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Approved by

D. T. Appleton Advanced Missions Studies Spacecraft Systems Analysis Project

(ACCESSION NUM CLITY FORM (CATEGORY) NUMBER) (NASA

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## PROJECT TECHNICAL REPORT TASK E-94

# STAGE SIZING DATA FOR AN UNMANNED PLANETARY SAMPLE RETURN MISSION

NAS 9-8166

5 FEBRUARY 1971

Prepared for NATIONAL AERONAUTICS AND SPACE ADMINISTRATION MANNED SPACECRAFT CENTER HOUSTON, TEXAS

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#### INTRODUCTION

Data were generated which can be used by mission planners for preliminary vehicle stage sizing for unmanned planetary sample return missions. These missions are characterized by an outbound leg (earth to planet) delivering an outbound payload and an inbound leg (planet to earth) delivering an inbound payload. The energy requirements can be asymmetric; that is, the outbound velocity requirement is not necessarily equal to the inbound velocity requirement.

Outbound stage weight ( $W_{SOUT}$ ) and inbound stage weight ( $W_{SIN}$ ) were calculated for a range of values of inbound and outbound payloads ( $P_{IN}$  and  $P_{OUT}$ ) and inbound and outbound velocity requirements ( $\Delta V_{IN}$  and  $\Delta V_{OUT}$ ). POUT was varied from 5,000 to 60,000 pounds,  $P_{IN}$  ranged from 1,000 to 10,000 pounds,  $\Delta V_{OUT}$  ranged from 11,000 to 24,000 feet per second, and  $\Delta V_{IN}$  ranged from 4,000 tc/30,000 feet per second.

A TRW Timeshare System program was written to generate the data. The data are presented in figures grouped at the end of this report.

#### DISCUSSION

A typical unmanned planetary sample return mission is depicted in the following illustration Mars

Earth

Inbound Stage Inbound Payload Inbound Payload Outbound Payload Outbound Stage

Earth

The basic elements of this mission are: the outbound stage, payload, and velocity requirement; and the inbound stage, payload, and velocity requirement. It should be noted that the outbound payload is not defined to include the inbound vehicle; the sum of these will be referred to as the total outbound payload. The outbound payload could include an orbiter, a lander, and a stage for the planet surface-to-orbit ascent phase.

It should also be noted that the velocity requirements are total requirements for each leg of the mission. For example, the outbound velocity requirement could include trans-Mars injection, midcourse maneuvers, and Mars orbit insertion plus any other maneuvers which would possibly be performed by the outbound propulsive vehicle.

#### METHOD AND EQUATIONS

The problem is to determine space vehicle stage sizes for outbound and inbound legs of space missions defined by payload and energy requirements.

The impulsive velocity increment imparted to a space vehicle is defined by the ideal rocket equation

(1)

$$\Delta V = g_0 I_{sp} \ln \left( \frac{W_0}{W_f} \right)$$

where:

g<sub>0</sub> = earth's acceleration of gravity at sea level (ft/sec<sup>2</sup>)
I<sub>sp</sub> = specific impulse (sec)
W<sub>0</sub> = initial vehicle weight (lb)

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 $W_f$  = final vehicle weight (lb)  $\Re_{M_f}$ 

 $\left(\frac{\Delta V}{g_0 I_{SD}}\right)$ 

For a given mission energy ( $\Delta V$ ) requirement the required mass ratio can then be written as

The initial vehicle weight is given by the expression

where: K = vehicle payload (1b)

 $W_S$  = stage weight (1b) = weight of propellant + inert stage weight The final vehicle weight is given by the expression.

$$I_{f} = K + (1 - \lambda) W_{S}$$
<sup>(4)</sup>

(3)

where:  $\lambda$  = propellant fraction =  $\frac{\text{weight of propellant}}{\text{stage weight}}$ 

hence the mass ratio can be written as

$$=\frac{K+W_{S}}{K+(1-\lambda)W_{S}}$$
(5)

and solving for the stage weight results in the expression

$$W_{\rm S} = \frac{K(R-1)}{1-R(1-\lambda)}$$
 (6)

By specifying K,  $\Delta V, g_0$ ,  $I_{sp}$ , and  $\lambda$ ; equation (6) can be used to solve for the required stage weight. The appropriate value of  $\lambda$  can be found from a scaling law which relates  $W_S$  and  $\lambda$ . This scaling law (see Table I) was input to the Timeshare program in tabular form, hence the problem became one of iterating for a value of  $W_S$  which satisfies both equation (6) and the scaling law.

The inbound mass ratio, where  $P_{IN} = K_{S_{i}}$  can be expressed as.

$$R_{IN} = e^{\left(\frac{\Delta V_{IN}}{I_{SP}IN^{g_{0}}}\right)} = \frac{P_{IN} + W_{SIN}}{P_{IN} + (1 - \lambda IN)W_{SIN}}$$

Similarly, the outbound mass ratio, where  $P_{IN} + W_{SIN} + P_{OUT} = K$ , can be expressed as

$$R_{OUT} = e^{\left(\frac{\Delta V_{OUT}}{I_{sp_{OUT}}g_{0}}\right)} = \frac{P_{IN} + W_{SIN} + P_{OUT} + W_{SOUT}}{P_{IN} + W_{SIN} + P_{OUT} + (1 - \lambda_{OUT})W_{SOUT}}$$
(8)

Note that the inbound and outbound  $I_{sp}$ 's need not be the same and that  $\lambda$  will vary depending on stage weight.

#### <u>Results</u>

A typical plot of the data is illustrated below.



These are plots of outbound stage weight (W<sub>SOUT</sub>) versus inbound stage weight (W<sub>SIN</sub>) for specified values of outbound payload (P<sub>OUT</sub>) and inbound payload (P<sub>IN</sub>) with the outbound velocity requirement ( $\Delta V_{OUT}$ ) and the inbound velocity requirement ( $\Delta V_{IN}$ ) as the parameters. The  $\Delta V_{IN}$  curves are vertical lines since W<sub>SIN</sub>, as calculated from equation (6), is a function of PiN,  $\lambda$ IN, and  $\Delta V_{IN}$  which are constant along any given line. The V<sub>OUT</sub> curves are not straight lines since W<sub>SOUT</sub>, as calculated from equation (6), is a function of the variables W<sub>SIN</sub> and  $\lambda_{OUT}$  as well as the constants POUT,  $\Delta V_{OUT}$ , and P<sub>IN</sub>. This is to say that W<sub>SIN</sub> and P<sub>IN</sub> are part of the total outbound non propulsive weight.(P<sub>OUT</sub> + P<sub>IN</sub> + W<sub>SIN</sub>). This brings up the point that all of the curves plotted at the end of this report, and of the format illustrated in Figure (a), are excerpts of one master plot as illustrated below.



Figure (b) Master Plot

The  $\Delta V_{OUT}$  curves emanate from the origin of the coordinate system. If  $\lambda_{OUT}$  were a constant, these curves would be straight lines with a slope of  $W_{S_{OUT}}/(P_{OUT} P_{IN} + W_{S_{IN}})$ 

If one now selects values for  $P_{OUT}$  and  $P_{IN}$ , a coordinate system can be defined for  $W_{SOUT}$  versus  $W_{SIN}$  whose origin will be displaced from the  $P_{OUT}$  +  $P_{IN}$  +  $W_{SIN}$ origin by the amount  $P_{OUT}$  +  $P_{IN}$  (see dashed line in Figure (c)).



Associated values of  $\Delta V_{IN}$  can be drawn, and the resulting  $W_{SOUT}$  versus  $W_{SIN}$  plot in Figure (c) is identical to the  $W_{SOUT}$  versus  $W_{SIN}$  plot of Figure (a) for the respective values of  $P_{OUT}$  and  $P_{IN}$ .

Data were generated for all combinations of the following values of input parameters.

Р <sub>ОИТ</sub> (1Ь)	P <sub>IN</sub> (1b)	∆V <sub>OUT</sub> (ft/sec)	$\Delta V_{IN}$ (ft/sec)
5,000	1,000	11,000	4,000
10,000	2,000	14,000	14,000
20,000	4,000	18,000	20,000
30,000	6,000	20,000	24,000
40,000 .	8,000	22,000	26,000
50,000	10,000	24,000	28,000
60,000	×		30,000

Figures 1 through 42 are plots of the data for the 42 combinations of the values of POUT and PIN shown above.

Although the curves were generated for a value of  $I_{sp}$  equal to 460, they can be used for sizing vehicles with other values of  $I_{sp}$ . For example, if it is desired to find a stage weight for a vehicle with an  $I_{sp}$  equal to 400 and a  $\wedge V$ equal to 20,000, the appropriate  $\Delta V$  to refer to on the plot would be:

 $\Delta V(plot) = 460 \left(\frac{\Delta V}{I_{sp}}\right) = 460 \left(\frac{20,000}{400}\right) = 23,000$ 

#### SUMMARY

Data were generated which can be used to determine outbound and inbound stage weight requirements for specified values of planetary sample return mission payload and energy ( $\Delta V$ ) requirements. The data were calculated by implementing an iterative technique on the TRW Timeshare System. This report contains plots of outbound stage weight versus inbound stage weight for 42 combinations of outbound and inbound payload requirements.

# Table I. Scaling Law

	Propellant Fraction ( $\lambda$ )			
Stage Size (W <sub>S</sub> )	$I_{sp} = 306$	$I_{sp} = 383$	I <sub>sp</sub> 460	
0	0	0	0	
10,000	.9000	.8800	.8000	
30,000	.9585	.9336	.8600	
40,000	.9671	.9430	.8710	
50,000	.9708	<b>.9528</b>	.8762	
60,000	.9728	.9580	.8807	
70,000	.9743	.9618	.8826	
80,000	.9753	.9645	.8847	
90,000	.9762	.9667	.8864	
100,000	.9768	.9685	.8887	
150,000	.9783	.9722	.8928	
200,000	.9793	.9743	.8951	
250,000	.9800	.9758	.8972	
300,000	<b>.</b> 9804	.9768	.8983	
350,000	.9808	.9775	.8989	
400,000	.9811	.9780	.8993	
500,000	.9815	.9787	.8997	
6,00,000	.9818	.9792	.9000	
700,000	9821	.9799	.9003	
1,000,000	<b>.</b> 9827 <sup>(</sup>	.9805 "	.9020	
100,000,000	.9830	<b>.9808</b> 6	.9040	



Figure 1.

OUTEOUND PAYLOAD = 5,000 POUNDS INBOUND PAYLOAD = 1,000 POUNDS



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OUTBOUND PAYLOAD = 5,000 POUNDS INBOUND PAYLOAD = 8,000 POUNDS





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Figure 11. Outbound Stage Weight versus Inbound Stage Weight  $(P_{OUT} = 10,000, P_{IN} = 8,000)$  ...

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OUTBOUND PAYLOAD = 20,000 POUNDS INBOUND PAYLOAD = 10,000 POUNDS

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Outbound Stage Weight versus Inbound Stage Weight ( $P_{OUT} = 20,000$ ,  $P_{IN} = 10,030$ )

Figure 18.





OUTBOUND PAYLOAD = 30,000 POUNDS INBOUND PAYLOAD = 2,000 POUNDS

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Outbound Stage Weight versus Inbound Stage Weight ( $P_{OUT}$  = 30,000,  $P_{IN}$  = 2,000) Figure 20.



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OUTBOUND PAYLOAD = 40,000 PUUNDS INBOUND PAYLOAD = 2,000 POUNDS

100 į ٦ſ 90 1.1 8 CLONE LIDCLIV CL 20 v. ~ INBOUND STAGE WEIGHT (1000 POUNDS) 60 50 \* Q2 40 ΰΰί 1000 30 20 υΰί 000 <u>0</u> Я ( an ЗE d 000 Ū 1,100 006 800 700 500 400 lec 000,1 009 300 **2**00, ,200 1 •• *,*,'' ۲ CONNOS STAGE MEIGHT (1000 POUNDS)

Outbound Stage Weight versus Inbound Stage Weight  $(P_{OUT} = 40,000, P_{IN} = 2,000)$ Figure 26.

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OUTBOUND PAYLOAD = 50,000 POUNDS INBOUND PAYLOAD = 2,000 POUNDS



OUTBOUND PAYLOAD = 50,000 POUNDS INBOUND PAYLOAD = 6,000 POUNDS



Figure 34. Outbound Stage Weight versus Inbound Stage Weight  $(P_{OUT} = 50,000, P_{IN} = 6,000)$ 

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OUTBOUND PAYLOAD = 60,000 POUNDS INBOUND PAYLOAD = 1,000 POUNDS

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Figure 39. Outbound Stage Weight versus Inbound Stage Weight ( $P_{OUT} = 60,000$ ,  $P_{IN} = 4,000$ )

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