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# POSSIBLE GEOPOTENTIAL IMPROVEMENT FROM SATELLITE ALTIMETRY

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#### NUMERICAL DEFINITION OF LOCALIZED FUNCTIONS ON A SPHERE

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### TABLE OF CONTENTS

	Page
ABSTRACT	v
POSSIBLE GEOPOTENTIAL IMPROVEMENT FROM SATELLITE ALTIMETRY by C. A. Lundquist and G. E. O. Giacaglia	1
1 INITIAL ASSUMPTIONS	3
2 TRACKING DATA	6
3 GEOPOTENTIAL DETAIL	8
4 FUNCTIONS OF ONE VARIABLE	12
5 FUNCTIONS ON A SPHERE	17
6 THE FUNCTIONS $W_{kj}$ ( $\theta$ , $\lambda$ )	20
7 EXAMPLES OF $W_{k_1}(\theta, \lambda)$	26
8 FUNCTIONS IN THREE DIMENSIONS	28
9 COEFFICIENTS OF $\mathscr{J}_1$ IN THE GEOPOTENTIAL	33
10 ACKNOWLEDGMENTS	41
REFERENCES	42
NUMERICAL DEFINITION OF LOCALIZED FUNCTIONS ON A SPHET by K. Hebb and S. G. Mair	RE 45
1 INTRODUCTION	47
2 METHOD	48
3 CHECKS	51
4 OUTPUT	53

#### ABSTRACT

To improve the geopotential representation, the use of satellite-toocean altitudes anticipates that the altimeter will be accurate to a few meters and that the open ocean approximates an equipotential surface to a few meters. Computational problems that might arise in the analyses could be largely circumvented by using a different, but equivalent, set of functions to represent the geopotential instead of using spherical harmonics. At any point on the geoid, only a very few of these alternative functions have significant values; the rest are negligible.

## RÉSUMÉ

Pour avoir une meilleure représentation du géopotentiel, l'emploi des altitudes entre les satellites et l'océan escompte que l'altimètre sera précis à quelques mètres près et qu'au grand large un océan est proche d'une surface équipotentielle à quelques mètres près. Pour représenter le géopotentiel, il est possible de circonvenir en grande partie les problèmes de calcul qui pourraient se présenter lors des analyses en employant à la place des harmoniques sphériques une série de fonctions qui soit différente mais équivalente. Quelque soit le point sur le géoïde, il n'y a que très peu de ces fonctions alternatives qui aient une valeur appréciable; les autres sont négligeables.

#### РЕЗЮМЕ

С целью улучшения формы представления потенциала земли, использование высот спутников над океаном предполагает, что (а) высота эта измеряется с точностью несмольких метров и (б) что поверхность открытого океана можно приблизительно принять за поверхность равного потенциала, также с точностью нескольких метров. Иссчислительные проблемы, которые могут возникнуть при анализе, можно избежать в значительной мере, замещая сферические функции, другими, да все-таки тождественными, представляющим VOтенциал земли. Для любой точки на геоде только несколько из этих других, замещающих функций, имеет важное значение, всеми остальными же можно пренебречь.

V

# POSSIBLE GEOPOTENTIAL IMPROVEMENT FROM SATELLITE ALTIMETRY

C. A. Lundquist and G. E. O. Giacaglia

## POSSIBLE GEOPOTENTIAL IMPROVEMENT FROM SATELLITE ALTIMETRY

C. A. Lundquist and G. E. O. Giacaglia\*

#### 1. INITIAL ASSUMPTIONS

A promising objective for an altimeter on a satellite is the collection of information about the geopotential. This is surely not the only objective, nor was it the motivation for early studies and experiments. For a brief history of spacecraft altimetry, see Lundquist (1967a). The possibility that satellite-to-ocean altimeters offer for improving the geopotential is the only subject discussed here, but this limitation by no means detracts from the importance of other objectives.

The present discussion will not be concerned with the altimeter hardware that might be selected for satellite use. An earlier study concluded that the data from any of the several possible systems could be used in essentially the same way with only minor differences in data-processing details (Lundquist, 1967a). Equipment options are under study by other groups (e.g., Raytheon, 1968a, b, c). An accuracy no poorer than a few meters is assumed, however.

Use of satellite-to-ocean altitudes for improving the geopotential accepts the concept that the open ocean is an equipotential surface to an accuracy of a few meters. A recent study at New York University (Greenwood, Nathan, Neumann, Pierson, Jackson, and Pease, 1967) reviews departure of mean sea level from an equipotential surface due to various geophysical phenomena. In fine detail, at decimeter precision, the sea level depends upon many factors that are of great interest to oceanography. Thus, a reliable description of sea level corresponding to an equipotential surface is a necessary step on the way toward more detailed applications of altimetry to oceanography problems.

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Among these oceanographic topics, waves deserve specific discussion. Clearly, the signal returned from the ocean must be processed by the altimeter in such a way as to average over the wave structure beneath the satellite. Since ocean waves seldom exceed a few tens of meters amplitude, an averaging accuracy of 10% is all that is required for the geopotential application. This may not be a completely solved problem to date, but it seems likely to be solved. If uncertainty remains at the time an altimeter is flown on a satellite, an appropriate in-flight calibration program can certainly be established. Laser tracking from a ground station probably can provide the standard for calibration when the station is near an ocean. Hereafter, the assumption is adopted that the altimeter provides altitudes properly corrected for the ocean waves, that is, for sea state, to an accuracy of a meter or so.

Other corrections must be made because an equipotential surface calculated from the expression in spherical harmonics applicable at satellite altitudes will not be correct at sea level, owing to the gaseous and solid mass above the geoid. Veis (1967) has discussed the atmospheric correction, which has a relative magnitude of  $10^{-6}$ . Madden (1968) has examined the mathematical questions concerned with the fact that the sea level lies within the smallest sphere containing the solid mass of the earth. He has shown that the correction that must be applied to correct the calculated equipotential is no larger than a few meters (Madden, 1968). His work also yields the formulas to make this correction. Hereafter, it will be assumed that these corrections are applied if necessary.

In summary, the discussions to follow assume that satellite-to-ocean altitudes can be measured to the accuracy with which the ocean is an equipotential surface. Quantitatively, this anticipates that the altimeter will be accurate to a few meters and that the open ocean is an equipotential surface to a few meters. The former seems to be possible in the judgment of design engineers, and the latter represents the best estimate of oceanographers.

The great value of satellite-to-ocean altitudes for improving a description of the geopotential resides in the fact that sea level is much more sensitive to fine detail in the potential than is the satellite motion governed by the potential. Stated another way, knowledge of a satellite orbit to 1 m tells much less about details in the potential than does knowledge of sea level to 1-m accuracy. Nevertheless, it seems likely that the altimeter data must be used concurrently to refine both the orbit and the potential.

#### 2. TRACKING DATA

The conclusion was reached in previous publications that satellite-toocean altitudes can be treated in the same manner as other satellite-tracking data (Lundquist, 1967a, b). The arguments supporting this conclusion will not be repeated here. The referenced publications give the general expressions by which altitude observations yield equations for improving both the orbit of the satellite and the geopotential representation. The equations are identical in form to the equations employed, for example, to utilize stationto-satellite range measurements.

Altitude observations will not alone be sufficient to determine an accurate orbit for the satellite carrying the altimeter. The semimajor axis, eccentricity, and position of perigee should be well determined from the altimetry. The orbit inclination and the position of the node will depend strongly upon tracking from fixed ground stations.

Laser tracking from ground stations is likely to yield the most useful data to blend with altitudes in orbit determination and geopotential improvement. Laser ranging is particularly compatible with altimetry because both are distance measurements and because laser systems can easily measure distances to meter accuracies or better (e.g., Plotkin, 1968; Bender, 1967; Lehr, Maestre, and Anderson, 1967). Other ground tracking data will be valuable in proportion to their ability to contribute to orbits approaching accuracies of a few meters.

The geodetic heights of tracking stations determined from conventional geodetic leveling referenced to sea level gauges can provide a valuable confirmation or calibration for the altimeter. For stations near the coast, this cross check can be accomplished through a simple calculation using the geodetic height, accurate geocentric station coordinates, and simultaneously

measured satellite-to-ocean altitudes and station-to-satellite ranges. Perhaps large lakes near tracking stations could provide a similar check. The probability that the satellite pass over the lake would be greatly increased if the latitude of the lake were the same as the inclination of the satellite.

#### 3. GEOPOTENTIAL DETAIL

A crucial question is the detail in the geopotential representation that may be expected from analyses of satellite-to-ocean altitudes of the accuracies anticipated. As an initial approach to this problem, present knowledge of the sea profile can be examined.

Geoid surfaces calculated from previous satellite-determined geopotentials give one indication of the expected profile. The geopotential contained in the 1966 Smithsonian Institution Standard Earth is a typical example (Gaposchkin, 1966a). This is a geopotential representation in spherical harmonics through indices 8, 8, with assorted higher degree terms. It reveals large-scale variations up to more than 100 m in the geoid position relative to a reference ellipsoid. Clearly, an altimeter accurate to a few meters should easily detect and confirm these large-scale features of sea level.

Something is also known about rather small-scale variations in sea level. For example, a shipboard measurement by von Arx (1966) has shown that in  $\sim 1^{\circ}$  of latitude over the Puerto Rico trench, the geoid has about a 15-m depression relative to an ellipsoid. A feature of this size would also be detected by an altimeter having an accuracy of a few meters. Although the Puerto Rico trench is unusual, it is surely not unique in the oceans. The signature in the geopotential of many such features would be obtained by a satellite that observed each square degree of the ocean.

This last remark has awesome consequences, for there are some 40,000 one-degree squares on the surface of a sphere and perhaps 25,000 of these would lie over the open ocean. To represent a geopotential that is allowed to have an arbitrary value for each one-degree square, an expansion with

some 40,000 terms and coefficients is required. From a slightly different point of view, an expansion in spherical harmonics through indices 180,180 is appropriate to represent variations having wavelengths of one degree. Thus it seems that to represent the detail that could be detected by an altimeter, a very extensive geopotential model is implied.

Stated in a more affirmative manner, satellite-to-ocean altimetry offers the possibility of a vast improvement in the knowledge of the geopotential. Perhaps the realization of this possibility should be discussed (or even executed) in more modest steps than the jump from an 8,8 to a 180,180 representation.

As a first step, the possible altimeter contribution to a spherical harmonic expansion through 15, 15 can be examined. This is the detail specified as an objective in the present United States National Satellite Geodesy Program (Rosenberg, 1965). Several authors have noted that even through this number of harmonics there may be coefficients that are difficult to determine only by their effects on the orbits of typical satellites (Strange and Rainey, 1968).

An expansion through 15,15 has a shortest wavelength of 12 degrees and 256 harmonic coefficients. To this detail, for altitude observations, there should be no difficulty in using exactly the same procedures and computer programs conventionally employed to determine geopotential coefficients from satellite-tracking data. The pertinent equations have been discussed (Lundquist, 1967b). Over the oceans, furthermore, the altitude measurements should easily supply the observational material necessary for a sound solution, thus alleviating the mentioned deficiencies in a solution based only on ground-station tracking.

Over land areas, there may still be a deficiency in information necessary for a full 15, 15 solution since the altitude data are of no help here. However, surface gravity measurements and astrogeodetic geoids may be available in enough detail to complete the requirements for the desired

solution. Procedures for using surface gravity information in combination with satellite geopotential solutions have been demonstrated (e.g., Köhnlein, 1967). The published combinations of this kind all suffer from poor distribution of gravity data. The oceans are covered particularly sparsely, but this is just where altimetry will fill the gap.

In summary, it is quite reasonable to expect that a modest number of well-distributed satellite-to-ocean altitudes, combined with ground-station tracking, surface gravity, and astrogeodetic geoids, will provide for a strong 15,15 geopotential solution. This may well be a convenient way to complete such a solution, although the use of enough satellites in resonance with various terms in the potential might eventually complete the task (Strange and Rainey, 1968).

The next step to consider in geopotential detail is probably a solution through 36, 36, corresponding to variations down to 5-degree wavelength. This degree of detail is suggested because it is common to average surface gravity over 5-degree squares, and a combination of commensurate surface and altimetry data could be made. This enterprise would pose some problems not encountered seriously in the 15,15 case.

The first problem arises from the number of coefficients in an expansion terminated at 36,36; there are  $37^2 = 1369$  of these coefficients. This says that the potential at any point is calculated by summing these many terms in a series. Also, the approach discussed for the 15,15 case, if used in the 36,36 case, would imply the inversion of a  $1369 \times 1369$  matrix to solve for the coefficients. These operations are possible on modern computers, but avoiding them would be a practical advantage.

The second problem with a 36,36 solution arises because there is little hope that the necessary data can be obtained for this detail in all parts of the globe. Over the oceans, an altimeter could provide enough observations for each  $5^{\circ} \times 5^{\circ}$  area, but many land areas lack correspondingly dense surface measurements. Also, the orbital perturbations caused by potential terms of

this degree are in general too small to be used to find the potential coefficients, although many resonance cases are an exception to this situation.

These problems could be largely circumvented by using a different, but equivalent, set of functions to represent the geopotential, instead of using spherical harmonics. These alternative functions are discussed in some detail in subsequent sections. In brief, there must be the same number of independent functions—that is, 1369 functions for the equivalent of a 36,36 representation. However, at any point on the geoid, only a very few of the functions have significant values; the rest are negligible, and the potential at any point is the sum of only a very few terms. If the coefficients of the alternative functions are adjusted, it is easy to represent geopotential detail where it is known. On the other hand, short-wavelength detail can be conveniently avoided where detailed data are not available. Finally, the alternative functions are a linear combination of the spherical harmonics so that the transformation back and forth between the potential expressed in the equivalent sets of functions can be performed easily with a matrix of constant coefficients.

If a geopotential expansion through 180, 180 is finally considered so as to include such detail as those caused by the Puerto Rico trench, the problems mentioned for the 36,36 representation are further exaggerated. Here, 32,761 terms in a spherical harmonic expansion contribute to the potential at each point, which is clearly an impractical way to specify the potential. Still, over the oceans an altimeter promises to measure this detail. Over land, corresponding data will very probably not be known, except perhaps in highly developed regions, such as the United States or Europe. Again, an alternative set of functions seems to be a way to plan for treatment of altimeter data.

The rest of this paper pursues this thought. No claim is made that this approach is unique. Nor has the utility of the method yet been demonstrated in practice, although typical cases could easily be simulated. The use of altimetry data seems to present no obstacles of principle, but rather to pose problems of numerical procedures. The discussions in the following sections suggest a likely solution to these problems.

#### 4. FUNCTIONS OF ONE VARIABLE

The characteristics of the functions suggested as alternatives to threedimensional spherical harmonics can first be illustrated by more simple functions of one variable (Giacaglia and Lundquist, 1968). Any function represented by a truncated Fourier series can be represented equivalently as a linear combination of these alternative functions of one variable in essentially the same way that alternative functions of three variables would replace the spherical harmonics.

To illustrate this situation, consider a real variable  $0 \le \lambda < 2\pi$  and a set of 2N + 1 functions (1,  $\cos \lambda$ ,  $\sin \lambda$ ,  $\cos 2\lambda$ ,  $\sin 2\lambda$ , ...,  $\cos N\lambda$ , sin N $\lambda$ ). These elementary trigonometric functions span a linear vector space of dimension 2N + 1. Any function in the space can be represented in the form

$$f(\lambda) = \sum_{j=0}^{N} (c_j \cos j\lambda + s_j \sin j\lambda) , \qquad (4.1)$$

where  $c_j$  and  $s_j$  are constants. Conversely, any function representable in this form is in the space. The set (cos  $j\lambda$ , sin  $j\lambda$ ) is a basis in the space.

Another set of functions forming a basis in the same space is desired, with the property that each function  $q_j(\lambda)$  have significant values for arguments near some  $\lambda = \lambda_j$ ,  $0 \le \lambda_j < 2\pi$ , and small values elsewhere in the same interval. For simplicity of language, this will be called the localized property of the function, since each is significant only in one locality in the domain of its argument.

A set of functions with this property can be generated by the requirement that

$$q_k(\lambda_i) = \delta_{ki}$$
,  $k = 0, 1, 2, ..., 2N$  (4.2)

for

$$\lambda_{j} = j \frac{2\pi}{2N+1}$$
,  $j = 0, 1, 2, ..., 2N$ 

Conditions (4.2) are sufficient to determine the coefficients in equation (4.1) for the representation of  $q_i$  as a linear combination of the trigonometric functions.

Imposing conditions (4.2) yields the relations

$$q_{Nj}(\lambda) = \frac{1}{2N+1} \left[ 1 + 2 \sum_{\ell=1}^{N} \cos \ell (\lambda - \lambda_{Nj}) \right] ,$$
  

$$\lambda_{Nj} = j \frac{2\pi}{2N+1} ,$$
  

$$j = 0, 1, 2, ..., 2N ,$$
  

$$0 \le \lambda < 2\pi .$$
(4.3)

The index N is added to keep track of the dimension (2N + 1) of the space in which the  $q_{Nj}$  have been generated. The inverse of (4.3) is

.

With equation (4.4), any function of the form (4.1) can immediately be rewritten as a completely equivalent linear combination of the  $q_{Nj}$ ; thus the first essential property of the  $q_{Nj}$  has been demonstrated. In addition, the functions have many other useful properties.

Evaluation of equation (4.4) for m = 0 yields the fact that

$$\sum_{j=0}^{2N} q_{Nj}(\lambda) = 1 \quad . \tag{4.5}$$

The  $\textbf{q}_{N\,j}^{}(\boldsymbol{\lambda})$  are orthogonal functions; that is,

$$\int_{0}^{2\pi} q_{Ni}(\lambda) q_{Nj}(\lambda) d\lambda = \frac{2\pi}{2N+1} \delta_{ij} \qquad (4.6)$$

Also,

$$\sum_{\ell=0}^{2N} q_{Ni}(\lambda_{N\ell}) q_{Nj}(\lambda_{N\ell}) = \delta_{ij} \quad .$$
(4.7)

From the form of (4.3), it is clear that all the  $q_{Nj}$  have the same shape. They differ only by translations in multiples of  $2\pi/(2N + 1)$  along the  $\lambda$  axis:

$$q_{Nj}(\lambda) = q_{N,0}(\lambda - \lambda_{Nj}) \quad . \tag{4.8}$$

Finally, the localized property of the  $q_{Nj}$  must be demonstrated. For each one of the 2N + 1 values of  $\lambda$  equally spaced between 0 and 2 $\pi$ , condition (4.2) ensures that all but one of the  $q_{Nj}$  are zero. Hence, a particular  $q_{Np}$  has a maximum value 1 at point  $\lambda_{Np}$  and zero at all the other 2N points. Another way to state this is that at each of the 2N + 1 points, only the one function with the same indices contributes to the value of any linear combination of the  $q_{Np}$ .

Further, the function  $q_{Ni}$  remains relatively small near  $\lambda_{Nj}$ ,  $i \neq j$ . This is illustrated for N = 15 in Figure 1. Note that the secondary maxima of  $q_{15,j}$  are substantially lower than the primary maximum. This is another manifestation of the localized property.

Closely related to the localized property is the property that if  $f(\lambda)$  is in the space spanned by the  $q_{N_1}(\lambda)$ , then

$$f(\lambda) = \sum_{j=0}^{2N} f(\lambda_{Nj}) q_{Nj}(\lambda) \qquad (4.9)$$

Equation (4.4) is a special case of this general formula. If  $f(\lambda)$  is not in the space spanned by the  $q_{Nj}(\lambda)$ , then the right side of (4.9) gives the projection of  $f(\lambda)$  on the space.

The relations given in this section and the procedures suggested are, of course, equivalent to numerical Fourier analysis. Thus, nothing essentially new has been accomplished. However, this formulation is useful as a guide to the subsequent treatment of the two- and three-dimensional cases.





#### 5. FUNCTIONS ON A SPHERE

The usual surface harmonics defined on a sphere have the expressions

$$X_{nm}(\theta, \lambda) = P_{nm}(\theta) \cos m\lambda , \quad n = 0, 1, ..., N; m = 0, 1, ..., n ,$$
$$Y_{nm}(\theta, \lambda) = P_{nm}(\theta) \sin m\lambda , \quad n = 1, 2, ..., N; m = 1, 2, ..., n ,$$
(5.1)

where for brevity  $P_{nm}(\theta)$  are associated Legendre functions more properly represented by  $P_{nm}(\cos \theta)$ . If the set of functions is truncated at n = N, there are  $M = (N + 1)^2$  independent functions in the set.

By analogy to the one-dimensional example, it is desired to define another set of M independent functions  $Z_j(\theta, \lambda)$  spanning the same space as the surface harmonics and having localized properties generated by the condition that

$$Z_{j}(\theta_{i},\lambda_{i}) = \delta_{ij}$$
,  $i, j = 1, 2, ..., M$  (5.2)

for M points,  $\theta_i$ ,  $\lambda_i$ , on the sphere. From these requirements follow immediately the relations analogous to (4.4):

$$X_{nm}(\theta, \lambda) = \sum_{j=1}^{M} X_{nm}(\theta_{j}, \lambda_{j}) Z_{j}(\theta, \lambda) ,$$
  
$$Y_{nm}(\theta, \lambda) = \sum_{j=1}^{M} Y_{nm}(\theta_{j}, \lambda_{j}) Z_{j}(\theta, \lambda) .$$
(5.3)

Since the Z<sub>j</sub> span the same space as the  $X_{nm}$ ,  $Y_{nm}$ , the former must also be expressible as linear combinations of the latter. Thus,

$$Z_{j}(\theta, \lambda) = \sum_{n=0}^{N} \sum_{m=0}^{n} \left[ A_{j}^{nm} X_{nm}(\theta, \lambda) + B_{j}^{nm} Y_{nm}(\theta, \lambda) \right] .$$
 (5.4)

The constants  $A_j^{nm}$  and  $B_j^{nm}$  can be determined either from conditions (5.2) and equation (5.4) or from inverting equation (5.3). The two operations are equivalent.

One important property of the  $Z_j$  follows directly from writing (5.3) for n = m = 0. Since  $X_{00}(\theta, \lambda) = 1$ , equation (5.3) gives

$$\sum_{j=1}^{M} Z_{j}(\theta, \lambda) = 1 \quad .$$
 (5.5)

Equations (5.3) are implicit definitions of the functions  $Z_{j}(\theta, \lambda)$  once a set of points  $\theta_{j}$ ,  $\lambda_{j}$  has been selected on the sphere. The equations (5.3) are conceptually simple, but the selection of points seems to be a more profound topic.

First, the points must be distributed in such a way that the matrix corresponding to the coefficients in equation (5.3) is not singular. That is,

$$\begin{array}{c|c} X_{00}(\theta_{1},\lambda_{1}) X_{00}(\theta_{2},\lambda_{2}) \dots X_{00}(\theta_{M},\lambda_{M}) \\ X_{10}(\theta_{1},\lambda_{1}) X_{10}(\theta_{2},\lambda_{2}) \dots X_{10}(\theta_{M},\lambda_{M}) \\ & & \\ & & \\ & & \\ Y_{11}(\theta_{1},\lambda_{1}) Y_{11}(\theta_{2},\lambda_{2}) \dots Y_{11}(\theta_{M},\lambda_{M}) \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ Y_{NN}(\theta_{1},\lambda_{1}) Y_{NN}(\theta_{2},\lambda_{2}) \dots Y_{NN}(\theta_{M},\lambda_{M}) \end{array} \right)$$

$$(5.6)$$

Clearly, also, it is desirable to distribute the  $M = (N + 1)^2$  points uniformly over the sphere in some sense. Of course, there are but five regular polyhedra, and only the tetrahedron has a number of vertices equal to the square of an integer. Hence, the distribution must depart somehow from ideal regularity.

Numerical experiments or general arguments show further that a distribution that is symmetrical with respect to the equatorial plane and has rotational symmetry about the polar axis yields a zero value for the determinant (5.6). For example, if N = 3, a distribution with one point at each pole and seven uniformly spaced points at 30°N and 30°S latitude is not an acceptable array of points, even though it is an attractively uniform distribution of the correct number of points.

If one selects an arbitrary distribution of points satisfying (5.6), then (5.3) and its inverse by mathematical brute force are virtually the end of the story, unless particular properties of the distribution allow further conclusions to be reached. The cases in which (5.3) must be inverted numerically to express the  $Z_i$  as combinations of the  $X_{nm}$ ,  $Y_{nm}$  can already be quite useful, since the inversion need be done only once to obtain a usable expression for the  $Z_i$ .

# 6. THE FUNCTIONS $W_{kj}^{(\theta, \lambda)}$

There is at least one distribution of points on a sphere for which much can be proved about the properties of the  $Z_{j}(\theta, \lambda)$ . This distribution recognizes that there are some natural requirements on the point distribution suggested by the wavelengths inherent in the surface harmonics. Thus, there are 2N + 1 independent functions of longitude involved in the surface harmonics, and it is natural to expect that there be 2N + 1 distinct longitudes in the point distribution. Similarly, one might expect (2N + 1)/2 divisions of latitude between the poles.

First, define N + 1 latitude values by the equations

$$\theta_{2i} = \frac{i2\pi}{2N+1} , \quad i = 0, 1, \dots, \left[\frac{N}{2}\right] ,$$
  
$$\theta_{2i+1} = \frac{(N-i)2\pi}{2N+1} , \quad i = 0, 1, \dots, \left[\frac{N-1}{2}\right] . \quad (6.1)$$

Figure 2 illustrates the spacing of these points and the indexing convention. Next, at each of these latitudes,  $\theta_k$ , define 2k + 1 equally spaced points in longitude:

$$\lambda_{kj} = \frac{j2\pi}{2k+1}$$
,  $j = 0, 1, ..., 2k$ . (6.2)

These are also illustrated in Figure 2.

For any positive integer N, equations (6.1) and (6.2) define  $(N + 1)^2$ points. There are N + 1 latitudes, starting at the North Pole. The spacing in latitude between circles of points is  $2\pi/(2N + 1)$ , except that the most southerly latitude is only half this distance from the South Pole. This most southerly latitude circle has three points. Below the single point at the North Pole, the next circle has five points. The second most southerly circle has



۰,



seven points, etc. The latitude circle nearest the Equator has the greatest number of points, namely, 2N + 1. Also, any meridian circle has 2N + 1 uniformly spaced intersections with the latitude circles. In this sense, the points are spaced equally in latitude and longitude. For notational brevity, this distribution of points will sometimes be referred to as the 1-3-5... distribution.

An important property of this distribution is that condition (5.6) is satisfied, and the Z<sub>j</sub> are well defined. For this particular point distribution, the functions  $Z_{i}(\theta, \lambda)$  will be denoted by  $W_{ki}(\theta, \lambda)$ , where

$$W_{kj}(\theta_{\ell}, \lambda_{\ell i}) = \delta_{kj,\ell i} \qquad (6.3)$$

Also,

$$W_{kj}(\theta, \lambda) = \sum_{n=0}^{N} \sum_{m=0}^{n} \left[ A_{kj}^{nm} X_{nm}(\theta, \lambda) + B_{kj}^{nm} Y_{nm}(\theta, \lambda) \right] , \qquad (6.4)$$

and

$$X_{nm}(\theta, \lambda) = \sum_{k=0}^{N} \sum_{j=0}^{2k} X_{nm}(\theta_{k}, \lambda_{kj}) W_{kj}(\theta, \lambda) ,$$

$$Y_{nm}(\theta, \lambda) = \sum_{k=0}^{N} \sum_{j=0}^{2k} Y_{nm}(\theta_{k}, \lambda_{kj}) W_{kj}(\theta, \lambda) . \qquad (6.5)$$

From (5.5) or (6.5) it follows that

$$\sum_{k=0}^{N} \sum_{j=0}^{2k} W_{kj}(\theta, \lambda) = 1 \quad .$$
 (6.6)

A number of further properties of the  $W_{kj}$  can also be proved. Consider initially  $k \neq 0$  and let  $\theta_k$  not be a zero of  $P_{nm}(\theta)$ , whatever the values of n and m. This is true for the 1-3-5  $\cdots$  distribution. It follows that

$$W_{kj}(\theta_{k}, \lambda) = \sum_{m=0}^{N} \left\{ \sum_{n=m}^{N} A_{kj}^{nm} P_{nm}(\cos \theta_{k}) \right\} \cos m\lambda + \left[ \sum_{n=m}^{N} B_{kj}^{nm} P_{nm}(\cos \theta_{k}) \right] \sin m\lambda \right\}$$
$$= \sum_{m=0}^{N} \left( a_{kj}^{m} \cos m\lambda + b_{kj}^{m} \sin m\lambda \right) . \qquad (6.7)$$

But equation (6.3) requires for a fixed k that

$$W_{kj}(\theta_k, \lambda_{k\ell}) = \delta_{j\ell} \qquad (6.8)$$

Equations (6.7) and (6.8) define uniquely a set of 2k + 1 functions of  $\lambda$ , namely,

$$W_{kj}(\theta_k, \lambda) = q_{kj}(\lambda) = \frac{1}{2k+1} \left[ 1 + 2 \sum_{m=1}^k \cos m(\lambda - \lambda_{kj}) \right] , \qquad (6.9)$$

$$j = 0, 1, ..., 2k$$

The  $q_{kj}(\lambda)$  are identically the functions discussed in Section 4. Thus, for each latitude circle defined by  $\theta_k$ , the  $W_{kj}$  evaluated for  $\theta = \theta_k$  reduce to the  $q_{kj}(\lambda)$ . This is one sense in which the  $W_{kj}$  are natural extensions of the  $q_{kj}$ . To illustrate another related property of the  $W_{kj}$ , it is convenient first to define a further set of functions closely related to the  $q_{kj}$ :

$$C_{0}(\theta) = \frac{1}{2N+1} \left( 1 + 2 \sum_{j=1}^{N} \cos j\theta \right) ,$$

$$C_{\ell}(\theta) = \frac{2}{2N+1} \left( 1 + 2 \sum_{j=1}^{N} \cos j\theta_{\ell} \cos j\theta \right) , \qquad (6.10)$$

$$\theta_{2i} = \frac{i2\pi}{2N+1} , \qquad i = 0, 1, \dots, \frac{N}{2} ,$$

$$\theta_{2i+1} = \frac{(N-i)2\pi}{2N+1} , \qquad i = 0, 1, \dots, \frac{N-1}{2} . \qquad (6.11)$$

These functions have the properties that

$$C_{\ell}(\theta_{j}) = \delta_{\ell j}$$
,  $j, \ell = 0, 1, ..., N$ , (6.12)

$$\sum_{\ell=0}^{N} C_{\ell}(\theta) = 1$$
 (6.13)

Conversely, if  $C_{\ell}(\theta)$  is a linear combination of functions cos  $j\theta$ , point distribution (6.11) and conditions (6.12) and (6.13) imply equations (6.10). Thus, the functions  $C_{\ell}$  are functions of latitude having localized properties similar to those of the  $q_{ki}$ .

Now for a fixed k in equation (6.4), the sum of the  $W_{kj}^{(\theta, \lambda)}$  for the values of j, (j = 0, 1, ..., 2k), can be shown to yield the result

$$\sum_{j=0}^{2k} W_{kj}(\theta, \lambda) = C_k(\theta) , \qquad (6.14)$$

and, in particular,

$$W_{00}(\theta, \lambda) = C_0(\theta) \quad . \tag{6.15}$$

Equations (6.14) and (6.15) are another manifestation of the localized properties of the  $W_{kj}$ .

# 7. EXAMPLES OF $W_{kj}(\theta, \lambda)$

The  $W_{kj}(\theta, \lambda)$  for any N are implicitly defined by equations (6.5). For small values of N it is possible to write explicit expressions for the  $W_{kj}$  in simple form.

For N = 1, the functions are

$$W_{00} = \frac{1}{3} (1 + 2 \cos \theta) ,$$
  

$$W_{1j} = \frac{2}{9} (1 + 2 \cos \theta_1 \cos \theta) + \frac{2 \sin \theta}{3 \sin \theta_1} \cos (\lambda - \lambda_{1j}) , \qquad (7.1)$$

for j = 0,1,2 ,

where

$$\theta_0 = 0 ,$$
  
$$\theta_1 = \frac{2\pi}{3} ; \quad \lambda_{10} = 0 , \lambda_{11} = \frac{2\pi}{3} , \quad \lambda_{12} = \frac{4\pi}{3}$$

For N = 2, the functions are

$$\begin{split} W_{00} &= \frac{1}{5} \left( 1 + 2 \cos \theta + 2 \cos 2\theta \right) , \\ W_{1j} &= \frac{2}{15} \left( 1 + 2 \cos \theta_1 \cos \theta + 2 \cos 2\theta_1 \cos 2\theta \right) \\ &+ \frac{2 \sin \theta (\cos \theta_2 - \cos \theta)}{3 \sin \theta_1 (\cos \theta_2 - \cos \theta_1)} \cos \left( \lambda - \lambda_{1j} \right) , \quad j = 0, 1, 2 \end{split}$$

$$W_{2j} = \frac{2}{25} (1 + 2 \cos \theta_2 \cos \theta + 2 \cos 2\theta_2 \cos 2\theta)$$

$$+ \frac{2 \sin \theta_2 \sin \theta (\cos \theta - \cos \theta_1)}{5 \sin^2 \theta_2 (\cos \theta_2 - \cos \theta_1)} \cos (\lambda - \lambda_{2j})$$

$$+ \frac{2 \sin \theta_1 \sin \theta (\cos \theta - \cos \theta_2)}{5 \sin^2 \theta_2 (\cos \theta_2 - \cos \theta_1)} \cos (\lambda + 2\lambda_{2j})$$

$$+ \frac{2 \sin^2 \theta}{5 \sin^2 \theta_2} \cos 2(\lambda - \lambda_{2j}) , \qquad j = 0, 1, 2, 3, 4$$

where

$$\begin{split} \theta_0 &= 0 \quad , \\ \theta_1 &= \frac{4\pi}{5} \quad ; \quad \lambda_{10} = 0, \ \lambda_{11} = \frac{2\pi}{3} \ , \ \lambda_{12} = \frac{4\pi}{3} \quad , \\ \theta_2 &= \frac{2\pi}{5} \quad ; \quad \lambda_{20} = 0, \ \lambda_{21} = \frac{2\pi}{5} \ , \ \lambda_{22} = \frac{4\pi}{5} \ , \ \lambda_{23} = \frac{6\pi}{5} \ , \ \lambda_{24} = \frac{8\pi}{5} \end{split}$$

Numerical examples for larger values of N are given by Hebb and Mair (1969).

#### 8. FUNCTIONS IN THREE DIMENSIONS

In three dimensions, the functions in which the potential is usually expanded can be written as

$$\mathcal{L}_{nm}(\mathbf{r},\theta,\lambda) = R_{n}(\mathbf{r}) X_{nm}(\theta,\lambda) ,$$

$$\mathcal{L}_{nm}(\mathbf{r},\theta,\lambda) = R_{n}(\mathbf{r}) Y_{nm}(\theta,\lambda) , \qquad (8.1)$$

where the  $X_{nm}$  and  $Y_{nm}$  are the surface harmonics in equation (5.1) and

$$R_{n}(r) = \left(\frac{a}{r}\right)^{n+1} \qquad (8.2)$$

There are  $M = (N + 1)^2$  functions (8.1) in a space that corresponds to a maximum value n = N.

As with the one- and two-dimensional cases, it is again desired to define an alternative set of functions  $\mathcal{J}_j(r,\theta,\lambda)$  that have localized properties generated by the condition that

$$\mathcal{J}_{i}(r_{j},\theta_{j},\lambda_{j}) = \delta_{ij} , \qquad (8.3)$$

where  $(r_j, \theta_j, \lambda_j)$  is a point in a selected set of  $(N + 1)^2$  points. It follows immediately that

$$\mathcal{X}_{nm}(\mathbf{r},\theta,\lambda) = \sum_{j=1}^{M} \mathcal{X}_{nm}(\mathbf{r}_{j},\theta_{j},\lambda_{j}) \stackrel{\mathcal{R}}{\mathcal{J}}_{j}(\mathbf{r},\theta,\lambda) ,$$

$$\mathcal{Y}_{nm}(\mathbf{r},\theta,\lambda) = \sum_{j=1}^{M} \mathcal{Y}_{nm}(\mathbf{r}_{j},\theta_{j},\lambda_{j}) \stackrel{\mathcal{R}}{\mathcal{J}}_{j}(\mathbf{r},\theta,\lambda) . \qquad (8.4)$$

Let the inverse of this be written as

$$\mathcal{J}_{j}(\mathbf{r},\theta,\lambda) = \sum_{n=0}^{N} \sum_{m=0}^{n} \left[ \mathcal{A}_{j}^{nm} \mathcal{X}_{nm}(\mathbf{r},\theta,\lambda) + \mathcal{B}_{j}^{nm} \mathcal{J}_{nm}(\mathbf{r},\theta,\lambda) \right] .$$
(8.5)

Analogously to equations (5.3), equations (8.4) are an implicit definition for the  $\mathcal{J}_j(\mathbf{r}, \theta, \lambda)$ . Again, the crucial question is the distribution of points  $(r_j, \theta_j, \lambda_j)$ . For the  $\mathcal{J}_j(\mathbf{r}, \theta, \lambda)$  to be well defined, it is necessary and sufficient that

$$\begin{aligned} & \mathcal{X}_{00}(\mathbf{r}_{1},\theta_{1},\lambda_{1}) \, \mathcal{X}_{00}(\mathbf{r}_{2},\theta_{2},\lambda_{2}) \dots \, \mathcal{X}_{00}(\mathbf{r}_{M},\theta_{M},\lambda_{M}) \\ & \mathcal{X}_{10}(\mathbf{r}_{1},\theta_{1},\lambda_{1}) \, \mathcal{X}_{10}(\mathbf{r}_{2},\theta_{2},\lambda_{2}) \dots \, \mathcal{X}_{10}(\mathbf{r}_{M},\theta_{M},\lambda_{M}) \\ & \dots \\ & \mathcal{Y}_{11}(\mathbf{r}_{1},\theta_{1},\lambda_{1}) \, \mathcal{Y}_{11}(\mathbf{r}_{1},\theta_{1},\lambda_{1}) \dots \, \mathcal{Y}_{11}(\mathbf{r}_{M},\theta_{M},\lambda_{M}) \\ & \dots \\ & \mathcal{Y}_{NN}(\mathbf{r}_{1},\theta_{1},\lambda_{1}) \, \mathcal{Y}_{NN}(\mathbf{r}_{2},\theta_{2},\lambda_{2}) \dots \, \mathcal{Y}_{NN}(\mathbf{r}_{M},\theta_{M},\lambda_{M}) \end{aligned}$$

$$\tag{8.6}$$

If all the points  $(r_j, \theta_j, \lambda_j)$  are distributed on a sphere of some radius  $r_j = r_0$ , then condition (8.6) reduces immediately to (5.6), and all the discussions of Sections 5, 6, and 7 are pertinent to the three-dimensional case. In this situation, equations (8.4) become

$$\mathcal{X}_{nm}(r,\theta,\lambda) = \left(\frac{a}{r_0}\right)^{n+1} \sum_{j=1}^{M} X_{nm}(\theta_j,\lambda_j) \mathcal{J}_j(r,\theta,\lambda) ,$$

$$\mathcal{Y}_{nm}(r,\theta,\lambda) = \left(\frac{a}{r_0}\right)^{n+1} \sum_{j=1}^{M} Y_{nm}(\theta_j,\lambda_j) \mathcal{J}_j(r,\theta,\lambda) , \qquad (8.7)$$

$$\left(\frac{r_{0}}{r}\right)^{n+1} X_{nm}(\theta, \lambda) = \sum_{j=1}^{M} X_{nm}(\theta_{j}, \lambda_{j}) \not \exists_{j}(r, \theta, \lambda) ,$$

$$\left(\frac{r_{0}}{r}\right)^{n+1} Y_{nm}(\theta, \lambda) = \sum_{j=1}^{M} Y_{nm}(\theta_{j}, \lambda_{j}) \not \exists_{j}(r, \theta, \lambda) . \qquad (8.8)$$

Equations (8.8) have the same form as equation (5.3), so their inverse can be expressed simply in terms

$$\mathcal{J}_{j}(\mathbf{r},\theta,\lambda) = \sum_{n=0}^{M} \sum_{m=0}^{n} \left[ a_{j}^{nm} \left(\frac{\mathbf{r}_{0}}{\mathbf{r}}\right)^{n+1} X_{nm}(\theta,\lambda) + b_{j}^{nm} \left(\frac{\mathbf{r}_{0}}{\mathbf{r}}\right)^{n+1} Y_{nm}(\theta,\lambda) \right] ,$$

$$(8.9)$$

where the  $a_j^{nm}$  and  $b_j^{nm}$  are identical to those of Sections 5, 6, and 7 if the same points on the sphere are selected. This form is convenient for investigating the properties of the  $\mathcal{J}_j(\mathbf{r}, \theta, \lambda)$ .

Let  $r = r_0 + h$ , so that

$$\left(\frac{r_0}{r}\right)^{n+1} = \left(\frac{r_0}{r}\right) \left(\frac{r_0}{r_0+h}\right)^n = \left(\frac{r_0}{r}\right) \left(1+\frac{h}{r_0}\right)^{-n} .$$
(8.10)

Expanding this in a series gives

$$\left(\frac{r_0}{r}\right)^{n+1} = \left(\frac{r_0}{r}\right) \left[1 + (-n)\left(\frac{h}{r_0}\right) + \frac{(-n)(-n-1)}{2}\left(\frac{h}{r_0}\right)^2 + \dots\right] \quad . \quad (8.11)$$
Substitution of (8.11) into (8.9) then gives

$$\begin{aligned}
\vec{\mathcal{J}}_{j}(\mathbf{r},\theta,\lambda) &= \sum_{n=0}^{M} \sum_{m=0}^{n} \left\{ \begin{pmatrix} \frac{\mathbf{r}_{0}}{\mathbf{r}} \end{pmatrix} \left[ \mathbf{a}_{j}^{nm} \mathbf{X}_{nm} + \mathbf{b}_{j}^{nm} \mathbf{Y}_{nm} \right] \\
&+ \left( \frac{\mathbf{r}_{0}}{\mathbf{r}} \right) \left( \frac{\mathbf{h}}{\mathbf{r}_{0}} \right) \left[ \mathbf{a}_{j}^{nm}(-\mathbf{n}) \mathbf{X}_{nm} + \mathbf{b}_{j}^{nm}(-\mathbf{n}) \mathbf{Y}_{nm} \right] \\
&+ \left( \frac{\mathbf{r}_{0}}{\mathbf{h}} \right) \left( \frac{\mathbf{h}}{\mathbf{r}_{0}} \right)^{2} \left[ \mathbf{a}_{j}^{nm} \frac{(-\mathbf{n})(-\mathbf{n}-1)}{2} \mathbf{X}_{nm} + \mathbf{b}_{j}^{nm} \frac{(-\mathbf{n})(-\mathbf{n}-1)}{2} \mathbf{Y}_{nm} \right] \\
&+ \dots \end{aligned}$$

$$(8.12)$$

But the first term on the right of (8.12) can be expressed simply in terms of the  $Z_j$  as defined in (5.4). Define  $\int_{j}^{0} j^{(r,\theta,\lambda)} by$ 

$$\oint_{j}^{0} (\mathbf{r}, \theta, \lambda) = \left(\frac{\mathbf{r}_{0}}{\mathbf{r}}\right) Z_{j}(\theta, \lambda) \quad .$$
(8.13)

Then

$$\begin{aligned} \mathcal{J}_{j}(\mathbf{r},\boldsymbol{\theta},\boldsymbol{\lambda}) &= \mathcal{J}_{j}^{0}(\mathbf{r},\boldsymbol{\theta},\boldsymbol{\lambda}) \\ &+ \left(\frac{\mathbf{h}}{\mathbf{r}_{0} + \mathbf{h}}\right) \sum_{n=0}^{M} \sum_{m=0}^{n} \left[ a_{j}^{nm}(-n) \; \mathbf{X}_{nm} + b_{j}^{nm}(-n) \; \mathbf{Y}_{nm} \right] \end{aligned}$$

+....

Since the  $\mathcal{J}_{j}$  will be evaluated on the geoid, a value of  $r_0$  can be selected such that

$$\frac{h}{r_0 + h} \sim -\frac{1}{2} \frac{1}{298}$$
 at the poles, and

$$\frac{h}{r_0 + h} \sim + \frac{1}{2} \frac{1}{298}$$
 at the Equator.

From the expanded form of  $\mathcal{J}_{j}(r,\theta,\lambda)$ , it can be seen that, for small values of (h/r), the function retains the localized properties imposed by the factor  $Z_{j}$  in the dominant term  $\mathcal{J}_{j}^{0}$ . If the 1-3-5... distribution is selected, then the  $Z_{j}$  becomes  $W_{jk}$ , and still more can be said about the behavior of the  $\mathcal{J}_{j}$ .

However, there may be advantages in selecting a distribution of points not lying on a sphere. For example, the ellipsoid best approximating the geoid might be chosen, and points distributed on it according to the 1-3-5<sup>···</sup> distribution. In this case, the terms on the right of equations (8.4) have different factors  $(a/r_j)^{n+1}$  because the  $r_j$  are different. Still, from general considerations, it seems that the first terms accounting for displacements of the geoid from the ellipsoid will be proportional to  $(h/r_R)$ , where  $r_R$  is on the reference ellipsoid and h is the distance from the ellipsoid. The maximum value of h for sea level will be less than 100 m, so  $(h/r_R) \sim 10^{-5}$ .

9. COEFFICIENTS OF 
$$\hat{\mathcal{J}}_j$$
 IN THE GEOPOTENTIAL

In spherical harmonics, the geopotential can be represented by

$$V(r,\theta,\lambda) = GM \sum_{n=0}^{N} \sum_{m=0}^{n} \left[ C_{nm} \mathcal{X}_{nm}(r,\theta,\lambda) + S_{nm} \mathcal{Y}_{nm}(r,\theta,\lambda) \right] , \quad (9.1)$$

where GM is the gravitational constant for the earth. For objects constrained to rotate with the earth, such as the oceans, the centrifugal potential must be added to this, namely,

$$+ \frac{\omega^2 r^2}{2} \sin^2 \theta , \qquad (9.2)$$

where  $\omega$  is the rotational rate of the earth.

Substituting expressions for  $\mathcal{X}_{nm}$  and  $\mathcal{Y}_{nm}$  into (9.1) gives

$$V(r,\theta,\lambda) = GM \sum_{j=1}^{M} \left[ \sum_{n=0}^{N} \sum_{m=0}^{n} C_{nm} \mathcal{X}_{nm}(r_{j},\theta_{j},\lambda_{j}) + S_{nm} \mathcal{Y}_{nm}(r_{j},\theta_{j},\lambda_{j}) \right] \mathcal{J}_{j}(r,\theta,\lambda)$$
(9.3)

If the coefficient  $L_{j}$  is defined by

$$L_{j} = \sum_{n=0}^{N} \sum_{m=0}^{n} \left[ C_{nm} \mathcal{X}_{nm}(r_{j}, \theta_{j}, \lambda_{j}) + S_{nm} \mathcal{Y}_{nm}(r_{j}, \theta_{j}, \lambda_{j}) \right] , \qquad (9.4)$$

then

$$V(r,\theta,\lambda) = GM \sum_{j=1}^{M} L_{j} \frac{\partial}{\partial j} (r,\theta,\lambda) \quad .$$
(9.5)

This is a representation of the geopotential that is completely equivalent to equation (9.1). However, each term in the sum dominates in one local region of the geoid, namely, the region around one of the selected grid of points. The functions  $\mathcal{J}_j$  were defined so as to produce this situation. Determining the coefficients L<sub>j</sub> is equivalent to determining the coefficients  $C_{nm}$  and  $S_{nm}$ , since the transformation and its inverse from  $\mathcal{J}_j$  to  $\mathcal{M}_{nm}$ and  $\mathcal{J}_{nm}$  also define the transformations between the coefficients.

In the space around the earth, the equation of an equipotential surface is

$$GM\sum_{j=1}^{M} L_{j} \overset{2}{\underset{j}{\partial}}_{j}(r,\theta,\lambda) - V = 0 , \qquad (9.6)$$

where V is a constant. The geoid, that is, mean sea level, is given by

$$GM\sum_{j=1}^{M} L_{j} \mathcal{J}_{j}(r,\theta,\lambda) + \frac{\omega^{2}r^{2}}{2} \sin^{2}\theta - V_{0} = 0 \quad .$$
 (9.7)

There are several ways that a determination of the geopotential might proceed utilizing the localized properties of the  $\mathcal{J}_j$  and equation (9.5). The particular procedure employed would depend somewhat upon the knowledge of the geopotential existing at the time the determination process is initiated. A simplified scenario, based on assumed conditions that might exist, can illustrate the general character of the procedures.

First, it can be assumed that the coefficients are available for a reasonably accurate geopotential in spherical harmonics through 15, 15. Presumably this geopotential representation would be the product of orbital analyses of many satellites, perhaps including altimeter data as outlined in Section 3 and in Lundquist (1967a). Second, it will be assumed that an altimeter-bearing satellite has been flown and has produced altitude data sufficient for a substantial improvement in the ocean geoid beyond the profile given by the 15,15 solution. The accuracy of the altitudes should be in the few-meter range as discussed in Section 1.

Third, laser tracking of the satellite to meter accuracy will be assumed from a network of several ground stations.

Fourth, it will be assumed that the knowledge of the geopotential (including coefficients for resonant harmonics) together with ground-station tracking data allows an orbit for the satellite to be determined with meter accuracy in the vicinity of the tracking stations. However, the orbit based on ground-station tracking may not be expected to maintain meter accuracy over the long stretches of ocean between ground stations.

This last assumption leads to the fifth assumption, namely, that the altitude data themselves must be used to help generate the orbit to meter accuracy over the oceans. At the same time, the altitudes will be used to define the ocean geoid. An improvement of the geopotential probably will not be required for orbit determination, but if it is required, the determination can be done as a separate step in the chain of calculations.

Given these assumptions, the procedure to be followed is broadly a differential improvement calculation. The steps of the process might go as follows:

From the ground-station tracking, initial orbital elements and a corresponding initial orbit would be generated. From this orbit, a position  $\vec{r}(t_a)$  of the satellite can be calculated for the time  $t_a$  of each altitude measurement.

From the position of the satellite and from the ocean geoid corresponding to the initial geopotential, the point  $\vec{S}$  on the ocean to which the altitude has been measured can be calculated. This calculation, of course, depends upon

the characteristics of the altimeter. The calculation might be quite different for a broad-beam radio altimeter than for a narrow-beam laser altimeter. The calculated or expected value of the altitude is then the magnitude h of the vector

$$\vec{h}(t_{a}) = \vec{r}(t_{a}) - \mathcal{K}_{3} \mathcal{K}_{3} \vec{s}[\vec{r}(t_{a}), V_{0}, L_{1}, L_{2}, \dots, L_{M}] \quad .$$
(9.8)

The position  $\vec{r}$  (t<sub>a</sub>) is to be considered as a function of the orbital elements  $E_k$ , although this dependency has not been explicitly indicated in equation (9.8). The transformations  $\mathcal{R}$  and  $\mathcal{R}_3$  carry the earth-fixed vector  $\vec{s}$  into the space-fixed system in which  $\vec{r}$  is expressed (see Gaposchkin, 1966b, or Lundquist, 1967a).

Formally expressing the differential of h gives

$$dh = \sum_{i,k} \frac{\partial h}{\partial r_{i}} \frac{\partial r_{i}}{\partial E_{k}} dE_{k} + \sum_{\ell,i,k} \frac{\partial h}{\partial S_{\ell}} \frac{\partial S_{\ell}}{\partial r_{i}} \frac{\partial r_{i}}{\partial E_{k}} dE_{k}$$
$$+ \sum_{\ell} \frac{\partial h}{\partial S_{\ell}} \frac{\partial S_{\ell}}{\partial V_{0}} dV_{0} + \sum_{\ell,j} \frac{\partial h}{\partial S_{\ell}} \frac{\partial S_{\ell}}{\partial L_{j}} dL_{j} + \sum_{j} \frac{\partial h}{\partial r_{i}} \frac{\partial r_{i}}{\partial L_{j}} dL_{j}$$
(9.9)

Because of the fifth assumption, it could be possible to neglect the last term, involving the dependence of h on the coefficients  $L_j$  through the dependence of  $r_j$  on the  $L_j$ .

If dh is identified with the difference between the calculated and the observed altitudes, the equation (9.9) leads to an observation equation for corrections  $\delta E_k$  to the orbital elements and for corrections  $\delta V_0$  and  $\delta L_i$  to the parameters specifying the geoid. The observation equation derived from equation (9.9) must also provide for errors  $\delta h$  in the observations of h. In conventional format, for each measurement  $h_i$  at some time  $t_i$ , an observation equation is written (see Kaula, 1966, p. 72):

$$h_i(observed at t_i) - h_i(calculated for t_i) = \mathcal{M}_{ij} \delta F_j - \delta h_i$$
, (9.10)

where  $\delta F_j$  are the corrections  $\delta E_j$ ,  $\delta V_0$ ,  $\delta L_j$ ; and  $\mathcal{M}_{ij}$  are the partial derivatives with respect to  $F_j$  from equation (9.9) evaluated at time  $t_i$ .

The next step in utilizing altimetry data is a solution for the  $\delta F_j$  from equations (9.10) and similar observation equations from ground-station tracking. The latter equations, by the assumptions above, will involve only the  $\delta E_j$ . Each of the equations (9.10) will have a term in  $\delta V_0$ . However, the occurrences of terms in  $\delta L_j$  are strongly limited by the localized properties of the  $\mathcal{J}_j$ .

To illustrate this situation, a simplified procedure can be considered. The surface of the reference surface can be divided into  $M = (N+1)^2$  areas centered on the points in the selected set from which the  $\mathcal{J}_j$  were derived. For the region around point  $(r_k, \delta_k, \lambda_k)$ , the term  $L_k \mathcal{J}_k$  dominates the sum in equation (9.7). Each line from the satellite through the subaltimeter point  $\vec{S}_i$ , for an observation at time  $t_i$ , intersects one of the M regions, noted for example by an index k,  $\vec{S}_i^k$ .

This suggests that a vector 
$$\vec{T}_{i}^{k}$$
 be defined by  
 $\vec{T}_{i}^{k} = \vec{S}_{i}^{k,0} - \vec{G}^{k,0}$ , (9.11)

where  $\vec{G}^{k,0}$  is the point with arguments  $\theta_k, \lambda_k$  on the surface defined by (9.7) with the initial values  $V_0^0$  and  $L_j^0$  in the geopotential, and  $\vec{S}_i^{k,0}$  is the subaltimeter point calculated with the initial  $V_0^0$  and  $L_j^0$ . The vector  $\vec{T}_i^k$  is a chord connecting two points on the geoid.

It is reasonable to expect that  $\overline{T}_{i}^{k}$  will be essentially unaffected by small changes in  $V_{0}$  and the  $L_{j}$ , since both terms on the right of (9.11) respond similarly to these changes. Thus,  $\overline{S}_{i}^{k}$  will be assumed to have a satisfactory representation as

$$\vec{S}_{i}^{k} = \vec{G}^{k} + \vec{T}_{i}^{k}$$
 (9.12)

This asserts that the dependence of  $\vec{S}_i^k$  on small changes in  $V_0$  and the  $L_j$  arises mainly through the dependence of  $\vec{G}^k$  on  $V_0$  and the  $L_j$ . But by the localized properties of the  $\vec{F}_j$ , only changes in the single coefficient  $L_k$  contribute significantly to changes in  $\vec{G}^k$ . Hence,

$$\frac{\partial \vec{S}_{i}^{k}}{\partial L_{j}} = \delta_{jk} \frac{\partial \vec{G}^{k}}{\partial L_{k}} \quad . \tag{9.13}$$

The result of equation (9.13) is a substantial simplification of equations (9.10) through a simplification of the form of  $\mathcal{M}_{ij}$ . To illustrate this, consider the submatrix of  $\mathcal{M}_{ij}$ , which concerns corrections  $\delta L_j$ . This submatrix has M columns corresponding to the M independent coefficients  $L_j$ . There will be as many rows as there are altitude measurements.

The altitudes can be collected into M sets corresponding to the regions into which the corresponding  $\vec{S}_i$  fall. The observation equations can be grouped in the same way, so that  $\mathcal{M}_{ij}$  first has some number of rows corresponding to altitudes to the first region, then some other number of rows corresponding to the second region, etc.

Consider next the submatrix of  $\mathcal{M}_{ij}$  corresponding to a region identified by index k. By equation (9.13), this submatrix has nonzero entries only in the kth column, where the entry in the row for the ith observation is

$$\sum_{\ell} \frac{\partial h}{\partial S_{\ell}^{k}} \left. \frac{\partial G_{\ell}^{k}}{\partial L_{j}} \right|_{t = t_{i}}$$
(9.14)

Note that here the subscript l denotes the component of the vector, not the particular observation. The latter is explicitly indicated by the observation time at which the expression is evaluated.

The solution of the observation equations proceeds with formation of the normal equations. However, the form of  $\mathcal{M}_{ij}$  in those columns that concern the  $\delta L_j$  is just that for which the solution of the normal equations is greatly simplified. Kaula discusses this in detail, and his development will not be repeated here. (See Kaula, 1966, beginning on page 104. The matrix  $\mathcal{M}$  has the form required in Kaula's equation 5.61 on page 105.)

In broad terms, when solving for the  $\delta F_j$ , there would be finally a largest submatrix to invert having the dimension of the number of orbital elements plus one for  $V_0$ . This is a vast simplification compared with inverting a matrix of this dimension plus M, particularly when M is very large.

As a final step, the  $\delta F_j$  are added to their respective  $F_j$ , resulting in an improvement to both orbital elements and to the geopotential coefficients. If necessary, the whole process can be iterated, beginning again with the improved elements and geopotential.

An additional feature of the procedure deserves mention. There will, of course, be no altitude observation equations for regions corresponding to land masses. Hence, the coefficients L for these regions will maintain their initial values, which presumably reflect the best information available from other arguments.

The scenario for a geopotential solution offered in this section has been drastically simplified and depends upon assumptions that may or may not prevail when an altimeter satellite is flown. In a more realistic treatment, most of the assumptions and approximations could be relaxed without essential effect on the general features of the procedures. Thus, it seems likely that use of functions  $\mathcal{J}_{j}(r, \theta, \lambda)$  can significantly facilitate an improvement of the

geopotential based on altitude observations. This allows the final conclusion that satellite-to-ocean altitudes promise substantial geopotential information in a form that can be analyzed without undue difficulty.

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#### REFERENCES

BENDER, P. L.

1967. Laser measurements of long distances. Proc. of the IEEE, vol. 55, pp. 1039-1045.

GAPOSCHKIN, E. M.

- 1966a. Tesseral harmonic coefficients and station coordinates from the dynamic method. <u>In</u> Geodetic parameters for a 1966 Smithsonian Institution Standard Earth, ed. by C. A. Lundquist and G. Veis, Smithsonian Astrophys. Obs. Spec. Rep. No. 200, vol. 2, pp. 105-258.
- 1966b. Orbit determination. <u>In</u> Geodetic parameters for a 1966 Smithsonian Institution Standard Earth, ed. by C. A. Lundquist and G. Veis, Smithsonian Astrophys. Obs. Spec. Rep. No. 200, vol. 2, 77-184.

GIACAGLIA, G. E. O., and LUNDQUIST, C. A.

1968. Representations for fine geopotential structure (abstract). <u>In</u> Guidance Theory and Trajectory Analysis Seminar Abstracts, NASA Electronics Research Center, Cambridge, Mass., pp. 15-16.

GREENWOOD, J. A., NATHAN, A., NEUMANN, G., PIERSON, W. J., JACKSON, F. C., and PEASE, T. E.

1967. Radar altimetry from a spacecraft and its potential applications to geodesy and oceanography. New York University Geophysical Sciences Laboratory Report No. TR-67-3, 94 pp.

HEBB, K., and MAIR, S. G.

1969. Numerical definition of localized functions on a sphere. Smithsonian Astrophys. Obs. Spec. Rep., this volume.

KAULA, W. M.

1966. Theory of Satellite Geodesy. Blaisdell Publishing Company, Waltham, Mass.

# KÖHNLEIN, W.

- 1967. The earth's gravitational field as derived from a combination of satellite data with gravity anomalies. <u>In Geodetic satellite</u> results during 1967, ed. by C. A. Lundquist, Smithsonian Astrophys. Obs. Spec. Rep. No. 264, pp. 57-72.
- LEHR, C. G., MAESTRE, L. A., and ANDERSON, P. H.
  - 1967. Satellite ranging with a laser and the correction for atmospheric refraction. Proc. Intl. Symp. Figure of the Earth and Refraction (Vienna), pp. 163-171.

LUNDQUIST, C. A.

- 1967a. Satellite altimetry and orbit determination. Smithsonian Astrophys. Obs. Spec. Rep. No. 248, 14 pp.
- 1967b. The interface between satellite altimetry and orbit determination (abstract). Proc. Guidance Theory and Trajectory Analysis Seminar, NASA Electronics Research Center, Cambridge, Mass., pp. 39-41.
- MADDEN, S. J.
  - 1968. The geoid in spheroidal coordinates (abstract). <u>In</u> Guidance Theory and Trajectory Analysis Seminar Abstracts, NASA Electronics Research Center, Cambridge, Mass., p. 17.

PLOTKIN, H. H.

 1968. Geos-B plans for laser tracking and experiments by GSFC. In Proc. Geos Program Review Meeting, 12-14 December 1967, vol. 1, pp. 205-216.

RAYTHEON COMPANY

- 1968a. Space geodesy altimetry study, by Kolker, M., and Tatsch, J. H. Monthly Progress Report, April 1968, NASA Contract NASW-1709, Space and Information Systems Division, Sudbury, Mass.
- 1968b. Space geodesy altimetry study, by Kolker, M., and Tatsch, J. H. Monthly Progress Report, May 1968, NASA Contract NASW-1709, Space and Information Systems Division, Sudbury, Mass.
- 1968c. Space geodesy altimetry study, by Weiss, E., and Kolker, M. Monthly Progress Report, June/July 1968, NASA Contract NASW-1709, Space and Information Systems Division, Sudbury, Mass.

#### ROSENBERG, J. D.

1965. The organization of the United States geodetic satellite program. <u>In</u> Reseau Géodésique European par Observation des Satellites, Proceedings of the Paris Symposium, Institut Géographique National, Paris, pp. 30-37.

STRANGE, W. E., and RAINEY, H. T.

- 1968. Status and requirements in gravimetric satellite geodesy (abstract).
   <u>In</u> Guidance Theory and Trajectory Analysis Seminar Abstracts,
   NASA Electronics Research Center, Cambridge, Mass., p. 18.
- VEIS, G.
  - 1967. Determination of the radius of the earth and other geodetic parameters as derived from optical satellite data. <u>In</u> Geodetic satellite results during 1967, ed. by C. A. Lundquist, Smithsonian Astrophys. Obs. Spec. Rep. No. 264, pp. 73-100.

VON ARX, W. S.

1966. Level surface profiles across the Puerto Rico trench. Science, vol. 154, pp. 1651-1654.

## NUMERICAL DEFINITION OF LOCALIZED FUNCTIONS ON A SPHERE

K. Hebb and S. G. Mair

### NUMERICAL DEFINITION OF LOCALIZED FUNCTIONS ON A SPHERE

#### K. Hebb and S. G. Mair

#### 1. INTRODUCTION

As stated in the preceding paper, the constants  $A_{j}^{nm}$  and  $B_{j}^{nm}$  of the expression

$$Z_{j}(\theta,\lambda) = \sum_{n=0}^{N} \sum_{m=0}^{n} \left[ A_{j}^{nm} X_{nm}(\theta,\lambda) + B_{j}^{nm} Y_{nm}(\theta,\lambda) \right]$$
(5.4)\*

can be determined either from inversion of the equations

$$X_{nm}(\theta, \lambda) = \sum_{j=1}^{M} X_{nm}(\theta_{j}, \lambda_{j}) Z_{j}(\theta, \lambda)$$
$$Y_{nm}(\theta, \lambda) = \sum_{j=1}^{M} Y_{nm}(\theta_{j}, \lambda_{j}) Z_{j}(\theta, \lambda)$$
(5.3)

or from equation (5.4) and the conditions

$$Z_{j}(\theta_{i},\lambda_{i}) = \delta_{ij} , \quad i, j = 1, 2, \dots M, \text{ where } \delta_{ST} = \begin{cases} 1 \ S = T \\ 0 \ S \neq T \end{cases}$$
(5.2)

For numerical evaluation of the constants, the latter method was used, and although involved, it provided a convenient way to introduce a series of checks that would attest to the validity of the coefficients  $A_i^{nm}$  and  $B_i^{nm}$ .

<sup>&</sup>lt;sup>\*</sup>The equations and numbers correspond to those in Lundquist and Giacaglia, this report.

#### 2. METHOD

The procedures had the following steps:

1) Define  $(N + 1)^2$  points on a sphere with spherical coordinates

$$(\theta_k, \lambda_{kj})$$

where

$$\theta_{2i} = \frac{i2 \pi}{2N+1}$$
,  $i = 0, 1, 2, ..., \left[\frac{N}{2}\right]$ ,

with the value of [P/2] representing the greatest integer contained in P/2, and

$$\theta_{2i+1} = \frac{2(N-i)\pi}{2N+1}$$
,  $i = 0, 1, 2, ..., \left[\frac{N-1}{2}\right]$ ;

that is,

$$\theta_i = \frac{i\pi}{2N+1}$$
 , ieven

$$\theta_i = \pi - \frac{i\pi}{2N+1}$$
, iodd

Also,

$$\lambda_{kj} = j \frac{2\pi}{2k+1}$$
,  $k = 0, 1, 2, ..., N$   
 $j = 0, 1, 2, ..., 2k$ 

There are  $(N + 1)^2$  different pairs  $(\theta_k, \lambda_{kj})$ .

.

2) Define the  $(N + 1)^2$  functions  $W_{kj}(\theta, \lambda)$ . The coefficients that are computed are the A's and the B's of the expression

$$\begin{split} W_{kj}(\theta,\lambda) &= \sum_{n=0}^{N} A_{kj}^{no} P_{no}(\theta) + \sum_{n=1}^{N} \sum_{m=1}^{n} (A_{kj}^{nm} \cos m\lambda + B_{kj}^{nm} \sin m\lambda) P_{nm}(\theta) , \quad k = 0, 1, 2, ..., N \\ &= 0, 1, 2, ..., 2k \end{split}$$

where the  $P_{nm}$  are associated Legendre polynomials. The above expression is analogous to equations (5.4) and (6.4).

3) Consider the  $(N + 1)^2$  conditions:

$$W_{kj}(\theta_{i}, \lambda_{i\ell}) = \delta_{ki} \delta_{j\ell} ,$$
  
k = 0, 1, 2, ..., N  
j = 0, 1, 2, ..., 2k  
i = 0, 1, 2, ..., N  
 $\ell = 0, 1, 2, ..., 2i$ .

For any given pair of values (k, j) there are  $(N + 1)^2$  coefficients  $A_{kj}^{nm}$  (n = 0, 1, 2, ..., N; m = 0, 1, 2, ..., n) and  $B_{kj}^{nm}$  (n = 0, 1, 2, ..., N; m = 0, 1, 2, ..., n), since there are

$$A_{kj}^{nm}$$
 :  $\frac{(N+1)(N+2)}{2}$ 

$$B_{kj}^{IIII} : \frac{IN(IN+1)}{2}$$

Total :  $(N + 1)^2$  coefficients

There are also  $(N + 1)^2$  conditions for every pair (k, j), so we can solve equation (2) for every such pair to find all  $(N + 1)^2$  coefficients  $A_{kj}^{nm}$  and  $B_{kj}^{nm}$  for each condition.

## 3. CHECKS

The following series of checks was written into the program:

1) The values

$$\begin{aligned} \mathbf{a}_{kj}^{0}(\theta) &= \sum_{n=0}^{N} \mathbf{A}_{kj}^{no} \mathbf{P}_{no}(\theta) \\ \mathbf{a}_{kj}^{m}(\theta) &= \sum_{n=m}^{N} \mathbf{A}_{kj}^{nm} \mathbf{P}_{nm}(\theta) \\ \mathbf{b}_{jk}^{m}(\theta) &= \sum_{n=m}^{N} \mathbf{B}_{kj}^{nm} \mathbf{P}_{nm}(\theta) \end{aligned}$$

for all  $\theta$  as defined above.

2) The summations

$$\sum_{k=0}^{N} \sum_{j=0}^{2k} A_{kj}^{00} = 1$$

$$\sum_{k=0}^{N} \sum_{j=0}^{2k} A_{kj}^{n0} = 0 , \quad n = 1, 2, ..., N$$

$$\sum_{k=0}^{N} \sum_{j=0}^{2k} A_{kj}^{nm} = 0 , \quad n = 1, 2, ..., N$$

$$\max_{k=0}^{N} \sum_{j=0}^{2k} A_{kj}^{nm} = 0 , \quad m = 1, 2, ..., n$$

$$\sum_{k=0}^{N} \sum_{j=0}^{2k} B_{kj}^{nm} = 0 .$$

3) (a) 
$$a_{kj}^{0}(\theta_{k}) = \frac{1}{2k+1}$$
  
 $a_{kj}^{m}(\theta_{k}) = \frac{2}{2k+1} \cos m\lambda_{kj}$ ,  $m = 1, 2, ..., k$   
 $k = 0, 1, ..., N$   
 $b_{kj}^{m}(\theta_{k}) = \frac{2}{2k+1} \sin m\lambda_{kj}$ ,  $j = 0, 1, ..., 2k$ 

(b) 
$$a_{kj}^{m}(\theta_{k}) = b_{kj}^{m}(\theta_{k}) = 0$$
,  $m = k + 1, ..., N$ .

(c) 
$$a_{kj}^{o}(\theta_s) = 0$$
 ,  $s \neq k$  .

(d) 
$$a_{kj}^{m}(\theta_{s}) = 0$$
 ,  $s > k$  .

(e) 
$$b_{kj}^{m}(\theta_{s}) = 0$$

4) (a) 
$$A_{kj}^{nm} = B_{kj}^{nm} = 0$$
, for  $m > k$ ,  $k = 0, 1, ..., N$ .

(b) For any N, k, 
$$B_{ko}^{nm} = 0$$
 .

(c) 
$$A_{k,2k+1-j}^{nm} = A_{kj}^{nm}$$
,  $j = 1, 2, ..., k$ .

(d) 
$$B_{k,2k+l-j}^{nm} = - B_{kj}^{nm}$$
.

#### 4. OUTPUT

The following printout lists the A and B coefficients of the expression

$$W_{kj}(\theta, \lambda) = \sum_{n=0}^{N} A_{kj}^{no} P_{no}(\theta) + \sum_{n=1}^{N} \sum_{m=1}^{n} (A_{kj}^{nm} \cos m\lambda + B_{kj}^{nm} \sin m\lambda) P_{nm}(\cos \theta) , \quad k = 0, 1, 2, ..., N$$
  
$$j = 0, 1, 2, ..., 2k$$

,

where the  $P_{nm}$  are the Legendre polynomials, for the cases N = 4, 5, and 9. The lengthy series of checks has been omitted to save space.

Each solution consists of the coefficients in the following order (consider N = 4):

$A_{kj}^{00}$	$A_{kj}^{l0}$	A <sup>20</sup> kj	$A_{kj}^{30}$	$A_{kj}^{40}$
$A_{kj}^{ll}$	$A_{kj}^{2l}$	A <sup>31</sup> kj	$A_{kj}^{4l}$	$A_{kj}^{22}$
$A_{kj}^{32}$	$A_{kj}^{42}$	$A_{kj}^{33}$	$A_{kj}^{43}$	$A_{kj}^{44}$
B <sup>ll</sup> kj	B <sup>21</sup> kj	B <sup>31</sup> kj	$B_{kj}^{4l}$	${\rm B}_{kj}^{22}$
B <sup>32</sup> ki	в <mark>42</mark> ki	в <mark>33</mark> ki	B <sup>43</sup> ki	$B_{ki}^{44}$

4	K== 0	J≖ 0			
SOLUTION 2.22222222 0. 0. 0. 0. 0.	22E-02	8.888888889E-02 0. 0. 0. 0.	1.2698412698E-01 n. n. 0.	3.5555555556E-01	4.0634920635E-01 0. 0. 0. 0.
4	K= 1	0 ≖L			
SULUTION 3.45296751 5.00192777 U. 0.	28E-02 98E-02	-9.4769277153E-02 -7.1390413031E-02 0. 0.	1.3171692109E-01 1.3685339714E-01 0. 0. 0.	-1.1851851852E-01 -1.3339194961E-01 	4.7041199453E=02 0. 0. 0. 0.
4	K= 1	J= 1			
SOLUTION 3.45296751 -2.50096388 0. 4.33179652 0.	28E-02 99E-02 52E-02	-9.4769277153E-02 3.5695206515E-02 0. -6.1825911271E-02 0.	1.3171692109E-01 -6.8426698571E-02 0. 1.1851851852E-01 0.	-1.1851851852E-01 6.6695974807E-02 0. -1.1552081703E-01 0.	4.7ñ41199453E-02 0. 0. 0. 0.
4	K= 1	J≖ 2			
SOLUTION 3.45296751 -2.50096388 0. -4.33179652 0.	28E-02 99E-02 52E-02	-9.4769277153E-02 3.5695206515E-02 0. 6.1825911271E-02 0.	1.3171692109E-01 -6.8426698571E-02 0. -1.1851851852E-01 0.	-1.1851851952E-01 6.6695974807E-02 0. 1.1552081703E-01 0.	4.7041199453E-02 0. 0. 0. 0.
4	K= 2	0 ≖ل			
SOLUTION 4.48678621 7.79354251 2.80839711 0.	18E-02 13E-02. 03E-02.	9.4759506055E-02 1.1305177049E-01 2.4586937148E-02 0.	8.4221083205E-02 6.6938346912E-02 0. 0.	-7.111111111E-02 4.2585824342E-02 0. 0.	-1.5273734n27E-01 2.4109420606E-02 0. 0.
4	K≊ 2	Jz 1			
SOLUTION				· · · · · · · · · · · ·	
4.48578621 3.02838904 -2.27204098 8.26552770 1.65073440	18E-02 62E-02 92E-02 93E-02 93E-02	9.4759506055E-02 2.6085177237E-02 -1.9891249992E-02 9.5337999370E-02 1.4451839054E-02	8.4221083205E-02 3.7649789460E-02 0. 8.7012051088E-02 0.	-7.1111111111F-07 -3.3758692188E-03 0. 1.7742207433E-02	-1.5273734627E-01 -1.9504930994E-02 0. 1.4171161873E-02 0.

4	K≡ 2	J= 2			
SOLUTION					
4.48678621	118E-02	9.47595060555-02	8.4221083205E-02	-7.1111111111E-02	-1.5273734027E-01
-6.92516030	019E-02	-8.2611062484E-02	-7.1118962917E-02	-1.7917042952E-02	7.4502206917E-03
8.67842434	403E-03	7.5977814182E=03	0.	0.	
-2.67094431	721E-02	-2.3383566790F=02	0.	0.	0.
					••
4	K= 2	J¤ 3			
C					
SOLUTION A ARETREST	195-02	9 4750504055c-00	9 40010000055-00	-7 1111111111	1 5070704-075 01
-6.92516030	)19E=02	-8.2611062484F=02	-7.1118962917E-02	→1.7917042952E=02	7.4502206917E=03
8.67842434	03E-03	7.5977814182E-03	0.	0.	0.
-4.37946225	555E-02	-6.9325618628E-02	-3.3833207084E-02	-3.0404065747E-02	2,2929421571E=02
2000094431		200000001906-02	0.		0.
4	K= 2	Jer Á			
-		<b>0-</b> 4			
SOLUTION					
4.48678621	18E-02	9.4759506055E=02	8.4221083205E=02	=7,1111111111E=02	-1.5273734027E-01
-2.27204098	392E=02	~1.9891249992F=02	0.	0.	0.
-8.2655277(	32E-02	-9.5337999370E-02	-8.7012061088E-02	-1.7742207433E-02	-1.4171161873E-02
-1.65073440	40E-02	-1.4451839054E-02	0.	9.	0.
,	~ ~				
4	K# 3	J≊ ()			
SOLUTION					
4.14314117	35E-02	-6.1571776113E-02	-2.9634106092E-02	1.1192913572E-01	-6.2154665253E-02
1.01102136	041E=01	-8.16^2427314E-02	-2.4266639431E-02	7.3925537240E-02	4.7268100759E-02
0.		0.	0.	0.	0.
υ.		0.	0.	<u>ो</u> •	0.
4	K= 3	J≊ 1			
SOLUTION					
4.71590931	13E-02	-7.7291826243E-02	-7.7852889994E-03	9.2269630994E-02	-5.4351608864E-02
7.15.60983	337E-02	-6,2967081103E-02	8.0438842919E-03	2.35040716398-02	-1.4719261378E-02
9.26194111	145-02	-8,3173771284F=02	1.8167799748E=02	2.1596481539E=02	3.7359276356E-02
-3.04103441	74E-02	5.5547909388E-03	3.2798899070E-03	-2.6983047406E-03	0.
		. –			
4	K⊒ 3	J≊ 2			
SULUTION					
4.25658492	78E-02	-6.4685324835E-02	-2.5306679909E-02	1.0803532970E-01	-6.0609174237E-02
-1.86514072	63E=02	1.2669107580F=02	1.5922362432E=02	-2.0700359354F-02	-3.3147257509E-02
		-3 7393,300,70-07	4.71210324405=02	#3 877456077AE-00	۸.
1.05097677	125E-02	-3.7282022987E-03 -8.8877024864F=02	4.7131932448E-03 -5.7910117838E-03	-3.8774568770E-03 5.4656774648E-02	0. -1.2986847301E-02

ŧ

4 K=	3 عدل 3			
SOLUTION 4.5114907297E- -1.0340575928E- -1.9051728117E- 4.0505456591E- 1.4845205588E-	02 -7.1681405309E-02 01 9.1099187180E-02 02 3.8994769988E-03 02 -3.0608786119E-02 02 -1.2808417898E-02	-1.5583041538E-02 -1.1832927009E-02 -1.6821191936E-03 -1.9724958580E-02 7.3698457234E-03	9.9286026997E-02 -3.3760480906E-02 1.3838483374E-03 4.1038549961E-02 -6.0630357168E-03	-5.7136487446E-02 2.4232468508E-02 0. -3.8151390722E-02 0.
4 K≖ SQLUTION	4 ≖ل 3			
4.5114907297E- -1.0340575928E- -1.9051728117E- -4.0505456591E- -1.4845205588E-	02 -7.1681405309E-02 01 9.1099187180E-02 02 3.8994769987E-03 02 3.0608786119E-02 02 1.2808417898E-02	-1.5583041538E-02 -1.1832927009E-02 -1.6821191936E-03 1.9724958580E-02 -7.3698457234E-03	9.9286026996E-02 -3.3760480906E-02 1.3838483373E-03 -4.1038549961E-02 6.0630357168E-03	-5.7136487446E-02 2.4232468508E-02 0. 3.8151390722E-02 0.
4 K=	5 =دل (			
SULUTION 4.2565849278E- -1.8651407263E- 2.9708443325E- -1.0509767747E- -1.7780464528E-	02 -6.4685324835E-02 02 1.2669107580E-02 02 -3.7282022987E-03 01 8.8877024864E-02 02 -1.2456857579E-03	-2.5306679909E-02 1.5922362432E-02 4.7131932448E-03 5.7910117838E-03 5.9101573927E-03	1.0803532970E-01 -2.6706359354E-02 -3.8774568770E-03 -5.4656774648E-02 -4.8621771348E-03	-6.0609174237E-02 -3.3147257509E-02 0. 1.298ñ847301E-02 0.
4 K≖	3 J <b>≖ 6</b>			
SOLUTION 4.7159093113E- 7.1506098337E- -2.7210909645E- -9.2619411114E- 3.0410344174E-	02 -7.7291826243E-02 02 -6.2967081103E-02 04 -7.5827402117E-03 02 8.3173771284E-02 02 -5.5547909388E-03	-7.7852889994E-03 8.0438842919E-03 -6.8107615702E-03 -1.8167799748E-02 -3.2798899070E-03	9.226963-994E-02 2.3504071639E-02 5.6030875284E-03 -2.1596481539E-02 2.6983047406E-03	-5.4351608864E-02 -1.4719261378E-02 0. -3.7359276356E-02 0.
4 K=	4 J≖ 0			
SULUTION 3.9658424590E- i.1176377803E- -1.3249928178E- U. U.	02 1.78162622815-02 01 1.5719524186E-02 03 -2.1012086924E-02 0. 0.	-8.2948316862E-02 -3.8002050498E-02 7.9966656246E-03 0.	-4.6476734641£-02 -4.7317582602F-02 5.1819641623E-03 0. 4.	7.1943364633E-02 3.6685180938E-02 2.2500509444E-03 0. 0.
4 K=	4 ا⊯دا			
SOLUTION 3.6005971115E- 9.4990165331E- 8.9978398907E- 7.3758413659E- 5.962640814E-	02 2.7868139894E=02 02 3.7251754488E=02 03 4.4301450956E=03 02 2.9638032419E=02 02 =55930147632E=03	-9.6919114257E-02 -2.8651973775E-02 -2.452346396E-03 -3.3706247530E-02 1.1172894162E-02	-3,3905850081E-02 -1,8149147798E-02 -4,3628412371E-03 -1,0663374212E-02 1,8593334982E-03	6.695A853328E-02 1.4189077473E-02 -2.1143562688E-03 5.0343554715E-02 7.6956274649E-04

4	K≘ 4,	J∞ 2			
SOLUTION 3.83964676 9.3773724 -8.0627433 1.05118133 -1.42167919	847E-02 179E-03 498E-03 390E-01 911E-03	2.1307242740E-02 3.6484158208E-03 1.1596090537E-02 3.0277081911E-02 -8.0344630852E-03	-8.7800323879E-02 -2.5303385336E-02 -8.4498398580E-03 -5.6006789628E-02 -1.2230415091E-02	-4.2110912250E-02 3.5737733211E-03 5.7119040176E-04 -2.4767977552E-02 -9.8933079664E-04	7.0207525542E-02 -4.1899528132E-02 1.7236390227E-03 1.1516420307E-02 -1.4463048682E-03
4	K= 4	J≖ 3			
SOLUTION 3.7566257( -5.3466674) -1.15679180 1.08827774 -1.1724785	044E-02 222E-02 582E-02 454E-01 751E-02	2.3585818409E-02 -1.1306896664E-02 -2.0143255791E-04 3.5602915005E-02 6.9276002764E-03	-9.0967246542E-02 2.5609084460E-02 1.3270777924E-02 -2.5525260374E-02 3.0450101556E-03	-3.9261324063E-02 1.721787^434E-02 1.8430495577E-03 -2.9344914810E-02 -2.5050735150E-03	6.9076495152E-02 -2.8542110659E-02 -1.1250254722E-03 -4.2301214896E-02 1.9486012777E-03
4	K <b>≃</b> 4	J= 4			
SOLUTION 3.7566257( -1.06772752 1.12953185 3.55429945 3.81936033	044E-02 254E-01 350E-02 378E-02 300E-03	2.3585818409E-02 -3.7453035737E-02 -5.3187596133E-03 -5.3315627259E-03 1.6104444165E-02	-9.0967246542E-02 4.7347299900E-02 -6.36693n2384E-03 -1.0855047805E-02 6.5076679438E-03	-3.9261324063E-02 2.1016295344E-02 -1.1423808035E-03 -2.5260605530E-02 5.6973289898E-03	6.9076495152E-02 3.8210970649E-02 3.9071724615E-04 -2.0647431985E-02 -2.2158676147E-03
4	K= 4	5 ≈ ل			
SOLUTION 3.7566257( -1.06772752 1.12953185 -3.55429945 -3.81936035	044E-02 254E-01 550E-02 978E-02 300E-03	2.3585818409E-02 -3.7453035737E-02 -5.3187596133E-03 5.3315627259E-03 -1.6104444165E-02	-9.0967246542E-02 4.7347299900E-02 -6.36693c2384E-03 1.0855047805E-02 -6.5076679439E-03	-3.9261324063E-02 2.1016295344E-02 -1.1423808035E-03 2.5260605530E-02 -5.6973289898E-03	6.9076495152E-02 3.8210970649E-02 3.9071724615E-04 2.0647431985E-02 2.2158676147E-03
4	K= 4	J≖ 6			
SOLUTION 3.7566257( -5.34666742 -1.15679186 -1.08827774 1.17247857	044E-02 222E-02 082E-02 054E-01 751E-02	2.3585818409E-02 -1.1306896664E-02 -2.0143255790E-04 -3.5602915005E-02 -6.9276002764E-03	-9.0967246542E-02 2.5609084460E-02 1.3270777924E-02 2.5525260374E-02 -3.0450101556E-03	-3.9261324063E-02 1.7217870434E-02 1.8430495577E-03 2.9344914810E-02 2.5050735150E-03	6.9076495152E-02 -2.8542110659E-02 -1.1250254722E-03 4.2301214896E-02 -1.9486012777E-03
4	K= 4	J= 7			
SOLUTION 3.83964678 9.37737243 -8.06274334 -1.05118133 1.42167919	847E-02 181E-03 498E-03 390E-01 911E-03	2.1307242740E-02 3.6484158208E-03 1.1596090537E-02 -3.0277081910E-02 8.0344630852E-03	-8.7800323879E-02 -2.5303385336E-02 -8.4498398581E-03 5.6006789628E-02 1.2230415091E-02	-4.2110912250E-02 3.573773321E-03 5.7119040176E-04 2.4767977552E-02 9.8933079664E-04	7.0207525542E-02 -4.1899528132E-02 1.7236390227E-03 -1.1516420307E-02 1.4463048682E-03
4	К= 4	J≊ 8			
SOLUTION 3.6005971: 9.49801653 8.99783989 -7.37584136 =1.59426608	115E-02 331E-02 907E-03 559E-02 314E-02	2.7868139893E-02 3.7251754488E-02 4.4301450956E-03 -2.9638032419E-02 5.5930147632E-03	-9.6919114257E-02 -2.8651973775E-02 -2.4523416396E-03 3.3706247530E-02 -1.1172894162E-02	-3.3905850081E-02 -1.8149147798E-02 -4.3628412371E-03 1.0663374212E-02 -1.8593336982E-03	6.6950853328E-02 1.4188077673E-02 -2.1143562688E-03 -5.0343554715E-02 -7.6956274649E-04

END OF RUN

	5	K≡ 0	J= 0			
501	UTION i.81818181818 3.694083694 0. 0. 0. 0. 0. 0.	2E-02 1E-01	4.6753246753E-02 0. 0. 0. 0. 0.	1.03P9610390F-01 0. 0. 0. 0. 0.	1.292929292929 0. 0. 0. 0. 0.	3.3246753247F-01 0. 0. 0. 0. 0.
	5	K= 1	J= 0			
501 -	UTION 2.325912988 3.504819489 9.750621996 0. 0. 0. 0. 0.	2E-02 9E-02 0E-02	-6.6211617220E-02 2.4800491962E-02 0. 0. 0. 0.	9.7595721277E-02 -4.5373084710E-02 0. 0. 0. 0. 0.	-1.1166970859F-01 5.5054105048F-02 0. 0. 0. 0.	9.20746695495-02 -1.00807701655-01 0. 0. 0. 0.
	5	K= ]	J= 1			
<b>ເ</b>	UTION 2.3259129AA -3.504819489 -4.875310998 0. A.444286351 0. 0.	2E - 02 9E - 02 0E - 02 3E - 02	-6.6211617220E-02 -1.2400245981E-02 0. 2.1477856066E-02 0. 0.	9.7595721277F-02 2.2686542355E-02 0. 0. -3.9294244006E-02 0.	-1.1166970859F-01 -2.7527052524F-02 0. 0. 4.7678253554E-02 0. 0.	9.2074669548F-02 5.0403850825F-02 0. 0. -8.7302030526F-02 0. 0.
	5	K= 1	J= 2			
501	UTION 2.3259129AA -3.5048194A9 -4.87531099A 0. 0. -P.444286351 0. 0.	3E-05	-4.6211617220E-02 -1.2400245981E-02 0. -2.1477856066E-02 0. 0.	9.7595721277E-02 2.2686542355E-02 0. 3.9294244006E-02 0. 0.	-1.1166970859F-01 -2.7527052524F-02 0. 0. -4.7678253554F-02 0.	9.2074669548E-02 5.0403850825E-02 0. 8.7302030526E-02 0.
	5	K= 2	J= 0			
501	_UTION 2.946805172 -1.417778939 2.532934502 0. 0. 0. 0. 0.	98E=02 94E=01 97E=02	7.7360935316E-02 5.0880111607F-02 1.1517793018E-02 0. 0. 0. 0.	7.6569323315E-02 6.3230300451E-02 1.3885236781E-02 0. 0. 0.	4.5467556507E-02 7.4400415412F-02 1.5880340911F-02 0. 0. 0.	-R.7087972930F-02 4.1291181189F-02 1.3865882272E-02 0. 0. 0. 0.

5	K= 2	J= 1			
SOLUTION					
2.946805177 -1.417778939 -1.874482296 0. 0. 1.073642115 0.	98E-02 94F-01 93E-03 97E-02	7.7360935316E-02 1.3255218162E-02 -9.3180902891E-03 0. 4.4993500289E-02 6.7699888748E-03 0.	7.6569323315E-02 2.4053771602E-02 -1.1233392527E-02 0. 6.6349312529E-02 8.1615374047E-03 0.	4.5467556507F-02 1.7513215741E-02 -1.2847465673E-02 0. 6.3219486652E-02 9.3342301888E-03 0.	-8.7087972930E-02 2.2786757946E-02 -1.1217734400E-02 0. 5.3066082960F-02 8.1501611097E-03 0.
0.5		,			
5	K= 2	J= 2			
SOLUTION					
2.94680517; -1.417778939 -1.079019021 0.	98E-02 94E-01 17E-02	7.7360935316E-02 -3.8695273965E-02 3.5591937802E-03 0. 3.0708351405E-02	7.6569323315E-02 -5.5668921828F-02 4.2907741364E-03 0. 3.5698977021F-02	4.5467556507F-02 -5.4713423447E-02 4.9072952180F-03 0. 4.5511304586F-02	-8.7087972930E-02 -4.3427348541E-02 4.2847932642E-03 0. 2.1005469252E-02
1.8ŋ4n48240 0. 0.	94E-02	-1.0954072103F-02 0.	-1.3205644921F-02 0.	-1.5103101704F-02 0.	-1.3187237689E-02 0.
5	к= 2	J= 3			
SOLUTION					
2.946805)7; -1.417778930 -1.079019021	AE-02 4E-01 7E-02	7.7360935316E-02 -3.8695273965E-02 3.5591937802E-03 0.	7.6569323315E-02 -5.5668921828E-02 4.2907741364E-03	4.5467556507F-02 -5.4713423447F-02 4.9072952180F-03	-8.7087972930E-02 -4.3427348541E-02 4.2847932642E-03 0.
0. -1.Rn404R240 C. ^.	94F-02	-3.0708351405E-02 1.0954072103E-02 0.	-3.5698977021E-02 1.3205644921E-02 0.	-4.5511304586E-02 1.5103101704F-02 0.	-2.1005469252E-02 1.3187237689E-02 0.
5	K= 2	J= 4			
SOLUTION		<b>-</b> .			
2.946805177 -1.417778934 -1.874482296	98E-02 94E-01 53E-03	7./360935316E-02 1.3255218162E-02 -9.3180902891E-03 0.	7.6569323315E-02 2.4053771602E-02 -1.1233392527E-02 0.	4.5467556507F-02 1.7513215741F-02 -1.2847465673E-02 0.	-8.7087972930E-02 2.2786757946E-02 -1.1217734400E-02 0.
0. -1.07364211; 0. 0.	¤7E−02	-4.4993500289E-02 -6.7699888748E-03 0.	-6.6349312529E-02 -8.1615374047E-03 0.	-6.3219486652F-02 -9.3342301889E-03 0.	-5.3066082960F-02 -8.1501611097E-03 0.
5	K= 3	0 ≃ل			
SOLUTION					
2.964590333 4.703263926 -5.445151256 4.182249645 0. 0.	80E-02 84E-02 58E-03	-5.7300680684E-02 6.5903627115E-02 1.9939219183E-02 -3.1383578078E-03 0.	1.9242794156E-02 -6.6666503382E-02 -2.3250305814E-02 2.5536887586E-03 0.	A.0896270473E-02 3.7697498020F-02 9.7667601404F-03 0. 0.	-9.9516926560E-02 2.9972960200E-02 -6.6383517166E-03 0. 0.
υ Γ		U7 🙍	v• 59	<b>●</b>	57 <b>Q</b>

5	Ka 3	1 سال			
SOLUTION 3.36671524 4.09731897 -1.91972697 -3.76807672 0. -1.68192069 1.81461011 0.	92E-02 22E-02 89E-02 87E-03 78E-02 42E-03	-6.8747945118E-02 4.4842554332E-02 -2.8767249362E-03 2.8275626812E-03 5.8075672879E-02 2.2679025096E-02 -1.3616824203E-03	3.6116026922E-02 -4.8430833590E-02 7.0545359600E-03 -2.3007940698E-03 -6.4105611092E-02 -1.8761733971E-02 1.1080040271E-03	4.1589799235E-02 3.1833692744E-02 -2.2201044325E-05 0. 4.4013617935E-02 1.3988707914E-02 0.	-8.3598223253E-02 3.4356277797E-03 3.3554067105E-03 0. -3.1908614800E-03 -2.5717202801E-03 0.
5	K= 3	5 = L			
SOLUTION					
3.04423610 4.58324909 2.03635744 2.60759000 0. -4.22970611 -3.26981444	044E-02 084E-02 078E-02 030E-03 025E-02 06E-03	-5.9567951797E-02 -1.2567337254E-02 -2.1470283068E-02 -1.9567340878E-03 6.69955045660E-02 -1.1446979383E-02 2.4536669374E-03	2.2584744842E-02 1.0997085039E-02 1.6721556199E-02 1.5921988981E-03 -7.0015648257E-02 6.7176112942E-03 -1.9965542679E-03	5.7072387066E-02 -3.7320644398E-03 -1.3633041603E-02 0. 4.2844178627E-02 -R.0922218683E-03 0.	-9.6364032140E-02 -1.5195819976E-02 1.7605936484E-03 0. 1.8066922295E-02 -4.8534760677E-04 0.
5	K= 3	3 ≊ئ			
SOLUTION					
3.22319852 4.31357822 2.60594515 -9.30638097 0. -2.95442356 4.07739191 0.	083E-02 133E-02 195E-02 195E-02 192E-04 106E-02 154E-03	-6.4662463743E-02 -6.5227030636E-02 1.437739A413E-02 6.9835031048E-04 2.7089126824E-02 -1.5145061934E-02 -3.0596726252E-03	3.0094039870E-02 7.0767000243E-02 -1.2150939252E-02 -5.6824920760E-04 -2.6171373811E-02 1.8713140868E-02 2.4896624498E-03	4.8480199043E-02 -4.6950377314E-02 R.7718625773E-03 0. 1.30145572R1F-02 -7.0237231779E-03 0.	-8.9279542685E-02 -3.2262879039E-03 -1.7968245006E-03 0. 1.9123789112E-02 5.7246459918E-03 0.
5	K= 3	Jz 4			
SOLUTION		•			
3.22319852 4.31357822 2.60594515 -9.30638097 0. 2.95442356 -4.07739191 0.	83E-02 33E-02 95E-02 22E-04 06E-02 54E-03	-6.4662463743E-02 -6.5227030636E-02 1.4377398413E-02 6.9835031048E-04 -2.7089126824E-02 1.5145061934E-02 3.0596726252E-03	3.0094039870E-02 7.0767000243E-02 -1.2150939252E-02 -5.6824920760E-04 2.6171373811E-02 -1.8713140868E-02 -2.4896624498E-03	4.8480199043E-02 -4.6950377314E-02 8.7718625773E-03 0. -1.3014557281F-02 7.0237231779E-03 0.	-8,9279542685E-02 -3,2262879039E-03 -1,7968245006E-03 0, -1,9123789112E-02 -5,7246459918E-03 0,
5	K= 3	J= 5			
SOLUTION	2				
3.04423610 4.58324909 2.03635744 2.60759000 0. 4.22970611 3.26981444 0.	044E-02 084E-02 030E-02 030E-03 25E-02 06E-03	-5.9567951797E-02 -1.2567337254E-02 -2.1470283068E-02 -1.9567347878E-03 -6.995504560E-02 1.1446979383E-02 -2.4536669374E-03	2.2584744842E-02 1.0997085039E-02 1.6721556199E-02 1.5921988981E-03 7.0015648257E-02 -6.7176112942E-03 1.9965542679E-03	5.7072387066E-02 -3.7320644398E-03 -1.3633041603E-02 0. -4.2844178627E-02 R.0922218683E-03 0.	-9.6364032140E-02 -1.5195819976E-02 1.7605936484E-03 0. -1.8066922295E-02 4.8534760677E-04 0.

SOLUTION 3.3667152492E-02 4.0973184722E-02 -1.9197269789E-02 -3.7680767286F-03 0. 1.6819206978E-02 -J.8146101142E-03 0.	-6.8747945118E-02 4.4842554332E-02 -2.8767240362E-03 2.8275426812E-03 -5.8075472679F-02 -2.2679025096E-02 1.3616824203E-03	3.6116026922E-02 -4.8430833590F-02 7.0545359600E-03 -2.3007940698E-03 6.4105611092E-02 1.8761733971E-02 -1.1080040271E-03	4.1589799235E-02 3.1833692744E-02 -2.2201044319E-05 0. -4.4013617935E-02 -1.3988707914E-02 0.	-9.3598223253E-02 3.4356277797E-03 3.3554067105E-03 0. 3.1908614800E-03 2.5717202901E-03 0.
5, K= 4	J= 0			
SOLUTION				
7.8492463533E-02 7.0434244601E-02 -2.7933858360E-02 P.1613282951E-03 0. 0. 0.	3.7786966201E-02 7.1284633390E-02 2.5734472462E-02 2.6863731112E-03 0. 0.	-3.4726926112E-02 5.1515316782E-02 1.2256627665F-02 1.9165359276E-03 0. 0.	-A.7859849894F-02 -1.7471389600F-02 -4.7590971718F-03 7.8879031535E-04 0. 0.	-).4126998329F-02 -3.4287474634F-02 -1.3638206598F-02 6.1584139388F-04 0. 0.
5 K= 4	J= 1			
SOLUTION				
3.0178090858E-02 6.7894244382E-02	3.2988501607E-02 6.6455366849E-02	-2.7653903977F-02 5.0385040708E-02	-9.5952736993F-02 4.8789327622F-03	-7.4541958764E-03 -2.2687216017E-02
-1.1250770756E-02	7.5717519606E-03	5.8691616117E-03	3.4519128493F-03	1.7146528894E-03
-4•/009495[49E=03 0•	5.3929977019E-02	3.7098388184E-02	2,1296732420F-03	-2.5129858167E-02
-7.1092213865E-03 5.3472127274E-03 0.	3.1976688675E-02 3.6176833617E-03	2.0067030689F-02 6.0910336770E-04	4.4588079087F-03 2.6978217671F-04	-3.4759337532E-03 2.1063016180E-04
5 K= 4	.J= 2			
SOLUTION				
2•8949205980E-02 4•9745998808E-02	3•648676n379E-02 1•0814919386E+02	-3.2810326707F-02 4.8470232958E-04	-9.0052721950F=02 -3.7129005869F=03	-1.7567143890F-02
1.6557889977E-03	-2.6974626619E-02	-1.4883508851F-02	6.2239091530F-04	7.5749824838F-03
0.	7.5137020063E-02	4.8239708772E-02	-7.8619103207F-03	-4.3453423282F-02
-1.5411087622E-02 -4.9188083052E-03 0.	7.8375539612E-03 -3.9391578019F-03	3⊾0296809284E-03 -3₊4751889768E-04	-2.9570498071F-03 -5.0702464135F-04	-5.1412135460F-03 -3.9585521752E-04
5 K= 4	J= 3			
SOLUTION				
2.9573126758E-02	3.4710649065E-02	-3.0192344063E=02	-9.3048236048F-02	-9.8490348002E-03
1.0224188269E-02	-1.7835070265E-02	-1.2117269507F-02	-4.4699318597F-03	-1.6150442321F-04
6.0247719679E-03	4.2896437906E-03 7.2850794797E-02	6.1195089438F=04 5.7377098826E=02	-3.9439515768F=04 1.3838788684E=03	-7,0792069694F-04 -2,2343077797E-02
-1.7482373247E=02	=2.0511415369E=02	-1,57n7634056F-02	-1.7033851578F-03	4,9929986388E-03
-1•23354(5/0/2≈03 0•	7∎6304#/3030 <u>6</u> ≣04		080911C401996804	2 <b>4.7.3 7.3 97 7 1 1 1 1 1 1 1 1</b> 1 <b>1</b> 1 1 1 1

K= 3

J= 6

5 K≖	4 J≊	4			
SOLUTION					
2.9375993219E-(	3.5271827	858E-02 -3.	1019519886E-02	-9.2101775671F-02	-1.0629416764E-02
6.9102891244E~(		3402-02 -5.	2611372448E-02	9.4719969209E-04	3.6384892817E-02
-3.1211392967E-0	)2 2++370708 )3 =2+0632134	699F=03 =3.	5003302914E=02 7238040522F=04	2.7751766810F=03	-3,3090276509E=03
0.	1.9558203	604E-02 1.	4157911215E-02	-1.3651808525E-02	-1.1621451519E-02
-1.4784483653E-0	-1.5534593	763E-02 -6.	6641742474E-03	4.4477904214E-03	8.6934366424E-03
7.2371077521E-(	03 2.1995071	865E-03 1.	7630764894E-03	-7.7680681806E-04	-6.0648537932E-04
0.•					
5 K=	∎ل 4	5			
SOLUTION					
2.9375993219E-0	02 3.5271827	858E-02 -3.	1019519886E-02	-9.2101775671E-02	-1.0629416764E-02
6.9102891244E-0		340E-02 -5.	2611372448E-02	9.4719969206E-04	3.6384892817E-02
-3.1211392967F-	02 2.0632134 03 -2.0632134	699E=03 =3.	7238040522E=04	1.3697200082F=04	1.0693973578F=04
0.	-1.9558203	604E-02 -1.	4157911215E-02	1.3651808525E-02	1.1621451519E-02
1.4784483653E-		763E-02 6.	6641742474E-03	-4.4477904214E-03	-8.6934366424E-03
-/+23/10//5218-0	UJ -2.1995071	005t=03 =1.	1030104894E=03	/•/080081805E=04	0,0040537932E=04
5 K=	∎ل 4	6			
SOLUTION					
2.9573126758E-0	02 3.4710649	065E-02 -3.	0192344063E-02	-9.3048236048E-02	-9.8490348002E-03
6.8805839088E-0	02 -3.6594274	590E-02 -2.	4016028980E-02	6.6224629327E-03	2.1013204406E-02
1.0224188269E-0	02 •1•/835070 Na 4,2004/37	265E=02 -1.	2117269507E-02	-4.4699318597E-03	-1.6150442320E-04
0+12411170195**	-7.2850794	797E-02 -5.	7377098826E=02	-1,3838788684E-03	2.2343077797E=02
1.7482373247E-0	02 2.6511415	369E-02 1.	5707634056E-02	1.7033851578E-03	-4.9929986388E-03
1.2335413707E-0	03 -9.2564875	838E-04 7.	5320246239E-04	-6.8311245135E-04	-5.33334291806-04
U •					
		_			
5 K=	4 ਹੋਬ	: 7			
SOLUTION					
2.8949205980E-	02 3.6486760	379E-02 -3.	2810326707E-02	-9.0052721950E-02	-1.2318916509E-02
6 . 9745998808E-	02 1.0814919	386E-02 4.	8470232964E-04	-3.7129005869F-03	-1.7567143890F-02
1.655/889977E=	03 -2.6974626	017E-02 -14	4083508851L=02	6.0424843784F-04	1.5/49824838E=03 4.7176187763E=04
-2+211341303954	-7.5137020	)063E=02 =4	8239708772E-02	7.8619103207E=03	4.3453423282E=02
1.5411087622E-	02 -7.8375539	613E-03 -3	0296809284E-03	2.9570498071E-03	5.1412135460E-03
4.9188083052E-	03 3.9391578	3018E-03 3	4751889768E-04	5.0702464135E-04	3.9585521752E-04
(j e					
5 K≆	∎ل 4	8			
SOLUTION					
3.0178090858E=	02 3.2988501	607E-02 -2	7653903977E-02	-9,5952736993F-02	-7.4541958764E-03
-1.1250770756F=	02 7.5717519	1606F=03 5.	8691616117F=02	3.4519128493E=03	1.7146528894F=03
-4.7069495149E-	03 -8.7322236	431E-04 -1.	3406788260E-03	-7.4122043868E-04	-5.7870161341E-04
0.	-5.3929977	019E-02 -3.	7098388184E-02	-2.1296732420F-03	2.5129858167E-02
7.1092213865E-	03 -3.1976688	675E-02 -24	00670306898-02	-4.4588079087F-03	3.4759337533E=03
0+ 	00 -000110833	0011C-03 -001	0.10201105-00	LENSINETIDITE MA	.v010000101006#06

5	K= 5	.)= 0			
SOLUTION 2.563842 -4.0268993 3.180617 4.536840 2.024982 0. 0. 0.	4443E-02 3390E-02 2426E-02 26]1E-03 2225E-04	-1.8089729640E-02 8.3255068275E-02 3.1038736351F-02 3.8002026471E-04 0. 0.	-5.9760801658F-02 -1.7343138543E-02 1.1639968812F-03 -2.9142912990E-03 0. 0.	3.1078079893F-02 -2.8667003953F-02 -5.1857528761F-03 9.2061250806F-04 0. 0.	6.1403020352E-02 1.0956503985E-02 8.7731808486E-03 -6.8964561143E-04 0. 0.
5	<b>K</b> = 5	J= 1			
SOLUTION 2.549080 -4.847897 1.540557 8.681740 -1.942956 7.023815 8.061311 5.705034	1385E-02 5337E-02 2149E-02 8379E-04 2142E-04 5423E-03 1690E-03 1911E-05	-3.7056877871E-03 5.9851160796E-02 1.5283510513E-02 -1.1900625428E-03 3.9890059871E-02 2.8349998831E-02 -2.3032611173E-03	-6.4457218810E-02 -2.1631544138E-02 -7.3715516476E-03 1.3390963749E-03 -8.9205194736F-03 -8.103751416E-03 -7.0438340888F-04	4.7976184174F-02 -4.0398584712F-02 -2.8836654686E-03 -4.7400898228F-04 -2.4668656940F-02 -8.0438224544F-03 1.1346229929F-03	4.3174897376E-02 9.8693362490E-03 -4.3557023490F-04 5.5223131404E-04 1.2592820805F-02 2.0921328636E-03 -1.7855494570F-04
5	K= 5	J= 2			
SOLUTION 2 · 394108 - 3 · 839448 6 · 095195 - 7 · 1469604 1 · 7 03523 1 · 315145 - 3 · 287423 - 1 · 094788	3643E-02 7950E-02 3998E-03 3125E-03 4486E-04 9417E-02 5234E-03 0441E-04	-1.2126655998E-02 3.3250215881E-02 -2.5281692667E-02 1.7319100745E-03 6.7607347082E-02 2.1589901080E-02 1.4006745132E-03	-6.7213167080E-02 -3.0904297107F-03 4.945722742E-03 1.0902853077F-03 -1.5380046367F-02 -3.0514537790F-03 -4.0579952290E-04	4.0538769510F-02 -1.5284829018F-02 9.4207967722F-04 -5.4708097392F-04 -4.0552212066F-02 -7.1237057907E-03 -1.5586504604F-03	5.3254457874F-02 1.2631458097E-02 -4.1410772765E-03 -2.2669177941E-04 2.0032876706F-02 3.2935630627E-03 1.7716731193E-04
5	ĸ= 5	J= 3			
SOLUTION 2.676427 -4.908697 -9.447710 1.963096 -1.326081 2.258904 -6.039436 1.530379	6896E - 02 6229E - 02 0649E - 03 7436E - 03 3445E - 04 0495E - 02 7172E - 03 4528E - 04	-9.5017628651E-03 -1.3243385138E-02 -2.6439441884E-02 9.9015906096E-05 7.7362874971E-02 -4.1530303107E-03 1.0895216206E-03	-5.8479864723E-02 4.5163735655E-03 5.2907851425E-03 -1.1627538047F-03 -1.7725892158E-02 1.5061352219E-03 1.4831069907F-03	3.9345210048F-02 1.1073747997F-03 1.0475132926E-02 1.4073472697E-03 -3.7160113133F-02 6.4043803352F-03 1.0461132531F-03	5.0959116873E-02 3.3110803569E-03 -2.8530916294F-03 -8.605205809F-05 1.5814523893F-02 6.5753247444F-04 5.5302299880E-05
5	κ= 5	J= 4			
SOLUTION 2 • 438558 • 4 • 089683 • 1 • 223555 7 • 267448 P • 4120P0 1 • 768056 4 • 987997 - 1 • 841988	9976E-02 7805E-02 0238E-02 1590E-03 1631E-05 1524E-02 8035E-03 6196E-04	-1.0357404678F=02 -4.9634673599E=02 -5.1409072046E=03 -2.2697964625E=03 5.5026807254E=02 -3.4832557137E=02 -1.6969557840E=03	-6.6234024833E-02 1.1916956056E-02 3.3169405538F-03 -3.4458417347F-04 -2.0744232158F-02 8.7250198115F-03 -2.7589359750E-05	4.1922926260F-02 2.7276527620F-02 1.3726426874E-03 -1.4649279058E-03 -3.3742615356F-02 5.0258783485E-03 -6.2443519630F-06	5.1179751081E-02 -1.1959418743F-02 7.0229855775E-04 2.0762560807F-04 5.3234604725E-03 -4.0205838076F-03 -4.0166906887F-04

5	K= 5	J= 5			
SOLUTION 2.54622035 -4.49192609 -1.57205934 -5.22017830 -2.88185017 1.54561493 2.98282384 2.00437082	79E-02 ñ0E-02 59E-02 44E-03 51E-05 52E-02 00E-03 33E-04	-9.4476806980E-03 -7.1850852077E-02 2.6059163068E-02 1.4389228923E-03 2.8032681806E-02 -1.6081147001E-02 6.2179668892E-04	-6.2876966899E-02 1.6960213499E-02 -6.7638947636E-03 5.3510194504E-04 -2.9709039929E-03 -3.2932059732E-03 -2.4747363572E-03	4.1361952057E-02 4.1633013287E-02 -7.3133133838F-03 6.1836433826E-04 -4.5323703292F-04 2.4536427995E-03 -8.0349725563F-04	5.0419752860E-02 -1.9330707951E-02 2.3408501587E-03 -1.0229027867E-04 8.1241323801E-04 -6.1736138072E-03 6.5380751174E-04
5	K≖ 5	J≖ 6			
SOLUTION		,			
2 • 54622035 - 4 • 49192609 - 1 • 57205934 - 5 • 22017830 - 7 • 88185017 - 1 • 54561493 - 2 • 98282386 - 2 • 00437082	79E-02 79E-02 59E-02 44E-03 51E-05 70E-02 00E-03 33E-04	-9.4476806981E-03 -7.1850852077E-02 2.6059163067E-02 1.4389228923E-03 -2.8032681806E-02 1.6081147001E-02 -6.2179668892E-04	-6.2876966898F-02 1.6960213499E-02 -6.7638947636F-03 5.3510194503F-04 2.9709039929E-03 3.2932059732E-03 2.4747363572E-03	4.1361952057F-02 4.1633013287E-02 -7.3133133838F-03 6.1836433826F-04 4.5323703293E-04 -2.4536427996E-03 8.0349725563E-04	5.0419752860E-02 -1.9330707951E-02 2.3408501587E-03 -1.0229027867E-04 -8.1241323802E-04 6.1736138072E-03 -6.5380751174E-04
5	K= 5	J <b>≖ 7</b>			
SOLUTION					
2 • 43855899 -4 • 08968378 -1 • 22355502 7 • 26744815 8 • 41208016 -1 • 76805615 -4 • 98799780 1 • 84198861	76E-02 05E-02 38E-02 90E-03 31E-05 24E-02 35E-03 97E-04	-1.0357404678E-02 -4.9634673599E-02 -5.1409072046E-03 -2.2697964625E-03 -5.5026807254E-02 3.4832557137E-02 1.6969557840E-03	-6.6234024833E-02 1.1916956056F-02 3.3169405538F-03 -3.4458417347E-04 2.0744232158F-02 -8.7250198115E-03 2.7589359750E-05	4.1922926260F-02 2.7276527620E-02 1.3726426874E-03 -1.4649279058E-03 3.3742615356E-02 -5.0258783485E-03 6.2443519608E-06	5.1179751081E-02 -1.1959418743E-02 7.0229855774E-04 2.0762560807E-04 -5.3234604725E-03 4.020583R076E-03 4.0166906887E-04
5	K≖ 5	8 zJ			
COLUTION					
SOLUTION 2.67642768 -4.90869762 -9.44771006 1.96309674 -1.32608134 -2.25890404 6.03943671 -1.53037945	96E-02 29E-02 49E-03 36E-03 45E-03 45E-04 95E-02 72E-03 28E-04	-9.5017628651E-03 -1.3243385138E-02 -2.6439441884E-02 9.9015906097E-05 -7.7362874971E-02 4.1530303107E-03 -1.0895216206E-03	-5.8479864723E-02 4.5163735654E-03 5.2907851425E-03 -1.1627538047E-03 1.7725892158E-02 -1.5061352219E-03 -1.4831069907E-03	3.934521004AE-02 1.1073747997E-03 1.0475132926E-02 1.4073472697E-03 3.7160113133E-02 -6.4043803352F-03 -1.0461132531E-03	5.0959116874E-02 3.3110803569E-03 -2.8530916294E-03 -8.6052058309E-05 -1.5814523893E-02 -6.5753247444E-04 -5.5302299880E-05
5	K= 5	9 ستل			
SOLUTION					
2 • 39410836. -3 • 83944879 6 • 09519539 -7 • 14696081 1 • 70352344 -1 • 31514594 3 • 28742362 1 • 09478804	43E-02 50E-02 58E-03 25E-03 25E-03 41E-04 34E-03 41E-04	-1.2126655998E-02 3.3250215882E-02 -2.5281692667E-02 1.7319100745E-03 -6.7602347082E-02 -2.1589901080E-02 -1.4006745132E-03	-6.72131670R0E-02 -3.0904297107E-03 4.9457222742E-03 1.0902853077E-03 1.53R0046367E-02 3.0514537790E-03 4.0579952290E-04	4.0538769510E-02 -1.5284829018E-02 9.4207967722E-04 -5.4708097393E-04 4.0552212066E-02 7.1237057907E-03 1.5586504604E-03	5.3254457874E-02 1.2631458097E-02 -4.1410772765E-03 -2.2669177941E-04 -2.0032876706E-02 -3.2935630628E-03 -1.7716731193E-04
5	K≊ 5	J≈ 10			
SOLUTION					
2 • 54908013 -4 • 84789763 1 • 54055721 P • 68174083 -1 • 94295621 -7 • 02381554 -8 • 06131116 -5 • 70503419	R5E-02 37E-02 49E-02 79E-04 42E-04 23E-03 90E-03 12E-05	-3.7056877871E-03 5.9851160796E-02 1.5283510513E-02 -1.1900625428E-03 -3.9890059871E-02 -2.8349998831E-02 2.3032611173E-03	-6.4457218810E-02 -2.1631544138E-02 -7.3715516476E-03 1.3390963749E-03 8.9205194736E-03 8.1037751416E-03 7.0438340888E-04	4.7976184174E-02 -4.0398584712E-02 -2.8836654686E-03 -4.7400898228F-04 2.4668656940E-02 8.0438224544E-03 -1.1346229929E-03	4.3174897375E-02 9.8693362490E-03 -4.3557023490E-04 5.5223131404E-04 -1.2592820805E-02 -2.0921328636E-03 1.7855494570E-04

N= 9	K= 0	J= 0			
SOLUT 5. 6. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0.	ION 8479532164£-03 9095816464E-02	1.5948963317E-02 1.0887825625E-01 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0.	3.0378977747E-02 1.1823883031E-01 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0.	3.9258986627E-02 2.6800801538E-01 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0.	6.0571007939E-02 2.8377319275E-01 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0.
N= 9	ν = 1	0 = L			
SOLUT 7 -6 4 -2 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	ION 9013707748E-03 4096236617E-02 9612012901E-03 3300277199E-02	-2.3293015465E-02 6.4708302049E-02 -8.6604819215E-03 2.4188441554E-02 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0.	3.7402669737E-02 -5.9962932054E-02 1.1375851638E-02 -4.3301173563E-02 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0.	-4.9473798560E-02 4.3861385475E-02 -1.5526708636E-02 4.1896883471E-02 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0.	5.8574791007E-02 -1.5622536347E-02 1.7499709725E-02 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0.
N= 9	κ= 1	J= 1			
SOLUT 7 -6 -2 1 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	IUN 9013707748E=03 4096236617E=02 4806006454E=03 1650138599E=02 2965263513E=03 0178631969E=02	-2.3293015465E-02 6.4708302049E-02 4.3302409608E-03 -1.2094220777E-02 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0.	3.7402669737E-02 -5.9962932054E-02 -5.6879258191E-03 2.1650586782E-02 0. 0. 0. 0. 0. 9.8517765083E-03 -3.7499916320E-02 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0.	-4.9473798560E-02 4.3861385475E-02 7.7633543183E-03 -2.0948441735E-02 0. 0. 0. 0. 0. 0. 0. 0. 0. 0.	5.8574791007E-02 -1.5622536347E-02 -8.7498548627E-03 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0.

N=	9	K= 1	2 = ل						
SOLL 7 -6 -2 1 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	UTION 7.901370774 2.450600644 1.65013859 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0.	8E-03 - 7E-02 7E-03 9E-02 - 1E-03 9E-02 -	-2.3293015465E-02 6.4708302049E-02 4.3302409607E-03 1.22094220777E-02 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0.	3.7402669737E-02 -5.9962932055E-02 -5.6879258193E-03 2.1650586782E-02 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0.	-4.9473798560E-02 4.3861385475E-02 7.7633543183E-03 -2.0948441735E-02 0. 0. 0. 0. 0. 0. 0. 0. 0. 0.	5.8574791007E-02 -1.5622536347E-02 -8.7498548627E-03 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0.			
N=	9	K= 2	J= 0						
SOLU	JTIUN 1.035892115 3.581723033 1.044482773 2.139516494 1.925984838 3.445917227 0. 0. 0. 0. 0. 0. 0. 0. 0. 0.	1E-02 8E-02 7E-02 4E-02 2E-03 8E-03	3.0022196300E-02 6.2860621061E-03 1.5586936116E-02 2.0395322344E-02 2.2953331912E-03 3.0882332244E-03 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0.	4.3068860613E-02 -1.5587040647E-02 2.1075944766E-02 1.0580636067E-02 2.5785169876E-03 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0.	5.1036906384E-02 -9.4282405855E-02 2.2437470766E-02 6.2563749083E-03 2.7840890411E-03 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0.	4.5240428117E-02 -1.1196115851E-01 2.4864572455E-02 1.4366743763E-03 0.00			
N=	9	K= 2	J= 1						
SOL	UTIUN 1.035892115 3.581723033 2.948998863 7.920063208 1.558154465 2.787805598 0. 0. 0. 0. 0. 0. 0. 0. 0. 0.	01E-02 08E-02 01E-03 06E-03 05E-03 05E-03 07E-03 04E-02 06E-03 71E-03	3.0022196300E-02 6.2860621081E-03 5.3030171304E-03 4.9440327638E-03 -2.4984331611E-03 0. 0. 0. 0. 1.5493514161E-02 1.7527332808E-02 1.3491629989E-03 1.8152179449E-03 0. 0. 0.	4.3068860612E-02 -1.5587040647E-02 5.8739358464E-03 5.7014718382E-03 -2.0860640632E-03 0. 0. 0. 0. 0. 0. 0. 1.9165058982E-02 1.3409972324E-02 1.5156142581E-03 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0.	5.1036906384E-02 -9.4282405855E-02 7.8055689851E-03 -4.1968173539E-04 -2.2523753481E-03 0. 0. 0. 0. 0. 2.2539520489E-02 2.7115285854E-03 1.6364464794E-03 0. 0. 0. 0. 0. 0.	4.5240428117E-02 -1.1196115851E-01 6.7008514856E-03 -1.1622939859E-03 0.22690398735E-03 0. 0. 0. 0. 0. 2.2295167885E-02 8.4445601078E-04 1.6485539658E-03 0. 0. 0. 0. 0. 0. 0. 0. 0. 0.			
N	=	9		K =	2	J= 2			
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N S <sup>1</sup>		9 UTION 1.035 3.581 8.171 1.861 5.951 1.064 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0.	89211 72303 41273 76556 62045 84698 84698 8482 05883 7204 26203	K = 151E-0 338E-0 314E-0 591E-0 590E-0 346E-0 149E-0 340E-0 340E-0 340E-0 341E-0	2 02 03 02 04 03 04 03 04 03 04 03 02 03 03 03 03	J= 2 3.0022196300E-02 6.2860621080E-03 -1.3096485188E-02 -1.5141693936E-02 7.0929696384E-04 9.5431654892E-04 0. 0. 0. 0. 9.0037338178E-03 1.2429462844E-02 -2.1829915886E-03 -2.9370843319E-03 0. 0. 0. 0. 0. 0. 0. 0. 0. 0.	4.3068860612E-02 -1.5587040647E-02 -1.6411908230E-02 -1.0991789872E-02 7.9680556944E-04 0. 0. 0. 0. 0. 1.2595717216E-02 5.4289775968E-03 -2.4523153834E-03 0. 0. 0. 0. 0. 0. 0. 0.	5.1036906385E-02 -9.4282405855E-02 -1.9024304368E-02 -2.7085057187E-03 8.6033082754E-04 0. 0. 0. 0. 1.2905081448E-02 4.4419435177E-03 -2.6478260245E-03 0. 0. 0. 0. 0. 0.	4.5240428117E-02 -1.1196115851E-01 -1.9133287713E-02 4.4395679766E-04 8.6669610984E-04 0. 0. 0. 0. 0. 1.4934541822E-02 -1.3663585274E-03 -2.6674163490E-03 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0.
N	=	9		k.=	2	J= 3			
5	OL. -	UTION 1.035581 8.171 1.861 5.951 1.064 0. 0. 0. 0. 0. 0. 0. 0. 0. 0.	8821 7230 4127 7655 6204 8469 8469 8482 7204 7204 7202	151E 338E 316E 590E 846E 150E 340E 340E 341E	02 02 02 04 03 02 04 03 02 03 03	3.0022196300E-02 6.2860621082E-03 -1.3096485188E-02 -1.5141693936E-02 7.0929696383E-04 9.5431654892E-04 0. 0. 0. 0. 0. 0. 0. 0. 0. 2.1829462844E-02 2.1829915886E-03 2.9370843319E-03 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0.	4.3068860612E-02 -1.5587040648E-02 -1.6411908230E-02 -1.0991789872E-02 7.9680556944E-04 0. 0. 0. 0. 0. 0. -1.2595717216E-02 -5.4289775968E-03 2.4523153834E-03 0. 0. 0. 0. 0.	5.1036906384E-02 -9.4282405855E-02 -1.9024304368E-02 -2.7085057188E-03 8.6033082754E-04 0. 0. 0. 0. 0. 0. -1.2905081448E-02 -4.4419435177E-03 2.6478260245E-03 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0.	4.5240428117E-02 -1.1196115851E-01 -1.9133287713E-02 4.4395679772E-04 8.6669610984E-04 0. 0. 0. 0. 0. 0. -1.4934541822E-02 1.3663585274E-03 2.6674163490E-03 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0.
N	=	9		K =	2	4 = ل			
S	- - -	UTION 1.035 3.581 2.948 7.920 -1.558 -2.78 0. 0. 0. 0. 0. 0. 0. 0. 0. 0.	58921 58921 17230 39988 00632 31544 78055 01196 49146 20654 54593	151E- 338L- 631L- 085E- 985L- 985L- 207E- 184L- 840E- 271E-	02 02 03 03 03 03 02 03 02 03 03	3.0022196300E-02 6.2860621081E-03 5.3030171303E-03 4.9440327638E-03 -1.8569635594E-03 -2.4984331611E-03 0. 0. 0. 0. 0. -1.55493514161E-02 -1.7527332808E-02 -1.8152179449E-03 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0.	4.3068860612E-02 -1.5587040647E-02 5.8739358464E-03 5.7014718382E-03 -2.0860640632E-03 0. 0. 0. 0. 0. 0. -1.9165058982E-02 -1.3409972324E-02 -1.3409972324E-02 -1.5156142581E-03 0. 0. 0. 0. 0.	5.1036906384E-02 -9.4282405855E-02 7.8055689852E-03 -4.1968173537E-04 -2.2523753481E-03 0. 0. 0. 0. 0. 0. -2.2539520489E-02 -2.7115285854E-03 -1.6364464794E-03 0. 0. 0. 0. 0.	4.5240428117E-02 -1.1196115851E-01 6.7008514856E-03 -1.1622939860E-03 -2.2690398735E-03 0. 0. 0. 0. 0. 0. 0. 0. 0. 0.

N=	9	к= 3	J= 0			
SOL - -	UTION 1.078641267 2.106127320 1.528004429 6.710501245 4.170434426 1.253136033 3.886789272 0. 0. 0. 0. 0. 0. 0. 0. 0. 0.	7E-02 0E-02 8E-02 2E-03 1E-03 4E-03 6E-04	-2.8340569027E-02 -4.7767601152E-02 -2.1979259321E-02 -2.0914608260E-03 4.0144393022E-03 -8.2481051469E-04 3.7911484950E-04 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0.	3.5145764621E-02 6.4216808036E-02 2.5056885931E-02 2.0562519561E-02 -4.3972211614E-03 3.6639293110E-04 -3.1967791471E-04 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0.	-2.7672168856E-02 -5.5993610028E-02 -2.2627304025E-02 -2.3734165923E-02 3.2641951871E-03 -3.8901508710E-04 2.6862551025E-04 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0.	7.1885977381E-03 2.1375092790E-02 1.7269568156E-02 3.0590320333E-03 -3.0313287056E-03 4.3255661155E-04 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0.
N=	9	K= 3	J= 1			
50L	UTION 1.220128656 9.583759494 1.017320829 7.219072166 1.069540772 2.562431758 3.501876130 0. 0. 1.321232781 1.119181746 3.771979097 1.747543768 1.686414662 0. 0. 0.	3E-02 3E-03 9E-03 8E-03 8E-05 9F-04 3E-02 7E-02 6E-03 8E-02 8E-03 8E-02 8E-03 8E-04	-3.2511576848E-02 -3.6180486793E-02 -1.4831976615E-02 1.8468327346E-03 -7.2462325380E-04 4.1047772893E-04 -3.4157067676E-04 0. 0. 0. -1.9393899441E-02 4.5367918621E-03 -3.3288477216E-04 1.6449176846E-04 0. 0. 0. 0. 0. 0. 0. 0. 0. 0.	4.1843344341E-02 5.3479432321E-02 1.7104555186E-02 7.1800193775E-03 1.1679571696E-03 -3.3010862435E-04 2.8801984891E-04 0. 0. 0. 2.2492942935E-02 5.0276278289E-03 -3.8935072913E-03 1.5897193493E-04 -1.3870304895E-04 0. 0. 0.	-3.6531288065E-02 -4.8139488171E-02 -1.6130435001E-02 -9.3404343185E-03 -5.2176180255E-04 3.5049048262E-04 -2.4202322186E-04 0. 0. 0. -2.1652558681E-02 -7.8656417327E-03 3.6071904263E-03 -1.6878732056E-04 1.1655224081E-04 0. 0. 0.	1.7677403354E-02 1.8577613803E-02 1.3046948594E-02 -5.7512404169E-04 8.8063774225E-04 -3.8972004061E-04 0. 0. 0. 1.7967146247E-02 3.2015636778E-03 1.8767928000E-04 0. 0. 0. 0. 0. 0. 0. 0. 0. 0.
N=	9	к= 3	J= 2			
SOL - - - -	UTION 1.106664580 1.878801084 2.937709026 6.785313833 3.439412494 1.6698027251 2.423373473 0. 0. 1.533134255 8.582418232 1.555871922 2.9.974702877 3.038814219 0. 0. 0. 0. 0. 0. 0. 0. 0. 0.	93E-02 98E-03 98E-04 98E-03 05E-03 95E-04 95E-04 97E-03 97E-03 97E-03 97E-03 97E-04 91E-04	-2.9166688280E-02 -4.5472631046E-02 4.0836242604E-03 2.7199356994E-03 -3.9958908128E-03 2.3319876830E-04 2.3637424240E-04 0. 0. 0. 0. -2.2186501850E-02 7.8907055060E-05 -2.0440471177E-03 -4.8783597331E-05 -2.9640392481E-04 0. 0.	3.6472302425E-02 6.2090139090E-02 -4.5153680416E-03 -8.6115811050E-03 3.5359940143E-03 2.2844225600E-04 -1.9931591970E-04 0. 0. 0. 2.5424722658E-02 1.6255540247E-02 1.5683462169E-03 -2.8645752849E-04 2.4993425797E-04 0. 0.	-2.9426826065E-02 -5.4438004870E-02 3.5878445948E-03 9.1864485796E-03 -3.4006477075E-03 -2.4254693957E-04 1.6748526616E-04 0. 0. 0. -2.3419502877E-02 -1.9470625911E-02 -1.7828872781E-03 3.0414424225E-04 -2.1001988091E-04 0. 0.	9.2660343271E-03 2.0821017768E-02 2.2117378927E-03 -2.9933166532E-03 2.2680220998E-03 2.6969463603E-04 0. 0. 0. 0. 1.8368851846E-02 -1.5164441041E-03 9.4592578004E-04 -3.3818637686E-04 0. 0. 0.

N=	9	K= 3	J= 3			
SOLU 1 1 -1 1 1 -1 -1 -1 -1 -1 -1	TION 1696323920 3680036712 4875521420 1252854177 423736054 0970835510 6489197904 3662897432 6741766261 3008589999 0766967044 7893393507 -	DE-02 DE-02 DE-02 3E-02 5E-03 9E-03 4E-05 5E-03 5E-03 BE-03 DE-04 7E-04	-3.1022961392E-02 -4.0315880028E-02 2.1737982014E-02 -3.5210380210E-03 2.7132944155E-03 -2.3127123989E-04 -8.4360990387E-05 0. 0. 0. 0. 0. 0. 0. 0. 0. 0.	3.9453005814E-02 5.7311557346E-02 -2.5117630110E-02 -8.8496980528E-03 -2.5053406032E-03 -8.1530097222E-05 7.1135028146E-05 0. 0. 0. 0. 1.0267641460E-02 1.1221325147E-02 3.4918157520E-03 3.5720669535E-04 -3.1166292195E-04 0. 0. 0.	-3.3369505026E-02 -5.0942591808E-02 2.3856242418E-02 1.2021068701E-02 2.2903119166E-03 8.6564000504E-05 -5.9774799426E-05 0. 0. 0. 0. 0. -8.9930470762E-03 -1.2522873723E-02 -2.4938211997E-03 -3.7926166667E-04 2.6189050787E-04 0. 0. 0. 0. 0. 0. 0. 0. 0. 0.	1.3933991971E-02 1.9576022494E-02 -1.9469994779E-02 2.0389246783E-03 -9.6252901191E-05 0. 0. 0. 0. 0. 0. 0. 0. 0. 0.
N=	9	K= 3	4 = ل			
SOLU 1 1 1 1 1 1 1 1 1 1 1 1 1	TIUN 169632392( 368003671( 487552142( 125285417; 423736054; 097083551 648919790]	DE - 02 DE - 02 DE - 02 3E - 02 5E - 03 3E - 05 5E - 03 3E - 05 5E - 03 8E - 03 8E - 03 0E - 04 7E - 04	-3.1022961392E-02 -4.0315880028E-02 2.1737982014E-02 -3.5210380210E-03 2.7132944155E-03 -2.3127123989E-04 -8.4360990387E-05 0. 0. 0. 0. 0. 0. 0. 0. 0. 0.	3.9453005814E-02 5.7311557346E-02 -2.5117630110E-02 -8.8496980528E-03 -2.5053406032E-03 -8.1530097225E-05 7.1135028145E-05 0. 0. 0. -1.0267641460E-02 -1.1221325147E-02 -3.4918157520E-03 -3.5720669535E-04 3.1166292195E-04 0. 0. 0.	-3.3369505026E-02 -5.0942591808E-02 2.3856242418E-02 1.2021068701E-02 2.2903119165E-03 8.6564000504E-05 -5.9774799426E-05 0. 0. 0. 8.9930470762E-03 1.2522873723E-02 2.4938211997E-03 3.7926166667E-04 -2.6189050787E-04 0. 0.	1.3933991971E-02 1.9576022494E-02 -1.9469994779E-02 2.0389246783E-03 -1.6329954893E-03 -9.6252901190E-05 0. 0. 0. 0. 0. 0. 0. 0. 0. 0.
N=	9	K= 3	J= 5			
SOLU 1 -2 -6 3 -1 -2 0 0 0 0 0 0 0 0 0 0 0 0 0	TION 106664580 878801084 937709027 785313833 439412494 698027251 423373473 533134255 582418252 555871922 974702877 038814219	3E-02 8E-02 0L-03 7E-04 8L-03 0E-03 5E-04 2E-02 7E-03 1L-03 3E-04 1E-04	-2.9166688280E-02 -4.5472631046E-02 4.0836242604E-03 2.7199356994E-03 -3.9958908128E-03 2.3319876830E-04 2.3637424240E-04 0. 0. 0. 0. 2.2186501850E-02 -7.8907055059E-05 2.0440471177E-03 4.8783597331E-05 2.9640392481E-04 0. 0. 0. 0. 0. 0. 0. 0. 0. 0.	3.6472302425E-02 6.2090139091E-02 -4.5153680416E-03 -8.6115811050E-03 3.5359940144E-03 2.2844225601E-04 -1.9931591970E-04 0. 0. 0. 0. -2.5424722658E-02 -1.6255540247E-02 -1.6683462168E-03 2.8645752849E-04 -2.4993425797E-04 0. 0. 0.	-2.9426826065E-02 -5.4438004870E-02 3.5878445948E-03 9.1864485795E-03 -3.4006477075E-03 -2.4254693958E-04 1.6748526616E-04 0. 0. 0. 2.3419502877E-02 1.9470625911E-02 1.7828872781E-03 -3.0414424225E-04 2.1001988091E-04 0. 0. 0.	9.2660343271E-03 2.0821017768E-02 -2.2117378927E-03 -2.9933166533E-03 2.6980220998E-03 2.6969463603E-04 0. 0. 0. 0. -1.8368851845E-02 1.5164441041E-03 1.5164441041E-03 -9.4592578004E-04 3.3818637686E-04 0. 0. 0. 0.

N=	9	k= 3	J= 6			
SOLU 1 9 1 -7 1 -2 3 0 0 0 0 0 0 0 0 0 0 0 0 0	TIUN 220128656 58375949 219072166 069540772 562431758 501876130 321232781 119181746 7/1979097 747543768 686414662	3E-02 3E-03 8E-02 9E-03 8E-03 7E-05 7E-04 3E-02 7E-02 6E-03 9E-03 8E-04	-3.2511576848E-02 -3.6180486793E-02 -1.4831976615E-02 1.3468327346E-03 -7.2462325380E-04 4.1047772893E-04 -3.4157067676E-04 0. 0. 0. 0. 0. 0. 0. 0. 1.9393699441E-02 -4.5367918621E-03 3.3288477216E-04 -1.66449176846E-04 0. 0. 0. 0. 0. 0. 0. 0. 0. 0.	4.1843344341E-02 5.3479432321E-02 1.7104555186E-02 7.1800193775E-03 1.1679571696E-03 -3.3010862434E-04 2.8801984891E-04 0. 0. 0. -2.2492942935E-02 -5.0276278289E-03 3.8935072913E-03 -1.5897193494E-04 1.3870304895E-04 0. 0. 0.	-3.6531288065E-02 -4.8139488171E-02 -1.6130435001E-02 -9.3404343185E-03 -5.2176180255E-04 3.5049048262E-04 -2.4202322186E-04 0. 0. 0. 2.1652558681E-02 7.8656417327E-03 -3.6071904263E-03 1.6878732056E-04 -1.1655224081E-04 0. 0.	1.7677403354E-02 1.8577613803E-02 1.3046948594E-02 5.7512404168E-04 8.8063774225E-04 -3.8972004061E-04 0. 0. 0. 0. 0. 0. 1.7967146247E-02 -3.2015636778E-03 2.5273483320E-03 -1.8767928000E-04 0. 0. 0. 0. 0. 0. 0. 0. 0. 0.
N=	9	K= 4	0 = L			
SOLU 1 -4 1 -9 5 -2 5 7 0 0 0 0 0 0 0 0 0 0 0 0 0	TIUN 126423011 986416433 930346378 029136678 284745388 243316948 134866737 855365851	5E-02 0E-02 8E-02 2E-03 5E-03 5E-03 5E-04 0E-05	2.7068836300E-02 -5.1374188923E-02 2.5718809492E-02 -1.7378925618E-02 4.6587687598E-03 -2.5711237799E-03 4.0375044286E-04 5.9769970218E-05 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0.	2.4510631526E-02 -3.1516845514E-02 2.2653156510E-02 -1.2401248111E-02 3.2084481471E-03 8.5559594132E-04 1.5670681099E-04 5.6450514471E-05 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0.	4.3045552713E-03 3.1805224742E-02 1.4639830313E-02 -6.8550903987E-03 1.3402470048E-03 7.4225216333E-04 1.0634067136E-04 3.4045795025E-05 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0.	-2.6116283935E-02 5.9918004748E-02 6.433118078E-04 4.8868738688E-03 -3.6225653258E-04 7.1448554012E-05 2.7127752425E-05 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0.
N=	9	K= 4	J= 1			
SULU 1 -5 1 -2 -2 -1 0 0 0 0 1 -3 5 2 0 0 0 0 0 0 0 0 0 0 0 0 0	TIUN 152873565 200984385 /31261792 432443606 322983666 355984169 2/2067040 381629323	3E - 02 9E - 02 1E - 02 6E - 03 5E - 03 3E - 04 6E - 04 8E - 05 $3E - 02 8E - 03 8E - 04 0E - 04 0E - 04 2E - 05$	2.6289081527E-02 -4.9208019950E-02 2.3139744529E-02 -8.0835507681E-03 1.2920082928E-03 2.0340563431E-04 -2.6068505732E-04 -5.6165399959E-05 0. 0. 0. 1.8293788189E-02 -7.5292476703E-03 5.8112664435E-03 -8.8621964673E-04 3.2246529098E-04 2.0442533781E-05 0. 0.	2.5762719744E-02 -3.3524158932E-02 2.2477065180E-02 -7.9361844559E-03 1.0997549319E-03 -4.5564103782E-04 -5.4060323143E-05 0. 0. 0. 1.7812109403E-02 -8.1828726886E-03 4.5338994296E-03 6.6446962226E-04 2.0245677446E-04 1.9307213050E-05 0. 0.	2.6483750902E-03 3.3273524316E-02 1.6100805602E-02 -2.9377032156E-03 8.1860504500E-04 -3.4156390326E-04 -7.3583824825E-05 -3.1992582353E-05 0. 0. 0. 1.1831693920E-02 -1.9924276237E-03 2.8036380288E-03 7.2403064709E-04 3.6008122374E-05 1.1644347694E-05 0. 0.	-2.4155439795E-02 5.9395026205E-02 6.6215943309E-03 1.1509252842E-03 5.2383011539E-04 -4.3541460302E-04 -6.7139678971E-05 0. 0. 0. 4.4023111755E-03 5.5782925027E-03 1.1182809476E-03 6.0691363332E-04 2.4436844684E-05 9.2782377726E-06 0. 0.

					,			
N=	9	K= 4		J= 2				
SOLU -4 -5 -6 (( ( ( ( ( ( ( ( ( ( ( ( ( ( ( ( ( (	JTION 130931594 5022990242 2.743529769 4.386502770 5.265874506 1.57156301 3.417906815 5.017559358 0. 1.978611950 9.258827360 1.978611950 9.258827360 1.958954762 1.211930635 5.460479824 5.460479331838 0. 0. 0. 0. 0. 0. 0. 0. 0. 0.	9E-02 1E-02 4E-03 7E-03 1E-04 9E-05 9E-02 7E-03 9E-03 1E-03 8E-04 6E-05	2.693 -5.100 2.803 -3.524 -4.735 1.935 -1.489 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0.	5924549E-02 4958338E-02 2326021E-03 6847700E-03 1492203E-03 2060517E-04 6453551E-05 6876159E-02 2058016E-02 1963750E-03 8906040E-03 5820258E-04 9396288E-05	2.4724054057E -3.1858998650E 2.7699942710E -5.0404084812E -3.4163798349E -3.4762705402E -1.4830254828E 4.3243602922E 0. 0. 0. 2.3954477094E -1.4252056224E 7.6461466119E -6.4542384262E -2.1907422148E -3.6285691262E 0. 0.	-02 4.022253 -02 3.205550 -03 4.818317 -03 2.739863 -03 -1.692848 -04 -4.562469 -04 5.607963 -05 2.608059 0. 0. 0. 0. -02 1.455348 -04 9.912463 -04 9.912463 -04 -7.442523 -04 -7.442523 -04 -2.204447 -05 -2.188421 0. 0. 0. 0. 0. 0. 0. 0. 0. 0.	9441E-03 -2 1205E-02 5 4977E-06 -1 0353E-04 -4 5653E-03 -7 8187E-04 -3 6938E-06 5 2090E-05 2 00 8502E-02 2 3947E-03 1 0856E-05 -4 6808E-05 -4 5204E-05 -1 0 0 0 0 0 0 0 0 0 0 0 0 0	5782051640E-02 9828861346E-02 0695425224E-03 8158214835E-03 7431484303E-05 0789532285E-04 4732767771E-05 0781064000E-05 8 8 8 8 8 8 8 8 8 8 8 8 8
N=	9	K= 4	•	j= 3				
SOL	UTION							
_	1.145718456	5E=02	2,650	0012092E=02 3987824E=02	2.5424018803E	-02 3.096386 -02 3.287633	4834E=03 =2	2.4685865485E-02
-	9.756942059	2E-03	-1,267	5745450E-02	-1.1567821286E	-02 -6.990646	5999E-03 -6	9276477355E-04
	5.008687783	6E-03	8.176	5084272E-03	7.1188943240E	-03 2.539055	1360E-03 -3	.0499533245E-03
-	3.455459772	5E-03	-3.298	3981133E-03	-2.6927886368E	-03 $-1.845473$	7854E-03 -9	9-9291801606E=04
-	6.142501324	4L-04	-1.010 5.654	6643311E=04	2.3958203291E	-04 3.670058	1283E-05 -3	3.5724277007E-05
~	3.927682925	5E-05	-2.988	4985109E-05	-2.8225257235E	-05 -1.702289	7512E-05 -1	.3563876213E-05
	υ.		υ.		0.	0.	(	)•
	0.		0.		0.	0.	(	).
	1 <b>.</b> 418800240	0E-02	2,592	7473279E-02	2.4606489962E	-02 1.793265	4544E-02 6	
-	2.826661289	4E-03	-1.019	6533302E-02	-8.3354691212E	-03 -4.377392	7048E-03 -4	+.6289119949E-03
-	5.108607865	5E-03	-4.668	4962371E-03	-3.4906863879E		'9588E-03 -4	4.4350465949E~04
	2°311212085 2°311212085	85-04 95-05	-5.674	4299486E-05		-05 -4.020672	4752E-05 6	5.1876262839E-05
	6.802946383	0E-05	5,176	2312592E-05	4.8887579588E	-05 2.948452	3383E-05	2.3493322748E-05
	υ.		υ.		0.	0.	(	D•
	0.		0.		0.	0.	(	) •
	0.		U.		0.	0.		J.
N=	9	K= 4	•	4 = ئ				
SOL	UTION		., ,	10703351 05	3 6004 1300415		00546 00 1	0 6017136376E 00
	1.138551961 5.084806959	3E-02	2.071 	1278325E-02 0888185E-02		$-02 \qquad 3.247851$	6192F=02	2,9217133273E=02 5,9678191983E=02
	1.995093752	5E-02	-2.612	6636427E=02	-2.5005816420E	-02 -1.643489	2475E-02 -	5.1809426253E-03
	6.324826933	2E-03	1.212	1189920E-02	1.2058322668E	-02 3,552206	9754E-03	4.2714125893E-03
	4./559//918	4E-03	4.412	1546609E-03	3.4051894662E		38032E-03	7.3764765126E-04
-	4.724124/13 3.019960837	6E-04	-0.249	3599206E=04	-3083139916916 -101557256697F	-04 -2.189505	5831E-05	1.2406911201E=05
	1.364069964	9E-05	1.037	8946408L-05	9.80252896628	-06 5.911990	2633E-06	4.7106847729E-06
	U.		υ,	-	U.e	0.	(	0.
	0.		0.		0.	0.	(	0 <b>.</b>
	0. 5.610203972	91-02	0.	1952023F=03	Ue 5.7245225050F	-03 3-292104	4514E-03 -	0. 2.2318184751E=03
-	4.588555047	0E=03	-8,111	2733970E-03	-4.4786927745E	-03 -3,557070	07028E-03 -	3.0417585840E-03
	3.263629678	8E-03	-2.835	6890491E-03	-1.8838356376E	-03 -6.687469	99113E-04	4.3988300828E-04
	1.680542997	6E-03	1.866	4901007E-03	7.4848958638E	-04 6.348230	04813E-04	7.0610602459E-04
	4.367132237	5E-04	4.094	19300685-04	1.29149336898		2898E-05 -	1,0303089933E=05 2,6715620910E=05
	10120122192	00-07		1930008E=03	-JeJJ727043120			0.
	U.		Ű.		0.	0.		0.
			Ū.		0.	0.		0.

N= 9	K= 4	J= 5			
COLUTION		·	,		
SULUTION 1.1385519 -5.0848069 -1.9950937 6.3248269 4.(559779 -4.5241247 -3.0199608 1.3640699 U. U. U. U. U. -5.6102038 4.5885550 3.2636296 -1.6805429 -4.3671322 7.(360251) U.	613E-02 595E-02 525E-02 525E-03 184E-03 151E-04 376E-04 649E-05 729E-03 470E-03 788E-03 976E-03 976E-03 975E-04 928E-05	2.6711278325E-02 -5.0380888185E-02 -2.612636427E-02 1.2121189920E-02 4.4121546609E-03 -8.3494412256E-04 -1.8773599206E-04 1.0378946408E-05 0. 0. 0. 0. -7.5711952023E-03 8.1112733970E-03 2.8356890491E-03 -1.8664901007E-03 -4.0940260158E-04 5.8861930068E-05 0.	2.5084778865E-02 -3.2437302747E-02 -2.5005816420E-02 1.2058322668E-02 3.4051894662E-03 -3.8513991691E-04 -1.1557256697E-04 9.8025289662E-06 0. 0. 0. 0. 5.7245225050E-03 4.4786927745E-03 1.8838356376E-03 -7.4848958638E-04 -1.2914933689E-04 5.5592904312E-05 0.	3.5451108254E-03 3.2478516192E-02 -1.6434892475E-02 3.552069754E-03 2.0495938032E-03 -4.1641796665E-04 -2.1895055831E-05 5.9119902632E-06 0. 0. 0. -3.2921044514E-03 3.5570707028E-03 6.6874699113E-04 -6.3482304813E-04 -6.3482304813E-04 -5.3528562898E-05 0.	-2.5217135275E-02 5.9678191983E-02 -5.1809426253E-03 4.2714125893E-03 7.3764765126E-04 -3.5218230408E-04 1.2406911201E-05 4.7106847728E-06 0. 0. 0. 2.2318184751E-03 3.0417585840E-03 -4.3988300828E-04 -7.0610602459E-04 7.0363089934E-05 2.6715620910E-05 0.
0.		0.	0.	0.	0.
0.		0.	0.	0.	0.
N= 9	K= 4	J= 6			
SOLUTION					
1.1457184	565E-02	2.6500012092E=02	2.5424018803E-02	3.0963864834L-03	-2.4685865485E-02
-9.1429418	560E-02 592E-03	-+++++++++++++++++++++++++++++++++++++	=3.2981162891E=02 =1.1567821286E=02	3.2876336289E=U2	5.9536496529E=U2 =6.9276477355E=()4
5.0086877	836E-03	8.1/650842/2E-03	7.1188943240E-03	2.5390551360E-03	-3.0499533245E-03
-3.4554597	725E-03	-3.2983981133E-03	-2.6927886368E-03	-1.8454737854E-03	-9.9291001606E-04
-3-3309377	288E-04	-1.8188004749E-05	7.6061003807E=04	8.4310277012E-04	6.9294862897E-04
5.1425013	2446-04	3.0546643311E=04 -/-9884985109E=05	2 • 3958203291E=04 -2 - 8225257235E=05	3.6700581283E=05 =1.7022897512E=05	-3.5724277006E-05
U.	2))[=0)	U.	0.	-1.1022897512E=05	-1.5585878215E=05
Ŭ.		U <b>.</b>	0.	0.	Ŭ.
υ.		U.	0.	0.	0.
-1.9188005	960E-02	-2.0927473279E-02	-2+4006489962E-02 8-3354601212E-03	-1. (932654544E-UZ 4.3773927049E-03	-6.4504674887E-03
5.1086078	655E-03	4.6684962370E-03	3.4906863879E-03	1.9295479588E-03	4.4350465949E-04
-9.9113/56	828E-04	-1.3/38053939E-03	5•4840136807E-05	-5.8226124974E-05	6.4743235309E-05
-5.8175809	999E-05	5.6744299486E-05	-4.7848031685E=05	4.0206724752E-05	-6.1876262839E-05
-6.8029463	830E-05	-5.1762312592E=05	-4.8887579588E-05	-2.9484523383E=05	-2,3493322748E=05
υ.		U.	0.	0.	U.
U.		υ.	υ.	0.	0.
N= 9	K= 4	J= 7			
CINE IT LONG					
1.1309315	949E-02	2.0935924549E-02	2.4724054057E+02	4.0222539441E-03	-2-5782051640E-02
-5.0229902	421E-02	-5.1004958338E-02	-3.1858998650E-02	3.2055501205E-02	5.9828861346E-02
2.1435291	643E-03	2.8032326022E-03	2.7699942711E-03	4.8183173976E-06	-1.0695425224E-03
-4.3865027	706E-03	-3,5246847700E-03	-5.0404084813E-03	2.7398630350E-04	-4.8158214834E-03
-202020742	0171-03	1,9352883829E=03	-3.4762705401F=04	-1.09284836535E=03	= 7 = 7431484301E=03 = 3 = 0789532285F=04
-3.4179068	151E-04	-1.4892060517E-04	-1.4830254828E-04	5.6079636937E-06	5.4732767771E-05
6.0175593	589E-05	4.5786453551E-U5	4.3243602922E-05	2.6080592090E-05	2.0781064000E-05
0.		0.	0.	0.	<b>U</b> •
Ú.		U.	0.	0.	Ŭ.
-1.9/86119	509E-02	-2,5546876159E-02	-2.3954477094E-02	-1.4553488502E-02	-2.8132726609L-03
9.2568213	607E-03	1.4752058016E-02	1.4252056224E-02	4.0105883947E-03	-1.4860167154E-03
-1.5589547	629E-03	-1.2971963750E-03	-/.6461466120E-04	-9.9124630857E-05	4.9266436368E=04
102119300 504604748	248E=04	3.0275820258E=04	2.1907422148E=04	2.204447340xE-05	4.5926245250E=04
5.0493318	386L-05	3.8419396288E-05	3.6285691262L-05	2.1884215204E-05	1.7437383138E-05
υ.		U.	υ.	0.	0.
υ.		0.	0.	0.	U •
U .		U .	U.	U.	0.

N= 9	K= 4	8 = ل			
SOLUTION					
1.1528/3565	3E-02	2.6289081527E-02	2.5762719745E-02	2.6483750901E-03	-2.4155439795E-02
-5.200984385	8E-02	-4.9208019950E-02	-3,3524158932E-02	3.3273524316E-02	5.9395026206E-02
-2.432443606	6t-02		-7-4361844559E-03	-2-9377032156F-03	6.0215943309E=03
1.322983666	5E-03	1.2920082928E=03	1.0997549319E=03	8.1860504500E-04	5.2383011539E-04
3.355984169	3L-04	2.0340563431E-04	-4.5564103781E-04	-3,4156390326E-04	-4.3541460302E-04
-2.2/2067040	061-04	-2,6068505732E-04	-5.4060323143E-05	-7.3583824825E-05	-6.7139678972E-05
-/•301029323 U•	02-05	-2.0105544454E=05	-2.20401318882=02	-3.1992382353E=05	-2,0491/48//3E-05
0.		Ú,	0.	0.	0.
0.		0.	0.	0.	0.
-1.399368628	3E-02 8E-03	-1.8293788189E-02	-1.7812109403E-02	=1.1831693920E=02	-4.4023111755E-03
-6.230892572	6E-03	-5.8112664435E-03	-4.5338994296E-03	-2.8036380288E-03	-1.1182809476E-03
3.127688282	8E-04	8.8621964673E-04	-6.6446962226E-04	-7.2403064709E-04	-6.0691363332E-04
-5.258437357	0E=04	-3,2246529098E-04	-2.0245677446E-04	-3.6008122374E-05	-2,4436844684E-05
-2:080093334	55-05	-2,0442555781E-05	-1.9307213050E=05	-1.1044347694E=05	-9.2182311126E-06
0.		0.	Ŭ.	0.	0.
υ.		υ.	υ.	0.	0.
N= 9	K= 5	0 =L			
SOLUTION					
1.111297535	/E=02	-2.4555369544E-02	1.0750237045E-02	1.4714574677E-02	-4.1497542542E-02
3.657256827 2.522682100	9E=02	-/.UI22//3466E-U3	-3+3832511732E=02	5.1917165640E-02	-1.8169819832E-02
1.426455618	2E=02	-8,2223992090E-03	-7.4175613262E-03	1.4462656157E-02	6.8932069252E=03
-5.891266196	2E=03	4.2326549455E-03	-7.7302661281E-04	-8.6626848085E-04	2.6942445767E-03
-1,501610952	4L-03	1.0655168816E-03	1.1070345119E-03	-9.4811117357E-04	5.7787565634E-04
-2.426090230	00E=04	-9.2240471200E=05 8.6274888074E=05	-7.6249074884E=05	-2.9756030381E-04 2.1355677779E-05	-1.4565043528E=04
1.542086636	6E-05	-1.0034127706E-05	9.2117843128E-06	-4.1554478017E-06	3.1728841932E-06
υ.		U .	0.	0.	0.
0.		0.	0.	0.	0.
0.		0 • 0 •	0.	0.	0.
Ŭ <b>.</b>		U <b>.</b>	0.	0.	0.
υ.		υ.	0.	0.	0.
0.		0.	U •	0.	0.
0.		U.	0.	0.	0.
υ.		υ.	υ.	0.	0.
0.		0.	0.	0.	0.
N= 9	K= 5	.1= 1			
		• •			
SOLUTION	161-112	-2.04200620765 02	0.80338004426 03	2.27021521055.02	-4-43652450046 03
4.503120940	0L=02	-1.2904836887E-02	-2.8980829855E-02	4.1777919639E=02	-2,3634343456E-02
2.013481727	17E-02	-2.3760978218E-02	1.4676482225E-02	-3.1152659770E-03	-1.0440297940E-02
1.247427754	+6E-02	-1.0210992373E-02	-3.4400/13525E-03	8.3730078336E-03	3.7732047861E-03
-3.933508555	07E-03	2.9261168932E=03	~1.9228273982E=03	5.3157732919E-04	-4.9992215115E-05
-6.228790120	)6E-05	1.0755966791E-04	-1.1585536072E-04	1.0925829788E-04	-9.0049372292E-05
1.087565955	06E-04	-5.2038095412E-05	5.4144773691E-05	-1.1444551180E-05	1.1587965863E-05
-1.479621292	25E-05	9.6276750303E-06	-8.8386423226E-06	3.9871229679E-06	-3.0443600895E-06
0.		U.	0.	U• ()•	0.
1.304745436	2E-02	-1.4489487796E-02	9.5964089946E-03	-7.6000731034E-04	-6.6730820094E-03
9.529054902	22E-03	-6.9119601981E-03	-2.3600605828E-04	3.9426324121E-03	6.9485633317E-03
-6.194065361	11E-03	4.6864128841E=03	-2,2883799417E-03	-2.2861068220E-04	1,2229973932E-03
-10463534215	71-04	202762367320E=04	103/437/1733E=U3 8.8647650008F=06	~102342349280E=03 -9,0250026771E=05	1.2823226273F=04
-9.878460499	7E-05	8.0391374475E-05	-4.3279604757E-05	2.4791500892E-05	-4.1432443924E-06
4,344560110	00E-06	-2.8269404543E-06	2,5952595475E-06	-1.1707249340E-06	8.9390477631E-07
0.		0.	0.	0.	0.
Ua		Ve	U e	Ue	Ue

N= 9 K=	5 J= 2			
SULUTION				
1.0478234916E-02	-2.2378225620E-02	/.7154245587E-03	1.9274466363E-02	-4.6362432110F-02
4.2327082674E-02	-1.2607310127E-02	-2.8697106673E-02	4.7626833308E-02	-1.7376967289E-02
1.0353517551E-02	-1.0945171924E-02	8.0614/23870E-03	-3,7050746661E-04	-4.2393818654E-03
1.3659/51448E-03	-4.3979526683L-03	-7.5607256553E-04	3.9566859980E-03	-5.6495995872E-03
5.2199020135E-03	-4.2752639653E-03	1.9877080804E-03	-6.8499664652E-04	-7.7640565377E-04
4.2541661723E-04	-5.0443436693E-04	-1.2154206410E-03	1.0723956028E-03	-7.3536668087L-04
3.9533066135E-04	-/.0045141475E-05	-1.1055/49272E-04	1.7316542649E-04	-3.7941679943E-05
3.4359991920E-06	-2.66/8041687E-05	-2.1487433653E-06	-1.1241579062E-05	-4.4572486440E-06
1.2972858310E-05	-8.4412453816E-06	1.7494460968E-06	-3.4957851437E-06	2.6692000368E-06
U •	U.	0.	0.	0.
0.	0.	0.	0.	0.
2.1768191259E=02	-2.4905681967E=02	1.5795672242E-02	-2.0853744228E-03	-1.1576844695E-02
1.5130221368E=02		~1.3420360673E=03	7.1339364198E-03	5.2053059100E-03
-4.8813002996E=02		~1.009/8345/10E=03	-/.992124/9/4E-04	1.56/14566/3E-03
2.7003638074180=03	-1 (1503022)05-04	- 200202022102E-04	4 0 9 0 0 4 4 9 9 9 0 E = 0 4	-3.8823938234E-04
	-1.0780333021F_04	5-43107723646-05	-3.3001412307E-05	4 28501303166-06
-8-4471497979t=04	5.4248500054E=04	-4-9802666011E-06	2 24660469645-06	-1 7153007030E-06
0.		0.	0.	
0.	U.	0.	0.	0.
		- •		
1= 9 K=	5 J= 3			
SOLUTION				
	2 -2.2387836952E-02	1.2076782270E-02		-4.0589665232E-02
		-3-9543799990E=02	1 15669337326-03	-2.5072805880E-02
		3.6010/94141E-03	-4.74030390535-03	-6-57205257621-03
-0.00983237661E=03		L-5335906016E-03	1.1055012755E=03	=1-8507237613E=03
1.982314/150E-03	3 -3,9586043884E-04	4.1118612177E-04	-3.4216055746E-04	1.8257261385E-04
-4,9129047140E-05	-8.8/01419652E-05	1.4823286869E=04	-1.5931062478E-04	1.4871248730E-04
-1.0339469754E-04	+ 9.4482781766E-05	-4.3457547549E-05	3.0442202991E-05	-2.3444300240E-06
-1.0098519866E-05	6.5709562341E-06	-6.0324358360E-06	2.7212395973E-U6	-2.0777972715E-06
U.	U.	0.	0.	0.
υ.	υ.	0.	0.	0.
2.4561467850E-02	2 -2./323815593E-02	1.9082080719E-02	-2.8804859867E-U3	-9.9752285301E-03
1,5073541034E-02	2 -9./126983334E-03	-5.1692312260E-03	1.1987218517E-02	-1.3942042152E-03
1.4613693615E-0:	-4.1565548048E-04	8.5951507629E-05	1.0052761651E-03	-7.0491693420E-04
1.0509177043E-03	4.2827483650E-05	-1.0894028872E-03	9.4992929540E-04	-6.2294455630E-04
3.0810635758E-04	+ -1.3653974767E=06	-1.5965522834E-04	2.1025128652E=04	1.0143274047E=04
-6.0003867307E-0	5 5.5623413829E-05	-2.3297752748E-05	2.2356841655E-U5	7.1865501796E-07
1.1654313192E-0	-1.5832877428E-06	6.9618020734E-06	-3+1404//90/4E=06	2.3979058785E=06
0.	0.	0.	0.	0.
0.	0.	0.	0.	0.
N= 9 κ=	5 J= 4			
SOLUTION				
1.0650509070E-0	2 -2.2065379320E-02	8.4500518611E=03	1.9766434740E-02	-4.0012923223E-02
4.2553777384E-0	2 <b>-1.</b> 2260953121E-02	-2.9150357247E-02	4.6526152229E-02	-1.8957312373E-02
-1.5817692958E-02	2 1.8182923681E-02	-1.1/0699/462E=02	1.9550763331E-03	1 3457547872E-03
-1.0210598004E=0		2 6735037499630E-04	-0,30303435130E-03	-1.040761876E-U3
		10010045376 03	-2+3010246249E-04 -1 0077701346E 03	9 10006210405 04
1.4612925750E=04		1021400940076216-03	-1.07///U1048E-U3 _4.4040200533F_05	
J. UHUUHD/JODE-U/	+ 201700000000000000000000000000000000000	-J.4]40152070F=05		4_8766212366F=04
L 2024303237475-04		3-82671350016-04	=1.7262354026F=05	1,3180637284F=06
0.40003940196400	()(Z)](Z)](D)	()* 202011220015=00		0.
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U. 8231951947F=03	2 = 2 1610399030F=02	1.3515250013E=02	-3.2705178454E-03	-8.8677198544E-03
1.05032666831-0	2 ~8.4605527960E-03	-4. 3852686385E=03	8.7681236049E-03	-8.1296148045E-03
1.81/64948391-0	3 -5.8825740001E-03	2.8884422364E-03	-4.7070324767E-04	-1.1488612610E-03
1.1019343756E-0	3 -5.1889624807E-04	1.4709725580E-04	-6.7035113864E-04	4.8784479996E-04
		1 000000115355 00	-6 1022226615E-U5	3.00455812026-05
-2.8879155094E-04	4 1.0387957254E-04	/ • 982041133300-08		J. 004JJ01202L-0J
-2.8879155094E-04 -5.6348913945E-0	4 1.038/95/254E=04 5 1.5113/39125E=05	-3.0164015533E=05	7.8029843138E-07	-8,2867731501E-06
-2.8879155094L-04 -5.6348913945L-04 -1.4027313443L-04	4 1.0387957254E-04 5 1.5113739125E-05 5 9.1273636068E-06	-3.0164015533E-05 -8.3793337452E-06	7.8029843138E-07 3.7799282754E-06	-8,2867731501E-06 -2,8861569797E-06
-2.8879155094E-0 -5.6348913945E-0 -1.4027313443E-0 0.	4 1.0387957254E-04 5 1.5113739125E-05 5 9.1273636068E-06 0.	-3.0164015533E-05 -8.3793337452E-06 0.	7.8029843138E-07 3.7799282754E=06 0.	-8.2867731501E-06 -2.8861569797E-06 0.

N=	9	K= 5	=L	5			
N= 50LU 4 -2 -1 -6 -1 -5 -2 0 0 0 0 1 -5 -2 0 0 0 0 -1 -5 -2 0 0 0 0 0 0 0 0 0 0 0 0 0	Y TIUN .099593226 .187892653 .324737088 .589294752 .156059617 .370939559 .413953721 .454061471 .194618102 .017761544 .453355083 .692842650 .624997513 .544702774 .444689571 .526390418	k = 5 $3L - 02$ $IL - 02$ $IL - 02$ $IL - 02$ $IL - 03$ $5L - 04$ $4L - 05$ $6L - 03$ $6L - 03$ $6L - 03$ $6L - 03$ $8L - 03$ $4L - 05$ $1L - 05$ $1L - 05$	J= -2.20087812 -1.08262846 2.61573133 1.15652408 4.23307398 3.44028164 -1.17624378 4.40052778 1.42800526 0. 0. -7.85995498 -6.21375905 -1.91478631 -7.38818363 -9.78818416 -7.73043921 -9.93199475 0. 0.	5 299E-02 339E-02 339E-02 335E-02 331E-03 606E-04 355E-05 517E-04 355E-05 517E-04 355E-05 517E-04 328E-04 555E-05 555E-05 540E-06	9.9792678155E-03 -3.0653082346E-02 -1.7265152041E-02 2.0681152040E-03 -1.9793173518E-03 -8.9700837198E-04 -1.6584145617E-05 -2.3963099313E-05 -1.3109735947E-06 0. 0. 6.7827024333E-03 -3.88995254493E-03 -1.1428775592E-04 8.0941546818E-04 2.1613866192E-04 7.0467403555E-05 9.1180216308E-06 0. 0.	1.9660708087E-02 4.5749545454E-02 2.0958702716E-03 -8.4551744917E-03 -2.8884525523E-04 8.035588601E-04 6.8716351845E-05 1.3522589666E-05 5.9138188185E-07 0. -1.1329947590E-03 6.2546602728E-03 7.4991469554E-04 -6.8762824860E-04 -2.4484170664E-04 -1.8757077619E-05 -4.1131513347E-06 0.	-4.3512255597E-02 -2.1263976248E-02 1.1419732015E-62 6.3476087022E-03 1.2308503658E-03 -5.8155290527E-04 7.0266225591E-05 -2.3607942765L-06 -4.5154850082E-07 U. 0. -9.8639412225E-04 -3.4345466396E-03 -1.8483303860E-03 4.0458749378E-04 1.3108489798E-04 1.3108489798E-04 1.3817318775E-05 3.1405868070E-06 0. 0.
N=	9	K= 5	J=	6			
SOLU 1 4 -2 -1 -6 -1 -3 -2 0 -7 -3 -2 0 0 -7 -3 -2 -3 -2 -3 -2 -3 -2 -3 -2 -4 -4 -4 -5 -2 -2 -2 -2 -2 -2 -2 -2 -2 -2	T10N .U99593226 .187892653 .324737088 .89294752 .156059617 .370939559 .413953721 .454061471 .194618102 .617761544 .45335083 .692842650 .624997513 .544702774 .444689571 .526390418	3L-02 1L-02 9L-02 7L-02 1L-03 5L-04 4L-03 5L-04 4L-03 6L-03 6L-03 6L-03 6L-03 6L-04 8L-04 1L-05	-2.20087812 -1.08262846 2.61573133 1.15652408 4.23307398 3.44028164 -1.17624378 4.40052778 1.42800526 0. 0. 7.85995498 6.21375905 1.91478633 7.38818365 9.78814116 7.73043921 9.93199475 0. 0.	299E-02 59E-02 339E-02 339E-02 331E-03 406E-04 375E-04 557E-05 517E-06 318E-03 517E-04 104E-03 328E-04 555E-05 540E-06	9.9792678155E-03 -3.0653082346E-02 -1.7265152041E-02 2.0681152040E-03 -1.9793173518E-03 -8.9700837198E-04 -1.6584145617E-05 -2.3963099313E-05 -1.3109735947E-06 0. 0. -6.7827024333E-03 3.8995254493E-03 3.8995254493E-03 1.1428775592E-04 -8.0941546818E-04 -2.1613866192E-04 -7.0467403555E-05 -9.1180216308E-06 0.	1.9660708087E-02 4.5749545454E-02 2.0958702716E-03 -8.4551744917E-03 -2.8884525523E-04 8.0355888601E-04 6.8716351845E-05 1.3522589666E-05 5.9138188184E-07 0. 1.1329947590E-03 -6.2546602728E-03 -7.4991469554E-04 6.8762824860E-04 2.4484170664E-04 1.8757077619E-05 4.1131513347E-06 0.	-4.3512255597E-02 -2.1263976248E-02 1.1419732015E-02 6.3476087022E-03 1.2308503658E-03 -5.8155290527E-04 7.0266225591E-05 -2.3607942765E-06 -4.5154850081E-07 0. 9.8639412226E-04 3.4345466396E-03 1.8483303860E-03 1.8483303860E-03 -4.0458749378E-04 1.3108489798E-04 -1.3817318775E-05 -3.1405888070E-06 0.
N=	9	к= <u>:</u>	= L	7			
SOLU 1 4 -1 -1 -1 -5 -1 -1 -1 -1 -1 -1 -1 -1 -1 -1	T10N 065050907 255377738 581769295 021059800 446975431 461292575 040045736 243052574 406059401 823195194 050326648 8817649483 101934375 887915509 634891394 402731344	0L=02 4L=02 8L=02 4L=02 9L=03 0L=04 9L=04 9L=04 9L=04 3L=02 3L=02 3L=03 5L=03 3L=05	-2.20653792 -1.2260953 1.81829236 7.75617115 -1.06930821 4.62728004 2.1493150 -1.02909366 -4.16832729 0. 0. 0. 2.16103990 8.46055275 5.88257400 5.18896248 -1.0387957 -1.51137391 -9.12736360 0.	320E-02 121E-02 508E-03 186E-03 186E-03 186E-04 556E-04 556E-04 914E-06 030E-02 960E-02 960E-03 001E-03 307E-04 254E-04 126E-05 068E-06	8.4500518612E-03 -2.9150357247E-02 -1.1706997462E-02 2.2357299629E-03 7.67359937429E-04 1.2140094537E-03 -3.2516457641E-05 5.4149153979E-05 3.8267135001E-06 0. 0. -1.3515250013E-02 4.3852686385E-03 -2.8884422364E-03 -7.4709725580E-04 -7.9820411535E-06 3.0164015533E-05 8.3793337452E-06 0.	1.9766434740E-02 4.6526152229E-02 1.9550763331E-03 -6.3655435130E-03 -2.3010246249E-04 -1.0977701348E-03 -4.3049299533E-05 -3.1956501305E-05 -1.7262354026E-06 0. 3.2705178455E-03 -8.7681236049E-03 -8.7681236049E-03 4.7070324767E-04 6.7035113864E-04 5.1933226615E-05 -7.8029843143E-07 -3.7799282754E-06 0.	-4.5512923231-02 -1.89573123731-02 7.81901578721-03 -1.34576478761-03 9.91489761271-05 8.19905310501-04 -1.63812678301-04 4.87662123661-06 1.31806372841-06 0. 8.86771985441-03 8.12961480451-03 1.84886126101-03 -4.87844799961-04 -3.00455812021-05 8.28677315011-06 2.88615697971-06 0.

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N= 9	ĸ	= 5	J= 8			
N= 9 SULUTI 1.1 4.0 -0.0 -4.0 -0.0 -1.0 -0.0	K UN 45959676767E 1072561404E 1366819318E 1898525008E 1823147150E 1229047140E 1339469754E 1098519866E 1073541034E 1613693615E 10035758E 1003867307E	= 5 -02 -03 -04 -03 -04 -05 -04 -05 -04 -05 -02 -02 -03 -04 -05 -04 -05 -04 -05 -04 -03 -03 -04 -03 -04 -03 -04 -05 -02 -04 -05 -04 -05 -05 -05 -04 -05 -05 -05 -05 -05 -05 -05 -05 -05 -05	J= 8 -2.2387836952E-02 -8.3103307369E-03 4.2946511645E-03 -6.0126735994E-04 -3.9309461653E-03 -3.9586043884E-04 -8.8701419652E-05 9.4482781766E-05 6.5709562340E-06 0. 2.7323815593E-02 9.7126983334E-03 4.1565548047E-04 -4.2827483650E-05 1.3653974766E-06 -6.5623413829E-05	1.2076782270E-02 -3.3143759936E-02 -3.8583280359E-03 3.6010794141E-03 1.5335906016E-03 4.1118612177E-04 1.4823286869E-04 -4.3457547549E-05 -6.0324358360E-06 0. 0. -1.9082080719E-02 5.1692312260E-03 -8.5951507627E-05 1.0894026872E-03 1.5965522834E-04 2.3297752748E-05 -0.00272148E-05	1.8647967895E-02 4.5847568406E-02 1.1544833732E-03 -4.7403039053E-03 1.1055012755E-03 -3.4216055746E-04 -1.5931062478E-04 3.0442202991E-05 2.7212395973E-06 0. 2.8804859867E-03 -1.1987218517E-02 -1.0052761651E-03 -9.4992929540E-04 -2.2356841655E-05	-4.0589665232E-02 -2.3672883886E-02 -1.6532102407E-04 -6.5720525762E-03 -1.8507237613E-03 1.8257261384E-04 1.4871248730E-04 -2.3444300239E-06 -2.0777972715E-06 0. 9.9752285301E-03 1.3942042152E-03 7.0491693420E-04 6.2294455630E-04 -1.0143274047E-04 -7.1865501796E-07
-1.1 U.	.6543131926	-05	U.	-6,9618020734E-06 0.	0.	-2.3979058785E-06 0.
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SOLUTI 1.00 4.2 1.00 7.3 5.2 4.2 3.5 5.2 4.2 0.5 0.5 0.5 0.5 1.4 -1.5 4.8 1.4 -2.4 0.5 0.5 0.5 0.5 0.5 0.5 0.5 0.5	UN 1478234916E 2327082674E 353517551E 3559751448E 2941661723E 2941661723E 2941661723E 2942651723E 1468191259E 1468191258E 146819158E 14681958E 14681958E 1468195	-02 -02 -02 -03 -03 -04 -04 -05 -02 -02 -02 -03 -03 -04 -04 -06	-2.2378225620E-02 -1.2607310127E-02 -1.0945171924E-02 -4.3979526683E-03 -4.2752639653E-03 -5.0443436693E-04 -7.0045141475E-05 -2.6678041687E-05 -8.4412453815E-06 0. 0. 2.4905681967E-02 1.1761649501E-02 -3.1473926475E-03 -4.1742729187E-04 1.7159392219E-04 1.0780333021E-04 -5.4248590054E-06 0.	<pre>/**/154245587E=03 /************************************</pre>	1.9274466363E-02 4.7626833308E-02 -3.7050746662E-04 3.9566859980E-03 -6.8499664652E-04 1.0723956028E-03 1.7316542649E-04 -1.1241579062E-05 -3.4957851437E-06 0. 2.0853744228E-03 7.1339364198E-03 7.9921247974E-04 -4.6985449993E-04 5.6165558876E-05 3.3901412307E-05 -2.2466046964E-06 0.	-4.6362432110E-02 -1.7376967289E-02 -4.2393818654E-03 -5.6695995871E-03 -7.7640565377E-04 -7.3536568087E-04 -3.7941679943E-05 -4.4572486440E-06 2.6692000368E-06 0. 1.1576844695E-02 -5.2053059100E-03 -1.5671456673E-03 3.8823938234E-04 1.7095259325E-04 -4.2859130316E-06 1.7153907039E-06 0.
N= 9	к	= ك	J= 10			
SOLUTI 1.0 4.5 2.0 1.0 -3.5 -4.2 -6.2 1.0 0. 0. 0. 0. 0. 0. 0. 0. 0.	LUN J99155//86E 5031209400E J1348172//E 24/42//546E 33108555/E 321155544E 2287901206E 08/5659556E +/96212925E 3047454362E 5290549022E (9406536/E 4635342154E 357181326/E 578460499/E 3445601100E	-02 -02 -02 -03 -04 -05 -04 -05 -02 -03 -03 -03 -03 -04 -05 -06	-2.04209629/5E-02 -1.290483688/E-02 -2.3/609/8218E-02 -1.02109923/3E-02 2.9261168932E-03 -2.2764599590E-05 1.0755966/91E-04 -5.2038095412E-05 9.6276/50303E-06 0. 1.4489487/96E-02 6.9119601981E-03 -4.6864128841E-03 -3.2962369350E-04 -1.9700373284E-04 -8.0391374475E-05 2.8269404543E-06 0.	9.8033800663E-03 -2.8980829855E-02 1.4676482225E-02 -3.4400/13524E-03 -1.9228273982E-03 -6.6283818478E-05 -1.1585536072E-04 5.4144/73691E-05 -8.8386423226E-06 0. 0. -9.5964089946E-03 2.3600605828E-04 2.2883799417E-03 -1.3743971933E-03 -8.8647650010E-06 4.3279604757E-05 -2.5952595475E-06 0.	2.2702152185E-02 4.1777919639E-02 3.1152659770E-03 8.3730078336E-03 5.3157732919E-04 3.8031790298E-05 1.0925829788E-04 -1.1444551180E-05 3.9871229679E-06 0. 0. 7.6000731034E-04 -3.9426324121E-03 2.2861068220E-04 1.2342949280E-03 9.0250026771E-05 -2.4791500892E-05 1.1707249340E-06 0.	-4.4365245904E-02 -2.3634343456E-02 -1.0440297940E-02 3.7732047861E-03 -4.9992215114E-05 2.5503833635E-05 -9.0049372291E-05 1.1587965863E-05 -3.0443600895E-08 0. 0. 6.6730820094E-03 -6.9485633317E-03 -1.2229973932E-03 -9.0093988140E-04 4.1432443924E-06 -8.9390477632E-07 0.

N= 9 K= 6	J≈ 0			
SOLUTION				
1.0185350928E=02	1.5187677508E-02	-4.6307077469E-03	-3.4716256251E-02	-3.6068102114E-02
-5./250309519E-03	3.6903767479E-02	4.7801859971E-02	3.3083647277E-03	-3.2246923551E-02
2.8813058669E=02	2.4803055321E-02	1.1685444906E-02	-9.1593184841E-03	-1.1871255498E-02
-7.4127322519E-03	8.0193648248E-03	1.0529302464E-02	6.1702629292E-03	9.4053428272E-03
8.0029090889E-03	3.2688926719E-03	4.6929615749E-04	-1.7492270766E-03	-6.5057157717E-04
8.9184299807E-04	1.8932441025E-03	1.4442419113E-03	1.0926359511E-03	2.2651263934E-04
-4.6803433217E-05	-4.4627731036E-04	-1.9327299015E-04	-1.6252153623E-04	2.0379007272E-04
1.0948452447E=04	4.7307818947E-05	-2.0442551631E+05	-3.0363683223E-05	-3,7600713506E-05
3 • 3 4 8 4 1 4 8 1 3 0 E = 0 3			3.2421009831E-06	2.2212/88959E-06
1.00090712040=00	1.00/21089012=08	0 0 0 0 0 0 0 1 0 0 0 1 0 0 1 0 0 1 0 0 1	4.3222269040E=07	_ <b>U</b> •
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Ο.	0.	0.	0.	0.
N= 9 K= 6	J= 1			
SOLUTION				
1.0953570412E-02	1.9276485089E-02	-1.6202149088E-03	-2.7367212023E-02	-3.3683382678E-02
6.1681390793E-04	3 <b>.</b> 4954404599E-02	4.8584115206E-02	-8.3513938436E-03	-4.3363185762E-02
2.2191572754E-02	2.1299441126E-02	4.0499929567E-03	-9.6547512036E-03	-1.7130521476E-02
-8.8613382301E-03	2.5499454673E=03	7.6491783643E=03	4.4247757476E-03	5.4407226468E-03
3.548/811552E-03	1.89421744655-03	-9.0686774705E-04	~1.16/4688895E=03	-1.4069528941E-03
		5.00101047155.07	3.0444483919E-04	5.01705/081E-04
=1 - /8405209/2t=05	_H_(19849/4096F_07	2-23280708785-05	1 9861411611E-05	2 0570752738E_05
-2.60352631765-05	=1,1113390411E=05	-1-0995442956E=05	-2-1241196841F=06	-1-8937591138E-06
-1.80299/3262E-06	-1.6187647329E-06	-5.6786259998E-07	-4.1966308455F-07	0.
0.	U.	0.	0.	0.
1.2240855215E-02	1,1783129590E-02	3.2357680662E-03	-4.0458826703E-03	-7.8861187614E-03
-3.3752997070E-03	1.9063891620E-03	5.4027114104E-03	1.7078360829E-03	7.4997509818E-03
5./330036051E-03	2.2497013016E-03	-6.8003616793E-04	-2.0768988480E-03	-1.5828334689E-03
-2.3362349065E-04	5.6599701/47E-04	1.8894584510E-03	1.2891550994E-03	6.7741157618E-04
6.2/1353/058E-05	-1.4725033842E-04	-2.1284058538E-04	-4.449053060E-05	2.5763547504E-04
1.7612977521E=04	1.0035612115E-04	3.3891536353E-05	3.5776328896E-06	-9.6849809880E-06
1.7513001929E=05	1.3458357064E-05	6.4244419855E-06	3.3779601589E-06	5.3533841063E-07
4.4439892801E=07	3.9898967210E-07	1.3996556014E-07	1.0343766027E-07	0.
υ.	U .	0.	0.	0.
N= 9 K= 6	J= 2			
SOLUTION	L. /351/581/5E=02	-4,1231401132E-03	-3,0675206901E-02	-3-6242183682E-02
-1.8118205089E=03	3.4805134/20E-02	4-9320662402E-02	-2.4137318141E-03	-3.6559047501E-02
1.5599319988L-02	1.2607360/90E-02	4.9846503318E-03	-7.1600949185E-03	-8,9339443470E-0
-5.7253412436E=03	2.3648903991E-03	6.1123291840E-03	1.9171269304E-03	-3.6123883555E-0
-2,3609904022E-03	-1.5125084425E-03	3.5035284101E-04	3.5635459927E-04	6.1310701884E-0
-3.5702092026E-04	-5.0807151447E-04	-1.9601475449E-03	-1.5057974154E-03	-7.4972112351E-04
-2.5573808524L-04	1.2095624305E-04	1.0685120352E-04	7.6135249174E-05	-1.9621702372E-04
-1.2997180309E-04	-/.1949017485E-05	-1.9207885653E-05	1.9146516910E-06	1.1560787725E-0
1.8/44059254E-06	-6.0604934017E-07	3.9700141867E-06	-6.5007550605E-07	1.0625040212E-0
1.6442538760E-06	1.4762418933E-06	5.1786559387E-07	3.8271418564E-07	0.
	U. PODE()-73315 03	U	U. 50966507405 03	
201820413519E=02	1009000710215-02	200204004071E-U3 8-7820006034F-03		8.6867702218F=0
- 107277033480L=V3	2 / 903688706F_03	=8_2500130210F=04	-2,1321891855F-03	=1.7932017797F=0
-8-2/17037913E=05	1.3774281006E=04	3_U350386156E-04	1.8026933970E-04	2.0117036422E-0
-/.49408/5068E-05	-1,1822621585E-04	-7.8411445297E-05	-3.0031849425E-05	-2.0165419205E-0
-1.45/3267/09E-04	-8.7014866377E-05	-3.8997/50682E-05	-1.1560727900E-05	-3.2120706052E-0
-2.5679126284E-05	-2.0497267286E-05	-9.2963194647E-06	-5.2017493799E-06	-6.9079758639E-0
-8.6297100565E-07	-1.7479151473E-07	-2.7179683067E-07	-2.0086389971E-07	0.
U .	U .	0.	0.	0.
		77		
		í t		

٢	1=	9	к=	6	J= 3			
ç		UTION						
		1.0502213	3792E-0	)2	1.6619312560E=02	=3.3638769299E=03	-3.2172768332E-02	-3.4951709682E-02
	-	3.6136022	2004E-0	13	3.6430275553E-02	4.7859283513E-02	-8.6211463762E-04	-3.6447013636E-02
		3.2892126	5449E-(	33	5.1995600027E-03	1.1866904554E=03	1.8908561977E-03	-1.4338782256E-03
	~	1 9463874	4289E-0	בר גו	2 9861676094E 03	3 3008433006E-03 8 1848037024E 05	-/•U424428647E=U5	-9.0345681260E-03
	_	4.0403947	74406-0	)4	-2,9881878094E=03		_1.7390418291E=03	-1.00387611948-04
		1.9954581	1688E-0	)4	1.0841708510E-04	1.8359030563E=04	-7.3137609737E-06	2.0234335330E=04
		1.2101/37	7579E-0	)4	6.U206166664E-05	-8.0109140286E-07	-1.6451993055E-05	-2.4980176361E-05
		1.2257962	2481F-6	5	1.3314966445E-05	3.8640137193E-06	3.6333099761E-06	-1.0610416255E-07
	-	1.3899523	3672E-0	16	-1.2479252408E-06	-4.3/77212181E-07	-3.2352332937E-07	0.
		U	count i	12				
	_	6 33548820	3930E-1	גר גר	2.0018382187E-02	1 14305/27165 02	-/.01/2100912E-00	-1.0465285714E=02 2.3647622775E 63
		2.2064990	3537E-0	13	9.5270942481E-04	4.7894204947E-04	-1-5034781299E=04	2.0864575363E=04
		5.6316202	2031E-0	)4	8.0482502230E-04	-1.5643048962E-03	-9.4642500485E-04	-4.4546945175E-04
		1.3989915	5225E-(	)4	2.3473030264E-04	2.8422946712E-04	4.3069965527E-05	-8.7023957995E-05
	-	4.243405	730/E-0	5	-1.5558687507E-05	1.5569578122E-05	1.771245546E-05	2.0390646588E-05
		1,9886116	6373E-0	5	1.7905797471E-05	6.8688053035E-06	4.6904919563E-06	2.8399795362E-07
		1.2313903	3452E-0	56	1.1055652908E=06	3.8783225735E-07	2.8661665941E-07	0.
		0.			U.	U•	0.	0.
1	4 =	9	κ=	ь	J= 4			
	SOL	UTION						
		1.0969544	4073E-0	52	1.8908108841E-02	-1.5129434933E-03	-2.8082100906E-02	-3.3397570410E-02
	-	1.4859592	2642E-0	14	3.5501940150E-02	4.8128522797E-02	-7.4574589645E-03	-4.2909446160E-02
	-	9.154738	15/3E-(	03	-1.0215225129E-02	-3.4135248422E-03	1.5021099887E-03	4.6624527533E-03
		1.3864450	0389E-(	03	-2.9234413059E-03	-4.0335687085E-03	-2•4412169944E-03	-6.8487627753E-03
	-	4.9080902	20076-0	35 34	-2.000417109725-03	9 • 7852055811E-04	0 3844538109E-04	1.7586230549E=03
	_	9.446050	1398F-(	0-4 05	-2.0703004799E-04	-2-4368847366E-04	-5,7367414051F=05	6-5095671665E=05
		5.115899:	3252E-0	05	3.9608/67581E-05	2.9559294669E-05	1.5653635889E-05	1.0856825866E-05
	-	2.4543337	7417E-0	05	-2.0420870305E-05	-8./500660610E-06	-5.2421807137E-06	-5.5769018675E-07
		1.0548718	8791E-(	96	9.4708370932E-07	3.3223692527E-07	2.4553047315E-07	0.
		0.			U.	0.	0.	0.
		2.5189019	9854E-0 0770E	12 	2.0995805441E-02	7.4023874614E-03	-1.1/29/60689E-02	-1.5248587753E-02
	_	4.9130810	6120L-1 4462F-1	05 03	-1.//060/3531E=03	8.6523270188E=03	4.3910081343E=03	-3.9877368833E-03
	-	6.126225	5862L-0	5	-/.28158/6359E-04	-1.0014/12643E-03	-8.7656416746E-04	-4.0585041309E-04
	-	2.4/28869	9013E-0	04	4.9371580542E-05	-1.5681896838E-05	6.0432600055E-05	2.4245711937E-04
		1.5283211	1597E-0	94	8.0552626460E-05	1.1430/53131E-05	-1,1009124037E-05	-2.2081213751E-05
	-	2.6005360	0999E-0	06	-1.2774098414E-06	-9.6496063106E-08	-2.2214410671E-06	5.7215242826E=07
	~	1.528245	7538E-0	56	-1.3720876307E-06	-4.8132828295E-07	-3.5571230067E-07	0.
		0.			0.	0.	U.	0.
I	¥=	9	K =	ь	J= 5			
:	50L	UTION						
	-	1.013171	1680E-	02	1.6535442021E-02	-5.0018369329E-03	-3.2103695009E-02	-3.7085564233E-02
	-	2.935595	3940E-	603	3.4921488778E-02	4.9447005120E-02	2.8932356854E-05	-3.3937888387E-02
	-	-1.9941827	2261E-	02		-5.5220857061E-03	2 0535440040E 03	1,2511799949E-U2
		H 6/5160	9097E- 0564E-	05	5.1854200300F=04	-1.1021100412E=05	-1.0379889642E-04	-1-4377535959F=04
		1.636130	7045E-	Ŭ4	2.2511081355E-04	1.1473080481E-03	7.8914502469E-04	4.50560255661-04
		1.0478304	4/44E-	05	-4.6935227068E-05	-1.1291454136E-04	-1.5361645242E-05	-2.7469909327L-04
	-	-1.907742.	2648E-	04	-1.1020559525E-04	-4.0854416215E-05	-7.1291026651E-06	7.3368129788E-06
		2.320780	3613L-	05	1.8085878757E-05	8.4/27120244E=06	4.5582268248E-06	6.7840976193E=07
	-	0.584860	1169E-	υï	~>•9120111519E~07	-2+U139332626E-07	~1.0002082/831E=0/	
		U.	30541-	02	U. 1.6272820331E=02	0. 3.2067926256E=03	-6.8793247230F-03	-1.2472/50239E-02
	-	6.520240	1524E-	03	2.4467756500E-03	5.2525189403E-03	4.0318286255E=03	-9.5385579548L-03
	-	6.821335	0206E-	03	-3.4203698865E-03	8.3802887343E-04	1.7942888386E-03	1.7689539961E-03
		-3.441610	1448E-	04	-1.0662131192E-03	1.7465953375E-03	1.2890120838E-03	7.2319424351E-04
		2.1518/4	8321E-	04	-4.0746006360E-05	-1.0845537582E-04	=3.4639070769E=05	-8.3298712763L-05
	-	-6.416356	3247E-	05	-4.0206212247L-05	-2+2388311886E-05	-9.1866221403E-06	-4.1114424127E-06
	-	-1./84186	1/14た <del>い</del> ()7ムフトー	05 06	-J 00000094778E-06	-100201411230E-U0 504685125030F-07	-00121332805E-01 4,04135235065E-07	-1.JZUY187246E-06
		1002020	UTTL-	00		0.	U.	0.
		~ •			- •			

N= 9	K= 6	J= 6			
E ( 1) 1 17 1 ( 16)					
SULUTION	R1/03F-02	1. 70425733456-02	-2.20350520715-03	-2 07711705005 02	3 40475400721 02
-1.576965	01193L-03	4 59705407605-112		-2.9771178099E-02	-3.404/3499/2E-02
-2.5/900	43031-02	-2-3872716823E-02	-7.1284456485E-03	9.4417325529E_03	1 6159719006E=02
1.926319	77220F=03	-4-1791633563E=03	-101207790789E=09	-3.9619457216E-03	9.12572436966=02
6-19321	50651-03	2-5056413637E=03	=6.9086910092E=04	=2.1411401952E=03	-1 64780810576-03
-1.529044	4249E-04	6.8519663457E-04	-1.4057440605E-03	-9-5865212311E-04	-4-9259U80483F-04
-3.854256	56902E-05	1.2205988083E-04	1.6228881988E-04	3-6824729036F-05	1.5476169801E-04
1.050679	J1927E-04	5.9495618760E-05	1.9197303539E-05	1.3332381396E-06	-6.5536461940F-06
-9.402636	52942E-06	-1.1724193832E-06	-3.4579059680E-06	-1.7962438906E-06	-2.9399976801L-07
2,238314	44121E-07	2.0096006116E-07	1.0496/80975E-08	5.2098688232E-08	0.
υ.		υ.	0.	0.	0.
8.495484	42429E-03	6.4305184793E-03	5.8738048707E-03	-1.2686702011E-03	4,9906009812E-04
<del>-</del> 6•384288	38232L-04	4.3944942828E-03	3.0018177185E-03	2.4140834592E-03	-4.3463728189E-03
-4.075400	57134E-03	-1.5210395378E-03	-6.3926430392E-04	7.3508055461E-04	-7.3374817142E-05
-6.419016	54679E-04	-1.1753052299E=03	8.4921479080E=04	6.5559482329E-04	4.4990219153E-05
-1.448399	94789E-05	-3.6116972064E-04	-1.3426518759E-04	-1.2919845660E-04	-1.6231973084E-04
-8.41/110	5/2/9E=05	-3.4419395367E-05	2.108/361890E=05	2.7560158185E-05	3.2993626465E-05
3.141060	5/12/E-05	1.4605912446E=05	1.30/1038506E=05	2.9529717453E=06	2.1368/503/1E-06
-1.84341	181126-06	-1.6550550059E=06	-5.8059322624E=07	-4.2907130035E-07	0.
0.		0.	0.	0.	0.
N= 9	K= 6	J= 7			
SOLUTION			3 30350530714 03		
1.07751	31793E-02	1.7962573365E-02	-2.2835952971E-03	-2.9771178599E-02	-3.4047549972E-02
-1.07696	29880E-03	3.0879049769E=U2	4.8023404979E=02	-4.7303419521E-03	-4.0231031098E-02
-2.57900	14303E=02	-2.038/2/10823E-U2	-/ 1284420482E-03	9.441/323528E-03	0.12572424045 02
6 10321	97220E-03	-4.1/91033343E=03	-1.0090004020E=02	-3.9018437210E-03	8 • 120 (24080E=00)
0.193213	647405 06		-0.9084910092E=04		
-1.02904	44249L=04 66002E=05	1 22050880835.04	1 62298910895-04	3 6924720036E-05	1 5476160901E-04
1.05067	00902L=09	5.9495618760E=05	1.01073035306-05	1-3332381306E=05	-6-5536461930F=06
-9.40264	620425-06	= ( 1724) 93832E=06	-3-4579059680E-06	_1_7962438906E=06	=2.9399976800F=07
2.23831	441211-007	2.0096006116E=07	7.0496/80974E=08	5-2098688232E=08	0.
U.		U.	0.	0.	Ŭ.
-8.49548	42429E-03	-6.4305184/93E-03	-5.8/38048707E-03	1.2686702011E-03	-4.9906009811E-04
6.384281	88232E-04	-4.3944942829E-03	-3.0018177185E-03	-2.4140834592E-03	4.3463728189E-03
4.07540	67134E-03	1.5210395378E-03	6.3926430392E-04	-7.3508055461E-04	7.3374017140E-05
6.419010	646/9E-04	1.1753052299E-03	-8.4921479081E-04	-6.5559482330E-04	-4.4990219154E-05
7.448399	94789E-05	3.6116972064E-04	1.3426518759E-04	1.2919845660E-04	1.6231973084E-04
8.417110	67279E-05	3.4419395367E-05	-2.1087361890E-05	-2.7560158185E-05	-3.2993626465E-05
-3.141060	67127E-05	-1.4605912446E-05	-1.3071038506E-05	-2.9529717453E-06	-2.1368750371E-06
1.84341	18112E-06	1.6550550059E-06	5.8059322624E-07	4.2907130035E-07	0.
υ.		υ.	0.	0.	0.
N= 9	K= 0	J= 8			
COL 117 1 ON					
SULUIION	116805-02	1-65354420211-02	-5.0018369328F-03	-3.2103695009F-02	-3.7085564233E-02
-2 04550	530405-02	3 4021489//8E_02	4-9447005120E=02	2.8932356873E=05	-3-3937888387E=02
-2,75559	222611-02	-1,7419947627F=02	-5.5220857061E-03	8-5598066249E=03	1.2611799949E=02
7.15339	/909/1-03	-/- 4070152/25E-03	-7. (027/88472E-03	-2,9535469980E-03	1.2266008279E-03
8.62516	40564E-04	5.1854200300E-04	-4.7652667819E-05	-1.0379889642E-04	-1.4377535959E-04
1.63613	07045E-04	2.2511081355E-04	1.1473080481E-03	7.8914502469E=04	4.5056025566L-04
1.04783	04/45E-05	-4.6935227068E-05	-1.1291454136E-04	-1.5361645242E-05	-2.7469909327E-04
-1.90774	22648E-04	-1.1020559525E-04	-4.0854416215E-05	-7.1291026651E-06	7.3368129788E-06
2.32078	03613E-05	1.8085878757E-05	8.4727120244E-06	4.5582268248E-06	6.7840976192E-07
-6.58486	07169E-07	-5.9120111518E-07	-2.0739332626E-07	-1,5326827831E-07	0.
υ.		U .	0.	0.	0.
-1.66729	63054E-02	-1.6272820331E-02	-3.2067926256E-03	6.8793247230E-03	1.2472750239E-02
6,52029	01524E-03	-2.4467756500E-03	-5.2525189403E-03	-4.0318286255E-03	9.5385579548E=03
6.82133	50206E-03	3.4203698865E=03	-8.3802887343E-04	-1.7942888386E-03	-1.7689539961E-03
3.44161	01448E-04	1.0662131192E=03	-1.7465953375E-03	-1.2890120838E-03	-7.2319424351E-04
-2.1518/	48321E-04	4.0746006360E-05	1.0845537582E-04	3.4639070769E-05	8.3298/12/63E-05
6.41635	63246E-05	4.0206212246E-05	2.2388311886E-05	9.1866221402E-06	4.11144241271-06
1.78418	61714E-05	5.8083694578E=06	1.828/4/1236E=06		10209181246E-06
-1.73628	50/42E-06	-1.5588092248E-06		-400413523598E-07	0.
0		U #	Ve	U 0	V e

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6011	17 1 ( ) b(						
SULU		3726 0	12	1 HOURI (188415 02	1 61204240225 02	3 000310000/E 03	2 2207170/105 02
	L 60709099999	010L-0	ν. 	1.09081088416=02		⇒2.8082100906E=02	=3,3397570410E=02
-	1048797920	544E-V	)4 )	3.5501940150E=02	4.8128522797E-02	-/ •45/4589645E-03	-4,2909446160E=02
-	9° (24 (281)	973E-U	13	-1.0215225129E-02	-3.41352484226-03	1.50210998876-03	4.6624527533E=03
	1.3864450	389E-C	13	-2.9234413059E-03	-4.0335687085E-03	-2.4412169944E-03	-6.8487627753E-03
	+.9085902	607E-0	33	-2.0541710972E-03	9.7852055812E-04	1.9457006741E-03	1.7586230549E-03
3	3.9819681	883E-C	)4	-2.6763064799E-04	1.4731835462E-03	9.3844588198E-04	4.0801239414E-04
- 9	9.4960507	398E-C	15	-2.3932781506E-04	-2.4368847366E-04	-5.7367414051E-05	6,5095671665E-05
	o.7758993	252E-C	15	3.9608/67581E-05	2.9559294670E-05	1.5653635889E-05	1.0856825866E-05
- 6	2。4543337	41/L-C	)5	-2.0420870305E-05	-8.1500660610E-06	-5.2421807137E-06	-5.5769018675E-07
1	1.0548718	791E-C	16	9.4708370932E-07	3.3223692527E-07	2.4553047315E-07	Ο.
(	J.			υ.	0.	0.	Ú.
- 2	2.5189019	854E-L	15	-2.0995805441E-02	-1.4023874614E-03	1.1729760689E-02	1.5248587753E-02
4	9.9150818	128E-C	13	-4.0506179778E-03	-8.6523270186E-03	-4.3910681343E-03	5.9877568853E-03
4	4.9821364	962E-L	13	1.7706073531E=03	-1.249297342/E-04	-1.6397825494E-03	-9.0774604810E-04
(	6.1262255	899E-L	)7	/.2815876359E-04	1.0014/12643E-03	8.7656416746E-04	4.0585041309E-04
	2.4/28869	0136-0	)4	-4.9371580543E-05	1.5681896837E-05	-6.0432600055E-05	-2.4245711937E-04
•	1.5283211	597E-C	)4	-8.0552626460E-05	-1.1430/53131E-05	1.1009124037E-05	2.2081213751E-05
4	2.6005360	998E-C	)6	/.2774098414E=06	9.6496063092E-08	2.2214410671E-06	-5.7215242826E-07
	1.5282457	538E-C	)6	1.37208/6307E=06	4.8132828295E=07	3.5571230067E-07	0.
(	) <b>.</b>			υ.	0.	0.	0.
N=	9	К=	ь	J= 10			
SOLI	JTION						
	1,0502213	792E-C	12	1.6619312560E-02	-3.3638/69299E-03	-3.2172768332E-02	-3.4951709682E-02
~.	3.6136022	004E-(	13	3.6430275553E-02	4.7859283513E-02	-8.6211463766E-04	-3.6447013636E-02
	3.2892126	4496-0	13	5.1995600027E=03	1.1866904554E=03	1.8908561977E-03	-1.4338782256E-03
	188268829	289E-L	73	1.0851016539E-03	3.3008433006E-03	-7.0424428641E-05	-9.0345681260E-03
	1.3363874	489E-(	13	-2∘9861676094E-03	8.1848037923E-05	1.9849662461E-03	1.1520920742E-03
-	4.0903947	44UE-(	)4	-1.3573398623E-03	-5.0597/50318E-04	-1.7390418291E-04	-1.0038761194E-04
	1.9954581	688F-(	)4	1.0841708510E-04	1.8359030563E-04	-7.3137609738E-06	2.0234335330E-04
	1.2101737	519E-(	)4	6.U206166664E-U5	-8.0109140285E-07	-1.6451993055E-05	-2.4980176361E-05
	1.2257962	981E-U	15	1.33149664452-05	3.8640137193E-06	3.6333099781E-06	-1.0610416255E-07
	1.3899523	612E-0	)6	-1.2479252408E-06	-4.3777212181E-07	-3.2352332937E-07	Û.
(	0.			Ο.	0.	0.	Ο.
-	2.6646856	930E-U	12	-2.6018382187E-02	-/.9/26/10058E-03	7.5172133912E-03	1.5465285714E-02
	6.3354868	568E-(	13	-5.4281139848E-03	-1.1439522716E-02	-4.6247755387E-03	-2.3467622775E-03
	2.2064990	537E-0	13	-9.5270942481E-04	-4.1894204947E-04	1.8034781299E-04	-2.0864575363E-04
-	5.6316202	031E=0	)4	-8.0482502230E-04	1.5643048962E-03	9.4642500485E=04	4.4546945175E-04
-	1.3989915	225E-0	)4	-2.3473030264E-04	-2.8422946712E-04	-4.3069965527E-05	8.7023957995E-U5
	4.2434051	307E-0	05	1.5558687507E-05	-1•5569578122E-05	-1.7771245546E-05	-2.0390646588E-05
-	1.9886116	3/3E-(	05	-1. /905/974/1E-05	-6.8688053035E-06	-4.6904919563E-06	-2.8399795362E-07
-	1.2313903	452E-0	16	-1,1055652908E-06	-3.8783225736E-07	-2.8661665941E-07	Ο.
	υ.			Ue	0.	0.	0.
N=	9	к=	6	J= 11			
50L	UTION						
	1.0347575	223E-(	02	1./351/581/5E-02	=4.1231401131E=03	-3.0675206901E-02	-3.6242183682E-02
-	1.8118205	089E-(	03	3.4805134720E-02	4.9320662402L-02	-2.4137318142E-03	-3.6559047501E-02
	1.5599319	988F-(	02	1.2607360790E-02	4 <b>.</b> 9846503318E=03	-7.1600949185E-03	-8.9339443470E-03
-	5.7253412	436E-(	03	2,3648903991E-03	6.1123291839E-03	1.9171269304E-03	-3,6123883555E-03
-	2.3609904	021E-0	03	-1.5125084425E-03	3.5035284102E-04	3.5635459927E-04	6.1310701884E-04
-	3.5702092	026E-0	04	-5.0807151447E-04	-1.9601475449E-03	-1.5057974154E-03	-7.4972112351E=04
-	2.5573808	524E-1	04	1.2095624305E-04	1.0685120352E-04	7.6135249174E=05	-1.9621702372E-04
-	1.2997180	309E-1	04	-1.1949017485E-05	-1.9207885653E-05	1.9146516910E-06	1.1560787725E-05
	1.8144059	254E-1	06	-6.0604934020E-07	3.9700141867E-06	-6.5007550606E-07	1.0625040212E-06
	1.6442538	760E-	06	1.4762418933E-06	5.1786559387E-07	3.8271418564E-07	0.
	U.			U.	0.	0.	0.
-	2.1820413	519E-1	02	-1.8985057321E-02	-5.8284684671E-03	9.5986659740E-03	1.4227243947E-02
	1.9244633	480E-	03	-2.1655684164E-03	-8.7829006034E-03	-2.7522027931E-03	-8.6867/92218E-03
	6.4428944	801F-	03	-2.1903688196E-03	8.2500130219E-04	2.1321891855E-03	1.7932017797E=03
	8.2717037	913E-1	05	-1.3714281006E-04	-3.0350386156E-04	=1.8026933971E-04	-2.0117036423E-05
	1.4940875	068E-	05	1,1822621585E=04	7.8411445297E-05	3.0031849425E-05	2,0165419205E-04
	1.4573267	109E-	04	8./014866377E-05	3.8997750682E-05	1.1560727900E-05	3.2120706053E-07
	2.5679726	284£-	05	2.0497267286E-05	9.2963194647E-06	5.2017493799E-06	6.9079758640E-07
	8.6297100	566E-	υī	1.1479151414E-07	2.7179683068E-07	2.0086389971E-07	0.
	U.	•		U.	0.	Ue	0.

N= 9	K= 6	J= 12			
SOLUTION 1.0953 6.1681 2.2191 -8.8602 3.5487 -8.8766 1.42603 -1.784 -2.6035 -1.8025 0. -1.224( 3.575 -5.733( 2.3366 -6.2711 -1.751 -4.4435 0.	3570412L-02 1390795L-04 1572754L-02 3382300L-03 7811552L-03 5551162L-05 1875452L-04 5263176L-05 9973262L-06 0855215L-02 2997070E-03 0036051L-03 2349065L-04 3537058L-05 2977521L-04 3001929L-05 9892801L-07	1.9276485089E-02 3.4954404599E-02 2.1299441126E-02 2.5499454673E-03 1.8942174465E-03 2.7611252536E-04 1.5796848833E-04 -8.0984974085E-07 -1.1113390411E-05 -1.6187647329E-06 0. -1.1783129590E-02 -1.9063891620E-03 -2.2497013016E-03 -5.6599701747E-04 1.4725033842E-04 -1.3458357064E-05 -3.9898967211E-07 0.	-1.6202149089E-03 4.8584115206E-02 4.0499929567E-03 7.6491783642E-03 -9.0686/74705E-04 5.0925655872E-04 5.0918106690E-07 2.2328070878E-05 -5.6786259998E-07 0. -3.2357680662E-03 -5.4027114104E-03 6.8003616793E-04 -1.8894584510E-03 2.1284058538E-04 -3.3891536353E-05 -6.4244419855E-06 -1.3996556014E-07 0.	-2.7367212023E-02 -8.3513938436E-03 -9.6547512036E-03 4.4247757476E-03 -1.1674688895E-03 3.6444483919E-04 4.8343610172E-05 1.9861411611E-05 -2.1241196841E-06 -4.1966308455E-07 0. 4.0458826703E-03 -1.7078360829E-03 2.0768988480E-03 -1.2891550994E-03 4.4449053060E-05 -3.5776328896E-06 -3.3779601589E-06 -1.0343766027E-07 0.	-3.3683382678E-02 -4.3363185762E-02 -1.7130521476E-02 5.4407226468E-03 -1.4069528941E-03 3.7087057081E-04 -5.3179642346E-05 2.0579752738E-05 -1.8937591138E-06 0. 0. 7.8861187614E-03 -7.4997509818E-03 1.5828334689E-03 -6.7741157618E-04 -2.5763547504E-04 9.6849809880E-06 -5.3533841063E-07 0.
N= 9	K= 7	0 = L			
SOLUTION 9.8681 -2.612 2.548 -4.749 -7.876 1.190 1.805 -6.307 2.310 3.233 -9.605 0. 0. 0. 0. 0. 0. 0. 0. 0. 0.	8531052E-03 0459974E-02 7592563E-02 1545678E-03 7786938E-03 5737803E-03 6275717E-04 3845843E-05 5863476E-05 5863476E-05 0154865E-06 6503356E-08	-8.1085101956E-03 3.9549868500E-02 -1.7118370708E-02 9.5323470428E-03 7.7006714652E-04 -1.0762762538E-03 2.5731276115E-05 1.5321266764E-05 -1.070026744E-05 -2.8028223490E-06 6.9369791617E-08 0. 0. 0. 0. 0. 0. 0. 0. 0. 0.	-1.3719150195E-02 -1.66092261028E-03 -7.2977909686E-03 -4.1261072365E-04 4.9384360248E-04 2.5843716961E-03 -9.7812705502E-05 7.8322798031E-05 -4.1622542318E-06 5.5960607065E-07 0. 0. 0. 0. 0. 0. 0. 0. 0. 0.	3.7529565435E-U2 -4.0927236483E-02 1.7315602146E-02 -8.8390101492E-03 -1.4621989802E-03 -1.2058513157E-03 2.5836294575E-04 -2.5743842106E-05 3.7575488805E-06 -3.8455244264E-07 U. U. U. O. O. O. O. O. O. O. O. O. O. O. O. O.	-1.0650436909E-02 1.4186732820E-02 1.3283842136E-02 1.0795364004E-02 -1.5122367759E-03 5.4766294978E-04 2.9041836068E-04 2.5922058318E-05 -5.2571546842E-06 3.4097445126E-07 0. 0. 0. 0. 0. 0. 0. 0. 0. 0.
N= 9	K= 7	J= 1			
SOLUTION 1.041 -3.311 2.684 -5.144 -2.587 5.658 8.155 -6.350 -7.304 -2.482 9.395 1.179 -3.487 -4.292 1.364 3.249 -1.781 3.658 2.528	0508590E-02 8108492E-02 8108492E-02 0124965E-03 8065120E-03 5773985E-04 99022832E-05 99022832E-05 9351914E-06 67438292E-08 931/3612E-02 7438292E-08 931/3612E-02 767930E-03 12065111E-03 985/844/E-04 2922620E-04 2992620E-04 12922620E-04	-1.5239931926E-U2 4.0360671846E-U2 1.2476543579E-U2 -3.0933061798E-05 -2.4227113211E-04 -2.3025845404E-U4 2.0754147994E-U5 2.5860257378E-U6 2.3873443624E-U6 -6.7853895234E-U8 -8.6646494805E-U3 5.5367595721E-03 5.6855408505E-U4 -3.1091334030E-04 -2.7561322154E-04 -2.004895531E-05 -2.004895531E-05 -1.0837796781E-U6	-1.1888076276E-02 2.1508073374E-04 -1.6900054593E-04 2.9224813435E-03 4.7840169750E-04 4.9639048792E-05 -4.5075837666E-05 4.6187036061E-06 -4.1070026818E-07 0. -3.7143779283E-04 -1.3900715933E-03 1.9184789286E-03 2.1042629193E-03 7.4496677476E-05 1.3521286048E-05 6.2939785324E-06 5.2666640120E-07 0.	2.6275173647E-02 -3.2848293896E-02 1.3576593524E-02 -7.1810433638E-03 -1.6096062000E-03 -3.9728067042E-04 -3.9851148483E-05 5.2066902218E-06 -3.0234784726E-06 3.4217097440E-07 0. 4.9745298291E-03 -2.4164133936E-03 -1.1262375754E-03 -1.2290858787E-03 6.7788390689E-05 -3.0342052371E-05 -1.2111368502E-06 -7.9901324868E-08 0.	-9.5770226823L-03 2.5409998455L-02 -5.8212726054E-03 6.9407097899E-03 5.8578248009E-04 -1.6351270463E-04 1.2001973686E-05 -1.2332852022E-05 3.5026139089E-06 -3.3352134142E-07 0. -2.8657560990E-03 8.0724039259E-03 8.0724039259E-03 -8.3571451365E-05 1.3538771452E-04 3.2991713553E-04 5.9995354699E-06 -1.1433814474E-06 7.0892574688E-08 0.

AL -

N= 9	K= 7	2 = ل			
SOLUTION					
9.111946	5506E-03	-1,1664657190E-02	-1.3855201021E-02	3.0903214020E-02	-9-6217820521E-03
-3.257247	3461E-02	4.3267054495E-02	-4.3609535236E-03	-3.2220720679E-02	2.0353572860E=02
1.813992	8211E=02	-1.1334481766E-02	-2.1296397229E-03	1.1773762901E-02	-6.3723191481E-03
-3,132185	2293E-03	8.6127163783E-03	-1.2945680311E-03	-4.0513908181E-03	-1.3664775841E-03
6.076712	4217E-05	~2.4958510429E-04	-6.6250890671E-04	2.0955601585E-04	-5.8162370180E-05
9.375401	7528E-05	2.2608058666E-04	-1./487451980E-03	1.0803825466E-03	-9.7370273866E-05
-1.060188	5908E-04	2.1359540533E-04	3.6770181628E-05	-1.0593883149E-04	-3.8547343225E-04
2.028329	9049E-04	-/.1491544441E-05	-4.3813702052E-06	1.5121559595E-05	-8.1929319648E-06
-2,302137	2313E-05	1.2812476926E-05	-4.7696423854E-06	1.2116165304E-06	2.6891524799E-07
5.220652	4440E-07	-1.2943724490E-06	2.2696753043E-08	-2.2985731287E-07	3.1149566112E-07
-8.775198	2318E-08	6.3372458029E-08	0.	0.	0.
2.002340	3765E-02	-1.2587742656E-02	-3.1961/09077E-03	1.2930036963E-02	-7.0728797990E-03
-3.920051	4023E=03	9.9088228031E-03	-2.4574990674E-03	-3.5538618910E-03	1.0171881707E-02
-5.813004	3950E-03	8.3131521047E-06	2.59805887646-03	-2.0349554052E-03	-4.9112556140E-06
1 544754	00245 04	-3.08/99931/2E-04	1.2972488002E=03	-6.9020064555E-04	8+6988789418E-05
L J HO / JO	00236-04	-1.0103000340E 05	1 • 1 3 3 9 1 2 1 6 1 1 E = U 3	5. (701361289E-05	-9.0410511916E-05
-4 006100	97256-05	2 22250454055 05	9 902977543E-06	3.4/43/883/2E-06	1.2949693351E-06
	79505-05	L- 7037711216F-06	-8.501//1144/L=00	1 16366055055 07	-1 39494903495-07
3.406969	97201-08	-Z-8215236173E-08	0.	0	0
J <b>.</b> /00,0,	)   E0E=00			v.	v.
N= 9	K= 7	J= 3			
SOLUTION					
1.098698	4461E=02	_1.2530736268E=02	-9.4843136421E-03	3.0869413851E-02	-7.1023470338E-03
-2.978362	5016E=02	4.U287291913E=U2	-5./150/42498E-04	-3.9945511450E-02	1.7274350611E-02
8.163953	8453E-03	-6.3795827435E-03	-1.7420849318E-03	3.8532478863E-03	-3.6001317468E-03
-2.906870	1752E=03	3.3923854145E-03	-1.5335913736E-03	-1.7832287970E-03	-7.7342300094E-03
4.956671	5601E-03	6.8292055632E-04	-1.8998057738E-03	2.2322182767E-U3	1.7508758407E-04
-5.929726	0654E-04	5.5359277719E-04	-1.9280652612E-03	8.6182328764E-04	-2.5828058638E-04
-2.678720	2140E-04	1.3248793103E-04	-3.0542388199E-05	-1.0834533622E-04	1.7633537447E-04
-1.359453	1796E-05	6.0433144526E-05	2.5777323336E=06	1.0694226889E-05	7.9893874072E-06
3.419215	3361E-05	-1./913950894E-05	2.4602343380E-06	7.7013573291E-07	-2.9761211092E-06
1.881222	4505E-06	-1.4095680056E-08	4.5076979211E-07	8.6498178746E-08	-2.7585412572L-07
7.//1134	3635E-08	-5.6121340314E-08	0.	0.	0.
2.142338	2343E-02	-1.8789558352E-02	-1.0584010490E-03	1.3593607023E-02	-6.7104648630E-03
-6.438024	0430E=03	1.3090561579E-02	-2.1109556074E-03	-5.9977711389E-03	6.9275985623E-03
-3.123901	0390E-03	1.0981358750E=03	1.0850493831E-03	-4.5386098567E-04	-4.6007168136E-04
9.000100	1942E+04	-4.4900104090E-04		0.102304//08E-04	4.43805800935-05
-20403100	6910E=04	4. 4071414030522=04	-3.28331400375-05	1.3031430090E=03	
10297991	40000-04	5 63191057216-06		-7 33731367405 04	1 70003355355-04
			9.1463471403E-07	-9 3116653050E ()9	2 00410753945-07
4.200710 5.444050			9.1483371403E=07	-8.51100559592=08	2.00419793886=07
-9.040099	00092-08	4.07749404072=08	0.	0.	0.
N= 9	k= 7	J= 4			
SOLUTION				a	1 2024
9,298692	6124E-03	-1.1756920939E-02	-1.6106826437E-02	3.1357109653E=02	-1.3074969364E-02
-3.064538	30013E-02	3.9985674297E-02	-8.1244256796E-04	-3.2207089546E-02	2.4022152304E-02
-1./85563	1637E-03	1.0/139/615/E-03	2.4392286206E-03	-2.1376194680E-03	3.21/3/03933E-03
-3.192227	1941E-04	5.2012682559E=04	-1.24/1//3508E-03	2.3982510615E=03	-1.1239976785E-02
5.956514	3311E-03	-1.5111/33235E-03	-2.1430091600E-03	9.115/882//5E-04	4.2395480388E-04
-1.000914	20936-03	4.908110/0/1E=04	3 03404095395 05	1 17374500225.04	2 35474315406-04
	10368E-05	0.09009777207E-00	- / • U D D U 4 9 0 D D 0 E = U D 	-4 26765865085.00	5 16237669266-06
-1 (1430/0	13801F=VF		2.5()731178045-02	-7.07102680606-06	2.77537133648-06
	20716-02	1.22030054375-04		3-9641735805E-08	2,2815644133E=07
-20101010	63355-00	4.6417450728F=08	U.	0.	0.
-UB461434 2.679363	29946E=02	-1.8249837641F-02	-4.5931947504E-03	1.5801223665E-02	-1.0541996246E-02
-5.643252	37//6E=03	1.1279203470E=02	-1.2436849807E-03	-7.6963948317E-03	-3.1439101595E-03
1.239413	37353E-03	-1.2708188836E-03	-4.2794207987L-04	-5.6154293380E-04	1.2060673385E-04
-/.688894	15510E-04	-3.2313002476E-05	-2.2904020226E-03	1.0996488227E-03	-3,3935812511E-04
-2.369228	2967E-04	1.1546216638E-04	1.8380305850E-05	-1.6415585345E-04	6.0986733991E-05
-4. 354841	7809E-05	-3.6529434756E-05	1.3805874418E-05	-3.0893476929E-05	-1.2516817024E-06
2.636418	12598E-05	-1.3401102996E-05	1.9094840422L-07	1.5419479234E-06	-3.2454940422E-06
-2.950461	12410E-06	1.0461632212E-07	-6,5967689049E-07	-1.8396383437E-08	-2.5339339908E-07
7.138389	93422E-08	-5.1551801685E-08	0.	0.	0.

N= 9	K= 7	J= 5			
SOLUTION					
1.052638	4347E-02	-1.3164552599E-02	-1.1268722494E-02	2.9515497150E-02	-8.5691478228E-03
-3,129303	7498E-02	4.0786148828E-02	-9.7572417689E-04	-3.6135881384E-02	2.0579035649E-02
-1,470990	0967E-02	1.0475144526E-02	1.3216752276E-04	-6.5554083399E-03	3.3920660425E-03
3.473309	5554E-03	-6.4688069852E-03	2.1736/80433E=04	4.2211244105E-03	-4.7870640744E~03
2.761105	2765E-03	3.7990542260E=04	-1.5368511946E-03	1.2716205528E-03	-2.2429740674E-04
-2.987808	20092-04	0.4985842767E-05	2.103/2864/UE-U3	-1.1153493820E-03	9.5288763037E-05
5.202014	4946E=04	-3.1857237608E-04	2 612760616EE 05	0.2301808271E-00	-1.2/40932803E-04
-7 110304	34935-05	1.5526021132E_05	-7 76167527555-06	2 3357532300E-05	_5 99/1717203E_07
4.416566	75605-05	-1.7402105689E-06	9.32370238275-07	-1.0907143650E=07	-1-7048722563E=07
4.802825	1678E-08	-3.4684895809E-08	U.	0.	0.
2.397068	8003E-02	-1,5064933198E-02	-2.7276/20218E-03	1.4977022594E-02	-7.7159683296E-03
-3.151466	0985E-03	1.09/2948858E-02	-4.0920623376E-04	-6.4245379592E-03	-8.6001450913E-03
5.459175	4706E-03	2.7990149427E-04	-1.9122081862E-03	1.9555250315E-03	1.9599752080E-04
-9.153250	8591E-04	4.2478273009E-04	7.0032083686E-05	1.3124577188E-04	5.7142882539E-05
1.027180	8559E-04	1.9956626914E-05	5.1397965997E-05	-1.3542681380E-05	3.5599239202E-04
-1./10541	6/40E=04	1.4741453790E=05	1.0890781962E=05	-/.53812//023E-06	1.020251/181E-05
-3.2(5653	08655-05				1.9302514163E=06
0,0000419		6 1074001704E 09	2.19219492928-01	1.5904903305E=07	2.992929293684L=01
-0-110111	21052-08	8.0018001198E=08	V •	0.	
N= 9	K= 7	J= 6			
SOLUTION					
1.024911	4091E=02			3.1425575293E-02	-8.5933020748E-03
-2.102043	73154-02	+ 3802048418E=02	-2077637E-03	~1.4071997559E~02	7.67211928965-03
3,998639	1438E-03	-1.0504592825E-02	1.8747474718E-03	4.6485107450E-03	3.0004834040E-03
-1.880453	4028E-03	-1.9211998783L-04	7.4988969975E-04	-7.7881137695E-04	-3.0104391044E-05
3,012850	54/3E-04	-1.5601417367E-04	6.1606157360E-04	-3.0156712310E-04	3.1894498699E-05
1,349580	2154E-04	-1.0376999286E-04	4.4384561976E-05	8.6283103259E-06	-2.7620015342E-04
1.549850	6857E-04	-3.0161120514E-05	-5.9131468732E-06	2.3784656216E-05	-3.7339492521E-06
4.345065	0490E-05	-2.3938316864E-05	7.9908/55224E-06	-1.7247436489E-06	-1.0711607458E-06
-3.497731	6938E-06	1.4/55068546E-06	-1.3057282743E-07	1.0577804258E-07	1.0536690009E-07
-20900309	19575-08	201430444300E=08	Ue 	0. 8.6124213161F=03	-3-97396974651-03
-1-153284	90616-03	/_5328267042F=03	6.7270920470E-04	-5.5121202370E-03	-1.0070733516E-02
4.721913	7838E-03	-2.5671960072E-04	-3.0950950253E-03	2.0290513166E-03	-1.1330066514E-04
-8.082142	2460E-04	6.4186856545E-04	2.0134254184E-03	-1.2077887742E-03	6.2320077383E-05
1.844630	3082E=04	-2.9933655215E-04	3.1967264613E-06	8.8026271192E-05	-2.4806419870E-04
1.575220	2246E-04	-5.0682215678E-05	1.6770686677E-05	9.3914843590E-06	6.7131103669E-07
8.169356	1553E-06	-5.3156785756E-06	4.8800340148E=06	-2.2013896473E-06	1.6808668399E-06
1,613687	8695E-06	-1.9048018579E-06	2.3865185519E=07	-2.9275047673E-07	-3.2428597376E-07
9,135516	3449E-08	-6.5974592351E-08	U.	U.	U.
N= 9	K= 7	J= 7			
SOLUTION					
1.007195	2322E-02	-1.2676133439E-02	~1.3080255879E-02	3.0186164667E-02	-1.0329556629E-02
-3.096057	19219E-02	4.0328705737E-02	~7.5119653440E-04	-3.4765810110E-02	2.1976669145E-02
-2.146505	1189E-02	1.8804084155E-02	2.4218817778E-03	-1.4496380018E-02	8.1540888430E-03
6.464919	2051E-03	-1.2794545909E-02	2.3644685804E-03	6.1672818366E-03	9. (888 (325 / UE-03
-2.328409	10303E=03	5.3595192321E-04	2.03228821907E=03	-1.00040606060E=03	1 21407934926 04
-2 652817	712306-04	2.2760787129F-04	=1.7747704581E=05	-6-3402905492F-05	2,2010806980E=04
-2:00201	48/11=04	2.0235314704E=05	1,0470892669E=05	-2,0588489921E-05	4.3686641237E=06
-2,083640	1100E-05	1.1391074484E-05	-3.4647304790E-06	6.2296908397E-07	7.1837587589E-07
1.325358	33293E=06	-5./316088813E-07	2.7569/73818E-07	-4.2883960833E-08	-3,5641535405E-08
1.004063	38683E-08	-/.2511177150E-09	U.	0.	0.
3.593068	8218E-03	-2.6276212912E-03	-4.6895074584E-03	4.5672616229E-03	-5.9896879624E-03
-5.030435	9598E=04	-2.1511519759E-04	3.8993265806E=04	-2. 9342123855E-03	-4.506/269905E-03
4.192998	14385E-U3	- 202626277126-04	1.62302707070F-03	-7-0342354003F-04	4.30279003775-04
-2°047100 0°29047100	548995-04	9-3146431870F-05	-8.4872829168E-05	1,9156006186E=04	-2.0386079647E-04
2,645444	34586E-05	-5,1426098163E-06	-6.8998506093E-05	1.9747424363E-05	-2.2118803366E-05
1.884795	3/61E-05	-8.5104050137E-06	-4.2989341517E-06	3.5673397436E-06	-4.7919780791E-06
-3.040481	7/161E-06	2.6964336749E-06	-5.2141544281E-07	3.7371369734E-07	3.3910655754E-07
-9.553025	45780E-08	6.8989776640E-08	υ.	0.	0.

N= 9	9	K= 7	j= 8			
E ()   1   1						
SOLUT	10N	J⊾ ∩ 2	1 1 2 ( ) 2 2 ( 2 0 5 ( 0 2	1 30003550005 03		
, L .	00/1992324		-1.20/0133439E-U2	-1.3080255880E-02	3.0186164667E-02	-1.0329556629E-02
	74450011921		400328703757E=02	-/oJ119033444EmU4	-3.4765810110E-02	2.1976669145E-02
	464010205	1-112	1,7045450005 07	2042100111116-03	~1.4496380018E=02	8.1540888430E-03
	. 4294000303	46-03	5 45051025215 04	2,2004408080025-00	De10/2818300E=03	9.1888132510E-03
	14244303030	16.03		200228821907E=03	-1,0054566060E-03	-1.1614231213E-04
1 e	4 5 2 4 0 3 7 3 7 4 5 2 0 1 7 1 2 2/			-1. 194//04561E-03	8.8755007992E-04	-1.2168783682E-04
<i>م</i> د و	111775/01		202109181129E=04	-2,5325598048E-05	-6.3402905492E-05	2.2010806980E-04
	111112401.			1.04708926696=05	-2.0588489921E-05	4.3686641237E-06
~~~ ( )	11222030110			-3.464/304/90E-06	6.2296908397E-07	7.1837587588E-07
1	00/0/20/09/91		-9.1316088812E-07	2. 1269113818E=07	-4.2883960832E-08	-3.5641535404E-08
1 e - 2	LU4003808		-/.25111//148E-09			0.
-26	0300000210 0300000210		2.02/02129125-03	4.0895074584E=03	-4.56/2616229E-03	5.9896879624E-03
20	0304339399			-308993265806E=04	2.9342723855E-03	4.5067269905E-03
	192990930		3.2650978758E=04	-/.5934580101E-04	-3.5727700336E-04	-1.2125681706E-03
	54215527U		**De4200000//16E=U4	-1.6230279229E-03	7.0342354803E-04	-4.3027990377E-04
- 70	546666490		-900140401010E=00	8.48/2829168E-05	-1.9156006186E-04	2.03860/964/E=04
- 1	0424704201 994705276		201420098104E=00	6 20003615165 00	-1.9/4/424363E-05	2.2118803366E-05
-16	009192210		8.5104050157E=06	4.2989341516E-U6	-3,56/339/436E-U6	4.7919780791E=06
2 e ()	5 5 5 0 5 0 5 7 5 5 5 5 5 5 5 5 5 5 5 5		~~ 2.09643301495-00	002141044281E=07	-3.13/1369/34E-07	-3.3910655754E-07
7 (	555029510	00-00	-0.898911664UE-08	0.	0.	0.
	0					
N= 0	9	K= 7	J= 9			
SOLU	TION					
1.	oU249114U9	1E-02	-1.1673026226E-02	-1.2124865653E-02	3.1425575293E-02	-8.5933020747E-03
÷.	<b>.</b> 112439340	0E-02	4.2059522763E-02	-2,9528943963E-03	-3.5765810062E-02	1.8500079665E-02
-2.	.192943731	5E-02	1.3802948418E-02	3.2963427637E-03	-1.4071997559E-02	7.6721192896E-03
. د	•998639143	8E-03	-1.0504592825E-02	1.8747474718E-03	4.6485107450E-03	3.0004834040E-03
-1,	<b>880453402</b>	8E-03	-1,9211998783E-04	7.4988969975E-04	-7.7881137695E-04	-3.0104391044E-05
, د	ol2850547	3E-04	-1.5601417367E-04	6.1606157360E-04	-3.0156712310E-04	3.1894498699E-05
1	<b>.</b> 349580215	4L-04	-1.0376999286E-04	4.4384561976E-05	8.6283103259E-06	-2.7620015342E-04
1	• 549850685	/L-04	-3.U161120514E-U5	-5.9131468732E-06	2.3784656216E-05	-3.7339492521E-06
4	.345065049	1E-05	-2.3938316864E-05	7.9908/55224L-06	-1.7247436489E-06	-1.0711007458E-06
~ J	.497731693	8E-06	1.4755068546E-06	-7.3057282743E-07	1.0577804258E-07	1.0536690009E-07
-2	.968309195	7E-08	2.14364445U6E-08	υ.	υ.	0.
-1	.128988049	4E=02	1.1683530909E=02	le4758512336E=04	-8.6124213161E-03	3.9739697465E-03
. د	.153284906	1E-03	-1.5328267042E-03	-6.1270920470E-04	5.5121202370E-03	1.0070733516E-02
-4	.121913783	8E-03	2.5671960072E=04	3.0950950253E=03	-2.0290513166E-03	1.1330066514E-04
8	.082142246	UE-04	-6.4186856545E-U4	-2.0134254184E-03	1.2077887742E-03	-6.2320077383E-05
-1	.844630308	2E-04	2.9933655215E-04	-3.1967264613E-06	-8.8026271192E-05	2.4806419870E-04
-1	.5/5220224	6L-04	5.0682215678E-05	-1.6170686677E-05	-9.3914843590E-06	-6.7131103670E-07
-8	.169356755	2E=06	5.3156785755E=06	-4.8800340148E-06	2.2013896473E-06	-1.6808668399E-06
-1	.613687869	5E-06	1.9048018579E-06	-2.3865185519E-07	2.9275047673E-07	3.2428597377E-07
-9	.135516344	9E-08	6.5974592351E-08	Ο.	Ú.	0.
N=	9	K= 7	J= 10			
-					,	
50LU	TION			1 13(033)(0)( 0)	- 	9 5(0)/700076 00
1	.052638434	1E-02	-1,3104002099E-U2		2.9991949/19UE-U2	-8.70714/822/E-03
<b>ز –</b>	.129303/49					2 20206404355
-1	.470990096	7E=02			-0.0004080099E-00	3.3920660425E-03
د	.4/3309555	4E-03	-0.4088009851E-03	2.1/36/80432E=04	4.2211244104E=03	-4.18/0640/44E=03
2	. 161105216	DE-03	3.19903422395-04	=1e008011940E=V0	1.02/10209928E=03	0 52007420375 05
->	.987808260	9E-04	6 4985842767E-U5	2 163/2864/UE=U3	-1.1153493820E=03	9.5288763037E-05
3	e2U2U14494	0L-04	-3,185/23/608E-04	104041040141E=05	0.42018082/1E-U5	
5	.105188521	UE-05	1.18/9266585E-06	-20010/486160E-U5	2 8132986456UE-U5	- 0 2 2 1 1 2 4 1 3 3 1 E - U6
-2	. /19304349	3E-05	1.0026921132E-05	-/.2016252/55t-06	2,335/5323U8E-06	-> 8941/1/203E-07
4	•416566756	UE=06	-1. /4U2105689E-06	903231023821E-01	~1,090/143650E=0/	-1.1048122563E-01
4	.802825167	8F-08	-3.4684895808E-08			
-2	.397068800	3E-02	1.5064933198E-02	2.1210120218E-03	-1.449//UZZ594E-UZ	1.1159683296E-03
ځ	./51466098	5E-03	-1.0972948858E=02	460920623376E-04	0 + 42403/9092E-03	
5	.459175470	6E-03	-2.7990149427E-04	1.9122081862E=03	-1.9999929U315E-U3	
9	. 153250859	16-04	-4.2478273009E-04	-/.UU32U83683E-05	-1.31245//188E-04	
- 1	.027180855	9E-04	-1.9956626914E-05	->+139/96599/E-05	1.3542681380E-05	
L	e/10541674	UE-04	-1.4741453790E-05	-1.0890/81962E-05	1.5381277024E-06	-I. 11038//181E-05
3	.215653086	5E-05	-1. /560508656E-05	40094714424E=06	-1.80059275118E-07	1 - YOUZO14163E-06
-6	.833219119	9E-07	-6.1349919729E-07	-2.1521549252E=07	=1,5904903305E-07	-2.577272736846-07
8	.318737210	56-08	-6.0076001796E-08	U e	U.	U.

n- ,	N- 1	5- 11			
SOLUTION					
9.2986926	124E-03	-1.1756920939E-02	-1.6106826437E-02	3.1357109653E-02	-1-3074969364E-02
-3.06453800	013E-02	3.9985674297E-02	-8.1244256796E-04	-3.2207089546E-02	2.4022152304E-02
-1./8556310	637E-03	1.0713976157E-03	2.4392286207E-03	-2.7376194680E-03	3.2173703933E-03
-3.79222719	940E-04	5.2012682560E-04	-1.2471/73508E-03	2.3982510615E-03	-1.1239976785E-02
5.95651433	311E-03	-1.5111733235E-03	-2.1430091600E-03	9.1157882775E-04	4.2395480388E-04
-1.60691420	093E-03	4.9581167071E-04	8.6119/14916E-04	-4.1263308076E-04	2.3983666508E-04
1.2172720	368L-05	6.5953977267E-05	-7.0360498538E-05	1.1737658022E-04	2.3547831540E-04
-1.23059414	480E-04	-1.4618502309E-05	2.8297816892E-05	-4.2676586508E-05	5.1623766826E-06
-1.0839482	891E-05	4.8859031999E-06	2.5073117893E-06	-2.0710268969E-06	2.7753713364E-06
-3./818/292	220E-06	1.2203995437E-06	-8.2006446132E-07	3.9641735805E-08	2.2815644133E-07
-6.4274346	335E-08	4.6417450728E-08	υ.	υ.	0.
-2.67936299	946t-02	1.8249837641E-02	4.5931947504E-03	-1.5801223665E-02	1.0541996246E-02
5.6932537	7/6E-03	-1.1279203470E-02	1.2436849807E-03	7.6963948317E-03	3.1439101595E-03
-1.2394737	353E-03	1.2708188836E-03	4.2794207987E-04	5.6154293381E-04	-1.2060673385E-04
1.6888945	510E-04	3.2313002476E-05	2.2904020226E-03	-1.0996488227E-03	3.3935812511E-04
2.3692282	967E-04	-1.1546216638E-04	-1.8380305850E-05	1.6415585345E-04	-6.0986733991E-05
4.3548417	809E-05	3.6529434756E-05	-1.3805874418E-05	3.0893476929E-05	1.2516817024E-06
-2.6364182	598E-05	1.3401102996E-05	-1,•9094840422E-07	-1.5419479234E-06	3.2454940422L-06
2.9504672	470E-06	-/.U461632212E-07	6.5967689049E-07	1.8396383437E-08	2.5339339908E-07
-7.1383893	422E-08	5.1551801685E-08	0.	U 🖕	0.
N= 9	K= 7	.1= 12			
SOLUTION					
1.0986984	461E-02	-1.2530736268E-02	-9.4843136421E-03	3.0869413851E-02	-7.1023470338E-03
-2.9783625	016E-02	4.0287291913E-02	-5./150/42500E-04	-3.9945511450E-02	1.7274350611E-02
8.1639538	453E-03	-6.3795827435E-03	-1.7420849318E-03	3.8532478863E-03	-3.6001317468E-03
-2.9068701	752L-03	3.3923854146E-03	-1.5335913736E-03	-1.7832287970E-03	-7.7342300094E-03
4.9566/15	601E-03	6.8292055631E-04	-1.8998057738E-03	2.2322182767E-03	1.7508758408E-04
-5.9297260	654L-04	5.5359277719E-04	-1.9280652612E-03	8.6182328764E-04	-2.5828058639E-04
-2.6787202	140E-04	1.3248793103E-04	-3.0542388200E-05	-1.0834533622E-04	1.7633537447E-04
-1.3594531	795E-05	6.0433144526E-05	2.5777323336E-06	1.0694226889E-05	7.9893874072E-06
3.4192153	361E-05	-1.7913950894E-05	2.4602343381E-06	7.7013573290E-07	-2.9761211092E-06
1.8812224	506E-06	-7.4095680058E-08	4.5076979211E-07	8.6498178745E-08	-2.7585412572E-07
1.111343	635E-08	-5.6121340314E-08	0.	0.	0.
-2.1423382	344E=02	1.6789558352E-02	1.0584010490E=03	-1.3593607023E-02	6.7104648630E-03
6.4380240	430E-03	-1.3090561579E-02	2.1109556074E=03	5.9977711389E-03	-6.9275985623E-03
3.7239616	390E-03	-1.0981358750E-03	-1.0850493831E-03	4.5386098567E=04	4.6007168136E-04
-9.0061567	945E-04	4.4906104096E=04	1.1814517855E-03	-6.1023647768E-04	-4,4380580093E-05
2.4051086	916E-04	-2.6782686682E=04	9.4852941018E=05	-1.3631456690E-05	2.6050908298E=04
-1.2575514	880E-04	-3.9971314029E=06	3.28331409376-05	-3.9309767774E-05	8.0049141119E=06
-8.6002104	370E=06	5.631819572UE=06		2,3323133748E-06	-1.78083333335E-06
-4.2089/89	137E-06	1.57551486500=06	-9.14633/1403E=0/	0.01100000000000000	-2.0041915586E-01
2.6460296	059E-08	-4.U//454046/E=08	0.	0.	0.
N= 9	K= 7	J= 13			
SOLUTION					
9.7719465	506E-03	-1.1664657190E-02	-1.3855201021E-02	3.0903214020E-02	-9.6217820521E-03
-3.2572473	461E-02	4. 3267054495E-02	-4.3609535237E-03	-3.2220720679E-02	2.0353572860E-02
1.8139928	211E-02	-1.1334481/66E-02	-2.7296397228E-03	1.1773762901E-02	-6.3723191482E-03
-3.1321852	293E-03	8.612/163783E-03	-1.2945680311E-03	-4.0513908181E-03	-1.3664775841L-03
6.0767124	202E-05	-2.4958510428E-04	-6.6250890671E-04	2.0955601585E-04	-5.8162370179E-05
4.3/54017	530E-05	2.2608058666E-04	-1.1487451980E-03	1.0803825466E-03	-9.7370273865E-05
-1.0601885	908E-04	2.1359540533E-04	3.6770181628E-05	-1.0593883149E-04	-3.8547343225E-04
2.0283299	049L-04	-/.1491544441E-05	-4.3813702052E-06	1.5121559595E-05	-8.1929319648E-06
-2.3021372	313E-05	1.2812476926E-05	-4.1696423854E-06	1.2116165304E-06	2.6891524799E-07
5.2206524	440E-07	-1.2943724490E-06	2.2696/53041E-08	-2.2985731287E-07	3.1149566112E-07
-8. (751982	318L-08	6.3372458029E-U8	0.	0.	0.
-2.0023403	165E-02	1.2587/42656E-02	3.1961/09077E-03	-1.2930036963E-02	7.0728797990E-03
3,9200514	023E-03	-9.9088228031E-03	2.4574990674E=03	3.5538618910E-03	-1.0171881707E-02
5.8130043	950E-03	-8.3131521053E-06	-2.5980588764E-03	2.0349554052E-03	4.9112556138E-06
-1.2292749	934E-03	3.8879993172E-04	-1.2972488002E-03	6.9020064555E-04	-8.6988789418E-05
-1.5467560	023E-04	1.5898611699E-04	-1./339127671E-05	-5.7701361289E-05	9.0410511915E-05
-6.2180500	112E-05	1.9103898348E-05	-9.4902977543E-06	-3.4743788372E-06	-1.2949693351E-06
3,9941998	725E-05	-2.2235985405E-05	8.3017/11447E-06	-2.1168546910E-06	-4.5182232852E-07
4.1461257	950E-06	-1./037/11217E-06	8.6964142462E-07	-1.1636695598E-07	1.3868680368E=07
2 0040400	7216-08	2 92152361735-09	U.	0.	0.

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N= 9	K= 7	J= 14			
SOLUTION					
1.041050859	0E-02	-1.5239931926E-02	-1.1888076276E-02	2.6275173647E-02	-9.5770226822E-03
-3.311810849	2E=02	4.0360671845E-02	2.1508073369E-04	-3.2848293895E-02	2.5409998455E-02
-5.144012496	8E-02 4E-03	-1.7880324850E-02	-1.6900054592E-04	103576593524E=U2 =7.1810433638F=03	-5.8212726054E-03
-2.587806512	0E-03	-3.0933061800E-05	2.9224813435E-03	-1.6096062000E-03	5.8578248009E-04
5.658577398	5E-04	-2.4227113211E-04	4.7840169751E-04	-3.9728067042E-04	-1.6351270464E-04
8.155902283	2E-05	-2,3025845404E-04	4.9639048791E-05	-3.9851148483E-05	1.2001973686E-05
-6.350152604	5E-05 3E-06	2.5840257377E=04	-4.5075837666E-05	5.2066902218E=06	-1.2332852022E=05
-2.482117407	7E-06	2.3873443624E-06	-4.1070026817E-07	3.4217(97440E-07	-3.3352334142E-07
9.395743829	2E-08	-6.7853895234E-08	0.	0.	0.
-1,179317361	2E=02	8.6646494805E-03	3.7143/79283E-04	-4.9745298291E-03	2.8657560990E-03
3+48/020/00	85-03 0F-03		1.3900715933E-03	2 • 4164133936E=03	-8.0724039259E-03 8.3571431365E-05
-1.061206511	1E=03	3.1091334030E-04	-2.1042629193E-03	1.0290858787E-03	-1.3538771452E-04
-3.249857844	1E-04	2.7561322154E-04	-7.4496677476E-05	-6.7788390689E-05	-3,2991713553E-04
1.781292262	0E-04	-3,1608310141E-05	-1.3521286048E-05	3.0342052371E-05	-5.9995354700E-06
-2.528151080	16-05	1.0837796781E=05	-5.26666640121E-07	7,9901324869F=08	-7-0892574688F=08
1,997127002	/E=08	-1.4422790667E-08	0.	0.	- 0.
N= 9	к= 8	0 =L			
SOLUTION					
9.657927427	6E-03	1,1179415273E-U2	-1.8151574376E-02	-1.5042115337E-02	1.5788660259E-02
3.927548279	1E-02	3.0671055687E-03	-4.2456678857E-02	-2.0378150082E-02	1.7059927326E-02
2.389432451	9E-02	1.1000455957E-02	-1.7238925720E-02	-1.3075033903E-02	-2.3371562898E-03
1.653707312	2E-02	_5.9197103035E=04	-/*3124546093E=03	-5.3416722768E=03	2 1319017430F-04
8.143497244	5E-05	-1.3304720587E-03	3.1980464528E-03	8.8463045728E-04	4.0292899473E=04
-2.556417486	5E-04	3.2967104789E-04	1.3725991352E-04	1.8667458306E-04	3.9209164808E-04
2.227407328	6E-04	-/.5762832016E-06	3.0446470805E-05	8.4689432551E-06	3.7563971757E-05
2.895617354	5E-05	1.01/9123822E=05 -/-6505410574E=07	-1.4198408733E-03	=3+3484820301E=06	-4+4280281446E=06 6-5451359847F=07
1.122610551	1E-01	/./739892774E-08	1.8733056858E-08	1.3344069450E-08	0.
0.		U.	0.	0.	0.
0.		0.	0.	0.	0.
0.		0.	0.	0.	0.
0.		0.	0.	0.	0.
U.		U.	0.	0.	0.
0.		U .	0.	0.	0.
0.		0	0.	0.	0.
0.		••	0.	0.	••
N= 9	к= в	J= 1			
SOLUTION					
9.448365809	1E-03	4.0943008893E-03	-1.9374806654E-02	-2.6357458110E-02	1.3735712657E-02
3.219905573	9E-02	2.9728881189E-03	-3.9823608160E-02	-9.0516897712E-03	3.2157239481E-02
2.795422938	4E-02	1.0863174351E-02	-6.5284675797E-03	-1.1760189098E-02	5,7149138366E-03
4.301462416	01-02	-1.0847503003F=03	-5.0095298959E=04	7.66436757298-05	1.7849405261E-03
2.165887352	2E=04	-4.3227347637E-04	5.8856830623E-04	2.6557553782E-04	-5.5281961203E-04
-2.317684389	15E-04	-2.4161438164E-04	3.2539567072E-05	-1.7943276499E-05	4.9118804816E-05
-6,505099454	NE-05	-1.0653565091E-06	-4.7169868588E-05	-8.1710931076E-06	-1.3617316470E-05
0,000/00900 -1,2273/8515	065-06 045-06	0.9243933780E=08 9.2577773804E=07	4.3359396524E=07	6.1383507994E-07	-5.8112125098E-07
-8.850417056	1E-08	-/.1109215095E-08	-1.8414090967E-08	-1.3116861309E-08	0.
1.036493172	9E-02	3.3269276058E-03	-3.3221819188E-03	-5.7206224575E-03	1.5423262437E-03
3,508332403	34E=03	1.3077119526E=03	-3.2246408581E-03	-1.5013937439E-03	7.8905864610E=03
4 951077225	0L-04	-1.0242010407E=04	2.1962355351E=03	7.9370323624E-04	~2,4091549063E-04
-2,320215632	5E-04	-4.9970515831E-05	1.6549376539E-04	4.5720862561E-05	3.6787559140E-04
1.029899885	0E-04	-3.6942763386E-05	-4.4191242397E-05	=1.6547623736E-05	8.1289969204E-06
4.789981723	50E-05	1.0910463788E=05	4.3348/36966E=08 3.2167438477E=07	-4,4/8/130141E-06 -1,5079920848F-07	-8.0086108200E-07 2.1273088187E-07
9.623479674	95-08	1.4105318924E=08	3.4421901649E-09	2.4519663271E-09	0.

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SOLUTION				1 /01/0/00/20/20/00 00
9.1459568410E-0	3 7.1720017222E=03	-2.0142931652E=02	-2.2156297849E-02	1,4359823766E-02
3.3238726027E-0	2 5.0880049569E-03	-4.3293381037E-02	-1.0160258527E-02	2.60/48300/04E-02
1.9683052361E=0	2 7.9420734710E-03	-8.8201588864E-03	-9.3/1196/282E=03	2.5281697871E=05
1.0037934910E=0	2 3.4973456210E=03	-4.7313259959E=03	-2,9834514523E-03	5.8428119713E-04
-1.6416077162E-0	4 -5.9788851078E-04	-5.6203024452E-04	-1.2616813544E=04	1.3190377383E=04
2.1453534494E-0	4 1.3102517783E-04	-1.2539082211E-03	-4.8017673315E-04	3.1/84225618E=04
2 <b>.</b> 46/288/898E=0	4 6.8140530722E=05	-3.2808155347E-05	-6.6790002378E-05	-4.2271843746E-04
-8.1872082852E-0	5 -4.4652458278E-06	4.4378550726E-05	-3.7637291328E-08	-1.3169557668E-05
-5.0802811764E-0	5 -1.7240746084E-05	-2.9644998506E-06	1.9705516176E-06	6.3295971655E-07
-2.3398528528E-0	6 =1.1799442072E=06	-3.6450294986E-07	-1.3613985499E-07	3.82090861212-01
2.45866/01//E-U	8 5.3032779632E-08	1.7468055292E-08	1.2442974189E-08	
1.8013909704E-C	2 7.8235508237E=03	-8.0902672403E-03	-8.2661711542E-03	2.0021573619E-03
8.1042527207E-0	13 2 <b>.</b> 9530474945E=03	-5.3185551460E=03	-2.1642633494E-03	1.0560570308E-02
3.5205577601E-C	3 -2,3883103209E-03	-2.5340494906E-03	-1.3990934339E-04	1.6566706819E-03
5.8671043414E-0	4 -4.6636251460E-04	1.9959793035E-03	5.3457119129E-04	-2.0085402431E-04
-3.1146825702E=0	14 _5.1257716269E-05	1.1607609576E-04	4.0185887277E-05	7.7154448907E-05
2.3274252663E=0	15 2.7194178359E-07	-4.4029949733E-06	4.6590832108E-07	3.7143819162E-06
-3.0638709221E-0	05 -1.5294908095E-06	-1.9447603974E-06	2 <b>.</b> 1979363539E-06	1.0610568853E-07
-5.7000995523E-0	06 -1.8813113116E-06	-4.8626562561E-07	1.0891460614E-07	-3,5267875995E-07
-1.6619216245E-0	)/ _2.2142738441E=08	-6.1671606723E-09	-4.8204338817E-09	0.
N= 9 K=	8 J= 3			
SOLUTION		1 11 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	3 310//057505 03	1 43034004086 (12
9.9602477241E-0	13 6.6526959033E=03	-1./100/21/80E-02	-2.2190405159L-02	2 43095439675-02
3.4817457258E-0	2 3.5438962241E=03	-4.1266203240E=02	-1,5056999805E-02	
1,2112641970E=0	12 6.1637457691E-03	-5.4577343570E-03	-4.3036297936E-03	4.1582843472005
5.6093064221E-0	9.1856651137E-04	-4.3004652172E-03	-1.4654219694E-03	-6.158/750985E-05
-2.3589260250E-0	13 1.8155210255E-03	1.3798989966E=03	5.0338739645E=04	-9.1946806302E-04
4.4988802196E-0	05 5.1842008145E-04	-2.5802548934E-03	-5.5833270261E-04	1.4404405299E=04
4.4920492292E-0	)4 6.3870560470E-06	-1.1006768179E-04	=/.5251551858E-U5	-6.6955641889E-05
-5.0103397648E-0	15 3.2067/19162E-05	3.3388504636E-06	1.1833021374E-05	-2,3439511034E+06
3.86945978056-0	)5 1.9216173400E=05	-1.9650194224E-07	-2.0504410461E-08	-1.7576474789E-06
4.6680146141L-0	16 1.0534543212E=06	2.0115442877E-07	-3.0532707632E-07	-1.1455618636E-07
5.9642789028E-0	)8 _2,8419302181E=08	-1.5927165946E-08	-1.1345356506E-08	0.
2.5194414812E-(	J2 1.1153018363E=02	-8.9235492068E-03	-1.0542028327E-02	3.6180349552E-03
1.1412674002E-0	02 3.1566338305E-03	-/.0811112908E-03	-3.3076367574E-03	9.3387021897E-03
3.5931565297E-0	)3 -9.9386579261E-04	-1.5249615683E-03	3.3901226762E-04	1.3649978673E-03
3.9133646379E-1	)4 -5.7689163930E-04	-3,9494504279E-04	4.6882918033E-05	1.3304073652E-04
1.6644020075E-	04 8.5268699784E-05	-1.5298581332E-05	2.212700888E-05	-3.5545520979E-04
-8.2998012868E-	3.7456399012E-05	5.2613997771E-05	1.8447452305E-05	-4.2346399170E-06
-2.4197515616L-	05 -2.5812299536E-06	3./462091987E-06	4.2481937973E-06	1.1479269718E-06
2.91667014461-	06 1.4031373999E-06	4.2698307808E-07	1.3967538782E=07	3.6917231938E-07
1.9137960502E-	J/ 1.9924835569E-08	9.8616836393E-09	7.0247473419E-09	0.
N= 9 K=	ئ J= 4			
SULUTION	UK 8.1512698769F-03	-1.9261906114E-02	-1.9951822178E-02	1.4386160420E-02
9.41859251250		=4.1367201767E=02	-1.4725581767E-02	2.4235684183E-02
5.6085196521L-		_8.6507217562E=04	-4-8365732943E-03	6.6757098644E-04
2.0246298628E=		-1.7515181558E-03	-H.1973659530F-07	-1.0914886315E-02
-1.2568930707E-		3 04204523305 03	-1 (1920)996145E-04	-1-0509162508E=03
-3.0880936775E-		5 6620492198E=09	-5 x513677442E-04	7.1803181385E-05
-3.6915161512E-	04 9.0684585577E=04		0 25004417105-04	3 56654249218=04
-1.6146905454E-	04 I.1409969957E-05	-1.40199939130-04	3 46359077695-06	2 0754150160E=05
1.4850/1/541E-		-0.449/209/20-00	-5 1007607000E.04	2.3156607304F=07
1.68383/5986E-	U5 -> 4/89198459E-06		-JOIJ91701200L-00	
-3.4987914102E-	U6 -2.804/52610/E-0/	2.30/30/07/E=08	0 0113013153E 00	()
-1.3/80990120E-	0/ 3.81/3//3731E-09	1.3843896065E-08	300010001100E-00 1 5770707100E-00	2 827832040NE (13
2.1045331835E-	U2 8.5661015682E-03	-1.144434/341E-UZ		1 7508470500E 03
1.0589616284E-	U2 3.25/1950059E-03		-+••***********************************	-2 7425/100704-04
-1.0658703/4/E-	04 -6.//00611605E-04		-2047714087085-04	1 75946606736 04
-2.0181350737E-	04 -4.7206708717E-04		-5 0572013202E NE	
8.1759443848L-	05 -5.2057439592E-06	-2.3204180430E-04	-7 1102007040E 04	
-8.1273048532E-	05 -4.9931616631E-06	-1.003402115546-05	-/+110370/007E-U0	
3.04858084/1E-	U5 1.0487517274E-06	-2.40022/91126-06		
1.65125/1006E-	06 -2.8880602291E=07	-1. Y0382/3407E-U/		()
-1.6654536855E-	U/ -6.45967/2935E-09	-1º2020318198E-08	-8°28284143015-03	

κ= 8

N= 9

J= 2

SULUTION				
9.0836249638E=03	5.4051990375E-03	-2.0708853900E-02	-2.4510304393E-02	1.2803711501E-02
3.2908705977E-02	3.1939059628E-03	-4.0613930932E-02	-8.8050879995E-03	3.1243029782E-02
-6.9557307926E-03	-9.1780826907E-04	3.9828770912E-03	5.8644889545E-03	8.3940976244E-05
-2.1551235369E-03	-7.5062958984E-05	1.6538816552E=03	2.2313960711E-03	-9.8755854145E-03
= 3 6 9 9 2 1 9 0 3 8 2 1 E = 0 3	3 57114014085-04	1 00770323635-03	=4.22/3//4993E=04	-1./29/12885/E-U3
-6-8168181868F-05	4.6224069612Em05	1.5470678714F=04	8.0449893828E=04 6.9775825589E=05	1,5333545680F=04
1.0688202764E=05	-2.8598784532E-05	-4.2580674576E-05	-1.6287431267E-05	-5.7233549652E-06
-3.9297409688E-05	-3.9844476839E-06	3.5390217774E-06	6.3567672152E-06	1.2012087138E-06
-6.3652979089E-07	-8.8195233560E-07	-3.2605179717E-07	-2.8588142230E-07	3.2536445417E-07
1.8495444079±-07	1.4518169639E-08	-1.1289188908E-08	-8.0415984406E-09	0.
2.6268948036E=02	1.3256303441E=02	-1.1163391781E-02	-9.9288465583E-03	2.1439440798E-03
1.3140018520E=02	2.7169125493E-03	-6.9162136634E-03	-4.4404412484E-03	-6.1659165512E-03
-1.000000000000000000000000000000000000	3.67705340308-04	1.0009101009E=03	=4.2494977859E=04 =2.1340102140E=04	-0.7962099271E=04
4.3256289459E=04	-3.1081625672E=06	-1.4416310720E-05	=7.4616044030E=05	3-2320891715E-04
1.3291114347E-04	-3.4047987/07E-05	-1.6364893388E-05	-1.1097743958E-05	1.5160631012E-05
1.1942204514E-05	1.3248654292E-05	-4.3278827871E-07	2.6211668693E-06	-1,1915350764E-06
-4.5616095767E-06	-1.4505849743E-07	-8.1544566431E-08	4.2452121909E-07	2,1252349638E-08
1.0117357544E-07	-1.5695625602E-08	1.4949302093E-08	1.0648797303E-08	0.
N= 9 K= 8	J= 6			
SOLUTION				
9.6889999073E-03	/ <b>。</b> 1544299904E-03	-1.8125526546E-02	-2.1678412293E-02	1,5750478513E-02
3.4561228132E-02	4.1247681515E-03	-4.2132913221E-02	-1.3848334245E-02	2.4505281612E-02
~1.7103353680E-02	-/.2399220287E-03	5.8504936229E-03	7.4362117145E-03	-2.3679666466E-03
-1.4990090038E-03	-2.01751019957E=03	4,4090693246E=03 8,5081624928E=04	2.7631197224E=04	-2.0019049720E-03
-2.69921093511-04	-2,9358121172E-05	2.2928207168E=03	6.1193079726E-04	-2.7663104488E-04
-3.6685222573E-04	-9.0373813505E-05	1.4352635166E=04	3.2096043697E-05	-3.2237877964E-04
-8.6137204950E-05	2.5850844367E-05	3.1769583387E-05	1.1840159131E-05	-7.6798361082E-06
-2.1387013342E-06	-2.0653037046E-06	-3.0961065106E-06	-1.0219414207E-06	-6.1783467945E-07
4.7297311420E-06	1.7598286783E-06	4.8388850752E-07	-2.1905014955E-09	-3.7816740673E-07
-1.8506007107E-07	-202402042123E-08	8.3300419628E=09		3 12404320255-03
1.08646681641=02	3-5963930084E=03	-4,3933705982F=03	-4-0162066919E=03	=1,0129919260F=02
-3.4569444761E-U3	2.4506558288E-03	2.4561585342E-03	3.4228890641E-04	-1.4956067051E-03
-3.0814713013E-04	6.5056870211E-04	1.0749276168E-03	1.8328134218E-04	2.9913374688E-05
-1.4714949845E-04	1.1226623282E-05	7.3995899300E-05	6.9435967069E-06	2.4976331823E-04
4.5251138954E-05	1.8862386352E-05	-2.1887657981E-05	6.9928118734E-06	9.8669894923E-06
-5.3316769046E-05	-2.0863271188E-05	-3.2374690739E-07	1.7336793767E-06	1.5995092489E-06
3,8515170899E-06		2.901/90/200E-0/	-1. 1945121129E-07	2.5232139042E=07
=1,00/1540001/La00	4.11900918192-08	-1607091440500-08	-1.19491211292-08	0.
N= 9 K= 8	J= 7			
SOLUTION				
9.1263059087E-03	7.4485293224E-03	-1.7969480614E-02	-2.1179819934E-02	1.5904304796E-02
3 • 4932439839E=02	4.0690077162E=03	-4.21/1/48988E-02	-104521389944E=02 10140492335E=02	-2 5434292029E-02
-1,1223711477E=02	=1,0144205209E=02 =3,4915098736E=03	6 3010765014E=03	3.1816170266E-03	4.4600964415E=03
1.4060815193E-03	-1.3835394976E-03	-1.2642610822E-03	-2.8234235657E-04	6.8780565839E-04
1.6115087533E-04	-2.4726008874E-04	1.9846415127E-04	1.6580907601E-04	-4.1486109707E-05
2.8288389030E=05	-9.1169919255E-06	3.5108755468E-05	1.2128601388E-06	-2.1775512929E-04
-5.91039551/9E-05	2.6207579035E=05	2.9312711737E-05	1.2019310112E-05	-3.5367779093E-06
4.8135318668E-05	1. 1098308483E-05	/ • 9194541810E-07	-4.2099166004E-06	-0,8113498917E-07
-20014804221E-U0				2. 7011000010E-01
1.6059821762E-02	6.2916687593E=03	-3.4254901796E-03	-6.6432850362E-03	3,0098888875E-03
6.5573198791E-03	1.6076917715E-03	-2.9390439050E-03	-3.6444424831E-03	-1.0286787941E-02
-4.3522005670E-03	1.4281553925E-03	1.4595941460E-03	-1.4206670036E-05	-1.5831019861E-03
-9°6082069331F-02	8.2538200848E-04	2.1120099293E-03	7.2835390985E=04	-5.2734474482E-04
-4.1454424170E-04	-1.5347541886E-04	8 8833214100E-05	6.9332200437E=05	-3, 3851682743E-04
-4,4155137214E-05	2 6 1485393434E-U6	0 0 0 1 3 0 5 1 7 2 7 E 0 5 6 6 1 8 4 7 9 6 2 2 5 E 0 6	20211021128E=06	
505175101780E=U2 =5,0317962719E=07	-1_U700432746E-06	-4.0855488324E=07	=3,9139167539E=07	=4,9442654463E=07
-6.0562830536E-08	-6.3254033308E-08	1.8017934461E=08	1.2834668181E-08	0.

K= 8

J= 5

N= 9

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SOLUTION				
9.2705464254E-03	6.4107464017E-03	-1.9923697380E-02	-2.2816389640E-02	1.3623133446E-02
3.4122142466E-02	3.1596178520E-03	-4.0903794767E-02	-1.1299176446E-02	2.8356871641E-02
-2.7253022521E-02	-1.0595507622E-02	1.0466441119E-02	1.3367522861E-02	-3.3904500267E-03
-1.1526588211E-02	-3.6457597747E-03	7.7474226909E-03	4.1058562443E-03	1.0592585428E-02
3.7532492132E-03	=1.4611096408E=03	-2.0902685213E-03	3.1575555557E-04	1.5550008333E-03
5.9707962082E-04	-5.3427831152E=04	-2.0975945582E-03	-7.2644096584E-04	2.2065930138E-04
2.3785958448E-04	4.4108036785E-05	-1.5043564183E-04	-4.5688034394E-05	2.7464865342E-04
7.7701890567E-05	-2.6120170941E-05	-3.1828664955E-05	-1.1587210853E=05	6,5346581860E-06
-2.9586301032E-05	-6.7238704108E-06	1.6381666563E-07	2.8182194984E-06	5.7576957757E-07
2.4/18623580E-06	1.1946673143E-07	1.7189198508E-07	-8.9980771151E-08	-1.1119083574E-07
-4.9857053526E-08	-/.4554175881E-09	1.7284684241E-09	1.2312353967E-09	0.
1.4684682303E-03	1.6825170570E-03	-8.2163/37029E-03	-2.7556143126E-03	-4.8859926352E-03
1.8701828307E-03	-2.2397656941E-03	-1./175/39141E-03	-1.4072091127E-03	-3.5229490658E-03
5.8130990141E-04	1.1522552042E=03	2.7178621546E-03	1.9349584858E-04	5.5585246039E-04
3.6643805289E-05	7.0186462822E-04	1.9656721187E-03	5.0992140468E-04	4.6001587793E-04
-9.3300893482E-05	3.0619143289E-04	8.0624938638E-05	1.3375509765E-04	-2.6067669523E-04
-1.1627451053E-04	4.6428780602E-06	-3.5879443543E-05	-8.5988096738E-06	-3.0605523891E-05
1.2333522313E-05	1.3507778471E-06	-1.3163445562E-05	-2.6948183183E-06	-3.9379235336E-06
-2.4534681833E-06	8.0927002383E-07	4.4555148602E-07	7.6509284391E-07	6.3582216995E-07
1.0620240959E-07	/.6052751851E-08	-1.8653144940E-08	-1.3287146002E-08	0.
N= 9 K= 8	J= 9			
	• •			
SULUTION 9.2705464254E-03	6.4107464017E-03	-1.9923697380E-02	-2.2816389640E-02	1.3623133446E-02
3.4122142467E-02	3.1596178521E-U3	-4.0903/94767E-02	-1.1299176446E-02	2.8356871641E-02
-2. (253022521E-02	-1.059550/622E-02	1.0466441119E-02	1.3367522861E-02	-3.3904500267E-03
-1.1526588211E-02	-3.6457597147E-03	1.1474226909E-03	4.1058562443E-03	1.05925854276-02
3.1532492132E-03	-1.4611096408E-03	-2.0902685213E-03	3.1575555557E-04	1.5550008333E-03
5.9707962082E-04	-5.3427831152E-04	-2.0975945582E-03	-7.2644096584E-04	2.2065930138E-04
2.3785958448E-04	4.4108036785E-05	-1.5043564183E-04	-4.5688034394E-05	2.7464865342E-04
1.1101890566E-05	-2.6120170941E-05	-3.1828664955E-05	-1.1587210853E-05	6.5346581860E-06
-2.9586301032E-05	-6./238/04108E-06	1.6381666560E-07	2.8182194984E-06	5.7576957756E-07
2.4/18623580E=06	1.1946673144E-07	1./189198508E-07	-8.9980771149E-08	-1.1119083574E-07
-4.9857053525E-08	-/.45541/5879E-09	1.7284684240E=09	1.2312353967E-09	0.
-1.4684682303L-03	-1.6825170570E-03	8.2163/37029E-03	2.7556143126E-03	4.8859926352E-03
-1.8/0182830/E-03	2.2397656941E-U3	1./175/39141E-03	1.4072091127E-03	3.5229490659E-03
-5.8130990140E-04	-1.1522552042E-03	-2.7178621546E-03	-1.9349584858E=04	-5.5585246039E-04
-3.6643805288L-05	-/.U186462822E-04	-1.9656721187E-03	-5.0992140468E-04	-4.6001587793E-04
9.3300893482E-05	_3.0619143289E-04	-8.06∠4938638E-05	-1.3375509765E-04	2.6067669523L-04
1.1627451053t-04	-4.6428780602E-06	3•5879443543E-05	8•5988096738E-06	3.0605523891E-05
-1.2333522313E-05	-1.3507178471E-06	1.3163445562E-05	2.6948183183E-06	3,9379235336E-06
2.4534681833E=06	-8.0927002382E-07	-4.4555148602E-07	-7.6509284391E-07	-6.3582216995E-07
-1.0620240959E-07	-/.6052751851E-08	1.8653144940E-08	1.3287146002E-08	0.
N= 0 V= 4	1- 10			
N= 9 K= 0	J- 10			
SOLUTION	1.44852032244=113	-1-7969480614F-07	-2.1170810034F-02	1.59042047068 00
3°15030340810F 03		- A 21717600000 AC=02	1 452134004451)2	2 27414518085 (12
3049324398396-02		0 0010000000000000000000000000000000000	1 01606003356-02	2 5/3/302020205.02
-2.29096088736-02	-1.01442032090-02	5 3010765015E-03	2 10140002333C=02	
	-J.+915090150E=05	- 1 2642610822E-03	-2 4234235459E-04	6 9790545939E-04
1.40608191936-05	- 10J0JJJJ779/0L-0J	- 102042010822E-05	1 65900076016-04	
2 8288380030F-05	160010260F=06	A.5108755468E=05	1.2128601392E=06	-2.1775512929F_04
	2 6207579035E_05	2-03127117375-05	1.2010310112E=05	-3.5367779092F-04
	1 10093094935=05	7.01045410111=07	=4 2600166004E=06	
	-1./3362861225	~4.3063947314F=07	1.6031944817F-07	2,95716083768-07
	1.42077030546-00		=3.6517779453F=09	0.
-1-6050821767F=07	-6.29166875038-03	3,42544017964=03	6.6432850362F=03	-3,0098888875F-03
-10000000000000000000000000000000000000	-0.271000107950-005 	2.4390439050F-03	3,64444248318-03	1.02x67x7941F=02
4.4522005670F=03	=1,4281553025F=03	-1_4595941460F=03	1.4206670035F=05	1.58310198616-03
9.60856663475-05	=8,2538200848F=04	-2,1120049293F=03	-7.2835340985F-04	5.27344744821-04
4-14544241701-04	1.5347541886F-04	-8.8833214100E-05	-6.9332200437E-05	3.3851682743E=04
4,4155137214F=05	-2. (485393434E-UA	-5.3013651727E-05	-5.5317651728E-UA	4.0612244417E-UA
-3.3173161780E-05	-9,4091285782E-06	-6.6184/96225E=06	8.2443838704E-07	-9.2731968702E-07
5.0317962/1/E-0/	1.0700432746E-06	4.0855488323E-07	3,9139167539E-07	4,9442054463E-01
6.0562830537E-08	6.3254033308E-08	-1.8017934461E-08	-1.2834668181E-08	Ο.

N= 9

к=

ь

J= 8

N=	9		к=	ხ	J= 11			
SO		J						
001	9.685	19999907	3E-0	3	/.1544299904E=03	~1.8125526546E=02	-2.1678412293E-02	1.5750478513E-02
	3.456	122813	2E-0	2	4.1247681515E-03	-4.2132913221E-02	-1.3848334245E-02	2.4505281612E-02
-	-1./10	335368	0E-0	2	-7.2399220287E-03	5.8504936229E-03	7.4362117145E-03	-2.3679666466E-03
	-6.836	5009003 5679479	3E=0	4	1_0087106644E=03	4.40908902466-03	2. 108141/319E-03	-2.05196497265-03
-	-2.699	210935	1E-0	4	-2.9358121172E-05	2.2928207168E-03	6.1193079726E-04	-2.7663104488E-04
-	-3.668	3522257	うに-0	4	-9.0373813505E-05	1.4352635166E-04	3.2096043697E-05	-3.2237877964E-04
-	-8.613	3720495	0E-0	5	2.5850844367E-05	3.7769583387E-05	1.1840159131E-05	-7.6798361082E-06
•	-2 - 138	3701334	3E=0 0F=0	5	-2.0053037046E=00	4 939995005106E-06	=1.0219414207E=06	-6.1783467944L-07
	-1.850	0600710	1E-0	7	-2.2462042123E-08	8.3500419627E-09	5.9479635758E-09	0.
-	-2.169	852040	2E-0	2	-8.2833367036E-03	8.8368541790E-03	1.0406458951E-02	-3.1269632025E-03
-	-1.086	5466816	4E-0	2	-3.5963930084E-03	4.3933705982E-03	4.0162066919E-03	1.0129919260E-02
	3.456	5944470	1E-0	5		-2+4561585342E+03	-3.4228890641E-04	1.4956067051E-03
	1.471	1494984	5E-0	4	-1.1226623282E-U5	-7.3995899299E-05	-6.9435967069E-06	-2.4976331823L-04
	-4.525	5113895	4E-0	5	-1.8862386352E-05	2.1887657981E-05	-6.9928118734E-06	-9.8669894923E-06
	5.331	1676904	ot-U	5	2.08632/1188E-05	3.2374690739E-07	-1.7336793767E-06	-1.5995092489L-06
	-3.851	1517089	9E-0	6	-1.1911173524E-06	-2.9617967256E-07	1.0911299586E-07	-2.5232139042E-07
	1.001	/348081	12-0	8	=4.1150657815E=08	1.01091448355-08	1.19451211296-08	0.
N=	9		к=	ದ	J= 12			
SO	LUTION	N						
	9.083	3624963	8F-0	13	5.4051990375E-03	-2.0708853901E-02	-2.4510304393E-02	1.2803711501E-02
	3.290	08/059/	1E-0	12	3.1939059628E-03	-4.0613930932E-02	-8.8050879995E-03	3.1243029782E-02
	-0.900 -/-155	5123536	0E-U	19	-9.1780826912E-04 -7.5062958989E-05	3.9828770912E=03	2.2313960711E_03	8-3940976252E-05
	-3.992	2198382	16-0	13	1.1023937437E-03	1.3/92/29310E-03	-4.2273774993E-04	-1.7297128857E-03
	-6.359	9881561	1E-0	4	3.5211491408E-04	1.9077032363E-03	8.6445653628E-04	-8.4876522682E-05
•	-6.816	5818186	8F-0	15	4.6224069612E-05	1.5970678714E-04	6.9775825589E-05	1.5333545680E-04
	1.068	3820276	4E-0	15	-2,8598784532E-05	-4.2580674576E-05	-1.6287431267E-05	-5.7233549652E-06
	-0.305	5297909	01-0	1	-8.8195233560E-U7	-3.2605179717E-07	-2.8588142230E-07	3_2536445417E=07
	1.849	3544407	9E-0	1	1.4518169639E-08	-1.1289188908E-08	-8.0415984406E-09	0.
•	-2.626	5894803	UE-U	2	-1.3256303441E-02	1.1163391781E-02	9.9288465583E-U3	-2.1439440798E-03
•	-1.314	4001852	0E-0	12	-2.7169125493E-03	6.9162136634E=03	4.4404412484E=03	6.1659165512E-03
	4.509	9332993	112-0	4	-3.6770534030E-04	1.7645585526E=03	2.1340102140E-04	-1.0123U26473E-04
	-4.325	5628945	9E-0	)4	3.1081625673E-06	1.4416310721E-05	7.4616044030E-05	-3.2320891715E-04
	-1.329	9111434	1E-0	4	3.404/987/07E-05	1.6364893387E-05	1.1097743957E-05	-1.5160631012E-05
	-1.194	4220451	45-0	15	-1+3248654292E-05	4.3278827872E=07	-2.6211668693E-06	1.1915350764E=06
	40201	1009970	45-0	70 )7	1.5695625602E-08	-1.4949302093E=08	-1.0648797303E-08	-2+12525498576-08
					•••••••••••••••			
N=	9		к=	୪	J= 13			
50		N 8602212	<u>んトー/1</u>	14	8.151260076/16_03	_1.02610/16114F=02	-1.0051600170F.00	1-43861404216-02
	3.601	3319652	1E-0		3.U316085146E-03	-4.1367201767E-02	-1.4725581767E-U2	2.4235684183E=02
	2.524	4629862	9E-0	3	-2.1717803808E-03	-8.6507217562E-04	-4.8365732943E-03	6.6757098644E-04
	-1.256	5893070	/E-U	13	6.5155850505E-04	-1.7515181558E-03	-8.1973659305E-U7	-1.0914886315E-02
	-3.088	8093677	5E-0	13	1.8282248141E-03	3.0620452138E-03	-1.0920996145E-04	-1.0509162508E-03
	-3.091	1910191 4640545	48-0	)4 )4	9.0084989377E-04	-1.4619993913F-04	9,2508441720E=06	3-56654249211-04
	1.48	5071754	16-0	94	-2.0088503752E-05	-8.4437235972E-06	-3.8435897268E-06	2.0754150160E-05
	1.683	3837598	6E-U	15	-5.4789198458E-06	-9.0387952613E-07	-5.1997487288E-06	2.3156607394E-07
•	-3.498	8791410	28-0	16	-2.8047526107E-07	5.5151956536E=08	4.5469636818E+07	-1.4539252461E-07
	-1.02/04	4533783	5E-0	)2	-8,5661015682E=03	1.1444347341E=02	1.5778727189E-02	-2.8248329680E-03
	-1.058	8961628	4E-0	2	-3.25/1950059E-03	7.6040609049E-03	4.7723488248E-03	-1.7598479509L-03
	1.005	5870374	/E-U	4	6.//00611605E-04	1.2486017229E-03	2.4997468908E-04	2.7425118079L-04
	2.018	8135073	1E-0	)4 1 5	4.7206708717E=04	2.4285079787E=03	1,1117009801E-03	-1.7584642673L-04
	-8°1/5	2944384 / 106454	86-0 26-0	15 15	202121439592E=06	2.3204180430E=04	7.1183987889F-05	1.01400/191/6-04
	-3.641	8580847	16-0	15	=1.04875172/4E-06	2.4602279112E=06	6.6695497295E-06	6.8779264770E-07
	-1.65	1257.100	6E-0	6	2.8880602291E-07	1.9638273465E-07	4.0143066983E-07	2.4912921695E-07
	1.66	5453685	5Ł-0	) /	6.45967/2935E-09	1.2620378798E-08	8.9898414567E-09	Ο.

N≓ 9	к=	ង	J= 14			
SOLUTION						
9,96024	77241E-03		6.6526959033E-03	=1,7156/21780E=02	-2-2196405759F-02	1-6303389608E-02
3.48174	57258E-02		3.5438962241E-03	-4.1266203240E-02	-1,5056999805E=02	2-4398643867E=02
1.21126	41970E-02		6./637457691E-03	-5.4577343570E-03	-4.3036297936E-03	4.7582843473E-04
5.60930	64221E-03		9.1856651137E-04	-4.3004652172E-03	-1.4654219694E-03	-6.1587750985E-03
-2.35892	60250E-03		1.8155210255E=03	1.3798989966E-03	5.0338739645E-04	-9.7946806302E-04
4.49888	02196E-05		5.1842008145E-04	-2.5802548934E-03	-5.5833270261E-04	1.4404405299E-04
4.49204	92292E-04		6.3870560469E-06	-1.1006/68179E-04	-7.5251551857E-05	-6.6955641890E-05
-5.01033	97649E-05		3.2067779762E-05	3.3388504636E-06	1.1833021375E-05	-2.3439511034E-06
3.86945	91805E-05		1.9216173400E-05	-1.9650194224E-07	-2.0504410447E-08	-1.7576474789E-06
4.66801	46141E-06		1.0534543212E-06	2.0115442877E-07	-3.0532707632E-07	-1.1455618636E-07
5.96427	89028E-08		-2.8419302181E-08	-1.5927165946E-08	-1.1345356506E-08	0.
-2.01944	14812E-02		-1.1153018363E-02	8.9235492068E-03	1.0542028327E=02	-3.6180349552E-03
-1.14120	140026-02		-3. (300338303E-03	7.0811112908E=03	3.30/636/5/5E-03	-9.338/02189/E-03
-1.01346	463/45-04		5. (689)639301-04	3.04045042705-04	-4 69920190346-05	-1.33040734525-04
-1.66440	200758-04		_8-5268699784F_05	1-5298581332E=05	-2,2212700888E_05	3 5545520070E_04
8.29980	12868E-05		-3, 7456399012E=05	=5.2613997771E=05	=1,8447452305E=05	4,2346399170E=06
2.41975	15616E-05		2.5812299536E-06	-3.7462091987E-06	-4.2481937973E-06	-1-1479269718E-06
-2.91661	01446E-06		-1.4031373999E-06	-4.2698307808E-07	-1.3967538782E-07	-3.6917231938E-07
-1.91379	60502E-07		-1.9924835569E-08	-9.8616836393E-09	-7.0247473419E-09	0.
N= 9	κ=	8	J= 15			
SOLUTION						
9.14595	68410E-03		7.1720017222E-03	-2.0142931652E-02	-2.2156297849E-02	1.4359823765E-02
3.32381	26027E-02		5.0880049570E-03	-4.3293381037E-02	-1.0160258527E-02	2.6748355754E-02
1.96830	52361E-02		/.9420734710E-03	-8.8201588864E-03	-9.3711967282E-03	2.5281697871E-03
1.00379	34910E-02		3.4973456210E-03	-4.7313259959E-03	-2.9834514523E-03	5.8428119715E-04
-1.64160	77161E-04		-5.9788851078E-04	-5.6203024453E-04	-1.2616813544E-04	1.3190377383E-04
2.14535	34494E-04		1.3102517783E-04	-1.2539082211E-03	-4.8017673315E-04	3.1784225618E-04
2.46728	87898E-04		6.8140530722E-05	-3.2808155347E-05	-6.6790002378E-05	-4.2271843745E-04
-8.18/20	82852E-05		-4.4652458278E-06	4.4378550726E-05	-3. (63/291313E=08	-1.3169557668E-05
-2.44045	285286-03			-2.9044998200E-00	1 34130954005 07	
- 45465	203202=00		5 3032770632E-00	- J. 6400294900E=07	-1.3813983499E=07	3.8209086727E=07
-1-80139	09704F=02		-/-8235508237E=03	8-0902672403E=03	8-2661711542E=03	-2-0021573619E-03
-8.70425	27207E-03		-2,9530474945E-03	5.3185551460E=03	2.1642633494E=03	=2.0021373019E=03
-3.52055	77601E-03		2.3883103209E-03	2.5340494906E-03	1.3990434339E-04	~1.6566706819E-03
-5.86710	43414E-04		4.0636251460E-04	-1.9959793035E-03	-5.3457119129E-04	2.0085402431E-04
3.11468	25702E-04		5.1257716269E-05	-1.1607609576E-04	-4.0185887278E-05	-7.7154448907E-05
-2.32742	52663E-05		-2./1941/8360E=07	4.4029949734E-06	-4.6590832108E-07	-3.7143819162E-06
3.0638/	09220E-05		7.5294908095E-06	1.9447603974E-06	-2.1979363539E-06	-1.0610568852E-07
5.70009	95523E-06		1.8813113116E-06	4.8626562561E=07	-1.0891460614E-07	3.5267875995E-07
1.66192	16245E-07		2.2142738441E-08	6./671606724E-09	4.8204338817E-09	0.
N= 9	K =	8	J= 16			
SOLUTION						
9.44836	58091E-03		4.0943008893E-03	-1.9374806654E-02	-2.6357458110E-02	1.3735712657E-02
3.21990	55739E-02		2.9728881189E-03	-3.9823608160E-02	-9.0516897713E-03	3.2157239482E-02
2.19542	29384E-02		1.0863174351E-02	-6.5284675797E-03	-1.1760189098E-02	5.7149138366E-03
1.18784	60521E-02		4.0239784484E-03	-5.7219134987E-03	-5.1664817772E-03	8.5882381083E-03
4.30146	24160E-03		-1.0847503003E-03	-5.0095298959E-04	7.6643675730E-05	1.7849405261E-03
2.16588	73522E-04		-4.3227347637E-04	5.8856830623E-04	2.6557553782E-04	-5.5281961203E-04
-2.37768	43895E-04		-2.4161438164±-04	3.2539567073E-05	-L. 1943216499E-05	4.9118804817E=05
-0.00009	94540E-05				-0*I(IAA)J0443E 04	
6)66C00	09338E=U0 85156E=U4		0.747777790AF=08	10000741400024-00	100400120442E=00 6.1383507004E=07	
-1044131	705675-00		=/_1109215095E=07	-1-84140909674-08	-1.3116861309F-08	0.
-1,03640	317298=02		-3-3269276058E-03	3.3221819188E-03	5.7206224575E-03	-1.5423262437E-03
-1.50834	24034E=03		-1.3077119526E=03	3.2246408581E-03	1.5013937439E=03	-7.8905864610E-03
-2.86508	03912E-03		1.8242676407E-04	1.4006171772E-03	-4.0746282059E-04	-1.1553813227E-03
-4.95107	72250E-04		3.7552820631E-04	-2.1962355351E-03	-7.9370323624E-04	2.4091549063E-04
2.32021	56325E-04		4.9970515831E-05	-1.6549376539E-04	-4,5720862561E-05	-3.6787559140E-04
-1.02989	98850E-04		3.6942763386E-05	4.4191242397E-05	1.6547623736E-05	-8,1289969204E-06
-4./8998	17230E-05		-1.0910463788E-05	-4.3348/36948E-08	4.4787130141E-06	8.5586108255E-07
-4046961	45245E-06		-1.3277942009E=06	-3.2167438477E-07	1.5079920848E-07	-2.1273088187E-07
	UF 100F _110				m/_4519564//18~110	12 <b>.</b>

SOLUTION				
8.7935060816E-03	-8.2137328938E=03	-2.0958989957E-02	-1.3544403395E-03	2.6846554465E-02
-1.8129086500E-02	-3.1590493411E-02	2.6827360449E-02	2.8495960530E-02	-1.0716638425E-02
2.9877029693E-02	-3.9927683951E-03	-7.8959335571E-03	3.9429213215E-03	1.6435180201E-02
-6.4208536810E-03	-5.7533213264E-03	4.2208695928E=03	5.5000251157E-03	1.0920302441E-02
1.7536912502E-03	-2.9343248390E-03	3.5850452064E=03	1.5756533509E-03	6.3359069947E-04
-6.5571392100E-04	1.0303835564E-03	1.6647870433E-03	-1.4957968269E-04	-1.1948320541E-03
1.88998998196-04	-2.2898157566E-04	-3.3103921681E-05	-2.0953635615E-04	4.2280555751E-04
-2.1843968293E-04	_4.0421020104E-05	-7.4458097564E-05	1.3535311428E-05	-3.3897729933E-05
1.9615471294E-05	-4.8865610311E-06	1.0762628552E-05	1.8838883252E-07	5.7478363557E-06
4.8389185774E-06	2.4307226987E-06	-3.1277117441E-07	8.1156922302E-07	-9.6249973749E-08
3.3168961231E-08	-1.4103915315E-07	2.6868662118E-08	-1.8878249003E-08	3.1502225899E-09
U .	0.	0.	0.	0.
U.	U.	0.	0.	0.
υ.	υ.	υ.	0.	0.
υ.	U .	0.	0.	0.
U •	U.	0.	0.	0.
0.	U.	0.	0.	0.
0.	U.	0.	0.	0.
υ.	υ.	υ.	0.	0.
υ.	U.	0.	0.	0.
N= 9 K= 9	J= 1			
SOLUTION				
30L0110N 8.4168143346F=03	1 01125608256-03	-2. 2173591101E-02	1 20003602355 02	2 44245521545 02
-1.22334359645-02	-4-00683161175-02	2.04760898056-02	2 (1546761865E-02	-2 55995012045-02
2 2013740551E=02	-4 55051210125-02	-1 /4521729675 02	4 45094774401E 03	7 2372200403E 02
		3.10/10501886-03	5 /3314449912-03	
-2.08824180836-03	-2.4005741618E-03	-8.4104913722E-04	1 20522000026-03	-1 31104327035-03
-2.7119747734+=04	4-1506696322E-04	1.98520548148-03	-2-3453265788E-04	2 52041259885-04
6-6713852538E=05	4.29658079171-04	-3-89674982374-05	5.4928047678E_06	7 36450005435-05
1.24730400511-02	-4.00105833305-05	6-51250728517E=05		1 09625526695-05
-2. (5635516071-05	-1-3226099851E=06	-1-0927927486E-05	6.2854860679E=07	=2.8942330784F=06
-1.8324976234E=06	-2-10678343711-06	6-1786365580E=08		1.5979628800E=07
-4-9116897206F=08	1.1477080260F=07	-2-2233489621E-08	1.7597898689E_08	-3.1072576598E=09
/_8/65/04103E=03	=1-5063701762E=04	=5-6201884683E=03	2.8311354733E=03	2.8304201020E=03
-8.51492918791-04	-/-94105972421-03	1.4049873038E=03	1.5129211691E=03	6-2436109004F=03
-1-05679794936-03	-2-34963682675-03	3_8576255942E=04	6-0186435029E-04	-5-6237026465E-04
-6.45471954148-04	2 / 868218638E=04	2.1730811282E-03	-3-6552567874E=04	-3-27760736075-04
2.0439932098E-05	1.70765015265-04	-1.1323256900E-04	-4,7900975931E=05	4-1163/497171-04
-/ //280113831-05	= 3, 5124355018E=05	2.08642949071-05	2.3741576867E=05	
4-52621582911-05	-1.1726839832E=06	-6.63131334711-06	3.3512951808E=06	9.96964126605=07
3.74351944245-06	-6.6491116747F=07	-6-8581243727E-07	1.3005045804E=07	3.30256402701-07
-8.8582873041E-08	-2.2169942411E-08	2.1158593879E-08	-3.0224997708E-09	5.1850959647E-10
				• • • • • • • • • • • • • • • • • • • •
N= 9 K= 9	J= 2			
SOLUTION				
8.9057/16445E-03	-2.8238651286E-03	-2.0399816876E-02	7.5694440605E-03	2.7410637403E-02
-1.1/30806212E-02	-3.3008462553E-02	2•6374/26499E-02	1.9034943724E-02	-2.1332572562E-02
2.0881804098E-02	-2.0679332144E-03	-1.1204786348E-02	3.9952926397E-03	8.0258306062E-03
->.1439059160E-03	-/.62170/0/52E-03	2•8338/90429E=03	3.6281599466E-03	2.7339567021E-03
1.6389389754E-04	-5.6417134615E-04	4.0069957446E-04	5.5106796034E=04	-3.4430140897E-04
-2.2943783049E-04	-4.8396484185E-05	-1.2592201332E-03	2.3213863108E=04	1.9924026443E-05
-3.0814285008E-05	-9.8875571140E-05	-2.8334820979E-06	6.2130063222E-05	-3.3581336202E-04
-2.4348652396E-05	6.5683527929E-05	-3.1246457679E-05	-4.8697418394E-06	1.0411595349E-05
-3.8268708555E-05	1.0515082069E-05	8.2539639980E-06	-6.4462016039E-07	-1.3225136783E-06
-3.8245534601E-06	1.2777797027E-06	3.1403109005E-07	3.6275888584E-09	-2.9517032713E-07
8.2652991135E-08	-5.0021257220E-08	9•4833929224E-09	-1.4038339087E-08	2.9795348407E-09
1.6245884727E-02	-2.4329874518E-03	-8.5439841163E-03	2.6043485604E-03	6,6788804798E-03
-3.6198442126E-03	-5.6541783726E-03	3.3386924645E-03	2.1547516877E-03	1.0681871976E-02
-9.5995843388E-04	-2.6953815247E-03	9.9340968300E-04	1.6542544096E-03	-9.1502177483E-04
-8.2463742080E-04	3.5434221182E-04	2.2370921223E-03	-1.0691740953E-04	-4.3691392203E-04
1.8496/19301E-04	1.8156549412E-04	-8.6750197110E-05	-4.5366332168E-05	1.7207778984E-04
-1.9739538367E-05	-3.2969871526E-05	9.2285934648E-06	7.7859911262E-06	-3.5161285150E-06
-5.3420628004E-06	-2.9333844121E-07	2.2232338270E-06	-8.3479072143E-07	1.6305197266E-07
-3.1040208301E-06	8.5252/52773E-07	5.5313501024E-07	-4.6232683734E-08	-4.8613840755E-07
1.30917356/8E-07	2.2139892544E-08	-3.7676665146E-08	4.9888836739E-09	-1.0228756028E-09

N= 9

K≈ 9

J= 0

N= 9	K= 9	J= 3			
SOLUTION.					
30L0110N 8.641699685	321-03	-1-5771873665F-03	-2-1724410996E-02	8 1072200070E 03	2 5454702426 02
-1.35164477	196-02	-1.3181798376E=02	2 4 2 8 9 (19 ) (15 ) F m (12	2-2363277157F-02	-1 01492250561-02
1,428830222	21E-02	-3. 1838266339E-03	-7.6297/41584E-03	8.1331477327E-04	6.4168103992E-03
-3./59709815	08E-03	-4.3942919408E-03	3.0160167787E-03	2.1439153678E-03	-4.1058193583E-03
1.108684193	34L-04	1.2766129586E-03	-3.4689/35119E-05	-8.5941157450E-04	5.3479635046E-04
1.165541595	53E-06	-3.0959938655E-04	-2,4202554615E-03	1.6168082648E-05	4.7652237897E-04
-2.88007539	12E-04	-1.7024587256E=04	3.4756010802E-05	8.3068077653E-05	-2.4662377174E-04
2. 1011 (990)	SUE-05	4.2400784365E-05	-2,2964951634E-06	-1.3718491075E-05	5.9072165918E-06
5-936610325	+20-00	-4 22883017216-07	-1. /607/50363E 07	-109625798045E-06	
-1.009907456	5/E-07	-1,9463561105F-08	8.1949219656E=09	8-9769303362E=07	-2.77053807831-09
2.1/98/814	30E-02	-4.0081946667E-03	-1.2163551040E-02	2.8247295839E-03	8.77374253141-03
-5.354466984	+9E-03	-1.1743286183E-03	4.3577635677E-03	3.0251038060E-03	1.0001198553E-02
-1.51436010	0E-03	-2./133310074E-03	5.8359023297E-04	1.4188071465E-03	-8.8927942708E-04
-/./51809538	39E-04	4.1552249995E-04	4.9613963155E-04	-1.9970261293E-04	-3.9240815412E-05
-5.005905408	58E-05	1.2907958737E-05	-1.3883979151E-05	-3,4797825438E-05	-2.6828641377E-04
-4 444021211	14E-06	4 a 7349396049E-03	-20/01090/1/4E-05	-1.5569177115E-05	7.5057163465E-07
+8.64318313	00L=00	_4_7197191119F_07	2.0802134723F=05	-3,4070249110E=00	3 93653549616-07
-1.0/1/824/9	-/E=07	5-4863829135E-09	4.6019758357E=08	=5,1065495031F=09	1.4993402291F=09
N= 9	K= 9	J= 4			
SOLUTION					
7.892898211	115-03	-2,7539004628F=03	-2-4125170503E-02	6-4912849217E_03	2-50344589151-02
-1.482521785	55E-02	-3.0668922879E=02	2.3457414500E=02	2.6632879563E-02	-1.7135724410F-02
6.8/5120158	37E-03	6.5923/64490E-04	-2.1457845095E-03	3.0196753169E-03	3.3201612571E-03
4.635699621	L9E-05	-1.1948522518E-03	2.0748718781E-03	8.3414829383E-04	-1.0446251428E-02
6.183456661	LUE-04	1.6902573227E-03	-1.2729328494E-03	-1.9257559227E-03	4.4914626440E-04
4.842668556	59E-04	-5.9568829492E-04	-1.5811615072E-03	3.6599787588E-04	4.2094919521E-04
4.007130211	13E-05	-5.6374651834E-05	1.1133493637E-04	5.5903970764E-05	1.4139097512E-04
-4.45388892	/8E-05	-7,3995968857E-05	-3.0733190813E-06	-5.3042697226E-06	-1.1281293858E-05
2 6 6 7 6 7 6 3 9 8	37E-05	4.01400620236-07	-1.8325118567E-06	3.1389809747E-06	1.9559582865E-06
		-3,0314009170E-07	-J. 60612087232E=07	-2.00304808943E-07	-2.9281093730E-07
2.42100588	511-02	-/_14437/2111F-03	-1-5789626719F=02	6-1002609185E-03	8.96056637445-03
-4.62886902	54E-03	-8.9435346729E-03	4.5426404391E-03	4.6366209817E-03	4.3246288763E-03
-3.099849474	41E-04	-2. 3043354865E-03	7.5810216206E-04	2.8598945848E-04	-1.0928761447t-04
-3.752238014	42E-04	4.4845286139E-04	-2.0416508017E-03	3.4620979645E-04	1.6708169197E-04
1,409907098	82E-06	-2.2273053065E-04	1.1964016949E-04	1.1989709058E-05	-4.0401593259E-04
5.03/7/576	57E-05	6.1009522938E=06	-6.8533183365E-07	-2.4136677041E-05	1.0865891216E-05
7.220138604	46E-06	2.8459809817E-06	-6.3855881906E-06	2.5762185415E-06	-1.0177502194E-06
2.890/1185	94E-00	-1.104/910200E-0/	-4 4500274272E 08	1 • 9883063894E-07	-1.1779243550E-07
3.418000200	J1L=08			204012004205-03	=1.934900702JL=09
N= 9	K= 9	j= 5			
SOLUTION					
30LUTION 9.490726770	051-03	=2-2009403244F=03	=1.8249100674F=02	7.46254342875-03	2-92736946381-02
-1.3/8456964	41E=02	-3.2010732303E-02	2.3617831959E=02	1.9215372101E-02	-2.2814825956E-02
-3.295408900	08E-03	1.0779248858E-03	-8.6876693755E-04	5.9300626760E-04	-2.8803490132E-03
1.25255572	55E-03	-5.8600849326±-04	3.6893646717E-04	-1.2506245506E-03	-9.5249689894E-U3
1.20833777	51E-03	4.2362839341E-03	-9.1448102268E-04	-7.8192970391E-04	7.3094710187E-04
1,002902000	61E-03	-5.4178409936E-04	3.9518272667E-04	-5.0798966389E-07	-3.1547392421E-04
8.32360815.	31E-05	-8,1668878539E-05	2.1107238027E-05	-7.3430811393E-05	4.6505078217E-04
-4.13253497	0/E-U5		1 10152740105	3.200/601/10E-05	- 1 + 4460 / 52 / 0 / E = 06
-2070837244	586-05	3,2074870324F=07		304400440933E=07 =1_0189760419F=07	-2019221098E-00 40494106551F-09
	90E=09	-5.8192607901F=08	4.0366173870F=08	-1.2472441006F-09	-2.13358770675-09
2.6/012626	10E-02	-3.2428821241E-03	-1.3058857586E-02	5.0398242793E-03	1.2059239127E-02
-5.517106020	01E-03	-1.6955737113E-03	4.4490901091E-03	5.1533734846E-03	-6.0420801947E-04
4.6109/837	96E-04	1.1878385493E-03	1.0473356476E-04	5,5299413878E-04	2.8905581091E-04
4.66318062	14E-04	4.5308488542E=05	-2.2402569683E-03	3.2176211023E-04	6.2278931033E=04
-8.9/3306/6	//E-05	-6,0104859662E-05	8.7162084977E-05	1,1025458628E=04	2,2006700058E-04
-1.386388960	53E-06	3 6 7045366745E=05		203940881488E=U5	2 58420300495 0
3,07655800	ロラニーリン・ ドントーリン	-201330194033E=U0 3.41815708427E=07	8,39966928766.07	4-8011405305F=08	=1_8328362491F=07
4.6564/621	491-08	6.4391886015E-08	3.4143880311E-08	9.7076904974E-10	2.3176940833E-09

N- 9	K- 9	J= 6			
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8,40022999	11E-03	-1.1477898992E-03	-2.2149213293E-02	9-2437736100F-03	2.6709201331F=02
-1.26874687	H8F=02	-3.1174756703E=02	2-3201170898E-02	2.1666972342E-02	-2.2152129499E-02
-9-83919608	336-03	-6-8856554797E-05	6. /909705252E_03	_3.5793935972E_03	-2 7154051477E-02
1.43()41993(	001-03	3 24514650068-03	_1_3117247160E_03	-2 03652003265 02	-7 73800004105 03
1 250427630	00E=03		2 52050340585 04		9 54447200505 04
L 620505050	105 06			-1.2132844050E=03	8.54447280586-04
0.42020091	196-04 055 05	-1.4294043/12E=04	2.51099304262=03	-4.20666/1692E-04	-3.3250609012E-04
2.14/1/055	25E-05	2.0115669833E=04	-1.1615603825E-04	-6.1005317425E-05	~/.8601296658E-05
2.042929711	86E-05	-1.6983/44593E-05	1.5/3894544/E-05	-3.5099517737E-06	6.6948508012E-06
-3.67452032	91E-05	-1.04/9/22/1/E-06	/•/627/53541E-06	-3.8198845419E-06	-2.2155675729E-07
2.43911159	29E-06	1.7003252664E-07	-7.2226047308E-07	2.1779152590E-07	2.6989871771E-07
-1.45474135	59E-08	2.5093682482E-08	-4.6539308843E-08	4.3477990161E-09	1.7230084432E-09
2.36520928	61E-02	-5.1210096197E-03	-1.3425376869E-02	2.2534231434E-03	9.9468569928E-03
-6.58714646	59E-03	-/.6682988541E-03	3.5558172606E-03	4.6311119142E-03	-8.5153174409E-03
5.02216510	14E-04	1./587466839E-U3	-l.1441964566E-03	-1.2545019924E-03	3.5296960341E-04
6.82548610	53E-04	-3.7622422119E-04	-8.4322051859E-04	-1.6598477201E-04	1.1411930455E-04
-2.19443620	22E-04	-1.3484058348E-05	-4.4873301340E-05	4.0310611635E-05	3.4592645979E-04
-6- 15432255	03E-05	-1-9762754308E-05	4.2078359468E=06	1-0342033729E-05	=1.3103493728E=05
-2. /428/543	556-05	-5 02750207878-06	1.2167810651E-06	-3 0868062020E-06	-5 1544604242E-07
-4 17216214	145-05		-1 20420420175 07	- 0003138626E 07	3 53007230425 07
-4011510214		- 40303079881E#08	-1829830420176-01	-3.0903138626E-07	3.0789123082E=01
-9.49548918	015-08	-4.4928282213E-08	-1.1513327389E-08	-6.21//424935E-09	-2.03/200/5132-09
N= 9	K= 9	J= 7			
SOLUTION					
8.54178474	14L-03	-2.3921626547E-03	-2,2041622210E-02	7.1192213926E-03	2-5554674973E-02
-1.4885/186	841-02	=4.2911082677E=02	2.47339400286=02	2.3295852278E=02	=1.8014887187E=02
-1. /4273004	201-02	2.9960721235E_U3	1.01421106136-02	-2.5301062866E-03	-6 98476415975-03
4 20060620	845-02	6.0703382167E_03		-3 01665520448-03	-0.67063621965-06
-1	105-06		-2 12027026115-06		1 14047730045 04
-1004140722	196-04		1 02202076455 02	7 45944207405 05	3 40033017135 04
1. 505((554)	912-04	0.01/2/13/140-00		- / + 9844 39 / 40E+03	-3.08923017122-04
100000001	20E-04	1.7331257105E=04	-8.1021101618E-05	-2.4525390707E-05	= 3.1/52351437E=04
2.88044352	352-05	5.6322405727E=05	-2.4/3820/55/E=05	-2.0193527189E-05	5.21506731296-06
2.70443051	74E~05	-8.6441139599E-07	-2.5202086890E-06	1.6406724762E=06	8.5078927931E=07
1.23898821	42E-06	-1.1923436162E-07	-1.7015863647E-07	-6.0278948844E-08	-4.6999194319E-07
1.27077721	87E-07	1.1200842668E-08	4.3021974384E-08	-5.3119074826E-09	-1.2654300010E-09
1.91062924	60E-02	-1.5979680556E-03	-1.1010709019E-02	4.0386513992E-03	7.1584211408E-03
-4.81215369	52E~03	-6.9303639248E-03	1.9610343036E-03	4.1282571253E-03	-1.0748779237E-02
1,24014585	04E-03	2.8689505140E=03	-7./172/88230E-04	-1.8676791780E-03	1.0206434938E-03
5.46521924	08E-04	-5.3031071722E-04	1.4032391367E-03	2.6047446848E-05	-3.5939181572E-04
1.72370832	65E-04	1.0290995956E-04	-5.0977427719E-05	-2.9340045273E-05	6.5771259702E-05
3,21284397	59E-05	-1.8732462418E-05	1.1016300169E-05	-5.6009160146E-06	-4.9191962705E-06
-3.56186907	59E-05	1.1492911409E-05	5.0452532656E-06	4.7002111055E-07	-1.8331662935E-06
5.60839640	86E-06	-1.8672204406E-01	-3.3309928345E-07	2.0973458587E-07	-3.5055185221E-07
9.58730820	12E-08	-1.3510888397E-08	-1.0001595485E-09	1.1631831712E-08	2.8848898209E-09
		• • • • • • • • • • • • • • • • • • • •	•		
N= 9	K= 9	J= 8			
SOLUTION					
8.43660621	51E-03	-2.4881348827E-03	-2.2257275491E-02	7.1864626734E-03	2,5885729059E-02
-1,36311586	20E-02	-3.2204450904E-02	2.4608532181E-02	2.3211800883E-02	-1.8748111114E-02
-2-32176008	38E-02	3-8399505087E-03	1.2270825297E-02	-3.2622882800E-03	-9.6215516511E-03
5-63688440	371-03	1-9059243519E-03	-4-2217695998E-03	-3,5356400453E-03	6.2466513496E-03
-1.4492/349	141-04	-1-25285584731-03	6.54060486951-04	1.1289370849F-03	-4.9175261667F-04
-4./7001738	181-04	2.21993/3906F=04	-1.3350689936E-04	-1.2820455551E-04	8.1115753830E-05
	845-05	-8.1010570633E=06	-1-40678168911-05	5-2542148821E-06	-1.8400539579E-04
/ JUR233EK	366-05	1-27876286815-06	=1,0097580263E=05	-1-1869416552F-05	2.19962807715-06
10200000000	40F-05	-6.41890083231-07	-5-8077706329F-06	2.8067605787F-06	6.2388440887F-07
2840V20292		H 4502607600F_07	/_4187930227E=00	=1-1763067351F=07	4-3783837030F-07
-4.02822099	100-00	7 60002673766 00	-3-112562566105-00	4-1062141074E-00	7.7333300700F-10
-1.1/618025	+0E-U/		-Javej0290010E=08 _0_2/76204016E=03	7017021717/0E=07 2 ()0002154505-03	3.86062666716 02
1.07694209			1 20408044015-03	2.66026766005.02	
-2.14681023	20E-US		1043F30433E VE	1 21/0000000E 00	0 120/1053075 0/
2.20190500	102-03		-Jely433/743/E-U3		1 44002034335 04
4.10885582	99E-04	-0.1030191223E-04	2 8 9 1 6 7 4 8 3 3 4 7 E = U 3		
1.40690107	22E=04	2.8201681605E-04	-+-5U36U9462UE-05	-8,0000480220E-05	-3.430/32/560E-04
-5,70389938	03E-05	6.9305899377E-05	->.1053286533E-05	-8.0663840459E-06	4.7689498235E-06
1.34419768	43E-05	-6.6125852664E-06	-1.U236764348E-05	9.1142510941E-07	-4. (146027101E-07
-1.0/50/985	19E-06	1.7359625640E-06	1.55554756852E=07	2.7712186274E-07	2.2569762860E-07
	301-018	8.53544042711.08	L_6714263176E-08	-1.6064380553E-08	3.0538266164F-09

N= 9	K= 9	J= 9			
SOLUTION					
8.80665220	075E-03	-1.6373766991E-03	-2.0729896227E-02	8.2994580333E-03	2.7570742063E-02
-1,3480818	627E-02	-3.1461297563E-02	2.3253453004E-02	2.1280141599E-02	-2.1901057791E-02
-2.5217975	634E-02	2.8943276290E-03	1.5036345163E-02	-5.4627189636E-03	-1.0015552341E-02
5.0081392	459 <b>L-</b> 03	8.7556645262E-03	-4.9124609410E-03	-4.4499528312E~03	9•9435956225E~03
-1.3/64030	528E-03	-3.2157667973E-03	/.4177145350E-04	1.2133057498E-03	-8,5494278097E-04
-8,9121756	177E-04	4.2598950796E-04	-2.2524695356E-03	3.2398161144E-04	3.6376644420E-04
-5.6680617	049E-05	-1.7437052958E-04	1.0840621874E-04	5.1880566312E-05	3.3107680499E-04
-2.4257531	117E-05	-3.0835842847E-05	1.6281491936E-05	1.8634433023E-05	-5-6146765047E-06
-3.1078689	643E-05	8.9607280303E-07	4+3340123043E-06	-2.2269569554E-06	-7.2971173263E-07
2.2316300	151E-06	-3.6779884914E-07	-4.0826536831E-07	8-3290572110E-08	-1.7737822977E-07
4. (537578	171E-08	1.2702084273E=08	1-0882977663F-08	-1-5805095364F-09	=2-6014331957E=10
8.2311981	9165-03	-9.0105339113F-04	4-3514978114F-03	2.2162397567E-04	7-5263086256E-03
-1.2924273	581E-03	1.3691819504E_03	8-9925269048F-04	1,1859538113E-03	-3-6263364211E-03
-2.3014360	8186-03	8-9179497626E-04	-2-6274101938E-03	_4.7903699068E_04	-9.3653113317E-04
2.5122587	3155-04	_4.9907674598F_04	4-1535/00050E-04	-1.9931764556E-05	-8 8785071208E-04
1.0269916	0395-04	-2.7099335216E=04	-6-9070724517E-04	-1-4377629599E-04	-2.69176314335-04
1 0052475	2545 04	1 83403903745 05	7 22010544085 05	9 71051444005 04	2 70447204295 05
10302412	2006-04				2 0 1044139438L=03
6 4742003	3912409	-3.148/8031/92=00	1 00//0/9/03E=03	-0,98347923182-08	4.94/0192833E=00
-4.0254134	1946-06	-2.034/418/4/3E-UB	2.4292776926E=07	-/.4032128594E-0/	-1.1308490448E-07
3.7401632	394E-08	-1.3423418582E-07	-2.5691248052E-08	1.82230508415-08	3.1394629826E-09
				5	
N= 0	×- 0	1= 10			
N- 7	~ 3	54 10			
E CH LLT V CAN					
50L0110N	0751-03	1 62727660018.02	-2.17204042275-02	9 200/590323F-03	2 7570742043E-02
0.0000000		-1.03/3/0075436 03	2 22524520045 02	2 12001415005 02	2 10010577015 02
-103400010	627L-02	-Jel40129/J0JL-02	1 6034346143E-02	-5 (427)00434E-03	-1 0015552341E=02
#20221/9/2		2.89452162902-03	1.00000040105-02		
5.0081392	4596-03	8.7556645262E=05	-4.9124809410E=03	-4.4499528512E-U5	9.94359562255-03
-1.3764030	528E-03	-3.215/66/9/3E-03	7.4177145350E=04	1.213305/4985-03	-8.54942780976-04
-8.9121756	176E-04	4.2598950796E-04	-2.2524695356E-03	3.2398161144E-04	3.637664442UE-04
-5.6680617	048E-05	-1.7437052958E-04	1.0840621874E-04	5.1880566312E-05	3.310/680499E-04
-2.4257531	117E-05	-3.0835842847E-05	1.6281491936E-05	1.8634433023E-05	-5.6146765047E-06
-3.1078689	643E-05	8.9607280302E-07	4.3340123043E-06	-2.2269569554E-06	-7.2971173262E-07
2.2316300	151E-06	_3.6779884915E-07	-4.0826536831E-07	8.3290572108E-08	-1.7737822977E-07
4.1537578	1/1E-08	1.2702084273E-08	1.0882977663E-08	-1.5805095363E-09	-2.6014331956E-10
-8.2311981	916E-03	9.0105339113E-04	-4.3514978114E-03	-2.2162397567E-04	-7.5263086256E-03
1.2924273	581E-03	-1,3691819504E-03	-8.9925269048E-04	-1.1859538113E-03	3.6263364211E-03
2.3014360	818E-03	-8.9179497626E-04	2.6274101938E-03	4.7903699068E-04	9.3653113317E-04
-2.5122587	315E-04	4.9907674598E-04	-4.1535700051E-04	1.9931764557E-05	8.8785071208E-04
-1.0269916	039E-04	2.7098335216E-04	6.9070724518E-06	1.4377629589E-04	2.6917631433E-04
-1.9052475	258E-04	-1.8368389274E-05	-7.2391056498E-05	8.7195144401E-06	-2.7044739438E-05
-6.4/42603	331E-05	3.1467665179E-06	-1.0877879783E-05	6.9834792314E-08	-4.9470752833E-06
4.0254134	194E-06	2.3474187473E-06	-2.4292176926E-07	7.4032128594E-07	1.1308490448E-07
-3.7401632	394E-08	1.3423418582E-07	2.5691248052E=08	-1.8553626891E-08	-3.1394629826E-09
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N= 9	K= 9	) J= 11			
SOLUTION					
8.4366062	151E-03	-2.4881348827E-03	-2.2257275491E-02	7.1864626733E-03	2.5885729059E-02
-1.3631158	620E-02	-3.2204450904E-02	2.4608532181E-02	2.3211800883E-02	-1.8748111114E-02
-2,3217600	838E-02	3.8399505087E-03	1.2270825297E-02	-3.2622882800E-03	-9.6215516510E-03
5.6368844	037E-03	1.9059243579E-03	-4.2277695998E-03	-3.5356400453E-03	6.2466513496E-03
-3.9992734	914E-04	-1,2528558473E-03	6.5406048695E-04	1.1289370849E-03	-4.9175261667E-04
-3.1/09173	838E-04	2.2199373906E-04	-1.3350689935E-04	-1.2820455551E-04	8.1115753830E-05
-9.6056560	384E-05	-8,1010570628E-06	-1.4067816891E-05	5.2542148819E-06	-1.8400539579E-04
7.2053335	535E-06	1.2787628682E-06	-1.0097580263E-05	-1.1869416552E-05	2.1996280771E-06
3.4802859	2441-05	-6-4189008321E-07	-5.8077/06329E-06	2.8067605787E-06	6.2388440887E-07
-4,0585240	9181-06	8-3592697500E-07	7.4187939222E=07	-1.1763067351E-07	4.3783837040E-07
-1.1/61802	546E=07	-2.5800264375E-08	-3.0256256617E=08	4-1962141976F-09	7.7333392708E-10
-01/6Q420	9471-02	2.0876882849F_03	9.2776204815E-03	-2.0900215658E-03	-3.8606346471E-03
2.1468702	3231-03	3-6806563790F-03	-1.2040886480E-03	-3.6692674690E-03	8.9252491938E-03
-2.2010060	076-02	-2-6765704870F-03	3.1943579438F-05	1.3149099389F-03	-8.1304185307F-04
-202017030	2001-01	6. 7030701223F-04	=2,9167493367F=03	3.5427713074F-04	1.4488392633F-04
-1 40400200	7776-04	_2,92016014056_04	4.5036004620F_05	8.53364802205-05	3,4307527560F_04
- 10-400-9010	003E 06	-6 020100100JE404	5-10532045335-05	8-0663840450F-06	_4_5689498235F_0A
2.1038993		-087303073711E-03 6 61250535466-14	1.()23676426200	-0.7742510041F-07	4,7146027101F_07
-1e34419/0	570L 0/	1 /250625004E=V0	-1-5554/540525-07	-2.771210574E-07	-2.2569762860F.07
1.00100198		- 1010000000000000000000000000000000000	-1.67142421766-00	1.60643005535.00	3_05382661665_00
0,0041410	1245-08	-0622277092115=08	-100114503110E=08	10004000000000000	200222001045=03
			95		

SULUTION				
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J= 15

N= 9

K= 9

N=	9	К=	У	J= 18			
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	. 143093219	71-0	5	-1. 7076501526E=04	1-1323256900E=04	4.7900975931E-05	-4-1163249717E-04
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	8.858287304	11-0	8	2.2169942411E-08	-2.1158593879E-08	3.0224997709E-09	-5.1850959648E-10

## BIOGRAPHICAL NOTES

CHARLES A. LUNDQUIST joined the Smithsonian Astrophysical Observatory as Assistant Director for Science in 1962. In this position, he is responsible for organizing and coordinating current research projects, as well as seeking new directions for future research.

From 1956 to 1960 he was Chief of the Physics and Astrophysics Section, Research Projects Laboratory, Army Ballistic Missile Agency; and from 1960 to 1962 he held concurrent positions as Director of the Supporting Research Office and Chief of the Physics and Astrophysics Branch of the Research Projects Division at the Marshall Space Flight Center.

Dr. Lundquist received his undergraduate degree from South Dakota State College in 1949 and his doctorate in 1954 from the University of Kansas.

GIORGIO E. O. GIACAGLIA received his B.S. in 1958 from the Polytechnical School in São Paulo, Brazil, and his Ph.D. in astronomy from Yale in 1965. Since 1966, he has been chief professor at the University of São Paulo.

Dr. Giacaglia came to SAO in 1968 on a year's leave of absence from the University, where he worked in the Research and Analysis Division, specializing in research in celestial mechanics. MISS KAREN HEBB received a B.S. in astrophysics from Marlboro College in 1965.

Miss Hebb joined SAO in 1964 and completed her thesis work on stellar and comet photometry. She is currently an astronomer with the Celescope and satellite geophysics programs.

MRS. SUSAN GOODRICH MAIR received a B.A. in mathematics from Connecticut College in 1965.

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## NOTICE

This series of Special Reports was instituted under the supervision of Dr. F. L. Whipple, Director of the Astrophysical Observatory of the Smithsonian Institution, shortly after the launching of the first artificial earth satellite on October 4, 1957. Contributions come from the Staff of the Observatory.

First issued to ensure the immediate dissemination of data for satellite tracking, the reports have continued to provide a rapid distribution of catalogs of satellite observations, orbital information, and preliminary results of data analyses prior to formal publication in the appropriate journals. The Reports are also used extensively for the rapid publication of preliminary or special results in other fields of astrophysics.

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