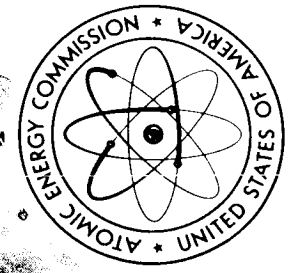


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# A Facsimile Report

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**I. PURPOSE**

The Transient Engine Simulation Program is designed to predict the transient operation of the NERVA rocket engine with minimum run time on the computer; however, the mathematical model is flexible enough to determine the thermal and hydrodynamic characteristics of a wide range of mono-fluid flow systems. Therefore while the Logical Order of Solution, Sec. III, B, is tied into the NERVA engine, it is also applicable to other systems.

## II. SUMMARY

### A. METHOD OF SOLUTION

The transient engine simulation program is a finite-difference, explicit solution, digital-computer program that calculates solid temperature, liquid temperature, and pressure distribution as functions of distance and time throughout the engine system. Separate analyses of the turbopump, hot-bleed port, reflector, shield, core, nozzle, and various tanks and lines are combined to represent the transient performance of the complete engine.

The turbopump assembly model consists primarily of an energy balance, including an energy storage term to account for the angular energy of the rotating machinery.

The analytical representation of the reflector, shield, and core (identified as parts in the program) is a one-fluid-channel finite-difference energy balance. The single-channel representation allows computation simplicity and improves computing speed but necessitates utilization of several unique analysis techniques. The flow channels in the various components are of different size and shape and thus requires incorporation of a "void fraction"\* in the heat-transfer analysis. The void fraction, when used properly, quite satisfactorily simulates the heat transfer of a many-channelled heat exchanger with a one-channel representation. However, this method destroys the hydrodynamic characteristics.

\* The void fraction is defined as the flow area divided by the total heat-transfer area (flow area plus metal area) of the heat exchanger.

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The fluid-pressure distribution is obtained by analyzing the various flow channels and calculating a bulk friction factor for use with the one-channel representation. This method has been tested for nuclear power engine cases and with test data for liquid, cold gas, and ambient gas flows; good results have been obtained in all cases for both heat-transfer and pressure-drop characteristics.

The nozzle, being a counter-current heat exchanger, is not adaptable to the basic model used for the reflector, shield, and core. Therefore, a model was developed treating the nozzle as a single-pass counter-current heat exchanger. The tubes are divided into finite distance increments for pressure-drop and heat-transfer calculations. Calculations are made for flow, heat-transfer coefficients, unique metal conductivities, and exit, entrance and turning pressure losses. Heat-transfer areas, wetted perimeter, and pressure-loss coefficients are required as input. The nozzle-tube representation is accurate for a nuclear transient run since the largest heat addition to the nozzle coolant is due to core exit gases; however this method gives poor results for a nozzle cool-down due to large heat additions from the nozzle tube jacket. A revised nozzle-tube program is presently being developed.

The hot-bleed port subroutine is also a counter-current finite difference routine which balances the turbine flow rate from both the diluent and hot inlet pressures. Entrance loss, exit loss, vena contracts, and angle of diluent injection are considered. The diluent extraction point can be varied within the engine. The representation of the hot bleed is moderately rigorous and agrees well with early tests run on a 2.5-in. hot-bleed port.

A linear predictor routine is used to project the program to the succeeding time point. The predictor is accurate enough to eliminate a closure on the pump discharge pressure, which greatly reduces the overall program running time.

At present a set of eight simultaneous partial differential equations are being programmed for inclusion in this program. The addition of these equations will enable the program to handle any transient fluid flow situation, including two-phase flow.

### B. CAPABILITIES AND ACCURACIES

The program is designed so that the physical characteristics of the system may be input; therefore, the program is extremely flexible and is capable of handling major design modifications.

The single-flow channel, however, somewhat limits the program since this does not permit prediction of the metal temperatures in the tie-rod channel. A model of the tie-rod channel is presently being "checked out", for the inclusion in the program, and it will correct this deficiency.

The program accuracy is a direct function of the input. The closure tolerances, increments for finite differences, pressure-drop constants, and the constants used by the program to calculate convective heat-transfer-film coefficients are input. However, reasonably large time and distance nodes result in only a small error, but greatly improve the program operating time\*. However, if proper input is applied to the program, the results will provide good agreement with test data.

Comparison of this program with data from NRX-A1 showed that the calculated values fell within the test data bandwidth (with the exception, as previously explained, of the nozzle chilldown, where there is a large heat addition to the fluid from the nozzle jacket).

\* For example,  $\Delta t = 1$  sec, and  $\Delta t = 0.2$  sec,

$$\dot{V}_p = 4.36 \quad \dot{V}_p = 4.44$$

This illustrates a difference of 1.8%.

## III. TECHNICAL DISCUSSION

## A. DERIVATION OF EQUATIONS\*

1. Turbopump

The turbopump model consists of four basic equations:

- (1) the turbine work
  - (2) the pump work
  - (3) a calculation of the pressure ratio across the turbine
  - (4) the energy balance on the turbopump assembly.
- a. Turbine Work Done

The turbine work is found by calculating the isentropic turbine work and multiplying it by a turbine efficiency factor.

Turbine work = Turbine efficiency x turbine isentropic

work, or

$$W_{T \text{ act}} = \eta_T W_T C_p (T_{11} - T_{12})_{\text{isen}} \quad (1)$$

Considering isentropic and ideal gas relationships,

$$T_{12} = T_{11} \frac{P_{11}^{\frac{\gamma-1}{\gamma}}}{P_{12}^{\frac{\gamma-1}{\gamma}}} \quad (2)$$

where

$$\frac{\gamma-1}{\gamma} = \frac{R}{\gamma C_p} \quad (3)$$

therefore,

$$T_{12} = T_{11} \frac{P_{11}^{\frac{R}{\gamma C_p}}}{P_{12}^{\frac{R}{\gamma C_p}}} \quad (4)$$

\* A glossary of terms appears as Section IV of this volume.

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Now, substituting pressures for temperature and rearranging algebraically.

$$\dot{W}_T \text{ act} = \eta_T \dot{W}_T C_p T_{11} \left[ 1 - \left( \frac{P_{12}}{P_{11}} \right)^{\frac{R}{\gamma C_p}} \right] \quad (5)$$

b. Pump Work Done

The pump work done is the flow times the enthalpy difference across the pump divided by the pump's efficiency

$$\dot{W}_P \text{ act} = \frac{\dot{W}_P \Delta h}{\eta_P}, \quad (6)$$

c. Pressure Ratio Across the Turbine

The pressure drop across the turbine is controlled by two choked nozzles, the turbine inlet nozzle ( $A_{tn}$ ) and the last-stage rotor of the turbine ( $A_{rn}$ ). Using the isentropic choked equation,\* it is possible to calculate  $P_{12}$  and  $P_{11}$  from the turbine flow rate as functions of  $T_{12}$  and  $T_{11}$ :

$$P_{12} = \frac{\dot{W}_T \sqrt{T_{12}}}{A_{rn} (.1596)} \quad \text{and} \quad P_{11} = \frac{\dot{W}_T \sqrt{T_{11}}}{K_t} \quad (7)$$

where

$$K_t = (.1596 A_{tn})$$

By equating  $\dot{W}_T$ , we obtain

$$\frac{P_{12}}{P_{11}} = \frac{K_t}{A_{rn} (.1596)} \sqrt{\frac{T_{12}}{T_{11}}} \quad (8)$$

\*Acker Shapiro, Dynamics and Thermodynamics of Compressible Fluid Flow, page 63, Ronald Press Co.

Actual temperature differential across the turbine is equal to the product of turbine isentropic temperature differential and turbine efficiency:

$$\Delta T = \eta_T \Delta T_{\text{isen}} \quad (9)$$

$$(T_{12} - T_{11}) = \eta_T (T_{12 \text{ isen}} - T_{11}) \quad (10)$$

solving for

$$\frac{T_{12}}{T_{11}} = 1 - \eta_T \left( 1 - \frac{T_{12 \text{ isen}}}{T_{11}} \right) \quad (11)$$

Now, since

$$\frac{T_{12 \text{ isen}}}{T_{11}} = \left( \frac{P_{12}}{P_{11}} \right)^{\frac{R}{\gamma C_p}} \quad (12)$$

then

$$\frac{T_{12}}{T_{11}} = \left( \frac{P_{12}}{P_{11}} \right)^{\frac{R}{\gamma C_p}} \quad (13)$$

Now, substituting for  $\frac{T_{12}}{T_{11}}$  in Equation 8, we obtain

$$\frac{P_{12}}{P_{11}} = \frac{K_t}{A_{rn} (.1596)} \sqrt{1 - \eta_T \left[ 1 - \left( \frac{P_{12}}{P_{11}} \right)^{\frac{R}{\gamma C_p}} \right]} \quad (14)$$

The above equation lends itself to a digital iteration solution.



d. Energy Balance on the Turbopump Assembly

To obtain the pump work at time (i + 1), the average pump work between this time (i + 1), and i, plus the change in rotational energy over that time difference is equated to the average turbine work for the same time period, as given by

$$\frac{W_{p \text{ act}}(i) + W_{p \text{ act}}(i+1)}{2} + \frac{d \left( \frac{I \omega^2}{2} \right)}{dt} = \frac{W_{T \text{ act}}(i) + W_{T \text{ act}}(i+1)}{2} \quad (15)$$

rearranging,

$$W_{p \text{ act}}(i+1) = W_{p \text{ act}}(i) - \frac{d(I \omega^2)}{dt} + W_{T \text{ act}}(i) + W_{T \text{ act}}(i+1) \quad (16)$$

Using finite difference integration on  $\frac{d(I \omega^2)}{dt}$  and solving for

$$\omega^2 = \frac{2\pi}{60} \left( N^2 \right) \quad (16a)$$

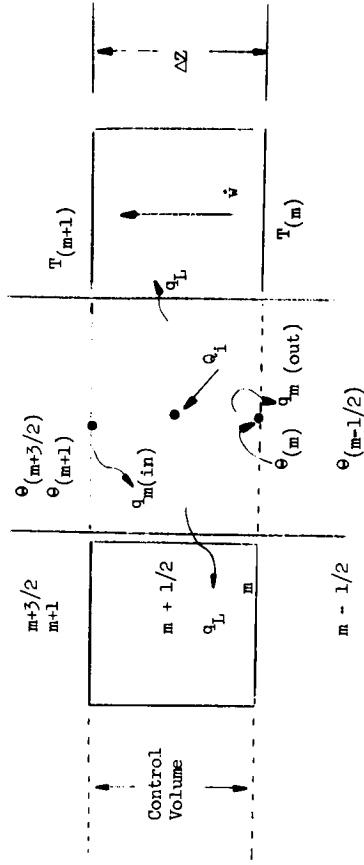
$$\frac{d(I \omega^2)}{dt} = \frac{I}{12G \Delta t} \left( \frac{2\pi}{60} \right)^2 \left( N^2(i+1) - N^2(i) \right) \quad (17)$$

Substituting into the above, the equation for  $W_{p \text{ act}}(i+1)$  is obtained as

$$W_{p \text{ act}}(i+1) = -W_{p \text{ act}}(i) - \frac{I}{12G \Delta t} \left( \frac{2\pi}{60} \right)^2 \left( \frac{N^2(i+1) - N^2(i)}{778} \right) + W_{T \text{ act}}(i+1) + W_{T \text{ act}}(i) \quad (18)$$

2. General Heat-Transfer Equations

The general heat-transfer model consists of two energy balances, one on a liquid node and one on a metal node. A control volume is assumed as follows:



The energy into the control volume is equated to the energy out of the control volume

$$\frac{\partial E_{in}}{\partial t} = \frac{\partial E_{out}}{\partial t}$$

The energy balance on the liquid assumes steady flow and steady-state over the distance increment, and thus no energy storage in the liquid. Therefore,

$$h_f \Delta Z F_p \left[ \theta_{(m+1/2,n)} - T_{(m+1/2,n)} \right] = \dot{V} C_p \left[ T_{(m+1,n)} - T_{(m,n)} \right] \quad (19)$$

Define

$$M = \frac{\dot{V} C_p}{h_f \Delta Z F_p} \quad (20)$$

and substitute into the above. Then,

$$T_{(m+1,n)} - T_{(m,n)} = \frac{1}{M} \left[ \theta_{(m+1/2,n)} - T_{(m+1/2,n)} \right] \quad (21)$$

Assuming the temperature distribution in the fluid control volume varies linearly with distance, the average temperature of the fluid node becomes

$$T_{(m+\frac{1}{2}, n)} = \frac{T_{(m+1, n)} + T_{(m, n)}}{2} \quad (22)$$

Now, substituting into the above and rearranging to solve for  $T_{(m+1, n)}$  we obtain the next fluid temperature

$$T_{(m+1, n)} = \frac{2\theta_{(m+\frac{1}{2}, n)} + (2M-1) T_{(m, n)}}{2M+1} \quad (23)$$

The energy balance on the metal control volume is more complex than that of the liquid; the energy from the previous node, plus the nuclear energy, minus the energy lost to the next node and the fluid, is equated to the energy storage,

$$\frac{\partial E_{in}}{\partial t} - \frac{\partial E_{out}}{\partial t} = \frac{\partial E_{storage}}{\partial t}$$

Substituting equivalent values,

$$q_m(in) + q_1 + q_m(out) - q_L = \frac{\partial E_{storage}}{\partial t} \quad (24)$$

Substituting and gathering terms,

$$\begin{aligned} \frac{2k(1-f) A_F}{f \Delta Z} \theta_{(m, n)} - \theta_{(m+\frac{1}{2}, n)} + q_1 - \frac{2k(1-f) A_F}{f \Delta Z} \theta_{(m+\frac{1}{2}, n)} - \theta_{(m+1, n)} \\ - \dot{v} C_P T_{(m+1, n)} - T_{(m, n)} = \frac{\Delta Z(1-f) A_F C_P R}{\Delta t f} \theta_{(m+\frac{1}{2}, n+1)} - \theta_{(m+\frac{1}{2}, n)} \end{aligned} \quad (25)$$

Define N as equal to

$$\frac{\Delta Z(1-f) A_F C_P R}{f \Delta t \dot{v} C_P} \quad (26)$$

Substituting and gathering terms

$$\begin{aligned} \theta_{(m+\frac{1}{2}, n+1)} - \theta_{(m+\frac{1}{2}, n)} \\ = \frac{1}{N} \left[ T_{(m, n)} - T_{(m+1, n)} \right] + \frac{2k \Delta t}{(\Delta Z)^2 \rho_R C_R} \left[ \theta_{(m+1, n)} - 2\theta_{(m+\frac{1}{2}, n)} + \theta_{(m, n)} \right] + \frac{q_1}{\dot{v} C_P N} \end{aligned} \quad (27)$$

Define S as equal to

$$\frac{2k \Delta t}{(\Delta Z)^2 \rho_R C_R} \quad (28)$$

Assuming the temperature gradient in the metal node varies linearly with distance,

$$\theta_{(m+1, n)} = \frac{\theta_{(m+\frac{3}{2}, n)} + \theta_{(m+\frac{1}{2}, n)}}{2} \quad (29a)$$

and

$$\theta_{(m, n)} = \frac{\theta_{(m+\frac{1}{2}, n)} + \theta_{(m-\frac{1}{2}, n)}}{2} \quad (29b)$$

Now, substituting Equations (29a) and (29b) into Equation (27),

$$\theta_{(m+\frac{1}{2}, n+1)} = \frac{1}{N} \left[ T_{(m, n)} - T_{(m+1, n)} \right] + \frac{S}{2} \left[ \theta_{(m+\frac{3}{2}, n)} - 2\theta_{(m+\frac{1}{2}, n)} + \theta_{(m-\frac{1}{2}, n)} \right] + \frac{q_1}{\dot{v} C_P N} \quad (30)$$

From Equation (25),

$$\theta_{(m+\frac{1}{2}, n)} = \frac{(2M+1) T_{(m+1, n)} - (2M-1) T_{(m, n)}}{2} \quad (31)$$

Substituting in the above and gathering terms

$$\theta_{(m+\frac{1}{2},n+1)} = \theta_{(m+\frac{1}{2},n)} \left[ 1 - \frac{2}{N(2M+1)} \right] + T_{(m,n)} \left[ \frac{1}{N} - \frac{2M-1}{N(2M+1)} \right] + \frac{Q_1}{\dot{w} C_p N} + \frac{2}{N} \theta_{(m+\frac{1}{2},n)} - 2\theta_{(m+\frac{1}{2},n)} + \theta_{(m-\frac{1}{2},n)} \quad (32)$$

Let

$$U = \frac{Q_1}{\dot{w} C_p N} = \frac{H \Delta T}{\rho_R C_R} \quad (33)$$

and substituting Equation (26) into (32), and  $Q_1 = \frac{H \Delta Z (1-f) A_F}{f}$

$$U = \frac{Q_1 f \Delta t}{\rho_R C_R \Delta Z (1-f) A_F}$$

Therefore,

$$\theta_{(m+\frac{1}{2},n+1)} = \theta_{(m+\frac{1}{2},n)} \left[ 1 - \frac{2}{N(2M+1)} \right] + T_{(m,n)} \left[ \frac{1}{N} - \frac{2M-1}{N(2M+1)} \right] + U + \frac{2}{N} \theta_{(m+\frac{1}{2},n)} - 2\theta_{(m+\frac{1}{2},n)} + \theta_{(m-\frac{1}{2},n)} \quad (34)$$

3. Pressure-Drop Calculation

The pressure-drop calculation is a combination friction and heat-transfer pressure drop that is proportional to  $\frac{\dot{w}^2}{A^2 \rho}$

$$\Delta P = \frac{\dot{w}^2}{A_F^2 \rho 2g} \frac{T_{(m+1,n)} - T_{m,n}}{T_{m,n}} + \frac{4\phi \Delta Z}{\beta} \quad (35)$$

Rearranging,

$$P_{(m,n)} - P_{(m+1,n)} = \frac{\dot{w}^2}{A_F^2 2g \rho} \frac{T_{(m+1,n)} - T_{(m,n)}}{T_{(m,n)}} + \frac{4\phi \Delta Z}{\beta} \quad (36)$$

and

$$P_{(m+1,n)} = P_{(m,n)} - \frac{\dot{w}^2}{A_F^2 \rho 2g} \left[ \frac{T_{(m+1,n)} - T_{(m,n)}}{T_{(m,n)}} \right] + \frac{4\phi \Delta Z}{\beta} \quad (37)$$

4. Flow Rate Capacitance Effects

The change in flow rate over the next time point is equated to the change in flow rate over the previous time point, plus the mass change

$$\dot{w}_{(m+1,n)} - \dot{w}_{(m,n)} = \dot{w}_{(m,n-1)} + \frac{A_T \Delta Z}{\Delta t} \left[ \rho_{(m,n-1)} - \rho_{(m,n)} \right] \quad (38)$$

Therefore,

$$\dot{w}_{(m+1,n)} = \dot{w}_{(m,n)} + \frac{A_T \Delta Z}{\Delta t} \left[ \rho_{(m,n-1)} - \rho_{(m,n)} \right] + \dot{w}_{(m,n-1)} - \dot{w}_{(m+1,n-1)} \quad (39)$$

5. Hot-Bleed-Port and Nozzle-Tube Model

The heat-transfer and pressure-drop equations explained in paragraphs 2 and 3, above, are basically the same as those used in the hot-bleed-port and nozzle-tube programs. Complete descriptions of the equations used in the hot-bleed-port and nozzle-tube programs are available in REON Reports 8209-64-2 and 8209-64-5, respectively. Copies of these reports may be obtained by contacting the Manager, Contracting Division, REON.

B. LOGICAL ORDER OF OPERATION

Covering subroutines are referenced by comparable letters in enclosing brackets. Unless otherwise referenced, see Figure 1, AZM.

Steps

1. Read in AGC-modified LASL (PRPTY) hydrogen properties subroutine.
2. Set up curves for the pump under investigation of  $\frac{\Delta H}{N^2}$  as a function of  $\frac{Q}{N}$  and  $\frac{h_{sv}}{N^2}$  for interpolation.
3. Read standard case, which details the parameters describing the physical system. See AZXC. If an error is detected, print "ERROR IN STANDARD INPUT" and stop. If a tape check occurs, print "BAD TAPE - FLUSH," and stop.
4. Set counter to begin storing at first part (ref. II,A in text). See AZXA.
5. Test next card to see if a standard input is desired. If there is no input remaining, print "END OF INPUT" and stop. If tape check occurs, print "BAD TAPE - FLUSH," and stop.
6. Read in the input for the next part. If no input cards remain, print, "END OF INPUT," and stop, transferring to AZM-12. If the same number of parts as contained in the standard case are read in and no final "T" card is encountered, to flag end of input, print "ZERO T CARD MISSING," and stop.
7. If the final "T" card has been read, go to step 18; if not, continue.
8. Print input for this part.
9. Prepare to set up the input curves (AZM-7). If this is the first part, all input curves are expected. If this is not the first part, the number of curves for one part will be expected.
10. Check the next curve. If the number of points is -1, go to step 12. If the number of points is greater than the maximum number or less than 2, print "ERROR IN PTS/CURVE" and go to step 237.

11. Set up the curve for linear interpolation. See AZM-8.
12. If the required number of curves are not read in, go to step 10.
13. If the number of nodes input for this part is greater than the maximum, print "TOO MANY NODES" and go to step 237.
14. Set inlet and outlet plenum densities and the density for each node to  $\rho = f(\theta_0 \text{ and } P_0 \text{ min})$ ; thus the density is determined by the initial metal temperature and the minimum outlet pressure. Set all metal temperatures equal to  $\theta_0$  and all flow rates to zero.
15. Compute total distance from AZM-19.

$$Z_{\text{max}} = (\text{Number of nodes} + \frac{1}{2}) \Delta Z$$

16. If there is not enough storage for this part, go to step 236.
17. Set the counter to read in the next part, and go to step 6.
18. If no parts have been read in and the final "T" card is read in, stop.

19. Set counter to compute input number of time points.

20. Begin program initialization.

21. If the diluent extraction point is zero or beyond the last part, print "NO DILUENT REMOVED" and stop.

22. Set time  $t_i = -\Delta t$ .

23. Time  $t_{i+1} = \Delta t + t_i$ .

24. If input  $P_1$  is not zero, go to step 31.

25. Interpolate input curves for  $P_1$  and  $T_1$  at time 0.

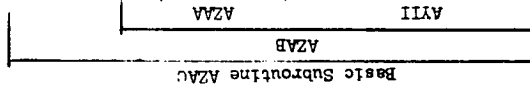
26. Find  $h_1 = f(P_1, T_1)$  in hydrogen properties subroutine.

27. Find  $\rho_1 = f(P_1, T_1)$  in hydrogen properties subroutines.

If error occurs, print "BAD TANK PRESS, TEMP" and stop the program.

28. Find  $S = f(P_2 \text{ and } T_1 + \Delta T)$  in parahydrogen properties subroutine.

29. Find vapor pressure at pump inlet. If the pressure is greater than the total pressure at the pump inlet, print "GAS AT PUMP INLET" and stop.



30. Find pump inlet saturated vapor head.

$$h_{sv} = \frac{P_1 - P_1 \text{ vapor}}{12 \rho_1} \frac{\text{ft-lbf}}{\text{lbm}} \quad (\text{Eq. PR34})$$

31. If the input gate position is not zero, go to step 33.

32. Interpolate input curve for gate position at time zero.

33. If input tank pressure is zero, go to step 35.

34. For functions of  $P_{1(i+1)}$  at  $P_{1 \text{ input}}$  and  $T_{1 \text{ input}}$ , find entropy and hydrogen properties at  $P_1$  and  $T_1$ . If an error occurs in the hydrogen properties subroutine, print "BAD TANK TEMP, PRS" and stop the program.

35. If input gate position is zero, go to step 37.

36. G.P. = G. F. input.

37.  $P_{10} = P_{1c} - I_{1(i+1)}$ ,  $T_{10} = T_{20} = T_{2(i+1)}$ , Pump-outlet conditions at zero time are set equal to pump-inlet conditions.

38. Set  $P_{0 \text{ min}}$  equal to the input minimum outlet pressure

39. Set  $M_{(i+1)}$  equal to input initial turbine speed

40. Set  $\dot{w}_{T(i+1)}$  equal to input pump flow-rate guess

41. Set  $\dot{w}_{c(i+1)}$  equal to input diluent flow-rate guess

42. Set  $\dot{w}_{n(i+1)}$  equal to input not-bleed-port flow-rate guess

43. The predicted values for  $P_0, P_8, T_8, P_{11}, T_{11}, T_{12}, Q_p, \dot{w}_p$  are  $\dot{w}_n$  set, and  $H$  are not used in the initial computations and are therefore set equal to zero.

44. Place input not-bleed-port parameters in storage for hot bleed port program.

45. Set initial  $T_0$  for nozzle tubes equal to the input initial metal temperature.

42. If the nozzle tube subroutine is not required, go to step 46.

43. Find  $\sqrt{T_6}$ ; if  $T_6 < 0$ , stop the problem.

44. If input  $P_{0 \text{ min}}$  is not zero, set  $P_6$  equal to input  $P_{0 \text{ min}}$ . If input  $P_{0 \text{ min}}$  is zero, interpolate input curve for  $P_{0 \text{ min}}$  at initial time and set  $P_6$  equal to this value.

45. Set the initial  $q_1$  guess equal to the input initial  $q_1$  guess.

46. If input  $P_{11}$  is not zero, set flag to proceed with turbopump calculations as though the hot-bleed port were replaced with a star bottle.

47. Set flags to print nozzle tube and/or hot-bleed port iterations if desired.

48. Set flag to print only inlet and outlet distance nodes for each part if desired.

49. Flag option to ignore nozzle tube choking.

50. Move print-out paper to a new page. Return to AZM-31 and go to AZA

51. Set  $t_i$  equal to  $t_{(i+1)}$ , and proceed to next time point.

52. If  $P_{0 \text{ min}}$  input is zero, interpolate input curve for  $P_{0 \text{ min}}$  at next time point.

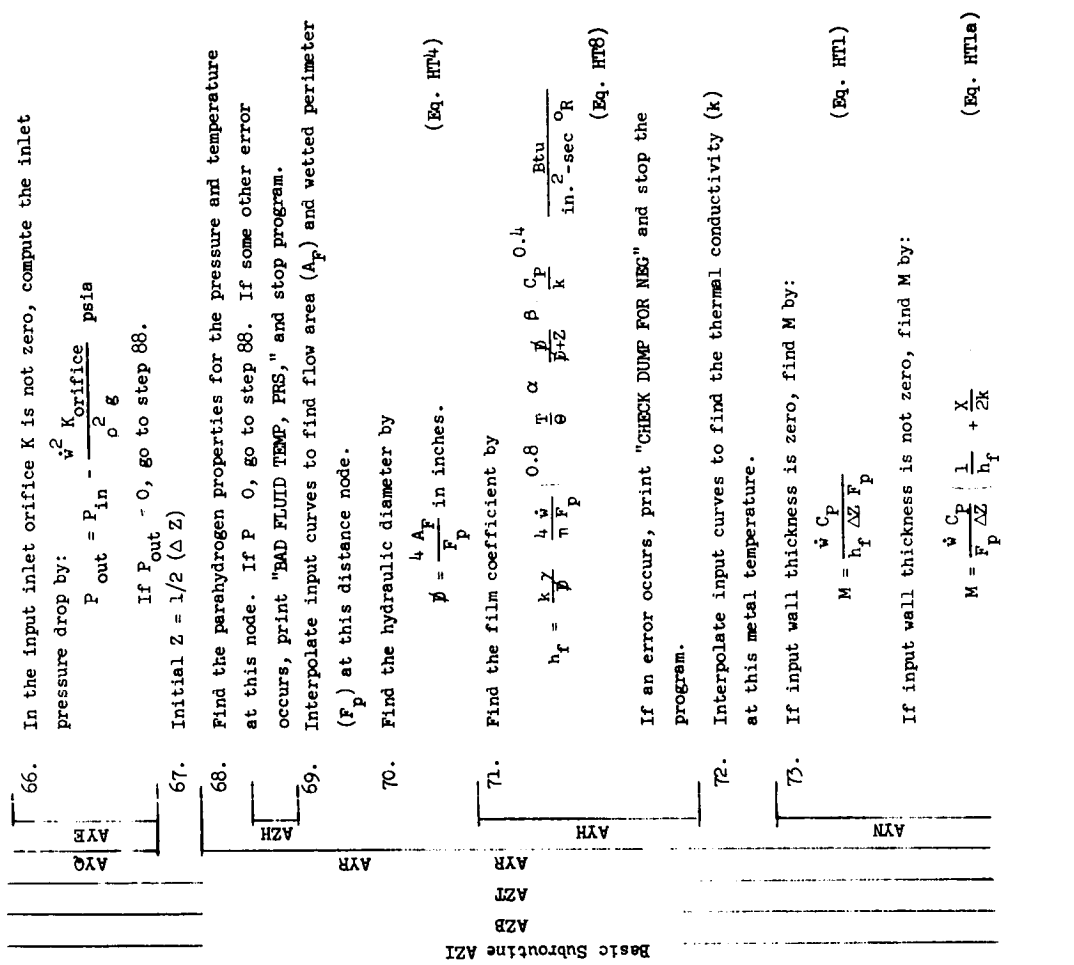
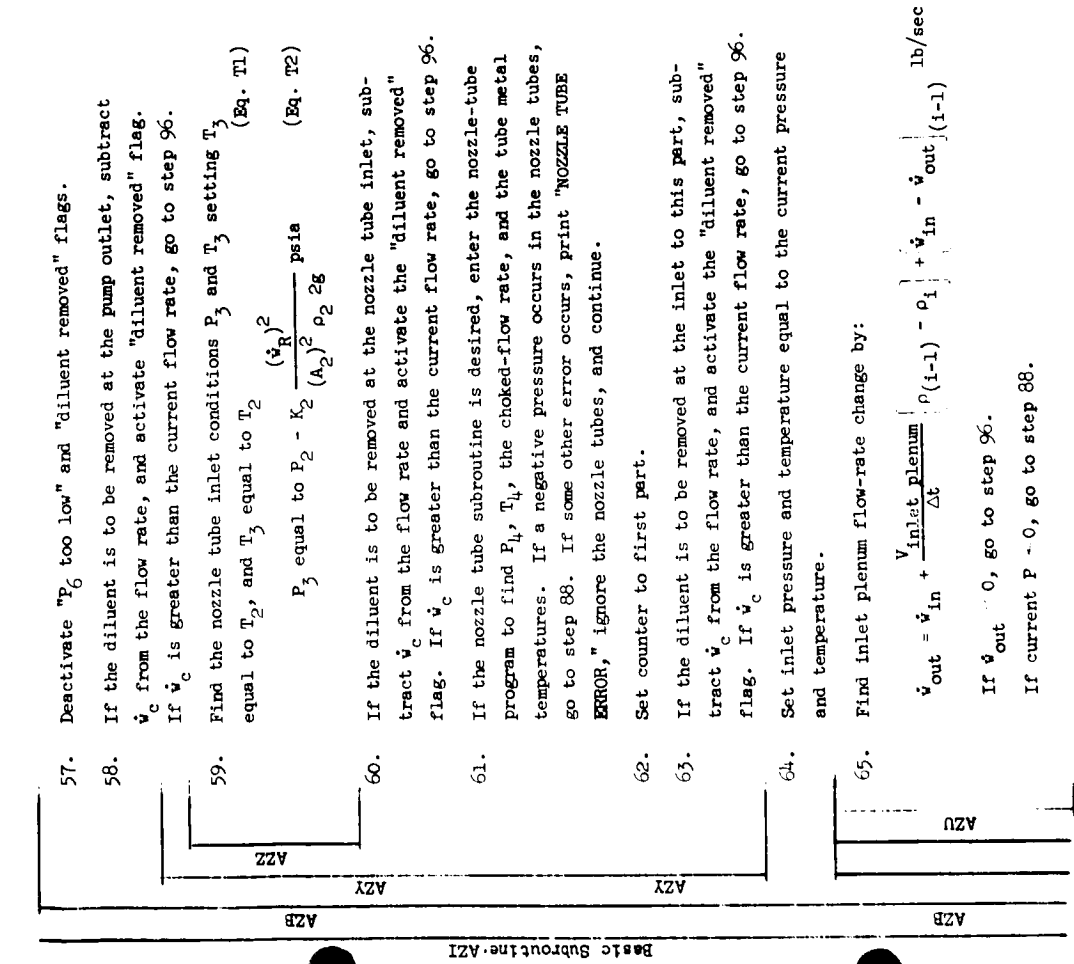
53. Set the following values at the current time point equal to the predicted values from the preceding time point:  $P_1, T_1, P_2, T_2, G.P., N, \rho_1, \Delta H, \dot{w}_p, \dot{w}_c, H_{sv}$ .

54. Print inlet conditions for this time point.

55. Begin iteration to find pump flow ( $\dot{w}_{P_i}$ ) by closing on the calculated pressure in comparison with the pressure required to choke the main nozzle.

56. Set diluent flow rate to the value computed by the hot-bleed-port program. Note that initially this value is that predicted in the previous time interval.

Set temperature equal to  $T_2$ , pressure equal to  $P_2$ , and flow rate equal to  $\dot{w}_p$ .



74. If  $M < 1/2$ , activate "M too small" flag.

75. Find fluid temperature for the next node by setting

$$T_{(m+1,n)} = \frac{2\theta_{(m+1/2,n)} + (2M-1) T_{(m,n)} \theta_R}{2M+1} \quad (\text{Eq. HT9})$$

76. Find the fluid pressure for the next node by:

$$P_{(m+1,n)} = P_{(m,n)} - \frac{v^2}{A_p^2 \rho} \frac{2\theta_{(m+1/2,n)} + (2M-1) T_{(m,n)} \theta_R}{T_{(m,n)}} + \frac{4\theta \Delta Z}{\beta} \text{ psia} \quad (\text{Eq. HT6})$$

If  $P_{(m+1,n)}$  is  $< 0$ , go to step 88.

77. Find the capacitance flow rate change by setting

$$\dot{v}_{(m+1,n)} + \dot{v}_{(m,n)} + \frac{A_f \Delta Z}{\Delta t} \left[ \frac{P_{(m,n-1)} - P_{(m,n)}}{\rho} \right] + \left[ \dot{v}_{(m,n-1)} - \dot{v}_{(m+1,n-1)} \right] \text{ lb/sec} \quad (\text{Eq. HT13})$$

If  $\dot{v}_{(m+1,n)} < 0$ , go to step 96.

78. Set  $Z = Z + \Delta Z$  (meaning, proceed to next distance node)

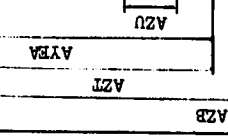
79. If all nodes for this part have not been processed, to to step 68.

80. If input outlet orifice  $K$  is not zero, find the pressure drop by:

$$P_{\text{out}} = P_{\text{in}} - \frac{v^2 K_{\text{outlet orifice}}}{\rho} \text{ psia} \quad (\text{Eq. HT12})$$

If  $P_{\text{out}} < 0$ , go to step 88.

81. Set outlet pressure equal to the current pressure.



82. Find the outlet flow rate change by:

$$\dot{v}_{\text{out}} = \dot{v}_{\text{in}} + \frac{V_{\text{outlet plenum}}}{\Delta t} \left[ \rho_{(i-1)} - \rho_{(i)} \right] + \dot{v}_{\text{in}(i-1)} - \dot{v}_{\text{out}(i-1)} \quad (\text{Eq HT13a})$$

If  $\dot{v}_{\text{out}} < 0$ , go to step 96.

83. Set outlet flow rate equal to the current flow rate.

84. Set increment counter to process next part. If all parts have not been processed, go to step 63.

85. Set  $P_6$  and  $T_6$  to current pressure and temperature.

86. If  $P_6$  is less than  $P_{0 \text{ min}}$ , activate "P<sub>0</sub> too low" flag.

87. Go to step 89. (Exit AZB)

88. If the current pressure is negative, go to step 97. If not, print "HEAT TRANSFER ERROR" and stop the program. (AZB, AZFF)

89. If a start bottle is used, go to step 99.

90. Enter hot-bleed port program to find  $\dot{v}_c$ ,  $\dot{v}_h$ ,  $\dot{v}_M$ , and  $P_8$ .

If a negative pressure occurs, go to step 101. If  $\dot{v}_h$  is negative somewhere, go to step 99.

91. If  $\dot{v}_M$  from the hot-bleed port program and the calculated  $\dot{v}_M$  agree within the input tolerance, go to step 93.

92. Calculate a new  $\dot{v}_p$  guess and adjust if necessary to arrive at a value between the given maximum and minimum values. If the maximum number of iterations has been exceeded, go to step 98. If not, go to step 56.

93. If the diluent flow rate used does not agree with  $\dot{v}_c$  from the hot-bleed port program within the input tolerance, and the maximum number of iterations has not been exceeded, go to step 56. If the maximum number of iterations has been exceeded, go to step 98.

94. Store the number of iterations for printing.

95. Go to step 102 and exit AZI.



Basic Subroutine AZ1

Basic Subroutine AZ1

96. A negative flow rate has occurred somewhere in the system. If the "DILUENT REMOVED" flag is active, subtract the diluent flow from the current pump flow, and use this as a lower limit on  $\dot{v}_p$ . If not, use the current  $\dot{v}_p$  as the lower limit. Go to step 92.

97. A negative pressure has occurred somewhere in the system. If the "DILUENT REMOVED" flag is active, add the diluent flow from the current pump flow and use this as an upper limit on  $\dot{v}_p$ . If not, use the current  $\dot{v}_p$  as an upper limit. Go to step 92.

98. Print "WR, WC NOT CLOSED"; set number of iterations to the maximum and go to step 95.

99. Compute nozzle choke flow as follows, assuming  $\dot{v}_h = 0$ :

$$\dot{v}_N \text{ choke} = \frac{0.1396 A^* P_6}{\sqrt{T_6}} \text{ lb/sec} \quad (\text{Eq. HT11})$$

100. If  $\dot{v}_N$  choke and  $\dot{v}_N$  calculated agree within the input tolerance, go to step 94. If not, go to step 92.

101. Halve the diluent flow rate. If the maximum number of iterations has been exceeded, go to step 98. If not, go to step 50.

102. Print the main engine system parameters. The following error messages are printed if applicable: "LIQ IN TUBE THROAT," "M TOO SMALL," "TEMP EXCEEDED MAX," "PG TOO LOW."

103. Set counter to first part. Prepare to transfer current values to past time values.

104. Set past time point inlet and outlet plenum densities and flow rates equal to current values.

105. Set past time point densities and flow rates for each node equal to current values.

106. If all parts have not been processed, set counter to next part and go to step 104.

AZFP

107. Print Values predicted from the preceding time point.

108. Find  $Q_{p1}$  from the following equations:

$$Q_{p1} = \frac{\dot{v}_p}{P_1 (0.00228)(1728)} \text{ gal/min} \quad (\text{Eq. PT18})$$

$$\beta = \frac{P_6}{\dot{v}_p} \quad (\text{Eq. PT19})$$

$$\alpha = (P_2 - P_6) \dot{v}_p^2 \quad (\text{Eq. PT14})$$

109. If a start bottle is not being used, go to step 127.

110. Set  $P_{11}$  and  $T_{11}$  equal to the input  $P_{11}$  and  $T_{11}$ .

111. Find  $\sqrt{T_{11}}$ . If  $T_{11} < 0$ , stop the program.

112. Find  $P_{11}$  from the following:

$$P_{11} = \dot{v}_T \frac{\sqrt{T_6}}{K_t} \text{ psi} \quad (\text{Eq. PT7})$$

113. De-activate "P<sub>12</sub> not closed" flag.

$$114. \text{ Find } \eta_t = \left[ -6.718076 \times 10^{-6} \frac{N_1}{\sqrt{T_{11}}} + \left( .11039226 \times 10^{-2} \right) \left[ \frac{N_1}{\sqrt{T_{11}}} \right] \right]$$

115. Set the upper limit on  $P_{12i}$  equal to  $P_{11i}$ .

116. Find  $C_{p11}$  from  $P_{11}$ ,  $T_{11}$ . If an error occurs, stop.

117. Begin the iteration to find  $P_{12i}$  by closing on  $\left( \frac{P_{12}}{P_{11}} \right)_i$

$$118. \text{ Find } T_{12} = T_{11} \left[ \frac{P_{12}}{P_{11}} \right]^{c_R} \quad (\text{Eq. PT44})$$

$$119. \text{ Find } \eta_T = \eta_T^i + \frac{7 R T_{12}}{(7+1) C_{p11} (778) (T_{11} - T_{12})} \quad (\text{Eq. PT45})$$

Basic Subroutine AYPA

AY1

AZH

AWB

Basic Subroutine

AZPI

AZK



$$120. \text{ Find } \left( \frac{P_{12}}{P_{11}} \right) = \frac{K_t}{2 A_{th} (.1396)} \sqrt{1 - \eta_{T1} \left[ 1 - \left( \frac{P_{12}}{P_{11}} \right) \right]} \left[ \frac{R}{778 C_p 11} \right] \quad (\text{Eq. PT9})$$

121. If  $\left( \frac{P_{12}}{P_{11}} \right)$  and  $\left( \frac{P_{12}}{P_{11}} \right)'$  are within the input closure tolerance, continue. If not, calculate a new  $P_{12}$  guess and adjust, if necessary, so it lies between the given minimum and maximum values. If the maximum number of iterations has been exceeded, activate the "P<sub>12</sub> not closed" flag and continue. If not, go to step 118.

$$122. \text{ Find } \dot{W}_{T \text{ act } i} = \dot{W}_{T i} \eta_{T i} C_p 11 T_{11} \left[ 1 - \left( \frac{P_{12}}{P_{11}} \right) \right] \quad \text{Btu/sec} \quad (\text{Eq. PT10})$$

123. Find  $\eta_p$  from program curves as a function of  $Q_p/W$  and  $NPSP/M^2$ .

$$124. \text{ If } \eta_p = 0, \text{ set } \dot{W}_p \text{ act } i = 0, \text{ and go to step 127.}$$

$$125. \text{ Find } \dot{W}_p \text{ act } i = \dot{W}_p \text{ act } i = \frac{\dot{W}_p \Delta h}{\eta_p} \quad \text{Btu/sec} \quad (\text{Eq. PT21})$$

126. Go to step 140. (Exit AYL).

$$127. \text{ Find } \dot{W}_{T i} = \dot{W}_{h i} + \dot{W}_{c i} \quad \text{lb/sec} \quad (\text{Eq. PT27a})$$

$$128. \text{ Find } K_6 = \frac{T_8 i \dot{W}_{T i}}{T_2 i \dot{W}_{c i} + T_6 i \dot{W}_{h i}} \quad \text{unitless} \quad (\text{Eq. PT27})$$

$$129. \text{ Find } K_{10} = \frac{\dot{v}_c}{\sqrt{P_2 - P_{HM}}} \quad \text{lb/sec, psia}^{1/2} \quad (\text{Eq. PT36})$$

$$130. \text{ Find } K_{16} = \frac{\dot{v}_h}{\sqrt{P_6 - P_{HM}}} \quad \text{lb/sec, psia}^{1/2} \quad (\text{Eq. PT35})$$

$$131. \text{ Find } K_{12} = \frac{\dot{v}_T}{V} \quad \text{lb/in.} \quad (\text{Eq. PT37})$$

$$132. \text{ Find } K_{13} = \frac{\dot{v}_h}{V_{HM}} \quad \text{lb/in.} \quad (\text{Eq. PT38})$$

$$133. \text{ Find } K_{14} = \frac{\dot{v}_c}{V_{CM}} \quad \text{lb/in.} \quad (\text{Eq. PT39})$$

$$134. \text{ Find } K_{15} = \frac{\dot{v}_c}{\sqrt{P_2 - P_{CM}}} \quad \text{lb/sec, psia}^{1/2} \quad (\text{Eq. PT40})$$

$$135. \text{ Find } K_{V(i+1)} = A \left[ \text{CP}(i+1) \right] - B \quad (\text{Eq. PT33})$$

$$136. \text{ Find } K_3 = 1/K_t^2 + K_{1(i+1)} + K_2 \frac{\text{lb}^2 \text{ sec}^2}{\text{lbm}^2 \text{ in.}^4 \text{ }^\circ\text{R}} \quad (\text{Eq. PT30})$$

where  $R (2 P_{H2O})$   
 $K_{1(i+1)} = \frac{R (2 P_{H2O})}{K_{V(i+1)}^{1.44}} \frac{\text{lb}^2 \text{ sec}^2}{\text{lbm}^2 \text{ in.}^4 \text{ }^\circ\text{R}} \quad (\text{Eq. PT30a})$

$$K_2 = \frac{R (K_{11} + K_9) (12)}{A^2 g} \frac{\text{lb}^2 \text{ sec}^2}{\text{lbm}^2 \text{ in.}^4 \text{ }^\circ\text{R}} \quad (\text{Eq. PT30b})$$

$$K_t = A_{tn} \sqrt{\frac{7.5}{R(12)}} \frac{2}{(7+1)} \quad (\text{Eq. PT30c})$$

$$137. \text{ Find } T_{11 i} = T_8 i, \text{ }^\circ\text{R} \quad (\text{Eq. PT6})$$

$$138. \text{ Find } \dot{W}_{T i} = P_{11 i} \frac{K_t}{\sqrt{T_{11}}} \quad \text{lbm/sec} \quad (\text{Eq. PT7})$$

139. Go to step 113.

140. Print corrected values.

141. If all of the desired number of time points have been computed, go to step 4.

Basic Subroutine AYPB

AZPP

142. Set counter to compute metal temperatures for the first part at the next time.
143. Deactivate "maximum temperature exceeded" flag for this part.
144. Set time to time at which last fluid computations were made.
145. Set the node counter to the first node for this part.

$$A = 1/2 (\Delta Z)$$

146. Find the average flow rate for this node

$$\dot{v}_{(m+1/2)} = 1/2 [\dot{v}_{(m)} + \dot{v}_{(m+1)}]$$

147. Interpolate the input curves to find  $A_F$  and  $F_P$  at this distance node.

148. Find the average pressure, temperature, and specific heat for this node.

$$T_{(m+1/2)} = 1/2 [T_{(m)} + T_{(m+1)}]$$

$$P_{(m+1/2)} = [P_{(m)} + P_{(m+1)}]$$

$$C_P (m+1/2) = 1/2 [C_{Pm} + C_{P(m+1)}]$$

149. Interpolate the input curves to find  $C_p$  and  $k$  for the metal temperature at this node.

150. Interpolate input curves for total heat-generation coefficient at this time point and fraction of total for this distance node. The internal heat-generation coefficient for this node will be the product of the total and the fraction.

151. If input wall thickness is 0, find  $M$

$$M = \frac{\dot{v} C_p}{h_f \Delta Z F_P} \quad (\text{Eq. HT1})$$

If not,

$$M = \frac{\dot{v} C_p}{F_P \Delta Z} \left[ \frac{1}{h_f} + \frac{X}{2k} \right] \quad (\text{Eq. HT1a})$$

152. If  $M < 1/2$ , activate "m too small" flag.

153. If input wall thickness is 0, find  $N$

$$N = \frac{f \Delta t \dot{v} C_p}{\Delta Z (1-f) A_F \rho_R C_R} \quad (\text{Eq. HT2})$$

If not,  $\Delta Z \pi (\rho - x) \rho_R C_R$   

$$N = \frac{\Delta Z \pi (\rho - x) \rho_R C_R}{\Delta t \dot{v} C_p} \quad (\text{Eq. HT2a})$$

154. If  $M \geq N$ , go to step 165.

155. Find  $S/2 = \frac{k_R \Delta t}{(\Delta Z)^2 \rho_R C_R}$  (Eq. HT3)

156. Find  $U = \frac{h \Delta t}{\rho_R C_R}, \theta_R$  (Eq. HT5)

157. Find metal temperature for the next time point.

$$\theta_{(m+1/2, n+1)} = \left[ \frac{1}{N} - \frac{2M-1}{N(2M+1)} \right] T_{(m, n)} + \left[ 1 - \frac{2}{N(2M+1)} \right] \theta_{(m+1/2, n)}$$

$$+ S \left[ \theta_{(m+3/2, n)} - 2\theta_{(m+1/2, n)} + \theta_{(m-1/2, n)} \right] + U, \theta_R \quad (\text{Eq. HT10})$$

158. If  $\theta_{(m+1/2, n+1)} \geq T_{max}$ , activate the "maximum temperature exceed" flag.

159. Set increment counter to compute the next node

$$Z = Z + \Delta Z$$

160. If all nodes for this part have not been computed, go to step 145.

161. Extrapolate metal temperatures at the ends of parts:

$$\theta_{(m-1/2)} = 2\theta_{(m+1/2)} - \theta_{(m+3/2)}$$

$$\theta_{(m \max + 3/2)} = 2\theta_{(m \max + 1/2)} - \theta_{(m \max + 5/2)}$$

162. Add the metal-temperature time-increment of this part to the current time. If it is less than the next fluid computation time, go to step 145.

163. Set the increment counter to compute the next part. If all the parts have not been computed, go to step 145.

164. Go to 166. (Exit AZJ)

165. Halve the time increment for this part. If  $\Delta t - \Delta t_{\min}$  print "DELTA T TOO SMALL" and stop. If not go to step 145.

166. If the outlet metal temperature of the last part is less than  $t_{\min}$  and this time point has already been printed, print "COOLDOWN REACHED," and go to step 4.

167.  $\text{Time}(i+1) = \text{Time}(i) + \Delta t$

168. If input tank pressure ( $P_1$ ) is not zero, go to step 175.

169. Interpolate the input curves of  $P_1$  and  $T_1$  for  $P_1$  and  $T_1$  at this time point.

170. Find the entropy at  $P_1$  and  $T_1$ .

171. Find the hydrogen properties of  $P_1$  and  $T_1$ . If an error occurs, print "BAD TANK PRS, TMP" and stop.

172. Find entropy at  $P_1$  and  $T_1 + \Delta T$ , where  $\Delta T$  is a temperature increment used in finding isentropic temperature changes across the pump.

173. Find vapor pressure at  $P_1$  and  $T_1$ . If the vapor pressure is greater than the total pressure, print "GAS AT PUMP INLET" and stop.

174. Find  $N_{\text{by}}(i+1) = \frac{P_1 - P_1 \text{ vapor}}{12 \rho_1} \cdot \frac{\text{ft, lbf}}{\text{lbm}}$  (Eq. PT34)

175. If input gate position is 0, interpolate input curves for G.P. at this time point.

176. If  $N_1 = 0$ , set  $N_{(i+1)} \text{ guess} = 5000$ . If not, set  $N_{(i+1)} \text{ guess} = N_1$ .

177. Begin iteration to find  $N_{(i+1)}$  by closing on  $W_p \text{ act}(i+1)$  computed by energy balance and work required.

178. Interpolate  $Q_p(i+1)$  not closed flag.

179.  $Q_p(i+1) \text{ guess} = Q_p(i)$ .

180. Begin iteration to find  $Q_p(i+1)$  by closing on  $\Delta H(i+1)$ .

181. Find  $\dot{V}_P(i+1) = Q_P(i+1) \rho_1$  (0.602228) (1728) lbm/sec (Eq. FT18)

182. Find  $P_2(i+1) = \alpha \dot{V}_P^2(i+1) + \beta \dot{V}_P(i+1)$ , psia (Eq. FT17)

183. Find  $T_2(i+1)$  from  $P_2, P_1$ , and  $T_1$  isentropically

where  $T_2(i+1) = T_1(i+1) + \frac{\Delta T (S'' - S)}{(S - S')}$ , °R

$S = S(P_1 \text{ and } T_1)$

$S' = S'(P_1 \text{ and } T_1 + \Delta T)$

$S'' = S(P_2 \text{ and } T_1)$

$\Delta T =$  small temperature increment, in. °R

184. Find parahydrogen properties at  $P_2$  and  $T_2$ . If an error occurs, go to step 191.

185. Find  $\Delta H_{(i+1)} = 776 \left[ h(P_2, T_2) - h(P_1, T_1) \right] \cdot \frac{\text{ft, lbf}}{\text{lbm}}$  (Eq. FT16)

If  $\Delta H_{(i+1)} \leq 0$ , go to step 192.

186. Find  $\Delta H/N^2 = f(Q/N \text{ and } N \text{FSP}/N^2)$  from the turbopump curves.

187. Find  $\Delta H_{(i+1)} = \left[ \frac{\Delta H}{N^2} \right]_{(i+1)} \cdot N_{(i+1)}^2 \cdot \frac{\text{ft, lbf}}{\text{lbm}}$  (Eq. FT20)

188. If  $\Delta H_{(i+1)}$  and  $\Delta H'_{(i+1)}$  are within the input closure tolerance, go to step 193.

189. Compute a new  $Q_p(i+1)$  guess, and adjust, if necessary, so that it is between the given maximum and minimum values.

190. If the maximum number of iterations has been exceeded, activate the  $Q_p(i+1)$  not closed flag and go to step 193. If not, go to step 181.

191. If  $T_2(i+1)$  is too low, go to step 192. If  $P_2(i+1)$  is too large, use the current value of  $Q_p(i+1)$  as an upper limit on  $Q_p(i+1)$  and go to step 189.

Basic Subroutine AYB

AYD

192. Use the current value of  $Q_p(i+1)$  as a lower limit on  $Q_p(i+1)$  and go to step 189.

193. If a start assistance is being used, find

$$\dot{v}_T(i+1) = \frac{P_{11}(i+1) K_t}{\sqrt{T_{11}(i+1)}} \text{ lb/sec, and go to step 216}$$

If  $T_{11}(i+1) < 0$ , stop.

194. Deactivate  $\dot{v}_H$  not closed flag.

195. Find  $P_6(i+1) = \beta \dot{v}_P(i+1)$ , psia (Eq. PT21)

196. Set  $\dot{v}_h(i+1)$  guess =  $\dot{v}_h(i)$

197. Begin iteration to find  $\dot{v}_h(i+1)$  by closing on  $P_8(i+1)$

198. Find  $P_{HM} = \left[ \frac{\dot{v}_h(i+1)}{K_{16}} \right]^2 - P_6(i+1)$ , psia (Eq. PT35)

If  $P_{HM} < 0$ , go to step 212.

199. Find  $\dot{v}_c = K_{10} \sqrt{P_2(i+1) - P_{HM}(i+1)}$ , lb/sec (Eq. PT36)

If  $P_2(i+1) < P_{HM}(i+1)$ , stop.

200. Find  $\dot{v}_T(i+1) = \dot{v}_h(i+1) + \dot{v}_c(i+1)$ , lb/sec (Eq. PT27a)

201. Find  $V_8(i+1) = K_{12} \dot{v}_T(i+1)$ , in./sec (Eq. PT37)

202. Find  $V_{HM}(i+1) = K_{13} \dot{v}_h(i+1)$ , in./sec (Eq. PT38)

203. Find  $V_{CM}(i+1) = K_{14} \dot{v}_c(i+1)$ , in./sec (Eq. PT39)

204. Find  $P_{CM}(i+1) = \left[ \frac{\dot{v}_c(i+1)}{K_{15}} \right]^2 - P_2(i+1)$ , psia (Eq. PT40)

$P_{CM}(i+1) < 0$ , go to step 212.

205. Find  $T_8(i+1) = K_6 \left( \frac{T_2 \dot{v}_c + T_6 \dot{v}_h}{2 \dot{v}_T} \right) (i+1)$ ,  $^{\circ}R$  (Eq. PT28)

and  $T_8(i+1)$  static =  $\left( \frac{T_8(i+1)}{Z-1} M^2 + 1 \right)^{\frac{\gamma-1}{\gamma}}$ ,  $^{\circ}R$  (Eq. PT41)

206. Find  $P_8(i+1)$  static

$$= \frac{A_H P_{HM} + (P_{CM} - P_{HM}) A_{cH} \cos \theta + \frac{1}{2} (V_{CM} \cos \theta - V_8) (V_{HM} - V_8) \dot{v}_h}{f V_8 P_{DH} L} \left[ \frac{2}{Z-1} M^2 + 1 \right]^{\frac{\gamma-1}{\gamma}}$$

psia (Eq. PT42)

207. Find  $P_8(i+1) = P_8(i+1)$  static  $\left[ \frac{Z-1}{2} M^2 + 1 \right]^{\frac{\gamma-1}{\gamma}}$ , psia (Eq. PT43)

208. Find  $P_8'(i+1) = \dot{v}_T(i+1) \sqrt{T_8(i+1) K_5}$ , psia (Eq. PT29)

209. If  $P_8(i+1)$  agrees with  $P_8'(i+1)$  within the input tolerance, go to step 213.

210. Compute a new  $\dot{v}_h(i+1)$  guess and adjust, if necessary, so that it lies between the given maximum and minimum values.

211. If the maximum number of iterations has been exceeded, activate the  $\dot{v}_h(i+1)$  not closed flag and go to step 213; if not, go to step 198.

212. Use the current  $\dot{v}_h(i+1)$  value as an upper limit on  $\dot{v}_h(i+1)$  and go to step 210.

213. Find  $\sqrt{T_{11}(i+1)}$ ; if  $T_{11}(i+1) < 0$ , stop.

214. Find  $P_{11}(i+1) = \frac{\dot{v}_c(i+1)}{K_t} \sqrt{T_{11}(i+1)}$ , psia

215. Deactivate the  $P_{12}(i+1)$  not closed flag.

216. Find  $T_T = -(0.5318076 \times 10^{-6}) \left[ \frac{N_{i+1}}{\sqrt{T_{11}(i+1)}} \right] + (0.11039226 \times 10^{-2})$

217. Set upper limit of  $P_{12}(i+1)$  equal to  $P_{11}(i+1)$

218. Find  $C_{P11}$  at  $P_{11}(i+1)$  and  $T_{11}(i+1)$ . If error occurs, stop.

219. Begin iteration to find  $P_{12}(i+1)$  closing on  $P_{12}/P_{11}(i+1)$

220. Find  $T_{12}(i+1) = T_{11}(i+1) \frac{P_{12}(i+1)}{P_{11}(i+1)}$ , OR (Eq. PT44)

221.  $T_T = T_T \left[ 1 + \frac{7R T_{12}(i+1)}{(7+1) C_{P11}(i+1) T_{11}(i+1)} - T_{12}(i+1) \right]$ , unitless (Eq. PT45)

222. Find  $P_{12}/P_{11} = \frac{K_t}{2 A_{rn}(0.1396)} \left[ 1 - \eta_T \left( 1 - \frac{P_{12}(i+1)}{P_{11}(i+1)} \right) \right]$ , unitless (Eq. PT9)

223. If  $(P_{12}/P_{11})(i+1)$  and  $P_{12}(i+1)/P_{11}(i+1)$  agree within the input tolerance, go to step 226.

224. Compute a new  $P_{12}(i+1)$  guess and adjust, if necessary so that it lies between the given maximum and minimum values.

225. If the maximum number of iterations have been exceeded, activate the  $P_{12}(i+1)$  not closed flag and go to step 228. If not, go to step 220.

226. Find  $W_T \text{ act}(i+1) = \frac{R}{778 C_{P11}} \frac{P_{12}}{P_{11}}$  Btu/sec (Eq. PT10)

Basic Subroutine AYB

AYK  
AYL  
AYM  
KRA  
AZF

227. Find  $\eta_p$  from program curves as a function of  $Q_p/N(i+1)$  and  $NFSP/N^2(i+1)$ . If  $\eta_p = 0$ , set  $W_p \text{ act}(i+1) = 0$ , and go to step 229.

228. Find  $W_p \text{ act}(i+1) = \frac{W_p \text{ act}(i+1) \Delta h(i+1)}{\eta_p}$ , Btu/sec (Eq. PT21)

229. Find  $W_p \text{ act}(i+1) = W_p \text{ act}(i) - \frac{I_{PT}}{(776) L_2 g \Delta t} \frac{2\pi^2}{60} N^2(i+1) - N^2(i) + W_T \text{ act}(i+1) + W_T \text{ act}(i)$ , Btu/sec (Eq. PT11)

230. If  $W_p \text{ act}(i+1)$  and  $W_p \text{ act}(i+1)$  are within the input tolerance, to go to step 234.

231. Compute a new  $N(i+1)$  guess, and adjust it if necessary so that it lies between the given maximum and minimum values.

232. If the maximum number of iterations have been exceeded, go to step 233; if not, go to step 178.

233. Print "PREDICTOR FAILED," and go to step 235.

234. If  $Q_p(i+1)$  is not closed, and/or  $W_h(i+1)$  is not closed, and/or  $P_{12}(i+1)$  is not closed, flags are activated. Go to step 233.

235. Go to step 51.

236. Print, "TOO MANY PARTS."

237. Read next input card. If a tape error has occurred print, "HELP HELP HEKILLIP" and stop.

238. If the last card read was the final "T" card, go to step 4; if not go to step 237.

IV. GLOSSARY OF TERMS

A. SYMBOLS

Symbol	Unit	Definition
T	$^{\circ}\text{R}$	Temperature - Fluid
P	$\text{lb}/\text{in.}^2$	Pressure
$\rho$	$\text{lb}/\text{in.}^3$	Density
$h_f$	$\text{Btu}/\text{sec}-^{\circ}\text{R}-\text{in.}^2$	Convective Heat Transfer Film Coefficient
$\theta$	$^{\circ}\text{R}$	Temperature - Metal
f	Unitless	Void Fraction
$F_p$	in.	Wetted Perimeter
$A_f$	$\text{in.}^2$	Flow Area
$\Delta Z$	in.	Distance node
M	Unitless	Equation Coefficient
N	Unitless, RPM	Defined in Equation 26 Turbine Speed
$\Delta t$	sec	Time increment
k	$\text{Btu}/\text{in.}-\text{sec}-^{\circ}\text{R}$	Thermal Conductivity
q	$\text{Btu}/\text{sec}$	Heat Flow
H	$\text{Btu}/\text{sec}-\text{in.}^3$	Internal Heat Generation
$\mathcal{U}$	$^{\circ}\text{R}$	Temperature Rise Due to Internal Heat Generation
S	--	Axial Conduction Coefficient
$C_p-C_R$	$\text{Btu}/\text{in.}-^{\circ}\text{R}$	Specific Heat Fluid, Metal
E	$\text{in.}-\text{lb}/\text{lb}-\text{sec}^2$	Gravitational Constant
$\dot{v}$	$\text{lb}/\text{m}/\text{sec}$	Flow Rate
W	$\text{Btu}/\text{sec}$	Work
$\phi$	in.	Hydraulic Diameter

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<u>Symbol</u>	<u>Unit</u>	<u>Definition</u>
I	in. <sup>2</sup> -lbm	Moment of Inertia
Q <sub>p</sub>	gal/min	Flow Rate
Q <sub>i</sub>	Btu/sec	Internal Heat Generated
H	ft lbf/lbm	Pump Head Rise
h	Btu/lb	Enthalpy
S	Btu/lb-°R	Entropy
φ	Unitless	Friction Factor
η <sub>T</sub>	Unitless	Turbine Efficiency
η <sub>P</sub>	Unitless	Pump Efficiency
γ	Unitless	Ratio of Specific Heats
ω	rad/sec	Rotational Speed

<u>Subscripts</u>	<u>Description</u>
HM	Hot Mixture
CM	Cold Mixture
c	Cold
h	Hot
N	Nozzle
T	Turbine

B. SUBSCRIPTS

<u>Subscripts</u>	<u>Description</u>
1	Pump Inlet
2	Pump Outlet
3	Nozzle Tube Inlet
4	Nozzle Tube Outlet
6	Nozzle Chamber - Core Outlet
8	Hot Bleed Port Outlet
11	Turbine Inlet
12	Turbine Outlet
m	Distance Node
n, i	Time
T act	Actual Turbine
P act	Actual Pump
isen	Isentropic

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SECTION V  
FIGURES

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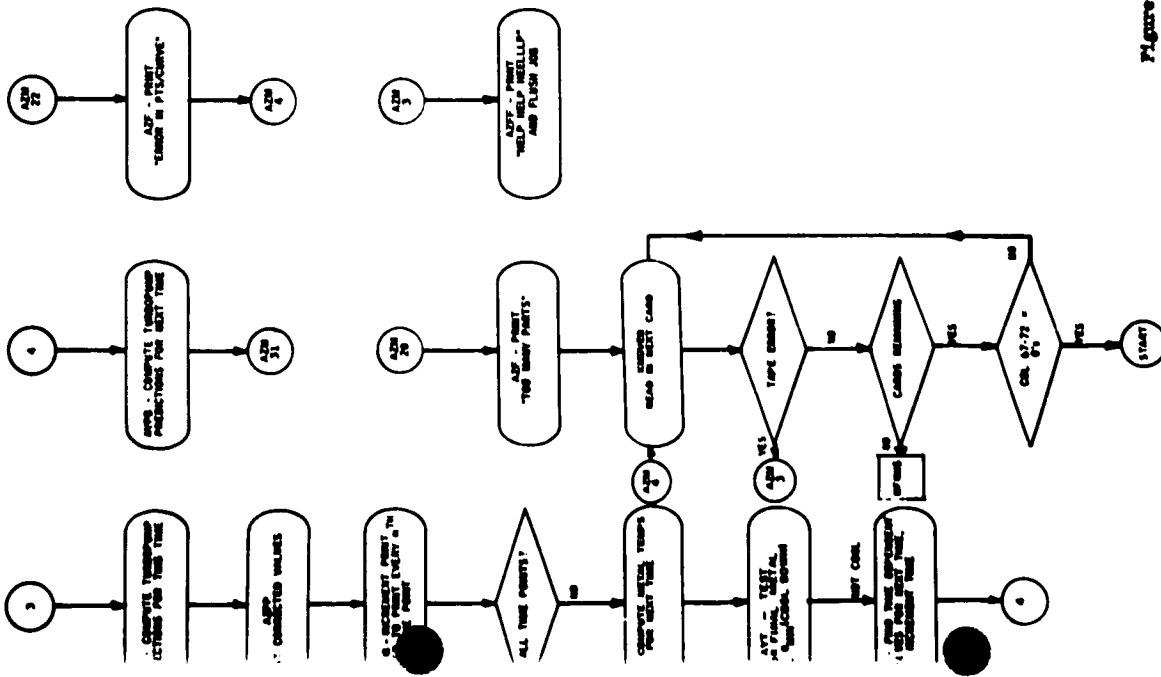


Figure 1  
AZH

12013 Master Control Region and Input Initialization

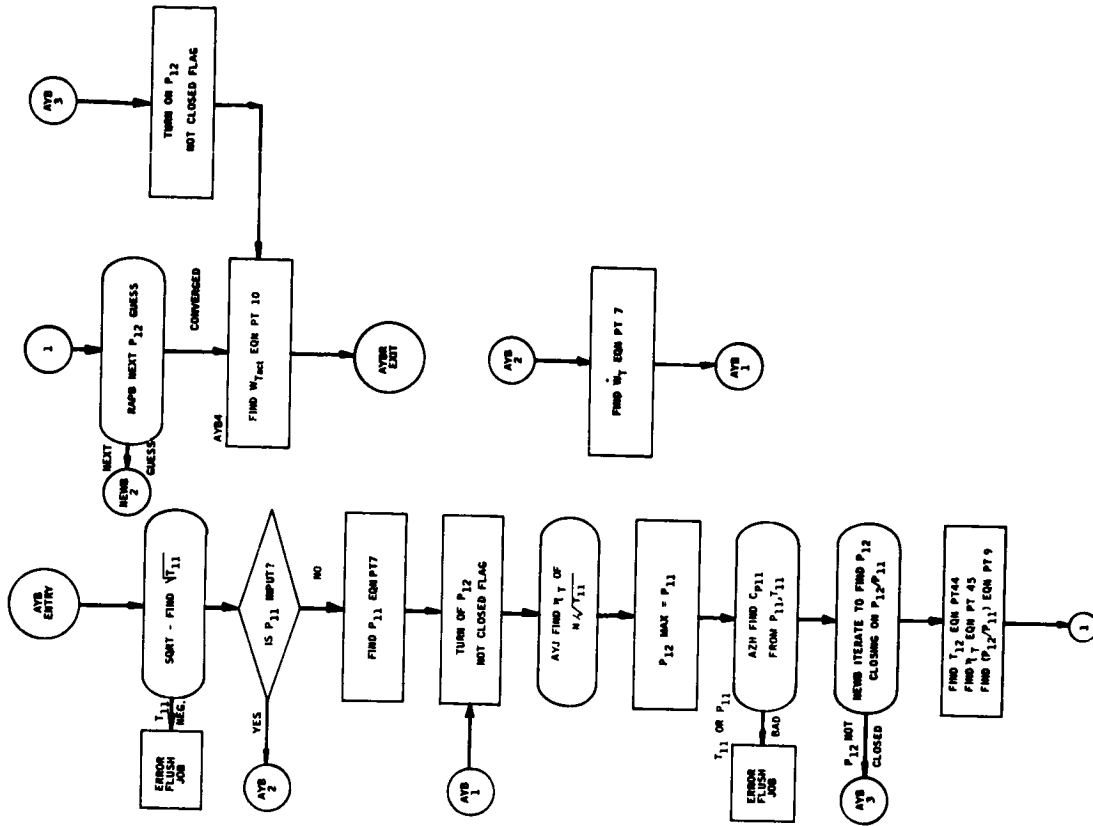


Figure 3  
AYB  
Find Actual Turbine Work  
Page 51

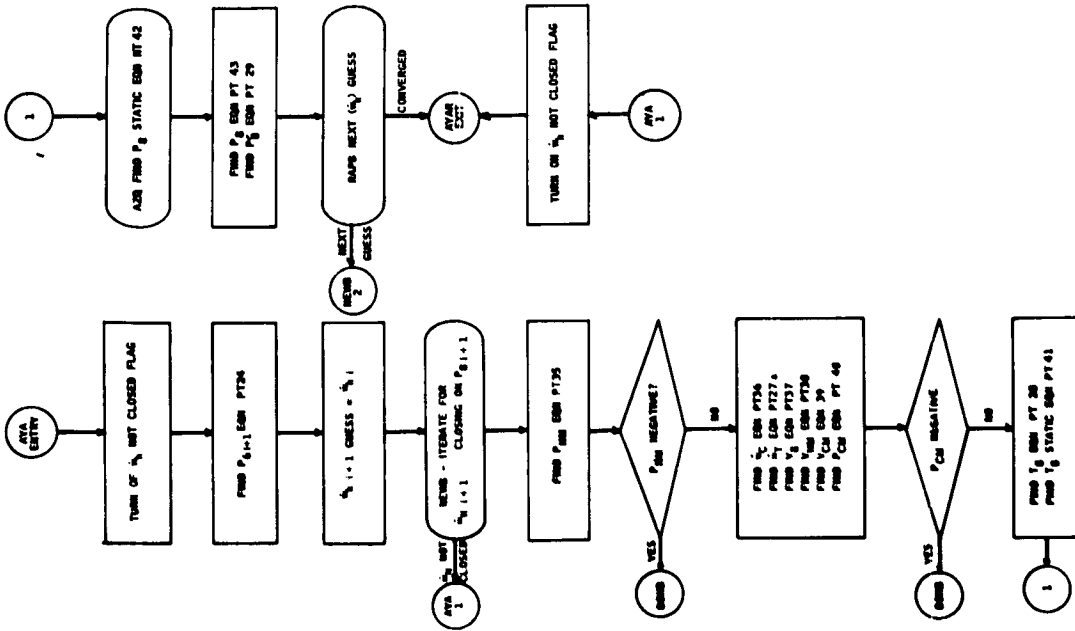


Figure 2  
 AYA  
 Iterate to Find  $\eta_b$  Closing on P 8  
 Page 50

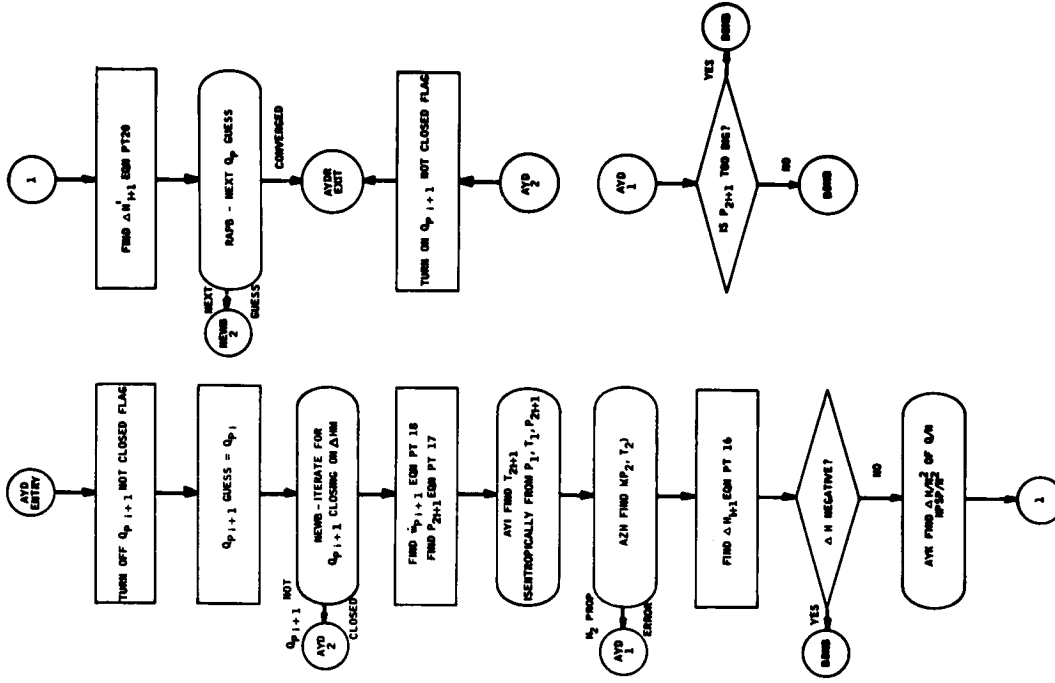
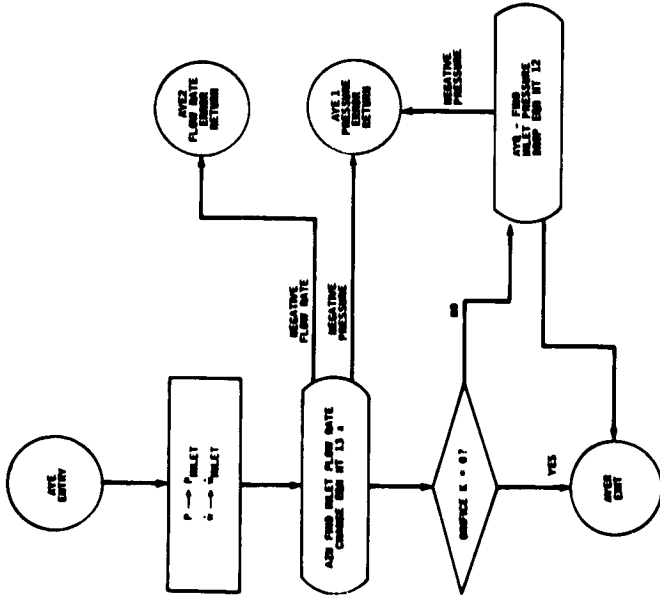


Figure 4  
 AYA  
 Find Pump Flow Rate  
 Page 52



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Figure 5  
AYE  
Find Inlet Pressure and Flow Rate Changes for One Part  
Page 53

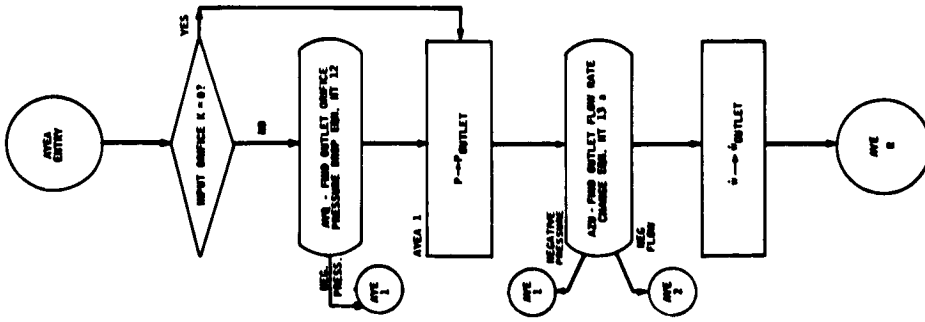


Figure 6  
 AREA  
 Find Outlet Pressure and Flow Rate for One Part  
 Page 54

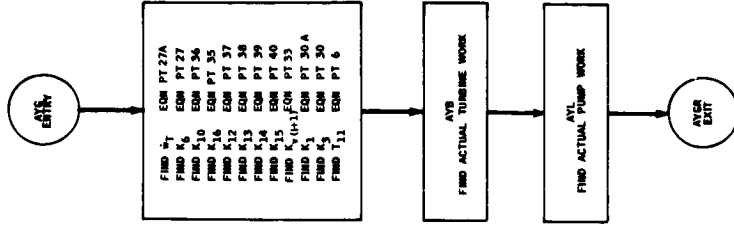


Figure 7  
 AVG  
 Region to Compute Part of Corrector Equations  
 Page 55

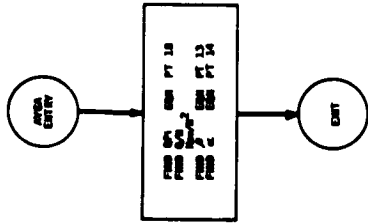


Figure 8  
AYIIA  
Compute Some Corrector Equations  
Page 56

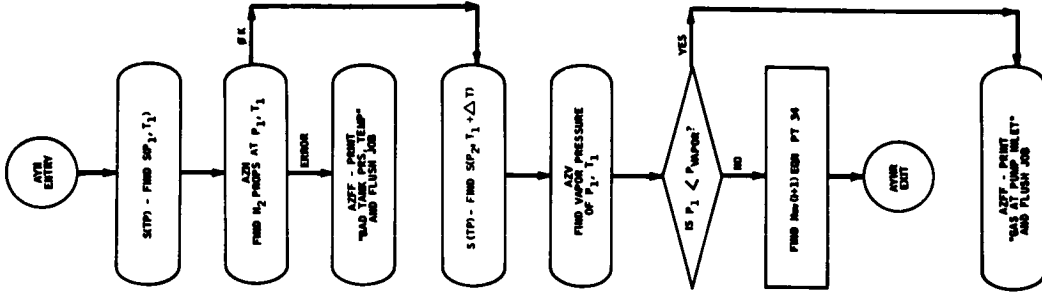


Figure 9  
AYIII  
Look-Up Isentropic Values  
Page 57

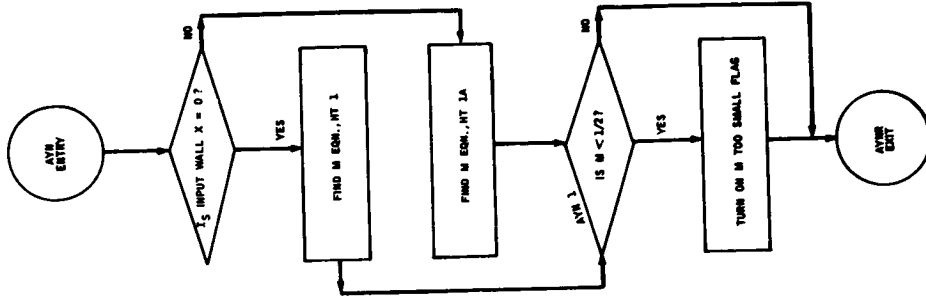


Figure 11  
AVL  
Compute Heat Resistance Term, M, for One Mode  
Page 59

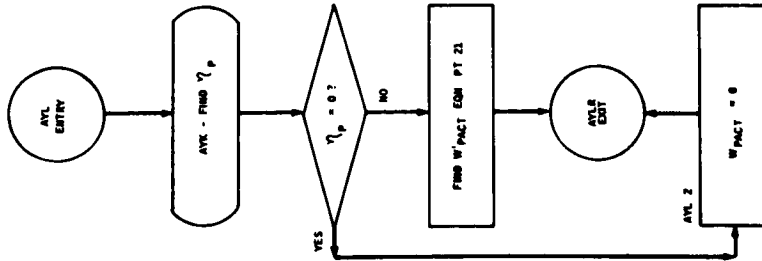


Figure 10  
AVL  
Compute Work Required by the Pump  
Page 58

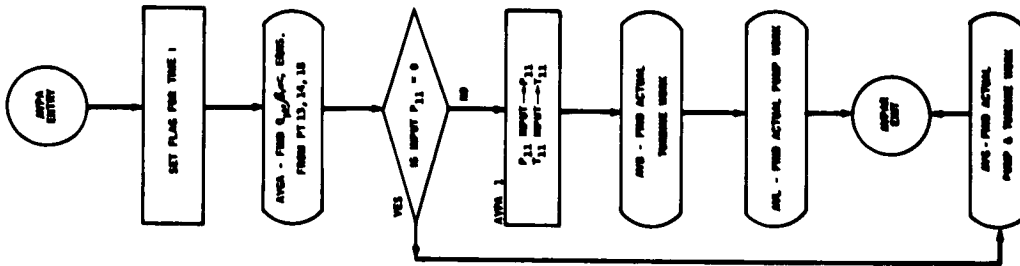


Figure 12  
AVM  
Pump and Turbine Master Control (Corrector)  
Page 60

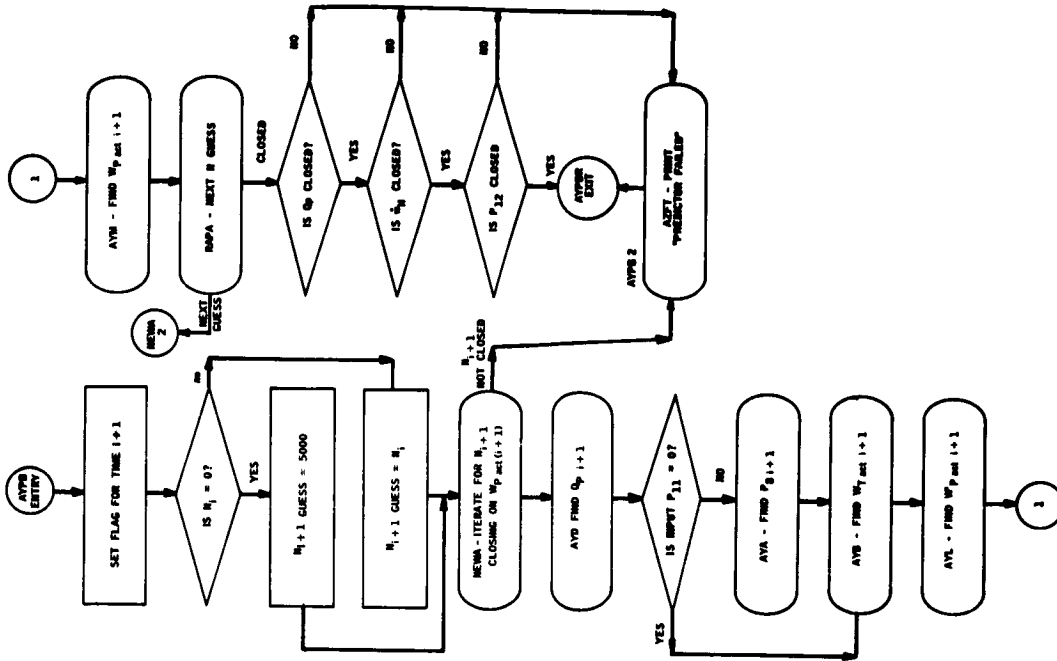


Figure 13  
ATFB  
Turbopump Master Control Time, 1+1 (Prediction)  
Page 61



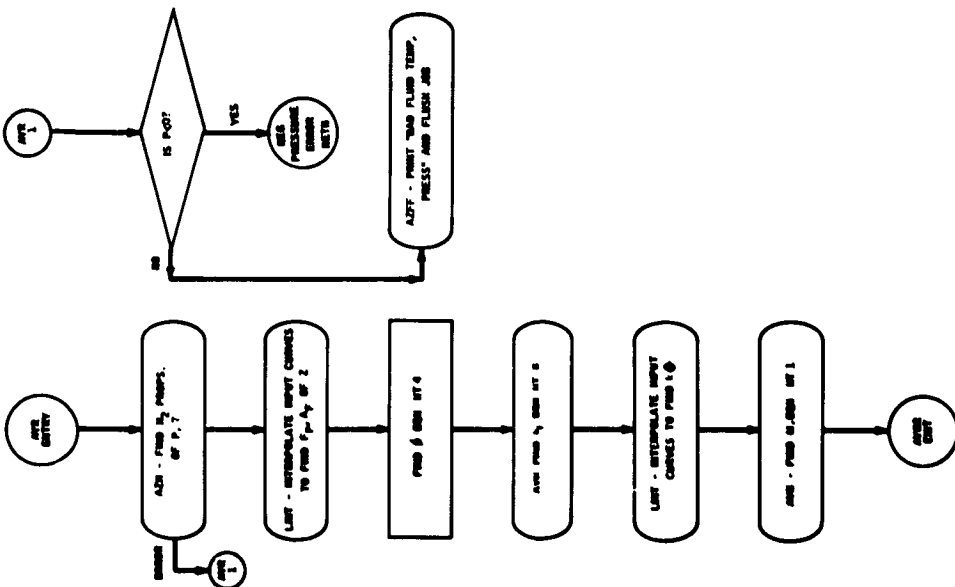


Figure 14  
A2Z  
Find Values For One Mode  
Page 62

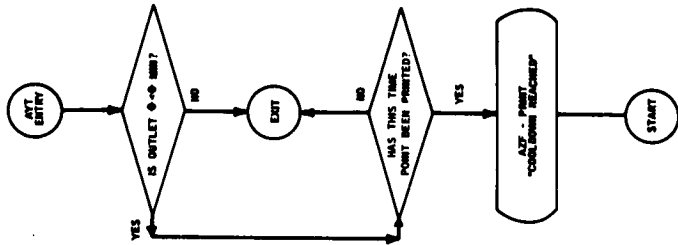


Figure 15  
A2Z  
Check for Cool-Down Reached  
Page 63

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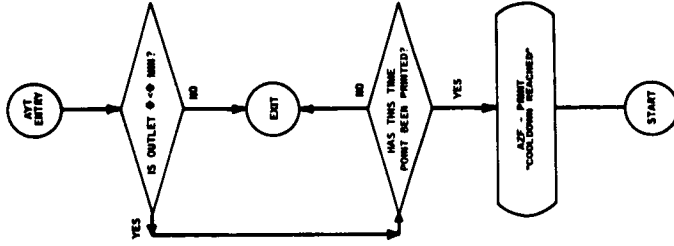


Figure 15  
 AYT  
 Check for Cool-Down Reached  
 Page 63

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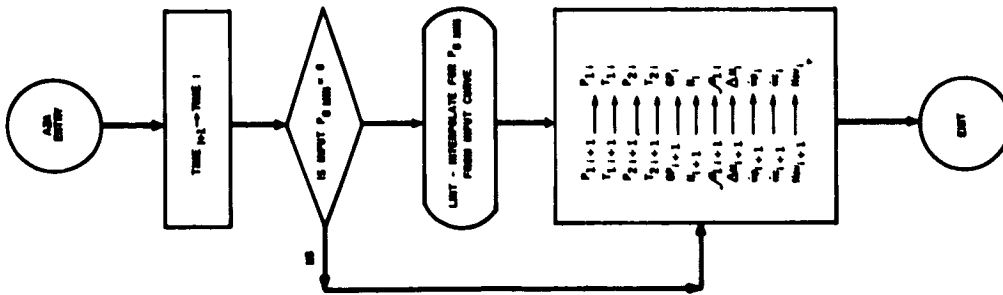


Figure 16  
 AZA  
 Set Values for One Time Step  
 Page 64

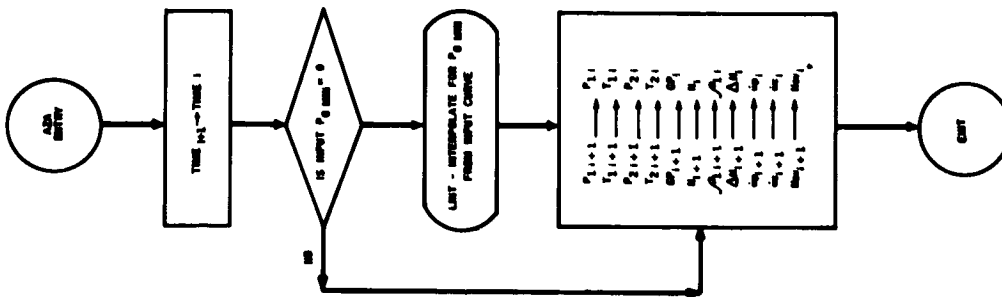


Figure 16  
AZA  
Set Values for One Time Step

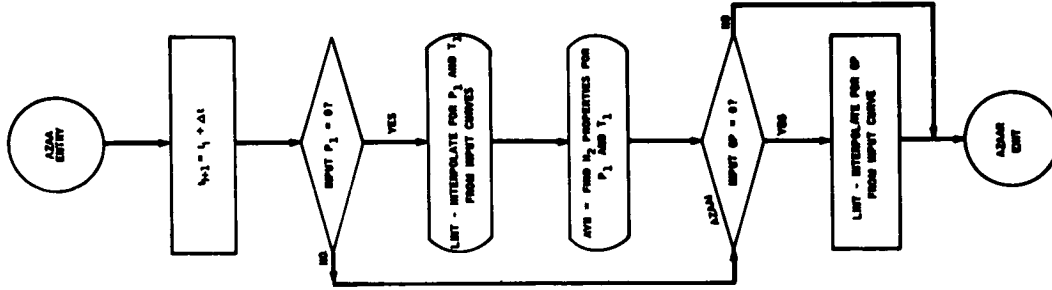


Figure 17  
AZAA  
Obtain Values for Next Time Point

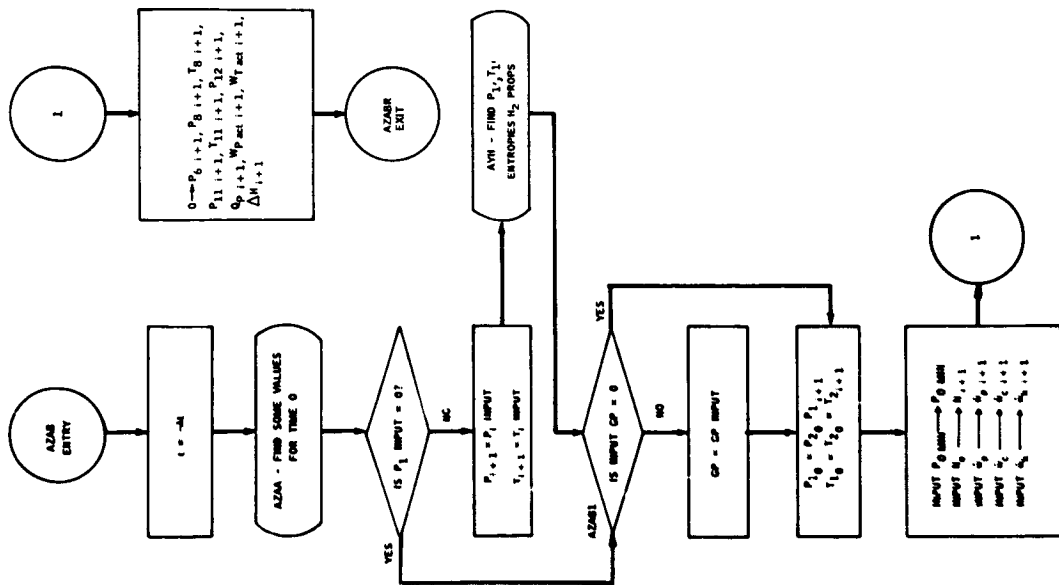


Figure 18  
AZAB  
Find Values at Zero Time  
Page 66

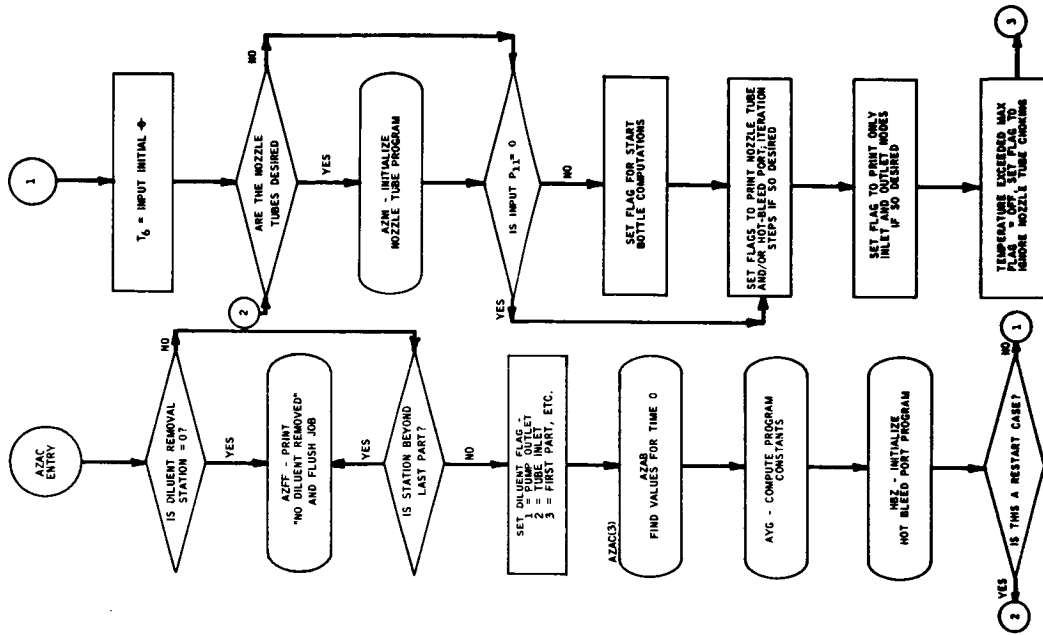


Figure 19  
AZAC  
Initialize Program  
Page 67

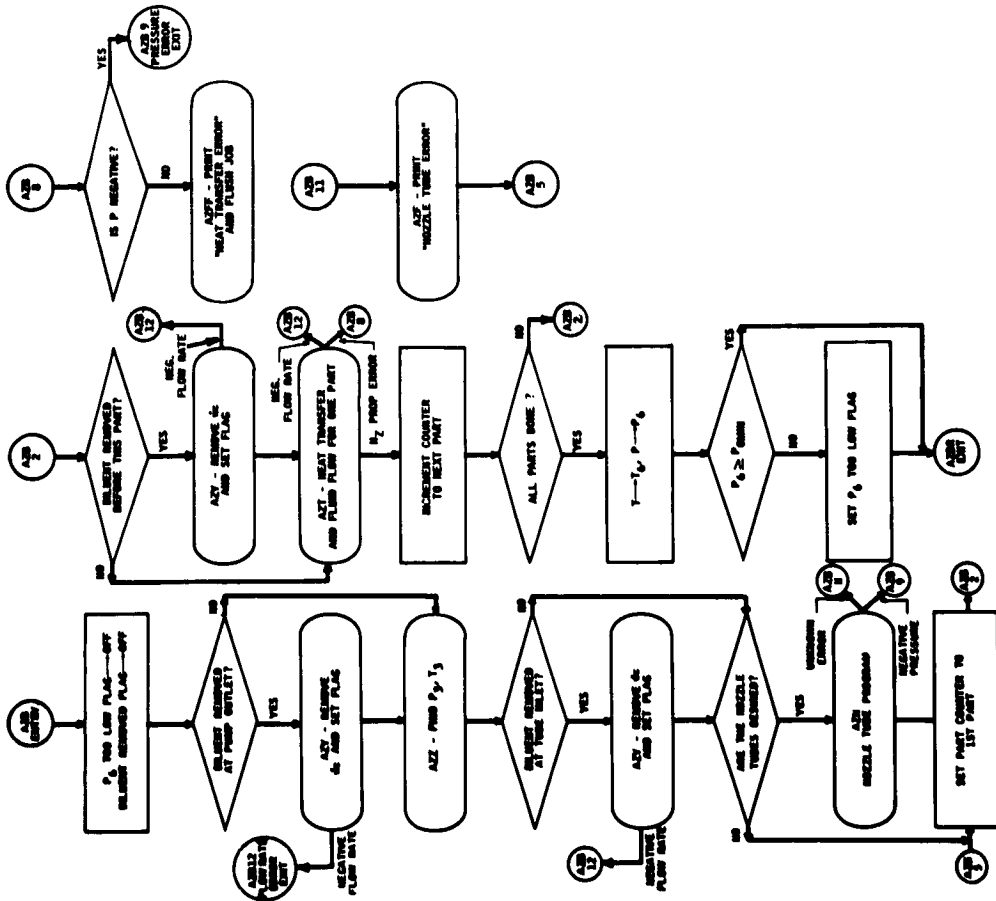


Figure 20  
AZZ  
Main Engine Heat Transfer and Fluid Flow  
Page 66

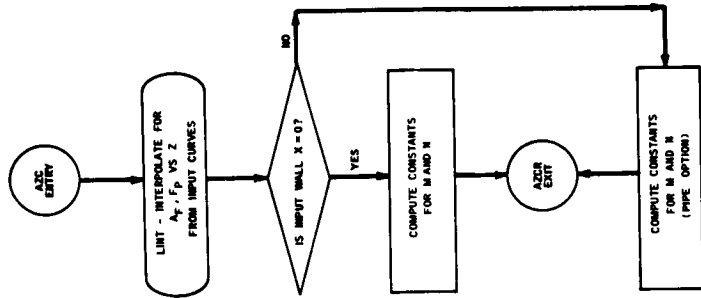


Figure 21  
AZZ  
Compute Some Values for One-Node Metal Temp  
Page 69

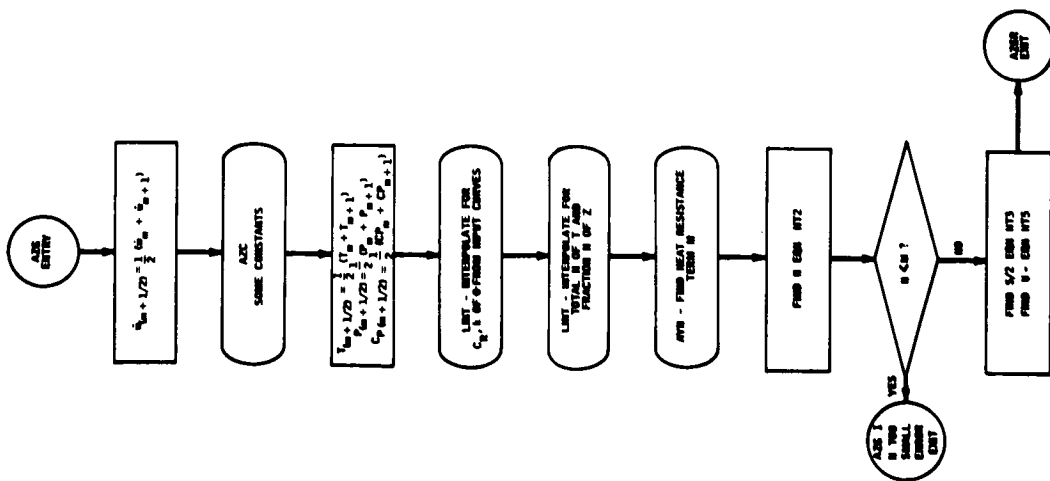


Figure 22  
AZG

Compute Base Values for One-Node Metal Temp

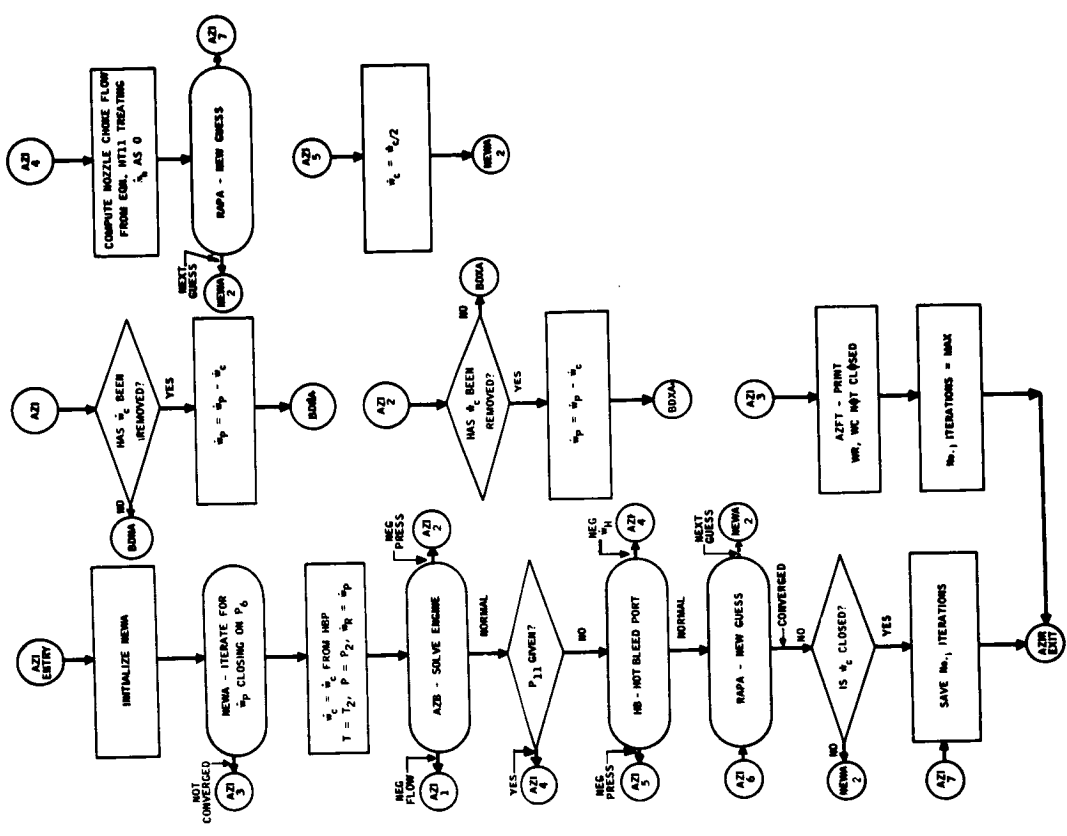


Figure 23  
AZI

Heat-Transfer Iteration Master Control

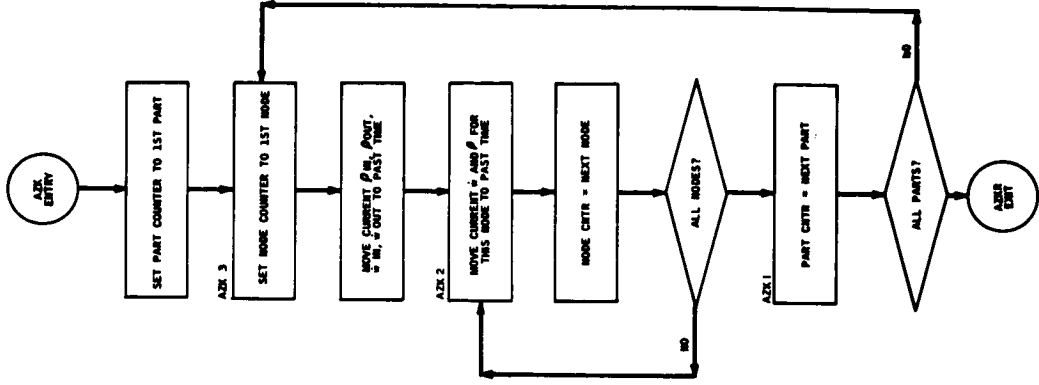


Figure 25  
AZK  
Move Current Values to Past Time Values for Each Part

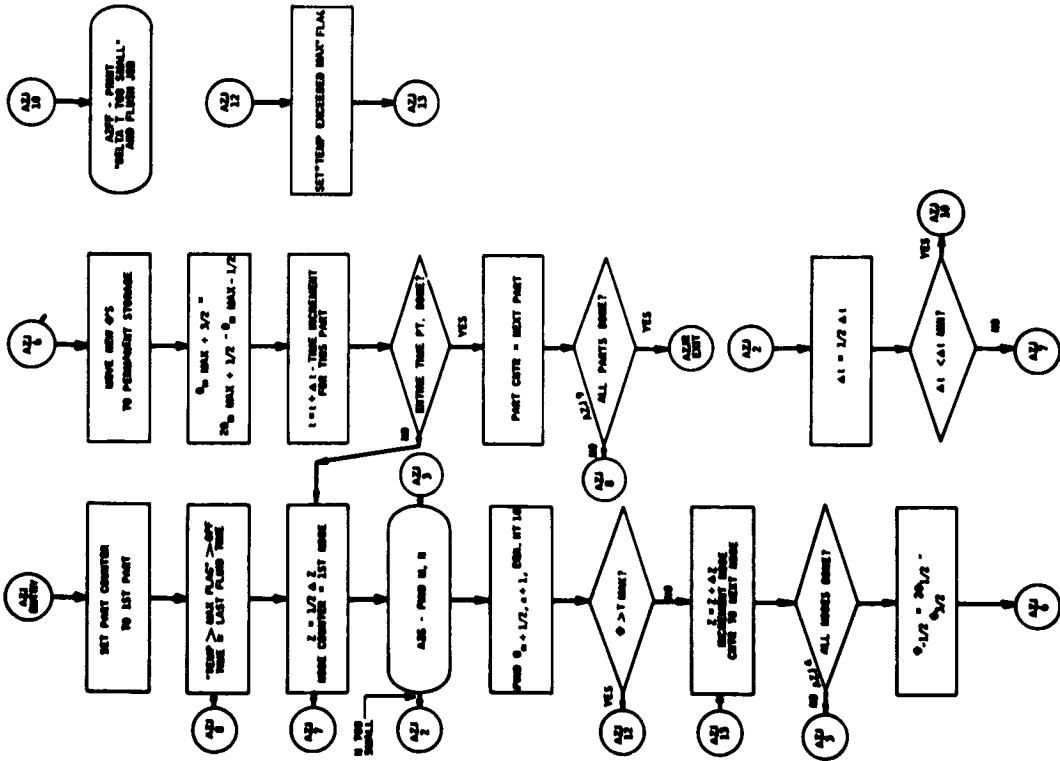


Figure 24  
AZJ  
Compute Metal Temps for One Time Point

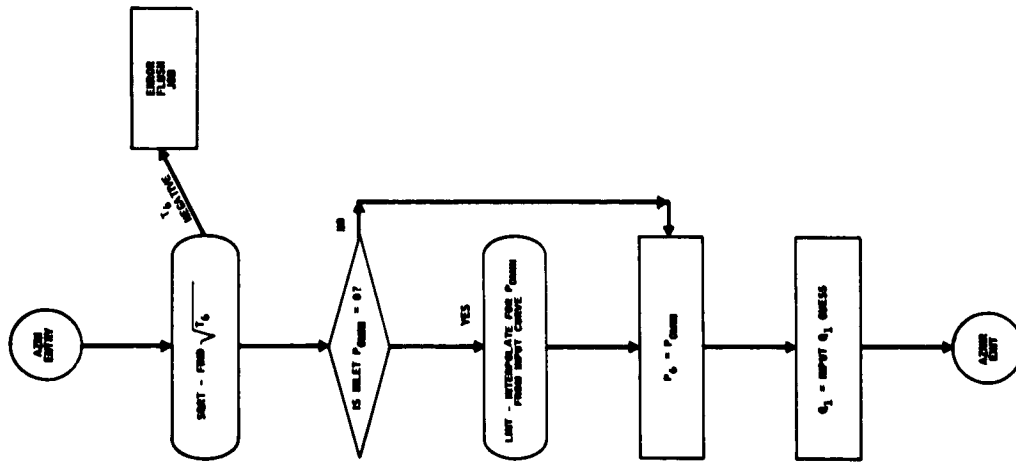


Figure 26  
AZMI  
Initialize Nozzle Tube Program  
Page 76

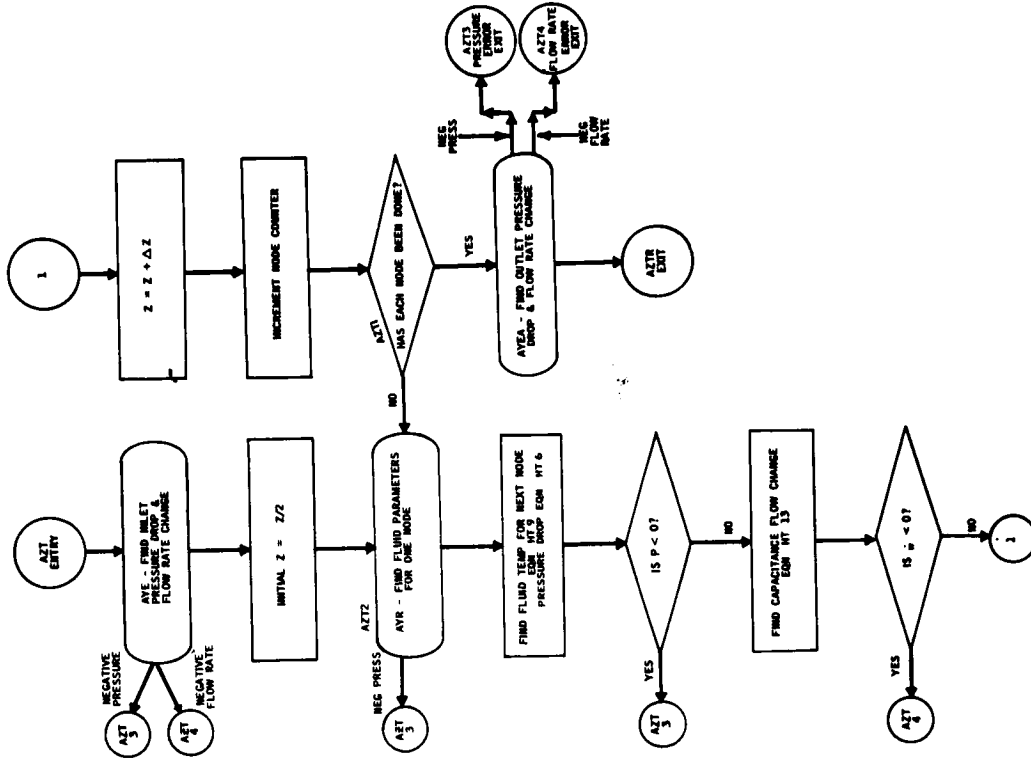


Figure 27  
AZT  
Fluid Node Corrections  
Page 75



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APPENDIX A  
NEVA ENGINE TRANSIENT PROGRAM

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A. INPUT

1. General Input

VALUES ARE ENTERED ON DATA CARDS ANYWHERE BETWEEN COLUMNS 1 AND 72 INCLUSIVE. EACH VALUE MUST BE PRECEDED BY A SIGN (+ OR -). THE FOLLOWING ARE THE ONLY ALLOWABLE SYMBOLS ON DATA CARDS.

0-9 THE INTEGERS. NOTE THAT THE ZERO IS PUNCHED WITH THE (0-7) KEY

. THE DECIMAL POINT IS PERMITTED BUT NOT NECESSARY. FOR EXAMPLE  
+10+10.+10.0

+ OR - EACH VALUE MUST BE PRECEDED BY A SIGN. NOTE THAT THE MINUS SIGN IS PUNCHED WITH THE (-SKIP,-) KEY.

E THIS IS USED TO INDICATE A POWER OF TEN. FOR EXAMPLE, +1000+1E3  
+10000E-1=1E4

L THIS INDICATES A RELATIVE LOCATION. IF NO L IS SUPPLIED, THE RELATIVE LOCATION IS ASSUMED TO BE ZERO. ALL SUCCESSIVE VALUES AFTER AN L ARE ASSUMED TO BE IN SEQUENCE. THE LOCATION INCREASING BY 1. IF TWO OR MORE VALUES ARE SUPPLIED WITH THE SAME RELATIVE LOCATION, THE LAST ONE ENCOUNTERED IS THE ONE USED. FOR EXAMPLE IF THE SIXTH AND SEVENTH INPUT VALUES (RELATIVE LOCATIONS = 6 AND 6) WERE 21 AND 13.5. THESE VALUES WOULD BE ENTERED AS L6+21+13.5

BLANKS ARE COMPLETELY IGNORED EXCEPT BETWEEN THE DIGITS OF A SINGLE NUMBER.

EXCEPT FOR SPECIFIED COLUMNS, THERE ARE NO ILLEGAL SYMBOLS ON T CARDS.

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3. Description

S = THIS VALUE IS SUPPLIED BY THE STANDARD CASE  
 0 = THIS VALUE AFFECTS THE LOGICAL SEQUENCE OF THE PROGRAM

a. Input

SYMBOL UNITS DESCRIPTION

SYMBOL	UNITS	DESCRIPTION
DELTA Z	IN	SO DISTANCE INCREMENT.
M MAX	NONE	SMO. DELTA Z STEPS. IF THIS VALUE IS 0 THIS PART WILL BE IGNORED.
PHI	NONE	SFRICTION FACTOR.
F	NONE	SVOID FRACTIO .
RHO R	LB/IN3	SMETAL DENSITY.
X	IN	S SMALL THICKNESS. IF THIS VALUE IS NOT 0 THE PIPE OPTION WILL BE USED.
KPRESS IN	1/IN4	SPRESSURE DROP K FOR INLET ORIFICE.
KPRESS OUT	1/IN4	SPRESSURE DROP K FOR OUTLET ORIFICE.
V INLET	IN3	SINLET PLENUM VOLUME.
V OUTLET	IN3	SOUTLET PLENUM VOLUME.

b. Input for Entire System

PRINT INTL NONE

SUPRINT INTERVAL. THIS VALUE IS OF THE FORM 1000AB. IF A IS 0 EACH MODE WILL BE PRINTED. IF A IS NOT 0 ONLY THE FIRST AND LAST MODES FOR EACH PART WILL BE PRINTED. A PRINTOUT WILL BE MADE EVERY B TIMES DELTA T SECONDS.

TIME 0 SEC

S INITIAL TIME. IF THIS VALUE IS NOT 0 THIS CASE WILL BE TREATED AS A RESTART CASE AND ADDITIONAL INPUT WILL BE REQUIRED.

DELTA T SEC

STIME INCREMENT.

NO. DEL T NONE

NUMBER OF TIME POINTS DESIRED.

MIN. T MIN SEC

SMINIMUM ALLOWABLE TIME INCREMENT.

2. Cases

a. Input Case

INLET CASE CONSISTS OF DATA FOR EACH PART FOLLOWED BY THE NOZZLE (SEE INPUT (IF ANY), AND A FINAL T CARD. THE DATA FOR EACH PART CONSISTS OF THE DATA CARDS FOR THAT PART FOLLOWED BY A PART CARD. THE PART CARD CONSISTS OF (1) T IN COL 1, (2) PART NAME IN COL 2-7, (3) ANY IDENTIFYING INFORMATION IN COL 8-72. THE FINAL INPUT WITH TWO EXCEPTIONS. (1) WHEN USING THE STANDARD CASE THE NUMBER OF PARTS MUST BE THE SAME AS IN THE STANDARD CASE. NOTE - SOME PARTS MAY BE IGNORED BY SETTING THE NUMBER OF MODES TO ZERO. (2) THE REQUIRED AMOUNT OF STORAGE MUST NOT EXCEED THE CAPACITY OF THE MACHINE. THE PROGRAM PRINTS A MESSAGE AND STOPS WHEN THIS OCCURS.

b. Standard Case

THE STANDARD CASE IS A FOUR PART CASE. INFORMATION IN THE INPUT CASE OVERRIDES THE STANDARD CASE BUT THE STANDARD CASE VALUES ARE RESET AT THE BEGINNING OF EACH NEW CASE. THOSE VALUES NOT IN THE STANDARD CASE ARE NOT RESET. IF THE STANDARD CASE IS NOT DESIRED, A CARD WHICH IS BLANK EXCEPT FOR AN M IN COL 1 AND Y IN THE FIRST CARD OF THE INPUT CASE. THE PROGRAM PRINTS A MESSAGE AND STOPS WHEN THE STANDARD CASE IS USED WITH OTHER THAN A FOUR PART CASE.

125	THETA 0	DEGR	INITIAL METAL TEMP. IF THIS VALUE IS NEGATIVE, THE PROGRAM WILL EXPECT METAL TEMPS TO BE INPUT FOR EACH MODE. METAL TEMPS ARE INPUT AS SPECIFIED FOR THE RESTART CASE.	ITER FLAG	NONE	135	THIS VALUE IS OF THE FORM 1000A+B. IF A IS NOT ZERO, EACH NOZZLE TUBE ITERATION STEP WILL BE PRINTED. IF B IS NOT ZERO, EACH HOT BLEED PORT ITERATION STEP WILL BE PRINTED.
	I MIN	DEGR	MINIMUM ALLOWABLE FLUID OVRLET TEMP.	GATE POS	PERCENT		TURBINE LINE VALVE GATE POSITION. IF THIS VALUE IS ZERO, THE PROGRAM WILL USE THE GATE POSITION CURVE.
	T MAX	DEGR	MAXIMUM ALLOWABLE TEMPERATURE.	A(KV)	NONE		CONSTANT FOR K SUB V.
	B/L STA	NONE	POSITION OF INLET TO DILUENT LINE. 1=AT PUMP DISCHARGE, 2=AT NOZZLE TUBE INLET, 3=AT FIRST PART INLET, ETC.	B(KV)	NONE		CONSTANT FOR K SUB V.
	P1	PSIA	STANK PRESSURE. IF THIS VALUE IS ZERO, THE PROGRAM WILL USE THE INLET PRESSURE AND TEMPERATURE CURVES.	GAINA	NONE		RATIO OF SPECIFIC HEATS.
130	T1	DEGR	STANK TEMP.	K2	NONE	140	K FOR NOZZLE TUBE INLET LINE PRESSURE DROP.
	P OUT MIN	PSIA	MINIMUM ALLOWABLE OUTLET PRESSURE. IF THIS VALUE IS 0 THE PROGRAM WILL USE THE P OUT MIN CURVE WHICH IN THIS CASE, MUST BE INPUT	G2	IN		DIAMETER OF NOZZLE TUBE INLET LINE.
	EPS P0	NONE	SHOT BLEED PORT OUTLET PRESSURE CLOSURE TOLERANCE.	DM	IN		DIAMETER OF HOT BLEED PORT.
	EPS P12	NONE	TURBINE OUTLET PRESSURE CLOSURE TOLERANCE.	DYL	IN		DIAMETER OF TURBINE LINE
	WOTP GUESS	LB/SEC	INITIAL PUMP FLOW RATE GUESS.	DTN	IN		DIAMETER OF TURBINE NOZZLE.
	WOTC GUESS	LB/SEC	INITIAL DILUENT FLOW RATE GUESS.	DRN	IN	145	DIAMETER OF ROLL CONTROL NOZZLE.
	WOTH GUESS	LB/SEC	INITIAL HOT BLEED PORT FLOW RATE GUESS.	IPT	LB-IN2		MOMENT OF PUMP AND TURBINE ROTOR.
	EPS WOOTC	NONE	DILUENT FLOW RATE CLOSURE TOLERANCE.	M INIT	RPM		INITIAL TURBINE SPEED.
	EPS WOOTR	NONE	HOT BLEED PORT FLOW RATE CLOSURE TOLERANCE.	EPS H	NONE		PUMP HEAD RISE CLOSURE TOLERANCE.
	A6	IN2	AREA OF CORE OUTLET.	EPS WP ACT	NONE	150	PUMP ACTUAL WORK CLOSURE TOLERANCE.
130	A STAR	IN2	MINIMUM NOZZLE THROAT AREA.	L	IN		LENGTH OF HOT BLEED PORT.
	PHI(INT)	NONE	NOZZLE TUBE FRICTION FACTOR. IF THIS VALUE IS 0 THE NOZZLE TUBES WILL BE IGNORED.	M	NONE		NUMBER OF POSITION STEPS IN HOT BLEED PORT.
	NO. PARTS	NO. OF SEGMENTS IN NOZZLE TUBES (DISTANCE MODES).		DGO	IN		DIAMETER OF HOT BLEED PORT COLD FLOW HOLES.
	WT WALL X	IN	NOZZLE TUBE WALL THICKNESS.	MCO	NONE		NUMBER OF HOT BLEED PORT COLD FLOW HOLES.
	G1 INIT	BTU/SEC-IN2	INITIAL NET TRANSFER GUESS FOR NOZZLE TUBES.	T	IN		THICKNESS OF HOT BLEED PORT COLD FLOW ANNULUS.
				R	IN	155	THICKNESS OF METAL BETWEEN HOT AND COLD FLOWS IN HOT BLEED PORT.
				THETA	DEG		DILUENT IMPINGEMENT ANGLE.
				L50	NONE		SHOT BLEED PORT COLD FLOW FILM COEFF PARAMETER.
				B COLD	NONE		SHOT BLEED PORT COLD FLOW FILM COEFF PARAMETER.

160 C COLD NONE SHOT BLEED PORT COLD FLOW FILM COEFF PARAMETER.  
 A HOT NONE SHOT BLEED PORT HOT FLOW FILM COEFF PARAMETER.  
 B HOT NONE SHOT BLEED PORT HOT FLOW FILM COEFF PARAMETER.  
 C HOT NONE SHOT BLEED PORT HOT FLOW FILM COEFF PARAMETER.  
 F COLD NONE SHOT BLEED PORT COLD FLOW FRICTION FACTOR.  
 F HOT NONE SHOT BLEED PORT HOT FLOW FRICTION FACTOR.  
 K PWR NONE SE FOR PWR-PWR-CORR.CC.  
 K PCR NONE SE FOR PCR. CC.  
 K IN NONE SE FOR HOT BLEED PORT INLET PRESSURE DROP.  
 K CC NONE INCOMPRESSIBLE FLOW E.  
 K CI NONE INCOMPRESSIBLE FLOW E.  
 B COLD FT-LBP/LB-DEGR SCALD GAS CONSTANT.  
 B HOT FT-LBP/LB-DEGR SHOT GAS CONSTANT.  
 E 11 NONE SE FOR PWR.  
 E 9 NONE SE FOR PWR.  
 E E NONE SE FOR PWR.  
 P 11 PSIA SUPPLEMENTARY IN TURBINE INLET START BOTTLE. IF THIS VALUE IS ZERO, THE PROGRAM WILL ASSUME THAT THERE IS NO START BOTTLE.  
 Y 11 DEGR TURBINE START BOTTLE TEMPERATURE.  
 BELLOWS FLAG NONE 00-IF THIS VALUE IS ZERO, THE BELLOWS SECTIONS WILL BE IGNORED.  
 BELLOWS K NONE STABLE OF BELLOWS SECTION PRESSURE DROP K VALUES VS DISTANCE (IN) INPUT AS 0.00. A MAXIMUM OF TEN PAIRS OF VALUES IS ALLOWED. THE DISTANCES MUST BE IN ASCENDING ORDER AND THE LAST DISTANCE SHOULD BE GREATER THAN OR EQUAL TO THE LENGTH OF THE HOT BLEED PORT.

5. Input Curves  
 a. General  
 EACH CURVE IS INPUT AS A SERIES OF POINTS, EACH PRECEDED BY A SIGN. THE FIRST NUMBER IS THE NUMBER OF POINTS IN THE CURVE. EACH FOLLOWING PAIR OF NUMBERS REPRESENTS A POINT ON THE CURVE. THE INDEPENDENT VARIABLE FIRST. FOR EXAMPLE, THE POINTS (1,10), (2,20) ARE INPUT AS 2+1+10+2+20. THE NUMBER OF POINTS PER CURVE MUST BE GREATER THAN OR EQUAL TO 2, OR EQUAL TO -1. IF THE NUMBER OF POINTS IS -1 THE CURVE WILL BE IGNORED. NOTE THAT A CURVE WHICH IS IGNORED IS NOT THE SAME AS A CURVE WHOSE DEPENDENT VARIABLE IS EVERYWHERE 0. A MAXIMUM NO. OF POINTS IS GIVEN FOR EACH CURVE. ALL CURVES MUST BE IN ASCENDING ORDER OF THE INDEPENDENT VARIABLE.

b. For Each Part

1100	A	SUB F	IN2	SFLOW AREA VS DISTANCE (IN) 10
1200	F	SUB P	IN	SMETTED PERIMETER VS DISTANCE (IN) 10
1300	F	RACT H	NONE	S FRACTION (PERCENT/100) OF INTERNAL HEAT GENERATION VS DISTANCE (IN) 10
1400	H	BTU/IN3-SEC	INTERNAL HEAT GENERATION COEFF VS TIME (SEC) 49	
1500	K	SUB R	BTU/SEC-IN-DEGR	SMETAL THERMAL CONDUCTIVITY VS TEMP (DEGR) 49
1600	C	SUB R	BTU/LB-DEGR	SMETAL HEAT CAPACITY VS TEMP (DEGR) 49
1700	T	1	DEGR	STANK TEMP VS TIME (SEC) 49
1800	P	1	PSIA	STANK PRESSURE VS TIME (SEC) 49
1900	P	OUT MIN	PSIA	SMINIMUM OUTLET PRESSURE VS TIME (SEC) 49
2000	GP		PERCENT	SGATE POSITION OF TURBINE LINE VALVE VS TIME (SEC) 10

c. For Entire System

6. Nozzle Tube Input

A SET OF NOZZLE TUBE INPUT VALUES IS CONTAINED IN THE STANDARD CASE BUT IS NOT RESET FOR EACH INPUT CASE. THE DATA CARDS FOR NOZZLE TUBE INPUT VALUES ARE PLACED BETWEEN THE LAST PART T CARD AND THE FINAL T CARD OF AN INPUT CASE.

IC	AF COLD	IN2	TABLE OF COLD FLOW AREA VS DISTANCE (IN) INPUT AS SEVEN PAIRS OF VALUES OF THE FORM +Z+NF.
IL4	FP COLD	IN	TABLE OF COLD FLOW NETTED PERIMETER VS DISTANCE (IN) INPUT AS SEVEN PAIRS OF VALUES OF THE FORM +Z+PP.
128	D	IN	TABLE OF DIAPETER VS DISTANCE (IN) INPUT AS FOUR PAIRS OF VALUES OF THE FORM +Z+D.
136	RF	NONE	TABLE OF RECOVERY FACTOR VS DISTANCE (IN) INPUT AS FOUR PAIRS OF VALUES OF THE FORM +Z+RF.
144	AF HOT	IN2	TABLE OF HOT FLOW AREA VS DISTANCE (IN) INPUT AS SEVEN PAIRS OF VALUES OF THE FORM +Z+HF.
158	SIGMA	NONE	TABLE OF STATIC TO STAGNATION TEMP RATIO VS DISTANCE (IN) INPUT AS NINE PAIRS OF VALUES OF THE FORM +Z+SIGMA.
176	K(P IN)	NONE	INLET PRESSURE DROP K
177	LENGTH	IN	LENGTH OF NOZZLE TUBES
178	A1	NONE	THERMAL CONDUCTIVITY CONSTANT
179	SIKX1	NONE	THERMAL CONDUCTIVITY CONSTANT
180	CIKX1	NONE	THERMAL CONDUCTIVITY CONSTANT
181	AIKF1	NONE	FILM COEFF CONSTANT
182	BIKF1	NONE	FILM COEFF CONSTANT
183	TEXT1 BUMP	NONE	INITIAL EXIT TEMP GUESS BUMPER
184	Z THRGT	IN	DISTANCE TO MINIMUM THROAT AREA
185	A THRGT	IN2	MINIMUM THROAT AREA

NOTE-- THE ABOVE TABLES MUST BE IN ASCENDING ORDER OF DISTANCE.

3. RESPARTING PROGRAM

AT THE PRESENT TIME, THE PROGRAM MAY NOT BE RESTARTED. THE FORMAT FOR INPUTTING METAL TEMPERATURES FOLLOWS:

LCC	SYMBOL	UNITS	DESCRIPTION
L-150	THETA	DEGR	METAL TEMPS FOR EACH NODE. THE FIRST VALUE IS A LINEAR EXTRAPOLATION OF THE FIRST TWO PRINTED NODES. THE SECOND VALUE IS EQUAL TO THE PRINTED TEMP FOR THE FIRST NODE. THE THIRD VALUE IS THE TEMP FOR THE SECOND NODE, ETC. THE LAST VALUE IS A LINEAR EXTRAPOLATION OF THE LAST TWO PRINTED NODES. TOTAL OF MMAX+2 VALUES.

C. PROGRAM MESSAGES

APPENDIX B

SAMPLE CASE - NERVA ENGINE TRANSIENT PROGRAM

BAD FLUID TEMP PRES PROPERTY ROUTINES. FLUID TEMP OR PRESSURE OUTSIDE RANGE OF HYDROGEN PROPERTY ROUTINES. USUALLY INDICATES DRASTIC ERROR IN INPUT OR CONVERGENCE

BAD TIME PRS. TYP P1 OR T1 NOT IN RANGE OF HYDROGEN PROPERTY ROUTINE

BAD TARE- FLUSH RTT CHECK ON INPUT TAPE

CHECK PUMP FOR NEG CONVERGENCE SOME QUANTITY NEGATIVE. DRASTIC ERROR IN INPUT OR CONVERGENCE

COOLDOWN REACHED OUTLET METAL TEMP LESS THAN THETA MIN

DELTA T TOO SMALL TIME INCREMENT LESS THAN MIN

END OF INPUT NO CASES REMAINING OR TCARD MISSING

ERROR IN PTS/CURVE NUMBER OF POINTS MUST BE GREATER THAN 1 AND LESS THAN MAXIMUM. CURVE MAY BE MISSING ALTOGETHER

ERROR IN STD INPUT TOO MANY CARDS OR TCARD MISSING IN STANDARD CASE

GAS AT PUMP INLET PRESSURE AND TEMP AT PUMP INLET DETERMINE GAS. PUMP OVERSPEEDS. MSV IS NEGATIVE

HEAT TRANSFER ERROR ERROR IN HEAT TRANSFER OTHER THAN NEGATIVE PRESSURE OR FLOW

HELP HELP HELLLL SOMETHING DRASTICALLY WRONG WITH INPUT OR INPUT TAPE-- SEE PROGRAMMER.

ILLEGAL CHARACTER ILLEGAL CHARACTER ON ONE OR MORE DATA CARDS. CARDS WITH ERRORS WILL BE PRINTED OUT. IF NO ILLEGAL CHARACTERS ARE FOUND. SEE PROGRAMMER.

LIG IN TUBE THROAT PLUID IN NOZZLE TUBE THROAT WAS LIQUID ON LAST PASS PRINTS ONLY AT PRINTED TIME POINTS

P TCC SMALL P LESS THAN 1/2 AT SCV. MCEE. PRINTED AT END OF PIP: B-EHE OCCURRED. MAY HAVE OCCURED AT SOPE TIME POINT BETWEEN PRINTING BUT PRINTED AT LATER POINT

NO DILUENT REMOVED NO INPUT DILUENT REMOVAL STATION

NOZZLE TUBE ERROR ERROR ON LAST PASS THROUGH NOZZLE TUBES. TUBES THEREFORE IGNORED.

P6 TOO LOW P6 LESS THAN P6MIN

PREDICTOR FAILED SOME ITERATION FAILED TO CLOSE IN TURBOPUMP PREDICT

TEMP EXCEEDED MAX METAL OR FLUID TEMPERATURE GREATER THAN THAT. PRINTED AFTER PART WERE OCCURED. MAY HAVE OCCURED BETWEEN PRINTED TIME POINTS BUT PRINTED LATER

TOO MANY HOSES NUMBER OF HOSES EXCEEDS MAXIMUM IN ONE OR MORE PART

TOO MANY PARTS NOT ENOUGH S-GRAB AVAILABLE FOR THIS MANY PARTS

WR. WC NOT CLOSED MAX ITERATIONS IN HEAT TRANSFER EXCEEDED

ZERO TCARD MISSING OCCURS ONLY WITH CASE USING STANDARD INPUT. TCARD LEFT OFF OR MORE PARTS THAN STANDARD CASE

\*\*\*\*\* NOT CLOSED THE SPECIFIED HOT BLEED PORT ITERATION DIDNT CLOSE

DEL Z	Z PIS	FRAC	WID P	MW R	MALL R	ENTY A	ENTY H	ENTY V	DEL V
1.10000	1.10000	1.10000	1.10000	1.10000	1.10000	1.10000	1.10000	1.10000	1.10000
DEL T <td>TIME O <td>DEL T <td>PIS <td>DI BIR <td>REL TO <td>PM TYP <td>HE TYP <td>DILUT <td>P1</td> </td></td></td></td></td></td></td></td>	TIME O <td>DEL T <td>PIS <td>DI BIR <td>REL TO <td>PM TYP <td>HE TYP <td>DILUT <td>P1</td> </td></td></td></td></td></td></td>	DEL T <td>PIS <td>DI BIR <td>REL TO <td>PM TYP <td>HE TYP <td>DILUT <td>P1</td> </td></td></td></td></td></td>	PIS <td>DI BIR <td>REL TO <td>PM TYP <td>HE TYP <td>DILUT <td>P1</td> </td></td></td></td></td>	DI BIR <td>REL TO <td>PM TYP <td>HE TYP <td>DILUT <td>P1</td> </td></td></td></td>	REL TO <td>PM TYP <td>HE TYP <td>DILUT <td>P1</td> </td></td></td>	PM TYP <td>HE TYP <td>DILUT <td>P1</td> </td></td>	HE TYP <td>DILUT <td>P1</td> </td>	DILUT <td>P1</td>	P1
1.10000	1.10000	1.10000	1.10000	1.10000	1.10000	1.10000	1.10000	1.10000	1.10000
NO MIN <td>PT CLS <td>PR CLS <td>WST P <td>WST C <td>WST H <td>WST C <td>WST H <td>WST C <td>A, A</td> </td></td></td></td></td></td></td></td>	PT CLS <td>PR CLS <td>WST P <td>WST C <td>WST H <td>WST C <td>WST H <td>WST C <td>A, A</td> </td></td></td></td></td></td></td>	PR CLS <td>WST P <td>WST C <td>WST H <td>WST C <td>WST H <td>WST C <td>A, A</td> </td></td></td></td></td></td>	WST P <td>WST C <td>WST H <td>WST C <td>WST H <td>WST C <td>A, A</td> </td></td></td></td></td>	WST C <td>WST H <td>WST C <td>WST H <td>WST C <td>A, A</td> </td></td></td></td>	WST H <td>WST C <td>WST H <td>WST C <td>A, A</td> </td></td></td>	WST C <td>WST H <td>WST C <td>A, A</td> </td></td>	WST H <td>WST C <td>A, A</td> </td>	WST C <td>A, A</td>	A, A
1.10000	1.10000	1.10000	1.10000	1.10000	1.10000	1.10000	1.10000	1.10000	1.10000
A STAR <td>MTD PF <td>PARIS <td>MALL Z <td>DI INY <td>SUT <td>SCALE P <td>SCALE P <td>SCALE P <td>SCALE P</td> </td></td></td></td></td></td></td></td>	MTD PF <td>PARIS <td>MALL Z <td>DI INY <td>SUT <td>SCALE P <td>SCALE P <td>SCALE P <td>SCALE P</td> </td></td></td></td></td></td></td>	PARIS <td>MALL Z <td>DI INY <td>SUT <td>SCALE P <td>SCALE P <td>SCALE P <td>SCALE P</td> </td></td></td></td></td></td>	MALL Z <td>DI INY <td>SUT <td>SCALE P <td>SCALE P <td>SCALE P <td>SCALE P</td> </td></td></td></td></td>	DI INY <td>SUT <td>SCALE P <td>SCALE P <td>SCALE P <td>SCALE P</td> </td></td></td></td>	SUT <td>SCALE P <td>SCALE P <td>SCALE P <td>SCALE P</td> </td></td></td>	SCALE P <td>SCALE P <td>SCALE P <td>SCALE P</td> </td></td>	SCALE P <td>SCALE P <td>SCALE P</td> </td>	SCALE P <td>SCALE P</td>	SCALE P
1.10000	1.10000	1.10000	1.10000	1.10000	1.10000	1.10000	1.10000	1.10000	1.10000
K, Z <td>D, Z <td>D, H <td>D, TL <td>D, TH <td>D, IM <td>I, PI <td>SPEED <td>M, CLS <td>M, CLS</td> </td></td></td></td></td></td></td></td>	D, Z <td>D, H <td>D, TL <td>D, TH <td>D, IM <td>I, PI <td>SPEED <td>M, CLS <td>M, CLS</td> </td></td></td></td></td></td></td>	D, H <td>D, TL <td>D, TH <td>D, IM <td>I, PI <td>SPEED <td>M, CLS <td>M, CLS</td> </td></td></td></td></td></td>	D, TL <td>D, TH <td>D, IM <td>I, PI <td>SPEED <td>M, CLS <td>M, CLS</td> </td></td></td></td></td>	D, TH <td>D, IM <td>I, PI <td>SPEED <td>M, CLS <td>M, CLS</td> </td></td></td></td>	D, IM <td>I, PI <td>SPEED <td>M, CLS <td>M, CLS</td> </td></td></td>	I, PI <td>SPEED <td>M, CLS <td>M, CLS</td> </td></td>	SPEED <td>M, CLS <td>M, CLS</td> </td>	M, CLS <td>M, CLS</td>	M, CLS
1.10000	1.10000	1.10000	1.10000	1.10000	1.10000	1.10000	1.10000	1.10000	1.10000
ME LTH <td>NO Z <td>D, CO <td>NO MLS <td>T <td>THETA <td>A, CALD <td>A, CALD <td>A, CALD <td>A, CALD</td> </td></td></td></td></td></td></td></td>	NO Z <td>D, CO <td>NO MLS <td>T <td>THETA <td>A, CALD <td>A, CALD <td>A, CALD <td>A, CALD</td> </td></td></td></td></td></td></td>	D, CO <td>NO MLS <td>T <td>THETA <td>A, CALD <td>A, CALD <td>A, CALD <td>A, CALD</td> </td></td></td></td></td></td>	NO MLS <td>T <td>THETA <td>A, CALD <td>A, CALD <td>A, CALD <td>A, CALD</td> </td></td></td></td></td>	T <td>THETA <td>A, CALD <td>A, CALD <td>A, CALD <td>A, CALD</td> </td></td></td></td>	THETA <td>A, CALD <td>A, CALD <td>A, CALD <td>A, CALD</td> </td></td></td>	A, CALD <td>A, CALD <td>A, CALD <td>A, CALD</td> </td></td>	A, CALD <td>A, CALD <td>A, CALD</td> </td>	A, CALD <td>A, CALD</td>	A, CALD
1.10000	1.10000	1.10000	1.10000	1.10000	1.10000	1.10000	1.10000	1.10000	1.10000
C, CALD <td>A, HOT <td>B, HOT <td>C, HOT <td>FRAC C <td>FRAC H <td>RETRN <td>RETRN <td>RETRN <td>RETRN</td> </td></td></td></td></td></td></td></td>	A, HOT <td>B, HOT <td>C, HOT <td>FRAC C <td>FRAC H <td>RETRN <td>RETRN <td>RETRN <td>RETRN</td> </td></td></td></td></td></td></td>	B, HOT <td>C, HOT <td>FRAC C <td>FRAC H <td>RETRN <td>RETRN <td>RETRN <td>RETRN</td> </td></td></td></td></td></td>	C, HOT <td>FRAC C <td>FRAC H <td>RETRN <td>RETRN <td>RETRN <td>RETRN</td> </td></td></td></td></td>	FRAC C <td>FRAC H <td>RETRN <td>RETRN <td>RETRN <td>RETRN</td> </td></td></td></td>	FRAC H <td>RETRN <td>RETRN <td>RETRN <td>RETRN</td> </td></td></td>	RETRN <td>RETRN <td>RETRN <td>RETRN</td> </td></td>	RETRN <td>RETRN <td>RETRN</td> </td>	RETRN <td>RETRN</td>	RETRN
1.10000	1.10000	1.10000	1.10000	1.10000	1.10000	1.10000	1.10000	1.10000	1.10000
SC, CMP <td>SC, INC <td>R, HOT <td>R, LI <td>R, V <td>R, E <td>P, LI <td>P, LI <td>P, LI <td>P, LI</td> </td></td></td></td></td></td></td></td>	SC, INC <td>R, HOT <td>R, LI <td>R, V <td>R, E <td>P, LI <td>P, LI <td>P, LI <td>P, LI</td> </td></td></td></td></td></td></td>	R, HOT <td>R, LI <td>R, V <td>R, E <td>P, LI <td>P, LI <td>P, LI <td>P, LI</td> </td></td></td></td></td></td>	R, LI <td>R, V <td>R, E <td>P, LI <td>P, LI <td>P, LI <td>P, LI</td> </td></td></td></td></td>	R, V <td>R, E <td>P, LI <td>P, LI <td>P, LI <td>P, LI</td> </td></td></td></td>	R, E <td>P, LI <td>P, LI <td>P, LI <td>P, LI</td> </td></td></td>	P, LI <td>P, LI <td>P, LI <td>P, LI</td> </td></td>	P, LI <td>P, LI <td>P, LI</td> </td>	P, LI <td>P, LI</td>	P, LI
1.10000	1.10000	1.10000	1.10000	1.10000	1.10000	1.10000	1.10000	1.10000	1.10000
SEC, 1 <td>R, 1 <td>SEC, 2 <td>K, 2 <td>SEC, 3 <td>K, 3 <td>SEC, 4 <td>K, 5 <td>SEC, 5 <td>K, 5</td> </td></td></td></td></td></td></td></td>	R, 1 <td>SEC, 2 <td>K, 2 <td>SEC, 3 <td>K, 3 <td>SEC, 4 <td>K, 5 <td>SEC, 5 <td>K, 5</td> </td></td></td></td></td></td></td>	SEC, 2 <td>K, 2 <td>SEC, 3 <td>K, 3 <td>SEC, 4 <td>K, 5 <td>SEC, 5 <td>K, 5</td> </td></td></td></td></td></td>	K, 2 <td>SEC, 3 <td>K, 3 <td>SEC, 4 <td>K, 5 <td>SEC, 5 <td>K, 5</td> </td></td></td></td></td>	SEC, 3 <td>K, 3 <td>SEC, 4 <td>K, 5 <td>SEC, 5 <td>K, 5</td> </td></td></td></td>	K, 3 <td>SEC, 4 <td>K, 5 <td>SEC, 5 <td>K, 5</td> </td></td></td>	SEC, 4 <td>K, 5 <td>SEC, 5 <td>K, 5</td> </td></td>	K, 5 <td>SEC, 5 <td>K, 5</td> </td>	SEC, 5 <td>K, 5</td>	K, 5
1.10000	1.10000	1.10000	1.10000	1.10000	1.10000	1.10000	1.10000	1.10000	1.10000
SEC, A <td>F, A <td>SEC, 7 <td>K, 7 <td>SEC, 8 <td>K, 8 <td>SEC, 9 <td>K, 9 <td>SEC, 10 <td>K, 10</td> </td></td></td></td></td></td></td></td>	F, A <td>SEC, 7 <td>K, 7 <td>SEC, 8 <td>K, 8 <td>SEC, 9 <td>K, 9 <td>SEC, 10 <td>K, 10</td> </td></td></td></td></td></td></td>	SEC, 7 <td>K, 7 <td>SEC, 8 <td>K, 8 <td>SEC, 9 <td>K, 9 <td>SEC, 10 <td>K, 10</td> </td></td></td></td></td></td>	K, 7 <td>SEC, 8 <td>K, 8 <td>SEC, 9 <td>K, 9 <td>SEC, 10 <td>K, 10</td> </td></td></td></td></td>	SEC, 8 <td>K, 8 <td>SEC, 9 <td>K, 9 <td>SEC, 10 <td>K, 10</td> </td></td></td></td>	K, 8 <td>SEC, 9 <td>K, 9 <td>SEC, 10 <td>K, 10</td> </td></td></td>	SEC, 9 <td>K, 9 <td>SEC, 10 <td>K, 10</td> </td></td>	K, 9 <td>SEC, 10 <td>K, 10</td> </td>	SEC, 10 <td>K, 10</td>	K, 10
1.10000	1.10000	1.10000	1.10000	1.10000	1.10000	1.10000	1.10000	1.10000	1.10000
FLOW AREA VS DISTANCE									
1.10000									
METED PERIMETER VS Z									
1.10000									
FRAC T HEAT GEN VS DIST									
1.10000									
INT HEAT GEN VS TIME									
1.10000									
THERMAL CONDUCTIVITY									
1.10000									
C, SW R VS TEMPERATURE									
1.10000									
INLET TEMP VS TIME									
1.10000									
INLET PRESSURE VS TIME									
1.10000									
OUTLET PRESSURE VS TIME									
1.10000									
GATE POSITION VS TIME									
1.10000									
PROGRAM INPUT									
DEL Z <td>Z PIS <td>FRAC <td>WID P <td>MW R <td>MALL R <td>ENTY A <td>ENTY H <td>ENTY V <td>DEL V</td> </td></td></td></td></td></td></td></td>	Z PIS <td>FRAC <td>WID P <td>MW R <td>MALL R <td>ENTY A <td>ENTY H <td>ENTY V <td>DEL V</td> </td></td></td></td></td></td></td>	FRAC <td>WID P <td>MW R <td>MALL R <td>ENTY A <td>ENTY H <td>ENTY V <td>DEL V</td> </td></td></td></td></td></td>	WID P <td>MW R <td>MALL R <td>ENTY A <td>ENTY H <td>ENTY V <td>DEL V</td> </td></td></td></td></td>	MW R <td>MALL R <td>ENTY A <td>ENTY H <td>ENTY V <td>DEL V</td> </td></td></td></td>	MALL R <td>ENTY A <td>ENTY H <td>ENTY V <td>DEL V</td> </td></td></td>	ENTY A <td>ENTY H <td>ENTY V <td>DEL V</td> </td></td>	ENTY H <td>ENTY V <td>DEL V</td> </td>	ENTY V <td>DEL V</td>	DEL V
1.10000	1.10000	1.10000	1.10000	1.10000	1.10000	1.10000	1.10000	1.10000	1.10000
FLOW AREA VS DISTANCE									
1.10000									
METED PERIMETER VS Z									
1.10000									
FRAC T HEAT GEN VS DIST									
1.10000									
INT HEAT GEN VS TIME									
1.10000									
THERMAL CONDUCTIVITY									
1.10000									
C, SW R VS TEMPERATURE									
1.10000									
INLET TEMP VS TIME									
1.10000									
INLET PRESSURE VS TIME									
1.10000									
OUTLET PRESSURE VS TIME									
1.10000									
GATE POSITION VS TIME									
1.10000									
PROGRAM INPUT									





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00121 12974 2  
KDAREN EQU 01  
LBR KISMET 49 WORDS  
TAPEN ROUTINES 9900  
3\*THE ABSOLUTE LOCATIONS OF PRTY,EXP,LN, SORT MUST NOT BE CHANGED  
4 PRTY BSS 49.5  
5 PQRRT BSS 5.5  
6 PEXP BSS 9.5  
7 PLOG BSS 5.5  
8 EXP13 BSS 0.5  
9 PAPT3 BSS 21.5  
10 DENT BSS 7.5  
11 DEN BSS 149.5  
12 DEN1 BSS 33.5  
13 THALT BSS 401.5  
14 THAL BSS 9.5  
15 THALL BSS 63.5  
16 PVT BSS 11.5  
17 PVT BSS 295.5  
18 PVT1 BSS 66.5  
19 NRAT BSS 1.5  
20 NRA BSS 111.5  
21 PST BSS 9.5  
22 PST BSS 116.5  
23 DSAT BSS 9.5  
24 DSA BSS 96.5  
25 DST BSS 5.5  
26 DST BSS 79.5  
27 PNBT BSS 5.5  
28 PNB BSS 216.5  
29 PNB1 BSS 0.5  
30 PPT BSS 5.5  
31 PPT BSS 249.5  
32 PPT1 BSS 95.5  
33 CPMT BSS 9.5  
34 CPH BSS 369.5  
35 CPMT1 BSS 0.5  
36 ENT BSS 7.5  
37 ENT BSS 387.5  
38 ENT BSS 139.5  
39 CP3T BSS 6.5  
40 CP3 BSS 370.5  
41 CP31 BSS 201.5  
42 VIST BSS 8.5  
43 VIS BSS 391.5  
44 VIST1 BSS 154.5  
45 INT BSS 501.5  
46 XLC BSS 2.5  
47 XLC BSS 11.5  
48 XLC1 BSS 102.5  
49\*EXP, LN, SORT FOLLOW RESPECTIVELY  
50 EXP BSS  
51 UNLIST  
161 LIST

2424C 0 24100 0 24277  
12974  
12974  
12701  
12706  
12713  
12720  
12730  
12755  
12764  
13205  
13246  
13257  
13257  
14100  
14177  
14212  
14611  
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15071  
15076  
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16777  
16766  
16777  
17554  
17675  
20507  
20716  
20724  
21506  
22017  
22027  
22636  
23070  
24055  
24057  
24072

EXP, LN, SORT FOLLOW RESPECTIVELY  
FDP  
UNLIST  
/LN 2

DEN CALLS  
POWER ROUTINE (AZE)

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PAGE 1  
JOB 12013.  
JOB 12013.

163*MASTER CONTROL REGION											
24416	0	60000	0	40316	164	BEGIN	STZ	PP41			
24417	0	76000	0	00016	165		+1	LMTM			
24420	0	07401	4	00053	166		+2	TSX	KBINLD,4,1	READ IN PRPTY	
24421	0	07400	4	40710	167		+3	TSX	ICURV,4		
24422	0	00061	0	00005	168		+4	PZE	5,,49		
24423	0	00000	0	00020	169		+5	PZE	16		
24424	0	00000	0	31113	170		+6	PZE	AYK01		
24425	-0	50000	0	32576	171		+7	CAL	ENDD		
24426	0	60200	0	00056	172		+8	SLW	KERROR		
24427	0	07400	4	27323	173		+9	TSX	AZXC,4	READ STANDARD CASE	
24430	0	63400	0	24603	174	START	SXA	AZM10,0			
24431	0	60000	0	32721	175		+1	STZ	X+3		
24432	0	07400	4	27161	176		+2	TSX	AZX,4	TEST INPUT FOR NEW CASE	
24433	0	07400	4	27236	177	GO	TSX	AZXA,4		INPUT	
24434	-0	52000	0	32612	178		+1	NZT	TCARD+11		
24435	0	02000	0	24615	179		+2	TRA	AZM12	END OF CASE	
24436	-0	50000	0	32577	180		+3	CAL	TCARD		
24437	0	56000	0	32600	181		+4	LDQ	TCARD+1		
24440	-0	76300	0	00006	182		+5	LGL	6		
24441	0	60200	0	34555	183		+6	SLW	FX	PART NAME	
24442	0	07400	4	32113	184		+7	TSX	PRTD,4		
24443	0	63400	0	24500	185		+8	SXA	AZM8,0		
24444	-0	77400	1	00006	186		+9	AXC	NCTMP,1		
24445	-0	52000	0	32721	187		+10	NZT	X+3	O= 1ST PART	
24446	-0	77400	1	00012	188		+11	AXC	NCURV,1		
24447	0	77400	2	00000	189		+12	AXT	0,2		
24450	-0	63400	1	24507	190		+13	SXD	AZM32,1		
24451	0	77400	1	00000	191		+14	AXT	0,1		
24452	-0	50000	1	24703	192	AZM7	CAL	AZM01,1		TABLE STORAGE ADDRESS	
24453	0	62100	0	24472	193		+1	STA	AZM24	LINTS	
24454	0	62100	0	24502	194		+2	STA	AZM6		
24455	0	62200	0	24465	195		+3	STD	AZM26		
24456	0	36100	0	40200	196		+4	ACL	FX1		
24457	0	62100	0	24474	197		+5	STA	AZM25		
24460	0	63400	1	24505	198		+6	SXA	AZM28,1		
24461	0	50000	2	36230	199		+7	CLA	AZD,2	NO. PTS	
24462	-0	12000	0	24503	200		+8	TMI	AZM27	-= CURVE NOT NEEDED	
24463	-0	30000	0	40306	201		+9	UFA	FIX		
24464	0	73400	4	00000	202		+10	PAX	,4		
24465	3	00000	4	24676	203	AZM26	TXH	AZM22,4,**0		TOO MANY PTS	
24466	-3	00001	4	24676	204		+1	TXL	AZM22,4,1	TOO FEW PTS.	
24467	-0	63400	4	24502	205		+2	SXD	AZM6,4		
24470	0	77400	1	00000	206		+3	AXT	0,1		
24471	0	50000	2	36231	207	AZM5	CLA	AZD+1,2			
24472	0	60100	1	00000	208	AZM24	STO	**0,1			
24473	0	50000	2	36232	209		+1	CLA	AZD+2,2		
24474	0	60100	1	00000	210	AZM25	STO	**0,1			
24475	1	77776	1	24476	211		+1	TXI	**+1,1,-2		
24476	1	77776	2	24477	212		+2	TXI	**+1,2,-2		
24477	2	00001	4	24471	213		+3	TIX	AZM5,4,1		
24478	0	00000	0	00000	214	AZM2	AXT	**0,2			

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24501	0	07400	4	42511	215		+1	TSX	LINTS,4		
24502	0	00000	0	00000	216	AZM6	PZE	**0,,**0			
24503	1	77634	2	24504	217	AZM27	TXI	**+1,2,-100			
24504	0	63400	2	24500	218		+1	SXA	AZM8,2		
24505	0	77400	1	00000	219	AZM28	AXT	**0,1			
24506	1	77777	1	24507	220		+1	TXI	**+1,1,-1		
24507	3	00000	1	24452	221	AZM32	TXH	AZM7,1,**0			
24510	0	50000	0	36065	222	AZM1	CLA	DMAX			
24511	-0	30000	0	40306	223		+1	UFA	FIX		
24512	0	62100	0	34556	224		+2	STA	FX+1	NO. DEL Z PTS	
24513	0	50000	0	40200	225		+3	CLA	FX1		
24514	0	60100	0	34562	226		+4	STO	FX+5		
24515	0	50000	0	36100	227		+5	CLA	DEL		
24516	0	60100	0	35625	228		+6	STO	PT+11		
24517	0	60000	0	35616	229		+7	STZ	PT+4		
24520	0	60000	0	35617	230		+8	STZ	PT+5		
24521	0	77400	2	00000	231		+9	AXT	0,2		
24522	0	53400	1	34556	232		+10	LXA	FX+1,1		
24523	-3	00060	1	24526	233		+11	TXL	**+3,1,NZMAX-2		
24524	-1	24670	0	25421	234		+12	SYR	AZF,,AZM11	TOO MANY NODES	
24525	0	02000	0	24654	235		+13	TRA	AZM4	FLUSH CASE	
24526	1	00001	1	24527	236		+14	TXI	**+1,1,1		
24527	0	52000	0	36077	237		+15	ZET	DTMI	INITIAL TIME	
24530	0	02000	0	24573	238		+16	TRA	AZM19		
239*RESTART CASE TRANSFERS AROUND HERE											
24531	0	50000	0	32640	240		+17	CLA	P+18	POMIN	
24532	0	52000	0	32721	241		+18	ZET	X+3	O=1ST PART	
24533	0	02000	0	24542	242		+19	TRA	AZM17		
24534	0	50000	0	36111	243		+20	CLA	DPO		
24535	-0	10000	0	24541	244		+21	TNZ	AZM17-1	POMIN INPUT	
24536	0	75400	0	00000	245		+22	PXA	,0		
24537	0	07400	4	42437	246		+23	TSX	LINT,4		
24540	0	00000	0	33441	247		+24	PZE	WPO		
24541	0	60100	0	32640	248		+25	STO	P+18	POMIN	
24542	0	50000	0	36103	249	AZM17	CLA	DTHO			
24543	0	12000	0	24546	250		+1	TPL	**3		
24544	0	50000	2	35636	251		+2	CLA	AZ01,2		
24545	0	02000	0	24547	252		+3	TRA	**2		
24546	3	00000	2	24556	253		+4	TXH	AZM9,2,0		
24547	0	56000	0	32640	254		+5	LDQ	P+18		
24550	0	07400	4	25564	255		+6	TSX	AZH,4		
24551	0	07400	4	42602	256		+7	TSX	ERROR,4		
24552	0	56000	0	33730	257		+8	LDQ	WPR+6	RHO	
24553	0	50000	0	36103	258		+9	CLA	DTHO		
24554	3	00000	2	24556	259		+10	TXH	AZM9,2,0		
24555	-0	60000	0	35620	260		+11	STQ	PT+6	INLET	
24556	-0	60000	2	35720	261	AZM9	STQ	AZ06,2			
24557	-0	12000	0	24561	262		+1	TMI	**2		
24560	0	60100	2	35636	263		+2	STO	AZ01,2		
24561	0	60000	2	36002	264		+3	STZ	AZ08,2		
24562	1	77777	2	24563	265		+4	TXI	**+1,2,-1		
24563	2	00001	1	24562	266		+5	TIX	AZM17,1,1		
24564	-0	60000	0	35634	267		+6	STQ	PT+18	OUTLET DENSITY	

24566	0	60100	2	35636	269	+8	STO	AZ01,2	
24567	0	50000	2	35636	270	+9	CLA	AZ01,2	
24570	0	60100	0	32633	271	+10	STO	P+13	T6
24571	0	60000	0	35626	272	+11	STZ	PT+12	
24572	0	60000	0	35627	273	+12	STZ	PT+13	
24573	0	50200	0	36064	274		AZM19	CLS	DELZ
24574	0	24100	0	40214	275	+1	FOP	FL2	
24575	-0	60000	0	35615	276	+2	STQ	PT+3	
24576	0	50000	0	36065	277	+3	LDQ	DMAX	
24577	0	26000	0	36064	278	+4	FHP	DELZ	
24600	0	30000	0	35615	279	+5	FAD	PT+3	
24601	0	60100	0	35615	280	+6	STO	PT+3	MAXIMUM Z
281*MOVE DATA TO STORAGE									
24602	0	77400	2	01775	282	+7	AXT	AZM25,2	
24603	0	77400	4	00000	283		AZM10	AXT	**0,4
24604	-3	00000	4	24606	284	+1	TXL	**2,4,0	
24605	-3	53475	4	24653	285	+2	TXL	AZM20,4,AZMT+AZM25+206	
24606	0	50000	2	36076	286	+3	CLA	AZMTE,2	
24607	0	60100	4	51162	287	+4	STO	AZMT,4	
24610	1	77777	4	24611	288	+5	TXI	**1,4,-1	
24611	2	00001	2	24606	289	+6	TIX	*-3,2,1	
24612	0	63400	4	24603	290	+7	SXA	AZM10,4	
24613	-0	62500	0	32721	291	+8	STL	X+3	
24614	C	02000	0	24433	292	+9	TRA	GO	READ IN NEXT PART
293*END OF MULTI-PHASE INPUT									
24615	0	52200	0	24603	294		AZM12	XEC	AZM10
24616	-3	00000	4	42602	295	+1	TXL	ERROR,4,0	NO INPUT
24617	1	62717	4	24620	296	+2	TXI	**1,4,-AZMTG	
24620	-0	63400	4	25321	297	+3	SXD	AZB3,4	
24621	-0	63400	4	26543	298	+4	SXD	AZPI4,4	
24622	-0	63400	4	26217	299	+5	SXD	AZK4,4	
24623	-0	63400	4	26056	300	+6	SXD	AZJ9,4	
24624	-0	63400	4	25217	301	+7	SXD	AZAC7,4	
24625	-0	50000	0	40304	302	+8	CAL	BLANK	
24626	0	60200	0	32612	303	+9	SLW	TCARD+11	
304*INITIALIZE FOR SINGLE AND MULTIPLE PARTS									
24627	0	50000	0	36101	305		AZM29	CLA	ONDT
24630	-0	30000	0	40306	306	+1	UFA	FIX	NO. TIME POINTS
24631	0	36100	0	40200	307	+2	ACL	FX1	
24632	0	73400	1	00000	308	+3	PAX	,1	
24633	0	07400	4	25201	309	+4	TSX	AZAC,4	
24634	0	07400	4	25034	310		AZM31	TSX	AZA,4
24635	0	07400	4	26324	311	+1	TSX	AZPC,4	
24636	0	07400	4	25633	312	+2	TSX	AZI,4	HEAT TRNS AND MBP ITERATION
24637	0	07400	4	26462	313	+3	TSX	AZPI,4	PRINT HT TRNS
24640	0	07400	4	26170	314	+4	TSX	AZK,4	MOVE METAL Tmps TO PERM STD
24641	0	07400	4	26664	315	+5	TSX	AZPP,4	PRINT PREDICTED VALUES
24642	0	07400	4	31601	316	+6	TSX	AZPPA,4	I TURBO-PUMP VALUES
24643	0	07401	4	26664	317	+7	TSX	AZPP,4,1	PRINT CORRECTED VALUES
24644	0	07400	4	26617	318	+8	TSX	AZPI8,4	BUMP PRINT COUNTER
24645	-2	00001	1	24430	319	+9	TNX	START,1,1	
24646	0	07400	4	25752	320		AZM2	TSX	COMPUTE METAL Tmps FOR NHXT TIME
24647	0	07400	4	32006	321	+1	TSX	AYT,4	TEST FOR COOLDOWN REACHED
24648	0	07400	4	26075	322	+2	TSX	AZP,4	INLET CONDITIONS FOR TIME +1

24651	0	07400	4	31627	323	+3	TSX	AZPB,4	
24652	0	02000	0	24634	324	+4	TRA	AZM31	TURBOPUMP PREDICTOR
329*EL FLUSHO FOR INPUT ERRORS-- TOO MANY PARTS									
24653	-1	24665	0	25421	326		AZM20	STR	AZF,,AZM21
24654	0	07478	4	00101	327		AZM4	TSX	KMOVEB,4,62
24655	-1	00014	0	32577	328	+1	FVE	TCARD,,12	
24656	0	16200	0	24664	329	+2	TQP	AZM3	
24657	0	12000	0	24661	330	+3	TPL	**2	
24660	0	07400	4	00076	331	+4	TSX	KFINIS,4	
24661	-0	50000	0	32612	332	+5	CAL	TCARD+11	PART FLAG
24662	-0	10000	0	24654	333	+6	TNZ	AZM20+1	
24663	0	02000	0	24430	334	+7	TRA	START	NEW CASE
24664	-1	24673	0	25417	335		AZM3	STR	AZFF,,AZM30
24665	-2	34646	6	04421	336		AZM21	BCI	3,TOO MANY PARTS
24670	-2	34646	6	04421	337		AZM11	BCI	3,TOO MANY NODES
24673	3	02543	4	76030	338		AZM30	BCI	3,HELP HELP HEELLLL
339*EL FLUSHO FOR MISSING CURVE OR TOO MANY POINTS									
24676	-1	24700	0	25421	340		AZM22	STR	AZF,,AZM23
24677	0	02000	0	24654	341	+1	TRA	AZM20+1	MULTI-PART
24700	2	59151	4	65160	342		AZM23	BCI	3,ERROR IN PTS/CURVE
24703	0	00012	0	34567	343		AZM01	PZE	WAF,,10
24704	0	00012	0	34625	344	+1	PZE	WFP,,10	
24705	0	00012	0	34663	345	+2	PZE	WH,,10	
24706	0	00061	0	34721	346	+3	PZE	WHT,,49	
24707	0	00061	0	35144	347	+4	PZE	WK,,49	
24710	0	00061	0	35367	348	+5	PZE	WCR,,49	
24711	0	00061	0	32773	349	+6	PZE	WTI,,49	
24712	0	00061	0	33216	350	+7	PZE	WPI,,49	
24713	0	00061	0	33441	351	+8	PZE	WPO,,49	
24714	0	00012	0	33664	352	+9	PZE	WGP,,10	

354*REGION TO EVALUATE FINITE DIFFERENCE TEMPERATURE EQUATIONS									
24715	0	63400	4	25025	355		AZT	SXA	AZTR,4
24716	0	63400	2	25026	356	+1	SXA	AZTR+1,2	
24717	0	50000	1	34556	357	+2	CLA	FX+1,1	
24720	0	73700	4	00000	358	+3	PAC	,4	
24721	-0	63400	1	24722	359	+4	SXD	**1,1	
24722	1	00000	4	24723	360	+5	TXI	**1,4,**0	
24723	0	75400	1	00000	361	+6	PXA	,1	
24724	0	73400	2	00000	362	+7	PAX	,2	
24725	-0	63400	4	25017	363	+8	SXD	AZT1,4	
24726	0	07400	4	30155	364	+9	TSX	AVE,4	
24727	0	02000	0	25032	365	+10	TRA	AZT3	ERROR
24730	0	02000	0	25030	366	+11	TRA	AZT4	ERROR
24731	0	50000	0	32620	367	+12	CLA	P+2	INLET TEMP
24732	0	60100	2	34163	368	+13	STO	AZ03,2	
24733	0	50000	0	32631	369	+14	CLA	P+11	WDOT
24734	0	60100	2	34101	370	+15	STO	AZ02,2	
24735	0	50000	0	32621	371	+16	CLA	P+3	INLET PRESS
24736	0	60100	2	34245	372	+17	STO	AZ04,2	
24737	0	50000	1	36064	373	+18	CLA	DEI Z,1	

24741	0	13100	0	00000	375	+20	XCA		INITIAL Z IN AC
24742	0	60100	0	32616	376	AZT2	STO	P	Z
24743	0	50000	2	35637	377	+1	CLA	AZ01+1,2	
24744	0	60100	0	32617	378	+2	STO	P+1	
24745	0	07400	4	31722	379	+3	TSX	AYR,4	
24746	0	02000	0	25032	380	+4	TRA	AZT3	
24747	0	56000	0	33746	381	+5	LDQ	TP+9	2M-1
24750	0	26000	0	32620	382	+6	FMP	P+2	T
24751	0	30000	0	32617	383	+7	FAD	P+1	METAL TEMP
24752	0	30000	0	32617	384	+8	FAD	P+1	
24753	0	24100	0	33745	385	+9	FDP	TP+8	
24754	0	13100	0	00000	386	+10	XCA		
24755	0	60100	2	34164	387	+11	STO	AZ03+1,2	T M+1,N
24756	0	60100	0	32620	388	+12	STO	P+2	
24757	0	30200	2	34163	389	+13	FSB	AZ03,2	
24760	0	24100	2	34163	390	+14	FDP	AZ03,2	
24761	0	13100	0	00000	391	+15	XCA		
24762	0	30000	0	33766	392	+16	FAD	TP+25	
24763	0	13100	0	00000	393	+17	XCA		
24764	0	26000	0	34002	394	+18	FMP	TP+37	
24765	0	60100	0	33772	395	+19	STO	TP+29	PRESSURE DROP TERM
24766	0	50000	0	32621	396	+20	CLA	P+3	
24767	0	30200	0	33772	397	+21	FSB	TP+29	
24770	0	60100	0	32621	398	+22	STO	P+3	PRESSURE
24771	0	60100	2	34246	399	+23	STO	AZ04+1,2	P M+1,N
24772	-0	12000	0	25032	400	+24	TMI	AZT3	
24773	0	50000	0	32623	401	+25	CLA	P+5	RHO M,N EQN HT13
24774	0	60100	2	34411	402	+26	STO	AZ07,2	
24775	0	30200	2	35720	403	+27	FSB	AZ06,2	RHO M,N-1
24776	0	13100	0	00000	404	+28	XCA		
24777	0	26000	0	34074	405	+29	FMP	TP+95	
25000	0	30000	0	32631	406	+30	FAD	P+11	
25001	0	30200	2	36003	407	+31	FSB	AZ08+1,2	
25002	0	30000	2	36002	408	+32	FAD	AZ08,2	
25003	-3	62716	1	25005	409	+33	TXL	**2,1,-AZMTG-1	*****
25004	0	50000	0	32631	410	+34	CLA	P+11	
25005	0	60100	2	34102	411	+35	STO	AZ02+1,2	
25006	0	60100	0	32631	412	+36	STO	P+11	WDOT M+1,N
25007	-0	12000	0	25030	413	+37	TMI	AZT4	
25010	0	50000	0	32622	414	+38	CLA	P+4	HF
25011	0	60100	2	34327	415	+39	STO	AZ05,2	
25012	0	50000	0	33731	416	+40	CLA	WPR+7	
25013	0	60100	2	34473	417	+41	STO	AZ09,2	
25014	0	50000	0	32616	418	+42	CLA	P	
25015	0	30000	1	36064	419	+43	FAD	DELZ,1	
25016	1	77777	2	25017	420	+44	TXI	**1,2,-1	
25017	3	00000	2	24742	421	AZT1	TXH	AZT2,2,**0	
25020	0	07400	4	30201	422	+1	TSX	AYEA,4	
25021	0	02000	0	25032	423	+2	TRA	AZT3	ERROR
25022	0	02000	0	25030	424	+3	TRA	AZT4	ERROR
25023	0	50000	0	33731	425	+4	CLA	WPR+7	
25024	0	60100	2	34473	426	+5	STO	AZ09,2	
25025	0	77400	4	00000	427	AZTR	AXT	**0,4	
25026	0	77400	4	00000	428	AZTR	AXT	**0,4	

25027	0	02000	4	00003	429	+2	TRA	3,4	
25030	0	52200	0	25025	430	AZT4	XEC	AZTR	
25031	1	00002	4	25026	431	+1	TXI	AZTR+1,4,2	ERROR EXIT FOR NEGATIVE FLOW RATE
25032	0	52200	0	25025	432	AZT3	XEC	AZTR	ERROR EXIT
25033	1	00001	4	25026	433	+1	TXI	AZTR+1,4,1	

435\*REGION TO COMPUTE CONSTANTS FOR ONE TIME STEP

25034	0	50000	0	34072	436	AZA	CLA	TP+93	
25035	0	60100	0	32630	437	+1	STO	P+10	NEW TIME
25036	0	52000	0	36111	438	+2	ZET	DPD	
25037	0	02000	0	25046	439	+3	TRA	AZAI+1	
25040	0	63400	4	25045	440	+4	SXA	AZAI,4	NEW POHIN
25041	0	50000	0	32630	441	+5	CLA	P+10	
25042	0	07400	4	42437	442	+6	TSX	LINT,4	
25043	0	00000	0	33441	443	+7	PZE	WPO	
25044	0	60100	0	32640	444	+8	STO	P+18	
25045	0	77400	4	00000	445	AZAI	AXT	**0,4	
25046	0	50000	0	34064	446	+1	CLA	TP+87	P1
25047	0	60100	0	32652	447	+2	STO	P+28	
25050	0	50000	0	34065	448	+3	CLA	TP+88	T1
25051	0	60100	0	32653	449	+4	STO	P+29	
25052	0	50000	0	32674	450	+5	CLA	P+46	P2
25053	0	60100	0	32654	451	+6	STO	P+30	
25054	0	50000	0	32675	452	+7	CLA	P+47	T2
25055	0	60100	0	32655	453	+8	STO	P+31	
25056	0	50000	0	34073	454	+9	CLA	TP+94	GP
25057	0	60100	0	32657	455	+10	STO	P+33	
25060	0	50000	0	32666	456	+11	CLA	P+40	N
25061	0	60100	0	32665	457	+12	STO	P+39	
25062	0	50000	0	34017	458	+13	CLA	TP+50	RHO 1
25063	0	60100	0	34060	459	+14	STO	TP+83	
25064	0	50000	0	34056	460	+15	CLA	TP+81	DELH (BTU/LB)
25065	0	60100	0	34066	461	+16	STO	TP+89	
25066	0	50000	0	32677	462	+17	CLA	P+49	WDOTP
25067	0	60100	0	32643	463	+18	STO	P+21	
25070	0	50000	0	34046	464	+19	CLA	TP+73	WDOTC
25071	0	60100	0	32644	465	+20	STO	P+22	
25072	0	50000	0	32636	466	+21	CLA	P+16	HSV
25073	0	60100	0	32635	467	+22	STO	P+15	
25074	0	02000	4	00001	468	+23	TRA	1,4	

470\*REGION TO OBTAIN CONSTANTS FOR TIME I+1

25075	0	50000	0	32630	471	AZAA	CLA	P+10	
25076	0	30000	0	32637	472	+1	FAD	P+17	
25077	0	60100	0	34072	473	+2	STO	TP+93	NEW TIME
25100	0	63400	4	25122	474	+3	SXA	AZAAR,4	
25101	0	52000	0	36107	475	+4	ZET	DPI	
25102	0	02000	0	25114	476	+5	TRA	AZAA1	
25103	0	50000	0	34072	477	+6	CLA	TP+93	
25104	0	07400	4	42437	478	+7	TSX	LINT,4	
25105	0	00000	0	33216	479	+8	PZE	WPI	
25106	0	60100	0	34064	480	+9	STO		

25110	0	07400	4	42437	482	+11	TSX	LINT,4
25111	0	00000	0	32773	483	+12	PZE	WTI
25112	0	60100	0	34069	484	+13	STO	TP+88
25113	0	07400	4	30493	485	+14	TSX	AYII,4
25114	0	52000	0	36130	486	AZAA1	ZET	OGP
25115	0	02000	0	25122	487	+1	TRA	AZAA8
25116	0	90000	0	34072	488	+2	CLA	TP+93
25117	0	07400	4	42437	489	+3	TSX	LINT,4
25120	0	00000	0	33644	490	+4	PZE	WGP
25121	0	60100	0	34073	491	+5	STO	TP+94
25122	0	77400	4	00000	492	AZAA8	AXT	000,4
25123	0	02000	4	00001	493	+1	TRA	1,4

TI

GP

495\*REGION TO FIND VALUES AT ZERO TIME

25124	0	63400	4	25174	494	AZAB	SXA	AZAB8,4
25125	0	90200	0	36100	497	+1	CLS	DELT
25126	0	60200	0	32637	498	+2	SLM	P+17
25127	0	60100	0	32630	499	+3	STO	P+10
25130	0	07400	4	25073	500	+4	TSX	AZAA,4
25131	0	90000	0	36107	501	+5	CLA	DPI
25132	0	10000	0	25137	502	+6	TZE	AZAB1
25133	0	60100	0	34064	503	+7	STO	TP+87
25134	0	90000	0	36110	504	+8	CLA	DTI
25135	0	60100	0	34065	505	+9	STO	TP+88
25136	0	07400	4	30453	506	+10	TSX	AYII,4
25137	0	90000	0	36130	507	AZAB1	CLA	OGP
25140	0	10000	0	25142	508	+1	TZE	0+2
25141	0	60100	0	34073	509	+2	STO	TP+94
25142	0	90000	0	34064	510	+3	CLA	TP+87
25143	0	60100	0	32674	511	+4	STO	P+46
25144	0	60100	0	32652	512	+5	STO	P+28
25145	0	90000	0	34065	513	+6	CLA	TP+88
25146	0	60100	0	32675	514	+7	STO	P+47
25147	0	60100	0	32653	515	+8	STO	P+29
25150	0	90000	0	36111	516	+9	CLA	DPO
25151	0	60100	0	32640	517	+10	STO	P+18
25152	0	90000	0	36143	518	+11	CLA	DNI
25153	0	60100	0	32666	519	+12	STO	P+40
25154	0	90000	0	36114	520	+13	CLA	DWP
25155	0	60100	0	32677	521	+14	STO	P+49
25156	0	90000	0	36115	522	+15	CLA	DWC
25157	0	60100	0	34066	523	+16	STO	TP+73
25160	0	90000	0	36116	524	+17	CLA	DWH
25161	0	60100	0	34045	525	+18	STO	TP+72
25162	0	60000	0	34042	526	+19	STZ	TP+69
25163	0	60000	0	34043	527	+20	STZ	TP+70
25164	0	60000	0	34052	528	+21	STZ	TP+77
25165	0	60000	0	32662	529	+22	STZ	P+36
25166	0	60000	0	34053	530	+23	STZ	TP+78
25167	0	60000	0	32664	531	+24	STZ	P+38
25170	0	60000	0	32700	532	+25	STZ	P+50
25171	0	60000	0	32670	533	+26	STZ	P+42
25172	0	60000	0	32672	534	+27	STZ	P+44
25173	0	00000	0	00000	535			

READ CURVES

P1

TI

GP

P1

25174	0	77400	4	00000	536	AZAB8	AXT	000,4
25175	0	02000	4	00001	537	+1	TRA	1,4
25176	2	22124	4	06321	538	AZAB2	BCI	3,BAD TANK PRS, TMP

540\*REGION TO INITIALIZE PROGRAM

25201	0	63400	4	25260	541	AZAC	SXA	AZAC8,4
25202	0	63400	1	25261	542	+1	SXA	AZAC8,1,1
25203	0	90000	0	36106	543	+2	CLA	DDIL
25204	-0	30000	0	40306	544	+3	UFA	FIX
25205	0	79700	4	00000	545	+4	PAC	,4
25206	3	00000	4	25210	546	+5	TXH	0+2,4,0
25207	-1	29263	0	25417	547	AZAC5	STR	AZFF, AZAC4
25210	-3	77775	4	25213	548	+1	TXL	AZAC1,4,-3
25211	-0	62500	4	32715	549	+2	STL	X-1,4
25212	0	02000	0	25222	550	+3	TRA	AZAC3
25213	-0	77400	1	15061	551	AZAC1	AXC	AZMTG,1
25214	1	00003	4	25215	552	+1	TXI	0+1,4,3
25215	-3	00000	4	25221	553	AZAC6	TXL	AZAC2,4,0
25216	1	76003	1	25217	554	+1	TXI	0+1,1,-AZMTS
25217	-3	00000	1	25207	555	AZAC7	TXL	AZAC5,1,000
25220	1	00001	4	25215	556	+1	TXI	AZAC6,4,1
25221	-0	62500	1	34557	557	AZAC2	STL	FX+2,1
25222	0	07400	4	25124	558	AZAC3	TSX	AZAB,4
25223	0	07400	4	27657	559	+1	TSX	AYC,4
25224	0	07400	4	44724	560	+2	TSX	HBZ,4
25225	0	90000	0	36077	561	+3	CLA	DTMI
25226	0	10000	0	25231	562	+4	TZE	0+3
25227	0	90000	0	36103	563	+5	CLA	DTHO
25230	0	60100	0	32633	564	+6	STO	P+13
25231	0	52000	0	36123	565	+7	ZET	DNZFF
25232	0	07400	4	26247	566	+8	TSX	AZNI,4
25233	0	90000	0	36201	567	+9	CLA	DP11
25234	0	60100	0	32742	568	+10	STO	X+20
25235	0	90000	0	36127	569	+11	CLA	DS+T
25236	-0	30000	0	40306	570	+12	UFA	FIX
25237	0	32200	0	40306	571	+13	ERA	FIX
25240	0	13100	0	00000	572	+14	XCA	,0
25241	0	75400	0	00000	573	+15	PXA	,0
25242	0	22100	0	40212	574	+16	DVP	FXIE3
25243	0	60100	0	47714	575	+17	STO	HB6
25244	-0	60000	0	44475	576	+18	STO	AZNS
25245	0	90000	0	36076	577	+19	CLA	DPRI
25246	-0	30000	0	40306	578	+20	UFA	FIX
25247	0	32200	0	40306	579	+21	ERA	FIX
25250	0	13100	0	00000	580	+22	XCA	,0
25251	0	75400	0	00000	581	+23	PXA	,0
25252	0	22100	0	40212	582	+24	DVP	FXIE3
25253	-0	60000	0	32725	583	+25	STO	X+7
25254	0	62100	0	32726	584	+26	SYA	X+8
25255	0	60000	0	32727	585	+27	SYZ	X+9
25256	-0	62500	0	32737	586	+28	STL	X+17
25257	0	07401	4	32541	587	+29	TSX	PL,4,1
25260	0	77400	4	00000	588	AZAC8	AXT	000,4
25261	0	77400	1	00000	589	+1	AXT	000,1

DILUENT REMOVAL FLAG

IN CORRECT PART

T6

PRINT HOT BLEED PORT  
PRINT NOZZLE TUBES

SKIP PRINT FLAG

RESTORE PAGE

25262 0 02000 4 00001 590 +2 TRA 1,4  
 25263 -0 54660 2 43143 591 AZAC4 BCI 3,NO DILUENT REMOVED

593\*REGION TO COMPUTE MAIN ENGINE HEAT TRANSFER

25264	0	63400	4	25331	594	AZB	SXA	AZBR,4	
25267	0	63400	1	25332	595		+1 SXA	AZBR+1,1	
25270	0	60000	0	32722	596		+2 STZ	X+4	
25271	0	60000	0	32744	597		+3 STZ	X+22	
25272	-0	52000	0	32716	598		+4 NZT	X	
25273	0	02000	0	25274	599		+5 TRA	**3	
25274	0	07400	4	27353	600		+6 TSX	AZY,4	DILUENT AT PUMP DISCHARGE
25275	0	02000	0	25337	601		+7 TRA	AZB12	MOOTR -
25276	0	07400	4	27347	602		+8 TSX	AZZ,4	P3 AND T3
25277	-0	52000	0	32717	603		+9 NZT	X+1	
25300	0	02000	0	25303	604		+10 TRA	**3	
25301	0	07400	4	27353	605		+11 TSX	AZY,4	DILUENT AT TUBE INLET
25302	0	02000	0	25337	606		+12 TRA	AZB12	
25303	-0	52000	0	36123	607		+13 NZT	DNZFF	
25304	0	02000	0	25310	608		+14 TRA	AZB5	
25305	0	07400	4	42636	609		+15 TSX	AZN,4	
25306	0	02000	0	25343	610		+16 TRA	AZB11	
25307	0	02000	0	25341	611		+17 TRA	AZB9	NEG PRESS
25310	-0	77400	1	15061	612	AZB5	AXC	AZMTG,1	
25311	-0	52000	1	34557	613	AZB2	NZT	FX+2,1	
25312	0	02000	0	25315	614		+1 TRA	**3	
25313	0	07400	4	27353	615		+2 TSX	AZY,4	
25314	0	02000	0	25337	616		+3 TRA	AZB12	HEAT TRANS
25315	0	07400	4	24715	617		+4 TSX	AZT,4	
25316	0	02000	0	25337	618		+5 TRA	AZB12	
25317	0	02000	0	25334	619		+6 TRA	AZB8	
25320	1	76003	1	25321	620		+7 TXI	**1,1,-AZMTS	
25321	3	00000	1	25311	621	AZB3	TXH	AZB2,1,**0	
25322	0	50000	0	32620	622		+1 CLA	P+2	T
25323	0	60100	0	32633	623		+2 STO	P+13	
25324	0	50000	0	32621	624		+3 CLA	P+3	P6
25325	0	60100	0	32656	625		+4 STO	P+32	
25326	0	56000	0	32640	626		+5 LQ	P+18	MIN PO
25327	0	04000	0	25331	627		+6 TLQ	**2	
25330	-0	62500	0	32722	628		+7 STL	X+4	P6 TOO LOW
25331	0	77400	4	00000	629	AZBR	AXT	**0,4	
25332	0	77400	1	00000	630		+1 AXT	**0,1	
25333	0	02000	4	00003	631		+2 TRA	3,4	
25334	0	50000	0	32621	632	AZB8	CLA	P+3	
25335	-0	12000	0	25341	633		+1 TMI	AZB9	
25336	-1	25345	0	25417	634		+2 STR	AZFF,,AZB7	
25337	0	52200	0	25331	635	AZB12	XEC	AZBR	
25340	1	00002	4	25332	636		+1 TXI	AZBR+1,4,2	
25341	0	52200	0	25331	637	AZB9	XEC	AZBR	
25342	1	00001	4	25332	638		+1 TXI	AZBR+1,4,1	NEG PRESSURE
25343	-1	43573	0	25421	639	AZB11	STR	AZF,,BUG1	
25344	0	02000	0	25310	640		+1 TRA	AZB5	
25345	3	02521	6	36063	641	AZB7	BCI	3,HEAT TRANSFR ERROR	

644\*REGION TO COMPUTE SOME CONSTANTS

25353	0	63400	4	25377	645	AZC	SXA	AZCR,4	
25354	0	50000	0	32616	646		+1 CLA	P	Z
25355	0	07400	4	42437	647		+2 TSX	LINT,4	
25356	0	00000	1	34567	648		+3 PZE	WAF,1	
25357	0	60100	0	33757	649		+4 STO	TP+18	AF
25360	0	50000	0	32616	650		+5 CLA	P	
25361	0	07400	4	42437	651		+6 TSX	LINT,4	
25362	0	00000	1	34625	652		+7 PZE	WFP,1	
25363	0	60100	0	33760	653		+8 STO	TP+19	FP

654\*PIPE OPTION BRANCHES OUT HERE TO AZC1

25364	0	52000	1	36071	655		+9 ZET	DPX,1	NOT 0=PIPE OPTION
25365	0	02000	0	25401	656		+10 TRA	AZC2	
25366	0	50000	0	40213	657		+11 CLA	FL1	
25367	0	30200	1	36067	658		+12 FSB	DVF,1	
25370	0	24100	1	36067	659		+13 FDP	DVF,1	
25371	0	26000	1	36064	660		+14 FMP	DELZ,1	
25372	0	24100	1	35625	661		+15 FDP	PT+11,1	
25373	0	26000	0	33757	662		+16 FMP	TP+18	
25374	0	60100	0	33765	663	AZC1	STO	TP+24	
25375	0	24100	0	32631	664		+1 FDP	P+11	
25376	-0	60000	0	33771	665		+2 STQ	TP+28	
25377	0	77400	4	00000	666	AZCR	AXT	**0,4	
25400	0	02000	4	00001	667		+1 TRA	1,4	
25401	0	50000	0	33757	668	AZC2	CLA	TP+18	AF -- PIPE OPTION
25402	0	24100	0	40275	669		+1 FDP	PI	
25403	0	26000	0	40216	670		+2 FMP	FL4	
25404	0	07400	4	24364	671		+3 TSX	SQRT,4	
25405	0	07400	4	42602	672		+4 TSX	ERROR,4	
25406	0	60100	0	33735	673		+5 STO	TP	DI
25407	0	30200	1	36071	674		+6 FSB	DPX,1	
25410	0	24100	1	35625	675		+7 FDP	PT+11,1	DELT
25411	0	26000	1	36071	676		+8 FMP	DPX,1	
25412	0	13100	0	00000	677		+9 XCA		
25413	0	26000	0	40275	678		+10 FMP	PI	
25414	0	13100	0	00000	679		+11 XCA		
25415	0	26000	1	36064	680		+12 FMP	DELZ,1	
25416	0	02000	0	25374	681		+13 TRA	AZC1	

683\*REGION TO PRINT ERROR MESSAGES

25417	-0	50000	0	25437	684	AZFF	CAL	AZF2	PRINT AND FLUSH
25420	0	02000	0	25422	685		+1 TRA	**2	

687\*PRINT MESSAGE AND RETURN

25421	-0	50000	0	00000	688	AZF	CAL	0	PRINT AND RETURN
25422	0	60000	0	25432	689		+1 STZ	AZF1+1	
25423	0	62100	0	25436	690	AZF3	STA	AZFR+1	
25424	0	63400	4	25435	691		+1 SXA	AZFR,4	
25425	-0	50060	0	00046	692		+2 CAL*	KICSTR	

25430	0	07400	4	00052	695	+5	TSX	DOU,4
25431	3	06000	0	00000	696	AZFL	PTH	000,,3072
25432	0	00000	0	00000	697	+1	PZE	000
25433	-1	00012	0	00012	698	+2	FVE	10,,10
25434	0	07401	4	32941	699	+3	TSX	PL,4,1
25435	0	07400	4	00000	700	AZFR	AXT	000,4
25436	0	02000	0	00000	701	+1	TRA	000
25437	0	00000	0	42602	702	AZF2	PZE	ERROR

25440	-0	50000	0	25444	704	AZFT	CAL	AZFT1
25441	0	60200	0	25432	706	+1	SLW	AZFL+1
25442	-0	50000	0	00000	707	+2	CAL	0
25443	0	02000	0	25423	708	+3	TRA	AZF3
25444	-2	13702	0	32630	709	AZFT1	SIX	P+10,,6002

25445	0	63400	4	25560	712	AZG	SXA	AZGR,4
25446	0	50000	2	34101	713	+1	CLA	AZ02,2
25447	0	30000	2	34102	714	+2	FAO	AZ02+1,2
25450	C	24100	0	40214	715	+3	FDP	FL2
25451	-0	60000	0	32631	716	+4	STQ	P+11
25452	0	07400	4	25353	717	+5	TSX	AZC,4
25453	0	50000	2	34163	718	+6	CLA	AZ03,2
25454	0	30000	2	34164	719	+7	FAD	AZ03+1,2
25455	C	24100	0	40214	720	+8	FDP	FL2
25456	-0	60000	0	32620	721	+9	STQ	P+2
25457	0	50000	2	34245	722	+10	CLA	AZ04,2
25460	0	30000	2	34246	723	+11	FAD	AZ04+1,2
25461	0	24100	0	40214	724	+12	FDP	FL2
25462	-0	60000	0	32621	725	+13	STQ	P+3
25463	0	50000	2	34473	726	+14	CLA	AZ09,2
25464	0	30000	2	34474	727	+15	FAD	AZ09+1,2
25465	0	24100	0	40214	728	+16	FDP	FL2
25466	-0	60000	0	33731	729	+17	STQ	WPR+7
25467	0	50000	2	35637	730	+18	CLA	AZ01+1,2
25470	0	07400	4	42437	731	+19	TSX	LINT,4
25471	C	00000	1	35367	732	+20	PZE	WCR,1
25472	0	13100	0	00000	733	+21	XCA	
25473	0	26000	1	36070	734	+22	FMP	DRHOR,1
25474	0	60100	0	33776	735	+23	STO	TP+33
25475	0	50000	2	35637	736	+24	CLA	AZ01+1,2
25476	0	07400	4	42437	737	+25	TSX	LINT,4
25477	0	00000	1	35144	738	+26	PZE	WK,1
25500	0	60100	0	33761	739	+27	STO	TP+20
25501	0	50000	0	33736	740	+28	CLA	TP+1
25502	0	07400	4	42437	741	+29	TSX	LINT,4
25503	0	00000	1	34721	742	+30	PZE	WHT,1
25504	0	60100	0	34075	743	+31	STO	TP+96
25505	0	50000	0	32616	744	+32	CLA	P
25506	0	07400	4	42437	745	+33	TSX	LINT,4
25507	C	00000	1	34663	746	+34	PZE	WH,1
25508	0	00000	0	00000	747	+35		

25511	C	26000	0	34075	748	+36	FMP	TP+96	FRACTION OF HEAT GEN COEFF
25512	0	60100	0	33777	749	+37	STO	TP+34	H
25513	0	50000	2	34327	750	+38	CLA	AZ05,2	
25514	0	60100	0	32622	751	+39	STO	P+4	
25515	0	07400	4	31545	752	+40	TSX	AYN,4	
25516	0	50000	0	33776	753	+41	CLA	TP+33	RHO C R
25517	0	24100	0	33731	754	+42	FDP	WPR+7	C P
25520	0	26000	0	33771	755	+43	FMP	TP+28	
25521	0	60100	0	32624	756	+44	STO	P+6	
25522	0	34000	0	32627	757	+45	CAS	P+9	H
25523	0	02000	0	25526	758	+46	TRA	**3	
25524	0	02000	0	25526	759	+47	TRA	**2	
25525	0	02000	0	25562	760	+48	TRA	AZG1	
25526	0	50000	0	33761	761	+49	CLA	TP+20	K
25527	0	24100	0	33776	762	+50	FDP	TP+33	
25530	0	26000	1	35625	763	+51	FMP	PT+11,1	DELT
25531	0	24100	1	36064	764	+52	FDP	DELZ,1	
25532	0	13100	0	00000	765	+53	XCA		
25533	0	24100	1	36064	766	+54	FDP	DELZ,1	
25534	0	13100	0	00000	767	+55	XCA		
25535	0	24100	0	40214	768	+56	FDP	FL2	
25536	-0	60000	0	32625	769	+57	STQ	P+7	S/2
25537	0	50000	0	33777	770	+58	CLA	TP+34	H
25540	0	24100	0	33776	771	+59	FDP	TP+33	
25541	0	26000	1	35625	772	+60	FMP	PT+11,1	
25542	0	60100	0	32626	773	+61	STO	P+8	
25543	0	50200	0	33746	774	+62	CLS	TP+9	
25544	0	24100	0	33745	775	+63	FDP	TP+8	
25545	0	13100	0	00000	776	+64	XCA		
25546	0	30000	0	40213	777	+65	FAD	FL1	
25547	0	24100	0	32624	778	+66	FDP	P+6	
25550	-0	60000	0	33747	779	+67	STQ	TP+10	
25551	0	50200	0	40214	780	+68	CLS	FL2	
25552	0	24100	0	33745	781	+69	FDP	TP+8	
25553	0	13100	0	00000	782	+70	XCA		
25554	0	24100	0	32624	783	+71	FDP	P+6	
25555	0	13100	0	00000	784	+72	XCA		
25556	0	30000	0	40213	785	+73	FAD	FL1	
25557	0	60100	0	33744	786	+74	STO	TP+7	
25560	0	07400	4	00000	787		AZGR	AXT	**0,4
25561	0	02000	4	00002	788	+1	TRA	2,4	
25562	0	52200	0	25560	789		AZG1	XEC	AZGR
25563	0	02000	4	00001	790	+1	TRA	1,4	

25564	0	63400	4	25625	793	AZH	SXA	AZHR,4	792*REGION TO COMPUTE PARA HYDROGEN PROPERTIES, TEMP IN AC, PRESS IN MQ
25565	-0	12000	4	00001	794	+1	TMI	1,4	
25566	0	16200	0	25571	795	+2	TQP	AZH2	
25567	0	52200	0	25625	796	AZH3	XEC	AZHR	
25570	0	02000	4	00001	797	+1	TRA	1,4	

25574	0	02000	0	25602	801	+3	TRA	AZM4	
25575	0	13100	0	00000	802	+4	XCA		
25576	0	34000	0	33722	803	+5	CAS	WPR	
25577	0	02000	0	25601	804	+6	TRA	**2	
25600	0	02000	0	25625	805	+7	TRA	AZMR	SAME PRESSURE
25601	0	13100	0	00000	806	+8	XCA		
25602	0	77400	4	00012	807		AZM4	AXT	10.4
25603	0	60000	4	33734	808	+1	STZ	WPR+10.4	
25604	2	00001	4	25603	809	+2	TIX	*-1.4.1	
25605	0	60100	0	33727	810	+3	STQ	WPR+5	TEMP
25606	-0	60000	0	33722	811	+4	STQ	WPR	PRESS
25607	0	07400	4	32022	812	+5	TSX	PRP.4	
25610	0	02000	0	25567	813	+6	TRA	AZM3	
25611	0	56000	0	33723	814	+7	LDQ	WPR+1	SP VOL FT**3/LB
25612	0	26000	0	40245	815	+8	FMP	FLCUP	IN3/FT3
25613	0	60100	0	33723	816	+9	STQ	WPR+1	IN**3/LB
25614	0	50000	0	25627	817	+10	CLA	AZM1	
25615	0	56000	0	33727	818	+11	LDQ	WPR+5	
25616	0	04000	0	25625	819	+12	TLQ	AZMR	
25617	0	50000	0	25630	820	+13	CLA	AZM1+1	
25620	0	04000	0	25622	821	+14	TLQ	**2	
25621	0	02000	0	25625	822	+15	TRA	AZMR	
25622	0	26000	0	25631	823	+16	FMP	AZM1+2	
25623	0	30000	0	25632	824	+17	FAD	AZM1+3	
25624	0	60100	0	33731	825	+18	STQ	WPR+7	
25625	0	77400	4	00000	826		AZMR	AXT	**0.4
25626	0	02000	4	00002	827	+1	TRA		2.4
25627	2	10550	0	00000	828		AZM1		
25630	2	11404	0	00000	829	+1			
25631	1	71763	5	54427	830	+2			
25632	2	01755	3	41217	831	+3			

833\*REGION TO ITERATE ON FLOW RATE FOR MULTIPLE PART CASE AT ONE TIME PT.

25633	0	63400	4	25705	834		AZ1	SXA	AZIR.4	
25634	0	50000	0	40305	835	+1	CLA		BIG	
25635	0	60100	0	40471	836	+2	STQ	NEWA9		
25636	0	60000	0	40472	837	+3	STZ	NEWA9+1		
25637	0	50000	0	32644	838	+4	CLA	P+22		
25640	0	60100	0	47403	839	+5	STQ	PR+50		INITIAL WDOTC GUESS
25641	0	50000	0	36120	840	+6	CLA	DWRE		WDOTR CLOSURE
25642	0	07400	4	40407	841	+7	TSX	NEWA.4		
25643	0	47406	0	32643	842	+8	PZE	P+21.,PR+53		
25644	0	00024	0	32631	843	+9	PZE	P+11.,NHIT		
25645	0	02000	0	25723	844	+10	TRA	AZ13		NIT CONVERGED
25646	0	50000	0	47403	845	+11	CLA	PR+50		
25647	0	60100	0	32644	846	+12	STQ	P+22		WDOTC= VALUE OBTAINED BY HOT BLEED P
25648	0	50000	0	32655	847	+13	CLA	P+31		
25651	0	60100	0	32620	848	+14	STQ	P+2		T2
25652	0	50000	0	32654	849	+15	CLA	P+30		
25653	0	60100	0	32621	850	+16	STQ	P+3		P2
25654	0	50000	0	32643	851	+17	CLA	P+21		
25655	0	60100	0	32631	852	+18	STQ	P+11		WDOTR=WDOTP
25656	0	00000	0	32666	853					WEATNSR 2 TAIN

25657	0	02000	0	25707	854	+20	TRA	AZ11		NEG FLOW
25660	0	02000	0	25715	855	+21	TRA	AZ12		NEG PRESS
25661	0	52000	0	32742	856	+22	ZET	X+20		
25662	0	02000	0	25732	857	+23	TRA	AZ14		P11, T11 GIVEN- SKIP HOT BLEED PORT
25663	0	07400	4	44757	858	+24	TSX	H8.4		HOT BLEED PORT PROGRAM
25664	0	02000	0	25732	859	+25	TRA	AZ14		WDOTR NEG, TREAT AS ZERO THIS PASS
25665	0	02000	0	25746	860	+26	TRA	AZ15		NEG PRESSURE, LOWER WDOTC
25666	0	07400	4	40477	861		AZ16	TSX	RAPA.4	CLOSE
25667	0	50000	0	32644	862	+1	CLA	P+22		
25670	0	56000	0	47403	863	+2	LDQ	PR+50		
25671	-0	60000	0	32644	864	+3	STQ	P+22		
25672	0	30200	0	47403	865	+4	FSB	PR+50		
25673	0	24100	0	47403	866	+5	FDP	PR+50		
25674	0	76000	0	00012	867	+6	DCT			
25675	0	07400	4	42602	868	+7	TSX	ERROR.4		WDOTC IN HBP=0
25676	0	13100	0	00000	869	+8	XCA			
25677	-0	34000	0	36117	870	+9	LAS	DWCE		
25700	0	02000	0	40427	871	+10	TRA	NEWA2+1		NOT CONVERGED TRY AGAIN WITH SAME WP
25701	0	02000	0	25702	872	+11	TRA	**1		
25702	0	52200	0	40427	873		AZ17	XEC	NEWA2+1	
25703	1	77754	4	25704	874	+1	TX1	**1.4.,-NHIT		
25704	0	63600	4	32732	875	+2	SCA	X+12.4		NO. ITERATIONS
25705	0	77400	4	00000	876		AZ1R	AXT	**0.4	
25706	0	02000	4	00001	877	+1	TRA		1.4	EXIT
878*NEGATIVE FLOW RATE- WDOTP TOO SMALL										
25707	-0	52000	0	32744	879		AZ11	NZT	X+22	
25710	0	02000	0	40466	880	+1	TRA	BDNA		
25711	0	50000	0	32643	881	+2	CLA	P+21		IF WDOTC HAS BEEN REMOVED LOWER
25712	0	30200	0	32644	882	+3	FSB	P+22		MINIMUM BY WDOTC
25713	0	60100	0	32643	883	+4	STQ	P+21		
25714	0	02000	0	40466	884	+5	TRA	BDNA		
885*NEGATIVE PRESSURE- WDOTP TOO BIG										
25715	-0	52000	0	32744	886		AZ12	NZT	X+22	
25716	0	02000	0	40463	887	+1	TRA	BDXA		
25717	0	50000	0	32643	888	+2	CLA	P+21		IF DILUENT HAS BEEN REMOVED RAISE
25720	0	30000	0	32644	889	+3	FAD	P+22		NEW MAXIMUM BY WDOTC
25721	0	60100	0	32643	890	+4	STQ	P+21		
25722	0	02000	0	40463	891	+5	TRA	BDXA		
892*NOT CONVERGED										
25723	-1	25727	0	25440	893		AZ13	STR	AZFT.,AZ101	
25724	0	77400	4	00024	894	+1	AXT	NHIT.4		
25725	0	63400	4	32732	895	+2	SXA	X+12.4		
25726	0	02000	0	25705	896	+3	TRA	AZ1R		
25727	-2	65173	6	06623	897		AZ101	BCI	3,HR, WC NOT CLOSED	
898*P11, T11 GIVEN- WDOTC =0, HOT BLEED PORT CLOSED										
25732	0	50000	0	32620	899		AZ14	CLA	P+2	
25733	0	07400	4	24364	900	+1	TSX	SQRT.4		
25734	0	07400	4	42602	901	+2	TSX	ERROR.4		
25735	0	60100	0	12512	902	+3	STQ	COMMON		ROOT T6
25736	0	56000	0	36122	903	+4	LDQ	DASTR		
25737	0	26000	0	32621	904	+5	FMP	P+3		P6
25740	0	24100	0	12512	905	+6	FDP	COMMON		
25741	0	76000	0	40241	906	+7	FMP	FL139		



25743	0	60100	0	34007	908	+9	STO	TP+42	WOOTN CHOKE
25744	0	07400	4	40477	909	+10	TSX	RAPA,4	
25745	0	02000	0	25702	910	+11	TRA	AZ17	
25746	0	50000	0	32644	911	NEG	PRESSURE IN HOT BLEED PORT, LOWER WOOTC		WOOTC= .5 WOOTC
25747	0	24100	0	40214	912	AZ15	CLA	P+22	NEW
25750	-0	60000	0	32644	913	+1	FDP	FL2	
25751	0	02000	0	40427	914	+2	STO	P+22	
					915	+3	TRA	NEWA2+1	

917\*REGION TO COMPUTE MAIN ENGINE METAL TEMPS

25752	0	63400	4	26057	918	AZJ	SXA	AZJR,4	
25753	0	63400	1	26060	919	+1	SXA	AZJR+1,1	
25754	0	63400	2	26061	920	+2	SXA	AZJR+2,2	
25755	0	63400	3	26062	921	+3	SXA	AZJR+3,3	
25756	0	63400	5	26063	922	+4	SXA	AZJR+4,5	
25757	-0	77400	1	15061	923	+5	AXC	AZMTG,1	
25760	0	60000	1	34561	924	AZJ8	STZ	FX+4,1	TEMP EXCEEDED MAX FLAG
25761	0	50000	1	34562	925	+1	CLA	FX+5,1	NO. TIME STEPS
25762	0	73400	5	00000	926	+2	PAX	,5	
25763	0	50000	0	32630	927	+3	CLA	P+10	
25764	0	60100	0	33736	928	+4	STO	TP+1	TIME
25765	0	77400	3	00000	929	AZJ7	AXT	0,3	
25766	0	75400	1	00000	930	+1	PXA	,1	
25767	0	73400	2	00000	931	+2	PAX	,2	
25770	0	50000	1	34556	932	+3	CLA	FX+1,1	NO. Z STEPS
25771	0	73700	4	00000	933	+4	PAC	,4	
25772	-0	63400	4	26030	934	+5	SKD	AZJ4,4	
25773	-0	63400	4	26044	935	+6	SKD	AZJ5,4	
25774	0	50000	1	36064	936	+7	CLA	DELZ,1	
25775	0	24100	0	40214	937	+8	FDP	FL2	
25776	0	13100	0	00000	938	+9	XCA		
25777	0	60100	0	32616	939	AZJ3	STO	P	Z
26000	0	07400	4	25445	940	+1	TSX	AZG,4	M,N FOR THIS NODE
26001	0	02000	0	26065	941	+2	TRA	AZJ2	N TOO SMALL, HALVE DELT
26002	0	50000	2	35640	942	+3	CLA	AZ01+2,2	
26003	0	30000	2	35636	943	+4	FAD	AZ01,2	
26004	0	30200	2	35637	944	+5	FSB	AZ01+1,2	
26005	0	30200	2	35637	945	+6	FSB	AZ01+1,2	
26006	0	13100	0	00000	946	+7	XCA		
26007	0	26000	0	32625	947	+8	FMP	P+7	S/2
26010	0	60100	0	12512	948	+9	STO	COMMON	
26011	0	56000	2	35637	949	+10	LDQ	AZ01+1,2	
26012	0	26000	0	33744	950	+11	FMP	TP+7	
26013	0	60100	0	12513	951	+12	STO	COMMON+1	
26014	0	56000	2	34163	952	+13	LDQ	AZ03,2	T M,N
26015	0	26000	0	13747	953	+14	FMP	TP+10	
26016	0	30000	0	12512	954	+15	FAD	COMMON	
26017	0	30000	0	12513	955	+16	FAD	COMMON+1	
26020	0	30000	0	32626	956	+17	FAD	P+8	U
26021	0	56000	0	36105	957	+18	LDQ	DTMAX	
26022	0	04000	0	26100	958	+19	TLQ	AZJ12	
26023	0	60100	3	26106	959	AZJ13	STO	AZJ1,3	

26025	0	30000	1	36064	961	+2	FAD	DELZ,1	
26026	1	77777	2	26027	962	+3	TXI	**+1,2,-1	
26027	1	77777	3	26030	963	+4	TXI	**+1,3,-1	
26030	3	00000	3	25777	964	AZJ4	TXH	AZJ3,3,**0	
26031	0	77400	3	00000	965	+1	AXT	0,3	
26032	0	75400	1	00000	966	+2	PXA	,1	
26033	0	73400	2	00000	967	+3	PAX	,2	
26034	0	50000	0	26106	968	+4	CLA	AZJ1	
26035	0	36100	0	40301	969	+5	ACL	188	
26036	0	30200	0	26107	970	+6	FSB	AZJ1+1	
26037	0	60100	2	35636	971	+7	STO	AZ01,2	LOWER EXTREME THETA = NEXT NODE
26040	0	50000	3	26106	972	AZJ6	CLA	AZJ1,3	
26041	0	60100	2	35637	973	+1	STO	AZ01+1,2	
26042	1	77777	2	26043	974	+2	TXI	**+1,2,-1	
26043	1	77777	3	26044	975	+3	TXI	**+1,3,-1	
26044	3	00000	3	26040	976	AZJ5	TXH	AZJ6,3,**0	
26045	0	50000	2	35636	977	+1	CLA	AZ01,2	
26046	0	30000	2	35636	978	+2	FAD	AZ01,2	
26047	0	30200	2	35635	979	+3	FSB	AZ01-1,2	UPPER EXTREME THETA BY LINEAR EXTRAF
26050	0	60100	2	35637	980	+4	STO	AZ01+1,2	
26051	0	50000	0	33736	981	+5	CLA	TP+1	
26052	0	30000	1	35625	982	+6	FAD	PT+11,1	
26053	0	60100	0	33736	983	+7	STO	TP+1	
26054	2	00001	5	25765	984	+8	TXI	AZJ7,5,1	
26055	1	76003	1	26056	985	+9	TXI	**+1,1,-AZHTS	
26056	3	00000	1	25760	986	AZJ9	TXH	AZJ8,1,**0	
26057	0	77400	4	00000	987	AZJR	AXT	**0,4	
26060	0	77400	1	00000	988	+1	AXT	**0,1	
26061	0	77400	2	00000	989	+2	AXT	**0,2	
26062	0	77400	3	00000	990	+3	AXT	**0,3	
26063	0	77400	5	00000	991	+4	AXT	**0,5	
26064	0	02000	4	00001	992	+5	TRA	1,4	
26065	0	50000	1	35625	993	AZJ2	CLA	PT+11,1	DELT
26066	0	24100	0	40214	994	+1	FDP	FL2	
26067	-0	60000	1	35625	995	+2	STO	PT+11,1	
26070	0	50000	0	36102	996	+3	CLA	DMDT	
26071	0	04000	0	26102	997	+4	TLQ	AZJ10	DELT T TOO SMALL
26072	0	75400	5	00000	998	+5	PXA	,5	
26073	0	56000	1	34562	999	+6	LDQ	FX+5,1	
26074	0	76300	0	00001	1000	+7	LLS	1	
26075	0	73400	5	00000	1001	+8	PAX	,5	
26076	-0	60000	1	34562	1002	+9	STO	FX+5,1	
26077	0	02000	0	25765	1003	+10	TRA	AZJ7	
26100	-0	62500	1	34561	1004	AZJ12	STL	FX+4,1	
26101	0	02000	0	26023	1005	+1	TRA	AZJ13	
26102	-1	26103	0	25417	1006	AZJ10	STR	AZFF,,AZJ11	
26103	2	42543	6	32160	1007	AZJ11	BCI	3,DELTA T TOO SMALL	
				26106	1008	AZJ1	BSS	NZMAX,F	

1010\*REGION TO MOVE METAL TEMPS FROM TEMPORARY TO PERMANENT STORAGE

26170	0	63400	4	26220	1011	AZK	SXA	AZKR,4	
26171	0	63400	2	26221	1012	+1	SXA	AZKR+1,2	
26172	0	77400	4	42717	1013	+2	AXT	AZMR-AZMT,4	REFERENCE TO PART STORAGE

26173 0 63400 4 26215  
 26174 0 50000 4 34556  
 26175 0 73400 2 00000  
 26176 1 00001 2 26177  
 26177 0 50000 4 35621  
 26200 0 60100 4 35620  
 26201 0 50000 4 35623  
 26202 0 60100 4 35622  
 26203 0 50200 4 35630  
 26204 0 60100 4 35626  
 26205 0 50200 4 35631  
 26206 0 60100 4 35627  
 26207 0 50000 4 34101  
 26210 0 60100 4 34002  
 26211 0 50000 4 34411  
 26212 0 60100 4 35720  
 26213 1 77777 4 26214  
 26214 2 00001 2 26207  
 26215 0 77400 4 00000  
 26216 1 76003 4 26217  
 26217 3 00000 4 26173  
 26220 0 77400 4 00000  
 26221 0 77400 2 00000  
 26222 0 02000 4 00001

1014 AZK3 SXA AZK1,4  
 1015 +1 CLA FX+1,4  
 1016 +2 PAX ,2  
 1017 +3 TXI \*\*1,2,1  
 1018 +4 CLA PT+7,4  
 1019 +5 STO PT+6,4  
 1020 +6 CLA PT+9,4  
 1021 +7 STO PT+8,4  
 1022 +8 CLS PT+14,4  
 1023 +9 STO PT+12,4  
 1024 +10 CLS PT+15,4  
 1025 +11 STO PT+13,4  
 1026 AZK2 CLA AZ02,4  
 1027 +1 STO AZ08,4  
 1028 +2 CLA AZ07,4  
 1029 +3 STO AZ06,4  
 1030 +4 TXI \*\*1,4,-1  
 1031 +5 TIX AZK2,2,1  
 1032 AZK1 AXT \*\*0,4  
 1033 +1 TXI \*\*1,4,-AZMTS  
 1034 AZK4 TXM AZK3,4,\*\*\*  
 1035 AZKR AXT \*\*0,4  
 1036 +1 AXT \*\*0,2  
 1037 +2 TRA 1,4

NO. DELZ POINTS

TEMPORARY  
PERMANENT

PRESET TO MAX STOR+1+AZMTB-AZMT

26223 0 63400 4 26245  
 26224 0 50000 0 33731  
 26225 0 24100 0 33732  
 26226 0 26000 0 33733  
 26227 0 56000 0 40224  
 26230 0 07400 4 27021  
 26231 0 60100 0 12524  
 26232 0 50000 0 40216  
 26233 0 24100 0 40275  
 26234 0 13100 0 00000  
 26235 0 24100 0 33733  
 26236 0 13100 0 00000  
 26237 0 56000 0 40256  
 26240 0 07400 4 27021  
 26241 0 13100 0 00000  
 26242 0 26000 0 33732  
 26243 0 13100 0 00000  
 26244 0 26000 0 12524  
 26245 0 77400 4 00000  
 26246 0 02000 4 00001

1039\*REGION TO COMPUTE HEAT TRANSFER COEFFICIENT,L  
 1040 AZL SXA AZLR,4  
 1041 +1 CLA WPR+7 C P  
 1042 +2 FDP WPR+8 K  
 1043 +3 FMP WPR+9  
 1044 +4 LDQ FL,4  
 1045 +5 TSX AZE,4  
 1046 +6 STO COMMON+10  
 1047 +7 CLA FL4  
 1048 +8 FDP PI  
 1049 +9 XCA  
 1050 +10 FDP WPR+9  
 1051 +11 XCA  
 1052 +12 LDQ FL,8  
 1053 +13 TSX AZE,4  
 1054 +14 XCA  
 1055 +15 FMP WPR+8 K  
 1056 +16 XCA  
 1057 +17 FMP COMMON+10  
 1058 AZLR AXT \*\*0,4  
 1059 +1 TRA 1,4

26247 0 63400 4 26264  
 26250 0 50000 0 32633  
 26251 0 63400 4 26264

1061\*NOZZLE TUBE ROUTINES  
 1062\*NOZZLE TUBE INITIALIZATION REGION  
 1063 AZNI SXA AZNIR,4  
 1064 +1 CLA P+13 T6  
 1065 +2 7

26252 0 07400 4 42602  
 26253 0 60100 0 32634  
 26254 C 50000 0 36111  
 26255 -C 10000 0 26261  
 26256 0 50000 0 36077  
 26257 0 07400 4 42437  
 26260 0 00000 0 33441  
 26261 0 60100 0 32656  
 26262 0 50000 0 36126  
 26263 0 60100 0 32641  
 26264 0 77400 4 00000  
 26265 0 02000 4 00001

1066 +3 TSX ERROR,4  
 1067 +4 STO P+14  
 1068 +5 CLA DPO  
 1069 +6 TNZ AZN11  
 1070 +7 CLA DTMI  
 1071 +8 TSX LINT,4  
 1072 +9 PZE WPD  
 1073 AZN11 STO P+32  
 1074 +1 CLA DQINT  
 1075 +2 STO QINT  
 1076 AZNIR AXT \*\*0,4  
 1077 +1 TRA 1,4

BAD THETA 0

26266 0 63400 4 26321  
 26267 0 50000 0 44463  
 26270 0 30200 0 44233  
 26271 0 60100 0 33743  
 26272 0 50000 0 44442  
 26273 0 30200 0 44443  
 26274 0 24100 0 44461  
 26275 0 26000 0 33743  
 26276 0 30000 0 44442  
 26277 0 60100 0 33752  
 26300 0 50000 0 44444  
 26301 0 30200 0 44445  
 26302 0 24100 0 44461  
 26303 0 26000 0 33743  
 26304 0 30000 0 44444  
 26305 0 56000 0 26323  
 26306 0 60000 0 32737  
 26307 0 04000 0 26311  
 26310 -0 62500 0 32737  
 26311 0 07400 4 24364  
 26312 0 07400 4 42602  
 26313 C 60100 0 33756  
 26314 0 56000 0 44234  
 26315 0 26000 0 33752  
 26316 0 24100 0 33756  
 26317 0 26000 0 40241  
 26320 0 60100 0 32651  
 26321 0 77400 4 00000  
 26322 0 02000 4 00001  
 26323 2 06740 0 00000

1079\*REGION TO COMPUTE CRITICAL FLOW IN NOZZLE TUBES  
 1080 AZNW SXA AZNWR,4  
 1081 +1 CLA AZN2  
 1082 +2 FSB AZN3  
 1083 +3 STO TP+6 Z  
 1084 +4 CLA PSUBC P1  
 1085 +5 FSB PSUBC+1 P2  
 1086 +6 FDP DELTAZ  
 1087 +7 FMP TP+6 Z-21  
 1088 +8 FAD PSUBC P1  
 1089 +9 STO TP+13  
 1090 +10 CLA TSUBC T1  
 1091 +11 FSB TSUBC+1 T2  
 1092 +12 FDP DELTAZ  
 1093 +13 FMP TP+6  
 1094 +14 FAD TSUBC T1  
 1095 +15 LDQ AZNW1 H2 CRITICAL TEMP  
 1096 +16 STZ X+17  
 1097 +17 TLQ AZNW2 H2 GAS  
 1098 +18 STL X+17 FLAG TO IGNORE NOZZLE TUBE CHOKE  
 1099 AZNW2 TSX SORT,4  
 1100 +1 TSX ERROR,4  
 1101 +2 STO TP+17  
 1102 +3 LDQ AZNW+1  
 1103 +4 FMP TP+13  
 1104 +5 FDP TP+17  
 1105 +6 FMP FL139  
 1106 +7 STO P+27 .1396  
 1107 AZNWR AXT \*\*0,4  
 1108 +1 TRA 1,4  
 1109 AZNW1 DEC 60.

AREA OF NOZZLE TUBE THROAT

26324 0 52000 0 32727  
 26325 0 02000 4 00001  
 26326 0 63400 4 26355  
 26327 0 07412 4 32541  
 26330 0 07400 4 00052  
 26331 3 02033 0 26372

1111\*PRINT REGIONS  
 1112\*REGION TO PRINT INLET CONDITIONS  
 1113 AZPC ZET X+9  
 1114 +1 TRA 1,4  
 1115 +2 SXA AZPCR,4  
 1116 +3 TSX PL,4,10  
 1117 +4 TSX DOUT,4  
 1118 +5 PTH AZPC3,,1051

26332	0	11616	0	00000	1119	+6	PZE	0.,5006
26333	-1	47064	0	00012	1120	+7	FVE	KPRINT,,20020
26334	0	07400	0	00052	1121	+8	TSX	DOUT,4
26335	3	05772	0	26357	1122	+9	PTM	AZPCL,,3066
26336	3	02064	0	26455	1123	+10	PTM	AZPS1*2,,1078
26337	-2	13672	0	32630	1124	+11	SIX	P*10,,6074
26340	-1	00024	0	00012	1125	+12	FVE	10,,20
26341	0	07400	0	00052	1126	+13	TSX	DOUT,4
26342	3	01765	0	26367	1127	+14	PTM	AZPC2,,1013
26343	0	13545	0	00001	1128	+15	PZE	1,,7013
26344	-1	00012	0	00012	1129	+16	FVE	10,,10
26345	0	07400	0	00052	1130	+17	TSX	DOUT,4
26346	-2	13576	0	32632	1131	+18	SIX	P*28,,6014
26347	0	05705	0	00001	1132	+19	PZE	1,,3013
26350	-2	13662	0	32665	1133	+20	SIX	P*39,,6066
26351	-2	13677	0	32657	1134	+21	SIX	P*35,,6079
26352	-2	13714	0	32676	1135	+22	SIX	P*48,,6092
26353	-2	13731	0	32637	1136	+23	SIX	P*17,,6105
26354	-1	47052	0	00012	1137	+24	FVE	KPRINT,,20010
26355	0	77400	0	00000	1138		AZPCR	AXT
26356	0	02000	0	00001	1139	+1	TRA	1,4
26357	3	14543	2	56360	1140		AZPCL	BCI
26362	-2	04760	0	10660	1141		AZPC2	BCI
26372	-1	45454	5	45454	1142		AZPC3	BCI

1144 REGION TO PRINT INLET AND OUTLET PRESSURE DROPS										
26373	0	63400	4	26424	1145		AZPD	SXA	AZPDR,4	
26374	0	44100	4	00000	1146	+1	LDI		0,4	
26375	-0	05700	7	77774	1147	+2	RIL		777774	
26376	0	60400	0	00001	1148	+3	STI		KINDX4	
26377	0	07400	0	00052	1149	+4	TSX		DOUT,4	
26400	3	01772	1	34555	1150	+5	PTM		FX,1,1018	PART NAME
26401	3	02001	4	26430	1151	+6	PTM	AZPD1*2,4,1025		IN OR OUT
26402	3	05744	0	26430	1152	+7	PTM	AZPD2,,3044		
26403	3	05773	0	26435	1153	+8	PTM	AZPD4,,3067		
26404	3	02071	0	26435	1154	+9	PTM	AZPD4,,1081		
26405	3	04056	0	26456	1155	+10	PTM	AZP53,,2094		
26406	3	04104	0	26444	1156	+11	PTM	AZPD7,,2116		
26407	3	02154	0	26444	1157	+12	PTM	AZPD7*2,,1132		
26410	1	13674	4	26442	1158	+13	POM	AZPD5*2,4,6076		
26411	1	13642	4	26435	1159	+14	POM	AZPD3*2,4,6050		DROP
26412	1	13727	4	26451	1160	+15	POM	AZPD8*2,4,6103		FLOW
26413	1	13755	4	26455	1161	+16	POM	AZPD9*2,4,6125		RHO
26414	1	00000	4	26444	1162	+17	POM	AZPD6*2,4		FVE
26415	0	07401	4	32541	1163	+18	TSX	PL,4,1		
26416	0	44100	0	00061	1164	+19	LDI	KINDX4		
26417	-0	05400	0	00001	1165	+20	LFT	1		
26420	0	02000	0	26424	1166	+21	TRA	AZPDR		
26421	0	07402	4	32541	1167	+22	TSX	PL,4,2		
26422	0	07400	4	32563	1168	+23	TSX	PC,4		
26423	-1	00012	0	00012	1169	+24	FVE	KPRINT,,10		
26424	0	77400	4	00000	1170		AZPDR	AXT	**0,4	
26425	0	02000	4	00001	1171	+1	TRA	1,4		
26426	-2	05455	5	05455	1172		AZPD	BCI	2,INLET/OUTLET	

26438	-0	75125	6	26264	1173		AZPD2	BCI	3,PRESSURE DROP=	
26433	-2	00000	1	35616	1174		AZPD3	SIX	PT*4,1	
26434	-2	00000	1	35617	1175	+1	SIX	PT*5,1		
26435	-2	06047	6	23121	1176		AZPD4	BCI	3, PSIA, PRESSURE=	
26440	-2	00000	1	35612	1177		AZPD5	SIX	PT,1	
26441	-2	00000	1	35613	1178	+1	SIX	PT*1,1		
26442	-1	00024	0	00012	1179		AZPD6	FVE	10,,20	
26443	-1	00012	0	00012	1180	+1	FVE	10,,10		
26444	-0	32261	6	22523	1181		AZPD7	BCI	3,LB/SEC RHO= LB/INS	FLOW
26447	-2	00000	1	35624	1182		AZPD8	SIX	PT*10,1	
26450	-2	00000	1	35614	1183	+1	SIX	PT*2,1		
26451	-2	00000	1	35621	1184		AZPD9	SIX	PT*7,1	RHO
26452	-2	00000	1	35623	1185	+1	SIX	PT*9,1		
26453	-2	33144	2	51360	1186		AZPS1	BCI	3,TIME=	SEC
26456	2	64346	6	64051	1187		AZPS3	BCI	2,FLOW RATE =	
26460	2	33046	4	22560	1188		AZP3	BCI	2,CHOKE FLOW=	

1190 ITERATION PRINT REGION										
26462	0	52000	0	32727	1191		AZPI	ZET	X*9	
26463	0	62000	4	00001	1192	+1	TRA	1,4		
26464	0	63400	1	26573	1193	+2	SXA	AZPIR,1		
26465	0	63400	2	26574	1194	+3	SXA	AZPIR*1,2		
26466	0	63400	4	26575	1195	+4	SXA	AZPIR*2,4		
26467	0	52000	0	36123	1196	+5	ZET	DNZFF		
26470	0	07400	4	26625	1197	+6	TSX	AZPN,4		
26471	0	77400	1	62717	1198	+7	AXT	AZMTB-AZMT,1		
26472	0	63400	1	26534	1199		AZPI3	SXA	AZPI1,1	
26473	0	07402	4	26373	1200	+1	TSX	AZPD,4,2		
26474	0	50000	1	34556	1201	+2	CLA	FX*1,1		NO. 2 POINTS THIS PART
26475	0	73400	2	00000	1202	+3	PAX	2		
26476	0	50000	1	36064	1203	+4	CLA	DELZ,1		
26477	0	60100	0	26610	1204	+5	STO	AZPI6		
26500	0	24100	0	40214	1205	+6	FDP	FL2		
26501	-0	60000	0	32616	1206	+7	STO	P		
26502	0	50000	1	35637	1207		AZPI2	CLA	AZ01*1,1	METAL TEMP
26503	0	60100	0	32617	1208	+1	STO	P*1		
26504	0	50000	1	34163	1209	+2	CLA	AZ03,1		METAL TEMP
26505	0	30000	1	34164	1210	+3	FAD	AZ03*1,1		
26506	0	24100	0	40214	1211	+4	FDP	FL2		
26507	-0	60000	0	32620	1212	+5	STO	P*2		
26510	0	50000	1	34245	1213	+6	CLA	AZ04,1		PRESSURE
26511	0	30000	1	34246	1214	+7	FAD	AZ04*1,1		
26512	0	24100	0	40214	1215	+8	FDP	FL2		
26513	-0	60000	0	32621	1216	+9	STO	P*3		
26514	0	50000	1	34327	1217	+10	CLA	AZ05,1		
26515	0	60100	0	32622	1218	+11	STO	P*4		HF
26516	0	50000	1	34411	1219	+12	CLA	AZ07,1		
26517	0	60100	0	32623	1220	+13	STO	P*5		RHO
26520	0	50000	1	34101	1221	+14	CLA	AZ02,1		
26521	0	30000	1	34102	1222	+15	FAD	AZ02*1,1		
26522	0	24100	0	40214	1223	+16	FDP	FL2		
26523	-0	60000	0	32631	1224	+17	STO	P*11		FLOW RATE
26524	0	07400	4	32442	1225	+18	TSX	PRINT,4		
26525	0	52000	0	32725	1226	+19	ZET	X*7		

26526	1	77777	2	26577	1227	+20	TXI	AZPI8,2,-1				
26527	C	50000	0	32616	1228	+21	CLA	P				
26530	0	30000	0	26610	1229	+22	FAD	AZPI6	DEL Z			
26531	0	60100	0	32616	1230	+23	STO	P				
26532	1	77777	1	26533	1231	+24	TXI	+01,1,-1				
26533	2	00001	2	26502	1232	+25	TIX	AZPI2,2,1				
26534	0	77400	1	00000	1233		AZPI1	AXT	**0,1			
26535	0	07401	4	26373	1234	+1	TSX	AZPD,4,1	OUTLET PRES DROP			
26536	0	52000	1	34560	1235	+2	ZET	FX+3,1				
26537	-1	26611	0	25421	1236	+3	STR	AZF,,AZPI7				
26540	0	52000	1	34561	1237	+4	ZET	FX+4,1				
26541	-1	26614	0	25421	1238	+5	STR	AZF,,AZPI9				
26542	1	76003	1	26543	1239	+6	TXI	+01,1,-AZMT5				
26543	3	00000	1	26472	1240		AZPI4	TRM	AZPI3,1,000			
26544	0	50000	0	32631	1241	+1	CLA	P+11	PRESET TO MAX STOR+1+D-AZMT			
26545	0	30200	0	32644	1242	+2	FSB	P+22	WDOTR			
26546	0	30200	0	32645	1243	+3	FSB	P+23	WDOTC			
26547	0	60100	0	32646	1244	+4	STO	P+24	WDOOTH			
2655C	0	30200	0	34007	1245	+5	FSB	TP+42	WDOOTN			
26551	0	24100	0	34007	1246	+6	FDP	TP+42	WDOOTNCHOKE			
26552	-0	60000	0	34024	1247	+7	STQ	TP+55				
26553	0	07400	4	00052	1248	+8	TSX	DOUT,4	ERROR			
26554	3	01772	0	26647	1249	+9	PTH	AZPN1,,1018				
26555	3	02001	0	26441	1250	+10	PTH	AZP3+1,,1025				
26556	3	02022	0	26647	1251	+11	PTH	AZPN1,,1042				
26557	3	04007	C	26460	1252	+12	PTH	AZP3,,2055				
26560	3	06017	0	26605	1253	+13	PTH	AZPI5,,3087				
26561	3	06055	0	26453	1254	+14	PTH	AZPS1,,3117				
26562	-2	13622	0	32646	1255	+15	SIX	P+24,,6034	FLOW			
26563	-2	13660	C	34007	1256	+16	SIX	TP+42,,6064	CHOKE FLOW			
26564	-0	00104	0	32732	1257	+17	FOR	X+12,,68				
26565	-3	13721	0	34024	1258	+18	SVN	TP+55,,6097	ERROR			
26566	-3	06051	0	32630	1259	+19	SVN	P+10,,3113				
26567	-1	23444	0	00012	1260	+20	FVE	10,,10020				
26570	0	07403	4	32541	1261	+21	TSX	PL,4,3				
26571	0	52000	0	32722	1262	+22	ZET	X+4				
26572	-1	25350	0	25421	1263	+23	STR	AZF,,AZB10	P6 TOO LOW			
26573	0	77400	1	00000	1264		AZPIR	AXT	**0,1			
26574	0	77400	2	00000	1265	+1	AXT	**0,2				
26575	0	77400	4	00000	1266	+2	AXT	**0,4				
26576	0	02000	4	00001	1267	+3	TRA	1,4				
									1268*PRINT ONLY INLET AND OUTLET			
26577	-3	00000	2	26534	1269		AZPI8	TXL	AZPI1,2,0			
2660C	0	50000	1	35615	1270	+1	CLA	PT+3,1	M MAX			
26601	0	60100	0	32616	1271	+2	STO	P				
26602	-0	63600	2	26604	1272	+3	SCD	**2,2				
26603	0	77400	2	00001	1273	+4	AXT	1,2				
26604	1	00000	1	26502	1274	+5	TXI	AZPI2,1,000				
26605	3	16325	5	12163	1275		AZPI5	BCI	2,ITERATIONS			
26607	2	55151	4	65113	1276	+2	BCI	1,ERROR=				
									1277	AZPI6	BSS	1,F
26611	-0	46063	4	64660	1278		AZPI7	BCI	3,M TOO SMALL			
26614	-2	32544	4	76025	1279		AZPI9	BCI	3,TEMP EXCEEDED MAX			

1281*ENTRY TO BUMP PRINT COUNTER									
26617	0	50000	0	32727	1282		AZPI8	CLA	X+9
2662C	-0	10000	0	26622	1283	+1	TNZ	**2	
26621	0	50000	0	32726	1284	+2	CLA	X+8	
26622	0	40200	0	40200	1285	+3	SUB	FX1	
26623	0	60100	0	32727	1286	+4	STO	X+9	
26624	0	02000	4	00001	1287	+5	TRA	1,4	

1289*NOZZLE TUBE PRINT									
26625	0	63400	4	26645	1290		AZPN	SXA	AZPNR,4
26626	0	07402	4	32541	1291	+1	TSX	PL,4,2	
26627	0	07400	4	00052	1292	+2	TSX	DOUT,4	
26630	3	23530	0	26647	1293	+3	PTH	AZPN1,,10072	
26631	3	02101	0	26461	1294	+4	PTH	AZP3+1,,1089	
26632	3	04100	0	26460	1295	+5	PTH	AZP3,,2112	
26633	-2	13636	0	32703	1296	+6	SIX	P+53,,6046	
26634	-2	13660	0	32702	1297	+7	SIX	P+52,,6064	
26635	-2	13701	0	32630	1298	+8	SIX	P+10,,6081	
26636	-2	13751	C	32651	1299	+9	SIX	P+27,,6121	CHOKE FLOW
26637	-2	13722	0	34063	1300	+10	SIX	TP+86,,6098	
26640	-1	00024	0	00012	1301	+11	FVE	10,,20	
26641	0	52000	0	32724	1302	+12	ZET	X+6	
26642	-1	43573	0	25421	1303	+13	STR	AZF,,BUG1	NOZZLE TUBE ERROR
26643	0	52000	0	32737	1304	+14	ZET	X+17	
26644	-1	26661	0	25421	1305	+15	STR	AZF,,AZPN2	
26645	0	77400	4	00000	1306		AZPNR	AXT	**0,4
26646	0	02000	4	00001	1307	+1	TRA	1,4	
26647	-0	54671	7	14325	1308		AZPN1	BCI	,NOZZLE TUBE INPUT TEMP=
26661	-0	33150	6	03145	1309		AZPN2	BCI	3,LIQ IN TUBE THROAT

1311*REGION TO PRINT PREDICTED AND CORRECTED VALUES, 0= PRED, 1= CORR									
26664	0	52000	0	32727	1312		AZPP	ZET	X+9
26665	0	02000	4	00001	1313	+1	TRA	1,4	
26666	0	63400	4	26740	1314	+2	SXA	AZPPR,4	
26667	0	63400	1	26741	1315	+3	SXA	AZPPR+1,1	
2667C	0	44100	4	00000	1316	+4	LDI	0,4	
26671	-0	05700	7	77776	1317	+5	RIL	777776	
26672	-0	04600	0	00000	1318	+6	PIA		
26673	-0	73700	1	00000	1319	+7	PDC	,1	PRED OR CORR
26674	0	07406	4	32541	1320	+8	TSX	PL,4,6	
26675	0	50260	1	26767	1321	+9	CLS*	AZPP6+2,1	MC
26676	0	30260	1	26771	1322	+10	FSB*	AZPP6+4,1	WH
26677	0	60260	1	26775	1323	+11	SLW*	AZPP6+8,1	WT
267CC	0	30000	0	32631	1324	+12	FAD	P+11	WDOOTR
267C1	0	60160	1	26773	1325	+13	STO*	AZPP6+6,1	WN
26702	0	07400	4	00052	1326	+14	TSX	DOUT,4	
26703	3	02044	1	26743	1327	+15	PTH	AZPP1,1,1060	
26704	3	04030	0	26745	1328	+16	PTH	AZPP2,,2072	
26705	-1	00024	0	00012	1329	+17	FVE	10,,20	
26706	0	07400	4	00052	1330	+18	TSX	DOUT,4	
26707	3	01765	C	26747	1331	+19	PTH	AZPP4,,1013	



1440\*REGION TO COMPUTE INLET AND OUTLET CAPACITANCE FLOW RATE CHANGE

27075	0	63400	4	27123	1441	AZU	SXA	AZUR,4	
27076	0	63400	2	27124	1442		+1 SXA	AZUR+1,2	
27077	0	96000	0	32621	1443		+2 LOQ	P+3	
27100	0	16200	0	27102	1444		+3 TOP	P+2	
27101	0	02000	4	00001	1445		+4 TRA	1,4	NEGATIVE PRESSURE
27102	0	44100	4	00000	1446		+5 LDI	0,4	
27103	-0	05700	7	77776	1447		+6 RIL	777776	
27104	-0	04400	0	00000	1448		+7 PIA		
27109	-0	73700	2	00000	1449		+8 PDC	,2	
27106	0	90000	0	32620	1490		+9 CLA	P+2	T
27107	0	07400	4	25564	1451		+10 TSX	AZM,4	
27110	0	07400	4	42602	1452		+11 TSX	ERROR,4	
27111	0	90200	0	33730	1453		+12 CLS	WPM+6	NEW RHO EOM HT13
27112	0	60260	2	27130	1454		+13 SLW	AZU1,2	
27113	0	30060	2	27132	1455		+14 FAD	AZU2,2	OLD RHO
27114	0	24100	0	32637	1456		+15 FDP	P+17	DELT
27115	0	24060	2	27134	1457		+16 FMP	AZU3,2	PLENUM VOLUME
27116	0	30060	2	27136	1458		+17 FAD	AZU5,2	OLD DELWDOT
27117	0	00160	2	27140	1459		+18 STO	AZU6,2	-CURRENT DELWDOT
27120	0	30000	0	32631	1460		+19 FAD	P+11	
27121	0	00100	0	32631	1461		+20 STO	P+11	
27122	-0	12000	0	27126	1462		+21 TMI	AZU4	NEGATIVE FLOW RATE
27123	0	77400	4	00000	1463	AZUR	AXT	000,4	
27124	0	77400	2	00000	1464		+1 AXT	000,2	
27129	0	02000	4	00003	1465		+2 TRA	3,4	
27126	0	92200	0	27123	1466	AZU4	XEC	AZUR	
27127	1	00001	4	27124	1467		+1 TXI	AZUR+1,4,1	ERROR RETURN
27130	0	00000	1	35621	1468	AZU1	PZE	PT+7,1	
27131	0	00000	1	35623	1469		+1 PZE	PT+9,1	
27132	0	00000	1	35620	1470	AZU2	PZE	PT+6,1	
27133	0	00000	1	35622	1471		+1 PZE	PT+8,1	
27134	0	00000	1	36074	1472	AZU3	PZE	DVI,1	
27135	0	00000	1	36075	1473		+1 PZE	DVO,1	
27136	0	00000	1	35626	1474	AZU5	PZE	PT+12,1	PAST TIME DELWDOT
27137	0	00000	1	35627	1475		+1 PZE	PT+13,1	
27140	0	00000	1	35630	1476	AZU6	PZE	PT+14,1	-CURRENT DELWDOT
27141	0	00000	1	35631	1477		+1 PZE	PT+15,1	

1479\*REGION TO COMPUTE VAPOR PRESSURE VS TEMP

27142	0	63400	4	27152	1480	AZV	SXA	AZVR,4	
27143	0	77400	4	00005	1481		+1 AXT	5,4	
27144	0	75400	0	00000	1482		+2 PXA	,0	
27145	0	30000	4	27161	1483	AZV2	FAD	AZV1+5,4	
27146	-2	00001	4	27152	1484		+1 TNX	AZVR,4,1	
27147	0	13100	0	00000	1485		+2 XCA		
27150	0	26000	0	33742	1486		+3 FMP	TP+5	
27151	0	02000	0	27145	1487		+4 TRA	AZV2	
27152	0	77400	4	00000	1488	AZVR	AXT	000,4	
27153	0	02000	4	00001	1489		+1 TRA	1,4	
27154	1	62526	4	30773	1490	AZV1	DEC	40835E-9,-.0037617,.238625,-7.92,96.38	

1492\*INPUT SUBROUTINES

1493\*TEST NEXT CASE FOR STANDARD INPUT DESIRED

27161	0	63400	4	27177	1494	AZX	SXA	AZXR,4	
27162	0	63400	0	27304	1495		+1 SXA	AZXB2,0	INITIALIZE XR FOR NEW CASE
27163	0	07476	4	00102	1496		+2 TSX	KTAKB,4,62	
27164	-1	00001	0	27215	1497		+3 FVE	AZX1,.1	
27165	0	12000	0	27170	1498		+4 TPL	0+3	
27166	-1	27217	0	25421	1499	AZX6	STR	AZF,..,AZX3	
27167	0	07400	4	00076	1500		+1 TSX	KFINIS,4	
27170	0	16200	0	27201	1501		+2 TOP	AZX4	
27171	-0	50000	0	27215	1502		+3 CAL	AZX1	
27172	0	32200	0	27216	1503		+4 ERA	AZX2	
27173	0	60200	0	27215	1504		+5 SLW	AZX1	
27174	-0	10000	0	27177	1505		+6 TNZ	AZXR	N CARD SAYS IGNORE STD INPUT
27175	0	07476	4	00101	1506		+7 TSX	KMOV,4,62	PASS N CARD
27176	-1	00016	0	00000	1507		+8 FVE	0,..,14	
27177	0	77400	4	00000	1508	AZXR	AXT	000,4	
27200	0	02000	4	00001	1509		+1 TRA	1,4	
27201	-1	27222	0	25421	1510	AZX4	STR	AZF,..,AZX5	
27202	0	07400	4	00052	1511		+1 TSX	DOUT,4	
27203	3	21544	0	27225	1512		+2 PTH	AZX7,..,9060	
27204	-1	00024	0	00000	1513		+3 FVE	KONLIN,..,20	
27205	0	07400	4	00076	1514		+4 TSX	KFINIS,4	
27206	0	07400	4	00055	1515	AZX8	TSX	KDEBUG,4	
27207	0	16200	0	27201	1516		+1 TOP	AZX4	
27210	-1	27212	0	25421	1517		+2 STR	AZF,..,AZX9	
27211	0	02000	0	24654	1518		+3 TRA	AZM4	
27212	3	14343	2	92721	1519	AZX9	BCI	3,ILLEGAL CHARACTER	
				27215	1520	AZX1	BSS	1,0	NOT 0= STD CASE
27216	-0	56060	6	06060	1521	AZX2	BCI	1,N	
27217	2	54524	6	06426	1522	AZX3	BCI	3,END OF INPUT	
27222	2	22124	6	06321	1523	AZX5	BCI	3,BAD TAPE- FLUSH	
27225	-2	32147	2	56023	1524	AZX7	BCI	9,TAPE CHECK ON KISNET INPUT TAPE, PLEASE SAVE TAPE	

1526\*READ IN ONE PART

27236	0	63400	4	27257	1527	AZXA	SXA	AZXR,4	
27237	-0	52000	0	27215	1528		+1 NZT	AZX1	
27240	0	02000	0	27250	1529		+2 TRA	AZX1	IGNORE STD CASE
27241	-0	62500	0	27322	1530		+3 STL	AZX1	INPUT FROM CORE
27242	0	07400	4	41664	1531		+4 TSX	A558,4	
27243	0	32577	0	36064	1532		+5 PZE	0,..,TCARD	
27244	0	07400	4	00056	1533		+6 TSX	KERROR,4	
27245	0	07400	4	00056	1534		+7 TSX	KERROR,4	
27246	-0	52000	0	32612	1535		+8 NZT	TCARD+11	
27247	0	02000	0	27261	1536		+9 TRA	AZX2	
27250	0	60000	0	27322	1537	AZX1	STZ	AZX1	INPUT FROM TAPE
27251	0	07400	4	41664	1538		+1 TSX	A558,4	
27252	0	32577	0	36064	1539		+2 PZE	0,..,TCARD	
27253	0	02000	0	27206	1540		+3 TRA	AZX8	
27254	0	02000	0	27166	1541		+4 TRA	AZX6	EOF
27255	-0	52000	0	36065	1542		+5 NZT	DMAX	0= IGNORE THIS PART
27256	0	02000	0	27237	1543		+6 TRA	AZX+1	
27257	0	77400	4	00000	1544	AZXR	AXT	000,4	

27261	0	60000	0	27322	1546	AZXA2	STZ	AZXB1	
27262	0	07400	4	41664	1547		+1	TSX	ASSB,4
27263	0	32577	0	44107	1548		+2	PZE	LVSAC,,TCARD
27264	0	02000	0	27204	1549		+3	TRA	AZXB
27265	0	02000	0	27166	1550		+4	TRA	AZXB
27266	-0	50000	0	27277	1551		+5	CAL	AZXA4
27267	0	32000	0	32577	1552		+6	AMS	TCARD
27270	-0	52000	0	32612	1553		+7	NZT	TCARD+11
27271	0	02000	0	27257	1554		+8	TRA	AZXB
27272	-1	27274	0	29421	1555	AZXA5	STR	AZF,,AZXA3	
27273	0	07400	4	00076	1556		+1	TSX	KFINIS,4
27274	-3	12551	4	66063	1557	AZXA3	BCI	3,ZERO TCARD MISSING	
27277	-2	07777	7	77777	1558	AZXA4	OCT	-20777777777	

1560\*READ ONE CARD FROM CORE

27300	-0	52000	0	27322	1561	AZXB	NZT	AZXB1	
27301	0	02000	0	00101	1562		+1	TRA	KMOVEB
27302	0	63400	4	27317	1563		+2	SXA	AZXB,4
27303	0	63400	1	27320	1564		+3	SXA	AZXB+1,1
27304	0	77400	4	00000	1565	AZXB2	AXT	000,4	
27305	0	77400	1	00000	1566		+1	AXT	0,1
27306	-0	90000	4	50032	1567	AZXB3	CAL	AZXB,4	
27307	0	60200	1	32577	1568		+1	SLB	TCARD,1
27310	1	77777	4	27311	1569		+2	TXI	*+1,4,-1
27311	1	77777	1	27312	1570		+3	TXI	*+1,1,-1
27312	3	77764	1	27306	1571		+4	TXM	AZXB3,1,-12
27313	0	63400	4	27304	1572		+5	SXA	AZXB2,4
27314	-0	76000	0	00003	1573		+6	SSM	
27315	0	13100	0	00000	1574		+7	XCA	
27316	0	76000	0	00003	1575		+8	SSP	
27317	0	77400	4	00000	1576	AZXB	AXT	000,4	
27320	0	77400	1	00000	1577		+1	AXT	000,1
27321	0	02000	4	00002	1578		+2	TRA	2,4
				27322	1579	AZXB1	BSS	1,0	

INPUT FROM TAPE  
ADDRESS FOR NEXT CARD  
TO SIMULATE KMOVEB  
NOT 0= INPUT FROM CORE

1581\*READ IN STANDARD CASE AS BCD

27323	0	63400	4	27345	1582	AZXC	SXA	AZXC,4	
27324	0	63400	1	27346	1583		+1	SXA	AZXC+1,1
27325	0	77400	1	00000	1584		+2	AXT	0,1
27326	0	07476	4	00101	1585	AZXC2	TSX	KMOVEB,4,62	
27327	-1	00014	1	50032	1586		+1	PVE	AZXB,1,12
27330	0	16200	0	27201	1587		+2	TQP	AZXB
27331	-0	12000	0	27336	1588		+3	YMI	AZXC1
27332	-0	50000	1	50045	1589		+4	CAL	AZXB+11,1
27333	0	10000	0	27340	1590		+5	TZE	AZXC4
27334	1	77764	1	27335	1591		+6	TXI	*+1,1,-12
27335	3	76650	1	27326	1592		+7	TXM	AZXC2,1,-12*CARDS
27336	-1	27350	0	25421	1593	AZXC1	STR	AZF,,AZXC3	
27337	0	07400	4	00076	1594		+1	TSX	KFINIS,4
27340	0	60000	0	27322	1595	AZXC4	STZ	AZXB1	
27341	0	07400	4	41664	1596		+1	TSX	ASSB,4
27342	0	32577	0	44107	1597		+2	PZE	LVSAC,,TCARD
27343	0	02000	0	27334	1598		+3	TRA	AZXC1

INPUT STORAGE  
COL 67-72  
TEST CARDS VS AVAILABLE STORAGE  
NOZZLE TUBE PARAMETERS

27345	0	77400	4	00000	1600	AZXC	AXT	000,4	
27346	0	77400	1	00000	1601		+1	AXT	000,1
27347	0	02000	4	00001	1602		+2	TRA	1,4
27350	2	55151	4	65160	1603	AZXC3	BCI	3,ERROR IN STD INPUT	

1605\*REGION TO STORE DILUENT TEMP AND PRESS

27353	0	52000	0	32742	1606	AZY	ZET	X+20	
27354	0	02000	4	00002	1607		+1	TRA	2,4
27355	0	50000	0	32620	1608		+2	CLA	P+2
27356	0	60100	0	32705	1609		+3	STO	P+55
27357	0	50000	0	32621	1610		+4	CLA	P+3
27360	0	60100	0	32704	1611		+5	STO	P+54
27361	0	50000	0	32631	1612		+6	CLA	P+11
27362	0	30200	0	32644	1613		+7	F5B	P+22
27363	0	60100	0	32631	1614		+8	STO	P+11
27364	-0	62500	0	32744	1615		+9	STL	X+22
27365	0	12000	4	00001	1616		+10	TMI	1,4
27366	0	02000	4	00002	1617		+11	TRA	2,4

DILUENT SET TO ZERO  
TC  
PC  
WDOTC  
WDOTR  
DILUENT REMOVED FLAG  
ERROR RETURN FOR NEGATIVE WDOTR

1619\*REGION TO COMPUTE P3 AND T3, NOZZLE TUBE INLET

27367	0	50000	0	32655	1620	AZZ	CLA	P+31	EQN T1
27370	0	60100	0	32703	1621		+1	STO	P+53
27371	0	60100	0	32620	1622		+2	STO	P+2
27372	0	56000	0	32757	1623		+3	LQO	C+8
27373	0	26000	0	32631	1624		+4	FMP	P+11
27374	0	24100	0	34071	1625		+5	FOP	TP+92
27375	0	26000	0	32631	1626		+6	FMP	P+11
27376	0	30000	0	32654	1627		+7	FAD	P+30
27377	0	60100	0	32702	1628		+8	STO	P+52
27400	0	60100	0	32621	1629		+9	STO	P+3
27401	0	02000	4	00001	1630		+10	TRA	1,4

CURRENT FLUID TEMP  
EQN T2  
WDOTR  
RHO2 PREDICTED  
P3  
CURRENT PRESSURE

1632\*REGION TO ITERATE FOR WDOOTH, CLOSING ON P8

27402	0	63400	4	27525	1633	AYA	SXA	AYAR,4	
27403	0	60000	0	32733	1634		+1	STZ	X+13
27404	0	56000	0	32677	1635		+2	LQO	P+49
27405	0	26000	0	32632	1636		+3	FMP	P+12
27406	0	60100	0	34042	1637		+4	STO	TP+69
27407	0	60000	0	40633	1638		+5	STZ	NEWB9+1
27410	0	50000	0	40305	1639		+6	CLA	BIG
27411	0	60100	0	40632	1640		+7	STO	NEWB9
27412	0	50000	0	32645	1641		+8	CLA	P+23
27413	0	60100	0	34045	1642		+9	STO	TP+72
27414	0	50000	0	36112	1643		+10	CLA	DP8E
27415	0	07400	4	40547	1644		+11	TSX	NEWB,4
27416	0	34043	0	34045	1645		+12	PZE	TP+72,,TP+70
27417	0	00017	0	34044	1646		+13	PZE	TP+71,,15
27420	0	02000	0	27527	1647		+14	TRA	AYA1
27421	0	50000	0	34045	1648		+15	CLA	TP+72
27422	0	24100	0	33753	1649		+16	FOP	TP+14
27423	-0	60000	0	12512	1650		+17	STO	COMMON

ERROR FLAG  
WDOTP  
EQN PT24  
P8  
MINWDOOTH  
MAX WDOOTH  
WDOOTH(I+1) GUESS = WDOOTH(I)  
NON CONVERGENCE  
WDOOTH  
EQN PT35

27424	0	26000	0	12512	1651	+18	FMP	COMMON		
27425	0	30200	0	34042	1652	+19	FSB	TP+69		
27426	0	12000	0	40624	1653	+20	TPL	BOX8	WDOTH TOO BIG	
27427	0	60200	0	47333	1654	+21	SLW	PR+10	PHR	
27430	0	50000	0	32674	1655	+22	CLA	P+44	P2	EQN PT36
27431	0	30200	0	47333	1656	+23	FSB	PR+10	PHR	
27432	0	07400	4	24364	1657	+24	TSX	SQRT,4		
27433	0	07400	4	42602	1658	+25	TSX	ERROR,4		
27434	0	13100	0	00000	1659	+26	XCA			
27435	0	26000	0	33740	1660	+27	FMP	TP+3		
27436	0	60100	0	34044	1661	+28	STO	TP+73	WDOTC	
27437	0	60100	0	47403	1662	+29	STO	PR+50		
27440	0	30000	0	34045	1663	+30	FAD	TP+72	WDOTH	EQN PT27A
27441	0	60100	0	34051	1664	+31	STO	TP+76	WDOYT	
27442	0	24100	0	33754	1665	+32	FDP	TP+15	K12	EQN PT37
27443	-0	60000	0	47447	1666	+33	STQ	PR+06	V8	
27444	0	50000	0	34045	1667	+34	CLA	TP+72	WDOTH	EQN PT38
27445	0	60100	0	47404	1668	+35	STO	PR+51		
27446	0	24100	0	33755	1669	+36	FDP	TP+16		
27447	-0	60000	0	47446	1670	+37	STQ	PR+85	VHR	
27450	0	50000	0	34046	1671	+38	CLA	TP+73	WDOTC	EQN PT39
27451	0	24100	0	33762	1672	+39	FDP	TP+21		
27452	-0	60000	0	47445	1673	+40	STQ	PR+84	VCM	
27453	0	50000	0	34046	1674	+41	CLA	TP+73	WDOYC	EQN PT40
27454	0	24100	0	33763	1675	+42	FDP	TP+22		
27455	-0	60000	0	12513	1676	+43	STQ	COMMON+1		
27456	0	26000	0	12513	1677	+44	FMP	COMMON+1		
27457	0	30200	0	32674	1678	+45	FSB	P+46	P2	
27460	0	12000	0	40624	1679	+46	TPL	BOX8	WDOTC, THEREFORE WDOTH TOO BIG	
27461	0	60200	0	47332	1680	+47	SLW	PR+9	PCM	
27462	0	50000	0	32633	1681	+48	LDQ	P+13	T6(11)	EQN PT28
27463	0	26000	0	34045	1682	+49	FMP	TP+72	WDOTH	
27464	0	61100	0	12514	1683	+50	STO	COMMON+2		
27465	0	50000	0	32675	1684	+51	LDQ	P+47		
27466	0	26000	0	34046	1685	+52	FMP	TP+73		
27467	0	30000	0	12514	1686	+53	FAD	COMMON+2		
27470	0	24100	0	34051	1687	+54	FDP	TP+76		
27471	0	26000	0	34036	1688	+55	FMP	TP+65		
27472	0	60100	0	34052	1689	+56	STO	TP+77	T8	
27473	0	60100	0	34053	1690	+57	STO	TP+78	T11	
27474	0	50000	0	47400	1691	+58	LDQ	PR+47	MH8(11)	EQN PT41
27475	0	26000	0	47400	1692	+59	FMP	PR+47		
27476	0	13100	0	00000	1693	+60	XCA			
27477	0	26000	0	32760	1694	+61	FMP	C+9		
27500	0	30000	0	40213	1695	+62	FAD	FL1		
27501	0	60100	0	33737	1696	+63	STO	TP+2		
27502	0	50000	0	34052	1697	+64	CLA	TP+77		
27503	0	24100	0	33737	1698	+65	FDP	TP+2		
27504	-0	60000	0	47355	1699	+66	STQ	PR+28	T8 STATIC, ASSUME MH8 SAME AS TIME I	
27505	0	07400	4	27034	1700	+67	TSX	AZ0,4	P8 STATIC	EQN PT42
27506	0	00000	0	36175	1701	+68	PZE	DRH		
27507	0	50000	0	33737	1702	+69	CLA	TP+2		
27510	0	56000	0	32764	1703	+70	LDQ	C+13	MACH NO. TERM	EQN PT43
27511	0	07400	4	27021	1704	+71	TSX	AZE,4		

27512	0	13100	0	00000	1705	+72	XCA			
27513	0	26000	0	47324	1706	+73	FMP	PR+3	P8 STATIC	
27514	0	60100	0	34043	1707	+74	STO	TP+70	P8 STAGNATION	
27515	0	50000	0	34052	1708	+75	LDQ	TP+77	T8	EQN PT29
27516	0	26000	0	34033	1709	+76	FMP	TP+62		
27517	0	07400	4	24364	1710	+77	TSX	SQRT,4		
27520	0	07400	4	42602	1711	+78	TSX	ERROR,4		
27521	0	13100	0	00000	1712	+79	XCA			
27522	0	26000	0	34051	1713	+80	FMP	TP+76		
27523	0	60100	0	34044	1714	+81	STO	TP+71	P8 PRIME	
27524	0	07400	4	40640	1715	+82	TSX	RAP8,4		
27525	0	77400	4	00000	1716	AYAR	AXT	000,4		
27526	0	02000	0	00001	1717	+1	TRA	L,4		
27527	-0	62500	0	32733	1718	AYAL	STL	X+13		
27530	0	02000	0	27525	1719	+1	TRA	AYAR		

1721 REGION TO SOLVE FOR ACTUAL WORK IN THE PUMP AND TURBINE										
27531	0	63400	4	27641	1722	AYB	SXA	AYBR,4		
27532	0	50060	1	27643	1723	+1	CLA*	AYBT,1	T11	EQN PT7
27533	0	07400	4	24364	1724	+2	TSX	SQRT,4		
27534	0	07400	4	42602	1725	+3	TSX	ERROR,4		
27535	0	60100	0	34006	1726	+4	STO	TP+41		
27536	0	52000	0	32742	1727	+5	ZET	X+20		
27537	0	02000	0	27647	1728	+6	TRA	AYB2	P11 GIVEN	
27540	0	24100	0	34037	1729	+7	FDP	TP+66	K T	
27541	0	26060	1	27645	1730	+8	FMP*	AYBM,1	WDOYT	
27542	0	60100	0	32662	1731	+9	STO	P+36	P11	
27543	0	60000	1	32740	1732	AYB1	STZ	X+18,1	ERROR FLAGS	
27544	0	24100	0	40224	1733	+1	FDP	FL10		
27545	-0	60000	0	32664	1734	+2	STO	P+38	P12 GUESS = P11/10	
27546	0	50000	1	32665	1735	+3	CLA	P+39,1	EQN PT8	
27547	0	24100	0	34006	1736	+4	FDP	TP+41		
27550	0	13100	0	00000	1737	+5	XCA			
27551	0	07400	4	30516	1738	+6	TSX	AYJ,4		
27552	0	60100	0	34003	1739	+7	STO	TP+38	ETAT PRIME	
27553	0	50060	1	27643	1740	+8	CLA*	AY...:	T11	EQN PT9A
27554	0	50000	0	32662	1741	+9	LDQ	P+	P11	
27555	-0	60000	0	40632	1742	+10	STQ	NEWB0		
27556	0	60000	0	40633	1743	+11	STZ	NEWB9+1		
27557	0	07400	4	25564	1744	+12	TSX	AZH,4		
27560	0	07400	4	42602	1745	+13	TSX	ERROR,4		
27561	0	50000	0	32750	1746	+14	CLA	C+1	R/776	
27562	0	24100	0	33731	1747	+15	FDP	MFR+7	CP(T11,P11)	
27563	-0	60000	0	34012	1748	+16	STQ	TP+45		
27564	0	50000	0	36113	1749	+17	CLA	DP12E	P12 EPSILON	
27565	0	07400	4	40547	1750	+18	TSX	NEWB,4		
27566	0	34011	0	32664	1751	+19	PZE	P+38,,TP+44		
27567	0	00062	0	34013	1752	+20	PZE	TP+46,,50		
27570	0	02000	0	27655	1753	+21	TRA	AYB3		
27571	0	50000	0	32664	1754	+22	CLA	P+38	P12	
27572	0	24100	0	32662	1755	+23	FDP	P+36	P11	
27573	-0	60000	0	34013	1756	+24	STQ	TP+46		
27574	0	13100	0	00000	1757	+25	XCA			





27746	0	50000	0	40225	1865	+95	CLA	FLR	
27747	0	24100	0	40236	1866	+96	FDP	FLG	
27750	0	26000	0	40225	1867	+97	FMP	FL12	
27751	0	60100	0	32754	1868	+98	STO	C+5	
27752	0	56000	0	36137	1869	+99	LDQ	DDTL	
27753	0	07400	4	30047	1870	+60	TSX	AYCA,4	
27754	0	60100	0	32755	1871	+61	STO	C+6	
27755	0	13100	0	00000	1872	+62	XCA		
27756	0	26000	0	32755	1873	+63	FMP	C+6	
27757	0	60100	0	32755	1874	+64	STO	C+6	
27760	0	56000	0	40225	1875	+65	LDQ	FL12	
27761	0	26000	0	40242	1876	+66	FMP	FL776	
27762	0	60100	0	32756	1877	+67	STO	C+7	
27763	0	56000	0	36135	1878	+68	LDQ	DD2	
27764	0	07400	4	30047	1879	+69	TSX	AYCA,4	EON T2A
27765	0	60100	0	12515	1880	+70	STO	COMMON+3	
27766	0	50200	0	36134	1881	+71	CLS	DK2	
27767	0	24100	0	12515	1882	+72	FDP	COMMON+3	
27770	0	13100	0	00000	1883	+73	XCA		
27771	0	24100	0	12515	1884	+74	FDP	COMMON+3	
27772	0	13100	0	00000	1885	+75	XCA		
27773	0	24100	0	40236	1886	+76	FDP	FLG	
27774	0	13100	0	00000	1887	+77	XCA		
27775	0	24100	0	40214	1888	+78	FDP	FL2	
27776	-0	60000	0	32757	1889	+79	STQ	C+8	
27777	0	50000	0	36176	1890	+80	CLA	DK11	
30000	0	30000	0	36177	1891	+81	FAD	DK9	
30001	0	24100	0	32755	1892	+82	FDP	C+6	
30002	0	26000	0	32754	1893	+83	FMP	C+5	
30003	0	60100	0	34032	1894	+84	STO	TP+61	
30004	0	50000	0	36167	1895	+85	CLA	DKPHM	
30005	0	30200	0	40213	1896	+86	FSB	FL1	
30006	0	60100	0	12516	1897	+87	STO	COMMON+4	
30007	0	24100	0	40214	1898	+88	FDP	FL2	
30010	-0	60000	0	32760	1899	+89	STQ	C+9	(K-1)/2
30011	0	50000	0	36167	1900	+90	CLA	DKPHM	
30012	0	24100	0	12516	1901	+91	FDP	COMMON+4	
30013	-0	60000	0	32764	1902	+92	STQ	C+13	
30014	0	56000	0	36136	1903	+93	LDQ	DDH	
30015	0	07400	4	30047	1904	+94	TSX	AYCA,4	
30016	0	13100	0	00000	1905	+95	XCA		
30017	0	26000	0	40272	1906	+96	FMP	FLGF	
30020	0	60100	0	32761	1907	+97	STO	C+10	G*AH
30021	0	56000	0	36154	1908	+98	LDQ	DTMET	
30022	0	26000	0	40277	1909	+99	FMP	RAD	
30023	0	07400	4	42374	1910	+100	TSX	COS,4	
30024	0	60100	0	32765	1911	+101	STO	C+14	COS TETA
30025	0	56000	0	36150	1912	+102	LDQ	DDCO	
30026	0	07400	4	30047	1913	+103	TSX	AYCA,4	
30027	0	13100	0	00000	1914	+104	XCA		
30030	0	26000	0	36151	1915	+105	FMP	DNH	
30031	0	13100	0	00000	1916	+106	XCA		
30032	0	26000	0	32765	1917	+107	FMP	C+14	
30033	0	13100	0	00000	1918	+108	XCA		

30034	0	26000	0	40272	1919	+109	FMP	FLGF	
30035	0	60100	0	32762	1920	+110	STO	C+11	G*ACN+COS(THETA)
30036	0	56000	0	36165	1921	+111	LDQ	DFHDT	
30037	0	26000	0	40275	1922	+112	FMP	PI	
30040	0	24100	0	40214	1923	+113	FDP	FL2	
30041	0	26000	0	36136	1924	+114	FMP	DDH	
30042	0	13100	0	00000	1925	+115	XCA		
30043	0	26000	0	36146	1926	+116	FMP	DL	
30044	0	60100	0	32763	1927	+117	STO	C+12	F*PI*DH*L/2
30045	0	77400	4	00000	1928	AYCR	AXT	**0,4	
30046	0	02000	4	00001	1929	+1	TRA	L,4	

30047	-0	60000	0	30054	1932	AYCA	STQ	AYCA1	1931*REGION TO COMPUTE AREA FROM DIAMETER
30050	0	26000	0	30054	1933	+1	FMP	AYCA1	
30051	0	24100	0	40216	1934	+2	FDP	FL4	
30052	0	26000	0	40275	1935	+3	FMP	PI	
30053	0	02000	4	00001	1936	+4	TRA	L,4	
				30054	1937	AYCA1	BSS	L,F	

30055	0	63400	4	30142	1940	AYD	SXA	AYDR,4	1939*REGION TO COMPUTE PUMP FLOW
30056	0	60000	0	32736	1941	+1	STZ	X+16	
30057	0	50000	0	40305	1942	+2	CLA	BIG	
30060	0	60100	0	40632	1943	+3	STO	NEWB9	
30061	0	60000	0	40633	1944	+4	STZ	NEWB9+1	
30062	0	56000	0	32666	1945	+5	LDQ	P+40	N I+1
30063	0	26000	0	30154	1946	+6	FMP	AYD01	
30064	0	60100	0	32700	1947	+7	STO	P+50	Q/N GUESS = .37
30065	0	50000	0	36144	1948	+8	CLA	DHE	
30066	0	07400	4	40547	1949	+9	TSX	NEWB,4	
30067	0	32676	0	32700	1950	+10	PZE	P+50, P+48	
30070	0	00031	0	34027	1951	+11	PZE	TP+58, +25	
30071	0	02000	0	30147	1952	+12	TRA	AYD2	
30072	0	56000	0	32700	1953	+13	LDQ	P+50	EON PT18
30073	0	26000	0	34017	1954	+14	FMP	TP+50	RH01
30074	0	24100	0	32752	1955	+15	FDP	C+3	
30075	-0	60000	0	32677	1956	+16	STQ	P+49	WDDTP(I+1)
30076	0	26000	0	32673	1957	+17	FMP	P+45	ALPHA
30077	0	30000	0	32632	1958	+18	FAD	P+12	BETA
30100	0	13100	0	00000	1959	+19	XCA		EON PT17
30101	0	26000	0	32677	1960	+20	FMP	P+49	
30102	0	60100	0	32674	1961	+21	STO	P+46	
30103	0	07400	4	30437	1962	+22	TSX	AYI,4	P2(I+1)
30104	0	60100	0	32675	1963	+23	STO	P+47	FIND T2 ISOENTROPICALLY
30105	0	56000	0	32674	1964	+24	LDQ	P+46	T2(I+1)
30106	0	07400	4	25564	1965	+25	TSX	AZH,4	
30107	0	02000	0	30151	1966	+26	TRA	AYD1	
30110	0	50000	0	33724	1967	+27	CLA	WPR+2	H2(I+1)
30111	0	30200	0	34070	1968	+28	FSB	TP+91	H1(I+1)
30112	0	60100	0	34056	1969	+29	STO	T+81	
30113	0	13100	0	00000	1970	+30	XCA		
30114	0	26000	0	40242	1971	+31	FMP	FL776	



30261	0	80000	0	32648	2078	+33	CLA	P+23	WOOTH	EQN PT38
30262	0	24100	0	47644	2079	+34	FDP	PR+85	VHM	
30263	-0	60000	0	33759	2080	+35	STO	TP+16	K13	
30264	0	80000	0	32644	2081	+36	CLA	P+22	NDOTC	EQN PT39
30265	0	24100	0	47643	2082	+37	FDP	PR+84	VCH	
30266	-0	60000	0	33762	2083	+38	STO	TP+21	K14	
30267	0	80000	0	32654	2084	+39	CLA	P+30	P2	EQN PT40
30270	0	30200	0	47332	2085	+40	FSB	PR+9		
30271	0	07400	4	24364	2086	+41	TSX	SORT,4		
30272	0	07400	4	42602	2087	+42	TSX	ERROR,4		
30273	0	60100	0	12512	2088	+43	STO	COMMON		
30274	0	80000	0	32644	2089	+44	CLA	P+22		
30275	0	24100	0	12512	2090	+45	FDP	COMMON		
30276	-0	60000	0	33763	2091	+46	STO	TP+22	K15	
30277	0	84000	0	34131	2092	+47	LDQ	DAKV	EQN PT33	
30300	0	26000	0	34073	2093	+48	FHP	TP+94		
30301	0	30200	0	34132	2094	+49	FSB	DBKV		
30302	0	60100	0	34040	2095	+50	STO	TP+67	KV(I+1)	
30303	0	80000	0	32753	2096	+51	CLA	C+4	4GR/12	EQN 30A
30304	0	24100	0	34040	2097	+52	FDP	TP+67		
30305	0	13100	0	00000	2098	+53	XCA			
30306	0	24100	0	34040	2099	+54	FDP	TP+67		
30307	-0	60000	0	34031	2100	+55	STO	TP+60	K1	
30310	0	80000	0	40213	2101	+56	CLA	FL1	EQN 30	
30311	0	24100	0	34037	2102	+57	FDP	TP+66	KT	
30312	0	13100	0	00000	2103	+58	XCA			
30313	0	24100	0	34037	2104	+59	FDP	TP+66		
30314	0	13100	0	00000	2105	+60	XCA			
30315	0	30000	0	34031	2106	+61	FAD	TP+60	K1	
30316	0	30000	0	34032	2107	+62	FAD	TP+61	K2	
30317	0	60100	0	34033	2108	+63	STO	TP+62	K3	
30320	0	50000	0	32641	2109	+64	CLA	P+35	T8	EQN 6
30321	0	60100	0	32643	2110	+65	STO	P+37	T11	
30322	0	07400	4	27531	2111	+66	TSX	AYB,4	TIME I	EQN PT7-10
30323	0	07400	4	31501	2112	+67	TSX	AYL,4		EQN PT21
30324	0	77400	4	00000	2113	AYGR	AXT	**0,4		
30325	0	07000	4	00001	2114	+1	TRA	L,4		
						2116*REGION TO COMPUTE ADDITIONAL QUANTITIES AT TIME I				
30326	0	50000	0	32643	2117	AYGA	CLA	P+21	NDOTP	EQN PT18
30327	0	24100	0	34060	2118	+1	FDP	TP+83	RHO1	
30330	0	26000	0	32752	2119	+2	FHP	C+3		
30331	0	60100	0	34061	2120	+3	STO	TP+84	QP(I)	
30332	0	24100	0	32645	2121	+4	FDP	P+39		
30333	-0	60000	0	34000	2122	+5	STQ	TP+35	Q/N	
30334	0	50000	0	32635	2123	+6	CLA	P+15		
30335	0	24100	0	32645	2124	+7	FDP	P+39		
30336	0	13100	0	00000	2125	+8	XCA			
30337	0	24100	0	32645	2126	+9	FDP	P+39		
30340	-0	60000	0	33773	2127	+10	STQ	TP+30	HSV/NSQ.	
30341	0	50000	0	32656	2128	+11	CLA	P+32	P6	EQN PT13
30342	0	24100	0	32643	2129	+12	FDP	P+21		
30343	-0	60000	0	32632	2130	+13	STQ	P+12	BETA	
30344	0	26000	0	32654	2131	+14	CLA	P+22	EQN PT14	
						2139*REGION TO COMPUTE FILM COEFFICIENT				
30353	0	63400	4	30430	2140	AYH	SXA	AYHR,4		
30354	0	63400	1	30431	2141	+1	SXA	AYHR+1,1		
30355	0	50000	0	32620	2142	+2	CLA	P+2	T	
30356	0	24160	4	00001	2143	+3	FDP*	1,4	THETA	
30357	-0	50000	4	00001	2144	+4	CAL	1,4		
30360	-0	73700	1	00000	2145	+5	PDC	+1		
30361	0	13100	0	00000	2146	+6	XCA			
30362	0	56000	1	00000	2147	+7	LDQ	0,1	ALPHA	
30363	-0	12000	0	30433	2148	+8	TMI	AYH1		
30364	0	07400	4	27021	2149	+9	TSX	AZE,4		
30365	0	60100	0	12524	2150	+10	STO	COMMON+10		
30366	0	50000	0	33741	2151	+11	CLA	TP+4		
30367	0	24100	0	33764	2152	+12	FDP	TP+23	D+DELZ	
30370	0	13100	0	00000	2153	+13	XCA			
30371	0	56000	1	00001	2154	+14	LDQ	1,1	BETA	
30372	-0	12000	0	30433	2155	+15	TMI	AYH1		
30373	0	07400	4	27021	2156	+16	TSX	AZE,4		
30374	0	60100	0	12525	2157	+17	STO	COMMON+11		
30375	0	50000	0	32631	2158	+18	CLA	P+11	NDOT	
30376	0	36100	0	40302	2159	+19	ACL	288		
30377	0	24100	0	33760	2160	+20	FDP	TP+19	F	
30400	0	13100	0	00000	2161	+21	XCA			
30401	0	24100	0	33733	2162	+22	FDP	WPR+9		
30402	0	13100	0	00000	2163	+23	XCA			
30403	0	56000	0	40256	2164	+24	LDQ	FL,8		
30404	-0	12000	0	30433	2165	+25	TMI	AYH1		
30405	0	07400	4	27021	2166	+26	TSX	AZE,4		
30406	0	60100	0	12526	2167	+27	STO	COMMON+12		
30407	0	50000	0	33731	2168	+28	CLA	WPR+7		
30410	0	24100	0	33732	2169	+29	FDP	WPR+8		
30411	0	26000	0	33733	2170	+30	FHP	WPR+9		
30412	0	56000	0	40226	2171	+31	LDQ	FL,4		
30413	-0	12000	0	30433	2172	+32	TMI	AYH1		
30414	0	07400	4	27021	2173	+33	TSX	AZE,4		
30415	0	13100	0	00000	2174	+34	XCA			
30416	0	26000	0	12526	2175	+35	FHP	COMMON+12		
30417	0	24100	0	33741	2176	+36	FDP	TP+4	0	
30420	0	26000	0	12524	2177	+37	FHP	COMMON+10		
30421	0	13100	0	00000	2178	+38	XCA			
30422	0	26000	0	12525	2179	+39	FHP	COMMON+11		
30423	0	13100	0	00000	2180	+40	XCA			
30424	0	26000	0	33732	2181	+41	FHP	WPR+8	K	
30425	0	13100	0	00000	2182	+42	XCA			
30426	0	26000	1	00002	2183	+43	FHP	2,1	GAMMA	
30427	0	60100	0	32622	2184	+44	STO	P+4	HF	

30430 0 77400 4 00000 2185 AYMR AXT \*\*0,4  
 30431 0 77400 1 00000 2186 \*1 AXT \*\*0,1  
 30432 0 02000 4 00002 2187 \*2 TRA 2,4  
 30433 -1 30434 0 25417 2188 AYV1 STR AZPF,,AYM2  
 30434 2 33025 2 34260 2189 AYV2 BCI 3,CHECK DUMP FOR NEG

2191\*REGION TO COMPUTE TEMP CHANGE IN AN ISOENTROPIC PRESS CHANGE

30437 0 63400 4 30450 2192 AYI SXA AYIR,4  
 30440 0 60100 0 34016 2193 \*1 STO TP+49 P2  
 30441 0 50000 0 34065 2194 \*2 CLA TP+88 T1  
 30442 0 54000 0 32674 2195 \*3 LDQ P+46 P2  
 30443 0 07400 4 41043 2196 \*4 TSX S(TP),4  
 30444 0 30200 0 34062 2197 \*9 FSB TP+85 S  
 30445 0 24100 0 34005 2198 \*6 FDP TP+40 S-SP  
 30446 0 26000 0 30452 2199 \*7 FMP AYI1 DELT  
 30447 0 30000 0 34065 2200 \*8 FAD TP+88 T1  
 30450 0 77400 4 00000 2201 AYIR AXT \*\*0,4  
 30451 0 02000 4 00001 2202 \*1 TRA 1,4  
 30452 2 02400 0 00000 2203 AYI1 DEC 2.

2205\*REGION TO COMPUTE CONSTANT ENTROPIES FOR AYI

30453 0 63400 4 30511 2206 AYI1 SXA AYIIR,4  
 30454 0 50000 0 34065 2207 \*1 CLA TP+88 T1  
 30455 0 54000 0 34064 2208 \*2 LDQ TP+87 P1  
 30456 0 07400 4 41043 2209 \*3 TSX S(TP),4  
 30457 0 60100 0 34062 2210 \*4 STO TP+85 S  
 30460 0 50000 0 34065 2211 \*5 CLA TP+88 T1(I+1)  
 30461 0 60100 0 33742 2212 \*6 STO TP+5  
 30462 0 54000 0 34064 2213 \*7 LDQ TP+87 P1(I+1)  
 30463 0 07400 4 25544 2214 \*8 TSX AZH,4  
 30464 -1 25176 0 25417 2215 \*9 STR AZFF,,AZAB2  
 30465 0 50000 0 33730 2216 \*10 CLA WPR+6  
 30466 0 60100 0 34017 2217 AYI11 STO TP+50  
 30467 0 50000 0 33724 2218 \*1 CLA WPR+2  
 30470 0 60100 0 34070 2219 \*2 STO TP+91 H1(I+1)  
 30471 0 50000 0 34065 2220 \*3 CLA TP+88 T1  
 30472 0 30000 0 30452 2221 \*4 FAD AYI1 DELT  
 30473 0 54000 0 34064 2222 \*5 LDQ TP+87 P1  
 30474 0 07400 4 41043 2223 \*6 TSX S(TP),4  
 30475 0 30200 0 34062 2224 \*7 FSB TP+85 S  
 30476 0 76000 0 00002 2225 \*8 CMS  
 30477 0 60100 0 34005 2226 \*9 STO TP+40 S-SP  
 30500 0 07400 4 27142 2227 \*10 TSX AZV,4 VAPOR PRESSURE  
 30501 0 30200 0 34064 2228 \*11 FSB TP+87 P1  
 30502 -0 12000 0 30504 2229 \*12 TMI \*\*2  
 30503 -1 30513 0 25417 2230 \*13 STR AZFF,,AYI12  
 30504 0 76000 0 00002 2231 \*14 CMS  
 30505 0 24100 0 34017 2232 \*15 FDP TP+50 RHO1  
 30506 0 13100 0 00000 2233 \*16 XCA  
 30507 0 24100 0 40225 2234 \*17 FDP FL12  
 30510 -0 60000 0 32636 2235 \*18 STO P+16 HSV(I+1)  
 30511 0 77400 4 00000 2236 AYIIR AXT \*\*0,4  
 30512 0 02000 0 00001 2237 \*1 TRA 1,4

30513 2 72162 6 02163 2238 AYI12 BCI 3,GAS AT PUMP INLET

2240\*REGION TO COMPUTE ETA T -- N/ROOT T IN AC

30516 0 60100 0 34023 2241 AYJ STO TP+54  
 30517 0 54000 0 30525 2242 \*1 LDQ AYJ1  
 30520 0 26000 0 34023 2243 \*2 FMP TP+54  
 30521 0 30000 0 30526 2244 \*3 FAD AYJ1+1  
 30522 0 13100 0 00000 2245 \*4 XCA  
 30523 0 26000 0 34023 2246 \*5 FMP TP+54  
 30524 0 02000 4 00001 2247 \*6 TRA 1,4  
 30525 -1 54523 1 45747 2248 AYJ1 DEC -6318076E-13,11039226E-10

2250\*REGION TO COMPUTE PUMP CHARACTERISTICS

30527 0 63400 4 30603 2251 AYK SXA AYKR,4  
 30530 0 63400 1 30604 2252 \*1 SXA AYKR+1,1  
 30531 0 44100 4 00000 2253 \*2 LDI 0,4  
 30532 -0 05700 0 00002 2254 \*3 RIL 2 RESET PARABOLA FLAG  
 30533 -0 77400 1 31023 2255 \*4 AXK AYK1,1  
 30534 -0 05400 0 00001 2256 \*5 LFT 1 I IN DECREMENT OF TSX = HEAD DESIRED  
 30535 0 02000 0 31076 2257 \*6 TRA AYK9 MARK 4 MOD 4 PUMP  
 30536 0 50000 0 33773 2258 \*7 CLA TP+30 HSV/NSQ.  
 30537 0 54000 0 31065 2259 \*8 LDQ AYK3 HSV/NSQ MAX  
 30540 0 04000 0 30542 2260 \*9 TLQ \*\*2  
 30541 0 13100 0 00000 2261 \*10 XCA  
 30542 0 26000 0 40235 2262 \*11 FMP FL12E8  
 30543 0 13100 0 00000 2263 \*12 XCA  
 30544 0 26060 4 00001 2264 \*13 FMP+ 1,4 RHO  
 30545 0 30000 0 40214 2265 \*14 FAD FL2  
 30546 0 60100 0 12512 2266 \*15 STO COMMON  
 30547 0 50000 0 40213 2267 \*16 CLA FL1  
 30550 0 24100 0 12512 2268 \*17 FDP COMMON  
 30551 -0 60000 0 12512 2269 \*18 STO COMMON X2  
 30552 0 50000 0 31066 2270 \*19 CLA AYK3+1 .36  
 30553 0 30200 0 34000 2271 \*20 FSB TP+35 Q/N  
 30554 0 60100 0 12513 2272 \*21 STO COMMON+1 X1  
 30555 -0 12000 0 30606 2273 \*22 TMI AYK4 IF PLUS USE -A- CURVE  
 30556 0 56000 1 00005 2274 \*23 LDQ 5,1 A5  
 30557 0 26000 0 12512 2275 \*24 FMP COMMON X2  
 30560 0 30000 1 00004 2276 \*25 FAD 4,1 A4  
 30561 0 13100 0 00000 2277 \*26 XCA  
 30562 0 26000 0 12513 2278 \*27 FMP COMMON+1 X1  
 30563 0 60100 0 12514 2279 \*28 STO COMMON+4  
 30564 0 56000 1 00003 2280 \*29 LDQ 3,1 A3  
 30565 0 26000 0 12512 2281 \*30 FMP COMMON  
 30566 0 30000 1 00001 2282 \*31 FAD 1,1  
 30567 0 30000 0 12516 2283 \*32 FAD COMMON+4  
 30570 0 13100 0 00000 2284 \*33 XCA  
 30571 0 26000 0 12513 2285 \*34 FMP COMMON+1 X1  
 30572 0 60100 0 12517 2286 \*35 STO COMMON+5  
 30573 0 56000 1 00002 2287 \*36 LDC 2,1  
 30574 0 26000 0 12512 2288 \*37 FMP COMMON .2  
 30575 0 30000 1 00000 2289 \*38 FAC 0,1 A0



Table with columns for job ID, region, and various numerical values. Rows range from 30752 to 31073.

Table with columns for job ID, region, and various numerical values. Rows range from 30752 to 31073. Includes labels like FMP, STO, XCA, FAD, LDO, FSB, FDP, TRA, AYK1, AYK2, AYK3.

Table with columns for job ID, region, and various numerical values. Rows range from 30752 to 31073. Includes labels like XI, PARTIAL Z WRT Q/N AT Q/N PRIME, D, G, DEMINOMATOR, E, D, F, F, D, D, G, C, G, E, DENOM, B, E, F, DENOM, A, Q/N, B, Q/N, C, AYKB.

Table with columns for job ID, region, and various numerical values. Rows range from 31074 to 31515.

Table with columns for job ID, region, and various numerical values. Rows range from 31074 to 31515. Includes labels like AYK1, AYK9, AYK01, AYK02.

Table with columns for job ID, region, and various numerical values. Rows range from 31074 to 31515. Includes labels like X3 CNST, EQN B CNST, HSV/N\*\*2, RHO1, NPSP/NSQ, MAXIMUM NPSP/NSQ, Q/N, X3 CNST, EQN B CNST, NPSP/NSQ, MAXIMUM NPSP/NSQ.

2490\*REGION TO COMPUTE WORK REQUIRED TO DRIVE THE PUMP

Table with columns for job ID, region, and various numerical values. Rows range from 31501 to 31515.

Table with columns for job ID, region, and various numerical values. Rows range from 31501 to 31515. Includes labels like AYL, SXA, CLA, STA, TSX, PZE, TZE, STO, CLA\*, FDP, FMP\*, STO\*, AYL\*, AXT, TRA.

Table with columns for job ID, region, and various numerical values. Rows range from 31501 to 31515. Includes labels like AYL, SXA, AYLR,4, AYLP,1, \*+2, AYK,4,0, \*\*0,0, AYL2, COMMON, AYLH,1, COMMON, WDOTP, AYL0,1, DELH, AYL1,1, \*\*0,4, 1,4.









Table with 7 columns: ID, Value 1, Value 2, Value 3, Value 4, Label, Description. Includes entries like 32201 -0 63400 4 00061 2821 +4 SXO KENDX4,4 and 32325 -0 71060 2 34362 2873 +23

Table with 7 columns: ID, Value 1, Value 2, Value 3, Value 4, Label, Description. Includes entries like 32327 -2 62446 6 36023 2875 +25 and 32475 3 77776 4 32513 2928 +5 TXH PP09,4,-2

32476	1	00001	4	32477	2929	+6	TXI	0*1,4,1
32477	-0	63400	4	40316	2930	+7	SXD	PP41,4
32500	0	02000	0	32513	2931	+8	TRA	PP09
32501	0	53400	4	32470	2932	PP07	LXA	PP06,4
32502	0	63400	4	32810	2933	+1	SXA	PP08,4
32503	0	07400	4	00052	2934	+2	TSX	DOU4,4
32504	3	01757	0	40317	2935	PP075	PTH	HEADER,,1007
32505	0	15947	0	00001	2936	+1	PZE	1,,7015
32506	-1	00024	0	00012	2937	+2	FVE	KPRINT,,20
32507	0	07400	4	00052	2938	+3	TSX	DOU4,4
32510	-2	17515	0	32616	2939	PP08	SIX	P,,8013
32511	0	15947	0	00001	2940	+1	PZE	1,,7015
32512	-1	00012	0	00012	2941	+2	FVE	KPRINT,,10
32513	0	53400	4	32504	2942	PP09	LXA	PP075,4
32514	1	00010	4	32515	2943	+1	TXI	0*1,4,8
32515	0	63400	4	32504	2944	+2	SXA	PP075,4
32516	0	53400	4	32470	2945	+3	LXA	PP06,4
32517	1	00010	4	32520	2946	+4	TXI	0*1,4,8
32520	0	63400	4	32470	2947	+5	SXA	PP06,4
32521	2	00001	2	32467	2948	+6	TXI	PP05,2,1
32522	0	77400	4	00000	2949	PP97	AXT	,4
32523	0	77400	2	00000	2950	PP98	AXT	,2
32524	0	77400	1	00000	2951	PP99	AXT	,1
32525	0	02000	4	00001	2952	+1	TRA	1,4
32526	0	07401	4	32541	2953	PZ	TSX	PL,4,1
32527	-0	53400	4	32575	2954	+1	LXD	COUNT,4
32530	3	00001	4	32533	2955	+2	TXH	PA,4,1
32531	0	07400	4	32563	2956	+3	TSX	PC,4
32532	-1	00024	0	00012	2957	+4	FVE	KPRINT,,20
32533	0	07400	4	00052	2958	PA	TSX	DOU4,4
32534	-2	13621	0	32616	2959	+1	SIX	P,,6033
32535	0	11625	0	00001	2960	+2	PZE	1,,5013
32536	-2	13737	0	32631	2961	+3	SIX	P*11,,6111
32537	-1	00012	0	00012	2962	+4	FVE	10,,10
32540	0	02000	0	32522	2963	+5	TRA	PP97

PRINT COLUMN HEADS

2964\*SUBROUTINE TO TEST LINE COUNT AND PRINT PAGE HEAD

32541	0	63400	4	32561	2965	PL	SXA	PLR,4
32542	0	44100	4	00000	2966	+1	LDI	0,4
32543	-0	05700	7	77700	2967	+2	RIL	777700
32544	-0	04600	0	00000	2968	+3	PIA	
32545	0	42200	0	32556	2969	+4	STD	PF
32546	-0	53400	4	32575	2970	+5	LXD	COUNT,4
32547	3	00000	4	32556	2971	+6	TXH	PF,4,0
32550	0	07400	4	00052	2972	PL1	TSX	DOU4,4
32551	3	27451	0	32577	2973	+1	PTH	TCARD,,12073
32552	3	04110	0	00036	2974	+2	PTH	KDATEA,,2120
32553	3	04124	0	32573	2975	+3	PTH	PL2,,2132
32554	-1	00001	0	00012	2976	+4	FVE	KPRINT,,1
32555	0	77400	4	00000	2977	+5	AXT	0,4
32556	1	00000	4	32557	2978	PF	TXI	*1,4,*0
32557	3	00067	4	32550	2979	+1	TXH	PL1,4,NLMAX
32560	-0	63400	4	32575	2980	PG	SXD	COUNT,4
32561	0	77400	4	00000	2981	PLR	AXT	*0,4

2983\*SUBROUTINE TO PRINT COLUMN HEADS

32563	-0	63400	4	00061	2984	PC	SXD	KINDX4,4
32564	0	07400	4	00052	2985	+1	TSX	DOU4,4
32565	3	02011	C	40317	2986	+2	PTH	HEADER,,1033
32566	0	11625	0	00001	2987	+3	PZE	1,,5013
32567	3	02127	C	40332	2988	+4	PTH	HEADER+11,,1111
32570	1	00000	4	00001	2989	+5	PON	1,4
32571	-0	53400	4	00061	2990	+6	LXD	KINDX4,4
32572	0	C2000	4	00002	2991	+7	TRA	2,4
32573	-2	06633	6	04633	2992	PL2	BCI	2, W. O.= 0718

CONFIDENTIAL R D WORK ORDER NO.

32575	0	00000	0	00000	2994	COUNT	PZE	0,,0
32576	0	02000	0	42566	2995	ENDD	TRA	END

32577	2997	TCARD	BSS	15,0
32616	2998	P	BSS	64,F
32716	2999	X	BSS	25,0
32747	3000	C	BSS	20,F
32773	3001	WTI	BSS	147,F
33216	3002	WPI	BSS	147,F
33441	3003	WPO	BSS	147,F
33664	3004	WGP	BSS	30,F
33722	3005	WPR	BSS	10,F
33734	3006	COLUM	BSS	1,F
33735	3007	TP	BSS	100,F
34101	3008	AZMTB	EQU	*+1
34101	3009	*BEGINNING OF PART STORAGE		
34163	3010	AZ02	BSS	NZMAX,F
34245	3011	AZ03	BSS	NZMAX,F
34327	3012	AZ04	BSS	NZMAX,F
34411	3013	AZ05	BSS	NZMAX,F
34473	3014	AZ07	BSS	NZMAX,F
34555	3015	AZ09	BSS	NZMAX,F
34567	3016	FX	BSS	10,0
34625	3017	WAF	BSS	30,F
34663	3018	WFP	BSS	30,F
34721	3019	WH	BSS	30,F
35144	3020	WMT	BSS	147,F
35367	3021	WK	BSS	147,F
35612	3022	WCR	BSS	147,F
35612	3024	PT	BSS	20,F
35636	3025	AZ01	BSS	NZMAX,F
35720	3026	AZ06	BSS	NZMAX,F
36002	3027	AZ08	BSS	NZMAX,F
36064	3028	D	EQU	*+1
36064	3029	DELZ	BSS	1,F
36065	3030	DNMAX	BSS	1,F
36066	3031	DFE	BSS	1,F
36067	3032	DVF	BSS	1,F
36070	3033	DRHOR	BSS	1,F

PERMANENT STORAGE  
 FIXED POINT AND OCTAL STORAGE  
 SOME PROG CNSTS (FLOATING PT)  
 INLET TEMP  
 INLET PRESS  
 OUTLET PRESS  
 GATE POSITION  
 PROPERTIES OF PARA HYDROGEN

TEMPORARY STORAGE  
 BEGINNING OF PART STORAGE

TEMPORARY FLOW RATE, LB/SEC  
 FLUID TEMPS, DEGR  
 PRESSURE, PSIA  
 FILM COEFF, BTU/IN<sup>2</sup>-SEC-DEGR  
 NEW FLUID DENSITIES, LB/IN<sup>3</sup>  
 CSUBP

FLOW AREA  
 WETTED PERIMETER  
 FRACT HEAT GEN VS DISTANCE  
 INT HEAT GEN VS TIME  
 THERMAL CONDUCTIVITY  
 HEAT CAPACITY OF METAL

FLOATING POINT STORAGE, EACH PART  
 OLD METAL TEMPS, DEGR  
 OLD DENSITIES, LB/IN<sup>3</sup>  
 PERMANENT FLOW RATE, LB/SEC  
 INPUT STORAGES  
 POSITION INCREMENT, IN  
 \*NC. POSITION PTS, 3= IGNORE THIS PT  
 FRICTION FACTOR  
 VOID FRACTION  
 METAL DENSITY

36071 3034 DPX BSS 1,F  
 36072 3035 DKDPI BSS 1,F  
 36073 3036 DRDPO BSS 1,F  
 36074 3037 DVI BSS 1,F  
 36075 3038 DVO BSS 1,F  
 36076 3039 AZMTE EQU \*+1  
 3040\*\*PART STORAGE ENDS HERE  
 36076 3041 ORG D+10  
 36076 3042 DPR1 BSS 1,F  
 36077 3043 DTMI BSS 1,F  
 36100 3044 DELT BSS 1,F  
 36101 3045 DNOT BSS 1,F  
 36102 3046 DNOT BSS 1,F  
 36103 3047 DTHO BSS 1,F  
 36104 3048 DTMIN BSS 1,F  
 36105 3049 DTMAX BSS 1,F  
 36106 3050 DOIL BSS 1,F  
 36107 3051 DPTI BSS 1,F  
 36110 3052 DTI BSS 1,F  
 36111 3053 DPO BSS 1,F  
 36112 3054 DPBE BSS 1,F  
 36113 3055 DP12E BSS 1,F  
 36114 3056 DNP BSS 1,F  
 36115 3057 DMC BSS 1,F  
 36116 3058 DMH BSS 1,F  
 36117 3059 DMCE BSS 1,F  
 36120 3060 DMRE BSS 1,F  
 36121 3061 DA6 BSS 1,F  
 36122 3062 CASTR BSS 1,F  
 36123 3063 DNZFF BSS 1,F  
 36124 3064 DNP BSS 1,F  
 36125 3065 DNT BSS 1,F  
 36126 3066 DQINT BSS 1,F  
 36127 3067 DSWT BSS 1,F  
 36130 3068 DGP BSS 1,F  
 36131 3069 DAKV BSS 1,F  
 36132 3070 DBKV BSS 1,F  
 36133 3071 DK BSS 1,F  
 36134 3072 DK2 BSS 1,F  
 36135 3073 DD2 BSS 1,F  
 36136 3074 ODH BSS 1,F  
 36137 3075 ODTL BSS 1,F  
 36140 3076 ODTN BSS 1,F  
 36141 3077 DORN BSS 1,F  
 36142 3078 DIPT BSS 1,F  
 36143 3079 DNI BSS 1,F  
 36144 3080 DHE BSS 1,F  
 36145 3081 DMPE BSS 1,F  
 36146 3082 OL BSS 1,F  
 36147 3083 ONX BSS 1,F  
 36150 3084 ODCO BSS 1,F  
 36151 3085 DMH BSS 1,F  
 36152 3086 DT BSS 1,F  
 36153 3087 DT BSS 1,F

\*WALL THICK, IN, NOT 0= PIPE OPTION  
 R FOR INLET PRESS DROP, 1/IN4  
 R FOR OUTLET PRESS DROP, 1/IN4  
 INLET PLENUM, IN3  
 OUTLET PLENUM, IN3  
 END OF PART STORAGE  
 WHOLE ENGINE SYSTEM INPUT  
 PRINT INTERVAL  
 \*INIT TIME, NOT 0= RESTART PROGRAM  
 TIME INCREMENT, SEC  
 NO. TIME INCREMENTS  
 MINIMUM TIME INTERVAL, SEC  
 INITIAL METAL TEMP, DEGR  
 MIN OUTLET METAL TEMP, DEGR  
 MAX ALLOWABLE FLUID TEMP, DEGR  
 STATION FOR REMOVAL OF DILUENT  
 \*TANK PRESSURE, PSIA, 0= USE CURVE  
 TANK TEMPERATURE, DEGR  
 \*MIN OUTLET PRESS, 0= USE CURVE  
 PB CLOSURE  
 P12 CLOSURE  
 INITIAL PUMP FLOW GUESS, LB/SEC  
 INITIAL DILUENT FLOW GUESS, LB/SEC  
 INITIAL HOT BLEED FLOW GUESS, LB/SEC  
 WOOD C CLOSURE  
 WOOD R CLOSURE  
 AREA OF CORE OUTLET, IN2  
 NOZZLE THROAT AREA, IN  
 \*NOZ TUBE FRICT FACTOR, 0= NO TUBES  
 NO. NOZ TUBE SEGMENTS  
 NOZ TUBE WALL THICKNESS, IN  
 INIT P1 FOR NOZ TUBES  
 \*7= PRINT NOZZLE TUBE ITERATIONS  
 \*GATE POSITION, PERCENT, 0=USE CURVE  
 CNST FOR KV COMP  
 CNST FOR KV COMP  
 K FOR KT COMPUTATION  
 K FOR NOZ TUBE INLET LINE  
 DIAM OF NOZ TUBE INLET LINE, IN  
 DIAM OF HOT BLEED PORT, IN  
 DIAM OF TURBINE LINE, SQIN  
 DIAM OF TURBINE NOZZLE, IN  
 DIAM OF ROLL CONTROL NOZZLE, IN  
 MOMENT OF PUMP AND TURBINE, LB-SQIN  
 INITIAL TURBINE SPEED, RPM  
 PUMP HEAD CLOSURE  
 PUMP WORK CLOSURE  
 LENGTH OF HOT BLEED PORT, IN  
 NO. POSITION STEPS IN HBP  
 DIAM OF COLD FLOW HOLES, IN  
 NO. COLD FLOW HOLES  
 THICKNESS OF COLD FLOW ANNULUS, IN  
 \*THICKNESS OF COLD FLOW ANNULUS, IN

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36154 3088 DTHET BSS 1,F  
 36155 3089 TK EQU \*+1  
 36155 3090 BSS 1  
 36156 3091 DA BSS 1,F  
 36157 3092 DB BSS 1,F  
 36160 3093 DC BSS 1,F  
 36161 3094 DAHOT BSS 1,F  
 36162 3095 DBHOT BSS 1,F  
 36163 3096 DCHOT BSS 1,F  
 36164 3097 DFCLD BSS 1,F  
 36165 3098 DFBOT BSS 1,F  
 36166 3099 BSS 1  
 36167 3100 DKPHM BSS 1,F  
 36170 3101 DKPCM BSS 1,F  
 36171 3102 DKIN BSS 1,F  
 36172 3103 DKCC BSS 1,F  
 36173 3104 DKCI BSS 1,F  
 36174 3105 DRC BSS 1,F  
 36175 3106 DRH BSS 1,F  
 36176 3107 DK11 BSS 1,F  
 36177 3108 DK9 BSS 1,F  
 36200 3109 DKE BSS 1,F  
 36201 3110 DP11 BSS 1,F  
 36202 3111 DT11 BSS 1,F  
 36203 3112 DKFLG BSS 1,F  
 36204 3113 ORG D+80  
 36204 3114 BELLO BSS 20,F  
 36230 3115 ORG D+100  
 36230 3116 AZD BSS 100\*NCURV,F  
 40177 3117 AZMTC EQU \*

DILUENT IMPINGENT ANGLE, DEG  
 THE NEXT 20 VALUES ARE FOR HBP  
 NOT USED  
 COLD FILM COEFF CNST  
 COLD FILM COEFF CNST  
 COLD FILM COEFF CNST  
 HOT FILM COEFF CNST  
 HOT FILM COEFF CNST  
 HOT FILM COEFF CNST  
 HBP COLD FRICTION FACTOR  
 HBP HOT FRICTION FACTOR  
 NOT USED  
 K FOR PHM,P08,CHM,CC  
 K FOR PCM,CC  
 K FOR DELTA P  
 COMPRESSIBLE  
 INCOMPRESSIBLE  
 COLD GAS CNST  
 HOT GAS CNST  
 K11 FOR P08  
 K9 FOR P08  
 KE FOR P08  
 \*TURBINE INLET PRESS, PSIA, 0=NO BOT  
 TURBINE INLET TEMP, DEGR  
 \*NOT 0=BELLOWS SECTIONS INPUT  
 BELLOWS SECTION INPUT  
 BELLOW SECTION CNSTS,(SEC, K)  
 CURVE INPUT STORAGES  
 D AND AZD MULTIPLES OF 10  
 END OF ALL CURVES

40200 0 00000 0 00001 3119 FX1 PZE 1  
 40201 0 00000 0 00002 3120 FX2 PZE 2  
 40202 0 00000 0 00003 3121 FX3 PZE 3  
 40203 0 00000 0 00004 3122 FX4 PZE 4  
 40204 0 00000 0 00005 3123 FX5 PZE 5  
 40205 0 00000 0 00006 3124 FX6 PZE 6  
 40206 0 00000 0 00007 3125 FX7 PZE 7  
 40207 0 00000 0 00010 3126 FX8 PZE 8  
 40210 0 00000 0 00011 3127 FX9 PZE 9  
 40211 0 00000 0 00012 3128 FX10 PZE 10  
 40212 0 00000 0 01750 3129 FX1E3 PZE 1000  
 40213 2 01400 0 00000 3130 FL1  
 40214 2 02400 0 00000 3131 FL2  
 40215 2 02600 0 00000 3132 FL3  
 40216 2 03400 0 00000 3133 FL4  
 40217 2 03500 0 00000 3134 FL5  
 40220 2 03600 0 00000 3135 FL6  
 40221 2 03700 0 00000 3136 FL7  
 40222 2 04400 0 00000 3137 FL8  
 40223 2 04440 0 00000 3138 FL9  
 40224 2 04500 0 00000 3139 FL10

40226	1	77631	4	63146	3141	FL.4	DEC	.4
40227	2	00714	6	31463	3142	FL.9	DEC	.9
40230	2	01431	4	63146	3143	FL1.1	DEC	1.1
40231	2	01463	1	46315	3144	FL1.2	DEC	1.2
40232	2	01600	0	00000	3145	FL1.5	DEC	1.5
40233	2	00746	3	14632	3146	FL.95	DEC	.95
40234	2	21606	5	00000	3147	FL1E5	DEC	1E5
40235	2	37436	0	64300	3148	FL12E8	DEC	12E8
40236	2	11601	5	77627	3149	FL6	DEC	385.7496
40237	2	12602	2	00000	3150	FLR	DEC	772.5
40240	2	00774	3	15101	3151	FLRB	DEC	.99297
40241	1	76435	7	15153	3152	FL139	DEC	.1396
40242	2	12604	7	70244	3153	FL776	DEC	777.97
40243	1	70444	0	16431	3154	FLGAL	DEC	.002228
40244	2	10440	0	00000	3155	FL144	DEC	144.
40245	2	13660	0	00000	3156	FLCUF	DEC	1728.
40246	2	16521	4	00000	3157	FL108	DEC	10800.
40247	2	07763	1	46315	3158	FL2RW	DEC	124.8
40250	1	75631	4	63146	3159	FL.1	DEC	.1
40251	1	76631	4	63146	3160	FL.2	DEC	.2
40252	1	76700	4	06112	3161	FL.219	DEC	.219
40253	1	77400	0	00000	3162	FL.25	DEC	.25
40254	2	00400	0	00000	3163	FL.5	DEC	.5
40255	2	00463	1	46315	3164	FL.6	DEC	.6
40256	2	00631	4	63146	3165	FL.8	DEC	.8
40257	2	02671	4	63146	3166	FL3.45	DEC	3.45
4026C	2	06602	1	72703	3167	FL48.2	DEC	48.28
40261	2	06720	C	00000	3168	FL58	DEC	58.0
40262	2	02731	4	63146	3169	FL3.7	DEC	3.7
40263	2	07410	0	00000	3170	FL66	DEC	66.
40264	2	07620	0	00000	3171	FL100	DEC	100.
40265	2	10401	4	63146	3172	FL128.	DEC	128.8
40266	2	10550	0	00000	3173	FL180	DEC	180.
40267	2	11440	0	00000	3174	FL288	DEC	288.
40270	2	12764	0	00000	3175	1000.	DEC	1000.
40271	2	02622	0	77327	3176	FLPI	DEC	3.1415927
40272	2	06401	3	10721	3177	FLGF	DEC	32.17405
40273	2	07401	3	10721	3178	FL2G	DEC	64.3481
40274	2	12601	5	77627	3179	FL2GI	DEC	771.4992
40275	2	02622	0	77324	3180	PI		
40276	2	03622	0	77325	3181	2PI		
40277	1	73435	7	50646	3182	RAD		
40300	2	06712	2	73406	3183	DEG		
						3184*OCTAL CONSTANTS		
40301	0	01000	0	00000	3185	188	DEC	188
40302	0	02000	0	00000	3186	288	DEC	288
40303	0	00000	0	00000	3187	ZERO	PZE	0,,0
40304	-2	06060	6	06060	3188	BLANK		
40305	3	77777	7	77777	3189	BIG	OCT	37777777777
40306	2	33000	0	00000	3190	FIX	OCT	233000000000

GRAVITY, IN-LB/LBF-SEC  
 GAS CNST, FT-LBF/LB-DEGR  
 GAS CNST, BTU/LB-DEGR  
 LB-DEGR\*\*./SEC-LBF  
 FT-LBF/BTU  
 FT\*\*3-MIN/GAL-SEC  
 SQIN/SQFT  
 CUIN/CUFT  
 2\*DENSTY OF WATER, LB/FT3

GRAVITY, FT-LB/LBF-SEC2  
 2\*GRAVITY, IN-LB/LBF-SEC2

40307 2 12060 6 06060 3192 BCDD BCI 1

40310	0	00000	0	00000	3193	CUT	PZE	0
40311	-0	75146	2	75121	3194	PR60		
40312	-0	46031	4	54764	3195		+1	
40313	-2	36060	6	06060	3196		+2	
40314	0	40307	0	36064	3197	PR61	PZE	D,,BCDD
40315	0	40317	0	32616	3198	PP40	PZE	P,,HEDER
40316	0	00000	0	00000	3199	PP41	PZE	0,,0
40317	-3	16024	3	16263	3200	HEDER		
40320	-0	42563	4	36063	3201		+1	
40321	2	64364	2	46063	3202		+2	
40322	-0	75125	6	26260	3203		+3	
40323	2	63143	4	46023	3204		+4	
40324	-2	05130	4	66060	3205		+5	BCI 1, RHO
40325	-2	06045	6	06060	3206		+6	
40326	-2	06261	0	26060	3207		+7	
40327	3	06360	2	72545	3208		+8	
40330	-2	06044	6	06060	3209		+9	BCI 1, M
40331	-2	33144	2	56060	3210		+10	
40332	-2	62446	6	36051	3211		+11	
40333	-2	02225	6	32160	3212		+12	
40334	-2	06360	0	66060	3213		+13	
40335	-1	16360	6	30660	3214		+14	
40336	3	06265	6	03160	3215		+15	BCI 2,HSV I HSVI+1
40340	2	42543	6	06360	3216		+17	
40341	-0	74660	4	43145	3217		+18	
40342	-1	00131	4	53163	3218		+19	
40343	-2	06060	6	06060	3219		+20	
40344	-2	62446	6	36047	3220		+21	
40345	-2	62446	6	36023	3221		+22	
40346	-2	62446	6	36030	3222		+23	
40347	-2	62446	6	36045	3223		+24	BCI 8, WDOT WDOT T
40357	-2	04760	0	66060	3224		+32	NT CHK P 1 T 1 P 2 T 2
40367	-0	57431	2	00134	3225		+40	8, P 6 G P P 8 T 8 P 11 T 11 P 12 N(I)
40370	-2	64721	2	36360	3226		+41	
40371	-2	64721	3	12001	3227		+42	
40372	-2	66321	2	36360	3228		+43	
40373	-2	66321	3	12001	3229		+44	
40374	2	14347	3	02160	3230		+45	
40375	-0	70260	3	12001	3231		+46	
40376	-2	30260	3	12001	3232		+47	
40377	2	43060	3	12001	3233		+48	
40400	-2	64760	3	12001	3234		+49	
40401	-1	04760	3	12001	3235		+50	
40402	-2	06060	6	06060	3236		+51	
40403	-2	04760	0	36060	3237		+52	
40404	-2	06360	0	36060	3238		+53	
40405	-2	04760	2	36060	3239		+54	
40406	-2	06360	2	36060	3240		+55	

3242\*NEWTONS ITERATION ROUTINE FOR ONE VARIABLE  
 3243\*CLOSURE IN AC, MAX AND MIN SET  
 3244\* TSX NENA,4  
 3245\* P7E

	PZE	(IYPRIME),MAX NO. ITERATIONS	NON-CONVERGENCE EXIT	EVALUATE
40407	0 40100 0 40473	3246*		
40410	0 40000 0 40475	3247*		
40411	-0 50000 4 00001	3248*		
40412	0 62100 0 40524	3249*		
40413	0 62100 0 40533	3250*		
40414	0 62100 0 40537	3251	CONVERGED	
40415	0 62100 0 40542	3252		
40416	0 62100 0 40433	3253		
40417	0 77100 0 00022	3254		
40420	0 62100 0 40477	3255		
40421	0 62100 0 40504	3256		
40422	-0 50000 4 00002	3257		
40423	0 62100 0 40504	3258		
40424	0 77100 0 00022	3259		
40425	0 62100 0 40427	3260		
40426	0 43400 4 40432	3261		
40427	0 77400 4 00000	3262		
40430	-2 00001 4 40441	3263		
40431	0 63400 4 40427	3264		
40432	0 77400 4 00000	3265		
40433	0 50000 0 00000	3266		
40434	0 56000 0 40471	3267		
40435	0 04000 0 40450	3268		
40436	0 56000 0 40472	3269		
40437	0 04000 4 00004	3270		
40440	0 50000 0 40251	3271		
40441	-0 52000 0 40475	3272		
40442	0 02000 0 40452	3273		
40443	0 13100 0 00000	3274		
40444	0 30000 0 40474	3275		
40445	0 24100 0 40214	3276		
40446	-0 60060 0 40433	3277		
40447	0 02000 0 40427	3278		
40450	0 50200 0 40253	3279		
40451	0 02000 0 40441	3280		
40452	0 60100 0 12512	3281		
40453	0 50060 0 40433	3282		
40454	-0 13000 0 00000	3283		
40455	0 26000 0 12512	3284		
40456	0 30060 0 40433	3285		
40457	0 60160 0 40433	3286		
40460	0 02000 0 40427	3287		
40461	0 52200 0 40432	3288		
40462	0 02000 4 00003	3289		
40463	0 56060 0 40433	3290		
40464	-0 60000 0 40471	3291		
40465	0 02000 0 40450	3292		
40466	0 56060 0 40433	3293		
40467	-0 60000 0 40472	3294		

40470	0 02000 0 40440	3300	+2 TRA	NEWA3-1	
		40471		BSS	2,F
		40473		BSS	3,F
40476	2 00746 3 14632	3303	-1 DEC		.95
40477	0 50000 0 00000	3304	RAPA CLA	**0	Y1
40500	-0 34000 0 40473	3305	+1 LAS	NEWA1	
40501	0 02000 0 40504	3306	+2 TRA	**3	
40502	0 02000 0 40504	3307	+3 TRA	**2	
40503	0 02000 0 40544	3308	+4 TRA	RAPA9	
40504	0 30200 0 00000	3309	+5 FSB	**0	Y2
40505	0 60100 0 12514	3310	+6 STO	COMMON+2	NEW E
40506	0 24100 0 00000	3311	RAPA8 FDP	**0	Y1
40507	0 13100 0 00000	3312	+1 XCA		
40510	-0 34000 0 40473	3313	+2 LAS	NEWA1	
40511	0 02000 0 40514	3314	+3 TRA	**3	CLOSURE
40512	0 02000 4 00001	3315	+4 TRA	1,4	
40513	0 02000 4 00001	3316	+5 TRA	1,4	
40514	0 50000 0 40475	3317	+6 CLA	NEWA1+2	OLD E
40515	0 10000 0 40537	3318	+7 TZE	RAPA1	FIRST PASS
40516	0 30200 0 12514	3319	+8 FSB	COMMON+2	
40517	0 10000 0 40537	3320	+9 TZE	RAPA1	E OLD= E NEW
40520	0 60100 0 12512	3321	+10 STO	COMMON	
40521	0 56000 0 12514	3322	+11 LDQ	COMMON+2	NEW E
40522	0 26000 0 40474	3323	+12 FNP	NEWA1+1	OLD X
40523	0 60100 0 12513	3324	+13 STO	COMMON+1	
40524	0 56000 0 00000	3325	RAPA5 LDQ	**0	NEWX
40525	-0 60000 0 40474	3326	+1 STQ	NEWA1+1	
40526	0 26000 0 40475	3327	+2 FNP	NEWA1+2	OLD E
40527	0 30200 0 12513	3328	+3 FSB	COMMON+1	
40530	0 24100 0 12512	3329	+4 FDP	COMMON	
40531	0 76000 0 00012	3330	+5 DCT		
40532	0 02000 0 40537	3331	+6 TRA	RAPA1	
40533	-0 60000 0 00000	3332	RAPA6 STQ	**0	NEW GUESS
40534	0 50000 0 12514	3333	RAPA2 CLA	COMMON+2	
40535	0 60100 0 40475	3334	+1 STO	NEWA1+2	NEW E
40536	0 02000 0 40427	3335	+2 TRA	NEWA2+1	
40537	0 56000 0 00000	3336	RAPA1 LDQ	**0	X
40540	-0 60000 0 40474	3337	+1 STQ	NEWA1+1	OLD X
40541	0 26000 0 40476	3338	+2 FNP	NEWA1+3	BUMPER
40542	0 60100 0 00000	3339	RAPA7 STQ	**0	NEW GUESS
40543	0 02000 0 40534	3340	+1 TRA	RAPA2	
40544	0 30260 0 40504	3341	RAPA9 FSB*	RAPA8-2	
40545	0 60100 0 12514	3342	+1 STO	COMMON+2	
40546	0 02000 0 40510	3343	+2 TRA	RAPA8+2	
40547	0 60100 0 40634	3344	NEWB STQ	NEWB1	
40550	0 60000 0 40636	3345	+1 STZ	NEWB1+2	
40551	-0 50000 4 00001	3346	+2 CAL	1,4	
40552	0 62100 0 40645	3347	+3 STA	RAP85	
40553	0 62100 0 40674	3348	+4 STA	RAP86	
40554	0 62100 0 40700	3349	+5 STA	RAP87	
40555	0 62100 0 40703	3350	+6 STA	RAP87	
40556	0 62100 0 40574	3351	+7 STA	NEWB8	
40557	0 77100 0 00022	3352	+8 ARS	18	
40560	0 62100 0 40640	3353	+9 STA	RAP8	





40740	-0	60000	0	41006	3462	+4	STQ	CURVC+3
40741	0	50000	4	00001	3463	+5	CLA	1,4
40742	0	10000	4	00004	3464	+6	TZE	4,4
40743	-0	73400	2	00000	3465	+7	PDX	,2
40744	-0	63600	2	40767	3466	+8	SCD	CURV7-1,2
40745	0	73400	2	00000	3467	+9	PAX	0,2
40746	0	63400	2	40754	3468	+10	SXA	CURV4,2
40747	-0	63400	2	40773	3469	+11	SXD	CURV8,2
40750	0	50000	4	00003	3470	+12	CLA	3,4
40751	0	62100	0	40760	3471	+13	STA	CURV5
40752	0	40000	0	41004	3472	+14	ADD	CURVC+1
40753	0	62100	0	40764	3473	+15	STA	CURV6
40754	0	77400	4	00000	3474	CURV4	AXT	**0,4
40755	0	77400	1	00000	3475	+1	AXT	0,1
40756	0	77400	2	00000	3476	+2	AXT	0,2
40757	0	63400	4	40770	3477	+3	SXA	CURV7,4
40760	0	50000	1	00000	3478	CURV5	CLA	**0,1
40761	0	60100	2	41007	3479	+1	STQ	CURVC+4,2
40762	0	50000	0	41005	3480	+2	CLA	CURVC+2
40763	0	07400	4	42437	3481	+3	TSX	LINT,4
40764	0	00000	1	00000	3482	CURV6	PZE	**0,1
40765	0	60100	2	41010	3483	+1	STQ	CURVC+5,2
40766	1	77776	2	40767	3484	+2	TXI	**1,2,-2
40767	1	77552	1	40770	3485	+3	TXI	**1,1,-150
40770	0	77400	4	00000	3486	CURV7	AXT	**0,4
40771	2	00001	4	40757	3487	+1	TXI	CURV5-1,4,1
40772	0	07400	4	42511	3488	+2	TSX	LINTS,4
40773	0	00000	0	41007	3489	CURV8	PZE	CURVC+,,**0
40774	0	50000	0	41006	3490	+1	CLA	CURVC+3
40775	0	07400	4	42437	3491	+2	TSX	LINT,4
40776	0	00000	0	41007	3492	+3	PZE	CURVC+4
40777	0	77400	1	00000	3493	CURVR	AXT	**0,1
41000	0	77400	2	00000	3494	+1	AXT	**0,2
41001	0	77400	4	00000	3495	+2	AXT	**0,4
41002	0	02000	4	00004	3496	+3	TRA	4,4
41003	2	33000	0	00000	3497	CURVC	OCT	233000000000
41004	0	00000	0	00001	3498	+1	PZE	1
				41005	3499		BSS	30

\*\*NO Z CURVES

DELTA Z(CURVES)

,,NO. OF Z CURVES

3502\*ENTROPY ROUTINE, TEMP IN AC, PRESS IN MQ

3503*	TSX	S(TP),4
3504*	ENTROPY IN AC	
41043	0	63400 4 41153
3505	S(TP)	SXA STPEX,4
3506		UNLIST
3892		LIST

3894\*AS58 HAS BEEN MODIFIED (SEE AZX)

3895	AS58	CLS 1,4
3896		UNLIST
41664	0	50200 4 00001

42374	0	30000 0 42435	4148	LIST		
			4149	COS	FAD	SIN+32
			4150		UNLIST	
			4181		LIST	
42437	0	60100 0 12912	4182	LINT	STO	COMMON
			4183		UNLIST	
			4270		LIST	

ADD PI/2 FOR COS

STORE ARGUMENT

42566	-0	62500 0 04171	4272	END	UNLESS 1	
					STL	2169
42572	-0	62500 0 04171	4273		CORE	AZN, LAST
				+4	STL	2169
42576	-0	62500 0 04171	4274		CORE	HBI, KSUBM
42602	0	02000 0 42603	4275	ERROR	TRA	**1
			4276		UNLESS 1	
42603	-0	62500 0 04171		+1	STL	2169
42607	-0	62500 0 04171	4277		CORE	BEGIN, PRTO
				+5	STL	2169
42613	-0	62500 0 04171	4278		CORE	NEWA, RAP89
42617	-0	63400 4 00061	4279	+13	SXD	KINDX,4,4
			4280		CORE	-10,10,S,4,4
42620	-0	62500 0 04171		+14	STL	2169
42624	0	07400 4 00055	4281	+18	TSX	KDEBUG,4
42625	-1	01163 0 32716	4282	+19	FVE	X,,AZMTB-X
42626	-1	07764 0 51162	4283	+20	FVE	AZMT,4*AZMTS
42627	-1	00165 0 44277	4284	+21	FVE	TY,,LQ1-TY
42630	-1	23421 0 44514	4285	+22	FVE	LAST,,10001
42631	-1	00226 0 47321	4286	+23	FVE	PR,,150
42632	0	60000 0 33734	4287	+24	STZ	COLUM
42633	0	07400 4 32442	4288	+25	TSX	PRINT,4
42634	0	07400 4 47024	4289	+26	TSX	HBP,4
42635	0	02000 0 24430	4290	+27	TRA	START

4292\*NOZZLE TUBE PROGRAM \*\* HUDSON

4293	AZN	SXA	AZNR,4
4294	+1	SXA	AZNR+1,1
4295	+2	SXA	AZNR+2,2
4296	+3	OCT	
4297	+4	TRA	**1
4298	+5	CLA	AZNS
4299	+6	STO	SHT
4300	+7	AXT	10,4
4301	+8	SXD	ITER5,4
4302	+9	AXT	BUG,4
4303	+10	SXA	ITER9,4
4304	+11	CLA	P+11
4305	+12	STO	WR
4306	+13	OCT	

ITER PRINT FLAG

NO. ITERATIONS

ERROR RETURN CURRENT FLOW RATE

42694 U 02000 0 42694 4307 +14 TRA 0+1  
 42695 0 50000 0 32643 4308 NOZZLE FLOW COMPUTED IGNORING CAPACITANCE  
 42696 0 30200 0 32644 4309 +15 CLA P+21  
 42697 0 30200 0 34045 4310 +16 FSB P+22  
 42698 0 60100 0 32645 4311 +17 FSB TP+72  
 42699 0 60000 0 32724 4312 +18 STD P+24  
 42700 0 60000 0 32724 4313 +19 STZ X+6  
 42701 0 60000 0 32731 4314 +20 STZ X+11  
 42702 0 50000 0 44224 4315 +21 CLA NYOTL  
 42703 0 24100 0 36124 4316 +22 FDP NUMBR  
 42704 0 76000 0 00012 4317 +23 DCT  
 42705 0 07400 4 44235 4318 +24 TSX DIVCK,+4  
 42706 -0 60000 0 44461 4319 +25 STD DELTAZ  
 42707 -0 63400 0 43262 4320 +26 SKD CNT6,0  
 42708 -0 63400 0 43377 4321 +27 SKD CNT7,0  
 42709 -0 63400 0 43460 4322 +28 SKD CNT8,0  
 42710 -0 63400 0 43536 4323 +29 SKD CNT9,0  
 42711 0 80000 0 32633 4324 +30 CLA T6  
 42712 0 30200 0 32620 4325 +31 FSB T3  
 42713 0 13100 0 00000 4326 +32 XCA  
 42714 0 26000 0 44467 4327 +33 FMP KON11  
 42715 0 60100 0 44513 4328 +34 STD MAKER  
 42716 0 56000 0 32633 4329 +35 LDQ T6  
 42717 0 26000 0 44154 4330 +36 FMP LVSBN+1  
 42718 0 13100 0 00000 4331 +37 XCA  
 42719 0 26000 0 44232 4332 +38 FMP KON55  
 42720 0 60100 0 44373 4333 +39 STD THINT  
 42721 0 60100 0 44440 4334 +40 STD TSUBH  
 42722 0 50000 0 32620 4335 +41 CLA T3  
 42723 0 56000 0 32621 4336 +42 LDQ P3  
 42724 0 07400 4 25564 4337 +43 TSX AZH,+4  
 42725 0 02000 0 43576 4338 +44 TRA AZH1  
 42726 0 50200 0 33723 4339 +45 CLS WPR+1  
 42727 0 24100 0 40245 4340 +46 FDP FLCUF  
 42728 0 26000 0 34063 4341 +47 FMP WR  
 42729 0 13100 0 00000 4342 +48 XCA  
 42730 0 26000 0 34063 4343 +49 FMP WR  
 42731 0 13100 0 00000 4344 +50 XCA  
 42732 0 26000 0 44223 4345 +51 FMP KON39  
 42733 0 30000 0 32621 4346 +52 FAD P3  
 42734 0 60100 0 44462 4347 +53 STD PIN  
 42735 0 77400 4 00060 4348 AZH4 AXI 48,+4  
 42736 0 60000 4 44357 4349 +1 STZ TY+48,+4  
 42737 2 00001 4 42725 4350 +2 TIX \*-1,+1  
 42738 0 50000 0 44462 4351 NUTHI CLA PIN  
 42739 0 60100 0 44442 4352 +1 STD PSUBC  
 42740 0 56000 0 32620 4353 +2 CLA T3  
 42741 0 60100 0 44444 4354 +3 STD TSUBC  
 42742 0 60100 0 44453 4355 +4 STD TCH  
 42743 0 50000 0 44373 4356 +5 CLA THINT  
 42744 0 60100 0 44454 4357 +6 STD THW  
 42745 0 50000 0 32641 4358 +7 CLA QHINT  
 42746 0 60100 0 44476 4359 +8 STD Q1  
 42747 0 50000 0 44144 4360 +9 CLA LYSNH+1

LOWER OI GUESS FLAG  
 TOTAL LENGTH

LENGTH OF DELTA Z

MAX ERROR OF CLOSURE BETWEEN T6  
 INPUT AND COMPUTED T6

.98

INITIAL GUESS OF EXIT TEMP

.025

RETURN HERE AFTER OI LOWERED

INITIAL GUESS OF COLD WALL TEMP

INITIAL GUESS OF HOT WALL TEMP  
 RESET OI WITH INITIAL GUESS

42741 0 60100 0 44434 4361 +10 STD DSUBH  
 42742 0 50000 0 44154 4362 +11 CLA LVSBN+1  
 42743 0 60100 0 44434 4363 +12 STD RSUBH  
 42744 0 50000 0 36124 4364 +13 CLA NUMBR  
 42745 0 60100 0 44367 4365 +14 STD NLEFT  
 42746 0 50000 0 44461 4366 +15 CLA DELTAZ  
 42747 0 60100 0 44460 4367 +16 STD NUM  
 42748 0 50000 0 44460 4368 DHRN CLA NUM  
 42749 0 07400 4 44515 4369 +1 TSX TIN1,+4  
 42750 0 00000 0 44143 4370 +2 HTR LVSCH,0,0  
 42751 0 00004 0 00001 4371 +3 HTR 1,0,+4  
 42752 0 60100 0 44435 4372 +4 STD DSUBH+1  
 42753 0 30000 0 44434 4373 +5 FAD DSUBH  
 42754 0 13100 0 00000 4374 +6 XCA  
 42755 0 26000 0 44472 4375 +7 FMP KON8  
 42756 0 60100 0 44413 4376 +8 STD DSUBH1  
 42757 0 50000 0 44460 4377 +9 CLA NUM  
 42758 0 07400 4 44515 4378 +10 TSX TIN1,+4  
 42759 0 00000 0 44153 4379 +11 HTR LVSBN,0,0  
 42760 0 00004 0 00001 4380 +12 HTR 1,0,+4  
 42761 0 60100 0 44437 4381 +13 STD RSUBH+1  
 42762 0 50000 0 44460 4382 +14 CLA NUM  
 42763 0 07400 4 44515 4383 +15 TSX TIN1,+4  
 42764 0 00000 0 44163 4384 +16 HTR LVSCH,0,0  
 42765 0 00007 0 00001 4385 +17 HTR 1,0,+7  
 42766 0 60100 0 44412 4386 +18 STD CH  
 42767 0 50000 0 44440 4387 FINO1 CLA TSUBH  
 42768 0 56000 0 32656 4388 +1 LDQ P+32  
 42769 0 07400 4 25564 4389 +2 TSX AZH,+4  
 42770 0 02000 0 43576 4390 +3 TRA AZH1  
 42771 0 56000 0 33731 4391 +4 LDQ WPR+7  
 42772 0 26000 0 32646 4392 +5 FMP P+24  
 42773 0 60100 0 12512 4393 +6 STD COMMON  
 42774 0 50000 0 44476 4394 +7 CLA Q1  
 42775 0 24100 0 12512 4395 +8 FDP COMMON  
 42776 0 76000 0 00012 4396 +9 DCT  
 42777 0 07400 4 44235 4397 +10 TSX DIVCK,+4  
 42778 -0 60000 0 12512 4398 +11 STD COMMON  
 42779 0 50000 0 44440 4399 +12 CLA TSUBH  
 42780 0 24100 0 44436 4400 +13 FDP RSUBH  
 42781 0 76000 0 00012 4401 +14 DCT  
 42782 0 07400 4 44235 4402 +15 TSX DIVCK,+4  
 42783 0 13100 0 00000 4403 +16 XCA  
 42784 0 30000 0 12512 4404 +17 FAD COMMON  
 42785 0 13100 0 00000 4405 +18 XCA  
 42786 0 26000 0 44437 4406 +19 FMP RSUBH+1  
 42787 0 60100 0 44441 4407 +20 STD TSUBH+1  
 42788 0 30000 0 44440 4408 +21 FAD TSUBH  
 42789 0 13100 0 00000 4409 +22 XCA  
 42790 0 26000 0 44472 4410 +23 FMP KON8  
 42791 0 60100 0 44446 4411 +24 STD TSUBH1  
 42792 0 50000 0 44444 4412 +25 CLA TSUBC  
 42793 0 56000 0 44442 4413 +26 LDQ PSUBC  
 42794 0 07400 4 25564 4414 +27 TSX AZH,+4

DIAMETER AT POINT N

RECOVERY FACTOR AT POINT N  
 NUMBER OF DELTA Z

TOTAL LENGTH USE TO POINT N+M  
 FIND DIAMETER AT POINT N+M N=1,2...

AVERAGE

FIND RECOVERY FACTOR AT POINT N+M

FIND CIRCUM. HOT

P6

FIND C SUB P HOT

NOZZLE FLOW (HOT SIDE)

C SUB P (WR)  
 FIND TEMP AT NEXT SEGMENT OF  
 HOT SIDE

TEMP AT BEGIN OF NEXT SEGMENT

MEAN HOT TEMP OF THE SEGMENT

C SUB P COLD











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44106 -1 00012 0 0001 44106 4955 SNT BSS 1,X
44106 4956 MODE FVE KPRINT,,10
44107 4957* DISTANCE VS COLD FLOW HEAT TRANSFER AREA
44107 4958 LVSAC BSS 1,F
44125 4959* DISTANCE VS COLD FLOW WETTED PERIMETER
44125 4960 LVSCC BSS 1,F
44143 4961* DISTANCE VS DIAMETER TABLE
44143 4962 LVSDM BSS 8,F
44153 4963* DISTANCE VS RECOVERY FACTOR TABLE
44153 4964 LVSRM BSS 8,F
44163 4965* DISTANCE VS CIRCUMFERENCE TABLE OF HOT FLOW AREA
44163 4966 LVSCM BSS 1,F
44201 4967* DISTANCE VS SIGMA
44201 4968 LVSIG BSS 10,F
44223 4969 KON39 BSS 1,F
44224 4970 NTOTL BSS 1,F
44225 4971 KON50 BSS 1,F
44226 4972 KON51 BSS 1,F
44227 4973 KON52 BSS 1,F
44230 4974 KON53 BSS 1,F
44231 4975 KON54 BSS 1,F
44232 4976 KON55 BSS 1,F
44233 4977 AZN5 BSS 2,F
44235 0 63600 4 44514 4978 DIVCK SCA LAST,4
44236 0 02000 0 43556 4979 +1 TRA BUG
44237 2 43165 3 12631 4980 +2 BCI 4, DIVIDING BY 0 AT LOC
44243 0 63600 4 44514 4981 ERLN SCA LAST,4
44244 0 02000 0 43556 4982 +1 TRA BUG
44245 2 55151 4 65160 4983 +2 BCI 7, ERROR WHEN TAKING LN OF A NUMBER LOC
44254 0 63600 4 44514 4984 EREXP SCA LAST,4
44255 0 02000 0 43556 4985 +1 TRA BUG
44256 2 55151 4 65160 4986 +2 BCI 7, ERROR WHEN GETTING EXP. OF A NUMBER LOC
44266 -2 33066 6 06060 4987 LTMW BCI 1, THN
44266 -2 33066 6 06060 4988 LTCM BCI 1, TCM
44267 -2 33033 3 14563 4989 +1 BCI 1, TH,INT
44270 2 14347 3 02160 4990 +2 BCI 1, ALPHA
44271 2 72144 4 42160 4991 +3 BCI 1, GAMMA
44272 2 22563 2 16060 4992 +4 BCI 1, BETA
44273 -2 62143 4 36063 4993 +5 BCI 2, WALL THICK.
44275 2 65131 2 33360 4994 +7 BCI 2, FRIC. FACTOR
44277 4995 TY BSS 48,H
44277 4996 INDAT BSS 8,H
44277 4997 MLEFT BSS 1,D
44277 4998 THENT BSS 3
44277 4999 THENT BSS 1,H
44277 5000 BSS 14
44277 5001 PRICY EQU DNZFF
44277 5002 QIINT EQU P+19
44277 5003 CM BSS 1,D
44277 5004 NUMBR EQU DNP
44277 5005 DSUBM BSS 1,D
44277 5006 BSS 6
44277 5007 BSS 10
44277 5008 XTHIK EQU DMT

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Z AT THROAT, THROAT AREA

STORAGE USE WITH ITERATION ROUTINE

INITIAL GUESS OF EXIT TEMP

NOZZLE TUBE FRICTION FACTOR  
INITIAL Q1 GUESS

NO. PARTS  
AVERAGE OF DIAMETERS N AND N+1

HALL THICKNESS

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44434 5009 DSUBM BSS 2,H
44436 5010 RSUBM BSS 2,H
44440 5011 TSUBM BSS 2,H
44442 5012 PSUBC BSS 2,H
44444 5013 TSUBC BSS 2,H
44446 5014 TSUBM BSS 1,H
44447 5015 TSUBCI BSS 1,H
44450 5016 ACI BSS 1,H
44451 5017 CCI BSS 1,H
44452 5018 DSUBC BSS 1,H
44453 5019 TCM BSS 1,H
44454 5020 THW BSS 1,H
44455 5021 HCI BSS 1,H
44456 5022 HHI BSS 1,H
44457 5023 KM BSS 1,H
44460 5024 NUM BSS 1,H
44461 5025 DELTAZ BSS 1,H
44462 5026 PIN BSS 1,F
44463 5027 AZN2 BSS 1,F
44464 -1 00160 6 06060 5028* TEMPORARY STORAGE AND CONSTANTS FOR CHECKOUT
44464 2 10440 0 00000 5029 LQ1 BCI 1,01
44466 1 67406 1 11565 5030 KON1 DEC 144.
44467 1 72507 5 34122 5031 KON17 DEC .001
44470 1 60517 4 26542 5032 KON11 DEC .01
44471 1 37667 6 33766 5033 KON12 DEC .00001
44472 2 00400 0 00000 5034 KON13 DEC .0000000001
44473 2 07401 4 63146 5035 KON8 DEC .5
44474 2 01400 0 00000 5036 KONS DEC 64.4
44475 5037 KON10 DEC 1.
44475 5038 AZN5 BSS 1,X
32621 5039 P3 EQU P+3
32620 5040 T3 EQU P+2
34063 5041 WR EQU TP+86
44476 5042 Q1 BSS 1,X
32633 5043 T6 EQU P+13
44477 5044 RMD4 BSS 1,X
44500 5045 TEMP BSS 10,X
44512 5046 SIGMA BSS 1,D
44513 5047 MAXER BSS 1,0
44514 5048 LAST BSS 1,X
44515 0 60100 0 44657 5049 TINI1 STO TINI+98
44516 -0 63400 1 44644 5050 +1 SXD TINI+87,1
44517 -0 63400 2 44645 5051 +2 SXD TINI+88,2
44520 -0 63400 4 44646 5052 +3 SXD TINI+89,4
44521 0 50000 4 00002 5053 +4 CLA 2,+4
44522 0 60100 0 44653 5054 +5 STO TINI+94
44523 0 40000 0 44650 5055 +6 ADD TINI+91
44524 0 73400 1 00000 5056 +7 PAX 0,1
44525 -0 63400 1 44552 5057 +8 SXD TINI+29,1
44526 0 76700 0 00001 5058 +9 ALS 1
44527 0 62100 0 44654 5059 +10 STA TINI+95
44530 0 50000 0 44653 5060 +11 CLA TINI+94
44531 0 77100 0 00021 5061 +12 ARS 17
44532 0 40200 0 44654 5062 +13 SUB TINI+95

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COLD FLOW HEAT TRANSFER AREA  
WETTED PERIMETER COLD FLOW  
HYDRAULIC DIAMETER OF COLD FLOW  
TEMP COLD WALL  
TEMP HOT WALL  
HEAT TRANSFER COEFFICIENT COLD SIDE  
HEAT TRANSFER COEFFICIENT HOT SIDE  
THERMAL CONDUCTIVITY

INLET PRESSURE



44533 0 73400 1 00000  
 44534 -0 63400 1 44534  
 44535 0 40700 0 44534  
 44536 0 73400 1 00000  
 44537 0 40000 4 00001  
 44540 0 62100 0 44544  
 44541 0 62100 0 44566  
 44542 0 62100 0 44570  
 44543 0 50000 0 44657  
 44544 0 34000 1 00000  
 44545 2 00002 1 44544  
 44546 0 02000 0 44547  
 44547 0 50000 0 44653  
 44550 0 76000 0 00001  
 44551 0 02000 0 44566  
 44552 2 00000 1 44554  
 44553 -0 53400 1 44647  
 44554 -3 00000 1 44554  
 44555 -0 53400 1 44554  
 44556 -0 75400 1 00000  
 44557 0 77100 0 00022  
 44560 0 76000 0 00002  
 44561 0 40000 0 44544  
 44562 0 62100 0 44603  
 44563 0 40000 0 44650  
 44564 0 62100 0 44601  
 44565 0 02000 0 44577  
 44566 0 50000 1 00000  
 44567 1 00002 1 44570  
 44570 0 30000 1 00000  
 44571 0 76500 0 00043  
 44572 0 26000 0 44651  
 44573 0 34000 0 44657  
 44574 1 77777 1 44552  
 44575 1 77777 1 44552  
 44576 1 77775 1 44552  
 44577 -0 53400 2 44647  
 44600 0 53400 1 44654  
 44601 0 50000 1 00000  
 44602 0 60100 2 12513  
 44603 0 50000 1 00000  
 44604 0 30200 0 44657  
 44605 0 60100 2 12512  
 44606 1 77776 2 44607  
 44607 2 00002 1 44601  
 44610 0 50000 0 12512  
 44611 0 60100 2 12512  
 44612 0 53400 4 44653  
 44613 -0 53400 2 44652  
 44614 1 77776 2 44615  
 44615 -0 75400 2 00000  
 44616 -0 73400 1 00000  
 44617 0 50000 1 12514  
 44620 0 30200 2 12512

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+14 PAX 0,1  
 +15 SXD TINI+31,1  
 +16 ADD TINI+95  
 +17 PAX 0,1  
 +18 ADD 1,4  
 +19 STA TINI+23  
 +20 STA TINI+41  
 +21 STA TINI+43  
 +22 CLA TINI+98  
 +23 CAS 0,1  
 +24 TIX TINI+23,1,2  
 +25 TRA TINI+26  
 +26 CLA TINI+94  
 +27 LBT  
 +28 TRA TINI+41  
 +29 TIX TINI+31,1,0  
 +30 LXD TINI+90,1  
 +31 TXL TINI+33,1,0  
 +32 LXD TINI+31,1  
 +33 PXD 0,1  
 +34 ARS 18  
 +35 CHS  
 +36 ADD TINI+23  
 +37 STA TINI+54  
 +38 ADD TINI+91  
 +39 STA TINI+52  
 +40 TRA TINI+50  
 +41 CLA 0,1  
 +42 TXI TINI+43,1,2  
 +43 FAD 0,1  
 +44 LRS 35  
 +45 FMP TINI+92  
 +46 CAS TINI+98  
 +47 TXI TINI+29,1,-1  
 +48 TXI TINI+29,1,-1  
 +49 TXI TINI+29,1,-3  
 +50 LXD TINI+90,2  
 +51 LXA TINI+95,1  
 +52 CLA 0,1  
 +53 STO COMMON+1,2  
 +54 CLA 0,1  
 +55 FSB TINI+98  
 +56 STO COMMON,2  
 +57 TXI TINI+58,2,-2  
 +58 T' ( TINI+52,1,2  
 +59 CL. COMMON  
 +60 STO COMMON,2  
 +61 LXA TINI+94,4  
 +62 LXD TINI+93,2  
 +63 TXI TINI+64,2,-2  
 +64 PXD 0,2  
 +65 PDX 0,1  
 +66 CLA COMMON+2,1  
 +67 FSB COMMON,2

BEGIN SEARCH FOR K+1 BEST POINTS

TEST EVEN/ODD K

K EVEN  
K ODD

BEGIN AITKENS INTERPOLATION

44621 0 10000 0 44634  
 44622 0 60100 0 44656  
 44623 0 56000 2 12512  
 44624 0 26000 1 12515  
 44625 0 60100 0 44655  
 44626 0 56000 1 12514  
 44627 0 26000 2 12513  
 44630 0 30200 0 44655  
 44631 0 24100 0 44656  
 44632 -0 60000 1 12515  
 44633 1 77776 1 44617  
 44634 0 50000 2 12514  
 44635 0 60100 1 12514  
 44636 2 00001 4 44614  
 44637 0 50000 1 12513  
 44640 -0 53400 1 44644  
 44641 -0 53400 2 44645  
 44642 -0 53400 4 44646  
 44643 0 02000 4 00003  
 44644 0 00000 0 00000  
 44652 0 00002 0 00000  
 44653 0 00000 0 00000

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+68 TZE TINI+79  
 +69 STO TINI+97  
 +70 LDQ COMMON,2  
 +71 FMP COMMON+3,1  
 +72 STO TINI+96  
 +73 LDQ COMMON+2,1  
 +74 FMP COMMON+1,2  
 +75 FSB TINI+96  
 +76 FDP TINI+97  
 +77 STQ COMMON+3,1  
 +78 TXI TINI+66,1,-2  
 +79 CLA COMMON+2,2  
 +80 STO COMMON+2,1  
 +81 TIX TINI+63,4,1  
 +82 CLA COMMON+1,1  
 +83 LXD TINI+87,1  
 +84 LXD TINI+88,2  
 +85 LXD TINI+89,4  
 +86 TRA 3,4  
 +87 DEC 0,.,.,1,.5  
 +93 PZE 0,0,2  
 +94 DEC 0,.,.,0

ESCAPE

5140\*HOT BLEED PORT ROUTINES

5141\*REGION TO INITIALIZE HOT BLEED PORT FOR EACH TIME POINT

44660 0 50000 0 32704  
 44661 -0 10000 0 44663  
 44662 0 50000 0 32702  
 44663 0 60100 0 47321  
 44664 0 60100 0 47325  
 44665 0 60000 0 47322  
 44666 0 50000 0 32656  
 44667 0 60100 0 47323  
 44670 0 60000 0 47324  
 44671 0 60000 0 47334  
 44672 0 50000 0 32705  
 44673 -0 10000 0 44675  
 44674 0 50000 0 32703  
 44675 0 60100 0 47352  
 44676 0 60100 0 47356  
 44677 0 60000 0 47353  
 44700 0 50000 0 32633  
 44701 0 60100 0 47354  
 44702 0 60000 0 47355  
 44703 0 60000 0 47365  
 44704 0 50000 0 32644  
 44705 0 60100 0 47403  
 44706 0 50000 0 34045  
 44707 0 60100 0 47404  
 44710 0 50000 0 32657  
 44711 0 60100 0 47350

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HBI CLA P+54  
 +1 TNZ \*+2  
 +2 CLA P+52  
 +3 STO PR  
 +4 STO PR+4  
 +5 STZ PR+1  
 +6 CLA P+32  
 +7 STO PR+2  
 +8 STZ PR+3  
 +9 STZ PR+11  
 +10 CLA P+55  
 +11 TNZ \*+2  
 +12 CLA P+53  
 +13 STO PR+25  
 +14 STO PR+29  
 +15 STZ PR+26  
 +16 CLA P+13  
 +17 STO PR+27  
 +18 STZ PR+28  
 +19 STZ PR+36  
 +20 CLA P+22  
 +21 STO PR+50  
 +22 CLA TP+72  
 +23 STO PR+51  
 +24 CLA P+33  
 +25 STO PR+23

PC  
\*CHECKOUT ONLY  
\*CHECKOUT ONLY  
PH  
P6  
P8  
P08  
TC  
\*CHECKOUT ONLY  
\*CHECKOUT ONLY  
TH  
T6  
T8  
T08  
WDOTC  
WDOTH  
G.P.

5169\*REGION TO OUTPUT MB QUANTITIES  
 44713 0 90000 0 47334 5170 H80 CLA PR+11  
 44714 0 60100 0 32660 5171 +1 STO P+34 P08  
 44715 0 90000 0 47365 5172 +2 CLA PR+36 T08  
 44716 0 60100 0 32661 5173 +3 STO P+35  
 44717 0 90000 0 47404 5174 +4 CLA PR+51 W00TH  
 44720 0 60100 0 32645 5175 +5 STO P+23  
 44721 0 90000 0 47407 5176 +6 CLA PR+54 W00TNCHOKE  
 44722 0 60100 0 34007 5177 +7 STO TP+42  
 44723 0 02000 4 00001 5178 +8 TRA 1.4

5179\*REGION TO INITIALIZE INPUT FOR HOT BLEED PORT  
 44724 0 90000 0 36152 5180 CLA DT  
 44725 0 60100 0 47341 5181 +1 STO P+16  
 44726 0 90000 0 36136 5182 +2 CLA OLM  
 44727 0 60100 0 47340 5183 +3 STO PR+15  
 44730 0 90000 0 36133 5184 +4 CLA OR  
 44731 0 60100 0 47342 5185 +5 STO PR+17  
 44732 0 90000 0 36150 5186 +6 CLA DDCO  
 44733 0 60100 0 47343 5187 +7 STO PR+18  
 44734 0 90000 0 36151 5188 +8 CLA DMH  
 44735 0 60100 0 47344 5189 +9 STO PR+19  
 44736 0 90000 0 36154 5190 +10 CLA OTHET  
 44737 0 60100 0 47345 5191 +11 STO PR+20  
 44740 0 90000 0 36147 5192 +12 CLA DNK  
 44741 0 60100 0 47370 5193 +13 STO PR+39  
 44742 0 90000 0 36146 5194 +14 CLA DL  
 44743 0 60100 0 47372 5195 +15 STO PR+41  
 44744 0 90000 0 36121 5196 +16 CLA DA6  
 44745 0 60100 0 47422 5197 +17 STO PR+65  
 44746 0 90000 0 36122 5198 +18 CLA DASTR  
 44747 0 60100 0 47430 5199 +19 STO PR+71  
 44750 0 90000 0 36203 5200 +20 CLA DKFLG  
 44751 0 60100 0 47455 5201 +21 STO PR+92  
 44752 0 90000 0 36131 5202 +22 CLA DAKV  
 44753 0 60100 0 47456 5203 +23 STO PR+93  
 44754 0 90000 0 36132 5204 +24 CLA DBKV  
 44755 0 60100 0 47457 5205 +25 STO PR+94  
 44756 0 02000 4 00001 5206 +26 TRA 1.4

5207\*HOT BLEED PORT PROGRAM -- KEN NAGASAWA  
 44757 0 63400 4 47051 5208 HB SXA HBR,4  
 44760 0 63400 2 47052 5209 +1 SXA HBR+1,2  
 44761 0 63400 3 47053 5210 +2 SXA HBR+2,3  
 44762 0 63400 1 47054 5211 +3 SXA HBR+3,1  
 44763 0 63400 5 47055 5212 +4 SXA HBR+4,5  
 44764 0 63400 6 47056 5213 +5 SXA HBR+5,6  
 44765 0 63400 7 47057 5214 +6 SXA HBR+6,7  
 44766 0 77400 1 00000 5215 +7 AXT O,1  
 44767 0 77400 2 00000 5216 +8 AXT O,2  
 44770 0 77400 3 00000 5217 +9 AXT O,3  
 44771 0 77400 5 00000 5218 +10 AXT O,5  
 44772 0 77400 6 00000 5219 +11 AXT O,6  
 44773 0 77400 7 00000 5220 +12 AXT O,7  
 44774 0 76000 0 00012 5221 +13 DCT  
 44775 0 02000 0 44776 5222 +14 TRA \*+1

44776	0	50000	0	47714	5223	+15	CLA	H86		
44777	0	60100	0	44105	5224	+16	STO	SWT		
45000	0	77400	4	00050	5225	+17	AXT	40,4		ITER PRINT FLAG
45001	-0	63400	4	43745	5226	+18	SKD	ITER5,4		NO. ITERATIONS
45002	0	77400	4	47065	5227	+19	AXT	H84,4		ERROR RETURN
45003	0	63400	4	44020	5228	+20	SXA	ITER9,4		INPUT
45004	0	07400	4	44660	5229	+21	TSX	H81,4		T6
45005	0	50000	0	47354	5230	+22	CLA	PR+27		P6
45006	0	56000	0	47323	5231	+23	LDQ	PR+2		
45007	0	07400	4	25564	5232	+24	TSX	AZH,4		
45010	0	07400	4	42602	5233	+25	TSX	ERROR,4		
45011	0	50000	0	33724	5234	+26	CLA	WPR+2		
45012	0	60100	0	47524	5235	+27	STO	Z+31		H06
45013	0	50000	0	47356	5236	+28	CLA	PR+29		T2C
45014	0	56000	0	47325	5237	+29	LDQ	PR+4		P2C
45015	0	07400	4	25564	5238	+30	TSX	AZH,4		
45016	0	07400	4	42602	5239	+31	TSX	ERROR,4		
45017	0	50000	0	33724	5240	+32	CLA	WPR+2		
45020	0	60100	0	47525	5241	+33	STO	Z+32		H02C
45021	0	56000	0	47404	5242	+34	LDQ	PR+51		WH
45022	0	26000	0	40262	5243	+35	FMP	FL3,7		
45023	0	60100	0	47453	5244	+36	STO	PR+90		Q INITIAL GUESS
45024	0	50000	0	47372	5245	+37	CLA	PR+41		LENGTH
45025	0	24100	0	47370	5246	+38	FDP	PR+39		NO OF DELTAS
45026	-0	60000	0	47371	5247	+39	STQ	PR+40		DELTA X
45027	0	50000	0	47370	5248	+40	CLA	PR+39		
45030	0	60100	0	47546	5249	+41	STO	Z+49		
45031	0	77400	7	00002	5250	+42	AXT	Z,7		
45032	0	50000	0	47323	5251	20.00	CLA	PR+2		P6
45033	0	56000	0	47354	5252	+1	LDQ	PR+27		T6= THIC
45034	-3	00000	6	45037	5253	+2	TXL	*+3,6,0		MR HOT NOT INPUT
45035	0	07400	4	47733	5254	+3	TSX	RHOMR,4		CALC. DENSITY = (P*144)/(RH*T)
45036	0	02000	0	45045	5255	+4	TRA	*+7		
45037	0	13100	0	00000	5256	+5	XCA			
45040	0	07400	4	25564	5257	+6	TSX	AZH,4		
45041	0	07400	4	42602	5258	+7	TSX	ERROR,4		
45042	0	56000	0	33730	5259	+8	LDQ	WPR+6		
45043	0	26000	0	40245	5260	+9	FMP	FLCUF		
45044	0	60100	0	47522	5261	+10	STO	Z+29		
45045	0	76000	0	00142	5262	+11	SLN	Z		COMPUTE WN ,K=1.4
45046	0	50000	0	36167	5263	+12	CLA	TK+10		
45047	0	30200	0	40213	5264	+13	FSB	FL1		
45050	0	60100	0	47465	5265	+14	STO	Z		K-1
45051	0	30000	0	40214	5266	+15	FAD	FL2		
45052	0	60100	0	47466	5267	+16	STO	Z+1		K+1
45053	0	24100	0	47465	5268	+17	FDP	Z		
45054	-0	60000	0	47467	5269	+18	STQ	Z+2		
45055	0	50000	0	40214	5270	+19	CLA	FL2		
45056	0	24100	0	47466	5271	+20	FDP	Z+1		
45057	0	13100	0	00000	5272	+21	XCA			
45060	0	56000	0	47467	5273	+22	LDQ	Z+2		
45061	0	07400	1	47752	5274	+23	TSX	POWER,1		
45062	0	13100	0	00000	5275	+24	XCA			

49064	0	24100	0	36175	9277	+26	FDP	TK+16	
49065	0	26000	0	40272	9278	+27	FMP	FLGF	
49066	0	60100	0	47930	9279	+28	STO	Z+35	
49067	0	24100	0	47354	9280	+29	FDP	PR+27	
49070	0	13100	0	00000	9281	+30	XCA		T6
49071	0	07400	4	24364	9282	+31	TSX	SQRT,4	
49072	0	07400	4	42602	9283	+32	TSX	ERROR,4	
49073	0	13100	0	00000	9284	+33	XCA		
49074	0	26000	0	47323	9285	+34	FMP	PR+2	
49075	0	13100	0	00000	9286	+35	XCA		P6
49076	0	26000	0	47430	9287	+36	FMP	PR+71	AN
49077	0	60100	0	47407	9288	+37	STO	PR+54	WH
49100	0	30000	0	47404	9289	+38	FAD	PR+51	WH
49101	0	60100	0	47404	9290	20.01	STO	PR+53	WR
49102	0	50000	0	47404	9291	+1	CLA	PR+53	
49103	0	24100	0	47522	9292	+2	FDP	Z+29	
49104	0	26000	0	40244	9293	+3	FMP	FL144	
49105	0	24100	0	47422	9294	+4	FDP	PR+65	A6
49106	-0	60000	0	47450	9295	+5	STQ	PR+87	V6
49107	0	50000	0	40254	9296	20.50	CLA	FL.5	
49110	-0	52000	0	47401	9297	+1	NZT	PR+48	MACH HOT MIX
49111	0	60100	0	47401	9298	+2	STO	PR+48	
49112	0	50000	0	47354	9299	+3	CLA	PR+27	
49113	0	60100	0	47367	9300	+4	STO	PR+38	THIC-T6
49114	0	50000	0	36167	9301	+5	CLA	TK+10	
49115	0	30200	0	40213	9302	+6	FSB	FL1	
49116	0	24100	0	40214	9303	+7	FDP	FL2	
49117	-0	60000	0	47472	9304	+8	STQ	Z+5	K-1/2
49120	0	26000	0	47401	9305	+9	FMP	PR+48	
49121	0	13100	0	00000	9306	+10	XCA		
49122	0	26000	0	47401	9307	+11	FMP	PR+48	
49123	0	30000	0	40213	9308	+12	FAD	FL1	
49124	0	60100	0	47473	9309	+13	STO	Z+6	
49125	0	50000	0	47367	9310	+14	CLA	PR+38	
49126	0	24100	0	47473	9311	+15	FDP	Z+6	
49127	-0	60000	0	47364	9312	+16	STQ	PR+35	THM
49130	0	26000	0	40272	9313	20.55	FMP	FLGF	
49131	0	13100	0	00000	9314	+1	XCA		
49132	0	26000	0	36167	9315	+2	FMP	TK+10	
49133	0	13100	0	00000	9316	+3	XCA		
49134	0	26000	0	36175	9317	+4	FMP	TK+16	R HOT
49135	0	07400	4	24364	9318	+5	TSX	SQRT,4	
49136	0	07400	4	42602	9319	+6	TSX	ERROR,4	
49137	0	60100	0	47521	9320	+7	STO	Z+28	C HOT
49140	0	13100	0	00000	9321	+8	XCA		
49141	0	26000	0	47401	9322	+9	FMP	PR+48	
49142	0	60100	0	47446	9323	+10	STO	PR+85	VHM
49143	0	56000	0	47340	9324	20.56	LDQ	PR+15	DH
49144	0	26000	0	47340	9325	+1	FMP	PR+15	
49145	0	24100	0	40216	9326	+2	FDP	FL4	
49146	0	26000	0	40271	9327	+3	FMP	FLPI	
49147	0	60100	0	47424	9328	+4	STO	PR+67	AH
49150	0	52000	0	47454	9329	+5	ZET	PR+91	HEAT TRANSFER FLAG
49151	0	02000	0	45507	9330	+6	TRA	21.99	NON ZERO

49152	0	50000	0	47404	5331	20.58	CLA	PR+51	WH
49153	0	76000	0	00003	5332	+1	SSP		PAKE ABSOLUTE
49154	0	24100	0	47446	5333	+2	FDP	PR+85	
49155	0	26000	0	40244	5334	+3	FMP	FL144	
49156	0	24100	0	47424	5335	+4	FDP	PR+67	AH
49157	-0	60000	0	47523	5336	+5	STO	Z+30	
49160	0	56000	0	47446	5337	+6	LDQ	PR+85	VHM
49161	0	26000	0	47446	5338	20.60	FMP	PR+85	
49162	0	60100	0	47466	5339	+1	STO	Z+1	
49163	0	56000	0	47450	5340	+2	LDQ	PR+87	V6
49164	0	26000	0	47450	5341	+3	FMP	PR+87	
49165	0	30000	0	47466	5342	+4	FAD	Z+1	
49166	0	60100	0	47465	5343	+5	STO	Z	
49167	0	07400	4	24364	5344	+6	TSX	SQRT,4	
49170	0	07400	4	42602	5345	+7	TSX	ERROR,4	
49171	0	60100	0	47451	5346	+8	STO	PR+88	VIN
49172	0	50000	0	47522	5347	20.65	CLA	Z+29	
49173	0	30000	0	47523	5348	+1	FAD	Z+30	
49174	0	24100	0	40214	5349	+2	FDP	FL2	
49175	-0	60000	0	47474	5350	+3	STQ	Z+7	RHO IN
49176	0	56000	0	36171	5351	20.70	LDQ	TK+12	KIN = .5
49177	0	26000	0	47465	5352	+1	FMP	Z	VIN 2
49200	0	60100	0	47465	5353	+2	STO	Z	VIN
49201	0	50000	0	47451	5354	+3	CLA	PR+88	VAM
49202	0	30200	0	47446	5355	+4	FSB	PR+85	
49203	0	60100	0	47466	5356	+5	STO	Z+1	
49204	0	13100	0	00000	5357	+6	XCA		
49205	0	26000	0	47466	5358	+7	FMP	Z+1	
49206	0	30000	0	47465	5359	+8	FAD	Z	
49207	0	24100	0	40273	5360	+9	FDP	FL2G	
49210	0	26000	0	47474	5361	+10	FMP	Z+7	RHO IN
49211	0	24100	0	40244	5362	+11	FDP	FL144	
49212	-0	60000	0	47335	5363	+12	STQ	PR+12	DELTA P
49213	0	50000	0	47323	5364	20.75	CLA	PR+2	P6
49214	0	30200	0	47335	5365	+1	FSB	PR+12	
49215	0	60100	0	47336	5366	+2	STO	PR+13	PHM O
49216	0	50000	0	36167	5367	20.76	CLA	TK+10	K
49217	0	30200	0	40213	5368	+1	FSB	FL1	
49220	0	60100	0	47465	5369	+2	STO	Z	
49221	0	50000	0	36167	5370	+3	CLA	TK+10	
49222	0	24100	0	47465	5371	+4	FDP	Z	
49223	-0	60000	0	47513	5372	+5	STQ	Z+22	K/K-1
49224	0	50000	0	47473	5373	+6	CLA	Z+6	
49225	0	07400	1	47752	5374	+7	TSX	POWER,1	
49226	0	60100	0	47465	5375	+8	STO	Z	
49227	0	50000	0	47336	5376	+9	CLA	PR+13	PHM O
49230	0	24100	0	47465	5377	+10	FDP	Z	
49231	-0	60000	0	47333	5378	+11	STQ	PR+10	PHM
49232	0	50000	0	36167	5379	20.77	CLA	TK+10	1.4
49233	0	30000	0	40213	5380	+1	FAD	FL1	
49234	0	60100	0	47466	5381	+2	STO	Z+1	
49235	0	50000	0	40214	5382	+3	CLA	FL2	
49236	0	24100	0	47466	5383	+4	FDP	Z+1	
49237	-0	60000	0	47465	5384	+5	STQ	Z	2/K+1



45412 0 07400 4 44513 5493 +19 TSX TINI,4  
 45413 0 00000 0 47760 5494 +20 HTR THOT,0,0  
 45414 0 00022 0 00001 5495 +21 HTR 1,0,18  
 45415 0 60100 0 47365 5496 +22 STO PR+36  
 45416 0 60100 0 47353 5497 +23 STO PR+26  
 45417 0 50000 0 47530 5499 +24 CLA Z+35  
 45420 -3 00000 6 45423 5500 +25 TXL \*\*3,6,0  
 45421 0 24160 7 47750 5501 +26 FDP\* NEWR+2,7  
 45422 0 26060 7 47747 5502 +27 FMP\* NEWR+1,7  
 45423 0 07400 4 24364 5503 +28 TSX SQRT,4  
 45424 0 07400 4 42602 5504 +29 TSX ERROR,4  
 45425 0 13100 0 00000 5505 +30 XCA  
 45426 0 26000 0 47431 5506 +31 FMP PR+72  
 45427 0 60100 0 47531 5507 +32 STO Z+36  
 45430 0 13100 0 00000 5508 +33 XCA  
 45431 0 26000 0 47531 5509 +34 FMP Z+36  
 45432 0 60100 0 47532 5510 +35 STO Z+37  
 45433 0 56000 0 47350 5511 +36 LDQ PR+23  
 45434 0 26000 0 47456 5512 +37 FMP PR+93  
 45435 0 30200 0 47457 5513 +38 FSB PR+94  
 45436 0 60100 0 47460 5514 +39 STO PR+95  
 45437 0 13100 0 00000 5515 +40 XCA  
 45440 0 26000 0 47460 5516 +41 FMP PR+95  
 45441 0 60100 0 47533 5517 +42 STO Z+38  
 45442 0 50000 0 40265 5518 +43 CLA FL128.  
 45443 0 24100 0 47533 5519 +44 FDP Z+38  
 45444 0 26060 7 47750 5520 +45 FMP\* NEWR+2,7  
 45445 0 24100 0 40244 5521 +46 FDP FL144  
 45446 0 26000 0 47532 5522 +47 FMP Z+37  
 45447 0 60100 0 47534 5523 +48 STO Z+39  
 45450 0 50000 0 36176 5524 +49 CLA TK+17  
 45451 0 30000 0 36177 5525 +50 FAD TK+18  
 45452 0 60100 0 47466 5526 +51 STO Z+1  
 45453 0 56000 0 47340 5527 +52 LDQ PR+15  
 45454 0 26000 0 47340 5528 +53 FMP PR+15  
 45455 0 24100 0 40216 5529 +54 FDP FL4  
 45456 0 26000 0 40271 5530 +55 FMP FLPI  
 45457 0 60100 0 47535 5531 +56 STO Z+40  
 45460 0 13100 0 00000 5532 +57 XCA  
 45461 0 26000 0 47535 5533 +58 FMP Z+40  
 45462 0 60100 0 47535 5534 +59 STO Z+40  
 45463 0 50060 7 47750 5535 +60 CLA\* NEWR+2,7  
 45464 0 24100 0 47535 5536 +61 FDP Z+40  
 45465 0 26000 0 47532 5537 +62 FMP Z+37  
 45466 0 24100 0 40272 5538 +63 FDP FLGF  
 45467 -0 60000 0 47536 5539 +64 STO Z+41  
 45470 0 26000 0 47466 5540 +65 FMP Z+1  
 45471 0 30000 0 47534 5541 +66 FAD Z+39  
 45472 0 30000 0 40213 5542 +67 FAD FL1  
 45473 0 07400 4 24364 5543 +68 TSX SQRT,4  
 45474 0 07400 4 42602 5544 +69 TSX ERROR,4  
 45475 0 60100 0 47537 5545 +70 STO Z+42  
 45476 0 50000 0 47365 5546 +71 CLA PR+36

MOB VS. TOB  
 TOB  
 TH  
 CALCULATE PO 8  
 MR HOT NOT INPUT  
 IR =2 RMOT,IR=1 R MIX IR7=1  
 IR =2 RMOT,IR=1 R MIX IR7=1  
 ATN  
 KT  
 KT2  
 GATE POS  
 A  
 B  
 KV  
 KV SQUARE  
 KV2  
 R HOT IR=2, R MIX IR=1  
 KT2  
 F  
 K11  
 K9  
 DTL EQU. DH  
 DTL EQU. DH  
 ATL  
 ATL  
 ATL SQUARE  
 R HOT IR=2, R MIX IR=1  
 ATL SQUARE  
 KT2  
 L  
 K11+K9  
 F  
 TOB

45477 0 07400 4 24364 5547 +72 TSX SQRT,4  
 45500 0 07400 4 42602 5548 +73 TSX ERROR,4  
 45501 0 24100 0 47531 5549 +74 FDP Z+36  
 45502 0 26000 0 47405 5550 +75 FMP PR+52  
 45503 0 13100 0 00000 5551 +76 XCA  
 45504 0 26000 0 47537 5552 +77 FMP Z+42  
 45505 0 60100 0 47322 5553 +78 STO PR+1  
 45506 0 60100 0 47334 5554 21.05 STO PR+11  
 45507 0 60000 0 47545 5555 21.99 STZ Z+48  
 45510 0 77400 1 00000 5556 +1 AXT 0,1  
 45511 0 63400 1 46220 5557 +2 SXA 23-93,1  
 45512 -3 00000 6 45515 5558\* HEAT TRANSFER PROGRAM 8/23/63  
 45513 0 50060 7 47752 5559 22.00 TXL \*\*3,6,0  
 45514 0 02000 0 45522 5560 +1 CLA\* NEWCP+2,7  
 45515 0 50000 0 47353 5561 +2 TRA \*\*6  
 45516 0 56000 0 47322 5562 +3 CLA PR+26  
 45517 0 07400 4 25564 5563 +4 LDQ PR+1  
 45520 0 07400 4 42602 5564 +5 TSX AZH,4  
 45521 0 50000 0 33731 5565 +6 TSX ERROR,4  
 45522 0 60100 0 47465 5566 +7 CLA WPR+7  
 45523 0 50000 0 47453 5567 +8 STO Z  
 45524 0 24100 0 47465 5568 +9 CLA PR+90  
 45525 0 13100 0 00000 5569 +10 FDP Z  
 45526 0 24100 0 47405 5570 +11 XCA  
 45527 0 13100 0 00000 5571 +12 FDP PR+52  
 45530 0 30000 0 47353 5572 +13 XCA  
 45531 0 60100 0 47362 5573 +14 FAD PR+26  
 45532 0 30000 0 47353 5574 +15 STO PR+33  
 45533 0 24100 0 40214 5575 22.10 FAD PR+26  
 45534 -0 60000 0 47413 5576 +1 FDP FL2  
 45535 0 50000 0 47352 5577 +2 STO PR+58  
 45536 0 56000 0 47321 5578 22.20 CLA PR+25  
 45537 0 16200 0 45541 5579 +1 LDQ PR  
 45540 0 02000 0 47063 5580 +2 TQP \*\*2  
 45541 0 07400 4 25564 5581 +3 TRA HB3  
 45542 0 07400 4 42602 5582 +4 TSX AZH,4  
 45543 0 50000 0 33731 5583 +5 TSX ERROR,4  
 45544 0 60100 0 47465 5584 +6 CLA WPR+7  
 45545 0 50000 0 47453 5585 +7 STO Z  
 45546 0 24100 0 47465 5586 +8 CLA PR+90  
 45547 0 13100 0 00000 5587 +9 FDP Z  
 45550 0 24100 0 47403 5588 +10 XCA  
 45551 0 13100 0 00000 5589 +11 FDP PR+50  
 45552 0 30000 0 47352 5590 +12 XCA  
 45553 0 60100 0 47361 5591 +13 FAD PR+25  
 45554 0 30000 0 47352 5592 +14 STO PR+32  
 45555 0 24100 0 40214 5593 22.30 FAD PR+25  
 45556 -0 60000 0 47412 5594 +1 FDP FL2  
 45557 0 56000 0 47340 5595 +2 STO PR+57  
 45558 0 26000 0 40271 5596 22.40 LDQ PR+15  
 45561 0 60100 0 47465 5597 +1 FMP FLPI  
 45562 0 56000 0 47424 5598 +2 STO Z  
 45563 0 26000 0 40216 5600 +3 LDQ PR+67  
 5600 +4 FMP FL4

KT  
 WT  
 NEW PH  
 POB  
 INITIALIZE FOR BELLOW SECTIONS  
 MR HOT NOT INPUT  
 C SUB P MIX  
 TH I  
 PH I  
 CSUBP HOT  
 QI  
 TH I+1  
 TH I+1/2  
 TC I  
 PC I  
 NEGATIVE PC (I)  
 CSUBP COLD  
 Q I  
 WC  
 TCI  
 TCI+1  
 TC I+1/2  
 DH  
 F PH  
 AH



45737	0	26000	0	47377	5709	+7	FMP	PR+46	
45740	0	60100	0	47445	5710	+8	STO	Z	
45741	0	50000	0	47453	5711	+9	CLA	PR+90	Q I
45742	0	24100	0	47445	5712	+10	FDP	Z	
45743	0	13100	0	00000	5713	+11	XCA		
45744	0	24100	0	47371	5714	+12	FDP	PR+40	DELTA X
45745	0	13100	0	00000	5715	+13	XCA		
45746	0	24100	0	40271	5716	+14	FDP	FLP1	
45747	0	13100	0	00000	5717	+15	XCA		
45750	0	76000	0	00002	5718	+16	CMS		
45751	0	30000	0	47416	5719	+17	FAD	PR+61	TMW I+1/2
45752	0	60100	0	47415	5720	+18	STO	PR+60	TCM I+1/2
45753	0	12000	0	45760	5721	+19	TPL	23.00	
45754	0	50000	0	47453	5722	22.99	CLA	PR+90	Q
45755	0	24100	0	40214	5723	+1	FDP	FL2	
45756	-0	60000	0	47453	5724	+2	STQ	PR+90	NEW Q GUESS
45757	0	02000	0	45512	5725	+3	TRA	22.00	
45760	0	50000	0	47341	5726	23.00	CLA	PR+16	THICK.
45761	0	30000	0	47341	5727	+1	FAD	PR+16	
45762	0	30000	0	47342	5728	+2	FAD	PR+17	RAD.
45763	0	30000	0	47340	5729	+3	FAD	PR+15	DM
45764	0	60100	0	47501	5730	+4	STO	Z+12	DM+R+2T
45765	0	13100	0	00000	5731	+5	XCA		
45766	0	26000	0	47342	5732	+6	FMP	PR+17	
45767	0	13100	0	00000	5733	+7	XCA		
45770	0	26000	0	40271	5734	+8	FMP	FLP1	
45771	0	60100	0	47423	5735	+9	STQ	PR+66	AREA COLD
45772	0	56000	0	47501	5736	23.10	LDQ	Z+12	
45773	0	26000	0	40271	5737	+1	FMP	FLP1	
45774	0	24100	0	40254	5738	+2	FDP	FL.5	
45775	-0	60000	0	47502	5739	+3	STQ	Z+13	FPC
45776	0	50000	0	47352	5740	23.20	CLA	PR+25	TCI
45777	0	56000	0	47321	5741	+1	LDQ	PR	PC I
46000	0	07400	4	25564	5742	+2	TSX	AZL,4	
46001	0	07400	4	42602	5743	+3	TSX	ERROR,4	
46002	0	56000	0	33730	5744	+4	LDQ	WPR+6	
46003	0	26000	0	40265	5745	+5	FMP	FLCUF	
46004	0	60100	0	47465	5746	+6	STO	Z	
46005	0	50000	0	47361	5747	+7	CLA	PR+32	TC I+1
46006	0	30200	0	47352	5748	+8	FSB	PR+25	TC I
46007	0	24100	0	47412	5749	+9	FDP	PR+57	TC I+1/2
46010	-0	60000	0	47466	5750	+10	STQ	Z+1	
46011	0	50000	0	36164	5751	+11	CLA	TK+7	FRICITION COLD
46012	0	24100	0	47342	5752	+12	FDP	PR+17	R
46013	0	13100	0	00000	5753	+13	XCA		
46014	0	26000	0	40214	5754	+14	FMP	FL2	
46015	0	26000	0	47371	5755	+15	FMP	PR+40	DELTA X
46016	0	30000	0	47466	5756	+16	FAD	Z+1	
46017	0	24100	0	47465	5757	+17	FDP	Z	
46020	0	26000	0	47403	5758	+18	FMP	PR+50	WC
46021	0	24100	0	47423	5759	+19	FDP	PR+66	AC
46022	0	26000	0	47403	5760	+20	FMP	PR+50	WC
46023	0	24100	0	47423	5761	+21	FDP	PR+66	
46024	0	26700	0	47244	5762	+22	END	FL144	

46025	0	24100	0	40273	5763	+23	FDP	FL2G	
46026	0	13100	0	00000	5764	+24	XCA		
46027	0	76000	0	00002	5765	+25	CMS		
46030	0	30000	0	47321	5766	+26	FAD	PR	PC I
46031	0	60100	0	47330	5767	+27	STO	PR+7	PC I+1
46032	0	12000	0	46034	5768	+28	TPL	23.30	
46033	0	02000	0	47063	5769	+29	TRA	H88	
46034	0	30000	0	47321	5770	23.30	FAD	PR	NEGATIVE PC (I+1)
46035	0	24100	0	40214	5771	+1	FDP	FL2	
46036	-0	60000	0	47477	5772	+2	STQ	Z+10	PC I+1/2
46037	0	50000	0	47342	5773	23.40	CLA	PR+17	RAD.
46040	0	30000	0	47342	5774	+1	FAD	PR+17	
46041	0	60100	0	47346	5775	+2	STO	PR+21	D SLA C
46042	0	30000	0	47371	5776	+3	FAD	PR+40	
46043	0	60100	0	47465	5777	+4	STO	Z	
46044	0	50000	0	47346	5778	+5	CLA	PR+21	
46045	0	24100	0	47465	5779	+6	FDP	Z	
46046	0	13100	0	00000	5780	+7	XCA		
46047	0	56000	0	36157	5781	+8	LDQ	TK+2	B COLD
46050	0	07400	1	47752	5782	+9	TSX	POWER,1	
46051	0	24100	0	47423	5783	+10	FDP	PR+66	
46052	0	26000	0	36160	5784	+11	FMP	TK+3	C COLD
46053	0	60100	0	47465	5785	+12	STO	Z	
46054	0	50000	0	47412	5786	23.50	CLA	PR+57	
46055	0	56000	0	47477	5787	+1	LDQ	Z+10	PC I+1/2
46056	0	07400	4	25564	5788	+2	TSX	AZL,4	
46057	0	07400	4	42602	5789	+3	TSX	ERROR,4	
46060	0	07400	4	26223	5790	+4	TSX	AZL,4	
46061	0	60100	0	47375	5791	23.65	STO	PR+44	LC I+1/2
46062	0	50000	0	47412	5792	+1	CLA	PR+57	TC I+1/2
46063	0	24100	0	47415	5793	+2	FDP	PR+60	TWC I+1/2
46064	0	13100	0	00000	5794	+3	XCA		
46065	0	56000	0	36156	5795	+4	LDQ	TK+1	A COLD
46066	0	07400	1	47752	5796	+5	TSX	POWER,1	
46067	0	60100	0	47466	5797	+6	STO	Z+1	
46070	0	56000	0	47403	5798	+7	LDQ	PR+50	WC
46071	0	26000	0	40271	5799	+8	FMP	FLP1	
46072	0	56000	0	40256	5800	+9	LDQ	FL.8	
46073	0	07400	1	47752	5801	+10	TSX	POWER,1	
46074	0	13100	0	00000	5802	+11	XCA		
46075	0	26000	0	47466	5803	+12	FMP	Z+1	
46076	0	60100	0	47466	5804	+13	STO	Z+1	
46077	0	50000	0	47502	5805	+14	CLA	Z+13	FPC
46100	0	56000	0	40251	5806	+15	LDQ	FL.2	
46101	0	07400	1	47752	5807	+16	TSX	POWER,1	
46102	0	24100	0	40216	5808	+17	FDP	FL4	
46103	0	26000	0	47466	5809	+18	FMP	Z+1	
46104	0	13100	0	00000	5810	+19	XCA		
46105	0	26000	0	47375	5811	+20	FMP	PR+44	LC I+1/2
46106	0	13100	0	00000	5812	+21	XCA		
46107	0	26000	0	47465	5813	+22	FMP	Z	
46110	0	60100	0	47373	5814	+23	STO	PR+42	H CI
46111	0	50000	0	47501	5815	23.70	CLA	Z+12	





DELTA X

46265	0	60100	0	47547	5925	+3	STO	Z+49
46266	0	77400	1	00002	5926	+4	ART	Z+1
46267	0	90000	1	47332	5927	+5	CLA	PR+9,1
46270	0	60100	1	47323	5928	+6	STO	PR+2,1
46271	0	90000	1	47363	5929	+7	CLA	PR+34,1
46272	0	60100	1	47354	5930	+8	STO	PR+27,1
46273	2	00001	1	46267	5931	+9	TIX	9-4,1,1
46274	0	02000	0	49512	5932	+10	TRA	22.00
46275	0	90000	0	47370	5933	25.00	CLA	PR+39
46276	0	60100	0	47546	5934	+1	STO	Z+49
46277	0	90000	0	32704	5935	+2	CLA	P+94
4630C	0	60100	0	47321	5936	+3	STO	PR
46301	0	60000	0	47322	5937	+4	STZ	PR+1
46302	0	90000	0	32709	5938	+5	CLA	P+95
46303	0	60100	0	47352	5939	+6	STO	PR+25
46304	0	60000	0	47353	5940	+7	STZ	PR+26
46305	0	90000	0	47361	5941	+8	CLA	PR+32
46306	0	56000	0	47330	5942	+9	LDQ	PR+7
46307	0	07400	4	25544	5943	+10	TSX	AZM,4
46310	0	07400	4	42602	5944	+11	TSX	ERROR,4
46311	0	56000	0	33730	5945	+12	LDQ	WPR+6
46312	0	26000	0	40245	5946	+13	FMP	FLCUP
46313	0	60100	0	47504	5947	+14	STO	Z+15
46314	0	56000	0	47343	5948	25.10	LDQ	PR+18
46315	0	26000	0	47343	5949	+1	FMP	PR+18
46316	0	24100	0	40216	5950	+2	FDP	FL4
46317	0	26000	0	47344	5951	+3	FMP	PR+19
4632	0	13100	0	00000	5952	+4	XCA	
46321	0	26000	0	40271	5953	+5	FMP	FLPI
46322	0	60100	0	47427	5954	+6	STO	PR+70
46323	0	56000	0	47504	5955	25.70	LDQ	Z+15
46324	0	50000	0	40215	5956	+1	CLA	FL3
46325	0	04000	0	46412	5957	+2	TLQ	26.00

RESTORING DELTA FOR HEAT TRANSFER  
PC. THIS ASSUMES PH, TM TO BE ZERO

PH

TC  
TM

TC 1+1  
PC 1+1

DCO

NO.

ACN

COMPRESSIBLE

TC 1+1  
TCM

PHM  
PCM LESS THAN PHM  
PCN=PCMV

PCN=PHM  
TCM  
PCM

25/09/64

46352	0	60100	0	47505	5979	+6	STO	Z+16
46353	0	90000	0	36173	5980	+7	CLA	TK+14
46354	0	30000	0	40213	5981	+8	FAD	FL1
46355	0	60100	0	47465	5982	+9	STO	Z
46356	0	90000	0	47330	5983	+10	CLA	PR+7
46357	0	30200	0	47332	5984	+11	FSB	PR+9
46360	0	24100	0	47465	5985	+12	FDP	Z
46361	0	26000	0	40272	5986	+13	FMP	FLGF
46362	0	24100	0	47505	5987	+14	FDP	Z+16
46363	0	26000	0	40267	5988	+15	FMP	FL288
46364	0	07400	4	24364	5989	+16	TSX	SQRT,4
46365	0	07400	4	42602	5990	+17	TSX	ERROR,4
46366	0	60100	0	47445	5991	+18	STO	PR+84
46367	0	24100	0	40244	5992	25.60	FDP	FL144
46370	0	26000	0	47427	5993	+1	FMP	PR+70
46371	0	13100	0	00000	5994	+2	XCA	
46372	0	26000	0	40255	5995	+3	FMP	FL.6
46373	0	13100	0	00000	5996	+4	XCA	
46374	0	26000	0	47505	5997	+5	FMP	Z+16
46375	0	13100	0	00000	5998	+6	XCA	
46376	0	50000	0	47403	5999	+7	CLA	PR+50
6000*WC ITERATION								
46377	0	07402	2	43624	6001	+8	TSX	ITER,2,2
46400	-0	47755	0	47576	6002	+9	MZE	IT+23,CLS2
46401	0	47754	0	47577	6003	+10	PZE	IT+24,CLS1
46402	0	40213	0	47600	6004	+11	PZE	IT+25,FL1
46403	3	47403	0	47314	6005	+12	PTH	YHD+5,PR+50
46404	3	00000	0	47302	6006	+13	PTH	XHD+5
46405	0	47757	0	47757	6007	+14	PZE	CLS4,CLS4
46406	0	02000	0	46601	6008	+15	TRA	27.00
46407	0	60100	0	47403	6009	+16	STO	PR+50
46410	-3	00000	6	45367	6010	+17	TXL	21.00,6,0
46411	0	02000	0	45352	6011	+18	TRA	20.90
6012* COMPRESSIBLE EQUATIONS								
46412	0	90000	0	47333	6013	26.00	CLA	PR+10
46413	0	60100	0	47332	6014	+1	STO	PR+9
46414	0	34000	0	47330	6015	+2	CAS	PR+7
46415	0	02000	0	46420	6016	+3	TRA	26.01
46416	0	02000	0	46423	6017	+4	TRA	26.02
46417	0	02000	0	46423	6018	+5	TRA	26.02
46420	0	56000	0	47403	6019	26.01	LDQ	PR+50
46421	0	26000	0	40254	6020	+1	FMP	FL.5
46422	0	02000	0	46576	6021	+2	TRA	H83
46423	0	90000	0	47402	6022	26.02	CLA	PR+49
46424	0	30200	0	40213	6023	+1	FSB	FL1
46425	-0	10000	0	46427	6024	+2	TNZ	26.10
46426	0	60000	0	47402	6025	+3	STZ	PR+49
46427	0	50000	0	40254	6026	26.10	CLA	FL.5
46430	-0	52000	0	47402	6027	+1	NZY	PR+49
46431	0	60100	0	47402	6028	+2	STO	PR+49
46432	0	56000	0	47402	6029	26.20	LDQ	PR+49
46433	0	26000	0	47402	6030	+1	FMP	PR+49
46434	0	60100	0	47466	6031	+2	STO	Z+1
46435	0	13100	0	00000	6032	+3	XCA	

KC IN = .5

PCI O  
PCM

RHO CM

VCM

ACN

VENA CAVA EFFECT

RHO CM

MR HOT INPUT

PCI O  
PCM = PHM

LOWER WC

MACH CM



44611	0	34000	0	47400	6141	27.10	LDQ	PR+47	
44612	0	26000	0	47400	6142	+1	FMP	PR+47	
44613	0	13100	0	00000	6143	+2	XCA		
44614	0	26000	0	47472	6144	+3	FMP	Z+5	K-1/2
44615	0	30000	0	40213	6145	+4	FAD	FL1	
44616	0	60100	0	47510	6146	+5	STO	Z+19	
44617	0	50000	0	36167	6147	+6	CLA	TK+10	
44620	0	30000	0	40213	6148	+7	FAD	FL1	
44621	0	24100	0	47472	6149	+8	FDP	Z+5	
44622	0	26000	0	40253	6150	+9	FMP	FL.25	
44623	0	13100	0	00000	6151	+10	XCA		
44624	0	50000	0	47510	6152	+11	CLA	Z+19	
44625	0	07400	1	47752	6153	+12	TSX	POWER,1	
44626	0	60100	0	47465	6154	+13	STO	Z	
44627	0	50000	0	36167	6155	27.20	CLA	TK+10	
44630	0	24100	0	47365	6156	+1	FDP	PR+36	TS 0
44631	0	26000	0	40272	6157	+2	FMP	FLGF	
44632	0	24160	7	47750	6158	+3	FDP*	NEHR+2,7	R HOT IR=2, R MIX IR=1
44633	0	13100	0	00000	6159	+4	XCA		
44634	0	07400	4	24364	6160	+5	TSX	SQRT,4	
44635	0	07400	4	42602	6161	+6	TSX	ERROR,4	
44636	0	13100	0	00000	6162	+7	XCA		
44637	0	26000	0	47400	6163	+8	FMP	PR+47	MHB
44640	0	24100	0	47465	6164	+9	FDP	Z	
44641	0	26000	0	47424	6165	+10	FMP	PR+67	AH
44642	0	13100	0	00000	6166	+11	XCA		
44643	0	26000	0	47334	6167	+12	FMP	PR+11	PB 0
44644	0	60100	0	47465	6168	+13	STO	Z	
44645	0	50000	0	47400	6169	+14	CLA	PR+47	
44646	0	30200	0	40213	6170	+15	FSB	FL1	
44647	0	10000	0	46671	6171	+16	TZE	27.30	MHB=1
44650	0	56000	0	47465	6172	+17	LDQ	Z	
44651	0	50000	0	47405	6173	+18	CLA	PR+52	WT
44652	0	07402	2	43624	6174	+19	TSX	ITER,2,2	
44653	0	47756	0	47561	6175	+20	PZE	IT+10,,CLS3	
44654	0	47754	0	47562	6176	+21	PZE	IT+11,,CLS1	
44655	0	40213	0	47563	6177	+22	PZE	IT+12,,FL1	
44656	3	47400	0	47316	6178	+23	PTH	YHD+7,,PR+47	
44657	3	00000	0	47304	6179	+24	PTH	XHD+7	
44660	0	47757	0	47757	6180	+25	PZE	CLS4,,CLS4	
44661	0	02000	0	46671	6181	+26	TRA	27.30	
44662	0	12000	0	46665	6182	+27	TPL	*+3	
44663	0	56000	0	47400	6183	+28	LDQ	PR+47	
44664	0	26000	0	40250	6184	+29	FMP	FL.1	
44665	0	34000	0	40213	6185	+30	CAS	FL1	
44666	0	50000	0	40213	6186	+31	CLA	FL1	
44667	0	50000	0	40213	6187	+32	CLA	FL1	
44670	0	02000	0	46610	6188	+33	TRA	27.10-1	
44671	0	50000	0	47365	6189	27.30	CLA	PR+36	TS 0
44672	0	24100	0	47510	6190	+1	FDP	Z+19	
44673	-0	60000	0	47355	6191	+2	STQ	PR+28	TS
44674	0	26000	0	40272	6192	27.40	FMP	FLGF	
44675	0	13100	0	00000	6193	+1	XCA		
44677	0	13100	0	00000	6195	+3	XCA		
44700	0	26060	7	47750	6196	+4	FMP*	NEHR+2,7	R HOT IR=2, R MIX IR=1
44701	0	07400	4	24364	6197	+5	TSX	SQRT,4	
44702	0	07400	4	42602	6198	+6	TSX	ERROR,4	
44703	0	60100	0	47511	6199	+7	STO	Z+20	
44704	0	13100	0	00000	6200	27.50	XCA		CH 8
44705	0	26000	0	47400	6201	+1	FMP	PR+47	MHB
44706	0	60100	0	47447	6202	+2	STO	PR+86	VB
44707	-0	50000	7	47750	6203	28.00	CAL	NEHR+2,7	
44710	0	62100	0	46712	6204	+1	STA	*+2	
44711	0	07400	4	27034	6205	+2	TSX	AZ0,4	
44712	0	00000	0	00000	6206	+3	PZE	*+0	COMPUTE PB
44713	0	50000	0	47510	6207	28.20	CLA	Z+19	
44714	0	56000	0	47513	6208	+1	LDQ	Z+22	
44715	0	07400	1	47752	6209	+2	TSX	POWER,1	K/K-1
44716	0	13100	0	00000	6210	+3	XCA		
44717	0	26000	0	47324	6211	+4	FMP	PR+3	PB
44720	0	60100	0	47514	6212	+5	STO	Z+23	PB 0 PRIME
44721	0	50000	0	47400	6213	28.30	CLA	PR+47	MACH HB
44722	0	30200	0	40213	6214	+1	FSB	FL1	
44723	-0	10000	0	46771	6215	+2	TNZ	28.50	
44724	0	50000	0	36167	6216	28.40	CLA	TK+10	
44725	0	30200	0	40213	6217	+1	FSB	FL1	
44726	0	60100	0	47465	6218	+2	STO	Z	K-1
44727	0	30000	0	40214	6219	+3	FAD	FL2	
44730	0	60100	0	47466	6220	+4	STO	Z+1	K+1
44731	0	24100	0	47465	6221	+5	FDP	Z	
44732	-0	60000	0	47465	6222	+6	STO	Z	K+1/K-1
44733	0	50000	0	40214	6223	+7	CLA	FL2	
44734	0	24100	0	47466	6224	+8	FDP	Z+1	
44735	0	13100	0	00000	6225	+9	XCA		K+1
44736	0	56000	0	47465	6226	+10	LDQ	Z	
44737	0	07400	1	47752	6227	+11	TSX	POWER,1	K+1/K-1
44740	0	13100	0	00000	6228	+12	XCA		
44741	0	26000	0	36167	6229	+13	FMP	TK+10	K
44742	0	24160	7	47750	6230	+14	FDP*	NEHR+2,7	R HOT IR=2, R MIX IR=1
44743	0	26000	0	40272	6231	+15	FMP	FLGF	
44744	0	24100	0	47365	6232	+16	FDP	PR+36	TS 0
44745	0	13100	0	00000	6233	+17	XCA		
44746	0	07400	4	24364	6234	+18	TSX	SQRT,4	
44747	0	07400	4	42602	6235	+19	TSX	ERROR,4	
44750	0	13100	0	00000	6236	+20	XCA		
44751	0	26000	0	47334	6237	+21	FMP	PR+11	PB 0
44752	0	13100	0	00000	6238	+22	XCA		
44753	0	26000	0	47424	6239	+23	FMP	PR+67	AH
44754	0	13100	0	00000	6240	+24	XCA		
44755	0	50000	0	47405	6241	+25	CLA	PR+52	WT
44756	0	07402	2	43624	6242	+26	TSX	ITER,2,2	
44757	-0	47755	0	47564	6243	+27	NZE	IT+13,,CLS2	
44760	0	47754	0	47565	6244	+28	PZE	IT+14,,CLS1	
44761	0	40213	0	47566	6245	+29	PZE	IT+15,,FL1	
44762	3	47405	0	47317	6246	+30	PTH	YHD+8,,PR+52	
44763	3	00000	0	47305	6247	+31	PTH	XHD+8	
44764	0	47757	0	47757	6248	+32	PZE	CLS4,,CLS4	

44677	0	13100	0	00000	6195	+3	XCA		
44700	0	26060	7	47750	6196	+4	FMP*	NEHR+2,7	R HOT IR=2, R MIX IR=1
44701	0	07400	4	24364	6197	+5	TSX	SQRT,4	
44702	0	07400	4	42602	6198	+6	TSX	ERROR,4	
44703	0	60100	0	47511	6199	+7	STO	Z+20	
44704	0	13100	0	00000	6200	27.50	XCA		CH 8
44705	0	26000	0	47400	6201	+1	FMP	PR+47	MHB
44706	0	60100	0	47447	6202	+2	STO	PR+86	VB
44707	-0	50000	7	47750	6203	28.00	CAL	NEHR+2,7	
44710	0	62100	0	46712	6204	+1	STA	*+2	
44711	0	07400	4	27034	6205	+2	TSX	AZ0,4	
44712	0	00000	0	00000	6206	+3	PZE	*+0	COMPUTE PB
44713	0	50000	0	47510	6207	28.20	CLA	Z+19	
44714	0	56000	0	47513	6208	+1	LDQ	Z+22	
44715	0	07400	1	47752	6209	+2	TSX	POWER,1	K/K-1
44716	0	13100	0	00000	6210	+3	XCA		
44717	0	26000	0	47324	6211	+4	FMP	PR+3	PB
44720	0	60100	0	47514	6212	+5	STO	Z+23	PB 0 PRIME
44721	0	50000	0	47400	6213	28.30	CLA	PR+47	MACH HB
44722	0	30200	0	40213	6214	+1	FSB	FL1	
44723	-0	10000	0	46771	6215	+2	TNZ	28.50	
44724	0	50000	0	36167	6216	28.40	CLA	TK+10	
44725	0	30200	0	40213	6217	+1	FSB	FL1	
44726	0	60100	0	47465	6218	+2	STO	Z	K-1
44727	0	30000	0	40214	6219	+3	FAD	FL2	
44730	0	60100	0	47466	6220	+4	STO	Z+1	K+1
44731	0	24100	0	47465	6221	+5	FDP	Z	
44732	-0	60000	0	47465	6222	+6	STO	Z	K+1/K-1
44733	0	50000	0	40214	6223	+7	CLA	FL2	
44734	0	24100	0	47466	6224	+8	FDP	Z+1	
44735	0	13100	0	00000	6225	+9	XCA		K+1
44736	0	56000	0	47465	6226	+10	LDQ	Z	
44737	0	07400	1	47752	6227	+11	TSX	POWER,1	K+1/K-1
44740	0	13100	0	00000	6228	+12	XCA		
44741	0	26000	0	36167	6229	+13	FMP	TK+10	K
44742	0	24160	7	47750	6230	+14	FDP*	NEHR+2,7	R HOT IR=2, R MIX IR=1
44743	0	26000	0	40272	6231	+15	FMP	FLGF	
44744	0	24100	0	47365	6232	+16	FDP	PR+36	TS 0
44745	0	13100	0	00000	6233	+17	XCA		
44746	0	07400	4	24364	6234	+18	TSX	SQRT,4	
44747	0	07400	4	42602	6235	+19	TSX	ERROR,4	
44750	0								

46765	0	02000	0	47017	6249	+33	TRA	MB1	
46766	0	30200	0	47403	6250	+34	FSB	PR+50	
46767	0	60100	0	47404	6251	+35	STO	PR+51	
46770	0	02000	0	47014	6252	+36	TRA	MB2+1	
46771	0	50000	0	47334	6253	28.50	CLA	PR+11	
46772	0	56000	0	47514	6254	+1	LDQ	Z+23	
46773	0	07402	2	43624	6255	+2	TSX	ITER,2,2	
46774	0	47755	0	47567	6256	+3	PZE	IT+10,,CLS2	
46775	0	47754	0	47570	6257	+4	PZE	IT+17,,CLS1	
46776	0	40213	0	47571	6258	+5	PZE	IT+18,,FL1	
46777	3	47404	0	47320	6259	+6	PTM	VMD+9,,PR+51	
47000	3	00000	0	47306	6260	+7	PTM	XMD+9	
47001	0	47757	0	47757	6261	+8	PZE	CLS4,,CLS4	
47002	0	02000	0	47017	6262	+9	TRA	MB1	
47003	0	12000	0	47013	6263	28.60	TPL	MB2	
47004	0	77400	1	00003	6264	+1	AKT	3,1	INITIALIZE FOR NEW GUESS
47005	0	60000	1	47572	6265	+2	STZ	IT+19,1	
47006	2	00001	1	47005	6266	+3	TIX	0-1,1,1	
47007	-0	76000	0	00142	6267	+4	SLT	Z	
47010	0	02000	0	47041	6268	+5	TRA	MB7	WDDTH NEG 2ND TIME
47011	0	56000	0	47404	6269	+6	LDQ	PR+51	LOWER WDDTH GUESS
47012	0	26000	0	40256	6270	+7	FMP	FL.8	
47013	0	60100	0	47404	6271	MB2	STO	PR+51	
47014	0	30000	0	47407	6272	+1	FAD	PR+54	WN
47015	0	77400	7	00002	6273	+2	AXT	2,7	
47016	0	02000	0	45101	6274	+3	TRA	20.01	NEW WR
47017	0	50000	0	47365	6275	MB1	CLA	PR+36	TOB
47020	0	60100	0	47353	6276	+1	STO	PR+26	TH
47021	0	52000	0	44105	6277	+2	ZET	SWT	
47022	0	07400	4	47024	6278	+3	TSX	HBP,4	PRINT
47023	0	02000	0	47044	6279	+4	TRA	HBR-5	
							4280+PRINT REGION		
47024	0	63400	4	47041	6281		SKA	HBP,4	
47025	0	63400	1	47042	6282	+1	SKA	HBP+1,1	
47026	0	50000	0	47334	6283	+2	CLA	PR+11	
47027	0	10000	0	47031	6284	+3	TZE	+2	
47030	0	60100	0	47322	6285	+4	STO	PR+1	PH
47031	0	77400	1	00031	6286	+5	AXT	25,1	
47032	0	07400	4	00052	6287	PRIN1	TSX	DOUT,4	
47033	3	02001	1	47136	6288	+1	PTM	MD1+25,1,1025	
47034	0	05722	0	00036	6289	+2	PZE	30,,3026	
47035	-3	11655	1	47352	6290	+3	SVN	PR+25,1,5037	
47036	0	05722	0	00031	6291	+4	PZE	25,,3026	
47037	1	00000	0	44106	6292	+5	PDN	MODE	
47040	2	00001	1	47032	6293	+6	TIX	PRIN1,1,1	
47041	0	77400	4	00000	6294	MBPR	AXT	**0,4	
47042	0	77400	1	00000	6295	+1	AXT	**0,1	
47043	0	02000	4	00001	6296	+2	TRA	1,4	
47044	0	76000	0	00140	6297	+3	SLF		
47045	0	77400	1	00144	6298	+4	AXT	100,1	
47046	0	60000	1	47713	6299	+5	STZ	IT+100,1	
47047	2	00001	1	47046	6300	+6	TIX	0-1,1,1	
47050	0	07400	4	44713	6301	+7	TSX	HBO,4	OUTPUT
47051	0	77400	4	00000	6302	HBR	AXT	**0,4	

47052	0	77400	2	00000	6303	+1	AXT	**0,2	
47053	0	77400	3	00000	6304	+2	AXT	**0,3	
47054	0	77400	1	00000	6305	+3	AXT	**0,1	
47055	0	77400	5	00000	6306	+4	AXT	**0,5	
47056	0	77400	6	00000	6307	+5	AXT	**0,6	
47057	0	77400	7	00000	6308	+6	AXT	**0,7	
47060	0	02000	4	00003	6309	+7	TRA	3,4	
47061	0	52200	0	47051	6310	MB7	XEC	HBR	ERROR
47062	1	00002	4	47052	6311	+1	YXI	HBR+1,4,2	RETURN FOR WDDTH NEG
47063	0	52200	0	47051	6312	MB8	XEC	HBR	
47064	1	00001	4	47052	6313	+1	YXI	HBR+1,4,1	ERROR RETN FOR PC NEGATIVE
					6314+ERROR RECOVERY FROM ITER				
47065	0	60200	0	47070	6315	MB4	SLW	MB5	NAME OF LOOP IN AC
47066	-1	47070	0	25421	6316	+1	STR	AZF,,MB5	
47067	0	02000	2	00007	6317	+2	TRA	7,2	NORMAL ITER RETURN
47070	-2	06060	6	06060	6318	MB5	BCI	3,	NOT CLOSED
47073	-0	52551	6	54644	6319	HOHD	BCI	,NERVOUS BALANCE	HOT BLEED PORT PROGRAM
47105	-0	72360	6	06060	6320	MD1	BCI	,PC PH P6 P8 P2C PC1C P11 PC I+1PH I+1PCW	
47117	-0	73044	6	06060	6321	+10	BCI	,PHM PD 8 DELTAPPHIC DM T R DCO NO.	
47131	-2	33025	6	32160	6322	+20	BCI	,THEYA DSLA CDSLA HG POS	
47143	-2	32366	6	06060	6323	+30	BCI	,TC TH T6 T8 T2C TC1C TC I+1TH I+1TCW	
47155	-2	33044	6	06060	6324	+40	BCI	,THM TO 8 TMC DELTASDELTALENGTHMCM**F MCM**F LCI	
47167	-0	33031	6	06060	6325	+50	BCI	,LMI KM M MB M HM M CM	
47201	-2	62366	6	06060	6326	MD3	BCI	,MC MH WT MR MN	
47213	-2	32366	3	16060	6327	+10	BCI	,TCMI THMI	
47225	2	12345	6	06060	6328	+20	BCI	,ACN AN ATN A-COOLD-COOLD	
47237	2	34023	4	64324	6329	MD4	BCI	,C-COLDA -HOT8 -HOTC -HOTFRIC-FRICE-MKIN KCIN-CXKIN-IVCM	
47251	-2	53044	6	06060	6330	+10	BCI	,VHM VS V6 VIN2 OSUBI HT FLCK FLAGA B	
47263	-0	26560	6	06060	6331	+20	BCI	,KV MR HOTMR MIXMR FLG	
47275	-0	43044	6	06060	6332	XHD	BCI	,MMH Q THW TCW TMI MC MCM MMB WT MH	
47307	-0	43044	6	06060	6333	YMD	BCI	,MMH Q THW TCW TMI MC PCW WT MH P8 0	
					47321	PR	BSS	100,F	
					47465	Z	BSS	50,F	
					47547	IT	BSS	100,F	
					47713	Y	BSS	1,0	
					47714	BSS	BSS	1,X	
					6339+		SUBROUTINES	TO CALCULATE NEW R HOT,R MIX NEW MOB,NEW CSUB (PH,MIX)	
47715	0	50000	7	47463	6340	NEWRCPL	CLA	PR+98,7	MR HOT IR=2, MR MIX IR=1
47716	0	30000	0	40213	6341	+1	FAD	FL1	
47717	0	60100	0	12512	6342	+2	STO	KOM	
47720	0	56000	0	40260	6343	+3	LDQ	FL48,2	
47721	0	26000	7	47463	6344	+4	FMP	PR+98,7	MR HOT IR=2, MR MIX IR=1
47722	0	30000	0	40242	6345	+5	FAC	FL76	
47723	0	24100	0	12512	6346	+6	FDP	KOM	
47724	-0	60060	7	47750	6347	+7	STG+	NEWR+2,7	NEW RMOT AND R MIX
47725	0	56000	0	40252	6348	+8	LDQ	FL.219	
47726	0	26000	7	47463	6349	+9	FMP	PR+98,7	MR HOT IR=2, MR MIX IR=1
47727	0	30000	0	40257	6350	+10	FAD	FL3.45	
47730	0	24100	0	12512	6351	+11	FDP	KOM	
47731	-0	60060	7	47752	6352	+12	STO+	NEWCP+2,7	NEW C SUBP HOT AND MIX
47732	0	02000	4	00001	6353	+13	TRA	1,4	
47733	0	60100	0	12512	6354	RHMNR	STO	KOM	P
47734	-0	60000	0	12513	6355	+1	STO	KOM+1	T COMPUTE DENSITY
47735	0	24160	7	47750	6356	+2	FDP+	NEWR+2,7	R HOT IR=2, R MIX IR=1

47736	0	26000	0	40244	6357	+3	FMP	FL144				
47737	0	24100	0	12513	6358	+4	FDP	KON+1	T			
47740	0	13100	0	00000	6359	+5	XCA					
47741	0	02000	4	00001	6360	+6	TRA	1,4				
47742	0	30200	0	40263	6361		NEWH	FS8	TEMP. IN AC			
47743	0	13100	0	00000	6362	+1	XCA					
47744	0	26060	7	47752	6363	+2	FMP*	NEWCP+2,7	C SUB P MIX			
47745	0	02000	4	00001	6364	+3	TRA	1,4				
47746	0	00000	0	36175	6365		NEWR	HTR	TR+16	R HOT		
47747	0	00000	0	47540	6366	+1	HTR	Z+43	R MIX			
47750	0	00000	0	47541	6367		NEWCP	HTR	Z+44	CP HOT		
47751	0	00000	0	47542	6368	+1	HTR	Z+45	CP MIX			
				12512	6369		KON	EQU	COMMON			
					6370*		POWER SUBROUTINE					
47752	0	07400	4	27021	6371		POWER	TSX	AZE,4			
47753	0	02000	1	00001	6372	+1	TRA	1,1				
47754	1	72507	5	34122	6373		CLS1	DEC	.01			
47755	1	67406	1	11565	6374		CLS2	DEC	.001			
47756	1	63643	3	34273	6375		CLS3	DEC	.0001			
47757	1	60517	4	26542	6376		CLS4	DEC	.00001			
					6377*		CAVEMAN ENTHALPY VS.	TEMP TABLE FOR HOT TEMPS				
47760	2	13651	0	00000	6378		THOT	DEC	1700.,510.,2000.,595.,2300.,680.,2700.,795.,3200.,940.			
47772	2	14764	0	00000	6379	+10	DEC		4000.,1155.,5500.,1600.,7500.,2150.,9000.,2550.,11000.			
50003	2	14575	2	00000	6380	+19	DEC		3050.,13000.,3555.,15000.,4050.,17000.,4500.,19100.,5000.			
50014	2	17470	4	00000	6381	+28	DEC		20000.,5200.,21000.,5400.,22000.,5600.,24000.,6000.			
					6382*		CAVEMAN TEMP VS.	SOME SORT OF THERMAL CONDUCTIVITY				
50024	0	00000	0	00000	6383		KSUBM	DEC	0.,0.,200.,115E-6,2000.,355E-6			

51162	0	00000	0	50032	6385		AZKI	BSS	12*CARDS,H	STORAGE FOR STANDARD CASE, BCD		
				00000	6386		AZNT	PZE		TEMP STORAGE FOR EACH PHASE PART		
				15061	6387		AZMTG	EQU	AZMT-AZMTB	GAP BETWEEN PART AND CURRENT STORAGE		
				37357	6388		AZMTP	EQU	AZD+100*NCNTP-1	END OF PART CURVES		
				01775	6389		AZMTS	EQU	AZMTE-AZMTB	SIZE OF STORAGE FOR EACH PART		
				00062	6390		CARDS	EQU	50	MAX NO. CARDS IN STD CASE		
				00012	6391		NCURV	EQU	10	TOTAL NO. CURVES		
				00006	6392		NCNTP	EQU	6	NO. CURVES FOR ONE PART		
				00024	6393		NHIT	EQU	20	MAX NO. HEAT TRANSFER ITERATIONS		
				00067	6394		NLMAX	EQU	55	MAX NO LINES/PAGE		
				00062	6395		NZMAX	EQU	50	MAX NO. NODES/PART		
				24416	6396			END	BEGIN			

SBCENT	*0065	*KPRINT	0001	22.70	*0090	ZPI	*0058	AYE1	0036
S8VYAS	0065	*KPUNCH	*0001	22.80	*0091	58BCD	0065	AYE2	0036
ALPHAC	0074	KRBUFF	*0001	22.90	0091	58EOF	0065	AYEA	0037
AS58C1	0065	*KRTAPE	*0001	22.95	0091	58IR1	0065	AYEA1	0037
AS58C2	0065	KSERCH	*0001	22.99	0092	58IR2	0065	AYER	0036
AS58C3	0065	KSHORT	*0001	23.00	0092	58IR4	0065	AYG	0037
AS58D1	0065	KSQZRD	*0001	23.10	*0092	58MIL	0065	AYGA	0038
AS58F1	0065	KSTART	*0001	23.20	*0092	58ONE	0065	AYGR	0038
AS58F2	0065	KSTIME	*0001	23.30	0093	58TEN	*0065	AYH	0039
AS58Y1	0065	KSTUFF	*0001	23.40	*0093	ACI	0079	AYH1	0040
*COMMON	0001	KTAKEB	0001	23.50	*0093	ANA	0077	AYH2	0040
DELTAZ	0079	KTIMEX	*0001	23.65	*0093	AS58	0064	AYHR	0040
DSUBHI	0078	KTUNIT	*0001	23.70	*0093	AS58A	0065	AYI	0040
FL128.	0058	KUNFLO	*0001	23.80	*0094	AS58B	0065	AYI1	0040
FL12E8	0058	KMBUFF	*0001	23.90	*0094	AS58C	0065	AYI1	0040
FL3.45	0058	KWITAP	*0001	23.91	*0095	AS58D	0065	AYI11	*0040
FL48.2	0058	*KMTAPE	*0001	23.92	0095	AS58E	0065	AYI12	0041
FL.219	0058	NEWRC	0103	23.93	7095	AS58F	0065	AYI1R	0040
GAMMAC	0074	ST1763	0064	23.94	0095	AS58G	0065	AYIR	0040
ITERTA	0077	ST59.4	0064	24.00	0095	AS58H	0065	AYJ	0041
ITERPX	0077	ST59.7	0064	25.00	0096	AS58J	0065	AYJ1	0041
KBINLD	0001	TSUBCI	0079	25.10	*0096	AS58K	0065	AYK	0041
KCLOCK	*0001	TSUBHI	0079	25.20	*0096	AS58P	0065	AYK01	0045
KDATEA	0001	1000.	0058	25.30	*0096	AS58Q	0065	AYK02	0045
KDATEN	*0001	188	0058	25.40	0096	AS58V	0065	AYK1	0044
KDEBEG	0001	20.00	*0083	25.50	0096	AS58W	0065	AYK2	*0044
*KDELAY	*0001	20.01	0084	25.60	*0097	AS58X	0065	AYK3	0044
KENTRY	*0001	20.50	0084	26.00	0097	AS58Y	0065	AYK4	0042
*KERROR	0001	20.55	*0084	26.01	0097	AS58Z	0065	AYK5	0042
*KFINIS	0001	20.56	*0084	26.02	0097	AYA	0029	AYK6	0042
KINDX1	*0001	20.58	*0085	26.10	0097	AYA1	0031	AYK7	0042
KINDX2	*0001	20.60	*0085	26.20	0097	AYAR	0031	AYK8	0042
*KINDX4	0001	20.65	*0085	26.30	0098	AYB	0031	AYK9	0045
KISBSF	*0001	20.70	*0085	26.40	*0098	AYB1	0031	AYKR	0042
*KISBSR	*0001	20.75	*0085	26.50	*0098	AYB2	0032	AYL	0045
KISETT	*0001	20.76	*0085	26.60	*0099	AYB3	0032	AYL2	0045
*KISORG	*0001	20.77	*0085	27.00	0099	AYB4	0032	AYLA	0046
*KISOUT	0001	20.80	0086	27.01	0099	AYBR	0032	AYL0	0046
KISREW	*0001	20.85	*0086	27.10	0100	AYBT	0032	AYLP	0046
KISRTT	*0001	20.90	0087	27.20	*0100	AYBW	0032	AYLR	0045
KISTAT	*0001	21.00	0087	27.30	0100	AYC	0032	AYLW	0046
KISNEF	*0001	21.05	*0089	27.40	*0100	AYCA	0035	AYM	0046
*KJOBND	*0001	21.99	0089	27.50	*0101	AYCA1	0035	AYN	0046
KLCSTR	0001	22.00	0089	28.00	*0101	AYCR	0035	AYN1	0046
KLCCAT	*0001	22.10	*0089	28.20	*0101	AYD	0035	AYPA	0047
KLR0UT	*0001	22.20	*0089	28.30	*0101	AYD01	0036	AYPA1	0047
*KMCVEB	0001	22.30	*0089	28.40	*0101	AYD1	0036	AYPAR	0047
KONLIN	0001	22.40	*0089	28.50	0102	AYD2	0036	AYPB	0047
*KOPIMP	*0001	22.50	*0090	28.60	*0102	AYDR	0036	AYPB1	0048
*KCVFLO	0001	22.60	*0090	288	0058	AYE	0036	AYPB2	0048

AYPB3 0048	AZC 0011	AZK 0017	AZM11 0019	AZQ 0025
AYPBR 0048	AZC1 0011	AZK1 0018	AZMR 0019	AZQR 0025
AYC 0048	AZC2 0011	AZK2 0018	AZNR 0074	AZT 0005
AYQ1 0048	AZCR 0011	AZK3 0018	AZNW 0019	AZT1 0006
AYOR 0048	AZO 0057	AZK4 0018	AZMW1 0019	AZT2 0006
AYR 0048	AZE 0025	AZKR 0018	AZMW2 0019	AZT3 0007
AYR1 0049	AZE1 0025	AZL 0018	AZNR 0019	AZT4 0007
AYR2 0049	AZER 0025	AZLR 0018	AZP3 0021	AZTR 0006
AYR3 0049	AZF 0011	AZM01 0005	AZPC 0019	AZU 0026
AYRR 0049	AZF1 0012	AZM1 *0003	AZPC1 0020	AZU1 0026
AYT 0049	AZF2 0012	AZM10 0004	AZPC2 0020	AZU2 0026
AYT1 0049	AZF3 0011	AZM11 0005	AZPC3 0020	AZU3 0026
AZ01 0055	AZFF 0011	AZM12 0004	AZPCR 0020	AZU4 0026
AZ02 0055	AZFR 0012	AZM17 0003	AZPD 0020	AZU5 0026
AZ03 0055	AZFT 0012	AZM19 0004	AZPD1 0020	AZU6 0026
AZ04 0055	AZFT1 0012	AZM2 *0004	AZPD2 0021	AZUR 0026
AZ05 0055	AZG 0012	AZM20 0005	AZPD3 0021	AZV 0026
AZ06 0055	AZG1 0013	AZM21 0005	AZPD4 0021	AZV1 0026
AZ07 0055	AZGR 0013	AZM22 0005	AZPD5 0021	AZV2 0026
AZ08 0055	AZM 0013	AZM23 0005	AZPD6 0021	AZVR 0026
AZ09 0055	AZM1 0014	AZM24 0002	AZPD7 0021	AZX 0027
AZA 0007	AZM2 0013	AZM25 0002	AZPD8 0021	AZX1 0027
AZA1 0007	AZM3 0013	AZM26 0002	AZPD9 0021	AZX2 0027
AZAA 0007	AZM4 0014	AZM27 0003	AZPDR 0020	AZX3 0027
AZAA1 0008	AZMR 0014	AZM28 0003	AZP1 0021	AZX4 0027
AZAAAR 0008	AZI 0014	AZM29 *0004	AZP11 0022	AZX5 0027
AZAB 0008	AZI01 0015	AZM3 *0005	AZP12 0021	AZX6 0027
AZAB1 0008	AZI1 0015	AZM30 0005	AZP13 0021	AZX7 0027
AZAB2 0009	AZI2 0015	AZM31 0004	AZP14 0022	AZX8 0027
AZABR 0009	AZI3 0015	AZM32 0003	AZP15 0022	AZX9 0027
AZAC 0009	AZI4 0015	AZM4 0005	AZP16 0022	AZXA 0027
AZAC1 0009	AZI5 0016	AZM5 0002	AZP17 0022	AZXA1 0027
AZAC2 0009	AZI6 *0015	AZM6 0003	AZP18 0022	AZXA2 0028
AZAC3 0009	AZI7 0015	AZM7 0002	AZP19 0022	AZXA3 0028
AZAC4 0010	AZIR 0015	AZM8 0002	AZP1B 0023	AZXA4 0028
AZAC5 0009	AZJ 0016	AZM9 0003	AZPIR 0022	AZXA5 *0028
AZAC6 0009	AZJ1 0017	AZMT 0104	AZPN 0023	AZXAAR 0027
AZAC7 0009	AZJ10 0017	AZMTB 0055	AZPN1 0023	AZXB 0028
AZACR 0009	AZJ11 0017	AZMTC 0057	AZPN2 0023	AZXB1 0028
AZB 0010	AZJ12 0017	AZMTE 0056	AZPNR 0023	AZXB2 0028
AZB10 0010	AZJ13 0016	AZMTG 0104	AZPP 0023	AZXB3 0028
AZB11 0010	AZJ2 0017	AZMTP 0104	AZPP1 0024	AZXB4 0028
AZB12 0010	AZJ3 0016	AZMTS 0104	AZPP2 0024	AZXC 0028
AZB2 0010	AZJ4 0017	AZN 0065	AZPP4 0024	AZXC1 0028
AZB3 0010	AZJ5 0017	AZN1 0074	AZPP5 0024	AZXC2 0028
AZB5 0010	AZJ6 0017	AZN2 0079	AZPP6 0024	AZXC3 0029
AZB7 0010	AZJ7 0016	AZN3 0078	AZPP7 0024	AZXC4 0028
AZB8 0010	AZJ8 0016	AZN4 0066	AZPPR 0024	AZXCRC 0029
AZB9 0010	AZJ9 0017	AZN5 0079	AZPS1 0021	AZXI 0104
AZBR 0010	AZJR 0017	AZNI 0018	AZPS3 0021	AZXR 0027

AZY 0029	DA6 0056	DNX 0056	EQT3 0064	FL.8 0058
AZZ 0029	DAHOT *0057	DNZFF 0056	EQT3R 0064	FL.9 *0058
BA 0065	DAKV 0056	*DOU 0001	EREXP 0078	FL.95 *0058
BCDD 0058	DASTR 0056	DP11 0057	ERLN 0078	FR 0065
BDNA 0060	DB *0057	DP1ZE 0056	ERROR 0065	FRICT 0078
BDNB 0062	DBHQT *0057	DP8E 0056	EXP 0001	FX 0055
BDXA 0060	DBKV 0056	DPD *0001	EXP13 *0001	FX1 0057
BDXB 0062	DC *0057	DPD1 *0001	FINQ1 0067	FX10 0057
BEGIN 0002	DCMOT *0057	DPDT *0001	FIX 0058	FX1E3 0057
BELLO 0057	DD2 0056	DPI 0056	FL1 0057	FX2 *0057
BETAC 0074	DDCO 0056	DPD 0056	FL10 0057	FX3 *0057
BIG 0058	DDH 0056	DPR1 0056	FL100 0058	FX4 *0057
BLANK 0058	DDIL 0056	DPX 0056	FL108 0058	FX5 *0057
BUG 0074	DDRN 0056	DQINT 0056	FL12 0057	FX6 *0057
BUG1 0074	DDTL 0056	DR 0056	FL139 0058	FX7 0057
BUG2 0074	DDTH 0056	DRC *0057	FL144 0058	FX8 *0057
C 0055	DEG *0058	DRH 0057	FL180 *0058	FX9 *0057
CARDS 0104	DEL 0056	DRHOR 0055	FL1E5 0058	F.A 0064
CCI 0079	DELZ 0055	DSA *0001	FL1.1 *0058	F.B 0064
CD 0065	DEN *0001	DSAT *0001	FL1.2 *0058	F.C 0064
CH 0078	DEN1 *0001	DST *0001	FL1.5 *0058	F.D 0064
CLOS0 0074	DENT *0001	DSTT *0001	FL2 0057	F.E 0064
CLS1 0104	DFCLO *0057	DSUBC 0079	FL288 0058	F.F 0064
CLS2 0104	DFP 0055	DSUBH 0079	FL2G 0058	F.G 0064
CLS3 0104	DFHOT 0057	DSHT 0056	FL2GI 0058	F.H 0064
CLS4 0104	DGP 0056	DT 0056	FL2RW 0058	F.I 0064
CNT6 0070	DHE 0056	DT11 0057	FL3 0057	F.J 0064
CNT7 0072	DHRN 0067	DTHO 0056	FL3.7 0058	F.K 0064
CNT8 0073	DIPY 0056	DTMET 0057	FL4 0057	F.L 0064
CNT9 0074	DIVCK 0078	DTI 0056	FL5 *0057	GO 0002
COLUM 0055	DK 0056	DTMAX 0056	FL58 0058	HB 0082
COS 0065	DK11 0057	DTMI 0056	FL6 *0057	HB1 0102
COUNT 0055	DK2 0056	DTMIN 0056	FL66 0058	HB2 0102
CP3 *0001	DK9 0057	DVF 0055	FL7 *0057	HB3 0099
CP31 *0001	DKCC *0057	DVI 0056	FL776 0058	HB4 0103
CP3T *0001	DKCI *0057	DVO 0056	FL8 *0057	HB5 0103
CPH *0001	DKDPI 0056	DWC 0056	FL9 *0057	HB6 0103
CPH1 *0001	DKDPO 0056	DWCE 0056	FLCUF 0058	HB7 0103
CPHT *0001	DKE *0057	DWN 0056	FLG 0058	HB8 0103
CURV1 0063	DKFLG 0057	DWP 0056	FLGAL 0058	HB1 0081
CURV4 0064	DKIN *0057	DWPE 0056	FLGF 0058	HB0 0082
CURV5 0064	DKPCM *0057	DWRE 0056	FLPI 0058	HBP 0102
CURV6 0064	DKPHM 0057	DWT 0056	FLR 0058	HBPR 0102
CURV7 0064	DL 0056	END 0065	FLRB 0058	HB1 0102
CURV8 0064	DMDT 0056	ENOD 0055	FL.1 0058	HB2 0082
CURVC 0064	DMAX 0055	ENT *0001	FL.2 0058	HCI 0079
CURVR 0064	DMDY 0056	ENT1 *0001	FL.25 0058	HD1 0103
CUT 0059	DNI 0056	ENTT *0001	FL.4 0058	HD3 *0103
D 0055	DNI 0056	EQT1 0064	FL.5 0058	HD4 *0103
DA 0057	DNP 0056	EQT2 0064	FL.6 0058	HDMD *0103

MEDER 0039	LN 0001	NUTMI 0064	PR98 0052	RMD4 00079
MHI 0079	LO 0065	NUTMW 0071	PR99 0052	RMDR 0103
ICURV 0043	LQ1 0079	NZMAX 0104	PRES3 0064	ROTAT 00073
IN 0065	LT6 0075	P 0055	PRIN1 0102	RSUM 0079
INDAT 00078	LTCM 0078	P3 0079	PRINT 0053	SCURV 0063
INT 00001	LTM 0075	PA 0054	PRP 0049	SET 0065
IR1 0065	LTMW 0078	PC 0055	PRP1 0050	SIGMA 0079
IR2 0065	LVSAC 0078	PEXP 00001	PRP10 0050	SIN 0065
IR4 0065	LVSAC 0078	PF 0054	PRP11 0050	SPACE 0064
IT 0103	LVSCH 0078	PG 00054	PRP4 0050	SGRT 0001
ITDCD 0077	LVSCH 0078	PI 0058	PRP6 0050	ST102 0064
ITER 0075	LVSIS 0078	PIN 0079	PRP7 0050	ST108 0064
ITER1 0075	LVSIN 0078	PL 0054	PRP8 0050	ST220 0064
ITER2 0075	MAKER 0079	PL1 0054	PRP9 0050	ST293 0064
ITER3 0076	MODE 0078	PL2 0055	PRPT1 00001	ST440 0064
ITER4 0076	NCTMP 0104	PLOG 00001	PRPTY 00001	STAR1 0064
ITER5 0076	NCURV 0104	PLR 0054	PRTD 0051	START 0002
ITER6 0076	NE 0065	PMB 00001	PSQT 00001	STF72 0064
ITER7 0076	NEHA 0060	PMB1 00001	PST 00001	STP1 0064
ITER8 0077	NEHA1 0061	PMBT 00001	PSTT 00001	STPIC 0064
ITER9 0077	NEHA2 0060	POWER 0104	PSUBC 0079	STP2 0064
ITERP 0077	NEHA3 0060	PP01 0053	PT 0055	STP3 0064
ITERR 0077	NEHA3 0060	PP04 0053	PYT 00001	STP2C 0064
ITERR 0077	NEHA3 0060	PP05 0053	PYT1 00001	STP3C 0064
ITEXP 0077	NEHA7 0060	PP06 0053	PYTT 00001	STP4 0064
KM 0079	NEHA8 0060	PP07 0054	PZ 0054	STP4C 0064
KCM 0104	NEHA9 0061	PP075 0054	Q 0077	STP5 0064
KCM1 0079	NEHAR 0060	PP08 0054	Q1 0079	STP5C 0064
KCM10 0079	NEHB 0061	PP09 0054	Q1INT 0078	STP6 0064
KCM11 0079	NEHB1 0062	PP40 0059	Q1NU 0074	STP6C 0064
KCM12 0079	NEHB2 0062	PP41 0059	Q1OK 0073	STP7 0064
KCM13 0079	NEHB3 0062	PP97 0054	RAD 0058	STP7C 0064
KCM17 0079	NEHB5 0062	PP98 0054	RAPA 0061	STP8 0064
KCM39 0078	NEHB6 0062	PP99 0054	RAPA1 0061	STP8C 0064
KCM40 0074	NEHB7 0062	PR 0103	RAPA2 0061	STP9 0064
KCM41 0074	NEHB8 0062	PRO1 0052	RAPA5 0061	STP9C 0064
KCM42 0074	NEHB8 0062	PRO2 0051	RAPA6 0061	STPXC 0064
KCM44 0074	NEHB9 0062	PRO23 0052	RAPA7 0061	STP6 0064
KCMS 0079	NEHBR 0062	PRO24 0051	RAPA8 0061	STPG1 0064
KCMS0 0078	NEHCP 0104	PRO3 0051	RAPA9 0061	STPG2 0064
KCMS1 0078	NEHW 0104	PRO4 0052	RAPB 0062	STPG3 0064
KCMS2 0078	NEHR 0104	PR10 0051	RAPB1 0063	STPG4 0064
KCMS3 0078	NLEFT 0078	PR11 0052	RAPB2 0063	STPG5 0064
KCMS4 0078	NLMAX 0104	PR12 0051	RAPB3 0062	STPZO 0064
KCMS5 0078	NRA 00001	PR13 0052	RAPB4 0063	SWT 0078
KCMS 0079	NRAT 00001	PR14 0052	RAPB5 0063	S(TP) 0064
KSUBR 0104	NTOTL 0078	PR15 0052	RAPB6 0063	T3 0079
LAST 0079	NUM 0079	PR60 0059	RAPB7 0063	T6 0079
LINT 0065	NUMBR 0078	PR61 0059	RAPB8 0062	TCARD 0055
LINTS 0065	NUTCW 0070	PR971 0052	RAPB9 0063	TCW 0079

TCMOK 0070	THINT 0078	TSUBH 0079	WH 0055	XHD 0103
TEMP 0079	THOT 0104	TY 0078	WHT 0055	XLC 00001
TEMPR 0064	THW 0079	VIS 0001	WK 0055	XLC1 00001
TES 0065	THWOK 0072	VIS1 00001	WPI 0055	XLCT 00001
TEST 00073	TINI 0079	VIST 00001	WPD 0055	XTHIK 0078
THAL 0001	TK 0057	WAF 0055	WPR 0055	Y 00103
THAL1 00001	TLO 0065	WCR 0055	WR 0079	YHD 0103
THALT 00001	TP 0055	WFP 0055	WTI 0055	Z 0103
THI 0065	TSUBC 0079	WGP 0055	X 0055	ZERO 00058