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VOLUME 7

SYNTHESIS OF CALCULATIONAL METHODS
FOR THE DESIGN AND ANALYSIS OF RADIATION
SHIELDS FOR NUCLEAR ROCKET SYSTEMS

NAGS

A FORTRAN IV DATA PROCESSING PROGRAM
FOR CALCULATION OF NEUTRON AND GAMMA RAY SOURCES AND
NEUTRON AND GAMMA RAY HEATING IN TWO DIMENSIONAL GEOMETRIES

by

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ABSTRACT

This report is Volume 7 of the nine volumes of the final report on "Synthesis of Computational Methods for the Design and Analysis of Radiation Shields for Nuclear Rocket Systems." Presented in this volume is a description of the Neutron Flux And Gamma Ray Source Edit (NAGS) program.

The NAGS program is a series of FORTRAN IV routines which process multigroup neutron and photon energy fluxes for two dimensional (R, Z or R, θ) geometry models. Fluxes input to the NAGS program are obtained from the ODD-K two dimensional transport program described in Volume 6 of this report. Additional required input data to the NAGS program is prepared automatically by the POINT program described in Volume 2 of this report.

The NAGS program provides: (1) neutron and photon energy sources and distributions for use in point kernel, Monte Carlo, and photon transport analyses, (2) neutron and gamma ray dose rates, and (3) energy deposition data for use in subsequent thermal analyses. Source distributions which are output from the NAGS program are employed as input to the KAP-V point kernel program (Volume 4), the ODD-K two dimensional transport program (Volume 6), and the FASTER Monte Carlo program (Volume 9).

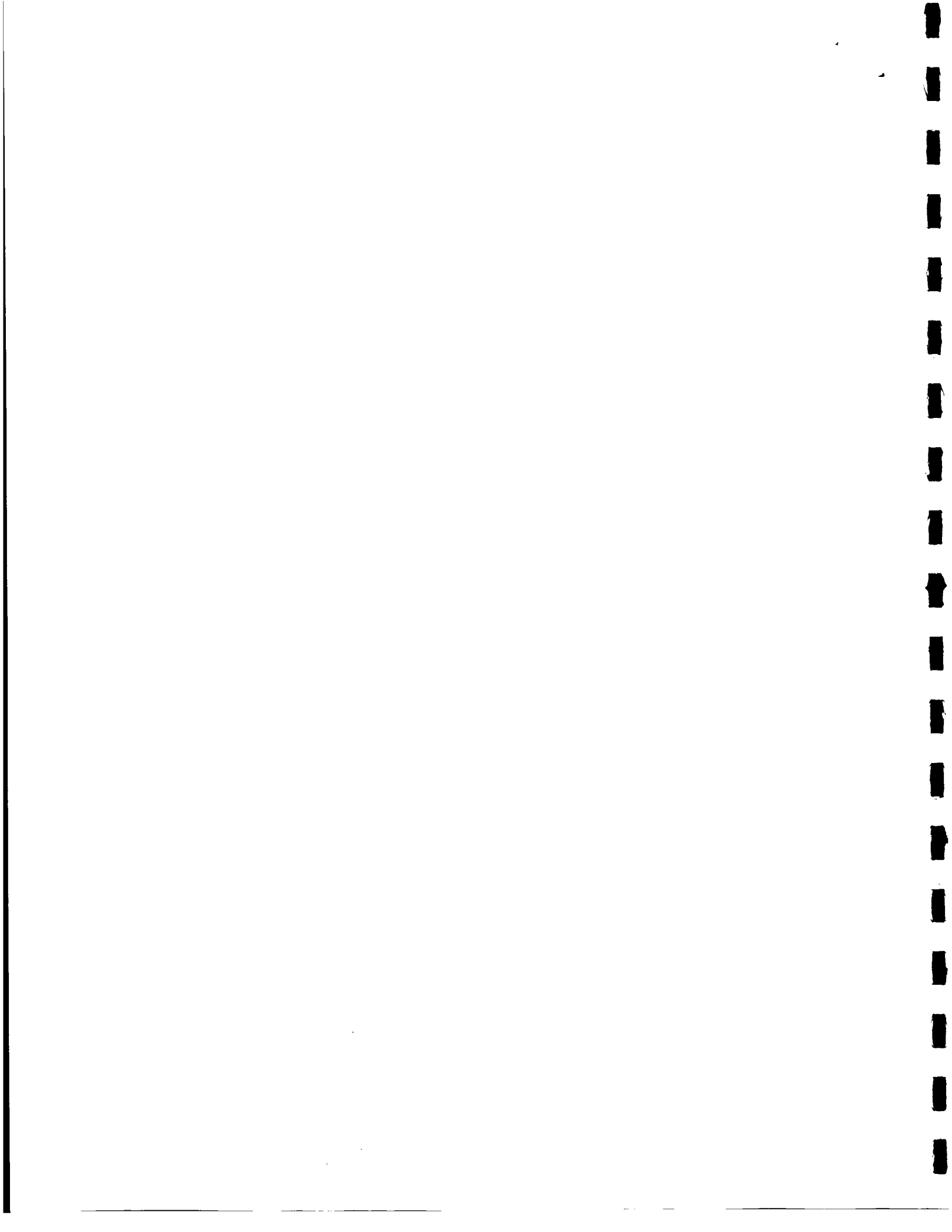


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SECTION

1.0 INTRODUCTION

This report is Volume 7 of nine volumes of the final report on "Synthesis of Computational Methods for the Design and Analysis of Radiation Shields for Nuclear Rocket Systems." Presented in this volume is a description of the Neutron Flux And Gamma Ray Source Edit (NAGS) program.

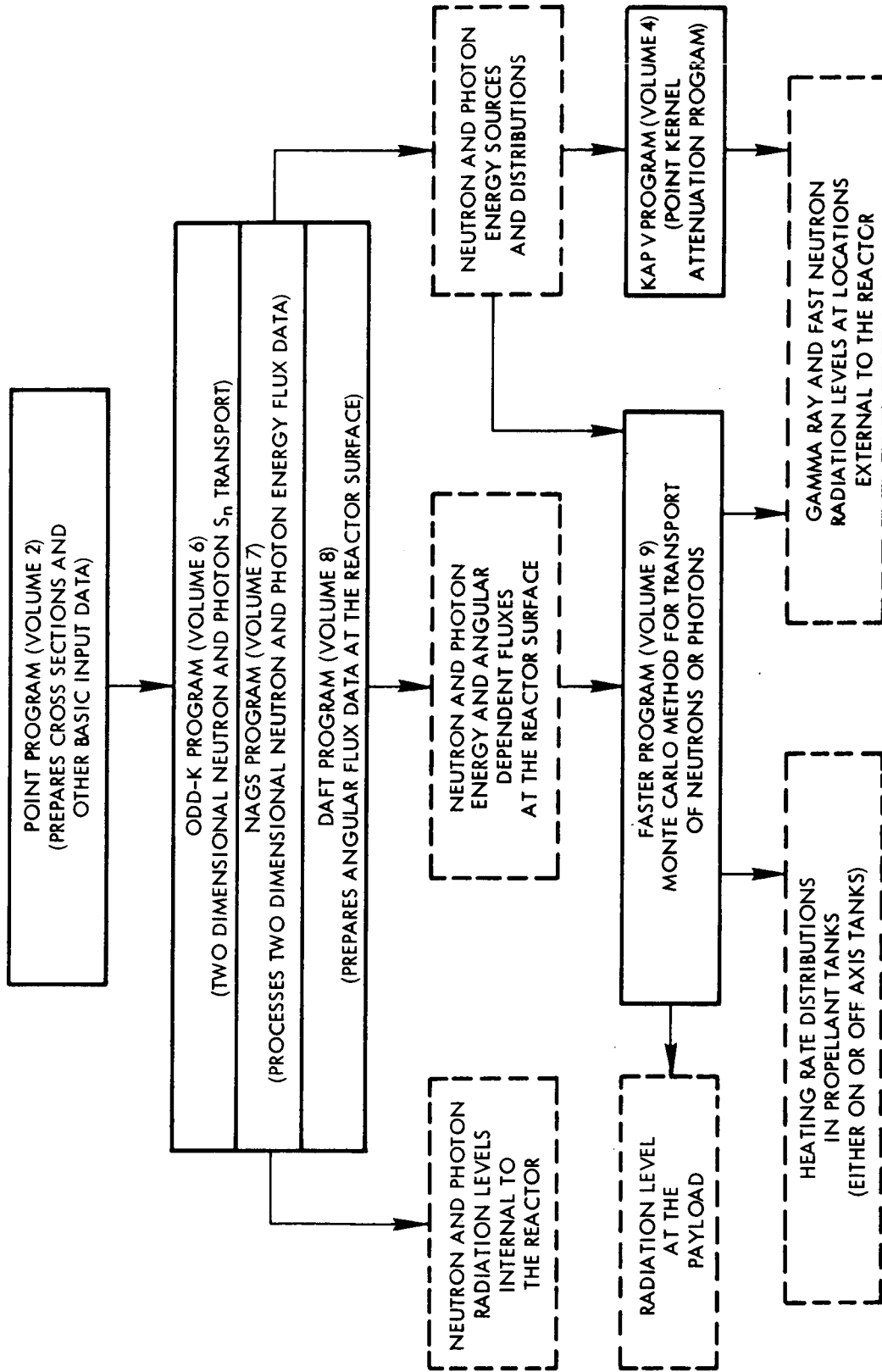
The NAGS program is a series of FORTRAN IV routines which process multigroup neutron and photon energy fluxes for two dimensional (R, Z or R, θ) geometry models. This program is an integral part of the "final" design method as schematically shown in Figure 1. The "final" design method is described in detail in Volume 1 of this report.

The starting point for the method is the POINT program (Volume 2) which prepares cross section and other basic data for use in the transport programs. In the "final" design method (Figure 2), the ODD-K two dimensional transport program (Volume 6) provides neutron and photon energy fluxes throughout the reactor geometry. The NAGS data processing program (Volume 7) processes these fluxes and calculates neutron and photon radiation levels and neutron and photon energy sources within the reactor system. These sources can be employed in either the KAP-V program (Volume 4) or the FASTER Monte Carlo program (Volume 9) for obtaining radiation levels at locations external to the reactor system. In addition, the FASTER program can compute heating rate distributions in the liquid hydrogen propellant (in either an on- or an off-axis tank) and the radiation level at the payload. Alternately, the DAFT program (Volume 8) can prepare neutron and photon energy and angular dependent fluxes at the reactor surface from the ODD-K program for use in the FASTER Monte Carlo code.

Fluxes input to the NAGS program are obtained from the ODD-K two dimensional transport program described in Volume 6. Additional input data needed for the NAGS program is prepared automatically by the POINT program described in Volume 2 of this report.

The need for automated data processing as a logical link in radiation and shielding methods is evident when the vast amount of data handling required in each step of a

of a complete, two dimensional radiation analysis of a reactor is considered. Particular difficult and time-consuming problems handled by the NAGS program are: (1) calculation of neutron and photon energy sources and distributions, (2) calculation of neutron and gamma ray dose rates, and (3) calculation of neutron, photon, and total energy deposition data.



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Figure 1. Schematic Diagram of the Final Design Method

SECTION

2.0 PROGRAM DESCRIPTION

The NAGS program is a special purpose program which serves as a link between the neutron transport solution and the photon transport solution using the discrete ordinates transport program, ODD-K. In addition, this program processes neutron and photon energy flux data simultaneously to calculate total heating and heating distributions in a reactor. The program also provides source distribution data for subsequent use in point kernel or Monte Carlo analyses.

The four basic operations of the NAGS program are:

- 1) Normalization of multigroup neutron and photon energy fluxes to units of per fission, per watt, or a selected power level.
- 2) Redefinition of the mesh cell description for use in photon problems.
- 3) Calculation of photon and neutron sources and distribution and heating rates for each region in the problem.
- 4) Calculation of the total photon and neutron sources and fissions in the reactor.

These four operations are discussed in detail in subsequent sections of this report.

The FORTRAN structure of the NAGS system consists of a main control link (MAIN) and four basic calculation routines (NAGS 1 through NAGS 4) which individually perform steps in reducing the neutron and photon energy flux data into usable forms. The final output of a NAGS problem is dependent upon the route or options chosen.

A brief description of each FORTRAN routine is shown in Figure 2. A description of each routine's function is as follows:

1) The MAIN subroutine initializes the problem by clearing out (set to 0.0) all data storage and allocates data storage on the basis of input pieces of data so that a variety of problems can be handled without program changes. This routine also handles the logical flow throughout the NAGS program system.

2) The NAGS 1 routine processes all geometrical data and neutron and photon energy flux data to obtain a binary work tape containing the flux data in a usable form for subsequent use.

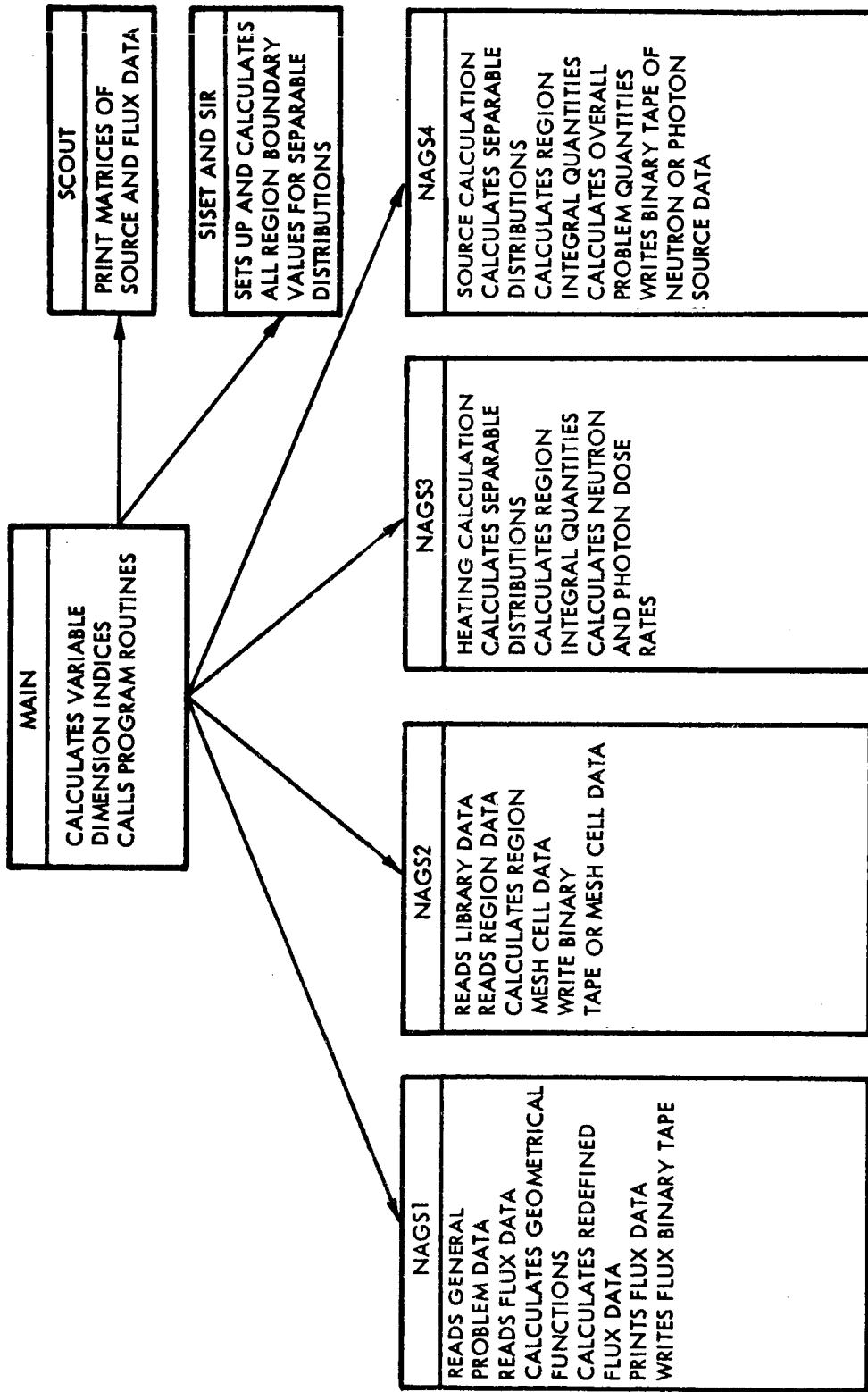
3) The NAGS 2 routine processes the elementwise neutron and photon reaction rate and flux data to obtain a regionwise source function and/or response function binary work tape for subsequent use.

4) The NAGS 3 routine calculates regionwise neutron and/or photon energy deposition distributions and integrals. In addition, NAGS 3 calculates neutron and photon dose rate throughout the two dimensional mesh cell array.

5) The NAGS 4 routine calculates regionwise photon source distributions and integrals for use in subsequent Monte Carlo or point kernel method analyses. The NAGS 4 routine also provides the two dimensional multigroup neutron or photon source data in each mesh cell for subsequent use in neutron or photon transport calculations.

In addition, a set of subroutines are included in the NAGS program system which calculate the region distribution data (SISET and SIR), processes neutron and photon energy flux data in the separable R and Z mesh cell directions (COLR and COLZ), and prints matrices of flux data (SCOUT). All NAGS subroutines are described more fully in Section 4.0 of this volume.

The NAGS program is an essential part of the two dimensional transport analysis system, which is shown schematically in Figure 3. As indicated in Figure 3, the POINT program prepared the macroscopic neutron and photon cross sections for use in the ODD-K program, and microscopic data for use in the NAGS program. The ODD-K neutron transport program run is the next step in the system (See Figure 3). Output from the neutron program are the neutron fluxes on cards (item A) and on tape (item B). The fluxes on cards (item A) are input to the first NAGS problem which computes the photon source data on cards for a redefined mesh (item C) and the neutron fluxes on cards (item D) for the redefined mesh. The photon source (item C) is then used in the ODD-K photon transport problem which produces photon energy fluxes on tape (item F) and on cards (item E). These photon energy fluxes (item E), and the previously computed neutron fluxes (item D), are employed in a final NAGS problem which calculates neutron and photon heating rates and dose rates.



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Figure 2. NAGS Basic Program Structure

Optionally, the neutron and photon energy flux tapes (items B and F) can be input to the DAFT program which produces appropriate angular, spatial and energy fluxes for input to the FASTER Monte Carlo program.

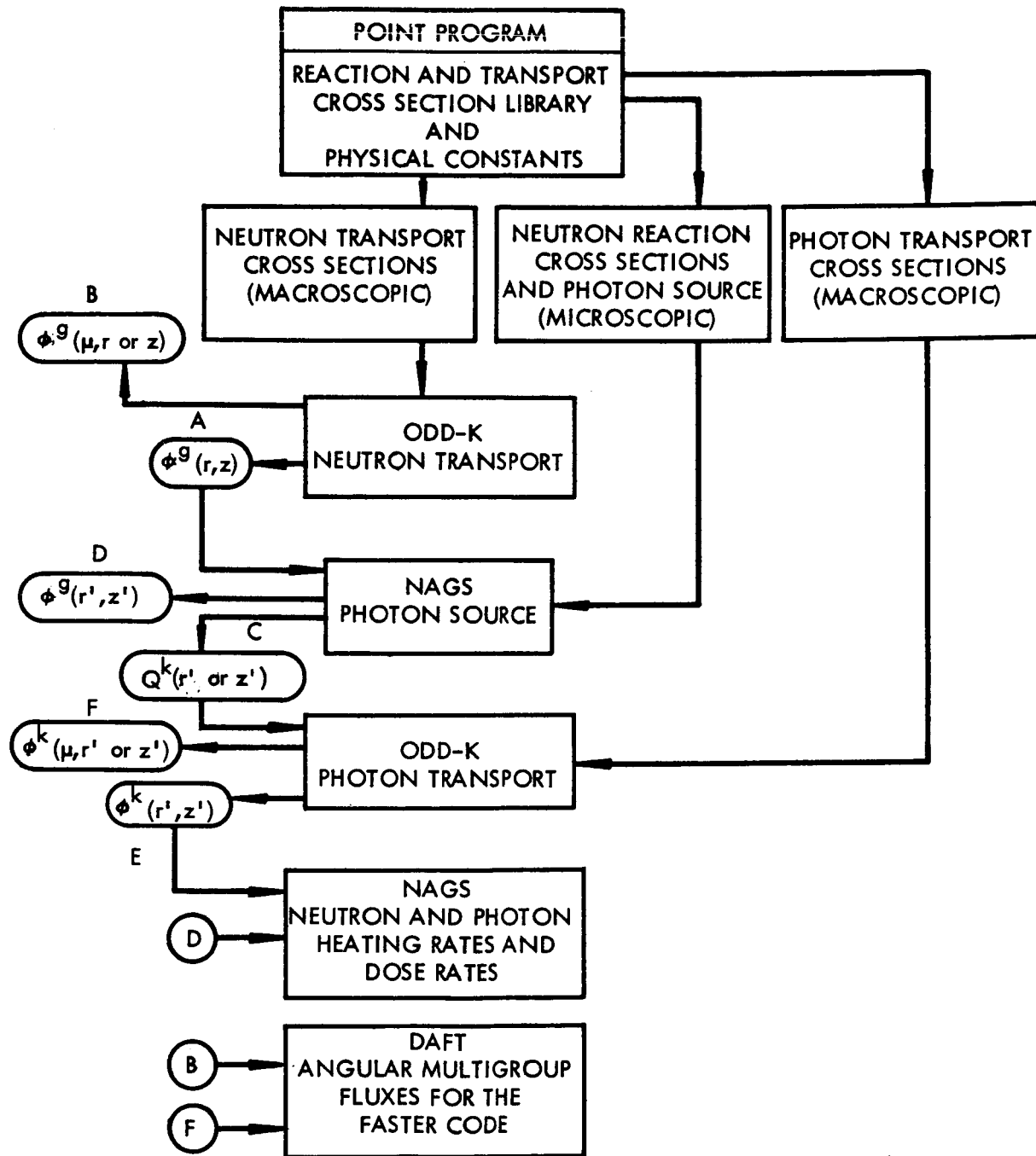
2.1 GEOMETRY

The problem geometry is described in the NAGS system as a two dimensional reactor mockup in the R, Z or R, θ geometry. This geometry is similar to that used in the discrete ordinate transport program, ODD-K. The reactor mockup is described geometrically in NAGS as a series of rectangular or angular sector regions in a two dimensional mesh cell layout. Figure 4 illustrates the limitations of the geometry and the method by which an irregular region, D, must be described. Since the program operates on each NAGS region as a separate problem, the number of NAGS regions which can be run in a single problem is unlimited.

The integration techniques used to obtain particle fluxes, reaction rates, response rates, or particle source data are identical to the ODD-K transport method program techniques. Hence, completely consistent results are obtained in NAGS and ODD-K, i.e., the total number of neutrons and photons from the ODD-K problem is conserved. Interpolation and extrapolation techniques employed in NAGS are based on a linear variation of flux or source in the mesh cells and an exponential falloff of flux or source at the external boundaries of the reactor mockup.

2.2 MULTIGROUP FLUX OPERATIONS

Flux data for the NAGS program are the multigroup neutron and photon energy fluxes from the discrete ordinate transport method program, ODD-K, described in Volume 6 of this report. These flux data are provided by ODD-K at the center of each mesh cell and is the average flux in the mesh cell. The program will accept flux data from either the R, Z or R, θ two-dimensional geometry solutions in ODD-K. The multigroup flux data are used in the NAGS system in a manner such that the total number of neutrons and photons from the ODD-K problem is conserved.



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Figure 3. Schematic Diagram of the Two Dimensional Transport Analysis System

The NAGS program requires input flux data to be in either binary tape or decimal data punched card form. The input channels used for the flux data is dependent upon the type of NAGS problem (photon source or neutron and/or photon heating) to be run. A complete description of the input channels is presented in Section 5. The operations performed on the input flux data for an R, Z problem are:

- 1) Redefinition of radial and axial mesh cell description if required.
- 2) Normalization of flux data to units of per fission, per watt, or a selected power level.
- 3) Generation of a group dependent binary work tape containing all particle flux data in a form suitable for subsequent data processing.

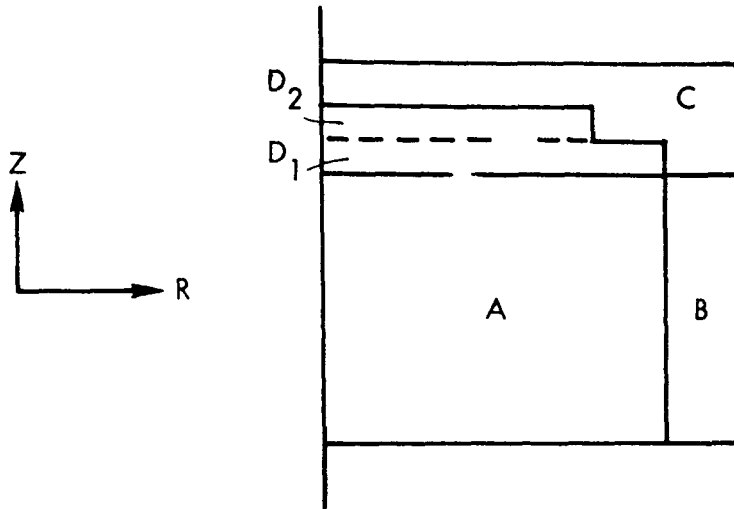
The above operations are performed in a similar manner for R, θ calculations.

2.2.1 Redefinition of Mesh Cell Data

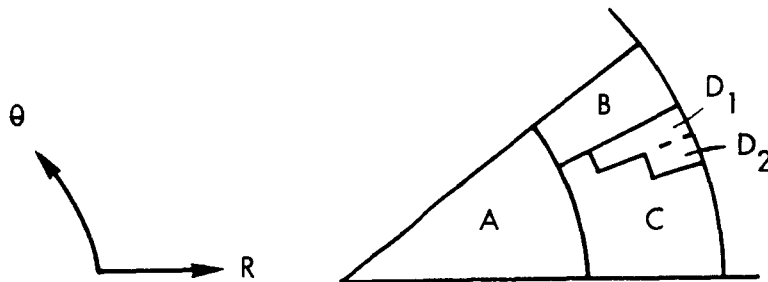
The NAGS Program is capable of redefining the radial or axial mesh cell description of the input problem geometry and fluxes. This procedure is included in order to increase the utility of the program by adjusting the mesh size in a NAGS problem to meet computer core memory limitations in subsequent problems. For example, a neutron transport problem with 16 energy groups, S_6 angular quadrature, P_0 scattering cross sections, and a total of 1200 mesh cells, is an approximate maximum ODD-K neutron transport problem. This same problem in photon transport, with 13 groups, S_6 angular quadrature, but with P_1 scattering cross sections will allow only a total of 800 mesh cells. Hence, in order to run linked neutron and photon transport problems, the linking program (NAGS) must include a technique for redefinition of the neutron transport mesh cell description in either (or both) the radial or axial direction to accommodate photon transport calculations.

Redefinition of mesh cells is done in a manner to conserve mesh cell fluxes in the redefined mesh cells. This procedure is restricted to the deletion of mesh lines internal to region boundaries of the problem geometry. The user specifies in the general problem input data, the mesh cell dimensions (coordinates) of the original or input flux data solution, as

1. R-Z GEOMETRY



2. R- θ GEOMETRY



NOTE: A, B, C, D ARE MASTER REGIONS; D_1 , D_2 ARE
SUBREGIONS OF MASTER REGION D

REGION DESCRIPTIONS FOR A, B, C, D_1 , D_2
ARE REQUIRED INPUT FOR NAGS

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Figure 4. Sample Geometries for the NAGS Code

well as the mesh cell coordinate identification numbers which will comprise the new (or redefined) mesh cell description. The average particle flux, ϕ_{lj} , in each group in each new (redefined) radial mesh cell is computed as:*

$$\phi_{lj} = \frac{\sum_{i=i_s}^{i_f} \phi_{ij} \cdot \Delta A_i}{\sum_{i=i_s}^{i_f} \Delta A_i}$$

where ϕ_{lj} is the centered average flux in the redefined radial mesh cell, l , for each axial mesh cell, j . The quantities i_s and i_f are the input flux mesh cell coordinate indices which form the left and right boundaries of the new or redefined radial mesh cell, l . The quantity, ΔA_i is the cross sectional area, $\pi (R_{i+1}^2 - R_i^2)$, of the mesh cell, i . The computed average flux data, ϕ_{lj} , is placed at the radial midpoint of the new mesh cell, $R_l = 1/2 (R_{i_s} + R_{i_f})$.

In a similar fashion, the average flux, ϕ_{lJ} , in each new axial mesh cell is obtained as:

$$\phi_{lJ} = \frac{\sum_{i=i_s}^{i_f} \phi_{li} \cdot \Delta Z_i}{\sum_{i=i_s}^{i_f} \Delta Z_i}$$

where ϕ_{lJ} is the centered average flux in each group in the redefined mesh cell, (l, J) and ϕ_{li} is the centered average flux previously computed in the redefined radial mesh cell, l , for each axial mesh cell, j . The quantities, i_s and i_f , are the input flux mesh cell coordinate indices which form the bottom and top boundaries of the new (or redefined) axial mesh cell, J . The quantity, ΔZ_i , is the height of each axial mesh cell, j . The computed average flux data, ϕ_{lJ} , is placed at the axial midpoint of the redefined mesh cell, $Z_J = 1/2 (Z_{i_s} + Z_{i_f})$.

*Note: The solution for the azimuthal variable, θ , in the R- θ solution is the same as for the variable Z in the R- Z solution.

The redefinition of the input flux data to a new mesh cell description is performed only if requested by the user in the general problem input data. The flux data which are processed by group are then normalized as described in the following section.

2.2.2 Flux Normalization

Normalization of the particle flux data is performed after redefinition of the mesh cell description. The constants for the calculation of the normalization factor, NF, are dependent upon the source of the flux data (i.e., neutron flux from ODD-K neutron transport, neutron flux from a previous NAGS problem, or photon flux from ODD-K). The user of NAGS has at his disposal a six parameter normalization factor. These six parameters are required input for each problem and are, also, descriptive of neutron flux normalization constants for an ODD-K problem. The normalization factor is computed as:

$$NF = \frac{\bar{\nu} \cdot K_1 \cdot P}{K_2 \cdot k_{eff} \cdot f \cdot A}$$

where:

$\bar{\nu}$ = the average number of neutrons per fission (e.g.,
 $\bar{\nu} = 2.445$ for a nuclear rocket flight-type reactor).

K_1 = the fissions per second per watt of power. K_1 is dependent upon the operating history, gamma ray energy production, and neutron and gamma ray energy leakage from a reactor system. For a nuclear rocket flight-type reactor with 15 minutes of full power operation, the fissions per second required to produce one watt of thermal power is calculated to be 3.21×10^{10} fissions/watt-second.

P = the total reactor power in watts. Hence $K_1 \times P$ gives the fissions per second at full reactor power.

K_2 = the parameter of radians. This parameter is 1.0 for R-Z, ODD-K problems and is included in the calculation of NF to account for symmetry in R- θ , ODD-K. In R- θ problems, the parameter K_2 is $\theta/2\pi$.

k_{eff} = the effective neutron multiplication factor (eigenvalue) of the ODD-K neutron transport problem and is used to normalize all fluxes to a critical ($k_{\text{eff}} = 1.0$) reactor system.

f = the fraction of fission events in the ODD-K problem which produce fission energy. This factor is included for the case when the $(n, 2n)$ neutron interactions are included in the flux solution as pseudo-fission events. For ODD-K problems with MSFC library cross sections, beryllium $(n, 2n)$ cross sections are not included as fission and f is input as 1.0.

A = the area (or volume) factor. This factor is required only if the neutron flux solution is normalized to some value other than the integral of fissions over the source volume. For ODD-K problems this value is always 1.0.

Hence, the normalization factor for a 5000 MW flight-type nuclear rocket reactor, in an R-Z ODD-K neutron transport problem with a multiplication factor of 1.01 is computed internally by NAGS as:

$$NF = \frac{2.445 * 3.21 \times 10^{10} * 5 \times 10^9}{1.0 * 1.01 * 1.0 * 1.0} = 3.89 \times 10^{20}$$

Fluxes printed out by NAGS using the above normalization constant will be in units of $\frac{\text{neutrons}}{\text{cm}^2\text{-sec}}$ at full power (5000 MW) conditions. In normalizing flux data from a photon transport problem, or a previous NAGS problem (see Figure 3), the six normalization parameters are normally set equal to 1.0 since the flux solution in the ODD-K photon transport problem is based on normalized distributed fixed source data supplied by the previous NAGS photon source problem. Also, the neutron flux data from the NAGS problem is a processed library data tape based on previously normalized flux data.

2.2.3 Generation of Particle Flux Tape

The final operation on the input flux data is the generation of a binary work tape containing the groupwise fluxes to be used in later reaction rate and response rate calculations.

This data tape can be saved for use in subsequent NAGS problems as indicated in Figure 3. For example, the neutron flux data tape used in the calculation of distributed photon sources is used as input for the combined neutron and photon energy deposition calculation. This neutron flux data tape has the same mesh cell description as the photon source data and the photon flux data.

The binary flux tape, which is generated on MSFC IBSYS Version 13 tape unit A-6, remains on this unit throughout the NAGS problem. The tape consists of a logical tape record of each group with a total of ICM (number of redefined radial mesh cells) X JCM (number of redefined axial mesh cells) pieces of data in each logical tape record.

2.3 MESH CELL OPERATIONS AND LIBRARY DATA

The computation of the neutron and photon interactions in each mesh cell of each region of a NAGS problem geometry is carried out using fluxes obtained in the redefined mesh cell description. The interaction calculations and the resultant product (neutron source, photon source, or particle energy deposition) are summed over all groups, materials, and interactions to provide total interactions, source strength, or energy deposition on an individual mesh cell basis throughout the two dimensional model. Subsequent operations on the mesh cell data provide the region integral distributions, as well as the integrals over all mesh cells and all regions. These final data processing operations are performed without alteration of mesh cell data so that all mesh cell data can be used in subsequent photon transport calculations. The procedure for obtaining particle interaction data in the program is carried out on a regionwise basis. The program requires as input, a library of physical constants and neutron and photon spectrum dependent data for each element or isotope (i.e. H, Be, U²³⁵, etc.) in the reactor geometry. Library data and region data, and the interaction calculations are described in the following sections.

2.3.1 Library Data

Library data for a NAGS problem include standard neutron and photon multigroup constants as well as nuclear data for each element in the reactor geometry.

The nuclear constants required in the library for each neutron and photon energy group are:

- 1) Prompt fission photon energy, Γ_p^k , for each photon group, k.
- 2) Fission product decay photon energy, Γ_p^k , for each photon group, k, and for a specific reactor operating history (e.g., a nuclear rocket reactor with 15 minutes operation of full power).
- 3) Photon flux to dose rate conversion factors, K_D^k , for each photon group, k.
- 4) Neutron flux to dose rate conversion factors, K_D^g , for each neutron group, g.
- 5) Neutron multigroup parameters of,
 - (a) Lethargy width, $\Delta \mu^g$, for each neutron group, g.
 - (b) Energy width, ΔE^g , for each neutron group, g.

The other nuclear library data are required for each element or isotope, m, in the library and are as follows:

- 1) Identification number, NID_m
- 2) Atomic mass, A_m
- 3) Average energy loss per neutron scattering event, $\frac{2 A_m}{(A_m + 1)^2}$
- 4) Average energy of each alpha particle emission from neutron capture, $E(n, \alpha)$
- 5) Microscopic thermal neutron (2200 meter/second) absorption cross section, σ_a^{2200}
- 6) A six (6) character alphanumeric title (i.e., HYDROG, CARBON, etc.)
- 7) Inelastic neutron scattering photon energy, Γ_{sgm}^k , from an inelastic event in neutron group, g, for photon energy release in group, k.
- 8) Neutron elastic scattering cross sections, σ_{em}^g , for each fast neutron group, g.
- 9) Neutron absorption cross section for (n, α) reaction, $\sigma_{n,\alpha}^g$ for each neutron group, g.
- 10) Neutron elastic scattering anisotropic correction factor for neutron energy deposition, $(1 - \bar{\mu}_0)^g$ for each neutron group, g.

- 11) Neutron radiative capture photon energy, Γ_{cm}^k , for each material and photon group, k.
- 12) Photon mass energy absorption coefficient $(\frac{\mu}{\rho})_{am}^k$ for each photon group, k.
- 13) Neutron fission cross sections, σ_{fm}^g , for each neutron group, g.
- 14) Neutron radiative capture cross sections, σ_{cm}^g , for each neutron group, g.
- 15) Neutron elastic scattering cross sections, σ_{em}^g , for each fast neutron group, g.
- 16) Neutron inelastic scattering cross sections, σ_{sm}^g , for each fast neutron group for which inelastic scattering is to be calculated.

The last four sets of cross section data (defined above) are required input only when the user employs the NAGS library option of region independent cross section data. This library option is the standard mode of input if the POINT program output with region independent cross section data (as furnished MSFC) is used.

2.3.2 Region Data

Region input data for a NAGS problem are dependent on the type of calculation being performed. The region data are processed on an individual region basis. Required data for each region are:

- 1) A seventy-two (72) character alphanumeric title describing the region
- 2) Region boundary mesh cell numbers in the redefined mesh cell description
- 3) The number of elements in the region, and
- 4) A program control word to control the reading of new region data or to proceed to the next step of the NAGS data processing.

There are two types of calculations which can be performed by NAGS. The first type is the neutron interaction calculation which results in the production of neutron and photon sources in the mesh cells. The second type is the calculation of neutron and/or photon interactions which results in energy deposition in the mesh cell.

Region input data required for a photon source calculation are dependent on the NAGS library (Refer to Section 2.3.1) used for the problem. The element microscopic cross section data described below are only required when the NAGS short library option is used. The standard MSFC mode is the NAGS long library option; element microscopic cross sections are not required. The region input data required for each element, m , follows as:

- 1) Element identification number, L_m ,
- 2) Element number density, N_m ,
- 3) Element microscopic groupwise neutron cross sections for,
 - (a) fission, σ_{fm}^g ,
 - (b) radiative capture, σ_{cm}^g ,
 - (c) elastic scattering, σ_{em}^g ,
 - (d) inelastic scattering, σ_{sm}^g .

The region data required for calculation of energy deposition of neutrons and photons are input for the material (e.g., fueled graphite, stainless steel, etc.) in the NAGS region. This technique is used because reactor components or structures are represented as part of a homogeneous region material in neutron and photon transport. For subsequent thermal analyses, the total heating and its distribution in these components is required. Hence, an Inconel bolt can be represented individually in a region to obtain its total heating. The input data required for the energy deposition calculation in each material, n , in each region are:

- 1) Material density in the region, ρ_n
- 2) Weight of the material in the region, W_n .

Input data for each element or constituent of the above material are required as:

- 1) Element identification number, L_m
- 2) Weight fraction, N_m of the element, L_m , in material, n .

The data are then processed on a mesh cell basis to obtain the total photon source or energy deposition in each mesh cell of a region.

An option is included in the program to eliminate repetitive input data for a NAGS region of identical composition to the previous NAGS region. This option is specified by a negative sign on the number of elements for a NAGS region. The program will then use the region element data (L_m , N_m and element cross sections) from the preceding NAGS region for all calculations in that region.

2.3.3 Mesh Cell Calculations

The mesh cell calculations are based on the redefined mesh cell description and fluxes. These fluxes are processed on a groupwise basis to obtain the total source or energy deposition in each mesh cell of a region. Mesh cell calculations are performed at both internal and external mesh cells of a region and at adjacent external mesh cells. Internal mesh cells are designated in Figure 5 by O's; external mesh cells are designated by X's.

Calculations in mesh cells, external to and adjacent to the region being calculated, provide results for use in interpolation or extrapolation of distribution values at the region boundaries. This procedure provides a calculated source or energy deposition distribution value at each boundary of a region. This calculation is described in detail in Section 2.4.3. The calculation of photon source and associated quantities at each mesh cell follow as:

- 1) Neutron fission density:

$$F_{IJ} = \sum_{m=1}^{NEL} \sum_{g=1}^{NGN} N_m \sigma_{fm}^g \phi_{IJ}^g$$

- 2) Fission neutron source density:

$$Q_{IJ}^g = \sum_{m=1}^{NEL} \sum_{g=1}^{NGN} N_m \nu^g \sigma_{fm}^g \phi_{IJ}^g$$

- 3) Photon source density in photon group, k , from neutron fission (prompt and decay):

$$Q_{FIJ}^k = \left(\Gamma_p^k + \Gamma_d^k \right) \cdot F_{IJ}$$

- 4) Neutron radiative capture density for element, m :

$$C_{mIJ} = \sum_{g=1}^{NGN} N_m \sigma_{cm}^g \phi_{IJ}^g$$

- 5) Photon source density in group, k , from neutron radiative capture:

$$Q_{CIJ}^k = \sum_{m=1}^{NEL} \Gamma_{cm}^k C_{mIJ}$$

- 6) Neutron inelastic scattering density for neutron group, g , and element, m :

$$S_{IJ}^m = N_m \sigma_{Sm}^g \phi_{IJ}^g$$

- 7) Photon source density in photon group, k , from neutron inelastic scatter:

$$Q_{SIJ}^k = \sum_{g=1}^{NI} \sum_{m=1}^{NEL} S_{IJ}^m \Gamma_{sgm}^k$$

- 8) Total photon source density in photon group, k , from all sources:

$$Q_{TIJ}^k = Q_{FIJ}^k + Q_{CIJ}^k + Q_{SIJ}^k$$

The mesh cell calculations of energy deposition are performed for neutrons and photons on a groupwise basis. The calculations follow as:

	X	X	X	
X	○	○	○	X
X	○	○	○	X
X	○	○	○	X
	X	X	X	

- INTERNAL MESH CELL
- × EXTERNAL MESH CELL
- REGION BOUNDARIES
- MESH CELL BOUNDARIES

611855-61B

Figure 5. Region Mesh Cell Description

1) Neutron kinetic energy deposition:

$$H_{IJ} = 1.603 \times 10^{-13} \sum_{m=1}^{NEL} \sum_{g=1}^{NFAST} \sigma_{em}^g \left(\frac{2A_m}{(A_m+1)^2} \right) (1.0 - \bar{\mu}_o)_m^g \left(\frac{N_m N_a \rho_n}{A_m} \right) \phi_{IJ}^g \cdot \frac{\Delta E^g}{\Delta \mu^g}$$

2) Photon energy deposition:

$$H_{IJ} = 1.603 \times 10^{-13} \sum_{m=1}^{NEL} \sum_{k=1}^{NGG} N_m \rho_n \left(\frac{\mu_a}{\rho} \right)_m^k \phi_{IJ}^k$$

The quantity, N_a , is Avogadro's number 0.60248×10^{24} .

2.4 REGION OPERATIONS

Region dependent quantities are calculated from the internal and external mesh cell data described in the previous section. These data are processed on a single region basis to obtain the total mesh cell photon source for photon transport, or the region source integral and energy, or spatial distribution data required for point kernel and/or Monte Carlo input, or region energy deposition integrals and distributions. The calculation of the photon source data and particle energy deposition data is discussed separately in the following sections. The region boundary mesh cell numbers I_S , I_F , J_S , and J_F define the NAGS region in the total mesh cell description. These values determine the limits of integration to be used in NAGS region calculations.

2.4.1 Photon Source

The photon source mesh cell data, described in the previous section, are processed in conjunction with the region and mesh cell dimensions to obtain final region quantities of:

- 1) Total region volume.
- 2) Total region weight.
- 3) Region integrals of:
 - a) photon source
 - b) neutron induced fissions
 - c) neutron source
 - d) photon energy spectrum including volume averaged spectrum
- 4) Region separable radial and axial distributions for photon source, neutron induced fission, and neutron source.

Intermediate and final region data are calculated from the internal and external mesh cells as shown in Figure 5. The region boundary values calculated from these data are shown in Figure 6.

The initial operation to obtain region source or fission distributions separable in the radial and axial directions with values at the top, bottom, left, and right boundaries defining the exterior boundary of a region are as follows:

1) External mesh cell values

a) Top External

$$S_t = \sum_{l=I_S}^{I_F} \sum_{k=1}^{NGG} S_{tl}^k \Delta A_l$$

b) Bottom External

$$S_b = \sum_{l=I_S}^{I_F} \sum_{k=1}^{NGG} S_{bl}^k \Delta A_l$$

c) Left External

$$S_l = \sum_{J=J_S}^{J_F} \sum_{k=1}^{NGG} S_{lJ}^k \Delta Z_J$$

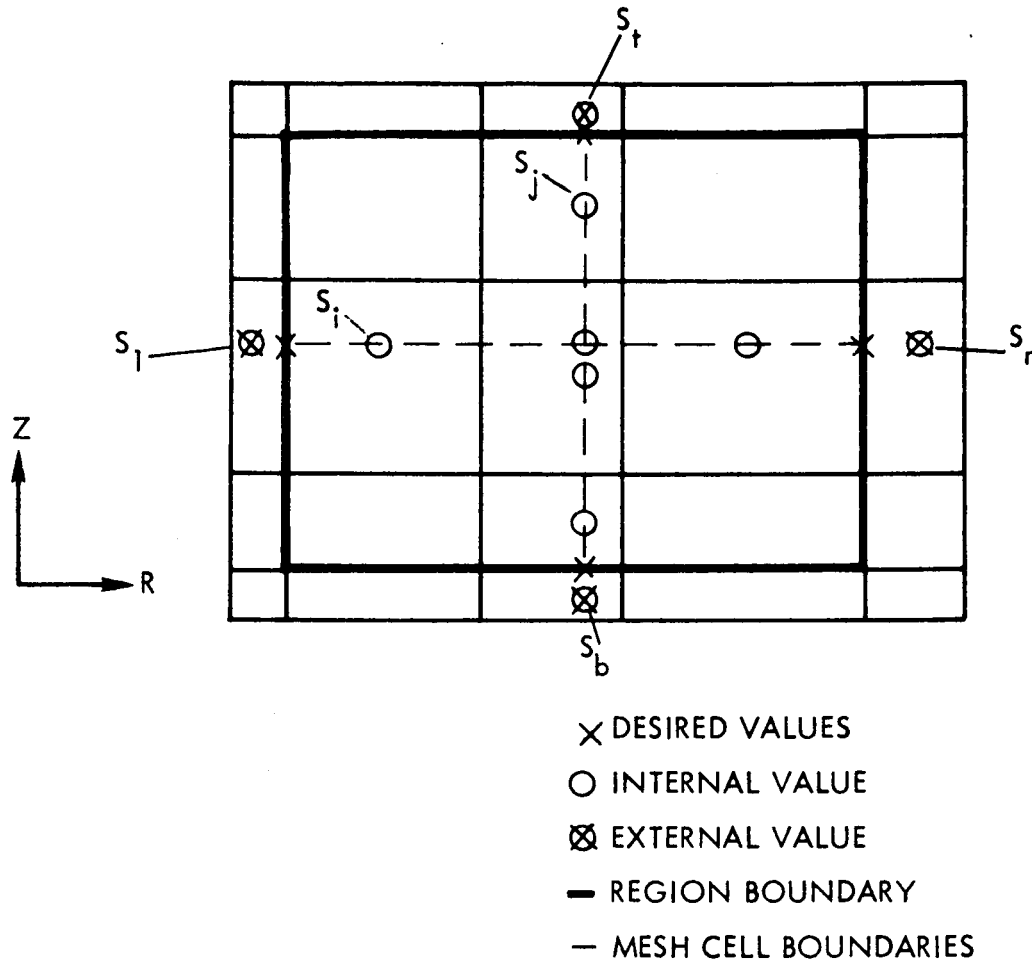
d) Right External

$$S_r = \sum_{J=J_S}^{J_F} \sum_{k=1}^{NGG} S_{rJ}^k \Delta Z_J$$

2) Internal mesh values

a) Radial

$$S_l = \sum_{J=J_S}^{J_F} \sum_{k=1}^{NGG} S_{lJ}^k \Delta Z_J$$



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Figure 6. Region Separable Distribution Description

b) Axial

$$S_J = \sum_{I=I_S}^{I_F} \sum_{k=1}^{NGG} S_{IJ}^k \Delta A_I$$

3) Region areas and volumes

$$\Delta A = \sum_{I=I_S}^{I_F} \Delta A_I$$

$$\Delta Z = \sum_{J=J_S}^{J_F} \Delta Z_J$$

$$V_R = \Delta A \cdot \Delta Z$$

4) Region integral values

$$S_T = \sum_{I=I_S}^{I_F} \sum_{J=J_S}^{J_F} \sum_{k=1}^{NGG} S_{IJ}^k \Delta A_I \Delta Z_J$$

5) Normalized distribution values

a) Internal

$$S_I \text{ (normalized radial)} = S_I \Delta A / S_T$$

$$S_J \text{ (normalized axial)} = S_J \Delta Z / S_T$$

b) External

$$S_{t,b} = S_{t,b} \Delta A / S_T$$

$$S_{l,r} = S_{l,r} \Delta Z / S_T$$

The normalization operation is performed as above for photon source, neutron induced fission, and neutron source. The values S_i , S_j , S_i , S_b , S_i and S_r are used to calculate boundary values shown in Figure 6 using the techniques described in Section 2.4.3.

The remaining region quantities are obtained as follows:

1) Region Weight

$$W_R = V \cdot \sum_{m=1}^{NEL} \frac{N_m A_m}{N_a}$$

2) Region photon source

a) Total Integrated Spectrum

$$Q_T^k = \sum_{J=J_S}^{J_F} \sum_{I=I_S}^{I_F} \sum_{k=1}^{NGG} Q_{TIJ}^k \Delta A_I \Delta Z_J$$

b) Average Spectrum

$$Q_T^k = Q_T^k / V_R$$

c) Total

$$Q_T^k = \sum_{k=1}^{NGG} Q_T^k$$

3) Region neutron induced fission

$$F = \sum_{J=J_S}^{J_F} \sum_{I=I_S}^{I_F} F_{IJ} \Delta A_I \Delta Z_J$$

4) Region neutron source

$$Q_T = \sum_{J=J_S}^{J_F} \sum_{I=I_S}^{I_F} \sum_{g=1}^{NGN} Q_{IJ}^g \Delta A_I \Delta Z_J$$

2.4.2 Energy Deposition

The energy deposition mesh cell data described in Section 2.3.3 is used in a fashion similar to that described for processing of photon source data. The final region quantities calculated are:

- 1) Element or constituent quantities
 - a) Density in region in gms/cc
 - b) Total energy deposition in kilowatts
- 2) Region quantities for each material in the region
 - a) Density in lbs/in.³
 - b) Weight in lbs
 - c) Total energy deposition in kilowatts
 - d) Photon energy deposition in kilowatts
 - e) Neutron energy deposition in kilowatts
 - f) Total energy deposition in Btu/hour, watts/gram, watts/cm³ in the solid material, Btu/lb-hour, and Btu/in.³-hour in the solid material
- 3) Region separable radial and axial energy deposition distributions (relative to a region volume average of 1.0 and region average energy deposition in Btu/in.³-hour).
- 4) Region mesh cell total energy deposition in Btu/in.³-hour.

These distribution quantities are calculated using the same techniques described for the photon source calculation. Region integrals are obtained as the summation of neutron and photon energy deposition or as separate quantities. The integrals are multiplied by appropriate conversion factors to obtain either metric or English units.

2.4.3 Interpolation and Extrapolation Procedure

The procedures for calculating the end (or boundary) points of a radial or axial source or response distribution in a NAGS region are described in this section. The techniques are discussed in general terminology because the calculation of boundary values for neutron or photon source, fission, or energy deposition distributions are the same.

As defined earlier, a NAGS region is a set of adjacent mesh cells having the same material composition and a rectangular outer boundary. The separable radial and axial distributions are calculated at the midpoints of the redefined mesh cells of a region. These data are used for all interpolation or extrapolation operations. The additional data used in these operations are the external boundary sources (or response values) calculated with material properties of the region, but with particle fluxes at the mesh cells external and immediately adjacent to the region, as shown in Figure 6. Dependent upon the position of the region in the reactor geometry, the calculation of the boundary value assumes one of five types of interpolation or extrapolation techniques, as shown in Figure 7. The mesh cell data (internal and external to the NAGS region) are denoted by the dashed lines and the open O's. The boundary values to be calculated are denoted by the solid lines and by X's. The special case where the mesh cell lies at the reactor centerline, outer radius, top boundary, or bottom boundary of the reactor geometry requires special techniques to obtain the boundary value. In addition, the calculation of the boundary values of a region of only one mesh cell in width (or height) is based on the value at that mesh cell and at the two adjacent external mesh cell values. All values of external mesh cell data are calculated with the nuclear properties of the NAGS region and are relative to the internal mesh cell values.

RADIAL OPERATIONS

Condition 1: Linear Interpolation at Internal Boundaries, $R_1 \neq 0.0$
or \neq Outer Radius of Reactor Geometry

The value at the radial boundaries R_1 is found by linear interpolation of adjacent mesh cell values as shown below

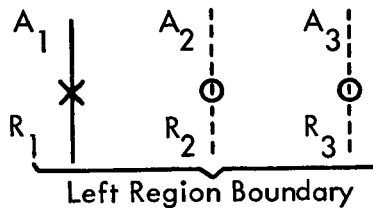


$$A_1 = \frac{A_2 R_2 + \frac{(A_3 R_3 - A_2 R_2)(R_1 - R_2)}{R_3 - R_2}}{R_1}$$

where: A_1 , A_2 , and A_3 are the values of the flux at the radial positions R_1 , R_2 , and R_3 , respectively.

Condition 2: Parabolic Extrapolation of Reactor Centerline, $R_1 = 0.0$

The derivative of the distribution, S_1 , must be zero at $R_1 = 0.0$ (i.e., $\delta S_1 / \delta r = 0.0$). The geometry with the two mesh cell values internal to the geometry used for parabolic extrapolations is as follows:

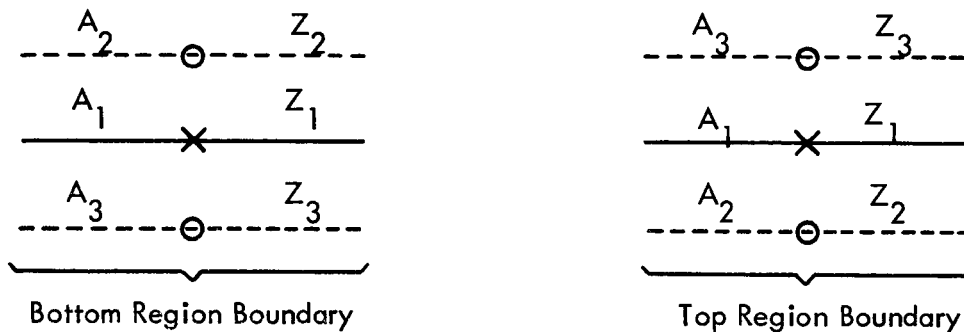


$$A_1 = \frac{A_3 R_2^2 - A_2 R_3^2}{R_2^2 - R_3^2}$$

Figure 7. Distribution Interpolation and Extrapolation Techniques

AXIAL OPERATIONS
Condition 1: Linear Interpolation Applies at Internal Boundaries,
 $Z_1 \neq$ Bottom or Top of Reactor Geometry

The value at the boundary Z_1 is found by linear interpolation of adjacent mesh cell values as shown below:

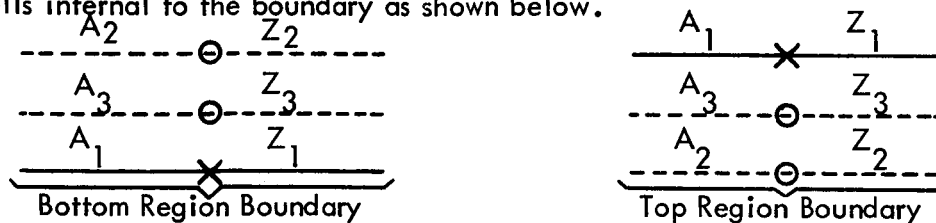


$$A_1 = A_2 + \frac{(A_3 - A_2)(Z_1 - Z_2)}{(Z_3 - Z_2)}$$

where: A_1 , A_2 , and A_3 are the values of the flux at the axial positions Z_1 , Z_2 , and Z_3 , respectively.

Condition 2: Logarithmic Extrapolation at External Boundaries $Z_1 =$
Bottom or Top of Reactor Geometry

The value at the boundary Z_1 is found by extrapolation from the two adjacent mesh cells internal to the boundary as shown below.



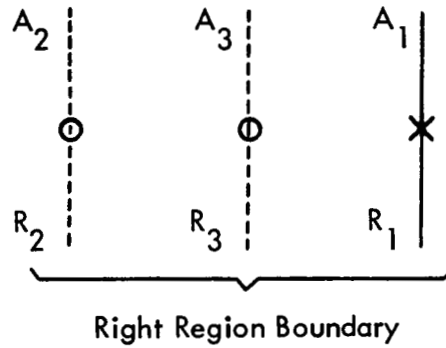
$$A_1 = A_3 \exp \left[\frac{(Z_1 - Z_3) \frac{A_3}{A_2}}{Z_3 - Z_2} \right]$$

Figure 7. (Continued) (2 of 3 Sheets)

Condition 3: Logarithmic Extrapolation at the External Boundary,

$R_1 = \text{Outer Radius of Reactor Geometry}$

The value at the boundary R_1 is found by logarithmic extrapolation from the two adjacent mesh cells internal to the boundary as shown below.



$$A_1 = A_3 \frac{R_3}{R_1} \exp \left[\frac{(R_1 - R_3) \frac{A_3 R_3}{A_2 R_2}}{R_3 - R_2} \right]$$

Figure 7. (Continued) (3 of 3 Sheets)

2.5 OVERALL PROBLEM OPERATIONS

At the completion of the region data processing, the NAGS program performs calculations and operations for all mesh cells in the reactor geometry. These final operations are dependent upon whether the neutron or photon source or energy deposition calculation option is used.

2.5.1 Neutron or Photon Source

The overall reactor geometry neutron and photon source calculations yield the integral photon source, neutron source, and fissions in the reactor. These integrations follow:

- 1) Total photon source

$$Q_{\text{Total}} = \sum_{J=1}^{\text{JCM}} \sum_{I=1}^{\text{ICM}} \sum_{k=1}^{\text{NGG}} Q_{\text{TIJ}}^k \Delta A_I \Delta Z_J$$

- 2) Total fissions

$$F_{\text{Total}} = \sum_{J=1}^{\text{JCM}} \sum_{I=1}^{\text{ICM}} F_{IJ} \Delta A_I \Delta Z_J$$

- 3) Total neutron source

$$Q_{\text{Total}} = \sum_{J=1}^{\text{JCM}} \sum_{I=1}^{\text{ICM}} \sum_{g=1}^{\text{NGN}} Q_{IJ}^g \Delta A_I \Delta Z_J$$

In addition, the NAGS program will prepare a group dependent neutron or photon source binary tape. This tape will contain either neutron, total photon, or fission product decay photon source for all mesh cells in the reactor geometry. These data (with minor intermediate processing to generate a tape with one logical record instead of NGN or NGG logical records) are compatible with distributed fixed source input requirements of the ODD-K discrete ordinate transport program. The options available to the NAGS user are controlled by input integer NPUN (Card Type 3). The program prepares a binary tape containing one of

the following sets of mesh cell data:

- 1) Total photon source for each group, k ,

$$Q_{TIJ}^k$$

- 2) Fission product decay photon source for each group, k ,

$$Q_{DIJ}^k = \Gamma_d^k F_{IJ}$$

- 3) Total neutron source for each group, g ,

$$Q_{IJ}^g = \chi^g Q_{IJ}$$

Special features are included in the NAGS program for the generation of a binary tape of source data. The user can increase the size of the mesh cell source data of a reactor geometry by placing zeros on the tape to the left, right, or top of the reactor geometry. This option, which positions the NAGS calculated source data in a larger mesh cell description, is included to permit, for example, a detailed neutron source calculation in the reactor core for use in a subsequent coarse reactor geometry. The detailed source calculation in the coarse geometry may not be possible in NAGS because of limited memory core storage; hence, this option can be used to reduce the flux data and then expand the source data. Further, this option, in conjunction with the mesh cell and flux redefining options, provides the user with considerable flexibility in running a linked neutron and photon transport problem using the ODD-K discrete ordinate transport program.

2.5.2 Neutron or Gamma Ray Dose Rates

At the completion of a NAGS mesh cell energy deposition calculation, the flux data at each mesh cell in the reactor geometry are used to calculate the neutron and photon dose rate at each of the mesh cells. This calculation of the neutron and photon dose rate follows:

- 1) Neutron dose rate

$$D_{NIJ} = \sum_{g=1}^{NGN} K_D^g \phi_{IJ}^g$$

- 2) Photon dose rate

$$D_{PIJ} = \sum_{k=1}^{NGG} K_D^k \phi_{IJ}^k$$

Since this operation is essentially a response function calculation, and is not stored in memory, the NAGS user can substitute other conversion factors in place of K_D^g or K_D^k , in the library to obtain mesh cell data as desired.

SECTION

3.0 INPUT DATA DESCRIPTION

The input data for a NAGS problem are subdivided into four sets of data. These four sets, which are the general, flux, library, and region data, are described in the following sections. A description of each set of data input and the routine (in parentheses) which reads this data is as follows:

1) General problem data - integer data pertaining to data or array dimensions (i.e., number of mesh, number of groups, etc.), problem title information, integer control words, flux normalization parameters, neutron fission parameters, and mesh cell specifications. (Subroutine MAIN and NAGS 1).

2) Flux data - input flux data required for NAGS operation including mode of input. (Subroutine NAGS 1).

3) Library data - neutron and photon multigroup quantities, and for each element: identification, physical constants and groupwise nuclear data. (Subroutine NAGS 2).

4) Region data - region title information, region composition by element or material, and depending upon the library option or type of calculation, region dependent multigroup neutron cross sections. (Subroutine NAGS 2).

A detailed description of the overall deck setup and input data requirements for a NAGS problem is included in the following sections:

3.1 GENERAL DATA

The initial data input to the NAGS program specifies: (1) the data array sizes of all input quantities, (2) the program input/output control options, (3) the flux normalization constants, (4) the fission neutron spectrum and the number of neutrons per fission event, and (5) the mesh cell dimensions of the problem geometry. These data are input as described in the following table:

<u>Card Type</u>	<u>FORTRAN Format</u>	<u>FORTRAN Variable</u>	<u>Meaning</u>
1	2413	ICT	Number of radial mesh intervals in the input flux solution.
		ICM	Number of redefined radial mesh intervals to be used in all calculations and output data.
		JCT	Number of axial* mesh intervals in the input flux solution.
		JCM	Number of redefined axial mesh intervals to be used in all calculations.
		NGN	Total number of neutron groups NOTE: If NTYPE = 3, then NGN is input as NGG since only photon fluxes are required input to the NAGS program when NTYPE = 3.
		NFAST	Number of fast neutron groups (Neutron kinetic energy is calculated for NFAST groups).
		NI	Number of fast neutron groups for photon productions from neutron inelastic scatter.
		NGG	Number of photon energy groups to be calculated
		NEL	Number of elements in the library data
		NTYPE	Program control word for the type of calculation to be performed. NTYPE = 1; Photon <u>or</u> neutron source calculation.

* Azimuthal coordinates in radians (R- θ input flux solutions) can be substituted for axial coordinates in centimeters (R-Z input flux solutions) without any program changes. All further references to axial will also imply azimuthal.

<u>Card Type</u>	<u>FORTRAN Format</u>	<u>FORTRAN Variable</u>	<u>Meaning</u>
			<p>NTYPE = 2: Combined neutron <u>and</u> photon energy deposition calculation.</p> <p>NTYPE = 3: Photon energy deposition calculation <u>only</u> (i.e., fission product decay heating).</p>
2	12A6	TITLE	Overall problem title (72 alphanumeric characters).
3	24I3	NCD	Not presently used by the program. NCD = 0.
		NBIN	Input flux data control word which specifies input mode of flux data for different types of calculations (refer to Section 3.2 for details).
		NLIB	<p>Library data option.</p> <p>NLIB = 0: Short library data option with region dependent neutron cross section data included with region input for each element, m, (refer to Section 3.3 for details).</p> <p>NLIB = 1: Standard MSFC option. Long library data option with region independent neutron cross section data included in the library for each element, m. (Refer to Section 3.3 for details on library.)</p>
		NEX NEX1	Source positioning indices in the radial direction for all calculated results. (See Section 2.5.1 for details.) These indices are provided to enable the user to perform a NAGS calculation on a section of a reactor geometry and then position this section of data in a different reactor or problem geometry.

<u>Card Type</u>	<u>FORTTRAN Format</u>	<u>FORTTRAN Variable</u>	<u>Meaning</u>
		NEX	The number of zero entries to the right of the NAGS calculated sources in each radial row.
		NEX1	The number of zero entries to the left of the NAGS calculated results in each radial row.
		ISTART	Starting radial mesh cell number in the NAGS input fluxes to be used in the redefinition of flux data. If in storage allocation, a flux edit is possible or desired for only a section of the input flux data then the user may specify $ISTART \neq 1$. ISTART is equal to the left mesh cell number of a section of the reactor geometry. The NAGS program redefines the flux data such that this left mesh cell number flux data will be the first mesh cell of the section. The mesh coordinates of the cells are altered to agree with the new mesh cell description.
		JSTART	Starting axial mesh cell number in the NAGS input to be used in redefinition of flux data. The discussion of ISTART is applicable to JSTART.
		NPUN	Binary tape output control word. Neutron or photon source data is placed on logical tape unit 9 which is MSFC IBSYS Version 13, Unit B-5. The tape contains NGN or NGG logical records each of size, $((NEX1 + ICM + NEX) * JCO)$. NPUN = 0: No binary data tape of sources is to be prepared. NPUN = 1: Neutron distributed source (Q_{IJ}^g) is to be placed on the binary tape of unit B-5. NPUN = 2: Total photon distributed source (Q_{TIJ}^k) is to be placed on the binary unit B-5.

<u>Card Type</u>	<u>FORTRAN Format</u>	<u>FORTRAN Variable</u>	<u>Meaning</u>
			NPUN = 3: Fission product decay photon distributed source (Q_{Dk}) is to be placed on the binary tape on unit B-5.
		JCO	Source positioning index in axial direction for all calculated results. (Refer to Section 2.5.1 for details.) This index is similar in operation to the NEX index in that the program generated B-5 binary tape has logical records of size $((NEX1 + ICM + NEX) * JCO)$ where the last $(NEX1 + ICM + NEX) * (JCO - JCM)$ pieces of data in each logical record are 0.0's.
4	(E12.5)	ZREF	Reference plane distance in inches from $Z = 0.0$. This input quantity adjusts all axial dimensions by $Z_s = ZREF - .3936 * Z_T$ so that energy deposition and source data can be printed relative to a Z plane other than at 0.0.
5	(6E12.5)	ENU	Average number of neutrons released per fission event, ν^9 . For photon flux input, ENU = 1.0.
		EFF	Fraction of fissions due to neutron fission events, EFF = 1.0, except where cross section data represents, (n, 2n) reactions by pseudo-fission. For ODD-K photon flux data, EFF = 1.0. For MSFC neutron cross section library data, EFF = 1.0.
		EFK	Multiplication factor, K_{eff} , of the ODD-K problem which provides input flux data. For photon flux data EFK = 1.0.
		VOLC	Volume of fissionable regions. For R-Z ODD-K input flux data, VOLC = 1.0.
		CONV	Conversion factor for input flux data in units of fissions per second.

<u>Card Type</u>	<u>FORTRAN Format</u>	<u>FORTRAN Variable</u>	<u>Meaning</u>
		PK	Area factors to account for partial geometrical solutions in ODD-K transport problems (i.e., PK = 1.0 for R-Z geometry but for R- θ problems, $PK = \frac{\theta}{2\pi}$.)
6	6E12.5	CHI	The fission neutron spectrum, χ^g (i.e., the fraction of a fission neutron born in each group, g). $\sum_{g=1}^{NGN} \chi^g \equiv 1.0$ NGN Values.
7	6E12.5	UNU	Neutron release (No. of neutrons) per neutron fission event by group, ν^g . NGN Values.
8	2413	IC	Mesh coordinate number of the right radial mesh coordinate of each redefined mesh cell. (e.g., if no redefining or reduction of mesh cell description is required, IC = 2, 3, 4, 5, 10, 11, 12, . . . ICT; or, if a reduction of two mesh intervals must be made, IC = 2, 4, 5, . . . 10, 12, . . . ICT, where 3 and 11 are removed.) There are ICM required values of IC.
9	2413	JC	Mesh coordinate number of the top mesh coordinate of each redefined mesh cell. The discussion of IC is applicable to JC. There are JCM required values of JC.
10	6E12.5	R	Radial mesh coordinate (line) dimensions for the input flux data (ICT + 1 values).
11	6E12.5	Z	Axial mesh coordinate (line) dimensions for the input flux data (JCT + 1 values).

3.2 FLUX DATA

Input flux data for the NAGS program are input as, either a FORTAN IV binary tape, or, as punched decimal data cards. The two modes, tape and cards, cannot be inter-mixed for combined neutron and photon calculations. Therefore, the user must provide the input flux data in a consistent form. Since there are three types of calculations which can be performed by the NAGS program and two flux input data modes, there exist five combinations of input control word combinations. The input control words NTYPE and NBIN which are input in the general problem data (Refer to Section 3.1.) determine the binary tape unit locations or punched data cards for each type of NAGS problem.

The input flux data for either binary tape or decimal data cards are assumed to be group dependent such that:

- 1) A logical tape record is ICT x JCT long and there are NGN (NTYPE = 1), NGG (NTYPE = 2 or 3), or NGN + NGG (NTYPE = 2) records on the binary tape, or
- 2) each neutron group or photon group is a set of punched decimal data cards and each new group begins on a new card.

The flux input data and the conditions of input mode are as follows:

<u>Card Type</u>	<u>FORTAN Format</u>	<u>FORTAN Variable</u>	<u>Meaning</u>
12	6E12.5 or FORTAN IV Binary Tape	SC	Input flux data NOTE: If the binary tape input mode is used, then card type 12, flux data, is deleted from the NAGS problem deck and binary tape (or tapes) must be submitted with the problem. <u>Conditions on input mode (which were input under general data)</u> NTYPE = 1: NBIN = 1: Neutron flux data as binary tape data on logical tape 11 which is MSFC IBSYS Version 13 unit B-6 NTYPE = 2: NBIN = 1: Neutron flux data as binary tape on logical tape 11. Photon flux data as binary tape data on logical tape 12 which is MSFC IBSYS Version 13 unit A-9.

<u>Card Type</u>	<u>FORTRAN Format</u>	<u>FORTRAN Variable</u>	<u>Meaning</u>
			NTYPE = 3: NBIN = 1: Photon flux data as binary tape data on logical tape 11. NTYPE = 2: NBIN = 2: Neutron and photon flux data as binary tape data on logical tape 11. NTYPE = 1, 2, or 3: NBIN = 3: Neutron and photon flux data as punched decimal data cards with each group of neutron or photon data starting on a new card (card type 12).

3.3 LIBRARY DATA

The library data for the NAGS program are a compilation of the nuclear and radiation data for the reactor geometry and for the elements in the reactor. These library data, which are assumed to be region independent, are obtained as a complete punched decimal data deck from the POINT program (Refer to Volume 2,) or can be input by the user.

The data are divided into two sections: referred to as general data and element data. The general data include neutron and photon group dependent quantities required for photon energy release from fission, neutron dose rate, neutron kinetic heating, and photon dose rate calculations. The element data are required for each element in the problem.

Each input data card is described in this section. Section 3.5 summarizes in table form, the order in which the general data, the element data, and the region data (Section 3.4) are input to the NAGS problem depending on the control word NLIB, and whether a source or energy deposition calculation is to be performed.

<u>Card Type</u>	<u>FORTRAN Format</u>	<u>FORTRAN Variable</u>	<u>Meaning</u>
<u>Data Cards 13 - 19 are the General Library Data</u>			
13	I3	NEL	Number of elements in the library
14	6E12.5	SFPS	Prompt fission photon spectrum for each photon energy group (Mev/fission) NGG values

<u>Card Type</u>	<u>FORTRAN Format</u>	<u>FORTRAN Variable</u>	<u>Meaning</u>
15	6E12.5	SFDS	Fission product decay photon spectrum for each photon energy group (Mev/fission) NGG values
16	6E12.5	DKG	Photon dose conversion factors for each photon energy group (Dose rate/Mev-cm ⁻² sec ⁻¹) NGG values
17	6E12.5	DK	Neutron dose conversion factors for each neutron group (Dose rate/n cm ⁻² sec ⁻¹) NGN values
18	6E12.5	DU	Letharge width ($\Delta \mu$) of each neutron group NGN values
19	6E12.5	DE	Energy width (ΔE) of each neutron group (Mev) NGN values
<u>Data Cards 20 - 26 are Required for Each Element</u>			
20	I3,4E12.5 , 10X, A6	NID	Element or nuclide identification number (a table of element identification numbers for the MSFC library are presented in volume 2 of this report.)
		AMU	Atomic weight of element (grams/gram-atom)
		ESS	Average fractional energy loss of a neutron elastic scattering event (isotropic scattering)
		ENA	Energy of charged particle (alpha) emission with neutron absorption (Mev/absorption)
		SA2200	Neutron absorption cross sections for thermal neutrons (2200 meter/second)
		LABEL	A six character descriptive title for the element
21	6E12.5	SINS	Neutron inelastic scatter photon energy spectra for each photon energy group arising from neutron inelastic scatter events occurring in the fast neutron groups (Mev/event)

<u>Card Type</u>	<u>FORTRAN Format</u>	<u>FORTRAN Variable</u>	<u>Meaning</u>
			NGG values for each of NI neutron groups with each NGG value defining a set of data starting on a new card
22	6E12.5	SS	Microscopic neutron elastic scatter cross sections for neutron kinetic energy deposition calculations. NFAST values
23	6E12.5	SNA	Microscopic neutron absorption cross sections for charged particle (alpha) emission NGN values
24	6E12.5	ECOS	Anisotropic correction factors for the NGN neutron energy groups to be used in neutron kinetic energy heating calculations. The factors account for anisotropy of elastic scattering as a fractional energy deposition per elastic scatter event ($0.0 \leq ECOS_m^g \leq 1.0$) NFAST values
25	6E12.5	SAS	Neutron radiative capture gamma ray spectra for gamma ray groups (Mev/capture). NGG values
26	6E12.5	SAG	Microscopic gamma ray mass energy absorption coefficients for gamma ray groups. ($cm^2/gram$). NGG values
The Following Data for each Element is Entered <u>Only</u> if: NLIB = 1			
26A	6E12.5	SF	Microscopic neutron fission cross sections, σ_{fm}^g . NGN values

<u>Card Type</u>	<u>FORTRAN Format</u>	<u>FORTRAN Variable</u>	<u>Meaning</u>
26B	6E12.5	SA	Microscopic neutron absorption cross sections (radiative capture), σ_{cm}^g NGN values
26C	6E12.5	SS	Microscopic neutron elastic scatter cross sections, σ_{em}^g NFAST values
26D	6E12.5	SIN	Microscopic neutron inelastic scatter cross sections for production of photons, σ_{sm}^g NI values

End of Element Data, Repeat From Card Type 20 for Each Element in the Library.

3.4 REGION* DATA

The final input to a NAGS problem are the region data which: (1) titles the region input and calculation data, (2) defines the location of the region in the two dimensional mesh cell description, (3) defines the number of elements in the region, (4) provides a program control word, and (5) depending on the type of NAGS problem (source or energy deposition), provides the material density and weight in the region, the element identification numbers, the element weight fractions or atom densities, and microscopic cross section data.

The description of a region in R, Z or R, θ geometry and the specification of the region external boundaries for a region are illustrated in Figure 8. These regions may be parts of a larger irregular region. The user must describe irregular regions as a composite of NAGS regions. The user must exercise caution in specifying regions so that region mesh overlays are avoided for photon source calculations since the NAGS region calculations are always initialized (all values set to 0.0) for each region and in photon source calculations the source data are saved for all mesh cells, for subsequent reactor geometry integrals, and for photon transport problems.

The input data cards for each region and each type of calculation are described below: These data cards are repeated for each NAGS region calculation in the problem. In addition, Section 3.5 summarizes in table form, the order in which the region data are input depending on the control word, NLIB, and whether a source or energy deposition calculation is to be performed.

*A region in the NAGS Code is defined as a rectangular (R, Z) or annular sector (R, θ) as illustrated in Figure 8.

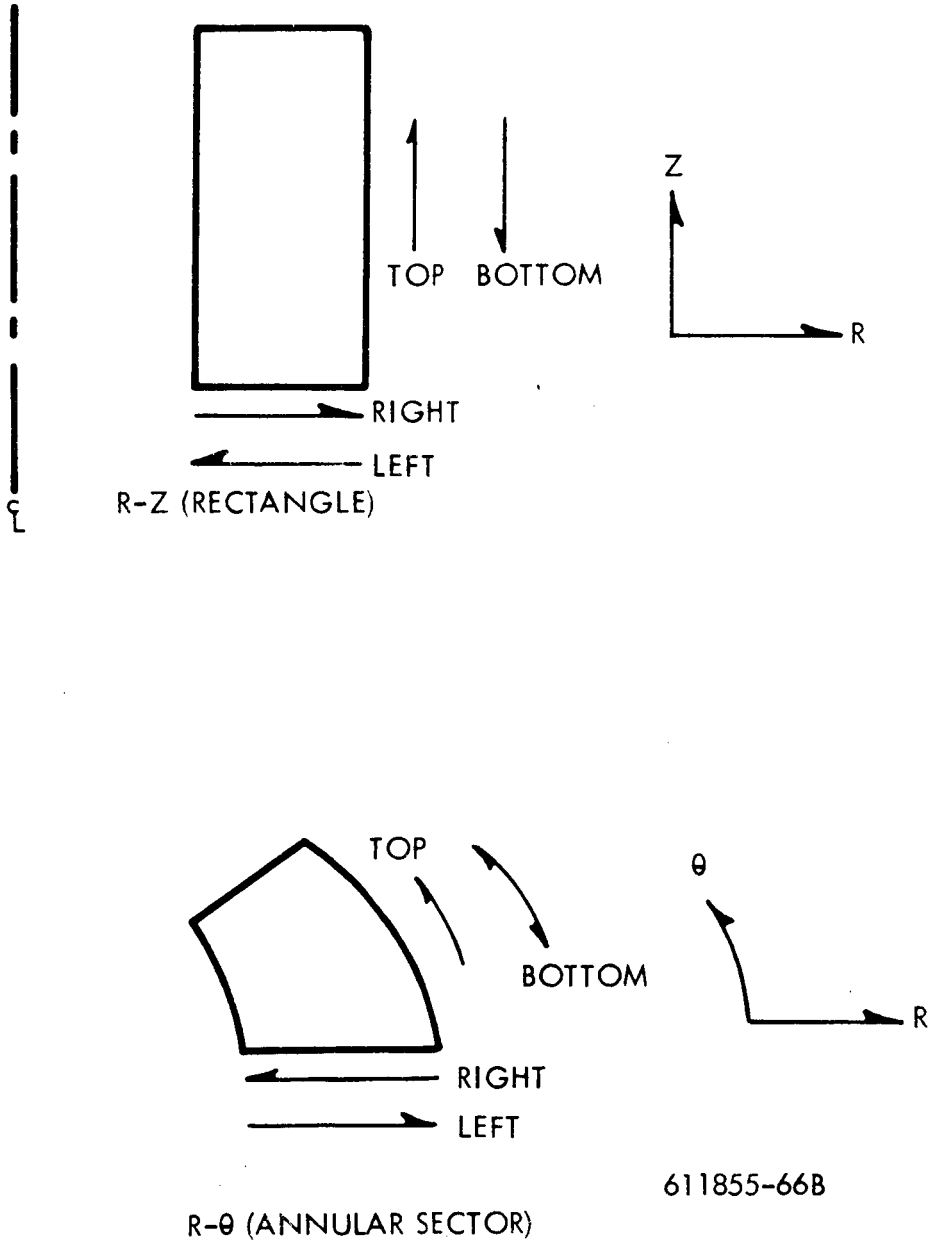


Figure 8. NAGS Region Geometry and Boundary Specification

<u>Card Type</u>	<u>FORTRAN Format</u>	<u>FORTRAN Symbol</u>	<u>Meaning</u>
27	(12A6)	ID	A 72 character title or description of the region
28	(613)	IS	IS is the radial mesh line number corresponding to the left boundary of the region (See Figure 8)
		IF	IF is the radial mesh line number corresponding to the right boundary of the region (See Figure 8)
		JS	JS is the axial (or angular) mesh line number corresponding to the bottom boundary of the region (See Figure 8)
		JF	JF is the axial (or angular) mesh line number corresponding to the top boundary of the region (See Figure 8)
		IEL	Number of elements in the region NOTE: If IEL is entered as a negative number, the program assumes that this region is identical in composition to the preceding region and the microscopic data cards (Card Types 26-28D) are deleted from the deck. The next data card will be the title card (CARD TYPE 27 of the next sub-region)
		IND	Control word. This data controls the sequence of operations which are to be performed at the completion of each region calculation. If, IND = 1, the program assumes another region follows and will return to read data (cards 27-28D) after calculations for the present region are completed. If, IND=2,

<u>Card Type</u>	<u>FORTRAN Format</u>	<u>FORTRAN Symbol</u>	<u>Meaning</u>
			the program assumes that this is the last region and when calculations are complete the program transfers control to the next NAGS operation, which is the calculation of region integrals and distributions.

The Following Set of Data (Card Types 29 and 30) Are Required Region Input Only for a NAGS Energy Deposition Calculation: NTYPE=1.

29	2E12.5	DGM	Density of the material (i.e., stainless steel, inconel, fueled graphite, beryllium) in the NAGS region (grams/cm ³ of the solid material)
		WTGM	Weight of the material in the NAGS region (kilograms)

There Are IEL (no. of Elements in Region) Required Data Cards Containing NLM, DNM:

30	I3, E12.5	NLM	Element identification number corresponding to the library element identification numbers NID.
		DNM	Weight fraction of the element NLM in the material described by DGM and WTGM (e.g., the weight fraction of Fe in stainless steel).

The Following Set of Data (Card Type 31) are Required Region Input Only For a NAGS Source Calculation: NTYPE = 1.

There are IEL (no. of elements in region)required sets of data (cards 28, 28A, 28B, 28C, 28D).

31	I3, E12.5	NLM	Element identification number corresponding to the library element identification number NID.
		DNM	Atom density of element in region (X10 ⁻²⁴)

<u>Card Type</u>	<u>FORTRAN Format</u>	<u>FORTRAN Symbol</u>	<u>Meaning</u>
The Following Neutron Cross Section Data are Input Only When NLIB = 0			
31A	6E12.5	SF	Microscopic neutron fission cross section, σ_{fm}^g . NGN values
31B	6E12.5	SA	Microscopic neutron absorption cross sections (radiative capture), σ_{em}^g . NGN values
31C	6E12.5	SS	Microscopic neutron elastic scatter cross sections, σ_{em}^g . NFAST values
31D	6E12.5	SIN	Microscopic neutron inelastic scatter cross sections for production of photons, σ_{sm}^g . NI values

3.5 SUMMARY OF LIBRARY AND REGION DATA

This section summarizes the three types of library and region data required as input to the NAGS program. The input is dependent on the controls NLIB and NTYPE. The three types of input discussed in Section 3.3 and 3.4 are: general library, element library and region input data. Table 1 and Figure 9 clarify the order in which these data are entered into the NAGS program.

TABLE 1

ORDER OF LIBRARY AND REGION INPUT DATA

If NLIB = 1 (Standard MSFC set-up), data are entered as follows:

Source Calculation (NTYPE = 1)

Cards 13 - 19 (general data)
 Cards 20 - 26D(data for element 1)
 Cards 20 - 26D(data for element 2)
 etc.
 Cards 27 - 28 (data for region 1)
 Card 31 (data for element 1, region 1)
 Card 31 (data for element 2, region 1)
 etc.
 Cards 27 - 28 (data for region 2)
 Card 31 (data for element 1, region 2)
 Card 31 (data for element 2, region 2)
 etc.

Heating Calculation (NTYPE = 2 or 3)

Cards 13 - 19 (general data)
 Cards 20 - 26D(data for element 1)
 etc.
 Cards 27 - 28 (data for region 1)
 Card 29* (data for region 1)
 Card 30* (data for element 1, region 1)
 Card 30* (data for element 2, region 1)
 etc.
 Cards 27 - 28 (data for region 2)
 Card 29* (data for region 2)
 Card 30* (data for element 1, region 2)
 Card 30* (data for element 2, region 2)
 etc.

If NLIB = 0, data are entered as follows:

Source Calculation (NTYPE = 1)

Cards 13 - 19 (general data)
 Cards 20 - 26 (data for element 1)
 Cards 20 - 26 (data for element 2)
 etc.
 Cards 27 - 28 (data for region 1)
 Cards 31 - 31D(data for element 1, region 1)
 Cards 31 - 31D(data for element 2, region 1)
 etc.
 Cards 27 - 28 (data for region 2)
 Cards 31 - 31D(data for element 1, region 2)
 Cards 31 - 31D(data for element 2, region 2)
 etc.

Heating Calculation (NTYPE = 2 or 3)

Cards 13 - 19 (general data)
 Cards 20 - 26 (data for element 1)
 Cards 20 - 26 (data for element 2)
 etc.
 Cards 27 - 28 (data for region 1)
 Card 29* (data for region 1)
 Card 30* (data for element 1, region 1)
 Card 30* (data for element 2, region 1)
 etc.
 Cards 27 - 28 (data for region 2)
 Card 29* (data for region 2)
 Card 30* (data for element 1, region 2)
 Card 30* (data for element 2, region 2)
 etc.

NOTE: Refer to Sections 3.3 and 3.4 for description of each data card.

*Cards marked with an asterisk must be inserted "by hand" at the proper location.
 All other data cards are punched as output from the POINT code.

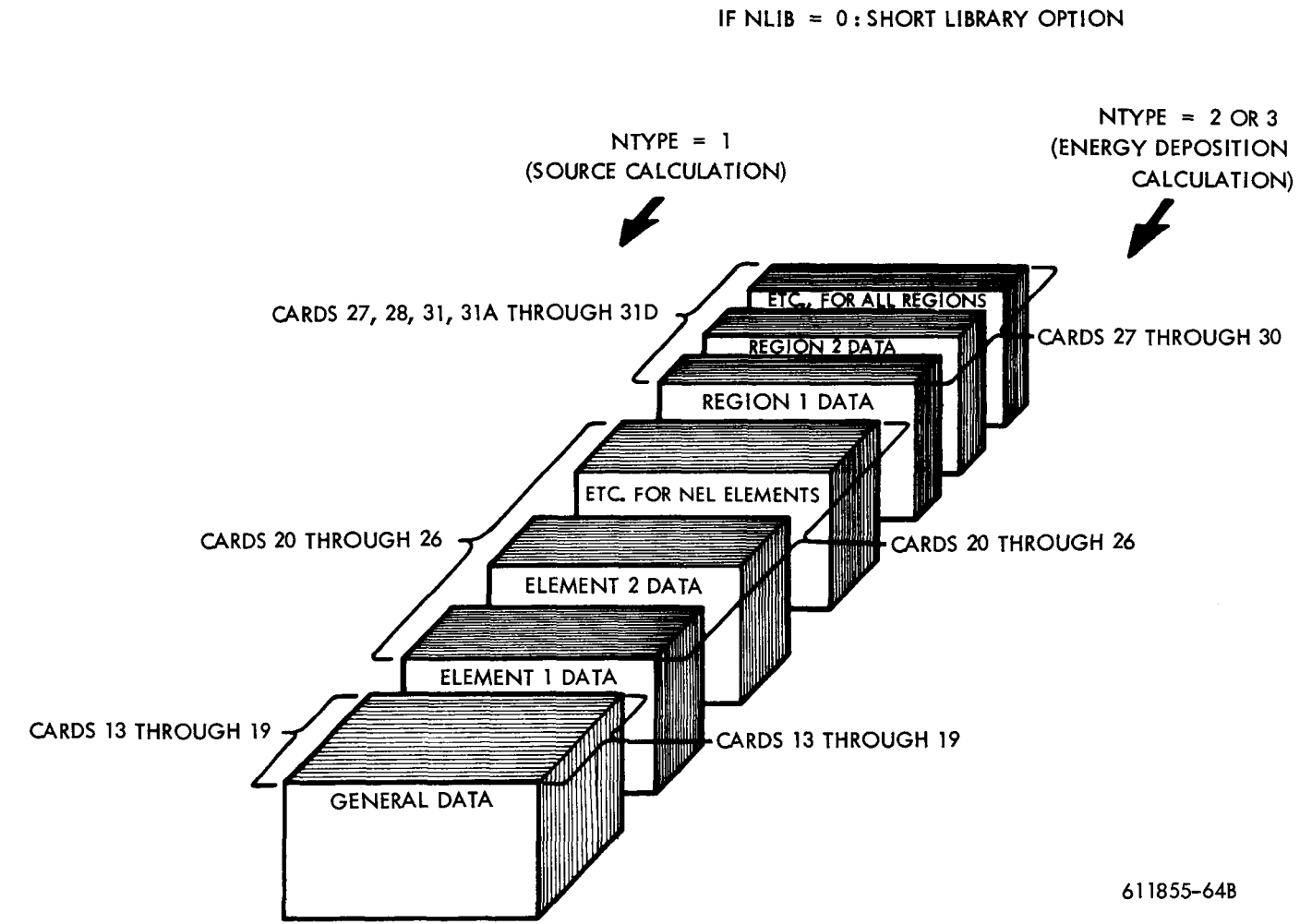
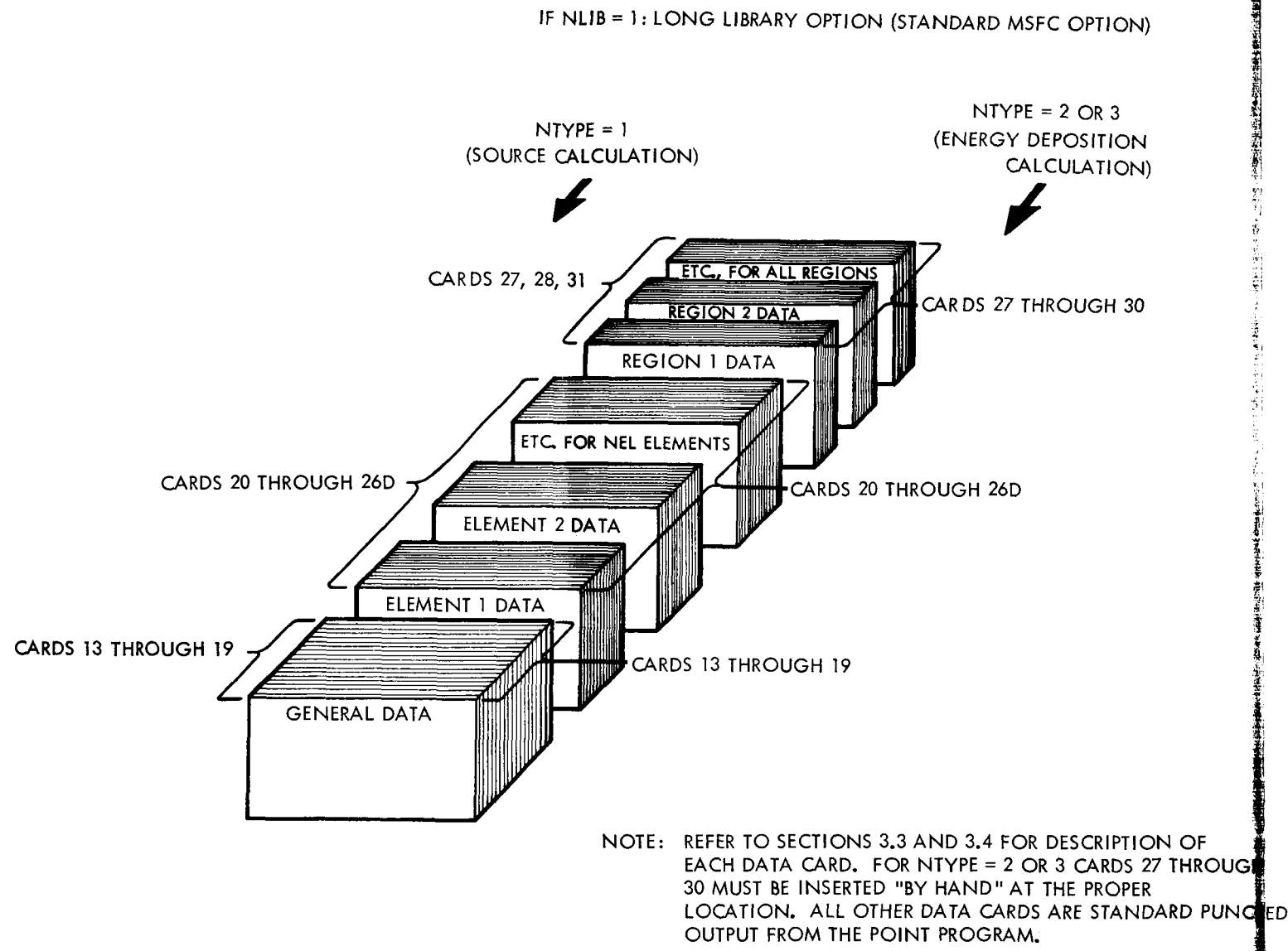


Figure 9. Deck Order of Library and Region Input

SECTION

4.0 PROGRAM STRUCTURE AND LOGIC

The NAGS program consists of five major routines and five minor routines written in FORTRAN IV. The program is structured for the IBM 7094 Model II IBSYS Version 13 monitor system using the overlay mode. Overlay is employed in the program to achieve maximum memory core storage for data without severe penalties in program logic or running time. In addition, the NAGS program uses the variable dimensioning capability in FORTRAN IV to "pack" data into a single data vector, hence, maximizing the program's utility by allowing a wide variety of problems. The program structure is illustrated in Figure 10 with the overlay levels A and B shown. A brief description of the operations performed in each routine are included in the figure to illustrate the structure of the program with respect to the data processing functions performed.

The logical flow of the NAGS program is presented in Figure 11. Simplified flow diagrams are included for the major routines only, since the minor routines are straight forward calculations or operations. The logical flow through NAGS is controlled by the MAIN routine. The NAGS1 through NAGS4 routines return to the MAIN routine for the next NAGS step.

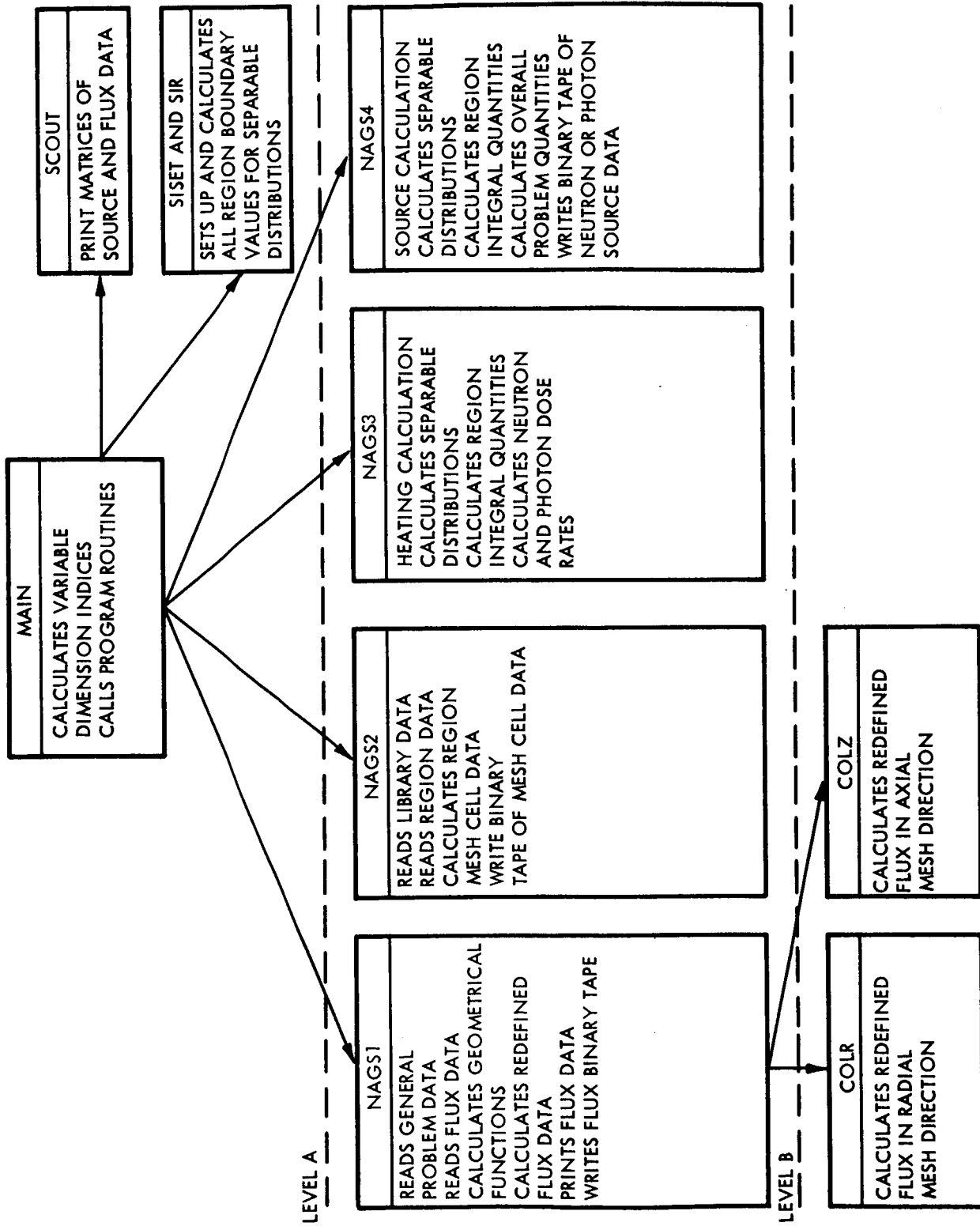


Figure 10. NAGS Program Structure

611855-69B

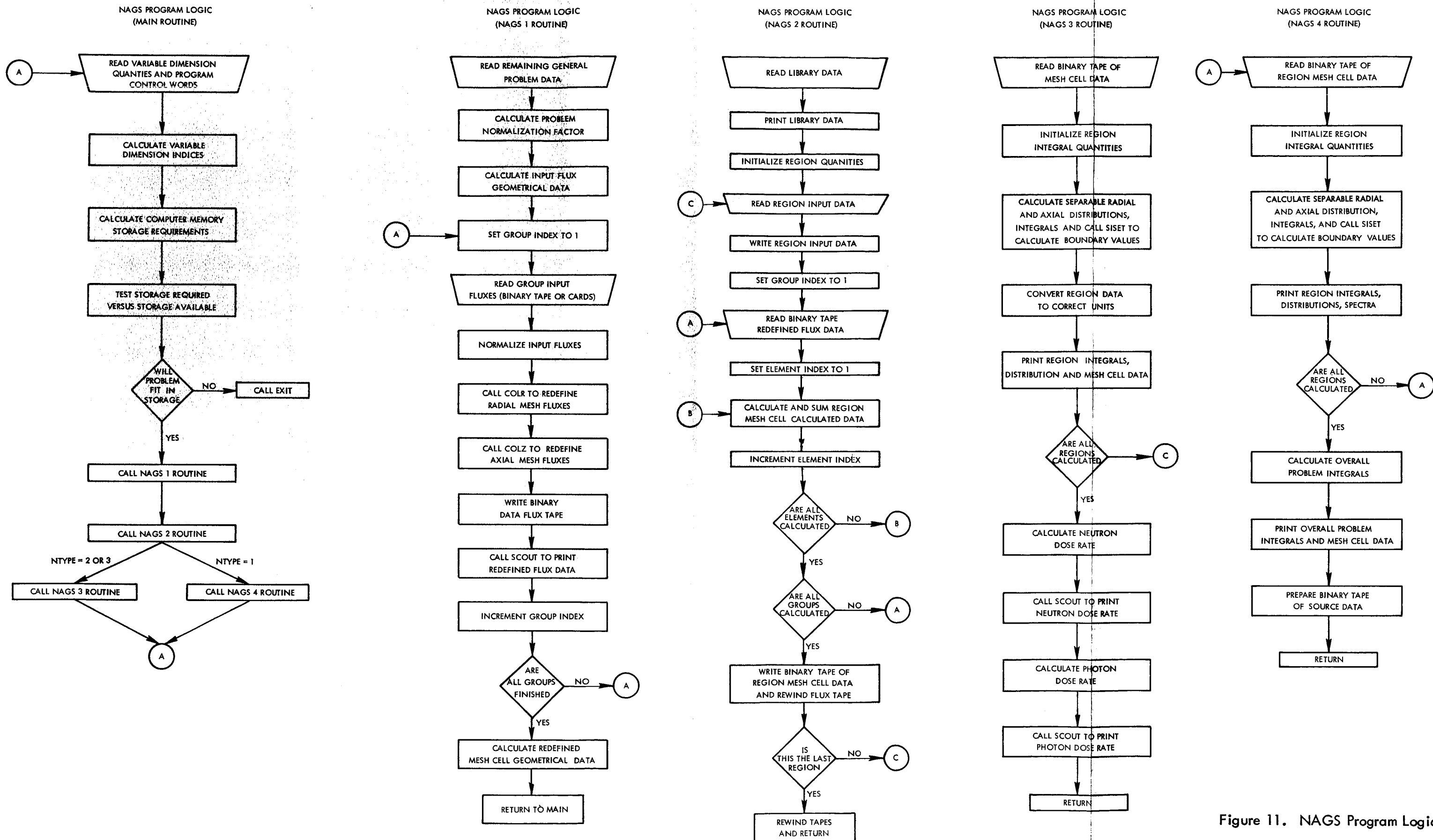


Figure 11. NAGS Program Logic

SECTION

5.0 OPERATING INSTRUCTIONS

The operating instructions and card deck setup for NAGS problems are similar to any production problem to be run under IBM IBSYS (Version 13) FORTRAN IV Monitor System. Problems may be run using either the binary object or source deck. The binary object deck is the preferred mode since compilation time is saved and the probability of damage for the source deck is eliminated. The deck setup for a binary object deck is described below and the deck setup with source decks is identical except the FORTRAN compiler card (\$IBFTC in columns 1 - 6) and program source decks are substituted for binary object decks.

NAGS PROGRAM DECK SETUP

1. An accounting card (dependent on computer installation)
2. A job card, \$JØB in columns 1 - 4.
3. A pause card, \$PAUSE in columns 1 - 6. (This card is required to permit the IBM 7094 operator to mount the required input tapes; hence, if no tapes are input, this card is not required.)
4. An execute card, \$EXECUTE, in columns 1 - 8 and IBJØB in columns 16 - 20.
5. An IBSYS job card, \$IBJØB, in columns 1 - 6 and GO, FIØCS, MAP in columns 16 - 27.
6. MAIN subroutine binary object deck (A FORTRAN loader card, \$IBLDR, in columns 1 - 6 is included in the punched binary object deck from the FORTRAN IV compiler).
7. Siset subroutine binary object deck.
8. SIR subroutine binary object deck.
9. SCØUT subroutine binary object deck.
10. An overlay origin card, \$ØRIGIN, in columns 1 - 7 and ALPHA, SYSUT3, REW in columns 16 - 31.
11. NAGS1 subroutine binary object deck.
12. An overlay origin card, \$ØRIGIN, in columns 1 - 7 and BETA, SYSUT3, REW in columns 16 - 31.

13. CØLZ subroutine binary object deck.
14. Same as card 12.
15. CØLR subroutine binary object deck.
16. Same as card 10.
17. NAGS2 subroutine binary object deck.
18. Same as card 10.
19. NAGS3 subroutine binary object deck.
20. Same as card 10.
21. NAGS4 subroutine binary object deck.
22. An entry control card, \$ENTRY, in columns 1 - 6.
23. A data control card, \$DATA, in columns 1 - 5.
24. NAGS Problem deck.
25. *Appropriate end of file cards to end job.*

This deck is then written off-line (card to tape) on an IBM Model 1401 or IBM Model 360/30 to manufacture a standard system input tape. Once the input has been written on tape, the machine operation is standard and the only operator action required is the tape mounting at the beginning of the job and tape dismounting at the completion of the job. The tapes used by NAGS are the following:

All BCD input	Logical Tape 5, MSFC IBSYS Version 13 A-2
All BCD output	Logical Tape 6, MSFC IBSYS Version 13 B-1
Flux Input Binary Tape	Logical Tape 11, MSFC IBSYS Version 13 B-6
Flux Input Binary Tape	Logical Tape 12, MSFC IBSYS Version 13 A-9
Redefined Flux Binary Work Tape	Logical Tape 10, MSFC IBSYS Version 13 A-6
Intermediate Binary Work Tape	Logical Tape 9, MSFC IBSYS Version 13 B-5
Overlay Tape	Logical Tape 3, MSFC IBSYS Version 13 A-4

The binary tapes always to be mounted at the beginning of a job are the input (5), work (9), work (10), and overlay (3) tapes. The standard save tape is the normal system BCD output (6) and tapes dependent on calculation type.

The binary tapes to be mounted and saved should be clearly labeled so that these tapes may be recalled for subsequent use as input tapes. The suggested tape labels for NAGS tapes are in parentheses in the following discussions. If the calculation is a source calculation, NTYPE=1, and the flux input mode is binary tape, NBIN=1, then a binary tape generated by the \emptyset DD-K neutron transport problem is a required input on logical tape 11. The save tapes from this source calculation are the binary tapes from logical tape 9 (NAGS SOURCE DATA) and logical tape 10 (NAGS REDEFINED FLUX DATA). If the calculation is an energy deposition calculation, NTYPE=2 or 3, and the flux input mode is binary tape, then three flux input modes exist. The first input mode (NBIN=1 for NTYPE=2) requires the binary tape (NAGS REDEFINED FLUX DATA) saved from logical tape 10 on the prior NAGS source calculation as a required input tape on logical tape 11. In addition, a second binary tape generated by the \emptyset DD-K photon transport problem is a required input on logical tape 13. The second input mode, NBIN=1 for NTYPE=3, requires the binary tape generated by the \emptyset DD-K photon transport problem as required input on logical tape 11. The third input mode, NBIN=2 for NTYPE=2, requires the binary tape (NAGS REDEFINED FLUX DATA) saved from logical tape 10 on the prior NAGS energy deposition, NTYPE=2, as a required input tape on logical tape 11.

The save tape from the energy deposition calculations is the binary tape from logical tape 10 (NAGS REDEFINED FLUX DATA).

When the deck and tape mounting and dismounting requests are set up in the preceding manner, the NAGS program will operate under normal IBSYS Version 13 Monitor SYSTEM control.

APPENDIX A

NAGS STORAGE ALLOCATION

The NAGS program uses the variable dimension capability of the FORTRAN IV programming language to allocate data storage in the program. This variable dimensioning, which occurs when input data is loaded, provides flexibility in using the program for a variety of problems without recompilation of the source program. There are 18,050 core locations available for input and calculated data. The total data storage locations required for a particular NAGS problem can be determined from the 7 input quantities on card 1 of the input data and the following four equations:

1. $X_1 = 2 * [(ICT * JCT) + (ICT + JCT + 1)]$
2. $X_2 = [(ICM * JCM) * (NGG + 2)] + [(ICM + JCM) * 10]$, for NTYPE = 1
or
 $X_2 = [(ICM * JCM) * 3] + [(ICM + JCM) * 10]$, for NTYPE = 2 or 3
3. $X_3 = [NEL * NGN * 3] + [(NI + 2) * NGG] + [(NFAST * 2) + NI] + 9$
4. $X_4 = [5 * NGG] + [4 * NGN]$

The summation of X's yields the total storage locations for a particular problem which must be less than 18,050. If this limit is exceeded, an error print is returned by the NAGS program and the problem is terminated.

APPENDIX B
PROGRAM SOURCE LISTING

```

$IBSYS
$JOB
SEXECUTE      IBJOB
              GO,NOMAP,PIOCS
$IBJOB       NOLIST,  DECK,NODD,M94/2,XR7
$IBFTC MAIN  MAIN PROGRAM FOR VARIABLE DIMENSION NAGS
C             COMMON ICT,ICM,JCT,JCM,NGN,NFAST,NI,NGG,NEL,IND,NTYPE
              COMMON NCD,NBIN,NLIB,NEX,NEXI,ISTART,JSTART,NPUN ,ZREF,JCO
              DIMENSION X(18050),IX(100)
              2 READ(5,1010) ICT,ICM,JCT,JCM,NGN,NFAST,NI,NGG,NEL,NTYPE
C THE QUANTITY NMAXRS IS THE MAXIMUM REAL STORAGE ALLOCATION FOR THE DATA
C VECTOR X AND ITS VALUE MUST CORRESPOND TO THE DIMENSION OF X
C THE QUANTITY NMAXIS IF THE MAXIMUM INTGER STORAGE ALLOCATION FOR THE
C DATA VECTOR IX AND ITS VALUE MUST CORRESPOND TO THE DIMENSION OF IX
NMAXRS=18050
NMAXIS = 100
I1 = ICT
I2 = ICM
I3 = JCT
I4 = JCM
I5 = NGN
I6 = NFAST
I7 = NI
I8 = NGG
I9 = NEL
I10 = ICT*1
I11 = ICM
I12 = JCT*1
I13 = ICM
I14 = JCM
I15 = I1*13
I16 = I1*13
I17 = NGG * 2
IF(NTYPE.GT.1) I17 = 3
C
C THE FOLLOWING FORTRAN STATEMENTS ARE THE VARIABLE DIMENSION SIZING
C
C J1 = 1
C R(ICT*1)
C J2 = J1 * I10
C Z(JCT*1)

```

```

1 MAIN
2 MAIN
3 MAIN
4 MAIN
5
6 MAIN
7 MAIN
8 MAIN
9 MAIN
10 MAIN
11
12 MAIN
13 MAIN
14 MAIN
15 MAIN
16 MAIN
17 MAIN
18 MAIN
19 MAIN
20 MAIN
21 MAIN
22 MAIN
23 MAIN
24 MAIN
25 MAIN
26 MAIN
27 MAIN
28 MAIN
29 MAIN
30 MAIN
31 MAIN
32 MAIN
33 MAIN
34 MAIN
35 MAIN
36 MAIN
37 MAIN
38 MAIN

```

39 MAIN
 40 MAIN
 41 MAIN
 42 MAIN
 43 MAIN
 44 MAIN
 45 MAIN
 46 MAIN
 47 MAIN
 48 MAIN
 49 MAIN
 50 MAIN
 51 MAIN
 52 MAIN
 53 MAIN
 54 MAIN
 55 MAIN
 56 MAIN
 57 MAIN
 58 MAIN
 59 MAIN
 60 MAIN
 61 MAIN
 62 MAIN
 63 MAIN
 64 MAIN
 65 MAIN
 66 MAIN
 67 MAIN
 68 MAIN
 69 MAIN
 70 MAIN
 71 MAIN
 72 MAIN
 73 MAIN
 74 MAIN
 75 MAIN
 76 MAIN
 77 MAIN
 78 MAIN
 79 MAIN
 80 MAIN

J3 = J2 * I12
 C RSF(ICM)
 J4=J3*I2
 C ZSF(JCM)
 J5= J4*I4
 C RS(ICM)
 J6=J5*I2
 C ZS(JCM)
 J7=J6*I4
 C VOLR(ICT)
 J8 = J7 * I1
 C VOLZ(JCT)
 J9 = J8 * I3
 C SC(ICT,JCT)
 J10=J9*I1*I3
 C TEMP(ICT,JCT)
 J11=J10*I1*I3
 C SG(ICM,JCM,NGG*2) OR SG(ICM,JCM*3)
 J12=J11*I2*I4*I17
 C UNU(NGN)
 J13 = J12 * I5
 C CHI(NGN)
 J14 = J13 * I5
 C SFPS(NGG)
 J15 = J14 * I8
 C SFDS(NGG)
 J16 = J15 * I8
 C DNM(NEL)
 J17 = J16 * I9
 C SA(NGN,NEL)
 J18 = J17 * I5*I9
 C SF(NGN,NEL)
 J19 = J18 * I5*I9
 C SIN(NI,NEL)
 J20 = J19 * I7*I9
 C SS(NFAST,NEL)
 J21 = J20 * I6*I9
 C SAS(NGG,NEL)
 J22 = J21 * I8*I9
 C SINS(NGG,NI,NEL)
 J23 = J22 * I8*I7*I9
 C AMU(NEL)



01 MAIN
02 MAIN
03 MAIN
04 MAIN
05 MAIN
06 MAIN
07 MAIN
08 MAIN
09 MAIN
90 MAIN
91 MAIN
92 MAIN
93 MAIN
94 MAIN
95 MAIN
96 MAIN
97 MAIN
98 MAIN
99 MAIN
100 MAIN
101 MAIN
102 MAIN
103 MAIN
104 MAIN
105 MAIN
106 MAIN
107 MAIN
108 MAIN
109 MAIN
110 MAIN
111 MAIN
112 MAIN
113 MAIN
114 MAIN
115 MAIN
116 MAIN
117 MAIN
118 MAIN
119 MAIN
120 MAIN
121 MAIN
122 MAIN

J24 = J23 + I9
C ESS(NEL)
J25 = J24 + I9
C ENA(NEL)
J26 = J25 + I9
C SA2200(NEL)
J27 = J26 + I9
C LABEL(NEL)
J28 = J27 + I9
C SNA(NGN,NEL)
J29 = J28 + I5+I9
C ECOS(NFAST,NEL)
J30 = J29 + I6+I9
C DK(NGN)
J31=J30+I5
C DE(NGN)
J32 = J31 + I5
C DU(NGN)
J33 = J32 + I5
C SAG(NGG,NEL)
J34 = J33 + I8+I9
C TSG(NGG)
J35 = J34 + I8
C RI(ICM)
J36 = J35 + I2
C ZI(ICM)
J37 = J36 + I4
C SGR(ICM*3)
J38 = J37 + I2*3
C SGT(ICM*3)
J39 = J38 + I2*3
C SGR(JCM*3)
J40 = J39 + I4*3
C SGL(JCM*3)
J41 = J40 + I4*3
C RSN(ICM)
J42=J41+I2
C ZSN(JCM)
J43=J42+I4
C DKG(NGG)
J44 = J43 + I8
C STC(NEL)

```

J45 = J44 * I9
J46= J45*I9
C STI(M)
  J47 =J46 *I9
  J49= J47
  J50 = 1
C IC(ICM)
  J51 = J50 * I2
C JC(JCM)
  J52 = J51 * I4
C NID(NEL)
  J53 = J52 * I9
C NLM(NEL)
  J54 = J53 * I9
C
  NTEST = J49
  NTEST2= J54
C
  NTEST1 = NTEST - NMAXRS
  NTEST3 = NTEST2 - NMAXIS
  WRITE(6,1000)I1,I2,I3,I4,I5,I6,I7,I8,I9,I10,I11,I12,I13,I14,I15,
  I116,I17,J1,J2,J3,J4,J5,J6,J7,J8,J9,J10,J11,J12,J13,J14,J15,J16,
  2J17,J18,J19,J20,J21,J22,J23,J24,J25,J26,J27,J28,J29,J30,J31,J32,
  3J33,J34,J35,J36,J37,J38,J39,J40,J41,J42,J43,J44,
  4J49,J50,J51,J52,J53,J54
  1000 FORMAT(70H)THE STORAGE REQUIREMENTS ARE DETERMINED FROM THE I ARR
  1Y AS FOLLOWS //(I7I6),/79H AND THE STARTING LOCATIONS OF EACH
  2VARIABLE ARE DETERMINED FROM THE J ARRAY //(I7I6)
  IF(NTEST1.LE.0) GO TO 6
  4 WRITE (6,1002) NTEST1
  1002 FORMAT (31H DIMENSION ERROR. OVERFLOW OF ,I5, 10H LOCATIONS)
  CALL EXIT
  6 IF(NTEST3.LE.0) GO TO 10
  8 WRITE (6,1004) NTEST3
  1004 FORMAT (31H FIXED POINT DIMENSION ERROR ,I5, 10H LOCATIONS)
  CALL EXIT
  10 WRITE(6,1006) NTEST,NMAXRS,NTEST2,NMAXIS
  1006 FORMAT(1H1,///.6X,31H YOUR NAGS IV PROBLEM HAS USED 15.27H LOCATION
  1NS OF THE AVAILABLEI6,31H REAL NUMBER STORAGE LOCATIONS //,6X,10H
  2AND USED 15.27H LOCATIONS OF THE AVAILABLEI4,33H INTEGER NUMBER ST
  3ORAGE LOCATIONS )
  NLINK=1
  MAIN 123
  MAIN 125
  MAIN 126
  MAIN 127
  MAIN 128
  MAIN 129
  MAIN 130
  MAIN 131
  MAIN 132
  MAIN 133
  MAIN 134
  MAIN 135
  MAIN 136
  MAIN 137
  MAIN 138
  MAIN 139
  MAIN 140
  MAIN 141
  MAIN 142
  MAIN 143
  MAIN 144
  MAIN 145
  MAIN 146
  MAIN 147
  MAIN 148
  MAIN 149
  MAIN 150
  MAIN 151
  MAIN 152
  MAIN 153
  MAIN 154
  MAIN 155
  MAIN 156
  MAIN 157
  MAIN 158
  MAIN 159
  MAIN 160
  MAIN 161
  MAIN 162
  MAIN 163
  MAIN 164
  MAIN 165

```

```

WRITE(6,1008) NLINK
CALL NAG1(
1 X(J1) , X(J2) , X(J3) , X(J4) , X(J5) , X(J6) , X(J7) ,
1 X(J8) , X(J9) , X(J10) , X(J11) , X(J12) , X(J13) , X(J14) ,
1 X(J15) , X(J16) , X(J17) , X(J18) , X(J19) , X(J20) , X(J21) ,
1 X(J22) , X(J23) , X(J24) , X(J25) , X(J26) , X(J27) , X(J28) ,
1 X(J29) , X(J30) , X(J31) , X(J32) , X(J33) , X(J34) , X(J35) ,
1 X(J36) , X(J37) , X(J38) , X(J39) , X(J40) , X(J41) , X(J42) ,
1 X(J43) , X(J44) , X(J45) , X(J46) ,
1 IX(J50) , IX(J51) , IX(J52) , IX(J53) ,
1 I1 , I2 , I3 , I4 , I5 , I6 , I7 , I8 , I9 , I10 , I11 ,
1 I12 , I13 , I14 , I15 , I16 , I17 )
12 NLINK#2
WRITE(6,1008) NLINK
CALL NAG2(
1 X(J1) , X(J2) , X(J3) , X(J4) , X(J5) , X(J6) , X(J7) ,
1 X(J8) , X(J9) , X(J10) , X(J11) , X(J12) , X(J13) , X(J14) ,
1 X(J15) , X(J16) , X(J17) , X(J18) , X(J19) , X(J20) , X(J21) ,
1 X(J22) , X(J23) , X(J24) , X(J25) , X(J26) , X(J27) , X(J28) ,
1 X(J29) , X(J30) , X(J31) , X(J32) , X(J33) , X(J34) , X(J35) ,
1 X(J36) , X(J37) , X(J38) , X(J39) , X(J40) , X(J41) , X(J42) ,
1 X(J43) , X(J44) , X(J45) , X(J46) ,
1 IX(J50) , IX(J51) , IX(J52) , IX(J53) ,
1 I1 , I2 , I3 , I4 , I5 , I6 , I7 , I8 , I9 , I10 , I11 ,
1 I12 , I13 , I14 , I15 , I16 , I17 )
IF (NTYPE.EQ.1) GO TO 14
NLINK#3
WRITE(6,1008) NLINK
CALL NAG3(
1 X(J1) , X(J2) , X(J3) , X(J4) , X(J5) , X(J6) , X(J7) ,
1 X(J8) , X(J9) , X(J10) , X(J11) , X(J12) , X(J13) , X(J14) ,
1 X(J15) , X(J16) , X(J17) , X(J18) , X(J19) , X(J20) , X(J21) ,
1 X(J22) , X(J23) , X(J24) , X(J25) , X(J26) , X(J27) , X(J28) ,
1 X(J29) , X(J30) , X(J31) , X(J32) , X(J33) , X(J34) , X(J35) ,
1 X(J36) , X(J37) , X(J38) , X(J39) , X(J40) , X(J41) , X(J42) ,
1 X(J43) , X(J44) , X(J45) , X(J46) ,
1 IX(J50) , IX(J51) , IX(J52) , IX(J53) ,
1 I1 , I2 , I3 , I4 , I5 , I6 , I7 , I8 , I9 , I10 , I11 ,
1 I12 , I13 , I14 , I15 , I16 , I17 )
14 IF (NTYPE.GT.1) GO TO 16
NLINK#4
WRITE(6,1008) NLINK

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MAIN 166
MAIN 167
MAIN 168
MAIN 169
MAIN 170
MAIN 171
MAIN 172
MAIN 173
MAIN 174
MAIN 175
MAIN 176
MAIN 177
MAIN 178
MAIN 179
MAIN 180
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MAIN 182
MAIN 183
MAIN 184
MAIN 185
MAIN 186
MAIN 187
MAIN 188
MAIN 189
MAIN 190
MAIN 191
MAIN 192
MAIN 193
MAIN 194
MAIN 195
MAIN 196
MAIN 197
MAIN 198
MAIN 199
MAIN 200
MAIN 201
MAIN 202
MAIN 203
MAIN 204
MAIN 205
MAIN 206
MAIN 207

```



```

CALL NAG4 (
1 X(J1) , X(J2) , X(J3) , X(J4) , X(J5) , X(J6) , X(J7) ,
1 X(J8) , X(J9) , X(J10) , X(J11) , X(J12) , X(J13) , X(J14) ,
1 X(J15) , X(J16) , X(J17) , X(J18) , X(J19) , X(J20) , X(J21) ,
1 X(J22) , X(J23) , X(J24) , X(J25) , X(J26) , X(J27) , X(J28) ,
1 X(J29) , X(J30) , X(J31) , X(J32) , X(J33) , X(J34) , X(J35) ,
1 X(J36) , X(J37) , X(J38) , X(J39) , X(J40) , X(J41) , X(J42) ,
1 X(J43) , X(J44) , X(J45) , X(J46) ,
1 IX(J50) , IX(J51) , IX(J52) , IX(J53) ,
1 I1 , I2 , I3 , I4 , I5 , I6 , I7 , I8 , I9 , I10 , I11 ,
1 I12 , I13 , I14 , I15 , I16 , I17 )
      16 GO TO 2
1008 FORMAT(/17H PROBLEM IN LINK I3)
1010 FORMAT(24I3)
      END
SIBFTC SIBSETR NULIST, DECK,NODD,M94/2,XR7
SUBROUTINE S1SET(SGLT,SGRT,SGBT,SGTP,R,RI,Z,I1,I2,I3,I4,I10,
1 I12,I13,I14,IRS,IR1,IZS,I71,K,RS,ZS )
DIMENSION SGLT(3),SGRT(3),SGBT(3),SGTP(3)
DIMENSION R(I10),RI(I2),Z(I12),ZI(I4),RS(I2),ZS(I4)
DIMENSION A(3),X(3)
IRF1 = IR1 + 1
IRS1 = IRS + 1
IRF2 = IR1 - 1
IRS2 = IRS - 1
IR1 = IR1 - IRS + 1
NT = 1
NK = 1
A(2) = RS(IRS)
A(3) = SGLT(K)
X(1) = R(IRS)
X(2) = RI(IRS)
X(3) = RI(IRS2)
IF(SGLT(K).GT.0.0) GO TO 2
NK = 3
A(3) = RS(IRS1)
X(3) = RI(IRS1)
IF(III.EQ.1) A(3) = SGRT(K)
      2 GO TO I4
      4 SGLT(K) = A(1)
      NT = 2
      NK=1
  
```

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MAIN 209
MAIN 209
MAIN 210
MAIN 211
MAIN 212
MAIN 213
MAIN 214
MAIN 215
MAIN 216
MAIN 217
MAIN 218
  
```

```

MAIN 221
MAIN 222
MAIN 223
S1SET 1
S1SET 2
S1SET 3
S1SET 4
S1SET 5
S1SET 6
S1SET 7
S1SET 8
S1SET 9
S1SET 10
S1SET 11
S1SET 12
S1SET 13
S1SET 14
S1SET 15
S1SET 16
S1SET 17
S1SET 18
S1SET 19
S1SET 20
S1SET 21
S1SET 22
S1SET 23
S1SET 24
S1SET 25
S1SET 26
S1SET 27
  
```

SISET 28
SISET 29
SISET 30
SISET 31
SISET 32
SISET 33
SISET 34
SISET 35
SISET 36
SISET 37
SISET 38
SISET 39
SISET 40
SISET 41
SISET 42
SISET 43
SISET 44
SISET 45
SISET 46
SISET 47
SISET 48
SISET 49
SISET 50
SISET 51
SISET 52
SISET 53
SISET 54
SISET 55
SISET 56
SISET 57
SISET 58
SISET 59
SISET 60
SISET 61
SISET 62
SISET 63
SISET 64
SISET 65
SISET 66
SISET 67
SISET 68
SISET 69

```

A(2) = RS(IR1)
A(3) = SGRT(K)
X(1) = R(IHF1)
X(2) = RI(IR1)
X(3) = RI(IRF1)
IF(SGRT(K).GT.0.0) GO TO 6
NK = 4
A(2) = RS(IHF2)
A(3) = RS(IR1)
X(2) = RI(IHF2)
X(3) = RI(IR1)
IF(III.GT.1) GO TO 6
A(2) = SGLT(K)
X(2) = R(IHF2)
6 GO TO 14
8 SGRT(K) = A(1)
NK = 2
NT = 3
IZF1 = IZ1 + 1
IZS1 = IZS + 1
IZF2 = IZ1 - 1
IZS2 = IZS - 1
III = IZ1 - IZS + 1
A(2) = ZS(IZS)
A(3) = SGRT(K)
X(1) = Z(IZS)
X(2) = ZI(IZS)
X(3) = ZI(IZS2)
IF(SGRT(K).GT.0.0) GO TO 10
NK = 5
A(3) = ZS(IZS)
A(2) = ZS(IZS)
X(2) = ZI(IZS1)
X(3) = ZI(IZS)
IF(III.GT.1) GO TO 10
A(2) = SGTP(K)
10 GO TO 14
12 SGRT(K) = A(1)
NT = 4
NK = 2
A(2) = ZS(IZ1)
A(3) = SGTP(K)

```



```

WRITE (6,1006) (NAME(I),I=1,3),K
DO 2 ISTAR = 1,14,8
  ISTOP=ISTAR + 7
  ISTOP = MIN0(I4,ISTOP)
  WRITE(6,1004)(I1,II=ISTAR,ISTOP)
  WRITE(6,1002) (Z1(II),II=ISTAR,ISTOP)
DO 2 J=1,13
  2 WRITE(6,1000) J,HI(J),(SC(J,I),I=ISTAR,ISTOP)
1000 FORMAT(I4,F8.2,1P8E12.4)
1002 FORMAT(12X,8(2X,F8.2,2X))
1004 FORMAT(4H01/J,8X,8(I6,6X))
1006 FORMAT(1H1,3A6,11H GROUP NO.,=,16)
RETURN
END
$ORIGIN ALPHA,SY3UT3,REW
$IBFTC NAGS1 NOLIST, DECK,NOOD,M94/2,XR7
SUBROUTINE NAG1( R,Z,RSF,ZSF,RS,ZS,VOLR,VOLZ,SC,TEMP,SG,UNU,CHI,
1SFPS,SFDS,DNM,SA,SF,SIN,SS,SAS,SINS,AMU,ESS,ENA,SA2200,LABEL,SNA,
2ECOS,DK,DE,DU,SAG,TSG,RI,ZI,SG8,SGT,SGL,SGR,RSN,ZSN,DKG,STC,
2STF,STI,
3IC,JC,NID,NLM,I1,I2,I3,I4,I5,I6,
4I7 , I8 , I9 , I10 , I11 , I12 , I13 ,
5I14 , I15 , I16 , I17 ,
COMMON ICT,ICM,JCT,JCM,NGN,NFAST,NI,NGG,NEL,IND,NTYPE
COMMON NCD,NBIN,NLIB,NEX,NEX1,ISTART,JSTART,NPUN ,ZREF,JCO
DIMENSION RSF(I13),ZSF(I14),R(I10),Z(I12),RSN(I13),ZSN(I14),
1DKG(I8),RS(I13),ZS(I14),VOLR(I1),VOLZ(I3),SC(I1,I3),TEMP(I15),
2SG(I13,I14,I17),UNU(I5),CHI(I5),SFPS(I8),SFD5(I8),DNM(I9),
3SA(I5,I9),SF(I5,I9),SIN(I7,I9),SS(I6,I9),SAS(I8,I9),
4SINS(I8,I7,I9),AMU(I9),ESS(I9),ENA(I9),SA2200(I9),LABEL(I9),
5SNA(I5,I9),ECOS(I6,I9),DK(I5),DE(I5),DU(I5),SAG(I8,I9),TSG(I8),
6HI(I2),ZI(I4),SGI(I2,3),SG8(I2,3),SGL(I4,3),SGR(I4,3),IC(I2),
7JC(I4),NID(I9),NLM(I9),ID(I2),TITLE(I2),BUF(27)
8,STC(I9) , STF(I9) , STI(I9)
2 CONTINUE
REWIND 10
REWIND 11
REWIND 12
READ(5,1032)(TITLE(I),I=1,12)
READ (5,1028)NCD,NBIN,NLIB,NEX,NEX1,ISTART,JSTART,NPUN,JCO
HEAD (5,1000) ZREF
1000 FORMAT(6E12.5)

```

SCOUR 4
SCOUR 5
SCOUR 6
SCOUR 7
SCOUR 8
SCOUR 9
SCOUR 10
SCOUR 11
SCOUR 12
SCOUR 13
SCOUR 14
SCOUR 15
SCOUR 16
SCOUR 17

NAGS 1
NAGS 2
NAGS 3
NAGS 4
NAGS 5
NAGS 6
NAGS 7
NAGS 8
NAGS 9
NAGS 10
NAGS 11
NAGS 12
NAGS 13
NAGS 14
NAGS 15
NAGS 16
NAGS 17
NAGS 18
NAGS 19
NAGS 20
NAGS 21
NAGS 22

NAGS 23
NAGS 24
NAGS 25
NAGS 26

```

READ (5,1030)ENU,EFF,EFK,VOLC,CONV,PK
READ (5,1030)(CHI(I),I=1,NGN)
READ (5,1030)(UNU(I),I=1,NGN)
READ (5,1028)(IC(I),I=1,ICM)
READ (5,1028)(JC(I),I=1,JCM)
READ (5,1030)(R(I),I=1,I10)
READ (5,1030)(Z(I),I=1,I12)
WRITE(6,1008)(TITLE(I),I=1,I2)
WRITE(6,1026)
WRITE(6,1010) ICT,ICM,JCT,JCM,NCD,NGN,NGG,NEL
WRITE(6,1012)NBIN,NL1B,NPUN,NEX,NEX1,ISTART,JSTART
WRITE(6,1026)
WRITE(6,1014)(IC(I),I=1,ICM)
WRITE(6,1016)(JC(I),I=1,JCM)
WRITE(6,1018)(R(I),I=1,I10)
WRITE(6,1020)(Z(I),I=1,I12)
WRITE(6,1024)(I,UNU(I),CHI(I),I=1,NGN)
WRITE(6,1002) ZREF
1002 FORMAT(1H0,10X,27HZERO REFERENCE PLANE IS AT F12.6,7H INCHES )
PNORM=ENU*CONV/(PK*EFF*EFK*VOLC)
WRITE(6,1022) ENU,EFF,EFK,VOLC,PK,CONV,PNORM
DO 4 J=1,I1
DO 4 I=1,I3
4 SC(I,J)=0.0
NGT = 15
IF (NTYPE.EQ.2) NGT = 15*18
IF (NTYPE.EQ.3) NGT = 18
C CALCULATE MESH INTERVAL AREAS AND VOLUMES ON ICT * JCT MESH
DO 6 I=1,ICT
6 VOLR(I) = 3.1415927*(R(I+1)*R(I+1)-R(I)*R(I))
DO 8 J=1,JCT
8 VOLZ(J) = Z(J+1)-Z(J)
C CALCULATE COLLAPSED MESH INTERVAL MIDPOINTS
IK = ISTART
DO 10 I=1,ICM
IL = IC(I)
RI(I) = 0.5*(R(IL)+R(IK))
10 IK = IC(I)
J1 = JSTART
DO 12 J = 1,JCM
J2 = JC(J)
ZI(J) = 0.5*(Z(J2)+Z(J1))
NAGS 27
NAGS 28
NAGS 29
NAGS 30
NAGS 31
NAGS 32
NAGS 33
NAGS 34
NAGS 35
NAGS 36
NAGS 37
NAGS 38
NAGS 39
NAGS 40
NAGS 41
NAGS 42
NAGS 43
NAGS 44
NAGS 45
NAGS 46
NAGS 47
NAGS 48
NAGS 49
NAGS 50
NAGS 51
NAGS 52
NAGS 53
NAGS 54
NAGS 55
NAGS 56
NAGS 57
NAGS 58
NAGS 59
NAGS 60
NAGS 61
NAGS 62
NAGS 63
NAGS 64
NAGS 65
NAGS 66
NAGS 67
NAGS 68

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```

12 J1 = JC(J)
   K=1
   WHEN ODDK PROVIDES A BINARY FLUX TAPE
14 READ(12)((SC(I,J),I=1,J1),J=1,I3)
   PPP = PNORM
   IF (NTYPE.EQ.2.AND.K.GT.I5) PPP = 1.0
   IF (NTYPE.EQ.3) PPP = 1.0
   DO 32 I=1,I1
   DO 32 J=1,I3
32 SC(I,J)=ABS(SC(I,J))*PPP
C CALCULATE COLLAPSED FLUXES IN AN ICM * JCM MESH FROM THE ICT * JCT
C VALUES
   IF(ICM.LT.ICT) CALL COLR(SC,TEMP,VOLR,VOLZ,IC,JC,I1,I3,I1,I3,I2,I2,
1I4)
   IF(JCM.LT.JCT) CALL COLZ(SC,TEMP,VOLR,VOLZ,IC,JC,I1,I3,I1,I3,I2,I2,
1I4)
   WRITE (10)((SC(I,J),I=1,I2),J=1,I4)
   IF(NTYPE.LT.3.AND.K.LE.I5)
1CALL SCOUT(SC,RI,ZI,I1,I3,I2,I4,K,18HNEUTRON FLUXES)
   IF(NTYPE.EQ.3)
1CALL SCOUT(SC,RI,ZI,I1,I3,I2,I4,K,18HPHOTON FLUXES)
   IF(K.GT.I5)
1CALL SCOUT(SC,RI,ZI,I1,I3,I2,I4,K,18HPHOTON FLUXES)
   K=K+1
   IF(K.LE.NGT) GO TO 14
   IF(NBIN.EQ.2) NBIN=1
   REWIND 10
   REWIND 11
   REWIND 12
C CALCULATE AREAS AND RADII OF THE COLLAPSED (ICM*JCM) PROBLEM
   IK = ISTART
   DO 34 I = 1,ICM
   IL = IC(I)
   VOLR(I) = 3.1415927*(R(IL)*R(IL)-R(IK)*R(IK))
   R(I) = R(IK)
34 IK = IC(I)
   R(ICM+1) = R(IL)
   J1 = JSTART
   DO 36 J = 1,JCM
   J2 = JC(J)
   VOLZ(J) = Z(J2)-Z(J1)
   Z(J) = Z(J1)

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NAGS 69
NAGS 70
NAGS 115
NAGS 116
NAGS 117
NAGS 118
NAGS 119
NAGS 120
NAGS 121
NAGS 122
NAGS 123
NAGS 124
NAGS 125
NAGS 126
NAGS 127
NAGS 128
NAGS 129
NAGS 130
NAGS 131
NAGS 132
NAGS 133
NAGS 134
NAGS 135
NAGS 136
NAGS 137
NAGS 138
NAGS 139
NAGS 140
NAGS 141
NAGS 142
NAGS 143
NAGS 144
NAGS 145
NAGS 146
NAGS 147
NAGS 148
NAGS 149
NAGS 150
NAGS 151

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36 J1 = JC(J)
Z(JCM*1) = Z(J2)
RETURN
1008 FORMAT(1H1// ,47X,16H PROGRAM NAGS IV // 16X,12A6//)
1010 FORMAT(30H NO.OF RADIAL MESH INTERVALS**I3,/,
1 30H NO.OF COL.INTERVALS (R) ****I3,/,
2 30H NO. OF AXIAL MESH INTERVALS**I3,/,
3 30H NO. OF COL. INTERVALS (Z) ***I3,/,
4 30H NO. OF BIN. FLUX CARDS*****I3,/,
5 30H NO. OF NEUTRON GROUPS*****I3,/,
6 30H NO. OF GAMMA RAY GROUPS*****I3,/,
7 30H NO. OF MATERIALS*****I3,/,
)
1012 FORMAT(30H BINARY CARD OPTION*****I3,/,
1 30H LIBRARY OPTION*****I3,/,
2 30H PUNCH OPTION*****I3,/,
3 30H NO. OF ZEROS (RT)*****I3,/,
4 30H NO. OF ZEROS (LT)*****I3,/,
5 30H STARTING INTERVAL (R)*****I3,/,
6 30H STARTING INTERVAL (Z)*****I3,/,
)
1014 FORMAT (8H0IC(I) ,24I3,/,8X,24I3)
1016 FORMAT (8H0JC(J) ,24I3,/,8X,24I3)
1018 FORMAT(6H0R(I) ,10F8.3,/(6X,10F8.3/))
1020 FORMAT(6H0Z(J) ,10F8.3,/(6X,10F8.3/))
1022 FORMAT(34H1PROBLEM NORMALIZATION PARAMETERS
1 32H EFFECTIVE NU *****IPE14.5//
2 32H FISSION FRACTION ***** E14.5//
3 32H KEFF ***** E14.5//
4 32H FISSION VOLUME ***** E14.5//
5 32H CONVERSION CONSTANT ***** E14.5//
6 32H NORMALIZATION CONSTANT ***** E14.5//
7 32H POWER NORMALIZATION FACTOR ** E14.5)
1024 FORMAT(38H1NEUTRON FISSION PARAMETERS BY GROUP
1 38H GROUP NU CHI
2(4X,12,5X,2E14.5/))
1026 FORMAT(55(2H. ))
1028 FORMAT(24I3)
1030 FORMAT(6E12.5)
1032 FORMAT(12A6)
1034 FORMAT (8X,6E10.5)
END
$ORIGIN BETA.SYSUT3.REW
$IBFTC COLRR NOLIST, DECK,NODD,M94/2,XR7
NAGS 152
NAGS 153
NAGS 154
NAGS 155
NAGS 156
NAGS 157
NAGS 158
NAGS 159
NAGS 160
NAGS 161
NAGS 162
NAGS 163
NAGS 164
NAGS 165
NAGS 166
NAGS 167
NAGS 168
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NAGS 170
NAGS 171
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NAGS 174
NAGS 175
NAGS 176
NAGS 177
NAGS 178
NAGS 179
NAGS 180
NAGS 181
NAGS 182
//NAGS 183
NAGS 184
NAGS 185
NAGS 186
NAGS 187
NAGS 188
NAGS 189
NAGS 190
NAGS 191
COLZR 1

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2 COLZR
3 COLZR
4 COLZR
5 COLZR
6 COLZR
7 COLZR
8 COLZR
9 COLZR
10 COLZR
11 COLZR
12 COLZR
13 COLZR
14 COLZR
15 COLZR
16 COLZR
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18 COLZR
19 COLZR
20 COLZR

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COLZ

NA 1

```

SUBROUTINE COLR(A,B,VR,VZ,IC,JC,I1,I2,I3,I4,I5,I6)
DIMENSION A(I1,I2),B(I1,I2),VR(I3),VZ(I4),IC(I5),JC(I6)
COMMON ICT,ICM,JCT,JCM,NGN,NFAST,NI,NGG,NEL,IND,NTYPE
COMMON NCD,NBIN,NLIB,NEX,NEX1,ISTART,JSTART,JPUN ,ZREF,JCO
DO 4 J=1,I4
IK = ISTART
DO 4 I = 1,I5
IL=IC(I)-1
VT = 0.0
B(I,J) = 0.0
IF(IL.EQ.IK) A(I,J)=A(IK,J)
IF(IL.EQ.IK) GO TO 4
DO 2 K = IK,IL
VT = VT + VR(K)
2 B(I,J) = B(I,J) + VR(K) * A(K,J)
A(I,J) = B(I,J) / VT
4 IK = IC(I)
RETURN
END
$ORIGIN BETA,SYSUT3,REW
$IRFTC COLZR NOLIST, DECK,NODD,M94/2,XR7
SUBROUTINE COLZ(A,B,VR,VZ,IC,JC,I1,I2,I3,I4,I5,I6)
DIMENSION A(I1,I2),B(I1,I2),VR(I3),VZ(I4),IC(I5),JC(I6)
COMMON ICT,ICM,JCT,JCM,NGN,NFAST,NI,NGG,NEL,IND,NTYPE
COMMON NCD,NBIN,NLIB,NEX,NEX1,ISTART,JSTART,JPUN ,ZREF,JCO
DO 20 I=1,I5
J1 = JSTART
DO 20 J = 1,I6
J2=JC(J)-1
VT = 0.0
B(I,J) = 0.0
IF(J1.EQ.J2) A(I,J)=A(I,J1)
IF(J1.EQ.J2) GO TO 20
DO 30 K = J1,J2
VT = VT + VZ(K)
30 B(I,J) = B(I,J) + VZ(K) * A(I,K)
A(I,J) = B(I,J) / VT
20 J1 = JC(J)
RETURN
END
$ORIGIN ALPHA,SYSUT3,REW
$IRFTC NAGS2 NOLIST, DECK,NODD,M94/2,XR7

```



```

SUBROUTINE NAG2( R,Z,RSF,ZSF,RS,ZS,VOLR,VOLZ,SC,TEMP,SG,UNU,CHI, NA
1SFPS,SFDS,DNM,SA,SF,SIN,SS,SAS,SINS,AMU,ESS,ENA,SA2200,LABEL,SNA, NA
2ECOS,DK,DE,DU,SAG,TSR,RI,ZI,SGR,SGT,SGL,SGR,RSN,ZSN,DKG,STC, NA
2STF,STI, NA
3JC,JC,NID,NLM,I1,I2,I3,I4,I5,I6, NA
4I7 , I8 , I9 , I10 , I11 , I12 , I13 , NA
5I14 , I15 , I16 , I17 ) NA
COMMON ICT,ICM,JCT,JCM,NGN,NFAST,NI,NGG,NEL,IND,NTYPE NA
COMMON NCD,NBIN,NLIB,NEX,NEX1,ISTART,JSTART,NPUN ,ZREF,JCO NA
DIMENSION RSF(I13),ZSF(I14),R(I10),Z(I12),RSN(I13),ZSN(I14), NA
1DKG(I8),RS(I13),ZS(I14),VOLR(I1),VOLZ(I3),SC(I1,I3),TEMP(I15), NA
2SG(I13,I14,I17),UNU(I5),CHI(I5),SFPS(I8),SFDS(I8),DNM(I9), NA
3SA(I5,I9),SF(I5,I9),SIN(I7,I9),SS(I6,I9),SAS(I8,I9), NA
4SINS(I8,I7,I9),AMU(I9),ESS(I9),ENA(I9),SA2200(I9),LABEL(I9), NA
5SNA(I5,I9),ECOS(I6,I9),DK(I5),DE(I5),DU(I5),SAG(I8,I9),TSG(I8), NA
6RI(I2),ZI(I4),SGT(I2,3),SGR(I2,3),SGL(I4,3),SGR(I4,3),IC(I2), NA
7JC(I4),NID(I9),NLM(I9),ID(I2),TITLE(I2),BUF(27) NA
8,STC(I9) , STF(I9) , STI(I9) NA
READ LIBRARY CONSTANTS FROM POINT CODE NA
CROSS DEFINITION NAGS DIMENSION
POINT ID NID GAM ID NO. (NEL)
A9 AMU ATOMIC MASS UN. (NEL)
A10 ESS (1-ALPHA)/2.0 (NEL)
A14 ENA Q(N,ALPHA) (NEL)
A16 SA2200 SIGMA(2200 M.) (NEL)
LABEL NUCLEIDE NAME (NEL)
A2 SAS Q(N,GAMMA) (NGG,NEL)
A6 SINS Q(N,N,GAMMA) (NGG,NI,NEL)
A15 SNA SIGMA(N,ALPHA) (NGN,NEL)
A1 ECOS 1-COS(THETA) (NFAST,NEL)
A7 SFPS PROMPT FISS. G. (NGG)
A8 SFDS DELAY FISS. GA. (NGG)
-- DKG GAMMA DOSE C. (NGG)
A4 DK NEUTRON DOSE C. (NFAST)
A12 DE ENERGY WIDTH (NGN)
A13 DU LEHARGY WIDTH (NGN)
SIGFI SIGMA FISSION (NGN,NEL)
SIGA SIGMA ABS. (NGN,NEL)
SINELA SIGMA INELASTIC (NI,NEL)
SSYMET SIGMA ELASTIC (NFAST,NEL)

```

C	SAG	GAMMA RAY EAC	(NGG,NEL)
***	REWIND 9		NA
	REWIND 10		NA
2	READ(5,1002)NEL		NA
	READ(5,1004) (SFPS(K1),K1=1,NGG)		NA
	READ(5,1004) (SFDS(K1),K1=1,NGG)		NA
	READ(5,1004) (DKG(K1),K1=1,NGG)		NA
	READ(5,1004) (DK(J),J=1,NGN)		NA
	READ(5,1004) (DU(J),J=1,NGN)		NA
	READ(5,1004) (DE(J),J=1,NGN)		NA
	DO 6 N=1,NEL		NA
	HEAD(5,1006) NID(N),AMU(N),ESS(N),ENA(N),SA2200(N),LABEL(N)		NA
	DO 4 K=1,NI		NA
4	READ(5,1004) (SINS(K1,K,N),K1=1,NGG)		NA
	READ(5,1004) (SS(K,N),K=1,NFAST)		NA
	READ(5,1004) (SNA(K,N),K=1,NGN)		NA
	READ(5,1004) (ECOS(K,N),K=1,NFAST)		NA
	READ(5,1004) (SAS(K,N),K=1,NGG)		NA
	READ(5,1004) (SAG(K,N),K=1,NGG)		NA
	IF(NLIH.EQ.0) GO TO 6		
	READ(5,1004) (SF(K,N),K=1,NGN)		NA
	READ(5,1004) (SA(K,N),K=1,NGN)		NA
	READ(5,1004) (SS(K,N),K=1,NFAST)		NA
	HEAD(5,1004) (SIN(K,N),K=1,NI)		NA
6	CONTINUE		NA
	WRITE(6,1008)		NA
	WRITE(6,1038) (SFPS(K1),K1=1,NGG)		NA
	WRITE(6,1038) (SFDS(K1),K1=1,NGG)		NA
	WRITE(6,1038) (DKG(K1),K1=1,NGG)		NA
	WRITE(6,1044)		NA
	WRITE(6,1038) (DK(JK),JK=1,NGN)		NA
	WRITE(6,1046)		NA
	WRITE(6,1038) (DU(JK),JK=1,NGN)		NA
	WRITE(6,1048)		NA
	WRITE(6,1038) (DE(JK),JK=1,NGN)		NA
	DO 8 N=1,NEL		NA
	WRITE(6,1026)N		NA
	WRITE(6,1028)		NA
	WRITE(6,1024) NID(N),AMU(N),ESS(N),ENA(N),SA2200(N),LABEL(N)		NA
	WRITE(6,1030)		NA
	WRITE(6,1020) NID(N), (SAS(K1,N),K1=1,NGG)		NA
	WRITE(6,1032)		NA

```

WRITE (6,1020) NID(N), (SAG(K1,N), K1=1,NGG)
WRITE (6,1034)
DO 8 K=1,NI
8 WRITE (6,1022) NID(N), K, (SINS(K1,K,N), K1=1,NGG)
10 NPASS=0
DO 12 I=1,I13
DO 12 J=1,I14
DO 12 K=1,I17
12 SG(I,J,K)=0.0
14 NPROB=0
14 READ (5,1010) (ID(I), I=1,12)
WRITE (6,1014) (ID(I), I=1,12)
READ (5,1002) IRS, IRF, IZS, IZF, IEL, IND
WRITE (6,1016) IRS, IRF, IZS, IZF, IEL, IND
IR1 = IRF - 1
IZ1 = IZF - 1
IF (NTYPE.GT.1) READ (5,1004) DGM,WTGM
WRITE (6,1040)
READ IN GROUP CONSTANTS FOR MICROSCOPIC MATERIALS AND COMPUTE GAMMA
A RAY SOURCES
NSKIP=0
IF (IEL.GT.0) GO TO 16
NSKIP=1
IEL=-IEL
16 DO 28 M=1,IEL
STC(M) = 0.0
STI(M) = 0.0
STF(M) = 0.0
IF (NSKIP.EQ.1) GO TO 18
READ (5,1042) NLM(M), DNM(M)
IF (NTYPE.GT.1) GO TO 18
IF (NLIB.GT.0) GO TO 18
READ (5,1004) (SF(K,M), K=1,NGN)
READ (5,1004) (SA(K,M), K=1,NGN)
READ (5,1004) (SS(K,M), K=1,NFAST)
READ (5,1004) (SIN(K,M), K=1,NI)
NL = NLM(M)
DO 20 JJ=1,NEL
IF (NL.EQ.NID(JJ)) GO TO 22
20 CONTINUE
WRITE (6,1000) NL
GO TO 28

```

C
C

79 NA
80 NA
81 NA
82 NA
83 NA
84 NA
85 NA
86 NA
87 NA
88 NA
89 NA
90 NA
91 NA
92 NA
93 NA
94 NA
95 NA
96 NA
97 NA
98 NA
99 NA
100 NA
101 NA
102 NA
103 NA
104 NA
105 NA
106 NA
107 NA
108 NA
109 NA

110 NA
111 NA
112 NA
113 NA
114 NA
115 NA
116 NA
117 NA
118 NA
119 NA

```

22 ID1=LABEL(JJ)
24 WRITE(6,1018) NLM(M),DNM(M),ID1
   IF (NTYPE.GT.1) GO TO 26
   MJ=M
   IF(NLIB.GT.0) MJ=JJ
   WRITE (6,1038)(SF(K,MJ),K=1,NGN)
   WRITE (6,1038)(SA(K,MJ),K=1,NGN)
   WRITE (6,1038)(SIN(K,MJ),K=1,NI)
   WRITE (6,1038)(SS(K,MJ),K=1,NFAST)
   WRITE (6,1038)(SAG(K,JJ),K=1,NGG)
28 WRITE(6,1040)
   NGT = I5
   IF(NTYPE.EQ.2) NGT=I5 + I8
   IF(NTYPE.EQ.3) NGT=I8
   DO 32 L = 1,3
   DO 30 J=IZ5,IZ1
   SGL(J,L) = 0.0
30 SGR(J,L) = 0.0
   DO 32 I=IRS,IR1
   SGT(I,L) = 0.0
32 SGB(I,L) = 0.0
   DO 68 K=1,NGT
   HEAD (10)((SC(I,J),I=1,I2),J=1,I4)
   DO 66 M=1,IEL
   NL = NLM(M)
   DO 34 JJ=1,NEL
   IF (NL.EQ.NID(JJ)) GO TO 36
34 CONTINUE
   WRITE (6,1000) NL
   GO TO 66
36 KLB = K = 15
   MJ=M
   IF(NLIB.GT.0) MJ=JJ
   IF(NTYPE.EQ.2.AND.K.GT.NFAST.AND.K.LE.I5) GO TO 68
   IF (NTYPE.NE.1) GO TO 38
   SAC = SA(K,MJ)*DNM(M)
   SFC = SF(K,MJ)*DNM(M)
   SIC = 0.0
   IF(K.LE.NI) SIC = SIN(K,MJ)*DNM(M)
   GO TO 42
38 IF (NTYPE.GT.2) GO TO 40
   IF (K.GT.I5) SAC = SAG(KLB,JJ)*1.603E-13*DNM(M)*DGM

```

NA 120
NA 121
NA 122

NA 127
NA 128
NA 129
NA 130
NA 131
NA 132
NA 133
NA 134
NA 135
NA 136
NA 137
NA 138
NA 139
NA 140
NA 141
NA 142
NA 143
NA 144
NA 145
NA 146
NA 147
NA 148

NA 149
NA 150

NA 153
NA 155
NA 156
NA 157

```

IF (K.LE.NFAST) SAC = SS(K,JJ)*DE(K)*ESS(JJ)*ECOS(K,JJ)*1.603E-13*NA
10.60248*DNM(M)*DGM/(AMU(JJ)*DU(K))
SFC=0.0
GO TO 42
40 SAC = SAG(K,JJ)*1.603E-13*DNM(M)*DGM
SFC=0.0
42 NGF=I17-1
DO 48 I = IRS,IR1
DO 48 J = IZS,IZI
SCV = SC(I,J)*VOLR(I)*VOLZ(J)
STI(M) = STI(M) + SIC*SCV
STC(M) = STC(M) + SAC*SCV
STF(M) = STF(M) + SFC*SCV
IF(NTYPE.GT.1) GO TO 46
DO 44 KG = 1,NGG
SG(I,J,KG) = SG(I,J,KG) + SC(I,J) * (SAC*SAS(KG,JJ)+SFC*(SFPS(KG)+
1SFDS(KG)))
IF(K.LE.NI) SG(I,J,KG) = SG(I,J,KG) + SIC*SINS(KG,K,JJ) *SC(I,J)
44 CONTINUE
SG(I,J,NGF) = SG(I,J,NGF) + SFC *SC(I,J)
SG(I,J,I17) = SG(I,J,I17) + SFC* UNU(K) *SC(I,J)
GO TO 48
46 IF(NTYPE.EQ.2.AND.K.GT.I5) SG(I,J,1) = SG(I,J,1)+SAC*SC(I,J)
IF(NTYPE.EQ.3) SG(I,J,1) = SG(I,J,1)+SAC*SC(I,J)
IF(NTYPE.EQ.2.AND.K.LE.NFAST) SG(I,J,2)=SG(I,J,2)+SAC*SC(I,J)
SG(I,J,I17) = SG(I,J,I17) + SAC *SC(I,J)
48 CONTINUE
SGARB=0.0
DO 50 KG=1,NGG
50 SGARB =(SAC*SAS(KG,JJ)+SFC*(SFPS(KG)+SFDS(KG)))+SIC*SINS(KG,K,JJ)
1 +SGARB
DO 56 J = IZS,IZI
IF(NTYPE.GT.1) GO TO 54
IF(IRS.EQ.1) GO TO 52
SGL(J,1) = SGL(J,1)+ SGARB * SC(IHS-1,J)
SGL(J,2) = SGL(J,2) + SFC*SC(IRS-1,J)
SGL(J,3) = SGL(J,3) + SFC*SC(IRS-1,J)*UNU(K)
52 IF(IR1.EQ.I2) GO TO 56
SGR(J,1) = SGR(J,1) + SGARB*SC(IR1+1,J)
SGR(J,2) = SGR(J,2) + SFC*SC(IR1+1,J)
SGR(J,3) = SGR(J,3) + SFC*SC(IR1+1,J)*UNU(K)
GO TO 56

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NA NA 160
NA NA 161
NA NA 163
NA NA 164
NA NA 165
NA NA 166
NA NA 167
NA NA 168
NA NA 169
NA NA 170
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NA NA 172
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NA NA 174
NA NA 175
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NA NA 180
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NA NA 184
NA NA 185
NA NA 186
NA NA 187
NA NA 188
NA NA 189
NA NA 190
NA NA 191
NA NA 192
NA NA 193
NA NA 194
NA NA 195
NA NA 196
NA NA 197

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```

54 IF(IRS.GT.1) SGL(J,1) = SGL(J,1) + SAC*SC(IRS-1,J)
   IF(IR1.LT.I2) SGR(J,1) = SGR(J,1) + SAC*SC(IR1+1,J)
56 CONTINUE
   DO 64 I = IRS,IR1
   IF(NTYPE.GT.1) GO TO 62
   IF(IZS.EQ.1) GO TO 58
   SGB(I,1) = SGB(I,1) + SGARB * SC(I,IZS-1)
   SGB(I,2) = SGB(I,2) + SFC * SC(I,IZS-1)
   SGB(I,3) = SGB(I,3) + SFC * SC(I,IZS-1)*UNU(K)
58 IF(IZ1.EQ.I3) GO TO 64
   SGT(I,1) = SGT(I,1) + SGARB*SC(I,IZ1+1)
   SGT(I,2) = SGT(I,2) + SFC *SC(I,IZ1+1)
   SGT(I,3) = SGT(I,3) + SFC *SC(I,IZ1+1)*UNU(K)
60 GO TO 64
62 IF(IZS.GT.1) SGB(I,1) = SGB(I,1) + SAC*SC(I,IZS-1)
   IF(IZ1.LT.I4) SGT(I,1) = SGT(I,1) + SAC*SC(I,IZ1+1)
64 CONTINUE
66 CONTINUE
68 CONTINUE
   REWIND 10
   WRITE(9) IRS,IRF,IZS,IZF, IEL,IND,DGM,WTGM,(NLM(M),DNM(M),M=1,IEL)
   1,(ID(I),I=1,12)
   WRITE(9) (((SG(I,J,K),I=IRS,IR1),J=IZS,IZ1),K=1,117), ((SGL(J,L),L=1,3),J=IRS,IR1),L=1,3)
   2,(STC(M),STF(M),STI(M),M=1,NEL)
   DO 70 I=IRS,IR1
   DO 70 J=IZS,IZ1
   DO 70 K=1,117
   SG(I,J,K) = 0.0
70 NPROB=NPROB+1
   IF(IND.EQ.1) GO TO 14
   WRITE(6,1050) NPROB
   REWIND 9
   RETURN
1000 FORMAT(13#ELEMENT NO. 13,18H IS NOT IN LIBRARY)
1002 FORMAT(2#13)
1004 FORMAT(6E12.5)
1006 FORMAT(I3,4E12.5,10X,A6)
1008 FORMAT(/7#HIPROMPT FISSION AND FISSION PROD. DECAY SPECTRA AND GAMA
      1 GAMMA DOSE CONSTANTS)
1010 FORMAT(12A6)
1012 FORMAT(8X,4E10.5)

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198 NA
199 NA
200 NA
201 NA
202 NA
203 NA
204 NA
205 NA
206 NA
207 NA
208 NA
209 NA
210 NA
211 NA
212 NA
213 NA
214 NA
215 NA
216 NA
217 NA
218 NA
219 NA
220 NA
221 NA
222 NA
223 NA
224 NA
225 NA
226 NA
227 NA
228 NA
229 NA
230 NA
231 NA
232 NA
233 NA
234 NA
235 NA
236 NA
237 NA
238 NA
239 NA

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1014 FORMAT(14H1REGION OUTPUT//55(2H.)/19X12A6/55(2H.)/) NA
1016 FORMAT(52H0REGION PARAMETERS(15,IF,JS,JF,NO. OF ELEM.,CONTROL)/6INA NA
14) NA
1018 FORMAT(13H0ELEMENT NO.=I4,13H NO. DENSITY=1PE12.4,13H ELEMENT ID NA
1A6//71H CROSS SECTIONS(ELASTIC SCATTER AND GAMMA RAY ENERGY ABSORPNA
TION) NA
1020 FORMAT(I4,4X,1P8E12.4/(8X,8E12.4)) NA
1022 FORMAT(2I4,1P8E12.4/(8X,8E12.4)) NA
1024 FORMAT(I4,4X,1P4E12.4,2X,A6) NA
1026 FORMAT(30H1LIBRARY DATA FOR ELEMENT NO. I3 /) NA
1028 FORMAT(4H GAM6X6HA.M.U.6X9H(1.-AL)/23X8H(Q(N,AL)4X19HSIGMA ABS.
ELEMENT/4H ID 43X16H(2200 M) NAME) NA
1030 FORMAT(1H09X10HQ(N,GAMMA)) NA
1032 FORMAT(1H09X27HMASS ABSORPTION COEFFICIENT/) NA
1034 FORMAT(1H0,5X,17HGRP Q(N,N7,GAMMA)) NA
1036 FORMAT(I4,4X,3E12.4/) NA
1038 FORMAT(/(8X,1P8E12.4)) NA
1040 FORMAT(55(2H.)) NA
1042 FORMAT(I3,E12.4) NA
1044 FORMAT(1H01X22HNEUTRON DOSE CONSTANTS) NA
1046 FORMAT(1H01X23HLETHARGY WIDTH BY GROUP) NA
1048 FORMAT(1H01X21HENERGY WIDTH BY GROUP) NA
1050 FORMAT(23H1NAGS IV HAS PROCESSED 15, 25H SEPERATE REGION PROBLEMS)NA
END NA
$ORIGIN ALPHA,SYSUT3,REW
$IBFTC NAGS3 NOLIST, DECK,NODD,M94/2,XR7
SUBROUTINE NAG3( R,Z,RSF,ZSF,RS,ZS,VOLR,VOLZ,SC,TEMP,SG,UNU,CHI,
1SFPS,SFDS,DNM,SA,SF,SIN,SS,SAS,SINS,AMU,ESS,ENA,SA2200,LABEL,SNA,
2ECOS,DK,DE,DU,SAG,TSG,RI,ZI,SGB,SGT,SGL,SGR,RSN,ZSN,DKG,STC,
2STF,STI,
3IC,JC,NID,NLM,I1,I2,I3,I4,I5,I6,
4I7 , I8 , I9 , I10 , I11 , I12 , I13 ,
5I14 , I15 , I16 , I17 )
COMMON ICT,ICM,JCT,JCM,NGN,NFAST,NI,NGG,NEL,IND,NTYPE
COMMON NCD,NBIN,NLIB,NEX,NEX1,ISTART,JSTART,NPUN ,ZREF,JCO
DIMENSION RSF(I13),ZSF(I14),R(I10),Z(I12),RSN(I13),ZSN(I14),
1DKG(I8),RS(I13),ZS(I14),VOLR(I1),VOLZ(I3),SC(I1,I3),TEMP(I15),
2SG(I13,I14,I17),UNU(I5),CHI(I5),SFPS(I8),SFDS(I8),DNM(I9),
3SA(I5,I9),SF(I5,I9),SIN(I7,I9),SS(I6,I9),SAS(I8,I9),
4SINS(I8,I7,I9),AMU(I9),ESS(I9),ENA(I9),SA2200(I9),LABEL(I9),
5SNA(I5,I9),ECOS(I6,I9),DK(I5),DE(I5),DU(I5),SAG(I8,I9),TSG(I8),
6RI(I2),ZI(I4),SGT(I2,3),SGB(I2,3),SGL(I4,3),SGR(I4,3),IC(I2),

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7 JC(I4),NID(I9),NLM(I9),ID(I2),TITLE(I2),BUF(27)
A,STC(I9),STF(I9),STI(I9)
DIMENSION SGLT(3),SGRT(3),SGBT(3),SGTP(3)
2 READ(9) IRS,IRF,IZS,IZF, IEL,IND,DGM,WTGM,(NLM(M),DNM(M),M=1,IEL)
1,(ID(I),I=1,12)
IRI = IRF - 1
IZI = IZF - 1
READ(9)((SG(I,J,K),I=IRS,IRI),J=IZS,IZI),K=1,117),((SGL(J,L),L=1,3)
1 SGR(J,L),J=IZS,IZI),L=1,3),((SGB(I,L),SGT(I,L),I=IRS,IRI),L=1,3)
2,(STC(M),STF(M),STI(M),M=1,NEL)
VOLT = 0.0
TSG(1) = 0.0
TSG(2) = 0.0
SGLT(1) = 0.0
SGRT(1) = 0.0
SGTP(1) = 0.0
SGBT(1) = 0.0
TS = 0.0
DO 4 I = IRS,IRI
SGTP(I) = SGTP(1) + SGT(I,1) * VOLR(I)
SGBT(I) = SGBT(1) + SGB(I,1) * VOLR(I)
RSF(I) = RI(I) / 2.54
4 RS(I) = 0.0
DO 6 J = IZS,IZI
SGRT(1) = SGRT(1) + SGR(J,1) * VOLZ(J)
SGLT(1) = SGLT(1) + SGL(J,1) * VOLZ(J)
ZSF(J) = ZREF - ZI(J) / 2.54
6 ZS(J) = 0.0
DO 8 J = IZS,IZI
DO 8 I = IRS,IRI
8 RS(I) = RS(I) + SG(I,J,3) * VOLZ(J)
DO 10 I = IRS,IRI
DO 10 J = IZS,IZI
10 ZS(J) = ZS(J) + SG(I,J,3) * VOLR(I)
VOLT = 0.0
DO 12 I = IRS,IRI
DO 12 J = IZS,IZI
VOLI = VOLR(I) * VOLZ(J)
VOLT = VOLT + VOLI
DO 12 K = 1,2
12 TSG(K) = TSG(K) + SG(I,J,K) * VOLI
TS = TSG(1) + TSG(2)

```

18 NAG
19 NAG
20 NAG
21 NAG
22 NAG
23 NAG
24 NAG
25 NAG
26 NAG
27 NAG
28 NAG
29 NAG
30 NAG
31 NAG
32 NAG
33 NAG
34 NAG
35 NAG
36 NAG
37 NAG
38 NAG
39 NAG
40 NAG
41 NAG
42 NAG
43 NAG
44 NAG
45 NAG
46 NAG
47 NAG
48 NAG
49 NAG
50 NAG
51 NAG
52 NAG
53 NAG
54 NAG
55 NAG
56 NAG
57 NAG
58 NAG
59 NAG


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VOLTR=0.0
DO 14 I=IRS,IRI
14 VOLTR=VOLTR+VOLR(I)
VOLTZ=0.0
DO 16 J=IZS,IZI
16 VOLTZ=VOLTZ+VOLZ(J)
DO 18 I=IRS,IRI
18 RS(I) =RS(I) *VOLTR/TS
DO 20 J=IZS,IZI
20 ZS(J)=ZS(J)*VOLTZ/TS
TSA = TS/VOLT
SGLT(1)=SGLT(1)/(TSA*VOLTZ)
SGRT(1)=SGRT(1)/(TSA*VOLTZ)
SGBT(1)=SGBT(1)/(TSA*VOLTR)
SGTP(1)=SGTP(1)/(TSA*VOLTR)
CALL SASET(SGLT(1),SGRT(1),SGBT(1),SGTP(1),R,RI,Z,ZI,I1,I2,I3,I4,
2110,I12,I13,I14,IRS,IRI,IZS,IZI,I,RS,ZS)
2 THE FOLLOWING SECTION IS THE CALCULATION OF ALL QUANTITIES IN METRIC
C AND MIXED ENGLISH UNITS
C TSG(1),THE INTEGRATED PHOTON HEATING IN THE REGION
C TSG(2),THE TOTAL INTEGRATED NEUTRON HEATING IN THE REGION
C TS IS THE TOTAL NEUTRON PLUS PHOTON INTEGRATED HEATING IN THE REGION
C VOLTR IS THE RADIAL CROSS SECTIONAL AREA OF THE REGION
C VOLTZ IS THE HEIGHT OF THE REGION
C RSF IS THE RADIAL MESH LINE DIMENSION IN INCHES
C ZSF IS THE AXIAL MESH LINE DIMENSION IN INCHES
C DGM IS THE DENSITY OF MATERIAL IN GMS/CC
C WTGM IS THE WEIGHT OF MATERIAL IN KILOGRAMS
C DLB IS THE DENSITY IN LBS/IN**3
C WTLB IS THE WEIGHT IN LBS
C VOLTI IS THE VOLUME OF THE REGION IN CUBIC INCHES
C TSWC IS THE TOTAL HEATING RATE IN WATTS/CC
L=3
DO 22 I=IRS,IRI
DO 22 J=IZS,IZI
22 SG(I,J,L) = SG(I,J,L) * 55.9616
DLB = DGM * 0.03613
WTLB = WTGM * 2.205
VOLTI = VOLT / 16.387
TSWC = TS / VOLT
TSW = TSWC * WTGM / DGM
TSG(I) = TSG(I) * WTGM / (DGM*VOLT)

```

NAG 60
 NAG 61
 NAG 62
 NAG 63
 NAG 64
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 NAG 96
 NAG 97
 NAG 98
 NAG 99
 NAG 100
 NAG 101



```

TSG(2) = TSG(2) * WTGM / (DGM*VOLT)
TSM = TSM * 3.415E+03
TSWG = TSWG / DGM
TSHI = TSWC * 55.9616
TSBL = TSBI / DLB
WRITE (6,1032) (ID(I),I=1,12)
WRITE(6,1016) IRS,R(IRS),IRF,R(IRF),IZS,Z(IZS),IZF,Z(IZF)
WRITE(6,1018) IEL
WRITE (6,1020)
DO 28 M=1,IEL
DO 24 N=1,NEL
IF(NID(N)-NLM(M))24,26,24
24 CONTINUE
GO TO 28
26 RHO=DNM(M)*DGM
WT = RHO*VOLT
WRITE(6,1022) NLM(M),LABEL(N),DNM(M),RHO,STC(M)
28 CONTINUE
WRITE (6,1026) DGM,DLB,WTGM,WTLB,ISM
WRITE (6,1030) TSG(1),TSG(2),TSB,TSWG,TSWC,TSBL,TSBI
WRITE (6,1032) (ID(I),I=1,12)
WRITE (6,1034)
IRT=IRI-IRS+1
IZT=IZI-IZS+1
ISTOP=MINO(IRT,IZT)
ISTOPI=MAXO(IRT,IZT)
SNL=SGLT(1)*TSBI
SNR=SGRT(1)*TSBI
SNB=SGBT(1)*TSBI
SNT=SGTP(1)*TSBI
RIN = R(IRS)/2.54
ZIN = ZREF - Z(IZS)/2.54
WRITE(6,1040) R(IRS),RIN,SGLT(1),SNL,Z(IZS),ZIN,SGBT(1),SNB
RIN = R(IRF)/2.54
ZIN = ZREF - Z(IZF)/2.54
DO 30 IP=1,ISTOP
I=IP+IRS-1
J = IP+IZS-1
RSK = RS(I) * TSHI
ZSK = ZS(J) * TSBI
30 WRITE (6,1040) RI(I),RSF(I),RS(I),RSK,ZI(J),ZSF(J),ZS(J),ZSK
I=I+1

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102 NAG
103 NAG
104 NAG
105 NAG
106 NAG
107 NAG
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142 NAG
143 NAG

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144 NAG
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178 NAG
179 NAG
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182 NAG
183 NAG
184 NAG
185 NAG

J=J+1
IP = IP+1
IF (ISTOP.EQ. ISTOP1) GO TO 42
IF (ISTOP.EQ. IRT) GO TO 36
RSK = RS(I) + TSBI
WRITE(6,1040) RI(I),RSF(I),RSK,Z(IZF),ZIN,SGTP(1),SNT
IP=IP+1
I=I+1
IF (IP.GT. ISTOP1) GO TO 34
DO 32 IS=IP, ISTOP1
RSK = RS(I) + TSBI
WRITE(6,1040) RI(I),RSF(I),RSK,Z(IZF),ZIN,SGTP(1),SNT
32 I=I+1
34 WRITE(6,1040) R(IRF),RIN,SGRT(1),SNR
GO TO 44
36 ZSK=ZS(J)+TSBI
WRITE(6,1040) R(IRF),RIN,SGRT(1),SNR,ZI(J),ZSF(J),ZS(J),ZSK
IP =IP+1
J=J+1
IF (IP.GT. ISTOP1) GO TO 40
DO 38 JS=IP, ISTOP1
ZSK=ZS(J)+TSBI
WRITE(6,1042) ZI(J),ZSF(J),ZS(J),ZSK
38 J=J+1
40 WRITE(6,1042) Z(IZF),ZIN,SGTP(1),SNT
GO TO 44
42 WRITE(6,1040) R(IRF),RIN,SGRT(1),SNR,Z(IZF),ZIN,SGTP(1),SNT
44 CONTINUE
WRITE (6,1032) (ID(I),I=1,12)
WRITE (6,1038)
DO 46 ISTAR=IRS,IR1,6
ISTOP=ISTAR+5
ISTOP= MIN0(ISTOP,IR1)
WRITE (6,1012) (ICP,ICP=ISTAR,ISTOP)
DO 46 J=IZS,IZ1
46 WRITE(6,1008) J, (SG(I,J,3),I=ISTAR,ISTOP)
DO 50 I=IRS,IR1
DO 50 J=IZS,IZ1
DO 48 K=1,3
48 SG(I,J,K) = 0.0
50 CONTINUE
IF (IND.EQ.1) GO TO 2

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```

IF (NTYPE.EQ.3) GO TO 58
DO 52 I=1,I4
DO 52 J=1,I4
52 SC(I,J) = 0.0
DO 56 K=1,I5
READ(10) ((SG(I,J,1),I=1,I2),J=1,I4)
IF (K.GT.I6) GO TO 56
DO 54 I=1,I2
DO 54 J=1,I4
54 SC(I,J)=SC(I,J)+SG(I,J,1)*DK(K)
56 CONTINUE
CALL SCOUT(SC,RI,ZI,I1,I3,I2,I4,K,18HNEUTRON DOSE )
58 IF (NTYPE.EQ.1) GO TO 64
DO 60 I = 1,I2
DO 60 J = 1,I4
60 SC(I,J) = 0.0
DO 62 K=1,I8
READ(10) ((SG(I,J,1),I=1,I2),J=1,I4)
DO 62 I=1,I2
DO 62 J=1,I4
62 SC(I,J)=SC(I,J)+SG(I,J,1)*DKG(K)
CALL SCOUT(SC,RI,ZI,I1,I3,I2,I4,K,18HGAMMA DOSE )
1000 FORMAT (17H0REGION VOLUME = IPE15.5)
1002 FORMAT (I2A6)
1004 FORMAT(44H0REGION AVERAGE SOURCE SPECTRUM (S(E,AVE.)) )
1006 FORMAT(3X,I3,2X,F8.3,F10.5,F11.5,10X,I3,2X,F8.3,F10.5,F11.5)
1008 FORMAT(I3,1X,1P8E13.5)
1010 FORMAT(47H0REGION PHOTON SOURCE AND FISSION DISTRIBUTIONS //
1 39H RADIAL
2 39H AXIAL
3 37H MESH DIMEN. SOURCE
4 37H MESH DIMEN. SOURCE /)
1012 FORMAT(1H0,4X,8(4X,I3,6X) )
1014 FORMAT(42H0REGION INTEGRAL SOURCE SPECTRUM (S(E)) )
1016 FORMAT(1H02X,23H REGION MESH BOUNDARIES//4X8LEFT,....I3,10X,F13.5/
1 4X8RIGHT,....I3,10X,F13.5/NAG
1 4X8BOTTOM,....I3,10X,F13.5/NAG
2) 4X8HTOP,....I3,10X,F13.5/NAG
1018 FORMAT(1H02X,19H NO. OF ELEMENTS,....I3/)
1020 FORMAT(1H03X,61HELEMENT NO. NAME WEIGHT FRACTION DENSITY
1 HEAT / 6X,8H(GAM ID)/)

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NAG 186
NAG 187
NAG 188
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NAG 196
NAG 197
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NAG 226
NAG 227

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1022 FORMAT(7X,I3.6X,A6.5X,I3E13.5)
1020 FORMAT(14H1REGION OUTPUT//55(2H )//19X12A6/55(2H )//)
1026 FORMAT(1M03X18HMATERIAL DENSITY
  1    ,22X,
  2    , 3X,17H MATERIAL WEIGHT
  3    , 20X,
  4    , 3X,19H HEATING DATA
1028 FORMAT(52H0REGION PARAMETERS(1S,IF,JS,JF,NO. OF ELEM.,CONTROL)//61NAG
  14)
1030 FORMAT(22X,
  1    ,22X,
  2    /,22X,
  3    ,22X,
  4    ,22X,
  5    ,22X,
  6    ,22X,
1032 FORMAT(1H1,2X,12A6/)
1034 FORMAT(32H0RELATIVE HEATING DISTRIBUTIONS ,//
  147H AXIAL DIMENSION IN INCHES IS FROM CORE INLET //
  254H RADIAL DIMENSIONS
  354H AXIAL DIMENSIONS
  454H
  554H
  654H (CM.) (INCHES)
  754H (CM.) (INCHES)
1036 FORMAT(34H0REGION INTEGRAL GAMMA RAY SOURCE=1PE15.5/27H0REGION INTNAG
  1EGRAL FISSIONS =E15.5)
1038 FORMAT(44H0HEATING DISTRIBUTION (BTU/IN**3-HOUR) )
1040 FORMAT(F10.4,2X,F10.4,2X,F10.4,2X,F10.4,4X,F12.3,4X,
  1    F10.4,2X,F10.4,2X,F10.4,4X,F12.3 )
1042 FORMAT(54X,F10.4,2X,F10.4,2X,F10.4,2X,F10.4,4X,F12.3 )
1044 FORMAT(/(8X,I3E12.4))
1046 FORMAT(55(2H. ))
  64 RETURN
  END
$ORIGIN ALPHA, SYSUT3, REM
$IBFTC NAGS4 NOLIST, DECK, NODD, M94/2, XR7
SUBROUTINE NAG4( R,Z,RSF,ZSF,RS,ZS,VOLR,VOLZ,SC,TEMP,SG,UNU,CHI,
  1SFPS,SFDS,DNM,SA,SF,SIN,SS,SAS,SINS,AMU,ESS,ENA,SA2200,LABEL,SNA,
  2ECOS,DK,DE,DU,SAG,TSG,RI,ZI,SGH,SGT,SGL,SGR,RSN,ZSN,DKG,STC,
  2STF,STI,
  3IC,JC,NID,NLM,I1,I2,I3,I4,I5,I6,

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417 , I8 , I9 , I10 , I11 , I12 , I13 ,
5114 , I15 , I16 , I17 ,
COMMON ICT,ICM,JCT,JCM,NGN,NFAST,NI,NGG,NEL,IND,NTYPE
COMMON NCD,NBIN,NLIB,NEX,NEX1,ISTART,JSTART,JPUN ,ZREF,JCO
DIMENSION RSF(I13),ZSF(I14),R(I10),Z(I12),RSN(I13),ZSN(I14),
1DKG(I8),RS(I13),ZS(I14),VOLR(I1),VOLZ(I3),SC(I1,I3),TEMP(I15),
2SG(I13,I14,I17),UNU(I5),CHI(I5),SFPS(I8),SFDS(I8),DNM(I9),
3SA(I5,I9),SF(I5,I9),SIN(I7,I9),SS(I6,I9),SAS(I8,I9),
4SINS(I8,I7,I9),AMU(I9),ESS(I9),ENA(I9),SA2200(I9),LABEL(I9),
5SNA(I5,I9),ECOS(I6,I9),DK(I5),DE(I5),DU(I5),SAG(I8,I9),TSG(I8),
6RI(I2),ZI(I4),SGI(I2,3),SGR(I2,3),SGL(I4,3),SGR(I4,3),IC(I2),
7JC(I4),NID(I9),NLM(I9),ID(I2),TITLE(I2),BUF(27)
8,STC(I9) , STF(I9) , STI(I9)
DIMENSION SGLT(3),SGRT(3),SGBT(3),SGTP(3)
2 READ(9) IRS,IRF,IZS,IZF, IEL,IND,DGM,WTGM, (NLM(M),DNM(M),M=1,IEL)
1,(ID(I),I=1,I2)
IRI = IRF - 1
IZI = IZF - 1
READ(9) ((SG(I,J,K),I=IRS,IRI),J=IZS,I2I),K=1,I17), ((SGL(J,L),
1SGR(J,L),J=IZS,I2I),L=1,3),((SGB(I,L),SGT(I,L),I=IRS,IRI),L=1,3)
2,(STC(M),STF(M),STI(M),M=1,NEL)
VOLT = 0.0
DO 4 I=1,NGG
4 TSG(I)=0.0
DO 6 I = 1,3
SGLT(I) = 0.0
SGRT(I) = 0.0
SGTP(I) = 0.0
6 SGBT(I) = 0.0
TS = 0.0
TSF = 0.0
TSN = 0.0
DO 10 I = IRS,IRI
DO 8 K = 1,3
SGTP(K) = SGTP(K) + SGT(I,K) + VOLR(I)
8 SGBT(K) = SGBT(K) + SGB(I,K) + VOLR(I)
RSN(I)=0.0
RSF(I)=0.0
10 RS(I) = 0.0
DO 14 J = IZS,I2I
DO 12 K = 1,3
SGLT(K) = SGLT(K) + SGL(J,K) + VOLZ(J)

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7 NAGS
8 NAGS
9 NAGS
10 NAGS
11 NAGS
12 NAGS
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 88 NAGS
 89 NAGS
 90 NAGS

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12 SGRT(K) = SGRT(K) * SGR(J,K) * VOLZ(J)
   ZSN(J)=0.0
   ZSF(J)=0.0
14 ZS(J) = 0.0
   DO 20 K=1,NGG
   DO 16 J = IZS,IZI
   DO 16 I = IRS,IRI
   IF (K.NE.NGG) GO TO 16
   RSF(I) = RSF(I) * SG(I,J,K*1) * VOLZ(J)
   RSN(I) = RSN(I) * SG(I,J,K*2) * VOLZ(J)
16 RS(I) = RS(I) * SG(I,J,K)*VOLZ(J)
   DO 18 I = IRS,IRI
   DO 18 J = IZS,IZI
   IF (K.NE.NGG) GO TO 18
   ZSF(J) = ZSF(J) * SG(I,J,K*1) * VOLR(I)
   ZSN(J) = ZSN(J) * SG(I,J,K*2) * VOLR(I)
18 ZS(J) = ZS(J) * SG(I,J,K) * VOLR(I)
   VOLT = 0.0
   DO 20 I=IRS,IRI
   DO 20 J=IZS,IZI
   VOLI = VOLR(I)*VOLZ(J)
   VOLT = VOLT * VOLI
   IF (K.NE.NGG) GO TO 20
   TSF = TSF * SG(I,J,K*1) * VOLI
   TSN = TSN * SG(I,J,K*2) * VOLI
20 TSG(K) = TSG(K) * SG(I,J,K)*VOLI
   DO 22 K=1,NGG
22 TS = TS * TSG(K)
   VOLTR=0.0
   DO 24 I=IRS,IRI
24 VOLTR=VOLTR*VOLR(I)
   VOLTZ=0.0
   DO 26 J=IZS,IZI
26 VOLTZ=VOLTZ*VOLZ(J)
   DO 28 I=IRS,IRI
   IF(TSF.LE.0.0) GO TO 28
   RSF(I)=RSF(I)*VOLTR/TSF
   RSN(I)=RSN(I)*VOLTR/TSN
28 RS(I) =RS(I) *VOLTR/TS
   DO 30 J=IZS,IZI
   IF(TSF.LE.0.0) GO TO 30
   ZSF(J) = ZSF(J) * VOLTZ / TSF
  
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ZSN(J) = ZSN(J) * VOLTZ / TSN
30 ZS(J)=ZS(J)*VOLTZ/TS
DO 32 K=1,3
IF(K.EQ.1) TSA = TS /VOLT
IF(K.EQ.2) TSA = TSF/VOLT
IF(K.EQ.3) TSA = TSN/VOLT
SGLT(K)=SGLT(K)/(TSA*VOLTZ)
SGRT(K)=SGRT(K)/(TSA*VOLTZ)
SGBT(K)=SGBT(K)/(TSA*VOLTR)
SGTP(K)=SGTP(K)/(TSA*VOLTR)
32 CONTINUE
CALL S1SET(SGLT,SGRT,SGBT,SGTP,R,RI,Z,ZI,I1,I2,I3,I4,I10,I12,I13,
1114,IRS,IR1,I2S,I21,I,RS ,ZS )
IF(TSF.LE.0.0) GO TO 34
CALL S1SET(SGLT,SGRT,SGBT,SGTP,R,RI,Z,ZI,I1,I2,I3,I4,I10,I12,I13,
1114,IRS,IR1,I2S,I21,2,RSF,ZSF)
CALL S1SET(SGLT,SGRT,SGBT,SGTP,R,RI,Z,ZI,I1,I2,I3,I4,I10,I12,I13,
1114,IRS,IR1,I2S,I21,3,RSN,ZSN)
C THE FOLLOWING SECTION IS THE CALCULATION OF ALL PERTINENT SOURCE DATA
C AND THE PRINTING OF SUCH
34 WRITE (6,1000) (ID(I),I=1,12)
1000 FORMAT(1H1,2X,12A6/)
1002 WRITE(6,1002) IRS,R(IHS),IRF,R(IRF),IZS,Z(IZS),IZF,Z(IZF)
1
1
1
2)
WRITE(6,1004) IEL
1004 FORMAT(1H02X,19H NO. OF ELEMENTS...I3/)
WRITE (6,1006)
1006 FORMAT(1H03X, 102HELEMENT NO. NAME ATOM DENSITY DENSITY
1 WEIGHT CAPTURES FISSIONS IN,SCATTER /6X,8H(GAM
2D)/)
WTT = 0.
DO 40 M=1,IEL
DO 36 N=1,NEL
IF(NID(N)-NLM(M))36,38,36
36 CONTINUE
GO TO 40
38 RHO = AMU(N)*DNM(M)/0.60248
WT = VOLT * RHO
NAGS 91
NAGS 92
NAGS 93
NAGS 94
NAGS 95
NAGS 96
NAGS 97
NAGS 98
NAGS 99
NAGS 100
NAGS 101
NAGS 102
NAGS 103
NAGS 104
NAGS 105
NAGS 106
NAGS 107
NAGS 108
NAGS 109
NAGS 110
NAGS 111
NAGS 112
NAGS 113
NAGS 114
NAGS 115
NAGS 116
NAGS 117
NAGS 118
NAGS 119
NAGS 120
NAGS 121
NAGS 122
NAGS 123
NAGS 124
NAGS 125
NAGS 126
NAGS 127
NAGS 128
NAGS 129
NAGS 130
NAGS 131
NAGS 132

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WRITE(6,1008) NLM(M),LABEL(N),DNM(M),RHO,WT,STC(M),STF(M),SII(M)
WTT = WTT + WT
1008 FORMAT(7X,I3,6X,A6,5X,1P6E13.5)
40 CONTINUE
WRITE(6,1010) VOLT,WTT
1010 FORMAT(1H0,2X,19H REGION VOLUME.....1PE14.5/
1H0,2X,19H REGION WEIGHT..... E14.5)
1 WRITE(6,1012) TS,TSF,TSN
1012 FORMAT(1H0,2X,18H REGION INTEGRATED//4X18H PHOTON SOURCE.....1PE14
1.5,/4X18H FISSIONS.....E14.5,/4X18H NEUTRON SOURCE...E14.5,/4XNAGS 142
247H PHOTON SOURCE BY GROUP(INTEGRATED AND AVERAGE))
DO 42 K=1,NGG
TST=TSG(K)/VOLT
42 WRITE(6,1014) K,TSG(K),TST
1014 FORMAT(19X,I3,1P2E14.5)
WRITE(6,1000) (ID(I),I=1,12)
WRITE(6,1022)
IRT=IR1-IRS+1
IZT=IZ1-IZS+1
ISTOP=MINO(IRT,IZT)
ISTOP1=MAXO(IRT,IZT)
WRITE(6,1024) R(IRS),(SGLT(K),K=1,3),Z(IZS),(SGBT(K),K=1,3)
DO 44 IP = 1,ISTOP
I = IP + IRS - 1
J = IP + IZS - 1
44 WRITE(6,1024) RI(I),RS(I),RSF(I),RSN(I),ZI(J),ZS(J),ZSF(J),ZSN(J)
I = I + 1
IP = IP + 1
J = J + 1
IF(ISTOP.EQ.ISTOP1) GO TO 56
IF(ISTOP.EQ.IRT) GO TO 50
WRITE(6,1024) RI(I),RS(I),RSF(I),RSN(I),Z(IZF),(SGTP(K),K=1,3)
IP = IP + 1
I = I + 1
IF(IP.GT.ISTOP1) GO TO 48
DO 46 IS = IP,ISTOP1
WRITE(6,1024) RI(I),RS(I),RSF(I),RSN(I)
46 I = I + 1
48 WRITE(6,1024) R(IRF),(SGRT(K),K=1,3)
GO TO 58
50 WRITE(6,1024) R(IRF),(SGRT(K),K=1,3),ZI(J),ZS(J),ZSF(J),ZSN(J)
IP = IP + 1
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J = J + 1
IF(IP,GT,ISTOP1) GO TO 54
DO 52 JS = IP,ISTOP1
WRITE(6,1026) ZI(J),ZS(J),ZSF(J),ZSN(J)
52 J = J + 1
54 WRITE(6,1026) Z(IZF),(SGTP(K),K=1,3)
GO TO 58
56 WRITE(6,1024) R(IRF),(SGRT(K),K=1,3),Z(IZF),(SGTP(K),K=1,3)
58 CONTINUE
IF(IND.EQ.1) GO TO 2
SNT = 0.0
SPT=0.0
SFT = 0.0
DO 60 I= 1,12
DO 60 J= 1,14
VOL1 = VOLR(I)*VOLZ(J)
SNT = SNT + SG(I,J,NGG+2)*VOL1
SFT = SFT + SG(I,J,NGG+1)*VOL1
DO 60 K=1,NGG
60 SPT = SPT + SG(I,J,K)*VOL1
WRITE(6,1016) SPT,SFT,SNT
1016 FORMAT(1H1,2X,23H TOTAL PHOTON SOURCE...1PE14.5,/,
1 1H0,2X,23H TOTAL FISSIONS..... E14.5,/,
2 1H0,2X,23H TOTAL NEUTRON SOURCE.. E14.5,/)
REWIND 9
CALL SCOUT (SG(1,1,NGG+2),RI,ZI,I2,I4,I2,I4,I4,K,18HNEUTRON SOURCE
1 CALL SCOUT ( SG(1,1,NGG+1),RI,ZI,I2,I4,I2,I4,I4,K,18HFISSION DENSITY
1 IF (NPUN,EQ.0) GO TO 72
IRMAX = NEX + NEX1 + I2
IZMAX = JCO
NTEST = IRMAX*IZMAX-2*I1*I3
IF(NTEST.GT.0) WRITE(6,1020) NTEST
DO 62 I=1,IRMAX
DO 62 J=1,IZMAX
62 SC(I,J) = 0.0
KKK = 1
IF (NPUN,EQ.1) NGPUN = NGN
IF (NPUN,GE.2) NGPUN = NGG
WRITE (9) IRMAX,IZMAX,I2,I4,NEX1,NGPUN
DO 70 K = 1,NGPUN
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IF(NPUN.EQ.1) GO TO 64
IF(NPUN.EQ.2) FMPY = 1.0
IF(NPUN.EQ.2) NGT = K
IF(NPUN.EQ.2) GO TO 66
NGT = NGG+1
FMPY = SFDS(K)
GO TO 66
64 NGT = NGG+2
FMPY = CHI(K)
66 DO 68 I = 1,12
DO 68 J = 1,14
IJ = I+ NEX1
68 SC(I,J)=SG(I,J,NGT)*FMPY
1 IF(NPUN.GT.1) CALL SCOUT(SC,RI,ZI,I1,I3,I2,I4,K,18HPHOTON SOURCE
)
1 IF(NPUN.EQ.1) CALL SCOUT(SC,RI,ZI,I1,I3,I2,I4,K,18HNEUTRON SOURCE
)
70 WRITE (9) ((SC(I,J),I=1,IRMAX),J=1,IZMAX)
REWIND 9
WRITE (6, 1018)
1018 FORMAT(65H THE FIXED SOURCE JCO BY (NEX1,ICM,NEX) HAS BEEN WRITTEN ON TAPE)
1020 FORMAT(52H GEOMETRY FOR TAPE WRITE IS TO LARGE FOR STORAGE BY IS)
1022 FORMAT(42HRELATIVE SOURCE AND FISSION DISTRIBUTIONS
FISSION NEUTRON
254H RADIUS PHOTON FISSION NEUTRON
354H HEIGHT PHOTON FISSION NEUTRON
522X,13HDISTRIBUTIONS,19X,22X,13HDISTRIBUTIONS //
654H (CM.) F(R) F(R)
754H (CM.) F(Z) F(Z)
1024 FORMAT(F10.4,2X,F10.4,2X,F10.4,4X,F12.4,4X,
F10.4,2X,F10.4,2X,F10.4,4X,F12.4 )
1026 FORMAT(54X,F10.4,2X,F10.4,2X,F10.4,4X,F12.4 )
1028 FORMAT(/(8X,1P8E12.4))
1030 FORMAT(55(2H. ))
72 RETURN
END
SENTRY
$DATA

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