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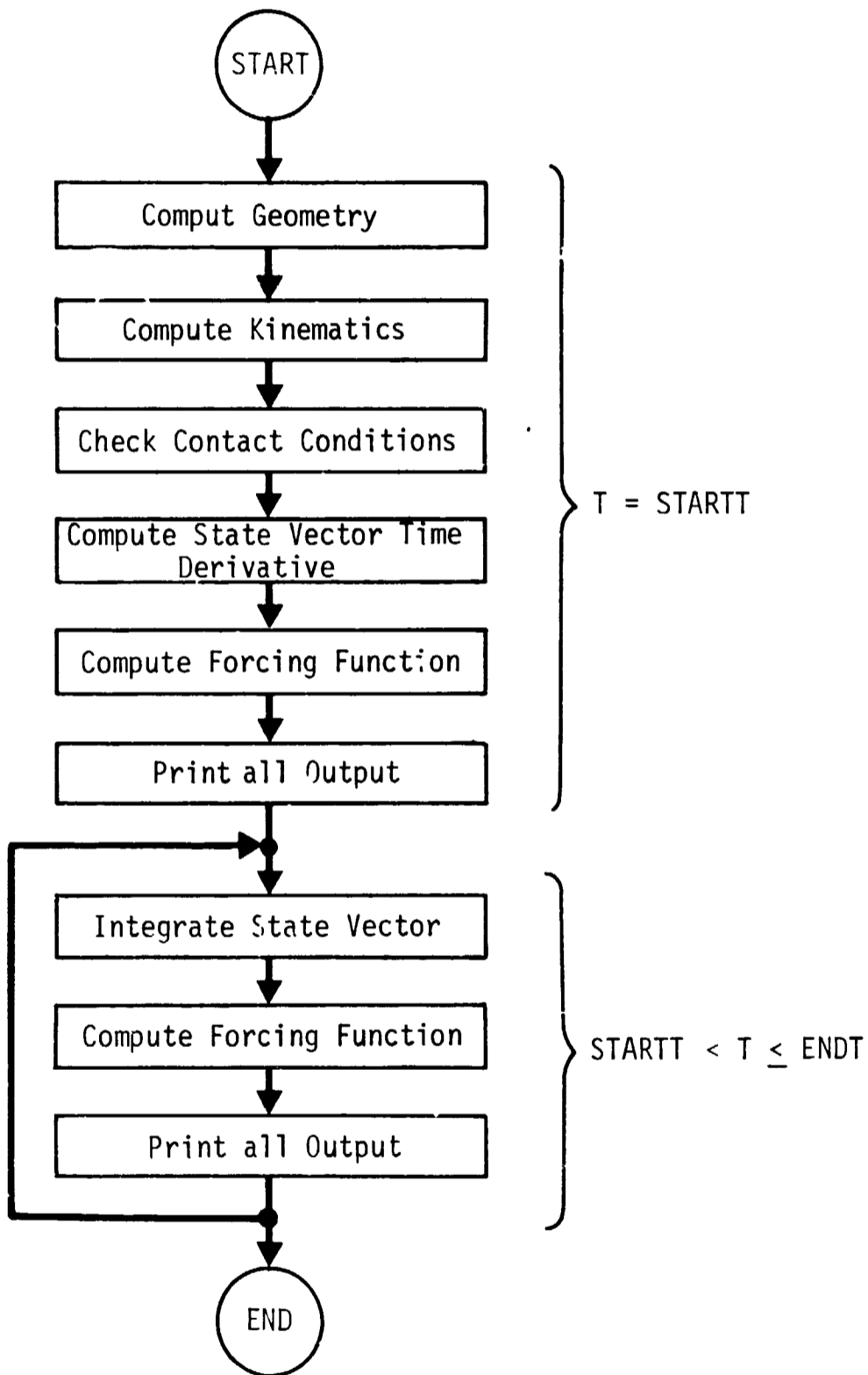


Fig. III-7 PROGRAM TIMHST Logic Flow

4. OVERLAY (3,0) PROGRAM PLOTTER

The final overlay (Fig. III-8) is only called if the optional plot indicator so specifies. If it is called it reads plot titles from tape, reads the plot variable time histories from tape, and plots those time histories that have been previously specified. (Fig. III-9).

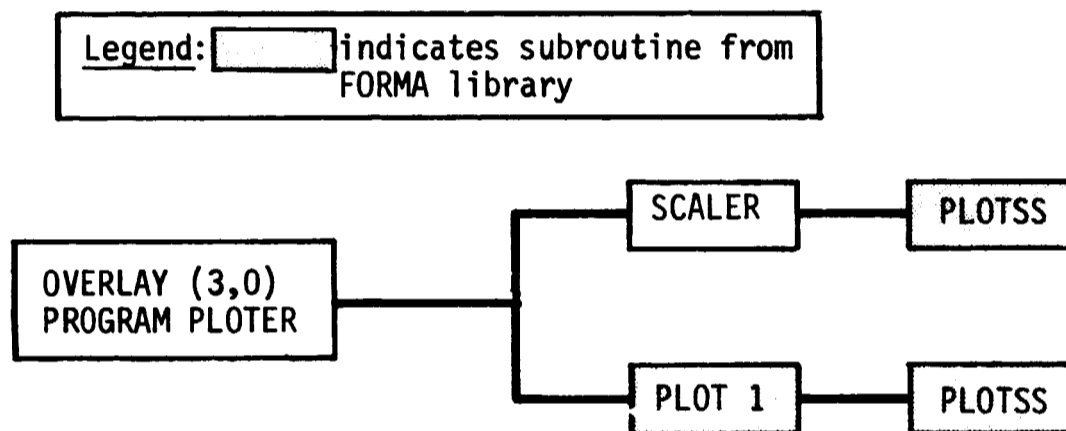


Fig. III-8. PROGRAM PLOTTER Calling Structure

C. PROGRAM INPUT DATA

The main program overlay, DOCK00, reads the initial program data. These data consist of three cards that are actually read by Subroutine START. This subroutine is from the FORMA library (Ref III-1). The first card sets a program run number (RUNNO); the second and third cards are used as title cards. The user may here indicate any comments applicable to the particular run.

The next card reads four integer variables with a 16I5 format. These variables are:

- | | |
|--------|---|
| MINIC | = 0 if intend to read entire state vector (e.g., continuing the simulation from a previous run) |
| | = 1 if desire to read 6x3 array of minimum initial conditions |
| IFPLOT | = 0 if no time history plot output is desired |
| | = 1 if plot output is desired. It will be necessary to insert (in the proper location) as many plot title cards as desired plots. |

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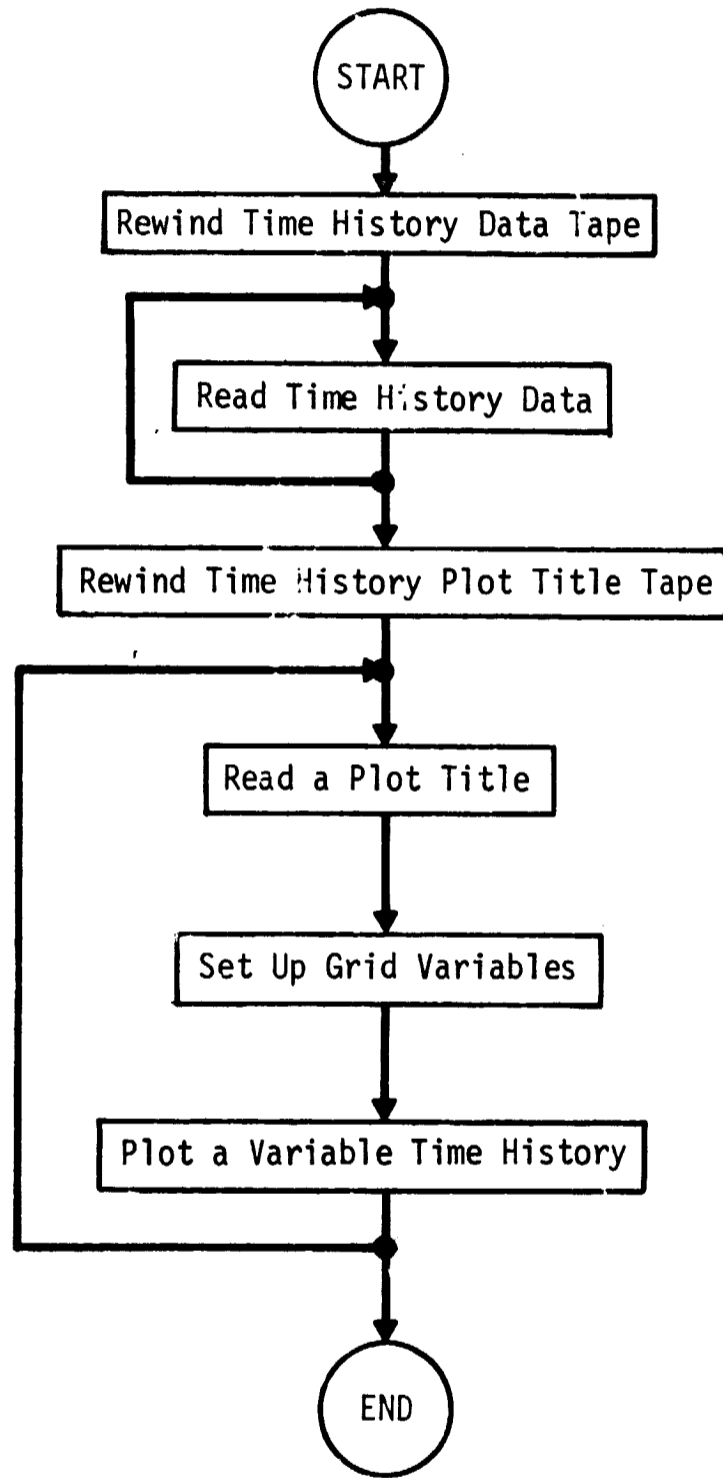


Fig. III-9. PROGRAM PLOTTER Logic Flow

IFPER = 0 if no prespective or stereo pairs plots are desired
 = 1 if perspective plots are desired
 = 2 if stereo pairs plots are desired

IFPNCH = 0 if do not want to punch state vector at end of simulation
 = 1 if desire to punch state vector at end of simulation (e.g., want to read state vector in as initial conditions for next run)

The next card reads two integer variables with a 16I5 format:

NCNSYS the number of control system parameters (34 in the present version of the program)

NFORCS the number of control system forces (10 in the present version)

The next card reads the simulation time variables and certain plot variables with an 8E10.0 format:

STARTT start time for the simulation

DELTAT time increment for numerical integration

ENDT end time for the simulation

XDLTA indicator for abscissa division on output plots. The total abscissa will be XDLTA x NXPL x 10 wide. The variable NXPL is read individually for each plot on the appropriate title card.

XPRNT print interval indicator. Program will print every XPRNT interval.

The next four cards read required program input scalars with an 8E10.0 format. Refer to Appendix A for a description of these data.

AA	2.25	probe geometry
AB	0.85	probe geometry
AD	0.708	probe geometry
AE	0.965	probe geometry
AF	3.085	probe geometry
AP	4.25	probe geometry

DLB	14.48	probe geometry
DLD	12.90	probe geometry
DLE	17.59	probe geometry
DLF	4.75	probe geometry
DLI	14.10	probe geometry
DLP	3.30	probe geometry
DLQ	16.53	probe geometry
DLS	2.055	probe geometry
FDO	11.5	probe geometry
PEO	10.5	probe geometry
ALPHAD	42.75	drogue cone half angle
CSPHER	2.58	radius of probe head
RADCON	13.56	radius of drogue cone
AKD1		retract force constant
AKD2		retract force constant
AKD3		retract force constant
RHOSO	2.08	stroke to open secondary orifice
FRETL	1000.0	limiting retract force
EXTL	11.12	probe extended length
TLAG		time lag for initiation of retract mode
TSTAR		capture time-program will compute if capture achieved during the run; if continuing a run where capture occurred during the previous simulation, must read in the correct value of capture time
HDMU		coefficient of friction for probe head on drogue
ARMMU		coefficient of friction for pitch arms on drogue
BINDMU		binding friction coefficient

The next three cards read the initial components of the vector from point T to point D in the T coordinate system (TDT0). These data are read by Subroutine READ (Ref III-1). The initial components of the vector from point C to point P in the C coordinate

system (CPCO) are read next. This array is followed by an array that reads the initial angular position (SIGMA) of the three pitch arms relative to the C coordinate system.

Vehicle inertia data are read next. Target vehicle mass and inertia is followed by chase vehicle mass and inertia. Mass is read by a scalar (AMT and AMC); the 3x3 inertia arrays (AIT and AIC) are read by Subroutine READ.

The next data read concerns probe stiffness and damping characteristics. There are eight of these arrays. They are, in order,

FSPROX	probe barrel load stroke curve
FDMROX	probe barrel damping-accounts for barrel friction
FSPALL	moment-rotation curve for probe loading
FDMALY	damping for probe rotation coordinates (y axis)
FSPALU	moment-rotation curve for probe unloading
FDMALZ	damping for probe rotation coordinates (z axis)
FSPATT	attenuator spring force curve-identical for three attenuators
FDMATT	attenuator damping curve-identical for three attenuators

Note that in setting up these arrays, the 1,1 element of each must be set to a floating point value one less than the number of columns in the array. The 2,1 element is a dummy value and is not used in the program.

With the exception of the first three data cards, the information read to this point has been read by PROGRAM SETUP, the first overlay. SETUP now calls Subroutine HSIG in order to read elastic data. HSIG initially reads five variables with a 3I5,2E10.0 format. These variables are:

IFELAS	= 0 no elastic properties to be read = 1 read elastic properties	
NMODET	number of TV modes	} not required if IFELAS = 0
NMODEC	number of CV modes	
ZETAT	TV modal damping (% critical)	
ZETAC	CV modal damping (% critical)	

If IFELAS = 1, the subroutine now reads the necessary modal data for the TV and then for the CV. Frequencies are read into a work space as are modal amplitudes. Subroutine REVISE, another FORMA subroutine, operates with three positioning vectors to take only those desired modes and store them in an array. The balance of the modal data is neglected.

Control now returns to SETUP and, depending on the value of MINIC established previously, two options are available:

- MINIC = 0 the complete state vector is read by READ. This option provides for a continuous series of runs; the output from one run is used as input to the next.
- 1 a 6x3 array of minimum initial conditions are read. These conditions have been previously detailed (Table II-1). These data are actually read by a call to Subroutine MINYS.

If the parameter IFPLOT was previously set to 1 it is now necessary to read a plot title card for each individual plot that is desired as output. This information will be written on a tape and therefore will be available when the plot overlay (PROGRAM PLOTTER) is called. The following information is required on each card. The format is (2I5,2X,I1,2X,2(A6,4X),4A10).

NCX	column indicator for abscissa variable. Refer to Subroutine SETPLT for location of individual variable in plot array.
NCY	column indicator for ordinate variable
NXPL	refer to description of XDLTA
XNAME	variable name for abscissa
YNAME	variable name for ordinate
PTITLE	plot title

A more detailed description of these data and the required format will be found under Subroutine PLOT (Ref III-1).

This concludes the data read by PROGRAM SETUP. The remainder of the data is read by Subroutines CONSYS and SETPER when they are called for the first time.

Subroutine CONSYS reads all data associated with the several control systems. This was done so that changes in control systems could be made without impacting the entire program. If it is desired to change the control laws it is necessary only to modify CONSYS and read new data. The basic program logic is unaltered although it might be necessary to read a new value for NCNSYS or NFORCS. Three data cards are required. The variables read here, using the 8E10.0 format, are:

FXCSM	CV axial thrust (400 lb in the current version)
AKRX	CMG roll channel gain
AKRY	CMG pitch channel gain
AKRZ	CMG yaw channel gain
AKDX	CMG roll channel gain
AKDY	CMG pitch channel gain
AKDZ	CMG yaw channel gain
OMFX	CMG roll channel filter break frequency
OMFY	CMG pitch channel filter break frequency
OMFZ	CMG yaw channel filter break frequency
ZETFX	CMG roll channel filter damping ratio
ZETFY	CMG pitch channel filter damping ratio
ZETFZ	CMG yaw channel filter damping ratio
AX	CMG roll channel transfer function gain
AY	CMG pitch channel transfer function gain
AZ	CMG yaw channel transfer function gain
BX	CMG roll channel time constant
BY	CMG pitch channel time constant
BZ	CMG yaw channel time constant
TLIM	total CMG torque limiting value

A detailed description of the CMG control system logic and definition of the input variables will be found in Appendix B. If the value of IFELAS is not equal to zero an array of modal slopes at the CMG sensor locations is now required. There must be as many modes here as target vehicle modes, NMODET. The input data for the TACS control system and the RCS control system is read as a 6x12 array CVEC by Subroutine READ. Definition of these data will be found in Appendix B of this volume and in Appendix A of Volume I.

The final data are required only if the variable IFPER is not equal to zero. This information is required for Subroutine SETPER which plots perspective or stereo pairs views of the probe and drogue. A complete description of required data will be found under the description of Subroutine PLOT3 (Ref III-1).

There is no further data required. When the simulation reaches ENDT, control returns to Subroutine START. The run is terminated with a STOP card.

Note that a consistent set of input units is used throughout this program. These units are

time in seconds
length in inches
mass in lb-sec²/in.
angle in degrees

A comprehensive summary of program input is detailed in Table III-1.

D. PROGRAM OUTPUT

A summary of PROGRAM DOCKEL output is presented in this section. Actual program output generated from the input listed in Appendix D will be found in Appendix E.

The output begins with a print of all data. Data that were read into the program by Subroutine READ is printed (by READ) immediately after they are read. Other data are printed just before the beginning of the numerical integration. The time history and other pertinent program output follows. This information is printed at every XPRNT interval during the course of the simulation. The following information is available at each print time:

SIMULATION TIME	Docking simulation time
Y(I) YDOT(I)	State vector and state vector time derivative
U - TARGET	Six velocity components for TV (See Equation II-143, Vol I)
X - TARGET	Three components of TV position vector in inertial space (see Equation II-135, Vol I)

TABLE III-1 . SUMMARY OF INPUT DATA

```

300 CALL START

1001 FORMAT (16I5)
1002 FORMAT (3I5, 2E10.0)
1003 FORMAT (2I5, 2X, I1, 2X, 2(A6,4X), 4A10)
1004 FORMAT (8E10.0)
2001 FORMAT (8A10)
2002 FORMAT (15,5X,6F10.0)
2003 FORMAT (PE10.C)

READ (NIT,1001) MINIC, IFPLOT, IFPER, IFPNCH

READ (NIT,1001) NCNSYS, NFORCS

READ (NIT,1004) STARTT, DELTAT, ENDT, XDLTA, XPRNT
READ (NIT,1004) AA, AB, AD, AE, AF, AP, DLB, OLD, DLE,
.         DLF, DLI, DLP, DLQ, DLS, FDO, PEO,
.         ALPHAD, CSPHER, RADCON, AKD1, AKO2, AKO3, RHOSO,
.         FRET, EXTL, TLAG, TSTAR, MDMU, ARHMU, BINOMU

CALL READ (TDT0 , N1, N2, 1, 3)

CALL READ (CPCC , N1, N2, 1, 3)

CALL READ (SIGMA , N1, N2, 1, 3)

READ (NIT,1004) AMT
CALL READ (AIT , N1, N2, 3, 3)

READ (NIT,1004) AMC
CALL READ (AIC , N1, N2, 3, 3)

DO 15 I = 1, 4
CALL READ (FSPRNG(1,1,I), N1, N2, 2, KTABLE)
CALL READ (FDAMP (1,1,I), N1, N2, 2, KTABLE)
15 CONTINUE

READ (NIT,1002) IFELAS, NMODET, NMODEC, ZETAT, ZETAC
IF (IFELAS .EQ. 0) GO TO 200
DO 100 L = 1, 2
CALL READ (VWORK , N), NCF, 1,100)
CALL READ (AWORK , NR, NC,100,100)
CALL READIM (JVEC , N), NC1, 1,100)
CALL READIM (IVEC , N), NC1, 1,100)
CALL READIM (IVEC , N), NC1, 1,100)
100 CONTINUE
200 CONTINUE

IF (MINIC .EQ. 0) CALL READ (Y , N1, N2, 1,100)
IF (MINIC .EQ. 1) CALL READ (DATIN, 6, 3, 6, 3)

IF (IFPLOT .EQ. 0) GO TO 90
180 READ (NIT,1003) NCX, NCY, NXPL, XNAME, YNAME, PTITLE
IF (NCX .NE. 0) GO TO 180
90 CONTINUE

READ (NIT,1004) FXCSH, AKPX, AKRY, AKRZ,
.         AKDX, AKDY, AKOZ, OMFY, OMFZ,

.         ZETFX, ZETFY, ZETFZ, AX, AY, AZ,
.         BX, BY, BZ, TLIM
IF (IFELAS .EQ. 0) GO TO 95
CALL READ (CMGSLP,6,NMODET,6,26)
95 CONTINUE
CALL READ ( CVFC,N1,N2, 6,12)

IF (IFPE4 .EQ. 0) GO TO 300
READ (NIT,2001) (PTITLE(I), I=1,8)
READ (NIT,2002) IFFIXD,RANGLE,EED,CANGLE
READ (NIT,2003) (CDELOC(I), I=1,3)
READ (NIT,2003) (VPLOC (I), I=1,3)

GO TO 300

```

GAMMA TARGET	Six direction cosines which orient TV body x and y axes with respect to inertial space (see Equation II-135, Vol I)
U - CHASE	Six velocity components for CV
X - CHASE	Three components of CV position vector in inertial space.
GAMMA CHASE	Six direction cosines which orient CV body x and y axes with respect to inertial space.
RHOS	Six parameters that characterize the deformation of the probe assembly (see Equation II-136, Vol I)
MODE VEL - TARGET	TV normal velocity coordinates
MODE DISP - TARGET	TV normal displacement coordinates
MODE VEL - CHASE	CV normal velocity coordinates
MODE DISP - CHASE	CV normal displacement coordinates
CON SYS PARAMETERS	Attitude control system parameters (see Appendix A, Vol I)
DSD VECTOR	x, y, z components of vector from D (apex of cone) to S (probe swivel point) in D coordinate system
PHI	Constraint displacement parameter (instantaneous distance between potential contact points) for each of 10 possible constraints (see Section II, Vol I)
LAMBDA	Constraint force for each of 10 possible constraints (see Section II, Vol I)
MODE	Constraint indicator; if zero constraint is "out", if unity the constraint is "in" (See Section II, Vol I)
RETRACT FORCE	Magnitude of retract force acting on probe barrel piston during the retract mode
BINDING FRICTION FORCE	Binding friction force acting on probe inner barrel.
FORCE AT PT D	Three components of force at apex of drogue cone
MOMENT AT PT D	Three components of moment at apex of drogue cone

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FORCE AT PT P	Three components of force at probe hard point
MOMENT AT PT P	Three components of moment at probe hard point
ELAPSED CP TIME	Total elapsed CDC 6400/6500 Central Processor time since beginning of run.

IV. CONCLUSIONS

This volume has presented the graphical output from a series of demonstration runs made with the digital computer program for docking simulation (DOCKEL). The results have a common denominator in that the several runs all considered a fixed orbital configuration. Also, the definition of the probe/drogue docking mechanism was held constant throughout as were the initial conditions. The intent was to demonstrate the overall versatility of the docking program and to present results that might indicate, in a qualitative way, the variations in response due to the inclusion of typical control systems, CV axial thrust, and elastic properties. A total of 12 cases were considered.

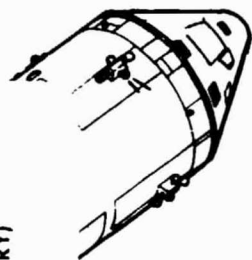
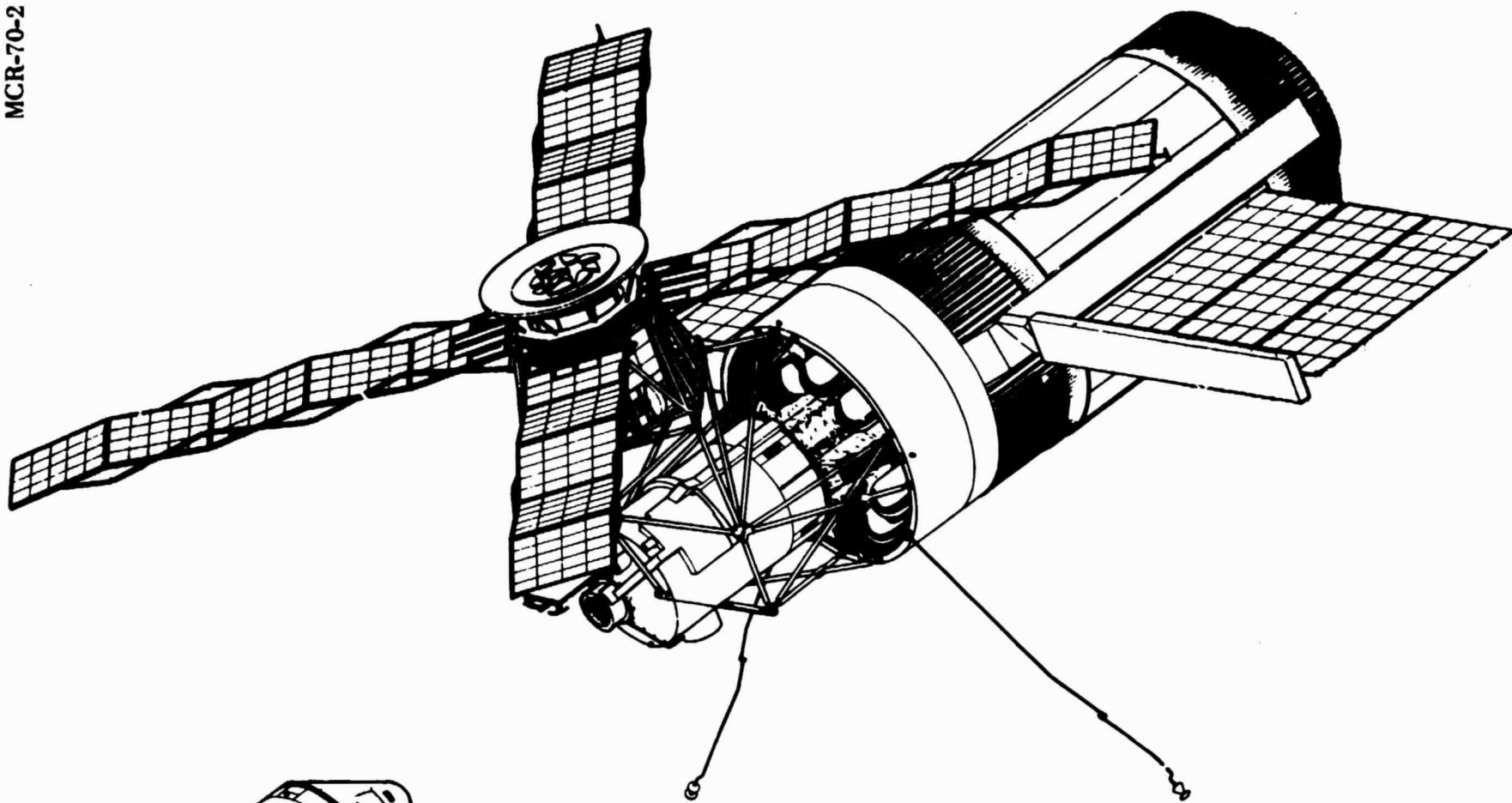
As the intent here was to demonstrate capability rather than provide a complete parametric study, conclusions drawn from these results must be limited to the particular configuration that was considered.

Chase vehicle axial thrust is required for successful probe capture. The effect of increasing thrust is to decrease time to capture while increasing postimpact velocities and loads. There appears to be no significant variation in probe deformation characteristics. The addition of a CMG attitude control system has little effect on probe deformation, capture success, and resulting loads. However, there is a sizable variation observed in postimpact rotational velocities. The CMG system appears to have a stabilizing effect, the degree of stabilization tends to increase with increasing CMG torque capability.

Addition of a TACS has a small effect on capture time, probe deformations, or vehicle rates. A slight increase in resultant forces can be noted as the magnitude of the TACS thruster output is increased. Increasing TACS capability tends to increase the stabilizing effectiveness of the system. The results for the case that considered a RCS show no great difference than the results for the case without this control system except that an RCS does have a tendency to correct the initial CV attitude error.

The most important conclusion to be drawn regarding the exclusion of vehicle elastic effects is that the resultant forces and moments acting on the TV are increased as elastic properties are deleted. Force peaks may be as much as 10% greater for the rigid case than for the case that assumed the TV to have all significant elastic modes with frequency less than 5 Hz. Conversely, the effect of omitting elastic properties is to radically decrease computer running time. The computer time required for the rigid case is only about 1/6 of that required for the case with 14 TV elastic modes.

Response of Flexible Space Vehicles to Docking Impact



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As all results were generated with the same vehicle and docking mechanism properties, no conclusions regarding variation in vehicle geometry, inertial properties, or probe mechanism characteristics can be established. A study of the effects on the docking response due to variations in these parameters would require a more extensive investigation than was possible here.

As has been mentioned previously, the intent of the numerical investigations conducted during the course of this study and presented in this volume was not to provide a complete parametric study for a particular configuration or class of configurations. Rather the intent was to provide an illustration of program capability and to illustrate the various available options, particularly those regarding control systems.

The program has, however, been formulated in a manner that lends itself to a parametric study. Care has been exercised in the formulation of the subroutines that read input data in order to make the actual data required a minimum. Likewise, the program output, particularly the time history plots, has been chosen to reflect that information most useful to the analyst.

V. REFERENCES

- III-1. FORMA (FORtran Matrix Analysis). Dynamics Memorandum 144. Martin Marietta Corporation, Denver Division, October 1969.
- A-1. Internal Letter to R. F. Nicholas from K. A. Bloom. North American Rockwell Space Division, November 15, 1968.
- A-2. Dwg DTT100340. North American Aviation, November 5, 1964.
- A-3. Verbal Communication, J. Barneburg, Manned Spacecraft Center, Houston, Texas.
- A-4. Letter 69MA2739 to H. Harcrow from C. F. DeWitt, North American Rockwell Space Division, March 6, 1969.

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APPENDIX A

DOCKING MECHANISM CHARACTERISTICS

This appendix presents a summary of several docking mechanism characteristics that are necessary program input data. A description of probe geometry, friction characteristics, probe preload calculations, attenuator and attachment structure force-deflection data, and retract mechanism characteristics are included.

A. GEOMETRY

Figure A-1 shows a line drawing of the docking probe. The geometry defined on this figure is delineated in Table A-1. The values, except where noted, are from Ref A-1.

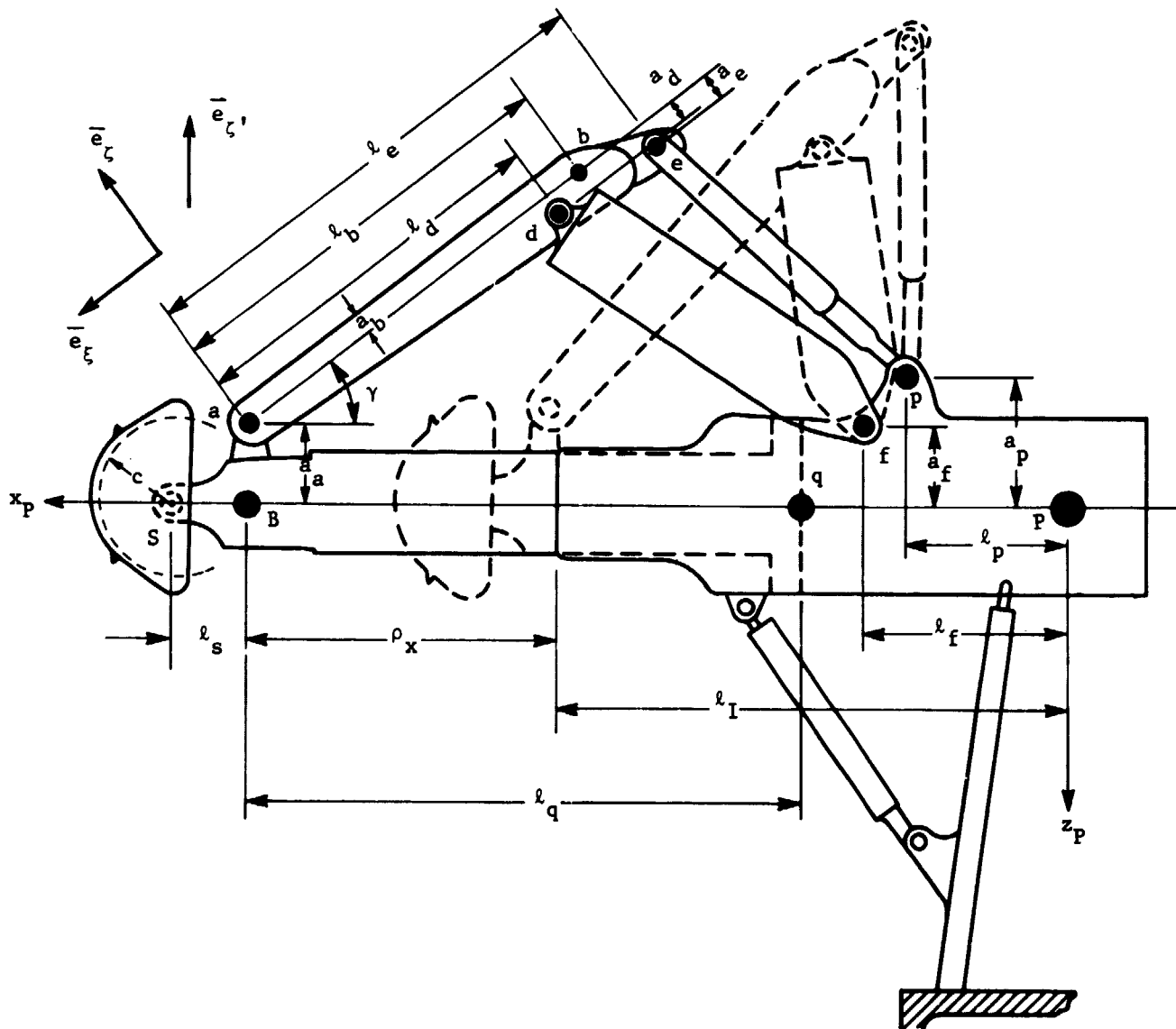


Fig. A-1 Probe Mechanism Geometry

Table A-1 Probe Geometry

$l_I = 14.10$ in.	$a_a = 2.25$ in.
$l_p = 3.30$ in.	$a_b^* = 0.85$ in.
$l_f = 4.75$ in.	$a_d^* = 0.708$ in.
$l_s = 2.055$ in.	$a_e^* = 0.965$ in.
$a_p = 4.25$ in.	$l_b^* = 14.48$ in.
$a_f = 3.085$ in.	$l_d = 12.90$ in.
	$l_e = 17.59$ in.
	$l_q = 16.53$ in.
	$c = 2.58$ in.
*Indicates value scaled from drawing, Ref A-2.	

Note that the analysis considers the probe head to be modeled as a sphere with a radius of 2.58 in. (Ref A-3).

B. BINDING FRICTION

A side load on the probe resulting from probe/drogue contact causes the probe motion to be influenced by a binding friction force. This force can be determined from a static representation of the probe and the pertinent forces, Fig. A-2.

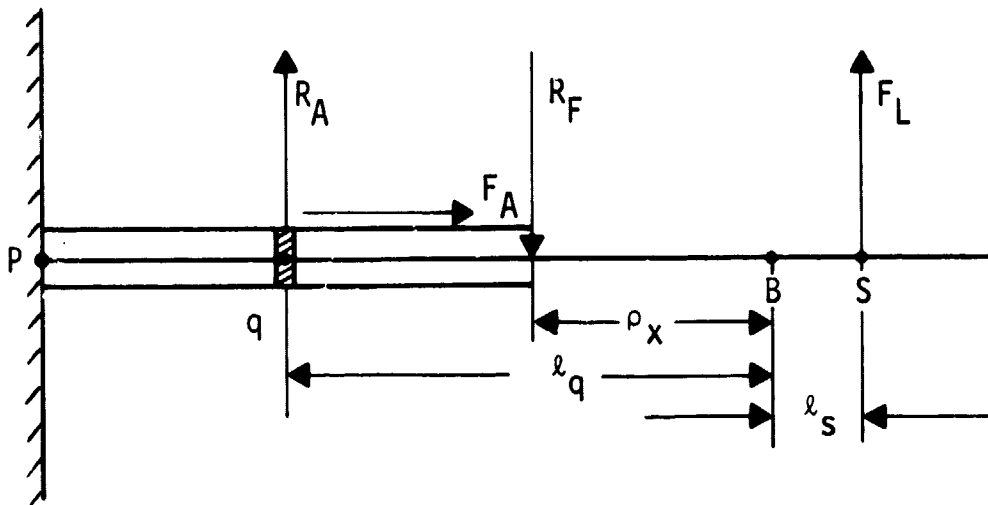


Fig. A-2 Binding Friction Model

From statics it follows that

$$F_L (\ell_q + \ell_s) = R_F (\ell_q - \rho_x)$$

$$R_A + F_L = R_F$$

$$R_F = F_L \left[\frac{\ell_q + \ell_s}{\ell_q - \rho_x} \right]; \quad R_A = F_L \left[\frac{\ell_q + \ell_s}{\ell_q - \rho_x} - 1 \right]$$

and the binding friction force is

$$F_A = \mu^* (R_F + R_A)$$

where μ^* is the binding friction coefficient. The ratio of forces

$$\frac{F_A}{F_L} = \mu^* \left[\frac{\ell_q + 2\ell_s + \rho_x}{\ell_q - \rho_x} \right]$$

can be written

$$\frac{F_A}{F_L} = \mu^*(T) f^*(\rho_x) = \mu(T) f(\rho_x)$$

where

$$\mu(T) \equiv f^*(\rho_{x_0}) \mu^*(T)$$

and is a function of temperature (T),

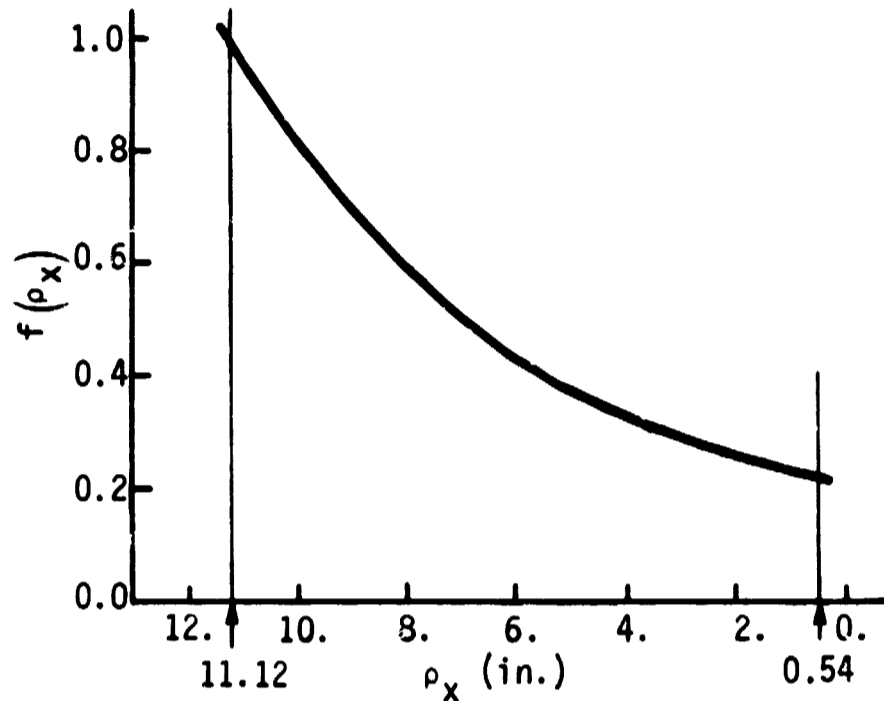
and

$$f(\rho_x) = f^*(\rho_x) / f^*(\rho_{x_0}).$$

Evaluation of $f(\rho_x)$ is presented in Table A-2 and shown in Fig. A-3. Values of $\mu(T)$ are given in Ref A-1.

Table A-2 Calculation of $f(\rho_x)$

ρ_x (in.)	$\ell_q + 2\ell_s + \rho_x$ (in.)	$\ell_q - \rho_x$ (in.)	$f^*(\rho_x)$	$f(\rho_x)$
11.12	31.77	5.41	5.87	1.0
9.	29.65	7.53	3.94	0.672
7.	27.65	9.53	2.902	0.495
5.	25.65	11.53	2.223	0.379
3.	23.65	13.53	1.747	0.298
1.	21.65	15.53	1.394	0.238
0.54	21.19	15.99	1.322	0.226

Fig. A-3 Graphical Representation of $f(\rho_x)$

C. ATTACHMENT STRUCTURE FORCE-DEFLECTION DATA

Probe attachment structure force-deflection data (moment versus angular deflection) is presented in Table A-3 and Fig. A-4. The data are from Ref A-4.

Table A-3 Attachment Structure Force-Deflection Data

Tip Deflection (in.)	Load (lb)	Unload (lb)	Angular Deflection (rad)	Load Moment (in.-lb)	Unload Moment (in.-lb)
0	0	0	0	0	0
0.2	230	150	0.00734	6,265	4,085
0.4	475	305	0.01468	12,940	8,310
0.6	715	450	0.02202	19,500	12,280
0.8	960	630	0.02936	26,170	17,180
1.0	1220	815	0.03670	33,220	22,200
1.2	1500	1040	0.04405	40,800	28,350
1.4	1800	1320	0.05135	49,100	36,000
1.6	2170	1725	0.05870	59,150	47,000
1.8	2650	2390	0.06605	72,300	65,150
1.93	3000	3000	0.07080	81,750	81,750

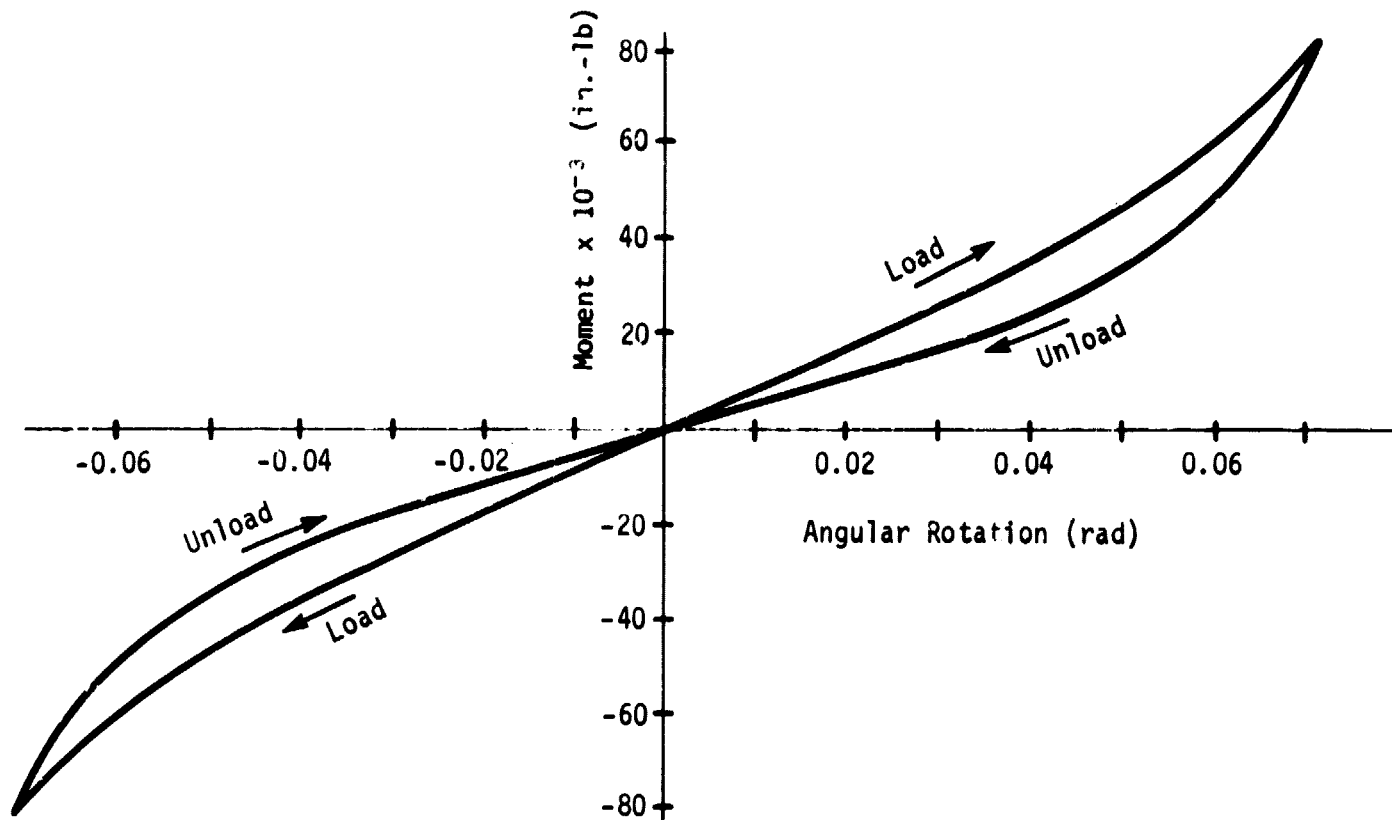


Fig. A-4 Graphical Representation of Attachment Structure Force - Deflection Data

D. PRELOAD BALANCE CALCULATION

When the probe is in the extended position, the three attenuator spring forces, the three tension link forces, and the probe extension spring force must be in static balance. These forces can be determined from the expression for virtual power:

$$\psi_B = F_B v_1^* + \sum_{j=1}^3 (F_{A_j} v_{j+3}^* + F_{T_j} v_{j+6}^*).$$

The velocities v_1 , v_{j+3} , and v_{j+6} , expressed in terms of $\dot{\rho}_x$, $\dot{\gamma}_1$, $\dot{\gamma}_2$, and $\dot{\gamma}_3$ are (refer to Vol I):

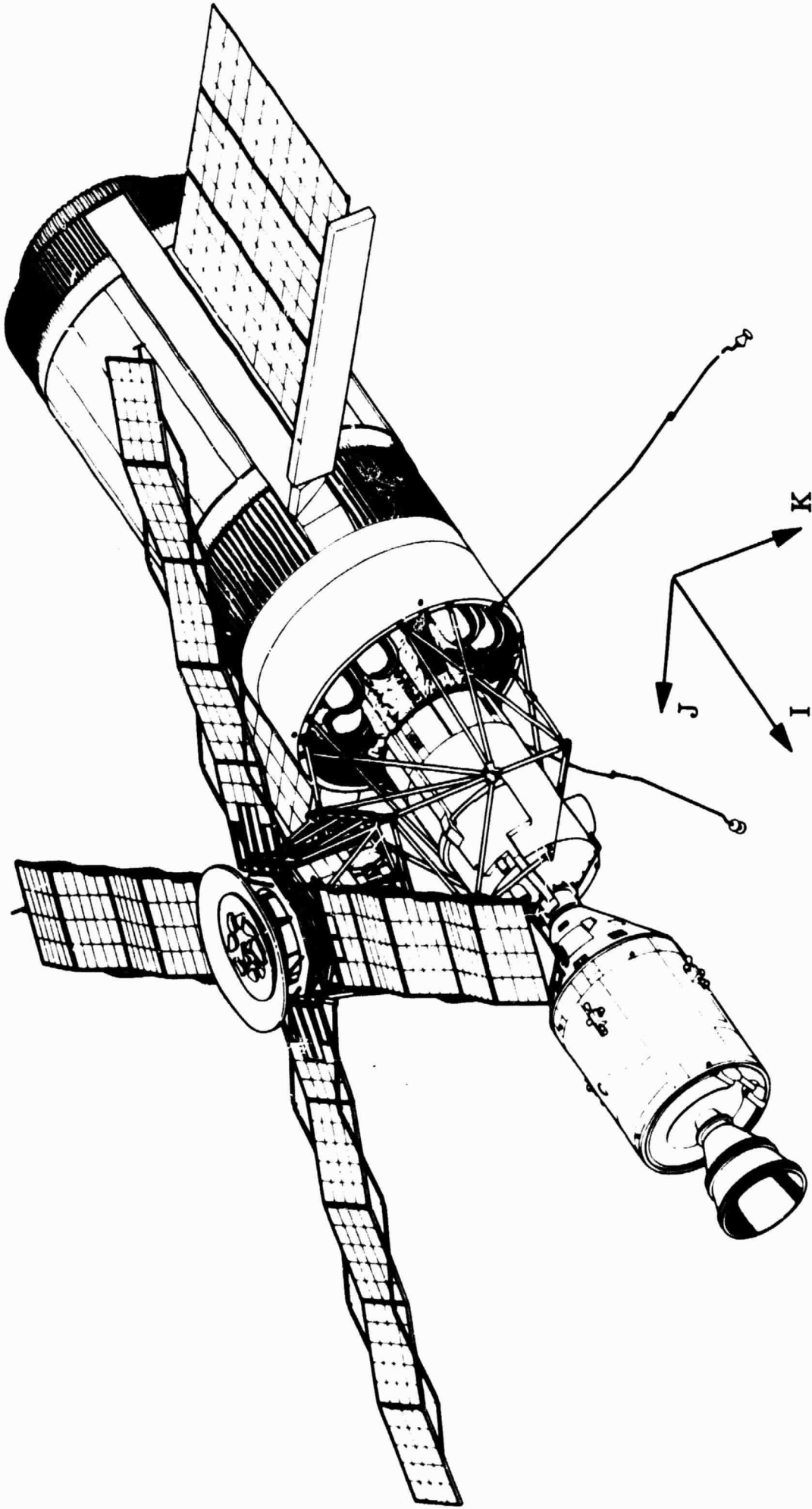


Fig. I-1 Baseline Configuration

$$\begin{pmatrix} v_1 \\ v_4 \\ v_5 \\ v_6 \\ v_7 \\ v_8 \\ v_9 \end{pmatrix} = \begin{bmatrix} 1 & & & & & & \\ f_1 & f_7 & & & & & \\ f_2 & & f_8 & & & & \\ f_3 & & & & f_9 & & \\ f_4 & f_{10} & & & & & \\ f_5 & & f_{11} & & & & \\ f_6 & & & & & & f_{12} \end{bmatrix} \begin{pmatrix} \dot{\rho}_x \\ \dot{\gamma}_1 \\ \dot{\gamma}_2 \\ \dot{\gamma}_3 \end{pmatrix}$$

It follows that

$$\psi_B = \begin{bmatrix} F_B & F_{A_1} & F_{A_2} & F_{A_3} & F_{T_1} & F_{T_2} & F_{T_3} \end{bmatrix} \begin{bmatrix} 1 & & & & & & \\ f_1 & f_7 & & & & & \\ f_2 & & f_8 & & & & \\ f_3 & & & & f_9 & & \\ f_4 & f_{10} & & & & & \\ f_5 & & f_{11} & & & & \\ f_6 & & & & & & f_{12} \end{bmatrix} \begin{pmatrix} \dot{\rho}_x^* \\ \dot{\gamma}_1^* \\ \dot{\gamma}_2^* \\ \dot{\gamma}_3^* \end{pmatrix}$$

Symmetry of the probe requires that

$$F_{A_1} = F_{A_2} = F_{A_3}, \quad F_{T_1} = F_{T_2} = F_{T_3},$$

$$\gamma_1 = \gamma_2 = \gamma_3, \quad \dot{\gamma}_1 = \dot{\gamma}_2 = \dot{\gamma}_3,$$

and therefore

$$\psi_B = \begin{bmatrix} F_B & F_{A_1} & F_{T_1} \end{bmatrix} \begin{bmatrix} 1 & & & & & & \\ (f_1 + f_2 + f_3) & (f_7 + f_8 + f_9) & & & & & \\ (f_4 + f_5 + f_6) & (f_{10} + f_{11} + f_{12}) & & & & & \end{bmatrix} \begin{pmatrix} \dot{\rho}_x^* \\ \dot{\gamma}_1^* \end{pmatrix}$$

The virtual power, expressed in another way, is

$$\psi_B = F_{\rho_x} \dot{\rho}_x^* + F_{\gamma_1} \dot{\gamma}_1^*$$

and the preload equilibrium equations are

$$\begin{Bmatrix} F_{\rho_x} \\ F_{\gamma_1} \end{Bmatrix} = \begin{bmatrix} 1 & (f_1 + f_2 + f_3) & (f_4 + f_5 + f_6) \\ & (f_7 + f_8 + f_9) & (f_{10} + f_{11} + f_{12}) \end{bmatrix} \begin{Bmatrix} F_B \\ F_{A_1} \\ F_{T_1} \end{Bmatrix} = \begin{Bmatrix} 0 \\ 0 \end{Bmatrix}.$$

Again, symmetry of the probe implies that

$$\begin{aligned} f_1 = f_2 = f_3, & \quad f_4 = f_5 = f_6 \\ f_7 = f_8 = f_9, & \quad f_{10} = f_{11} = f_{12} \end{aligned}$$

and the equilibrium equations reduce to

$$\begin{bmatrix} 1 & 3f_1 & 3f_4 \\ & 3f_7 & 3f_{10} \end{bmatrix} \begin{Bmatrix} F_B \\ F_{A_1} \\ F_{T_1} \end{Bmatrix} = \begin{Bmatrix} 0 \\ 0 \end{Bmatrix}.$$

The coefficients f_1, f_4, f_7, f_{10} can be calculated using known geometry. The notation used here is that of Volume I.

$$f_1 = \overline{fd} \cdot \overline{i_p} / |\overline{fd}|$$

$$\overline{fd} \cdot \overline{i_p} = l_I - l_f + \rho_x - l_d \cos \gamma - a_d \sin \gamma = 9.665$$

$$\overline{fd} \cdot \overline{j_p} = 0$$

$$\overline{fd} \cdot \overline{k_p} = a_f - a_a - l_d \sin \gamma + a_d \cos \gamma = -6.247$$

$$|\overline{fd}| = 11.508$$

$$f_1 = u_{Alx} = 0.84113, \quad u_{Aly} = 0., \quad u_{Alz} = -0.5437$$

$$f_7 = (l_d \sin \gamma - a_d \cos \gamma) u_{Alx} - (l_d \cos \gamma + a_d \sin \gamma) u_{Alz} = 11.8312$$

$$f_4 = \frac{\overline{pe} \cdot \overline{i}_p}{|\overline{pe}|}$$

$$\overline{pe} \cdot \overline{i}_p = l_I - l_p + \rho_x - l_e \cos\gamma - a_e \sin\gamma = 7.187$$

$$\overline{pe} \cdot \overline{j}_p = 0$$

$$\overline{pe} \cdot \overline{k}_p = a_p - a_a - l_e \sin\gamma + a_e \cos\gamma = -7.657$$

$$|\overline{pe}| = 10.5012$$

$$f_4 = -u_{T1x} = -0.6844, u_{T1y} = 0., u_{T1z} = -0.7292$$

$$f_{10} = -(l_e \sin\gamma - a_e \cos\gamma)u_{T1x} + (l_e \cos\gamma + a_e \sin\gamma)u_{T1z} = -17.683$$

Assuming now that the attenuator preload (Ref A-1) is

$$F_{A_1} = 65/2 = 32.5 \text{ lb}$$

yields $F_{T_1} = 21.8 \text{ lb}$ and $F_B = -37.2 \text{ lb}$.

E. EXTEND SPRING LOAD-DEFLECTION DATA

The data presented in Table A-4 and Fig. A-5 for the probe extend spring load-deflection are from Ref A-1.

Table A-4 Extend Spring Load-Deflection Data

Deflection (in.)	Load (lb)	ρ_x (in.)
15.	- 69.	11.12*
13.5	- 74.8	9.62
12.	- 81.	8.12
10.	- 89.3	6.12
9.	- 93.75	5.12
7.5	-101.	3.62
6.5	-106.2	2.62
5.5	-112.5	1.62
4.75	-118.	0.87
4.44	-121.	0.56
4.2	-125.	0.32
4.07	-130.	0.19

Note: 1. * indicates fully extended probe.
 2. $\rho_x = \delta - 3.88$ in.
 3. Bottoming spring constant $\equiv 40 \times 10^3$ lb/in.

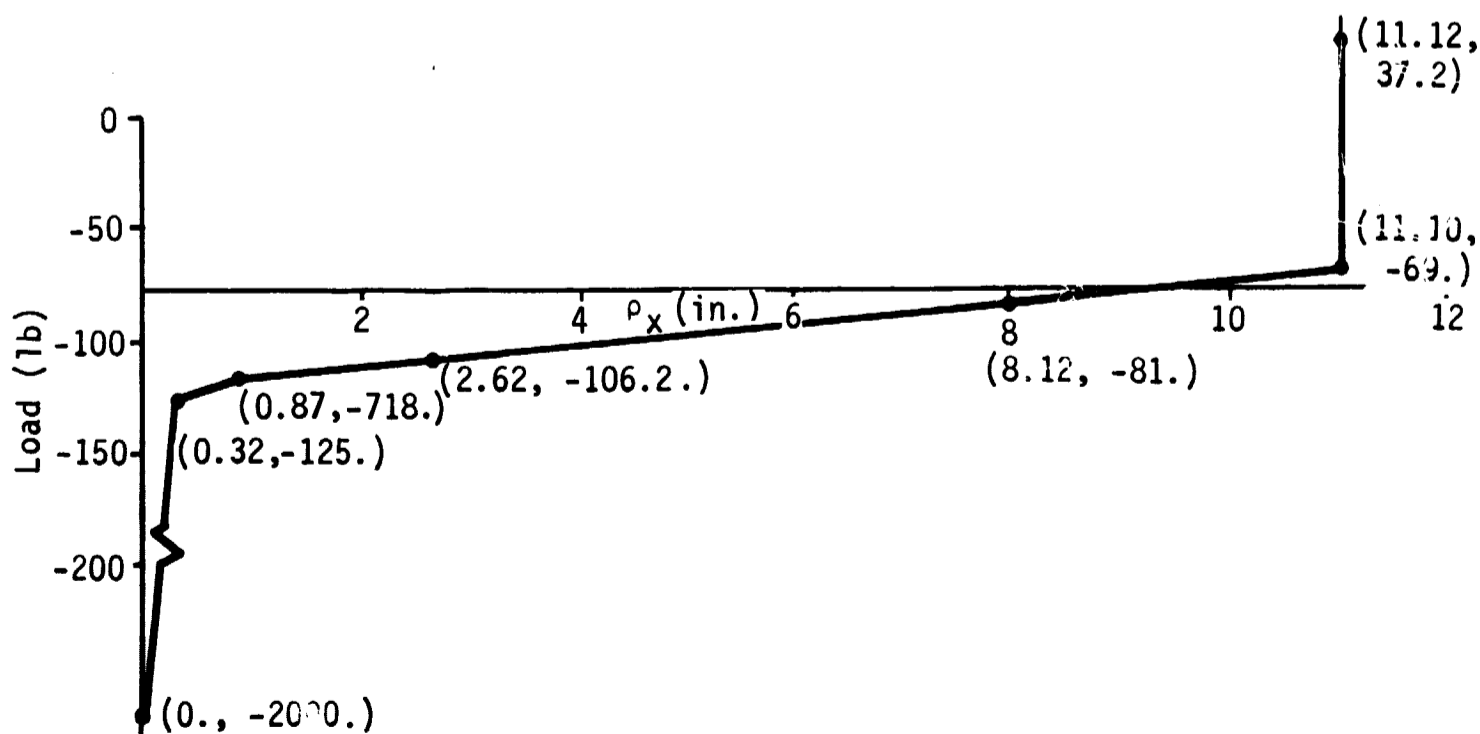


Fig. A-5 Graphical Representation of Extend Spring Load-Deflection Data

2. Target Vehicle

The TV coordinate system is defined in Fig. I-3. Vehicle inertial properties are shown in Table I-3. The elastic effects of this vehicle are considered through the inclusion of significant elastic modes with natural frequencies less than 5 Hz.

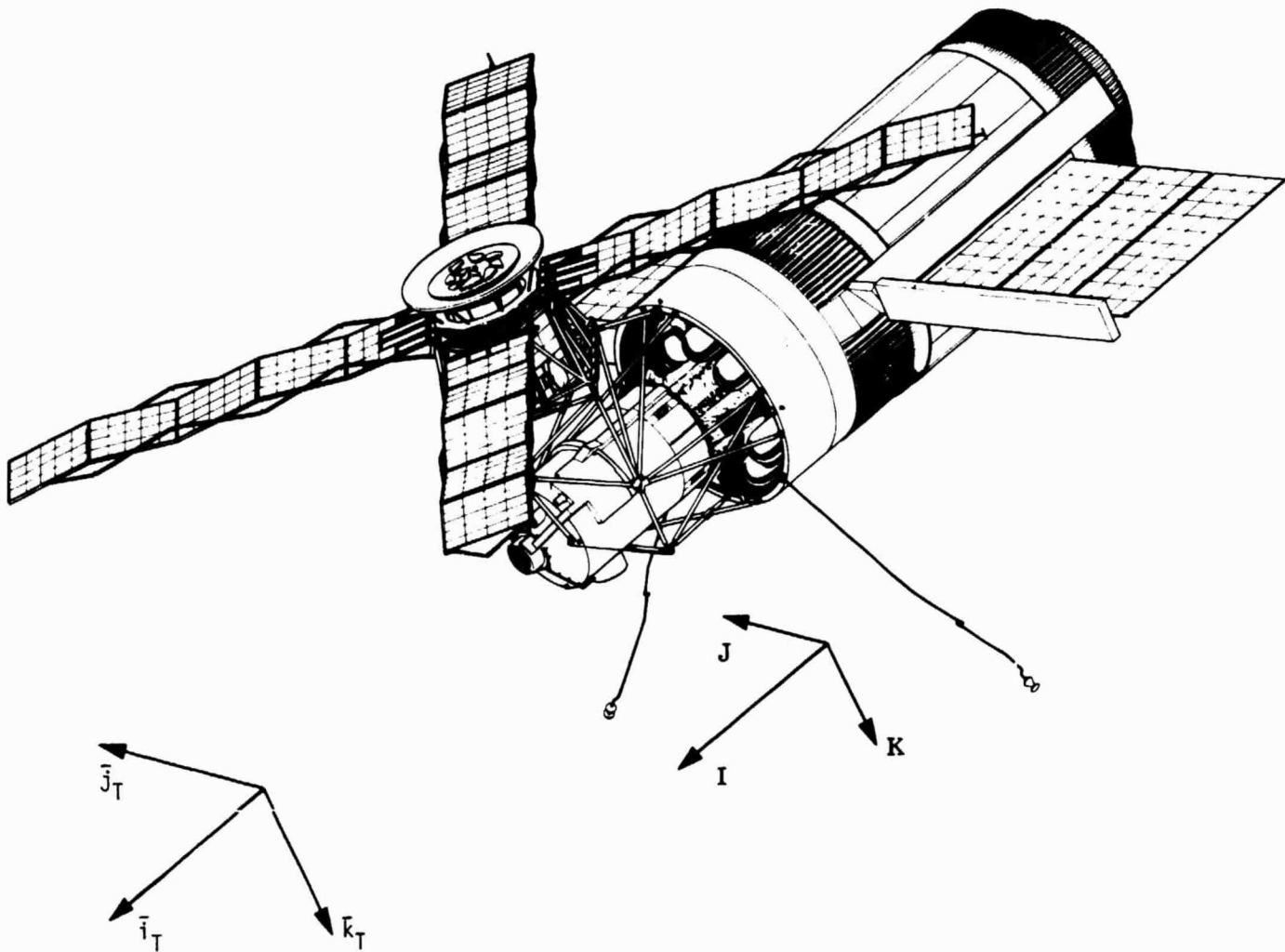


Fig. I-3 Target Vehicle Coordinate System

Table I-3 Target Vehicle Inertial Properties

M = 296.4 lb-sec ² /in.	
$I_{xx} = 6.428 \times 10^6$ lb-in.-sec ²	$I_{xy} = 1.622 \times 10^4$ lb-in.-sec ²
$I_{yy} = 2.474 \times 10^7$ lb-in.-sec ²	$I_{xz} = 3.528 \times 10^6$ lb-in.-sec ²
$I_{zz} = 2.512 \times 10^7$ lb-in.-sec ²	$I_{yz} = -1.575 \times 10^5$ lb-in.-sec ²

F. ATTENUATOR LOAD-STROKE DATA

The attenuator load-stroke data shown in Table A-5 is from Ref A-1. The data are shown graphically in Fig. A-6.

Table A-5 Attenuator Load-Stroke Data

Attenuator Deflection, δ_A (in.)	Load (lb)	Unload (lb)	Δ_A (in.)	Average Load (lb)
0	65	0	11.5	- 32.5
0.25	56	21	11.25	- 38.5
0.5	63	28	11.0	- 45.5
1.0	78	47	10.5	- 62.5
1.5	103	70	10.0	- 86.5
2.0	140	107	9.5	-123.5
2.5	203	167	9.0	-185.0
3.0	330	280	8.5	-305.0
3.07	360	360	8.43	-360.0

Note: $fd_0 = 11.5$, $\Delta_A = fd_0 - \delta_A$.

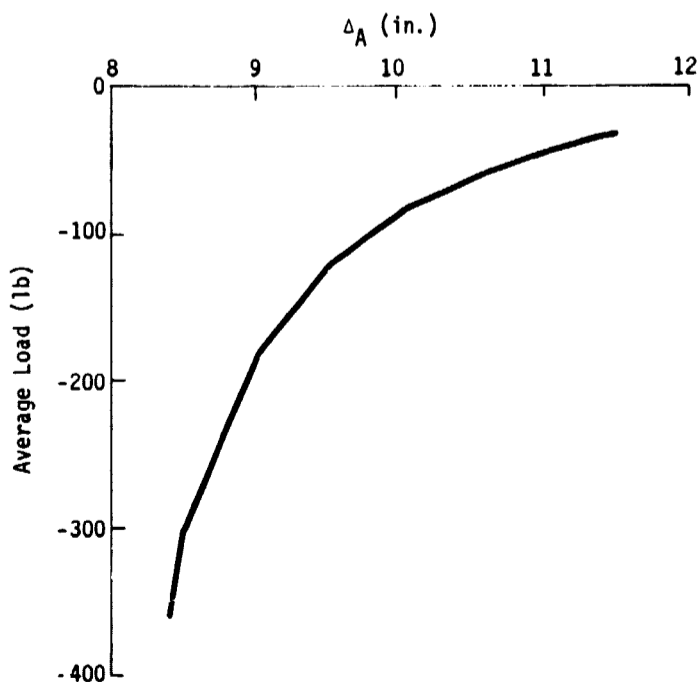


Fig. A-6 Graphical Representation of Attenuator Load-Stroke Data

G. ATTENUATOR DAMPING CHARACTERISTICS

The attenuator damping characteristics shown in Table A-6 are from Ref A-1.

Table A-6 Attenuator Damping Characteristics

Attenuator Velocity (in./sec)	Load (lb)		
	T = 70°F - 250°F	T = -65°F	T = -80°F
1.32	78	78	78
0.12	18	18	18
- 0.12	- 18	- 18	- 18
- 0.24	- 210	- 500	- 690
- 0.60	- 405	- 680	- 915
- 1.20	- 630	- 890	-1205
- 2.76	- 910	-1240	-1710
- 4.8	-1175	-1610	-2210
- 7.2	-1435	-2005	-2770
- 9.6	-1680	-2370	-3335
-12.0	-1920	-2730	
-14.4	-2170	-3115	
-16.8	-2450	-3550	
-18.25	-2685	-3850	
-19.2	-2980		

H. RUNNING FRICTION

The probe running friction data shown in Fig. A-7 are from Ref A-1.

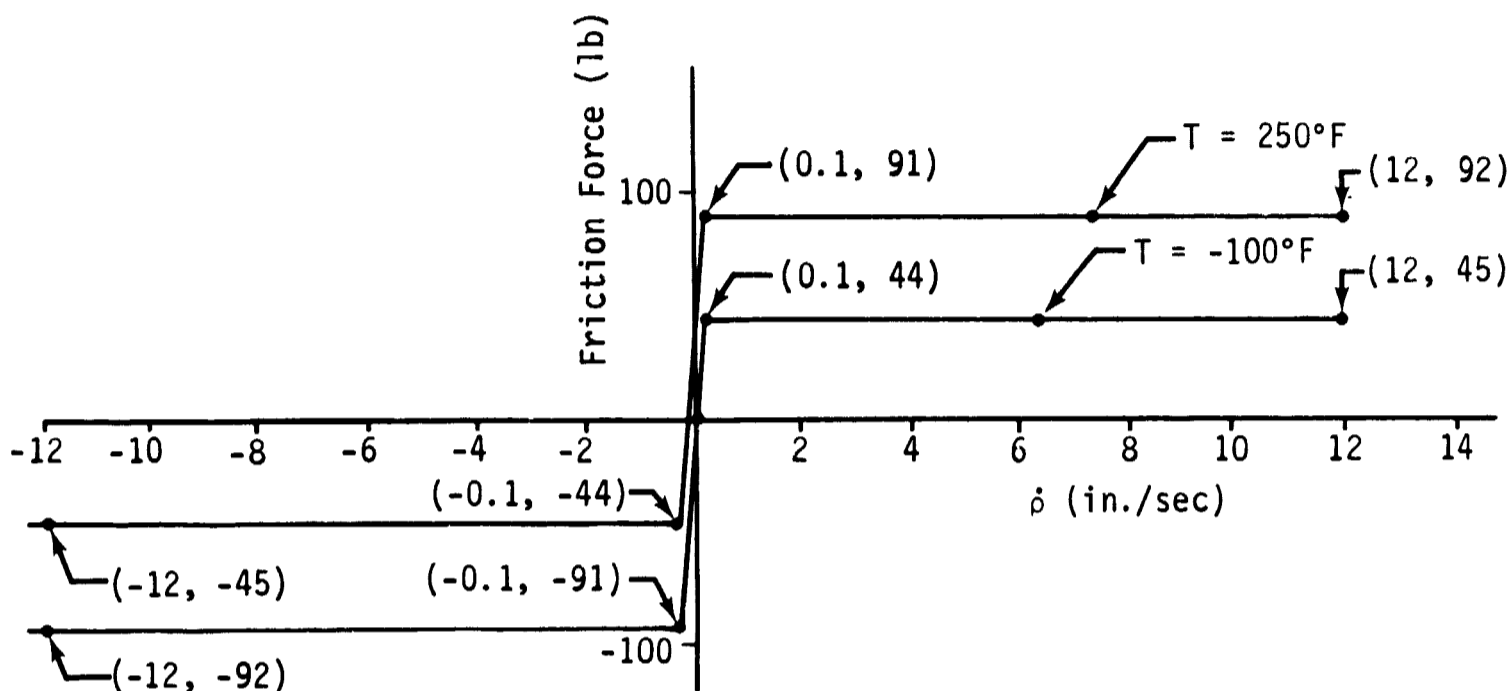


Fig. A-7 Graphical Representation of Running Friction

I. RETRACT FORCE

The flow rate of a compressible perfect gas through an orifice can be expressed by the equation,

$$\dot{W} = C_o \sqrt{\frac{gY}{R} \left(\frac{2}{\gamma + 1}\right)^{\frac{\gamma+1}{\gamma-1}} \frac{A_o p_B}{\sqrt{T_B}}}$$

Data from Ref A-1 indicate the following values for the docking probe retract system:

p_B = Bottle pressure = 7.2×10^5 lb/ft²;

Bottle volume = 3.55×10^{-3} ft³;

T_B = Bottle temperature = 530°R;

Bottle gas mass = 0.0827 lb-sec²/ft;

A_o = Bottle orifice area = 1.35×10^{-7} ft²;

Bottle secondary orifice area = 9.43×10^{-7} ft²;

Stroke to open secondary orifice = 0.7547 ft;

γ = Specific heat ratio = 1.05;
 Retract piston area = 0.0328 ft²;
 R = Gas constant = 55.16 ft/°R;
 C_o = Orifice coefficient = 0.62 (assumed).

The flow rates for the primary and secondary orifices are then:

$$\dot{W}_{\text{primary}} = 1.22 \times 10^{-3} \text{ lb/sec};$$

$$\dot{W}_{\text{secondary}} = 8.5 \times 10^{-3} \text{ lb/sec};$$

An expression for the retract piston force time history can be constructed from the flow rate and probe geometry, Fig. A-8.

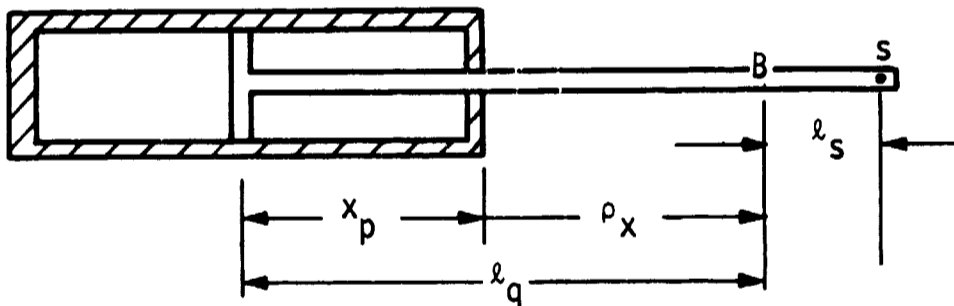


Fig. 8 Schematic for Retract Piston Force Time History

The force acting on the piston is

$$F_p = \frac{12\dot{W}RT \Delta t}{x_p} = \frac{12\dot{W}RT \Delta t}{l_q - \rho_x}$$

Evaluating the above yields $F_{p1} = \frac{428.22 \Delta t}{16.53 - \rho_x}$ for $2.08 \leq \rho_x \leq 11.12$

(primary orifice open) and $F_{p2} = F_{p1}^* + \frac{2983.5(\Delta t - \Delta t^*)}{16.53 - \rho_x}$ for $\rho_x <$

2.08 (primary and secondary orifices open). The value F_{p1}^* is the value of F_{p1} at the time (Δt^*) that the secondary orifice opens.

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APPENDIX B

CONTROL SYSTEMS CHARACTERISTICS

This appendix summarizes the attitude control systems considered in the docking simulation. Three control systems are described; each system may be included or omitted at the user's option.

A. CONTROL MOMENT GYRO ATTITUDE CONTROL SYSTEM

A block diagram for the CMG system acting on the target vehicle is shown in Fig. B-1. The transfer function (1/F) for each channel is of the form.

$$\frac{1}{F_{x,y,z}} = \frac{1}{\left[\frac{s^2}{\omega_f^2} + \frac{2\zeta s}{\omega_f} + 1 \right]^2}$$

with the parameters for the three channels shown in Table B-1.

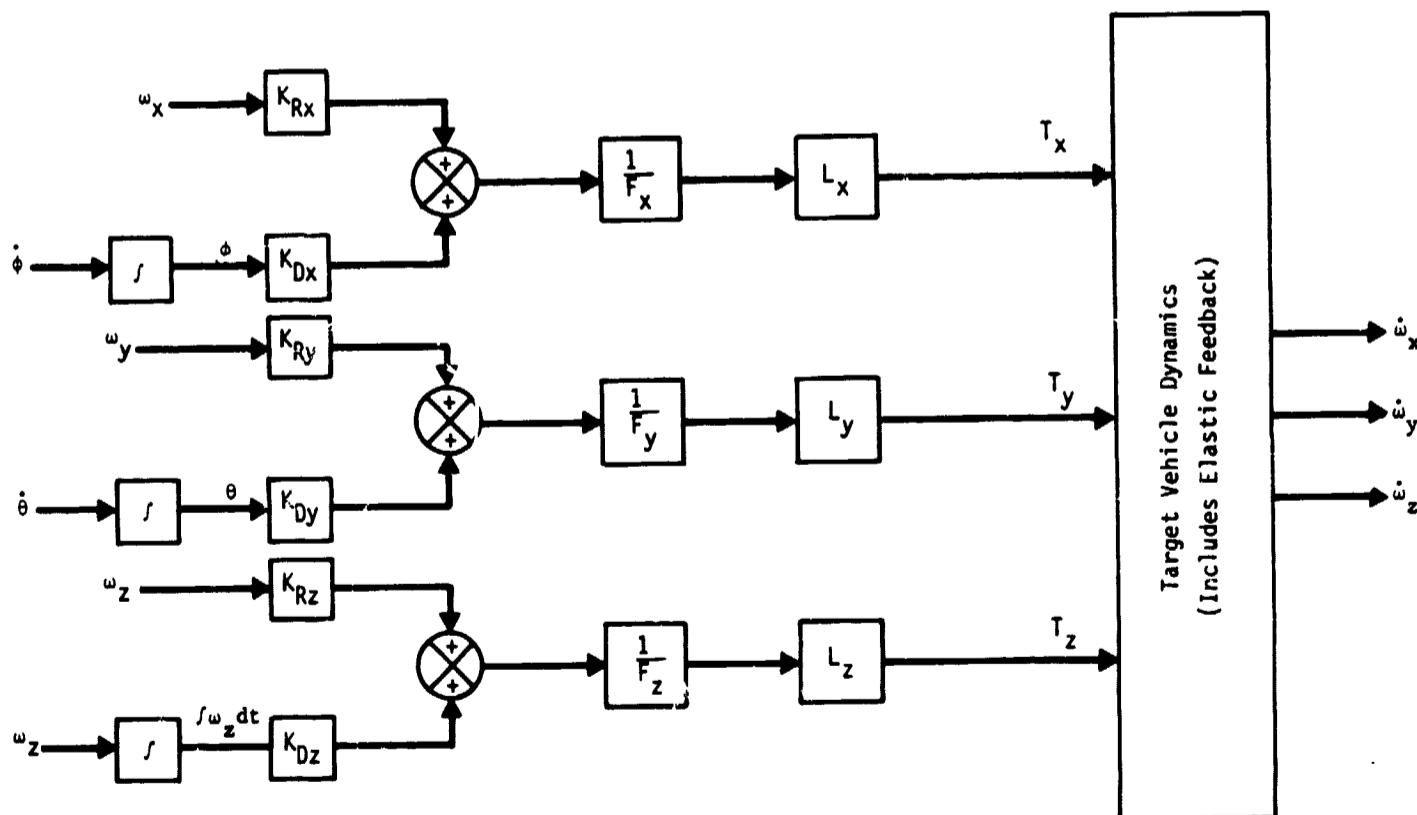


Fig. B-1 Control Moment Gyro Attitude Control System Block Diagram

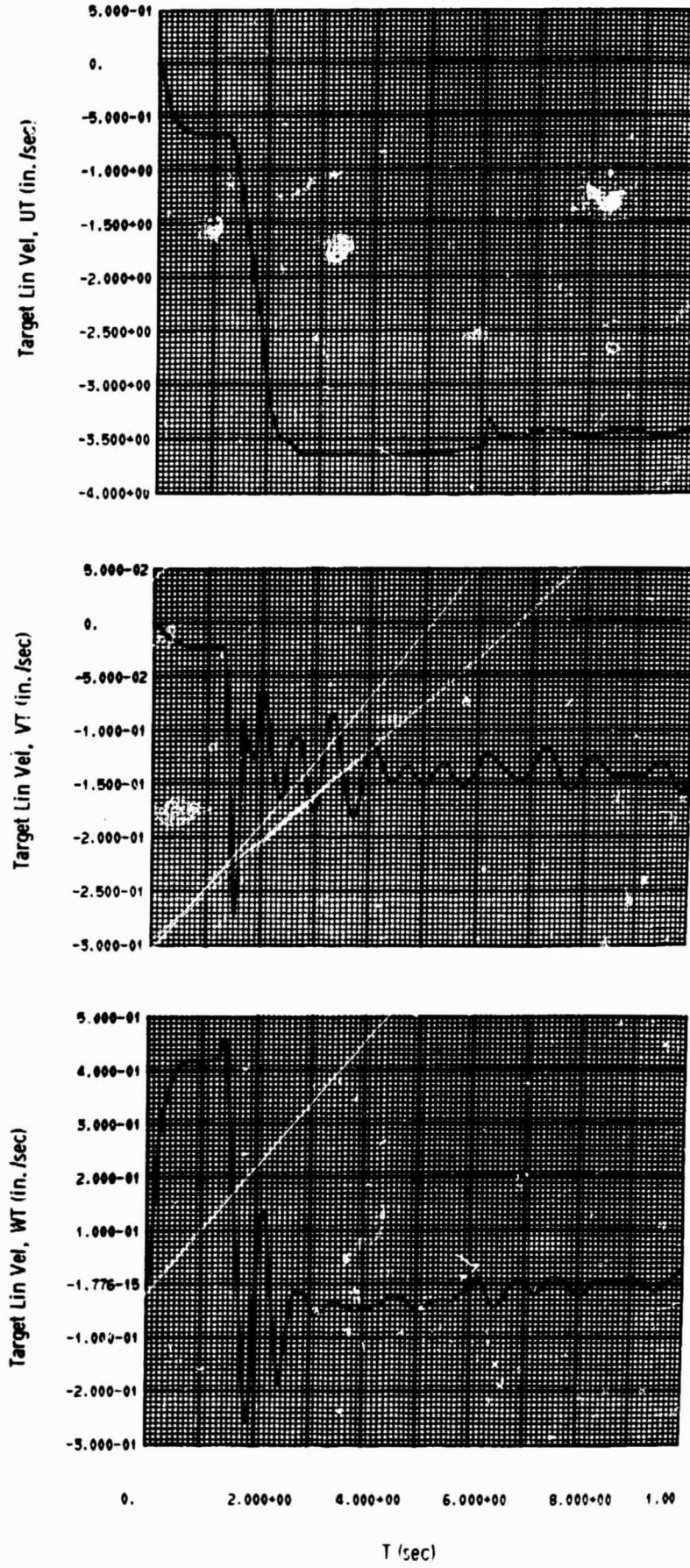


Fig. II-1 Output for Case SC-1 (Sheet 1 of 15)

Table B-1 CMG Attitude Control System Parameters

Parameter	Control Channel		
	x	y	z
K_D (in.-lb/rad)	5.57×10^5	27.18×10^5	53.8×10^5
K_R (in.-lb sec/rad)	25×10^5	176×10^5	242×10^5
ζ , Filter Damping Ratio	0.5	0.5	0.5
ω_f , Filter Break Frequency (rad/sec)	2.2	1.25	1.9

The transfer function $L_{x,y,z}$ is

$$L_x = L_y = L_z = \frac{a}{\tau s + 1}$$

with $a = 0.61$, $\tau = 0.24$. The total CMG output torque is limited to 1440 in.-lb.

B. THRUSTER ATTITUDE CONTROL SYSTEM/REACTION CONTROL SYSTEM

A block diagram for the TACS/RCS is shown in Fig. B-2. The TACS is a control system acting on the target vehicle. The RCS controls the chase vehicle. Significant control system parameters for the two systems are presented in Tables B-2 and B-3.

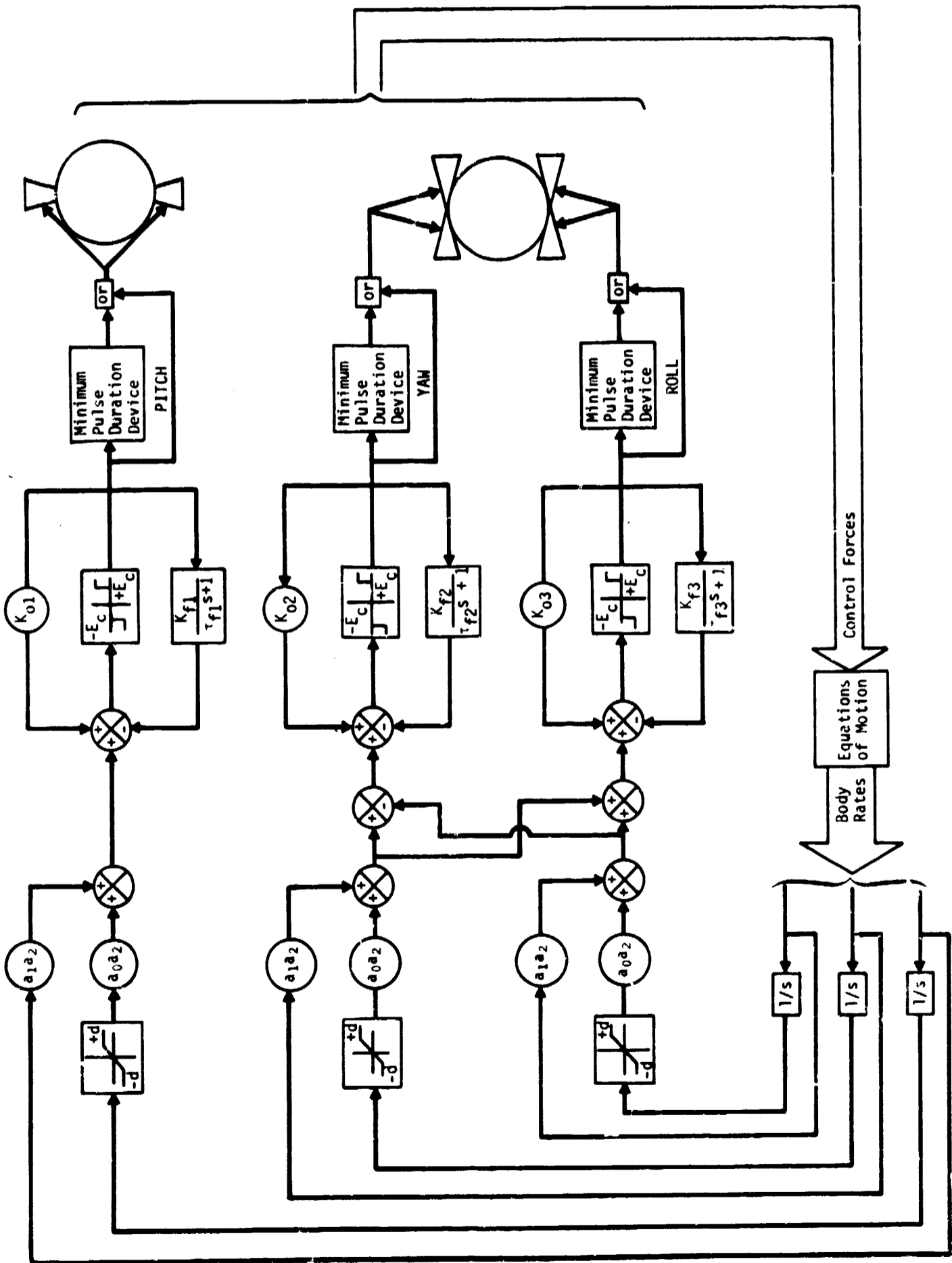


Fig. B-2 Thruster Attitude Control System/Reaction Control System Block Diagram

Table B-2 Thruster Attitude Control System Parameters

Parameter	Control Channel		
	Pitch	Yaw	Roll
d, Displacement limit (deg)	±2	±2	±2
a ₁ , Rate gain (deg/deg/sec)	20	20	20
a ₀ , Displacement gain (deg/deg)	2	2	2
a ₂ , Mixer gain (volt/deg)	20	20	20
K _o , Feedback gain (volt/volt)	0	0	0
K _f , Feedback gain (volt/volt)	0	0	0
τ _f , Time constant (sec)	0.5	0.5	0.5
Switch dead space (volts)	±20	±20	±20
E _c , Switch output (volts)	±100	±100	±100
Minimum pulse width (sec)	0	0	0

Table B-3 Reaction Control System Parameters

Parameter	Control Channel		
	Pitch	Yaw	Roll
d, Displacement limit (deg)	±4	±4	±4
a ₁ , Rate gain (deg/deg/sec)	1	1	1
a ₀ , Displacement gain (deg/deg)	0.5	0.5	0.5
a ₂ , Mixer gain (volt/deg)	10	10	10
K _o , Feedback gain, (volt/volt)	0.007	0.007	0.007
K _f , Feedback gain (volt/volt)	1.0	1.0	1.0
τ _f , Time constant (sec)	1.0	1.0	1.0
Switch dead space (volts)	±20	±20	±20
E _c , Switch output (volts)	±100	±100	±100
Minimum pulse width (sec)	0	0	0

Each thruster is assumed to produce 100 lb of thrust. Using known geometry for the TV and the CV yields the control forces (torques) shown in Table B-4.

Table B-4 TACS/RCS Control Forces and Moments

<u>TACS</u>	
$T_x = 28,320 \text{ in.-lb}$	(2 nozzles, 11.8 ft center line to nozzle)
$F_y = 200 \text{ lb}$	(2 nozzles)
$F_z = 100 \text{ lb}$	(1 nozzle)
<u>RCS</u>	
$T_x = 15,360 \text{ in.-lb}$	} (2 nozzles, 6.4 ft center-line to nozzle)
$T_y = 15,360 \text{ in.-lb}$	
$T_z = 15,360 \text{ in.-lb}$	

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APPENDIX C

PROGRAM DOCKEL LISTING

Appendix C presents a complete listing of DOCKEL. Sample input data appear in Appendix D. Sample output, using the input of Appendix D, appears in Appendix E. Subroutines required by the program that are included in the FORMA library are not included in this appendix. A listing and a complete description of these subroutines will be found in Ref III-1.

```

SUBROUTINE ATXBV (A,B,C)
  DIMENSION A(3,3), B(3), C(3)
C
C   CODED BY CARL BODLEY   MARCH 1968
C
  DO 10 I=1,3
  C(I) = 0.0
  DO 10 K=1,3
10 C(I) = C(I) + A(K,I)*B(K)
  RETURN
  END

```

```

SUBROUTINE AVPBV (ALP,A,BET,B,C)
  DIMENSION A(3), B(3), C(3)
C
C   CODED BY CARL BODLEY   MARCH 1968
C
  DO 10 I=1,3
10 C(I) = ALP*A(I) + BET*B(I)
  RETURN
  END

```

```

SUBROUTINE AXB3 (A,B,C)
  DIMENSION A(3,3), B(3,3), C(3,3)
C
C   CODED BY CARL BODLEY   JUNE 1968
C
  DO 10 I=1,3
  DO 10 J=1,3
  C(I,J) = 0.0
  DO 10 K=1,3
10 C(I,J) = C(I,J) + A(I,K)*B(K,J)
  RETURN
  END

```

```

SUBROUTINE AXBT3 (A,B,C)
  DIMENSION A(3,3), B(3,3), C(3,3)
C
C   CODED BY CARL BODLEY   MARCH 1968
C
  DO 10 I=1,3
  DO 10 J=1,3
  C(I,J) = 0.0
  DO 10 K=1,3
10 C(I,J) = C(I,J) + A(I,K)*B(J,K)
  RETURN
  END

```

```

SUBROUTINE AXBV (A,B,C)
  DIMENSION A(3,3), B(3), C(3)
C
C   CODED BY CARL BODLEY   MARCH 1968
C
  DO 10 I=1,3
  C(I) = 0.0
  DO 10 K=1,3
10 C(I) = C(I) + A(I,K)*B(K)
  RETURN
  END

```

SUBROUTINE BAKOFF

```

C
C SUBROUTINE TO INCREMENT THE RHO COORDINATES IN SUCH A WAY THAT NO
C PHICON .LT. 0.
C
C SUBROUTINES THAT ARE CALLED ARE --- INV2NP AND MULT
C
C CODED BY CARL BODLEY, JULY 1969
C
COMMON /BTOData/ TRHO(9,6), BLS(10,6), BLY(7,39)
COMMON /PHILAM/ PHICON(10), ALAM(10), MODE(10)
COMMON /TRNFMS/ TRTI(3,3), TRCI(3,3), TRTC(3,3), TRHT(3,3), TRHC(3,3),
* TRRT(3,3,3), TRRC(3,3,3), TRPC(3,3), TRDT(3,3),
* TRPD(3,3), TRHD(3,3), TRRD(3,3,3), TRPT(3,3),
* TRHP(3,3), TRTP(3,3), TRRP(3,3,3)
COMMON /VECTOR/ Y(150), YDT(150)
COMMON /YPSTNS/ NUT, NXT, NGAMT, NUC, NXC, NGAMC, NRHO,
* NXITOT, NXIT, NXICDT, NXIC, NOELCS
C
DIMENSION DELPHI(10), DELRHO(6), BC(6,6), BCI(6,6), MKV(6)
DIMENSION IVEC(10), JVEC(6)
C
DATA EPSN/0.005 /
DATA JVEC/1,2,3,4,5,6/
C
DO 10 I=1,10
  AMODE = MODE(I)
10 DELPHI(I) = AMODE*(EPSN - PHICON(I))
C
  IVEC(4) = 0
  DO 15 I=1,3
    IP4 = I + 4
    IP7 = I + 7
    IVEC(I) = MODE(I)
    IVEC(IP4) = MODE(IP4)
    IF (MODE(I) .EQ. 0 .AND. MODE(IP4) .EQ. 0) IVEC(IP4) = 1
  15 IVEC(IP7) = 1
C
  NVAL = 0
  DO 20 I=1,10
    IF (IVEC(I) .EQ. 0) GO TO 20
    NVAL = NVAL + 1
    IVEC(I) = NVAL
  20 CONTINUE
C
  CALL REVISE (BLS, IVEC, JVEC, BC, 10, 6, 6, 6, 10, 6)
  CALL REVISE (DELPHI, IVEC, JVEC(1), MKV, 10, 1, 6, 1, 10, 6)
C
  IF (MODE(4) .EQ. 0) GO TO 50
C
  DO 25 I=1,3
  25 MKV(I+3) = -DELPHI(4)*TRHT(2, I)
C
  50 CALL INV2NP (BC, BCI, 6, 6)
  CALL MULT (BCI, MKV, DELRHO, 6, 6, 1, 6, 6)
C
  DO 60 I=1,6
  L = I + NRHO - 1
  60 Y(L) = Y(L) + DELRHO(I)
C
RETURN
END

```

C-4

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SUBROUTINE CONSYS

C

```

COMMON /BC1234/ BC1(10,6), BC2(10,6), BC3(10,26), BC4(10,26)
COMMON /CSFORC/ FORCS(10), NFORCS
COMMON /CSYSTM/ CVEC(6,15), EULR(6), EDOT(6)
COMMON /CMGDTA/ FXCSM, AKRX, AKRY, AKRZ, AKDX, AKDY, AKDZ, OMX, OMY,
*             OMFZ, ZETFX, ZETFY, ZETFZ, AX, AY, AZ, BX, BY, BZ,
*             TLIM
COMMON /IFOUTS/ MINIC, IFPLOT, IFPER
COMMON /JBATCH/ JBA
COMMON /MISCNO/ ANUM
COMMON /NMODES/ NMODET, NMODEC, IFELAS
COMMON /PHILAM/ PHICON(10), ALAM(10), MODE(10)
COMMON /PULSES/ QPA(6)
COMMON /RETRCT/ AKD1, AKD2, AKD3, RHOSO, FRET, EXTL, TLAG, TSTAR, FRET
COMMON /TIMESS/ STARTT, DELTAT, T, ENDT, TMST, NSECS
COMMON /VECTOR/ Y(150), YDT(150)
COMMON /YPSYNS/ NUT, NXT, NGAMT, NUC, NXC, NGAMC, NRHO,
*             NXITDT, NXIT, NXICDT, NXIC, NOELCS

```

C

DIMENSION OMGG(3)

C

```

DATA NIT, NOT / 5, 6 /
DATA IIST, TEST / 0, 0.0 /

```

C

SET FORCE TRANSFORMATIONS AND READ CONTROL AND ELASTIC INPUT.

C

```

IF (JBA .EQ. 1 .AND. IIST .EQ. 0) GO TO 3
GO TO 5
3 CALL ZERO (BC1, NFORCS, 6, 10)
CALL ZERO (BC2, NFORCS, 6, 10)
CALL ZERO (BC3, NFORCS, NMODET, 10)
CALL ZERO (BC4, NFORCS, NMODEC, 10)
READ (NIT, 2001) FXCSM, AKRX, AKRY, AKRZ, AKDX, AKDY, AKDZ, OMX, OMY,
*             OMFZ, ZETFX, ZETFY, ZETFZ, AX, AY, AZ, BX, BY, BZ,
*             TLIM
2001 FORMAT (8E10.0)
IF (IFELAS .EQ. 0) GO TO 15
CALL READ (BC3(2,1), NI, NMDT, 10, 26)
IF (NMDT .EQ. NMODET) GO TO 15
WRITE (NOT, 1001)
1001 FORMAT (25H16YRO SIGS NOT COMPATIBLE)
STOP
15 BC2(1,1) = 1.
BC1(5,4) = 1.
BC1(6,2) = 1.
BC1(7,3) = 1.
DO 4 I = 1,3
BC1(I+1, I+3) = 1.
4 BC2(I+7, I+3) = 1.0
C
5 CONTINUE
IF (IIST .EQ. 1) GO TO 10
C
CALL READ (CVEC, NRC, NCC, 6, 15)
BC1(6,4) = -CVEC(3,12)
BC1(6,6) = CVEC(1,12)
BC1(7,4) = CVEC(2,12)
BC1(7,5) = -CVEC(1,12)
IF (MINIC .EQ. 0) GO TO 8
DO 7 I=1,3
Y(INDELCS +I) = CVEC(I ,1)*ANUM

```

7 Y(NDELCS+18+I) = CVEC(I+3,1)*ANUM

C
C
C

COMPUTE CONSTANTS FOR THE CMG SYSTEM.

8 OMF4X = OMF4**4
 OMF4Y = OMF4**4
 OMF4Z = OMF4**4
 OMFZ1X = 4.*ZETFX*OMFX
 OMFZ1Y = 4.*ZETFY*OMFY
 OMFZ1Z = 4.*ZETFZ*OMFZ
 OMFZ2X = (4.*ZETFX**2 + 2.)*OMFX**2
 OMFZ2Y = (4.*ZETFY**2 + 2.)*OMFY**2
 OMFZ2Z = (4.*ZETFZ**2 + 2.)*OMFZ**2
 OMFZ3X = OMFZ1X*OMFX**2
 OMFZ3Y = OMFZ1Y*OMFY**2
 OMFZ3Z = OMFZ1Z*OMFZ**2
 10 IIST = 1

C
C
C
C

COMPUTE CONTROL SIGNALS AND FORCES FOR THE CMG SYSTEM.

DLT = T-(TSTAR-TLAG)
 IF (MODE(4) .EQ. 1) TEST = 1.
 IF (MODE(8) .EQ. 1 .AND. DLT .GE. 0.4) TEST = 0.
 FORCS(1) = FXCSM*TEST
 YDT(NDELCS) = FORCS(1)

C

OMGG(1) = Y(NUT + 3)
 OMGG(2) = Y(NUT + 4)
 OMGG(3) = Y(NUT + 5)
 CALL MULTAD (BC3(2,1),Y(NXITDT),OMGG,3,NMODET,1,10,150,3)
 SNP = SIN(Y(NDELCS + 1))
 CSP = COS(Y(NDELCS + 1))
 SNT = SIN(Y(NDELCS + 2))
 CST = COS(Y(NDELCS + 2))
 YDT(NDELCS + 1) = OMGG(1)*SNP*SNT/CST
 * +OMGG(3)*CSP*SNT/CST
 YDT(NDELCS + 2) = OMGG(2)*CSP - OMGG(3)*SNP
 YDT(NDELCS + 3) = OMGG(3)
 YDT(NDELCS + 4) = OMF4X*(AKRX*OMGG(1)+AKDX*Y(NDELCS+1)
 * -Y(NDELCS+ 7))- OMFZ1X*Y(NDELCS+ 4)
 * -OMFZ2X*Y(NDELCS+ 5)-OMFZ3X*Y(NDELCS+ 6).
 YDT(NDELCS + 5) = Y(NDELCS + 4)
 YDT(NDELCS + 6) = Y(NDELCS + 5)
 YDT(NDELCS + 7) = Y(NDELCS + 6)
 YDT(NDELCS + 8) = (AX*Y(NDELCS + 7) - Y(NDELCS + 8))/BX
 YDT(NDELCS + 9) = OMF4Y*(AKRY*OMGG(2)+AKDY*Y(NDELCS+2)
 * -Y(NDELCS+12))- OMFZ1Y*Y(NDELCS+ 9)
 * -OMFZ2Y*Y(NDELCS+10)-OMFZ3Y*Y(NDELCS+11)
 YDT(NDELCS + 10) = Y(NDELCS + 9)
 YDT(NDELCS + 11) = Y(NDELCS + 10)
 YDT(NDELCS + 12) = Y(NDELCS + 11)
 YDT(NDELCS + 13) = (AY*Y(NDELCS + 12) - Y(NDELCS + 13))/BY
 YDT(NDELCS + 14) = OMF4Z*(AKRZ*OMGG(3)+AKDZ*Y(NDELCS+3)
 * -Y(NDELCS+17))- OMFZ1Z*Y(NDELCS+14)
 * -OMFZ2Z*Y(NDELCS+15)-OMFZ3Z*Y(NDELCS+16)
 YDT(NDELCS + 15) = Y(NDELCS + 14)
 YDT(NDELCS + 16) = Y(NDELCS + 15)
 YDT(NDELCS + 17) = Y(NDELCS + 16)
 YDT(NDELCS + 18) = (AZ*Y(NDELCS + 17) - Y(NDELCS + 18))/BZ
 C
 FORCS(2) = -Y(NDELCS + 8)


```

FORCS(3) = -Y(NDELCS + 13)
FORCS(4) = -Y(NDELCS + 18)
IF (FORCS(2) .LT. -TLIM) FORCS(2) = -TLIM
IF (FORCS(2) .GT. TLIM) FORCS(2) = TLIM
IF (FORCS(3) .LT. -TLIM) FORCS(3) = -TLIM
IF (FORCS(3) .GT. TLIM) FORCS(3) = TLIM
IF (FORCS(4) .LT. -TLIM) FORCS(4) = -TLIM
IF (FORCS(4) .GT. TLIM) FORCS(4) = TLIM

```

C
C
C
C
C

CALCULATE CONTROL SIGNALS (INCLUDING SIGNALS TO BE INTEGRATED) AND FORCES FOR TACS AND RCS.

```

DO 17 I=1,3
EULR(I) = Y(NDELCS+7)
EULR(I+3) = Y(NDELCS+I+18)
EDOT(I) = OMGG(I)
17 EDOT(I+3) = Y(NUC+I+2)
SNP = SIN(Y(NDELCS + 19))
CSP = COS(Y(NDELCS + 19))
SNT = SIN(Y(NDELCS + 20))
CST = COS(Y(NDELCS + 20))
YDT(NDELCS + 19) = EDOT(4)+EDOT(5)*SNP+SNT/CST
                +EDOT(6)*CSP+SNT/CST
YDT(NDELCS + 20) = EDOT(5)*CSP - EDOT(6)*SNP
YDT(NDELCS + 21) = EDOT(5)*SNP/CST + EDOT(6)*CSP/CST

```

C
C
C

```

DO 50 I = 1,6
50 CALL CSLOOP (I)

```

```

STOR = OPA(2)
OPA(2) = OPA(3)
OPA(3) = STOR
DO 65 I=1,6
FORCS(I + 4) = -OPA(I)
65 YDT(NDELCS + 27 + I) = ABS(OPA(I))

```

C
C

```

RETURN
END

```

SUBROUTINE CONTAK

```

C
C SUBROUTINE TO SET CONSTRAINT MODE BASED ON INPUT GEOMETRY ONLY.
C THE SUBROUTINE IS CALLED INITIALLY AND ONLY ON THE 4TH TIME OF THE
C RUNGE-KUTTA-GILL LOOP.
C
C SUBROUTINES THAT ARE CALLED ARE --- BAKOFF, GEOM AND KINMAT.
C
C CODED BY CARL BODLEY, JULY 1969
C
C COMMON /LIPARM/ FLAMC(3),ORMAG(3)
C COMMON /PHILAM/ PHICON(10),ALAM(10), MODE(10)
C
C DIMENSION IFTEST(8)
C
C DATA NIT,NOT/5,6/
C DATA EPSU, IFCAP, MAXITR, IIST /
C * 0.01, 0, 15, 0/
C
C IF (IIST .GT. 0) GO TO 5
C DO 8 I=1,8
C 8 MODE(I) = 0
C IIST = 1
C 5 ICOUNT = 0
C 10 DO 10 I=1,8
C IFTEST(I) = 0
C IF (PHICON(I) .LE. EPSU) MODE(I) = 1
C IF (PHICON(I) .LT. 0.) IFTEST(I) = 1
C 10 CONTINUE
C
C IF (IFCAP .EQ. 1) MODE(8) = 1
C IF (MODE(8) .EQ. 1) MODE(4) = 0
C IF (MODE(8) .EQ. 1) IFCAP = 1
C MODE( 9) = MODE(8)
C MODE(10) = MODE(8)
C
C DO 15 I=1,3
C IP4 = I + 4
C IF (FLAMC(I) .LE. 0.0) MODE(IP4) = 0
C IF (MODE(I) .EQ. 1 .AND. MODE(IP4) .EQ. 1) GO TO 20
C GO TO 15
C 20 IF (PHICON(I) .LE. PHICON(IP4)) MODE(IP4) = 0
C IF (PHICON(I) .GT. PHICON(IP4)) MODE(I) = 0
C 15 CONTINUE
C
C IF (MODE(8) .EQ. 1 .AND. PHICON(8) .GE. EPSU) IFTEST(8) = 1
C PHCN9 = ABS(PHICON(9))
C PHCN10 = ABS(PHICON(10))
C IF (MODE(8) .EQ. 1 .AND. PHCN9 .GE. EPSU) IFTEST(8) = 1
C IF (MODE(8) .EQ. 1 .AND. PHCN10 .GE. EPSU) IFTEST(8) = 1
C
C IFOUT = 0
C DO 25 I=1,8
C 25 IFOUT = IFOUT + IFTEST(I)*MODE(I)
C IF (IFOUT .EQ. 0 .AND. ICOUNT .GT. 1) RETURN
C
C ICOUNT = ICOUNT + 1
C IF (ICOUNT .EQ. MAXITR) GO TO 999
C
C CALL BAKOFF
C CALL GEOM
C CALL KINMAT
C GO TO 100
C
C 999 WRITE (NOT,1001)
C 1001 FORMAT (31HISUBR, CONTAK DOES NOT CONVERGE/
C * 17HOPROGRAM STOPPED.)
C STOP
C END

```

SUBROUTINE CSLOOP (MCHNL)

```

C
C SUBROUTINE CSLOOP COMPUTES THE SIGNALS AT NECESSARY POINTS IN THE
C CONTROL LOOPS FOR ALL CHANNELS.
C
C VARIABLE DEFINITION (PER CHANNEL)
C D1 THRU D5 - SIGNALS WITHIN THE CONTROL SYSTEM.
C ANGLE - ANGULAR ORIENTATION (RADIAN)
C TFL - CONTROL SYSTEM FIRST ORDER TIME CONSTANT.
C A0, A1, A2, C01, CFL - CONTROL SYSTEM GAIN CONSTANTS.
C ANGVEL - ANGULAR RATE OF CHANGE OF BODY (RAD/SEC).
C ANGLMT - ANGULAR ORIENTATION ERROR LIMIT OF BODY (INPUT IN DEGREES).
C QP - OUTPUT FORCE REQUEST SIGNAL TO MINIMUM PULSING DEVICE.
C D4D - DERIVATIVE OF SIGNAL D4.
C
C
C COMMON /CSYSTEM/ CVEC(6,15), EULR(6), EDOT(6)
C COMMON /MISCNO/ ANUM
C COMMON /PULSES/ QPA(6)
C COMMON /VECTOR/ Y(150), YDT(150)
C COMMON /YPSTES/ NUT,NXT,NGANT,NUC,NXC,NGANC,NRHO,
C * NXITDT,NXIT,NXICDT,NXIC, NDELCS
C
C DIMENSION D5(6)
C DATA D5 /0.,0.,0.,0.,0.,0. /
C
C D4 = Y(NDELCS + MCHNL + 21)
C
C INITIALIZE CONTROL SYSTEM VARIABLES.
C
C 5 ANGLMT = CVEC(MCHNL,2) * ANUM
C ECLM1 = CVEC(MCHNL,3)
C ECLM0 = CVEC(MCHNL,4)
C FIRSTR = CVEC(MCHNL,5)
C A0 = CVEC(MCHNL,6)
C A1 = CVEC(MCHNL,7)
C A2 = CVEC(MCHNL,8)/ANUM
C C01 = CVEC(MCHNL,9)
C CFL = CVEC(MCHNL,10)
C TFL = CVEC(MCHNL,11)
C
C ANGLE = EULR(MCHNL)
C ANGVEL = EDOT(MCHNL)
C
C IF (ANGLE .GT. ANGLMT) ANGLE = ANGLMT
C IF (ANGLE .LT. -ANGLMT) ANGLE = -ANGLMT
C D1 = (A1 * ANGVEL + A0 * ANGLE) * A2
C
C COMPUTE THE COUPLING TERMS IN CASE OF THE YAW AND ROLL CHANNELS.
C
C IF (MCHNL .EQ. 2 .OR. MCHNL .EQ. 5) GO TO 20
C IF (MCHNL .EQ. 1 .OR. MCHNL .EQ. 4) MALT = MCHNL + 2
C IF (MCHNL .EQ. 3 .OR. MCHNL .EQ. 6) MALT = MCHNL - 2
C ANGLMT = CVEC(MALT,2) * ANUM
C A0 = CVEC(MALT,6)
C A1 = CVEC(MALT,7)
C A2 = CVEC(MALT,8) / ANUM
C ANGLE = EULR(MALT)
C ANGVEL = EDOT(MALT)
C IF (ANGLE .GT. ANGLMT) ANGLE = ANGLMT
C IF (ANGLE .LT. -ANGLMT) ANGLE = -ANGLMT
C DALT = (A1 * ANGVEL + A0 * ANGLE) * A2

```

```
IF (MCHNL .EQ. 1 .OR. MCHNL .EQ. 4) D1 = D1 + DALT
IF (MCHNL .EQ. 3 .OR. MCHNL .EQ. 6) D1 = D1 - DALT
```

C
C
C

```
COMPUTE REMAINING SIGNALS IN THE CONTROL LOOP.
```

```
20 D2 = D1 - D4 + D5(MCHNL)
   D3 = 0.0
   IF (D2 .GT. ECLMI) D3 = ECLMO
   IF (D2 .LE. -ECLMI) D3 = -ECLMO
   D5(MCHNL) = C01 * D3
   D4D = (CFL * D3 - D4) / TFL
   OP = FTRSTR * D3 / ECLMO
   OPA(MCHNL) = OP
   YDT(NDELCS + MCHNL + 21) = D4D
```

C

```
RETURN
END
```

PROGRAM DOCKOD (INPUT,OUTPUT,FILMPL,TAPES=INPUT,TAPE6=OUTPUT,
PUNCH,TAPE1,TAPE2,TAPE3)

C
C
C
C
C

MAIN OVERLAY OF PROGRAM DOCKEL

CODED BY BODLEY/MERZ/PARK 1969

COMMON /ANGLES/ ALPHAD,SALPD,CALPD,TALPD, SSIGMA(3),CSIGMA(3)
COMMON /BC1234/ BC1(10,6), BC2(10,6), BC3(10,26), BC4(10,26)
COMMON /BINDFR/ FI,BINDMU
COMMON /BTOATA/ TRHO(9,6), BLS(10,6), BLV(7,39)
COMMON /CHANGE/ Z(150),ZDT(150)
COMMON /CHGDTA/ FXCSM, AKRX,AKRY,AKRZ,AKDX,AKDY,AKDZ,OMFX,OMFY,
OMFZ,ZETFX,ZETFY,ZETFZ,AX,AY,AZ,BX,BY,BZ,
TLIM
COMMON /CSFORC/ FORCS(10), NFORCS
COMMON /CSYSM/ CVEC(6,15), EULR(6), EDOT(6)
COMMON /FORMOM/ FANDM(12)
COMMON /FUNGAM/ SGAMMA(3),CGAMMA(3),SGSS(3),SGCS(3),
CGSS(3),CGCS(3)
COMMON /GEOMTY/ AA,AB,AD,AE,AF,AP,DLB,DL0,DLE,DLF,DLI,OLP,DL0,DLS,
TDT0(3),CPCD(3),RADCON,CSPHER,ROTALP,PEO,FDO
COMMON /IFOUTS/ MINIC,IFPLOT,IFPER
COMMON /JBATCH/ JBA
COMMON /JCOUNT/ JIL
COMMON /LATCHL/ VLAM(6)
COMMON /LIPARM/ FLAMC(3), QRMAG(3)
COMMON /LOCLEN/ LOC(12), LEN(12)
COMMON /LOCPTC/ CSC(3),CAC(3,3),CQC(3,3),
CPC(3),PSC(3),PAC(3,3),POC(3,3)
COMMON /LOCPTD/ DSD(3),DHD(3),DGD(3),DAD(3,3),ORD(3,3),
DOD(3,3),ORD(3,3)
DHPD(3),DBD(3,3),DFD(3,3),DPD(3,3)
COMMON /LOCPTH/ DSH(3)
COMMON /LOCPTI/ OTI(3),OCI(3),TCI(3)
COMMON /LOCPTP/ PSP(3),PAP(3,3),POP(3,3)
COMMON /LOCPTT/ THT(3),TCT(3),TST(3),TAT(3,3),TRT(3,3),
CST(3),CAT(3,3), QRT(3,3), TDT(3),
DHT(3),DGT(3),DST(3), DAT(3,3),DQT(3,3),ORT(3,3)
COMMON /LSTART/ RUNNO,DATE,NPAGE,UNAME(3),TITLE1(12),TITLE2(12)
COMMON /MASS/ AMT,ANC,AIT(3,3),AIC(3,3)
COMMON /MFREQD/ FREQT(26),FREQC(26),ZETAT,ZETAC
COMMON /MISCNO/ ANUM
COMMON /MODATA/ HATD(3,26),SIGATD(3,26),HATP(3,26),SIGATP(3,26)
COMMON /NCNTRL/ NCNSYS
COMMON /NE@TNS/ NE@TN
COMMON /NMODES/ NMODET,NMODEC,IFELAS
COMMON /PERTIT/ PTITL(8),IFFIXD,RANGLE,EED,CANGLE,
COELOC(3),VPLOC(3)
COMMON /PHILAM/ PHICOM(10),ALAM(10),MODE(10)
COMMON /PLTR / K1,NCOLS,NTIMES,XOLTA,NPLTS
COMMON /PULSES/ QPA(6)
COMMON /PUNCHY/ IFPNCH
COMMON /QPRKTA/ QRK(150),PRK(4)
COMMON /RETRCT/ AKD1,AKD2,AKD3,RHOSO,FRETL,EXTL,TLAG,TSTAR,FREY
COMMON /SKEWMS/ TDTS0(3,3),THTS0(3,3),TRTS0(3,3,3),DRTS0(3,3,3),
PSCS0(3,3),PSPPS0(3,3),PQCS0(3,3,3),POPSPS0(3,3,3),
CSCS0(3,3),CQCS0(3,3,3),DHTS0(3,3)
COMMON /SLIDFR/ HDMU,ARMU,BFV(8,39)
COMMON /SPRMP/ FSPRNG(2,20,4),FDAMP(2,20,4)
COMMON /TAPED/ NTAPE1,NTAPE2,NTAPE3
COMMON /TIMESS/ STARTT,DELTA, T, ENDT, TMST, NSECS

```

COMMON /TRNFMS/ TRTI(3,3),TRCI(3,3),TRTC(3,3),TRMT(3,3),TRHC(3,3),
* TRRT(3,3,3),TRRC(3,3,3),TRPC(3,3),TRDT(3,3),
* TRPD(3,3),TRHD(3,3),TRRD(3,3,3),TRPT(3,3)
* TRMP(3,3),TRTP(3,3),TRRP(3,3,3)
COMMON /VECMAG/ FDMAG(3), PEMAG(3)
COMMON /VECTOR/ Y(150),YDT(150)
COMMON /YPSTNS/ NUT,NXT,NGAMT,NUC,NXC,NGAMC,NRHO,
* NXITDT,NXIT,NXICDT,NXIC,NDELCS

```

C

```

DATA NTAPE1, NTAPE2, NTAPE3, JBA, DOCKEL/
* 1, 2, 3, 0,6LDOCKEL/
DATA NUT, NXT, NGAMT, NUC, NXC, NGAMC, NRHO, NXITDT
1 / 1, 7, 10, 16, 22, 25, 31, 37 /
DATA K1 /30000/

```

C

C

```

PROGRAM DOCKEL
COMMON MAP

```

C

C

C

C

C

SUBROUTINE

C

C

C

```

B C C C D F F G H H K L L M P P P R R R S S S S T V
A O O S O O T E L S I A O I I L R E O U F E E E I E
K N N L C R A O A I N M C N E O E T O N T T T T M C
O S T O K F B M T G M R A Y R T E R T K P P T U H T
F Y A O D U L C A H T S C E N A S T E L P P S R
F S K P O N E H T O E E R T K A R T E T

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COMMON

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ANGLES		X		X		X			X	X	
BC1234	X	X									X
BINDFR		X				X		X	X	X	
BTDATA	X	X	X		X	X					X
CHANGE		X					X		X		
CMGDTA	X	X									
CSFORC	X	X							X	X	X
CSYSTM	X	X	X								
FORMOM			X	X			X		X	X	
FUNGAM		X		X		X			X		
GEOMTY		X	X		X	X	X		X		X
IFOUTS	X	X			X		X		X		X
JBATCH	X	X							X		X
JCOUNT		X		X	X	X			X		X
LATCHL		X		X					X	X	
LIPARM		X	X	X		X					
LOCLEN		X				X		X			
LOCPTC		X	X	X	X						
LOCPTD		X	X	X	X		X		X	X	
LOCPTH		X	X	X	X						
LOCPTI		X	X	X	X				X		
LOCPTP		X	X	X	X	X			X		
LOCPTT		X	X	X	X				X		
LSTART		X									
MASS		X		X						X	X
MFREQD		X		X						X	X
MISCNO	X	X	X	X	X	X	X	X	X	X	X
MODATA		X	X	X	X	X					

C	NCNTRL					X					X
C	NEQTNS	X	X			X X	X	X		X X	X
C	NMODES	X	X	X X X X X X					X	X X	X
C	PERTIT			X					X		
C	PHILAM	X X X	X X		X X		X X		X		X
C	PLTR		X				X				X
C	PULSES	X	X X								
C	PUNCHY		X				X				X
C	QPRKTA		X					X			X
C	RETRCT	X	X		X		X X		X		X
C	SKEWMS		X X		X						
C	SLIDFR		X		X					X	X
C	SPRDMP		X		X					X	
C	TAPED		X				X		X X X		
C	TIMESS	X	X X	X	X X		X X X	X	X X X X X		X
C	TRNFMS	X	X X	X X	X X				X		X
C	VECMAG		X		X X						
C	VECTOR	X X	X X	X X	X X	X	X X	X X		X	X
C	YPSTNS	X X	X X	X X	X X X X		X X	X X			X

THE FOLLOWING REQUIRED SUBROUTINES HAVE NO COMMON BLOCKS

ATX9V
 AVPBV
 AXB3
 AXBT3
 AXBV
 INV2NP
 MULT3
 MULTAD
 SKEWV

THE FOLLOWING REQUIRED SUBROUTINES ARE FROM THE FORMA LIBRARY

AABB
 MULT
 PAGEHD
 PLOT1
 PLOT3
 PLOTSS
 PUNCH
 READ
 READIM
 REVISE
 START
 VCROSS
 VDOT
 WRITE
 WRITIM
 ZERO

CALL BPLT(0,2HLC)
 CALL INIT280

1 CALL START

JBA = JBA + 1

CALL OVERLAY (DOCKEL,1,0)
 CALL OVERLAY (DOCKEL,2,C)
 IF (IFPLOT .NE. 0) CALL OVERLAY (DOCKEL,3,0)

GO TO 1

END

```
      SUBROUTINE FTABLE(X,Y,SLOPE,BINTR,TABLE,POINT,NDIR,MM)
C
      DIMENSION TABLE(2,1)
C
      II = 1
      JJ = 2
      NPOINT = POINT + 0.1
      NTABLE = NPOINT + 1
      IF (NDIR .EQ. 1) GO TO 1
      II = 2
      JJ = 1
      1 IF (X .GE. TABLE(II,2)) GO TO 5
      MM = 2
      GO TO 25
      5 IF (X .LE. TABLE(II,NTABLE)) GO TO 10
      MM = NTABLE - 1
      GO TO 25
      10 DO 15 KK = 3,NTABLE
      IN = KK
      IF (X .LE. TABLE(II,KK)) GO TO 20
      15 CONTINUE
      20 MM = IN - 1
      25 LL = MM + 1
      SLOPE = (TABLE(JJ,LL) - TABLE(JJ,MM)) / (TABLE(II,LL) - TABLE
      * (II,MM))
      Y = TABLE(JJ,MM) + SLOPE * (X - TABLE(II,MM))
      BINTR = Y - X*SLOPE
C
      RETURN
      END
```


SUBROUTINE FORFUN

C
C
C
C
C

SUBROUTINE TO COMPUTE FORCING FUNCTION

CODED BY A C PARK SEPT 1969

```

COMMON /BTDATA/ TRHO(9,6), BL5(10,6), BLV(7,39)
COMMON /FORMOM/ FANDM(12)
COMMON /PHILAM/ PHICON(10), ALAM(10), MODE(10)
COMMON /SKEWMS/ TDTSO(3,3), THTSO(3,3), TRTSO(3,3,3), DRTSO(3,3,3),
*             PSCSO(3,3), PSPPSO(3,3), POCSSO(3,3,3), POPPSO(3,3,3),
*             CSCSO(3,3), CQCSO(3,3,3), DHTSO(3,3)
COMMON /TIMESS/ STARTT, DELTAT, T, ENDT, TMST, NSECS
COMMON /TRNFMS/ TRTI(3,3), TRCI(3,3), TRTC(3,3), TRHT(3,3), TRHC(3,3),
*             TRRT(3,3,3), TRRC(3,3,3), TRPC(3,3), TRDT(3,3),
*             TRPD(3,3), TRHD(3,3), TRRD(3,3,3), TRPT(3,3),
*             TRHP(3,3), TRTP(3,3), TRRP(3,3,3)

```

C

DIMENSION TLDS(7,12)

C

IF (TMST .EQ. 0.) CALL ZERO (TLDS(5,4), 3,3,7)

C

DO 12 I=1,7

DO 12 J=1,3

J6 = J+6

TLDS(I,J) = BLV(I,J)

12 TLDS(I,J6) = BLV(I,J6)

C

CALL MULT3 (TRHT(2,1), DHTSO, TLDS(1,4), 1,3,3,3,3,7)

CALL MULT3 (TRHC(2,1), PSCSO, TLDS(1,10), 1,3,3,3,3,7)

C

DO 18 K=1,3

K1 = K+1

CALL MULT3 (TRRT(2,1,K), DRTSO(2,1,K), TLDS(K1,4), 1,3,3,3,3,7)

CALL MULT3 (TRRC(2,1,K), POCSSO(1,1,K), TLDS(K1,10), 1,3,3,3,3,7)

18 CONTINUE

C

DO 20 I=1,4

DO 20 J=10,12

20 TLDS(I,J) = -TLDS(I,J)

C

CALL MULT3 (TRTC, PSCSO, TLDS(5,10), 3,3,3,3,3,7)

C

CALL MULT (ALAM(4), TLDS, FANDM, 1,7,12,1,7)

C

RETURN

END

SUBROUTINE GEOM

COMPUTES GEOMETRY AND ROTATION TRANSFORMATIONS

```

C
C
C
COMMON /ANGLES/ ALPHAD,SALPD,CALPD,TALPD,SSIGMA(3),CSIGMA(3)
COMMON /FUNGAM/ SGAMMA(3),CGAMMA(3),SGSS(3),SGCS(3),
* CGSS(3),CGCS(3)
COMMON /GEOMTY/ AA,AB,AD,AE,AF,AP,DLB,OLD,OLE,DLF,DLI,DLP,OLQ,DLS,
* TDT(3),CPC(3),RADCON,CSPHER,ROTALP,PEO,FDO
COMMON /JCOUNT/ JIL
COMMON /LIPARM/ FLAMC(3),ORMAG(3)
COMMON /LOCPTC/ CSC(3),CAC(3,3),CQC(3,3),
* CPC(3),PSC(3),PAC(3,3),POC(3,3)
COMMON /LOCPTD/ DSD(3),DHD(3),DGD(3),DAD(3,3),DRD(3,3),
* DQD(3,3),QRD(3,3)
* DHPD(3),DBD(3,3),DFD(3,3),DPD(3,3)
COMMON /LOCPTH/ DSH(3)
COMMON /LOCPTI/ OTI(3),OCI(3),TCI(3)
COMMON /LOCPTP/ PSP(3),PAP(3,3),POP(3,3)
COMMON /LOCPTT/ THT(3),TCT(3),TST(3),TAT(3,3),TRT(3,3),
* CST(3),CAT(3,3),QRT(3,3),TDT(3),
* DHT(3),DGT(3),DST(3),DAT(3,3),DQT(3,3),DRT(3,3)
COMMON /MISCNO/ ANUM
COMMON /MODATA/ HATD(3,26),SIGATD(3,26),HATP(3,26),SIGATP(3,26)
COMMON /NMODES/ NMODET,NMODEC,IFELAS
COMMON /TIMESS/ STARTT,DELTAT,T,ENDT,TMST,NSECS
COMMON /TRNFMS/ TRTI(3,3),TRCI(3,3),TRTC(3,3),TRHT(3,3),TRHC(3,3),
* TRRT(3,3,3),TRRC(3,3,3),TRPC(3,3),TRDT(3,3),
* TRPD(3,3),TRHD(3,3),TRRD(3,3,3),TRPT(3,3)
* TRHP(3,3),TRTP(3,3),TRRP(3,3,3)
COMMON /VECTOR/ Y(150),YDT(150)
COMMON /YPSTNS/ NUT,NXT,NGAMT,NUC,NXC,NGAMC,NRHO,
* NXITDT,NXIT,NXICDT,NXIC,NDELCS
C
DIMENSION UCLP(3),UCLD(3),UCMD(3),UCND(3),SKEWLD(3,3)
DIMENSION EAP(3),EAD(3)
DIMENSION WV(3),VW(3)
C
IF (TMST .GT. 0.0) GO TO 100
C
PSP(2) = 0.0
PSP(3) = 0.0
C
TRHD(1,1) = CALPD
TRHD(2,1) = -SALPD
TRHD(3,1) = 0.0
C
DO 12 J=1,3
PAP(2,J) = -AA*SSIGMA(J)
12 PAP(3,J) = AA*CSIGMA(J)
C
100 CONTINUE
C
CALL MULT (SIGATP,Y(NXIC),EAP,3,NMODEC,1,3,150)
EAP(2) = EAP(2)+Y(NRHO+1)
EAP(3) = EAP(3)+Y(NRHO+2)
CALL SKEWV (EAP,TRPC)
CALL MULT (SIGATD,Y(NXIT),EAD,3,NMODET,1,3,150)
CALL SKEWV (EAD,TRDT)
DO 11 I=1,3
TRPC(I,I) = 1.0
11 TRDT(I,I) = 1.0

```

C

```

DO 6 I=1,2
IT = 3*I+NGAMT-4
IC = 3*I+NGAMC-4
DO 6 J=1,3
TRTI(I,J) = Y(IT+J)
6 TRCI(I,J) = Y(IC+J)
TRTI(3,1) = TRTI(1,2)*TRTI(2,3)-TRTI(2,2)*TRTI(1,3)
TRTI(3,2) = TRTI(1,3)*TRTI(2,1)-TRTI(1,1)*TRTI(2,3)
TRTI(3,3) = TRTI(1,1)*TRTI(2,2)-TRTI(2,1)*TRTI(1,2)
TRCI(3,1) = TRCI(1,2)*TRCI(2,3)-TRCI(2,2)*TRCI(1,3)
TRCI(3,2) = TRCI(1,3)*TRCI(2,1)-TRCI(1,1)*TRCI(2,3)
TRCI(3,3) = TRCI(1,1)*TRCI(2,2)-TRCI(2,1)*TRCI(1,2)
FNRMT = SQRT(TRTI(1,1)*TRTI(1,1)+TRTI(1,2)*TRTI(1,2)
+ TRTI(1,3)*TRTI(1,3))
*
FNRMT = SQRT(TRTI(3,1)*TRTI(3,1)+TRTI(3,2)*TRTI(3,2)
+ TRTI(3,3)*TRTI(3,3))
*
FNRMC = SQRT(TRCI(1,1)*TRCI(1,1)+TRCI(1,2)*TRCI(1,2)
+ TRCI(1,3)*TRCI(1,3))
*
FNRMC = SQRT(TRCI(3,1)*TRCI(3,1)+TRCI(3,2)*TRCI(3,2)
+ TRCI(3,3)*TRCI(3,3))
DO 40 J=1,3
TRTI(1,J) = TRTI(1,J) / FNRMT
TRTI(3,J) = TRTI(3,J) / FNRMT
TRCI(1,J) = TRCI(1,J) / FNRMC
40 TRCI(3,J) = TRCI(3,J) / FNRMC
TRTI(2,1) = TRTI(3,2)*TRTI(1,3) - TRTI(3,3)*TRTI(1,2)
TRTI(2,2) = TRTI(3,3)*TRTI(1,1) - TRTI(3,1)*TRTI(1,3)
TRTI(2,3) = TRTI(3,1)*TRTI(1,2) - TRTI(3,2)*TRTI(1,1)
TRCI(2,1) = TRCI(3,2)*TRCI(1,3) - TRCI(3,3)*TRCI(1,2)
TRCI(2,2) = TRCI(3,3)*TRCI(1,1) - TRCI(3,1)*TRCI(1,3)
TRCI(2,3) = TRCI(3,1)*TRCI(1,2) - TRCI(3,2)*TRCI(1,1)
DO 45 I=1,2
IT = 3*I + NGAMT - 4
IC = 3*I + NGAMC - 4
DO 45 J=1,3
Y(IT+J) = TRTI(I,J)
45 Y(IC+J) = TRCI(I,J)

```

C

```

DO 14 I=1,3
INXT = I + NXT - 1
INXC = I + NXC - 1
OTI(I) = Y(INXT)
14 OCI(I) = Y(INXC)

```

C

```

DO 15 I=1,3
II = I+NRHO+2
SGAMMA(I) = SIN( Y(II))
CGAMMA(I) = COS( Y(II))
S6SS(I) = SGAMMA(I)*SSIEMA(I)
SGCS(I) = SGAMMA(I)*CSIGMA(I)
C6SS(I) = CGAMMA(I)*SSIGMA(I)
15 C6CS(I) = CGAMMA(I)*CSIGMA(I)

```

C

```

EXTN = DLI + Y(NRHO)
PSP(1) = EXTN + DLS

```

C

```

CALL MULT (HATP,Y(NXIC),MV,3,NMODEC,1,3,150)
CALL AVPBV (1.0,CPCO,1.0,MV,CPC)
CALL MULT (HATD,Y(NXIT),MV,3,NMODET,1,3,150)
CALL AVPBV (1.0,TDTO,1.0,MV,TOT)
CALL ATXBV (TRPC,PSP,PSC)

```

```

C
CALL AVPBV (1.0,CPC,1.0,PSC,CSC)
C
DO 18 J=1,3
PAP(1,J) = EXTN
CALL ATXBV (TRPC,PAP(1,J),PAC(1,J))
18 CONTINUE
C
CALL AXBT3 (TRTI,TRCI,TRTC)
CALL AXBT3 (TRPC,TRTC,TRPT)
CALL AXBT3 (TRPT,TRDT,TRPD)
CALL AVPBV (1.0,OCI,-1.0,OTI,TCI)
CALL AXBV (TRTI,TCI,TCT)
CALL AXBV (TRTC,CSC,CST)
CALL AVPBV (1.0,TCT,1.0,CST,TST)
CALL AVPBV (1.0,TST,-1.0,TDT,DST)
CALL AXBV (TRDT,DST,DSD)
C
C
PHIH = 0.0
IF (DSD(2).EQ.0.0 .AND. DSD(3).EQ.0.0) GO TO 21
PHIH = ATAN2(DSD(3), DSD(2))
21 CONTINUE
SPHIH = SIN(PHIH)
CPHIH = COS(PHIH)
C
TRHD(1,2) = CPHIH*SALPD
TRHD(1,3) = SPHIH*SALPD
TRHD(2,2) = CPHIH*CALPD
TRHD(2,3) = SPHIH*CALPD
TRHD(3,2) = -SPHIH
TRHD(3,3) = CPHIH
CALL AXBV (TRHD,DSD,DSH)
BGR = DSH(1)
C
CALL AXB3 (TRHD,TRDT,TRHT)
CALL AXB3 (TRHT,TRTC,TRHC)
C
DO 22 I=1,3
DHD(I) = BGR*TRHD(1,I)
22 DGD(I) = DSD(I) + CSPHER*TRHD(2,I)
C
CALL ATXBV (TRDT,DHD,DHT)
CALL ATXBV (TRDT,DGD,DGT)
CALL AVPBV (1.0,TDT,1.0,DHT,THT)
CALL AXBT3 (TRHC,TRPC,TRHP)
CALL AXBT3 (TRTC,TRPC,TRTP)
C
DO 24 K=1,3
C
UCLP(1) = -CGAMMA(K)
UCLP(2) = -SGSS(K)
UCLP(3) = SGCS(K)
CALL ATXBV (TRPD,UCLP,UCLD)
CALL SKEWV (UCLD,SKEWLD)
CALL AVPBV (1.0,CPC,1.0,PAC(1,K),CAC(1,K))
CALL AXBV (TRTC,CAC(1,K),CAT(1,K))
CALL AVPBV (1.0,TCT,1.0,CAT(1,K),TAT(1,K))
CALL AVPBV (1.0,TAT(1,K),-1.0,TDT,DAT(1,K))
CALL AXBV (TRDT,DAT(1,K),DAD(1,K))
C
C
CHECK FOR PIERCE POINT

```

```

CALL PIERCE (DAD(1,K),UCLD,DSD,RADCON,ALPHAD,SALPD,CALPD,TALPD,
1          ROTALP,DLB)
C  IF NO PIERCE POINT, CONTINUE
CALL ROOTS (DAD(1,K),UCLD,RADCON,ROTALP,PHIC,FLAMC(K),ORMAG(K),
          JIL,K)
C
DRD(1,K) = ROTALP
DRD(2,K) = RADCON * COS(PHIC)
DRD(3,K) = RADCON * SIN(PHIC)
CALL ATXBV (TRDT,DRD(1,K),DRT(1,K))
C
CALL AVPBV (1.0,TDT,1.0,DRT(1,K),TRT(1,K))
CALL AVPBV (1.0,FAP(1,K),FLAMC(K),UCLP,POP(1,K))
CALL ATXBV (TRPC,POP(1,K),PQC(1,K))
CALL AVPBV (1.0,CPC,1.0,PQC(1,K),CQC(1,K))
CALL AVPBV (1.0,DAD(1,K),FLAMC(K),UCLD,DQD(1,K))
CALL ATXBV (TRDT,DQD(1,K),DOT(1,K))
CALL AVPBV (1.0,DRT(1,K),-1.0,DQT(1,K),QRT(1,K))
CALL AVPBV (1.0,DRD(1,K),-1.0,DQD(1,K),QRD(1,K))
C
DO 26 I=1,3
26 UCMD(I) = QRD(I,K)/ORMAG(K)
C
CALL AXBV (SKEWLD,UCMD,UCND)
C
DO 28 J=1,3
TRRD(1,J,K) = UCLD(J)
TRRD(2,J,K) = UCMD(J)
28 TRRD(3,J,K) = -UCND(J)
CALL AXB3 (TRRD(1,1,K),TRDT,TRRT(1,1,K))
CALL AXB3 (TRRT(1,1,K),TRTC,TRRC(1,1,K))
CALL AXB3 (TRRC(1,1,K),TRPC,TRRP(1,1,K))
C
24 CONTINUE
C
RETURN
END

```

SUBROUTINE HLATCH(L)

```

C
C SUBROUTINE TO APPLY HARD-LATCH CONSTRAINT FORCES AT DOCKING
C COLLAR, MODIFIES STATE VECTOR(S), Y, YDT.
C CODED BY CARL BODLEY JAN. 2, 1970
C
COMMON /JCOUNT/ JIL
COMMON /LATCHL/ VLAM(6)
COMMON /LOCPTC/ CSC(3), CAC(3,3),COC(3,3),
* CPC(3),PSC(3),PAC(3,3),POC(3,3)
COMMON /LOCPTT/ THT(3),TCT(3),TST(3),TAT(3,3),TRT(3,3),
* CST(3),CAT(3,3), QRT(3,3), TDT(3),
* DHT(3),DGT(3),DST(3), DAT(3,3),DQT(3,3),DRT(3,3)
COMMON /MASS/ AMT, AMC, AIT(3,3), AIC(3,3)
COMMON /MODATA/ HATD(3,26),SIGATD(3,26), HATP(3,26),SIGATP(3,26)
COMMON /NMODES/ NMODET, NMODEC, IFELAS
COMMON /TRNFMS/ TRII(3,3),TRCI(3,3),TRTC(3,3),TRHT(3,3),TRHC(3,3),
* TRRT(3,3,3),TRRC(3,3,3),TRPC(3,3),TRDT(3,3),
* TRPD(3,3),TRHD(3,3),TRRD(3,3,3),TRPT(3,3)
* TRHP(3,3),TRTP(3,3),TRRP(3,3,3)
COMMON /VECTOR/ Y(150),YDT(150)
COMMON /YPOSTNS/ NUT,NXT,NGAMT,NUC,NXC,NGAMC,NRHO,
* NXITDT,NXIT,NXICDT,NXIC, NDELCS

C
DIMENSION BA1(6,6), BA2(6,6), BA3(6,26), BA4(6,26),
* DFT(3),PFC(3),TFT(3),CFC(3), CFT(3),
* DFTSQ(3,3),PFCSQ(3,3),TFTSQ(3,3),CFCSQ(3,3), W63(6,3),
* AITI(3,3),AICI(3,3), VFLAM(6),
* CUT(6,6),CUC(6,6),CXT(26,6),CXC(26,6),CLAM(6,6),CLAMI(6,6),
* V1(6),V2(6),V3(6),V4(6),RV(6),VEC1(3),VEC2(3),VEC3(3),VEC4(3),
* TDDTR(3),CPDTR(3),OMDT(3),OMPC(3),OMGD(3),OMGP(3)

C
DATA I1ST,DFD1 / 0, 18.1 /

C
IF (I1ST .GT. 0) GO TO 5
CALL ZERO (BA1,6,6,6)
CALL ZERO (BA2,6,6,6)
DO 7 I=1,6
7 BA1(I,I) = 1.
CALL INV2NP (AIT,AITI,3,3)
CALL INV2NP (AIC,AICI,3,3)
I1ST = 1
5 CONTINUE
GO TO (100,200), L
100 DO 10 I=1,3
DFT(I) = TRDT(1,I)*DFD1
TFT(I) = TDT(I) + DFT(I)
10 CFT(I) = TFT(I) - TCT(I)
CALL MULT3 (CFT,TRTC,CFC,1,3,3,1,3,1)
CALL AVPBV (1.,CFC,-1.,CPC,PFC)
CALL SKEWV (DFT,DFTSQ)
CALL SKEWV (PFC,PFCSQ)
CALL SKEWV (TFT,TFTSQ)
CALL SKEWV (CFC,CFCSQ)

C
DO 20 I=1,3
I3 = I + 3
DO 20 J=1,3
J3 = J + 3
BA1( I,J3) = TFTSQ(I,J)
BA2( I, J) = TRTC(I,J)
20 BA2( I3,J3) = TRTC(I,J)

```

```

CALL MULT3 (TRTC,CFCSQ,BA2(1,4),3,3,3,3,6)
CALL MULT3 (TRTC,PFCSQ,W63,3,3,3,3,6)
CALL MULT3 (TRTC,HATP,BA4,3,3,NMODEC,3,3,6)
CALL MULT3 (TRTC,SIGATP,BA4(4,1),3,3,NMODEC,3,3,6)
CALL MULTAD (W63,SIGATP,BA4,3,3,NMODEC,6,3,6)

```

C

```

DO 30 I=1,3
  I3 = I + 3
  DO 30 J=1,NMODET
    BA3(I,J) = HATD (I,J)
30 BA3(I3,J) = SIGATD(I,J)
CALL MULTAD (DFTSQ,SIGATD,BA3,3,3,NMODET,3,3,6)

```

C

```

CALL MULT3 (BA1(1,4),AITI,W63,6,3,3,6,3,6)
DO 40 I=1,6
  DO 40 J=1,3
    JP3 = J + 3
    CUT(J,I) = BA1(I,J)/AMT
40 CUT(JP3,I) = W63(I,J)
CALL MULT3 (BA2(1,4),AICI,W63,6,3,3,6,3,6)
DO 50 I=1,6
  DO 50 J=1,3
    JP3 = J + 3
    CUC(J,I) = BA2(I,J)/AMC
50 CUC(JP3,I) = W63(I,J)
DO 45 I=1,6
  DO 45 J=1,NMODET
45 CXT(J,I) = BA3(I,J)
DO 55 I=1,6
  DO 55 J=1,NMODEC
55 CXC(J,I) = BA4(I,J)
CALL MULT3 (BA1,CUT,CLAM,6,6,6,6,6)
CALL MULTAD (BA2,CUC,CLAM,6,6,6,6,6)
CALL MULTAD (BA3,CXT,CLAM,6,NMODET,6,6,26,6)
CALL MULTAD (BA4,CXC,CLAM,6,NMODEC,6,6,26,6)
CALL INV2NP (CLAM,CLAMI,6,6)

```

C

```
IF (JIL .NE. 4) RETURN
```

C

```

CALL MULT3 (BA1,Y(NUT),V1,6,6,1,6,150,6)
CALL MULT3 (BA2,Y(NUC),V2,6,6,1,6,150,6)
CALL MULT3 (BA3,Y(NXITDT),V3,6,NMODET,1,6,150,6)
CALL MULT3 (BA4,Y(NXICDT),V4,6,NMODEC,1,6,150,6)
DO 60 I=1,6
60 RV(I) = -V1(I) + V2(I) - V3(I) + V4(I)
CALL MULT3 (CLAMI,RV,VFLAM,6,6,1,6,6,6)
DO 65 I=1,6
65 VI(I) = -VFLAM(I)
CALL MULTAD (CUT,VFLAM,Y(NUT),6,6,1,6,6,150)
CALL MULTAD (CUC,VI,Y(NUC),6,6,1,6,6,150)
CALL MULTAD (CXT,VFLAM,Y(NXITDT),NMODET,6,1,26,6,150)
CALL MULTAD (CXC,VI,Y(NXICDT),NMODEC,6,1,26,6,150)
RETURN

```

C

C

```

200 CALL MULT3 (HATD,Y(NXITDT),TDDTR,3,NMODET,1,3,150,3)
CALL MULT3 (HATP,Y(NXICDT),CPDTR,3,NMODEC,1,3,150,3)
CALL MULT3 (SIGATD,Y(NXITDT),OMDT,3,NMODET,1,3,150,3)
CALL MULT3 (SIGATP,Y(NXICDT),OMPC,3,NMODEC,1,3,150,3)
DO 70 I=1,3
  I1 = NUT + I + 2
  I2 = NUC + I + 2

```

OMGD(I) = Y(I1) + OMOT(I)
 70 OMGP(I) = Y(I2) + OMPC(I)

C

VEC1(1)=Y(NUT)+Y(NUT+4)*TDT(3)-Y(NUT+5)*TDT(2)+2.*TDDTR(1)
 VEC1(2)=Y(NUT+1)+Y(NUT+5)*TDT(1)-Y(NUT+3)*TDT(3)+2.*TDDTR(2)
 VEC1(3)=Y(NUT+2)+Y(NUT+3)*TDT(2)-Y(NUT+4)*TDT(1)+2.*TDDTR(3)
 VEC2(1) = OMGD(2)*DFT(3) - OMGD(3)*DFT(2)
 VEC2(2) = OMGD(3)*DFT(1) - OMGD(1)*DFT(3)
 VEC2(3) = OMGD(1)*DFT(2) - OMGD(2)*DFT(1)
 VEC3(1)=Y(NUC)+Y(NUC+4)*CPC(3)-Y(NUC+5)*CPC(2)+2.*CPDTR(1)
 VEC3(2)=Y(NUC+1)+Y(NUC+5)*CPC(1)-Y(NUC+3)*CPC(3)+2.*CPDTR(2)
 VEC3(3)=Y(NUC+2)+Y(NUC+3)*CPC(2)-Y(NUC+4)*CPC(1)+2.*CPDTR(3)
 VEC4(1) = OMGP(2)*PFC(3) - OMGP(3)*PFC(2)
 VEC4(2) = OMGP(3)*PFC(1) - OMGP(1)*PFC(3)
 VEC4(3) = OMGP(1)*PFC(2) - OMGP(2)*PFC(1)

C

I = NUT + 3
 J = NUT + 4
 K = NUT + 5
 RV(1) = -Y(J)*VEC1(3)+Y(K)*VEC1(2)-OMGD(2)*VEC2(3)+OMGD(3)*VEC2(2)
 RV(2) = -Y(K)*VEC1(1)+Y(I)*VEC1(3)-OMGD(3)*VEC2(1)+OMGD(1)*VEC2(3)
 RV(3) = -Y(I)*VEC1(2)+Y(J)*VEC1(1)-OMGD(1)*VEC2(2)+OMGD(2)*VEC2(1)
 I = NUC + 3
 J = NUC + 4
 K = NUC + 5
 VEC1(1)=Y(J)*VEC3(3)-Y(K)*VEC3(2)+OMGP(2)*VEC4(3)-OMGP(3)*VEC4(2)
 VEC1(2)=Y(K)*VEC3(1)-Y(I)*VEC3(3)+OMGP(3)*VEC4(1)-OMGP(1)*VEC4(3)
 VEC1(3)=Y(I)*VEC3(2)-Y(J)*VEC3(1)+OMGP(1)*VEC4(2)-OMGP(2)*VEC4(1)
 CALL MULTAD (TRTC,VEC1,RV,3,3,1,3,3,6)

C

RV(4) = 0.0
 RV(5) = 0.0
 RV(6) = 0.0

C

CALL MULT3 (BA1,YDT(NUT),V1,6, 6,1,6,150,6)
 CALL MULT3 (BA2,YDT(NUC),V2,6, 6,1,6,150,6)
 CALL MULT3 (BA3,YDT(NXITDT),V3,6,NMODET,1,6,150,6)
 CALL MULT3 (BA4,YDT(NXICDT),V4,6,NMODEC,1,6,150,6)
 DO 80 I=1,6
 80 RV(I) = RV(I) - V1(I) + V2(I) - V3(I) + V4(I)
 CALL MULT3 (CLAM1,RV,VLAM,6,6,1,6,6,6)
 DO 85 I=1,6
 85 VI(I) = -VLAM(I)
 CALL MULTAD (CUT,VLAM,YDT(NUT),6, 6,1, 6,6,150)
 CALL MULTAD (CUC,V1 ,YDT(NUC),6, 6,1, 6,6,150)
 CALL MULTAD (CXT,VLAM,YDT(NXITDT),NMODET,6,1,26,6,150)
 CALL MULTAD (CXC,V1 ,YDT(NXICDT),NMODEC,6,1,26,6,150)
 RETURN
 END

SUBROUTINE HSIG

```

C
C SUBROUTINE TO SELECT CERTAIN AMPLITUDES (ROWS) AND MODES (COLUMNS)
C OF THE CHASE AND TARGET VEHICLE VIBRATION MODAL MATRICES.
C
C SUBROUTINES CALLED ARE -- READ, READIM AND REVISE.
C
C CODED BY CARL BODLEY, JULY 1969
C
C   DIMENSION AWORK(100,100), VWORK(100), JVEC(100), IVEC(100)
C
C   COMMON /MFREQD/ FREQT(26), FREQC(26), ZETAT, ZETAC
C   COMMON /MODATA/ HATD(3,26),SIGATD(3,26), HATF(3,26),SIGATP(3,26)
C   COMMON /NMODES/ NMODET, NMODEC, IFELAS
C
C   DATA NIT,NOT/5,6/
C
C   READ (NIT,1002) IFELAS, NMODET, NMODEC, ZETAT, ZETAC
1002 FORMAT (3I5, 2E10.0)
C
C   IF (IFELAS .EQ. 0) GO TO 200
C
C   DO 100 L=1,2
C   CALL READ (VWORK,N1,NCF,1,100)
C   CALL READ (AWORK,NR,NC,100,100)
C   CALL READIM (JVEC,N1,NC1,1,100)
C   IF (NC1 .NE. NC .OR. NCF .NE. NC) GO TO 999
C   NM = 0
C   DO 10 I=1,NC
C   IF (JVEC(I) .NE. 0) NM = NM + 1
10 CONTINUE
C   GO TO (51,52), L
C 51 IF (NM .NE. NMODET) GO TO 999
C   GO TO 53
C 52 IF (NM .NE. NMODEC) GO TO 999
C 53 CALL READIM (IVEC,N1,NC1,1,100)
C   IF (NC1 .NE. NR) GO TO 999
C   N3 = 0
C   DO 20 I=1,NR
C   IF (IVEC(I) .NE. 0) N3 = N3 + 1
20 CONTINUE
C   IF (N3 .NE. 3) GO TO 999
C -----REVISE TO FORM H (DEFL. AMPLITUDE) -----
C   GO TO (54,55), L
C 54 CALL REVISE (AWORK,IVEC,JVEC,HATD ,NR,NC,3,NMODET,100,3)
C   GO TO 56
C 55 CALL REVISE (AWORK,IVEC,JVEC,HATP ,NR,NC,3,NMODEC,100,3)
C 56 CALL READIM (IVEC,N1,NC1,1,100)
C   IF (NC1 .NE. NR) GO TO 999
C   N3 = 0
C   DO 30 I=1,NR
C   IF (IVEC(I) .NE. 0) N3 = N3 + 1
30 CONTINUE
C   IF (N3 .NE. 3) GO TO 999
C -----REVISE TO FORM SIG SLOPE AMPLITUDE -----
C   GO TO (57,58), L
C 57 CALL REVISE (AWORK,IVEC,JVEC,SIGATD,NR,NC,3,NMODET,100,3)
C   CALL REVISE (VWORK,1,JVEC,FREQT,1,NC,1,NMODET,1,1)
C   GO TO 100
C 58 CALL REVISE (AWORK,IVEC,JVEC,SIGATP,NR,NC,3,NMODEC,100,3)
C   CALL REVISE (VWORK,1,JVEC,FREQC,1,NC,1,NMODEC,1,1)
100 CONTINUE

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```
C      RETURN
C
200  NMODET = 1
      NMODEC = 1
      ZETAT = 0.0
      ZETAC = 0.0
      FREQT(1) = 0.0
      FREQC(1) = 0.0
      DO 210 I=1,3
        MATD(I,1) = 0.0
        MATP(I,1) = 0.0
        SIGATD(I,1) = 0.0
210  SIGATP(I,1) = 0.0
C      RETURN
C
999  WRITE (NOT,1001)
1001 FORMAT (33H1DATA INTO HSI6 IS NOT COMPATIBLE/
•      17H0PROGRAM STOPPED.)
C      STOP
C      END
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SUBROUTINE INV2NP (A,B,N,KR)
DIMENSION A(KR,1), B(KR,1), W(150), U(150), IV(150),
*       IRE(150), BIN(150)
DATA NIT,NOT/5,6/
C
C MATRIX INVERSION (A** - I = B) -- RANK ANNIHILATION METHOD.
C ALGORITHM FORMULATED BY CARL BODLEY.
C THE INVERSION CHECK B*A IS CALCULATED AND PRINTED.
C CALLS SUBROUTINE PAGEHD.
C THE MAXIMUM SIZE IS
C   N = 150
C CODED BY CARL BODLEY JANUARY, 1967.
C
C SUBROUTINE ARGUMENTS
C A = INPUT MATRIX TO BE INVERTED. SIZE(N,N).
C B = OUTPUT MATRIX INVERSE OF A. SIZE(N,N).
C N = INPUT SIZE OF MATRICES A AND B. (MAX=150).
C KR = INPUT ROW DIMENSION OF MATRICES A AND B IN CALLING PROGRAM.
C
1001 FORMAT (25HIN EXCEEDS INV2 ALLOWABLE./ 17HOPROGRAM STOPPED.)
1003 FORMAT (///10X,45HSUBROUTINE INV2 HAS CALCULATED THE DATA BELOW
*       ///10X,40HTHE DIAGONALS OF INVERSION CHECK B*A ARE
*       // (8X,7E16.8))
1004 FORMAT (///10X,42HTHE MAXIMUM OFF-DIAGONAL ELEMENT OF B*A IS
*       E17.8, 2X, 4HAT ( I3, 1H, I3, 1H) )
1006 FORMAT (19HIMATRIX IS SINGULAR/ 17HOPROGRAM STOPPED.)
C
IF (N .GT. 150) GO TO 97
IF (N .EQ. 1 .AND. A(1,1) .EQ. 0.0) GO TO 99
IF (N .EQ. 1 .AND. A(1,1) .NE. 0.0) GO TO 98
C
C GENERATE INITIAL ROW INDICES.
IT = 1
GO TO 90
91 IT = 2
90 DO 5 I=1,N
IRE(I) = I
5 IV(I) = I
C
C CONDITION A FOR MAXIMUM DIAGONAL ELEMENTS
NM1 = N - 1
DO 6 L=1,NM1
SMAX = 0.0
DO 8 J=L,N
LA = IRE(J)
I = L
K = LA
IF (IT .EQ. 2) I = LA
IF (IT .EQ. 2) K = L
IF (ABS(A(K,I)) .LE. SMAX) GO TO 8
JMAX = J
SMAX = ABS(A(K,I))
8 CONTINUE
LS = IRE(L)
IRE(L) = IRE(JMAX)
6 IRE(JMAX) = LS
DO 7 L=1,N
LA = IRE(L)
BIN(L) = A(LA,L)
IF (IT .EQ. 2) BIN(L) = A(L,LA)
7 IF (BIN(L) .EQ. 0.0) BIN(L) = 1.0
C

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C GENERATE INITIAL B AND ABAR
  DO 10 L=1,N
    LA = IRE(L)
    I = L
    K = LA
    IF (IT .EQ. 2) I = LA
    IF (IT .EQ. 2) K = L
    DO 15 J=1,N
      M = J
      M1 = LA
      IF (IT .EQ. 2) M = LA
      IF (IT .EQ. 2) M1 = J
    15 B(M,M1) = 0.0
      B(I,K) = 1.0/BIN(L)
    10 A(K,I) = A(K,I) - BIN(L)
C
C INVERSION LOOP, USES ROW OF ABAR WITH MAXIMUM S.
  DO 35 L=1,N
    SMAX = 0.0
    DO 23 J=L,N
      LA = IV(J)
      S = 1.0
      DO 26 K=1,N
    26 S = S + A(LA,K)*B(K,LA)
        IF (ABS(S) .LE. SMAX) GO TO 23
        LMAX = J
        SMAX = ABS(S)
    23 CONTINUE
        IF (SMAX .GT. 1.0E-99) GO TO 60
        IF (IT .EQ. 2) GO TO 99
        GO TO 65
    60 LS = IV(L)
        IV(L) = IV(LMAX)
        IV(LMAX) = LS
        LA = IV(L)
        DO 25 I=1,N
          W(I) = 0.0
        DO 25 J=1,N
    25 W(I) = W(I) + A(LA,J)*B(J,I)
          S = 1.0 + W(LA)
        DO 30 I=1,N
    30 U(I) = B(I,LA)
          DO 35 I=1,N
            DO 35 J=1,N
    35 B(I,J) = B(I,J) - U(I)*W(J)/S
C
C RESTORE A
  65 DO 40 L=1,N
    LA = IRE(L)
    I = L
    K = LA
    IF (IT .EQ. 2) I = LA
    IF (IT .EQ. 2) K = L
    40 A(K,I) = A(K,I) + BIN(L)
    IF (SMAX .LE. 1.0E-99) GO TO 91
C
  RETURN
C
  98 B(1,1) = 1.0/A(1,1)
  RETURN
  99 WRITE (NOT,1006)
  STOP

  97 WRITE (NOT,1001)
  STOP
  END

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SUBROUTINE KINMAT

C
C
C
C
CCOMPUTES KINEMATICS FROM ROTATION TRANSFORMATIONS
AND GEOMETRY

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COMMON /ANGLES/ ALPHAD, SALPD, CALPD, TALPD, SSIGMA(3), CSIGMA(3)
COMMON /BTDATA/ TRHO(9,6), BLS(10,6), BLV(7,39)
COMMON /FUNGAM/ SGAMMA(3), CGAMMA(3), SGSS(3), SGCS(3),
                CGSS(3), CGCS(3)
* COMMON /GEOMTY/ AA, AB, AD, AE, AF, AP, DLB, DLD, DLE, DLF, DLI, DLP, DLO, DLS,
*                TDTO(3), CPCO(3), RADCON, CSPHER, ROTALP, PEO, FDO
COMMON /LIPARM/ FLAMC(3), QRMAG(3)
COMMON /LOCPTC/ CSC(3), CAC(3,3), CQC(3,3),
*                CPC(3), PSC(3), PAC(3,3), PQC(3,3)
COMMON /LOCPTD/ DSD(3), DHD(3), DGD(3), DAD(3,3), DRD(3,3),
*                DDD(3,3), QRD(3,3)
*                DHPD(3), DBD(3,3), DFD(3,3), DPD(3,3)
COMMON /LOCPTH/ DSH(3)
COMMON /LOCPTP/ PSP(3), PAP(3,3), POP(3,3)
COMMON /LOCPTT/ THT(3), TCT(3), TST(3), TAT(3,3), TRT(3,3),
*                CST(3), CAT(3,3), QRT(3,3), TOT(3),
*                DHT(3), DGT(3), DST(3), DAT(3,3), DQT(3,3), DRT(3,3)
COMMON /MODATA/ HATD(3,26), SIGATD(3,26), HATP(3,26), SIGATP(3,26)
COMMON /NMODES/ NMODET, NMODEC, IFELAS
COMMON /PHILAM/ PHICON(10), ALAM(10), MODE(10)
COMMON /SKEWMS/ TDTSQ(3,3), THTSQ(3,3), TRTSQ(3,3,3), DRTSQ(3,3,3),
*                PSCSQ(3,3), PSPPSQ(3,3), PCCSQ(3,3,3), POPPSQ(3,3,3),
*                CSCSQ(3,3), CQCSQ(3,3,3), DHTSQ(3,3)
COMMON /SLIDFR/ HDMU, ARMMU, BFV(8,39)
COMMON /TIMESS/ STARTT, DELTAT, T, ENDT, TMST, NSECS
COMMON /TRNFMS/ TRTI(3,3), TRCI(3,3), TRTC(3,3), TRHT(3,3), TRHC(3,3),
*                TRRT(3,3,3), TRRC(3,3,3), TRPC(3,3), TRDT(3,3),
*                TRPD(3,3), TRHD(3,3), TRRD(3,3,3), TRPT(3,3),
*                TRHP(3,3), TRTP(3,3), TRRP(3,3,3)
COMMON /VECMAG/ FOMAG(3), PEMAG(3)
COMMON /VECTOR/ Y(150), YDT(150)
COMMON /YPSTNS/ NUT, NXT, NGAMT, NUC, NXC, NGAMC, NRHO,
*                NXITD, NXIT, NXICD, NXIC, NDELCS

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C

DIMENSION TEMP(3,26), TEMO(3,26), CGAM(3,3)

C

DATA IFSF /1/

C

IF (TMST. GT. 0.0) GO TO 2

C

COSALP = CSPHER/SALPD

IF (HDMU.EQ.0.0 .AND. ARMMU.EQ.0.0) IFSF = 0

C

CALL ZERO (TRHO,6,6,9)

CALL ZERO (BLS,10,6,10)

CALL ZERO (BLV(5,1),3,3,7)

C

DO 1 I=1,3

BLV (I+4,I) = -1.0

1 TRHO(I,I) = 1.0

C

2 CONTINUE

C

CALL SKEWV (TDT, TDTSQ)

C

DO 4 I=1,3

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I3 = I+3
C
TRM1 = DLD*SGAMMA(I) - AD*CGAMMA(I)
TRM2 = DLD*CGAMMA(I) + AD*SGAMMA(I)
TRM3 = AF-AA-TRM1
C
FDI = DLI - DLF + Y(NRHO) - TRM2
FDJ = TRM3*SSIGMA(I)
FDK = -TRM3*CSIGMA(I)
FDMAG(I) = SORT(FDI*FDI+FDJ*FDJ+FDK*FDK)
C
UAJX = FDI/FDMAG(I)
UAJY = FDJ/FDMAG(I)
UAJZ = FDK/FDMAG(I)
C
TRHO(I3, 1) = UAJX
TRHO(I3,I3) = TRM1*UAJX + TRM2*(UAJZ*CSIGMA(I) - UAJY*SSIGMA(I))
C
TRM1 = DLE*SGAMMA(I) - AE*CGAMMA(I)
TRM2 = DLE*CGAMMA(I) + AE*SGAMMA(I)
TRM3 = AP-AA-TRM1
C
PEI = DLI - DLP + Y(NRHO) - TRM2
PEJ = TRM3*SSIGMA(I)
PEK = -TRM3*CSIGMA(I)
PEMAG(I) = SORT(PEI*PEI+PEJ*PEJ+PEK*PEK)
C
UTJX = PEI/PEMAG(I)
UTJY = PEJ/PEMAG(I)
UTJZ = PEK/PEMAG(I)
C
BL5(I, 1) = -UTJX
BL5(I,I3) = -TRM1*UTJX - TRM2*(UTJZ*CSIGMA(I) - UTJY*SSIGMA(I))
C
4 CONTINUE
C
CALL SKEWV (THT, THTSQ)
CALL SKEWV (CSC, CSCSQ)
CALL SKEWV (DHT, DHTSQ)
CALL SKEWV (PSC, PSCSQ)
CALL SKEWV (PSP, PSPPSQ)
C
PSPPSQ(1,1) = 1.0
PSPPSQ(2,1) = 0.0
PSPPSQ(3,1) = 0.0
C
DO 10 J=1,3
IF (IFSF .EQ. 0) GO TO 10
BFV(1,J) = TRHT(1,J)
BFV(2,J) = TRHT(3,J)
10 BLV(1,J) = TRHT(2,J)
C
CALL MULT3(TRHT(2,1),TTSQ,BLV(1,4),1,3,3,3,7)
IF (IFSF .NE. 0)
*CALL MULT3(TRHT(1,1),THTSQ,BFV(1,4),1,3,3,3,8)
IF (IFSF .NE. 0)
*CALL MULT3(TRHT(3,1),THTSQ,BFV(2,4),1,3,3,3,8)
C
DO 11 J=1,3
IF (IFSF .EQ. 0) GO TO 11
BFV(1,J+6) = -TRHC(1,J)
BFV(2,J+6) = -TRHC(3,J)

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11 BLV(1,J+6) = -TRHC(2,J)
C
  CALL MULT3(TRHC(2,1),CSCSQ,BLV(1,10),1,3,3,3,3,7)
  IF (IFSF.NE.0)
  *CALL MULT3(TRHC(1,1),CSCSQ,BFV(1,10),1,3,3,3,3,8)
  IF (IFSF.NE.0)
  *CALL MULT3(TRHC(3,1),CSCSQ,BFV(2,10),1,3,3,3,3,8)
C
  CALL MULT (DHTSQ,SIGATD,TEMP,3,3,NMODET,3,3)
  CALL AAB8 (1.0,HATD,1.0,TEMP,TEMQ,3,NMODET,3)
  CALL MULT3(TRHT(2,1),TEMQ,BLV(1,13),1,3,NMODET,3,3,7)
  IF (IFSF.NE.0)
  *CALL MULT3(TRHT(1,1),TEMQ,BFV(1,13),1,3,NMODET,3,3,8)
  IF (IFSF.NE.0)
  *CALL MULT3(TRHT(3,1),TEMQ,BFV(2,13),1,3,NMODET,3,3,8)
C
  CALL MULT (PSCSQ,SIGATP,TEMP,3,3,NMODEC,3,3)
  CALL AAB8 (1.0,HATP,1.0,TEMP,TEMQ,3,NMODEC,3)
  CALL MULT3(TRHC(2,1),TEMQ,BLV(1,13+NMODET),1,3,NMODEC,3,3,7)
  IF (IFSF.NE.0)
  *CALL MULT3(TRHC(1,1),TEMQ,BFV(1,13+NMODET),1,3,NMODEC,3,3,8)
  IF (IFSF.NE.0)
  *CALL MULT3(TRHC(3,1),TEMQ,BFV(2,13+NMODET),1,3,NMODEC,3,3,8)
C
  CALL MULT3(TRTC,TEMQ,BLV(5,13+NMODET),3,3,NMODEC,3,3,7)
C
  CALL MULT3(TRHP(2,1),PSPPSQ,BL5(4,1),1,3,3,3,3,10)
C
  CALL MULT3(TRTP,PSPPSQ,BL5(8,1),3,3,3,3,3,10)
C
  DO 16 I=1,3
  I4 = I+4
C
  DO 14 J=1,3
  J3 = J+3
  J6 = J+6
  BLV(I4,J3) = -TDTSQ(I,J)
14 BLV(I4,J6) = TRTC(I,J)
C
  DO 15 J=1,NMODET
15 BLV(I4,J+12) = -HATD(I,J)
C
16 CONTINUE
C
  CALL MULT3(TRTC,CSCSQ,BLV(5,10),3,3,3,3,3,7)
C
  DO 50 K=1,3
  K1 = K+1
  K2 = 2*K+1
  K3 = K2+1
C
  CALL SKEWV (TRT(1,K), TRTSQ(1,1,K))
  CALL SKEWV (CQC(1,K), CQCSQ(1,1,K))
  CALL SKEWV (DRT(1,K), DRTSQ(1,1,K))
  CALL SKEWV (POC(1,K), POCsq(1,1,K))
  CALL SKEWV (POP(1,K), POPPSQ(1,1,K))
C
  POPPSQ(1,1,K) = 1.0
  POPPSQ(2,1,K) = 0.0
  POPPSQ(3,1,K) = 0.0
C
  DO 20 J=1,3

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IF (IFSF .EQ. 0) GO TO 20
BFV(K2,J) = TRRT(1,J,K)
BFV(K3,J) = TRRT(3,J,K)
20 BLV(K1,J) = TRRT(2,J,K)
C
CALL MULT3(TRRT(2,1,K),TRTSQ(1,1,K),BLV(K1,4),1,3,3,3,3,7)
IF (IFSF .NE. 0)
*CALL MULT3(TRRT(1,1,K),TRTSQ(1,1,K),BFV(K2,4),1,3,3,3,3,8)
IF (IFSF .NE. 0)
*CALL MULT3(TRRT(3,1,K),TRTSQ(1,1,K),BFV(K3,4),1,3,3,3,3,8)
C
DO 22 J=1,3
IF (IFSF .EQ. 0) GO TO 22
BFV(K2,J+6) = -TRRC(1,J,K)
BFV(K3,J+6) = -TRRC(3,J,K)
22 BLV(K1,J+6) = -TRRC(2,J,K)
C
CALL MULT3(TRRC(2,1,K),CQCSQ(1,1,K),BLV(K1,10),1,3,3,3,3,7)
IF (IFSF .NE. 0)
*CALL MULT3(TRRC(1,1,K),CQCSQ(1,1,K),BFV(K2,10),1,3,3,3,3,8)
IF (IFSF .NE. 0)
*CALL MULT3(TRRC(3,1,K),CQCSQ(1,1,K),BFV(K3,10),1,3,3,3,3,8)
C
CALL MULT (DRTSQ(1,1,K),SIGATD,TEMP,3,3,NMODET,3,3)
CALL AAB (1,0,HATD,1,0,TEMP,TEMQ,3,NMODET,3)
CALL MULT3(TRRT(2,1,K),TEMQ,BLV(K1,13),1,3,NMODET,3,3,7)
IF (IFSF .NE. 0)
*CALL MULT3(TRRT(1,1,K),TEMQ,BFV(K2,13),1,3,NMODET,3,3,8)
IF (IFSF .NE. 0)
*CALL MULT3(TRRT(3,1,K),TEMQ,BFV(K3,13),1,3,NMODET,3,3,8)
C
CALL MULT (PQCSQ(1,1,K),SIGATP,TEMP,3,3,NMODEC,3,3)
CALL AAB (1,0,HATP,1,0,TEMP,TEMQ,3,NMODEC,3)
CALL MULT3(TRRC(2,1,K),TEMQ,BLV(K1,13+NMODET),1,3,NMODEC,3,3,7)
IF (IFSF .NE. 0)
*CALL MULT3(TRRC(1,1,K),TEMQ,BFV(K2,13+NMODET),1,3,NMODEC,3,3,8)
IF (IFSF .NE. 0)
*CALL MULT3(TRRC(3,1,K),TEMQ,BFV(K3,13+NMODET),1,3,NMODEC,3,3,8)
C
CALL MULT3(TRRP(2,1,K),PQPPSQ(1,1,K),BL5(K+4,1),1,3,3,3,3,10)
C
CGAM(1,K) = FLAMC(K)+SGAMMA(K)
CGAM(2,K) = -FLAMC(K)+CGSS(K)
CGAM(3,K) = FLAMC(K)+CGCS(K)
C
CALL MULT3(TRRP(2,1,K),CGAM(1,K),BL5(K+4,K+3),1,3,1,3,3,10)
C
50 CONTINUE
C
JT = 12+NMODET
C
DO 69 I=1,4
I3 = I+3
I4 = I+4
C
DO 60 J=10,12
IF (IFSF .EQ. 0) GO TO 60
BFV(I, J) = BFV(I, J)
BFV(I4, J) = -BFV(I4, J)
60 BLV(I, J) = -BLV(I, J)
C
DO 62 J=1,NMODEC

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```
JJ = J+JT
IF (IFSF .EQ. 0) GO TO 62
BFV( I,JJ) = -BFV( I,JJ)
BFV(I4,JJ) = -BFV(I4,JJ)
62 BLV( I,JJ) = -BLV( I,JJ)
C
DO 64 J=1,3
64 BL5(I3, J) = -BL5(I3, J)
C
69 CONTINUE
C
DO 70 I=4,6
I1 = I+1
70 BL5(I1, I) = -BL5(I1,I)
C
DO 72 I=1,3
I4 = I+4
PHICON( I) = PED - PEMAG(I)
72 PHICON(I4) = ORMAG(I) - AB
C
PHICON( 4) = -DSH(2) - CSPHER
PHICON( 8) = DSD(1) - COSALP
PHICON( 9) = DSD(2)
PHICON(10) = DSD(3)
C
RETURN
END
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SUBROUTINE LAMRHO

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C
COMMON /BINDFC/ FI,BINDMU
COMMON /BTDATA/ TRHO(9,6), BLS(10,6), BLV(7,39)
COMMON /GEOMTY/ AA,AB,AD,AE,AF,AP,DLB,DLQ,DLE,DLF,DLI,DLP,DLQ,OLS,
*   TOTO(3),CPCO(3),RADCON,CSPHER,ROTALP,PEO,FDO
COMMON /IFOUTS/ MINIC,IFPLOT,IFPER
COMMON /JCOUNT/ JIL
COMMON /MISCNO/ ANUM
COMMON /NMODES/ NMODET, NMODEC, IFELAS
COMMON /PHILAM/ PHICON(10),ALAM(10), MODE(10)
COMMON /RETRCT/ AKD1,AKD2,AKD3,RHOS0,FRETL,EXTL,TLAG,TSTAR,FRET
COMMON /SPRDMP/ FSPRNG(2,20,4),FDAMP(2,20,4)
COMMON /TIMESS/ STARTT,DELTAT, T, ENDT, TMST, NSECS
COMMON /TRNFMS/ TRI(3,3),TRCI(3,3),TRTC(3,3),TRHT(3,3),TRHC(3,3),
*   TRRT(3,3,3),TRRC(3,3,3),TRPC(3,3),TRD*(3,3),
*   TRPD(3,3),TRHD(3,3),TRRD(3,3,3),TRPT(3,3)
*   ,TRHP(3,3),TRTP(3,3),TRRP(3,3,3)
COMMON /VECMAG/ FDMAG(3), PEMAG(3)
COMMON /VECTOR/ Y(150),YDT(150)
COMMON /YPSTNS/ NUT,NXT,NGAMT,NUC,NXC,NGAMC,NRHO,
*   NXITDT,NXIT,NXICDT,NXIC, NDELCS

C
DIMENSION BC(6,6),BCI(6,6),MKV(6),VM(10),FD(6),DDOT(6),
*   IVEC(10),JVEC(6),VCON(10),FT(6),SIDF(2),WV3(3),ANVEC(3)

C
DATA JVEC/1,2,3,4,5,6/
DATA IIST,CKV / 0, 0.9975 /
DATA BTOL,MAXITR/ 5., 15 /
DATA NIT,NOT /5, 6 /

C
IF (IIST .GT. 0) GO TO 7
FROXU = (DLQ+2.*DLS+EXTL)/(DLQ-EXTL)
NALY = NRHO + 1
NALZ = NRHO + 2

C
ISCD = 13 + NMODET
DO 15 I=1,3
15 VM (I) = 0.

C
IIST = 1
7 CALL MULT3 (BLV ,Y( NUT),VM ( 4),7, 6,1,7,150,10)
CALL MULTAD (BLV(1, 7),Y( NUC),VM ( 4),7, 6,1,7,150,10)
CALL MULTAD (BLV(1, 13),Y(NXITDT),VM ( 4),7,NMODET,1,7,150,10)
CALL MULTAD (BLV(1,ISCD),Y(NXICDT),VM ( 4),7,NMODEC,1,7,150,10)

C
100 IVEC(4) = 0
DO 17 I=1,3
IP4 = I + 4
IP7 = I + 7
IVEC(I ) = MODE(I )
IVEC(IP4) = MODE(IP4)
IF (MODE(I) .EQ. 0 .AND. MODE(IP4) .EQ. 0) IVEC(IP4) = 1
17 IVEC(IP7) = 1

C
NVAL = 0
DO 20 I=1,10
VCON(I) = -VM(I)
IF (IVEC(I) .EQ. 0) GO TO 20
NVAL = NVAL + 1
IVEC(I) = NVAL
20 CONTINUE

```

```

C
CALL REVISE (RL5,IVEC,JVEC,BC,10,6,6,6,10,6)
CALL REVISE (VCON ,IVEC,JVEC(1),MKV,10,1,6,1,10,6)
C
IF (MODE(4) .EQ. 1 .OR. MODE(8) .EQ. 1) GO TO 105
WV3(1) = (1.0-CKV)*(EXTL-Y(NRHO))/DELTAT
WV3(2) = (CKV-1.0)*Y(NALY)/DELTAT
WV3(3) = (CKV-1.0)*Y(NALZ)/DELTAT
CALL MULT3 (BC(4,1),WV3,MKV(4),3,3,1,6,2,6)
GO TO 50
105 IF (MODE(4) .EQ. 0) GO TO 50
C
DO 25 I=1,3
25 MKV(I+3) = VM(4)*TRHT(2,I)
C
50 CALL INV2NP (BC,BCI,6,6)
CALL MULT3 (BCI,MKV,YDT(NRHO),6,6,1,6,6,150)
DO 65 I=1,3
NGM = NRHO + 2 + I
IP4 = I + 4
IF (MODE(I) .EQ. 1 .OR. MODE(IP4) .EQ. 1) GO TO 65
YDT(NGM) = (1.0-CKV)*(49.*ANUM-Y(NGM))/DELTAT
65 CONTINUE
C
CALL MULT3 (TRHC,YDT(NRHO),DDOT,6,6,1,9,150,6)
C
C
C
CALL FTABLE (Y(NRHO),FD(1),SLOPE,BINTR,FSPRNG(1,1,1),
* FSPRNG(1,1,1),1,MM)
STEST = Y(NALY)*YDT(NALY)
IF (STEST .GE. 0.) CALL FTABLE (Y(NALY),FD(2),SLOPE,BINTR,
* FSPRNG(1,1,2),FSPRNG(1,1,2),1,MM)
IF (STEST .LT. 0.) CALL FTABLE (Y(NALY),FD(2),SLOPE,BINTR,
* FSPRNG(1,1,3),FSPRNG(1,1,3),1,MM)
STEST = Y(NALZ)*YDT(NALZ)
IF (STEST .GE. 0.) CALL FTABLE (Y(NALZ),FD(3),SLOPE,BINTR,
* FSPRNG(1,1,2),FSPRNG(1,1,2),1,MM)
IF (STEST .LT. 0.) CALL FTABLE (Y(NALZ),FD(3),SLOPE,BINTR,
* FSPRNG(1,1,3),FSPRNG(1,1,3),1,MM)
DO 40 I=1,3
IP3 = I + 3
40 CALL FTABLE (FDMAG(I),FD(IP3),SLOPE,BINTR,FSPRNG(1,1,4),
* FSPRNG(1,1,4),1,MM)
C
CALL RETRAK
FD (1) = FD (1) + FRET
C
DO 27 I=1,6
IL = 4
IF (I .LE. 3) IL = I
CALL FTABLE (DDOT(I),FDD,SLOPE,BINTR,FDAMP(1,1,IL),
* FDAMP(1,1,IL),1,MM)
27 FT(I) = FD(I) + FDD
C
DO 600 I=1,7
IF (IVEC(I) .EQ. 0) GO TO 600
NCN = IVEC(I)
ANVEC(NCN) = MODE(I)
600 CONTINUE
C
CALL MULY3 (FT,TRHO,FD,1,6,6,1,9,1)

```

```

      CALL MULT3 (FD(4),BCI(4,1),WV3,1,3,3,1,6,1)
      DO 605 I=1,3
605  WKV(I) = WV3(I)*ANVEC(I)
      DO 610 I=1,3
      WV3(I) = FD(I)
      DO 610 J=1,3
610  WV3(I) = WV3(I) - WKV(J)*BC(J,I)
      CALL MULT3 (WV3,BCI(1,4),WKV(4),1,3,3,1,6,1)
      FI = 0.
      IF (MODE(4) .EQ. 1 .OR. MODE(8) .EQ. 1) GO TO 652
      DO 615 I=4,6
615  WKV(I) = 0.
      GO TO 151
652  RODMAG = ABS(DDOT(1))
      IF (RODMAG .LT. 1.E-9) GO TO 151
      VALUE = (DLQ+2.*DLS*Y(NRMH))/ (DLQ-Y(NRMH))
      VALUE = BINDMU*VALUE/FROXD
      ICNT = 0
153  CALL MULT3 (TRPT(2,1),WKV(4),SIDF,2,3,1,3,6,2)
      FSID = SQRT(SIDF(1)*SIDF(1) + SIDF(2)*SIDF(2))
      FIP1 = (DDOT(1)/RODMAG)*VALUE*FSID
      FBDLT = FIP1 - FI
      IF (ABS(FBDLT) .LE. BTOL) GO TO 151
      ICNT = ICNT + 1
      IF (ICNT .EQ. MAXITR) GO TO 999
      FI = FIP1
      DO 152 I=4,6
152  WKV(I) = WKV(I) + FBDLT*BCI(I,I)
      GO TO 153
C
151  DO 45 I=1,10
      IV = IVEC(I)
      ALAM(I) = 0.
      IF (IV .EQ. 0) GO TO 45
      IF (MODE(IV) .EQ. 1) ALAM(I) = WKV(IV)
45  CONTINUE
      IF (MODE(4) .EQ. 1) ALAM(4) = -TRHT(2,1)*WKV(4)
      *      - TRHT(2,2)*WKV(5) - TRHT(2,3)*WKV(6)
C
      IF (JIL .NE. 4) RETURN
C
      IF (ALAM(4) .GE. 0.) GO TO 57
      MODE(4) = 0
      GO TO 100
57  IFT = 0
      DO 55 I=1,7
      IF (ALAM(I) .GE. 0.) GO TO 55
      IFT = 1
      MODE(I) = 0.
55  CONTINUE
C
      IF (IFT .EQ. 0) RETURN
      GO TO 100
C
999  WRITE (NOT,1001)
1001 FORMAT (36HISUBROUTINE LAMRHO DOES NOT CONVERGE/
      *      17HOPROGRAM STOPPED.;
      STOP
C
      END

```

SUBROUTINE LOCATE

```

C
C     SUBROUTINE TO ESTABLISH LOCATION OF KEY LEADING ELEMENTS
C     IN STATE VECTOR AND TO ESTABLISH LENGTH OF SUBVECTORS
C     OF STATE VECTOR
C
COMMON /LOCLN/ LOC(12), LEN(12)
COMMON /NCNTRL/ NCNSYS
COMMON /NEQTN/ NEQTN
COMMON /NMODES/ NMODET, NMODEC, IFELAS
COMMON /YPSTNS/ NUT,NXT,NGAMT,NUC,NXC,NGAMC,NRHO,
      *      NXITDT,NXIT,NXICDT,NXIC, NDELCS
C
DATA   NIT, NOT   / 5, 6 /
C
NXIT   = NXITDT + NMODET
NXICDT = NXIT + NMODET
NXIC   = NXICDT + NMODEC
NDELCS = NXIC + NMODEC
NEQTN  = NDELCS + NCNSYS - 1
C
IF (NEQTN .GT. 150) GO TO 20
C
LOC( 1) = NUT
LOC( 2) = NXT
LOC( 3) = NGAMT
LOC( 4) = NUC
LOC( 5) = NXC
LOC( 6) = NGAMC
LOC( 7) = NRHO
LOC( 8) = NXITDT
LOC( 9) = NXIT
LOC(10) = NXICDT
LOC(11) = NXIC
LOC(12) = NDELCS
C
DO 10 I=1,11
10 LEN( I) = LOC(I+1) - LOC(I)
LEN(12) = NCNSYS
C
      CALL WRITM(LOC,1,12,6H   LOC,1)
      CALL WRITM(LEN,1,12,6H   LEN,1)
C
GO TO 30
C
20 WRITE(NOT,21)
21 FORMAT(/,10X, 38MO. OF EQUATIONS EXCEEDS 150. STOP RUN)
STOP
C
30 RETURN
END

```

SUBROUTINE MINYS

C
C

```

COMMON /GEOMTY/ AA,AB,AD,AE,AF,AP,DLB,DLD,DLE,DLF,DLI,DLP,DLQ,OLS,
*             TDTO(3),CPCO(3),RADCON,CSPHER,ROTALP,PEO,FOO
COMMON /LOCPTP/ PSP(3),PAP(3,3),POP(3,3)
COMMON /MISCNO/ ANUM
COMMON /NEQNS/ NEQTN
COMMON /VECTOR/ Y(150),YDT(150)
COMMON /YPSINS/ NUT,NXT,NGAMT,NUC,NXC,NGAMC,NRHO,
*             NXITDT,NXIT,NXICDT,NXIC, NOELCS
DIMENSION TRIC(3,3),TRIT(3,3),TRTC(3,3)
DIMENSION DATMIN(6,3)
DATA NIT,NOT/ 5, 6/

```

C

```

1001 FORMAT (/// 10X,33HTHE DATMIN ARRAY IS AS FOLLOWS -- //
*10X,50H1 TARGET EULER ANGLES - PSI, THETA, PHI (DEGREES)/
*10X,58H2 CHASE / TARGET EULER ANGLES - PSI, THETA, PHI (DEGREES)/
*10X,56H3 CHASE ANGULAR VELOCITY - OMEGA X, OMEGA Y, OMEGA Z - (,
*             12HDEGREES/SEC)/
*10X,55H4 CHASE C.G. VELOCITY IN X,Y,Z DIRECTIONS REFERENCED TO,
*             19H CHASE (LENGTH/SEC)/
*10X,58H5 D TO S DISTANCE IN X,Y,Z DIRECTIONS REFERENCED TO TARGET,
*             9H (LENGTH)/
*10X,55H6 RHO(X), (LENGTH), GAMMA(1,2,3), (DEGREES), -----)

```

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```

ROUTINE READS MINIMUM INITIAL CONDITIONS AND INITIALIZES THE Y(I) VECTOR.

```

```

READ MINIMUM INITIAL CONDITIONS AS FOLLOWS.

```

```

1 TARGET EULER ANGLES - PSI, THETA, PHI - (DEGREES)

```

```

2 CHASE / TARGET EULER ANGLES - PSI, THETA, PHI (DEGREES)

```

```

3 CHASE ANGULAR VELOCITY - OMEGA X, OMEGA Y, OMEGA Z - (DEGREES/SEC)

```

```

4 CHASE C.G. VELOCITY IN X,Y,Z DIRECTIONS REFERENCED TO CHASE (LENGTH/SEC)

```

```

5 D TO S DISTANCE IN X,Y,Z DIRECTIONS REFERENCED TO TARGET (LENGTH)

```

```

6 RHO - X, (LENGTH), GAMMA (DEGREES), -----, REFERENCED TO CHASE

```

```

CALL READ (DATMIN,6,3,6,3)

```

```

ZERO SPACES AND CHANGE DEGREES TO RADIANS.

```

```

DO 5 I = 1,NEQTN

```

```

5 Y(I) = 0.0

```

```

   DATMIN(6,2) = DATMIN(6,2) * ANUM

```

```

   DO 10 I = 1,3

```

```

     DO 10 J = 1,3

```

```

       TRIT(I,J) = 0.0

```

```

       TRIC(I,J) = 0.0

```

```

       TRTC(I,J) = 0.0

```

```

10 DATMIN(I,J) = DATMIN(I,J) * ANUM

```

```

COMPUTE TRIT(I,J), TRTC(I,J), TRIC(I,J) ROTATION TRANSFORMATIONS.

```

```

CS1IT = COS(DATMIN(1,1))

```

```

CS2IT = COS(DATMIN(1,2))

```

```

CS3IT = COS(DATMIN(1,3))

```

```

SN1IT = SIN(DATMIN(1,1))

```

```

SN2IT = SIN(DATMIN(1,2))

```

```

SN3IT = SIN(DATMIN(1,3))

```

```

CS1TC = COS(DATMIN(2,1))

```

```

CS2TC = COS(DATMIN(2,2))

```

```

CS3TC = COS(DATMIN(2,3))

```

```
SN1TC = SIN(DATMIN(2,1))
SN2TC = SIN(DATMIN(2,2))
```

D

```
SN3TC = SIN(DATMIN(2,3))
TRIT(1,1) = CS1IT * CS2IT
TRTC(1,1) = CS1TC * CS2TC
TRIT(2,1) = SN1IT * CS2IT
TRTC(2,1) = SN1TC * CS2TC
TRIT(3,1) = - SN2IT
TRTC(3,1) = - SN2TC
TRIT(1,2) = CS1IT * SN2IT * SN3IT - SN1IT * CS3IT
TRTC(1,2) = CS1TC * SN2TC * SN3TC - SN1TC * CS3TC
TRIT(2,2) = SN1IT * SN2IT * SN3IT + CS1IT * CS3IT
TRTC(2,2) = SN1TC * SN2TC * SN3TC + CS1TC * CS3TC
TRIT(3,2) = CS2IT * SN3IT
TRTC(3,2) = CS2TC * SN3TC
TRIT(1,3) = CS1IT * SN2IT * CS3IT + SN1IT * SN3IT
TRTC(1,3) = CS1TC * SN2TC * CS3TC + SN1TC * SN3TC
TRIT(2,3) = SN1IT * SN2IT * CS3IT - CS1IT * SN3IT
TRTC(2,3) = SN1TC * SN2TC * CS3TC - CS1TC * SN3TC
TRIT(3,3) = CS2IT * CS3IT
TRTC(3,3) = CS2TC * CS3TC
CALL MULT (TRIT,TRTC,TRIC,3,3,3,3,3)
```

C

C

```
FILL IN THE Y(I) STATE VECTOR WITH INITIAL CONDITIONS.
```

C

```
PSP(1) = DLI + DLS + DATMIN(6,1)
PSP(2) = 0.0
PSP(3) = 0.0
Y(NRHO) = DATMIN(6,1)
DO 25 I = 1,3
  Y(NGAMT + I - 1) = TRIT(I,1)
  Y(NGAMT + I + 2) = TRIT(I,2)
  Y(NUC + I - 1) = DATMIN(4,I)
  Y(NUC + I + 2) = DATMIN(3,I)
DO 20 J = 1,3
20 Y(NXC + I - 1) = Y(NXC + I - 1) + TRIT(I,J) * (TDTC(J) + DATMIN
  * (5,J)) - TRIC(I,J) * (CPCO(J) + PSP(J))
  Y(NGAMC + I - 1) = TRIC(I,1)
  Y(NGAMC + I + 2) = TRIC(I,2)
25 Y(NRHO + I + 2) = DATMIN(6,2)
```

C

```
WRITE (NOT,1001)
CALL WRITE (Y,1,NEQTN,6HYINITL,1)
```

C

```
RETJRN
END
```

```
SUBROUTINE MULT3 (A,B,Z,NRA,NRB,NCB,KRA,KRB,KRZ)  
DIMENSION A(KRA,1), B(KRB,1), Z(KRZ,1)
```

```
C  
DO 10 I=1,NRA  
DO 10 J=1,NCB  
Z(I,J) = 0.0  
DO 10 K=1,NRB  
10 Z(I,J) = Z(I,J) + A(I,K) * B(K,J)  
C  
RETURN  
END
```

```
SUBROUTINE MULTAD (A,B,Z,NRA,NRB,NCB,KRA,KRB,KRZ)  
DIMENSION A(KRA,1), B(KRB,1), Z(KRZ,1)
```

```
C  
DO 10 I=1,NRA  
DO 10 J=1,NCB  
DO 10 K=1,NRB  
10 Z(I,J) = Z(I,J) + A(I,K) * B(K,J)  
C  
RETURN  
END
```



```

SUBROUTINE PIERCE (DA,DL,DS,R,ALPHA,SALP,CALP,TALP,
1          ROTALP,DAB)
C
C          SUBROUTINE TO ESTABLISH IF PIERCE POINTS LIE
C          BELOW DROGUE LIP
C          OR IF PROBE HAS PIERCED DROGUE
C
DIMENSION DA(3),DL(3), DS(3)
DIMENSION DB(3),DC(3),DD(3)
DIMENSION          PHIPP(2),RPP(2),SPHIPP(2),CPHIPP(2)
C
DATA  NIT, NOT  / 5, 6 /
C
IF ((DA(1).LE.0.0) .OR. (DL(1).LE.0.0) .OR.
1(SQRT(DA(2)*DA(2)+DA(3)*DA(3))/DA(1).GE.TALP)) GO TO 100
IF ((DS(1).LE.0.0) .OR. (SQRT(DS(2)*DS(2)+DS(3)*DS(3))/DS(1).GE.
1TALP)) GO TO 110
C
CALL AVPBV(1.0,DA,DAB,DL,DB)
C
IF (SQRT(DB(2)*DB(2)+DB(3)*DB(3))/DB(1) .LT. TALP) RETURN
C
DD(1) = DA(2)*DB(3) - DA(3)*DB(2)
DD(2) = DA(3)*DB(1) - DA(1)*DB(3)
DD(3) = DA(1)*DB(2) - DA(2)*DB(1)
C
E = -DD(1)/(TALP*SQRT(DD(2)*DD(2)+DD(3)*DD(3)))
DENOM = SQRT(1.0 - E*E)
BETA = ATAN2(DD(2),DD(3))
C
PHIPP(1) = ATAN2(E, DENOM) - BETA
PHIPP(2) = ATAN2(E,-DENOM) - BETA
C
DO 12 I=1,2
SPHIPP(I) = SIN(PHIPP(I))
12 CPHIPP(I) = COS(PHIPP(I))
C
CALL AVPBV(1.0,DB,-1.0,DA,DC)
C
IF (DD(1).EQ.0.0) GO TO 30
IF (DD(2).EQ.0.0) GO TO 40
C
30 DO 35 I=1,2
35 RPP(I) = DD(2)/(DC(1)*SALP+SPHIPP(I) - DC(3)*CALP)
GO TO 60
C
40 DO 45 I=1,2
45 RPP(I) = DD(1)/(SALP+(DC(3)*CPHIPP(I) - DC(2)*SPHIPP(I)))
C
60 RMAX = AMAX1(RPP(1),RPP(2))
C
IF (RMAX+CALP .LE. POTALP) GO TO 106
C
RETURN
C
100 WRITE(NOT,101)
101 FORMAT(/,10X, 37HPITCH ARM ORIENTATION ERROR, STOP RUN)
STOP
106 WRITE(NOT,107)
107 FORMAT(/,10X,38HPITCH ARM HAS PIERCED DROGUE, STOP RUN)
STOP
110 WRITE(NOT,111)

111 FORMAT(/,10X, 34HPROBE HAS PIERCED DROGUE, STOP RUN)
STOP
END

```

```
PROGRAM PLOTTER
C
COMMON /PLTR / K1,NCOLS,NTIMES,XDLTA,NPLTS
COMMON /TAPE/ NTAPE1, NTAPE2, NTAPE3
COMMON /TIMES/ STARTT,DELTA, T, ENDT, TMST, NSECS
C
DIMENSION Z(500,60), PTITLE(4)
C
REWIND NTAPE1
REWIND NTAPE2
C
NCOLP1 = NCOLS+1
IZ = 0
KPL = NTIMES/NPLTS+1
KCOUNT = KPL-1
C
DO 200 NI=1,NTIMES
KOUNT = KOUNT+1
IF (KOUNT .NE. KPL) READ(NTAPE1) DUMMY
IF (KOUNT .NE. KPL) GO TO 201
IZ = IZ+1
READ(NTAPE1) (Z(IZ,K),K=1,NCOLP1)
KOUNT = 0
201 CONTINUE
200 CONTINUE
C
210 READ (NTAPE2) NCX,NCY,NXPL,XNAME,YNAME,PTITLE
IF (NCX.EQ.0) CALL FRAME
IF (NCX.EQ.0) RETURN
C
XSTART = STARTT
XDELTA = XDLTA
IF (NXPL .GT. 0) XDELTA = FLOAT(NXPL)*XDLTA
IF (NCX .GT. 1) CALL SCALER(Z(1,NCY),Z(1,NCX),IZ,XSTART,XDELTA)
C
CALL PLOT1 (Z(1,NCX),Z(1,NCY),IZ, 1,XSTART,XDELTA,
XNAME,YNAME,PTITLE,1,1,0,500)
C
GO TO 210
C
END
```

SUBROUTINE PREENT

C

```

COMMON /BINDFR/ FI,BINDMU
COMMON /CHANGE/ Z(150),ZDT(150)
COMMON /FORMOM/ FANOM(12)
COMMON /IFOUTS/ MINIC,IFPLOT,IFPER
COMMON /LOCLN/ LOC(12), LEN(12)
COMMON /LOCPTD/ DSD(3),DHD(3),DGL(3),DAD(3,3),DRD(3,3),
*           DQD(3,3),QRD(3,3)
*           ,DHPD(3),DBD(3,3),DFD(3,3),OPD(3,3)
COMMON /MISCNO/ ANUM
COMMON /NEQINS/ NEQIN
COMMON /PHILAM/ PHICON(10),ALAM(10), MODE(10)
COMMON /PUNCHY/ IFPNCH
COMMON /RETRCT/ AKD1,AKD2,AKD3,RHOS0,FRETL,EXTL,TIAG,TSTAR,FRET
COMMON /TIMESS/ STARTT,DELTAT, T, ENDT, TMST, NSECS
COMMON /VECTOR/ Y(150),YDT(150)
COMMON /YPSTNS/ NUT,NXT,NGAMT,NUC,NXC,NGAMC,NRHO,
*           NXITDT,NXIT,NXICDT,NXIC, NOELCS

```

C

DIMENSION NAMES(36)

C

```

DATA NIT,NOT /5,6/
DATA NAMES /6HU - TA,6HRGET ,6H           ,6HX - TA,6HRGET ,6H           ,
*           6HGAMMA ,6HTARGET,6H           ,6HU - CH,6HASE ,6H           ,
*           6HX - CH,6HASE ,6H           ,6HGAMMA ,6HCHASE ,6H           ,
*           6HRHOS ,6H           ,6H           ,6HMODE V,6HEL - T,6HARGET ,
*           6HMODE D,6HISP - ,6HTARGET,6HMODE V,6HEL - C,6HASE ,
*           6HMODE D,6HISP - ,6HCHASE ,6HCON SY,6HS PARA,6HMETERS/

```

C

```

IF(TMST .EQ. 0.0) KOUNT = NSECS
IF(TMST .EQ. 0.0) GO TO 10
KOUNT = KOUNT+1

```

10 CONTINUE

C

ALTER Y AND YDT FOR PRINTING AND PLOTTING

C

```

DO 12 I=1,NEQIN
Z(I) = Y(I)
12 ZDT(I) = YDT(I)
DO 13 I=1,3
JI = NUT+2+I
JJ = NUC+2+I
Z(JI) = Y(JI)/ANUM
ZDT(JI) = YDT(JI)/ANUM
Z(JJ) = Y(JJ)/ANUM
13 ZDT(JJ) = YDT(JJ)/ANUM
DO 14 I=1,5
J = I+NRHO
Z(J) = Y(J)/ANUM
14 ZDT(J) = YDT(J)/ANUM
DO 15 I=1,3
J = NOELCS+I
K = NOELCS + I + 18
Z(K) = Y(K)/ANUM
ZDT(K) = YDT(K)/ANUM
Z(J) = Y(J)/ANUM
15 ZDT(J) = YDT(J)/ANUM

```

C

IF(KOUNT .NE. NSECS) GO TO 100

C

```

WRITE(NOT,730) T
730 FORMAT(1H,///, 37X,17HSIMULATION TIME =, E10.4)

```

```

C
  WRITE(NOT,600)
600 FORMAT(///,35X,4HY(I),3CX,7HYDOT(I))
  DO 5 I = 1,12
    K = (I - 1) * 2 + 1
    L = K + 2
    WRITE (NOT,500) (NAMES(J), J = K,L)
500 FORMAT (1X, 3A6)
    NBEGIN = LOC(I)
    NEND = LOC(I) + LEN(I) - 1
    DO 5 J = NBEGIN,NEND
      5 WRITE (NOT,605) Z(J), ZDT(J)
605 FORMAT (27X,E17.8,17X,E17.8)
C
  WRITE(NOT,610) (DSD(I), I = 1,3)
610 FORMAT(//,13HDSO VECTOR = , 3(5X,E17.8))
C
  WRITE(NOT,615)
615 FORMAT (1H0,16X,3HPHI,22X,5HLANDA,23X,4HMODE,/)
  WRITE(NOT,620) (I,PHICON(I),ALAM(I),MODE(I),I = 1,10)
620 FORMAT (3X,12,5X,E17.8,10X,E17.8,15X,I3)
C
  WRITE(NOT,630) FRET
630 FORMAT(///, 10X,16HRETRACT FORCE = , E17.8)
C
  WRITE(NOT,631) FI
631 FORMAT(/, 10X, 24HBINDING FRICTION FORCE =, E17.8)
C
  WRITE(NOT,640) (FANDM(I),I=1,12)
640 FORMAT(///,10X,16H FORCE AT PT D =, 3(2X,E17.8),/,
  *           10X,16HMOMENT AT PT D =, 3(2X,E17.8),/,
  *           10X,16H FORCE AT PT P =, 3(2X,E17.8),/,
  *           10X,16HMOMENT AT PT P =, 3(2X,E17.8))
C
  CALL CPWMS (CP)
C
  WRITE (NOT,635) CP
635 FORMAT(///,30X,18HELAPSED CP TIME = , E17.8)
C
  IF (IFPER .NE. 0) CALL SETPER
C
  KOUNT = 0
100 CONTINUE
C
  IF (IFPLOT .NE. 0) CALL SETPLT(CP)
C
  CALL SETTPE
  IF (T.GE.ENDT .AND. IFPNCH.NE.0)
    * CALL PUNCH (Y,1,NEOTM,6HYINITL,1)
C
  RETURN
  END

```

SUBROUTINE RETRAK

```

C
COMMON /PHILAM/ PHICON(10),ALAM(10), MODE(10)
COMMON /RETRCT/ AKD1,AKD2,AKD3,RHOS0,FRETL,EXTL,TLAG,TSTAR,FRET
COMMON /TIMESS/ STARTT,DELTAT, T, ENDT, TMST, NSECS
COMMON /VECTOR/ Y(150),YDT(150)
COMMON /YPSTNS/ NUT,NXT,NGAMT,NUC,NXC,NGAMC,NRHO,
*           NXITDT,NXIT,NXICDT,NXIC, NDELCS
C
IF (MODE(8) .EQ. 0) TSTAR = T + TLAG
IF (T - TSTAR .LE. 0.0) GO TO 10
C
AKD = AKD1
IF (Y(NRHO) .LT. RHOS0) AKD = AKD2
FRET = AKD + (T - TSTAR)/ABS(AKD3 + EXTL - Y(NRHO))
IF (FRET .GT. FRETL) FRET = FRETL
C
GO TO 20
C
10 FRET = 0.0
C
20 RETURN
C
END

```

SUBROUTINE ROOTS (DA,DL,R,RCTNA,PHIC,FLC,FGC,NRK,NPA)

```

C
DIMENSION DA(3), DL(3)
C
DATA GESLAM, TOLER, MAXITR / 50.0, 0.01, 150 /
DATA NIT, NOT / 5, 6 /
C
FLC = GESLAM
IC = 0
50 G = FLC
PHIC = ATANZ(DA(3)+G*DL(3), DA(2)+G*DL(2))
RCP = R*COS(PHIC)
RSP = R*SIN(PHIC)
G1 = (RCTNA-DA(1))*DL(1)+(RCP-DA(2))*DL(2)+(RSP-DA(3))*DL(3)
IF (ABS(G-G1) .LT. TOLER) GO TO 60
IC = IC + 1
IF (IC .EQ. MAXITR) GO TO 200
FLC = G1
GO TO 50
C
60 QR1 = RCTNA - DA(1) - G*DL(1)
QR2 = RCP - DA(2) - G*DL(2)
QR3 = RSP - DA(3) - G*DL(3)
FGC = SQRT(QR1*QR1 + QR2*QR2 + QR3*QR3)
C
RETURN
C
200 WRITE(NOT,1001)
1001 FORMAT(/,10X,45H SUBROUTINE ROOTS DOES NOT CONVERGE, STOP RUN)
STOP
C
END

```

SUBROUTINE RUNKTA

```

C
C SUBROUTINE TO NUMERICALLY INTEGRATE A SET OF FIRST ORDER
C DIFFERENTIAL EQUATIONS
C
C REFERENCE FOR GILL-RUNGE-KUTTA ALGORITHM ---
C MATHEMATICAL METHODS FOR DIGITAL COMPUTERS, ANTHONY RALSTON,
C HERBERT S. WILF (ART. BY MICHAEL J. ROMANELLI, PAGE 115).
C
C CODED BY CARL BOOLEY, JULY 1969
C
C SUBROUTINES THAT ARE CALLED ARE --- GEOM, KINMAT, CONTAK AND VECTR.
C
COMMON /JCOUNT/ JIL
COMMON /NEQNS/ NEQTN
COMMON /QPRKTA/ QRK(150), PRK(4)
COMMON /TIMESS/ STARTT, DELTAT, T, ENDT, TMST, NSECS
COMMON /VECTOR/ Y(150), YDT(150)
C
DATA NT / 0 /
C
DO 120 J = 1,4
  JIL = J
  DO 110 I=1,NEQTN
    Z = YDT(I)*DELTAT
    GO TO (103,101,101,105), JIL
101 R = PRK(JIL)*(Z - QRK(I))
    GO TO 107
103 R = PRK(JIL)*Z - QRK(I)
    GO TO 107
105 R = (Z - 2.*QRK(I))/6.
107 Y(I) = Y(I) + R
110 QRK(I) = QRK(I) + 3.*R - PRK(JIL)*Z
    IF (JIL .EQ. 1 .OR. JIL .EQ. 3) T = T + DELTAT/2.
    CALL GEOM
    CALL KINMAT
    IF (JIL .EQ. 4) CALL CONTAK
120 CALL VECTR
C
NT = NT + 1
ANT = NT
TMST = ANT*DELTAT
T = STARTT + TMST
C
RETURN
END

```

```

SUBROUTINE SCALER (V,H,N, XSTART,SCALE)
C
C   DIMENSION V(1),H(1)
C
C   DATA  NIT,NOT  /5, 6/
C
1001 FORMAT (54H)HORIZONTAL SCALE COULD NOT BE SHIFTED IN 10000 MOVES.
*       //9H HMIN  = E15.8 /
*       9H HMAX  = E15.8 /
*       9H SCALE = E15.8 )
C
VMAX = V(1)
VMIN = V(1)
HMAX = H(1)
HMIN = H(1)
DO 10 I=1,N
IF (V(I) .LT. VMIN) VMIN = V(I)
IF (V(I) .GT. VMAX) VMAX = V(I)
IF (H(I) .LT. HMIN) HMIN = H(I)
10 IF (H(I) .GT. HMAX) HMAX = H(I)
C
CALL PLOTSS (VMAX,VMIN,VTOP,VBOT)
CALL PLOTSS (HMAX,HMIN,HTOP,HBOT)
SCALE = (VTOP-VBOT)/10.000
HS     = (HTOP-HBOT)/10.000
IF (HS .GT. SCALE) SCALE = HS
XSTART = -5.*SCALE
XS     = XSTART
C
I = 0
15 I = I+1
IF (I .GT. 10000) GO TO 999
IF (HMIN .GE. XSTART) GO TO 20
XSTART = XS - FLOAT(I)*SCALE
GO TO 15
C
20 I = 0
25 I = I+1
IF (I .GT. 10000) GO TO 999
IF (HMAX .LE. XSTART+10.*SCALE) RETURN
XSTART = XS + FLOAT(I)*SCALE
GO TO 25
C
C
999 WRITE (NOT,1001) HMIN,HMAX,SCALE
STOP
END

```

SUBROUTINE SETPER

SUBROUTINE TO COMPUTE PROBE POINT LOCATIONS AND
PLOT FRAME IN PERSPECTIVE OR STEREO

CODED BY BODLEY/PARK OCTOBER 1969

C
C
C
C
C
C

```
COMMON /ANGLES/ ALPHAD,SALPD,CALPD,TALPD, SSIGMA(3),CSIGMA(3)
COMMON /FUNGAM/ SGAMMA(3),CGAMMA(3),SGSS(3),SGCS(3),
*                CGSS(3),CGCS(3)
COMMON /GEOMTY/ AA,AB,AD,AE,AF,AP,DLB,DLD,OLE,OLF,DLI,OLP,OLQ,OLS,
*                TDT(3),CPCD(3),RADCON,CSPHER,ROTALP,PEO,FDO
COMMON /IFOUTS/ MINIC,IFPLOT,IFPER
COMMON /JBATCH/ JBA
COMMON /LOCPTD/ DSD(3),DHD(3),DGD(3),DAD(3,3),DRD(3,3),
*                DDD(3,3),ORD(3,3)
*                ,DHPD(3),DBD(3,3),DFD(3,3),DPD(3,3)
COMMON /LOCPTI/ OTI(3),OCI(3),TCI(3)
COMMON /LOCPTP/ PSP(3),PAP(3,3),POP(3,3)
COMMON /LOCPTT/ THT(3),TCT(3),TST(3),TAT(3,3),TRT(3,3),
*                CST(3),CAT(3,3),QRT(3,3),TDT(3),
*                DHT(3),DGT(3),DST(3),DAT(3,3),DQT(3,3),DRT(3,3)
COMMON /MISCNO/ ANUM
COMMON /PERTIT/ PTITL(8),IFFIXD,RANGLE,EED,CANGLE,
*                COELOC(3),VPLOC(3)
COMMON /TRNFMS/ TRTI(3,3),TRCI(3,3),TRTC(3,3),TRHT(3,3),TRHC(3,3),
*                TRRT(3,3,3),TRRC(3,3,3),TRPC(3,3),TRDT(3,3),
*                TRPD(3,3),TRHD(3,3),TRRD(3,3,3),TRPT(3,3)
*                ,TRHP(3,3),TRTP(3,3),TRRP(3,3,3)
COMMON /VECTOR/ Y(150),YDT(150)
COMMON /YPSTNS/ NUT,NXT,NGAMT,NUC,NXC,NGAMC,NRHO,
*                NXITDT,NXIT,NXICDT,NXIC,NDELCS
```

C

```
DIMENSION DPCD(3),DFCD(3),DBBD(3),DDD(3,3),DED(3,3),ODI(3)
DIMENSION WV(3),VM(3),ILOC(50)
DIMENSION SHP(186,3),RS(2),HS(2),FINOT(2)
DIMENSION TRDI(3,3),OVI(3),OEI(3)
DIMENSION CLOC(333,3),MLOC(345,2)
DIMENSION COEYLC(3),VPNTLC(3)
```

C

```
DATA NIT,NOT / 5,6 /
DATA INTL /0/
DATA (ILOC(I),I=1,50)
* / 1, 4, 4, 4, 6, 7, 8, 6, 7, 8,21,22,23,12,13,14,
*   9,10,11, 2, 2, 2, 3, 3, 3,
*   5, 6, 7, 8, 7, 8, 6,21,22,23,18,19,20,15,16,17,
*   18,19,20, 9,10,11,12,13,14 /
```

C

```
IF (JBA.GT.1) GO TO 98
IF (INTL.NE.0) GO TO 98
READ (NIT,1001) (PTITL(I),I=1,8)
1001 FORMAT (8A10)
READ (NIT,1002) IFFIXD,RANGLE,EED,CANGLE
1002 FORMAT (15,5X,6E10.0)
READ (NIT,1003) (COELOC(I),I=1,3)
READ (NIT,1003) (VPLOC(I),I=1,3)
1003 FORMAT (8E10.0)
98 CONTINUE
IF (INTL.NE.0) GO TO 81
DO 82 I=1,3
COEYLC(I) = COELOC(I)
#2 VPNTLC(I) = VPLOC(I)
```



```

C
81 IF (IFFIXD .NE. 0) GO TO 97
C ESTABLISH ODI, TRDI
  CALL ATXBV (TRTI,TDI,MV)
  CALL AVPBV (1.0,OTI,1.0,MV,ODI)
  CALL AXB3 (TRDI,TRTI,TRDI)
97 CONTINUE
C
  IF (INTL .NE. 0) GO TO 99
C
  DO 90 I=1,25
  MLOC(I,1) = ILOC(I)
90 MLOC(I,2) = ILOC(I+25)
C
  IF (IFFIXD .NE. 0) GO TO 96
C ESTABLISH OVI, OEI
  CALL ATXBV (TRDI,COEYLC,MV)
  CALL AVPBV (1.0,ODI,1.0,MV,OEI)
  CALL ATXBV (TRDI,VPNTLC,MV)
  CALL AVPBV (1.0,ODI,1.0,MV,OVI)
96 CONTINUE
C
C COMPUTE PROBE HEAD COORDINATES
  DLFI = ANUM*6.
  DO 10 L=1,2
  L1 = 1 + 31*(L-1)
  L2 = L1 + 30
  AL = L
  FI = ANUM*180.*(AL-1.)
  DO 10 I=L1,L2
  SHP(I,1) = 0.
  SHP(I,2) = CSPHER*COS(FI)
  SHP(I,3) = CSPHER*SIN(FI)
  FI = FI + DLFI
10 CONTINUE
  L2 = 62
  FI = -135.*ANUM
  DO 20 J=1,4
  DO 20 L=1,2
  DLFI = 180*(L-1) - 135*(2-L)
  FI = FI + DLFI*ANUM
  L1 = L2 + 1
  L2 = L1 + 16 - L
  AL = 6*(1 + 14*(2-L))
  AL = ANUM*AL
  DLAL = 12*(L-1) - 6
  DLAL = ANUM*DLAL
  DO 20 I=L1,L2
  SHP(I,1) = CSPHER*COS(AL)
  SHP(I,2) = CSPHER*COS(FI)*SIN(AL)
  SHP(I,3) = CSPHER*SIN(FI)*SIN(AL)
  AL = AL + DLAL
20 CONTINUE
C
C COMPUTE DROGUE-CONE COORDINATES
  RS(1) = CSPHER*CALPD
  HS(1) = RS(1)/TALPD
  RS(2) = RADCON
  HS(2) = ROTALP
  FINOT(1) = 0.
  FINOT(2) = ANUM*180.
  DLFI = ANUM*6.

```

```

L2 = 209
DO 30 L=1,2
DO 30 J=1,2
FI = FINOT(J)
L1 = L2 + 1
L2 = L1 + 30
DO 30 I=L1,L2
CLOC(I,1) = HS(L)
CLOC(I,2) = RS(L)*COS(FI)
CLOC(I,3) = RS(L)*SIN(FI)
FI = FI + DLFI
30 CONTINUE
C
C COMPUTE MLOC ARRAY
IR = 25
IS = -8
DO 40 L=1,10
IS = IS+31
IT = IS
DO 40 J=1,30
IT = IT+1
IR = IR+1
MLOC(IR,1) = IT
MLOC(IR,2) = IT+1
40 CONTINUE
L2 = 11
IR = 325
IS1 = 210
IS2 = 272
DO 50 L=1,2
IS1 = IS1+34*(L-1)
IS2 = IS2+34*(L-1)
L2 = L2-2*(L-1)
DO 50 I=1,L2
I1 = IS1+3*(I-1)
I2 = IS2+3*(I-1)
IR = IR+1
MLOC(IR,1) = I1
MLOC(IR,2) = I2
50 CONTINUE
C
INTL = 1
99 CONTINUE
C
IF (IFFIXD .NE. 0) GO TO 95
C MODIFY COEYLC, VPNTLC
CALL AVPBV (1.0,OEI,-1.0,ODI,WV)
CALL AXBV (TRDI,WV,COEYLC)
CALL AVPBV (1.0,OVI,-1.0,ODI,WV)
CALL AXBV (TRDI,WV,VPNTLC)
95 CONTINUE
C
C ESTABLISH DHPD
CALL ATXBV (TRPD,PSP,WV)
CALL AVPBV (1.0,OSD,-1.0,WV,DHPD)
C
WV(2) = 0.0
WV(3) = 0.0
C
C ESTABLISH DPCD
WV(1) = DLP
CALL ATXBV (TRPD,WV,WV)

```

```

      CALL AVPBV (1.0,DHPD,1.0,C,VW,DPCD)
C
C ESTABLISH DFCO
      WV(1) = DLF
      CALL ATXBV (TRPD,WV,VW)
      CALL AVPBV (1.0,DHPD,1.0,C,VW,DFCO)
C
C ESTABLISH DBDO
      WV(1) = DLI+Y(NRHO)
      CALL ATXBV (TRPD,WV,VW)
      CALL AVPBV (1.0,DHPD,1.0,C,VW,DBDO)
C
C DSD COMPUTED BY GEOM
C DAD COMPUTED BY GEOM
C
      DO 100 K=1,3
C
C ESTABLISH DPO
      WV(1) = DLP
      WV(2) = -AP*SSIGMA(K)
      WV(3) = AP*CSIGMA(K)
      CALL ATXBV (TRPD,WV,VW)
      CALL AVPBV (1.0,DHPD,1.0,C,VW,DPO(1,K))
C
C ESTABLISH DFO
      WV(1) = DLF
      WV(2) = -AF*SSIGMA(K)
      WV(3) = AF*CSIGMA(K)
      CALL ATXBV (TRPD,WV,VW)
      CALL AVPBV (1.0,DHPD,1.0,C,VW,DFO(1,K))
C
C ESTABLISH DDO
      TRM = AA+DLD*SGAMMA(K)-AD*CGAMMA(K)
      WV(1) = DLI+Y(NRHO)-DLD*CGAMMA(K)-AD*SGAMMA(K)
      WV(2) = -TRM*SSIGMA(K)
      WV(3) = TRM*CSIGMA(K)
      CALL ATXBV (TRPD,WV,VW)
      CALL AVPBV (1.0,DHPD,1.0,C,VW,DDO(1,K))
C
C ESTABLISH DED
      TRM = AA+DLE*SGAMMA(K)-AE*CGAMMA(K)
      WV(1) = DLI+Y(NRHO)-DLE*CGAMMA(K)-AE*SGAMMA(K)
      WV(2) = -TRM*SSIGMA(K)
      WV(3) = TRM*CSIGMA(K)
      CALL ATXBV (TRPD,WV,VW)
      CALL AVPBV (1.0,DHPD,1.0,C,VW,DED(1,K))
C
C ESTABLISH DBO
      TRM = AA+DLB*SGAMMA(K)
      WV(1) = DLI+Y(NRHO)-DLB*CGAMMA(K)
      WV(2) = -TRM*SSIGMA(K)
      WV(3) = TRM*CSIGMA(K)
      CALL ATXBV (TRPD,WV,VW)
      CALL AVPBV (1.0,DHPD,1.0,C,VW,DBO(1,K))
C
      100 CONTINUE
C
C ROW 1-23 OF CLOC
      DO 200 J=1,3
      CLOC( 1, J) = DHPD(J)
      CLOC( 2, J) = DPCD(J)
      CLOC( 3, J) = DFCO(J)

```

```
CLOC( 4, J) = DBBD(J)
CLOC( 5, J) = DSD(J)
DO 200 I=1,3
CLOC( 5+I, J) = DAD(J,I)
CLOC( 8+I, J) = DPD(J,I)
CLOC(11+I, J) = DFD(J,I)
CLOC(14+I, J) = DDD(J,I)
CLOC(17+I, J) = DED(J,I)
CLOC(20+I, J) = DBD(J,I)
200 CONTINUE
C
C ROW 24-209 OF CLOC
DO 210 I=1,186
  II = I+23
  DO 210 J=1,3
    CLOC(II,J) = DSD(J)
    DO 210 K=1,3
      210 CLOC(II,J) = CLOC(II,J) + SHP(I,K)+TRPD(K,J)
C
  CALL PLOT3 (CLOC,MLOC,COEYLC,VPNTLC,RANGLE,IFPER,0,IFPER,
    * EED,CANGLE,PTITL ,333,345,333,345)
C
  RETURN
END
```

SUBROUTINE SETPLT(CPTNE)

C
C
C
C
C
CSUBROUTINE TO WRITE DATA ON NTAPE1 SO THAT IT CAN
BE RECALLED FOR PLOTTING

CODED BY A C PARK AUG 1969

```

COMMON /BINDFR/ FI,BINDMU
COMMON /CHANGE/ Z(150),ZDT(150)
COMMON /CSFORC/ FORCS(10), NFORCS
COMMON /FORMOM/ FANDM(12)
COMMON /LATCHL/ VLAM(6)
COMMON /LOCPTD/ DSD(3),OH0(3),DGD(3),DAD(3,3),ORD(3,3),
*                DQD(3,3),QRD(3,3)
*                ,DHPD(3),DBD(3,3),DFD(3,3),DPD(3,3)
COMMON /NMODES/ NMODET, NMODEC, IFELAS
COMMON /PHILAM/ PHICON(10),ALAM(10), MODE(10)
COMMON /RETRCT/ AKD1,AKD2,AKD3,RH0SO,FRETL,EXTL,TLAG,TSTAR,FRET
COMMON /TAPED/ NTAPE1, NTAPE2, NTAPE3
COMMON /TIMESS/ STARTT,DELTA T, T, ENDT, TMST, NSECS
COMMON /YPSTNS/ NUT,NXT,NGAMT,NUC,NXC,NGAMC,NRHO,
*                NXITDT,NXIT,NXICDT,NXIC, NDELCS

```

C

IF (TMST .GT. 0.0) GO TO 10

LS1 = NUT

LE1 = LS1+5

LS2 = NUC

LE2 = LS2+5

LS3 = NRHO

LE3 = LS3+5

N1 = NDELCS+1

N2 = NDELCS+2

N3 = NDELCS+3

N4 = NDELCS+19

N5 = NDELCS+20

N6 = NDELCS+21

10 CONTINUE

C

WRITE (NTAPE1) T,

```

*                (Z(I),I=LS1,LE1), (Z(I),I=LS2,LE2),
*                (Z(I),I=LS3,LE3),
*                (DSD(I),I=1,3),
*                (ALAM(I),I=1,10), (VLAM(I),I=1,6),
*                (FANDM(I),I=1,6),
*                Z(N1),Z(N2),Z(N3),Z(N4),Z(N5),Z(N6),
*                (FORCS(I),I=2,10)

```

C

RETURN

END

SUBROUTINE SETTPE

C

C

C

CODED BY A C PARK SEPT 1969

```

COMMON /CSFORC/ FORCS(10), NFORCS
COMMON /FORMOM/ FANDM(12)
COMMON /LATCHL/ VLAM(6)
COMMON /TAPED/ NTAPE1, NTAPE2, NTAPE3
COMMON /TIMESS/ STARTT,DELTA T, T, ENDT, TMST, NSECS

```

C

```

WRITE (NTAPE3) T, (FANDM(I),I=1,6), (FORCS(I),I=2,7),
*                (VLAM(I),I=1,6), (FANDM(I),I=7,12),
*                FORCS(1), (FORCS(I),I=8,10)

```

C

IF (T.GE.ENDT) ENDFILE NTAPE3

C

RETURN

END

PROGRAM SETUP

```

C
C CODED BY CARL BODLEY, FRED NERZ AND COLT PARK, JULY 1969.
C
C   DIMENSION PTITLE(4), SIGMA(3)
C
COMMON /ANGLES/ ALPHAD,SALPD,CALPD,TALPD, SSIGMA(3),CSIGMA(3)
COMMON /BINDFR/ FI,BINDMU
COMMON /CSFORC/ FORCS(10), NFORCS
COMMON /GEOMTY/ AA,AB,AD,AE,AF,AP,DLB,DLD,DLE,DLF,DLI,DLP,DLQ,DLR,
*             TDTQ(3),CPCQ(3),RADCON,CSPHER,ROTALP,PEQ,FQO
COMMON /IFOUTS/ MINIC,IFPLOT,IFPER
COMMON /JBATCH/ JBA
COMMON /JCOUNT/ JIL
COMMON /MASS/ AMT, AMC, AIT(3,3), AIC(3,3)
COMMON /MFREQD/ FREQT(26), FREQC(26), ZETAT, ZETAC
COMMON /MISCNO/ ANUM
COMMON /NCNTRL/ NCNSYS
COMMON /NEQTN/ NEQTN
COMMON /NMODES/ NMODET, NMODEC, IFELAS
COMMON /PLTR / K1,NCOLS,NTIMES,XDLTA,NPLTS
COMMON /PUNCHY/ IFPNCH
COMMON /QPRKTA/ QRK(150), PRK(4)
COMMON /RETRCT/ AKD1,AKD2,AKD3,RHOSO,FRETL,EXTL,TLAG,TSTAR,FRET
COMMON /SLIDFR/ HDMU, ARMMU, BFV(8,39)
COMMON /SPRDMP/ FSPRNG(2,20,4),FDAMP(2,20,4)
COMMON /TAPED/ NTAPE1, NTAPE2, NTAPE3
COMMON /TIMESS/ STARTT,DELTAT, T, ENDT, TMST, NSECS
COMMON /VECTOR/ Y(150), YDT(150)
C
DATA NIT,NOT/5,6/
DATA NTMHST /58/
DATA NPLTS /500/
DATA KTABLE /20/
C
1001 FORMAT (16I5)
1003 FORMAT (2I5,2X,1I,2X,2(A6,4X),44I0)
1004 FORMAT (8E10.0)
2001 FORMAT (////15X,40H THE INPUT SCALARS TO PROGRAM DOCKEL ARE *
*           //23X,          10H STARTT = F10.6,
*           /23X,          10H DELTAT = F10.6,
*           /23X,          10H ENDT   = F10.6,
*           /23X,          10H XDLTA  = F10.6,
*           /23X,          10H XPRNT  = F10.6,
*           /23X,          10H ZETAT  = F10.6,
*           /23X,          10H ZETAC  = F10.6,
*           /23X,          10H IFELAS = I5,
*           /23X,          10H IFPLOT = I5,
*           /23X,          10H IFPER  = I5,
*           /23X,          10H JBATCH = I5,
*           /23X,          10H MINIC  = I5,
*           /23X,          10H IFPNCH = I5 )
2005 FORMAT ( /23X,          10H NCOLS  = I5,
*           /23X,          10H NCNSYS = I5,
*           /23X,          10H NFORCS = I5,
*           /23X,          10H NEQTN  = I5,
*           /23X,          10H NMODET = I5,
*           /23X,          10H NMODEC = I5 )
2002 FORMAT (// 23X,
* 10H AA   = E15.8,/23X,10H AB   = E15.8,/23X,
* 10H AD   = E15.8,/23X,10H AE   = E15.8,/23X,
* 10H AF   = E15.8,/23X,10H AP   = E15.8,/23X,

```

```

* 10H DLB = E15.8/23X, 10H DLD = E15.8/23X,
* 10H DLE = E15.8/23X, 10H DLF = E15.8/23X,
* 10H DLI = E15.8/23X, 10H DLP = E15.8/23X,
* 10H DLQ = E15.8/23X,
* 10H DLS = E15.8/23X, 10H FDO = E15.8/23X,
* 10H PEO = E15.8/23X, 10H ALPHAD = E15.8/23X,
* 10H CSPHER = E15.8/23X, 10H RADCON = E15.8/23X,
* 10H AKD1 = E15.8/23X, 10H AKD2 = E15.8/23X,
* 10H AKD3 = E15.8/23X, 10H RHOSO = E15.8/23X,
* 10H FRETLE = E15.8/23X, 10H EXTL = E15.8/23X,
* 10H TLAG = E15.8/23X, 10H TSTAR = E15.8/23X,
* 10H BINDMU = E15.8/23X,
* 10H HDMU = E15.8/23X, 10H ARMMU = E15.8

```

```
2003 FORMAT (///// 25X,30H THE TARGET VEHICLES MASS IS E15.8)
```

```
2004 FORMAT (///// 25X,30H THE CHASE VEHICLES MASS IS E15.8)
```

```

C
3001 FORMAT (24H1 ERROR CHECK AT NERROR = I3, 8H FAILED,
* /17H0 PROGRAM STOPPED.)
3002 FORMAT (52H1 MECHANISM SPRING, DAMPING OR FRICTION NOT COMPATIBLE/
* 17H0 PROGRAM STOPPED.)

```

```
C
REWIND NTAPE1
```

```
C
IF (JBA .GT. 1) GO TO 50
```

```
C
REWIND NTAPE2
REWIND NTAPE3
```

```
C
READ (NIT,1001) MINIC,IFPLOT,IFPER,IFPNCH
READ (NIT,1001) NCNSYS,NFORCS
```

```
C
READ (NIT,1004) STARTT,DELTAT,ENDT,XDLTA,XPRNT
NSECS = XPRNT
NTIMES = (ENDT-STARTT)/DELTAT + 1.1
```

```
C
READ (NIT,1004)
* AA,AB,AD,AE,AF,AP,DLB,DLD,DLE,DLF,DLI,DLP,DLQ,DLS,FDO,PEO,
* ALPHAD,CSPHER,RADCON,AKD1,AKD2,AKD3,RHOSO,FRETLE,EXTL,
* TLAG,TSTAR,BINDMU,HDMU,ARMMU
```

```
C
CALL READ (TDT0,N1, N2, 1, 3)
CALL READ (CPC0,N1, N2, 1, 3)
```

```

C
ANUM = ATAN2(1.,1.)/45.
SALPD = SIN(ANUM*ALPHAD)
CALPD = COS(ANUM*ALPHAD)
TALPD = SALPD/CALPD
ROTALP = RADCON/TALPD
CALL READ (SIGMA,N1,42,1,3)
DO 10 I=1,3
SIGMA(I) = SIN(ANUM*SIGMA(I))
10 CSIGMA(I) = COS(ANUM*SIGMA(I))

```

```

C
READ (NIT,1004) AMT
CALL READ (AIT, N1, N2, 3, 3)
WRITE (NOT,2003) AMT
READ (NIT,1004) AMC
CALL READ (AIC, N1, N2, 3, 3)
WRITE (NOT,2004) AMC

```

```

C
DO 15 I=1,4
CALL READ (FSPRNG(1,1,I),N1,N2,2,KTABLE)

```

```

NFSPR = FSPRNG(1,1,I) * 1.1
IF (NFSPR .NE. N2) GO TO 900
DO 17 J=3,N2
  JM1 = J - 1
  IF (FSPRNG(1,J,I) .LE. FSPRNG(1,JM1,I)) GO TO 900
17 CONTINUE
CALL READ (FDAMP(1,1,I),N1,N2,2,KTABLE)
NFDMP = FDAMP(1,1,I) * 1.1
IF (NFDMP .NE. N2) GO TO 900
DO 18 J=3,N2
  JM1 = J - 1
  IF (FDAMP(1,J,I) .LE. FDAMP(1,JM1,I)) GO TO 900
  IF (FDAMP(2,J,I) .LE. FDAMP(2,JM1,I)) GO TO 900
18 CONTINUE
15 CONTINUE
C
25 CALL HSIG
C
  NCOLS = NTHMST
  NCOLP1 = NCOLS + 1
C
  CALL LOCATE
C
50 IF (MINIC .EQ. 0) CALL READ(Y,N1,N2,1,150)
  IF (MINIC .EQ. 1) CALL MINYS
C
  IF (JBA.GT.1) GO TO 90
  IF (IFPLOT.EQ.0) GO TO 90
  NERROR = 0
  LIMPLT = NPLTS * NCOLP1
  IF (LIMPLT .GT. K1) GO TO 901
180 READ (NIT,1003) NCX,NCY,NXPL,XNAME,YNAME,PTITLE
  NERROR = NERROR + 1
  IF (NCX .GT. NCOLP1 .OR. NCY .GT. NCOLP1) GO TO 901
  WRITE (NTAPE2) NCX,NCY,NXPL,XNAME,YNAME,PTITLE
  IF (NCX.NE.0) GO TO 180
C
C PRINT INPUT SCALARS.
90 CALL PAGEHD
  WRITE (NOT,2001) STARTT,DELTA,ENDT,XDLTA,XPRNT,ZETAT,ZETAC,
  * IFELAS,IFPLOT,IFPER,JBA,MINIC,IFPNCH
  WRITE (NOT,2005) NCOLS,NCNSYS,NFORCS,NEQTN,NMODET,NMODEC
  WRITE (NOT,2002)
  * AA,AB,AD,AE,AF,AP,DLB,DLD,DLE,DLF,DLI,DLP,DLQ,DLS,FDD,PEO,
  * ALPHAD,CSPHER,RADCON,AKD1,AKD2,AKD3,RHOSO,FRETL,EXTL,
  * TLAG,TSTAR,BINDMU,HDMU,ARMMU
C
C SET INTEGRATION CONSTANTS.
  PRK(1) = .5
  PRK(2) = 1. - SORT(.5)
  PRK(3) = 1. + SORT(.5)
  PRK(4) = .5
C
C SET INITIAL VALUES.
  JIL = 4
  T = STARTT
  THST = 0.0
  DO 30 I=1,NEQTN
30 ORK(I) = 0.
C
  RETURN
900 WRITE (NOT,3002)
  STOP
901 WRITE (NOT,3001) NERROR
  STOP
  END

```


C-54

MCR-70-2 (Vol II)

```
SUBROUTINE SKEW (VEC,SKV)
DIMENSION VEC(3), SKV(3,3)
```

C
C
C

```
CODED BY CARL BODLEY   JUNE 1968
```

```
SKV(2,3) = VEC(1)
SKV(3,1) = VEC(2)
SKV(1,2) = VEC(3)
SKV(3,2) = -SKV(2,3)
SKV(1,3) = -SKV(3,1)
SKV(2,1) = -SKV(1,2)
SKV(1,1) = 0.0
SKV(2,2) = 0.0
SKV(3,3) = 0.0
RETURN
END
```

```
PROGRAM TIMHST
```

C
C

```
COMMON /TIMESS/ STARTT,DELTAT, T, ENDT, TMST, NSECS
```

```
CALL GEOM
CALL KINMAT
CALL CONTAK
CALL VECTR
CALL FORFUN
CALL PREENT
1 CALL RUNKTA
CALL FORFUN
CALL PREENT
IF (T .GE. ENDT) RETURN
GO TO 1
END
```

SUBROUTINE VECTR

C
C
C

COMPUTES TIME DERIVATIVE OF STATE VECTOR

```

COMMON /BC1234/ BC1(10,6), BC2(10,6), BC3(10,26), BC4(10,26)
COMMON /BTDATA/ TRHO(9,6), BL5(10,6), BLV(7,39)
COMMON /CSFORC/ FORCS(10), NFORCS
COMMON /JCOUNT/ JIL
COMMON /MASS/ AMT, AMC, AIT(3,3), AIC(3,3)
COMMON /MFREQD/ FREQT(26), FRFQC(26), ZETAT, ZETAC
COMMON /MISCNO/ ANUM
COMMON /NEQTN/ NEQTN
COMMON /NMODES/ NMODET, NMODEC, IFELAS
COMMON /PHILAM/ PHICON(10), ALAM(10), MODE(10)
COMMON /SLIDFR/ HDMU, ARMMU, BFV(8,39)
COMMON /TIMESS/ STARTT, DELTAT, T, ENDT, TMST, NSECS
COMMON /TRNFMS/ TRTI(3,3), TRCI(3,3), TRTC(3,3), TRHT(3,3), TRMC(3,3),
* TRRT(3,3,3), TRRC(3,3,3), TRPC(3,3), TRDT(3,3),
* TRPD(3,3), TRHD(3,3), TRRD(3,3,3), TRPT(3,3),
* TRHP(3,3), TRTP(3,3), TRRP(3,3,3)
COMMON /VECTOR/ Y(150), YDT(150)
COMMON /YPSTNS/ NUT, NXT, NGAMT, NUC, NXC, NGAMC, NRHO,
* NXITDT, NXIT, NXICDT, NXIC, NOELCS

```

C

```

DIMENSION GAMDTT(3,3), GAMDTC(3,3), OMEGT(3,3), OMEGC(3,3)
DIMENSION AITI(3,3), AICI(3,3), TZOMT(26), OMSOT(26),
1 TZOMC(26), OMSOC(26)
DIMENSION V1(6), V2(6), V3(6), V4A(3), V4B(3), V5A(3), V5B(3),
1 V26A(26), V26B(26), T33(3,3)
DIMENSION VEL(8), FOR(8), BIGF(39)
DATA ILATCH, ROV/ 0, 1.0 /

```

C

```
IF (TMST .GT. 0.0) GO TO 5
```

C

```
CALL INV2NP(AIT, AITI, 3, 3)
CALL INV2NP(AIC, AICI, 3, 3)
CALL ZERO (BIGF, 39, 1, 39)

```

C

```
PI = 180.*ANUM
FPI = 4.*PI
FPISO = 4.*PI**2

```

C

```
FPIZT = FPI*ZETAT
FPIZC = FPI*ZETAC

```

C

```
DO 2 I=1,NMODET
TZOMT(I) = FPIZT*FREQT(I)
2 OMSOT(I) = FPISO*FREQT(I)**2

```

C

```
DO 4 I=1,NMODEC
TZOMC(I) = FPIZC*FREQC(I)
4 OMSOC(I) = FPISO*FREQC(I)**2

```

C

```
IST = 36+2*NMODET
KD = 12+NMODET+NMODEC

```

C

```
NOMT = NUT + 3
NOMC = NUC + 3

```

C

```
5 CONTINUE
```

C

```
IF (V(NRHO) .LE. ROV .AND. JIL .EQ. 4 .AND.
```

```

      *           MODE(8) .EQ. 1) ILATCH = 1
      IF (ILATCH .EQ. 1) CALL HLATCH(1)
      CALL SKEWV (Y(NOMT), OMEGT)
      CALL SKEWV (Y(NOMC), OMEGC)
C
      CALL ATXBV (TRTI, Y(NUT), YDT(NXT))
      CALL ATXBV (TRCI, Y(NUC), YDT(NXC))
C
      CALL AXB3 (OMEGT, TRTI, GAMDTT)
      CALL AXB3 (OMEGC, TRCI, GAMDTC)
C
      DO 30 I=1,2
      IT = 3*I+NGAMT-4
      IC = 3*I+NGAMC-4
      DO 30 J=1,3
      YDT(IT+J) = GAMDTT(I,J)
30 YDT(IC+J) = GAMDTC(I,J)
C
      CALL LAMRHO
C
      IF (HDMU.EQ.0.0 .AND. ARMMU.EQ.0.0) GO TO 90
C
      DO 100 I=1,8
      VEL(I) = 0.0
      CALL MULTAD(BFV(I,1),Y(NUT),VEL(I),1,6,1,8,150,8)
      CALL MULTAD(BFV(I,7),Y(NUC),VEL(I),1,6,1,8,150,8)
      CALL MULTAD(BFV(I,13),Y(NXITDT),VEL(I),1,NMODET,1,8,150,8)
      CALL MULTAD(BFV(I,13+NMODET),Y(NXICDT),VEL(I),1,NMODEC,1,8,150,8)
100 CONTINUE
C
      NLAM = 3
      DO 200 I=1,7,2
      I1 = I+1
      NLAM = NLAM+1
      COF = HDMU
      IF (I.GT.1) COF = ARMMU
      VELMAG = SORT(VEL(I)*VEL(I)+VEL(I1)*VEL(I1))
      FOR(I) = -COF*VEL(I)*ALAM(NLAM)/VELMAG
200 FOR(I1) = -COF*VEL(I1)*ALAM(NLAM)/VELMAG
C
      CALL MULT (FOR,BFV,BIGF,1,8,KD,1,8)
C
      90 CONTINUE
C
      CALL CONSYS
C
      CALL MULT (FORCS,BC1,V1,1,NFORCS,6,1,10)
      CALL MULT (ALAM(4),BLV(1,1),V3,1,7,6,1,7)
      CALL AXB3 (OMEGT,AIT,T33)
      CALL AXBV (OMEGT,Y(NUT),V2(1))
      CALL AXBV (T33,Y(NOMT),V2(4))
C
      DO 60 I=1,3
      I3 = I+3
      V4A(I) = V2(I) + (V1(I)+V3(I)+BIGF(I))/AMT
60 V4B(I) = V1(I3) + V2(I3) + V3(I3) + BIGF(I3)
C
      CALL AXBV (AITI,V4B,V5B)
C
      DO 61 I=1,3
      I3 = I+3
      YDT(I) = V4A(I)

```

```

51 YDT(I3) = V5B(I)
C
CALL MULT (FORCS,BC3,V26A,1,NFORCS,NMODET,1,10)
CALL MULT (ALAM(4),BLV(1,13),V26B,1,7,NMODET,1,7)
C
DO 62 I=1,NMODET
II = I+36
IJ = II+NMODET
YDT(II) = V26A(I) + V26B(I) - TZOMT(I)*Y(II) - OMSQT(I)*Y(IJ)
*      + BIGF(I+12)
62 YDT(IJ) = Y(II)
C
CALL MULT (FORCS,BC2,V1,1,NFORCS,6,1,10)
CALL MULT (ALAM(4),BLV(1,7),V3,1,7,6,1,7)
CALL AXB3 (OMEGC,AIC,T33)
CALL AXBV (OMEGC,Y(NUC),V2(1))
CALL AXBV (T33,Y(NOMC),V2(4))
C
DO 63 I=1,3
I3 = I+3
V4A(I) = V2(I) + (V1(I) + V3(I)+BIGF(I+6))/AMC
63 V4B(I) = V1(I3) + V2(I3) + V3(I3) + BIGF(I+9)
C
CALL AXBV (AICI,V4B,V5B)
C
DO 64 I=1,3
I15 = I+15
I18 = I+18
YDT(I15) = V4A(I)
64 YDT(I18) = V5B(I)
C
CALL MULT (FORCS,BC4,V26A,1,NFORCS,NMODEC,1,10)
CALL MULT (ALAM(4),BLV(1,13+NMODET),V26B,1,7,NMODEC,1,7)
C
DO 65 I=1,NMODEC
II = I+15
IJ = II+NMODEC
YDT(II) = V26A(I) + V26B(I) - TZOMC(I)*Y(II) - OMSQC(I)*Y(IJ)
*      + BIGF(I+12+NMODET)
65 YDT(IJ) = Y(II)
C
IF (ILATCH .EQ. 1) CALL HLATCH(2)
RETURN
END

```

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APPENDIX D

PROGRAM DOCKEL INPUT DATA

This Appendix presents a listing of required DOCKEL input data. These data are for the Baseline Configuration and were used to generate the results presented in Chapter II. Numerical output obtained from these data are shown in Appendix E.

SC-1										
NASA-2128C										
BASELINE CONFIGURATION										
	1	1	1	C						
	34	10								
	0.		0.01	10.	0.5	50.				
	2.25		.85	.708	.965	3.095	4.25	14.48	12.90	
	17.59		4.75	14.10	3.30	16.53	2.055	11.5	10.50	
	42.75		2.58	13.56	0.0	0.0	5.41	2.08	1000.0	
	11.12		10.15	0.0	0.28	.26	.26			
TOTO	1		3							
	1	1		407.88		0.8309		36.167		
0000000000										
CPCO	1		3							
	1	1		134.7		-7.7		-7.7		
0000000000										
SIGMA	1		3							
	1	1		180.		300.		60.		
0000000000										
				296.4000						
AIT	3		3	INERTIA FOR CLUSTER ONLY						
	1	1		+6.428E+06		+1.622E+04		+3.528E+06		
	2	1		+1.622E+04		+2.474E+07		-1.575E+05		
	3	1		+3.528E+06		-1.575E+05		+2.512E+07		
0000000000										
				78.8577						
AIC	3		3							
	1	1		155240.		16956.		16932.		
	2	1		16956.		539016.		-79212.		
	3	1		16932.		-79212.		539028.		
0000000000										
FSPROX	2		8							
	1	1		7.		0.		0.32	.87	
	1	5		2.62		8.12		11.1	11.12	
	2	1		0.		-2000.		-125.	-118.	
	2	5		-106.2		-81.		-69.	731.0	
0000000000										
FDMROX	2		5							
	1	1		4.0		-12.		-0.1	0.1	
	1	5		12.0						
	2	1		0.0		-92.		-91.	91.	
	2	5		52.						
0000000000										
FSPALL	2		19							
	1	1		19.0		-0.0708		-0.06605	-0.0587	
	1	5		-0.05135		-0.0367		-0.02936	-0.02202	
	1	9		-0.01468		-0.00734		0.00734	0.01468	
	1	13		0.02202		0.02936		0.03670	0.05135	
	1	17		0.05870		0.06605		0.07080		
	2	1		0.0		-81.75	+03	-72.3	+03 -59.15 +03	
	2	5		-49.1	+03	-33.22	+03	-26.17	+03 -19.5 +03	
	2	9		-12.94	+03	-6.25E	+03	6.256	+03 12.94 +03	
	2	13		19.5	+03	26.17	+03	33.22	+03 49.10 +03	
	2	17		59.15	+03	72.30	+03	81.75	+03	
0000000000										
FDMALY	2		3							
	1	1		2.0		0.0		1.0		
	2	1		0.0		0.0		1.0	-06	
0000000000										
FSPALU	2		19							
	1	1		18.0		-0.0708		-0.06605	-0.0587	
	1	5		-0.05135		-0.0367		-0.02936	-0.02202	

1	9	-0.01468		-0.00734		0.00734		0.01468	
1	13	0.02202		0.02936		0.0367		0.05135	
1	17	0.05870		0.06605		0.0708			
2	1	0.0		-81.75	+03	-65.15	+03	-47.0	+03
2	5	-36.0	+03	-22.2	+03	-17.18	+03	-12.28	+03
2	9	-8.31	+03	-4.085	+03	4.085	+03	8.31	+03
2	13	12.28	+03	17.18	+03	22.2	+03	36.0	+03
2	17	47.0	+03	65.15	+03	81.75	+03		
000000000									
FOMALZ	2	3							
1	1	2.0		0.0		1.0			
2	1	0.0		0.0		1.0	-06		
000000000									
FSPATT	2	10							
1	1	9.0		8.43		8.5		9.0	
1	5	9.5		10.0		10.5		11.0	
1	9	11.25		11.50					
2	1	0.0		-760.0		-305.0		-185.0	
2	5	-123.5		-86.5		-62.5		-45.5	
2	9	-38.5		-32.5					
000000000									
FDMATT	2	16 ATTEN. DAMPING (T=TEMP= +70 THRU +250 DEG F)							
1	1	15.0		-19.2		-18.25		-16.8	
1	5	-14.4		-12.0		-9.6		-7.2	
1	9	-4.8		-2.76		-1.20		-0.60	
1	13	-0.24		-0.12		0.12		1.32	
2	1	0.		-2980.		-2685.		-2450.	
2	5	-2170.		-1920.		-1680.		-1435.	
2	9	-1175.		-910.		-630.		-405.	
2	13	-210.		-18.		18.		78.	
000000000									
FREQ	1	14	1	0.01	0.01				
	1	96							
1	5	0.		0.		2.54996194E-01		2.56654233E-01	
1	9	2.59230144E-01		2.63558032E-01		2.66530243E-01		3.16363216E-01	
1	13	4.08638136E-01		4.08671735E-01		4.08675934E-01		4.08678470E-01	
1	17	4.08678774E-01		4.08875139E-01		5.10929768E-01		5.13945264E-01	
1	21	5.37976914E-01		5.38156352E-01		5.74922575E-01		5.81649117E-01	
1	25	5.86156855E-01		5.86943106E-01		6.17050186E-01		6.18100481E-01	
1	29	6.18829615E-01		6.18840578E-01		7.15880147E-01		8.57194549E-01	
1	33	8.76752892E-01		9.04248565E-01		9.05857860E-01		9.20249224E-01	
1	37	9.88036352E-01		1.02627491E+00		1.06010342E+00		1.09757768E+00	
1	41	1.11870753E+00		1.11875386E+00		1.11876104E+00		1.11876459E+00	
1	45	1.11876506E+00		1.11889359E+00		1.25392463E+00		1.2590902E+00	
1	49	1.30060590E+00		1.30091512E+00		1.36216324E+00		1.36281889E+00	
1	53	1.36672613E+00		1.37554721E+00		1.37958881E+00		1.73465346E+00	
1	57	1.81008596E+00		1.81094561E+00		1.81107947E+00		1.82252375E+00	
1	61	2.11352028E+00		2.13162065E+00		2.13181872E+00		2.13471946E+00	
1	65	2.14928675E+00		2.78612394E+00		2.88460197E+00		2.90610104E+00	
1	69	3.31360816E+00		3.85170624E+00		4.12990059E+00		4.14176135E+00	
1	73	4.47363853E+00		4.68029637E+00		6.12480919E+00		6.33019624E+00	
1	77	6.65320423E+00		7.50817221E+00		7.95936849E+00		8.30724494E+00	
1	81	8.94704006E+00		9.38847045E+00		9.79588804E+00		1.00854674E+01	
1	85	1.03479378E+01		1.11819072E+01		1.17654872E+01		1.22070518E+01	
1	89	1.23384923E+01		1.25791755E+01		1.47431405E+01		1.75212818E+01	
1	93	2.52185445E+01		4.39829177E+01		5.28482614E+01		8.88177531E+01	
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1	1	3.37096783E-02		1.23539660E-02		-1.59449945E-02		-4.34111732E-04	
1	5	3.57812083E-02		-2.43781212E-02		2.35864798E-03		5.93297350E-04	
1	9	-4.80510784E-04		2.86124847E-06		5.95135453E-04		-7.72296766E-05	
1	13	7.54610732E-07		1.13132248E-06		1.95837124E-07		2.09693245E-07	

1	17	7.9395516CE-C8	1.92548456E-C5	6.17025205E-05	1.24977151E-C4
1	21	2.01805904E-05	2.91987366E-05	5.86912477E-03	7.94923731E-05
1	25	2.46479748E-06	2.10084411E-C4	2.30859386E-03	1.0985548CE-C4
1	29	3.06015576E-05	1.52113891E-06	2.02330550E-02	4.81375751E-03
1	33	3.97618063E-03	6.17778992E-C6	7.71207804E-04	6.67015316E-C3
1	37	4.81624098E-03	2.75076466E-03	5.85791268E-04	4.82502094E-04
1	41	5.95146487E-06	2.23030764E-C6	4.75653357E-07	3.03218252E-C7
1	45	1.25060419E-07	2.71882806E-05	8.50025176E-05	1.17011315E-04
1	49	-9.62123889E-07	-4.12844677E-C6	1.07137173E-05	1.38935231E-C4
1	53	2.60864398E-03	1.74962268E-04	6.04076638E-04	4.28118908E-03
1	57	3.15612193E-05	7.03016400E-C6	4.08273876E-04	1.42170985E-C5
1	61	1.68447020E-03	1.17703399E-03	3.47239825E-04	2.45452095E-03
1	65	7.24354186E-04	3.06177881E-C5	-5.79596544E-04	2.26075309E-C4
1	69	6.06747606E-06	-4.21192149E-04	5.05314330E-05	2.23933093E-04
1	73	-3.78903618E-C4	1.02142122E-C4	-2.56064876E-04	5.71255238E-C5
1	77	-2.59390862E-04	-2.65493979E-04	8.67187204E-04	2.84514565E-03
1	81	4.75644775E-05	9.00861691E-C4	7.73672058E-04	-6.13259226E-04
1	85	-1.98280055E-03	6.17674589E-02	4.15375434E-03	3.37380770E-04
1	89	2.04984887E-03	4.42937788E-C4	2.78800581E-03	-2.08751501E-C3
1	93	1.28418761E-03	7.4829220E-04	3.30279460E-04	1.27781896E-04
2	1	5.12305849E-C2	-9.38024557E-C2	3.02482483E-03	1.13541500E-C2
2	5	-4.77465311E-03	1.85895868E-02	-7.12965330E-03	-6.77275097E-03
2	9	7.05480541E-03	-2.81927842E-C6	-7.57665369E-03	-8.18171770E-C3
2	13	-4.02767476E-05	-8.44746263E-05	-1.23409744E-05	-1.52574010E-05
2	17	-5.31044093E-06	-1.50324529E-C3	1.57474057E-03	-1.28803286E-C3
2	21	-1.06291004E-04	1.65694373E-04	-5.04402141E-05	-4.56511191E-03
2	25	4.74056828E-07	-2.48415143E-C3	-3.15687166E-04	-1.63810216E-C3
2	29	-7.52210968E-05	-9.35274382E-06	4.45609851E-03	8.98498502E-03
2	33	-2.27800082E-02	9.07101958E-C7	-3.08334165E-03	9.25577209E-C4
2	37	-1.38663972E-02	4.57833566E-02	1.64751749E-02	-1.54098939E-02
2	41	-8.01084343E-05	-2.16464105E-C4	-2.56562958E-05	-3.64312972E-C5
2	45	-1.13274068E-05	-1.72692110E-03	6.98141186E-04	-4.93337745E-04
2	49	-3.22884382E-05	4.00262597E-C5	3.12055788E-05	-1.54029390E-C3
2	53	4.64187617E-04	1.25919799E-02	2.05443035E-03	-6.26650314E-03
2	57	9.27369053E-05	1.19602774E-C3	1.33604028E-03	-2.99914585E-C4
2	61	9.38544874E-03	-7.50081000E-04	-2.44707813E-04	7.64415830E-04
2	65	1.39814868E-02	1.42695203E-C4	-2.11763155E-03	6.86906506E-C4
2	69	3.63629420E-03	-1.50813437E-02	1.82028141E-01	6.35892015E-02
2	73	-4.41588856E-03	-1.32801069E-C2	-6.45130556E-02	-1.49810078E-C1
2	77	7.31403070E-02	-3.95898658E-02	-3.28627534E-02	1.08226046E-02
2	81	-2.12644730E-02	3.16180286E-C4	-7.44669028E-03	-2.23929926E-C3
2	85	1.18435727E-02	-6.31011855E-04	1.28152957E-02	4.67712916E-03
2	89	-3.40669164E-03	-3.72410981E-C2	4.36326396E-04	-7.24800955E-C3
2	93	3.26548153E-03	-3.91671271E-04	-3.13290351E-04	1.00457022E-04
3	1	-2.11585247E-02	-1.46326584E-C2	-9.31244414E-02	-2.01675988E-C3
3	5	-3.60273501E-02	-8.58750492E-03	3.17591518E-03	6.77441643E-04
3	9	2.81078096E-03	-6.63618234E-C6	-8.67791524E-03	2.05171220E-C3
3	13	9.39534805E-06	2.45356634E-06	1.38114974E-06	2.75995360E-07
3	17	2.79969117E-07	4.83999644E-C5	-2.17516492E-04	-1.80126598E-C4
3	21	-1.77733337E-05	-5.64411234E-05	5.21399193E-03	9.02113934E-04
3	25	-5.99149926E-06	-3.38981921E-C3	2.19304817E-03	1.62777600E-C4
3	29	-4.23221267E-04	-1.00276510E-05	1.82785419E-02	-2.80294086E-03
3	33	1.73807862E-03	-1.18390157E-05	-4.20914862E-03	5.91410353E-C3
3	37	3.87151615E-03	-2.02442955E-03	5.71566533E-05	2.55949822E-03
3	41	1.30523402E-05	2.86476085E-C5	3.38002610E-06	4.70551521E-C6
3	45	1.43176900E-06	2.45000441E-04	-2.41877551E-04	1.56480255E-04
3	49	-1.29462024E-05	-5.17450306E-C5	-4.44193955E-05	-1.70417615E-C3
3	53	5.22249285E-04	5.47823067E-05	1.21926002E-02	-6.17484979E-03
3	57	-6.72031620E-05	-4.52914706E-C4	5.80743529E-05	-7.47069084E-C4
3	61	4.23715659E-03	-5.84963413E-03	-1.88011752E-03	4.72411822E-03
3	65	3.91863542E-03	-1.28264833E-C4	3.28906411E-03	7.26718985E-C4
3	69	2.57811648E-03	8.73291314E-02	1.32490167E-02	5.52847365E-03

3	73	-3.47557168E-02	2.08432504E-01	-7.26947275E-02	-3.65157930E-02
3	77	-1.39919243E-01	-2.07244730E-02	-9.99155049E-04	1.42645257E-02
3	91	-3.53340564E-03	-1.97234480E-02	-5.38536789E-03	-5.58437218E-04
3	85	1.23432852E-03	-5.92216145E-04	-8.87614287E-04	8.76745164E-05
3	89	3.34002997E-02	-3.81946911E-03	-2.48992180E-03	-1.09488268E-02
3	93	-2.80716917E-02	-1.03347817E-02	-6.25110713E-03	-2.50590566E-03
4	1	-8.93415952E-05	1.55241722E-04	-7.89469238E-06	4.05163293E-04
4	5	-3.45607720E-07	-5.30425150E-05	1.56814891E-06	1.44918000E-05
4	9	-8.61620263E-05	1.75803543E-08	-1.03938572E-05	1.02789918E-04
4	13	4.33068938E-07	9.06960409E-07	1.32282933E-07	1.63396906E-07
4	17	5.68267388E-08	1.62046315E-05	-1.53817201E-05	1.20564434E-05
4	21	8.70371213E-07	-1.50909450E-06	1.02755587E-06	-2.05353464E-05
4	25	1.66511971E-08	-8.65963986E-07	1.32326402E-06	-8.72062029E-06
4	29	-7.16749529E-08	-4.33837206E-08	-6.97736674E-06	7.94473003E-05
4	33	-6.06633040E-05	3.35099469E-08	-6.67214830E-07	-7.87958766E-07
4	37	-9.54997450E-05	9.11613406E-05	7.52470318E-05	-1.51255750E-04
4	41	-1.01314596E-06	-2.16815703E-06	-2.73362939E-07	-3.60627943E-07
4	45	-1.14215576E-07	-1.81152441E-05	2.38784693E-05	-2.26492917E-05
4	49	-1.74198528E-06	2.65528163E-06	6.20921358E-08	1.21554186E-07
4	53	-2.26817197E-06	5.11630313E-05	-4.32653442E-06	-7.33685352E-06
4	57	1.42294181E-07	-1.95153930E-06	7.71425467E-07	-1.18421115E-07
4	61	-1.19561416E-06	6.74967040E-07	-2.55157711E-07	-1.08855286E-06
4	65	3.76019298E-05	-7.06738308E-07	-1.45321163E-05	-5.33550108E-05
4	69	-2.78048204E-06	-2.25906648E-05	-1.60498447E-04	3.92336142E-04
4	73	8.96926103E-06	-1.94132105E-06	6.44527863E-05	1.12072829E-04
4	77	-1.58839741E-05	-3.24326203E-04	-9.92925184E-04	4.06000168E-04
4	81	6.69216094E-04	8.60146264E-05	-7.27628659E-05	-6.11310125E-06
4	85	-2.88796664E-04	-3.28890383E-06	-2.13124281E-05	-1.40758312E-03
4	89	-6.55122870E-06	-1.42473673E-04	-2.89849238E-04	-3.22982410E-04
4	93	1.31602059E-04	-2.50006673E-05	-1.15230946E-05	3.10234628E-05
5	1	1.02183012E-04	6.14775207E-05	1.64926485E-04	1.02137621E-06
5	5	-2.15430359E-05	-1.53093243E-05	-7.48192471E-06	1.88631953E-06
5	9	-1.65605342E-05	5.70711648E-09	6.59998080E-06	-1.42711977E-05
5	13	-1.53522060E-08	-5.77712911E-09	-2.06530253E-09	-8.40538883E-10
5	17	-3.83000922E-10	-1.29362846E-07	1.36751055E-06	1.68919011E-06
5	21	2.26327656E-07	4.48352372E-07	-1.20642163E-05	-1.73584909E-06
5	25	5.02943364E-09	3.32046519E-06	-4.98332774E-06	-3.93624537E-07
5	29	8.36185062E-07	1.97771122E-08	-4.10665447E-05	6.63712519E-06
5	33	-2.87508835E-06	1.28069355E-08	4.86933640E-06	-1.24403550E-05
5	37	-8.84079359E-06	2.71912021E-06	5.96268958E-06	-2.66516232E-06
5	41	-1.99116097E-10	-5.03258206E-08	-3.97403024E-09	-8.75488731E-09
5	45	-2.53344827E-09	-3.99690263E-07	-1.80274203E-07	-1.19289719E-06
5	49	-1.54388979E-07	-1.82861751E-07	1.11692905E-07	1.50935382E-06
5	53	-8.57796957E-07	1.22314384E-07	-2.17772630E-05	9.79375070E-06
5	57	9.37232854E-08	4.32177631E-07	-1.64465741E-07	5.64589302E-07
5	61	-5.76687833E-06	1.26649631E-05	4.03392305E-06	-5.82954152E-06
5	65	-7.58710747E-06	-1.87042565E-06	-3.10103897E-05	-1.02125718E-05
5	69	-1.65755093E-05	-5.03973732E-04	-6.78329340E-05	-3.01052375E-05
5	73	9.21420522E-05	-8.60706584E-04	3.40795306E-04	1.66454611E-04
5	77	6.72030479E-04	9.71086634E-05	-1.15828719E-05	-1.23063476E-04
5	81	1.86838462E-05	1.52246500E-04	4.47292369E-05	1.47849693E-04
5	85	-1.88613366E-06	1.58469387E-05	-2.53133594E-05	-4.33034942E-06
5	89	-4.52437275E-04	4.07025564E-05	3.25524272E-05	6.93614015E-05
5	93	2.37830910E-04	1.18757856E-04	7.32310828E-05	2.63028255E-05
6	1	4.76396242E-05	-1.92321805E-04	3.42858309E-05	1.64299459E-05
6	5	-1.62114099E-05	-6.83422694E-05	-1.80612386E-05	-1.12956142E-05
6	9	1.16881227E-05	-1.05065077E-08	-1.88619584E-05	-1.22076663E-05
6	13	-6.19088436E-08	-1.29501851E-07	-1.89421645E-08	-2.34219179E-08
6	17	-8.15008043E-09	-2.28900753E-06	2.30175076E-06	-1.86806692E-06
6	21	-1.62428558E-07	2.53865465E-07	-3.45668679E-07	-6.30310881E-06
6	25	-2.75438674E-09	-5.84902704E-06	-8.75246359E-07	-2.35431010E-06
6	29	-1.63774916E-07	-1.51471046E-08	9.75208860E-06	-1.70103600E-06

6	33	-4.30797683E-05	-6.27490920E-09	-7.37695132E-06	6.38298151E-07
6	37	-5.77514648E-06	8.31166651E-05	2.73673951E-05	-2.04650660E-05
6	41	-9.88046685E-08	-3.19709432E-07	-3.65667220E-08	-5.44178057E-08
6	45	-1.67650292E-08	-2.47715272E-06	7.24731882E-07	-2.57722296E-07
6	49	-4.01906760E-08	3.79463867E-08	5.98114400E-08	-3.16303218E-06
6	53	9.85115469E-07	1.95231868E-05	3.99452721E-06	-9.90464587E-06
6	57	1.46514564E-07	2.07342643E-06	1.69676170E-06	-3.589286 8E-07
6	61	1.49506284E-05	2.34629505E-06	7.94984771E-07	-1.85423516E-06
6	65	2.01834373E-05	-3.49299599E-07	-1.33288665E-05	2.04597369E-05
6	69	2.06284689E-05	-7.26241060E-05	8.43336884E-04	2.95370420E-04
6	73	-2.42927781E-05	-5.33902708E-05	-2.91409169E-04	-6.99210016E-04
6	77	3.57077277E-04	-1.99783042E-04	-1.70726467E-04	4.24958510E-05
6	81	-8.80366283E-05	1.20824504E-05	-1.38882395E-04	-2.19827808E-05
6	85	1.73717650E-04	-2.90861643E-06	1.45813036E-04	6.27014304E-05
6	89	-4.36324202E-05	-4.63522378E-04	6.05549064E-05	-9.79977440E-05
6	93	-9.59324927E-06	-1.51363965E-05	-4.75292573E-06	2.56011385E-05

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JT	1	96					
	1	31	1	0	2		
	1	37	3	4	5	6	
	1	54	7	8			
	1	65	9				
	1	70	10	11	12	13	14

000000000

IHT	1	6					
	1	1	1	2	3	0	0

000000000

ISIGT	1	6					
	1	1	0	0	0	1	2

000000000

FREQSC	1	1					
	1	1	0.0				

000000000

MODESC	6	1					
	1	1	0.0				
	2	1	0.0				
	3	1	0.0				
	4	1	0.0				
	5	1	0.0				
	6	1	0.0				

000000000

JC	1	1					
	1	1	1				

000000000

IHC	1	6					
	1	1	1	2	3	0	0

000000000

ISIGC	1	6					
	1	1	0	0	0	1	2

000000000

INCOND	6	3					
	2	1	180.		3.		180.
	3	1	0.		0.1		0.
	4	1	6.		0.		-2.
	5	1	13.8		0.		9.15
	6	1	11.12		36.38		0.0

000000000

1	2	2	T, SEC	UT	TARGET LTN VEL	(I COMP/T TRIAD), IPS
1	3	2	T, SEC	VT	TARGET LTN VEL	(J COMP/T TRIAD), IPS
1	4	2	T, SEC	WT	TARGET LTN VEL	(K COMP/T TRIAD), IPS
1	5	2	T, SEC	OMXT	TARGET ROT VEL	(I COMP/T TRIAD), DPS
1	6	2	T, SEC	OMYT	TARGET ROT VEL	(J COMP/T TRIAD), DPS

2	1	-2.91474528E-05	-1.52660247E-C5	7.94852302E-C4	2.66242646E-C5
2	5	5.20392374E-05	2.77615483E-D7	2.35689672E-05	2.17862838E-04
2	9	3.44388233E-05	1.09246492E-C5	-5.56375182E-04	-2.35773047E-C4
2	13	1.41511359E-05	1.27635645E-05		
3	1	1.21136805E-05	-1.15872227E-C5	1.94109146E-05	-3.99939026E-C5
3	5	7.79460617E-05	-1.54271345E-05	-7.81754333E-04	-2.26373116E-04
3	9	2.34721117E-04	7.93266973E-C5	-9.32890174E-06	-9.90928984E-C5
3	13	2.84309935E-05	2.11170183E-04		
4	1	-7.17712332E-06	-6.13312115E-C5	-9.90614064E-05	9.73504723E-C5
4	5	7.47866263E-05	-1.44918745E-04	5.24854656E-05	-4.54864112E-06
4	9	4.08274598E-05	-2.74983309E-C5	8.83878113E-05	-4.09555955E-C4
4	13	4.06192304E-05	-5.57115100E-06		
5	1	-5.07791649E-03	1.43951491E-C2	-7.92058377E-03	-2.61401214E-C2
5	5	-7.15160868E-03	2.25925616E-03	-4.69875981E-03	-3.31425635E-03
5	9	-6.28561112E-03	-4.30982556E-C3	3.16609280E-02	1.07251359E-C2
5	13	-9.10841690E-04	-1.35164385E-04		
6	1	-2.14941189E-02	-1.30899041E-C3	-5.04784146E-C3	1.52679139E-C3
6	5	5.75175350E-03	-9.86934598E-04	8.60929157E-04	-1.74451642E-02
6	9	2.33170332E-04	4.06231986E-C2	3.43828044E-03	1.59705874E-C3
6	13	5.12837618E-03	5.56540263E-03		

000000000

CVEC

6 12

1	1	0.0	2.0	20.0	100.0
1	5	28320.0	2.0	20.0	0.0
1	9	0.0	0.0	0.5	-484.0
2	1	0.0	2.0	20.0	100.0
2	5	100.0	2.0	20.0	0.0
2	9	0.0	0.0	0.5	0.831
3	1	0.0	2.0	20.0	100.0
3	5	-200.0	2.0	20.0	0.0
3	9	0.0	0.0	0.5	36.17
4	1	0.0	4.0	20.0	100.0
4	5	15360.0	0.5	1.0	0.0
4	9	0.007	1.0	1.0	
5	1	-3.0	4.0	20.0	100.0
5	5	15360.0	0.5	1.0	0.0
5	9	0.007	1.0	1.0	
6	1	0.0	4.0	20.0	100.0
6	5	15360.0	0.5	1.0	0.0
6	9	0.007	1.0	1.0	

000000000

SC-1

0	0.0	2.5	30.
100.	300.	0.	
12.	0.	0.	

STOP

MCR-70-2 (Vol II)

APPENDIX E
PROGRAM DCKEL OUTPUT

Appendix E presents sample output from DOCKEL. This output was obtained using the input data of Appendix D. Although the program is capable of printing output at each integration interval, only a small percentage of that information is presented here.

E-2

MCR-70-2 (Vol II)

RUN NO. SC-1

DATE 18FE70
RUN BY

NAS8-21289
BASELINE CONFIGURATION

CARD INPUT MATRIX TDT0 (1 X 3)

1 1 4.07880000E+02 8.30900000E-01 3.61670000E+01

END OF READ.

CARD INPUT MATRIX CPC0 (1 X 3)

1 1 1.34700000E+02 -7.70000000E+00 -7.70000000E+00

END OF READ.

CARD INPUT MATRIX SIGMA (1 X 3)

1 1 1.80000000E+02 3.00000000E+02 6.00000000E+01

END OF READ.

CARD INPUT MATRIX AIT (3 X 3)

INERTIA FOR CLUSTER ONLY

1	1	6.42800000E+06	1.62200000E+04	3.52800000E+06
2	1	1.62200000E+04	2.47400000E+07	-1.57500000E+05
3	1	3.52800000E+06	-1.57500000E+05	2.51200000E+07

END OF READ.

THE TARGET VEHICLES MASS IS 2.96400000E+02

RUN NO. SC-1

DATE 16FE70
RUN BYNAS8-21280
BASELINE CONFIGURATION

CARD INPUT MATRIX AIC (3 X 3)

1	1	1.95240000E+05	1.69560000E+04	1.69320000E+04
2	1	1.69560000E+04	5.39016000E+05	-7.92120000E+04
3	1	1.69320000E+04	-7.92120000E+04	5.39028000E+05

END OF READ.

THE CHASE VEHICLES MASS IS 7.88577000E+01

CARD INPUT MATRIX FSPROX (2 X 8)

1	1	7.00000000E+00	0.	3.20000000E-01	8.70000000E-01
1	5	2.62000000E+00	8.12000000E+03	1.11000000E+01	1.11200000E+01
2	1	0.	-2.00000000E+03	-1.25000000E+02	-1.18000000E+02
2	5	-1.06200000E+02	-8.10000000E+01	-6.90000000E+01	7.31000000E+02

END OF READ.

CARD INPUT MATRIX FDMROX (2 X 5)

1	1	4.00000000E+00	-1.20000000E+01	-1.00000000E-01	1.00000000E-01
1	5	1.20000000E+01			
2	1	0.	-9.20000000E+01	-9.10000000E+01	9.10000000E+01
2	5	9.20000000E+01			

END OF READ.

RUN NO. SC-1

DATE 16FE70
RUN BYNAS8-21280
BASELINE CONFIGURATION

CARD INPUT MATRIX FSPALL (2 X 19)

1	1	1.80000000E+01	-7.08000000E-02	-6.60500000E-02	-5.87000000E-02
1	5	-5.13500000E-02	-3.67000000E-02	-2.93600000E-02	-2.20200000E-02
1	9	-1.46800000E-02	-7.34000000E-03	7.34000000E-03	1.46800000E-02
1	13	2.20200000E-02	2.93600000E-02	3.67000000E-02	5.13500000E-02
1	17	5.87000000E-02	6.60500000E-02	7.08000000E-02	
2	1	0.	-8.17500000E+04	-7.23000000E+04	-5.91500000E+04
2	5	-4.91000000E+04	-3.32200000E+04	-2.61700000E+04	-1.95000000E+04
2	9	-1.29400000E+04	-6.25600000E+03	6.25600000E+03	1.29400000E+04
2	13	1.95000000E+04	2.61700000E+04	3.32200000E+04	4.91000000E+04
2	17	5.91500000E+04	7.23000000E+04	8.17500000E+04	

END OF READ.

CARD INPUT MATRIX FDMALY (2 X 3)

1	1	2.00000000E+00	0.	1.00000000E+00
2	1	0.	0.	1.00000000E-06

END OF READ.

CARD INPUT MATRIX FSPALU (2 X 19)

1	1	1.80000000E+01	-7.08000000E-02	-6.60500000E-02	-5.87000000E-02
1	5	-5.13500000E-02	-3.67000000E-02	-2.93600000E-02	-2.20200000E-02
1	9	-1.46800000E-02	-7.34000000E-03	7.34000000E-03	1.46800000E-02
1	13	2.20200000E-02	2.93600000E-02	3.67000000E-02	5.13500000E-02
1	17	5.87000000E-02	6.60500000E-02	7.08000000E-02	
2	1	0.	-8.17500000E+04	-6.51500000E+04	-4.70000000E+04
2	5	-3.68000000E+04	-2.22000000E+04	-1.71800000E+04	-1.22800000E+04
2	9	-8.31000000E+03	-4.08500000E+03	4.08500000E+03	8.31000000E+03
2	13	1.22800000E+04	1.71800000E+04	2.22000000E+04	3.60000000E+04
2	17	4.70000000E+04	6.51500000E+04	8.17500000E+04	

END OF READ.

CARD INPUT MATRIX FDMALZ (2 X 3)

1	1	2.00000000E+00	0.	1.00000000E+00
2	1	0.	0.	1.00000000E-06

END OF READ.

RUN NO. SC-1

DATE 16FE78
RUN BYNAS8-21200
BASELINE CONFIGURATION

CARD INPUT MATRIX FSPATT (2 X 10)

1	1	9.0000000E+00	8.4300000E+00	8.5000000E+00	9.0000000E+00
1	5	9.5000000E+00	1.0000000E+01	1.0500000E+01	1.1000000E+01
1	9	1.1250000E+01	1.1500000E+01		
2	1	0.	-3.6000000E+02	-3.0500000E+02	-1.8500000E+02
2	5	-1.2350000E+02	-8.6500000E+01	-6.2500000E+01	-4.5500000E+01
2	9	-3.8500000E+01	-3.2500000E+01		

END OF READ.

CARD INPUT MATRIX FDMATT (2 X 16) ATTEN. DAMPING (T=TEMP= +70 THRU +250 DEG F)

1	1	1.5000000E+01	-1.9200000E+01	-1.8250000E+01	-1.6800000E+01
1	5	-1.4400000E+01	-1.2000000E+01	-9.6000000E+00	-7.2000000E+00
1	9	-4.8000000E+00	-2.7600000E+00	-1.2000000E+00	-6.0000000E-01
1	13	-2.4000000E-01	-1.2000000E-01	1.2000000E-01	1.3200000E+00
2	1	0.	-2.9800000E+03	-2.6850000E+03	-2.4500000E+03
2	5	-2.1700000E+03	-1.9200000E+03	-1.6800000E+03	-1.4350000E+03
2	9	-1.1750000E+03	-9.1000000E+02	-6.3000000E+02	-4.0500000E+02
2	13	-2.1000000E+02	-1.8000000E+01	1.8000000E+01	7.8000000E+01

END OF READ.

CARD INPUT MATRIX FREQ (1 X 96)

1	5	0.	0.	2.5499619E-01	2.5665423E-01
1	9	2.5923014E-01	2.6355803E-01	2.6653024E-01	3.1636321E-01
1	13	4.0863813E-01	4.0867173E-01	4.0867593E-01	4.0867847E-01
1	17	4.0867877E-01	4.0887513E-01	5.1092976E-01	5.1394526E-01
1	21	5.3797691E-01	5.3815635E-01	5.7492257E-01	5.8164911E-01
1	25	5.8615685E-01	5.8694310E-01	6.1705018E-01	6.1810048E-01
1	29	6.1882961E-01	6.1884857E-01	7.1500014E-01	8.5719454E-01
1	33	8.7675289E-01	9.0424856E-01	9.0585786E-01	9.2024922E-01
1	37	9.8803635E-01	1.0262749E+00	1.0601834E+00	1.0975776E+00
1	41	1.1187075E+00	1.1187538E+00	1.1187610E+00	1.1187645E+00
1	45	1.1187650E+00	1.1188935E+00	1.2539246E+00	1.2590902E+00
1	49	1.3006059E+00	1.3009151E+00	1.3621632E+00	1.3628188E+00
1	53	1.3667261E+00	1.3755472E+00	1.3795888E+00	1.7346534E+00
1	57	1.8100859E+00	1.8109456E+00	1.8110794E+00	1.8225237E+00
1	61	2.1135202E+00	2.1316206E+00	2.1318187E+00	2.1347194E+00
1	65	2.1492867E+00	2.7861239E+00	2.8846019E+00	2.9061010E+00
1	69	3.3136081E+00	3.8517062E+00	4.1299005E+00	4.1417613E+00
1	73	4.4736385E+00	4.6802963E+00	6.1248091E+00	6.3301962E+00
1	77	6.6532042E+00	7.5081722E+00	7.9593684E+00	8.3072449E+00
1	81	8.9470480E+00	9.3884704E+00	9.7958880E+00	1.0089467E+01
1	85	1.0347937E+01	1.1181907E+01	1.1765487E+01	1.2207051E+01
1	89	1.2338492E+01	1.2579175E+01	1.4743140E+01	1.7521281E+01
1	93	2.5218544E+01	4.3982917E+01	5.2848261E+01	8.8817753E+01

END OF READ.

RUN NO. SC-1

DATE 16FE70
RUN BYNAS8-21280
BASELINE CONFIGURATION

CARD INPUT MATRIX RTMODE (6 X 96)

1	1	3.37096783E-02	1.23539660E-02	-1.59449945E-02	-4.34111732E-04
1	5	3.57812083E-02	-2.43781212E-02	2.35864798E-03	5.93297350E-04
1	9	-4.80510784E-04	2.86124847E-06	5.95135453E-04	-7.72296766E-05
1	13	7.54610732E-07	1.13132248E-06	1.95837124E-07	2.09693285E-07
1	17	7.93955160E-08	1.92548456E-05	6.17025205E-05	1.24977151E-04
1	21	2.01805904E-05	2.91987366E-05	5.86912477E-03	7.94923731E-05
1	25	2.46479748E-06	2.10084411E-04	2.30859386E-03	1.09899480E-04
1	29	3.06015576E-05	1.52113891E-06	2.02338550E-02	4.81375751E-03
1	33	3.97618063E-03	6.17778992E-06	7.71287804E-04	6.67019316E-03
1	37	4.81624098E-03	2.75076466E-03	5.85791268E-04	4.82502094E-04
1	41	5.95146487E-06	2.23030764E-06	4.75653357E-07	3.03218252E-07
1	45	1.25060419E-07	2.71882806E-05	8.50025176E-05	1.17011315E-04
1	49	-9.62123889E-07	-4.12844677E-06	1.07137173E-05	1.38935231E-04
1	53	2.60864398E-03	1.74962268E-04	6.04076638E-04	4.28118908E-03
1	57	3.15612193E-05	7.03016400E-06	4.08273876E-04	1.42170985E-05
1	61	1.68447020E-03	1.17703399E-03	3.47239825E-04	2.45452095E-03
1	65	7.24354186E-04	3.06177881E-05	-5.79596544E-04	2.26075309E-04
1	69	6.06747606E-06	-4.21192149E-04	5.05314330E-05	2.23933093E-04
1	73	-3.78903618E-04	1.02142122E-04	-2.56064876E-04	5.71295238E-05
1	77	-2.59398862E-04	-2.65493979E-04	8.67187204E-04	2.84514565E-03
1	81	4.75644775E-05	9.00861691E-04	7.73672058E-04	-6.13299226E-04
1	85	-1.98280055E-03	6.17674589E-02	4.15375434E-03	3.37380770E-04
1	89	2.04984887E-03	4.42937788E-04	2.78800581E-03	-2.08751501E-03
1	93	1.28418761E-03	7.42829220E-04	3.30279468E-04	1.27781896E-04
2	1	5.12305849E-02	-9.38024557E-02	3.02482483E-03	1.13541500E-02
2	5	-4.77465311E-03	1.85895868E-02	-7.12965330E-03	-6.77275097E-03
2	9	7.05480541E-03	-2.81927842E-06	-7.57665369E-03	-8.18171770E-03
2	13	-4.02767476E-05	-8.44746263E-05	-1.23409744E-05	-1.52574010E-05
2	17	-5.31844093E-06	-1.50324529E-03	1.57474857E-03	-1.28803286E-03
2	21	-1.06291004E-04	1.65694373E-04	-5.04402141E-05	-4.56511191E-03
2	25	4.74056828E-07	-2.48415143E-03	-3.15687166E-04	-1.63810216E-03
2	29	-7.52210968E-05	-9.35274382E-06	4.45609851E-03	8.98498502E-03
2	33	-2.27800082E-02	9.07101958E-07	-3.08334165E-03	9.25577209E-04
2	37	-1.38663972E-02	4.57833566E-02	1.64751749E-02	-1.54098939E-02
2	41	-8.01084343E-05	-2.16464105E-04	-2.56562958E-05	-3.64312972E-05
2	45	-1.13274068E-05	-1.72692110E-03	6.98141186E-04	-4.93337745E-04
2	49	-3.22884382E-05	4.00262597E-05	3.12055788E-05	-1.54029390E-03
2	53	4.64187617E-04	1.25919799E-02	2.05443835E-03	-6.26650314E-03
2	57	9.27369053E-05	1.19602774E-03	1.33604028E-03	-2.99914585E-04
2	61	9.38544874E-03	-7.50081000E-04	-2.44707813E-04	7.64415830E-04
2	65	1.39814868E-02	1.42695283E-04	-2.11763155E-03	6.86906506E-04
2	69	3.63629420E-03	-1.50813437E-02	1.82028141E-01	6.35892015E-02
2	73	-4.41588856E-03	-1.32801869E-02	-6.45130556E-02	-1.49810078E-01
2	77	7.31403070E-02	-3.95398658E-02	-3.28627534E-02	1.08226846E-02
2	81	-2.12644730E-02	3.16188286E-04	-7.44669828E-03	-2.23929026E-03
2	85	1.18435727E-02	-6.31011855E-04	1.28152957E-02	4.67712016E-03
2	89	-3.40669164E-03	-3.72418981E-02	4.36326396E-04	-7.24800995E-03

RUN NO. SC-1

DATE 16FE70
RUN BYNAS8-21280
BASELINE CONFIGURATION

CARD INPUT MATRIX RTHODE (6 x 96) CONTINUED

2	93	3.26548153E-03	-3.91671271E-04	-3.13290351E-04	1.00457022E-04
3	1	-2.11585247E-02	-1.46326584E-02	-9.31244414E-02	-2.01675988E-03
3	5	-3.60273501E-02	-8.58750492E-03	3.17591518E-03	6.77441643E-04
3	9	2.81078096E-03	-6.63618234E-06	-8.67791524E-03	2.05171220E-03
3	13	9.39534805E-06	2.45356634E-06	1.38114974E-06	4.05995360E-07
3	17	2.79969117E-07	4.83999644E-05	-2.17516492E-04	-1.80126598E-04
3	21	-1.77733337E-05	-5.64411234E-05	5.21399193E-03	9.02113934E-04
3	25	-5.99149926E-06	-3.38981921E-03	2.19304817E-03	1.62777600E-04
3	29	-4.23221267E-04	-1.00276510E-05	1.82785419E-02	-2.80294086E-03
3	33	1.73807862E-03	-1.18396157E-05	-4.20914862E-03	5.91410353E-03
3	37	3.87151615E-03	-2.02442955E-03	5.71566533E-05	2.55949822E-03
3	41	1.30523402E-05	2.86476085E-05	3.38002610E-06	4.70551521E-06
3	45	1.43176900E-06	2.45000441E-04	-2.41877551E-04	1.56480255E-04
3	49	-1.29462024E-05	-5.17450306E-05	-4.44193955E-05	-1.70417615E-03
3	53	5.22249285E-04	5.47823067E-05	1.21926002E-02	-6.17484979E-03
3	57	-6.72031620E-05	-4.52914706E-04	5.80743529E-05	-7.47069084E-04
3	61	4.23715659E-03	-5.84963413E-03	-1.88011752E-03	4.72411822E-03
3	65	3.91863542E-03	-1.28264833E-04	3.28906411E-03	7.26718985E-04
3	69	2.57811648E-03	8.73291314E-02	1.32490167E-02	5.52847369E-03
3	73	-3.47557168E-02	2.08432504E-01	-7.26947275E-02	-3.65157930E-02
3	77	-1.39919243E-01	-2.07244730E-02	-9.99155049E-04	1.42645257E-02
3	81	-3.53340564E-03	-1.97234480E-02	-5.38535789E-03	-5.58437218E-04
3	85	1.23432852E-03	-5.92216145E-04	-8.87614287E-04	8.76749164E-05
3	89	3.34002997E-02	-3.81946911E-03	-2.48992180E-03	-1.09488268E-02
3	93	-2.80716917E-02	-1.03347817E-02	-6.25110713E-03	-2.50590566E-03
4	1	-8.93415952E-05	1.55241722E-04	-7.89459238E-06	4.05163293E-04
4	5	-3.45607720E-07	-5.30425150E-05	1.56814891E-06	1.44918000E-05
4	9	-8.61620263E-05	1.75803543E-03	-1.03938572E-05	1.02789918E-04
4	13	4.33068938E-07	9.06960409E-07	1.32282933E-07	1.63396906E-07
4	17	5.68267388E-08	1.62046315E-05	-1.53817201E-05	1.20564434E-05
4	21	8.70371213E-07	-1.50989450E-06	1.02755587E-06	-2.05353464E-05
4	25	1.66511971E-08	-8.65963986E-07	1.32326402E-06	-8.72062029E-06
4	29	-7.16749529E-08	-4.33837206E-08	-6.97736674E-06	7.94473003E-05
4	33	-6.06633040E-05	3.35099469E-08	-6.67214830E-07	-7.87958766E-07
4	37	-9.54997450E-05	9.11613486E-05	7.52470318E-05	-1.51295750E-04
4	41	-1.01314596E-06	-2.16815703E-06	-2.73362939E-07	-3.60627943E-07
4	45	-1.14215576E-07	-1.81152441E-05	2.38784693E-05	-2.26492917E-05
4	49	-1.74198528E-06	2.65528163E-06	6.20921358E-08	1.21554186E-07
4	53	-2.26817197E-06	5.11630313E-05	-4.32653442E-06	-7.33685352E-06
4	57	1.42294181E-07	-1.95153930E-06	7.71425467E-07	-1.18421115E-07
4	61	-1.19561416E-06	6.74967040E-07	-2.55157711E-07	-1.08855286E-06
4	65	3.76019298E-05	-7.06738388E-07	-1.45321163E-05	-5.33550108E-05
4	69	-2.78048204E-06	-2.25906648E-05	-1.60498447E-04	3.92336142E-04
4	73	8.96926103E-06	-1.94132105E-06	6.44527863E-05	1.12072829E-04
4	77	-1.58839741E-05	-3.24326283E-04	-9.92925184E-04	4.06000168E-04
4	81	6.69216094E-04	8.60146264E-05	-7.27628659E-05	-6.11310125E-06
4	85	-2.88796664E-04	-3.28898383E-06	-2.13124281E-05	-1.40758312E-03

RUN NO. SC-1

DATE 16FE70
RUN BY

NAS8-21280
BASELINE CONFIGURATION

CARD INPUT MATRIX RTMODE (6 X 96) CONTINUED

4	89	-6.55122870E-06	-1.42473673E-04	-2.89849238E-04	-3.22982418E-04
4	93	1.31602059E-04	-2.50006673E-05	-1.15238946E-05	3.10234628E-05
5	1	1.02183012E-04	6.14775207E-05	1.64926485E-04	1.02137621E-06
5	5	-2.15438359E-05	-1.53093243E-05	-7.48192471E-06	1.88631953E-06
5	9	-1.65605342E-05	5.70711648E-09	6.59998080E-06	-1.42711977E-05
5	13	-1.53522060E-08	-5.77712911E-09	-2.06538253E-09	-8.48538883E-10
5	17	-3.83800922E-10	-1.29362846E-07	1.36751055E-06	1.68919011E-06
5	21	2.26327656E-07	4.48352372E-07	-1.20642163E-05	-1.73584909E-06
5	25	5.02943364E-09	3.32846519E-06	-4.98332774E-06	-3.93624537E-07
5	29	8.36185062E-07	1.97771122E-08	-4.10665447E-05	6.63712519E-06
5	33	-2.87508835E-06	1.28069355E-08	4.86933648E-06	-1.24483550E-05
5	37	-8.84079359E-06	2.71912021E-06	5.96268958E-06	-2.66516232E-06
5	41	-1.99116097E-10	-5.03258206E-08	-3.97403024E-09	-8.75488731E-09
5	45	-2.53344827E-09	-3.99690263E-07	-1.80274203E-07	-1.19289719E-06
5	49	-1.54388979E-07	-1.82861751E-07	1.11692905E-07	1.50935382E-06
5	53	-8.57796957E-07	1.22314384E-07	-2.17772680E-05	9.79375070E-06
5	57	9.37232854E-08	4.32177631E-07	-1.64465741E-07	5.64589302E-07
5	61	-5.76687833E-06	1.26649631E-05	4.83392385E-06	-5.82954152E-06
5	65	-7.58710747E-06	-1.87842565E-06	-3.18103897E-05	-1.02125718E-05
5	69	-1.65755093E-05	-5.03973732E-04	-6.78329348E-05	-3.01852375E-05
5	73	9.21420522E-05	-8.60706584E-04	3.40795300E-04	1.66454611E-04
5	77	6.72830479E-04	9.71886634E-05	-1.15828719E-05	-1.23863476E-04
5	81	1.86838462E-05	1.52246588E-04	4.67292369E-05	1.47849693E-04
5	85	-1.88613366E-06	1.58469387E-05	-2.53133594E-05	-4.33034942E-06
5	89	-4.52437275E-04	4.07825564E-05	3.25524272E-05	6.93614015E-05
5	93	2.37830910E-04	1.18757856E-04	7.32318828E-05	2.63028255E-05
6	1	4.76396242E-05	-1.92321805E-04	3.42858389E-05	1.64299459E-05
6	5	-1.62114099E-05	-6.83422694E-05	-1.80612386E-05	-1.12956142E-05
6	9	1.16881227E-05	-1.05865877E-08	-1.88619584E-05	-1.22076663E-05
6	13	-6.19888436E-08	-1.29581851E-07	-1.89421645E-08	-2.34219179E-08
6	17	-8.15888843E-09	-2.28988753E-06	2.30175076E-06	-1.86886692E-06
6	21	-1.62428558E-07	2.53865465E-07	-3.45668679E-07	-6.30318881E-06
6	25	-2.75438674E-09	-5.84902704E-06	-8.75246359E-07	-2.35431010E-06
6	29	-1.63774916E-07	-1.51471046E-08	9.75288868E-06	-1.70103688E-06
6	33	-4.38797683E-05	-6.27498920E-09	-7.37695132E-06	6.38298151E-07
6	37	-5.77514648E-06	8.31166651E-05	2.73673951E-05	-2.04650668E-05
6	41	-9.88046685E-08	-3.19789432E-07	-3.65667220E-08	-5.44178857E-08
6	45	-1.67650292E-08	-2.47715272E-06	7.24731882E-07	-2.57722296E-07
6	49	-4.81906760E-08	3.79463867E-08	5.98114400E-08	-3.16303218E-06
6	53	9.85115469E-07	1.95231868E-05	3.99452721E-06	-9.90464587E-06
6	57	1.46514564E-07	2.07342643E-06	1.69676170E-06	-3.58928608E-07
6	61	1.49586284E-05	2.34629585E-06	7.94984771E-07	-1.85423516E-06
6	65	2.81834373E-05	-3.49299599E-07	-1.33288663E-05	2.84597369E-05
6	69	2.06284689E-05	-7.26241860E-05	8.43336884E-04	2.95378428E-04
6	73	-2.42927781E-05	-5.33982708E-05	-2.91409169E-04	-6.99210076E-04
6	77	3.57077277E-04	-1.99783042E-04	-1.78726467E-04	4.24958510E-05
6	81	-8.80366283E-05	1.28824504E-05	-1.38882395E-04	-2.19827888E-05
6	85	1.73717650E-04	-2.98861643E-06	1.45813036E-04	6.27814384E-05
6	89	-4.36324282E-05	-4.63522378E-04	6.05549864E-05	-9.79977448E-05
6	93	-9.59324927E-06	-1.51363965E-05	-4.75292573E-06	2.56011385E-05

END OF READ.

RUN NO. SC-1

DATE 14FE70
RUN BYNAS8-21280
BASELINE CONFIGURATION

CARD INPUT INTEGER MATRIX JT (1 X 96)

1	31	1	0	2	-0	-0	-0	-0	-0	-0	-0	-0	-0	-0	-0
1	37	3	4	5	6	-0	-0	-0	-0	-0	-0	-0	-0	-0	-0
1	54	7	8	-0	-0	-0	-0	-0	-0	-0	-0	-0	-0	-0	-0
1	65	9	-0	-0	-0	-0	-0	-0	-0	-0	-0	-0	-0	-0	-0
1	70	10	11	12	13	14	-0	-0	-0	-0	-0	-0	-0	-0	-0

END OF READIN.

CARD INPUT INTEGER MATRIX IHT (1 X 6)

1	1	1	2	3	0	0	0
---	---	---	---	---	---	---	---

END OF READIN.

CARD INPUT INTEGER MATRIX ISIGT (1 X 6)

1	1	0	0	0	1	2	3
---	---	---	---	---	---	---	---

END OF READIN.

CARD INPUT MATRIX FREOSC (1 X 1)

1	1	0.
---	---	----

END OF READ.

CARD INPUT MATRIX MODESC (6 X 1)

1	1	0.
2	1	0.
3	1	0.
4	1	0.
5	1	0.
6	1	0.

END OF READ.

RUN NO. SC-1

DATE 16FE70
RUN BY

NAS0-21200
BASELINE CONFIGURATION

CARD INPUT INTEGER MATRIX JC (1 X 1)

1 1 1

END OF READIN.

CARD INPUT INTEGER MATRIX IHC (1 X 6)

1 1 1 2 3 0 0 0

END OF READIN.

CARD INPUT INTEGER MATRIX ISIGC (1 X 6)

1 1 0 0 0 1 2 3

END OF READIN.

OUTPUT MATRIX LOC (1 X 12)

1 1 1 7 10 16 22 25 31 37 51 65 66 67

END OF WRITIN.

OUTPUT MATRIX LEN (1 X 12)

1 1 6 3 6 6 3 6 6 14 14 1 1 26

END OF WRITIN.

RUN NO. SC-1

DATE 16FE78
RUN BYNAS8-21280
BASELINE CONFIGURATION

CARD INPUT MATRIX INCOND (6 X 3)

2	1	1.80000000E+02	3.00000000E+00	1.80000000E+02
3	1	0.	1.00000000E-01	0.
4	1	6.00000000E+00	0.	-2.00000000E+00
5	1	1.30000000E+01	0.	9.15000000E+00
6	1	1.11200000E+01	3.63800000E+01	0.

END OF READ.

THE DATMIN ARRAY IS AS FOLLOWS --

- 1 TARGET EULER ANGLES - PSI, THETA, PHI (DEGREES)
- 2 CHASE / TARGET EULER ANGLES - PSI, THETA, PHI (DEGREES)
- 3 CHASE ANGULAR VELOCITY - OMEGA X, OMEGA Y, OMEGA Z - (DEGREES/SEC)
- 4 CHASE C.G. VELOCITY IN X,Y,Z DIRECTIONS REFERENCED TO CHASE (LENGTH/SEC)
- 5 D TO S DISTANCE IN X,Y,Z DIRECTIONS REFERENCED TO TARGET (LENGTH)
- 6 RHO(X), (LENGTH), GAMMA(1,2,3), (DEGREES), -----

RUN NO. SC-1

DATE 16FE78
RUN BY

MAS8-21200
BASELINE CONFIGURATION

OUTPUT MATRIX YINYL (1 X 107)

	(1)	(2)	(3)	(4)	(5)	(6)	(7)	(8)	(9)	(10)
1 1	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.000E+00
1 11	0.	-0.	0.	1.000E+00	0.	6.000E+00	0.	-2.000E+00	0.	1.745E-03
1 21	0.	5.038E+02	0.531E+00	4.610E+01	-9.986E-01	-3.426E-15	-5.236E-02	-3.251E-15	1.000E+00	-3.426E-15
1 31	1.112E+01	0.	0.	6.350E-01	6.350E-01	6.350E-01	0.	0.	0.	0.

END OF WRITE.

RUN NO. SC-1

DATE 16FE70
RUN BYNAS8-21280
BASELINE CONFIGURATION

THE INPUT SCALARS TO PROGRAM DOCKEL ARE

```
STARTT = 0.
DELTAT = .010000
ENDT = 5.000000
XDLTA = .500000
XPRNT = 50.000000
ZETAT = .010000
ZETAC = .010000
IFELAS = 1
IFPLOT = 1
IFPER = 1
JBATCH = 1
MINIC = 1
IFPNCH = 0
NCOLS = 58
NCNSYS = 34
NFORCS = 10
NEQTN = 100
NMODET = 14
NMODEC = 1

AA = 2.25000000E+00
AB = 8.50000000E-01
AD = 7.00000000E-01
AE = 9.65000000E-01
AF = 3.00500000E+00
AP = 4.25000000E+00
DLB = 1.44800000E+01
OLD = 1.29000000E+01
OLE = 1.75900000E+01
DLF = 4.75000000E+00
DLI = 1.41000000E+01
DLP = 3.30000000E+00
DLQ = 1.65300000E+01
OLS = 2.05500000E+00
FDD = 1.15000000E+01
PEO = 1.05000000E+01
ALPHAD = 4.27500000E+01
CSPHER = 2.50000000E+00
RADCON = 1.35600000E+01
AKD1 = 0.
AKD2 = 0.
AKD3 = 5.41000000E+00
RHOSO = 2.00000000E+00
FRETLL = 1.00000000E+03
EXTL = 1.11200000E+01
TLAG = 1.01500000E+01
TSTAR = 0.
BNDMU = 2.00000000E-01
HDMU = 2.60000000E-01
ARMMU = 2.60000000E-01
```

RUN NO. SC-1

DATE 16FE70
RUN BY

NAS8-21280
BASELINE CONFIGURATION

CARD INPUT MATRIX CMGSLP (6 X 14)

1	1	-7.26375859E-05	1.14622589E-04	4.27000728E-06	2.73991503E-04
1	5	-5.58963318E-04	2.72508185E-04	1.31209158E-05	3.11969468E-05
1	9	-2.09105069E-04	-6.34475302E-05	2.57131685E-04	4.79394787E-05
1	13	-4.86035021E-04	-5.91527509E-04		
2	1	-2.91474528E-05	-1.52660247E-05	7.94852302E-04	2.66242646E-05
2	5	5.20392374E-05	2.77615483E-07	2.35689672E-05	2.17862838E-04
2	9	3.44388233E-05	1.09246492E-05	-5.56375182E-04	-2.35773047E-04
2	13	1.41511359E-05	1.27635645E-05		
3	1	1.21136805E-05	-1.15872227E-05	1.94109146E-05	-3.99939026E-05
3	5	7.79460617E-05	-1.54271345E-05	-7.81754333E-04	-2.26373116E-04
3	9	2.34721117E-04	7.93266979E-05	-9.32898174E-06	-9.90988884E-05
3	13	2.84309935E-05	2.11170183E-04		
4	1	-7.17712332E-06	-6.13312115E-05	-9.90614064E-05	9.73504723E-05
4	5	7.47866263E-05	-1.44918745E-04	5.24854656E-05	-4.54864112E-06
4	9	4.08274598E-05	-2.74983309E-05	8.83878113E-05	-4.09595955E-04
4	13	4.06192304E-05	-5.57115100E-06		
5	1	-5.07791649E-03	1.43951491E-02	-7.92058377E-03	-2.61401214E-02
5	5	-7.15160868E-03	2.25925616E-03	-4.69875981E-03	-3.31425635E-03
5	9	-6.28561112E-03	-4.30982556E-03	3.16689280E-02	1.07251359E-02
5	13	-9.10841698E-04	-1.35184385E-04		
6	1	-2.14941189E-02	-1.30899041E-03	-5.04784146E-03	1.52679139E-03
6	5	5.75175350E-03	-9.86934598E-04	8.60929157E-04	-1.74451642E-02
6	9	2.33170332E-04	4.06231986E-02	3.43828044E-03	1.59705874E-03
6	13	5.12837618E-03	5.56540263E-03		

END OF READ.

CARD INPUT MATRIX CVEC (6 X 12)

1	1	0.	2.00000000E+00	2.00000000E+01	1.00000000E+02
1	5	2.83200000E+04	2.00000000E+00	2.00000000E+01	0.
1	9	0.	0.	5.00000000E-01	-4.84000000E+02
2	1	0.	2.00000000E+00	2.00000000E+01	1.00000000E+02
2	5	1.00000000E+02	2.00000000E+00	2.00000000E+01	0.
2	9	0.	0.	5.00000000E-01	8.31000000E-01
3	1	0.	2.00000000E+00	2.00000000E+01	1.00000000E+02
3	5	-2.00000000E+02	2.00000000E+00	2.00000000E+01	0.
3	9	0.	0.	5.00000000E-01	3.61700000E+01
4	1	0.	4.00000000E+00	2.00000000E+01	1.00000000E+02
4	5	1.53600000E+04	5.00000000E-01	1.00000000E+00	0.
4	9	7.80000000E-03	1.00000000E+00	1.00000000E+00	-0.
5	1	-3.00000000E+00	4.00000000E+00	2.00000000E+01	1.00000000E+02
5	5	1.53600000E+04	5.00000000E-01	1.00000000E+00	0.
5	9	7.00000000E-03	1.00000000E+00	1.00000000E+00	-0.
6	1	0.	4.00000000E+00	2.00000000E+01	1.00000000E+02
6	5	1.53600000E+04	5.00000000E-01	1.00000000E+00	0.
6	9	7.00000000E-03	1.00000000E+00	1.00000000E+00	-0.

END OF READ.

SIMULATION TIME = 1.0000E+00

	Y (I)	YOOT (I)
U - TARGET	-6.53045006E-01	1.04489443E-03
	-2.15296265E-02	-2.93016913E-05
	4.21112870E-01	1.61888245E-03
	8.07355482E-03	9.53540921E-06
	-1.41768653E-01	-6.05199704E-07
	-7.77701543E-03	1.61410641E-05
X - TARGET	-5.21302477E-01	-6.53877036E-01
	-1.53549278E-02	-2.15089943E-02
	3.34713360E-01	4.19820841E-01
GAMMA TARGET	9.99998047E-01	-4.89715037E-06
	-9.81799367E-05	-1.35990022E-04
	1.97379776E-03	2.47431090E-03
	9.79759316E-05	1.35456131E-04
	9.99999990E-01	-2.78767074E-08
	1.03453033E-04	1.41177751E-04
U - CHASE	8.58759832E+00	5.05363808E+00
	1.15379688E-01	5.57880229E-02
	-4.86358729E-01	-3.18536303E-01
	-4.40033010E-02	3.09762868E-02
	-2.12584833E+00	-1.43167297E-03
	-3.69721167E-01	7.28028290E-04
X - CHASE	5.77267510E+02	-8.59916630E+00
	8.58538920E+00	6.95529936E-02
	4.63857310E+01	-2.14950036E-01
GAMMA CHASE	-9.96660732E-01	3.05757588E-03
	-5.28755205E-03	-6.42089657E-03
	-8.14826775E-02	-3.69822766E-02
	-5.33994329E-03	-6.49388014E-03
	9.99985652E-01	-3.47793193E-05
	4.25067028E-04	2.39652990E-04
RHOS	1.10982264E+01	5.44338967E-03
	-3.74396055E-02	9.35990137E-03
	-3.78674898E-02	9.46687245E-03
	3.64116305E+01	-1.22738947E-02
	3.64116305E+01	-1.22738947E-02
	3.64116305E+01	-1.22738947E-02
MODE VEL - TARGET	1.86025829E+00	-2.62472549E+00
	2.38658132E-02	-1.69005590E+00
	-1.11416716E-01	-1.29515334E+00
	-2.94527082E-01	-3.72909725E+00
	-6.81618420E-02	-7.20357223E-01
	1.37123926E-01	8.19891655E-01
	-3.31043875E-02	1.89194079E-01
	3.82133007E-01	-5.55055817E+00
	8.94793303E-02	1.06823524E+00
	-1.12393872E+00	-2.62309029E+01
	4.14524264E-02	4.46126669E+00
	9.79290972E-03	1.66462476E+00
	-1.97382413E-01	-2.43849375E+00
	5.08066735E-01	-1.51734524E+01
MODE DISP - TARGET	1.25016579E-01	1.06025829E+00
	5.56075022E-02	2.38658132E-02
	3.39648586E-02	-1.11416716E-01
	9.85978327E-02	-2.94527082E-01
	1.64411383E-02	-6.81618420E-02
	-1.76372356E-02	1.37123926E-01
	-2.45617058E-03	-3.31043875E-02
	7.29899271E-02	3.82133007E-01
	-5.99018196E-03	8.94793303E-02

SIMULATION TIME * 2.0000E+00

	Y(I)	YDOT(I)
U - TARGET	-2.92500222E+00	-4.33237595E+00
	-6.21314193E-02	8.32196263E-02
	4.88168815E-03	1.76284667E+00
	1.62787922E-02	-1.11940089E-02
	-4.39953601E-02	-6.28986819E-01
	-1.84191350E-02	2.25111596E-02
X - TARGET	-1.83395271E+00	-2.92504233E+00
	-1.19475142E-01	-6.01361284E-02
	5.25535528E-01	-5.75612441E-03
GAMMA TARGET	9.99993202E-01	-5.53155289E-06
	-6.83185793E-04	-3.22392058E-04
	3.62349628E-03	1.46578365E-03
	6.80913035E-04	3.20442742E-04
	9.99999571E-01	-3.97471657E-07
	6.28424448E-04	2.85281463E-04
U - CHASE	4.99497071E+00	-1.05079835E+01
	2.10683254E-01	-3.60982604E-01
	-1.40371155E+00	8.11409280E+00
	-8.57522487E-02	-3.99648551E-01
	-4.11412849E-01	-9.12065775E+00
	-4.99507286E-01	-2.91502002E+00
X - CHASE	5.68619289E+02	-5.11133096E+00
	8.94968806E+00	1.85372586E-01
	4.67962378E+01	8.96916267E-01
GAMMA CHASE	-9.94968176E-01	7.60701381E-04
	-4.73674784E-03	-8.70951159E-03
	-1.80079427E-01	-7.15050959E-03
	-4.83047918E-03	-8.82395718E-03
	9.99988092E-01	-4.30525708E-05
	6.94264842E-04	6.16647538E-04
RHOS	8.28638651E+00	-2.05405689E+00
	-7.58542247E-01	1.03977408E+00
	-1.56254770E-01	1.11011733E+00
	4.10404460E+01	8.02809176E-01
	4.20344247E+01	3.40905873E+00
	4.20344247E+01	3.40905873E+00
MODE VEL - TARGET	-4.43161843E-01	4.09308404E+01
	-9.12136389E-01	9.48114313E+00
	2.34052872E-01	1.10555415E+01
	7.67400712E-01	-2.40921923E+01
	2.92187539E-01	-7.94078383E+00
	5.19550647E-01	1.01759708E+01
	-5.98328746E-01	-5.24617638E+00
	1.66697353E+00	2.02652587E+00
	7.73582901E-01	1.15723822E+01
	-1.72509866E+00	-1.60914665E+02
	-2.95066004E+00	6.81719773E+01
	-9.69809800E-01	2.54266010E+01
	4.84002381E-01	9.89043244E+00
	1.31710399E-01	-7.32339196E+01
MODE DISP - TARGET	-2.80359424E+00	-4.43161843E-01
	-4.65378222E-01	-9.12136389E-01
	-4.02792647E-01	2.34052872E-01
	4.93559802E-01	7.67400712E-01
	1.69878518E-01	2.92187539E-01
	-2.08999272E-01	5.19550647E-01
	7.33686795E-02	-5.98328746E-01
	4.77347900E-02	1.66697353E+00
	-5.60180494E-02	7.73582901E-01

SIMULATION TIME = 3.0000E+00

	Y (I)	YDOT (I)
U - TARGET	-3.62879327E+00 -1.75869214E-01 -3.49752468E-02 4.68304968E-02 -9.29079562E-02 -5.82215661E-02	2.70251822E-02 9.16717120E-02 -3.78989240E-01 -1.63764919E-02 1.08454253E-01 1.82182053E-02
X - TARGET	-5.32837713E+00 -2.44423989E-01 4.85512855E-01	-3.62879586E+00 -1.70883862E-01 -5.41588080E-02
GAMMA TARGET	9.99985412E-01 -1.36196067E-03 5.22699523E-03 1.35554715E-03 9.9998324E-01 1.23034784E-03	-9.73769205E-06 -9.30873558E-04 1.62038350E-03 9.24604383E-04 -2.26492818E-06 8.22189888E-04
U - CHASE	2.73072373E+00 6.30877772E-01 -1.33118432E+00 -6.70345066E-02 -1.48337410E-01 -1.07332872E-01	-4.53267738E-02 -1.98772924E-01 -1.45516564E+00 5.30127509E-02 1.93569898E+00 9.87835153E-03
X - CHASE	5.65268238E+02 9.37671927E+00 4.77835806E+01	-2.86147718E+00 5.99604441E-01 1.03890974E+00
GAMMA CHASE	-9.94453689E-01 -1.82263966E-02 -1.04677795E-01 -1.04307166E-02 9.99944612E-01 1.40463039E-03	2.90496188E-04 -1.86676589E-03 -2.57738160E-03 -1.98537578E-03 -2.28691216E-05 9.67519340E-04
RHOS	8.37668599E+00 1.88430323E-01 -2.67195898E-02 4.17529626E+01 4.17492037E+01 4.17492037E+01	1.03794276E+00 7.02326801E-01 -1.68203285E+00 -1.75578215E+00 -1.75572786E+00 -1.75572786E+00
MODE VEL - TARGET	-8.48283480E+00 -1.73386068E+00 2.54073656E-01 -1.79007689E+00 -8.60054031E-01 1.69674172E+00 -2.67295387E-01 -2.95725881E+00 1.48549871E+00 2.78579583E+00 1.43460451E+00 6.30986045E-01 -3.73477736E-01 5.09282102E-01	-2.38460302E+01 4.47581672E+00 9.89725666E+00 -1.86999728E+01 -6.61594444E+00 2.12469889E+00 1.26195189E+01 -8.58976865E+00 -5.03248224E+00 -7.44586274E+01 1.38894067E+01 4.20387732E+00 3.28533826E+00 -5.32548574E+01
MODE DISP - TARGET	1.12492445E+00 -1.58933329E-01 -2.73954888E-01 4.79335487E-01 1.57722253E-01 -6.09398816E-02 -1.65634717E-01 1.83154881E-01 2.42287191E-02	-8.48283480E+00 -1.73386068E+00 2.54073656E-01 -1.79007689E+00 -8.60054031E-01 1.69674172E+00 -2.67295387E-01 -2.95725881E+00 1.48549871E+00 -7.44586274E+01 1.38894067E+01 4.20387732E+00 3.28533826E+00 -5.32548574E+01

SIMULATION TIME = 4.0000E+00

	Y(I)	YDOT(I)
U - TARGET	-3.63913070E+00	-1.59850724E-02
	-1.19115700E-01	1.48101404E-01
	-4.23676731E-02	1.93284810E-02
	3.08857880E-02	-4.01679320E-02
	-8.92711047E-02	-3.89352592E-03
	-3.45333487E-02	4.71212358E-02
X - TARGET	-4.95941947E+00	-3.63499696E+00
	-3.75745536E-01	-1.11490042E-01
	4.19867796E-01	-6.72743896E-02
GAMMA TARGET	9.99974787E-01	-1.18302356E-05
	-2.07605079E-03	-6.85604303E-04
	6.79079997E-03	1.55691113E-03
	2.06342020E-03	5.99842596E-04
	9.99996129E-01	-2.24981479E-06
	1.86643464E-03	5.43136883E-04
U - CHASE	2.69960005E+00	-5.07114744E-02
	4.23450183E-01	-5.45114168E-01
	-1.38343445E+00	5.02415244E-02
	-7.53520338E-02	-2.71163593E-02
	-1.26881752E-01	-1.86776523E-01
	-4.84383186E-01	-7.89263142E-01
X - CHASE	5.62415196E+02	-2.83816931E+00
	9.82762236E+00	3.76362724E-01
	4.88656633E+01	1.88820687E+00
GAMMA CHASE	-9.94164229E-01	3.47870608E-04
	-1.54914376E-02	-7.04856351E-03
	-1.86759076E-01	-2.21665587E-03
	-1.58057664E-02	-7.15697436E-03
	9.99872878E-01	-1.14299010E-04
	2.09873806E-03	5.54149785E-04
RHOS	9.29282526E+00	7.80345663E-01
	-1.15015688E-02	1.12586096E+00
	-1.16949325E-01	1.15759078E+00
	4.81234558E+01	-1.45667304E+00
	4.81137275E+01	-1.45666210E+00
	4.01197275E+01	-1.45666210E+00
MODE VEL - TARGET	6.38142317E+00	-3.86627826E+01
	-2.54148473E+00	-6.75041474E+00
	-5.43676645E-01	8.69022484E+00
	1.85215515E-01	-1.34458243E+01
	-2.46999759E-01	-3.50663153E+00
	6.98697636E-01	-3.79254521E+00
	1.44267788E+00	-1.16787748E+01
	1.63113727E+00	2.89245574E+01
	3.46404368E-01	-1.46421920E+01
	3.14909536E+00	-2.95373693E+00
	2.01430591E-01	1.20114253E+01
	1.53188756E-01	1.60560681E+00
	2.43184264E-01	1.82561961E+00
	8.18344627E-01	-9.85685043E-01
MODE DISP - TARGET	1.49588748E+00	6.38192317E+00
	1.97834414E-01	-2.54148473E+00
	-2.49922856E-01	-5.43676645E-01
	3.71343186E-01	1.85215515E-01
	9.62664448E-02	-2.46999759E-01
	6.34740962E-02	6.98697636E-01
	1.60509754E-01	1.44267788E+00
	-2.88411338E-01	1.63113727E+00
	8.32348117E-02	3.46404368E-01

SIMULATION TIME = 9.0000E+00

	Y(I)	YDOT(I)
U - TARGET	-3.61778613E+00	1.22062597E-02
	-1.48646556E-01	-4.42768697E-02
	-4.05588690E-02	-8.63708772E-05
	3.81064695E-02	1.18883335E-02
	-8.77866404E-02	1.79324042E-03
	-4.29508000E-02	-1.29544181E-02
X - TARGET	-1.25901880E+01	-3.61771304E+00
	-5.02332046E-01	-1.38544389E-01
	3.59314570E-01	-7.12397133E-02
GAMMA TARGET	9.99961074E-01	-1.49053278E-05
	-2.76451757E-03	-7.53394641E-04
	8.37902250E-03	1.53024710E-03
	2.74381182E-03	7.44026423E-04
	9.99993156E-01	-3.70750892E-06
	2.48162950E-03	6.71339155E-04
U - CHASE	2.75428341E+00	3.51061527E-02
	5.43896005E-01	1.71208112E-01
	-1.41126653E+00	-2.87300756E-02
	-7.08268001E-02	7.09483171E-03
	-7.96960278E-02	6.48559926E-02
	-2.54976510E-01	2.24187312E-01
X - CHASE	5.59561134E+02	-2.90313383E+00
	1.02607277E+01	4.78051063E-01
	4.99286076E+01	1.10311121E+00
GAMMA CHASE	-9.93776021E-01	2.48417986E-04
	-2.12363496E-02	-4.44199743E-03
	-1.09353722E-01	-1.39492305E-03
	-2.16686897E-02	-4.55755578E-03
	9.99761378E-01	-1.80833440E-04
	2.76663758E-03	7.42099813E-04
RHOS	1.02862428E+01	7.54185667E-01
	3.58392749E-03	1.83300166E-01
	3.37410718E-02	-2.86908528E-01
	3.81659166E+01	-1.56117499E+00
	3.81659166E+01	-1.56117499E+00
	3.81659166E+01	-1.56117499E+00
MODE VEL - TARGET	4.92428797E+00	3.26271309E+01
	-1.01583405E+00	-1.20396352E+01
	-5.81462339E-01	9.44762534E+00
	-4.82587239E-01	-1.72688116E+01
	-5.63955707E-01	-4.83357421E+00
	4.22686815E-01	-3.95456432E+00
	-2.01302575E+00	5.82221007E-01
	4.43095861E-01	-2.19992791E+01
	-4.95937024E-01	-1.13423527E+01
	1.73644194E+00	3.86531306E+01
	5.92813919E-01	-4.29851166E+00
	1.72191023E-01	-4.77085901E+00
	-1.67267885E-01	-2.0557083E+00
	1.17750559E-01	1.05622357E+01
MODE DISP - TARGET	-1.63518153E+00	4.92428797E+00
	4.10038619E-01	-1.01583405E+00
	-2.32558864E-01	-5.81462339E-01
	4.03574258E-01	-4.82587239E-01
	4.80814874E-02	-5.63955707E-01
	8.58597789E-02	4.22686815E-01
	-4.13328757E-03	-2.01302575E+00
	2.91179860E-01	4.43095861E-01
	6.19632979E-02	-4.95937024E-01

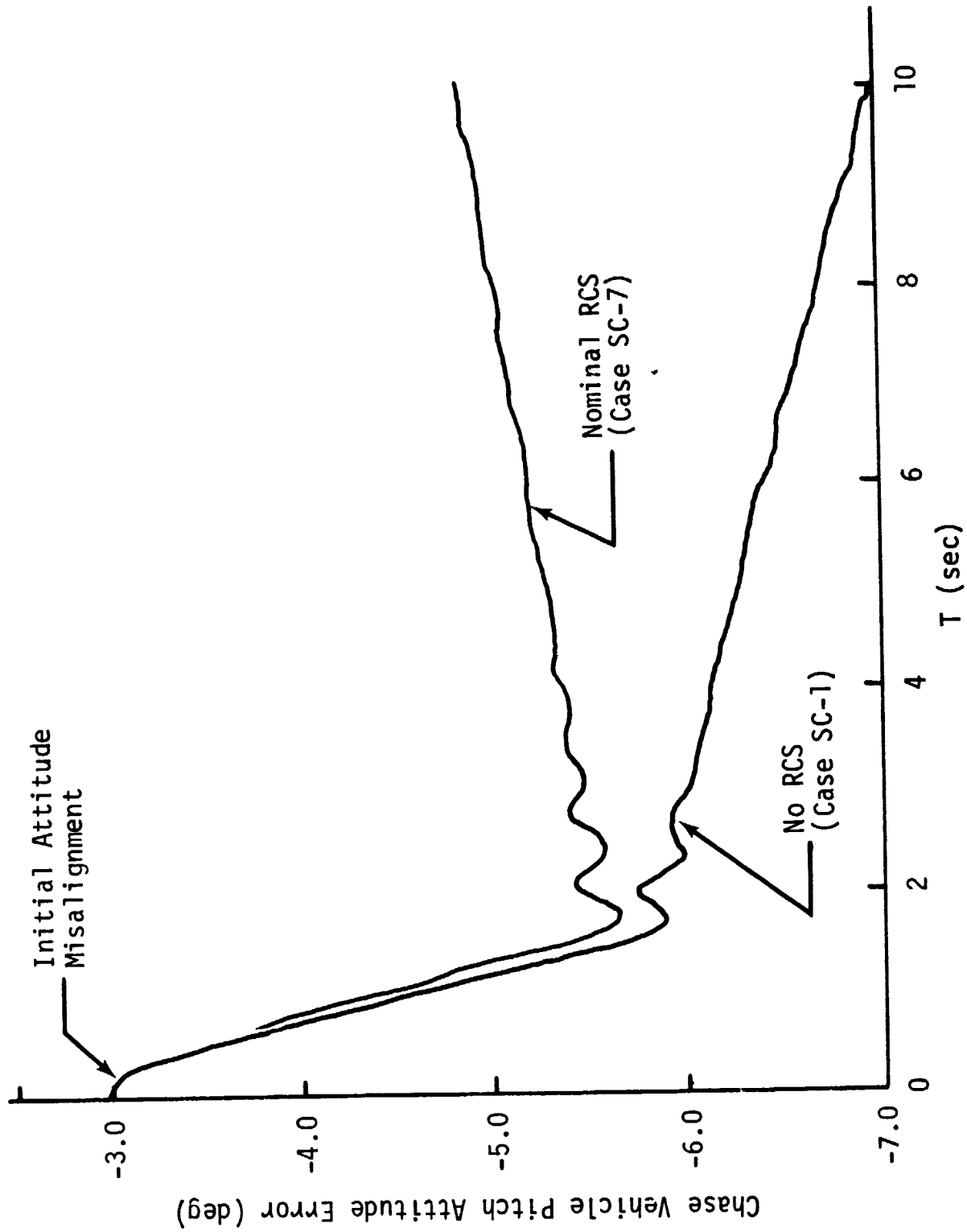


Fig. II-17 RCS Effectivity

III. DIGITAL COMPUTER PROGRAM

The digital computer program for the docking simulation of two elastic vehicles (PROGRAM DOCKEL) was developed to provide numerical evaluation of the analytical formulation presented in Volume I. It was used to generate the results presented in this volume. A summary description of this program is presented in the following sections.

A. APPLICABILITY AND LIMITATIONS

Although the program has been verified through an extensive analysis of a typical Apollo Applications Program (AAP) configuration, it is not restricted to any particular orbital configuration. The program was designed with complete versatility to the user as a primary objective and therefore many options have been included. These options may be exercised at the user's discretion as best benefits his requirements. Also, because of the great complexity of the overall dynamics program, it was necessary to impose several limitations on the program.

The first limitation is strictly a hardware-imposed restraint; the program was developed on, and as such is limited to, the Control Data Corporation 6400/6500 series computers. This is a relatively minor restriction in that modification to any other current digital computer could be made with a minimum of effort. Primarily, the uniqueness lies in the use of the plotting subroutines for the response time histories and the optional perspective/stereo pairs plots.

A far more severe restriction is the assumption of a known and relatively invariant description of the probe and drogue docking mechanism. Although consistent variations in geometry and stiffness or damping characteristics are permitted, no deviation from either the overall geometrical configuration or the basic kinematical relationships of the probe-drogue are permissible. However, the general description of both the target and chase vehicles are quite arbitrary. Input parameters describing the location of the drogue cone on the target vehicle and the probe on the chase vehicle are arbitrary as are the inertial characteristics of both vehicles.

Several of the user selected input options are itemized:

- 1) The location of the drogue cone apex (D) with respect to the target vehicle center of mass (T) is defined with an input vector;
- 2) The location of the probe hard-point (P) with respect to the chase vehicle center of mass (C) is defined with an input vector;
- 3) The orientation of the probe pitch arms with respect to the drogue at the initiation of the simulation are defined with an input vector;
- 4) The target vehicle total mass and inertial properties about the center of mass are defined with an input scalar and input matrix, respectively;
- 5) The chase vehicle total mass and inertial properties about the center of mass are defined with an input scalar and input matrix, respectively;
- 6) Stiffness and damping characteristics of the probe barrel and the three pitch arms are defined by input matrices;
- 7) Modal characteristics for the target and chase vehicles are defined by an input vector of structural frequencies and input matrix of normal modes. Additional input data required here are three integer vectors that select the desired frequencies and modes from the complete arrays;
- 8) Control system parameters are defined at the user's option. As many as three control systems can be included. Chase vehicle axial thrust can be varied through the input data.

B. OVERLAY STRUCTURE AND LOGIC FLOW

The requirement for a large amount of core storage locations, especially to store the time history data for plot output, dictated the necessity to use an overlay structure in the formulation of the program. The program comprises four overlays (Fig. III-1).

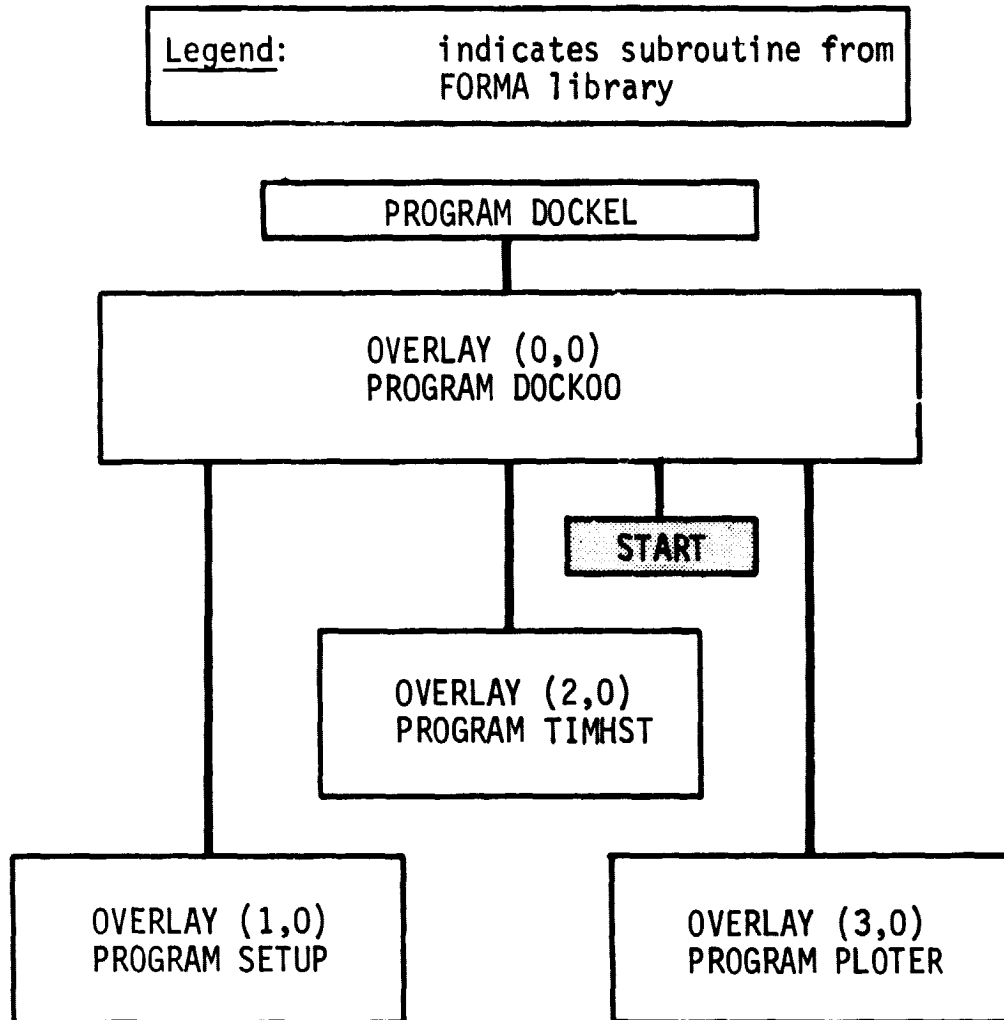


Fig. III-1 PROGRAM DOCKEL Overlay Structure

1. OVERLAY (0,0) PROGRAM DOCKOO

This overlay (Fig. III-2) is the control overlay for the entire program. Its basic function is to allocate sufficient storage locations for program variables through definition of several COMMON blocks. These COMMON blocks are then available to the other three overlays which are called, in turn, by this overlay.

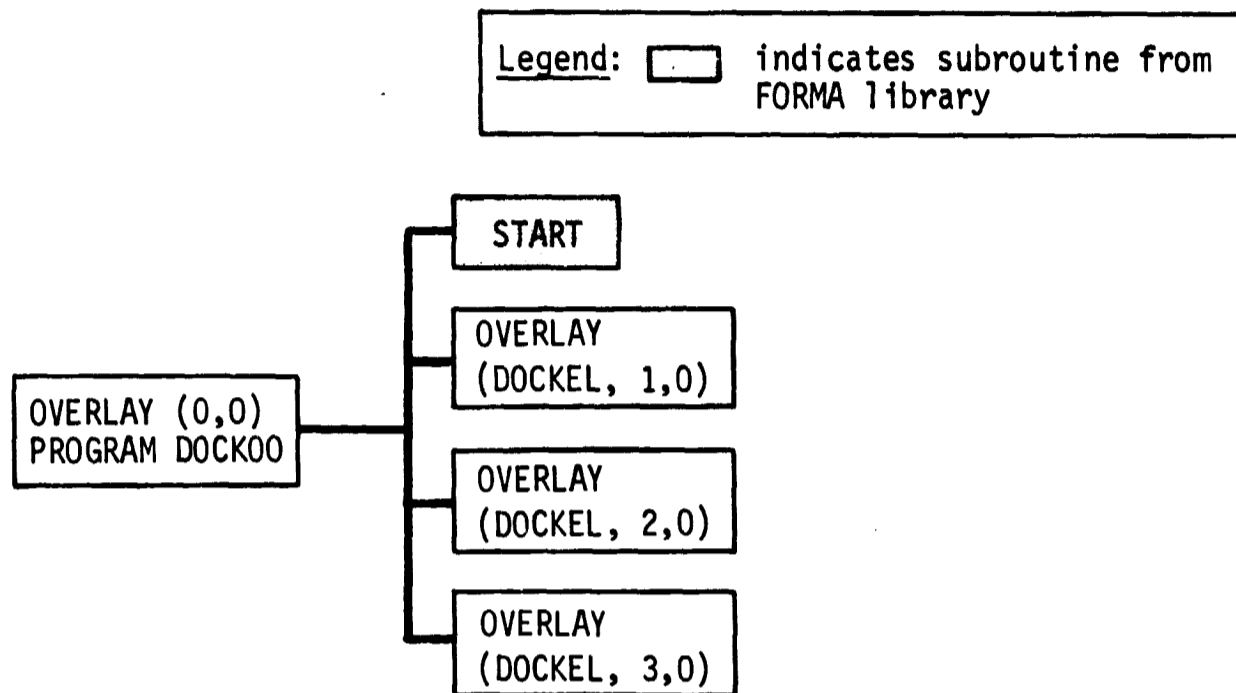


Fig. III-2 PROGRAM DOCKOO Calling Structure

DOCKOO also initializes several program variables with DATA statements, initializes systems plotting subroutines, calls a FORMA subroutine to read a program run number and two title cards, and increments a batch indicator that allows the operator to run several jobs under the same run without the necessity of rereading an entire new set of input data. The overlay (Fig. III-3) then calls the overlay whose function is to read input data and compute program variables (SETUP), the overlay that computes the docking simulation time history (TIMHST), and, if so indicated by the plot option indicator, the overlay that plots docking program variable time histories (PLOTTER). Control then returns to the beginning of the overlay and, if data are available, begins another simulation run. If no more data are available, the run is terminated.

2. OVERLAY (1,0) PROGRAM SETUP

The main function of this overlay (Fig. III-4) is to read a majority of required program input data, compute several variables that will be required in the time history evaluation, read and write the title cards on tape for the plot overlay and set integration constants for use in the time history integration subroutine. The subroutine also prints input data. The logic flow for the program is shown in Fig. III-5.

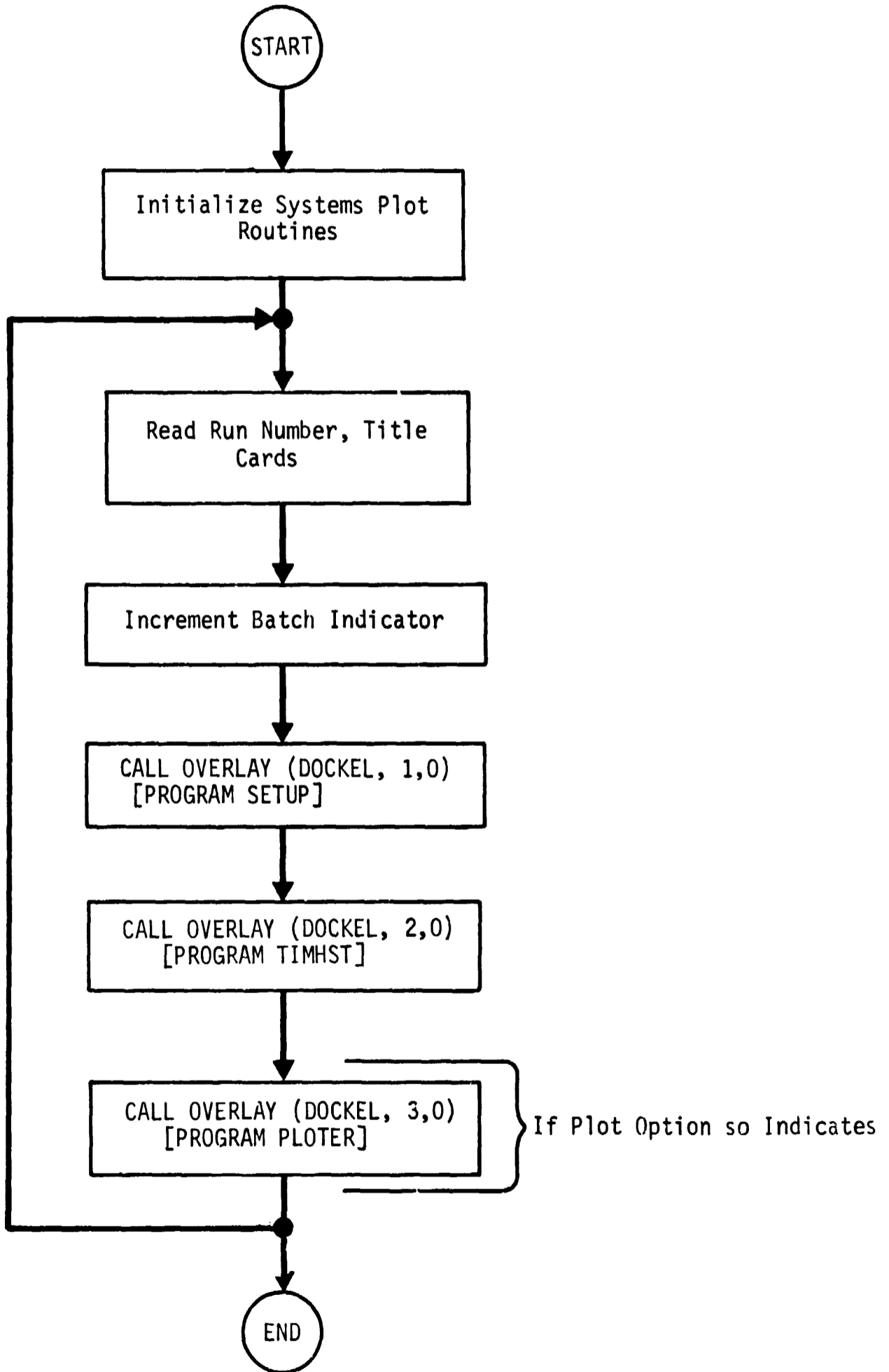


Fig. III-3 PROGRAM DOCK00 Logic Flow

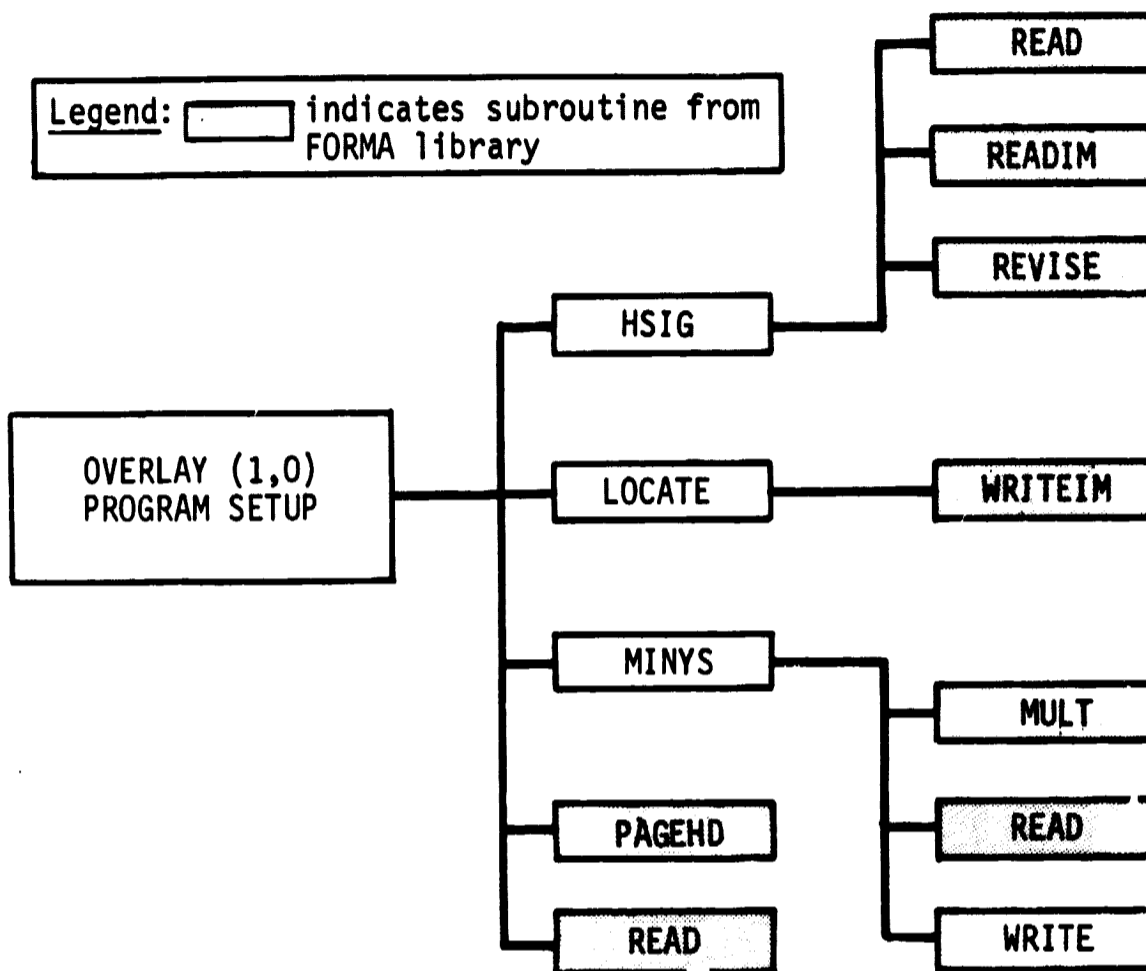


Fig. III-4. PROGRAM SETUP Calling Structure

3. OVERLAY (2,0) PROGRAM TIMHST

PROGRAM TIMHST, as the name indicates, is the overlay that computes the docking simulation time history. The program calling structure is indicated in Fig. III-6. The overlay begins by computing and printing the state vector and all other pertinent variables for the initial time. It then proceeds through the time history integration, using the Runge-Kutta numerical technique, until time reaches the specified final time. The time history variables are written on a tape so as to be available for plotting. The output may be printed at each integration interval if desired. This logic is indicated in Fig. III-7.

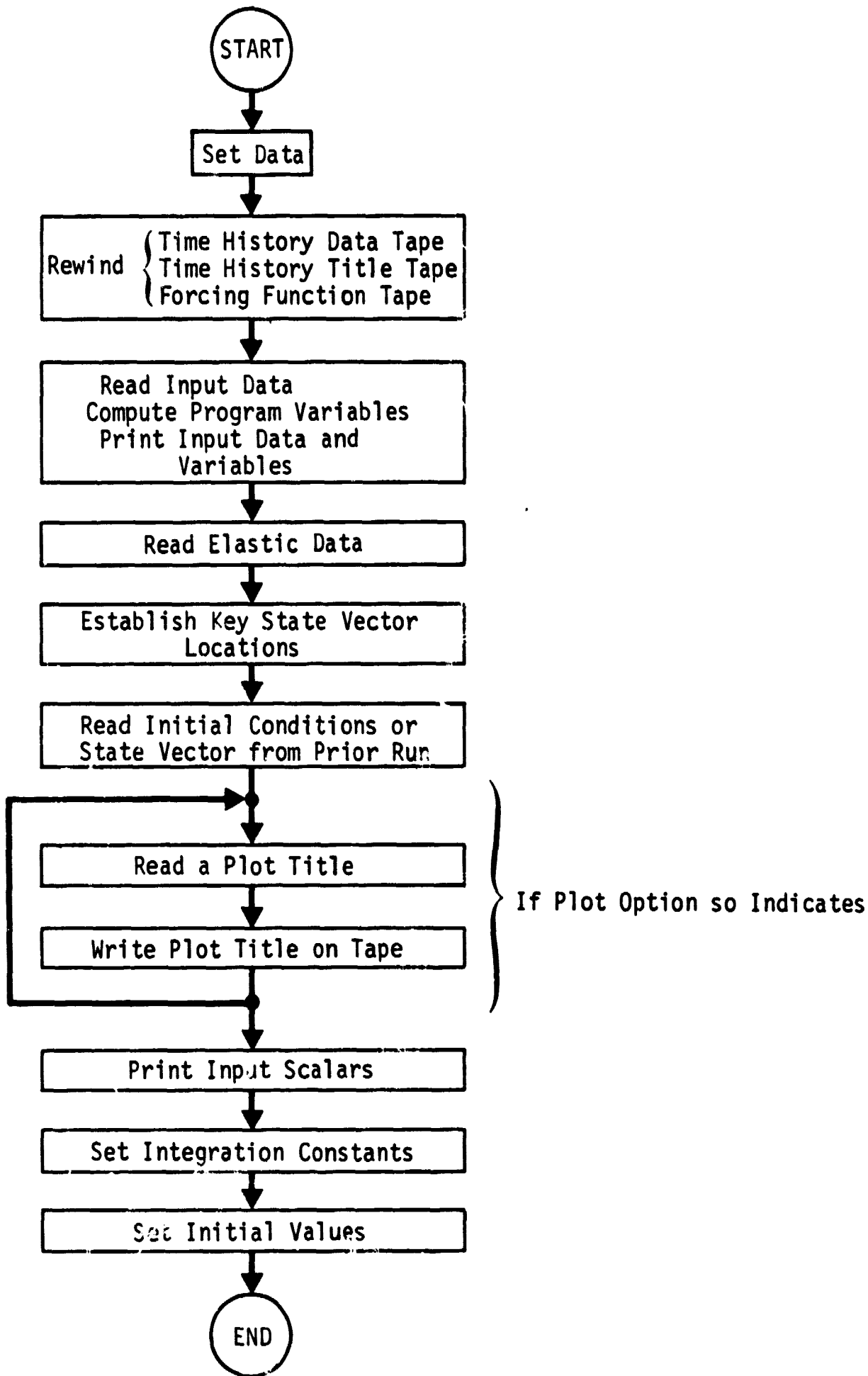


Fig. III-5 PROGRAM SETUP Logic Flow

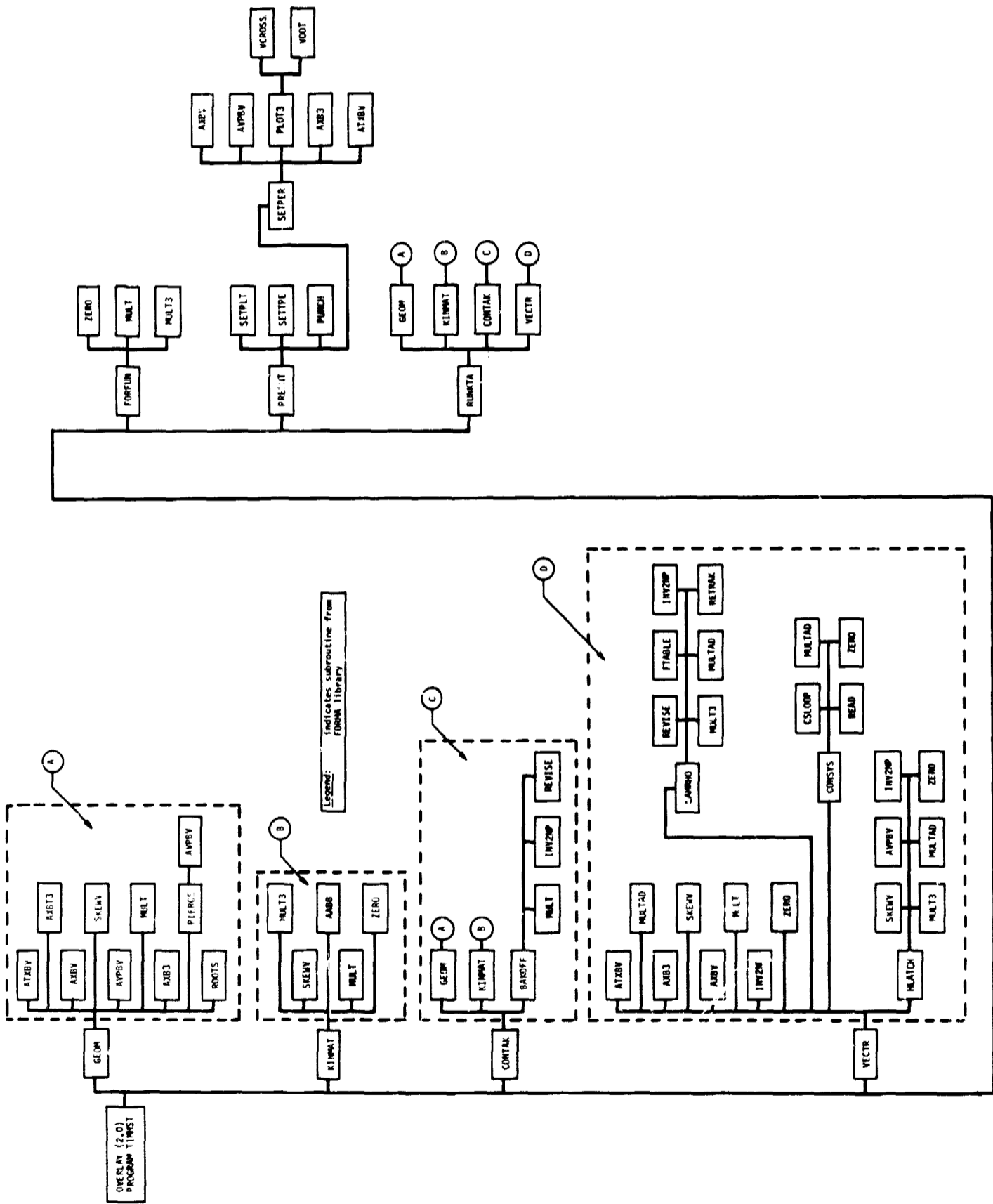


Fig. III-6 PROGRAM TIMHST Calling Structure