https://ntrs.nasa.gov/search.jsp?R=19690002041 2020-03-12T06:05:57+00:00Z

NASA CR 97807



# Solar Proton Forecast System and Procedures Used During the Mariner V Mission

Charles C. Gonzalez Edward L. Divita

JET PROPULSION LABORATORY CALIFORNIA INSTITUTE OF TECHNOLOGY PASADENA, CALIFORNIA

October 1, 1968

# Technical Report 32-1303

# Solar Proton Forecast System and Procedures Used During the Mariner V Mission

Charles C. Gonzalez Edward L. Divita

JET PROPULSION LABORATORY CALIFORNIA INSTITUTE OF TECHNOLOGY PASADENA, CALIFORNIA

October 1, 1968

### **TECHNICAL REPORT 32-1303**

Copyright © 1968 Jet Propulsion Laboratory California Institute of Technology

Prepared Under Contract No. NAS 7-100 National Aeronautics & Space Administration

# Preface

The work described in this report was performed by the Project Engineering Division of the Jet Propulsion Laboratory.

### Acknowledgment

The authors wish to thank Robert Doeker and the personnel in the Space Disturbance Forecast Center, Environmental Sciences Service Administration, Boulder, Colorado, for valuable suggestions and assistance in the development of the forecast procedures described herein and for providing preflare forecasts and preflare and flare-associated data. The authors also wish to thank Don Robbins and his associates in the Radiation and Fields Branch at the Manned Spacecraft Center, Houston, Texas, for valuable suggestions in the use of solar radio emission data as a real-time predictor of solar proton event time-integrated flux and for providing real-time access to radio emission data from the Solar Particle Alert Network Observatories. Thanks are also due Arthur Covington, Radio and Electrical Engineering Division of the National Research Council, Ottawa, Canada, for providing 2800-MHz solar radio burst profiles. Finally, this work was made possible by the Mariner 67 Project, through Dan Schneiderman and Conway Snyder.

## Contents

Ι.		1
11.	Requirements for Solar Forecast System and Procedures	2
	A. Engineering Requirements	2
	B. Scientific Requirements	3
Ш.	General Considerations	3
	A. Solar Activitiy	3
	B. Solar Proton Events	4
IV.	Predicting Solar Proton Events and Sizes Using Solar Radio Emission	5
	A. Theoretical Considerations	5
	B. Solar Data from the Last Solar Cycle	5
	C. Correlation of Radio Emission Parameters with Time-Integrated Proton Flux	8
	D. Selection of Parameters and Techniques to Predict Proton Events	20
	E. Limitations on Near-Earth Predictions Using Radio Emissions	20
V.	Forecast Procedures for Predicting Proton Events	22
	A. Data and Preflare Forecast Network	22
	B. Description of SDFC Facilities and Services	22
	C. Techniques and Criteria Used to Obtain Radio Burst Energy	<b>2</b> 5
	D. Checkout of Operational Network	26
	E. Recommended Procedures for Forecasting Solar Proton Events	27
	F. Solar Forecast System and Forecast Procedures Used During Mariner V Mission	29
VI.	Conclusions	29
VII.	Recommendations	30
Арр	endix A. Flare Classification	31
Арр	Dendix B. Calculation of Area of Radio Burst Profile	32
Glos	ssary	33
Refe	erences	34

# Contents (contd)

Tables

1.	Results of high-energy proton testing of Mariner V subsystems and components		•	•	3
2.	Occurrence of solar activity on the sun and detection at earth as a function of time		•		4
3.	Optical and radio parameters of solar activity used in correlation, false alarm, and miss frequency analyses of RF data and proton events .				6
4.	Estimates of the duration of 2800-MHz bursts associated with proton events of the last cycle and of delay time between bursts and proton events			•	8
5.	False alarm percentage and miss frequency for the prediction method using RF energy and the 95% confidence limits on time-integrated proton flux estimates	•			11
6.	False alarm percentage and miss frequency for the prediction method using RF energy and the 99% confidence limits on time-integrated proton flux estimates				11
7.	Cumulative false alarm percentage and miss frequency for the RF energy prediction method using the time-integrated proton flux estimates				12
8.	Cumulative false alarm percentage and miss frequency for the RF energy prediction method using the 95% confidence limits on time-integrated proton flux estimates	•	•		12
9.	False alarm percentage and miss frequency for the time-integrated prediction method using RF peak flux and the 95% confidence limits on time-integrated proton flux estimates	•	٠	٠	14
10.	Cumulative false alarm percentage and miss frequency for the prediction method using RF peak flux and the time-integrated proton flux estimates		•	•	14
11.	Cumulative false alarm percentage and miss frequency for the prediction method using the RF peak flux and the 95% confidence limits on time-integrated proton flux estimates	•	•	•	14
12.	Comparison of regression equations, correlation coefficients, and standard deviations derived in the linear least squares analysis of the solar activity parameters and proton event time-integrated flux	•	•	•	16
13.	Summary of a correlation analysis of some radio burst parameters with integrated proton flux		.•	.•	16
14.	Summary of statistical results of prediction of proton event fluxes on real-time basis using radio burst energy	•	.•	.•	22
15.	Summary of statistical results of prediction of proton event fluxes on real-time basis using peak radio flux	•		·	22
16.	Network of solar observatories supplying information to Space Disturbance Forecast Center				24

# Contents (contd)

### Tables (contd)

17.	Comparison of time-integrated proton fluxes using the RF	
	energy prediction method and RF energies computed using data points separated by different time intervals	25
18.	Sequence of events in the time span from a 28-day prediction to the occurrence of a solar proton event	27
		~'
A-1.	Flare class or importance	31

## Figures

1.	Model of the composite spectra of solar type IV radio emission in the range 10,000 to 25 MHz				5
2.	Model of a fixed-frequency (centimeter wavelength) outburst associated with a solar proton event				5
3.	Time history envelope and mean of the flux of proton events compared with three events of the last solar cycle		•	.•	8
4.	Time-integrated proton flux having energy greater than 30 MeV as a function of RF burst energy		•	•	9
5.	False alarm percentage for RF energy and time-integrated flux ( $E>30~{\rm MeV}$ ) prediction method		•	•	11
6.	Cumulative false alarm percentage for RF energy and time-integrated flux (E $>$ 30 MeV) prediction method	•		•	12
7.	Time-integrated proton flux for energies greater than 30 MeV as a function of RF burst peak flux			•	13
8.	Reconstruction, 2800-MHz radio burst profile of November 12, 1960 .		•		14
9.	False alarm percentage for RF peak flux and time-integrated flux(E > 30 MeV) prediction method		•		15
10.	Cumulative false alarm percentage for RF peak flux and time-integrated flux ( $E > 30$ MeV) prediction method				15
11.	Time-integrated proton flux having energy greater than 30 MeV as a function of plage area				17
12.	Time-integrated proton flux having energy greater than 30 MeV as a function of plage brightness				17
13.	Time-integrated proton flux having energy greater than 30 MeV as a function of flare importance			•	18
14.	Time-integrated proton flux having energy greater than 30 MeV as a function of sunspot area		•	•	18
15.	Time-integrated proton flux having energy greater than 30 MeV as a function of the product of burst duration and peak radio flux .	,		•	19

# Contents (contd)

## Figures (contd)

16.	Time-integrated proton flux having energy greater than 30 MeV as a function of the time difference between maximum of RF burst and flare maximum		•	•	19
17.	Time-integrated proton flux having energy greater than 30 MeV as a function of the time delay between start of PCA and start of RF burst .		•		20
18.	Peak proton flux ( $E > 30$ MeV) as a function of time-integrated proton flux ( $E > 30$ MeV)	•	•		21
19.	Solar flare warning system			•	23
20.	A typical 2800-MHz radio burst profile showing the areas to be evaluated			·	25
21.	Operational procedure for forecasting solar proton events used for Mariner V Venus encounter, October 19, 1967				28
B-1.	Partial areas under radio burst profile used in numerical integration technique to evaluate RF energy			•	32

### Abstract

A solar forecasting system and forecasting procedures for predicting the time of occurrence of solar proton events and the associated time-integrated proton flux on a real-time basis for the Mariner V mission are discussed. The solar forecasting system utilizes solar activity data obtained from solar observational networks and provided by the Space Disturbance Forecast Center (SDFC) at Boulder, Colorado. Since SDFC does not provide forecasts of proton events and their sizes on a realtime basis, statistical methods are developed, based on past solar cycle data, in order to use the solar activity data obtained on a real-time basis in predicting proton events and their sizes. The 2800-MHz radio burst energy is correlated with time-integrated proton flux. Several other solar parameters are correlated with time-integrated proton flux. However, none results in a better correlation. In addition, procedures for receiving data, making forecasts, and reporting the forecasts to the project on a real-time basis are described. Statistical uncertainties in the prediction method and uncertainties in the data are discussed, and their influence on the value of the predictions is evaluated. A brief history of the real-time forecasting of proton events using the method and procedures is presented. This history indicates that the forecast system and the forecast procedures have both scientific and engineering applications during the operational phase of a long-term interplanetary mission. Finally, recommendations are made to improve forecasting techniques and forecast procedures for reliable and timely warnings of pending solar proton events and their sizes.

## Solar Proton Forecast System and Procedures Used During the Mariner V Mission

#### I. Introduction

The Mariner V mission to Venus took place during the time period June-October 1967, when moderate to large proton events were expected, based on statistical analysis of past solar cycle data. Radiation tests of selected spacecraft subsystems demonstrated that exposure to proton fluxes as large as those expected during the Mariner V mission could significantly degrade the performance of critical spacecraft subsystems. Consequently, real-time forecasting of proton events and their sizes during the operational phase of the mission was desired so that the spacecraft operation team could, if necessary, implement options to use subsystems insensitive to proton radiation. In addition, if proton events were forecast during the mission, mission operations could be altered to allow collection of fields and particle data. Therefore, the Mariner V Project Office supported the development of a real-time forecast system.

Only short-term real-time predictions of solar flare proton events and their sizes are expected to provide an adequate forecast during an interplanetary mission because of the gross uncertainties associated with longterm predictions.

Methods of forecasting solar proton events and procedures for using the forecasts during the Mariner V mission on a real-time basis were developed utilizing data from the solar observational network made available through the Space Disturbance Forecast Center (SDFC) in Boulder, Colorado. SDFC also provides short-term prediction of solar activity, which can be used to establish periods of probable solar proton activity but does not currently predict proton event sizes. In addition, the Manned Spacecraft Center (MSC) is developing the Solar Particle Alert Network (SPAN) to predict the proton radiation to which astronauts may be exposed during the Apollo mission. SPAN is combined with solar observatories operated by SDFC and the Air Weather Service of the USAF to form the National Solar Flare Patrol. The methods and forecasting system presented here utilized the radio and solar observatories of the National Solar Flare Patrol as data sources for making real-time forecasts.

The forecast methods are based on statistical analyses of solar activity data and solar proton flux from the past solar cycle. In the statistical analyses several parameters of solar activity coincident with the occurrences of solar flares were correlated with the time-integrated proton flux which usually follows the large solar flares. The best correlations were obtained through single-parameter correlations of the 2800-MHz radio burst energy as the predictor of proton event time-integrated flux. However, the peak 2800-MHz radio flux will be used as a preliminary predictor to provide early alert since the peak radio flux may occur after as little as 20% of the radio burst is completed.

The forecast methods were incorporated into a forecast system and operational procedures were established for reporting forecasts to the *Mariner V* Project. The sun, however, was unexpectedly inactive during the course of the *Mariner V* mission.

In addition, statistical analyses were performed on past cycle data to estimate the average time available after a forecast for operational considerations and the reliability of the forecast methods. The results indicate that there is sufficient time after the occurrence of a solar flare and radio event to forecast an expected large proton event before the arrival of a significant amount of radiation near earth and within the trajectory of *Mariner V*. The results also demonstrate that forecasts of events at or above the threshold level established for Venus of  $2 \times 10^{10}$  protons/cm<sup>2</sup>, for energy > 30 MeV, have an estimated false alarm probability between 0–40%.

When the threshold radiation levels are exceeded, the forecasts have both scientific and engineering applications; when the thresholds are not exceeded, the predictions have only scientific applications. Forecast procedures are established to account for both of these applications. The procedures presented cover generally a time span from 28 days before a solar flare or radio event until after an observed proton event is completed or an expected proton event is considered a false alarm.

### II. Requirements for Solar Forecast System and Procedures

The requirements for a solar proton event forecasting system and procedures for using forecasts during the *Mariner V* mission are divided into two parts: engineering requirements and scientific requirements. Engineering requirements are related to possible radiation effects on spacecraft subsystems; scientific requirements are related to data which may be obtained when a solar proton event occurs.

### **A. Engineering Requirements**

The engineering requirements for a solar proton event forecasting system are that the predictions be reliable and that adequate warning time be provided prior to the occurrence of proton events larger than established radiation flux criteria.

The established proton radiation flux criterion for reporting forecasts to the Project based on predictions made near earth is that the time-integrated proton flux must be 10<sup>9</sup> protons/cm<sup>2</sup> or greater having energy greater than 30 MeV within the 95% confidence band. This criterion is based on the radiation test threshold levels listed in Table 1, which were established for radiation-sensitive Mariner IV subsystems and components (Ref. 1). The criterion was derived from the level of  $2 imes 10^{10}$  protons/ cm<sup>2</sup> having energy greater than 33 MeV, which is the level at which the more sensitive subsystems were tested and no significant degradation was observed. Because the predictions are made near earth and the worst condition for spacecraft exposure is at Venus encounter, it was necessary to reduce the level of  $2 \times 10^{10}$  protons/cm<sup>2</sup> at the spacecraft to a corresponding value of  $1 \times 10^{10}$ protons/cm<sup>2</sup> near earth to account for the assumed inverse square of the distance effect. Then this level was reduced to  $1 \times 10^9$  protons/cm<sup>2</sup> to account for the uncertainties in the measured proton fluxes taken during the last solar cycle and the uncertainties in making a prediction based on near-earth data and extrapolating the data to near Venus. Consequently, when the prediction made near earth is 10<sup>9</sup> protons/cm<sup>2</sup> having energy greater than 30 MeV, the actual flux near Venus may be as much as  $2 \times 10^{10}$  protons/cm<sup>2</sup> having energy greater than 30 MeV.

The peak flux requirement was obtained from a regression equation for peak flux as a function of time-integrated flux rather than from the radiation test threshold damage level of  $6.0 \times 10^5$  protons/cm<sup>2</sup>-s having energy above 40 MeV (See Table 1). The comparable peak flux derived from the regression equation corresponding to the threshold time-integrated flux of 10<sup>9</sup> protons/cm<sup>2</sup> is  $6.5 \times 10^3$ protons/cm<sup>2</sup>-s (E > 30 MeV). As a result, the peak flux requirement is conservatively established for the spacecraft subsystems as 10<sup>4</sup> protons/cm<sup>2</sup>-s having energies greater than 30 MeV because it is lower than the radiation test threshold level for peak flux. In addition, the predicted peak flux will be consistent with the predicted time-integrated flux from which it is obtained through the regression equation.

The amount of after-prediction time required to implement counter-measures before a significant flux is encountered was not established by the Project Office. However, limits on the time available based on the capabilities of the forecast method presented using data of the past solar cycle were taken from Section IV-C. The time limits are:

	Test l	evels	
Subsystem/ components	Flux rate, protons/cm <sup>2</sup> -s	Integrated flux, protons/cm <sup>2</sup>	Remarks
Data encoder	$8  imes 10^6$ to $1  imes 10^7$	4.3 × 10 <sup>10</sup>	No transient damage; no permanent damage
Squibs	$3.9  imes 10^7$	$2.1  imes 10^{10}$	No significant
	(E > 60 MeV)	(E > 60 MeV)	degrading effects
Batteries		$2 \times 10^{10}$	No apparent
		(E > 60 MeV)	effect on spacecraft batteries at about 10 <sup>10</sup> protons/cm <sup>2</sup>
Solar cells	$1 \times 10^7$	2.1 × 10 <sup>10</sup>	No transient
(Silicon P/N, 1Ω-cm)		(E > 36 MeV)	effects; loss of power, P/P₀ range 0.73–0.80
Command control and sequencing subassemblies	2.0 × 10 <sup>r</sup>	$8.55  imes 10^{10}$ to $1.02  imes 10^{11}$	No observable effects
Sun sensor	$3.5 \times 10^7$	$2 \times 10^{10}$	No observable effects
Canopus tracker	$6  imes 10^5$ (E > 40 MeV)	2 × 10 <sup>10</sup>	Failed at listed flux-rate (loss of roll control)
<sup>a</sup> E>33 MeV unless	otherwise indicated.	·····	•

Table 1. Results of high-energy proton testing of Mariner IV subsystems and components<sup>a</sup>

- (1) An average time delay of 0.7 h (using the lower 95% confidence limit on the average) between the time at which the RF emission ends and the start of the proton event, including the time for data transmission and making the prediction.
- (2) An average time delay of 3.1 h (using the lower 95% confidence limit on the average) between the time at which the RF emission ends and the maximum of the proton event, including the time for data transmission and making the prediction.

These limits are expected to be conservative for an engineering application because they include small radio events and small proton events, both of which are usually associated with shorter periods.

Prediction reliability requirements were not established by the Project Office. However, estimates of the reliability available based on the capabilities of the forecast method presented using data of the past solar cycle were taken from the false alarm study results presented in Section IV-D. The estimated probability that the proton event will occur when the predicted time-integrated proton flux is 10° protons/cm<sup>2</sup> (E > 30 MeV) and greater is between 60 and 100%. This probability range for proton fluxes greater than 10° protons/cm<sup>2</sup> was determined based on the estimates of probability from the data samples in the flux range between 10<sup>7</sup>-10<sup>10</sup> protons/cm<sup>2</sup>.

### **B. Scientific Requirements**

For scientific applications of the forecasting system it is required that predictions be reliable and timely forecasts of the occurrence and size of proton events. Events of any size are of scientific interest, but predictions must be reliable enough to establish a tracking priority since tracking is usually being shared with other spacecraft and satellites. Again, the reliability requirement and the time required after the prediction to implement spacecraft tracking were not established. Results were based on the capabilities of the method presented and indicate the reliability and the time available for arranging tracking time.

### **III. General Considerations**

### A. Solar Activity

The level of solar activity is generally measured by the sunspot number computed over a specified period of time (Ref. 2). The sunspot number is obtained from  $S_n = K(S + 10g)$ , where S is the total number of sunspots, g is the total number of groups determined from a single observation by a specified observatory, and K is a weighting factor dependent on the characteristics of the observatory and determined in such a way that a uniform set of sunspot numbers is derived from different observatories (Ref. 2). Solar activity as indicated by the sunspot number exhibits a quasiperiodic behavior with a mean frequency of about 11 yr and with known limits on the observed cycles ranging from 7 to about 16 yr. The activity indicated by the sunspot number is usually averaged over consecutive months or years. Although the occurrence of a particular sunspot group does not mean that solar activity will follow, observations indicate that as the number of sunspots on the solar disk increases, the general solar activity increases. The regions near sunspots are normally sources of various types of solar activity which may result in the emission of particles and electromagnetic radiation.

Sunspot data from the past 215 years have been analyzed statistically to predict the level of solar activity expected in the current cycle and the time of maximum activity (Refs. 3 and 4). These predictions, using the average yearly sunspot number, give only the expected solar activity averaged over a period of 1 yr. The sun must be observed regularly to predict the occurrence of solar flares and the emission of particles. Active regions, called plages and faculae, whose temperature and brightness are higher than the surrounding areas are present on the sun. Sunspots are almost always found in plages. High magnetic fields are frequently found in regions near sunspots. Temperature gradients between cooler sunspots and hotter surrounding areas cause regions of stress which lead to transient solar activity such as solar flares. Forecasts of solar flare activity can be made as much as a month prior to an event, but for increased accuracy are made between 3 days and several hours prior to the event and are based on plage size and brightness, sunspot area and class, sunspot magnetic configuration, radio emission, past history of the active region, and other solar disk and limb features. When a flare occurs, there is an increase in solar electromagnetic emission in the optical, ultraviolet, X-ray, and radio frequency range. Protons have been measured from the same region in which radio emissions occur. However, not all radio emissions are associated with proton events, and conversely. Typical solar activity occurrences are shown in Table 2 as a function of time.

### **B. Solar Proton Events**

The releases of energy which occur at the time of a solar flare occasionally include the emission of charged particles from the sun which reach the earth from 30 min to several hours later. These particles when defined as solar cosmic rays consist of protons having energies above 5–10 MeV and may extend to energies up to 20 BeV and more.

Predictions of average monthly and yearly proton fluxes using a predicted sunspot number and the past solar cycle proton flux have been made (Refs. 3 and 4). These prediction techniques were derived statistically, based on the correlation of past cycle proton data with sunspot number data. One study also involved the correlation of proton flux with average total sunspot area.<sup>1</sup> Predictions using these techniques may be made for periods of 6 months preceding the end of a solar cycle. Predictions of yearly proton fluxes are useful in planning a mission but do not give time of occurrence or size of an individual proton event; instead, they give an average expected proton flux for a specific time period in the future.

The data taken during the past solar cycle indicate that as the solar cycle approaches solar maximum and solar activity increases, flares and proton events become more numerous. Exceptionally large proton events of the

Time	Occurrence of events on the sun	Detection of events at earth
— 3-0 day	Growth of active regions	Optical observation of plages, sunspots, and magnetic complexity.
0	Beginning of solar flare	
0–10 min	Occurrence of solar flare with increased optical, X-ray, ultraviolet, and radio emissions (including 2800-MHz burst) followed by proton emission.	Direct detection of solar flare emissions and indirect detection by measurement of ionospheric effects. Commencement of arrival of 2800-MHz radio burst emission.
10 min–1 h		Recording of 2800-MHz radio burst emission
14 h		Arrival of protons
1–10 h		Characteristic rise of proton flux
10–20 h		Peak of moderate flux proton event (10 <sup>7</sup> —10 <sup>8</sup> protons/cm²)
20–40 h		Peak of high flux proton event (> 10 <sup>8</sup> protons/cm
100–150 h		Termination of proton even

### Table 2. Occurrence of solar activity on the sun and detection at earth as a function of time

last cycle occurred in a period of 2 to 3 years before and after the solar maximum. Solar maximum for the current solar cycle was predicted to occur during the 1968–69 time period; consequently, large proton events were expected during the *Mariner V* mission.

Based upon events of the past cycle, with few exceptions, the occurrence of a solar proton event can be associated with the occurrence of a flare. Moderate to large events ( $\ge 5 \times 10^7$  protons/cm<sup>2</sup> at E > 30 MeV) are usually preceded by a solar flare generally of class 2b or greater (see Appendix A for a discussion of flare classification). A prediction of occurrence of a flare of class 2b or greater along with other conditions such as a large, magnetically complex associated sunspot group indicates the possibility of the occurrence of a pending solar proton event. However, some of the electromagnetic radiation occurring at the time of a flare may be associated directly with proton emission. Furthermore, electromagnetic radiation will propagate through space much faster than solar particles and may reach the earth several hours before the arrival of solar particles (see Table 2). Thus it may be possible to use this radiation to predict the occurrence and size of a solar proton event. The energy radiated in

<sup>&</sup>lt;sup>1</sup>Private communication from S. Pierce, JPL.

the 2800-MHz solar radio burst coincident with the occurrence of the flare may be considered a predictor of proton events.

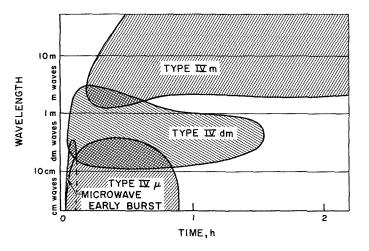
### IV. Predicting Solar Proton Events and Sizes Using Solar Radio Emission

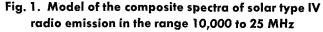
### **A. Theoretical Considerations**

Radio emission from the sun covers a broad range of frequencies and types of emission. Various types of emission are produced, e.g., thermal radiation, synchrotron radiation, and bremsstrahlung. However, the only type that has been consistently related to solar proton events is the type IV continuous broad-band emission caused by synchrotron radiation. This emission is divided into various component types as shown in Fig. 1 (from Ref. 5). The RF emission of interest is the centimeter wavelength radio burst in the region of 3 to 30 cm (microwave) with main emphasis on the 10.7-cm (2800-MHz) bursts. This emission as shown in Fig. 1 is included in the type IV  $\mu$  region. A sample burst is shown in Fig. 2 (from Ref. 6). A centimeter outburst, sometimes referred to as a microwave outburst has a peak intensity which usually is greater than 100 flux units.<sup>2</sup> These bursts usually last more than 10 min and up to approximately 1 h or more.

The outbursts at microwave frequencies are believed to be synchrotron emission caused by electrons (0.5 to 5 MeV) constrained temporarily by magnetic fields in the solar chromosphere and corona. It is generally assumed that the flare mechanism which accelerates electrons to

<sup>2</sup>One flux unit =  $10^{-22}$  W/m<sup>2</sup>-Hz (Ref. 7).





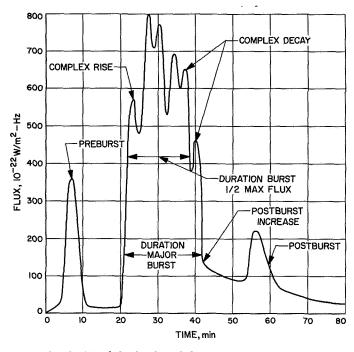


Fig. 2. Model of a fixed-frequency (centimeter wavelength) outburst associated with a solar proton event (from Ref. 6)

relativistic energies also accelerates protons and heavier nucleons to subrelativistic and relativistic energies. The high-energy nucleons escape directly from the solar plasma (Ref. 8). The lower energy nucleons are part of the plasma which eventually leaves the sun. The mean energy of accelerated electrons seems to be nearly independent of the intensities of the outburst. Therefore, the intensity of the outburst is not a measure of the energy of the accelerated electrons, but rather a measure of the number of accelerated electrons (Ref. 9). If we assume that an equal number of positive ions and electrons are accelerated and that the majority of positive ions accelerated are protons, then it follows that the total energy radiated should be directly related to the time-integrated proton flux. Therefore, the correlation of type IV solar radio emission with solar proton events may be simply a case of correlating phenomena which are physically related.

### **B.** Solar Data from the Last Solar Cycle

Radio burst data were compiled to obtain a source of selected radio burst parameters.<sup>3, 4</sup> A compilation is presented in Table 3 along with various other solar activity

<sup>&</sup>lt;sup>3</sup>Private communication from M. D. Lopez, Manned Spacecraft Center, Houston, Tex.

<sup>&</sup>lt;sup>4</sup>Private communication from A. Covington, Canadian National Research Council, Ottawa, Canada.

ivity used in correlation, false alarm, and	ses of RF data and proton events
ar acti	RF dat
solo	of
of	ses
o parameters of solar activi	uency analy
adio	req
ind radio	iss
άĎ	E
Optical	
Table 3.	

etc	Plage	Plage	Sunspot	Flare	Flare location		RF peck intensity.	RF burst energy.	Time-integrated flux for	RF burst, UT	irst, T	Burst duration.	Particle rise time.	Particle onset time.
	area	brightness	area	importance	Lat	Long	10 <sup>-22</sup> W/m <sup>2</sup> -Hz	10 <sup>-18</sup> J/m <sup>2</sup> -Hz	E > 30 MeV, protons/cm <sup>2</sup>	Start	Max	min	4	LT.
6/18/55	6,000	4.0	639	e	\$22	W21	1575	43		1907	1908			
7/9/55			No flare data available	ilable			309	30		1906	1922			
2/16/56	8000	4.0	1734-1437	2	N20	E08	650	09		1757	1813			
2/19/56	18,000	3.5	1734-1437	+1	N25	W23	650	29		1427	1435			
3/13/56	10,000	3.5	1237	2	N21	E50	850	14		1452	1454			-
3/15/56	°000¢	3.0	1089	2	N22	E21	1300	43		1622	1627			
6/20/56			No flare data available	ilable			340	12		1938	1939			
8/31/56			_		N16	E16	>340 off scale	>61	$2.5 \times 10^7$	1231				1430
9/17/56	17,500°	3.5	361	2+	S20	V17	320	13		1940	1947			
11/13/56	4000	3.5	814-465	2	<b>81N</b>	01V	180	13	1 × 10 <sup>8</sup>	1433 <sup>d</sup>	1440			2000
12/26/56	3000	3.5	1002	2	S17	11W	915	132		1403	1454			
1/6/57	5000	3.5	2089-1351	1	N16	W53	585	42		1758	1827			
4/12/57	5100	3.0	369-237	2	S25	W73	525	12		1855	1900			
4/14/57	0009	3.5	937-665	F	S23	W28	37	40	<u> </u>	1700	1915			
4/16/57	0006	3.0	1000-432	ņ	N30	E85	1650	87		1043	1050			
4/17/57	8006	3.0	1000-432	3+ 3+	N20	E69	6000	546		2006	2042			
6/3/57	4500	3.0	787	ę	S18	W18	290	17		1042	1051			
6/19/57	9006	3.5	166	2	N20	E45	2325	34	No estimate	1608	1610			
7/15/57			No associable flare	are			300	12		2019	2043			
7/16/57	1200	2.5	769-530	+	S33	W28	350	23		1741	1756			
7/20/57			No associable flare	lare			145	14		1735	1750			
7/24/57	5500	3.0	504	<u></u>	S24	W27	0011	94	$7.5 \times 10^6$	1759 <sup>d</sup>	1838			2015
8/1/57	6500	3.5	1092-845	ri-	S35	E04	25	22		1400	1815			-
8/9/57	6200	3.5	1092-845	-	S33	W77	40	27	$1.5 \times 10^{\circ}$	1304 <sup>d</sup>	1517			1600
8/28/57	8200	3.0	774	5+	S28	E30	760	10	No estimate	2017	2019			0000(8/29)
8/31/57	8000	3.5	1317	m	N25	W02	3900	350	$8.0 \times 10^7$	13004	1321	65.0		1500
9/2/57	0009	3.5	626	2+	S34	W36	120	30	$5.0 \times 10^7$	1300 <sup>d</sup>	1324			1700
9/3/57	15,000	3.5	597	n	N23	0E.M	1350	51		1417	1426			
9/18/57	6800°	4.5	1998	+ °	N20	E02	275	47		1821	1825	_		
9/21/57	5500	4.0	491	n	N10	90M	290	13	$1.5 \times 10^6$	13304	1337	14.5		1700
9/26/5/	19,500	3.0	232	ლ -	N22	EIS	110	25	4.0 × 10 <sup>-</sup>	1915"	1945	0.0		2100
10/07/01	007'+1		No hiret varordad	 >	070	No lonical			01 × 10°	No buret	iret .	2		0200
1/15/58	0006	3.5	786	<b>5</b> +	S13	W58	1350	21		1640	1643			
6/5/58	4000	3.0	314	2+	S18	E69	387	35	-	1614	1623			
6/28/58	12,000	3.0	245-114	ī	\$26	W20	23	32		1500	1745			
7/30/58	19,000°	3.0	106-56/1	2	S13	W64	400	15		1525	1529			
8/2/58	°000,91	3.0	106-56/1	Ļ	<b>S14</b>	06M	2050	26		1840	1842			
8/22/58	6400	3.5	1192	e	N18	W10	1500	192	7.0 × 10 <sup>7</sup>	1430 <sup>d</sup>	1506	120	10.0	1530
10/24/58	2000	3.5	439	2+	S05	W57	185	18	;	1439	11511			
12/11/58	8500	3.0	1318-710	2	S02	E00	1225	14		1805	1810			
12/12/58	10,000	3.5	1318	2+	SO3	W08	1500	20		1257	1301			
1/21/59	7500	3.5	1886-1476	e	N10	E48	¢00	12		1702	1708			

Image         Define         Define <thdefine< th="">         Define         <thdefine< th=""> <thdefine< th=""> <thdefine< th=""></thdefine<></thdefine<></thdefine<></thdefine<>	area <sup>a</sup> 2400 2400 2400 2400 2400 4000 13,000 11,000 11,000 12,000 1		importance <sup>3</sup> 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	<u> </u>				$F > 30 \text{ MeV}_{1}$ protons/cm <sup>2</sup> 9.6 × 10 <sup>8</sup> 9.1 × 10 <sup>8</sup> 9.1 × 10 <sup>8</sup> 4.0 × 10 <sup>8</sup>		Max 1535 1412 1412 1412 1415 1450 2257 2154 2154 2154 2128 2156 1906 1248 2128 2156 1906 1248 2108		20.0 12.0	UT 0030(5/11) 0000(7/17) 0300(1/12)
1         360         101         401         401         412         413           1400-465         2         N11         W00         225         120         1430         1431           2724-173         1         1         N10         817         120         1400         1412           2724-173         2         N10         817         120         1400         1420         1304           2724-173         2         N10         847         232         1300         1430         1430           1103-307         2         N10         847         232         1304         1304         1304           1103-307         2         N10         847         232         111         234         226           1103-307         2         N10         847         232         1204         1206         232           111-456         2         1         1<20         120         1204         1206         120           111-456         2         1         1         1<20         1206         1206         120         120           111-456         2         1         2         2         2         <	2400 6000 6000 8500 11,000 17,500 17,500 12,0000 12,0000 12,0000 12,0000000000	1400-945 1400-945 1064-866 2274-1732 513-264 806-5563 1152-947 152-947 152-947 152-947 1111-856 1152-947 1111-856 1111-856 1111-856 11412 1981-141			E20 W21 E87 W50 E83 E83 E83 E83 E83 E11 E11 E11 E11 E11 E03	60 325 516 526 526 2220 2220 220 520 520 520 520 520 520 5	50 52 53 53 53 53 53 53 53 53 53 53 53 53 54 54 55 55 56 56 57 57 56 57 57 56 57 57 57 57 57 57 57 57 57 57 57 57 57	9.6 × 10 <sup>6</sup> 9.1 × 10 <sup>6</sup> 4.0 × 10 <sup>6</sup>	1450 1410 1368 1340 1355 1356 2254 2010 2010 1645 1139 2010 2013 2112 2112 2112 2112 2112 2010 1645 11246 11246 11246 1246 1256 1266 1266 1266 1266 1266 1266 126	1535 1412 1317 1315 1345 1450 2257 2257 2154 1740 1740 1740 2128 2128 2128 2128 2128 2134 1906 1248 1910		20.0	(11/2)0000 (71/1) (21/1)0000 (21/1)0000
1400-465         2         NII         W00         325         50         1400         1412           227-172         1         140         131         131         131           227-172         1         140         131         132         132           237-364         2         140         131         132         132           115-467         2         140         131         132         132           115-461         2         130         131         130         132           115-461         2         140         141         126         126           115-461         2         140         141         126         126           115-461         2         140         141         126         126           115-461         2         140         141         126         126           111-461         2         146         143         126         200           111-461         2         126         126         201         201           111-461         2         2         2         2         2         201           1111-461         2         2	13,000° 13,000° 13,000° 11,000 11,000 9000 12,000 12,000 12,000 12,000 3500 3500 3500 3500 3500 3500 3500	1400-945 1064-866 2274-1732 513-264 806-5563 1152-947 152-947 152-947 1152-947 1152-947 111-856 1111-856 1111-856 1111-856 1111-856 1981-11412 1981-11412 1981-11412 1981-11412 1981-11412 1981-11412 1981-11412 1981-11412 1981-11412 1981-11412 1981-11412 1981-11412 1981-11412 1985-114120	· · · · · · · · · · · · · · · · · · ·		W 50 E87 E83 E84 E83 E83 E83 E83 E83 E90 E11 E11 E11 E03	325 160 51 51 51 225 900 900 1800 1225 520 520 520 520 520 520 220 220	80 10 12 13 13 13 14 14 15 15 14 15 15 15 15 15 15 15 15 15 15 15 15 15	9.6 × 10 <sup>6</sup> 9.1 × 10 <sup>6</sup> 7.0 <sup>6</sup>	1410 1308 1340 1355 2254 2100 <sup>4</sup> 2100 <sup>4</sup> 2112 2112 2112 2112 2112 2112 2112 21	1412 1315 1345 1345 2257 2154 2154 1740 1740 1740 2154 2128 2156 1906 1248 2128 2128 2128 2128 2128 2128 2128			0030(5/11) 0000(7/17) 0300(7/12)
104-465         2+1         N09         87         160         10         137         137           153-477         2+1         N01         893         232         23         234         227           113-46         2         N01         843         2120         29         1324         227           113-46         2         N01         841         96         130         2234         226           113-47         2         N11         867         2360         736         134         226           113-46         2         N10         641         900         736         134         200         201 <td>4000 8500 8500 11,000 17,500 12,000 12,000 12,000 12,000 12,000 12,000 3500 3500 3500 3500 3500 3500 3500</td> <td>1064-866 2274-1732 513-264 806-5563 1152-947 1552-947 1522-947 1152-947 1152-947 1152-947 1111-856 1111-856 1111-856 1111-856 11412 1981-11412</td> <td>++++++++++++++++++++++++++++++++++++++</td> <td></td> <td>E87 W50 E84 E83 E83 E83 E83 E11 E11 E11 E11 E03 E03</td> <td>160 525 51 51 520 900 1225 520 520 520 520 520 875 875 270</td> <td>0 28 28 28 29 29 29 29 29 29 29 29 29 29 29 20 20 20 20 20 20 20 20 20 20 20 20 20</td> <td>9.6 × 10<sup>6</sup> 9.1 × 10<sup>6</sup> 4.0 × 10<sup>6</sup></td> <td>1308 1340 1350 2254 2100<sup>4</sup> 2010 1645 1135 2013 2112 2112 2118<sup>4</sup> 1858 1858 1858 1858</td> <td>1317 1345 1450 2257 2154 2154 1740 1740 1740 2128 2128 2128 2128 1906 1248 1910</td> <td></td> <td>20.0</td> <td>(11/2)0000 (71/7)0000 (71/1)0000</td>	4000 8500 8500 11,000 17,500 12,000 12,000 12,000 12,000 12,000 12,000 3500 3500 3500 3500 3500 3500 3500	1064-866 2274-1732 513-264 806-5563 1152-947 1552-947 1522-947 1152-947 1152-947 1152-947 1111-856 1111-856 1111-856 1111-856 11412 1981-11412	++++++++++++++++++++++++++++++++++++++		E87 W50 E84 E83 E83 E83 E83 E11 E11 E11 E11 E03 E03	160 525 51 51 520 900 1225 520 520 520 520 520 875 875 270	0 28 28 28 29 29 29 29 29 29 29 29 29 29 29 20 20 20 20 20 20 20 20 20 20 20 20 20	9.6 × 10 <sup>6</sup> 9.1 × 10 <sup>6</sup> 4.0 × 10 <sup>6</sup>	1308 1340 1350 2254 2100 <sup>4</sup> 2010 1645 1135 2013 2112 2112 2118 <sup>4</sup> 1858 1858 1858 1858	1317 1345 1450 2257 2154 2154 1740 1740 1740 2128 2128 2128 2128 1906 1248 1910		20.0	(11/2)0000 (71/7)0000 (71/1)0000
272-472         1+         N9         W6         23         12         1346         1446           913-364         2         N10         E4         2         N10         E4         22           913-364         3         N10         E4         2200         234         235           913-364         3         N10         E4         2200         811         9.6 × 10 <sup>2</sup> 2184         230           913-364         3         N10         E4         2200         731         1132         2183         2184         200           966-583         3         N10         E4         2200         732         9.1 × 10 <sup>2</sup> 2184         200           910-4121         2         N18         E4         200         732         9.1 × 10 <sup>2</sup> 2184         200           910-4112         2         N18         14 <td>8500 4000 11,000 19,000 17,500 12,000 12,000 12,000 12,000 12,000 12,000 13,000 3500 3500 3500 3500 3500 3500 3500</td> <td>2274-1732 513-264 806-5563 1152-947 1552-947 152-947 1152-947 1111-856 1111-856 1111-856 1111-856 1111-856 1111-856 1981-1412</td> <td>+ + + + + + + + + + + + + + + + + + +</td> <td></td> <td>W50 E84 E83 E47 E47 E47 E41 E48 E63 E11 E11 E03</td> <td>525 51 2220 2250 2550 520 520 5500 575 875 875 270</td> <td>22 28]1 28]1 28]2 29 29 29 20 29 20 20 20 20 20 20 20 20 20 20 20 20 20</td> <td>9.6 × 10<sup>6</sup> 9.1 × 10<sup>6</sup> 4.0 × 10<sup>6</sup></td> <td>1340 1350 2254 2100<sup>4</sup> 2010 1645 1135 2013 2112 2118<sup>4</sup> 1858 1858 1858 1858</td> <td>1345 1450 1450 2257 2154 1740 1740 1740 2128 2128 2128 2128 2128 1906 1248 1910</td> <td></td> <td>12.0</td> <td>(11/2)0000 (71/7)0000 (21/1)0000</td>	8500 4000 11,000 19,000 17,500 12,000 12,000 12,000 12,000 12,000 12,000 13,000 3500 3500 3500 3500 3500 3500 3500	2274-1732 513-264 806-5563 1152-947 1552-947 152-947 1152-947 1111-856 1111-856 1111-856 1111-856 1111-856 1111-856 1981-1412	+ + + + + + + + + + + + + + + + + + +		W50 E84 E83 E47 E47 E47 E41 E48 E63 E11 E11 E03	525 51 2220 2250 2550 520 520 5500 575 875 875 270	22 28]1 28]1 28]2 29 29 29 20 29 20 20 20 20 20 20 20 20 20 20 20 20 20	9.6 × 10 <sup>6</sup> 9.1 × 10 <sup>6</sup> 4.0 × 10 <sup>6</sup>	1340 1350 2254 2100 <sup>4</sup> 2010 1645 1135 2013 2112 2118 <sup>4</sup> 1858 1858 1858 1858	1345 1450 1450 2257 2154 1740 1740 1740 2128 2128 2128 2128 2128 1906 1248 1910		12.0	(11/2)0000 (71/7)0000 (21/1)0000
913-264         2         N0         E44         51         26         1330         1430         1430         1430           1135-97         3+         N0         E43         2210         29         1234         2037         130         1430         1430           1135-97         3+         N0         E41         200         75         2010         2134         2037           1135-97         3+         N0         E41         2030         114         1145         2001         2031           1135-97         3+         N16         F67         2030         114         1145         2001         2031           1111-655         2+         N18         F67         2030         114         1145         2033         2046         2030         2046         2030         2046         2030         2046         2030         2030         2034         1120         2030         2030         2031         2046         2030         2030         2030         2031         2046         2030         2030         2030         2030         2030         2030         2030         2030         2030         2030         2030         2030         2046	4000 11,000 17,500 17,500 17,500 12,000 12,000 12,000 12,000 12,000 12,000 12,000 12,000 13,000 14,000 12,000 13,000	513-264 513-264 806-5563 1152-947 1522-947 1111-856 1111-856 1111-856 1111-856 1111-856 1111-856 1111-856 1981-1412 1981-1412 1981-1412 1981-1412 1981-1412 1981-1412 1981-1412 1981-148 575 1150 1150	ла на		E84 E83 E47 E47 E41 E47 E61 E11 E11 E03 E03	51 2220 2550 900 900 520 5500 5500 5500 875 875 270 220	26 811 75 15 73 23 23 23 26 17 17 17	9.6 × 10 <sup>6</sup> 9.1 × 10 <sup>6</sup> 4.0 × 10 <sup>6</sup>	1350 2254 2100 <sup>4</sup> 2010 1645 1139 2043 2043 2043 2112 2118 <sup>4</sup> 1858 1858 1858 1246 1246 2056 <sup>4</sup>	1450 2257 2154 2154 2021 1740 1740 2046 2128 2154 1906 1248 1910		20.0	(11/2)0000 (7/1/1)0000 (21/1)0000
100-5561         2+         V(2)         800         224         224         224         229         221           1552-547         3+         N(10         641         900         73         96         2104         2134         200         201 <td< td=""><td>11,000 17,500 17,500 17,500 12,000 12,000 12,000 12,000 12,000 13,000 3500 3500 3500 3500 3500 3500 3500</td><td>806-5563 1152-947 1522-947 806-563 1152-947 1111-856 1111-856 1111-856 1111-856 111-856 1981-1412 1981-1412 1981-1412 1981-1412 1948 2622-1948 575 1150 1650</td><td>6 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7</td><td></td><td>E83 E47 E41 E41 E41 E48 E48 E48 E48 E11 E11 E03</td><td>2220 2550 900 1225 520 5500 5500 875 875 270 220</td><td>29 811 14 15 10 10 13 13 11 11</td><td>9.6 × 10° 9.1 × 10° 4.0 × 10°</td><td>2254 2100<sup>t</sup> 2010 1645 1/39 2043 2043 2112 2118<sup>d</sup> 1858 1858 1858 1858 1858</td><td>2257 2154 2021 1740 1740 2046 2046 2128 2154 1906 1248 1910</td><td></td><td>20.0 12.0</td><td>0030(5/11) (7/1/7) 0000(7/12) (7/1/2) 0300(1/12)</td></td<>	11,000 17,500 17,500 17,500 12,000 12,000 12,000 12,000 12,000 13,000 3500 3500 3500 3500 3500 3500 3500	806-5563 1152-947 1522-947 806-563 1152-947 1111-856 1111-856 1111-856 1111-856 111-856 1981-1412 1981-1412 1981-1412 1981-1412 1948 2622-1948 575 1150 1650	6 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7		E83 E47 E41 E41 E41 E48 E48 E48 E48 E11 E11 E03	2220 2550 900 1225 520 5500 5500 875 875 270 220	29 811 14 15 10 10 13 13 11 11	9.6 × 10° 9.1 × 10° 4.0 × 10°	2254 2100 <sup>t</sup> 2010 1645 1/39 2043 2043 2112 2118 <sup>d</sup> 1858 1858 1858 1858 1858	2257 2154 2021 1740 1740 2046 2046 2128 2154 1906 1248 1910		20.0 12.0	0030(5/11) (7/1/7) 0000(7/12) (7/1/2) 0300(1/12)
1532-947         3++         N18         Exf         2350         811         9.6 X 10 <sup>4</sup> 2104         2134         200         201           1132-947         3         N10         E41         900         75         1146         7139         1740         201         201           1111-456         2         N17         E60         1800         146         1739         203         2043         2046         2011	19,000 17,500 9000 9000 12,000 12,000 12,000 9000 9000 9000 9000 9000 9000 9000	1552-947 806-563 1152-947 1111-856 1111-856 1111-856 1111-856 1981-1412 1981-1412 1981-1412 1981-1412 1981-1412 1948 2632-1948 2632-1948 2632-1948 1650 1650	5 3 5 5 - 3 5 5 3 3 <del>3</del> + + + + + + + + + + + + + + + + + + +		E47 E41 E90 E90 E11 E11 E11 E03	2550 900 1800 1225 520 520 5500 875 40 270 220	811 75 732 732 732 732 71 11 712	9.6 × 10 <sup>6</sup> 9.1 × 10 <sup>8</sup> 4.0 × 10 <sup>8</sup>	2100 <sup>4</sup> 2010 1645 1139 2043 2112 2112 2118 1858 1858 1858 1858 1858	2154 2021 1740 1740 2046 2128 2154 1906 1248 1906 1910		20.0	(11/30000 (71/1/0000 (21/1)0000
800-653         3         N(1)         E41         900         75         2010         2031           1111-555         2         N/15         W/17         E90         1800         144         1739         1740           1111-555         2         N/16         W/12         1225         1 <td>17,500 9000 12,000 12,000 12,000 12,000 9000 9000 9000 9000 9000 3500 3500 3</td> <td>806-563 1152-947 1111-856 1111-856 1981-1412 1981-1412 1981-1412 1948 2622-1948 575 1150 1650 1650</td> <td>~ + ++++ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~</td> <td></td> <td>E41 E90 E12 E67 E11 E11 E11 E03</td> <td>900 1800 520 520 570 875 875 270 220</td> <td>75 25 25 25 25 25 25 25 25 25 25 25 25 25</td> <td>9.1 × 10<sup>8</sup></td> <td>2010 1645 1739 2043 2112 2118<sup>d</sup> 1858 1815 1815 2056<sup>d</sup></td> <td>2021 1740 1746 2046 2128 2154 1906 1248 1910</td> <td></td> <td>12.0</td> <td>(71/7)0000 (21/1)0000</td>	17,500 9000 12,000 12,000 12,000 12,000 9000 9000 9000 9000 9000 3500 3500 3	806-563 1152-947 1111-856 1111-856 1981-1412 1981-1412 1981-1412 1948 2622-1948 575 1150 1650 1650	~ + ++++ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~		E41 E90 E12 E67 E11 E11 E11 E03	900 1800 520 520 570 875 875 270 220	75 25 25 25 25 25 25 25 25 25 25 25 25 25	9.1 × 10 <sup>8</sup>	2010 1645 1739 2043 2112 2118 <sup>d</sup> 1858 1815 1815 2056 <sup>d</sup>	2021 1740 1746 2046 2128 2154 1906 1248 1910		12.0	(71/7)0000 (21/1)0000
IIII-455         2         NI/T         E60         1800         146         1445         1740           1011-455         2         N16         W12         1225         1	9000 9000 12,000 12,000 12,000 7500 7500 13,000 3500 3500 3500 3500 3500 3500 3500	1111-856 1111-856 1111-856 1981-1412 1981-1412 1981-1412 1981-1412 2622-1948 575 1150 1650	5 3 5 5 - 3 5 5 <del>3</del> 5		E90 W12 E67 W15 W15 W16 E03	1800 1225 520 5500 875 40 220	146 146 15 15 15 15 15 15 17 17	9.1 × 10 <sup>8</sup> 4.0 × 10 <sup>8</sup>	1645 1739 2043 2112 2112 2118 <sup>d</sup> 1858 1858 1815 2056 <sup>d</sup>	1740 1140 2046 2154 1906 1248 1910 2108		12.0	0000(7/17) (7/1/10000 (2/1/10000
IIII-65         3+         NI         W12         1225         14         1139         1140           1981-412         2         N18         667         320         350         323         2046           1981-412         2         N18         667         320         320         323         2046           1981-412         2         N16         W31         5500         722         9,1 × 10'         1138         1006           1011-536         1 +         N10         E11         270         10         1336         1246         1226           2023-1948         2 +         N00         W16         40         10         1336         1307         1326         1208         1208           2023-1948         2 +         N00         W16         40         10         40         1357         1208	9000 12,000 12,000 12,000 9 7500 9 7500 9 3500 3500 3500 3500 3500 3500 3500	1111–856 1981–1412 1981–1412 1981–1412 1011–536 2632–1948 2632–1948 375 1150 1650	5 3 5 5 - 3 5 5 <del>3</del>		W12 E67 E18 W31 E11 W16 W44 E03	1225 520 520 5200 5500 875 40 220	732 732 11 13 13	9.1 × 10 <sup>8</sup> 4.0 × 10 <sup>8</sup>	1139 2043 2112 2118 <sup>d</sup> 1858 1858 1815 1815	1140 2046 2128 2154 1906 1910 1910 2108		12.0	0000(7/1/) (7/1/) (2/1/) (2/1/) (2/1/) (2/1/)
1981-1412         2         N18         E67         320         15         2043         2046         126           1981-1412         2         N19         E67         320         732         9,1<	12,000 12,000 7500 9000 9000 5000 3500 3500 3500 3500 3	1981-1412 1981-1412 1981-1412 1011-536 2632-1948 2632-1948 575 1150 1650	6 9 5 5 - 3 5 5	·	E67 E48 W31 W16 W44 E03 E03	520 520 5500 875 40 220	15 30 10 11 13 13	9.1 × 10 <sup>8</sup> 4.0 × 10 <sup>8</sup>	2043 2112 2118 <sup>d</sup> 1858 1858 1815 2056 <sup>d</sup>	2046 2128 2154 1906 1248 1910 2108		12.0	0000(7/17) 0300(1/12) 0300(1/12)
1981-1412         2         N19         Eds         520         30         2112         2128         2134         120           1981-1412         3+         N10         W11         5300         732         9,1<×10	12,000 7500 9000 3500 3500 3500 3500 3500 3500 3	1981–1412 1981–1412 1011–536 2622–1948 2622–1948 375 1150 1650 1650	5 3 5 5 <del>-</del> - + + + + + + + + + + + + + + + + + +		E48 W31 W16 W44 E03	520 5500 270 875 40 220	30 732 11 15 13 13	9.1 × 10 <sup>8</sup> 4.0 × 10 <sup>6</sup>	2112 2118 <sup>d</sup> 1858 1246 1815 2056 <sup>d</sup>	2128 2154 1906 1248 1910 2108		12.0	(21/1)0000 (21/1)0000
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	12,000 7500 9000 3500 3500 3500 3500 3500 3500 3	1981–1412 1011–536 2622–1948 275 1150 1650 1650	6 7 7 7 <del>7</del> 7 + + + +		W31 E11 W16 W44 E03	5500 270 875 40 220	732 10 13 13 13	9.1 × 10 <sup>8</sup> 4.0 × 10 <sup>4</sup>	2118 <sup>d</sup> 1858 1246 1246 1815 2056 <sup>d</sup>	2154 1906 1248 1910 2108		12.0	(21/1)0000 (21/1)0000 0300(1/12)
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	7500 9000 5000 3500 3500 3500 3500 3500 3	1011–536 2622–1948 2622–1948 575 1150 1650 1650	5 3 5 <del>5</del> + + +		E11 W16 W44 E03 W40	270 875 40 220	00 11 20 20 20 20 20 20 20 20 20 20 20 20 20	4.0 × 10 <sup>5</sup>	1858 1246 1815 2056 <sup>d</sup>	1906 1248 1910 2108			0300(1/12) 0300(1/16)
2622-1948         24         NO7         W (6)         87.3         11         124.6         124.8         124.6         124.8         124.6         124.8         124.6         124.8         124.6         124.8         124.6         124.6         124.6         124.8         124.6         124.6         124.6         124.6         124.6         124.6         124.8         124.7         124.6         124.8         124.7         124.6         124.8         124.7         124.6         124.8         124.7         124.6         124.8         124.7         124.	9000 13,000 5000 3500 3500 3500 3500 3500 3500	2622-1948 2622-1948 575 1150 1650	6 3 5 5 7 4 4		W16 W44 E03 W40	875 40 220	117 13 13	4.0 × 10 <sup>6</sup>	1246 1815 2056 <sup>d</sup>	1248 1910 2108			0300(1/12) 0300(1/16)
2622-1948         2+         N06         W44         4.0         16         1815         1910         6           375         3         N22         E03         7200         113         No estimate         2036 <sup>4</sup> 2108         6           1650         2         N12         E11         1750         127         No estimate         2048         2135         6           1650         2         N13         W90         60         107         1046         1357         108         2           1650         3         N13         W90         60         60         107         1434         90         2.33           830         857         065         60         107         1406         1035         1046         2.33           1100         2         N22         R03         136         1309         90         3.0           11100         2         N22         R05         140         17         No estimate         1148         1006         2.33           11100         2         3         N22         E60         125         1040         1236         1346         40         100	13,000 3500 5000 3500 3500 3500 3500 3500	2622–1948 575 1150 1650 1650	ю о р		W44 E03 W20	40	81 117	4.0 × 10 <sup>t</sup>	1815 2056 <sup>d</sup>	1910 2108			0300(1/12)
575         3         N22         EG3         720         113         4.0 × 10 <sup>4</sup> 2056 <sup>4</sup> 2108         1357         6           1130         2         S20         W68         700         117         No estimate         1340         1357         6           1630         2         N11         E17         1750         160         6.0 × 10 <sup>4</sup> 1434         90         30           No associable flare         3         N13         W90         600         6.0 × 10 <sup>4</sup> 1434         90         30           S00         3+         N27         160         6.0 × 10 <sup>4</sup> 1444         90         30            3         N27         E60         4.0 × 10 <sup>4</sup> 1446         1705         1228           11100         2+         N22         K22         1000         185         5.0 × 10 <sup>4</sup> 1743         90         30           925         1+         N22         K27         1000         185         1743         123         40         100           1100         2         6.0         106         5.0 × 10 <sup>4</sup> 1745         123         23         23         23	3500 5000 3500 3500 3500 3500 3500 3500	575 1150 1650	6 6		E03	220	117	$4.0 \times 10^{5}$	2056 <sup>d</sup>	2108			0300(1/12) 0300(1/16)
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	5000 3000 3500 3500 3900 3900 3900	1150 1650 1650	2		W KO		211				-	Ŷ	0300(1/10)
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	3000 3500 3900 3900 3900	1650	-			200		No estimate	1340	1357		,	
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	3500 3900 2500	1650	6		E37	1150	127		2048	2118			
No associable flare         73         18         1745         2122         223           850         3         N13         W90         600         69         6.0 × 10"         1/145         1203         1046         2-3           7<500	4500 3900 2500	-	7		E11	1750	160	$6.0 \times 10^{6}$	1518 <sup>d</sup>	1556			0300(3/31)
850         3         N13         W90         600         69         6.0 × 10 <sup>6</sup> 2-3 $< 500$ $3+$ 509         E07         693         69 $4.0 \times 10^6$ $1143$ 1209         30         30 $3$ N21         E06 $4.23$ $4.6$ No estimate $1143$ 1209         30         30 $1100$ $2++$ N22         E26 $1100$ $26$ $6.0 \times 10^6$ $1173$ 90         30 $1725$ $1+$ N22         E67 $2000$ $185$ $2.4 \times 10^6$ $1792$ $1792$ $1792$ $1206$ $10.0$ $1725$ $1+$ N22         E67 $2000$ $185$ $2.022$ $1346$ $40$ $100$ $1775$ $3+$ N27         W04 $500$ $026$ $2.1 \times 10^6$ $1326$ $1222$ $1206$ $1346$ $40$ $1000$ $1775$ $3+$ N27         W04 $500$ $2.4 \times 10^6$	4500 3900 2500	No associable flar				75	18		1745	2122			
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	3900	850	m		06M	600	69	$6.0 \times 10^{6}$	<1025	1046		ĩ	1030
3         NR1         E06         423         46         No estimate         1148         1209           1100         2+         N22         W27         140         17         No estimate         2138         1928           925         1         522         E67         2000         185         1702         1756           925         1         522         E67         2000         185         1702         1756           1225         1+         N22         W27         140         17         2056         2122           3         N13         E07         56         20         22         2056         1346         40           1775         3+         N27         W04         5500         206         2.4 × 10°         1320°         1346         40           1775         3+         N26         V30         400         1320°         1346         40         10.0           3         K07         E74         330         23         No estimute         128         1838           1400         3         S07         E24         330         206         4.0 × 10°         1745         8-10	2500	<200	3+		E07	695	69	$4.0 \times 10^{6}$	1406 <sup>d</sup>	1434	8	3.0	1800
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	0026		ю ,		E06	425	46	No estimate	1148	1209			00/1
1100         2 +         Nu22         E26         1100         26         6.0 × 10°         1923         1928           925         1         522         E67         2000         185         205.6         2122         205.6         2122           1775         3         N13         E07         56         200         185         1.022         1.756         132.0 <sup>4</sup> 1437           1775         3 +         Nu27         W04         5500         606         2.4 × 10°         1320 <sup>4</sup> 140         10.0           3         N13         E07         550         606         2.4 × 10°         1320 <sup>4</sup> 140         10.0           3 +         Nu26         E74         330         2.3         No estimate         1828         1837         40         10.0           1400         3         507         E32         1500         138         3.0 × 10°         151.3         1610         13.0 × 10°         11.3         40         10.0           1400         3         507         E32         1200         88         4.0 × 10°         11.3         11.3         11.3         8-10°         8-10°         11.3         11.3	nncz	, ,	m		W27	140	21	No estimate	2140	2158	-		~2300
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	13,000	1100	5 -		E26	0011	26	6.0 × 10°	1923	1928		-	0000~
11/75         3         N13         EO/         56         20 $1220^4$ 1837         40         10.0           1775         3+         N27         W04         5500         606 $2.4 \times 10^6$ 1320 <sup>4</sup> 13246         40         10.0           acidated with proton event uncertain         N25         W90         400         23         No estimate         1320 <sup>4</sup> 1346         40         10.0           3+         N26         E74         330         23         No estimate         1828         1838         80         10.0           3+         N26         E74         330         23         No estimate         1828         10.0         10.0           1400         3         S07         E33         1200         138         3.0 × 10°         1376 <sup>4</sup> 1745         8-10           1400         3         S07         E23         1200         88         4.0 × 10°         1356 <sup>4</sup> 160         1.13           1400         3         S07         E23         1200         88         4.0 × 10°         16102         1113           1400         3         S07         W08         W00	3500	925			EO/	330	29 59		1/12	00/1			
1775         3+         N27         Wod         5500         606         2.4 × 10°         1320°         1346         40         10.0           aciated with proton event uncertain         N25         W90         400         255         4.5 × 10°         1320°         1346         40         10.0           3+         N25         EY4         330         23         No estimate         1828         1838         80         10.0           1400         3         S07         E32         1500         138         3.0 × 10°         1604°         1745         8-10           1400         3         S07         E32         1200         88         4.0 × 10°         1313         8-10         8-12           1400         3         S07         W20         111         36         1.3 × 10°         1510°         1610         8-12           1400         3         S06         W90         900         94         5.0 × 10°         1952°         1651         42         46           1400         3         S06         W90         900         94         5.0 × 10°         1952°         1651         42         46           1350         1	5800	6771	- m		E07	270 26	7 8		1628	1837			
ocicited with proton event uncertain         N25         W90         400         25 $4.5 \times 10^7$ 2023         2027 $3+$ N26         E74         330         23         No estimate         1838         1838         8-10 $1400$ 3         S07         E23         1500         138         3.0 $\times 10^6$ 1745         8-10 $1400$ 3         S07         E23         1200         88 $4.0 \times 10^7$ <1102	8000	1775	+ 8	,	W04	5500	606	$2.4 \times 10^{6}$	1320 <sup>d</sup>	1346	40	10.0	1400
3+         N26         E74         330         23         No estimate         1828         1838         1838         1838         1745         8-10           1400         3         507         E32         1500         138         3.0 × 10°         1745         8-10           1400         3         507         E32         1200         88         4.0 × 10°         1745         8-10           1400         3         507         W20         111         36         1.3 × 10°         1810 <sup>4</sup> 1610         8-12           1400         3         506         W90         1800         94         5.0 × 10°         1552 <sup>4</sup> 1621         42         4-6           1350         1         N08         W30         900         95         4.0 × 10°         1930 <sup>4</sup> 2001         10.0           1350         1         N08         W30         900         95         4.0 × 10°         1939 <sup>4</sup> 2001         10.0           1350         1         N08         W30         900         95         6.0 × 10°         1939 <sup>4</sup> 2001         10.0           1         1         N08         800         36		ssociated with proton	svent uncertain		06M	400	25	$4.5 \times 10^7$	2023	2027			
1400         3         S07         E32         1500         138         3.0 × 10 <sup>6</sup> 164 <sup>4</sup> 1745         8-10           1400         3         507         E23         1200         88         4,0 × 10 <sup>7</sup> 71102         1113         8-10           1400         2         507         W20         111         36         1.3 × 10 <sup>7</sup> 1510 <sup>4</sup> 1610         8-12           1400         3         507         W20         111         36         1.3 × 10 <sup>7</sup> 1510 <sup>4</sup> 1610         8-12           1400         3         506         W90         1800         94         5.0 × 10 <sup>6</sup> 1522 <sup>4</sup> 1621         42         4-6           1350         1         N08         W80         900         95         4.0 × 10 <sup>7</sup> 1930 <sup>4</sup> 2001         10.0           1350         1         N13         E29         800         36         6.0 × 10 <sup>6</sup> 2211 <sup>4</sup> 2218         1.1.5           1+         N19         W90         8         8         8 × 10 <sup>6</sup> 2211 <sup>4</sup> 201         1.1.5	7500		3+		E74	330	23	No estimate	1828	1838			~0500(12/6)
1400         3         S07         E23         1200         88         4.0 × 10'          1113         8-12           1400         2         507         W20         111         36         1.3 × 10'         1510 <sup>4</sup> 1610         8-12           1400         3         506         W90         1800         94         5.0 × 10'         1510 <sup>4</sup> 1610         42         4-6           1350         1         N08         W80         900         95         4.0 × 10'         1930 <sup>4</sup> 2001         10.0           5500         3         N13         E29         800         36         6.0 × 10''         1930 <sup>4</sup> 2001         10.0           1+         N19         W90         900         36         6.0 × 10''         2211 <sup>4</sup> 2218         1.5	4000	1400	e		E32	1500	138	$3.0 \times 10^{6}$	1604 <sup>d</sup>	1745		8-10	0000(7/12)
1400         2         S07         W20         111         36         1.3 × 10 <sup>4</sup> 1610         42         4-6           1400         3         506         W90         1800         94         5.0 × 10 <sup>6</sup> 152d <sup>4</sup> 1621         42         4-6           1350         1         N08         W80         900         95         4.0 × 10 <sup>7</sup> 1930 <sup>4</sup> 2001         10.0           1350         1         N13         E29         800         36         6.0 × 10 <sup>6</sup> 2211 <sup>4</sup> 2218         1.5.5           1+         N19         W90         900         36         6.0 × 10 <sup>6</sup> 2211 <sup>4</sup> 2218         1.5.5	5700°	1400	e	·	E23	1200	88	$4.0 \times 10^7$	<1102	1113		8-12	1300
$ \begin{array}{c cccc} 1400 & 3 & 506 & \text{W90} & 1800 & 94 & 5.0 \times 10^6 & 1552^4 & 1621 & 42 & 4-6 \\ 1350 & 1 & N08 & W80 & 900 & 95 & 4.0 \times 10^7 & 1930^4 & 2001 & 10.0 \\ \hline <500 & 3 & N13 & E29 & 800 & 36 & 6.0 \times 10^8 & 2211^4 & 2218 & 1.5 \\ 1+ & N19 & W90 & 800 & 36 & 8 \times 10^6 & 2211^4 & 2218 & 1.5 \\ \hline & & & & & & & & & & & & & & & & \\ \hline & & & &$	5700°	1400	2		W20	, u	36	$1.3 \times 10^7$	1510 <sup>d</sup>	1610			1545
1350         1         N08         W80         900         95         4.0 × 10 <sup>3</sup> 1390 <sup>4</sup> 2001         10.0           <500	5600	1400	e	<u> </u>	06M	1800	94	$5.0  imes 10^{\circ}$	1552 <sup>d</sup>	1621	42	\$	0300(7/21)
<500         3         N13         E29         800         36         6.0 × 10 <sup>4</sup> 2218         1.5           1+         N19         W90         8         8         × 10 <sup>6</sup> 2211 <sup>d</sup> 2218         1.5             8         8         × 10 <sup>6</sup> 2         2         1.5	9009	1350	-		W80	006	95	$4.0 \times 10^{7}$	1930 <sup>d</sup>	2001	<u>.</u>	10.0	2100
1+ N19	3600	<200	ę		E29	800	36	$6.0 \times 10^{6}$	2211 <sup>d</sup>	2218		1.5	2330
	2200		1+	·	06M		8	$8 \times 10^{6}$					
	"Plage and sunspot area, solar disk $ imes$ 10–				<sup>c</sup> Complex gro	uping of plage re	gions; area given is	for plage region ass	ciated with e	event.	l		

parameters and proton event data (Refs. 6, 10, and 11). The time-integrated proton flux for the 9/26/57 event was estimated from statistical analyses connecting the timeintegrated proton flux above 30 MeV with that above 100 MeV. Some of the RF burst energies presented in Table 3 for the 2800-MHz radio emissions have been previously correlated with solar proton event time-integrated flux.<sup>3</sup> Previous studies were also performed to correlate peak radio flux, duration of the burst, and average radio flux with proton flux. In addition, 3750-MHz data have been considered. The results of these studies indicate that correlations made with the 2800-MHz radio emission and the time-integrated proton flux are more significant than those obtained using the 3750-MHz radio emission. This does not rule out the possibility that further study of the 3750-MHz data might also provide good correlation when new data are available.3 However, the correlations described in this report use only 2800-MHz data, except for those presented in Section IV-D-3. Further correlation studies might include the frequency of approximately 2695 MHz since this is the frequency being used by the MSC observatories which will provide the radio data for use in SPAN (Ref. 12). When new data are taken at various frequencies and when past cycle data are refined, new frequencies or a combination of frequencies may be used to demonstrate more significant correlations.

### Table 4. Estimates of the duration of 2800-MHz bursts associated with proton events of the last cycle and of delay time between bursts and proton events

Duration time, min	60.3±29.1
Delay time between start of RF to start of proton event, h	3.9±1.4
Delay time between start of RF to maximum of proton event, h	8.6±3.7
Delay time between maximum of RF to start of proton event, h	$3.3\pm1.4$

A statistical analysis was performed to obtain the average radio burst duration and the delay times between bursts and proton events for those events given in Table 3 for which data were available. These are the same solar events which were used in making the correlations between 2800-MHz burst data and time-integrated proton flux. Table 4 lists the average and the estimated 95% confidence limits on the average for the delay time from maximum and start of radio burst to the start of the proton event and from the start of the radio burst to the maximum of the proton event and the time of burst duration. Figure 3 (from Ref. 13) shows an envelope and mean of the time history of solar proton events of the past solar cycle and the time history of three different solar proton events.

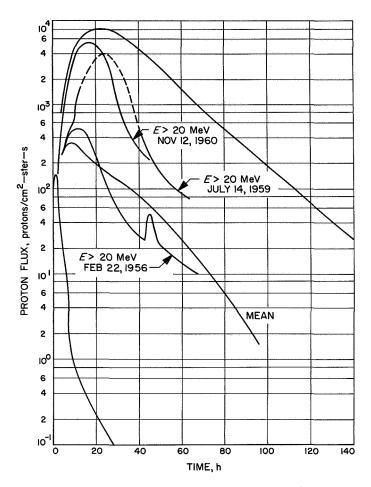


Fig. 3. Time history envelope and mean of the flux of proton events compared with three events of the last solar cycle (from Ref. 13)

### C. Correlation of Radio Emission Parameters with Time-Integrated Proton Flux

The data used in the analyses of 2800-MHz radio bursts are given in Table 3 and consist of 81 radio events and 24 associated proton events.<sup>5</sup> The solar events for which only radio events are listed may have been associated with proton events that were undetected because the fluxes were below earth-based detector cutoffs or did not arrive at the earth because of propagation conditions or trapping in space. The results presented, using the radio events and the RF predictions techniques, were based on all 81 radio events.

1. Single-parameter correlations. Correlations were made between the  $log_{10}$  of the 2800-MHz radio burst

<sup>&</sup>lt;sup>5</sup>Also M. D. Lopez (see footnote 3).

energy and the  $\log_{10}$  of the associated time-integrated proton flux having energies greater than 30 MeV. The correlations were made using a total of 24 radio events observed by the Canadian National Research Council Observatory at 2800 MHz. A linear least squares analysis was performed using the data, and the correlation coefficient and regression equation were found. The linear regression analysis was performed with the listed 24 data points (See Table 3) and the 13 points selected as described below.

The regression analysis was performed first with data from the 24 events and then with data from 13 events selected from the 24. The selection of the 13 points was made by statistically analyzing the data to discard outliers (See Fig. 4). This was accomplished by computing the average proton flux and the standard error of the mean for a particular interval of radio energy. Those events whose proton flux was greater than 3 times the standard error of the mean (3S) were eliminated. The procedure was repeated with the remaining points in the interval. If no events were eliminated on the first or successive

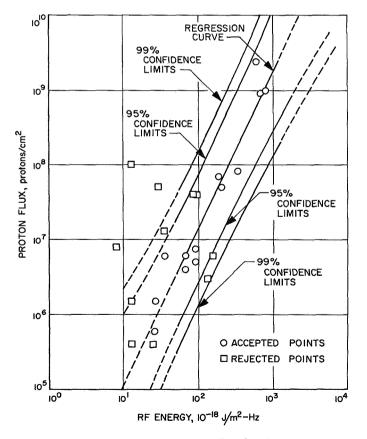


Fig. 4. Time-integrated proton flux having energy greater than 30 MeV as a function of RF burst energy

trials, then all events whose proton flux was greater than 2S were eliminated and the procedure repeated until no events were eliminated. After this was done, 16 points remained. At this point, a check was made to see if the differences of the averages of neighboring intervals exceeded  $3S_D = 3(S_{x1}^2 + S_{x2}^2)^{\frac{1}{2}}$ , where  $S_{x1}$  is the standard error of the mean of interval 1 and  $S_{x2}$  the standard error of the mean of interval 2. The differences of the averages did exceed  $3S_p$  for three intervals which had radio energies greater than 40 flux units (50-100, 100-500, 500-1000) representing moderate to large radio and proton events. Thus, a linearly increasing relationship between the log of RF energy and the log of proton fluxes truly exists only at the upper ranges of the curve of radio energy vs proton flux. Because of the large scatter of data, the events with radio energy less than 40 radio energy flux units were neglected, it being assumed that major interest is centered on the large events. A linear least squares analysis was performed and the correlation coefficient was calculated for the remaining 13 points. The correlation coefficient is 0.962; thus a linear regression approximation was considered applicable. The linearity of the relationship between radio energy and proton flux for the large events was used over the entire range of radio events in all of the analyses of this section (again because major interest is centered on the large events). However, the results of the analyses for radio events of less than 40 radio energy flux units are questionable. The solid line in Fig. 4 indicates the region over which use of a linear relationship is justified on the basis of the tests described above; the dashed line indicates the region over which it is not.

Equations (1) and (1a) give the regression equations for the selected 13 data points and the total 24 data points, respectively. See Table 3 for the values used:

$$\log_{10}(PF) = 2.976 + 2.083 \log_{10}(RFE)$$
(1)

$$\log_{10}(PF) = 4.778 + 1.285 \log_{10}(RFE)$$
 (1a)

where

PF = is the time-integrated proton flux for energies greater than 30 MeV (protons/cm<sup>2</sup>)

RFE = radio burst energy in units of (10<sup>-18</sup> J/m<sup>2</sup>-Hz)

The correlation coefficients with the 95% confidence intervals are 0.962 (0.873, 0.989) and 0.716, (0.432, 0.871) for the 13 and 24 points, respectively. Figure 4 shows the relationship between radio burst energy and proton event flux derived from Eq. (1) which is used to predict timeintegrated proton flux having energy greater than 30 MeV from the area of the associated RF burst profile at 2800 MHz.

The 95% and 99% confidence intervals for the prediction of a single-event time-integrated proton flux were determined for Eq. (1). The prediction of a single-event timeintegrated proton flux will lie in the following confidence interval (Ref. 14):

$$Y' \pm t_{\alpha/2} S_{yx} \left( 1 + \frac{1}{n} + \frac{(X - \bar{X})^2}{(n-1) S_x^2} \right)^{\frac{1}{2}}$$
(2)

where

 $t_{\alpha/2}$  = the percentage point of the student *t*-distribution

 $1 - \alpha =$ confidence interval

 $X = \log_{10}$  of radio energies at which confidence limits were computed

 $\bar{X} = \log_{10}$  of average radio energy

$$S_{yx} = \left(\sum_{i=1}^{n} \frac{(Y_i - Y'_i)^2}{(n-2)}\right)^{\frac{1}{2}} = \text{estimated standard deviation of predicted flux of proton event from actual flux of proton event}$$
(3)

$$S_x = \left(\sum_{i=1}^{n} \frac{(X_i - \bar{X})^2}{(n-1)}\right)^2 = \text{estimated standard deviation of radio burst energy of actual events from the average event energy}$$
(4)

 $Y_i = \log_{10}$  of observed proton flux of the selected events

 $Y'_i = \log_{10}$  of predicted estimate of integrated proton flux from regression equation

 $X_i = \log_{10}$  of the radio energies of the selected events.

For the 95 and 99% confidence intervals,  $S_{yx} = 0.317$ ,  $S_x^2 = 0.279$ ,  $t_{0.025} = 2.201$ , and  $t_{0.005} = 3.106$ .

Several things must be taken into account when using these confidence limits. First, the confidence limits and regression equation must be applied with caution below 40 radio energy flux units. Secondly, the confidence limits were determined based on the  $S_{yx}$  computed for all data points instead of an  $S_{yx}$  computed for each interval of data points, which effectively cancelled the resolution available for the grouping of the data. However, this effect is assumed to be negligible, except for the smaller events near and below 40 flux units. Finally, the 95 and 99% confidence limits apply only when a proton event follows a radio event because these limits were determined based on the correlation between radio event energies and associated time-integrated proton fluxes. The probability that a proton event will occur is presented below. For each of the 81 radio burst energies the predicted value of proton flux from Eq. (1) and the 95% confidence interval was compared with the actual value of proton flux associated with that event. If the actual value fell within the 95% confidence interval, it was counted as a successful prediction. If the actual value fell below the 95% confidence interval, or if no proton event occurred after detection of a radio event, the event was called a "false alarm." The occurrence of a proton event of smaller magnitude than predicted is important in engineering applications. In this application there are threshold limits established for radiation damage to the spacecraft from solar proton events. A prediction of an event of size greater than these limits which is followed by an event of size less than these limits would have to be considered

# Table 5. False alarm percentage and miss frequencyfor the prediction method using RF energyand the 95% confidence limitson time-integrated protonflux estimates

Time-integrated proton flux, protons/cm <sup>2</sup>	Number of predicted events	Number of faise alarms	False alarms, %	Number of misses
(1–10) × 10 <sup>5</sup>	39	31	79.5	0
(1–10) × 10 <sup>6</sup>	23	17	74	2°
(1–10) × 10 <sup>7</sup>	14	8	$\begin{cases} 43^{a} \\ 14.3^{b} \end{cases}$	3
$(1-10) \times 10^{8}$	4	1	25	1
(1–10) × 10 <sup>9</sup>	1	0	Ö	0
<sup>a</sup> No proton event o <sup>b</sup> Proton event occu <sup>e</sup> No burst recorded	rred.			

a false alarm even though an event of some magnitude did occur. However, from the standpoint of scientific applications an event of any size is significant.

False alarm analyses were performed in two ways. Using the first method, the RF energy range was divided into intervals corresponding to predictions of proton flux in the ranges 1 to  $10 \times 10^n$  (protons/cm<sup>2</sup>), where n = 5

# Table 6. False alarm percentage and miss frequencyfor the prediction method using RF energyand the 99% confidence limitson time-integrated protonflux estimates

Time-integrated proton flux, protons/cm <sup>2</sup>	Number of predicted events	Number of false alarms	False alarms, %	Number of misses
(1-10) × 10 <sup>5</sup>	39	31	79.5	0
$(1-10) \times 10^{6}$	23	17	74	2ª
$(1-10) \times 10^7$	14	6	43	2
$(1-10) \times 10^{8}$	4	1	25	1
$(1-10) \times 10^{9}$	1	0	0	0

through 9 consecutively. The criterion for selecting a false alarm was then applied.

Because of the scarcity of data from the last solar cycle, especially at the higher flux ranges, the false alarm probability is questionable. The information available, however, is given in Tables 5 and 6 and Fig. 5. There was no significant change in the false alarm percentage in going from a 95% confidence interval to a 99% confidence interval. Of all the false alarms given in Tables 5 and 6, only two events resulted from the case of a radio burst which

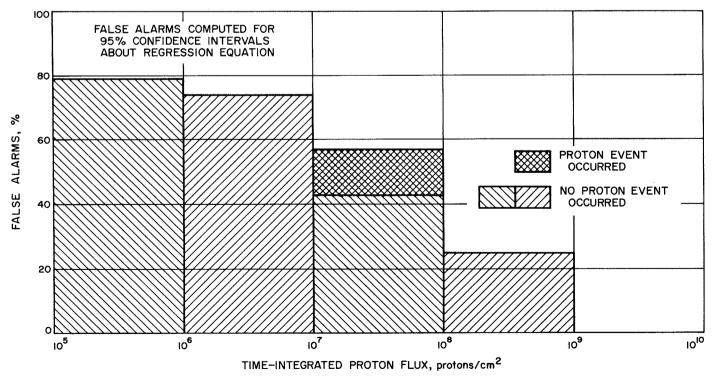


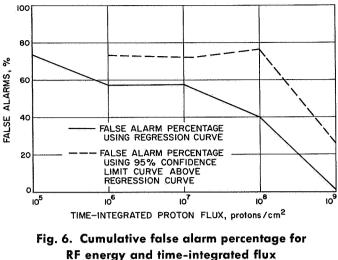
Fig. 5. False alarm percentage for RF energy and time-integrated flux (E > 30 MeV) prediction method

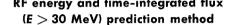
gave a prediction of a higher flux than the actual flux; these false alarms did not result when the 99% confidence intervals were used. These two events resulted in predicted fluxes (including their 95% confidence intervals) that were higher than the actual flux by a factor of about 1.2 and 1.7, respectively. Factors of 1 to 2 or less cannot be considered very significant because of uncertainties in the value of the proton flux. The rest of the false alarms resulted from radio bursts in which no proton event was detected.

In the above analysis, the event was called a miss if the actual value fell above the upper 95% confidence limit or if a proton event occurred during the time interval when the 2800-MHz radio flux was being observed and no RF was detected. The possibility of a flux being higher than predicted might not be important in scientific applications, but it is extremely important in engineering applications.

Although Tables 5 and 6 give a number of misses, only one miss occurred where no radio burst was recorded (11/4/57 proton event). The others resulted from timeintegrated proton flux predictions whose estimates plus the 95% confidence interval were less than the actual proton flux. Four of the misses involved a flux higher than the 99 or 95% intervals by the following factors: one by about a factor of 4 and 8 ( $8 \times 10^6$  protons/cm<sup>2</sup> actual flux), two by about a factor of 5 and 10  $(4.5 \times 10^7 \text{ to } 5 \times 10^7)$ protons/cm<sup>2</sup> actual flux), and one by a factor of 33 and 60  $(1 \times 10^8 \text{ protons/cm}^2 \text{ actual flux})$ . Except for the latter miss, these misses were not considered significant because they occurred for low proton flux events. Another miss involved a prediction higher than the 95% confidence interval by a factor of only 1.45, which is less than the uncertainty error in the measured proton data. The number of misses decreased by 1 when the 99% confidence interval about the estimate was considered.

Figure 6 and Tables 7 and 8 show the results of the second method of obtaining false alarm percentages and misses. In this analysis, a value of RF energy from Fig. 4 was chosen which corresponds to a specified proton flux value. The number of predicted events was compared with the number of false alarms for all predicted values above the flux value. Instead of taking a confidence interval about the predicted flux value, any value of proton flux which fell below the predicted level was counted as a false alarm. The false alarm percentages were obtained in one case by using the value of radio energy giving a particular estimate of proton flux (see Table 7) and in the other case by using the values of radio energy giving the





same proton flux on the estimate plus 95% confidence limit curve (see Table 8). As shown in Fig. 4, the radio energy giving a particular flux decreases when the curves lying above the actual regression curve are considered. The reason for using the curve lying above the regression

 Table 7. Cumulative false alarm percentage and miss frequency for the RF energy prediction method using the time-integrated proton flux estimates

Time-integrated proton flux, protons/cm <sup>2</sup>	Number of predicted events	Number of false alarms	False alarms, %	Number of misses
>105	81	59	73	1
>106	42	24	57	<b>5</b> °
>10"	19	11	58	5
>10 <sup>8</sup>	5	2	40	1
>109	1	0	0	1

Table 8. Cumulative false alarm percentage and<br/>miss frequency for the RF energy prediction<br/>method using the 95% confidence<br/>limits on time-integrated<br/>proton flux estimates

Time-integrated proton flux, protons/cm <sup>2</sup>	Number of predicted events	Number of false alarms	Faise alarms, %	Number of misses
>106	81	59	73	ja.
>107	32	23	72	3
>108	13	10	77	l ï
>10°	4	1	25	0

curve is that a lower miss frequency occurs at the lower radio energies. However, an increase in false alarms will occur if this is done. In this analysis, either of the two curves was chosen, and all events predicted above a certain flux were considered. For example, the number of events predicted above 10<sup>9</sup> protons/cm<sup>2</sup> would be the same as the number of radio events whose energy was equal to or greater than the energy on the curve which would give a value of 10° protons/cm<sup>2</sup>. This was compared to the actual number of events which occurred with proton fluxes equal to or greater than 10<sup>9</sup> protons/cm<sup>2</sup>, and the excess number of events over that number predicted would be the number of false alarms. A miss would be any event not preceded by a radio event or preceded by one less than the radio energy corresponding to that flux or greater.

The second method is useful in predicting false alarm probability for any estimate equal to or greater than a certain proton flux. Two curves were considered in the second method in order to analyze the tradeoff between the miss frequency and false alarm rate as the value of radio flux, used as a threshold for a particular proton flux or greater, was decreased. As can be seen from Tables 7 and 8, the false alarm percentage increased when the 95% confidence limit curve was used and the miss frequency decreased.

The false alarm probability and miss frequency selected for use with the radio burst energy predictor are obtained from the results in Table 5. When an estimate of the timeintegrated proton flux within the 95% confidence limits is made, the probability of having a false alarm or miss is assumed to be the percentage of false alarms or misses presented in Table 5 except for those predicted events having time-integrated flux greater than 10<sup>8</sup> protons/cm<sup>2</sup>. For these events the false alarm probability is given as a range. For those predicted events between 10<sup>8</sup>-10<sup>9</sup> protons/cm<sup>2</sup> the false alarm probability is in the range of 25-40%, and for those between 109-1010 protons/cm<sup>2</sup> the false alarm probability is in the range of 0-40%. These false alarm probability ranges are based on the average false alarm probability for events in the interval 10<sup>7</sup>-10<sup>9</sup> protons/cm<sup>2</sup> and the estimated false alarm probabilities for the intervals 10<sup>8</sup>-10<sup>9</sup> and 10<sup>9</sup>-10<sup>10</sup> protons/cm<sup>2</sup>. This rough approximation was made because the data sample in these last two intervals is considered inadequate to obtain representative false alarm probabilities for each interval.

Another parameter of the radio burst profile is the peak radio flux. The peak in the radio burst profile occurs early in the event, in most cases at least before the halfway point in time. Of 24 radio events, 23 were used in the correlation of the  $log_{10}$  of proton flux and the  $log_{10}$  of radio burst peak flux (one event had no recorded peak flux). The correlation coefficient (based on a linear least squares approximation) is 0.542. Data selection similar to that used in obtaining the regression of proton flux on radio energy was not used because the peak flux data were scattered in such a way as to make results of such an analysis difficult to interpret. However, events with peak radio fluxes less than 250 flux units were discarded because of the large amount of scatter for low peak fluxes. The second linear least squares analysis was made on the remaining 17 events. The regression curves are shown in Fig. 7 along with the 95 and 99% confidence limits on the predicted proton flux.

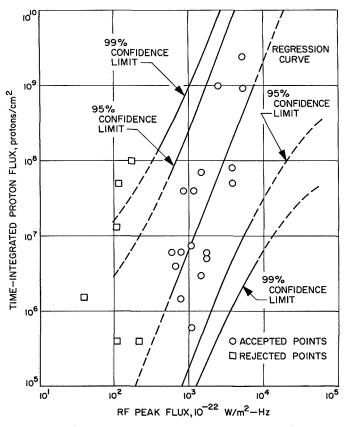


Fig. 7. Time-integrated proton flux for energies greater than 30 MeV as a function of RF burst peak flux

The linear regression equations found using the 17 and 23 events are given below in Eqs. (5) and (5a):

$$\log_{10}(PF) = 2.489 \log_{10}(peak) - 0.622$$
 (5)

$$\log_{10}(PF) = 4.380 + 0.964 \log_{10}(peak)$$
 (5a)

13

where

PF = the time-integrated proton flux for energies greater than 30 MeV (protons/cm<sup>2</sup>)

and

peak = the peak radio flux of the radio burst profile in units of  $10^{-22}$  W/m<sup>2</sup>-Hz

The correlation coefficients and 95% confidence limits on the correlation coefficients for the 17 and 23 event samples are 0.756 and (0.423, 0.909), and 0.542 and (0.158, 0.783), respectively.

Confidence limits of 95 and 99% were computed for the peak flux regression equation in the same manner as that for the radio energy. The standard deviation of predicted proton flux from the actual proton flux is  $S_{yx} = 0.698$  for the  $\log_{10}$  of the fluxes (see Eq. 3). The dotted lines (shown in Fig. 7) are used where the curve is extrapolated out of the range of data, and its use in these ranges is questionable.

The correlation of peak radio flux with proton flux is not as good as the correlation of radio energy with proton flux. In addition to the poorer correlation obtained using peak radio flux, it is difficult in some cases to define the peak flux with the same precision as the radio energy. The difficulty of determining the peak flux is demonstrated in Fig. 8 for a multiple peak radio event.

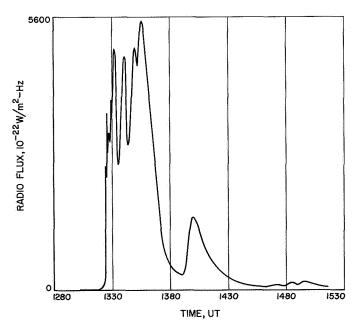


Fig. 8. Reconstruction, 2800-MHz radio burst profile of November 12, 1960

# Table 9. False alarm percentage and miss frequencyfor the prediction method using RF peak fluxand the 95% confidence limits ontime-integrated protonflux estimates

Fime-integrated proton flux, protons/cm <sup>2</sup>	Number of predicted events	Number of false alarms	Faise alarms, %	Number of misses
$(1-10) \times 10^{5}$	34	26	76.5	0
$(1-10) \times 10^{6}$	22	15	68	1ª
$(1-10) \times 10^7$	19	13	68.5	4
$(1-10) \times 10^{8}$	5	1	20	1
$(1-10) \times 10^{9}$	0	0	0	0

### Table 10. Cumulative false alarm percentage and miss frequency for the prediction method using RF peak flux and the time-integrated proton flux estimates

Time-integrated proton flux, protons/cm <sup>2</sup>	Number of predicted events	Number of false alarms	False alarms, %	Number of misses
>105	80	57	71.2	0
>106	46	30	65.2	<b>6</b> <sup>a</sup>
>107	24	17	71	. 5
>108	5	3	60	2
>10°	0	0	0	1

Table 11. Cumulative false alarm percentage and<br/>miss frequency for the prediction method<br/>using the RF peak flux and the<br/>95% confidence limits on<br/>time-integrated proton<br/>flux estimates

Time-integrated proton flux, protons/cm <sup>2</sup>	Number of predicted events	Number of false alarms	False alarms, %	Number of misses
>106	80	57	71.2	1ª
>10 <sup>7</sup>	63	53	84.2	3
>10 <sup>8</sup>	37	34	92	1
>109	12	9	75	1

The radio burst profile presented in Fig. 8 is that associated with the 11/12/60 proton event, one of the large proton events of the last solar cycle. The rate of change of radio flux in the burst in Fig. 8 at the leading edge of the burst profile is 978 flux units/min, and the highest flux

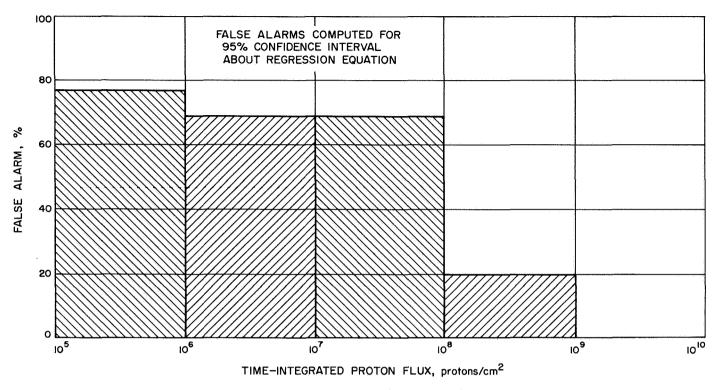
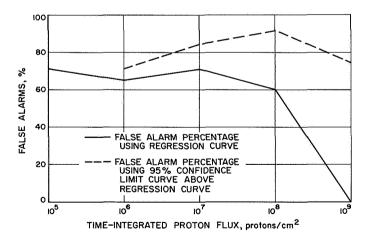
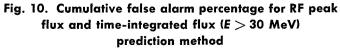


Fig. 9. False alarm percentage for RF peak flux and time-integrated flux (E > 30 MeV) prediction method

reached at the leading edge was about 5000 flux units. In Fig. 7 one can see that the peak radio flux giving an integrated proton flux of  $10^9$  protons/cm<sup>2</sup> (estimate plus 95% confidence interval) is about 1800 flux units. Therefore, after 2 to 4 min (plus time to obtain RF data) it would have been possible to predict a proton flux of  $10^9$  protons/cm<sup>2</sup> and be well inside the 95% confidence interval of the regression equation.





A false alarm and miss frequency analysis similar to that described previously using the RF energy predictor was performed. The results are shown in Figs. 9 and 10, and Tables 9, 10, and 11. Again, most of the false alarms resulted from lack of occurrence of proton events. Many of the misses from the RF peak flux analysis were insignificant. The results of the false alarm and miss frequency analysis showed the same general characteristics as those discussed previously for the RF energy predictor.

The false alarm probability and miss frequency selected for use with the radio burst peak flux predictor is obtained from Table 9. The results of the false alarm probabilities are summarized below:

Time-integrated proton flux, protons/cm <sup>2</sup>	False alarm probability, %
105-106	77
106-107	68
10 <sup>7</sup> -10 <sup>8</sup>	69
10 <sup>8</sup> -10 <sup>9</sup>	20-45
10°-1010	0-45

The above results were determined in the same manner as described previously for the RF energy predictor.

1 parameter **3** parameters 5 parameters Description 13 events 13 events 23 events 13 events 23 events 24 events log<sub>10</sub> (PF) = 2.976 + 2.083 log<sub>10</sub> (PF) = 4.778 + 1.285 log10 (PF) =  $\log_{10} (PF) =$  $\log_{10}(PF) =$ Linear regression log10 (PF) = 3.435 - 0.04874 4.326 - 0.445 3.960 - 0.4123.48 - 0.00507 equations log10 (RFE) log10 (RFE) log10 (plage area) log<sub>10</sub> (plage area) log10 (plage area) log10 (plage area) + 0.412 log10 + 0.161 log10 + 0.0602 log10 + 0.05785 log10 (sunspot area) (sunspot area) (sunspot area) (sunspot area) + 1.409 log10 + 2.142 log10 + 1.309 log10 2.252 log10 (RFE) + (RFE) (RFE) (RFE) + 0.0447 log10 0.4072 log10 (plage brightness) (plage brightness) 0.107 log10 0.1133 log10 (flare importance) (flare importance) Linear correlation 0.962 0.716 0.964 0.750 0.965 0.767 coefficients 0.317 0.312 Standard deviations 0.317

 
 Table 12. Comparison of regression equations, correlation coefficients, and standard deviations derived in the linear least squares analysis of the solar activity parameters and proton event time-integrated flux

2. Multiple parameter correlation. A multiple linear least squares analysis was used to find the correlation coefficient and the regression equation using five solar parameters as the independent variables and time-integrated proton flux as the dependent variable. These five solar parameters considered were the radio burst energy, the plage area, the plage brightness, the sunspot area, and the flare importance. The  $\log_{10}$  of the radio burst energy, plage area, sunspot area, and time-integrated proton flux were used. The analysis was performed for the 13 solar events used previously in the radio energy analysis and for 23 of the 24 events used previously (Table 3 and Figs. 11–14; there were incomplete data on one event).

A complete analysis on multiple parameters was not performed; rather only a simple analysis was made to compare regression equations and correlation coefficients obtained with the additional parameters with the ones obtained using only the radio energy. The quantity  $S_{yx}$ was computed for the equation using 13 events. The regression equations, correlation coefficients, and standard deviations  $S_{yx}$  obtained in the multiple parameter correlation analysis are given in Table 12, which compares all the regression equations and associated parameters.

The results given in Table 12 indicate that there are no major differences in the correlation coefficients and  $S_{yx}$ 's with use of the additional parameters. The regression equations show large fluctuation in the coefficients of the terms representing the parameters other than radio energy. Also, the coefficients of the terms for the other parameters are smaller than the coefficient of the radio energy term by at least a factor of 3. This means that time-integrated proton flux is better correlated with radio energy than with the other parameters.

3. Other radio burst parameters. The following radio burst parameters were correlated with the integrated proton flux for the associated proton event through a linear regression analysis (Figs. 15–17). The data in the frequency range 2800–3000 MHz were obtained at various observatories.

- (1) Product of burst duration and peak flux. Burst duration alone was shown to have a poor correlation.<sup>6</sup>
- (2) Time difference (min) between the maximum of the RF burst and flare maximum.
- (3) Time delay (h) between the start of the proton event and the start of the RF burst.

Table 13 summarizes the correlation coefficients determined in this analysis.

Table 13. Summary of a correlation analysis of some radio burst parameters with integrated proton flux

Radio burst parameter	<b>Correlation coefficient</b>
1	0.607
2	() 0.260
3	0.060

These results indicate that only the correlation between the radio burst energy and the peak radio flux with the proton flux discussed previously is high enough to be useful.

<sup>&</sup>lt;sup>6</sup>M. D. Lopez (see footnote 3).

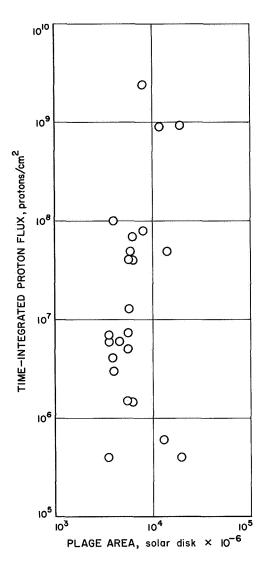
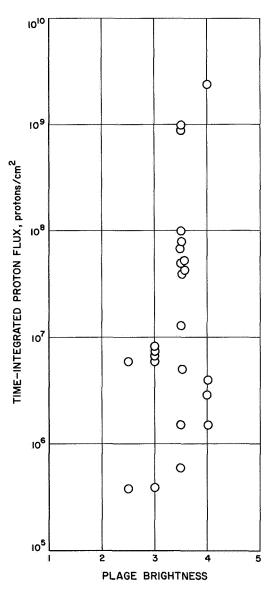
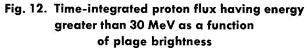


Fig. 11. Time-integrated proton flux having energy greater than 30 MeV as a function of plage area





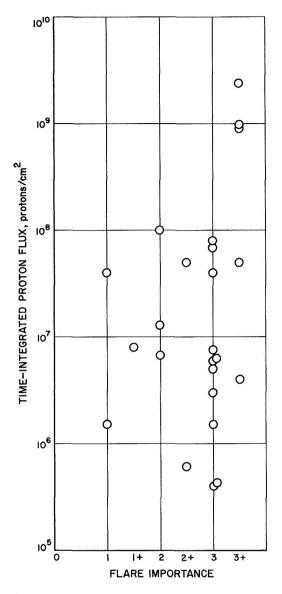


Fig. 13. Time-integrated proton flux having energy greater than 30 MeV as a function of flare importance (see Appendix A)

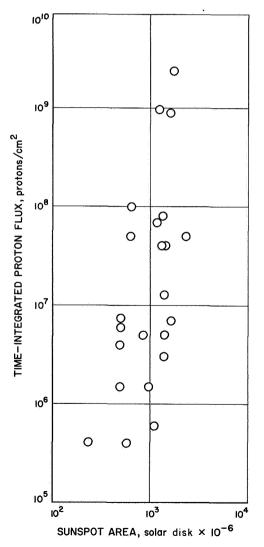
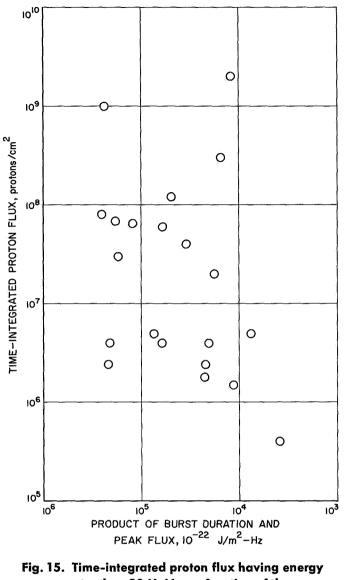
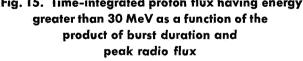
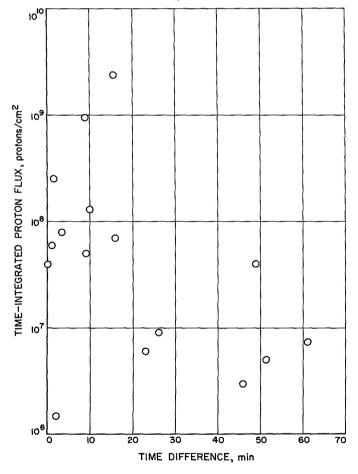
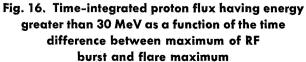


Fig. 14. Time-integrated proton flux having energy greater than 30 MeV as a function of sunspot area









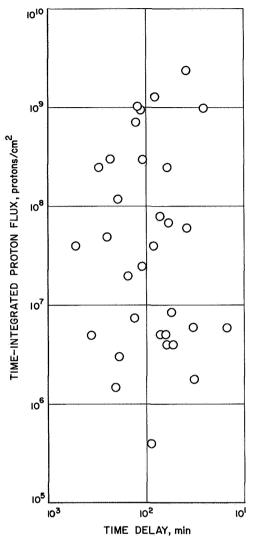


Fig. 17. Time-integrated proton flux having energy greater than 30 MeV as a function of the time delay between start of PCA and start of RF burst

### D. Selection of Parameters and Techniques to Predict Proton Events

The regression equation relating time-integrated proton flux and radio burst energy (Eq. 1) is selected for making the final forecast of time-integrated proton flux on a realtime basis during long-term interplanetary missions. The regression equation relating time-integrated proton flux and peak radio flux (Eq. 5) is selected for making preliminary predictions of time-integrated proton flux when the observable peak radio flux indicates that a large event is expected. Equation (1) was selected on the basis of the value of its correlation coefficient. Equation (5) was selected on the basis of the timeliness of the forecast when using peak radio flux. False alarm percentages as a function of time-integrated proton flux (Tables 5 and 9) and estimated burst duration time and delay times given in Table 4 are selected for use in completing the evaluation of the forecasts.

A forecast of the associated peak proton flux of the pending proton event is obtained from Fig. 18, using the predicted time-integrated proton flux. The relationship between peak and time-integrated proton flux presented in Fig. 18 was determined by linear regression analysis, using data of the last solar cycle (Refs. 6 and 11 were used except as noted previously).

Confidence limits of 95% are also shown on Fig. 18 so that when the time-integrated proton flux is estimated, the peak proton flux with its associated 95% confidence limits may be estimated and compared with the threshold radiation levels established as requirements for alerting project personnel.

A summary of major parameters obtained by using the selected techniques is presented in Tables 14 and 15 for various values of radio burst energy and peak radio flux, respectively.

### E. Limitations on Near-Earth Predictions Using Radio Emissions

Several limitations are inherently present when applying RF emissions observed near earth to techniques for forecasting proton flux in space. Propagation characteristics of solar protons in interplanetary space are such that the protons may reach certain points in interplanetary space without prior warning from a solar radio burst. This may be caused by proton events originating on the side of the sun away from the earth. In addition, the reception of radio energy at earth does not mean that all points in interplanetary space will contain solar protons. The particle propagation characteristics of the interplanetary medium will influence the arrival time of protons and determine whether or not they will arrive at all. This phenomenon is dependent on the position of the particleproducing flare on the sun's disk. Although the influence of the position of the flare on the arrival or nonarrival of protons at earth has been studied, no direct relationship has been found. Finally, the time for protons to travel from the sun to a spacecraft traveling to Venus may be considerably less than the time it takes them to arrive at earth. This would allow a shorter warning time than that based on observations from earth.

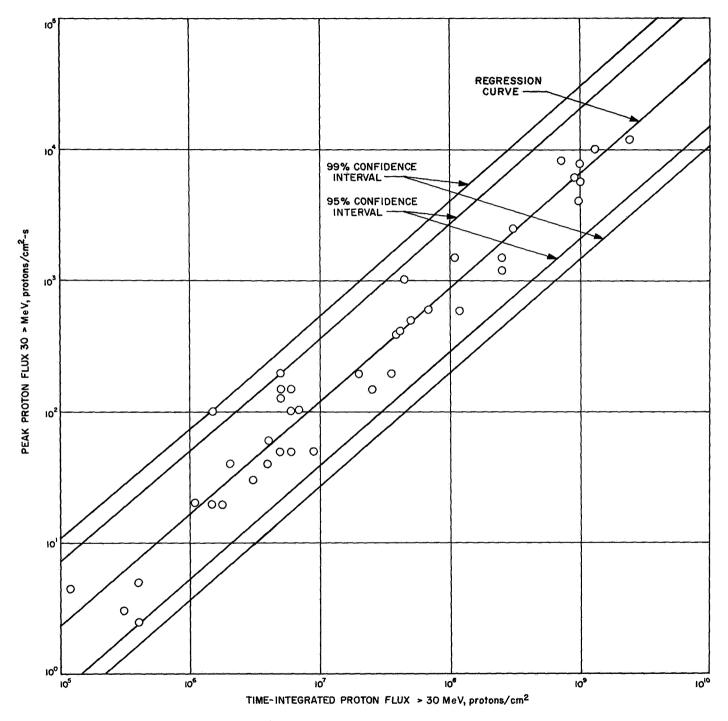


Fig. 18. Peak proton flux (E > 30 MeV) as a function of time-integrated proton flux (E > 30 MeV)

Radio energy received on	flux (E 95 %	oroton time-integrated > 30 MeV) includes confidence level,	Probability	time avai	l range of lable after tion, h	Estimated peak proton flux range	Threshold level for proton time-integrated	Threshold level for proton peak flux
real-time basis, 10 <sup>-18</sup> J/m²-Hz	Estimate	protons/cm² 95 % confidence interval	of false alarm, %	To start of proton event	To peak of proton event	(E > 30 MeV), protons/cm <sup>2</sup> -s	flux exceeded in the 95 % confidence interval	exceeded in the 95 % confidence interval
40	$2.1 \times 10^{6}$	$4.0 \times 10^{5}$ -1.2 × 10 <sup>7</sup>	74	0.7-4.5	3.1-11.5	$7.5 \times 10^{0}$ - $1.4 \times 10^{2}$	No	No
100	$1.4 \times 10^7$	$2.7 \times 10^{6}$ -7.2 × 10 <sup>7</sup>	57	0.7-4.5	3.1-11.5	$4.0 \times 10^{1}$ - $6.8 \times 10^{2}$	No	No
200	$6.0  imes 10^7$	$1.1 \times 10^{7}$ -3.2 × 10 <sup>8</sup>	57	0.7-4.5	3.1-11.5	$1.3 \times 10^{2}$ -2.4 × 10 <sup>3</sup>	No	No
400	$2.5  imes 10^8$	$4.5 \times 10^{7}$ -1.4 × 10 <sup>9</sup>	25-40	0.7-4.5	3.1~11.5	$4.5 \times 10^{2} - 8.8 \times 10^{3}$	Yes	Yes
1000	$1.7 \times 10^{\circ}$	$2.7 \times 10^{8}$ -1.2 × 10 <sup>10</sup>	0-40	0.7-4.5	3.1-11.5	$2.1 \times 10^{3}$ -5.8 × 10 <sup>4</sup>	Yes	Yes
2000	$7.0  imes 10^{9}$	$1.0 \times 10^9$ -5.0 $\times 10^{10}$	0-40	0.7-4.5	3.1-11.5	$6.5 \times 10^{3}$ -2.0 × 10 <sup>5</sup>	Yes	Yes

# Table 14. Summary of statistical results of prediction of proton event fluxes on real-time basis using radio burst energy

 Table 15. Summary of statistical results of prediction of proton event fluxes

 on real-time basis using peak radio flux

Peak radio flux received	flux (E 95 %	proton time-integrated > 30 MeV) includes confidence level,	Probability	time avai	l range of lable after tion, h	Estimated peak proton flux range	Threshold level for proton time-integrated flux exceeded	Threshold level for proton peak flux exceeded in
on real-time basis, 10 <sup>-22</sup> W/m <sup>2</sup> -Hz	Estimate	protons/cm² 95% confidence interval	of false alarm, %	To start of proton event	To peak of proton event	(E > 30 MeV), protons/cm <sup>2</sup> -s	in the 95 % confidence interval	the 95 % confidence interval
600	$1.8 \times 10^{6}$	$4.6 \times 10^{4}$ -7.0 × 10 <sup>7</sup>	68	1.6-4.4	4-11.4	$1.0 \times 10^{\circ}$ -6.5 × $10^{2}$	No	No
1000	$6.5  imes 10^6$	$1.8 \times 10^{5}$ -2.2 $\times 10^{8}$	68	1.6-4.4	4-11.4	$3.9 \times 10^{\circ}$ -1.8 × 10 <sup>3</sup>	No	No
3000	$9.5  imes 10^7$	$2.6  imes 10^{6} - 3.8  imes 10^{9}$	68	1.6-4.4	4-11.4	$3.8 \times 10^{1}$ -2.1 × 10 <sup>4</sup>	Yes	Yes
6000	$5.5 imes10^8$	$1.2 \times 10^{7}$ -2.5 $\times 10^{10}$	20-68	1.6-4.4	4-11.4	$1.3 \times 10^{2}$ - $1.0 \times 10^{5}$	Yes	Yes
10,000	$1.9  imes 10^9$	$3.0 \times 10^{7}$ -1.2 $\times 10^{11}$	0-45	1.6-4.4	4-11.4	$3.1 \times 10^{2}$ - 4.3 × 10 <sup>6</sup>	Yes	Yes
30,000	$3.0 imes10^{10}$	$1.6 \times 10^{8}$ -5.6 $\times 10^{12}$	0-45	1.6-4.4	4-11.4	$1.3 \times 10^{3}$ - $1.4 \times 10^{7}$	Yes	Yes

### V. Forecast Procedures for Predicting Proton Events

### A. Data and Preflare Forecast Network

The network established to transmit solar data and information into centralized agencies consists of solar observatories located throughout the world. Two agencies have been established to provide forecasts of solar activity and solar proton events from preflare solar data: the Space Disturbance Forecast Center, in Boulder, Colorado, which provides forecasts and solar information to civilian agencies, and the Astrogeophysical Forecast Facility at Ent Air Force Base, Colorado, which provides forecasts and other information to military agencies. Figure 19 and Table 16 present information on the location of the observatories, observing hours, times at which data are reported, and methods of communication with SDFC.<sup>7</sup> The solar observatories use optical and radio telescopes to measure various solar parameters. SDFC obtains the data from the observatories to make forecasts and to fulfill special data requests made by its users.

The Manned Spacecraft Center has established a solar proton forecasting network (SPAN) consisting of three radio and optical observatories to support their prediction analyses (Ref. 12). The observatories are located in Carnarvon, Australia, the Canary Islands, and Houston, Texas. Most of the RF data used in the forecasting system established for the *Mariner V* mission were provided by these observatories via SDFC.

### **B. Description of SDFC Facilities and Services**

Several types of forecasts of the probability of occurrence of proton events are provided by SDFC. These forecasts are issued for periods of 1, 2, 3, 7, and 28 days. The 28-day forecasts are based on location of active regions on the sun. The shorter-range forecasts are based on a number of parameters which are cross-correlated with solar activity. The 28- and 7-day forecasts are provided in routine weekly TWX's. The 1-, 2-, and 3-day forecasts are provided in TWX's twice daily.

<sup>&</sup>lt;sup>7</sup>Private communication from R. Doeker, SDFC, Boulder, Colo.

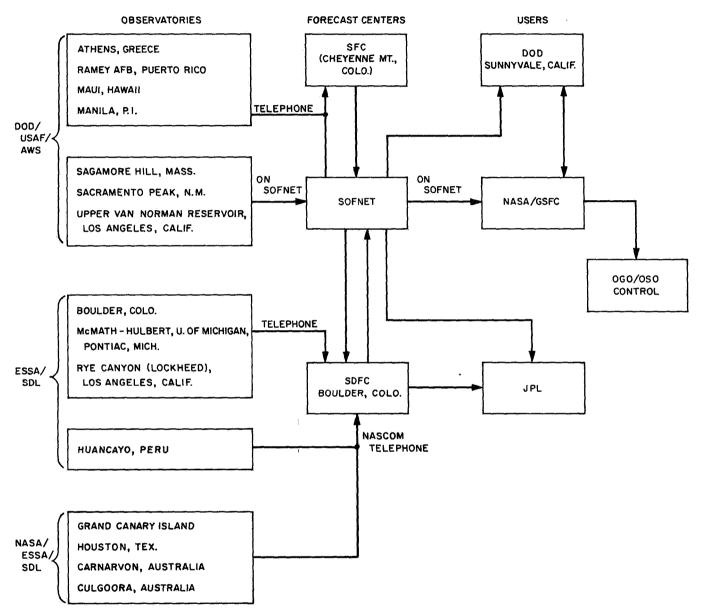


Fig. 19. Solar flare warning system

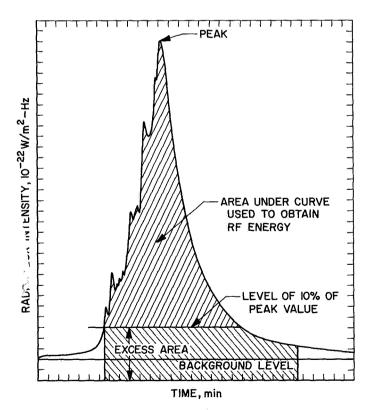
Constraints         Supported Support         Option Support         Option Support         Option Support         Option Support         Option							Real-	Reports of flares of class 2 or greater	greater	Routine reports	
Image: Section of the section of t	Observatory location	Supported by DOD	Supported by NASA/ ESSA	Radio	Optical	Observatory patrol times (±1 h), UT	time patrol site		Time to SOFNET, min	Communications system	Time to SOFNET, min
memoryl, and all back i be fried (SONET)     25     MI TWA to Behoeir (SONET)       and all back     1     20     MI TWA to Behoeir (SONET)       all back     1     1     23     1       all back     1     1     23     MI TWA to Behoeir (SONET)       all back     1     1     23     MI TWA to Behoeir (SONET)       all back     1     1     23     MI TWA to Behoeir (SONET)       all back     1     1     2     MI TWA to Behoeir (SONET)       all back     1     1     2     MI TWA to Behoeir (SONET)       all back     1     1     2     MI TWA to Behoeir (SONET)       all back     1     1     2     All to Beolder (SONET)       all back     1     1     2     All to Beolder (SONET)       all back     1     1     2     All to Beolder (SONET)       all back     1     1     1     2     All to Beolder (SONET)       all back     1     1	Athens, Greece	1			1	04–16	/	Mil Tel to Ent (SOFNET)	5	Mil WXTT to TIK (SOFNET)	8
Image: Second	Capri, Italy		>		7	05-17		Com Tel to Naples Mil Tel to Ent (SOFNET)	25	Mil TWX to Belvoir (SOFNET)	1-day report
Mil Tei le Ent (SONET)     Mil Tei le Ent (SONET)     Mil At The NX to GSFC (SONET)       Mil Tei le Ent (SONET)     SONET     SONET       11-23     V     NASA Tei lo Boulder     2     Mil WAT Tro TK (SONET)       7     Mil Tei le Ent (SONET)     3     SONET     3       11-23     V     Cam Tei lo Boulder (SONET)     3     Cam Tei lo Boulder (SONET)       7     NASA Tei lo Boulder (SONET)     3     Cam Tei lo Boulder (SONET)     3       7     NASA Tei lo Boulder (SONET)     3     Cam Tei lo Boulder (SONET)       7     NASA Tei lo Boulder (SONET)     3     Cam Tei lo Boulder (SONET)       7     NASA Tei lo Boulder (SONET)     3     Cam Tei lo Boulder (SONET)       7     NASA Tei lo Boulder (SONET)     3     Cam Tei lo Boulder (SONET)       7     NASA TAX Lo GSC (SONET)     3     Cam Tei lo Boulder (SONET)       8     NASA TAX Lo GSC (SONET)     3     Cam Tei lo Boulder (SONET)       9     NASA TAX Lo GSC (SONET)     3     Cam Tei lo Boulder (SONET)       11-224     V     NASA TAX Lo GSC (SONET)     3     Cam Tei lo Boulder (SONET)       11     12-24     V     NASA TAX Lo GSC (SONET)     3     Cam Tei lo Boulder (SONET)       11     12-24     V     NASA TAX Lo GSC (SONET)     3     Cam Te	Wandlastain (Garmany)	······································			`	06-18		Com Tel to Frankfurt	20	Mil TWX to Belvoir (SOFNET)	1-day report
r     r     r     07-19     r     MASA Tel lo Beulder     2     MASA TWX to GSFC (SOTNET)       r     r     r     r     11-23     r     SOFNET     5     MIT rel to Enric (SOTNET)       r     r     r     r     r     r     11-23     r     SOFNET       r     r     r     r     r     r     r     sofNET     sofNET       r     r     r     r     r     r     sofNET     sofNET       r     r     r     r     r     sofNET     sofNET       r     r     r     r     r     r     sofNET       r     r     r     r     r     r     sofNET       r     r     r     r     r     sofNET     sofNET       r     r     r     r     r     sofNET     sofNET       r     r     r     r     r     sofNET       r     r     r     r     sofNET     sofNET	Nera (Holland),				<b>-</b>	}		Mil Tel to Ent (SOFNET)			
Image: Solution of the second state of the second	Meudon (France)			,	``	07 10		NASA Tel to Roulder	c	NASA TWX to GSFC (SOFNET)	30
Note:     11-23     V     Softweit     0     Softweit       11-23     V     Cam Tel to beouler (SONET)     3     Cam Tel to Beouler (SONET)     3     Cam Tel to Beouler (SONET)       11-23     V     Cam Tel to Beouler (SONET)     3     Cam Tel to Beouler (SONET)     3     Cam Tel to Beouler (SONET)       11-23     V     Cam Tel to Beouler (SONET)     3     Cam Tel to Bouler (SONET)     3     Cam Tel to Bouler (SONET)       11-24     V     NASA TWX to GSFC (SONET)     3     Cam Tel to Bouler (SONET)     3     Com Tel to Bouler (SONET)       11-21     V     V     11-22     V     Cam Tel to Bouler (SONET)     3     Com Tel to Bouler (SONET)       11     V     V     V     11-22     V     Cam Tel to Bouler (SONET)     3     Com Tel to Bouler (SONET)       11     V     V     V     NASA TWX to GSFC (SONET)     3     Com Tel to Bouler (SONET)       11     V     V     V     NASA TWX to GSFC (SONET)     3     Com Tel to Bouler (SONET)       11     V     V     V     NASA TWX to GSFC (SONET)     3     Com Tel to Bouler (SONET)       11     V     V     NASA TWX to GSFC (SONET)     3     Com Tel to Van Norman (SONET)       11     V     V     NASA TWX to	Grana Canary Islana Damay AFR D D	/	*	<b>~</b>	× >	10-22	<u> </u>	Mil Tel to Ent (SOFNET)	( <sup>ر</sup> )	Mil WXTT to TIK (SOFNET)	15
Image: Solution is a service (SONET)     3     Com Tel to Belvoir (SONET)     3     Com Tel to Belvoir (SONET)       Image: Solution is a service service is a service is a service is a service is a servi	Sagamore Hill Mass.	~ `>		>	⊾	11-23	- `>	SOFNET	0	SOFNET	5
11-23     11-23     1     Com Tel to Boulder (SOFNET)     5       12-24     12-24     12-24     1     5     3       11     1     12-24     1     0     3       11     1     1     1     1     3       12     1     1     1     1     3       13     1     1     1     1     3       14     1     1     1     3     3       13     1     1     1     1     3       14     1     1     1     1     3       11     1     1     1     1     3       11     1     1     1     1     3       11     1     1     1     1     3       11     1     1     1     1     3       11     1     1     1     1     3       11     1     1     1     1     3       11     1     1     1     1     3       11     1     1     1     1     1       11     1     1     1     1     1       11     1     1     1     1     1 <td>NRL, Washington, D.C.</td> <td></td> <td></td> <td><u> </u></td> <td>&gt;</td> <td>11-23</td> <td>-</td> <td>Com Tel to Belvoir (SOFNET)</td> <td>e</td> <td>Com Tel to Belvoir (SOFNET)</td> <td>Beginning of</td>	NRL, Washington, D.C.			<u> </u>	>	11-23	-	Com Tel to Belvoir (SOFNET)	e	Com Tel to Belvoir (SOFNET)	Beginning of
11-23     /     Com Tel to Jicara     5       12-24     /     ESSA Tel to Boulder (SOFNET)     3       12-24     /     12-24     /     Com Tel to Boulder (SOFNET)     3       12-24     /     12-24     /     Com Tel to Boulder (SOFNET)     3       12-24     /     13-01     /     Com Tel to Boulder (SOFNET)     3       13-01     /     /     13-01     /     SOFNET     3       14-02     /     /     14-02     /     SOFNET     3       11     /     /     /     /     /     0       11     /     /     /     /     14-02     /     0       11     /     /     /     /     14-02     /     0       11     /     /     /     /     /     /     0       11     /     /     /     /     /     /     0       11     /     /					•						day report
Image: Solution of the solution of SOFNET)     3       Image: Solution of SOFNET)     12-24     V       Image: Solution of SOFNET)     3       Image: Solution of Solution	Huancayo, Peru		7		>	11-23	2	Com Tel to Jicara ESSA Tel to Boulder (SOFNET)	ŝ	NASA TWX to GSFC (SOFNET)	90
1     1     12-24     1     Com Tel to Boulder (SOFNET)     3       1     1     12-24     1     NASA Tel to Boulder (SOFNET)     3       1     1     1     1     1     2-01     1     2       1     1     1     1     1     1     2     1       1     1     1     1     1     2     0     2       1     1     1     1     1     2     0     2       1     1     1     1     1     2     0     2       1     1     1     1     1     2     0     2       1     1     1     1     1     2     0     2       1     1     1     1     1     2     0     2       1     1     1     1     1     1     2     0       1     1     1     1     1     1     2     0     2       1     1     1     1     1     1     1     1     1       1     1     1     1     1     1     1     1     1       1     1     1     1     1     1	Ottawa Canada			>	1.11	1224		Com Tel to Boulder (SOFNET)	n	Com Tel to Belvoir (SOFNET)	15
1     12-24     1     NASA Tel to Boulder (SOFNET)     3       1     12-01     1     20     2       1     1     1     1     1     2       1     1     1     1     1     2       1     1     1     1     1     2       1     1     1     1     2     2       1     1     1     1     2     2       1     1     1     1     2     2       1     1     1     1     2     2       1     1     1     1     2     2       1     1     1     1     2     2       1     1     1     1     2     2       1     1     1     1     2     2       1     1     1     1     1     2       1     1     1     1     1     1       1     1     1     1     1     2       1     1     1     1     1     2       1     1     1     1     1     1       1     1     1     1     1     1       1     1 <t< td=""><td>Dontine Mich</td><td></td><td>_</td><td>•</td><td>~</td><td>12-24</td><td>&gt;</td><td>Com Tel to Boulder (SOFNET)</td><td>'n</td><td>Com Tel to Boulder (SOFNET)</td><td>15</td></t<>	Dontine Mich		_	•	~	12-24	>	Com Tel to Boulder (SOFNET)	'n	Com Tel to Boulder (SOFNET)	15
Indext     Image:	(McMath-Hulbert)		<b>_</b>		<b>`</b>		<b>`</b>		I		<u> </u>
Index         Image: Solution of the solution	Houston, Tex.		>	7	>	12-24	7	NASA Tel to Boulder (SOFNET)	e	NASA TWX to GSFC (SOFNET)	15
Indext     Indext     Indext     SOFNET     0       Indext     Indext     Indext     Indext     SOFNET     0       Indext     Indext     Indext     Indext     Indext     Indext     Indext       Indext     Indext     Indext     Indext     Indext     Indext <td>Boulder, Colo.</td> <td></td> <td>7</td> <td>&gt;</td> <td>&gt;</td> <td>1301</td> <td>7</td> <td>Com Tel to Boulder (SOFNET)</td> <td>3</td> <td>SOFNET</td> <td>S</td>	Boulder, Colo.		7	>	>	1301	7	Com Tel to Boulder (SOFNET)	3	SOFNET	S
oirl oirl (1)     /     /     /     14-02     /     SOFNET     0       oirl (1)     /     /     /     /     14-02     /     SOFNET     3       /     /     /     /     /     14-02     /     Com Tel to Boulder (SOFNET)     3       /     /     /     /     /     /     /     14-02     /     Mil TWX to Ent (SOFNET)     3       /     /     /     /     /     /     /     /     3       /     /     /     /     /     /     /     3       /     /     /     /     /     /     3       /     /     /     /     /     /     3       /     /     /     /     /     /     3       /     /     /     /     /     /     3       /     /     /     /     /     /     16-04       /     /     /     /     /     /     /       /     /     /     /     /     /     /       /     /     /     /     /     /     /       /     /     /     /     /     <	Sacramento Peak, N.M.	7			>	1301	7	SOFNET	0	SOFNET	ŝ
(on)     /     /     14-02     /     Com Tel to Boulder (SOFNET)     3       (on)     /     /     /     14-02     Mil Twy to Ent (SOFNET)     3       /     /     /     /     14-02     Mil Twy to Ent (SOFNET)     3       /     /     /     /     /     14-02     Mil Twy to Ent (SOFNET)     3       /     /     /     /     /     /     /     15       /     /     /     /     /     /     15       /     /     /     /     /     /     5       /     /     /     /     /     /     5       /     /     /     /     /     /     5       /     /     /     /     /     /     5       /     /     /     /     /     16       /     /     /     /     /     16       /     /     /     /     /     16       /     /     /     /     /     16       /     /     /     /     /     16       /     /     /     /     /     16       /     /     /     /<	Los Angeles, Calif. (Van Norman Reservoir)	7	<u> </u>	7	>	1402	7	SOFNET	ò	SOFNET	C,
v     v     14-02     Com Tel to Boulder (SOFNET)     3       v     v     v     14-02     Mil TWX to Ent (SOFNET)     15       v     v     v     16-04     v     Mil Tel to Ent (SOFNET)     5       v     v     v     v     v     16-04     v     5       v     v     v     v     v     14-02     Mil Tel to Ent (SOFNET)     5       v     v     v     v     v     v     0     5       v     v     v     v     vois Tel to GSFC (SOFNET)     5       v     v     v     vois Tel to GSFC (SOFNET)     5       v     v     v     vois Tel to Ent (SOFNET)     15       v     v     v     vis Tel to Ent (SOFNET)     16       v     v     vis Tel to Ent (SOFNET)     10       vis Tel to Ent (SOFNET)     vis Tel to Ent (SOFNET)     2       v.d.     vis Tel to Ent (SOFNET)     10       v.d.     vis Tel to Ent (SOFNET)     10       v.d.     vis Tel to Ent (SOFNET)     2       v.d.     vis Tel to Ent (SOFNET)     2       v.d.     vis Tel to Ent (SOFNET)     2       v.d.     vis Tel to Ent (SOFNET)     5       v.d.	Los Angeles, Calif. (Lockheed, Rye Canyon)		~		>	1402	7	Com Tel to Boulder (SOFNET)	ε	Com Tel to Boulder (SOFNET)	
v     v     14-02       v     v     16-04     v       v     v     v     20-08     v       v     v     v     21-09     v       v     v     v     v     21-09       v     v     v     v     21-09       v     v     v     v     v       v     v     v     v     v       v     v     v     v     v       v     v     v     v     v       v     v     v     v     v       v     v     v     v     v       v     v     v     v     v       v     v     v     v     v       v     v     v     v     v       v     v     v     v     v       v     v     v     v     v       v     v     v     v     v       v     v     v     v     v       v     v     v     v     v       v     v     v     v     v       v     v     v     v     v       v     v     v     v     v   <	Los Angeles, Calif. (Mt. Wilson)				2	1402		Com Tel to Boulder (SOFNET)	ς,	Com Tel to Van Norman (SOFNET)	30
V     V     16-04     V       V     V     V     20-08     V       V     V     V     21-09     V       V     V     V     22-10     V       V     V     V     V     22-10       V     V     V     V     22-10       V     V     V     V     22-10       V     V     V     V     V       Solver     V     V     V     V       Solver     V     V     V     V       Solver     Solver     Solver     V       Solver     Solver     Solver     Solver	Stanford, Calif.		>	>		1402		Mil TWX to Ent (SOFNET)	15	Com Tel to Belvoir (SOFNET)	15
V     V     V     20–08     V       V     V     V     21–09       V     V     V     22–10     V       V     V     V     V     22–10     V       V     V     V     V     02–14     V       V.A.     V.A.     SofNet     SofNet     SofNet       Ciolo. (Space Disturbance Forecast Center)     Itelephone     Titk	Maui, Hawaii	2	7		~	1604	7	Mil Tel to Ent (SOFNET)	5	MII WXTT to TIK (SOFNET)	8
v     v     21–09       v     v     v     22–10       v     v     v     v	Culgoora, Australia		2	7	7	20-08	7	Com Tel to Canberra NASA Tel to GSFC (SOFNET)	ŝ	Com Tel to Canberra NASA TWX to GSFC (SOFNET)	õ
V     V     V     22–10     V       V     V     V     22–10     V       V     V     V     02–14     V       × Va.      SoFNET      SoFNET       ∴ Va.        SoFNET       ∴ Va.	Tokyo, Japan			>		2109		Com Tel to Fuchu, Japan Mil Tel to Ent (SOFNET)	15	Mil TWX to Belvoir (SOFNET)	<b>6</b> 0
V     V     22–10     V       V     V     02–14     V       ce names appearing herein are defined as follows:     20–14     V       Va.     .va.     SOFNET       Va.     .itelephone     .itelephone	Manila, P.I.	7	2	2	7	22-10	>	Mil Tel to Ent (SOFNET)	10	Mil WXTT to TIK (SOFNET)	8
V     02–14     V       ce names appearing herein are defined as follows:     SOFNET       ce.     SoFNET       va.     SOFNET       colo. (Space Disturbance Forecast Center)     Itelephone       Itelephone     Tix	Carnarvon, Australia		7	>	>	22-10	2	NASA Tel to Boulder (SOFNET)	2	NASA TWX to GSFC (SOFNET)	õ
SOFNET TIK WXTT	Tehran, Iran	7			7	02-14	1	Mil Tel to Ent (SOFNET)	5	Mil TT to TIK (SOFNET)	g
Ft. Belvoir, Va. Boulder, Colo. (Space Disturbance Forecast Center) commercial telephone Ent AFB Colo. WXTT	<sup>a</sup> Abbreviations and place na	mes appearing	herein are defir	ned as follow	YS:	SC		iolar Observatories Forecast Network: Te	etype loop	is connecting all U.S. solar observatories	
Boulder, Colo. (Space Disturbance Forecast Center) commercial telephone Ent AFB Colo. willthore telephone							÷Ψ	o the Space Disturbance Forecast Center active at Ent AFR Colo. Goddard Space	at Boulder, e Flight Cei	. Colo., the Astrogeophysical Forecusi afer. Greenbelt, Md., Ft. Belvoir, Va.,	
commercial telephone TIK Ent AFB Colo. WXTT willthry telephone		(Space Disturb	ance Forecast Ce	snter)			- 0	nd Tinker AFB, Oklahoma City, Okla.			
Ent AFB Colo. willtary talankana		ephone						inker AFB, Oklahoma City, Okla.			
								vireless teletype			

Table 16. Network of solar observatories supplying information to Space Disturbance Forecast Center $^{a}$ 

The SDFC service also includes transmitting data received from observing stations to users. Under special arrangements, data transmitted to SDFC by a participating station are not generally interpreted, but SDFC will interpret information for its users upon request. In addition, SDFC provides data on other activity parameters, including the class of optical flares, plage area, brightness, sunspot area, magnetic complexity, and any proton data available to it from earth-based detectors, satellites, and probes.

### C. Techniques and Criteria Used to Obtain Radio Burst Energy

1. Calculations of area of radio burst profile. The area under the curve of the radio burst flux-vs-time profile is computed by a numerical integration (Appendix B). The RF energy used in the prediction is shown in Fig. 20 as the area under the curve. The prediction techniques use the area remaining under the burst profile after the base line of the profile is raised by 10% of the peak value. This part of the burst profile was selected because the only areas available in the literature are the areas of the burst profile greater than the 10% difference. Studies of the radio





burst profile indicated that use of this part of the area eliminated the results of postburst increase (Fig. 2) in the smaller bursts, where the postburst increase may contribute significantly to the burst profile area.<sup>8</sup>

2. Selection of data interval. Two considerations are important in determining the time interval for recording and transmitting. First, the burst profile data should provide an accurate determination of the proton flux; second, the time interval for transmitting the real-time data should minimize delay time prior to forecasting.

The time intervals were determined using four representative burst profiles from the last solar cycle and one from this cycle. Points were taken from the curves at 30-s intervals. The numerical procedure described in Appendix B was used to compute the burst profile area using data points separated by 30-s, 1-min, 2-min, 4-min, and 8-min intervals. Each of these burst profile areas was substituted into Eq. (1) to obtain corresponding proton fluxes. Then proton fluxes for each event were obtained by substituting burst profile areas, determined by planimeter, into Eq. (1). The planimeter-related proton fluxes were normalized to 1.0, and the corresponding proton fluxes determined numerically for each event were normalized using the planimeter-related fluxes. The results (Table 17) show that significant differences in computed fluxes may occur when the time interval on the radio event data is greater than 4 min.

### Table 17. Comparison of time-integrated proton fluxes using the RF energy prediction method and RF energies computed using data points separated by different time intervals<sup>a</sup>

Events	<u> </u>		ed time-integ vals on radio		. <u></u>
	30 s	Time intervals on radio flux data           30 s         1 min         2 min         4 min           .904         .916         .897         .887           .981         .966         1.036         .918		8 min	
11/12/60	.904	.916	.897	.887	.775
11/20/60	.981	.966	1.036	.918	.954
7/17/61	.957	.960	.975	.898	1.240
7/20/61	.978	.985	.969	.778	2.040
7/7/66	1.099	1,111	1.158	.893	1.777

Partial areas were computed, using data points taken for specific intervals of time, to determine whether a reliable estimate of the total area could be made before

<sup>&</sup>lt;sup>8</sup>M. D. Lopez (see footnote 3).

all burst profile data points were transmitted. If after some time into the burst a reliable estimate could be made, then data should be transmitted at least at this time interval. The method of partial areas did not indicate any feasible way of making a prediction of area before burst termination. Therefore, a prediction of proton flux before the end of burst requires a different procedure. Correlation of flux with the radio peak flux may provide a procedure, since an increase in radio flux beyond certain limits indicates a large event. For large proton events, the threshold radio peak flux value may be exceeded 2 to 4 min after the start of a burst. Data transmitted at 4-min intervals are adequate for this purpose.

3. Selection of RF flux level criteria. Radio burst data from SDFC were received for use in the proton flux prediction techniques when the radio flux increased 500 flux units over background. An attempt was made to exclude as many false alarms as possible and still not miss any major events. One can see by looking at the peak flux values in Table 3 that only one proton event in the last cycle with integrated flux greater than  $5 \times 10^7$  protons/cm<sup>2</sup> would have been missed if radio events whose flux never increased beyond 500 flux units above background were ignored.

#### **D. Checkout of Operational Network**

On October 30 and 31, 1967, simulated data on solar activity including proton events were provided by SDFC. The simulation was primarily performed for the Apollo Project at MSC but with JPL invited to participate. Proton data from riometer stations, however, were sent from Anchorage directly to Houston via teletype lines and were not available to JPL. JPL received information on general solar activity, radio emission data, and some *Pioneer* proton data.

The simulation of solar activity consisted of five solar events. Sufficient radio data on two events were provided for use in the regression equations. In the one event, the peak radio flux (1520 flux units) at 2695 MHz was provided 20 min after the event was to have occurred. RF burst data at 2695 MHz can be used in place of 2800-MHz burst data. The regression equation for peak radio flux vs integrated proton flux was used to estimate the expected integrated proton flux for particles of energies greater than 30 MeV. The value obtained was  $1.80 \times 10^7$  protons/cm<sup>2</sup> based on a peak flux of 1520 flux units, with a 95% confidence interval of  $5.0 \times 10^5$  to  $6.0 \times 10^6$  protons/cm<sup>2</sup>. No proton flux data were reported on this event. In another event, radio data at 2695 MHz from the Sagamore Hill Observatory (Massachusetts) were transmitted, starting 30 min after initial solar activity was reported (including a Sb flare). The burst had started 6 min after the initial report. The radio burst lasted 48 min, and the last data were sent 15 min after the termination of the burst. The data were transmitted in sufficient detail to be used in the regression equation derived for the radio burst energy vs integrated proton flux. A value for the integrated proton flux above 30 MeV of  $3.5 \times 10^6$  protons/cm<sup>2</sup> with a 95% confidence interval of  $7.0 \times 10^5$  to  $2.0 \times 10^7$  protons/cm<sup>2</sup> was obtained based on a computed burst energy of 52 ( $10^{-18}$  J/m<sup>2</sup>-Hz). Again, no proton flux data were reported. The radio event coincided with a 3b white light flare.

In the other events (and in the two mentioned above) the general solar activity data reported were sufficient to indicate impending solar activity, but no quantitative predictions of a proton event could be made. Data and information reported included:

- (1) Plage brightness and area.
- (2) Sunspot area.
- (3) Flare area and position with respect to associated sunspots.
- (4) Ionospheric effects (due to electromagnetic radiation accompanying the optical part of the flare).

In one of the events, 3 h after the active region was first reported, *Pioneer VI* particle data were reported. Data from *Pioneer VI* were again reported 1 h later and from *Pioneer VII* 3½ h later. The following data were reported:

- (1) Solar wind velocity.
- (2) Cosmic ray data: counts per min over four energy ranges and quiescent values (the latter for *Pioneer VI* only).
- (3) Interplanetary magnetic field information.
- (4) Qualitative information on the  $H^+$  density and temperature.

The *Pioneer* data would be especially useful for one concerned with a spacecraft in interplanetary space; and an estimate of the solar cosmic ray flux in space could have been made (at least with *Pioneer VI* data). The additional information would be useful if a particle propagation model was incorporated into the proton event forecasting techniques.

The results of the simulation were evaluated to deter mine the type of information gained about the operation of the forecast system and the type of information on solar activity available for use in the prediction techniques.

First, on the operation of the alert system, the simulated data were devised for the exercise on the basis of past experience. Moreover, time delays in transmitting real-time data were made to conform to those expected from past experience. The delay in receiving the radio data from Sagamore Hill was about 15 to 20 min after the time of observation. Information such as this is useful in estimating the effectiveness of the system; and no difficulties are anticipated on the basis of the time delays indicated in the simulation. The experience obtained in the simulation indicates that a direct link between cognizant personnel and SDFC would facilitate reception and comprehension of information.

Solar cosmic ray data made available from the *Pioneer* probes indicate that data may be available to confirm proton flux estimates made after a radio burst. Moreover, the data might be used in forecasting techniques which account for proton propagation in space. The inclusion of such data in forecasting proton events is necessary because predictions based on measurements of solar parameters from earth are used to forecast proton fluxes in interplanetary space. Finally, it might be useful to receive real-time proton data based on riometer data to determine the type of data being transmitted and the associated time delays in obtaining the proton data.

### E. Recommended Procedures for Forecasting Solar Proton Events

The forecast procedure developed to evaluate solar activity and to predict proton events on a real-time basis in preparation for the *Mariner* 1967 Venus encounter is shown in the flow chart given in Fig. 21. A time span of 28 days is covered from the initial forecast of possible solar activity until the final period, when possible proton activity is imminent. The procedures are listed step-wise, each step being dependent on the information obtained in the prior step. The sequence of events is shown in Table 18. The times indicated are based on past experience and can fluctuate for specific cases.

The forecast procedures are described below as applied to any interplanetary mission. Active periods may be forecast from the 28- and 7-day solar activity predictions. The 28-day solar activity predictions are repeated weekly

#### JPL TECHNICAL REPORT 32-1303

# Table 18. Sequence of events in the time span froma 28-day prediction to the occurrenceof a solar proton event

Time	Event
— 28 days	-28-day SDFC prediction on solar activity
—7 days	-7-day SDFC prediction on solar activity
—3 days	-3-day SDFC prediction on flares and proton events
—2 days	-2-day SDFC prediction on flares and proton events
—1 day	-1-day SDFC prediction on flares and proton events
—1 day-0	SDFC special arrangement notification of unusual or imminent solar activity
0	Peak optical intensity of flare
0–15 min	SDFC special arrangement notification of solar flare activity
0—1 h	Data on RF emission from SDFC, also solar activity parameters such as associated plage area, brightness, sunspot area, and flare intensity
1-2 h	RF emission data and any riometer data (proton-induced) from SDFC
2–24 h	Proton data (riometer data, onset times, etc.) from SDFC
24-100 h	Postevent data from SDFC

and thus can be updated. The 28- and 7-day forecasts are simply used to establish periods of time when solar activity is expected. No actual predictions of proton events are made based on these forecasts.

The 1-, 2-, and 3-day forecasts lead to alerts that define periods of possible proton activity. In addition, the 1-, 2-, and 3-day forecasts may lead to definite action by cognizant personnel. There are three levels of action which can be taken. In each case cognizant project personnel are advised of the pending activity. In the case of a forecast of high solar activity (with the expectation of a proton event), cognizant personnel are put on a 24-h alert. During this time, contact is maintained with SDFC via telephone to evaluate the solar activity. The forecast of high solar activity and possible proton events is based on changes in size and brightness of the active region, the past history of the region, and the magnetic complexity of the associated sunspots. Moderate activity with low expectation of proton events would be another possible forecast. This prediction would involve the existence of active regions of size, brightness, and magnetic complexity different from those regions producing proton events. In this case, through special arrangement with SDFC, cognizant personnel are informed of any changes in the active regions which might produce a proton event. If the activity increases significantly, the status of the alert would be the same as that employed during the high solar activity. For low activity, where the active regions

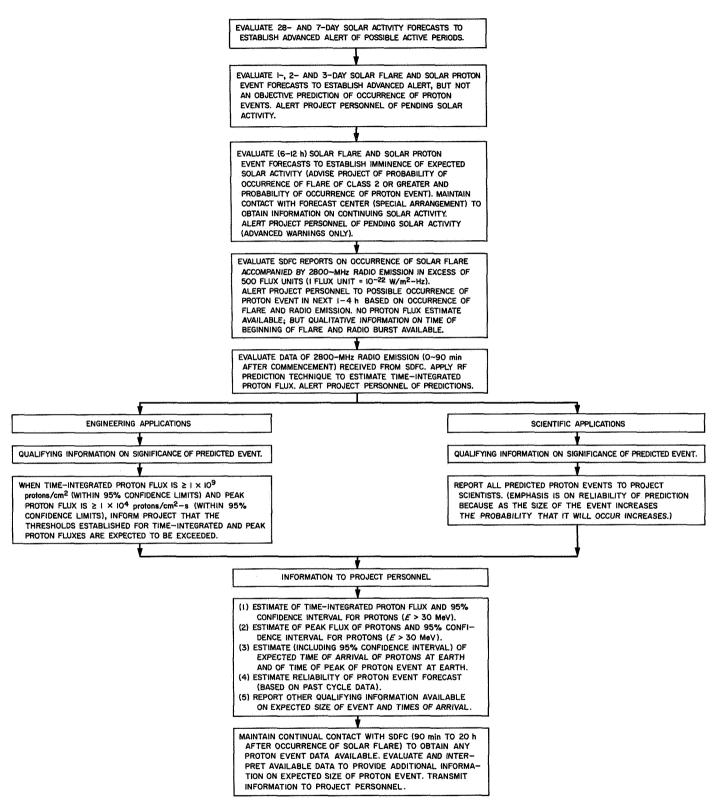


Fig. 21. Operational procedure for forecasting solar proton events used for Mariner V Venus encounter, October 19, 1967

are very small or declining rapidly and no activity is expected, cognizant personnel will use TWX to follow the situation. However, the special arrangement with SDFC will be used in the event of changes in the situation.

The next level in the forecast procedure is the actual occurrence of a radio event with an increase in the radio flux of 500 units above the background level. Normally, radio events occur at times of predicted high solar activity and cognizant personnel will be available to receive the radio data in real-time. Problems may arise causing a delay in the transmission of radio data. However, as soon as the commencement of the radio burst is reported, the following information may be reported to the appropriate mission operations support personnel:

- (1) Confirmation of the radio burst and the expected proton event, with supporting qualitative information as to the expected size of the proton event and other characteristics of solar activity.
- (2) Time of beginning of the radio burst.
- (3) Related statistical information on RF burst and proton event delay times (Table 4).

When additional RF data reported are sufficient to make the estimates of the time-integrated proton flux, the following information may be reported to cognizant project personnel.

- (1) Estimate of the time-integrated proton flux and the associated 95% confidence limits for protons of energies greater than 30 MeV.
- (2) Estimate of the peak proton flux and the associated 95% confidence limits for protons of energies greater than 30 MeV.
- (3) Estimate as to whether the time-integrated proton flux within the 95% confidence limits exceeds  $1 \times 10^9$ protons/cm<sup>2</sup> and/or the peak flux within the 95% confidence limits exceeds  $1 \times 10^4$  protons/cm<sup>2</sup>-s.
- (4) The probability of false alarms occurring for the predicted time-integrated proton flux.
- (5) Estimate as to whether the event is expected to affect the operation of spacecraft subsystems.
- (6) Time of termination of the radio event.

When the data reported are not sufficient to make a prediction of the proton time-integrated flux, this fact is reported to cognizant project personnel with qualifying information. Any additional information or data (e.g., spacecraft or ground-based measurements) received from SDFC on actual proton fluxes will be evaluated and included in the forecast to cognizant project personnel.

### F. Solar Forecast System and Forecast Procedures Used During Mariner V Mission

The forecast procedures established for the *Mariner V* encounter sequence were followed. But because the sun was very inactive during the several months before and during encounter, only the network services consisting of daily routine TWX's and reports of very-low-energy particle events were used. One solar proton event was forecast and was evaluated as follows:

Data were transmitted for a small event which occurred from 2359 to 0050 UT on August 18-19, 1967, after the radio flux exceeded the initial criteria of 500 flux units. At 0105 UT (August 19) the JPL answering service received notification of the radio event in the form of a peak flux and preburst level. At 0236 UT the IPL answering service received preburst levels and 5 data points spaced about 10 min apart. The burst was small and indicated an energy of about 50-100 (10<sup>-18</sup> J/m<sup>2</sup>-Hz), giving a time-integrated flux estimate  $7.5 \times 10^6$  protons/cm<sup>2</sup> for  $75 (10^{-18} \text{ J/m}^2\text{-Hz})$ . The proton flux estimate and 95% confidence interval of  $1.5 \times 10^6$  to  $4 \times 10^7$  protons/cm<sup>2</sup> was reported to the Mariner V cognizant project personnel as information only to complete the alert cycle because the threshold limit established on time-integrated proton flux was not exceeded. No proton event was reported as of August 21, 1967, 2235 UT.

### **VI.** Conclusions

The forecast system and operational procedures based on statistical analyses of past solar cycle data allow timely and reasonably reliable predictions of proton events and their sizes on a real-time basis. The solar forecast system was established to alert both engineering and scientific personnel in mission operations of pending solar activity. The RF prediction techniques provide estimates of the time-integrated proton flux, and when the scientific or engineering requirements are met, the forecasts are reported to the project for use in decisions concerning the mode of operation of the spacecraft and priorities for spacecraft tracking and scientific data collection.

SDFC and the network of solar observatories provided the information and data necessary to make the solar proton event forecasts. The time delay between recording the radio burst at the observatory and reception of the information at JPL is about 15 to 20 min. The prediction techniques are readily applied during the burst and after all the data are received. A delay of only a few minutes occurs in transmitting the subsequent forecast and recommendations to the project. After the occurrence of a radio event the prediction techniques developed provide forecasts of time-integrated proton fluxes from 15 min to 3.5 h before the arrival of protons at earth and at least 3 h before the peak proton flux reaches earth.

The operational procedures followed during the period of Venus encounter (October 19, 1967) were applied, but since the sun was quite inactive only minimum alert conditions were imposed. The procedures consisted of monitoring the SDFC daily TWX's and making a report to the project of the inactivity of the sun as required.

Of the single-parameter correlations made, the highest correlation coefficient was obtained by correlating the 2800-MHz burst energy with time-integrated proton flux. The correlation of the 2800-MHz peak radio flux with time-integrated proton flux also proved useful as a preliminary predictor. It is more timely, but it is not as reliable as the radio energy as a predictor. More complete analyses were performed using single-parameter correlations than were performed using multiple-parameter correlations because the latter did not significantly improve the results. However, as more data become available, a multiple correlation and regression study may produce a more timely and reliable predictor.

The reliability analysis of the prediction techniques was limited by lack of data from the last cycle. Facilities for acquiring the data, however, have been expanded by NASA owing to the Apollo effort, and as solar radio and proton events occur in the present cycle it may be possible to obtain better resolution in the false alarm and miss frequency predictions.

Forecasts of the occurrence of proton events can be verified and the forecasts of their magnitude may be continually refined by using available real-time proton data obtained from satellite sensors, neutron monitors, and indirectly measured data (mainly riometer absorption) taken during the early phase of the event (Ref. 15). Real-time data from the ground-based system including neutron monitors and riometer stations may be available in the future through SDFC, starting on a trial basis in early 1968. A more rigorous study of the propagation of protons in space is required in order to make accurate predictions of the environment at the position of the spacecraft in interplanetary space.

### VII. Recommendations

The solar forecast system developed for the *Mariner V* Mission should be implemented with appropriate modifications for interplanetary missions in the time span 1968– 1971. The recommended modifications are described below:

- (1) A new data compilation should be made and additional statistical analyses should be performed to improve the existing correlation and false alarm probabilities.
- (2) Statistical analyses of radio burst data and correlations of radio burst data with proton flux data should be performed at 2800 MHz and other frequencies. These analyses should include both single frequencies and combinations of frequencies. Also, other solar parameters should be statistically studied.
- (3) Forecast reliability analyses should be performed to include all known factors which influence reliability.
- (4) Techniques using available real-time proton data in combination with the RF techniques to predict both time-integrated and peak proton fluxes should be studied.
- (5) The propagation of particles in interplanetary space should be analyzed, with consideration given to the location of the flare on the sun's disk and transport of particles to the spacecraft.
- (6) Facilities for receiving and analyzing data from SDFC should be automated to ensure a more effective system.

# Appendix A

### **Flare Classification**

Flare class or importance is assigned in accordance with established scales. In the past, classification was based on the corrected area of the flare at the time of maximum brightness. Currently, a dual scale incorporating both area and intensity is used. The two systems are contrasted in Table A-1.

Corrected area, solar hemisphere × 10 <sup>-6</sup>	Old system	New system <sup>b</sup>		
< 100	1-	Sf	Sn	Sb
100-250	1,1+*	1f	1n	1.6
250-600	2, 2+ª	2f	2n	2b
600-1200	3	3f	3л	Зb
> 1200	3+	4f	4n	46

Table A-1. Flare class or importance

# Appendix B Calculation of Area of Radio Burst Profile

The numerical integration to obtain RF burst energy is performed by taking five points on the curve (Fig. B-1), the last point in each calculation being the same as the first point in the next calculation.

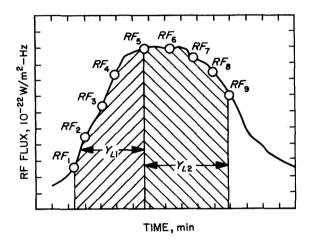


Fig. B-1. Partial areas under radio burst profile used in numerical integration technique to evaluate RF energy

The following quantities are defined:

 $H = 4.0 \times (\text{time interval between values of RF flux in seconds})$   $RF_i = i\text{th value of radio flux in units of 10<sup>-22</sup>W/m<sup>2</sup>-Hz}$   $X_1 = 7.0 \times (H) \times (RF_1) \times 10^{-4}$   $X_2 = 32.0 \times (H) \times (RF_2) \times 10^{-4}$   $X_3 = 12.0 \times (H) \times (RF_3) \times 10^{-4}$   $X_4 = 32.0 \times (H) \times (RF_4) \times 10^{-4}$   $X_5 = 7.0 \times (H) \times (RF_5) \times 10^{-4}$  $Y_{L1} = (X_1 + X_2 + X_3 + X_4 + X_5)/90$ 

 $(Y_{L1}$  represents the partial area under the curve in units of  $10^{-18}$  J/m<sup>2</sup>-Hz)

The next partial area is found in the same manner, and the calculation is repeated until the entire area under the curve is covered.

The area of the curve of interest is chosen in the following way: A flux value which is 10% of the peak value of the curve is selected as indicated on Fig. 20. The  $RF_1$  value is selected at the intersection of the 10% line and the curve. Subsequent RF values are then selected at an equal time interval along the curve for use in the numerical integration technique. The area computed will include an excess area as shown in Fig. 20. This area must be subtracted from the numerically computed area to obtain the area above the 10% line.

# Glossary

Flare	a sudden increase in solar radiation which may fall in the X-ray, UV, or radio parts of the spectrum, but generally is in the visible part.		
Flare class or importance	determined by flare area and intensity (see Appendix A).		
OGO	Orbiting Geophysical Observatory.		
OSO	Orbiting Solar Observatory.		
Peak	peak flux of solar radio event, $10^{-22}$ W/m <sup>2</sup> -Hz.		
PF	solar proton event time-integrated flux for energies greater than 30 MeV.		
Plage	a bright area in the chromosphere of the sun.		
Plage area	area of sun's disk, covered by a plage, solar disk $ imes 10^{-6}.$		
Plage brightness	optical intensity of brightest part of plage, on a scale of 1 to 5.		
RF	solar radio frequency burst emission at the time of a flare.		
RFE	solar radio frequency burst emission energy, $10^{-18}$ J/m <sup>2</sup> -Hz		
SDFC	Space Disturbance Forecast Center.		
SOFNET	Solar Observatories' Forecast Network.		
Solar proton event	solar proton emission at the time (within several hours) and from the region of a flare.		
Solar radio event	solar radio emission at the time (within several minutes) and from the region of a flare.		
Sunspot	small region in the photosphere of the sun which is darker than the surrounding area.		
Sunspot area	area of a sunspot, solar disk $\times$ 10 <sup>-6</sup> . (When it is correlated with a solar proton event the area represented is that of the sunspots associated with the active region producing the proton event.)		
$S_x$	estimated standard deviation of radio burst energy of $x$ actual events from the average event energy.		
$S_{yx}$	estimated standard deviation of predicted flux of $y$ proton event using $x$ radio event from actual flux of proton event.		
Type IVµ radio emission	radio emission in the microwave region (from the solar at- mosphere) at the time of a solar flare believed to be electron- induced synchrotron radiation.		
. <b>X</b> .	$\log_{10}$ of radio energies at which confidence limits were computed.		
$ar{x}$	log <sub>10</sub> of average radio energy.		

 $X_i$  log<sub>10</sub> of the radio energies of selected events.

### Glossary (contd)

- $Y'_i$  log<sub>10</sub> of predicted estimate of integrated proton flux from a regression equation relating proton flux and radio burst energy.
- $Y_i$  log<sub>10</sub> of observed proton flux of the selected events.

### References

- 1. Anspaugh, B. E., *High Energy Proton Testing of Mariner IV Components*, Technical Memorandum 33-314, Jet Propulsion Laboratory, Pasadena, Calif., Jan. 1, 1967.
- Smith, H. J., and Smith, E. V. P., Solar Flares, The MacMillan Co., New York, 1963.
- 3. Webber, W. R., Sunspot Number and Solar Cosmic Ray Predictions for Cycle 20 (1965–1975) with Preliminary Estimates for Cycle 21, Report D2-113522-1, The Boeing Co., Seattle, Wash., 1967.
- Yule, G. U., "On a Method of Investigating Periodicities in Disturbed Series, with Special Reference to Wolfer's Sunspot Numbers," *Phil. Trans.*, Vol. 226, Royal Society of London, 1926.
- Wild, J. P., "The Radio Emission from Solar Flares," J. Phys. Soc. Japan, Vol. 17, Supplement A-11, pp. 249–258, 1962; International Conference on Cosmic Rays and the Earth Storms, Sept. 1961.
- Fletcher, J. D., "Solar Radio Emission as a Criterion for Solar Proton Event Warning," AIAA J., Vol. 2, p. 2193, 1964.
- 7. Kundu, M. R., Solar Radio Astronomy, Interscience Publishers, New York, 1965.
- Maxwell, A., Defouw, R. J., and Cummings, P., "Radio Evidence for Solar Corpuscular Emission," *Planet. Space Sci.*, Vol. 12, pp. 435–449, 1964.
- Takakura, T., and Ono, M., "Yearly Variation in Activities of Outbursts of Microwaves and Flares During a Solar Cycle with Special Reference to Unusual Cosmic Ray Increases," J. Phys. Soc. Japan, Vol. 17, Supplement A-11, pp. 207-210, 1962, International Conference on Cosmic Rays and the Earth Storms, Sept. 1961.
- "Estimates of Proton Fluxes Expected In the Solar Flare Radiation Environment During Mariner Mars 1969 Missions," in *The Planetary-Interplanetary Program*, Space Programs Summary 37-41, Vol. II, pp. 32–39. Jet Propulsion Laboratory, Pasadena, Calif., Sept. 30, 1966 (Confidential).
- 11. Webber, W. R., An Evaluation of the Radiation Hazard Due to Solar Particle Events, Report D2-90469, The Boeing Co., Seattle, Wash., 1963.
- Higgins, P. W., Operational Procedures for Apollo Dose Radiation, NASA SP-71, Second Symposium on Protection Against Radiations in Space, 12–14 October 1964, pp. 151–156.

### **References** (contd)

- 13. Solar Proton Manual, Edited by F. B. McDonald, NASA TR R-169, Washington, Dec. 1963.
- 14. Dixon, W. J., and Massey, F. J., Jr., Introduction to Statistical Analysis, McGraw-Hill, New York, 1957.
- 15. Webber, W. R., An Evaluation of Solar Cosmic Ray Events During Solar Minimum, Report D2-84274-1, The Boeing Co., Seattle, Wash., 1966.