896  
00001897  
00001898  
00001899  
00001900  
00001901  
00001902  
00001903  
00001904  
00001905  
00001906  
00001907  
00001908  
00001909  
00001910  
00001911  
00001912  
00001913  
00001914  
00001915  
00001916  
00001917  
00001918  
00001919  
00001920  
00001921  
00001922  
00001923  
00001924  
00001925  
00001926  
00001927  
00001928  
00001929  
00001930  
00001931  
00001932  
00001933  
00001934  
00001935  
00001936  
00001937  
00001938  
00001939  
00001940  
00001941  
00001942  
00001943  
00001944  
00001945  
00001946  
00001947  
00001948  
00001949  
00001950  
00001951  
00001952  
00001953  
00001954  
00001955  
00001956  
00001957  
00001958  
00001959  
00001960  
00001961  
00001962  
00001963  
00001964  
00001965  
00001966  
00001967  
00001968  
00001969  
00001970  
00001971  
00001972  
00001973  
00001974  
00001975  
00001976  
00001977  
00001978  
00001979  
00001980  
00001981  
00001982  
00001983  
00001984  
00001985  
00001986  
00001987  
00001988  
00001989  
00001990  
00001991  
00001992  
00001993  
00001994  
00001995  
00001996  
00001997  
00001998  
00001999  
00002000  
00002001  
00002002  
00002003  
00002004  
00002005  
00002006  
00002007  
00002008  
00002009  
00002010  
00002011  
00002012  
00002013  
00002014  
00002015  
00002016  
00002017  
00002018  
00002019  
00002020  
00002021  
00002022  
00002023  
00002024  
00002025  
00002026  
00002027  
00002028  
00002029  
00002030  
00002031  
00002032  
00002033  
00002034  
00002035  
00002036  
00002037  
00002038  
00002039  
00002040  
00002041  
00002042  
00002043  
00002044  
00002045  
00002046  
00002047  
00002048  
00002049  
00002050  
00002051  
00002052  
00002053  
00002054  
00002055  
00002056  
00002057  
00002058  
00002059  
00002060  
00002061  
00002062  
00002063  
00002064  
00002065  
00002066  
00002067  
00002068  
00002069  
00002070  
00002071  
00002072  
00002073  
00002074  
00002075  
00002076  
00002077  
00002078  
00002079  
00002080  
00002081  
00002082  
00002083  
00002084  
00002085  
00002086  
00002087  
00002088  
00002089  
00002090  
00002091  
00002092  
00002093  
00002094  
00002095  
00002096  
00002097  
00002098  
00002099  
00002100  
00002101  
00002102  
00002103  
00002104  
00002105  
00002106  
00002107  
00002108  
00002109  
00002110  
00002111  
00002112  
00002113  
00002114  
00002115  
00002116  
00002117  
00002118  
00002119  
00002120  
00002121  
00002122  
00002123  
00002124  
00002125  
00002126  
00002127  
00002128  
00002129  
00002130  
00002131  
00002132  
00002133  
00002134  
00002135  
00002136  
00002137  
00002138  
00002139  
00002140  
00002141  
00002142  
00002143  
00002144  
00002145  
00002146  
00002147  
00002148  
00002149  
00002150  
00002151  
00002152  
00002153  
00002154  
00002155  
00002156  
00002157  
00002158  
00002159  
00002160  
00002161  
00002162  
00002163  
00002164  
00002165  
00002166  
00002167  
00002168  
00002169  
00002170  
00002171  
00002172  
00002173  
00002174  
00002175  
00002176  
00002177  
00002178  
00002179  
00002180  
00002181  
00002182  
00002183  
00002184  
00002185  
00002186  
00002187  
00002188  
00002189  
00002190  
00002191  
00002192  
00002193  
00002194  
00002195  
00002196  
00002197  
00002198  
00002199  
00002200  
00002201  
00002202  
00002203  
00002204  
00002205  
00002206  
00002207  
00002208  
00002209  
00002210  
00002211  
00002212  
00002213  
00002214  
00002215  
00002216  
00002217  
00002218  
00002219  
00002220  
00002221  
00002222  
00002223  
00002224  
00002225  
00002226  
00002227  
00002228  
00002229  
00002230  
00002231  
00002232  
00002233  
00002234  
00002235  
00002236  
00002237  
00002238  
00002239  
00002240  
00002241  
00002242  
00002243  
00002244  
00002245  
00002246  
00002247  
00002248  
00002249  
00002250  
00002251  
00002252  
00002253  
00002254  
00002255  
00002256  
00002257  
00002258  
00002259  
00002260  
00002261  
00002262  
00002263  
00002264  
00002265  
00002266  
00002267  
00002268  
00002269  
00002270  
00002271  
00002272  
00002273  
00002274  
00002275  
00002276  
00002277  
00002278  
00002279  
00002280  
00002281  
00002282  
00002283  
00002284  
00002285  
00002286  
00002287  
00002288  
00002289  
00002290  
00002291  
00002292  
00002293  
00002294  
00002295  
00002296  
00002297  
00002298  
00002299  
00002300  
00002301  
00002302  
00002303  
00002304  
00002305  
00002306  
00002307  
00002308  
00002309  
00002310  
00002311  
00002312  
00002313  
00002314  
00002315  
00002316  
00002317  
00002318  
00002319  
00002320  
00002321  
00002322  
00002323  
00002324  
00002325  
00002326  
00002327  
00002328  
00002329  
00002330  
00002331  
00002332  
00002333  
00002334  
00002335  
00002336  
00002337  
00002338  
00002339  
00002340  
00002341  
00002342  
00002343  
00002344  
00002345  
00002346  
00002347  
00002348  
00002349  
00002350  
00002351  
00002352  
00002353  
00002354  
00002355  
00002356  
00002357  
00002358  
00002359  
00002360  
00002361  
00002362  
00002363  
00002364  
00002365  
00002366  
00002367  
00002368  
00002369  
00002370  
00002371  
00002372  
00002373  
00002374  
00002375  
00002376  
00002377  
00002378  
00002379  
00002380  
00002381  
00002382  
00002383  
00002384  
00002385  
00002386  
00002387  
00002388  
00002389  
00002390  
00002391  
00002392  
00002393  
00002394  
00002395  
00002396  
00002397  
00002398  
00002399  
00002400

```

.230 CONTINUE  

.240 CONTINUE  

      IF (LN.EQ.N) GO TO 245  

      GO TO 210  

C  

.245 READ ( 3 ) WTHX, WFEX, GAMA, RHOX, WFEPIX  

      DNM = -2. * DEL  

C  

      DO 275 I = 1,N  

      IF (I.EQ. 1) WRITE( 6,246)  

      246 FORMAT( 1H1 )  

      L = N - I + 1  

      H = L  

      WFE = WFE(X(L))  

      WTH = WTH(X(L))  

      GAMA = GAMA(L)  

      RHO = RHO(X(L))  

      DRHO = 0.  

      IF (RHO.NE. 0.) DRHO = 1. /RHO  

      DAO = 1./AO  

      DO 265 IT = 1,IT  

      THETA = THT(IT)  

C  

      IF (I.NE. 1) GO TO 250
```

```

      DERIVATIVES WITH RESPECT TO PSI  

      LAST STATION  

      ULP = (4. * UL(I+1,IT) - 3. * UL(I,IT) - UL(I+2,IT) ) / DNM  

      VLP = (4. * VL(I+1,IT) - 3. * VL(I,IT) - VL(I+2,IT) ) / DNM  

      WLP = (4. * WL(I+1,IT) - 3. * WL(I,IT) - WL(I+2,IT) ) / DNM  

      PHSLP = (4. * PHSL(I+1,IT) - 3. * PHSL(I,IT) - PHSL(I+2,IT) ) / DNM  

      PHTLP = (4. * PHTL(I+1,IT) - 3. * PHTL(I,IT) - PHTL(I+2,IT) ) / DNM  

      GO TO 260  

.250 IF (I.EQ.N) GO TO 255  

      (NOTE - 'I' IS COUNTING BACKWARDS)  

      ULP = (UL(I+1,IT) - UL(I-1,IT) ) / DNM  

      VLP = (VL(I+1,IT) - VL(I-1,IT) ) / DNM  

      WLP = (WL(I+1,IT) - WL(I-1,IT) ) / DNM  

      PHSLP = (PHSL(I+1,IT) - PHSL(I-1,IT) ) / DNM  

      PHTLP = (PHTL(I+1,IT) - PHTL(I-1,IT) ) / DNM  

      GO TO 260  

C  

      255 ULP = (UL(I-2,IT) + 3. * UL(I,IT) - 4. * UL(I-1,IT) ) / DNM  

      FIRST STATION  

      00002119  

      00002120
```

```

VLP = (VL(I-2,IT) + 3. * VL(I,IT) - 4. * VL(I-1,IT) ) /DNM
WLP = (WL(I-2,IT) + 3. * WL(I,IT) - 4. * WL(I-1,IT) ) /DNM
PHSLP = (PHSL(I-2,IT) + 3. * PHSL(I,IT) - 4. * PHSL(I-1,IT) ) /DNM
PHTLP = (PHTL(I-2,IT) + 3. * PHTL(I,IT) - 4. * PHTL(I-1,IT) ) /DNM
00002130
00002140
00002150
00002160
00002170
00002180
00002190
00002200
00002210
00002220
00002230
00002240
00002250
00002260
00002270
00002271
00002280
00002281
00002285
00002286
00002290
00002300
00002310
00002320
00002350
00002360
00002370
00002380
00002400
00002420
00002430
00002710
00002720
00002730
00002740
00002790
00002800
00002810
00002820
00002830
00002840
00002880
00002890

C
C
C
      COMPUTATION OF STRAINS ** (STR 139, PG.17) **
240  ESI = DAO * (ULP + WFE * WL(I,IT))
      ETH = DAO * (DRHO * VLZ(I,IT) + GAM * UL(I,IT) + WTH * WL(I,IT))
      ESTH = DAO/2. * (DRHO * ULZ(I,IT) + VLP - GAM * VL(I,IT) )
      GSI = PHSL(I,IT) - DAO * (WFE * UL(I,IT) - WLP )
      GTH = PHTL(I,IT) - DAO * (WTH * VL(I,IT) - DRHU * WLZ(I,IT) )
      EKSI = DAO * PHSLP
      EKTH = DAO * (DRHO * PHTL(I,IT) + GAM * PHSL(I,IT) )
      EKSTH = DAO/2. * (DRHO * PHSLZ(I,IT) + PHTLP - GAM * PHTL(I,IT) +
1  DAO/2. * (WFE-WTH)*(DRHO*ULZ(I,IT) - VLP-GAM*VL(I,IT)))
      IF(PFLAG.EQ.-10.) WRITE(6,261) L, THEIA, ESI, ETH, ESTH, GSI,
1      GTH, EKSI, EKTH, EKSTH
261  FORMAT(/// 1X, 34HCHECKPRINT OF STRAINS AT STATION ,I4, 5X,
1  7THETA ,1PE12.4// 8E13.4 )
C
C
      COMPUTATION OF INTERNAL FORCES ** (STR 139, PG.12) **
ENFE(IT) = B1(L,IT) * ESI + B3(L,IT) * ETH - ENTSI(L,IT)
ENTH(IT) = B3(L,IT) * ESI + B2(L,IT) * ETH - ENTTH(L,IT)
ENFT(IT) = G1(L,IT) * ESTH
QFE(IT) = G2(L,IT) * GSI
EMFE(IT) = D1(L,IT) * EKSI + D3(L,IT) * EKTH - EMTSI(L,IT)
EMTH(IT) = D3(L,IT) * EKSI + D2(L,IT) * EKTH - EMTTH(L,IT)
EMFT(IT) = G13(L,IT) * EKSTH
QTH(IT) = G3(L,IT) * GTH
265  CONTINUE
C
      WRITE (6,268) L, (ENFE(J), ENTH(J), ENFT(J), QFE(J), J = 1,III)
      WRITE (6,270) (EMFE(J), EMTH(J), EMFT(J), QTH(J), J = 1,III)
C
268  FORMAT (1H-//11X,9HSTATION ,I4// 19X, 5HM(XI),11X, 8HM(THETA), 7X,00002800
1  11HM(XI),THETA),10X, 5HQ(XI) / (12X, 1P4E17.7) )
C
270  FORMAT (1H-//18X, 5HM(XI),11X, 8HM(THETA), 7X,11HM(XI),THETA), 8X,
1  8HQ(THETA) / (12X, 1P4E17.7) )
C
275  CONTINUE

```

```

C      IF(IPFLAG .EQ. -.1.F+10) WRITE(6,280)
      280 FORMAT (1H-, 9MLEFT SUMS.)
      RETURN
      290 FORMAT (////10X, 9MSTATION ,I4)
      300 FORMAT (//// 10X, 9MTHETA = ,F7.2//11X, 9MENDF = ,F5.1//21X,1MU,00002930
      1 16X,1HV,16X,1HW,12X, 7MPhi(XI), 9X,10MPhi(THETA) / (12X,1P5E17.7))00002940
      00002950
      00002960
      END
C

```

\* MEMORY MAP \*

SYSTEM FILE BLOCK ORIGIN  
 FILES 1. UNIT06 0000 THRU 03765  
 2. UNIT01 03766  
 3. UNIT02  
 4. UNIT03  
 5. UNIT04  
 6. UNIT05  
 7. UNIT07  
 8. UNIT08  
 9. UNIT09  
 10. UNIT10  
 11. UNIT11  
 12. UNIT12  
 13. UNIT13  
 14. UNIT14  
 15. UNIT15  
 16. UNIT16

(NO BUFF POOL ATTACHED)  
 (NO BUFF POOL ATTACHED)  
 (NO BUFF POOL ATTACHED)  
 (NO BUFF POOL ATTACHED)  
 (NO BUFF POOL ATTACHED)  
 (NO BUFF POOL ATTACHED)  
 (NO BUFF POOL ATTACHED)  
 (NO BUFF POOL ATTACHED)  
 (NO BUFF POOL ATTACHED)  
 (NO BUFF POOL ATTACHED)  
 (NO BUFF POOL ATTACHED)  
 (NO BUFF POOL ATTACHED)  
 (NO BUFF POOL ATTACHED)  
 (NO BUFF POOL ATTACHED)  
 (NO BUFF POOL ATTACHED)  
 (NO BUFF POOL ATTACHED)  
 (NO BUFF POOL ATTACHED)

04266  
 04275  
 04302 THRU 76606  
 PRE-EXECUTION INITIALIZATION  
 CALL ON OBJECT PROGRAM  
 OBJECT PROGRAM

LINK	DECK	ORIGIN	CONTROL SECTIONS	(/NAME/=NON 0 LENGTH, (LOC)=DELETED, *=-NOT REFERENCED
0	EXEC	04302	/// (176706)	EVEN 04303 ..... 04577 *
	DECRD	04613	DECRD (04613)	
	NOFPT	04732	/FPSIGQ/ 04732	
	.FPTRP	04733	EVEN 04743	FP.DVR 05030 * FP.DIV 05041 *
			FP.UND 05002 *	/NOOVRQ/ 05121 *
			.FPOUT 05060 *	FP.LDC 05124 *
			/MOUNDQ/ 05122 *	/FPSIGQ/(04732)
			OVFLOW 05125 *	
			/.LOT / 05132	/.LVEC / 05174
	.LINK	05132	.LXSTR 05222	.LXOUT 05324 *
	.LXCON	05222	IDEXIT 05342 *	.LXCAL 05346
			.LXARG 05655 *	.LXERR 05336
				.OBCLS 05534 *
				.CLSE 05702 *
				/TDUMPC/ 05676 *

.LFBL	05703	.LUNB	05704 *	.DFOUT	05705	CTES..	05707 *
SC.SMT	05710	.OPNFO	05711 *	.CLSFO	05712	.WRTFU	05713 *
.REFDQ	05714 *	CNTL..	(05715	.LRECT	(05146)	.LVEC	(05174)
.LOVRY	(05720)	.LDF	(05132)	.LXTST	06476	.LXOVL	06544
.LXSEL	06472	.LXSCL	06473	.LXDIS	06722	.LXFLG	06723
.LXRCT	06555 *	.LXIND	06714				
.LTCM	06730	E.2	06751	F.3	06752	E.4	06753
.E.1	06750	CC.2	06755	CC.3	06756	CC..	06757
.XCC.	06754	.EXIT.	06760	.FXARG	07322 *	/OPTM./	07376 *
XIT	06760	.FXOUT	07314 *	/NOHSHQ/	07442 *	.FCNV.	07444
FXEM	06761	/HMDSQ /	07440 *	.FDX1	07471	.FDX2	07472
FCNV	07410	.CNVSW	07465	.DRC20	07660	.DDSW	07670
	07463	.DBC10	07632	.DDBC	07762	.DDRS1	10226 *
	07474	.FIXSW	07705	.D2	10235	.FERR2	10322 *
	07677	.DI	10233	.LNTP	10456	.ADUT	10525
	10230 *	.DNPT	10373	.DEXPN	10772	.FX0	10773
	10356	.FLT	10701	.LOUT	11327	.OOUT	11350
	10544	.INTG	11207	.KOUNT	12131	.LIST	12134
	11136	.TEST	12126	EVEN	12211	.BUF	12242
	11402	.OUTBF	12212	.GAIN	12245	.GAIN1	12246
	12145	.WIDTH	12244	.DDDFL	12303	.DDFLG	12304
	12243	EVEN	12267	.FEXP	123J7	.DIG	12310
	12256	.PEX	12306	.FBLT.	12527	.FBDT.	12547
	12305	.FCNT	12431	.FWLR.	12637	.FWLR.	(112637)
	12326	.FRLR.	(12573)				
F10B	12326	.FRITE	12771	.FRIN.	13611	.FBCK	14142
		.FBIP.	12677	.FSEL	14124		
F10H	12777	.FFIL.	13564				
F10S.	14007	.FIOC	14067	.FBCB	14572		
		.FICK	14144				
FR00.	14504	.FRDD	14253	.FBIW	15324		
FR0D.	14531	.FRDD	14504				
FBCD.	14557	.FRD	14531				
FR0B.	14622	.FBCD	14557				
FWRB.	14651	.FRDB	14622				
FBIW.	15322	.FWRB	14651				
FEFT.	15741	.FRID	15322				
		.FEFT	15741				

FBST.	15760	..FBST	15760
FRMT.	16042	..FRMT	16042
FVIO.	16070	..FVIO	16070
UNIT06	16157	..UN06	16157
UN01	16160	.UN01.	16160
UN02	16161	.UN02.	16161
UN03	16162	.UN03.	16162
UN04	16163	.UN04.	16163
UN05	16164	.UN05.	16164
UN07	16165	.UN07.	16165
UN08	16166	.UN08.	16166
UN09	16167	.UN09.	16167
UN10	16170	.UN10.	16170
UN11	16171	.UN11.	16171
UN12	16172	.UN12.	16172
UN13	16173	.UN13.	16173
UN14	16174	.UN14.	16174
UN15	16175	.UN15.	16175
UN16	16176	.UN16.	16176
FSCD	16177	COSD	16177
FSCN	16230	COS	16230
FSQR	16424	SQRT	16424
FSLD1	16477	.FSL1.	16515
FSLB1	16534	.FBL1.	16552
FSLI	16572	.SLI.	16572
FSLD0	16626	.FSL0.	16644
FSLB0	16663	.FBL0.	16701
FSL0	16721	.SLO.	16721
FILE.0	16755	FILE	16756
//	76706		

1	DLKDY	17117	///	/(176706)	DATLNK	17150
	DMTP	17164	EVFN	17165	DINTRP	17451
	CF3P	17510	EVEN	17511	CODIMA	20524
	ENTP	20652	EVEN	20653	ENTERP	21041
2	GMVD	21105	///	/(176706)	GEOM	27137

SIND	16201	.FSDI.	16523 *
SIN	16231	.FBDI.	16560 *
		.SLI1.	16577 *
		.FSD0.	16652 *
		.FBD0.	16707 *
		.SL02.	16727
		.SDI.	16605
		.SDI1.	16613
		.SD0.	16734
		.SD02.	16743

3.13 PROGRAM NOMENCLATURE

Ⓐ

A0	a	Reference length
A0 (50, 50)	$A_0$	Boundary matrix, see Equation (1.46), Section 1.8
A1 (50, 50)		Another designation for A0 (50, 50)
ALF1		ENTRY to function subprogram TMP1, used to define the coefficient of thermal expansion for the stress calculations of layer one
ALF2		As ALF1, for layer two
ALM0 (5, 5)	$\bar{A}_0$	Boundary displacement matrix at the first meridional station, Equation (1.36), 0th harmonic
ALM1 (5, 5)		As ALM0 (5, 5) for the 1st harmonic
ALMN (5, 5)	$\bar{A}_N$	As ALM0 (5, 5) for the terminal boundary
ANX		Angle between the generator and axis of revolution; cone-cylinder option of GEOM.
AXL		Axial surface length

Ⓑ

B**		Modified B matrix for dynamic response, Equation (1.56), Section 1.9
B0 (50, 50)	$B_0$	Boundary matrix; see Equation (1.40), Section 1.8
B1 (50, 50)		Same as B0 (50, 50)
BBB		FUNCTION subprogram to define membrane stiffness, Equation (1.28).



BCD (36)		Three title cards read in executive program
BCIB		Boundary condition indicator for the terminal boundary; entered with the general data, GDA. See Section 2.8.
BCIT		As BCIB, for the initial boundary
BFCN		Deck name for the static version of subprogram, BBB
BMTX (160)		COMMON array which includes $\Omega$ , $\Lambda$ and $l$ boundary matrices for the 0th and 1st harmonics
BN (50, 50)	$B_N$	Terminal boundary matrix; Equation (1.46), Section 1.8
BNDTB (17)		Special boundary array for station N read with the geometry data, GMDA. See Sections 1.8, 2.8.
BNDTX (17)		As BNDTB, for station one
©		
C0, C1 (50, 50)	$C_0$	Boundary matrices; see Equation (1.46), Section 1.8.
CEXT		Number of time cycles desired. Read with GDA data, Section 3.3.2.
CN (50, 50)	$C_N$	Terminal boundary matrix, Equation (1.46), Section 1.8.
CODIMA		Parabolic curve fitting subroutine, see Section 3.5.4.
COEFC		Stiffness coefficient array set up in the DATLYR subroutine.
ⓓ		
DATLD		Subroutine used to set up pressure loads

DATLNK		Sub-executive subroutine which monitors GEOM, DATLYR and DATLD
DATLYR		Subroutine which sets up the stiffness coefficient array, COEFC
DBBDD		Deck name for the Dynamics version of subprogram BB
DCC1, 2, 3	$D_m$	External damping coefficients found in the COEFC array
DCK1, 2, 3	$K_m$	Spring coefficients, in COEFC
DCM1, 4	$M_m$	Mass coefficients of translation and rotation, in COEFC
DDD		ENTRY to function subprogram BBB, used to define the bending stiffness coefficients of the COEFC array
DECRD		Data read subroutine; see Section 3.5.1
DEL	$\Delta$	Interval size between meridional stations
DELT	$\delta$	Time increment (seconds), read with GDA data. See Section 3.3.2.
DELTH		Interval size between circumferential stations. Constant = 2°.
DKDMP		Deck name for the Dynamics deck which sets up spring and damping coefficients of the array COEFC
DKK1, 2, 3		FUNCTION and ENTRY points to the subprogram which sets up spring coefficient
DMASS		Deck name for Dynamics deck which forms the mass coefficients
DMM1, 4		FUNCTION and ENTRY points of deck DMASS

DMP1, 2, 3		ENTRY points to deck DKDMP to set up the translational damping coefficients
DN1		ENTRY point to function subprogram, E11. Sets up distance from neutral axis of the first layer used in stress calculations.
DN2		As DN1 for the second stresses
DPRSS		Deck name for the Dynamics version of PPPN which supplies the pressure loadings
DTMP		Deck name for the Dynamics version of ENTT which gives the temperature load and moment
DYLMN		Subroutine subprogram in the Dynamics deck which sets up the L, M and N matrices of Equation (1.51), Section 1.9
Ⓔ		
E0	$E_0$	Reference Young's Modulus
E11, 2		FUNCTION subprograms used to define the moduli of elasticity for the two layers at which stresses are desired
EM		Number of radii entered for the discrete point geometry option
EMTT		ENTRY point to subprogram ENTT; used to set up temperature moments
EN		Number of meridional stations
ENF		Number of Fourier harmonics where the first one is the 0th one
ENTH		Number of circumferential stations, internally set at ninety

ENTT		FUNCTION subprogram which sets the value of the temperature load, $t_T$ . Equation (1.15), Section 1.6
Ⓔ		
F(50, 50)	F	Matrix of equilibrium Equation (1.34), Section 1.7
FGHPE		Subroutine which forms the F, G and H matrices of Equation (1.34). In the Statics version the force matrix PE is also set up here.
FPRNT		Fourier component print values, read with GDA data. See Section 3.3.2.
Ⓒ		
G (50, 50)	G	Matrix of equilibrium Equation (1.34), Section 1.7
G**	$g_{i,j}^*$	Modified g matrix for dynamic response, Equation (1.56), Section 1.9
GAMA	$\gamma$	$\rho'/\rho$
GDA		General data array, read by the executive program
GEOM		Geometry subroutine
GIN		Geometry indicator read with GMDA data; see Section 2.5
GMDA		The geometry data array; see Section 3.3.3
GMI		GIN
GMTX		Dynamics subroutine subprogram which modifies the B and g matrices and forms the P and X matrices of Equation (1.60), Section 1.10

H (50, 50)	H	Equilibrium matrix of Equation (1.34), Section 1.7
H0	$h_0$	Reference thickness
①		
I		Station number within each block of stiffness coefficients, COEFC, in PANDX subroutine
IFDYN		PANDX flag which determines when L, M and N matrices of the Dynamics routine have been completed
IFGFG		PANDX flag to determine entry into the FGHPPE subroutine
IFLG		Stiffness coefficient block indicator; used in PANDX
IFMX		PANDX flag which shows whether the PE (force) matrix is complete
IRSFG		PANDX flag for boundary computations
IRTE		PANDX indicator for first or last station within a coefficient block
②		
JPATH		Path indicator through the Fourier harmonic loop of PANDX; used to skip setting up the boundary conditions and the FGHPPE subroutine
③		
KFCN		Deck name for the Statics version of subprogram DKK1
KPATH		Path indicator through the Fourier harmonic loop of PANDX; used to skip boundary conditions and the DYLMN subroutine

KPTR, KPTW		Variable tape numbers 10 or 12 used in the Dynamics version for storing P and X matrices by subroutine GMTX
KZTR, KZTW		Variable tape number 8 or 11 used in GMTX for preserving the three previous solution matrices (Z) at each time interval
Ⓐ		
L (50, 50)	$L_i$	Matrix used in the Dynamics version to modify the g matrix, Equation (1.51), Section 1.9
LL0 (5)	$l_0$	Initial boundary, $l$ matrix; Equation (1.38), Section 1.7
LLN (5)	$l_N$	Terminal boundary, $l$ matrix
Ⓜ		
M (50, 50)	$M_i$	As L (50, 50)
M (THETA)	$M_\theta$	Bending moment per unit length in the circumferential direction
M (XI)	$M_\xi$	Bending moment per unit length in the meridional direction
M (XI, THETA)	$\bar{M}_{\xi\theta}$	Bending moment; shear
MFE		Current temperature moments at a given meridional station and for k harmonics
MM		Absolute station number in PANDX subroutine
MMN		Station number within block of loads in PANDX
MTP		First derivative of the temperature moments

Ⓐ

N		Fixed point form of EN, number of meridional stations
N (50, 50)	$N_i$	As L (50, 50)
N (THETA)	$N_\theta$	Membrane force, circumferential
N (XI)	$N_\xi$	Membrane force, meridional
N (XI, THETA)	$\bar{N}_{\xi\theta}$	Membrane shear force
NNF	n	Fixed point form of ENF, number of Fourier harmonics
NTH		Fixed point form of ENTH, number of circumferential stations = 90

ⓐ

ØMG0 (5, 5)	$\Omega_1$	Boundary force matrix for the 0th harmonic; Equation (1.36), Section 1.7
ØMG1 (5, 5)	$\Omega_2$	As ØMG0 (5, 5) for the 1st harmonic
ØMGN (5, 5)	$\Omega_3$	As ØMG0 (5, 5) for the terminal boundary

ⓑ

P (50, 50)	P	Matrix of Equation (1.60), Section 1.10
PANDX		Sub-executive subroutine which directs the formation of the various matrices needed in computing the P and X matrices of Equation (1.60), Section 1.10. This subroutine calls the RSLT, FGHPE, DYLMN and GMTX subroutines, the latter two in the Dynamics version only.
PF (50)	p	Force matrix of Equation (1.34), Section 1.7

PEL		Meridional distance to a station from the initial station
PFCN		Deck name for the Statics version of subroutine PPPN
PFE	$p_{\xi}$	Fourier component for load in the meridional direction
PFLAG		Print flag, read with GDA, general data. See Section 3.3.2.
PHI0	$\phi_0$	Initial opening angle from vertical axis for sphere or toroid
PHIN	$\phi_N$	Final opening angle from vertical axis for sphere or toroid
PHI (THETA)	$\phi_{\theta}$	Rotation in the circumferential direction
PHI (XI)	$\phi_{\xi}$	Rotation in the meridional direction
PHS		Program name for PHI (XI)
PHT		Program name for PHI (THETA)
PN	$p_{\zeta}$	Fourier component for load in the normal direction
P0I		Poisson's ratio
P0IS1		ENTRY point to function subprogram, E11. Sets up Poisson's ratio for use in the stress calculations for the first layer.
P0IS2		As P0IS1 for the second stresses
PPPF		ENTRY point to function subprogram, PPPN. Defines the meridional pressure.
PPPH		As PPPF for circumferential pressure



PPPN		FUNCTION subprogram for pressure loadings. See Section 1.5 for sign convention.
PTH	$P_{\theta}$	Fourier component for load in the circumferential direction
Ⓞ		
Q (THETA)	$Q_{\theta}$	Transverse force per unit length in the circumferential direction
Q (XI)	$Q_{\xi}$	Transverse force per unit length in the meridional direction
Ⓡ		
R	r	Normal distance from axis to shell
R (50, 50)	R	Boundary matrix of Equation (1.46), Section 1.8
RA1		Radius of cone or cylinder at station 1
RC		Radius of curvature of sphere or toroid
RCURV		Input values of meridional radius of curvature
RCURZ		Input values of circumferential radius of curvature
RHØX	$\rho$	$R/A_0$
RIPT		Discrete radii for general shell shape
RØFF		Offset distance of center of curvature from axis of revolution, for toroids
RSLT		Subroutine which computes the boundary matrices for the P and X matrices

⑤

S (50, 50)	S	Boundary matrix of Equation (1.46), Section 1.8
SCR1, 2, 3	$B_m$	Membrane stiffness coefficients
SCD1, 2, 3	$D_m$	Bending stiffness coefficients
SCG1, 2, 3	$G_m$	Shear stiffness coefficients
SCG13	$G_{13}$	Shear twist stiffness coefficient
SCMTSI	$M_{\xi}^T(n)$	Meridional thermal moment coefficients
SCMTTH	$M_{\theta}^T(n)$	Circumferential thermal moment coefficients
SCNTSI	$t_{\xi}^T(n)$	Meridional thermal load coefficients
SCNTTH	$t_{\theta}^T(n)$	Circumferential thermal load coefficients
SIG0	$\sigma_0$	Reference stress
SIG (THETA)	$\sigma_{\theta}$	Circumferential stress
SIG (THETA, ETA)	$\tau_{\theta\xi}$	Circumferential transverse shear stress
SIG (XI)	$\sigma_{\xi}$	Meridional stress
SIG (XI, ETA)	$\tau_{\xi\xi}$	Meridional transverse shear stress
SIG (XI, THETA)	$\sigma_{\xi\theta}$	In-plane shear stress
SUMS		Subroutine which does the Fourier summing for the deflections and rotations, computes the internal loads and, in the Static version, stresses

⑥

TCTR Time cycle number

TFCN		Deck name for the Statics version of function subprogram, ENTT
TFE		Current temperature load at a given meridional station and for k harmonics
THT		Circumferential angle THETA (degrees) at which print-outs of results are desired. (5 permitted)
TMP1, 2		FUNCTION subprograms used to define the temperature for the two layers at which stresses are desired
TTF1, 2		Deck names for function subprograms, TMP1 and TMP2, respectively
TTP		First derivative of the temperature loads
TU	t	Current time
Ⓚ		
U	$u_{\xi}$	Meridional displacement; see Figure 1.2
Ⓛ		
V	$u_{\theta}$	Circumferential displacement; see Figure 1.2
Ⓜ		
W	w	Normal displacement; see Figure 1.2
W (THETA)	$\omega_{\theta}$	Circumferential curvature, print heading
W (XI)	$\omega_{\xi}$	Meridional curvature, print heading
WDOT	$\frac{dw}{dt}$	Velocities
WFEPX	$\frac{\partial \omega_{\xi}}{\partial \xi}$	First derivative of meridional curvatures

WFEX	$\omega_{\xi}$	Program name for W (XI)
WTHX	$\omega_{\theta}$	Program name for W (THETA)
⊗		
X (50)	x	Matrix of Equation (1.62), Section 1.10
XI	$\xi$	Meridional distances to stations computed in GEOM
XIPT		Discrete XI distances or arc lengths array entered with GMDA
⊙		
Z (50)	z	Solution matrix, Equation (1.38), Section 1.7
ZMTRX		Subroutine which solves for the Z matrix using the P and X matrices
ZP		Solutions for previous time cycle
ZPP, ZPPP		Solution matrices for the second and third previous cycles
ZTA	$\zeta$	Circumferential distance to a station
ZX (50)		Another name for Z (50)