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### INTERRELATED STRUCTURE OF HIGH ALTITUDE ATMOSPHERIC PROFILES

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### FOREWORD

For flight simulation of the Space Shuttle, involving aerodynamic heating, performance and trajectory dispersion studies, it is important the atmospheric model used reflect properly the type atmosphere the space vehicle will actually sense, with respect to changing altitude.

Therefore, this study does provide a mathematical model to compute realistic vertical profiles of pressure, temperature and density. Each parameter is given as a product of a steady state function and a perturbation factor. The model shows the interrelationship of the thermodynamic perturbations. Probabilities of profiles can be ascertained from the maximum and m inimum deviation from steady state. Also, density and temperature perturbations are completely specified if the structure of the pressure perturbation is known. This reported model is valid from 90 km down to  $\sim 45$  km altitude.

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### 1. INTRODUCTION

Simulated space shuttle trajectories through model atmospheres permit computation of important reentry parameters such as dynamic pressure and stagnation heating rate. Since these parameters are direct functions of the thermodynamic properties of the atmosphere, it is highly important that the model atmosphere reflect properly the type atmosphere the space shuttle will see. Density, pressure, and temperature as a function of altitude must be known since the shuttle's dynamic pressure and stagnation heating rate at any altitude are functions of the altitude history of the atmospheric variable as well as the immediate value. Therein lies the complexity of the problem. It also turns out, as this report will show, that the atmospheric variables are not only dependent upon each altitude, but also their altitude history. This report will discuss primarily this feature of the atmosphere.

The atmospheric model presented in this report is described in a different manner from previous models. Each thermodynamic variable, pressure, temperature, and density, is given as the product of a steady state function and a perturbation factor. The perturbation factor is described such that maximum and minimum deviation from the steady state can be determined and hence probability of profiles can be ascertained once an adequate sample has been determined.

The model also gives a true picture of the interrelationship of the perturbations of the thermodynamic variables.

### 2. METHODOLOGY

### 2.1 Data Storage

Processed thermodynamic and wind data from 67 high altitude ROBIN flights was keypunched onto cards and transferred to magnetic tape. The data was processed by the May 1970 high altitude ROBIN program. (See Luers, July 1970.) Data for the 67 soundings was acquired from four different sources which cover essentially the central portion of the Western Hemisphere.

Table I is a log of the individual flights.  $\Delta h$  is the altitude range for which the data is available.

In the appendix are tab print-outs of density, pressure, temperature, density ratio, and wind speed and direction at each altitude (km intervals) for the 67 soundings. The data has been included in this report for those readers interested in further development of the model. Missing data for several of the flights was due to loss of radar tracking or to the Mach-Reynolds number being out of the drag table. Flight 56 was eliminated from the data bank due to an insufficient number of data points.

### 2.2 Method of Approach

Logs of the pressure data listed in the appendix were fitted by a polynomial of degree k. Coefficients of the polynomial were determined by a least squares program for k = 2, 3, ..., 6. The coefficients of the resulting collection of data were then paired and linearly correlated for each k.

The rationale for correlating coefficients as discussed above is based on the fact that the resulting linear relations provide a convenient tool for computing probabilities of various profiles. It will be shown (Section 3) that one parameter is sufficient to describe the behavior of each profile.

TABLE I

### FLIGHT LOG

Flight No.	Date	Time Zulu	Latitude	Station	Maes (Kg)	Diameter (Meters)	Time Local	Δh	Source
	25 Nov 69	1755	37.84	Wallops	2260.	1.00	1255	100-44	-
2	25 Nov 69	2117	37.84	Wallops	.0944	1.00	1617	100-32	1
ñ	18 Jun 70	1800	37.84	Wallops	.0951	1.00	1300	100-38	-
4	01 Oct 69	1622	34, 10	Pt. Mugu	, 1168	1.00	0822	100-31	1
ŝ	12 Nov 69	1959	34.10	Pt. Mugu	. 1094	1.00	1159	60-37	-
9	15 Apr 70	2006	34.10	Pt. Mugu	1137	1.00	1206	100-44	-
7	09 Sep 70	1559	34.10	Pt. Mugu	1145	1.00	0759	100-40	-
80	23 Sep 70	1845	34.10	Pt. Mugu	.1161	1.00	1045	87-37	-
6	21 Oct 70	1542	34.10	Pt. Mugu	.1159	1.00	0742	100-42	-
10	02 Feb 69	2	32.49	White Sands	.0478	0.66	¢.	100-48	-1
11	09 Feb 69	2034	32.49	White Sands	.0940	1.00	1334	100-46	1
12	09 Feb 69	1803	32.49	White Sanda	. 1001	1.00	1103	100-38	-
13	18 Feb 68	1810	29.60	Eglin	.1196	1.00	1310	100-37	-
14	18 Feb 68	1900	29.60	Eglin	.1151	1.00	1400	100-38	-
15	18 Feb 68	2010	29.60	Eglin	.1175	1.00	1510	95-35	1
16	19 Oct 68	1249	28.25	Patrick	.1177	1.00	0749	100-52	I
17	19 Nov 68	1833	28.25	Patrick	.1103	1.00	1333	100-41	1
18	20 Nov 68	2140	28. 25	Patrick	.1109	1.00	1640	100-32	1
19	20 Nov 68	2100	28.25	Patrick	.1128	1.00	1600	100-49	1
20	14 Jul 69	1300	28. 25	Patrick	.1180	1.00	080	100-43	1
21	09 Sep 70	1500	28. 25	Patrick	.1157	1.00	1000	75-36	1
22	04 Nov 70	1600	28. 25	Patrick	.1156	1.00	1100	100-43	-
23	13 Nov 70	1600	28.25	Patrick	.1152	1.00	1100	92-53	-
24	18 Nov 70	1600	28.25	Patrick	.1142	1.00	1100	100-49	1
25	09 Dec 70	1700	28.25	Patrick	.1128	1.00	1200	100-42	1
26	13 Nov 69	2100	22.00	Kauai	.1128	1.00	1100	98-54	-
27	02 Sep 70	1000	-7.97	Ascension	.1150	1.00	0060	100-49	1
28	21 Sep 70	2219	32.35	Wallops	.0972	1.00	1819	100-44	2
29	30 Nov 70	1847	37.84	Wallops	.0989	1.00	1347	100-33	7
30	19 Jan 71	1943	37.84	Wallops	.1136	1.00	1443	96-38	7
31	21 Jan 71	1818	37.84	Wallops	.1146	1.00	1318	100-32	2
32	21 Jan 71	1902	37.84	Wallops	.1116	1.00	1402	100-38	2

TABLE I (Continued)

FLIGHT LOG

31         21 Jan Ti         193         37.84         Wallopa          1132         1.00         1439         100-13           34         21 Jan Ti         200         37.84         Wallopa           100         1499         100-13           35         25 Jul Ti         1033         2.8.25         Cape Kennedy         .1116         1.00         1033         100-13           36         28 Jul Ti         1003         -7.97         Azcension         .1118         1.00         1033         100-43           36         0.011         1003         -7.97         Azcension         .1118         1.00         1033         100-43           40         20 Nov Ti         1103         -7.97         Azcension         .1118         1.00         1033         100-43           41         23 Dec 70         1709         34.10         PL Mugu         .1115         1.00         0736         70-35           41         23 Dec 70         1103         34.10         PL Mugu         .1116         1.00         1033         100-43           42         13 Nov 63         2134         22.00         Barking Suda         .1112         1.00	Flight No.	Date	Time Zulu	Latitude	Station	Mass (Kg.)	Diameter (Meters)	Time Local	ЧÞ	Source
31 $21$ Jan Ti $200$ $71.46$ Validya $100$ $140$ $149$ $100$ $149$ $100$	33	21 Jan 71	1938	37.84	Wallops	.1132	1.00	1438	100-31	2
32         23 Jul TI         153         28.25         Cape Kennedy         1143         1.00         1033         100-45           7	72	71 Tan 71	2049	37.84	Wallops	.0931	1.00	1549	84 - 36	7
8.         22.889         7.1         15.3         28.2.5         Cape Kennedy         1.11         1.00         1031         100-4           9.         06         01.11         1003         -7.97         Ascension         1.117         1.00         0903         100-45           9.         06         06         11         1003         -7.97         Ascension         1.118         1.00         0903         100-45           9.         06         06         11         103         -7.97         Ascension         1.118         1.00         0903         100-45           41         10         PL. Mugu         1.113         1.00         0736         05-51           42         04         Mar 71         1833         34.10         PL. Mugu         1.113         1.00         0736         05-51           43         04         Mar 71         1833         34.10         PL. Mugu         1.113         1.00         0736         05-51           44         04         Mar 71         1833         22.00         Barking Sanda         1.113         1.00         100-35           45         13         0011         22.00         Barking Sanda <td< th=""><th>5 5</th><th>28 Jul 71</th><th>1538</th><th>28. 25</th><th>Cape Kennedy</th><th>.1146</th><th>1.00</th><th>1038</th><th>100-44</th><th>ŝ</th></td<>	5 5	28 Jul 71	1538	28. 25	Cape Kennedy	.1146	1.00	1038	100-44	ŝ
77 $71$ <t< th=""><th>2</th><th>22 Sep 71</th><th>1533</th><th>28. 25</th><th>Cape Kennedy</th><th>.1149</th><th>1.00</th><th>1033</th><th>100-45</th><th>£</th></t<>	2	22 Sep 71	1533	28. 25	Cape Kennedy	.1149	1.00	1033	100-45	£
38         2.8 Jul 71         1003         -7.97         Accension         1123         1.00         0903         1003         100-44           40         2.0 Nov 70         1733         -7.97         Accension         .1113         1.00         0903         1003         100-43           41         2.3 Dec 70         1703         34.10         PL. Mugu         .1113         1.00         0903         100-43           42         08 Jan 71         1564         34.10         PL. Mugu         .1113         1.00         0903         100-45           43         13 Nove 9         2134         22.00         Barking Sanda         .1113         1.00         1033         100-45           44         13 Nove 9         2134         22.00         Barking Sanda         .1113         1.00         1134         90-55           45         13 Nove 9         2134         22.00         Barking Sanda         .1113         1.00         1103         90-55           47         23 Sap 70         2203         22.00         Barking Sanda         .1112         1.00         1103         100-45           48         15 Sap 70         2103         22.00         Barking Sanda         .1112	37	09 Jun 71	1003	- 7. 97	Ascension	.1137	1.00	0603	100-49	£
$70$ $66 \operatorname{Cr} 11$ $1103$ $-7, 97$ Accention $1184$ $1.00$ $1003$ $100-42$ $41$ $23 \operatorname{Dec} 70$ $1396$ $34.10$ $Pt. Mugu$ $11154$ $1.00$ $0909$ $100-31$ $42$ $23 \operatorname{Jan} 71$ $1614$ $34.10$ $Pt. Mugu$ $11151$ $1.00$ $0909$ $100-31$ $42$ $0.4 \operatorname{Mar} 71$ $15164$ $34.10$ $Pt. Mugu$ $11131$ $100$ $0736$ $67-51$ $45$ $13800 \operatorname{co} 60$ $23134$ $22.00$ $\mathrm{Barking Sanda}$ $11124$ $100$ $1033$ $100-45$ $46$ $13800 \operatorname{co} 7213$ $22.00$ $\mathrm{Barking Sanda}$ $11124$ $100$ $1123$ $100-45$ $47$ $23500$ $\mathrm{Barking Sanda}$ $11123$ $100$ $1203$ $100-45$ $47$ $23500$ $\mathrm{Barking Sanda}$ $11123$ $100$ $1123$ $100-45$ $61$ $00311$ $00311$ $22.000$ $\mathrm{Barking Sanda}$ <th< th=""><th>38</th><th>28 Jul 71</th><th>1003</th><th>-7.97</th><th>Ascension</th><th>.1143</th><th>1.00</th><th>0603</th><th>100-44</th><th>e</th></th<>	38	28 Jul 71	1003	-7.97	Ascension	.1143	1.00	0603	100-44	e
40         20         Nov 70         1536         34,10         Pt. Mugu         1154         1,00         0736         776         777           41         23         De Mar 71         1614         34,10         Pt. Mugu         11159         1,00         009         100-31           42         23         Jat.10         Pt. Mugu         11151         1,00         0756         67-31           43         13         Jat.10         Pt. Mugu         11151         1,00         0756         67-31           44         OMM 711         1333         Jat.10         Pt. Mugu         11151         1,00         0756         67-31           45         113Nov 69         2134         22.00         Barking Sanda         11123         1,00         100-31         00-36           47         2356 70         2203         Barking Sanda         1113         1,00         1103         100-45           47         2356 70         2203         Barking Sanda         11156         1,00         1103         100-56           47         2106 70         2213         22.00         Barking Sanda         11153         100         1103         100-56           49	: s	06 Oct 71	1103	-7.97	Ascension	.1188	1.00	1003	100-42	e
41         23 Dec 70         1709         34.10         PL Mugu         1159         1.00         0909         100-31           42         08 Jan 71         1614         34.10         PL Mugu         11159         1.00         0909         100-31           43         0.8 Mar 71         1856         34.10         PL Mugu         11151         1.00         0133         96-54           44         13 Nov 69         2114         22.00         Barking Sanda         1124         1.00         1013         96-55           45         15 Nov 69         2134         22.00         Barking Sanda         1113         1.00         1104         90-55           46         07 Oct 70         2221         22.00         Barking Sanda         1113         1.00         1103         100-36           47         23 Sep 70         2203         22.00         Barking Sanda         11163         1.00         1123         100-36           48         07 Oct 70         2221         22.00         Barking Sanda         11163         1.00         1123         100-36           51         0807 71         1431         0031         22.00         Barking Sanda         1163         1.00	4	20 Nov 70	1536	34.10	Pt. Mugu	.1154	1.00	0736	70 - 37	۳
47         10         PL, Mugu         1115         1.00         0814         100-45           43         29 Jan 71         1556         34.10         PL, Mugu         11151         1.00         0736         67-51           44         13 Nov 69         21134         22.00         Barking Sanda         11128         1.00         10134         98-54           45         13 Nov 69         2104         22.00         Barking Sanda         11128         1.00         10134         90-55           46         10 Sap 70         22010         Barking Sanda         11128         1.00         1104         90-52           49         27 Oct 70         22210         Barking Sanda         11155         1.00         1103         100-36           40         21 Oct 70         2221         22.00         Barking Sanda         1115         1.00         1123         100-36           51         16 Nov 71         1233         28.25         Cape Kennedy         1664         1.00         1133         90-32           51         15 Dac 71         1633         28.25         Cape Kennedy         1660         1.00         1333         97-36           51         15 Dac 71	4	23 Dec 70	1709	34.10	Pt. Mugu	.1159	1.00	6060	100-31	£
3         27         34.10         Pt. Mugu         .1145         1.00         0756         67-51           44         04 Mar 71         1353         34.10         Pt. Mugu         .1131         1.00         1033         100-44           45         13 Nov 69         2134         22.00         Barking Sands         .1132         1.00         1033         100-44           46         13 Nov 69         2134         22.00         Barking Sands         .1132         1.00         1031         100-56           47         23 Sep 70         2209         22.00         Barking Sands         .1133         1.00         1221         100-56           49         21 Oct 70         2221         22.00         Barking Sands         .1153         1.00         1231         100-56           40         21 Oct 70         2221         22.00         Barking Sands         .1153         1.00         1231         100-56           41         0.01         1031         22.00         Barking Sands         .1163         1.00         1231         100-50           42         13         0.01         1031         12.0         1031         102-51         100-50           51	: ;	08 Jan 71	1614	34.10	Pt. Mugu	.1159	1.00	0814	100-45	e
4.         04 Mar 71         1833         34,10         Pt. Mugu         1151         1.00         1033         100-44           4.5         13 Nov 69         2134         22,00         Barking Sande         .1128         1.00         1134         95-54           4.6         16 Sep 70         2104         22,00         Barking Sande         .1113         1.00         1123         100-51           4.7         23 Sep 70         2203         22.00         Barking Sande         .1113         1.00         1221         100-56           4.8         07 Oct 70         2103         22.00         Barking Sande         .1113         1.00         1221         100-30           5.1         16 No7 71         1433         23.2.00         Barking Sande         .1163         1.00         1129         100-30           5.1         16 No7 71         1433         28.25         Cape Kennedy         .1649         1.00         1137         96-33           5.1         18 No7 71         1833         28.25         Cape Kennedy         .1649         1.00         1137         90-32           5.3         18 No7 71         1833         28.25         Cape Kennedy         .1650         1.00	2 E T	29 Jan 71	1556	34.10	Pt. Mugu	.1145	1.00	0756	67-51	ŝ
5         13 Nov 66         2134         22.00         Barking Sanda         1128         1.00         1134         98-54           47         23 Sep 70         2104         22.00         Barking Sanda         .1112         1.00         1104         90-52           47         23 Sep 70         22104         22.00         Barking Sanda         .1113         1.00         1201         100-56           48         07 Oct 70         2211         22.00         Barking Sanda         .1113         1.00         1221         100-30           50         23 Jan 71         0031         22.00         Barking Sanda         .1165         1.00         1123         100-30           51         0 7 Oct 70         2103         22.00         Barking Sanda         .1163         1.00         100-30           51         16 Nor 71         1433         22.00         Barking Sanda         .1163         100-30         100-30           51         16 Nor 71         1433         28.25         Cape Kennedy         .1649         1.00         1137         90-30           52         15 Dec 71         1833         28.25         Cape Kennedy         .1660         1.00         1133         91-31     <		04 Mar 71	1833	34.10	Pt. Mugu	.1151	1.00	1033	100-44	e
46         16         58 p 70         2104         22.00         Barking Sanda         1142         1.00         1104         90-52           47         23 Sep 70         2209         22.00         Barking Sanda         1113         1.00         1209         100-56           48         07 Oct 70         2221         22.00         Barking Sanda         1115         1.00         1221         100-55           49         21 Oct 70         2103         22.00         Barking Sanda         1115         1.00         1123         100-55           50         23 Jan 71         0031         22.00         Barking Sanda         1115         1.00         1133         100-56           51         0.5 Tot         1433         22.00         Barking Sanda         1163         1.00         1133         100-30           52         16 Nov 71         1433         28.25         Cape Kennedy         1649         1.00         1137         92-30           53         15 Dec 71         1333         28.25         Cape Kennedy         1660         1.00         1133         97-30           54         15 Dec 71         1333         28.25         Cape Kennedy         1649         1.00	: ¥	13 Nov 69	2134	22.00	Barking Sands	.1128	1.00	1134	98-54	£
47       23 Sep 70       2209       22.00       Barking Sanda       .1079       1.00       1209       100-54         48       07 Oct 70       22211       22.00       Barking Sanda       .1113       1.00       1221       100-55         49       21 Oct 70       2103       22.00       Barking Sanda       .1153       1.00       1123       100-30         50       23 Jan 71       0031       22.00       Barking Sanda       .1153       1.00       1133       100-30         51       03 Feb 71       2129       22.00       Barking Sanda       .1163       1.00       1133       100-30         52       16 Nov 71       1433       28.25       Cape Kennedy       .1660       1.00       1137       92-33         53       15 Dec 71       1833       28.25       Cape Kennedy       .1660       1.00       1137       92-33         54       15 Dec 71       1833       28.25       Cape Kennedy       .1650       1.00       1137       92-33         56       15 Dec 71       1833       28.25       Cape Kennedy       .1650       1.00       1137       92-33         57       11 Jan 72       1833       28.25       Cap	46	16 Sep 70	2104	22.00	Barking Sands	.1142	1.00	1104	90-52	3
48         07 Oct 70         221         22.00         Barking Sanda         1113         1.00         1221         100-55           49         21 Oct 70         2103         22.00         Barking Sanda         1156         1.00         1103         100-35           50         23 Jan 71         0031         22.00         Barking Sanda         1163         1.00         1129         100-30           51         03 Feb 71         2129         22.00         Barking Sanda         1163         1.00         1137         100-30           52         16 Nov 71         1658         22.00         Barking Sanda         1164         1.00         1137         90-33           53         18 Nov 71         1658         28.25         Cape Kennedy         1660         1.00         1137         92-36           54         15 Dec 71         1833         28.25         Cape Kennedy         1660         1.00         1137         92-36           55         15 Dec 71         1833         28.25         Cape Kennedy         1660         1.00         1133         97-39           56         15 Dec 71         1833         28.25         Cape Kennedy         1602         10         1133	47	23 Sep 70	2209	22.00	Barking Sande	.1079	1.00	1209	100-54	۳
49       21 Get 70       2103       22.00       Barking Sanda       .1156       1.00       1103       100-30         51       03 Feb 71       2129       22.00       Barking Sanda       .1163       1.00       1129       100-30         52       16 Nov 71       1433       28.25       Cape Kennedy       .1649       1.00       1129       100-30         52       16 Nov 71       1433       28.25       Cape Kennedy       .1649       1.00       0333       95-40         53       18 Nov 71       1637       28.25       Cape Kennedy       .1649       1.00       1137       92-40         54       15 Dec 71       1733       28.25       Cape Kennedy       .1649       1.00       1137       92-33         56       15 Dec 71       1833       28.25       Cape Kennedy       .1630       1.00       1137       92-33         57       11 Jan 72       1433       28.25       Cape Kennedy       .1650       1.00       1333       91-45         58       12 Jan 72       1633       28.25       Cape Kennedy       .1650       1.00       1333       91-45         60       15 Feb 72       1433       28.25       Cape Kenn	48	07 Oct 70	2221	22.00	Barking Sands	.1113	1.00	1221	100-56	e
50       23 Jan 71       0031       22.00       Barking Sanda       1163       1.00       1431       100-30         51       03 Feb 71       2129       22.00       Barking Sanda       1185       1.00       1129       100-30         52       16 Nov 71       1433       28.25       Cape Kennedy       1649       1.00       1137       95-40         53       18 Nov 71       1433       28.25       Cape Kennedy       1640       1.00       1137       92-38         54       15 Dec 71       1637       28.25       Cape Kennedy       1660       1.00       1137       92-38         55       15 Dec 71       1333       28.25       Cape Kennedy       1650       1.00       1137       92-38         56       15 Dec 71       1333       28.25       Cape Kennedy       1650       1.00       1333       97-58         57       11 Jan 72       1633       28.25       Cape Kennedy       1650       1.00       0333       97-58         58       12 Jan 72       1633       28.25       Cape Kennedy       1650       1.00       0333       97-58         60       15 Feb 72       1833       28.25       Cape Kennedy	64	21 Oct 70	2103	22.00	Barking Sands	.1156	1.00	1103	100-35	ŝ
51       03 Feb 71       2129       22.00       Barking Sanda       .1185       1.00       1129       100-30         52       16 Nov 71       1433       28.25       Cape Kennedy       .1649       1.00       0133       95-40         53       18 Nov 71       1658       28.25       Cape Kennedy       .1649       1.00       0137       92-38         54       15 Dec 71       1637       28.25       Cape Kennedy       .1660       1.00       1137       92-38         55       15 Dec 71       1733       28.25       Cape Kennedy       .1650       1.00       1333       97-58         56       15 Dec 71       1833       28.25       Cape Kennedy       .1650       1.00       1333       97-58         57       11 Jan 72       1433       28.25       Cape Kennedy       .1650       1.00       1333       97-58         58       12 Jan 72       1633       28.25       Cape Kennedy       .1650       1.00       0333       92-33         59       15 Feb 72       1833       28.25       Cape Kennedy       .1650       1.00       0333       97-36         60       15 Feb 72       1833       28.25       Cape Kennedy	20	23 Jan 71	0031	22.00	Barking Sands	.1163	1.00	1431	100-30	e.
52       16 Nov 71       1433       28. 25       Cape Kennedy       .1649       1.00       0933       95-40         53       18 Nov 71       1658       28. 25       Cape Kennedy       .1643       1.00       1137       92-38         54       15 Dec 71       1637       28. 25       Cape Kennedy       .1660       1.00       1137       92-38         55       15 Dec 71       1637       28. 25       Cape Kennedy       .1636       1.00       1333       97-58         56       15 Dec 71       1833       28. 25       Cape Kennedy       .1650       1.00       1333       97-58         57       11 Jan 72       1433       28. 25       Cape Kennedy       .1650       1.00       1333       97-58         58       12 Jan 72       1633       28. 25       Cape Kennedy       .1650       1.00       1333       92-33         59       15 Feb 72       1433       28. 25       Cape Kennedy       .1650       1.00       1333       92-33         60       15 Feb 72       1833       28. 25       Cape Kennedy       .1650       1.00       1333       92-33         61       15 Feb 72       1833       28. 25       Cape	5	03 Feb 71	2129	22.00	Barking Sands	.1185	1.00	1129	100-30	£
53       18 Nov 71       1658       28.25       Cape Kennedy       .1643       1.00       1158       90-32         54       15 Dec 71       1637       28.25       Cape Kennedy       .1660       1.00       1137       92-38         55       15 Dec 71       1637       28.25       Cape Kennedy       .1682       1.00       1137       97-58         56       15 Dec 71       1833       28.25       Cape Kennedy       .1670       1.00       1233       100-45         57       11 Jan 72       1433       28.25       Cape Kennedy       .1670       1.00       1333       97-58         58       12 Jan 72       1433       28.25       Cape Kennedy       .1670       1.00       1133       92-33         59       15 Feb 72       1433       28.25       Cape Kennedy       .1616       1.00       0333       92-33         60       15 Feb 72       1833       28.25       Cape Kennedy       .1616       1.00       1333       92-33         61       15 Feb 72       1833       28.25       Cape Kennedy       .1620       1.333       92-33         61       15 Feb 72       1833       28.25       Cape Kennedy       .162	52	16 Nov 71	1433	28. 25	Cape Kennedy	.1649	1.00	0933	95-40	4
54       15 Dec 71       1637       28. 25       Cape Kennedy       .1660       1.00       1137       92-38         55       15 Dec 71       1733       28. 25       Cape Kennedy       .1148       1.00       1233       100-45         56       15 Dec 71       1833       28. 25       Cape Kennedy       .1670       1.00       1333       97-58         57       11 Jan 72       1433       28. 25       Cape Kennedy       .1670       1.00       1333       97-39         58       12 Jan 72       1433       28. 25       Cape Kennedy       .1650       1.00       0333       95-31         59       15 Feb 72       1433       28. 25       Cape Kennedy       .1650       1.00       1333       92-33         60       15 Feb 72       1433       28. 25       Cape Kennedy       .1629       1.00       1333       92-31         61       15 Feb 72       1833       28. 25       Cape Kennedy       .1629       1.00       1333       92-33         61       15 Feb 72       1833       28. 25       Cape Kennedy       .1629       1.00       1333       92-33         61       15 Feb 72       1833       28. 25       Cap	5	18 Nov 71	1658	28.25	Cape Kennedy	.1643	1.00	1158	90 - 32	4
55       15 Dec 71       1733       28.25       Cape Kennedy       .1148       1.00       1233       100-45         56       15 Dec 71       1833       28.25       Cape Kennedy       .1682       1.00       1333       97-58         57       11 Jan 72       1433       28.25       Cape Kennedy       .1682       1.00       1333       97-58         58       12 Jan 72       1633       28.25       Cape Kennedy       .1650       1.00       0933       79-30         58       12 Jan 72       1633       28.25       Cape Kennedy       .1616       1.00       0933       95-31         59       15 Feb 72       1433       28.25       Cape Kennedy       .1629       1.00       0933       94-45         60       15 Feb 72       1833       28.25       Cape Kennedy       .1629       1.00       1333       92-39         61       15 Feb 72       1833       28.25       Cape Kennedy       .1629       1.00       1333       92-39         61       15 Feb 72       1833       28.25       Cape Kennedy       .1629       1.00       1333       93-42         62       16 Feb 72       1833       28.25       Cape Kennedy<		15 Dec 71	1637	28.25	Cape Kennedy	.1660	1.00	1137	92-38	4
56       15 Dec 71       1833       28. 25       Cape Kennedy       .1670       1.00       1333       97-58         57       11 Jan 72       1433       28. 25       Cape Kennedy       .1670       1.00       0933       79-30         58       12 Jan 72       1633       28. 25       Cape Kennedy       .1670       1.00       0933       79-30         59       15 Feb 72       1433       28. 25       Cape Kennedy       .1616       1.00       0933       92-33         60       15 Feb 72       1703       28. 25       Cape Kennedy       .1629       1.00       1333       92-39         61       15 Feb 72       1833       28. 25       Cape Kennedy       .1629       1.00       1333       92-39         61       15 Feb 72       1833       28. 25       Cape Kennedy       .1629       1.00       1333       92-39         62       16 Feb 72       1833       28. 25       Cape Kennedy       .1629       1.00       1333       93-42         63       17 Feb 72       1833       28. 25       Cape Kennedy       .1616       1.00       1333       94-44         64       18 Feb 72       1633       28. 25       Cape	5 3	15 Dec 71	1733	28. 25	Cape Kennedy	.1148	1.00	1233	100-45	4
57       11 Jan 72       1433       28.25       Cape Kennedy       .1670       1.00       0933       79-30         58       12 Jan 72       1633       28.25       Cape Kennedy       .1650       1.00       0933       92-33         59       15 Feb 72       1433       28.25       Cape Kennedy       .1616       1.00       0933       92-33         60       15 Feb 72       1703       28.25       Cape Kennedy       .1616       1.00       0933       92-33         61       15 Feb 72       1833       28.25       Cape Kennedy       .1629       1.00       1333       92-39         61       15 Feb 72       1833       28.25       Cape Kennedy       .1629       1.00       1333       92-39         61       15 Feb 72       1833       28.25       Cape Kennedy       .1629       1.00       1333       92-42         62       16 Feb 72       1833       28.25       Cape Kennedy       .1629       1.00       1333       92-42         63       17 Feb 72       1639       28.25       Cape Kennedy       .1616       1.00       1333       94-44         64       18 Feb 72       1633       28.25       Cape Kennedy </th <th>2 </th> <th>15 Dec 71</th> <th>1833</th> <th>28.25</th> <th>Cape Kennedy</th> <th>.1682</th> <th>1.00</th> <th>1333</th> <th>97-58</th> <th>4</th>	2 	15 Dec 71	1833	28.25	Cape Kennedy	.1682	1.00	1333	97-58	4
58       12 Jan 72       1633       28.25       Cape Kennedy       .1650       1.00       1133       92-33         59       15 Feb 72       1433       28.25       Cape Kennedy       .1616       1.00       0933       95-31         60       15 Feb 72       1703       28.25       Cape Kennedy       .1616       1.00       0933       95-31         61       15 Feb 72       1833       28.25       Cape Kennedy       .1629       1.00       1333       92-39         61       15 Feb 72       1833       28.25       Cape Kennedy       .1629       1.00       1333       92-39         62       16 Feb 72       1833       28.25       Cape Kennedy       .1629       1.00       1333       92-45         63       17 Feb 72       1639       28.25       Cape Kennedy       .1616       1.00       1139       89-40         64       18 Feb 72       1433       28.25       Cape Kennedy       .1615       1.00       1139       89-40         65       18 Feb 72       1433       28.25       Cape Kennedy       .1615       1.00       1139       94-41         64       18 Feb 72       1603       28.25       Cape Kennedy </th <th>. 5</th> <th>11 Jan 72</th> <th>1433</th> <th>28. 25</th> <th>Cape Kennedy</th> <th>.1670</th> <th>1.00</th> <th>6660</th> <th>79-30</th> <th>4</th>	. 5	11 Jan 72	1433	28. 25	Cape Kennedy	.1670	1.00	6660	79-30	4
59       15 Feb 72       1433       28.25       Cape Kennedy       .1616       1.00       0933       95-31         60       15 Feb 72       1703       28.25       Cape Kennedy       .1629       1.00       1203       94-45         61       15 Feb 72       1833       28.25       Cape Kennedy       .1629       1.00       1333       92-39         61       15 Feb 72       1833       28.25       Cape Kennedy       .1629       1.00       1333       92-39         62       16 Feb 72       1833       28.25       Cape Kennedy       .1629       1.00       1333       93-42         63       17 Feb 72       1639       28.25       Cape Kennedy       .1616       1.00       1139       89-40         64       18 Feb 72       1433       28.25       Cape Kennedy       .1615       1.00       1139       89-40         65       18 Feb 72       1603       28.25       Cape Kennedy       .1624       1.00       1133       94-41         66       23 Feb 72       1603       28.25       Cape Kennedy       .1624       1.00       1103       94-41         65       23 Feb 72       1503       28.25       Cape Kennedy </th <th>58</th> <th>12 Jan 72</th> <th>1633</th> <th>28.25</th> <th>Cape Kennedy</th> <th>.1650</th> <th>1.00</th> <th>1133</th> <th>92-33</th> <th>4</th>	58	12 Jan 72	1633	28.25	Cape Kennedy	.1650	1.00	1133	92-33	4
60       15 Feb 72       1703       28.25       Cape Kennedy       .1629       1.00       1203       94-45         61       15 Feb 72       1833       28.25       Cape Kennedy       .1629       1.00       1333       92-39         62       16 Feb 72       1833       28.25       Cape Kennedy       .1629       1.00       1333       92-39         62       16 Feb 72       1833       28.25       Cape Kennedy       .1629       1.00       1333       93-42         63       17 Feb 72       1639       28.25       Cape Kennedy       .1616       1.00       1139       89-40         64       18 Feb 72       1433       28.25       Cape Kennedy       .1615       1.00       0333       94-44         65       18 Feb 72       1603       28.25       Cape Kennedy       .1624       1.00       0103       94-34         66       23 Feb 72       1503       28.25       Cape Kennedy       .1624       1.00       1103       94-34         65       23 Feb 72       1503       28.25       Cape Kennedy       .1620       1.00       1033       94-34         66       23 Feb 72       1503       28.25       Cape Kennedy </th <th></th> <th>15 Feb 72</th> <th>1433</th> <th>28.25</th> <th>Cape Kennedy</th> <th>.1616</th> <th>1.00</th> <th>0933</th> <th>95-31</th> <th>4</th>		15 Feb 72	1433	28.25	Cape Kennedy	.1616	1.00	0933	95-31	4
61       15       Feb 72       1833       28.25       Cape Kennedy       .1629       1.00       1333       92-39         62       16       Feb 72       1833       28.25       Cape Kennedy       .1629       1.00       1333       93-42         63       17       Feb 72       1833       28.25       Cape Kennedy       .1616       1.00       1139       89-40         64       18       Feb 72       1433       28.25       Cape Kennedy       .1615       1.00       033       94-44         64       18       Feb 72       1603       28.25       Cape Kennedy       .1615       1.00       033       94-44         65       18       Feb 72       1603       28.25       Cape Kennedy       .1626       1.00       1033       94-34         66       23       Feb 72       1503       28.25       Cape Kennedy       .1620       1003       93-32         66       23       Feb 72       1503       28.25       Cape Kennedy       .1620       1003       93-32         66       23       Feb 72       1503       28.25       Cape Kennedy       .1620       1003       93-32         67       10	, , , ,	15 Feb 72	1703	28.25	Cape Kennedy	.1629	1.00	1203	94-45	4
62       16 Feb 72       1833       28.25       Cape Kennedy       .1629       1.00       1333       93-42         63       17 Feb 72       1639       28.25       Cape Kennedy       .1616       1.00       1139       89-40         63       17 Feb 72       1639       28.25       Cape Kennedy       .1615       1.00       1139       89-40         64       18 Feb 72       1433       28.25       Cape Kennedy       .1615       1.00       0933       94-44         64       18 Feb 72       1603       28.25       Cape Kennedy       .1624       1.00       1103       94-41         65       23 Feb 72       1503       28.25       Cape Kennedy       .1620       1.00       1003       93-32         66       23 Feb 72       1503       28.25       Cape Kennedy       .1620       1.00       1033       93-32         66       23 Feb 72       1503       28.25       Cape Kennedy       .1620       1.00       1033       93-32	3 5	15 Eah 72	1833	28.25	Cape Kennedy	.1629	1.00	1333	92-39	4
62       10 feb 12       139       89-40         63       17 Feb 72       1639       28.25       Cape Kennedy       .1616       1.00       1139       89-40         63       17 Feb 72       1639       28.25       Cape Kennedy       .1615       1.00       0933       94-44         64       18 Feb 72       1433       28.25       Cape Kennedy       .1615       1.00       1103       94-41         65       18 Feb 72       1603       28.25       Cape Kennedy       .1624       1.00       1003       93-32         66       23 Feb 72       1503       28.25       Cape Kennedy       .1620       1.00       1033       93-32         66       23 Feb 72       1503       28.25       Cape Kennedy       .1620       1.00       1033       93-32         66       23 Feb 72       1503       28.25       Cape Kennedy       .1628       1.00       1133       86-37	5	10 100 H	1833	28. 25	Cape Kennedy	.1629	1.00	1333	93-42	4
63       1/ FeO (2       100       0933       94-44         64       18 Feb 72       1433       28.25       Cape Kennedy       1615       1.00       0933       94-44         64       18 Feb 72       1603       28.25       Cape Kennedy       1624       1.00       1103       94-41         65       18 Feb 72       1603       28.25       Cape Kennedy       1620       1.00       1003       93-32         66       23 Feb 72       1503       28.25       Cape Kennedy       1620       1.00       1033       93-32         66       23 Feb 72       1503       28.25       Cape Kennedy       1628       1.00       1133       88-37	62	10 feb 10	0291	28.25	Cape Kennedy	.1616	1.00	1139	89-40	4
64     18 Feb /2     1433     94-41       65     18 Feb 72     1603     28.25     Cape Kennedy     1624     1.00     1003     93-32       66     23 Feb 72     1503     28.25     Cape Kennedy     .1620     1.00     1003     93-32       66     23 Feb 72     1503     28.25     Cape Kennedy     .1620     1.00     1033     93-32       66     23 Feb 72     1503     28.25     Cape Kennedy     .1628     1.00     1133     88-37	63	11 Fe0 12	(C)1	28.25	Cape Kennedy	. 1615	1.00	0933	94-44	4
bb         18 feb 12         100         1003         93-32           66         23 Feb 72         1503         28, 25         Cape Kennedy         1620         1,00         1003         93-32           66         23 Feb 72         1503         28, 25         Cape Kennedy         1620         1,00         1133         88-37		18 Feb 12	2071	28.25	Cape Kennedy	.1624	1.00	1103	94-41	4
60 23 FeB (2 1303 - 1303 - 1313 - 88-37 - 1628 - 1.00 - 1133 - 88-37	<b>8</b> :	18 Feb 12	1603	28.25	Cape Kennedy	.1620	1.00	1003	93-32	4.
	3	23 Feb (2	6671	28.25	Cape Kennedy	.1628	1.00	1133	88-37	4

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### 3. DEVELOPMENT OF MODEL

### 3.1 Introduction

Development of thermodynamic profiles can be based entirely on the functional representation of one variable, for example, pressure, and the others following by application of the hydrostatic law and the equation of state. Ideally, density should be the fitted variable since the ROBIN program first computes density and later pressure and temperature. Therefore, any daily and seasonal trends associated with the earth's atmosphere would most likely appear as perturbations in density. Numerical integration of density introduces "smoothed" pressure data and any trends that were observed in the former are partially suppressed. It is for this reason that density should be the primary variable investigated in the determination of daily and seasonal trends within the earth's atmosphere. However, it turned out that the function needed to fit density adequately could not be integrated analytically (hydrostatic law) to determine pressure. But the function needed to fit pressure adequately could be differentiated (hydrostatic law) to determine density. (In both cases the gas law could be used to determine temperature.) Thus, a model based on pressure data has been developed which is discussed in the sections that follow.

Section 3.2 is concerned with the derivation of atmospheric equations needed for development of the model. The particular set of equations used in the final model will be of a somewhat different nature but the methodology employed in this section is necessary for their derivation. Since the atmospheric equations are in terms of unknown parameters a technique must be developed for their specification. This topic is discussed in Section 3.3. Probably the most important section of this report and the one that led to the development of the model is Section 3.4. The properties of the coefficients are discussed briefly and then used in the derivation of the model (Section 3.5). Properties of the model are presented in Section 3.6.

### 3.2 Derivation of Atmospheric Equations

Mathematical equations describing the behavior of thermodynamic variables must be compatible with the physical laws which relate these variables. These laws impose a major constraint in the mathematics in that once one variable is specified by a particular equation, the others are uniquely determined. However, this fact can be used to advantage since only one variable need be expressed in terms of a function.

The laws which govern the interrelationships of the variables pressure, density, and temperature are the hydrostatic and gas laws (equation of state). The hydrostatic law is used to express density as a function of pressure while the equation of state relates temperature to pressure and density as their ratio. Therefore, the three basic equations needed for development of the model are derived as follows.

3.2.1 Pressure

Pressure is assumed to be of the form

$$P = \exp \left[\beta_0 + \beta_1 z + \dots + \beta_k z^k\right]$$
(1)

where P is pressure in millibars and 100-z is geometric altitude.

3.2.2 Density

The hydrostatic law is used to express density in terms of the derivative of pressure with respect to z. Thus,

$$\rho = \frac{100}{g(z)} \frac{dP}{dz} = \frac{100}{g(z)} [\beta_1 + 2\beta_2 z + \dots + k\beta_k z^{k-1}] \exp[\beta_0 + \beta_1 z + \dots + \beta_k z^k]$$
(2)

where

$$g(z) = \frac{g_s}{[1 + (h/r)]^2} = \frac{9.7803}{\{1 + [(100-z)/6372.8988]\}^2}$$

is the acceleration due to gravity;  $g_s$  is the gravitational constant at sea level in meters per sec<sup>2</sup>; h is geometric altitude in kilometers; r is the radius of the earth in kilometers;  $\rho$  is density in grams per cubic meter; and the factor of 100 is the conversion from millibars per kilometer to gram meters per sec<sup>2</sup> per cubic meter.

3.2.3 Temperature

The equation of state now relates temperature to pressure and density as

T = 348.385 
$$\frac{P}{\rho} = \frac{3.48385 g(z)}{\beta_1 + 2\beta_2 z + ... + k\beta_k z^{k-1}}$$
 (3)

where T is temperature in  ${}^{o}K$ .

Now that the necessary equations for building the model are at hand the problem of determining the  $\beta$ 's still remains. This topic will now be discussed.

### 3.3 Determination of $\beta$ 's

Pressure data from each flight was fitted by an exponential of the form given in Equation (1). Coefficients of Equation (1) were calculated for each flight using a least squares fitting program on the log pressure,

$$\log P = \beta_0 + \beta_1 z + \ldots + \beta_k z^k \qquad (4)$$

The coefficients of the associated polynomials (Equation (4)) for k = 2, 3, ..., 6are listed in Tables II through VI. The large coefficients observed for Flights 5, 34, 40, 43, and 57 are due to missing data at either the high altitudes, low altitudes, or both. Data in these regions control the tailing off of the polynomials and, hence, affect considerably the resulting  $\beta$ 's. Standard errors of estimate are included to illustrate the goodness of fit for each of the polynomials.  $\beta$ 

### TABLE II

LIGHT NO.	βο	βι	β <sub>2</sub>	ERROR OF
1	-8, 12471	0. 18282	-0.00051334	0.04324
2	-8.05348	0.17695	-0.00042348	0.06502
3	-8.40256	0.21065	-0.00085854	0.04661
4	-8.33824	0.19536	-0.00061598	0.06616
5	-7.47391	0.16481	-0.00038991	0.04330
6	-8.21276	0.19600	-0.00072226	0.06784
7	-8.36383	0.19877	-0.00068798	0.04767
8	-8.24857	0.19371	-0.00063229	0.05127
9	-8.32785	0.19587	-0.00070052	0.03977
10	-8.27462	0.19597	-0.00072163	0.03926
11	-8.15785	0.19528	-0.00070827	0.01890
12	-8.22003	0.19335	-0.00066042	0.04387
13	-8.25296	0.19100	-0.00059909	0.05980
14	-8.21710	0.18725	-0.00054446	0.05496
15	-8.34522	0.19328	-0.00060478	0.04457
16	-8.32353	0.21071	-0.00095915	0.00100
17	-8.25261	0.19267	-0.00061472	0.02089
18	-8.2/520	0,19160	-0.00059704	0 02090
19	-0.19023 9 20954	0 20047		0.03012
20	-7 64680	0 16441	-0.00030203	0.02054
27	-8 19361	0. 19264	-0.00065993	0.03994
23	-8.44420	0.20912	-0.00090403	0.02228
24	-7,93187	0.17094	-0.00030589	0.06039
25	-8.06619	0.18080	-0.00048883	0.03394
26	-8.59139	0.22538	-0.00118690	0.07933
27	-8.25783	0.19542	-0.00067208	0.03520
28	-8.21245	0.19815	-0.00072891	0.01832
29	-8.01403	0.17428	-0.00038922	0.04103
30	-8.13331	0.18053	-0.00045106	0.01396
31	-7.98065	0.16874	-0.00029860	0.03684
32	-8.02432	0.17139	-0.00034352	0.03828
33	-7.92963	016499	-0.00025491	0.04037
34	-8.84573	0.19838	-0.00056994	0.06188
35	-8.54030	0.21061	-0,00086091	0.02530
36	-8.38349	0.20628	-0.00082931	0.03215
37	-8.27600	0,19989	-0.00076264	0.03796
38	-8.39017	0.20550	-0.00080354	0.03069
39	-8.38614	0.20550	-0,00080104	0.03137
40	-7.70396	0.16501	-0.00030903	0.01413
41	-8.35109	0.19045	-0.00050509	0.06500
42	+0,11102 9 E00E0	0.19323	0.00062355	0.00500
43 44	-0.30737 -8 30666	0. 19303	-0.00083664	0,05120
45	-8.57042	0, 22430	-0,00116930	0.06295
46	-8.49977	0.21158	-0.00089328	0.01693
47	-8.25388	0.19494	-0.00064960	0.04150
48	-8.21772	0.19296	-0.00060946	0.05410
49	-7.94802	0.17887	-0.00045035	0.04384
50	-8.22031	0.19170	-0.00060193	0.06592
51	-8.07256	0.18578	-0.00053655	0.05463
52	-8.51436	0.20988	-0.00085903	0.05240
53	-8.07836	0.18008	-0.00045090	0.03560
54	-8.45551	0.20439	-0.00077983	0.06486
55	-7.91244	0.17333	-0.00037606	0.08324
56	-8,09522	0,1 <b>7</b> 755	-0.00023551	0.05607
57	-7.93997	0.17008	-0.00031990	0.02849
58	-8.41788	0.19005	-0.00052232	0.03272
59	-8,24288	0.18850	-0.00055150	0.06078
60	-8.28778	0.19920	-0.00076395	0.01891
61	-8.08772	0.18572	-0.00056983	0.02794
62	-8.24843	0.19767	-0.00074026	0.02383
63	-8.32545	0.20184	-0.00078373	0.03482
64	-8.07918	0.18802	-0,00061957	0.03480
65	-8.37411	0.20590	-0.00084575	0.03350
		o 100\7		

### POLYNOMIAL COEFFICIENTS FOR THE SECOND DEGREE

### TABLE III

### POLYNOMIAL COEFFICIENTS FOR THE THIRD DEGREE

					STANDARD
FLIGHT		_	_	_	ERROR OF
NO.	βo	βι	β <sub>2</sub>	β <sub>3</sub>	ESTIMATE
1	-8.042229	0.1643246	0.00031985	-0.00000991891	0.02587240
2	-8.112371	0.1877381	-0.00082299	0.00000391672	0.06031915
3	-8.426510	0.2154843	-0.00105489	0.00000211134	0.04553572
4	-8. 429127	0.2117578	-0.00121444	0.00000578225	0.05456262
5	-1.144247	-0.2251876	0.00755328	-0.00005348949	0.04256370
6	-8.256495	0.2058112	-0.00116398	0.0000525861	0.06531323
7	-8. 351914	0.1962848	-0.00058348	-0.00000116111	0.04740940
, B	_8 983369	0 2660244	-0.00272337	0 00001834276	0 02292984
9	-8. 139646	0.1984170	-0.00081134	0.00000127381	0.03946556
10	-8 271891	0 1953128	-0.00068950	-0.00000041186	0.03974839
10	-8 131840	0 1997177	-0.00042518	-0.00000349485	0.01539622
11	9 774825	0.1072177	0.00032318	0.00000063006	0.04377834
12	-0.220033	0.174/4/4	0.00071807	0.00000413036	0.05670559
14	9 100716	0.1936403	0.00020010	-0.00000157621	0.05445362
14	-0.177210	0.1030403	-0.00037787	0.00000137021	0.03443302
15	-0, 412/3/	0.2022927	-0.00090838	-0.00000287143	0.04201007
10	-8,200400	0.1901099	-0.00019425	-0.00001062334	0.03091802
17	-8.200519	0.1950232	-0.00074095	0.00000142833	0.02006531
18	-8.378507	0.2105151	-0.00129810	0.00000686726	0.02185582
19	-8.210257	0.2008673	-0.00089595	0.00000238505	0.02002853
20	-8.250962	0.2098073	-0.00115048	0.00000483245	0.02431444
21	-8.8/1900	0.2545835	-0.00241355	0.00001581660	0.00768885
22	-8.160122	0.1853056	-0,00033737	-0.00000376163	0.03718745
23	-8.465879	0.2122194	-0.00102992	0.0000152586	0.02220533
24	-7.821230	0.1435682	0.00104893	-0.00001771008	0.03800036
25	-8.008142	0.1682531	0.00005669	-0.0000627038	0.02370014
26	-8.729509	U. 2554501	-0.00270670	0.00002111103	0.07057039
27	-8.225112	0.1873277	-0.00027142	-0.0000523741	0.03234969
28	-8.192782	0.1933294	-0.00051237	-0.0000255593	0.01614304
29	-8.050149	0.1810018	-0.00064180	0.0000251327	0.03822576
30	-8.133439	0.1805473	-0.00045174	0.0000000689	0.01396127
31	-7.969798	0.1667530	-0.00022495	-0.0000072202	0.03657059
32	-7.994626	0.1648009	-0.00007371	-0.00000289395	0.03584775
33	-7.939727	0.1668100	-0.00032138	-0.0000064220	0.04015656
34	-8.342692	0.1533551	0.00064689	-0.00001014024	0.05764908
35	-8.515565	0.2060408	-0.00066818	-0.00000221713	0.02432815
36	-8.333467	0.1982395	-0.00050658	-0.00000364669	0.030666 <b>60</b>
37	-8.280911	0.2011014	-0.00082284	0.0000078686	0.03790310
38	-8.422417	0.2127331	-0.00112924	0.00000387743	0.02753891
39	-8.347606	0.1986191	-0.00052116	-0,00000310974	0.02943360
40	-9.412742	0.2816499	-0.00288612	0.00001847380	0.00371011
41	- 8, 599390	0, 2284481	-0.00187566	0.00001230579	0.03751611
42	-8.244085	0. 2234569	-0.00209199	0.00001680482	0 03359397
43	-8 612957	0 2035429		0 0000153917	0.005356362
44	-8 339464	0 2100147	-0.00116817	0.00000394615	0.04030793
45	-8 705358	0.2536844	-0.00765475	0.00003063440	0.04730782
46	-8.103338	0.2061446	0.00203423	0.00002082440	0.05205976
40	-0.437300	0.1670795	-0.00008158	-0.00000241375	0.01000817
48	P 090436	0.1670703	0.00001074	-0.00002019915	0.01030203
40	-0.007430	0.1039701	0.00091770	-0.00002213272	0.04276608
47	-7.935040	0.1764902	-0.00035822	-0.00000094494	0.04353522
50	-0.3/30/5	0.2189627	-0.00158256	0.00000933928	0.01913767
51	-6.1/2103	0.2034845	-0.00117338	0.0000606505	0.03614183
52	-8.807382	0.2456055	-0.00205504	0.00001172554	0,04077614
53	-8.370456	0.2103686	-0.00132751	0.0000748481	0.02003007
54	-8.897025	0.2570627	-0.00249645	0.00001634878	0.03971226
55	-7.774537	0.1418134	0.00106948	-0.00001752165	0.05968714
50	-	-	-	•	-
57	-8.812108	0.2360510	-0,00185296	0.00001130449	0.01013397
58	-8.599733	0.2106347	-0.00115186	0.00000559592	0.02346729
59	-8.520740	0.2239589	-0.00168469	0.00001020890	0.02993843
60	-8.376140	0.2118022	-0.00124108	0,00000521453	0.01437523
61	-8.052038	0.1814186	-0.00042770	-0.00000137323	0.02764148
62	-8.355115	0.2116005	-0.00123191	0.00000504255	0.01973364
63	-8.764022	0.2493538	-0.00226941	0,00001395010	0.01150004
64	-8.043036	0.1829320	+0.00042974	-0.00000204118	0.03442616
65	-8.585769	0.2346363	-0.00187124	0.00001051777	0.01235391
66	-8.724858	0.2572674	-0.00284977	0.00002089420	0.01739950
67	-8.766315	0.2426032	-0.00199998	0,00001152999	0.01107606
			-	-	

### TABLE IV

FLIGHT NO.	βο	β1	$\beta_z \times 10^2$	$\beta_3 \times 10^4$	β4 × 10 <sup>6</sup>	STANDARD ERROR OF ESTIMATE
	-7 09006	0. 14369	0.20123	-0.57205	0. 42220	0.01494
2	-7.96458	0. 14121	0.23087	-0. 68068	0. 52930	0.01987
	-8. 13937	0.18519	0.11850	-0.54382	0.45559	0.03024
4	-8.30026	0.17182	0.14344	-0.54216	0.43477	0.02283
5	-240.18430	19.43453	-59.51882	81.11329	-41.23646	0.02995
6	-8.13842	0.15999	0.25946	-0.99753	0.93760	0.04544
7	-8.26595	0.16532	0.17835	-0.62861	0.51417	0.03328
8	-9.16251	0.29011	-0.38255	0.39006	-0.13594	0.02251
9	-8.24927	0.16465	0.18609	-0.70797	0.62130	0.01683
10	-8.24019	0.18198	0.04904	-0.35928	0.34150	0.03/12
11	-8.10563	0.17864	0.04755	-0.29599	0.24171	0.02590
12	-8.130/3	0.10287	0.28322	-0. 79604	0, 59900	0.02976
14	-8.07936	0.14197	0.26830	-0.79281	0.62665	0.02779
15	-8.09304	0.14051	0.25895	-0.71832	0.53374	0.02459
16	-8,16517	0.14875	0.43589	-1.59176	1.54742	0.03818
17	-8.24511	0.18777	-0.01304	-0.14760	0.13717	0.01821
18	-8.33432	0.19660	-0.03617	-0.14657	0.15826	0.01370
19	-8.21605	0.20341	-0.11300	0.09715	-0.07330	0.01989
20	-8.22929	0.20156	-0.04859	-0.13407	0.15999	0.02275
21	-8.18985	0.18716	0.00023	-0.21448	0.20935	0.00726
22	-8.08651	0.15728	0.19202	-0.65724	0.54353	0.02308
23	-7.97648	0.11585	0.52501	-1.63124	1.49682	0.01290
24	-7.79707	0.13319	0.19859	-0.46470	-0.01781	0.02368
25	-8.01073	0.10922	-0.00199	2 05498	-1.92070	0.05995
20	-8.92970	0.32174	0.14094	-0. 56831	0.50582	0.02720
28	-8, 15536	0.17858	0.06707	-0.35067	0.28699	0.00686
29	-7.96110	0,15252	0.13046	-0.42896	0.33888	0.01669
30	-8.16812	0.18801	-0.09087	0.10427	- <b>0.</b> 07894	0.01320
31	-7.90762	0.14718	0.10926	-0.31007	0.22268	0.02763
32	-7.99895	0.16638	-0.01879	-0.00071	-0.02244	0.03581
33	-7.90601	0.15636	0.03716	-0.15055	0.11375	0.03801
34	-5.22960	-0.22484	1.66369	-2.91702	1.75976	0.03192
35	-8.43498	0.18315	0.10141	-0.46711	0.38449	0.01770
36	-8.09129	0.14156	0.33322	-1.01207	0.82078	0.01100
37	-8,24350	0.18502	-0.09872	-0.00090	0.03542	0.02748
30	-8 21833	0.16301	0.20065	-0.67582	0.53727	0.01199
40	-11, 22771	0.44755	-0.84536	0.99842	-0.43747	0.00249
41	-8.55927	0.21887	-0.12962	-0.00216	0.08818	0.03643
42	-8.32082	0.25383	-0.46292	0.88989	-0.65622	0.01387
43	-21.95636	1.52964	-4.99262	8.04989	-4.89909	0.00584
44	-8.24077	0.17171	0.19737	-0.83833	0.78374	0.02989
45	-8.88603	0.31351	-0.78944	1.87034	-1.73343	0.03977
46	-8.52742	0.21872	-0.14610	0.17132	-0,17200	0.01654
47	-8.09823	0.15129	0.22908	-0.69232	0.51524	0.01220
48	-7.98812	0.12925	0.40849	-1.20721	1.13907	0.01449
49	-1.84781	0.14152	-0.07083	-0, 10180	0. 13947	0.00913
50	-0. 56705	0,17917	0.04156	-0.29410	0.25339	0.01928
52	-8, 50246	0.19372	0.07703	-0.48928	0.44598	0.03721
53	-8,01289	0.15878	0.10927	-0. 37670	0.28985	0.01133
54	-8.71522	0.22674	-0.08858	-0.17293	0.24030	0.03832
55	-7.65170	0.09320	0.51310	-1.33072	1.05046	0.03414
56	-	-	-	-	-	-
57	-7.86109	0.13890	0.16564	-0.42580	0.29607	0.00510
58	-8.29927	0.16286	0.12397	-0.41193	0.31193	0.01354
59	-8.33514	0.18953	0.01702	-0.27348	0.25376	0.02084
60	-8.30914	0.19830	-0.03983	-0.15159	0,10100	0.01350
61	-(.02230 _8 15769	0.17530	0. 0%501	-0. 63190	0.34145	0,01521
63	-8.61543	0.22725	-0.11676	-0.08317	0.15681	0,01052
61	-7.65916	0.10644	0.42769	-1, 14070	0,90346	0,01865
65	-8,55410	0.22853	-0.15108	0.02317	0.06308	0.01209
66	-8.78404	0.26716	-0.33581	0.30947	-0.06713	0.01664
67	-8.78894	0.24575	-0.21478	0.14351	-0.01881	0,01106

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### POLYNOMIAL COEFFICIENTS FOR THE FOURTH DEGREE

### TABLE V

							STANDARD
NO	Α.	A	8 ~ 102	a v 101	a ~ 106	A V 105	ERROR OF
NO.	Po	P1	p2 x 10	p3 X 10-	P4 X 10-	β <sub>5</sub> × 10 <sup>-</sup>	ESTIMATE
1	-7.99234	0.14569	0.17531	-0.44700	0.16991	0.18021	0.01488
2	-7.97383	0.14575	0.18276	-0.48998	0.21268	0.18624	0.01957
3	-8.29961	0.16353	0.37088	-1.64203	2.45600	-1.29058	0.02613
4	-8.26276	0.15369	0.33261	-1.28096	1.64353	-0.70073	0.01802
5	-1496.55600	148.66640	- 588. 79720	1160.01900	-1135.91800	442.29540	0.02545
6	-8.06538	0.11535	0.83722	-3.78426	6.55969	-4.01578	0.03526
7	-8.25110	0.15693	0.27954	-1.08375	1.37094	-0.57118	0.03278
8	-8.57488	0.19009	0.24773	-1.46327	2.43072	-1.35088	0.02183
9	-8.22720	0.15169	0.34788	-1.46111	2.08814	-1.01161	0.01448
10	-8.1/802	0.14102	0.62146	-3.3354Z	6.80956	-4.97543	0.02775
11	-8,10530	0.18037	0.02425	-0.17932	-0.00242	0.18084	0.01123
12	-8.00570	0.13468	0.50192	-2.08591	3.23977	-1.79422	0.01701
14	-8.05603	0.11555	0. 33703	-1.90838	2.70041	-1.33423	0.02441
)5	-7.96704	0.12872	0.42275	-1.404/0	1.05005	-0.78968	0.02018
16	-8.16740	0 15037	0. 31771	-1.03170	1. 70070	-0.01441	0.02320
17	-8. 25462	0 19325	-0.08021	0 16071	0 45116	0.21250	0.03817
18	-8, 34091	0 19984	-0.07047	-0.01063	-0.06742	0.12276	0.01763
19	-8, 19871	0, 19135	0.06257	-0.85271	2.07398	-1 71783	0.01348
20	-8.19068	0.17843	0.24531	-1. 52646	2,91961	-1.93657	0.01703
21	- 5. 49759	-0.14677	1.61365	-4, 01383	4. 57585	-1.96247	0 00687
22	-8.07585	0.15090	0.27313	-1.04151	1, 30512	-0. 53445	0.02270
23	-7.89993	0.09669	0.69857	-2.35195	2, 88863	-1,01223	0.01284
24	-7.84630	U. 10007	-0.27893	2.06734	-5.32931	1. 10099	0.03092
25	-8,02145	0.17551	-0.08051	0.32347	-0.72970	0.49095	0.02331
26	-9.09794	0.39751	-1.83920	7.30270	-14.03210	10.09284	0.05578
27	-8.13008	0.13354	0.64235	-3.22701	6.39778	-4.62115	0.01752
28	-8.16122	0.18225	0.01810	-0.11095	-0,20024	0.34939	0.00637
29	-7.95638	0.15016	0.15577	-0.53081	0.51050	-0.10246	0.01659
30	-8.31682	0.23036	-0,46881	1.52602	-2.44255	1.43250	0.00515
31	-7.94824	0.16713	-0.10216	0.52788	-1.16853	0.81836	0.02305
32	-8.05086	0.19475	-0.34889	1.43360	-2.63212	1.68222	0.02931
33	-7.96082	0.18285	-0.23933	0.92930	-1.65301	1.02421	0.03202
34	-6.71738	0.00316	0.34596	0.69013	-2.94470	2.35223	0.03094
35	-8,49455	0.20637	-0.15356	0.66187	-1.77681	1.48998	0.01526
36	-8.02308	0.12057	0.53936	-1.87308	2.42359	-1.08258	0.00986
37	-8.18059	0.14223	0.67305	-3,67331	7.60756	-5.62428	0.02381
38	-8.38259	0.18939	0.18101	-1.35014	2.75745	-1.94431	0.02372
39	-8.25003	0.17527	0.07013	-0.11631	-0.49893	0.69080	0.01093
40	-10.03/30	0 20551	-3. (3991	7.41507	- (. 44111	3.01232	0.00191
47	-8 35120	0,20334	-0.71285	-0.44444	2 17010	-0.39071	0.00300
43	-74, 10129	8.01082	-37 06011	87 00254	-3.17818	1.03413	0.00700
44	-8, 18420	0.13715	0.64477	-2.99631	5 13736	-3 10073	0.02002
45	-9,05186	0.38820	-1.76320	7.04300	-13, 67162	9 94849	0.02002
46	-8.69710	0.25849	-0.48716	1. 52389	-2,68165	1. 76116	0.01640
47	-8.13966	0.17427	-0.09858	1,13590	-3.83620	3, 70336	0.00822
48	-7.87200	0.07525	1.13958	-5.31532	10.87668	-8,46749	0.03571
49	-7.79806	0.12512	0.39261	-1.35721	1.76758	-0.80718	0.00810
50	-8.32501	0.20328	-0.04717	-0.19287	0.28628	-0.08392	0.00895
51	-8.06775	0.16739	0.16268	-0.76030	1.00522	-0.42962	0.01693
52	-7.37051	-0.05291	1.96409	-6.97602	10.67394	-6,01645	0.02228
53	-7.85407	0.12950	0.30165	-0.95015	1.07875	-0.40642	0.01081
54	-7.79585	0.03020	1.38071	-5.09391	7.78671	-4.31223	0.02840
55	-7.59033	0.05491	1.01798	-3.81074	6.14512	-3.70521	0.02408
56		-	-	-	-	-	-
57	-8.97916	0.28261	-0.54153	1.24399	-1.60237	0.83448	0.00406
58	-8,15076	0.13252	0.33854	-1.08731	1.28123	-0.51696	0.01267
59	-8.28522	0.17736	0.11200	-0.58929	0.72047	-0.25228	0.02055
60	-8.38159	0.21713	-0,20675	0.50059	-0.98815	0.75747	0.01321
01 47	-7.36711	0.05395	0.76305	-2.25124	2.79473	-1.27392	0.01171
02	-7.95165	0.12684	0.48204	-1.86003	2.74494	-1.46572	0.01370
63	-8.04739	0.12000	0.62322	-2.44191	3.67216	-1.98048	0.00756
01	-1.30613	0.01564	1.22174	-4.19775	6. 23386	-3.43897	0.01227
64	-0.02282	0.24566	-0.29521	0.55471	-0.82241	0.54492	0.01172
47	-0.9/999	0.31048	- 0. 66063	1. 37208	-1.62121	0.83238	0.01469
01	-7.30320	U. 33657	- 0. 80341	1.91226	- 2. 50985	1.32856	0,00930

### POLYNOMIAL COEFFICIENTS FOR THE FIFTH DEGREE

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### TABLE VI

### POLYNOMIAL COEFFICIENTS FOR THE SIXTH DEGREE

FLIGHT NO.	βe	₿ı.	$\beta_2 \times 10^2$	<sup>و</sup> 10 × 10	$\beta_4 \times 10^5$	$\beta_5 \times 10^7$	β <sub>6</sub> × 10 <sup>9</sup>	STANDARD ERROR OF ESTIMATE
<u>├</u>		0 15966	-0.06861	0 11120	- 0 68409	0 94549	-0 56409	0.01374
	-8.01817	0.17777	-0.30868	0.24517	-0.79602	1.07920	-0.51989	0.01023
3	-8.25233	0.12549	1.01396	-0.58705	1.53499	-1.96463	0.98687	0.01864
4	-8.28174	0.16717	0,12890	-0.00796	-0.16456	0.35054	-0.20320	0.01656
5	15618.67000	-1964.47400	10241.56000	-2833.45600	4387.94100	- 3606. 56800	1229.22500	0.01439
6	-8.11679	0,16207	-0.04130	0.26238	-1.50714	0.65344	-2.03184	0.03223
Ŕ	-6. 32897	-0.27206	3,96555	-1.64995	3.48649	- 3. 69434	1.56108	0.02027
9	-8,24348	0.16588	0.09073	0.03486	-0.38138	0.79716	-0.51628	0.01296
10	-8.18255	0.14493	0.54204	-0.27107	0.45349	-0,11126	-0.24762	0.02770
11	-8,10018	0.17261	0.17590	-0.13272	0.40210	-0.63981	0.40611	0.01072
12	-8.06928	0,12104	0.73645	-0.30538	0.80996	-0.88264	0. 38427	0.02266
13	-8.07133	0.14184	0.20097	-0,00066	-0.25958	0.55402	-0.34032	0.02541
15	-7.67871	0.01850	1.49623	-0.65155	1.42395	-1.58870	0.71774	0.02044
16	-8.22857	0.21753	-1.07433	1.12289	-4.88376	9.23921	-6.39719	0.02787
17	-8. 24862	0.18813	0.01097	-0.04709	0.15702	-0.26255	0.17087	0.01767
18	-8.32936	0.19150	0.05754	-0.07768	0.20013	-0.2029/	0. 13341	0.01270
20	-0.180/8	0.16846	0. 42945	-0. 28456	0. 72976	-0.87175	0. 39654	0.01643
21	7.79714	-2.13003	13.67678	-4.23271	7.16414	-6.33664	2. 29977	0.00629
22	-8.08797	0.16168	0.07415	0.03839	-0.34257	0.67929	-0.42850	0.02218
23	-8.72855	0.34806	-2.22534	1.44755	-4.81231	7.69092	-4.72251	0.01153
24	-7.86227	0.18294	-0.61650	0.47759	-1.53862	2.18161	-1.13824	0.03020
25	-7.97756	0.13728	0.61250	-0.45536	1.51758	- 2, 37182	1. 37133	0.01552
20	-9.13891	0. 11199	1. 08943	-0.68143	1.97175	-2.76863	1, 507 53	0.01515
28	-8,15633	0.17751	0.11079	-0.07914	0.20905	-0. 32386	0.21209	0,00603
29	-7.95409	0.14848	0.18204	-0.06904	0.09606	-0.06953	0.02949	0.01657
30	-8.29118	0.22129	-0.36073	0.09413	-0.08678	-0.06253	0.10393	0.00499
31	-7.94230	0.16284	-0.03631	0.01338	-0.00735	-0.06026	0.06966	0.02295
32	-8.02554	0.17318	0.03437	-0.11342	0.52500	-0.95603	0.60429	0.03169
34	-22.01576	2.83192	-20,41888	7.83499	-15.95680	16.44811	-6.75537	0.01410
35	-8.51332	0.21575	-0.29489	0,15803	-0.46678	0.58347	-0.24979	0.01513
36	-8.07634	0.14084	0,27483	-0.02905	-0.23175	0.58325	-0.39069	0.00959
37	-8.13253	0.09328	1.68862	-1.18221	3.78637	- 5. 80177	3. 42441	0.01294
38	-8.34008	0.15075	0.90763	-0.66498	Z. 06637	-3.01751	-0.97209	0.01040
39	-8.33930	0.40643	-0. 50035	-0.40966	-1.25409	-1.35590	0. 59395	0.00189
41	-8.31124	0,11623	1.11423	-0.64567	1.63003	-1.94634	0.89543	0.02428
42	-8.34227	0.26448	-0.55376	0.09357	0.08882	-0.46937	0.39563	0.00599
43	-1516.69800	223.21890	-1369.56700	447.02380	-818.08550	795.91640	-321.62510	0.00544
44	-8.19942	0.15097	0.38477	-0.10999	-0.12699	0.69920	-0.60129	0.01907
45	-9.1558/	-0 17036	-2.81025	1. 51990	-4. 11025	-10.81422	6. 42710	0.01449
47	-8.16049	0.18957	-0.40344	0.36578	-1.37698	2.22158	-1.31294	0.00737
48	-7. 59005	-0.09058	4.18980	-2.98955	10.76254	-19.11576	13. 23842	0.02598
49	-7.79538	0.12308	0.42541	-0.15627	0.23651	-0, 16185	0.04161	0.00803
50	-8.31060	0.19323	0.10262	-0.10635	0.26355	-0.30451	U. 14101 0 15057	0.00715
51	-8.03193	0.14239	U. 53508 K. JK391	-0.29247	U. 08457 5. 25673	-0.11715	2. 55667	0.01470
53	-7.69763	0.09453	0. 59732	-0.21747	0. 37299	-0. 32824	0.12326	0.01070
54	-6.15905	-0.39586	5.51090	-2.44672	5.48310	-6.13230	2.71480	0.01769
55	-7.59053	0.05510	1.01441	-0.37842	0.60539	-0.35587	-0.00888	0.02408
56		-	-	•	•		-	0,00322
57	-11.97017	0.10751	-3.42445	1.04904	-1.7/512	1. 54302	0, 11673	0.01256
59	-8,14865	0,13618	0.53865	-0. 26202	0.55664	-0, 58852	0, 25374	0.01975
60	-8, 56831	0.27646	-0.89311	0.42825	-1.16719	1. 56764	-0.81524	0.01266
61	-7.25729	0.02510	1.04577	-0.35938	0.61018	-0.53334	0.19611	0.01163
62	-8.04751	0.15438	0.18990	-0.03701	-0.11757	0.36565	-0, 26268	0.01362
63	-7. 47614	-0.01058	1.77746	-0.75249	1.55252	-1.59639	1. 19879	0.00489
65	-8.85787	0.31740	-1.03534	0. 16718	-1. 17917	1.49486	-0.73865	0.01040
66	-9, 19575	0. 36857	-1, 22987	0. 10217	-0, 79357	0. 82204	-0, 33619	0.01369
67	-10.28907	0, 54723	-2.55078	0.91553	-1.84467	1.91016	-0,78991	0.00808

coefficients within each column are determined by dividing the coefficients by the factor heading that column. Plots of standard error of estimate versus the degree of each polynomial for seven flights are illustrated in Figure 1. In general, the standard errors for the 6th degree polynomials are at least half those of the 2nd degree polynomials. Pressure calculated by Equation (1) for polynomials of degrees 3 and 5 is compared to data from Flights 1, 2, 12, 32, 50, and 63. These flights were chosen for several reasons. First, temperature profiles determined from the data of Flights 1, 50, and 63 appear to be quadratic. This data can, therefore, be used for comparison with calculated data using a 3rd degree polynomial (any polynomial of degree less than 3 would not explain the quadratic behavior of temperature). The profiles for Flights 2, 12, and 32 appear quartic. The data from these flights can be compared to that calculated using a 5th degree polynomial. The second reason for choosing these flights was to illustrate the improvement in goodness of fit with increasing degree polynomial. Results are tabulated in Tables VII through XVIII including percent differences and standard errors of estimate. Percent differences show deviations of observed data from Equation (1) at various altitudes while the standard error indicates the goodness of fit over the entire altitude range. The goodness of fit improved considerably with increasing degree polynomial.

### 3.4 Properties of $\beta$ 's

This section is concerned with the distribution of the  $\beta$ 's as well as their interrelationship. The distributions are needed to compute probabilities of profiles while the latter provides information to build a realistic model. The results of this section form the final basis for the model.

The coefficients tabulated in Table III for the 3rd degree were plotted for each pair of  $\beta$ 's. These plots can be found in Figures 2 through 7. It is obvious that the  $\beta$ 's are highly correlated and this fact will be used to advantage



Standard Error of Estimate Versus Degree Polynomial for Flights 3, 9, 14, 34, 47, 57, and 65. Figure l.

	ST ANDARD Error CF Estimate	14.3071		STANDARD Error of Estimate	0°7254
	PERCENT Difference	111 11 1 4 10000000000 20000000000000000000000000		PERCENT DIFFERENCE	9 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1
I	CALCULATED TEMP.		TED 1	CALCULATED TEMP.	2017 - 20
FLIGHT	CBSERVED TEMP.	N N N N N N N N N N N N N N N N N N N	LCULA	DBSERVED TE4P.	2000 2000 2000 2000 2000 2000 2000 200
L FOR	STANDARD LROOR OF ESTIMATE	0 / 2 0	HAT CA VD (3) L FOR ]	STANDARD ERROR OF ESTIMATE	. 0158
NOMIAI	85.87.17 51.84.68.01 51.84.68.01		III A TO TH , (2), AN TNOMIAI	PERCENT DIFFERENDE	1
LE POL	CALCULATEC DENSTTY	しついしょうシューション いしたしょう、 していしょう、 していしょう、 していしょう、 している。 している している。 している。 している している。 している したい。 している している したい。 している したい。 したい。 したい。 したい。 したい。 している したい。 したい。 したい。 したい。 したい。 したい。 したい。 したい。	ABLE V ED DAT IONS (1) E POLS	CAL CULATEF. De NSITY	4000 400 400 400 400 400 400 400 400 40
DEGRI	1115130 UTARASO	またので、1000円でので、1000円でので、1000円でので、1000円でので、1000円でので、1000円でので、1000円でので、1000円でので、1000円で、10000000000	T DEGRE	OBSFRVED DEALTY	4004 4004 4004 4004 4004 4004 4004 400
THIRD	51400669 50166 06 55114676	6 11	N OF C BY ] FIFTH	ST4110420 Erpor of Estl4115	. do .
OR THE	ne jegange Undergrange	20 100 300000 3100 30000 3100 3001090 1 11	APARISC OR THE	P L R C F N T D I F F ER FN C E	
μ <b>τ</b> η	CALOW AT G	・・・・・・・・・・・・・・・・・・・・・・・・・・・・・・・・・・・・・	ы СО СО	5 2015 2 2015 1971 1971 2 2 2 1 2 10	00000000000000000000000000000000000000
	Selissike Cikolisike	1 + 10 つたちとうこうべつのの たまのうかからようというのの いいようないたいで、10 かん いいようないたいで、10 かん いいよいないで、10 かんの いいよいないで、10 かん たいののので、10 かんのの たいののので、10 かんのの たいののので、10 かんのの たいののので、10 かんのの たいのののので、10 かんのの たいのののので、10 かんのの たいのののので、10 かんのの たいのののので、10 かんのの たいのののので、10 かんのの たいのののので、10 かんのの たいのののので、10 かんのの たいのののので、10 かんののので、10 かんののので、10 かんののので、10 かんのののので、10 かんのの たいののので、10 かんのので、10 かんののので、10 かんののので、10 かんののので、10 かんののののののの たいのののので、10 かんののので、10 かんののので、10 かんののので、10 かんののので、10 かんのののので、10 かんののので、10 かんののので、10 かんののので、10 かんのののので、10 かんののので、10 かんのののので、10 かんののので、10 かんのののので、10 かんののので、10 かんののので、10 かんののので、10 かんのののので、10 かんのののので、10 かんのののので、10 かんのののので、10 かんのののので、10 かんのののので、10 かんののののので、10 かんののので、10 かんののののので、10 かんののののののののののので、10 かんののののののののので、10 かんのののののののののののののののののののののののののののののののののののの		por SS (p E	00004 40004 4000 4000 4000 4000 4000 4
	100-dl1			100-ALT	01000000000000000000000000000000000000

TABLE VII

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COMPARISON OF OBSERVED DATA TO THAT CALCULATED BY EQUATIONS (1), (2), AND (3)

	STANCARD Ergor CF Estimate	19.0697		ITANDARD RROR OF STINATE	12.0447
	PERCENT Difference	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1		PERCENT IFFERENCE	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1
8	CALCULATED TEMG.	まままと Z こ Z こ Z こ Z こ Z こ Z こ Z こ Z こ Z こ Z	ED	CALCULATED	200 197 197 207 209 201 201 201 201 201 201 201 201 201 201
LIGHT	OPSERVEO Temp.		CULAT	BSERVEO ( Tehp.	2024 2024 2025 2024 2024 2025 2024 2025 2025
(3) FOR FJ	STANJARJ Errop of Estimate	• • 9 3 0	AT CAL (3) FOR F	STANDARN Error of O Estimate	599 <b>3</b> *
NOMIAL	PERCENT Cifference	9 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	TO TH. 2), AND	PFRCENT LFFEQENCE	864 874 874 874 874 874 874 874 874 874 87
IS (1), (2 E POLYI	CALCULATEC Density	0 0 0 3 0 3 0 0 0 0 0 0 0 0 0 0 0 0 0 0	ALE X D DATA NS (1), ( S POLYI	ALCULATED DENSITY D	00353 00353 01573 01573 01573 01573 01573 01573 015550 015550 0000000000
UATION DEGREH	07537440 06 ASTIT	0 0 0 0 0 0 0 0 0 0 0 0 0 0	TA BSERVE QUATIO DEGREE	RSFRVED C. DENSITY	
BY EQ THIRD ]	STAND/RD Evoqr Of Estimate		N OF O] BY E( FIFTH ]	STANDARD Epror of d Estimate	. 1662
R THE	PERCINT JIFFSPENCE	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	PARISO R THE	P E CENT I F F E P EN C E	5 5 5 5 5 5 5 5 5 5 5 5 5 5
ΨC	CALOULATED PPESSURE	100 100 100 100 100 100 100 100	COM	ALCULATED PPFSSiPE D	000 000 000 000 000 000 000 000
	1855.2V-10 Par 55UU	82432 824 824 824 824 824 824 824 82		DASFRVED C PRESSUPE	Korner
	100-ALT	<b>300 101 101 101 101 000 000</b> 100 101 101 101 101 101 101 101 101 101			きょう うち ちゅうり うちょう うちょう うちょう うちょう しょう うちょう しょう しょう しょう しょう しょう しょう しょう しょう しょう し

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TABLE IX

COMPARISON OF OBSERVED DATA TO THAT CALCULATED

	PERCENT DIFFERENCE	-16.15
TED 12	CALCULATED TEME.	1 1 7 1 7 7 1 6 1 6
LCULA	085ERVE0 Tepe	197. 203.
AT CA (3) FOR FJ	STANJARJ Ferir Of Fstimate	.1486
A TO TH 2), AND VOMIAL	PARCINT Parents Clerents	5
ED DAT NS (1), ( POLYN	CALCULATE C DPASTTY	10000 1000 1000
BSERVI JUATIOI DEGREE	04522VLC 0EN3TTY	5555 5555 1110 1110 100
N OF O BY E( THIRD I	51410280 80200 05 85114170	8323.
R THE	PEPGATU TEPGATNOE	
COM FO	האברמורה הביקיטיר	7 0 0 1 0 0 7 0 0 1 0 7 0 1 0 0 7 0 0 0 7 0 7 0 7 0 7 0 7 0 7 0 7 0

100-4LT 325, JV 1

TABLE XI

STANCARD Error of Estimate	16.7 <b>8</b> 23												
PERCENT Difference	-16.15	-15.13	2.44		7.67	-10.05	- 28	-2.66	-3.22	7 -	2.56	5.61	9.14
CALCULATED TEME.	170.			191.	190	2 . 8	217.	227	238.	250.	263.	277.	2 à 2 •
OBSERVED Temp.	197.	203.	179.	175.	184.	229.	218.	234.	246.	262	256.	261.	265.
STANJART FERDR OF FSTIMATE	.1486												
PERCINT Cifference	3 • 5 C	16.31	f.1#	-6.10	-17.05	2.11	 ĴĢ	1.67	2.6.2	7.76	50.	14.01	-14.62
CALCULATEC DPNSITY	136JD.	1-1-0.	.13331	11200.	52710.	. 57758	. 37 871	.15971	.31158	.58467	1.07918	1.91129	3,27679
04522VLC 04422VLC	.:00:-		11254.	21912.	51910	.[3641	97972.	.13555	. 35236	.54393	1.37424	2,11562	3.73536
STANDARD Royca Of Estimate	8323.												
PEPCATUSE 1166.240MSE	-12.57	· . 55	÷.	2.14	[ 7 • 7 •	€9 <b>°</b> ∩-	e : • •	-1.15		5 M . N	<b>2</b> + 5 5	15.	15
כאבטטראדרים הפיקיטווי	20072.	• 1 • 5 • 6 •		57437 .	.r. 391	. 552	• • • 0 11	.1[~]1	.21:20	102240	5:5:4.	1.51731	2.7.3.0
0455 a.V. 1 € 26055 a.V. 1	(::'''		.(11).		• 5 2 2 3 5	• 6 2 2 3 •		52411	.212:5	6101×*	2,202.	4.5.25	2.9:5-1
0-4LT	. 3	3	94	4	5	<u>ب</u>	0 2	с, С	- <b>- - -</b>	1	ະ <b>ຈ</b>	., U	ĉ C

### TABLE XII

# COMPARISON OF OBSERVED DATA TO THAT CALCULATED BY EQUATIONS (1), (2), AND (3) FOR THE FIFTH DEGREE POLYNOMIAL FOR FLIGHT 12

STANDARD Error of Estimate	12.6648												
PERCENT DIFFERENCE	19.68	-4.80	. 30	3.15	3.42	-11.43	2.00	1.57	-92	44 ° M I	24	20	4.94
CALCULATED TEMP.	545.	194.	180.	181.	191.	206.	222.	238.	248.	253.	255.	260.	279.
OBSERVED TEMP.	197.	203.	179.	175.	184.	229.	218.	234.	246.	262.	256.	251.	265.
STANDARD ERROR OF ESTIMATE	6790*												
PERGENT Difference	-21.19	0	2.07	-2.93	-5.77	8.59	1.75	-1.19	-2.85	3.21	10	1.08	-5.83
CAL FULATED DENST 1 Y	. 06644	.00120	. 20714	.00776	.01052	. 03493	. 08(18	.154.91	24462 *	. 56: 97	1.07714	2.02747	3.54408
OUSERVED DENSITY	• 00351	.00115	. 30711	.00413	.01953	.03641	. 07279	.15665	.30296	.54393	1.67924	2.00563	3.75595
STANDARD Frong of Estimate	6600 •												
PEPCENT Diffequence	2.22	- 29	2.47	.28	-2.16	-1.47	7 4	1	10.1-		1 1 1		1.60
CALCULATED PPESSUPE	1.000.	.0357	01154	100	-01013	12101	15121	19251	781341	12824	78956		2.62393
3οί,ζω3ος Ουλέρλευ	02017	C 2 2 2 -		.00417		C 2 10 L		. 10500	21145	46996	70973	1.50256	2.45698
100-AL T	c	· v	-	• u • <del>•</del>		, u		- F	E ·	р <b>и</b> Г К			

XIII	
ЭЛ	
$\mathbf{AB}$	

## COMPARISON OF OBSERVED DATA TO THAT CALCULATED BY EQUATIONS (1), (2), AND (3) FOR THE THIRD DEGREE POLYNOMIAL FOR FLIGHT 32

STAND ROENT EPROF FLPENCE ESTIN	STANDARD Standard Stande CF Stimate
	3256

### TABLE XIV

## COMPARISON OF OBSERVED DATA TO THAT CALCULATED BY EQUATIONS (1), (2), AND (3) FOR THE FIFTH DEGREE POLYNOMIAL FOR FLIGHT 32

STANDARD Error of Estimate	14.2456	
PERCENT DIFFERENCE		•
<b>CALCULATED</b> TEMP.	171 172 173 173 173 173 173 173 173 173 173 173	
085E4VE0 Temp.	10000000000000000000000000000000000000	• • • • •
STANDARD Error of Estimate	.0632	
PERCENT DIFFEPENCE	1111 100000000000000000000000000000000	
CALCULATED DENSITY	000 00 00 00 00 00 00 00 00 00 00 00 00	3 • 98555
ORSEPVEN Density	4 4 4 4 4 4 4 4 4 4 4 4 4 4	3.99921
STANNARD EPPOR OF ESTIYATE	8 2 0 0 0	
P F P C E N T D T F F F C E N C E		84
GALGULATED PRESSUPE	00000 00000 00000 00000 00000 00000 000 000	2.74217
gegebyen Presven	1000 1000	2.75519
0- AL T	407 ww 3 3 0 R 9 6 6 6 6 6 7 6 7 6 7 6 7 6 7 6 7 6 7 6	

		STANCARD Erfor CF Estimate	7 C - 6 S -	STANDARD Error of Estimate	7.1374
TABLE XV COMPARISON OF OBSERVED DATA TO THAT CALCULATED BY EQUATIONS (1), (2), AND (3) FOR THE THIRD DEGREE POLYNOMIAL FOR FLIGHT 50		PERCENT Olfference	1 N N N N N N N N N N N N N N N N N N N	PERCENT LFFEXENCE	-16.94
	Q	CALCULATED TEME.	C 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	CALCULATED	162.
	CULATE GHT 50	ORSERVED TE4P.	CULATE	D BSERVED	190.
	T CAL( 3) OR FLI	STANDARD Error of Estimate	r CALC (3)	STANDAPD Error of Stimate	.2287
	TO THA , AND ( MIAL F	PIGCENT Pigcent	C THA'	PE ROCNT Leferiance	11.49
	) DATA 5 (1), (2) POLYNO	GALUNLATER O.KSTTY	LE XVI DATA 7 State 227955 227955 2275555 227555 2275555 2275555 2275555 2275555 2275555 22755555 2275555 22755555 227555555 22755555 22755555 22755	ALCULATEN JENSITY D	2 5000 .
	SERVEI JATIONS GREE I	11154-2 5° A2-300	TAB.	JASE PVED C DEMSITY	. C 3 0 4 6 2 2 4 2 4
	51400/60 F1304_0F E911461E	OF OBS BY EQI	514417420 Eporg of Estimate	.0142	
	ARISON THE TI		ARISON THE F	o FR CENT I FFF O ENCF	8 년 11년 11년 11년
	COM F FOR	6.46016.41-0 6213500	FOR PORT STREET	ALGULATED PPESSUAF	+2002+ -00066
		1,1,2,1,1 1,1,0,1,0 1,1,0,1,0	し、「「「「「「」」」」」」」」」」」」」」」」」」」」」」」」」」」」」」」	קריריטערק קריריטערק קריריטער	. 10165 . 10165
		103-217	ちょうか きゅうかう ひらかう ひうしょう しょう うか ひろう ひろう ちょう ひょう ひょう ひょう ひょう ひょう ひょう ひょう ひょう ひょう ひ	100-ål T	<b>e</b> u

ESTIM															
DIFFELENCE	• 16.0t			-1-85	1 4 1		3.89	7	1.12					1.07	5 O
TEMP.	162.	4 5 B	175.	185.	196.	208.	222.	215.	247	256.	261.	261.	255.	246.	232.
TENP.	190.		159.	188.	195.	209.	213	235.	244 .	256.	26.3.	276.	250.	241.	212.
ESTIMATE	.2287														
DIFFERENCE	11.49	2.74		6.9	.29	1.9	-2.43	- 02		- 10		1.5.4		-1.55	-10.11
Y LISH JC	.00052	. 001.7	00365	- 00ASE	.0185.3	10970.	.0414.4	.1596.5	30347	• 56941	1.06547	2.02247	3.94749	8.07861	17.28748
DENSITY	.0045	.00134	00359	.00417	.[1459	186±0.	5474Q.	.15968	. 30544	.57019	1.6439	1.92320	4.00923	6.16757	19.07610
ESTIMATE	.0142														
LEFFOUNCE	- 1 - 1 -	1.50		-1.38	.20	-, 72	1.42	47	5 × *	19	78	11	ۍ. ۵	40.	20.4
ppfsSilar	+2002*	•0002•	. 30174	22700.	14010.	. 12 * 9 5	.05191	.10751	.21530	.41957	2762.	1.51795	20102.5	5.57257	11.49.354
Johnshee	· [["	.20165	.19174	19433.	. 61 54 5	76263 *	.05107	.10912	. 21448	• 41 6 4 4		1.52259	2.89599	5.57027	11.59517
	e	ŝ	10	15	5	52	0 M	۴ ن	с э	<b>د</b> 5	05	55	60	е 10	20

		STANDARD Error CF ESTIMATE	e. 5365	
COMPARISON OF OBSERVED DATA TO THAT CALCULATED BY EQUATIONS (1), (2), AND (3)		PERCENT DIFFERENCE	11 11 11 100000000000000000000000000000	
	ň	CALCULATED TEMF.	* * * * * * * * * * * * * * * * * * *	
	IGHT 6	CBSERVES TEMP.	117. 1991. 2198. 2198. 2051. 2052. 2053.	
	D (3) FOR FL	STANDARD Errûr of Estimate	2 4 9 9	
	(2), AN	PERCENT CIFFERENCE	20120000 201200000 20140000000 20140000000 2014000000 2014000000 20140000000 20140000000 201400000000 20140000000000	Π
	NS (1), POLYN(		<ul> <li>C10829</li> <li>C10829</li> <li>C10829</li> <li>C10829</li> <li>C10829</li> <li>C10829</li> <li>C10820</li> <li>C1082</li></ul>	LE XVD
	QUATIO EGREE	025 - 342 - C	2010 2010	TAB
	BY E HIRD D	STANDERD F1200 DF ESTIMETE	τ υ υ υ	
	( THE T	HEROLAT DIFECRENCE	0 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	
	FOF	CALOULATED PRESSURE	0.10 0.10	
		- 2012 0-12 0-12 0-12 0-13 0-13 0-13 0-13 0-13 0-13 0-13 0-13	795113 65115 65115 17553 175553 175553 175553 175553 1755555 175555 1755555 17555555 17555	
		103-ALT	よ C C き き は d G G G G G G G G G G G G G G G G G G	

TABLE XVII

## COMPARISON OF OBSERVED DATA TO THAT CALCULATED BY EQUATIONS (1), (2), AND (3) FOR THE FIFTH DEGREE POLYNOMIAL FOR FLIGHT 63

STANDARD Error of Estimate	<b>8.</b> 9229
PERCENT DIFFERENCE	
CALCULATED TEMP.	178. 187. 202. 221. 238. 256. 266.
OBSERVED TEMP.	1171 1977 1987 1987 1987 1987 1987 1987
STANJARJ Error of Estimate	• 0825
PERSENT DIFFERENCE	
CALCULATED DENSITY	. 100 100 100 100 100 100 100 100 100 100
OASF PVED DEMSITY	444 444 444 444 444 444 444 444
STANDARD Erpor of Estimate	. 055
PERCFHT NIFFERENCE	00330054 • 00336 • 00340 • 003400 • 00340 • 003400 • 0034000 • 00340000 • 0034000 • 0034000000000 • 00
CALCULATED PPESSURE	0000 0000 0000 0000 0000 0000 0000 0000 0000
B GNSSBAG D SA ASBO D SA ASBO	900 10 10 10 10 10 10 10 10 10 10 10 10 1
108-4L T	

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in construction of the model. Linear equations best representing the points of each figure were derived through a linear least squares program. The set of linear functions used in the fitting procedure were:

$$\beta_{0} = m_{0,1}\beta_{1} + b_{0,1}$$

$$\beta_{0} = m_{0,2}\beta_{2} + b_{0,2}$$

$$\beta_{0} = m_{0,3}\beta_{3} + b_{0,3}$$

$$\beta_{1} = m_{1,2}\beta_{2} + b_{1,2}$$

$$\beta_{1} = m_{1,3}\beta_{3} + b_{1,3}$$

$$\beta_{2} = m_{2,3}\beta_{3} + b_{2,3}$$
(5)

A tabulation of slopes  $(m_{i,j})$ , intercepts  $(b_{i,j})$  and linear correlation coefficients (1. c. c.) for each of the fits are included in Table XIX. Similar data are included for degrees 2, 4, 5, and 6. Standard deviations for the slopes and intercepts are provided. The  $\beta_i$  versus  $\beta_j$  entry in the leftmost column denotes the relation

$$\beta_{i} = m_{i,j}\beta_{j} + b_{i,j}$$

These relationships provide the means of computing probabilities of profiles. Without them the joint distribution of the  $\beta$ 's must be known. However, even if this distribution were determined it is doubtful that it would have much meaning due to the insufficient number of data points. Therefore, the profiles will be characterized by the one parameter,  $\beta_3$ .

Before anything can be said about the probabilities of various profiles the distribution of  $\beta_3$  parameters must be known. The histogram of Figure 8 indicates the relative frequencies of the  $\beta_3$  parameters observed in this study. If it is assumed that this sample of parameters comes from a normal population,
### TABLE XIX

### CORRELATION AND LINEAR DATA FOR THE COEFFICIENTS OBTAINED FROM THE DIFFERENT DEGREE POLYNOMIALS

	b <sub>i,j</sub>	۴ b	m <sub>i,j</sub>	° m	L.C.C.	DEGRE
AFTAD VS PETAL	578155+01	.187565+30	-+127225+02	.9FA71 E+00	459	2
BETAS VE SETTS	774228+21	.5084F-11	* 76 * Q A T + C T	+87161F+92	.754	2
RETAL VS RETAR	•1500PE+05	•114005-02	<b>*</b> •66588⊑+02	.17039E+01	731	د
		.039495-01	871145+61	.458395+00	925	3
PEIAU VE PEIAS		265405-01	+24440F+C3	.20761F+02	. 842	3
NETAN VE PETAR	-, 020107411	275775-01	215745+05	.243055+14	- 753	3
DETAN VE DETAR	174315+55	172755-32	302995+92	10179E+01	367	3
AFTAL VS DETAR	196567+90	.159142-02	.27797E+04	17472E+03	.895	3
PETA2 VS DETA3	706165-03	• 2574 PE+ 34	953045+02	+26597E+01	-,977	3
			- 64,555454	.24(595+0)	964	4
BETAC VS PETAL	699957+91	+44/3/F+U1 749705-04		.956997+01	455	4
RETAR VS GETAR		• 313 342 UL . 487775-01	58691F+86	6C933E+03	728	4
HEING VS DEIRZ	- 837405+01	-567578+01	509215+05	877125+05	. 595	4
NETAU VS 1-104		248?85-12	20206E+C2	.74520F+00	951	4
12181 V5 12181 DETA1 V5 FETA7	205975400	501535-02	A44255+03	.63227F+02	.853	4
OCTAL VE DETAL	202135400	.656CSE-02	994355+05	.10093E+05	75%	4
AFTA2 VS BETAS	- RON27F-03	.11870E-07	453185+02	+149655+01	-,958	4
AFTAS VE DETEL	\$12295-23	.20541E-03	. 513765+04	.31756E+03	.901	4
RETAR VC DETAL	. 4 2 204F = 9 2	.201915-0 <del>5</del>	123245+03	.31663E+91	-,98J	4
		587545-04		.319975+00	912	5
BE FAR VS 73141	++721191+91 - 9975+5+04	•==2916=91 .400696=04	595965+51	745245+11	.715	5
HE FOUL VE DETAZ		.61174F=01	123855+64	.27883E+07	553	5
SETAD VS PETAL		.627977-01	.561575+13	.147075+05	.4.7	5
RETAS VE GETAG	914597+01	.67775-01	694365+07	.21522F+07	382	5
RETAL VE DETAD	.185077+00	.631275-02	127525+02	.64739E+00	930	5
PETAL VS OFTAR	.194365+70	.679995-02	.302076+03	.270075+02	.920	5
BETAL VE STAA	+175327+01	·79257E-02	149945+03	.100595+04	728	5
PETAL VS DETAS	·158707+00	.857488-0?	.105205+07	· 289382 +05	- 07A	2
BETAR VS DETAR	1307(F-03	.211508-03	26 1475+02	• 369135+00 77207E+02	9/0	5
PETA2 VS DETA4	FE4775-03	. 79185-07	.17747E+04	+//25/ETUZ	- 457	Ś
RETAR VS BETAR	116395-32	.425528-03	14/205+0h - 540495+0h	+ 1 H T H L T U D	994	ś
RETAR VS DETAL	-,242573-34	•55101t=05 041645-05	-,949932+62 .77107F106	**************************************	.950	5
HETAS VN PETAS BETAL VN PETAS	4/03/1-04 .410265-06	.798855-07	-,14391E+03	.26959E+01	989	5
						٤
RETAU VS DETAL	721252+01	.71653E-01	577158+01	*14294* *00	- 971	6
NETAD VS DETAP	437745+01	.133515+00	•73337E+E7	4 777545 FU1 . 4 7876 FAD 7	- 977	6
RETAD VS PETAR	#32007+01	+19:575+30	105972+04 E01007+07	·100702+03	.714	6
NETAG VE PETAG	- 43055549 <b>1</b>	•/>·/>·//•UU	+34004040702 	5 6686E + 06	542	6
HETED VS BETAN		+2997902700 . 798967103	U3437F+03	12993E+09	. 301	6
HETAU VN HETER Detai ve detag		12917F=01	13312E+02	34098E+00	941	6
SCINI VE SETAR	196717403	243575-01	.312105+03	.17283E+02	.915	6
AFTAL VS BETAL	196935492	366657-31	11544E+05	+111325+04	801	6
RETAL VS BETAS	176757+04	.4580 - 31	.703905+05	1C720E+06	•645	6
AFTAL VS DETAR	.15974F+03	F33587-01	02532E+0A	.21104E+09	490	6
BETAS VE DETAT	- , 5779003	094572-07	244465+02	.69874E+C0	973	6
BETAS VS DETAL	.115175-03	.233385-02	<b>.</b> 054385+03	·616475+02	.893	6
BETAS VS BETAS	.869525-63	.201855-07	61107F+C5	.57330E+04	- 1759	0 4
RETAR VE DETAG	+137165+02	.356135-02	. 85 2655 + 07	.140965+37	• 513	0 4
BETTER VE RETAL	100467-01	449245-04	413978+02	+135495991 +08702437		6
RETAR VS RETAR	461567-34	.855275+04	297355404	-140347700	759	6
HETAY VS PETAS		• 11 · 745 - 33	- 72072Ex 03	. 964002 - 32	-, 95 4	6
PETAL VE OFTAC	●437531-5K ●45763-55	+1)0255+05 48857E=0E	-+129122792	.746725+03	. 894	6
HELEN A. HELEN	• • • • • • • • • • • • • • •	•1	PTIM METUS		4.977	6



Relative Frequency

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Figure 8. Histogram of  $\beta_3$  Parameters.

then the maximum likelihood estimators of u and  $\sigma$  are given by  $\hat{u} = \overline{\beta}$  and  $\hat{\sigma} = S$  where  $\overline{\beta}$  is the sample mean and S is the sample standard deviation. The dashed curve of Figure 8 represents the normal distribution that the parameters would have if  $u = \overline{\beta}$  and  $\sigma = S$ . The chi-square test was used to determine the goodness of fit of the normal curve to the sample distribution. Essentially, the test compares the differences of the observed  $(n_i)$  and theoretical  $(e_i)$  frequencies to some limiting value  $\chi_0^2$ . Specification of the critical region and degrees of freedom k then determines  $\chi_0^2$ . If

$$\chi^{2} = \sum_{i=1}^{N} \frac{(n_{i} - e_{i})^{2}}{e_{i}} > \chi_{0}^{2}$$

the hypothesis that the parameters were sampled from a normal population is rejected. The degrees of freedom are found from  $k = N-1-\ell$  where N is the number of cells used in constructing the histogram and  $\ell$  is the number of unknowns (i.e., u and  $\sigma$ ). Hence,  $\chi_0^2 = 15.5$  for 8 degrees of freedom (11 cells) and critical region 0.05. The particular values used in computing  $\chi^2$  are listed in Table XX. Calculations show  $\chi^2 = 15.1$  indicating that the sample data might well come from a normal population. It is therefore assumed that the  $\beta$ 's are normally distributed with maximum likelihood estimators  $\hat{u} = \overline{\beta}$  and  $\hat{\sigma} = S$ .

### 3.5 Derivation of Model

The results of the previous section can now be utilized to derive the equation necessary to complete the atmospheric model. The final model was based on the hi linear correlation existing between all pairs of  $\beta$ 's. Each  $\beta$  of Equation (1) was replaced by the corresponding linear relation in  $\beta_3$ . The particular choice of using a third degree polynomial in fitting the data was based on the quadratic appearance of the log profiles for pressure. It turns out, as will be shown, that

TABLE XX

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CHI-SQUARE TEST FOR NORMALITY OF  $\beta^{\,\rm I}S$ 

Cell Boundries B	<u>B - 0.20</u> 0.94 t	Accumulative Cell Area Left of t A	Cell Area Lef: of t AA	Theoretical Frequency e <sub>i</sub>	Observed Frequency n <sub>i</sub>
-1.8	-2.13	0.0166	0.0166	1.1	2
-1.4	-1.70	0.0446	0.0280	1.8	2
-1.0	-1.28	0.1003	0.0557	3.6	2
-0.6	-0.85	0.1977	0.0974	6.2	2
-0.2	-0.43	0.3336	0.1359	8.7	12
0.2	0.00	0.5000	0.1664	10.7	14
0.6	0.43	0.6664	0.1664	10.7	12
1.0	0.85	0.8023	0.1359	8.7	4
1.4	1.28	0.8997	0.0974	6. 2	9
1.8	1.70	0.9554	0.0557	3. 6	3
2.2	2.13	0.9834	0.0280	1.1	5

Equation (1) can be factored into two components, one of the components containing a quadratic. Any polynomial of degree different from 3 cannot provide a quadratic component.

The two fundamental components of the model will now be derived and each discussed in the following two sections. To do this Equation (1) must first be rewritten in a form consisting of two factors. The linear relations given by Equation (5) for  $\beta_0$ ,  $\beta_1$ , and  $\beta_2$  as functions of  $\beta_3$  are first substituted into Equation (1). All terms in  $\beta_3$  are grouped together and expressed as one factor. Thus,

$$P = \exp[b_{0,3} + m_{0,3}\beta_{3} + (b_{1,3} + m_{1,3}\beta_{3})z + (b_{2,3} + m_{2,3}\beta_{3})z^{2} + \beta_{3}z^{3}]$$

$$= \exp[b_{0,3} + b_{1,3}z + b_{2,3}z^{2} + \beta_{3}(m_{0,3} + m_{1,3}z + m_{2,3}z^{2} + z^{3})]$$

$$= \exp[b_{0,3} + b_{1,3}z + b_{2,3}z^{2}] \cdot \exp[\beta_{3}(m_{0,3} + m_{1,3} + m_{2,3}z^{2} + z^{3})]$$
(6)

The two components on the right hand side of Equation (6) form the basis of the model. The unit for  $\beta_3$  is km<sup>-3</sup>.

### 3.5.1 Steady State Model

The first factor on the right hand side of Equation (6) consists only of the constants  $b_{0,3}$ ,  $b_{1,3}$ , and  $b_{2,3}$ . Hence, it is time invariant and will hereafter be referred to as steady state pressure, denoted P(z). The particular values of the b's can be found in Table XIX under degree 3. It is interesting to note that the functional values of P(z) are very close to those of the 1962 standard pressure. This fact will be discussed later in Section 3.6.

The above definition of steady state pressure provides the means for deriving density and temperature steady states. This is accomplished by assuming that the hydrostatic and gas laws are applicable under steady state conditions (i.e., quiet atmosphere). Therefore, the following three equations

define a steady state atmosphere. The steady state pressure is given by

$$P(z) = \exp[b_{0,3} + b_{1,3}z + b_{2,3}z^{2}] ; \qquad (7)$$

steady state density by

$$\rho(z) = \frac{100}{g(z)} [b_{1,3} + 2b_{2,3}z] \exp[b_{0,3} + b_{1,3}z + b_{2,3}z^2] ; \qquad (8)$$

and steady state temperature by

$$T(z) = \frac{3.48385g(z)}{b_{1,3} + 2b_{2,3}z}$$
(9)

The units are the same as those defined in Sections 3.2.1, 3.2.2, and 3.2.3.

### 3.5.2 Perturbation Model

The second factor on the right hand side of Equation (6) is defined to be the pressure perturbation function, denoted  $P(\beta_3, z)$ . The function describes deviations from steady state in terms of the one parameter  $\beta_3$ . The corresponding values of the slopes  $m_{0,3}$ ,  $m_{1,3}$ , and  $m_{2,3}$  are listed in Table XIX under degree 3. The behavior of this function is discussed in Section 3.6.

The definitions of steady state functions combined with the hydrostatic and gas laws provide the means of deriving perturbation functions for density and temperature. The hydrostatic law is first applied to Equation (6) after which the steady state density is factored out. The factor that remains is defined to be the density perturbation function. These definitions then imply that the temperature perturbation must be the ratio of the pressure and density perturbations. This is easily proved by noting that both pressure and density are factorable into the product of steady state and perturbation functions. The equation of state then produces the desired result. Therefore, the density

factorization is accomplished as follows

$$\rho = \frac{100}{g(z)} \frac{dP}{dz} = \frac{100}{g(z)} \left[ P(\beta_3, z) \frac{dP(z)}{dz} + P(z) \frac{dP(\beta_3, z)}{dz} \right]$$

$$= \frac{100}{g(z)} \frac{dP(z)}{dz} \left\{ P(\beta_3, z) + \left[ \frac{P(z)}{dP(z)/dz} \right] \left[ \frac{dP(\beta_3, z)}{dz} \right] \right\}$$

$$= \rho(z) \left[ P(\beta_3, z) + \frac{\beta_3 (m_{1,3} + 2m_{2,3}z + 3z^2)}{b_{1,3} + 2b_{2,3}z} P(\beta_3, z) \right]$$

$$= \rho(z) \left[ 1 + \frac{\beta_3 (m_{1,3} + 2m_{2,3}z + 3z^2)}{b_{1,3} + 2b_{2,3}z} \right] P(\beta_3, z)$$

$$= \rho(z) \rho(\beta_3, z) \cdot \cdot$$

The temperature factorization is immediate.

$$T = 348.385 \frac{P}{\rho} = 348.385 \frac{P(z) \cdot P(\beta_3, z)}{\rho(z) \cdot \rho(\beta_3, z)}$$
$$= T(z) \cdot \frac{P(\beta_3, z)}{\rho(\beta_3, z)} = T(z) \cdot T(\beta_3, z)$$

The perturbation functions are therefore defined by the following equations. The pressure perturbation is given by

$$P(\beta_3, z) = \exp[\beta_3(m_{0,3} + m_{1,3}z + m_{2,3}z^2 + z^3] ; \qquad (10)$$

the density perturbation by

$$\rho(\beta_{3},z) = \left[1 + \frac{\beta_{3}(m_{1,3} + 2m_{2,3}z + 3z^{2})}{b_{1,3} + 2b_{2,3}z}\right] \exp[\beta_{3}(m_{0,3} + m_{1,3}z + m_{2,3}z^{2} + z^{3}]$$
(11)

;

and the temperature perturbation by

$$T(\beta_{3},z) = \frac{1}{\left[1 + \frac{\beta_{3}(m_{1,3} + 2m_{2,3}z + 3z^{2})}{b_{1,3} + 2b_{2,3}z}\right]}$$
(12)

The perturbations have no units. The model is now complete and consists entirely of the steady state and perturbation functions along with the distribution of  $\beta_3$  parameters.

### 3.6 Properties of Model

The perturbation profiles defined by the largest positive and negative  $\beta_3$ parameters (Flights 26 and 48) observed in this study are shown in Figure 9. The general perturbation function is denoted by the symbol  $\lambda$ . The parameters define envelopes which contain all perturbations determined from the  $\beta_3$ 's. This fact is easily verified since the cubic argument of  $P(\beta_3, z)$  has three real roots independent of  $\beta$ . These roots correspond to the altitudes at which  $P(\beta, z) = 1$ . The maxima and minima points of the perturbation are identical to those of its argument but are not independent of  $\beta$  in the sense that negative  $\beta$ 's reverse the roles of these points. Therefore, the maximum point for positive  $\beta$ 's becomes the minimum point for negative  $\beta$ 's and vice versa. As  $\beta$  approaches zero the profiles tend to flatten out and approach a limiting value of 1.

The density envelope is similar in some respects to that of the pressure envelope but differs both in the maximum and minimum amplitudes and the length of the overlapping profiles (i.e., the distance between the two extreme points at which  $\lambda(\beta_3, z) = 1$ ). Also, the envelope lags the pressure envelope by 8 kilometers. The structure of the temperature envelope is entirely different from that of the other envelopes but this is to be expected since it is determined by the ratio of pressure and density perturbation.





It is interesting to note that the perturbation model controls the behavior of the atmosphere. The model shows that the upper atmosphere is highly dependent on the perturbations occurring in the lower regions. The central portion is affected to a much lesser extent. The deviations in this range are within 10% of the steady state.

The effects of the perturbations on the steady state atmosphere are best illustrated by the plots shown in Figures 10 through 24. The ratio of steady state pressure to that of the 1962 standard pressure is plotted in Figure 10 for Flight 1. This profile is represented by the dotted curve. The dashed curve shows the effects of the pressure perturbation on steady state. This profile is determined by the product of steady state ratio and pressure perturbation. The observed ratio (pressure values are listed in the appendix) is represented by the solid curve. Similar plots for density are shown in Figure 11. Temperature profiles are plotted in Figure 12. The remaining figures are similar plots for Flights 26, 48, 50, and 63. The rationale for choosing Flights 1, 50, and 63 in illustrating the effects of perturbations on steady state has been explained in Section 3.3. Flights 26 and 48 were included since the largest and smallest  $\beta_3$ 's were observed for these flights. In general, the agreement between observed and calculated profiles is quite encouraging.

Probabilities of profiles are computed by specifying  $\beta_3$ . The most likely profiles corresponding to the parameter  $\overline{\beta}_3 = 0.0000023$  are within 1% of steady state. Sixty-eight percent of the parameters are expected to lie within one standard deviation (S = 0.0000092) of the mean. The perturbation envelopes defined over this range are plotted in Figure 25. The question of whether or not the observed profiles actually fall within these envelopes is partially answered by inspection of Table XXI. The model predicts that when  $\beta_3$  is within  $1\sigma$  of the mean  $\overline{\beta}_3$  then the other parameters  $\beta_0$ ,  $\beta_1$ , and  $\beta_2$  are also within  $1\sigma$  of their means.



Figure 10. Observed, Calculated, and Steady State Pressure Ratios for Flight 1.

























Figure 17. Observed, Calculated, and Steady State Density Ratios for Flight 48.



Figure 18. Observed, Calculated, and Steady State Temperature For Flight 48.













Figure 22. Observed, Calculated, and Steady State Pressure Ratios for Flight 63.











Figure 25. Perturbation Envelopes for  $\beta$ Parameters Within  $l\sigma$  of Mean.

The sample means and standard deviations are computed as

$$\overline{\beta} = \frac{1}{N} \sum_{i=1}^{N} \beta_{i}$$

and

$$S^{2} = \frac{1}{N-1} \sum_{i=1}^{N} (\beta_{i} - \overline{\beta})^{2}$$

respectively, where N is the sample size and  $S^2$  is the standard deviation squared. The functional means and standard deviations are computed through Equations (5) as  $\overline{\beta}_i = b_{i,3} + m_{i,3}\overline{\beta}_3$  and  $\sigma_{\beta_i} = m_{i,3}\sigma_{\beta_3}$ , respectively. The standard deviations predicted by the model are in general lower than those of the samples. Certain of the flights are therefore expected to have profiles lying partially or totally outside the  $1\sigma$  envelope of Figure 25. However, the percent deviations in these cases are expected to be very low (i.e., the relative deviations from the envelope).

### TABLE XXI

### COMPARISON OF SAMPLE AND FUNCTIONAL MEANS AND STANDARD DEVIATIONS

Parameter	Sample Mean	Functional Mean	Sample Standard Deviation	Functional Standard Deviation
β <sub>0</sub>	-8.33451	-8.33480	0.26793	0.19958
β1	0.20294	0.20296	0.02857	0.02520
β <sub>2</sub>	-0.000924	-0.000926	0.000908	0.000879
β3	0.0000023	0.000023	0.0000092	0.0000092

### 4. MODEL CONSTRUCTION\*

The construction of an atmospheric model based on the findings of this report is easily and quickly accomplished. The first step is to generate a data base containing all the necessary information needed to build the model. To do this one would have to keypunch the data (e.g., the data listed in the appendix) onto cards and code a program that transfers this information to magnetic tape. Now that the data is stored on tape it is a relatively simple task to code a program for generating  $\beta$  coefficients. The program would first compute the logs of all pressure data for each flight and then use a least squares routine to fit a polynomial to the data.

Once the  $\beta$ 's are determined a linear least squares program computes the slopes and intercepts of all pairs of coefficients. The model is then developed as described in Section 3.5.

<sup>\*</sup> The computer program that performs all the necessary operations is located at Huntsville, Alabama.

### 5. CONCLUSIONS AND RECOMMENDATIONS

Atmospheric models are described in this report as the product of steady state and perturbation functions. This concept is very useful both for analysis and computer purposes. It allows one to compute the probability of a given profile where each profile of pressure, density, and temperature is completely specified by one parameter. The parameters are normally distributed with mean 0.0000020 and standard deviation 0.0000094.

The perturbation profiles indicate that large fluctuations from steady state at high altitudes greatly affect what happens at the lower altitudes. For example, positive deviations from steady state pressure at altitudes greater than 87 kilometers correspond to negative deviations in the region less than 53 kilometers. The central region is effected to a much lesser extent. The magnitudes of such deviations are controlled entirely by the distribution of parameters used in the development of the model. The fact that 68% of the parameters are within one standard deviation of the mean indicates that the atmosphere over the altitude range 90 to 50 kilometers is close to a steady state condition most of the time.

A useful feature of the model lies in the fact that if the structure of the pressure perturbation is known then the density and temperature perturbations are completely specified. Therefore, expected deviations from the steady state model can be computed at each altitude.

The limitations of the model depend heavily on the results of Section 3.4. The distributions and interrelationships of the parameters were determined regardless of location or time of year. This fact might well have been the controlling factor in the resulting correlation of  $\beta$ 's. For example, if the sample data had been obtained from one location only the correlation coefficients

would be expected to increase. Furthermore an additional increase in correlation is expected for those  $\beta$ 's taken from the same months or seasons. If these changes do occur it is quite possible that the b's and m's of Equation (5) will change accordingly. Therefore, it is highly important that extreme care be taken in correlating parameters.

One further comment on the model is in order. The particular choice of the third degree polynomial in constructing the model is not necessarily the optimum. In fact, some of the profiles are better explained by polynomials of higher degree. However, as Table XIX shows, the correlation coefficients are generally lower in these cases.

It is recommended that future work be concerned with modifications of the existing model. Specifically, updating of the model should include:

(1) Updating the data base to include more data from specific locations such as Cape Kennedy and Vandenberg.

(2) Extending the model to describe the atmosphere in the altitude range from 40 kilometers to the ground.

(3) Validating the mathematics of the model. In particular, investigating the effects of fitting data in terms of the variable z = 80-Z instead of 100-Z. If appreciable changes are noted, it might be feasible to generalize the fitting variable to arrive at the optimum solution.

(4) Investigating the possibilities of using polynomials of degree higher than three.

### 6. REFERENCE

Luers, James K., "A Method of Computing Winds, Density, Temperature, Pressure, and their Associated Errors From the High Altitude ROBIN Sphere Using an Optimum Filter", Final Report, Contract No. F19628-67-C-0102, University of Dayton Research Institute, Dayton, Ohio, July 1970. APPENDIX A

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TABLE XXII

# TAB PRINT-OUT OF DENSITY

A DEP CHRIC METERS

					DENSITY II	N GRAMS FE	K CUDIC W					
FLIGHT NO. Altitude	Ţ	2	<b>8</b> 7)	t	S	ور	2	æ	σ	10	11	12
			F 1000	0.000		00054	- 00031		.00045	.00053	.00051	.00053
100	4400 <b>0</b> .					.0006	00038		.00055	.00063	.00063	.00062
66	.01054	3 . n n n n .				00077	01000		.00069	.00075	.00078	•00072
98		29003.	84nnn.				54000		.00082	-00087	• 0 0 0 8 e	.00082
97	.00091	96000.	• 00080						70000	.00101	.00122	82000.
96	.00106	.C0111	.0000	•000 <b>•</b> 0					.00116	.00120	00148	.00115
95	.00125	.0130	.00115	.00122		07100.				-00142	.00178	.00139
46	.00147	.00152	.00140	.00147			10100.			0.171	.00212	.00167
53	.00175	.00178	.00171	.00175		.0010/	291.00 *			70200	.00250	.00203
26	.00203	.0209	.00207	.06207		.0200	5510 <b>0</b> .			00050	00299	.00255
16	.00239	.00247	.00260	.00242		.00200	11111			.00111	01349	.00311
06	.00282	.00295	.00327	.00285			00364		00335	.0331	.00411	.00385
69	.00335	.00351	.00403	.00335		05000.	10000		E0700 -	.00462	.00481	.00467
88	.00403	.60412	• 0 0 2 0 4					00512		.00561	.00561	.00567
87	e 7 4 0 0 .	.00454	.00622	• 0 0 4 7 9		.0000.		21230	00642	.00675	.00675	.00682
96	.00569	.0576	.00761	.06582		*~~~		33200	00706	.00811	.00303	.00819
85	.00676	.00676	.00931	.00708		. 00 8 2 9 4 9 4 9 4 9 4 9 4 9 4 9 4 9 4 9 4 9					.00966	.00985
3 6	. 30803	•C0794	.01128	.00870		.01033	.0000	61600.			.01173	.01173
83	.03956	<b>6860].</b>	.01357	.01058				CTTT0.	01285	11768	01410	.01396
82	.01189	.01133	.01631	.01299		.01465	2071 <b>0</b> .			01612	01679	.01662
81	.01396	.01363	.01911	.01579		.01762	6741N.	62010.		01800	.01999	.01959
	.01679	.01619	.02239	.01879		.02059	51910.	+ U I Y 7 Y	- 1 - 1 - 1	02200	02372	.02302
52	.02020	.01373	.02584	. 12255		51320.		. ULUCO	.02475	.02530	.02777	.02667
78	.02392	.02365	.02942	.02667		CU02U.		. 13210	.02857	.02569	.03146	.02985
11	.02761	.62925	.03338	8/100.			01250	.13661	.03213	.03176	.03437	.03325
76	.03138	.03288	.03661	00/00			.03001	04118	.03641	.03425	.03815	.03641
75	.03555	.63771	26240 .			. 04564	.04915	.04514	.04112	.03611	<b>.</b> 04463	.04163
74	.04163	.04263	C10C0.	. U4 5C7		05382	.05092	.05150	.04687	.04051	.05208	.04/45
73	.04919					.06260	.05993	.06060	.05461	.04728	.06193	.05554
72	.05860	12/63.				.07415	.07033	.07033	.06498	.05657	.07568	.06650
71	. 3630.3					09403	.08316	.08491	.07703	.06553	•08929	0/0/0.
70	.07265	045/0°				00760	.09500	.09500	.08800	.07500	.10300	.09200
69	00620.	00,00				10829	.10829	.10715	.09689	.09347	.10829	.10373
68	.08777	.09639	12423	• • • • • • •		12575	.12575	.12316	.11149	.11668	.13612	.12316
67	.10371	.11279	61141.			14566	14713	13830	.12653	.14419	.15890	.13977
66	.12947	17621.	.1/06/			46665	17165	15998	.14165	.16665	.17165	.15665
65	.15332	.14998	.19498	.10448		* 70007	10025	18084	.16011	.18460	.19214	.18054
<b>6</b> 4	.18460	.17330	. 22228	.15512		. 1077	22102	20614	.18064	.21252	.23377	.21677
63	.21339	1461.	. 25077	- ZUDI-			25428	22974	.20561	.24170	.24649	16662.
62	.23692	.22734	. 29195	• 2 3 2 1 3						1		

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TABLE XXII (Continued)

# TAB PRINT-OUT OF DENSITY

### DENSITY IN GRAMS PER CUBIC METERS

	12	.27839	.30286	.33902	.35086	.41474	.47274	26245	.65662	.75291	.82500	.93411	1.07824	1.19768	1.31670	1.48153	1.71410	2.00563	2.23631	2.65088	3.05470	3.42164	3.75596	4.44163	5.58126							
	11	.29731	.32733	.37016	.39086	.46327	.50260	.55514	.68819	.77422	.87306	.99759	1.10905	1.22094	1.36937	1.69104	1.85123															
	10	.27569	.31204	.34940	.37132	.42356	.47274	.52150	.59960	.66057	.76893	.87062	.98582	1.11629	1.18503																	
	σ	.23785	.27533	. 30789	.35568	.40591	.45781	.52150	• 59349	.70319	.77694	.90690	.9960	1.00140	1.26403	1.51146	1.73124	1.96630	2.30408	2.62489	3.08464											
	æ	.26755	.30898	.35978	.40259	.46327	.53245	.58318	.64400	.73870	.86505	.99759	1.19120	1.31396	1.48787	1.69104	1.83409	2.14327	2.52997	2.88479	3.35418	3.76748	4.27540	5.18190	6.11792	6.92140						
	~	.27569	.32122	.35632	.40649	.46327	.51752	.59439	.69451	.77422	.88107	1.00666	1.16040	1.29071	1.43520	1.69104	1.95407	2.18259	2.48479	2.80631	3.35418	3.69835	4.55510									
	ъ	. 24860	.28145	.31481	• 35 95 3	.40150	.47772	.52710	.66294	.73160	.82500	.94318	1.06798	1.20931	1.40887	1.63119	1.83409	2.12360	2.37184													
1	10		.29980	.34940	.43649	.45886	.52250	.58319	.64400	.73870	. A 25 0 0	.94318	1.06798	1.25582	1.43520	1.63119	1.93693	2.19259	2.46223	2.72884	3.02475	3.56009	4.23544	4.59684	5.84959	6.73434						
	t	.26758	.30898	.35276	.40259	.46327	.53743	.60561	.68188	.76711	.85764	.96131	1.08851	1.27908	1.40887	1.64615	1.86837	2.14327	2.41702	2.72884	3.20444	3.76748	4.27540	4.90430	5.68860	6.60963	7.91111	9.14047	10.77727	12.26738	13.82610	10.73952
	P)	. 32974	.38852	.42551	.49467	.55151	.62700	+6094 *	.78921	.88785	.96917	1.07014	1.17067	1.27908	1.49887	1.61622	1.83409	2.14327	2.55256	3.04071	3,50392	4.00942	4.63501	5.36697	6.22526							
	2	.25406	.28451	.31135	.33614	.37944	.44238	48224	.56923	•63216	.71285	.76180	.90367	1.63489	1.18503	1.36191	1.57697	1.82966	2.16854	2.46395	08466.2	3.52553	4.11557	4.85803	5.79593	6.36021	7.40306	8.97120	10.28290	11.57300	13.82610	
	4	.26487	.29674	. 32964	.36350	.41033	.47274	.53271	.60612	.69608	.77694	.87062	.9960	1.11629	1.27720	1.46657	1.62833	1.86798	2.05560													
	FLIGHT NO. Altitude	61	60	59	58	57	56	55	54	53	52	51	50	67	81	47	4 Q	45	11	£ 7	42	41	t 0	39	36	37	36	35	34	33	32	30

TABLE XXII (Continued)

# TAB PRINT-OUT OF DENSITY

### DENSITY IN GRAMS PER CUBIC METERS

FLIGHT NO.	13	14	15	16	17	18	19	20	21	22	23	24
ALTITUDE												
100	.00050	.00049		.00050	.00050	. 00 04 0	.03050	.00050		.00034		.00066
66	• 0 0 0 5 4	.00060		.00060	.03060	.01050	.00063	.00065		.00052		.00074
98	.00063	.00073		02000.	.00070	.00360	.00030	.00081		.00071		.00087
16	.00077	.00088		05000*	06000 *	.00080	.00100	<b>86000</b> .		06000*		.00102
96	• 0 0 0 0 4	.0103		.00100	.00110	.00100	.00120	.00121		.00112		.00120
95	.00109	.00119	.00116	.00130	.00140	.00120	.00150	.00147		.00139		.00139
64	.00125	.00133	.00139	.00150	.00160	.00160	.00190	.00175		.00168		.00163
53	.00146	.0157	.00164	.00180	.00190	.00190	.00229	.00212		.00192		.00190
92	.00173	.00175	.00182	.00209	.00231	.00231	.00269	.00254		.00224	.00203	.00224
91	.00208	.0208	. 0 C C C C C C	.00239	. C 32 7 D	.00281	.00320	• 00307		.00260	• 0 0 2 4 4	.00262
06	.00254	.0250	.09231	.00288	. 60320	.0330	.00371	.00365		.00301	• 0 0 2 9 <del>8</del>	.00307
89	.00324	.06309	.00278	.00358	.05377	.00389	.00419	.90438		.00358	.00362	.00354
88	.00417	.00389	.00348	6 7 7 0 0 *	67+00*	.0045A	66700 *	.00527		.00426	• 00435	.00412
87	.00523	06403*	.00457	.00572	.00528	.00539	.00578	.00638		.00517	.00517	.00473
86	.00645	.0009	.00589	.00728	.03629	.00642	.00682	.00768		.00662	.00668	.00589
85	.00795	.00756	.00732	.00931	07740	.00740	.00811	.00923		.00756	.00748	.00636
91	.00947	.60318	.0308	.01167	. 60880	.00880	.00956	.01119		•000 <b>•</b>	•00899	.00755
6.3	.01115	•01115	.01092	.01461	.01047	.01035	.01150	.01345		.01069	.01069	.00857
82	.01327	.01327	.01285	.01783	• 6 1244	.01230	.01368	.01603		.01285	.01299	.01092
81	.01546	.01562	.01496	.02144	.01463	.01463	.01662	.01911		.01546	.01546	.01330
90	.01799	.01819	.01739	.02539	.01719	.01739	.01999	.02259		.01839	.01839	.01619
79	.02114	.02114	.02020	.02889	• 0 2 0 4 4	.02067	.02349	.02631		.02208	.02185	.01973
78	.02447	.02365	.02310	.03245	.02392	.02420	.02750	.03025		.02640	• 02585	26220.
77	.02957	.02729	.02632	.03531	. 62793	.02825	.03210	.03370		.03146	64020*	.02889
76	.03285	.(3138	• 02989	.03773	.03250	.03288	.03661	.03661		.03773	.03587	- 0 3 4 3 7
75	.03685	.03598	.03381	.04118	• 03728	.03771	• 04 075	• 03945	996£0 *	<b>.042</b> 92	• 0 4 5 0 5	61040.
74	.04012	.04062	.03711	.04814	.04163	.04213	.04564	.04463	• 04413	.04564	.04764	.04564
73	.04629	.04529	.04398	.05613	.04687	.04861	• 05208	.05208	.04919	.05092	.05324	- 05092
72	.05194	.05128	.05327	.06593	.05594	.05594	.05993	.06260	• 02 794	.05927	.06193	.05993
11	.06039	.05896	.06650	26220.	.06727	. 16574	.07186	.07797	.06880	.07186	.07186	-07033
70	. 07440	.07178	.09316	.08753	.0316	.07703	.08316	.09541	.08403	.08578	.08491	.08666
69	.09200	.0200	00860 *	00660.	.09600	.08700	.09500	.10800	00260 .	.09300	.09300	00660.
68	.11057	.11285	.13487	.11399	.10943	.09917	.11057	.12083	.10601	.10259	.10031	.10715
67	.12575	.12316	.12057	.13094	.12964	.11408	.13094	.13742	.12316	.11797	.11408	.12057
66	.14566	.14419	.13683	.15154	.14566	.13095	.15596	.15449	.13977	.13242	.13389	12621.
65	.16498	.16498	.15998	.17332	.16832	.15332	.18165	.17832	.15998	.14665	.15498	.15332
<b>6b</b>	.19214	.18272	.18649	.19779	.19779	.17895	.21286	.20721	.18272	.16765	.17518	.17330
63	.21252	.20627	.20614	.22740	.21890	.20402	.23377	.25077	. 21252	.18489	-20402	.20827
29	. 24649	•22256	.23452	.25367	.24410	.23452	.26803	• 29674	.23692	.21777	.23692	.21538

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TABLE XXII (Continued)

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# TAB PRINT-OUT OF DENSITY

### DENSITY IN GRAMS PER CUBIC METERS

54	4 4 4 5 5 5 5 5 5 5 5 5 5 5 5 5
23	809779999999999999999999999999999999999
22	<ul> <li></li></ul>
21	● / / / / / / / / / / / / / / / / / / /
20	84000000000000000000000000000000000000
19	80000000000000000000000000000000000000
18	44 45 45 45 45 45 45 45 45 45
17	2000 2000 2000 2000 2000 2000 2000 200
16	• 22 • 22 • 22 • 22 • 22 • 22 • 22 • 22
15	90000030000000000000000000000000000000
4	$\begin{array}{c} 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 $
13	44444700000000000000000000000000000000
FLIGHT NO. Altitude	ႧႧႧႧႧႧႧႧႧႧႧႵႵႵႵႵႵႵႵႵႵႵႵႵႦჿႦႦႦႦႦႦႦႦႦ ჃჿႧჾჁႧႧႵႦჿႧႧႦႧႦႦႦႦჿჿჂჿႦႦႦႦႦႦႦႦ

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### TAB PRINT-OUT OF DENSITY

#### DENSITY IN GRAMS PER CUBIC METERS

FLIGHT NO. Altitude	55	26	27	28	53	30	31	32	S S	34	35	36
100	.00060		• 00047 • 00057	.00055 .00066	• 00065 • 00076		.00060	.00062 .00075	.00062 .00073			
86	.00081	*****	.00065	•00019	.00087		.00083	• 00089	.00085		.00062	
76	• 00096	.00082	.00081	*0000*	. 00398		.00096	.00102	66000 .		• 00086	
<b>P</b> 1	• 00113	.0104	16000.	.00113	.07111	.00117	.00111	.00116	.00117		.00108	.00105
47 1	• 0 0 1 0 4	.00185	. 1115 	.00157	421CD •	.00135	.00128	.00133	.00138		.00127	• 1 1 1 S
• •	. 00180	- C C C C C	• 00174C	• 0 0 1 C 0	• 101 44	10100 ·	54100 ·	• 00104	20100.			04100 ·
26.	.00224	01274	P0200 .	.00239	.00203	-00230	60200 ·	.00214	00220		.00183	.00205
16	.00265	.00286	.00262	.00289	.00244	.00272	.00250	.00256	.00261		.00215	.00245
06	.00317	.00301	.00327	.00343	.03297	.00318	.00300	• 00306	.00311		.00264	•00564
69	.00373	.60331	.00400	.00406	.00365	.00374	.00358	.00363	.00367		.00330	.00352
88	• • • • • •	.00389	.00490	.00482	• 03440	• 00440	.00427		.00436		.00406	.00431
87	.00528	.00501	.00589		.00532	.00515	.00505		.00515		•00+66	.00523
86	.00662	.0622	.00705		.00631	.00600	.00593		.00607		.00612	.00637
<b>9</b> 2	.01732	.60795	.00843		.00745	.00698	.00698		• 00 7 0 9		.00745	.00775
3 ( 60 (	.00870	.01042	• 00995		.00882	.00810	.00816		.00824	.00608	00600 .	12600.
50	.01023	.01334	.01161		. 61037	.00942	.00945	• 00925	.03951	•00694	.01075	.01141
82	.01202	.01548	.01354	.01386	. 61224	.01096	.01089	.01074	.01093	.00782	01280	.01379
81	.01413	.01762	.01562	.01647	.01434	.01287	.01243	.01240	.01245	.00888	.01513	.01656
	.01539	.61939	• 01799	.01965	.01646	.01503	.01419	• 01422	.01414	.01014	.01781	119610.
67	.01926	.02185	.02067	.03625	.01953	.01754	.01618	•01624	.01599	.01155	10120.	
87	.02227	.02420	.02365	.12674	11220.	44020.	.01840	.01835	.01810.	.01523	• 1 5 4 7 5	94/20.0
			• UC/ C3	•U3U69		10000	000700	10020		10110.	1.070	97220
9,2	.02561	. 0 4 4 0 0	. 03101	.U3376 n7800	• U/044	- U / / 85	, 02730	• U 2 2 4 6 - N 2 4 9 7	. U2221	• 1 1 1 4 4 0 2 0 1 0	.03817	
e / -	.03661		.04213	.04714	.03496	.03769	.03252	.02864	.02774	02388	.04432	.04733
73	.04166	.05266	.04919	.05660	.04326	.04376	.03915	.03535	.03302	.02933	.05239	.05352
72	<b>16610</b>	.06260	.05794	.06867	.05351	. 05 009	.04737	.14485	.04162	.03686	.06232	.DE189
71	.05962	.07874	.06803	.07923	.06559	.05909	.05853	.05656	.05352	.04585	.07324	•02424
70	.07265	.09016	.08141	.09167	.07800	.07015	.06912	.06965	.06686	.05688	.08859	.05191
69	00060.	.11100	.09700	.10607	.08694	.08538	.08456	.08481	•08209	.07176	.10116	.10431
68	.10373	.12381	.10943	.12066	.09757	.09787	.10159	.10026	.10079	.08939	.11537	.11806
67	.11927	.11927	.12834	.13721	.11295	.10931	.11374	.11581	.11408	.10544	•13379	.13682
66	.13536	.15743	.14713	.15918	.12783	.12803	.13018	.13521	.13042	.12394	.14593	.15846
65	.15832	.18165	.16998	.17284	• 14402	.14976	.15295	•14934	.15167	.14742	.16653	.17759
64	.19402	.19025	.19967	.19287	.16315	.17300	.17326	.17329	.17357	.16956	.18560	.19590
63	.22102	.24015	.22102	.22821	.18228	.20048	.19652	.19488	• 10 404	.19312	. 22993	• 22238
29	.25128	.24410	. 25367	.25425	.21334	.23295	. 22606	.22130	.21534	.22017	. 26436	.25251

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### TAB PRINT-OUT OF DENSITY

DENSITY IN GRAMS PER CUBIC METERS

GHT NO. TIFUDE	25	Ś Ż	27	2 G	62	30	31	2 £	33	すり	35	ч С
	.29920	.26758	.28650	.30050	.24316	.26307	.24354	. 25172	. 23876	.24284	.30941	.28707
	.32428	.32122	.32429	.32212	.25834	.30597	.27845	.26812	.26524	.27242	.34358	. 32922
	.35632	.33902	.38053	.38552	.30971	. 33558	.31850	.32484	.30544	.30720	-33034	.37458
	.39086	.43776	.41822	43964	.34762	.38522	.36389	.35611	.34736	.34694	62404.	.40926
	. 45445	.47209	.47651	.47144	.34914	16;24.	.40317	.39711	.39511	.39702		.46787
	.49762	.52250	.52748	.58297	.45198	.50759	.45602	.45608	.46314	.45607	.50680	.53198
	.55514	.57196	.58318	.55073	.51237	.57017	.52989	.53154	.51012	.50574	.57427	.60864
	.61374	.69451	.66294	.71194	• 58649	. 64 84 1	.59911	.58587	.57585	.58039	.64035	.67157
	.67478		.76711	.79984	.67007	.74986	.69734	.64574	.65217	.62901	.70369	.77656
•	.75291		.86505	.91877	.78825	.83438	.73512	.75663	.74750	.72308	.80313	.87756
_	. 36155		.97038	.93857	.88638	.94148	.86743	.84720	.85367	.83458	.96123	1.01027
~	.98582		1.16040	1.11816	1.01901	1.08.352	.97209	.96656	.97648	.92814	1.09804	1.14701
~	1.05303		1.31396	1.26126	1.14235	1.20473	1.15498	1.12191	1.10737	1.05890	1.26690	1.36896
_	1.25086			1.47633	1.27758	1.42198	1.34803	1.34703	1.29758	1.21838	1.45428	1.50037
	1.51146			1.64753	1.46139	1.59483	1.58904	1.50592	1.48421	1.41907	1.68261	1.65378
_	1.66268			1.86875	1.67083	1.85.257	1.73994	1.67821	1.67857	1.63439	1.96492	1.85139
	1.92697			2.22621	1.93025	2.09146	1.99590	1.93911	1.97327	1.89812	2.27789	2.10562
	2.19113			2.61802	2.12617	2 . 35 / 95	2.26625	2.25938	2.23662	2.21127	2.60882	
	2.62483				2.47127	2.66 541	2.59267	2.55555	2.62836	2.51178		
	3.17449				2.87174	2.97463	3.01084	3.02924	2.93480	2.85738		
					3.42512	3.46454	3.51067	3.40418	3.37455	3.42128		
					3.91296	3.92870	4.07164	3.99021	3.97129	3.91291		
					4.64674	4.69253	4.61199	4.51380	4.57667	4.50359		
					5.51468	5.30539	5.31370	5.26096	5.30437	5.26167		
					6.60912		6.25703		6.03867	6.13555		
					7.72383		7.39527		7.22885	6.99457		
					8.53238		8.73858		8.25016			
					9.63381		10.08260		6**96*6			
					10.76467		11.91097		11.53350			
							13.88157		13.51058			

### TAB PRINT-OUT OF DENSITY

#### DENSITY IN GRAMS PER CUBIC METERS

FLIGHT NO. Altitude	37	36	39	04	41	42	54	4	45	<b>4</b> 6	4 7	8) -7
100	.00028	.0[042 .0067				.00054		.00056 .00068			.0007	
86	.00052	.00071	.00080		.03061	.00103		.00077	.00046		.00082	.00042
97	.00073	.0005.	• 0 0 0 4 4		• 00075	.00127		.00087	.00080		.00095	.00041
96	66000 .	.00102	.00108		06000 .	.00155		• 00096	.00130		.00108	.00058
95	.00132	.0121	.00125		. 60106	.00185		.00109	.00183		.00120	<b>7</b> 500 <b>0</b> •
<b>7</b> 6	.00171	.0146	.00143		.00126	.00214		.00130	• 00224		.00138	.00134
93	.03217	.00175	.00175		.03152	.00252		.00162	.00256		.00165	.00186
92	.03263	.00216	.00209		.00146	.00292		•00200	.00277		.00200	.00248
91	.00336	.0273	.00252		.00233	.00347		.00267	.00292	.00239	.00246	.00320
06	.00363	.C0340	.00305		.00294	•0340 <b>9</b>		.00330	.00314	.00269	.00301	.00364
69	.00423	.09426	.00367		.00374	.00478		.00405	.00341	.00330	.00367	.00441
58	• 00464	.00514	.00441		.00463	.00560		.00496	20700 .	.00438	• 00447	.00496
87	.00583	.00622	.00527		.00567	.00652		•0000	.00507	.00579	.00540	.00549
86	.00659	.00739	.00629		.00685	.00753		.00729	.00626	.00714	.00642	.00613
85	.00320	.00871	.00755		• 0 3 8 2 2	.00868		.00972	.00795	.00854	.00751	.00692
94	.00976	.C1018	• 00902		. C0968	.00997		.01037	.01030	.0107	•00864	.00806
83	.01159	.01177	.01079		.01135	.01152		.01236	.01321	.01147	.01057	.0369
82	.01372	.01373	.01300		.01326	.01325		.01462	.01551	.01261	.01262	.01181
81	.01616	.61595	.01552		.01530	.01534		.01726	.01771	.01392	.01508	.01461
50	.01989	.01862	.01864		.01756	.01780		.02032	.01963	.01609	.01802	.01613
62	.0220	.02178	.02227		.02037	.02067		.02350	.02197	.01898	.02152	.02233
7.6	.02545	.02561	.02648		.02241	.02406		.02768	.02541	.02284	.02547	• 02722
77	.02900	,02344	.03149		.02564	.02783		.03160	.03058	.02910	• 03040	.03257
76	.03256	.03307	.03753		.02872	.03193		.03595	.03448	.03692	.03609	.03780
75	.03643	.03583	.04406		.03160	.03635		.04122	. J3755	.04286	.04234	.04251
74	.04130	.04107	.05173		.03512	.04104		.04470	.04408	.04975	•0+634	.04566
73	.04881	.04400	.05863		.03991	.04816		.05082	.05252	.05484	.05479	.05086
72	.05873	.05672	.06779		.04718	.05674		.05758	. 36262	.06294	.06276	.06410
71	.07120	.06748	.07890		.05484	.06738		.06624	.07887	.07829	.07244	•07799
70	.08439	.68140	.09492	.07696	.06426	.08213		.07757	.09057	.08304	.08828	.08829
69	.09733	•09692	.10587	.09140	.07715	.09382		.08892	.11128	.09725	.10278	.09774
68	.11140	.11544	.12003	.10454	.08776	.10612		•06349	.12801	.11060	•11394	.11851
67	.12876	.13331	.13715	.11976	.10056	.12230	.11164	.10952	.11990	.14708	.12995	.12751.
66	.14980	.15511	.15592	.13689	.11917	.13805	.13645	.13085	.15820	.14501	.15633	.14338
65	.16582	.18353	.17677	.15795	.14340	.15585	.11862	.14571	.18141	.18070	.17077	.16440
<b>64</b>	.18472	.20919	•19949	.17850	.16992	.19133	.14276	.16805	.19011	.20028	.17512	.18644
63	.21859	.24502	.22562	.20081	• 19341	.20394	.21634	.20142	• 23999	.24626	.21515	.24541
29	. 24062	.27385	.25384	.22670	. 22143	.23483	.20722	.22033	.24513	.26053	.24135	.21105

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### TAB PRINT-OUT OF DENSITY

#### DENCITY IN CLAMS PER CUBIC METE

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	47	4 2 2 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5
	46	9 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
	t.	5000000000000000000000000000000000000
UC N. ET EFO	5 4	• 577 • 777 • 777 • 7779 • 7779 • 7779 • 77797 • 77707 • 77707
an PES CUE	43	2000 2000 2000 2000 2000 2000 2000 200
VV TO AT 1 T	42	<ul> <li>444440</li> <li>46000</li> <li< td=""></li<></ul>
	41	. 287949 . 287949 . 315927 . 315927 . 315927 . 315927 . 315928 . 315928 . 315928 . 315928 . 315928 . 315928 . 41128 . 51128 . 51128 . 25557 . 79737 . 79747 . 79747
	D a	<pre>************************************</pre>
	6	• • • • • • • • • • • • • • • • • • •
	38	0 0 0 0 0 0 0 0 0 0 0 0 0 0
	47	• 2 • 3 • 4 • 4 • 5 • 4 • 4 • 4 • 4 • 4 • 4 • 4 • 4
	FLIGHT NO. ALTITUDE	ႷႳႧႧႺႧႦჄႦႺႱႦႺჿႦႦႦႦႦႦႦႦႦႦႦႦ ჃႳႧჾႠႳႧႵႦႠႱႺႱჿႵႵႵႵႵႵႵႵႵႵႵႦႦႦႦႦႦႦႦႦႦ ჃႳႧჾႠႳႧႵႦႠႺႺჿႦႠႳႺႵႦჂႵႵႵႵႵႵႦႦႦႦႦႦႦႦႦ

### TAB PRINT-OUT OF DENSITY

#### DENSITY IN GRAMS PER CUBIC METERS

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Q	••		•••••		
59	.00124 .00164 .00161		• 00000 • 001000 • 01000 • 01000		
58		.00179 .00288 .00288 .003288 .003288 .003458 .003458 .003458	• 00561 • 00731 • 010900	00000000000000000000000000000000000000	
57				01921 01921 02219 02219 02571 02972 03596 015245 015255 015255 015255 015255 015255 0152555 0152555 01525555 015255555 01525555555555	
56	.00097 .00110 .01127 .00127 .00127	.00192 .00192 .00246 .00246 .00296	.00632 .00786 .00966 .01171 .01171	.011655 .02664 .02664 .02664 .02664 .03566 .03566 .04681 .04681 .04681 .04681 .04681 .04681 .058664 .05864 .05864 .05864 .05864 .05864 .05864 .05866 .0586646 .058664 .058664 .0586646 .0586646 .0586646 .0586646 .05866646 .05866646 .058666666666666666666666666666666666666	
55	.00065 .00065 .00071 .00079 .001079 .001127	.00192 .00192 .00192 .00294 .00358 .00358 .00358	.00651 .00799 .00966 .01162 .01393	.01655 .026282 .026282 .026282 .026282 .038381 .038381 .038383 .038383 .05197 .05197 .1370844 .137084 .1370844 .137084	
54		.00182 .00196 .00223 .00223 .00263	.00565 .00838 .01031 .01031 .01249 .01475	01741 02029 02020 02020 02020 02020 02020 02020 02020 02020 02020 02020 02020 02020 02020 000000	• 6 6 9 3 •
53		.00318 .00318 .01460 .01460	.00624 .00718 .00821 .00958 .01137	013500	• 23614
52		.00203 .00231 .00261 .00302 .00356 .00451	.00579 .00730 .00730 .01138 .01438	011734 02079 02079 02079 02079 02079 02079 000023244 00002334 000023 000023 000023 000023 000023 0000023 0000023 0000023 0000023 0000023 0000023 0000023 0000023 0000023 0000023 0000023 00000000	21842*
51	.00049 .00054 .00071 .00087 .001097 .001097 .001097 .00109	. 00209 . 00305 . 00305 . 00365 . 00365 . 00365 . 00365 . 00365 . 00506 . 00505 . 0050	.00719 .00854 .01013 .01213 .01213	011702 012027 02027 02027 02027 02027 02057 02057 01494 01494 01494 01494 01494 01494 01494 01494 01496 01492 01492 01496 01492 014966 01496 0146 0146 0146 0146 0146 0146 0146 014	. 23526
50		. C C 2 0 1 . C C 2 0 1 . C C C 2 4 7 . C C C 2 9 7 . C C C 3 5 8 . C C C 5 1 1 . C	.00704 .00819 .01127 .01127	.01569 01569 01858 02191 02191 021958 023991 024491 024491 058696 058696 058686 05866866 0586866 05868666 0000000000	.22565
67	.01063 .00173 .001373 .00196 .001112 .001112 .001134 .001134	. 00190 . 00226 . 00226 . 002272 . 00400 . 00483	.00592 .00823 .01975 .01153	.01602 .01602 .02549 .025411 .02571 .02575 .03575 .03575 .04104 .04104 .05495 .09485 .09485 .09485 .09485 .09485 .09485 .09485 .09485 .09485 .09485 .09485 .09485 .09485 .09485 .09485 .09485 .09485 .004855 .004855 .004855 .0048555 .004855555555555555555555555555	.23843
FLIGHT NO. Altitude	400 99 97 95 95 95	200000 200000 20000	9 0 0 0 0 0 0 0 0 0 1 3 M 6	90000005990000000099 90000005990000000099 900000059900000000	62

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### TAB PRINT-OUT OF DENSITY

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	60	.26191	.29259	.32992	. 39335	.44085	.50784	.57932	.63968	.72407	.81717	25006.	1.05208	1.22431	1.32400	1.49118	1.66239	1.92041															
	66	.26112	.28868	.33691	.39234	.43198	.49309	.56057	.64222	.68462	.78896	.90161	82066.	1.12369	1.35518	1.52960	1.77291	1.98722	2.19405	2.47219	2.77824	3.17758	3.77347	4.47602	5.20898	6.28538	7.45728	6.61468	9.81410	11.23769	12.76394	14.93433	
	9	.25419	.28595	.32537	.38158	88144.	.51322	.57033	.66814	.74503	.83889	.96330	1.07767	1.23603	1.42455	1.59349	1.77966	2.02549	2.36077	2.77540	3.08290	3.46683	4.12329	5.05090	5.95823	6.48128	7.38399	8.17269	9.46557	11.48515			
	57	.26260	. 29945	. 34455	. 39677	.43486	.48759	.54871	.62530	.74409	.85806	.97450	1.09898	1.26588	1.40653	1.60290	1.81296	1.99604	2,26262	2.62537	3.04108	3.56194	4.12806	4.71595	5.33728	6.23301	7.08983	8.4938	9.74270	11.66522	13.51626	15.66470	18.60927
C METERS	56	.40841	.47433	.57258	.72765																												
S PER CUBI	55	.27490	.32951	.34619	.40111	.46555	.50392	• 56546	.63709	.70472	.81723	.96192	1.07606	1.21163	1.41042	1.57729	1.68396	2.04106															
Y IN CRAM	u t	.25:78	.2963	.32143	.36420	.41651	.48 160	. 54 1547	.63 370	.73761	.85 245	.98350	1.09/17	1.27 345	1.42579	1.62310	1.81781	1.96084	2.25743	2.64293	3.04609	3.47703	3,93829	4.72300	5.63198								
DENSIT	5	.26592	.30057	.34041	.39741	. 440 31	.50464	.56927	.64201	.73779	. 84623	.95629	1.07002	1.20045	1.41921	1.60094	1.78261	1.95299	2.20353	2,53271	3.01032	3.51029			5.55233	6.57571	7.70988	8.11850	9.75617	11.21229	13.23664		
	52	.27625	.31806	. 37243	.41221	.45272	.51864	.57860	.65933	.78214	.84424	1.02316	1.09150	1.23725	1.41939	1.57919	1.80114	1.98623	2.25218	2.55928	3.04590	3.56952	4.40440										
	51	.27199	.32904	.36221	.41670	.48277	.51257	.61191	. 66868	.74259	.83896	.96818	1.13293	1.28437	1.41243	1.60109	1.84006	2.00748	2.39529	2.63932	3.07321	3.63870	3.97697	4.57292	5.29844	6.32886	6.99033	8.64619	9.64284	11.06260	13.05556	14.81796	19.92613
	50	.26476	.30544	12072.	.38981	.45203	.51208	.57019	.65312	.73347	.85175	.96507	1.06408	1.23239	1.44861	1.57921	1.70547	1.92320	2.15205	2.52390	2.97724	3.46369	4.00923	4.62255	5.26727	6.03397	6.84006	8.16357	9.15689	10.80267	12.92738	15.42297	19.03610
	64	.27249	.32066	.37923	.43060	.47895	.54595	.61494	.69136	.79939	.90236	1.01283	1.16860	1.34160	1.49090	1.64961	1.90843	2.15263	2.62500	2.83947	3.36075	3.99419	4.40066	5.20536	5.91527	6.84979	8.20566	9.83424					
	FLIGHT NO. ALTITUDE	61	60	59	58	57	56	55	54	53	52	15	50	6+3	<b>4</b> 8	47	46	4.0	44	M 7	42	44	40	39	36	37	36	35	4M	33	32	31	30

### TAB PRINT-OUT OF DENSITY

#### DENSITY IN GRAMS PER CUBIC METERS

67 67							10167	10234	00314	10385	10453	00531 .00413	00606 .00522	0705 .00689	10642 .00853	11019 .01027	01195 .01189	01411 .01336	11643 .01498	11898 .01723	12179 .02047	12503 .02419	12822 .02857	33170 .03374	33566 .03880	04012 .04386	04543 .05030	15272 .06015	16165 .07070	07183 .08416	08360 .09890	10014 .11393	11506 .12855	13149 .14486	14467 .16580	16386 .18977	18913 .21719	21630 .24323
65						.00134	.00196 .0	.00266 .0	. 00334 .0	• 00374 •0	.00401 .0	.00439 .0	.00528 .0	.00645 .0	.00803 .0	. 0980.	.01194 .0	.01433 .(	.01691 .0	.01950 .0	.02217 .0	.02538 .0	.02964 .0	.03460 .0	.04102 .0	.04785 .[	.05524 .0	.05273 .0	• 07096 • 0	.08166 .(	.09526 .(	.11143 .1	.12694 .1	.14457 .1	.16557 .1	.18962 .1	.21716 .1	. 24283 .
64						.00170	.00191	.00214	.00241	.00270	.00353	.00428	.00582	.00715	.00858	05600 .	.01129	.01321	.01596	.01896	.02229	.02569	.12960	.03363	.03859	.04426	.05165	.06008	.07056	.07855	.09143	.10371	.12172	.13693	.15720	.18266	.21070	.24173
63											.00374	.00445	.00530	.00639	.00792	.00998	.01225	.01412	.01611	.01849	.02184	.02599	.03041	.03624	.04235	.04735	.05297	.06253	.07297	.09531	.10036	.11393	.12665	.14046	. 15566	.17501	.19749	.22020
62							.0178	. 6 0 2 0 3	.00235	.60293	.60401	.00521	.00617	. 00732	.00838	.0937	.01054	.01221	.01435	.01741	.02107	.62479	.02958	.03578	.04247	•0+959	.05787	.06359	.06359	°C 7996	.09571	.11193	.12005	.13406	.15741	.17576	.19625	.22026
61								.00262	.00320	.00334	.00326	.00371	.00437	.00569	.00737	.00921	.01120	.01296	.01492	.01703	.02000	.02378	.02305	.03285	.03857	• 0++24	.05112	.05832	.06974	.08023	.09156	.10845	.12518	.13407	.15315	.17629	.20296	. 22863
FLIGHT NO. Altitude	100 99	86	97	96	95	54	93	26	16	<b>0</b> 6	58	88	87	86	85	919	83	82	81	30	62	78	77	76	75	74	73	72	71	20	69	68	67	66	65	64	63	62

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#### TABLE XXII (Concluded)

### TAB PRINT-OUT OF DENSITY

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		à	NI I LICNA	LAMS PER	CUBIC ME	TERS	
FLIGHT NO. Altitude	61	62	63	67 67	f 5	66	67
61	. 25899	.25920	.25015	.25866	.26812	. 24 765	.2817
60	. 29733	.29950	. 29531	.29803	.30348	.28059	30.62
59	.34037	12142.	.34529	33611	34836		3466
58	.39729	. 39136	.397.99	.36825	37484		3914
57	• 44317	.46235	.46364	.41903	42717		. 44 85
56	. 49689	.48538	.51733	.49510	. 49464		4965
55	.55530	.56962	.57853	.53779	. 56165		.5775
54	.63397	.65693	.65599	.63445	. 66479		.6973
53	.72595	.72608	.71230	.70001	- 74392		.7271
52	.82445	.81076	.81570	.81546	. 83746		8746
51	.90363	.94712	.92794	.96687	.91578		.5913
50	1.04635	1.62511	1.04294	1.06292	1.08390		1.0970
<b>6</b> †	1.11376	1.17819	1.16262	1.19319	1.21090		1.2207
1- CE	1.33504	1.37621	1.35753	1.35376	1.37815		1.4410
47	1.51144	1.53305	1.54412	1.66568	1.53789		1.6741
46	1.72495	1.71220	1.72732	1.86696	1.73338		1.8886
с С	1.96039	1.96133	1.89328	2.09510	1.92667	1.95525	2.0881
1 1	2.13931	2.12222	2.18724	2.9953.5	2.17427	2.28724	2.3397
N 4	2.44639	2.47245	2.52406		2.52294	2.52015	2.5906
42	2.84474	2.80450	2.99142		2.82454	2.89541	2.99241
41	3.39322		3.37310		3.35490	3.42789	3.4156
4 0	3.93526		3.98668			3.99753	3.7702
39	4.42210					4.58518	オロドオ・オ
38						5.31123	5.50887
37						6.16768	6.2551
36						7.26621	
35						8.47842	
1 M						9.70786	
33						11.23915	
2						12.72767	
100							

0 m 2 61.61 TABLE XXIII

## TAB PRINT-OUT OF PRESSURE

#### PRESSURE IN MILLIBARS

FLIGHT 40. Altiture	-	r.	₽1.	t	ur.	Ś	2	¢	σ	10	11	12
										10.00	1002	00030
100	.00534	.00733	.00025	.00025		•00020	. 6.0.22		. 50.00	// n u u		00035
66	9×ù00°	. 000 to	.01030	.00030		.96035	. 6 6 6 3 4			20 10 10		C4000
80	. 992646	.00246	• 00035	.00035		.00041	•00034					01000
1-0	.03654	. 10155	.00042	.00042		.00350	.00045			• • • • • • •	14000.	
96	5 U U U U	.03165	.0001	.90950		.00058	. 00051		.00052	.00055	.1900.	
		22-02-	00000	.00041		•000•	. 60061		.00063	.000.66	4/ FO G •	
0	74700	19113.	. 00073	.00073		.00081	.00071		.0004	8/00.	64000°	
. 0	<pre>0.00</pre>	.0101	00088	.00048		.0005	. 00985		.01099	.0033	.00107	+6000.
		11123	. 00103	.00107		.00114	.00103		. 00107	.00111	• 00129	11100.
- <b>-</b>		.01146	.01127	.0127		.00136	.00123		.00127	•00132	.00155	
		00171	. 1615 8	.00152		.00154	. CO14A		.00151	.00159	.00136	.00160
			1011	00182		.00107	.00179		.00190	.00193	.01223	55100.
			7200	.00217		.00238	.00214		. 00214	.00232	.00255	.00233
			10287	00258		.00201	.00257	.00259	.00257	.00282	.00314	.00203
				00%00		.00380	• 00334	.00323	.00332	.06339	.00372	.00340
3 1 1				00.368		00427	.00376	.03386	.03370	.00410	• 00440	.00412
<b>ر ۲</b>				.00445		00513	. 00452	.00466	.00445	.00491	.03527	.00500
						.00525	.0549	.00560	. 10554 3	•00294	.00630	.00599
						00753	.00657	. նն5 ዶ0	.01553	.00711	.00753	.00721
24				297.00		02600.	.00790	.00618	.00781	.00851	.00391	.00855
	14160.					.010.7	0955	06600 *	0 1600 .	.01019	.01073	.01035
5	19896.			- 00 - 146		01299	.01135	.01195	.01129	.01217	.01250	.01242
54						01554	01358	• 0 1 4 4 4	.01350	.01435	.01531	.01478
78	.51291	.01275				01834	01609	01732	.01616	.01730	.01197	. 01740
77	.01529	• 11 574				02152	11911	.02039	.01891	.01987	.02111	.02043
75	. 31829	1 1 1 1 2	01220.			0.2510	62262	-02411	. 02716	.02310	.02464	.02394
75	. 92133	.07155	0.4470.0				12934	.02850	.02585	.02643	.02870	.02760
74	26420.	12423.		154/6.			07113	.03282	.07014	.03000	.03304	.03160
73	11526.		0 + 4 C D •				03654	.03827	. 07480	.03420	. 03940	.03677
22	. 5744 B	• C 44 4 5	• 04/25	• 5.040		792.01	67247.	.04461	.0.055	.03497	.04540	.04257
11	£ 20 t0 *					1515	. 64965	.05167	.04732	.04526	. 15305	.64930
70	• 64713	- 94 - 5	\[	6 / 2 CL •			05963	.06081	.05557	.05188	.06238	.05757
<b>б</b> а	• CE 44 2	26750.	. 06455			0.000	DEAD7	. 10.7.0	. 05397	.05983	.07274	.06699
5 A	. 56223	.05759.	42220 *	. 17 / 1		4 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	14070	08395	+ 2 + 2 <b>-</b> -	.07000	.08440	.07913
£ 7	. 37115	. 07 79 1	• Ja 20 E	1, 40.			07200	00700	. 08535	.08236	.09852	.09327
6.F	. 0.5 2 9 A	. C.9.54A	.13690	.09643						04710	.11431	.10522
u S	03560 .	• 34 ¥ 2 0	.12425	.110 2		04011.		• • • • • •		11498	.13126	.12146
64	.11247	.11391	.14419	.12745		24/11.			12011	13298	.15232	.13938
63	.17105	17171.	.16772	.14556		04/21.	• 14769		4 1 5 1 4	15541	.17476	.16143
29	.15369	.15205	.19275	.16724		.14200	10001 •		• • • •			1

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## TAB PRINT-OUT OF PRESSURE

#### PRESSURE IN MILLIBARS

FLIGHT HO. Altituge		<b>n</b> i	٣	£	•1	۲	~	æ	n	10	11	12
5.1	47716	17771	- 2214 A	. 10125		.17058	.19229	.19587	.15931	1796z	.20225	.18619
		20171	25096	. 21729	. 21255	19793	.22035	.21019	.13362	.20780	.23114	. 21385
		. 22268	20001	.25.317	. 25.273	.22319	. 25765	.25095	.22192	.24670	.26562	.24425
		26148	33836	79427	VEEDS.	.26011	. 2005 .	.29196	. 25217	.27498	.30068	.27924
		22298	5 406 2	77579	19957	.27 490	. 33244	.32313	.25895	.31367	ちゅうさい 。	.31785
- 4	82472	37434	44814	. 374.96	10202	34692	.37890	.38820	+ 329A4	.35552	.38951	.36230
, n . n	14227	10242	5003	47.245	6181.4	.38581	. 43336	.43523	. 3/ 5 7 2	.40416	.43821	• 40906
	1221	4444	5 444 6	40519	.48746	.49285	• 49439	.43062	.42929	.45624	• 4 97 80	.46931
5 P		12121	. 46516	56.350	54063	. 56279	.56224	88426.	.49451	.51574	.57113	.53180
5.2	5 447 0	0.000	75111	.64 207	. 50149	.63227	. 64490	.62324	.53422	.58710	.65156	.60459
	66.224	.62101	. 44472	12222	. 6. 765	.72244	.73104	.69010	. 64558	.66224	.73591	.69712
	. 75.196	.63776	. 95.76 B	.87111	. 79195	.81849	.A7603	.85139	. 73767	.75270	- 84042	.19232
0 < L /	95572	fice2.	1. 37574	.93622	. 89757	.93028	. a5595	.94567	. 82 87 A	. 65552	. 95324	11 006 .
	95417	00.64.	1.20107	1.07156	1.04225	1.05144	1.08345	1.09051	• 9+335	•96262	1.08092	10620-1
1.7	1. 1945 0	1.02935	1. 35 GD B	1.21907	1.27204	1.20331	1.24251	1.30086	1.07595		1.22320	1.150/0
. v.	1.25257	1.17277	1.51619	1.38764	1.47333	1.36878	1.41345	1.36878	1.23239		1.38689	1.30776
t.	1.47039	1. 72799	1.71026	1.54107	1.61008	1.56047	1.61009	1.55646	1.41666			1.50256
5	1.59930	1.53124	1.04151	1.796,49	1.73869	1.77692	1.84727	1.8372A	1.61372			1./ 0100
t.		1.74 777	2.20819	2.04437	1.89.772		2.08667	2.06143	1. 85348			1.925
t 2		2.002.2	2.51440	2.33629	2.05765		2.39732	2.45509	2.12499			2.20456
		2.31740	2.84A66	2.67109	2.40143		2.74947	2.76842				2.53408
		2.69162	3 1002 2	3.06902			3.12490	2.96984				07070-N
<b>4</b> 9		3.13750	3.77430	3.49116				3.51028				20763 00
38		3+64741	4.36001	4.00048				4.21460				
37		4.25371		4.59127				4.62304				
36		65079.4		5.26925								
35		5.63034		6.11939								
35		6,65875		7.05117								
<b>1</b>		7.67759		R.16922								
32		8.92942		9.40555								
10				10.85906								
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## TAB PRINT-OUT OF PRESSURE

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FLIGHT 40. Altiture	13	4	1 J	ц Т	17	1. R	19	20 .	21	22	23	54
100	.2000.	.00030		.00927	.00029	.00025	.00029	.00028		.00032		0 1 0 0 0 1 0
66	. 10036	.01136		.00333	.03031	.00029	.00032	.00033		.00036		.00046
	. 90 64 2	.00942		.00037	.00035	<b>45000</b> .	.00041	0 70 00 *		• 0 0 3 4 2		+6000.
9.7	84000.	67000		• 60040	• • • 0 0 ° •	.06043	• 00049	• 0 0 0 4 8		.00149		-00062
96	100.557	. 00058		.00055	.00054	.00052	.00056	•00029		.00358		.00073
0 0	. 30 66 7	C/CCO.	.00356	.00071	.06730.	.000F1	.00070	.00072		.00070		49COD.
10	. 13 67 7	1.000.	.00078	. COJAJ	. 070A1	e7006.	• 0003A	.00086		.00045		.00099
5	00000	PC000.	7 ED UC .	.00100	.0001	.0003	. 60107	. 30104		.00101		.00115
26	90106 .	.01104	. 0110 e	.00118	.00119	.00112	.00128	.01126		. 6 0 1 2 2	.00113	9910 <b>0</b> .
91	.00123	.00128	.09127	.00136	.00143	.00177	.00161	.00154				FC100 .
00	. 00146	.03149	. 03147	.00163	.00170	.00154	- C0134	.00185		.00170	64100 ·	10100.
5.0	.00172	.00174	.00172	.90197	.00701	.01199	• 00225	.03223		20200.		
	.00207	.01208	.00201	.00232	.00242	.03235	.00272	.00269		.00240		• • • • • • • • • • • • • • • • • • • •
7.4	. 00 25 1	.01250	. 97243	.00281	. 05247	.00298	.00324	.00324		6 2 0 0 °	\$ / 20 <b>0</b> •	
ЯF.	. 00 20 5	20100.	. 30249	.90345	.00345	.00346	• 00391	.00390		.00359	14590.	00200
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## TAB PRINT-OUT OF PRESSURE

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92	.00134	.09119	.00126	.00105		.00106	.00125	.00124		•000Je	.00112	.00113
41	. 30159	.03143	.09153	.00126		.00124	.00145	.00143		.00116	.00136	.00137
0	.00146	. 00174	.00195	.00149	.00174	.00144	.00171	.09165		.00141	.00162	.00169
89	.Jn2?1	51500.	.00222	.00176	.06297	.00167	• 00202	.00191		.00170	.00191	.0200
	. 57 25 3	.01256	.00267	.00207	• D n 2 4 7	.00195	.00239	.00222		.00202	• 0 12 25	• 6200 •
<b>7</b>	. 90313	.03*09	.00320	• 00 245	.00295	.00235	.00286	.00263		.00236	.00265	• 00306
2	. 36 27 3	.03371	.00393	<b>100394</b>	. OC359	.00290	27203 .	.00317		.00274	.00315	.00363
5	. 0. 44.5	.03443	.00457	.00755	.00413	.00361	.00411	.00384		.00321	.00376	• 00423
	. 30520	.00528	.00546	• 0 0 • 3 •	.05496	.00450	.00495	.00467		.00383	.00453	.03503
	00672	. 07627	.00652	.00531	.05571	.30558	.00535	. 69569		.00460	.00547	.00593
A 7	.00751	.00744	.00778	.00652	.00670	.00588	.00717	.00691		•00355	.00661	.00703
	20900.	.01942	75000.	.00932	.09789	.00841	.00952	.0CA37		•00688	.00801	.00529
	91058	.01045	.01192	.00933	.05930.	.01020	.01033	.01008		.00801	• 00969	.009R6
79	. 91253	12210.	. 01 7J A	. 01200	.01099	.01227	.012 75	.01209	.01041	.00959	.01157	+ 1 1 1 1 + + + + + + + + + + + + + + +
78	. 31491	.j1464	. 01547	.01452	.01300	.01463	.01469	.01445	.0123A.	.01143	.01398	.01395
11	.01749	. 01729	.01820	.01741	.01541	.01732	.01736	.01718	.01456	.01358	.01652	.01554
76	7 665	.0203	.07130	.02075	.01829	.02077	. 62036	45C2D.	.01730	.01510	.01960	.01957
	- 120 -	. 07 vi	. 12479	.02459	.02176	.023A3	.02364	.02400	.02036	.01902	.02293	.02309
74	. 32450	6279Å	.02858	.02885	• 02585	.02775	.02713	.02815	.02371	•02244	.02665	91/20 ·
2.7	.0323	.03250	.03339	.03380	.03050.	.03215	.03102	•03293	. 02R01	.02640	.03078	.05161
72	0.479	. 93773	.03931	02020.	.03582	.03714	.03559	.03827	.03271	.03105	.03546	.03799
11	.04576	.04791	.04455	.04555	.04165	.04244	.04110	.04431	.03819	•03545	.04091	. 64316
	. 15 31 0	.95107	.05196	.05269	.04922	.04985	. C4788	.05141	. 04437	.04276	.047.56	. 55021
	26.149	04970	. 06072	.04980	• 05579	.05807	.05621	.05977	.05169	.05018	.05502	.05847
- et 	07122	. 25955	27070	.07011	.06471	.06754	. 04535	.06959	.05019	.05875	.06419	.06919
5.3	.04267	5 4 7 7 A	. 09.24.2	.08055	<b>*6*</b> 2 <b>0 *</b>	.07863	.07689	. 1 9188	.07015	.06875	.07495	.07933
- 4	05550	.03766	0 95 96	15290.	. 0.560	.09100	.04916	.09365	. 08173	.08021	• 0 86 9+	.09172
	11076	11011	11070	.10555	.09978	.16485	.10356	.10946	.034A6	.09291	.10048	.10574
5.	12715	12449	AF751.	.12105	.11501	.12037	.12048	.12843	.11982	.10737	.11582	.12138
	. 14541	.14312	.14751	.13933	.13256	.13818	.13935	.15070	.12715	.12407	.13350	67627.
29	. 16735	. 15 369	.15891	.16035	.15284	.15 462	.16130	.17682	.14721	.14337	.15368	<b>10405</b>

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FLTGHT 10. ALTITUNE	с .т	Ĺ	5	52	۲. ۲	JI t	55	56	57	53	59	60
61	. 1915 5	4ù221 *	.19335	.18538	.17659	.15146	.18555	.21010	.17049	.16578	.17735	.16260
50	.22034	. 2144B	.27199	. 21373	. 20 195	.20926	.21540	.25251	•19748	.19173	.20385	146 0 2 .
59	6 52 5c •	.24550	. 25550	.24576	.23451	50222	. 24793	.30337	.22930	.22110	.23374	.23899
E L	82202 .	F50F5.	R 7505 .	. 24468	.26 337	.27144	. 29282		. 26368	.25513	.26893	.27404
57	.33579	.32093	. 37695	.32623	.30927	.35872	. 17446		.30336	.29455	.30870	.31380
55	. <b>7</b> 8505	* 35 70 *	.34332	.37256	90738 *	.35207	.37170		. 34762	.34015	.35297	.35917
55	. 44 05 7	. 41944	. 47 P1 4	.42575	.40631	.40121	.42326		.39750	.39208	.40350	.41143
54	. 55.35.4	.47854	1664.	46394	. 46421	.45727	. 48001		.45351	.45202	•46176	.46932
5.3	.57653	.54451	.5660 B	.55 113	. 53116	.52311	.54533		.51917	.51842	.52606	.53430
52	. 55 85 8	.62109	. 64427	.63193	.61677	.59960	• 61764		.59625	.59333	.59728	•60793
51	. 75013	19907.	.7125	.72190	.69383	.69740	.70590		.68437	.68067	.67659	.69156
5	. A5.53 A	. 97570	11658.	. 82377	87067.	.78925	. A 055 T		.78423	.77713	.76931	.70568
49	10220.	.9165A	20240.	.93509	.90089	50206.	.92311		14768.	.88576	.87164	.89317
r t	1.19546	1.14795	1.07331	1.06412	1.02551	1.03259	1.04683		1.02652	1.01443	.4066.	1.01931
47	1.25675	1.19515	1.22079	1.20974	1.16371	1.17697	1.18750		1.17154	1.15949	1.12831	1.15509
т. Т	1.42923	1. 34439	1.34433	1.36925	1.37060	1.33952	1.34716		1.37541	1.32252	1.28536	1.30963
45	1.5-176	1.57759	1.56727	1.54915	1.51099	1.52019	1.52841		1.51951	1.50781	1.46730	1.48839
4 4	1.45701	1.77549	1.77740	1.74958	1.71130	1.72608			1.72456	1.71806	1.67091	
10 <b>1</b>	2.11823	1.94673	2.01944	1.98547	1.94644	1.95811			1.95003	1.96169	1.89591	
¢ 7	2.41929	2.21175	20202.5	2.25332	2.21434	2.23091			2.21547	2.24306	2.15355	
41	2.76969	2.5226	2.61949	2.56 196	2.57981	2.55174			2.53234	2.55902	2.43832	
10	3.17256	2. 89599	2.971A4	2.92565		2.31207			2.92120	2.92960	2.77544	
49	3.63349	7272.5	7. 3P143			3.33096			3.34571	3.37970	3.17405	
æ.	4.15579	77785	7.44958		3.81105	3.82503			3.62920	3.91330	3.64149	
37	4.78431	4.72412	4.79550		4.39671				4.33378	4.51632	4.19618	
36	5.49921	4.94573	5.03766		5. 0f.124				5.07118	5.18319	4.85698	
45	6.32549	5.67927	5.78553		5. 80737				5.78519	5.95175	5.62837	
34		6.51136	6.68129		6.66399				5.65904	6.61234	6.53990	
33		7.47349	7.69345		7.65912				7.69835	7.83783	7.56938	
ć 2		A. 53636	A. 85547		9.85568				A. 91602		8.73016	
1.		9.95077	16.22.291						10.31734		10.08049	
10		11.57617	11.87964						11.98770			

## TAB PRINT-OUT OF PRESSURE

#### PRESSURE IN MILLIBARS

FLIGHT NO. Altiture	61	62	63	64	65	66	67
100							
9							
80 70							
96							
95							
44				.00105	1,000.		
5		.00104		.00121	.00085	<r 1000="" th="" •<=""><th></th></r>	
56	.00178	.01122		.00140	.00108	40100.	
41	.00156	.0014I		.00151	.00137		
σ	. 00198	.03158		.001A5	.00170	.00163	
. 6	92200 -	.00201	.00195	.00213	.00207	.00203	
	.00252	.00245	.09234	. 0624A	.00247	.00750	.00217
87	.00399	.00299	.00291	.00296	.00293	•00304	. 00262
. u:	. 00347	.03353	.00336	.00 357	.00349	.00366	. 66719
K	.00410	82700"	.01404	.00432	.00419	.00439	.00.493
	.00449	.03522	.00449	.05720	.00502	. 30527	5 1 7 1 7 1 S
	.00.535	.03517	.00594	.00521	.0.635	.30632	. 005-39
	. 00 7 0 0	.01725	.00720	78700.	.00730	.00756	00100
	E E A UU	. 09451	. 03 45 4	.00976	. O C R 7 9	.00902	- 00B4 3
	STO JU	.01072	.01029	.01042	.01153	.01070	.00395
0.1	.01161	.01185	.01221	.01238	.01251	.01254	.01175
	11369	.01493	. 01447	.01467	.01477	.01488	.01388
- <b>-</b>	. 01616	. 01562	.01716	.01731	.01739	.01742	.01539
75	. 101016	- 01973	.07034	.02932	.02045	.02027	.01935
	102247	. 02342	.02410	.02776	.02405	.02349	. 02284
	1264	. 02776	.02838	.02772	.02830	.02711	. 0?578
, P		03291	.03316	.03228	.03323	.03119	.03125
	03623	. 13870	.03856	. 03762	.03885	.03587	.03652
. •	04240	.045.04	.04515	. 04 793	.04526	.04132	. 04275
	04040	. 15.214	.05271	. 05 0 a5	.05252	.04770	.05015
	05766	.06051	.06163	.05399	.06095	.0513	.05833
		- 07044	07191	.06958	.07041	• 06 3 92	.06913
c †		73195.	08 34 2	07973	.08225	.07422	.08072
		10374	09621	.09200	.09517	.08607	. 09355
5		10755	11037	10630	.10975	.09933	.10920
<b>.</b>			12612	.12215	.12655	.11402	.12502
51			3027.	14076	.14593	.13087	. 1 4445
2	• 1991 •			16.224	16.814	.15021	.16666
62	.15 491	.16135	10401 •	- 10 01 -	14204 .		

#### TABLE XXIII (Concluded)

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## TAB PRINT-OUT OF PRESSURE

#### PRESSURE IN MILLIBARS

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FLTCHT 40. ALTITUDE	<b>6</b> 1.	6,7	4 4	3	9:	56	. 67
61	.19206	. 194 - 2	.14657	ê5 28 ₽.	. 10253	.17251	.1017
L · L	. 20.979	.21120	51242	.21264	26012 .	.19790	.2202
г, С	\$ 16 20.	. 74145	. 24 34 0	201 42.	. 21 171		. 2514
5 8	. 27 45 2	.27720	. 27924	.27.11	. 28593		. 2957
57	.31496	. 71922	. 32027	.31:45	32419		. 3270
56	. 36.61 P	. 35369	10692.	. 75 95 1	14974		3725
55	.41138	.41506	.41956	67,07.	.41938		. 4246
54	. 45 871	.47396	. 47.97 6	.45374	.47725		. 4 854
53	. 53543	.54034	. 54432	.52425	. 54433		.557.
ر ۲	. 61970	.51534	. 51937	.60212	.52010		. 6347
51	, 5923A	5,006,3 .	. 70447	•68544	.70710		.7250
5 7	79.22	.79353	. 7994 .	-74 738	51218.		. 8250
5 1	. AAA2C	19868.	.96618	.80446	F 22 10 .		.9390
с я	1.00642	1.01956	1.03034	1.01849	1.07541		1.0649
4 7	1.1419	1.15146	1.15790	1.16081	1.17497		1.7109
4 F	1.73250	1.31858	1.32474	1.35442	1.32847		1.3725
45	1.47.309	1.47556	1.50162	1.50942	1.50371	1.29303	1.5605
46	1 • 56 ar 3	1.63091	1.70123	1.71637	1.76208	1.49580	1.7593
<del>ار</del> ا	1.99631	1.91162	1. 9? g7 4		1.92924	1.72477	2.0073
t 2	2.14755	2.16262	P.193AB		2.19131	1.94376	2.2737
t 1	2.44661		2 * 4 8 2 4 2		2.48958	2.28939	2.5937
1- C	3 1997 .5		2.84297			2.64363	2.9350
40	3.20638					3.06056	3.3347
6 F.						3.53424	3.8051
37						4.07391	4.3674
36						4.71535	
3.5						5.47898	
14						6.35506	
۲.						7.36909	
12						8.52089	
11							
5							

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TABLE XXIV

# TAB PRINT-OUT OF TEMPERATURE

KELVIN	
DEGREES	
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TEMPERA	

100       212       193       185       212         99       207       207       194       183       203         97       207       207       203       184       177         95       207       203       184       173       203         94       207       205       205       205       103       174         93       205       205       205       205       173       179         91       205       205       205       205       173       174         91       205       205       205       173       174         92       205       205       205       173       174         93       201       161       187       177       186         94       195       201       161       186       176         95       199       201       161       186       177         95       199       197       170       177       181         96       196       197       170       177       173         91       196       197       197       176       177	212 203 192									
99     209     194     183     203       94     207     197     184     173       95     205     205     205     197     184       91     205     205     205     184     173       92     205     205     205     184     173       91     206     206     205     184     173       92     205     205     205     173     193       91     206     206     184     173       92     205     205     173     189       93     204     205     205     173       93     204     205     205     173       93     204     205     201     165       93     196     201     166     173       94     196     201     161     186       77     199     194     193     174       95     198     194     167     177       96     199     194     191     177       77     199     194     191     177       77     193     193     191     177       77     193     193     191	203 192	189 251		205 1	76 20	19 19	17 23	215		191
98       207       197       197       197       193         97       205       205       203       184       183         94       205       205       203       184       183         92       205       205       205       173       197         92       205       205       205       173       193         93       205       205       205       173       184         91       206       205       205       173       189         92       205       205       205       173       189         93       201       205       205       173       189         94       205       205       201       163       177         95       196       201       161       186       177         95       196       201       161       176       177         95       196       201       161       176       177         91       196       194       163       177       176         92       196       194       191       177       177         77       193 <t< td=""><td>192</td><td>184 317</td><td></td><td>194 1</td><td>78 19</td><td><b>39</b> 19</td><td>5</td><td>55 208</td><td></td><td>189</td></t<>	192	184 317		194 1	78 19	<b>39</b> 19	5	55 208		189
97       205       201       205       203       184       177         94       205       205       205       103       184       177         93       205       205       205       205       173       179         94       205       205       205       173       179       177         91       205       205       205       173       179       177         93       205       205       203       164       173       179         93       205       205       203       164       173       179         94       205       205       203       164       187       177         95       196       201       165       173       179         95       196       201       165       174       177         93       196       197       161       173       178         94       196       196       197       177       177         95       196       197       167       177       177         91       196       196       197       177       177         74       <		188 276		186 1	81 19	30 20	3 2:	11 199		187
96       207       203       184       177         93       206       206       206       182       177         94       205       205       205       179       179         91       205       205       205       171       182       177         91       205       205       205       171       182       177         92       205       205       205       171       183       177         93       201       205       203       161       186       176         94       201       201       161       186       186       176         95       199       201       161       186       176         95       199       201       161       186       177         95       199       197       170       177         96       196       197       170       177         97       196       197       170       177         97       196       197       170       177         97       198       197       177       171         77       203       193	163	192 240		186 1	86 17	79 20	17 2:	196 196		188
95       206       206       206       182       173         92       205       205       205       173       179         91       205       205       205       173       179         92       205       205       205       173       179         91       205       203       171       183       173         92       205       203       171       183       173         93       204       205       201       161       186         94       204       205       201       161       186         95       196       201       161       186       175         95       196       201       161       186       177         96       199       197       170       173         91       186       191       166       177         77       193       193       174       177         77       193       193       174       177         77       193       193       174       177         77       193       193       174       177         77 <td< td=""><td>177</td><td>196 215</td><td></td><td>198 1</td><td>1 06.</td><td>75 20</td><td>5</td><td>12 198</td><td></td><td>191</td></td<>	177	196 215		198 1	1 06.	75 20	5	12 198		191
94       206       205       205       173       173         92       205       205       179       176         91       205       205       179       176         92       205       205       173       183         93       206       179       176       173       189         93       201       205       201       163       186       173         93       201       201       161       183       189       173         94       196       201       161       163       186       178         95       196       201       161       181       178         95       196       201       161       181       173         95       196       201       167       177       173         91       187       191       177       177       177         77       193       194       191       177       177         77       193       193       194       177       177         77       193       193       194       177       177         75       203 <t< td=""><td>174</td><td>201 200</td><td></td><td>188 1</td><td>1 26</td><td>75 20</td><td>3 2</td><td>13 204</td><td>199</td><td>192</td></t<>	174	201 200		188 1	1 26	75 20	3 2	13 204	199	192
93       203       205       205       179       176         91       204       205       205       173       179         92       205       205       205       173       179         93       205       205       205       173       179         94       205       205       201       163       186         95       199       201       161       186         95       196       201       161       186         95       196       201       161       186         96       196       197       176       173         97       196       201       161       187         97       196       197       176       173         98       196       197       177       177         91       187       183       174       177         77       193       196       173       178         77       193       193       191       177         75       209       216       183       171         77       209       206       217       190 <td< td=""><td>173</td><td>202 189</td><td></td><td>187 1</td><td>1 16</td><td>75 20</td><td>00 2:</td><td>4 212</td><td>197</td><td>192</td></td<>	173	202 189		187 1	1 16	75 20	00 2:	4 212	197	192
92     205     205     205     173     173       91     204     201     101     163       93     201     201     161     183       87     193     201     161     183       86     196     201     161     183       86     196     201     161     183       86     196     201     161     183       87     196     201     161     183       87     196     201     161     183       80     196     201     161     183       81     197     197     170     173       83     196     197     197     176       84     196     197     177     173       80     196     197     177     173       81     197     197     197     177       77     186     193     197     177       77     203     216     219     177       77     203     216     216     177       77     203     216     216     177       77     203     216     216     216       74     203 <td< td=""><td>176</td><td>198 193</td><td></td><td>186 1</td><td>.89 1</td><td>77 19</td><td>36 2:</td><td>15 217</td><td>199</td><td>194</td></td<>	176	198 193		186 1	.89 1	77 19	36 2:	15 217	199	194
91     205     203     171     183       93     2014     202     168     186       87     199     201     161     185       86     196     201     161     186       86     196     201     161     186       85     196     201     161     186       85     196     201     161     186       86     196     201     161     186       87     199     201     161     186       81     196     201     161     178       83     197     197     170     173       84     196     197     170     177       81     196     197     170     173       81     198     197     170     177       77     193     198     197     177       77     193     198     197     177       77     193     198     197     177       77     193     198     197     177       77     193     198     197     177       77     203     205     216     216       77     203     216 <t< td=""><td>179</td><td>191 180</td><td></td><td>187 1</td><td>.86 1</td><td>30 15</td><td>31 2:</td><td>13 217</td><td>210</td><td>196</td></t<>	179	191 180		187 1	.86 1	30 15	31 2:	13 217	210	196
90     204     202     168     186       85     191     201     163     189       85     196     201     161     186       85     196     201     161     186       85     196     201     161     186       86     196     201     161     186       87     199     201     167     181       80     196     201     167     173       81     197     197     174     173       81     197     191     180     173       81     193     193     174     173       81     193     193     174     173       81     193     193     174     173       81     193     193     174     173       77     193     193     193     177       77     203     203     215     219       77     203     216     216     187       77     203     203     216     216       77     203     216     216     216       77     203     216     217     226       74     226     217 <td< td=""><td>183</td><td>183 177</td><td></td><td>187 1</td><td>162 16</td><td>31 16</td><td>33 21</td><td>17 214</td><td>222</td><td>199</td></td<>	183	183 177		187 1	162 16	31 16	33 21	17 214	222	199
89     202     201     163     189       86     196     201     161     186       85     196     201     161     186       86     196     201     161     186       87     196     201     161     186       86     196     201     161     186       81     195     201     161     186       83     196     197     176     173       80     186     191     166     173       81     187     199     197     176       77     193     193     174     177       77     193     193     174     177       77     193     193     174     177       77     193     193     174     177       77     193     193     197     177       77     203     205     215     203       77     203     206     215     216       74     205     216     217     203       77     209     214     217     203       77     203     216     216     216       74     226     217 <td< td=""><td>186</td><td>177 177</td><td></td><td>187 1</td><td>78 1</td><td>96 17</td><td>₹ 5</td><td>10 207</td><td>222</td><td>197</td></td<>	186	177 177		187 1	78 1	96 17	₹ 5	10 207	222	197
68       201       201       162       190         86       196       201       161       186         85       196       201       161       181         87       195       201       161       183         87       196       201       161       186         87       196       201       161       183         83       197       197       170       173         83       197       197       170       173         83       196       197       170       173         80       187       199       197       177         77       186       194       177         77       188       198       197         77       203       216       217       177         77       203       216       216       217         77       203       216       216       216         77       203       216       216       216         77       203       216       216       217         77       203       216       216       216         71       2	189	173 178		187 1	76 1/	<b>1 1 1</b>	5	35 197	216	192
87     199     200     161     186       85     196     201     161     185       84     196     201     161     185       85     196     201     161     185       83     197     170     173       81     197     170     173       82     199     197     170     173       81     187     193     197     170       83     196     197     170     173       81     187     193     197     177       73     186     194     173       74     186     198     197     177       77     193     198     197     177       77     193     198     197     177       77     202     203     197     177       77     203     205     217     219       77     203     216     216     216       77     203     216     216     216       71     203     216     217     229       77     223     216     226     234       64     213     223     243       64     21	190	169 177		1.85	1.25 1.	92 <b>1</b> 7		73 186	201	180
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65     196     201     162     181       83     195     201     163     178       83     197     197     197     176       81     197     197     171     173       81     187     197     174     173       81     187     197     174     173       81     187     193     191     175       79     187     193     191     177       77     193     193     191     177       77     193     193     191     177       76     202     193     191     177       77     203     203     203     203       75     209     200     217     190       77     209     201     215     201       73     205     212     219     216       74     226     212     214     212       71     226     217     219     226       74     226     213     216     212       75     229     228     214     226       64     213     226     234       64     213     226     243	185	171 176	181	180 1	1.25 1.	92 1	74 1	54 173	171	165
84     195     201     163     178       82     197     197     170     173       81     186     197     170     173       83     186     197     170     173       80     186     197     170     173       80     186     197     170     173       73     186     193     187     177       76     188     198     187     177       77     193     188     194     180       76     202     203     203     216     183       77     203     203     215     210     217       74     203     216     215     211     186       75     203     216     215     211     196       71     206     212     214     216     212       71     206     212     216     212     216       71     206     217     226     212     226       71     226     223     216     226       71     229     217     229     234       64     213     226     243     243       64     213	181	173 177	178	178	1.26 1.	11 11	5	54 170	167	160
53     192     199     166     175       63     190     197     170     173       79     186     195     174     175       78     186     195     174     175       78     186     193     187     177       78     186     193     187     177       78     186     193     187     177       77     188     193     187     177       77     193     198     197     177       77     202     203     183     177       76     203     198     203     183       77     203     215     210     217       77     203     216     215     219       77     206     212     219     214       71     226     212     219     212       71     226     212     216     212       71     226     223     216     226       64     247     229     234       64     213     226     243       64     213     226     243	178	175 177	177	176 1	1, 1,	90 11	77 1	57 168	165	155
62     190     197     170     173       61     186     191     186     191     180     173       77     186     191     187     174     173       77     193     195     174     173       77     193     196     187     177       77     193     194     180     177       77     193     196     203     183       75     202     192     216     186       75     209     206     217     219       75     209     206     217     219       76     209     206     217     219       77     209     216     216     216       77     209     211     215     201       71     205     212     219     214       71     226     223     214     212       71     226     223     214     212       71     229     218     226     234       64     213     226     223     234       64     213     229     226     243       64     213     229     243       64 <td< td=""><td>175</td><td>177 177</td><td>175</td><td>177 1</td><td>180 11</td><td>87 13</td><td>8 1</td><td>73 170</td><td>167</td><td>154</td></td<>	175	177 177	175	177 1	180 11	87 13	8 1	73 170	167	154
61     169     195     174     175       79     186     191     180     177       78     186     191     181     177       78     193     187     180     177       76     193     187     181     177       77     193     187     180     177       76     202     192     203     186       75     203     205     215     219       74     209     200     217     190       75     209     201     215     201       71     209     201     215     201       73     205     212     219     214       71     206     212     219     214       71     226     212     216     212       71     226     223     216     226       65     217     229     217     229       65     213     226     234     235       65     213     226     243       64     213     226     243	173	179 178	175	177 1	181 11	36 18	30	77 172	173	156
60     186     191     180     175       79     187     193     187     177       76     203     192     203     183       75     203     192     203     183       75     203     192     216     188       75     203     192     216     183       75     209     200     217     291       73     209     201     217     201       71     205     212     219     214       71     205     212     219     214       71     205     212     219     214       71     205     212     219     214       71     205     212     219     212       71     205     212     219     216       71     205     212     219     221       71     226     223     216     226       66     217     229     234       64     213     226     233       64     213     226     243       64     213     226     243	173	192 180	175	178 1	184 11	95 18	32 1	32 177	179	159
79     187     199     187     17       78     108     194     160       75     202     198     194     160       75     202     190     203     185       74     209     200     215     196       74     209     206     215     201       74     209     206     215     201       73     203     211     215     201       71     205     212     209     214       71     205     212     209     214       71     205     212     209     214       71     205     212     209     214       71     205     212     209     214       71     205     212     209     214       71     206     223     216     228       66     247     229     234       65     213     226     243       64     213     226     243       64     213     226     243	175	184 193	176	180	187 1	87 18	34 11	36 193	185	165
78     188     194     181       77     193     198     194     181       75     202     192     215     183       75     209     206     217     219       73     209     210     217     219       74     209     210     217     219       73     205     212     219     214       71     205     212     219     214       71     205     212     219     214       71     226     212     219     212       70     226     223     216     218       69     247     229     218     225       64     213     228     217     229       65     213     228     217     229       65     213     228     217     229       65     213     226     234       64     213     226     234       64     213     226     243	177	187 185	179	184 1	102 1	88 16	38 1	90 189	190	176
77     193     196     203     183       75     202     192     216     185       75     209     200     217     190       74     209     200     217     190       73     209     200     215     201       74     209     200     217     190       73     205     212     219     214       71     205     212     219     214       71     226     212     214     212       71     226     212     214     216       71     226     212     214     216       71     226     223     216     226       60     247     229     217     229       65     213     229     217     229       65     213     229     217     233       64     213     229     228     234       64     213     229     243	1.80	193 189	183	190	1 861	92 19	<b>33 1</b> ,	34 196	197	188
76     202     192     216     186       75     209     206     215     190       74     209     206     215     201       73     209     206     215     201       71     209     206     215     201       71     209     206     215     201       71     205     212     219     214       71     206     212     214     213       70     226     223     216     218       69     247     229     218     229       65     217     229     218     229       66     233     210     223     233       65     217     229     218     229       65     217     229     217     239       65     217     229     217     233       64     213     226     223     234       64     213     226     243	183	199 194	183	197 2	205 1	<b>3</b> 9 20	1	98 204	204	204
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74     209     206     215     201       73     205     212     219     216       71     205     212     219     214       71     205     212     219     214       71     205     212     219     214       71     205     212     219     214       71     226     221     216     212       70     226     223     216     228       69     247     229     218     225       65     217     229     218     226       66     243     213     233       65     213     228     217     229       65     217     229     218     225       65     217     229     234       64     213     226     234       64     213     229     228       213     229     228     234	190	220 202	204	212 2	35 2:	25 23	3	12 214	221	237
73     208     711     215     210       71     205     212     209     214       71     206     212     214     216       71     206     212     214     216       71     206     212     214     216       70     226     213     216     218       69     247     229     218     226       65     247     229     217     229       65     213     239     228     217     229       65     213     229     217     233       64     213     229     234     233       65     213     229     234       64     213     229     234       64     213     229     243	201	222 208	220	219 2	555 2:	24 2:	31 2	25 220	231	234
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71     206     212     214     212       70     226     223     216     208       69     247     228     217     220       68     247     228     217     229       68     233     228     217     229       68     233     228     217     229       67     233     228     217     239       65     217     229     218     233       65     217     229     234     233       65     217     229     234     233       64     213     229     234     233       65     217     229     234     233       64     213     229     226     243	214	220 213	220	222	52 25	16 23	5	33 233	215	227
70     226     223     216     208       69     247     228     217     220       68     247     229     218     225       63     247     229     218     229       66     239     228     217     229       65     217     229     218     233       66     233     270     218     233       65     217     229     217     233       64     213     229     234       65     217     229     234       64     213     229     234	212	216 212	221	219 2	2 0 5	09 23	3	32 236	202	223
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64 213 229 226 243	233	229 219	237	235	2 661	16 2:	25 2	12 211	222	234
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	243 249	244 228	236	245	217 2	38 2.	34 2	19 227	221	238
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FLIGHT NO. Altitude	ϣͺϐͺϐ;ϧͺϐ;ϗͺ϶ϗ;ϗ;ϗ;ϗ;ϲ;;;;;;;;;;;;;;;;;;;;;;;;;;;	301

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100			373	195				156		163					222	190	236
66			329	172				138		165			165		221	179	225
96	169		252	167	156		180	132		175	190		174	413	223	173	215
26	149		215	169	164		176	137		186	135		181	464	227	171	206
96	149	196	180	172	173		177	141		201	108		191	349	224	170	193
95	157	138	163	174	179		181	149		210	105		203	243	218	168	184
-16	169	189	155	175	183		183	159		205	116		207	197	213	167	178
53	182	191	152	176	185		181	166		193	132		204	170	210	166	174
26	191	192	156	172	184		179	174		179	154		198	156	206	165	172
91	194	131.	163	166	193		172	177		170	179	191	191	151	202	168	174
06	188	149	168	163	181		166	190		167	198	200	186	156	197	169	177
69	179	198	175	159	181		160	185		166	214	193	182	166	192	171	179
88	176	183	190	162	181		158	188		165	211	174	179	179	189	174	182
87	173	181	183	164	181		159	193		166	197	161	179	193	189	179	183
85	171	179	185	169	192		162	198		168	190	160	181	205	187	183	185
85	170	177	186	173	182		165	202		170	179	164	185	212	198	188	186
34	171	177	187	179	183		171	207		174	167	170	186	213	189	191	187
63	174	175	188	186	183		176	210		176	160	180	188	207	190	193	187
82	176	175	189	190	182		182	213		179	167	196	187	200	192	194	188
81	179	176	191	194	193		188	215		182	177	209	187	191	193	195	189
90	183	177	194	197	182		195	216		186	191	211	187	184	195	195	192
79	185	181	197	199	193		202	217		191	202	210	187	179	197	196	195
78	188	195	202	200	184		209	217		193	206	205	189	177	199	198	201
77	193	138	208	205	186		217	219		200	201	190	188	178	199	201	207
76	199	192	217	214	186		225	222		207	209	179	189	184	201	204	215
75	203	199	225	223	189	-	236	226		212	224	185	192	196	206	209	223
74	206	212	231	232	191		244	231		227	222	190	195	215	213	218	231
73	204	219	225	229	200		246	228		231	217	204	207	224	217	223	230
72	202	220	217	224	204		239	224		235	212	209	212	207	214	223	222
11	203	213	209	219	206		236	219		236	198	193	215	200	210	221	217
20	198	203	207	212	202	210	232	210		232	204	219	206	209	209	213	214
69	202	210	211	209	213	207	224	215		234	195	217	208	220	229	216	218
68	210	217	215	206	219	212	228	222		255	202	222	219	212	231	220	218
67	212	218	217	209	223	217	230	223	202	248	549	197	223	229	229	223	216
65	227	219	217	211	227	221	225	230	196	238	217	233	216	235	231	229	228
65	230	227	228	209	232	222	217	235	264	245	222	219	230	235	229	235	231
64	238	238	236	214	236	228	214	233	250	243	544	227	257	239	241	237	231
63	222	241	231	213	240	234	220	238	192	234	223	215	239	211	242	243	239
62	225	243	241	223	245	239	223	238	237	245	252	235	245	281	244	252	250

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KELVIN
DEGREES
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TEMPERATURE

5	3 5	0						26	56	9	92 2	5	5	2 2 2	56	26	27	5	10			t V	26	5	25	54	25	23	24	54	n N	5	20
5 0	246	- 40			1 + 2	6 4 2	256	252	258	254	255	263	259	251	261	274	275	278	25.8			253	250	248	249	249	251	241	247	240	231	224	212
t 3	244	, , , , , ,			11	542	249	253	251	254	258	254	252	260	265	260	263	246			200	272	251	243	245	243	233	224					
60 †	227		127	2.24	642	264																											
47	258		220	2.54	259	247	258	245																									
4 C	247	5.02	111	342	241	232	273	247	261	249																							
4.5	264	ר ת ליו	204	231	251	260	269	253																									
t t	227	202	272	25.7	261	252	253	274	258	258	255	242	25.8	25.8	0 4 6 4 4 6	4 6	202		<b>h</b> / 2														
۴ <u>۹</u>	215	552	5.2	2 32	2.11	228	223	237	248	260	040																						
4 2	242	243	240	オリン	247	275	5	152	251	251		35.4						2 <del>1</del> 2															
4	223	231	2+2	237	144	254	540	254	254	26.2	20.0					2 1	4 I 2	562	260	250	256	250	94.6			4 C 9 t			122		c 2 7	212	612
0 †	242	247	248	243	247	0.9.0	- 1 - 1 - 1	5	264				5 L 5 L			212	228	253	248	256	250	251	1010		4 6	202	1 4 3						
3 G	241	250	246	248	250			1000	5 4 4	- 10				197		5 C	265	261	264	266	262												
38	233	228	243	240	247	25.1		25.5		4 1				192		564	262	262	267														
11	236	225	249	237	24.0	5 1 5 1 6 1	1 M 1 M	240			101	500	192	286																			
36	245	245	247	258	222	100	100	2 1 0				5	<b>8</b> 42	247	256	265	269	258															
35	223	232	242	25.0		0.00	5 0 0 7 7 0				9/2	261	260	257	255	252	246	243	243														
FLIGHT NO. Altitude	61	60	. 0				0 U	C	•	5	52	51	50	<b>6</b> <del>1</del>	81	47	4 C	45	55	<b>M</b> 4		. t	rd -	4	39	38	37	36	35	46	33	32	44 40

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# TAB PRINT-OUT OF TEMPERATURE

KELVIN
DEGREES
N
TEMPERATURE

FLIGHT NO. Altitude	52	5	54	55	56	57	58	59	60	61	62	63	64	65	66	67
100				269												
66 80				294 294												
26				296	203											
96				291	210			177								
36				215	212			C 14	202				216	183		
94				261	209			100			204		221	153	177	
93				243	112		£ 0 7	3 0 4 4 0 0	4 8 4	183	602		227	141	154	
92	191		204	226	÷22		101	101	161	180	212		233	142	144	
91	190		220	213					157	206	199		239	15R	147	
06	199	191	225	202	223			204	160	244	174	181	245	180	156	
83	202	191	122	061			204	203	172	245	163	183	202	196	163	183
88	202	187	197				205	198	185	239	168	184	176	193	174	174
87	189	199	1 1 1 1 1 1		747		216	188	198	212	172	182	174	188	180	101
<b>8</b> 6	177	195	241					182	204	193	182	177	175	181	181	160
85	170	203	150	5 - T	1/1		182	177	203	184	194	170	183	178	180	163
<b>7</b> 0	166	206	241					174	202	182	203	169	191	176	184	211
83	162	207	155	0 / T	7 0 T			173	197	188	206	177	194	177	186	184
82	160	202	162	5.1	1/1			172	193	194	206	186	191	181	191	196
81	161	202	168					175	190	201	200	193	191	156	196	102
80	164	2002	4/1	107	181	188	187	181	191	202	195	194	193	196	202	
79	169	146					0.01	189	193	200	197	194	198	202	202	5 C T
78	175	195	195	+ F C C		404	194	196	196	200	195	196	203	204	215	, v , v
77	186	195				202	197	207	199	202	192	195	210	202	222	
76	192	143	007	C 1 0	000	205	200	216	202	202	192	198	214	204	229	
75	199	0 6 T	c12 222	247		238	203	226	208	206	195	208	218			110
* 1		101	230	247	218	212	205	234	214	211	198	218	112	245		
21	0 <b>1</b> 0 7 7 0	0 - 0	231	238	227	217	205	235	218	216	212	412 412	017		100	210
22	2040	201	227	223	225	219	209	230	219	214	422	212	117	201	2.5	202
21					223	218	208	224	219	214	122	612	200		+ 0	204
11	1020	2 2 2	0 4 G	204	213	218	208	219	218	219	220	213	422		 	1 4
69	202			 	000	218	212	214	216	215	219	219	219		2 U U	
68	236	3 0	0 F 2	, t t t	2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	217	212	217	224	218	236	229	228	672	+ • • •	0 1 0
67	5 . 5 . 1 .		2 2 2	, c , c , c	0.00	220	223	227	234	235	243	238	102	622	010	, r , r
66	0 + 2			 	100	224	230	230	236	237	238	247	1   1	2 2 2		0.0
65	251	22		221	210	224	230	232	239	237	244	251	233	232	110	
64	544	4 9 N		1 1 1	0 4 0 4 0 7 7	224	228	234	243	237	250	253	212	<b>4</b> 62	-1 C 5 F N	
63	234	232		100		225	227	236	249	242	255	259	233	242	237	8.73
62	224	229	142	277	0 D T	/ 1	ļ	•								

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TABLE XXIV (Concluded)

# TAB PRINT-OUT OF TEMPERATURE

#### TEMPERATURE IN DEGREES KELVIN

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Q	23	5	22	25	35	56	52	5	92 92	32	22	26	26	22	33	52	26	26	26	26	26	27	292	2	24							
66	242	245															230	227	238	238	232	230	232	231	230	226	222	228	229	233		
65	250	252	251	265	264	264	259	250	254	251	268	258	262	261	266	267	271	272	266	270	258											
64	250	248	250	262	261	252	263	254	262	257	263	252	261	262	251	247	251	266														
63	259	251	245	544	240	247	252	254	266	264	264	267	271	264	263	267	276	270	266	255	257	248										
62	242	245	246	246	239	261	253	251	259	264	257	269	265	258	263	268	265	277	269	268												
61	245	544	244	240	242	252	257	257	256	256	266	260	277	262	263	262	261	271	269	263	251	247	252									
60	243	249	252	242	247	246	247	255	257	259	267	260	254	268	269	274	270															
53	236	245	241	238	248	549	250	250	267	263	262	270	270	254	256	253	257	265	267	270	267	256	242	243	232	226	222	232	234	237	235	
58	227	233	236	232	232	230	239	235	242	246	246	251	249	248	253	258	259	253	246	253	257	247	233	228	242	544	253	250	237			
57	226	229	230	235	243	248	252	252	243	242	544	248	246	254	554	256	265	265	260	256	249	246	247	249	245	247	237	238	229	229	229	224
56	179	185	184	174																												
55	236	227	249	245	242	256	260	262	269	263	255	261	264	258	262	278	260															
54	245	248	252	258	258	254	255	249	247	245	543	250	245	252	252	256	270	266	258	255	255	257	245	236								
53	229	236	240	242	241	544	248	251	250	543	252	257	261	251	254	260	268	270	261	256	251			239	235	228	249	239	239	233		
52	233	234	230	240	251	250	256	255	246	260	245	262	263	261	266	264	271	270	270	257	250	245										
FLIGHT NO. Altitude	61	60	59	5.8	57	56	5.5	54	53	52	51	50	0		1		1 1 1	E		10 C	1	I	39	99	37	36	35	46	33	32	31	30

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TABLE XXV

# TAB PRINT-OUT OF DENSITY RATIO

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FLIGHT HO. Altitude	4	~'	m	t	ſ	9	~	60	თ	10	11	. 12	13	14	15	16	17
	•	010	Ċ			600 T	024.		006.	1.070	1.030	1.070	1.000	066°		1.000	1.000
	1 <b>1 1 1</b> 1	4 • 4 8 0		. 850		1.120	• 5 • 0		020.	1.070	1.670	1.050	.910	1.010		1.020	1.020
			0.90	0.0		1.693	.700		.980	1.060	1.110	1.020	006.	1.040		166.	ייינ
						1.070	022		. 97 6	1.030	1.180	.980	.910	1.040		1.070	1.070
7							. 420		.960	1.000	1.210	.970	.930	1.020		066.	1.090
96 7	1.000		5 : 5 : 7 :				• •		0.90.	666.	1.220	.950	.900	.980	.960	1.070	1.160
95	1.638	1.0/0	·	1.010		50.0				020	1.220	. 950	.860	.910	.950	1.030	1.100
94	1.610	1.043	.966	1.010		046.				•		020		0.00	930	1.020	1.080
93	066.	1.016	.976	.990		.950	126							820	. R5 0	.980	1.080
92	.95ú	096.	.970	.970		016.	.330		0 0 0 0 0						. 77.0	920	1.040
91	.920	.050	1.000	.930		1.600	0 9 5 •							102.	.730	016.	1.010
90	963.	626.	1.630	.900		1.020	923		150.				. 850	. 810	730	046.	066.
69	.800	.929	1.070	. 640		1.043	026.						. 910		.760	.980	095 .
88	. 880	( <u>0</u> 6.	1.106	. 970		1.673	026.	010	.00	1.010	1.020		.950	690	. 830	1.040	.960
87	.870	.890	1.130	. 870		1.090			. 040				9.40	026.	066.	1.100	.950
86	.860	.87C	1.153	.980		1.1/0	1.400						1.000	.950	920	1.170	.930
<b>8</b> 5	.850	.850	1.170	. 890		1.680					1.010	1.030	066.	.960	. 55 0	1.220	.920
9 t	.840	026.	1.180	.910		1.050	.450		5 U M C			1.020	020	026.	.950	1.270	.910
<b>6</b> 3	.840	. 960	1.140	026 .		1.074	<b>,</b> 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1			•			040	960	930	1.290	. 900
82	. 660	.923	1.183	.940		1.060	026.	0 2 6 .	• 430					070		1.290	. 8.8.0
18	. 840	.920	1.150	.950		1.663	.920	. 940	920	9/6.	1.010		•		028.	1.270	.860
0.6	. 440	.810	1.120	0+6.		1.630	.910	. 380	.910	046.				000	. 860	1.230	. 370
62	.860	. 840	1.160	.960		1.033	. 310	0.56.	116.					860	078	1.180	. 370
78	. 87 Ú	.460	1.073	.970		1.020	.910	1.000	005. 000					.850	820	1.100	. 870
17	.860	. 3 2 0	1.040	066.		1.000	.900	1.004	17.4						800	1.010	.870
76	. 840	. 8 .	096.	1.000		.960	900	006.	. 85 0	. 07			. 850	.830	7.60	. 950	. 860
75	. 820	.870.	066.	1.010		026.	, ju u				000	. 830	.800	.810	7 - 0	.960	. 830
74	. А 3 С	. 35 u	1.000	0/6.		016.				703	906.	. 820	. 800	.800	.7E.D	.970	.810
73	. 850	. j. j.							820	710	. 53.0	. 840	.780	.770	0	066.	. 840
72	. 5 9 3	. 351	1.00						. 850	.740	. 990	.870	.790	.770	.e/0	1.020	. 680
7	002°		1.000					026.	. 886	.760	1.020	.900	.850	.820	956.	1.000	.950
2.2	. 8.50		1.0.10	010 •T			. 55 .	950	. 580	.750	1.630	.920	.920	.920	• 98 <b>0</b>	066 .	.56.0
69	. 790		1.070						. 850	820	.950	.910	016.	066.	.920	1.000	.960
69	.770	. 850	1.640	0.5					.860	609.	1.050	.950	.970	.950	.930	1.010	1.000
67	. 893	. 873	1.143	086.						1.40	1.680	. 950	066.	.980	.930	1.030	066.
66	. ຮອບ	.883	1.150	1986.		055.					020.1	940	.990	066.	.960	1.040	1.010
65	.926	<b>6</b> 36 <b>.</b>	1.170	066.		1.000					1.020	960	1.020	0.20.	066 *	1.050	1.050
64	.98ū	.923	1.160	0.46.							1.100	1.020	1.000	.960	.970	1.070	1.030
63	<b>066</b> .	676.	1.100	.970		.000				1.010	1.030	1.000	1.030	.930	.960	1.060	1.020
62	°66°	.951	1.220	.970		.00	1. JOV	105.	•	~ ~ ~ ~		, , , , , , , , , , , , , , , , , , ,					

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FLIGHT NO. Altitude	຺຺ ຺຺຺຺຺຺຺຺຺຺຺຺຺຺຺຺຺຺຺຺຺຺຺຺຺຺຺຺຺຺຺຺຺຺

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FLIGHT NO.	18	19	20	21	22	23	54	25	26	27	28	29	30	31	32	5 F	7 M
										ć				200		376 .	
100	. 8 00	1.000	1.00		. 580		1.550	1.210			1.124	1.285		1.207	1-2-1	1.230	
5 C		1.1000					1.210	1.150	.620	960	1.116	1.236		1.183	1.257	1.203	
	1.20.	0.1.1	1.170		1.070		1.210	1.140	980	.950	1.116	1.170		1.135	1.210	1.161	
96		1 1 1 0 0	1.200		1.110		1.190	1.120	1.630	. 963	1.124	1.097	1.159	1.097	1.150	1.161	
5 UP 17 (17	066.	1.243	1.210		1.150		1.150	1.110	1.550	.960	1.135	1.032	1.139	1.058	1.096	1.142	
94	1.100	1.303	1.200		1.150		1.123	1.100	1.550	.970	1.131	.985	1.123	1.024	1.054	1.107	
63	1.630	1.300	1.200		1.090		1.380	1.070	1.450	.970	1.127	• 962	1.101	666.	1.023	1.062	
92	1.080	1.263	1.190		1.050	.950	1.050	1.050	1.280	.990	1.121	<b>9</b> 79	1.079	• 979	1.063	1.032	
91	1.090	1.233	1.180		1.000	.943	1.510	1.020	1.100	1.010	1.113	.938	1.048	.961	.987	1.006	
06	1.640	1.17]	1.150		.950	640.	.970	1.000	. 95 0	1.030	1.083	.938	1.004	• 946	. 565	.981	
68	1.620	1.100	1.150		.940	.950	.930	.980	.870	1.053	1.666	.958	.983	.941	. 553	- 90t	
60	1.000	1.090	1.150		.930	.950	.900	.970	.850	1.070	1.052	.961	.962	.933		.952	
87	.930	1,053	1.160		.940	.940	.360	.360	.910	1.070		.966	.936	.918		.936	
90	.970	1.030	1.160		1.000	1.010	.993	1.000	.940	1.070		• 62 •	.907	.897		.917	
85	.930	1.029	1.160		.950	016.	006.	.920	1.000	1.060		.937	.878	.877		.892	
1	.920	1.303	1.170		046.	046.	.790	.910	1.090	1.043		.922	.847	.853		.862	.636
	666.	1.000	1.170		.930	.930	.780	. 890	1.160	1.010		.901	.819	.822	.805	.827	.603
8.2	. 630	066.	1.160		.930	. 940	067.	.870	1.120	.980	1.003	. 88ė	.793	.788	· 777 •	.791	• 566
	. 8.8.0	1.000	1.150		.930	.930	.303	.850	1.060	1+6•	.991	.863	+22.	.748	• 7 4 6	.749	• 534
	. 670	1.200	1.130		.920	.920	.910	.820	.970	006.	£96 <b>*</b>	• 843	.752	.710	.711	102.	.507
62	.680	1.003	1.120		646.	.930	. 8 + 0	.820	.930	.880	1.543	. 532	.747	.689	.691	.631	265*
2 B	. 830	1.000	1.106		.960	.940	. 870	. 810	. 880	.860	.972	. 806	.747	•669	.667	• 654	.481
77	.680	1.703	1.050		.980	.950	096 .	.790	.930	.850	• 942	.761	. 745	.650	• 633	• 625	- 470
76	5.8.5	1955.	985		1.610	.963	.920	.770	.910	.833	.901	.708	• 7 4 6	.632	.601	• 596	.467
		076 -	916	.920	066	.970	0 + 6 •	.750	.860	.830	669.	.676	.747	.630	.576	• 569	• 100
ъ.	840	016.	169.	. 840	.910	.950	.910	.730	.880	. 84 3	• 5 • 0	• 695	.752	• 649	.571	. 553	.476
	640	900	.900	. 350	.880	.920	. 380	.720	.910	.853	.978	.748	. 756	.677	.611	.571	. 202
72		0.06.	0.40	. 870	.896	.930	006.	.750	076°	.870	1.031	• 804	.752	.711	.673	.625	• • • •
	.860	C 7 E .	1.0.20	010.	.946	046.	.920	.790	1.030	.830	1.030	.858	.773	.765	. / 40		
20	. 3.80	.950	1.090	.950	996.	.970	066 •	.930	1.030	.930	1.040	.891	.801	.790	• 796	• 764	. 65 0
. 9	. 673	.956	1.080	. 970	.930	.930	.990	006.	1.116	0.70.	1.061	.860	. 854	• 8 4 6	848.	.621	B17.
	673.	(76.	1.000	026.	006.	.880	0 + 6 •	.91C	1.130	.960	1.058	. 856	.859	.891	. 850	• 6 6 4	<b>5</b> 0.
57	. 83.	1.110	1.050	.950	.910	.880	.933	.920	.926	066 .	1.058	.871	.843	.877	. 893	.850	. 813
		1.060	1.050	.950	.900	.910	• 950	.920	1.070	1.000	1.C82	.869	.870	.885	.919	• 886	248 *
5 G	626.	1.093	1.070	.960	. 880	.930	.923	.950	1.690	1.020	1.037	. 864	.899	.918	. 896	.910	. 885
1 / 1 (	. 950	1-130	1.100	970	.390	.930	.920	1.030	1.010	1.060	1.024	. 866	.918	.920	.920	.921	n n 5 •
		1 1 0 0		1.000	.670	.960	.980	1.040	1.130	1.040	1.674	. 858	545.	.925	.917	. 16 .	606°
29 29	996.	1.120	1.240	066 •	.910	066.	.900	1.050	1.020	1.063	1.062	.891	.973	• 945	• 925	995.	826.

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13	1.150 1.150 1.150 1.150	<pre>4444444</pre>	
19		4 ••••• •••••• •••••• •••••• •••••• •••••	4 4 4 4 4 4 4 4 4 4 4 4 4 4
FLIGHT NJ. Aliitudé	1 3 9 9 9 F 6	្រាល់ ដាម្លាល់ មាល់ ង ប្រាល់ ដាម លំ មាល់ ងា	,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,

# TAB PRINT-OUT OF DENSITY RATIO

CENSITY RATIO

51	.965	195.	1.008	1.034	1.061	1.123	1.158	1.185	1.193	1.174	1.142	1.134	1.114	1.101	1.087	1.074	1.059	1.055	1.038	1.024	965 •	.991	• 44 •	.950	• 923	060.	•859	. 863	.901	£25°	.962	.970	.585	1.022	• 995	666 *	1.021	1.009	.983
50	.925	. 998	1.036	1.070	1.081	1.107	1.124	1.140	1.156	1.143	1.129	1.129	1.116	1.092	1.064	1.030	1.004	086 .	• 965	• • • • •	• 929	• 933	.936	.933	.931	.919	. 688	.876	.884	006*	• 953	• 962	• 963	.970	• 968	•958	.971	• 96 •	276 .
t 9	1.247	1.235	1.193	1.141	1.111	1.107	1.097	1.078	1.058	1.047	1.038	1.050	1.055	1.045	1.646	1.035	1.020	1.003	• 6 8 4	• 364	543	176 .	.941	.952	• 956	. 947	.926	•920	. 947	. 381	1.011	• 939	.946	.967	. 977	1.003	.972	.965	• 996
4 8			• 596	• 4 8 7	•575	.776	.918	1.055	1.161	1.232	1.211	1.157	1.083	199.	.926	.870	.843	.843	.855	.879	- 902	.951	.990	1.015	1.012	.981	.910	.879	.963	1.020	1.009	.977	1.040	•98•	.975	.986	066.	1.155	.882
47		1.2.1	1.164	1.129	1.071	.991	• 946	.936	.936	.947	.950	.963	.976	.981	010.	• 6 4 4	.935	.919	.913	706.	.901	.916	•926	.947	•966	.977	.984	276.	-942	846.	1.009	1.028	1.000	1.002	1.063	1.025	.930	1.013	1.009
46										.920	.849	. 866	.957	1.052	1.079	1.074	1.053	.997	.912	. 338	.805	. 808	.931	106.	. 958	.989	.992	• 9+8	• 945	1.024	676 .	.972	.970	1.135	.986	1.084	1.063	1.159	1.089
45			. 653	. 551	1.290	1.511	1.535	1.452	1.296	1.124	.991	.895	.880	.921	• 546	666 •	1.077	1.149	1.122	1.066	.982	• 935	• 324	.953	• 923	. 866	e79.	e05 •	.940	1.632	1.035	1.113	1.123	• 925	1.075	1.089	1,009	1.129	1.024
t t	1.126	1.120	1.043	1.034	• 952	. 892	. 891	.919	.978	1.023	1.041	1.063	1.083	1.097	1.102	1.096	1.094	1.075	1.058	1.039	1.017	1.000	1.007	.984	• 962	.951	. 391	.878	.865	. 867	.886	.889	.820	. 845	.889	.874	. 892	846.	.921
£ 7																																		.861	.927	.712	. 758	1.018	. 866
42	1.086	500 · T	1.455	904•I	1.538	1.528	1.467	1.429	1.366	1.336	1.290	1.255	1.223	1.185	1.138	1.091	1.043	1.002	.959	.923	. 990	.830	. 975	.867	. 855	• 339	.818	. 932	.852	.881	.938	.938	.931	£ †6 °	.938	• 935	.963	.960	.981
41				160.	.893	. 375	. 3ot	. 362	.970	166.	.927	<b>5</b> 89.	1.011	1.030	1,035	1.033	1.012	.997	.959	.921	.878	. 954	. 829	.799	.769	.729	.703	.690	.738	.717.	. 734	.771	. 77 .	. 776	. 810	. 360	• 902	.910	.925
																															. 879	.914	.917	• 35 •	.930	816.	.946	-945	• 947
39			1.1.55		1.0/1	1.032	1.014	<b>266</b>	.978	016.	•962	.963	.963	.957	.951	.949	.943	938	.941	•934	.932	.948	.963	186.	1.005	1.016	1.031	1.014	1.018	1.032	1.084	1.059	1.053	1.558	1.060	1.051	1.059	1.062	1.061
38	• 311		1.000		1.012	• 999	1.001	• 993	1.011	1.051	1.073	1.118	1.123	1.130	1.117	1.095	1.065	1.023	.933	.360	.931	.927	.931	.917	. 885	.851	. 319	.830	. 852	.833	.930	.969	1.013	1.028	1.054	1.101	1.111	1.153	1.144
37	. 563	- -		100.	295.	1.090	1.172	1.231	1.217	1.173	1.145	1.116	1.070	1.059	1.041	1.031	1.021	1.037	• 993	576.	.945	<u>1</u> + 6 •	.925	.903	.872	. 0 4 6	. 318	. 344	.892	.931	•96•	.973	.977	566.	1.018	.995	.931	1.029	1.005
36					1-042	1.932	1.014	196.	.959	546.	.927	<b>+</b> 26 •	146.	.951	.963	• 26 •	.330	266.	956 .	966.	-992	• 935	666.	1.002	1.963	196.	. 011	.925	.929	. 375	1.053	1.043	1.035	1.350	1.077	1.356	1.043	1.046	1. 355
35				779 T	1/1 •1	1.049	.987	.919	. 856	.823	. 833	.865	.847	100.	.92.	.937	.941	.935	.926	.910	.891	.637	663.	•69•	.633	.881	. 5.84	.905	.935	.958	1.012	1.612	1.612	1.032	.992	666.	. 585	1.082	1.105
FLIGHT NO. Altitude	150				0.0	46	•6	63	92	16	06	69	Ċ.B	87	Å٥	92	g t g	83	82	81	8 C	52	78	17	76	75	74	73	72	71	76	69	68	67	66	65	÷9.	63	62

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# TAB PRINT-OUT OF DENSITY RATIO

	51	1.006	1.076	1.047	1.066	1.094	1.030	1.091	1.059	1.045	1.047	1.068	1.103	1.105	1.073	1.070	1.073	1.021	1.060	1.016	1.026	1.053	• 995	<b>9</b> 88 <b>•</b>	- 387	1.015	.963	1.022	.975	• 956	.963	. 938 1. 082
	50	.980	999.	.985	166.	1.025	1.029	1.017	1.034	1.033	1.063	1.064	1.036	1.060	1.100	1.055	• 995	<b>87</b> 6.	.953	.971	<b>766</b>	1.004	1.003	• 999	.981	.969	.942	• 965	.926	• 933	.954	1.034
	4 9	1.008	1.048	1.096	1.162	1.086	1.097	1.097	1. 395	1.124	1.127	1.117	1.138	1.154	1.125	1.102	1.113	1.095	1.162	1.093	1.122	1.153	1.101	1.125	1.102	1.099	1.131	1.158				
	80 †	1.100	1.101	1.037	1.104	1.069	1.023																									
	4 7	.963	1.029	1.017	1.080	1.013	1.069	1.035	1.107																							
	4 Q	1.052	1.148	1.098	1.089	1.132	1.191	1.024	1.145	1.108	1.163																					
	u t	.986	1.051	. 978	1.121	1.074	1.045	1.022	1.098																							
	t t	1.016	.832	616.	.931	.925	.969	+16 •	-912	.972	.981	1.001	.979	1.005	.973	• 364	1.028	.975	.925													
	5 1	.573	71	8 O S •	• 9513	. 937	1.018	1.067	1.028	195.	. 971	1.356																				
0	. 42	.981	.989	1.018	1.016	1.021	1.057	1.061	1.054	1.073	1.089	1.095	1.126	1.098	1.107	1.119	1.103	1.152														
I TAS YI	ч т	<b>:</b> 36 <b>:</b>	• 341	.913	• 35 9	.937	.915	. 946 .	646.	<b>†</b> 36 •	.929	• 3+6	.915	. 316	.977	426.	.375	.973	.937	. 365	.933	446	.949	* 0 * *	. 361	1.010	.971	.991	.991	19E .	1.013	1.030
DENSI	5 7	.953	. 543	.954	. 543	.996	1.030	1.015	1.054	<b>3</b> 66 <b>.</b>	1.678	1.045	1.071	1.078	1.043	1.031	1.051	1.067	1.084	1.038	1.057	1.639	1.036	1.016	• 993	1.028						
	€£	1.098	1.071	1.039	1.105	1.111	1.136	1.086	1.107	1.132	1.105	1.094	1.199	1.102	1.132	1.115	1.102	1.110	1.085	1.064	1.065											
	3.6	1.124	1.172	1.118	1.153	1.134	1.087	1.110	1,092	1.076	1.064	1.139	1.398	1.140	1.104	1.129	1.128	1.125	1.093													
	37	1.045	1.123	1.072	1.099	1.107	1.033	<b>†66</b> *	1.104	1.084	1.167	1.050	1.087	• 993																		
	36	1.062	1.076	1.083	1. 3.7	1.360	1.069	1.085	1.064	1.093	1.096	1.1.1.4	1.117	1.177	1.145	1.105	1.080	1.112														
	35	1.145	1.123	1.693	1.036		1.013	1.624	1.014	.991	1.033	1. [50	1.453	1.090	1.104	1.124	1.146	1.159	1.155													
	FLIGHT NO. ALTITUDE	61	60	53	58	57	5ú	55	54	53	52		5	49	<b>6</b> 4	47	4 6	4 U	t	M 4	t.	t t		65	3.5	27	36	35	ar i M	5 I	25	16

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65	• 918	1.112 1.245 1.286 1.286	959	1.025 1.025 1.038	1.017 .975 .944	6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6	
t Q	1.165	1.003 .928 .7928	1.057	1.079 1.035 .982 .956	9640 949 949	00000000000000000000000000000000000000	
63		982	- 963 - 964 - 966	. 995 1. 044 1. 065 1. 022	. 969 . 925 . 930	17 17 17 17 17 17 17 17 17 17 17 17 17 1	
62		1.010 .950 .905 .924	1.138	1.053 .980 .917 .684	.863 .871 .871		00000000000000000000000000000000000000
61		1.226 1.235 1.054	. 794 . 660	.926 .963 .974	. 893 . 853 . 851	0 - 1 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	99990 9999 9999 9999 9999 9999 9999 99
60	9 4 0 0	1.010 1.132 1.132 1.722 1.722 1.722	11.1 1.1 1.1 1.1 1.1 1.1 1.1 1.1 1.1 1.	. 914 . 912 . 897 . 894		••••••• •••••••• ••••••••• •••••••••• ••••	• • • • • • • • • • • • • • • • • • •
59	1.024 1.104	1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 -		959 958	958 956	2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	04200000000000000000000000000000000000
53		. 338 . 915 . 909	. 753 . 661	- 705 - 764 - 784	100 100 100 100 100 100 100 100 100 100		
57					613 613	. 801 . 801 . 796 . 794	. 787 . 787 . 864 . 864 . 864 . 996 . 996 . 997 . 9977 . 9977 . 9977 . 9977 . 9977 . 9977 . 99777 . 99777 . 99777 . 997777 . 997777 . 997777777777
56	1.153 1.091 1.049			.988 1.010 1.010	- 225 - 232 - 232 - 232		
55	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	. 835 . 935 . 916 . 716	967 1985 1986	1.004 1.010 1.010	. 973 . 973 . 973	. 955 . 927 . 832 . 750 . 750	. 780 . 8837 . 8837 . 9994 . 9947 . 99437 . 1981 . 1981
5 D		- 754 - 754 - 703	• 753 • 753 • 899	1.053 1.078 1.086	1.010 1.010 1.010 1.010 1.00 1.00 1.00	• • • • • • • • • • • • • • • • • • •	
53		1.003	1.005 .983 .983			. 863 . 856 . 913 . 925	
25		9990 9950 9950 9950	.777 .777 .819 .875	918 949 949	1.040 1.040 1.040 1.047	1.024 1.011 1.004	4 9 9 9 9 9 9 9 9 9 9 9 9 9
FLIGHT HO. Altitudé	1 9 9 9 6 6 6 9 7 9 6 5	5 0 0 0 0 0 0 5 0 0 0 0 0 0		6. 3 M C	25 18 79 0 79	8 T 2 2 2 4 8 7 8 7 8 7 8 7 8 7 8 7 8 7 8 7 8 7 8	

TABLE XXV (Concluded)

# TAB PRINT-OUT OF DENSITY RATIO

ļ	67	1.042	1.007		1005	1.00.1	1.017	866.	1.030		1.100	1000	1.092	1.093	1.068	1.050	1.094	1119			1.000	1.035	166.	666 .	<b>996</b>	<b>* † 6 .</b>	.958	1.027	1.003									
	66	.916																			166 .	1.013	.970	.967	. 992	1.000	100	000	040			1.016	.992	.971	.939			
	65	266.		1111	1.001	.959	.968	976			1.053	1.047	1.071	1.010	1.056	1.041	1 1 1 2		1.000	1.0.1	.980	.963	.971	546	179.													
	t 0	057		オング・	.977	- 942	.950	900	•		1.005	.986	1.018	1.000	1.055	1.076			1.0.0	1.089	1.066	-992																
	63	900		• 96.5	866 .	1.018				1.032	1.039	1.003	1.018	1.023	1.016			1001	1.032	1.4008	.963	.968	. 971	000			044 .											
	- 52	020	•	• 579	989	1.001			a. 16.	1.016	1.040	1.022	1.612	1111	000			1.545	1.024	666 .	. 997	939	011		076 •													
	61		646.	. 972	486.	1015			f 66 .	.991	1.004	1.022	1.034			6 T N • T		1.014	1.010	1.036	799.	94.7		4 C 7 C 7 C	142.	296.	• 665 •	• 956										
	5 G		. 965	956.	054			י די די	1.021	1.033	1.013	010				1.022	1.653	1.006	966 "	. 970	977																	
0	63		• 366	. 9.44	0.74	r	1004	6/6.	.991	1.000	1.017	190			1 1 7 1 7	• 995	.966	1.032	1.022	120.1		++0 • <b>+</b>	1.5.	.951	.928	, 919	310	. 967	. 971	1.008	1.027			0 F F -	.971	M+6 *	.946	
FY RATI	ίς		646.	346			<b>976</b> •	1.001	1.031	1.017					1.000	1.043	1.063	1.082	5 4 3 4 4 7 4 5				1.142	1.059	1.029	1.033	1.032	1.092	1.110	1,039	710.4	4.0		146.	.992			
LENSI	29		572.	040		956.	1.000	.086	.980	010	5 - C - C - C - C - C - C - C - C - C -	• • • •	1.543	1.0.1	1.075	1.070	1.689	1.568		40.00	1.000	1.115	1.CUZ	1.010	. 1.015	1.031	1.033	1.619	995	000.1			1.004	.985	1.008	165.	.992	1.011
	56		1.511		166.1	1.655	1.862																															
	55		1 017		1.10.1	1.001	1.026	1.055			1.008	1.0.4	• 392	1.020	1.061	1.048	1 . 01.7			1.024	.992	1.038																
	.ສ ເມ		i C	•	245.	676.	- 937	110			516.	1.012	1.038	1.004	1.084	1.608				1.046	1.061	.997	666.	1.017	7 1 0 1 1					r + ∩ + 7								
	53			101.	.983	136.	105	000		11001	1.015	1.017	1.039	1.357	. 1.154				1.0/3	1.070	1.340	699.	. 175	000						1.00	1.055	1.052	.959	186.	69C .	~~ 0 .	•	
	55			1.022	1.543	1.077	1 1 1 1 1 1 1 1 1		1.00	1.042	1.032	1.044	1.192	1-654	1.178			1.004	1.[78	1.055	1.051	1.010	700.					7.040										
	FLIGHT NO.	ALTIUUE		61	60	10			74	56	55	54	53				2	64	4.5	47	46	1	4 d 7 d	t t T -	יי די	t.	-1- t		39	38	37	36	2 U 2 M	) 	<b>*</b> •	n (	25	30
TABLE XXVI

													r 0	0 e	•		<u>.</u>		<u>^</u>		<b>n</b> •				56	35	6	+	ور	N	æ	ņ	Ģ	Ģ	Ņ	Ņ
	σ												Ċ		-	20			_ i		50		200	0	0 20	0 26	0 27	0 26	0 25	0 25	0 24	12 0	1 24	0 24	72 0	0 24
													ŭ	10.01		10.00		10°01					94.00	17.00	37.50	49.00	51.00	49.60	+5.00	38.00	31.00	25.00	21.00	15.00	10.00	00.60
													5.3	- 0			2.	0.				<u> </u>		37 1	22 1	1 1	19	17 1.	- <b>1</b> 61	1 1	1 1	1 1	17 1	.e		1 2
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													20.00								20.00 20.00	20 · 00	39.00	37.00	20.00	22.00	30.00	42.00	51.00	62.60	72.00	77.00	74.00	65.00	58.00	50.00
													16.0	147	1 22			110		0 0	1		303	282	273	272	274	277	257	243	219	201	189	199	219	238
													000											000	000	0 C	000	000	000	000	000	000	000	300	000	000
	÷												30.5				• · · ·	•	•			0	14.	54	35.	43.	47.1	47.		24	39.1	31.(	20.1	11.(	11-	
	ų												97	96	0	40	0	, .		0	404	191	206	199	192	155	120	6	51	23	307	253	227	214	215	229
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# TAB PRINT-OUT OF WIND SPEED AND DIRECTION

HIND SPEED AND DIPECTION

СМТ 410. ГТТИЛГ	*1		<b>N</b> .	-	<b>P</b> 7)		t.	2.	10		υ	~			•0		
210.02	1 2.2	557.000	982	163.000	11	60°.90	277			<b>5</b> 0.000	240	15.000	289	38.000	254	119.000	243
231.001	0 2AF.	247.000	282	A9.000	35	49.000	263	133.010	246	61.000	233	32.000	287	32.000	254	128.000	674
276.00	0 293	242.013	297	66.003	102	30. 00	265	135.010	292	57.000	223	39.001	277	36.000	245	127.090	255
224.00	3 282	245.000	282	FC.00J	ę.	27.00	279	133.000	277	50.000	216	33.00.	258	44.000	222	124.000	256
229.00	9 2 R.F.	000.045	241	P1.700	101	25.000	247	134.0110	276	32.000	228	10.005	196	27.000	223	123. N 10	250
247.03	642 6	757.00	23 4	01.000	103	15.00	225	134.000	276	39.000	272	21.000	142	16.000	24.3	124.000	251
100.354	289	264.000	28C	87.900	99	19.000	300	137.000	263	47.000	283	35.000	152	23.000	232	130.030	257
261.135	782 (	747.000	579	89.300	76,	24.000	30.8	143.000	264	39.000	284	5+.000	133	18.000	217	126.000	252
160.036	402 6	748.000	2.8.2	91.300	11	5.000	213	133.000	242	54.000	264	62.000	111	13.000	192	129.000	259
254.03(	502 6	247.009	744	<b>89.030</b>	f J	26.COD	173	127.300	271	63.000	250	47.000	96	A.000	261	129.000	262
243.03	3 293	257.900	282	000.100	-1 F-	32.000	151	1 34.930	267	67.000	265	45.000	66	22.000	230	121.000	255
224.03	28.9	243.000	285	000.70	74	32.000	118	134.000	250	73.000	264	37.000	102	3.000	312	109.000	253
230.000	290	254.000	293	94.787	(ب: ه	16.000	101	119.330	256	71.000	266	38.000	06	17.000	339	99.030	263
25 · C 3 (	3 296	260.300	511	72.300	t B	2.000	3°	117.040	259	70.000	261	50.000	92	12.000	192	92.030	258
224.001	1 2 <del>0</del> 2	264.010	294	76.300	ທ ຊ	600.00	357	113.030	265	7A.000	256	100.04	85	26.000	234	A3.000	275
264.096	235	261.010	500	70.000	5	5.600	₽.	102.010	263	7A.000	245	49.000	105	22.000	178	73.000	262
164 . 0 0	28.9	231.050	2 8 2	54.000	e F	8.000	288	98.000	267	54.000	245	40.000	84	24.000	123	58.030	273
201.07	291	713.000	2 4 4	45.000	A 7	11.090	273	91.000	263	54.000	263	35.000	107	19.000	64	78.000	267
		203.900	5 T	47.000	69	17.000	264	91.000	252	52.030	22 0	55.000	86	10.000	60	54.002	245
		1.9.300	998	43.000	55	14.003	252	63.000	265	34+000	232	53.000	50	10.000	187	54.000	277
		145.703	7 8 7	44.300	100	19.600	227	84.300	2A1	30.090	266	43.000	77	30.000	108	68.000	270
		175.303	24.8	42.000	75	9.003	249	R1.000	281	41.300	292	32.000	62	22.000	56	43.000	255
		171.003	273	21.000	44	9.000	223	101.000	276	36.000	286	47.000	92	32.000	55	40.00	286
		157.360	241	36.000	94	13.000	160	85.000	262	34.000	256	52.000	107	25.000	44	46.000	284
		159.003	294			2.000	195	82.000	255	34.000	264	48.000	100	22.000	346	42.000	270
		151.903	644			11.000	280	79.000	257	31.000	241	37.000	96	0 0 0 0 U	241	36.000	262
		153.030	282			23.600	308	90.000	272	28.000	245	27.000	92	9.000	156	36.000	274
		159.000	279			20.000	245	80.000	271			29.000	96	11.000	72	34.000	274
		169.000	290			000.6	176	69.000	267			24.000	103	16.000	68	19.000	255
		144.009	277			11.000	126	68.000	269			27.000	95	14.000	86		
		121.003	979			7.000	0	63,000	268			35.000	107	17.000	0.2		
		107.000	279			11.000	65	54.000	59			25.000	79	•	•		

# TAB PRINT-OUT OF WIND SPEED AND DIRECTION

	•0	267	258	254	253	250	251	251	262	262	263	1/2	565	260	260	265	259	253	254	258	256	266	263	252	263	265	268	264	266	246	267	267	255
	-	157.003	150.000	151.000	162.000	159.030	141.000	138.000	139.000	138.000	139.000	137.000	132.000	125.000	125.000	130.000	135.030	138.000	127.000	116.000	132,000	129.000	125.000	123.000	115.000	103.000	91.000	89.603	77.000	69.000	80.000	74.000	64.000
	~	257	249	544	246	250	256	260	259	254	270	271	256	257	250	252	246	247	243	253	263	268	574	279	285	273	264	273	258	253	257	246	234
	-	RF.300	116.000	142.000	150.000	152.000	149.000	147.000	175.000	138.000	141.000	137.000	129.000	129.000	127.000	124.000	126.600	116.000	121.000	102.000	110.010	124.000	111.000	119.000	121.000	104.000	94.000	106.000	66.000	85.000	84.000	73.000	54.000
	÷	246	245	251	250	250	265	258	2 t 5	235	534	247	290	282	276	250	245	312	245	279	267	249	243										
	Ŧ	70.000	68.00C	65.000	59.000	47.000	53.000	64.000	20.000	57.000 ·	49.000	51.000	45.000	37.000	40.000	29.000	25.000	23.000	26.000	58.000	36.000	46.000	35.000										
		5 <sup>+</sup>	25	22	25	22	15	15	16	53	25	28	11	28	30	23	23	20	55	28	6 2 7	<b>3</b> 9	33	02	5	5	23	30	12	21	16	22	62
	-	179.000	169.000	167.000	166.000	153.000	143.000	139.000	1 3 A. 000	141.000	156.000	151.000	156.000	150.000	145.000	155.030	148.000	132.003	130.000	125.000	128.000	114.000	107.000	134.000	102.000	95.003	94.000	86.000	84.000	78.000	500044	84.000	86.000
		25	26	54	19	19	25	ŝ	54	20	19	22	20	22	5	20	℃	82	32	31	27	<b>6£</b>	56	22	32	27	25	2 € 1	54	30	m	14	22
	1.	15A.000	159.00	157.00	150.(00	154.00	142.000	138.400	140. 100	154.130	162.400	159.300	155.300	146.300	137.000	144.003	142.000	137.000	130.000	129.000	131.000	119.000	111.000	107.000	98.000	91.000	97.000	94.000	94.000	84.000	91,900	84.000	85.000
z	~	25	27	25	19	21	27	29	<b>₽</b>	24	6L 71	02	18	17	5	21	19	6 ()	4	5 E.	30	6	2	26	37	45	31	29	12	26	~	11	18
DIRECTIO	-	15A.000	151.000	154.000	159.000	149.000	143.030	13A.000	142.000	159.000	147.500	141.030	141.000	137.000	129.000	000.611	143.000	134. 500	140.000	132.000	129.000	120.633	111.000	103.000	104.000	89.000	69.600	87.000	91.000	80.000	95.000	81.000	82.000
CNA D	2	201	100	196	193	197	193	191	193	197	1 ° 0	180	198	4 5	191	191	171	177	172	1.5	219	199	2,18	220	210	211	204	204	209	203	208	206	
ATNO SPIE	<b>4</b>	900.000	89.300	67.000	96.003	P5.001	A2.000	78.900	68.130	69.109	FC.003	60.000	F0.300	64.000	54.070	61.300	F6.300	65.000	64.000	40.990	4 8.000	55.000	55.200	71.000	A5.003	000.10	96.300	97.000	91.003	P. 2000	7 A.000	A1.000	
	-	269	512	2 €, A	255	25.3	249	24.2	222	233	622	241	250	50	255	258	241	- M - M - M	212	235		75.4	262	270	272	5 4 4	25.8	260	262	264	25.3	264	262
	4	95.000	93.007	95.000	95.000	95.003	84,000	A7.000	000.47	64,09Q	63.935	63.303	45.000	69.100	61.000	79.903	67-000	64.000	67.000	100-1-1	10000	50°°°5	57.200	6.0.00	97.000	92.090	000 . 6	94.000	95.003	94.000	94.300	79.000	70.000
	C'	26.32	5	20	25.2	25.9	254	524	5	256	261	267	26.5	257	260	•																	
	+4 • 1	149.200	152.039	157.070	155.033	145.032	15.3.000	157.030	155.039	150.000	177.000	180.030	177.300	1.45.015	181-000																		
	FLT5HT 11 ALTITU0	£.1	i C V			22	9	5	t. U	5 2	5.5	. <b>.</b> .	5	0	- -	1.7	1	: -3	1		5		- C		- <b>40</b>	4.4	9 2	R.	46	1			06

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											243	238	234	231	228	422		6 6 6	257	340	337	505	304	925	315 1	260 1	233 1	224	299	243	237	777
	26										86.000	83.000	78.000	71-000	63.000	52.000	39.600	24.000	2.000	8.030	15.000	21.000	000 02	35,000	34.000	42.000	44.000	15.000	000.6	10.000	34.000	14.000
	10										232	223	217	212	207	204	002	198	202	216	248	2 H I	992 992		277	270	268	270	281	290	462 162	607
	2										61.000	65.000	69.003	72.000	73.000	73.000	72.000	68.000 67.000	52.000	43.000	39.000	57.006		1 70.000	195.000	180.000	151.000	134.000	135.000	142.000	145.000	1 35 • 0 00
	t										234	246	260	270	279	287	293	162	302	303	303	200£	462 462	180	284	293	275	274	275	276	271	269
	2										101.000	100.000	137.000	109.000	117.000	126.000	134.000		142.000	136.000	125.000	116.000			000-68	90.000	87.010	90.000	96.000	103.000	107.000	116.000
											92	5	92	8 6	87	8 Q	28	75	90 -1	15	327	305	297	000	294	290	284	280	284	262	294	062
	N										17.000	24.900	32.000	3A . 000	42.000	43.000	1000 • 2 • 1	40.000 46.000	29,000	27.000	28.000	4.8.000	73.000		100.000	000-26	86.000	79.000	79.000	90.000	107.000	121.000
z	2										316	296	248	19 A	173	153	141	126	г м 5 б 1	8.2	58	0 t	F 6 6		1 C C	198	210	221	235	252	264	267
DIRECTIC	2										30.00	17.030	11.090	13.000	16.000	19.090	19.000	20.00	21.000	21.000	22.00	18.000	4.000	5000°62		65.000	70.090	82.000	57.500	86.003	92.000	91.000
UNA U	•																			82	975	300	802	100	245	;;	4	36	329	398	305	311
VIND SPEE	2																			A.300	12.000	17.909	20.030		35,000	42,000	41.000	35.000	36.209	47.500	56.000	4 A . 000
-	Ð										305	321	122	337	341	346	4 c 1	155	. <b>r</b>	. e.	38	47	10 1 1	5 P 5 V	- <b>- -</b>		101	111	111	106	102	101
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	σ										242	540	542	122	225	217	207	192	1441	111	19	19		562	100	106		27.9	25.9	26 A	272	274
											24.000	15.000	0-0-20.	96.0.30	89.030	75.010	51.039	47.000	20.0.00	27.630	24.010	21.095	42.009	F9.00	000 411			143.000	17.000	L36.030	131.300	144.000
	FLIGHT ND. ALTITUDE	190 99	46 70	95 0 F	4 7 7 7	н: • Ф	0. C	90	6 E	2 H H	35	3 t	* *	92	<b>٩</b>	0 £	79	«   	- <b>-</b>	. V	74	74	72				57	99	-	54	53	62

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	2	319	339	119	100	71	69	27	103	122	119	111	72	57																			
	~	51.000	15.000	12.000	14.000	20.5302	14.000	9.030	24.000	47.000	40.000	25.000	16.000	19.000																			
	.0	187	208	299	293	267	273	277	267	262	270	269	261	250	259	254	259	263	269	268	269	296	269	544	199	188	244	289	305	282	264	311	241
	Š	20.000	0.00.0	14.000	-30 • Ú D D	51.000	62.000	74.000	82.030	85.000	107.000	107.000	000.06	86.000	93.030	95.000	82.000	72.000	69.000	53.000	54.000	29.000	37.000	22.000	12.000	20.000	9.000	15.000	16.003	21.000	26.000	19.000	18.030
	10	2 A O	270	263	263	265	275	275	257	258	265	265	276	281	287	277	275	277	274	258	269												
	₹,	114.000	104.000	102.000	93.000	84.200	84.000	85.009	A5 .003	90.000	95.000	100.000	104.000	119.00r	133.000	137.000	144.000	139.000	127.000	113.000	109.000												
	4	254	263	264	269	256	254	241	241	243	249	264	266	253																			
	~	127.000	131.000	129.000	109.000	109.000	104.000	100.001	89.000	87.000	89.000	A2.000	79.000	77.000																			
	<b>m</b>	289	291	662	288	276	270	279	277	269	266	263	253	258	260	269	268	271	259	263													
	<b>N</b> :	133.400	130.000	119.°C3	107.100	92.000	99.100	91.300	87. 300	92.390	8.9.00	75.000	71.900	73.300	75.000	76.002	72.000	67.000	67.000	67.300													
z	٩.	265	260	263	270	26 F	255	247	8 M 2	240	244	249	251	252	246	243	242	240	247	255	264												
DIPECTIO	<b>∼</b>	A6.J00	34.000	91.000	112.000	123.000	124.000	126.000	119.000	107.600	108.033	105.000	109.000	113.000	130.000	115.000	1.14.000	96.000	92.000	103.000	. 86.000												
04V U	<b>*</b> *	314	5 4	79	0 ř.	35	168	153	156	145	148	159	179	103	107	117	<b>6</b> 6	76	75	41	110	0	<b>6</b> 3	96	8 t	9 T	96						
WIND SPEE	~	24.000	100.01	46.009	000.04	20.100	22.300	18.009	35.003	44.000	41.900	26.000	21.900	45.003	47.000	52.000	84.000	47.700	18.700	21.000	41.000	76.900	57.000	65.000	36.900	53.000	46.000						
	5)	108	114	114	119	116	100	9	3 8	£	8 8	95	82	7 8	81	۲. ۲	88	87	68	88													
	0	152.000	154.000	157.063	165.003	159.900	151.000	152.000	149.000	137.000	1 2 2 . 0 0 0	124.009	171.003	111.000	107.500	114.900	102.000	102.000	85.900	92.000													
	c	2F 5	25 A	252	247	251	202	247	200	2 E. O	254	26.8	202	259	760	252	527	2:04	760	261	754	25.3	257	2 × 0	25.9	26,3	271	529	272	293	257	245	254
	•	147.900	155.000	156.000	147.030	1*5.000	129.950	124.000	128.030	17.000	134.000	139.906	131.500	122.090	123.000	1 2 2 . 0 0 0	176.000	1 79.010	133.000	1 2 1 . 0 0 0	124.030	121.930	124.030	120.000	113.000	1CP.030	91.000	000.10	A2.000	87.000	77.000	67.030	62.000
	FLIGHT "	<b>61</b>	60	ц С	5 3	57	5 G	и. И	5 L	5.3	52	51	5 C	64	<b>1</b> 3	47	т. т.	1. 1-	44	F 4	£ 3	14	4 0	0 F.	3.5	37	35	35	at Pi	5	32	11	30

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	114.950	130			154.090	60 . • † •	102.350		103.050							
•	110.553				153.720	) t † t	114°510	t t	121.440	0 J			141.830	251		
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	34.720	128			173.620	К. н М	147.290	14	147.700	<u>,</u>				240	166 760	æ
t	9 U - 2 U C	127	?64.]40	159	171.400	28	152.460	4	149.230	16			100.00	100		
m	81.779	129	234.0A0	154	162.730	°5	154.170	4-12	148.490	16						, u , N
0	75.510	132	205.560	€1 ₽;	150.200	21	152.270	40	145.470	16				2007		
ς σ	69.253	136	178.459	37	132.920	18	147.420	<b>£</b> £	140.400	15			32.540	5020	51. 51. 51.	
0	61.000	543	152.310	с т	111.560	13	140.570	27	133.790	15			30.010	2/2		
-	51.450	154	127.930	64	86.45O	21	130.390	22	125.960	44			36.490	582		200
5	600.44	170	104.323	5.5	62.250	28	117.440	е Г	116.770	13			45.610	262	129-21	
17	066.04	192	P1.553	£ 0	41.100	41	100.770	16	105.370	13			54.090	462		
51	44.047	215	61.J2 D	55	27.020	76			95.670	44			61.160	293	024.55	
	51.A00	2 2 3	79.91Ŋ	<u>م</u> م	27.940	122			84.230	15			67.670	562	37.900	2 2 1
	61.625	245	21.330	97	35.720	149			71.050	19			72.870	598	42.640	
	71.310	202	7.480	146	67.933	164			57.380	25			75.953	302	46.010	211
	1000.02	252	16.403	226	60.070	173			43.790	34	117.280	348	77.000	308	49.020	
	95.4 25.4	261	30.150	24.2	70.4.60	190	14.480	151	31.440	t-0	j20°26	350	77.090	314	52.280	50
727		265	42.533	549	80.250	197	30.960	172	20.290	62	76.240	356	75.900	320	56.040	5
^	97.450	269	52.900	254	90.100	193	48.740	179	11.190	103	62.515	ŝ	76.500	328	59.750	
• •	94.103	27.3	61.450	259	98.51D	201	<b>55.</b> 360	184	14.310	177	53.750	17	78.990	τ <u>ι</u> τι		0 4
1	95.409	277	67 <b>.</b> 950	254	106.590	209	79.070	191	29.470	204	58.770	62	0 4 4 ° 5 8 ° 6 ° 6 ° 6 ° 6 ° 6 ° 6 ° 6 ° 6 ° 6 °	1 U U		
M J	95.593	686	72.500	959	115.890	219	88.300	199	10.2.74	217	55.540	÷	106.95 109.95	アレナ		6 3
f []	99.57]	2 A G	75.310	275	126.430	22 A	96.993	210	68.810	222	39.050	20	175.72 101 010	007 007	000.000	ř 4
179	1:2.060	289	74.590	291	138.490	236	107.760	223	31.840	232	8.543		102.201	r .		i ir
020	104.547	0 62	71.480	247	151.050	544	121.990	235	116.093	240		122	0000011	4.	56.250	52
545	121.570	291	54 <b>•</b> 951	295	165.130	523	140.290	247	141.550	5 U 5 U 1 U		21.7	113.000	159	46.810	
<b>5</b> 2	139.1*0	0.2	56.110	306	177.190	260	150.001			190	1 4 5 4 7 5	25.5	93.060	354	40.950	32
271	150.753	5.5	4 P.130	371	180.770				004 204	100	205.083	262	72.880	352	41.100	320
277	171.513	662	4.5.030	0.0		200		271	188.180	274	203.275	269	55.640	t	49.190	306
271	155.050	24.8	54°470	124					165.260	2.8.2	1 82 . 360	275	52.720	33	54.190	29 29
260	141.743	2.84	D16.02		1010.000						157.210	283	59.570	53	49.840	286
652	123.593	271	7.21L	142	102.550					100	1 27. 240	288	56.590	67	44.390	276
276	143.300	255	9.100	422	72.870					100	1 22 - 64 8	292	56.950	86	41.870	275
299	154.400	267	7.510	515	61.730						1 22 7 20	205	71.890	100	41.220	27
711	177.619	273	8.620	157	71.400	245		667				207	91.780	103	40.400	271
305	192.720	281	23.723	145	73.880	282	95.320					206	01110	105	43.870	27:
285	199.320	282	34.220	148	73.210	29.2	91.550	297	9.270	2	11.11		0 1 7 ° 7 C		54.780	2
56.9	195.610	290	52.220	150	69.160	296	81.480	297	76.210	567	8> • 3 U U	007		111		4

					MTND SPER	D AND	DIRECTI	ZC										
בעדראד א בעדראד א	С Г	<b>.</b>		c		0		31	M)	N		£	Ň	.*	ñ	ŝ	P)	Ś
51	27.790	ちょく	1 43.940	202	76.130	191	62.743	2 A.F.	73,550	289	77.140	285	A3.220	277	50.900	121	59. 810	264
л С С	47.5.00	510	147.757	262	684.933	162	80.620	273	80.400	276	99-010	272		265	65.300		52.100	2
59	46.410	251	197.680	202	P4.950	186	101.100	263	96.303	262	101.650	526	95.280	255	77.380	102	45.640	
5 5	31.550	25,9	200-540	664	P7.14C	210	111.710	25 A	103.160	256	107.970	252	107.950	254	86.040	3	45.570	2
57	22.440	227	212.025	299	77.500	236	113.630	264	97,730	263	99.930	260	105.070	260			41.760	1
55	26.5 0	275	277.913	299	76.980	2 4 0	107.900	265	93,700	267	90.910	264	91.205	266	120.040	82	40.500	9
ц.	49.130	2r 0	214.373	746	64,946	244	045*#6	26.0	91.390	258	83.770	262	82.010	266	109.150	8	31.333	17
5 1 1	39.710	5:2	004.754	2.6	73.500	227	99.FAC	564	86.193	258	80.910	265	83.790	265	103.120	26	24.380	22
	40.970	292	600.475	239	59 <b>.</b> 950	719	92,930	265	83,900	257	73.080	263	78.540	270	129.950	26	9.890	2 2
52	36.750	406	775.800	244	69 <b>.1</b> 90	206	93.140	265	A7,390	252	77.810	262	79.070	268	138.170	16	9.050	202
5	19.720	245	277.447	294	79.920	102	96.520	261	91.530	259	73.470	256	70.350	264	113.930	86	22.870	266
0	29.4.20	162	213.797	0 62	92.45r	202	96.770	273	<b>GA.9A</b> 3	271	93.490	265	74.950	265	128.990	112	2.660	320
1	9. A 2C	360	219.770	279	105.780	2 <u>0</u> 5	88.099	062	84,900	284	96.870	277	100.400	272	114.320	26	10.360	275
	1.510	111	219.860	291	92.150	205	58.700	249	69.410	282	84.910	279	100.620	278	102.220	<b>1</b> 6	0.550	160
1 7	F. B50	< ₹	212.140	0 5 10	101.310	202	57. P.A.D	280	75.560	27.8	74.976	277	84.290	275	97.080	101	9.050	239
i Du Te	19.590	1 in 2	269.530	295	115.910	200	74.719	285	78.140	282	77.220	276	80.270	267	92.710	66	17.710	17
4 D	A.2?C	212	193.540	295	101.200	202	55. A00	266	57.250	276	65.560	274	66.610	266	95.640	16	14.530	134
t	19.110	σ	175.153	280	81.999	201	33.050	261	38.950	269	50.190	280	55.410	268	90.870	06		
t 3			169.847	295	A3.590	519	26.180	227	37,150	263	23.710	247	39.260	262		•		
t- 5			157.530	243	8.Z80	104	36.00	241	3F.93J	256	33.970	259	44.170	252				
4			137.903	285	85.530	1 45	35.470	220	46.410	231	34.580	247	39.850	249				
10 1			129.310	2.9.3	75.220	194	44.5.80	236	44.020	228	49.270	237	55.680	225				
¢ 1			114.550	281	54.390	197	33.740	205	22.750	221	22.440	242	33.090	250				
			192.373	275	45.450	230	26.300	230	22.450	208	22.170	211	20.870	254				
2			89.543	26.9			24.110	244			23.330	272	31.340	234				
<b>3</b> 5			91.020	273			15.430	230			18.123	190	13.620	184				
35			59.450	252			17. 460	250			24.740	256		, ,				
14			89.953	270			10.180	217			14.550	201						
33			74.630	267			16. 680	280			5.260	214						
25							17.110	16			11.040	336						
+1   -											11.410	317						
30																		

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FLICHT W	<b>9</b> . <b>3</b> :	•	۴	e	<b>P</b> )	σ	40		41		4	•	M 1		Ŧ		4	10
ALTIVUS	u. <sup>,</sup>																	
100	27.920	244	143.670	274							77.853	89		-	42.730	88		
60	7.610	114	94.4.80	610							49.720	93		-	03.450	67		
66	9-9-45	29	54.770	599	43.950	139			192.240	121	27.320	100			69.230	66	31.750	85
07	56.507	75	42.240	34.0	129.540	264			166.130	311	13.570	82			49.450	σ	56.350	36
96	70.1.00	c 2	54.663	•	206.583	110			143.400	596	14.960	12			45.630	327	75.120	17
. IL D	16 . 54	71	55.753	17	239.273	274			129.510	282	28.890	345			60.980	293	84.220	و
t D	72.210	72	63.160	1	248.129	277			117.590	270	43.493	338			83.110	276	86.500	359
5	67.875	17	5.9.500	22	244.613	279			105.810	55.8	48.383	335			96.460	263	82.550	350
6	51.000	er er	62.540	21	228.440	290			95.290 3	24.8	54.350	335		•	03.540	251	74.660	141
10	36.790	М¢	53.199	17	201.320	2 A D			86.290 S	823	54.780	330			06.930	243	65.140	425
06	23.650	115	43.763	σ	1:0.75	2 8 0			78.970	529	60.540	324			05.020	235	61.950	3 0 2
64	10.070	162	32.430	355	1.05.480	290			73.285	21	59.430	319		•	00.350	230	66.930	283
E C	26.039	193	25.290	131	45.163	277			69.200	15	58.100	311			94.430	224	77.710	999
17	36.720	214	23.510	295	16.920	114			64.900	212	56.843	302			A6.570	217	84.190	942
5	46.950	224	024.64	262	74.420	104			59.950	212	57.750	291			79.570	211	87.130	n 42
. L	54.470	230	43.310	245	124.330	113			55.540	216	69.530	279			71.650	205	86.523	244
	61.870	274	53.750	236	160.310	103			51.750	223	65.140	268			64.520	197	82.660	239
e.	67.470	97.9	11.403	533	1.1.220	113			50.740	234	72.550	257			59.900	191	76.010	2 35
~	72.750	272	97.733	212	193.560	103			53.640	246	81.140	549			56.300	185	71.200	232
	76.749	246	101.759	232	1.89.900	103			59.240	152	070.68	243			50.740	179	62.380	822
	Ca 1 47	251	112.710	222	141.340	104			71.500	265	97.500	6⊻2			47.370	173	51.790	222
29	78.410	256	129.920	233	161.950	104			85.940	270	103.450	236			43.456	159	38.150	
	77.045	261	127.690	523	137,350	104			102.750	274	107.490	231			39.210	169	23.640	
77	74 P 00	247	122.950	233	99.030	104			121.543	276	110.340	232			33.470	178	0.00	161
76	001.77	274	117.230	245	64.900	102			141.270	276	111.110	231			31.290	199		202
40	74.5.00	283	109.250	237	ú62°27	с С			160.590	276	110.300	232			37.053	227	3.450	
74	79.140	289	97.933	543	23.700	77			178.190	27 L	104.250	234			50.900	5 4 2		
	A5.990	062	A3.513	249	12.070	5 5			190.900	273	104.203	239			64.200	242	12000	
72	97.770	297	73.590	757	8.57 n	61¢			199.560	270	104.300	246			73.0DU	107	20.600	
71	192.030	2 4 2	51.653	750	28.510	012			201.750	269	102.510	500				274	15.490	6 C E
70	136.150	281	25. 720	245	57.913	226	153.570	262	204.450	5.0		2.54			73.720	573	34.280	315
49	105 10	284	29.49	156	77,290	233	151.210	254	061.805	207		+ F 0 1					42.240	260
6.9	134.010	289	51 . 750	136	67.350	232	153.793	253	213,199	256 272	119.560	251		257	80.850 80.850	261	43.410	233
67	1 64.7 70	2 A 6	61.520	1 35	с <b>ч</b> , (50	239	157.170	852	216.350	223	104+000						14.570	500
66	105.040	291	52.676	142	71.020	253	160.390	266	217.580	251	135.140	5.54		200	14.0.36.0	25.0	9.050	301
65	107.760	142	75.120	148	55.130	5°7	15P.710	273	234.440	5.5	122.540	000			164.870	270	39.960	244
, F.L.	906.36	285	23.260	174	41.510	3¢ 1	149.520	278	191.120		101.000	200	100.010		175.060	267	34.560	238
63	A1.590	162	15.620	217	37.260	269	139.850	612	100.001	1	0.00	200		222	167.290	262	14.260	223
62	58.500	305	14.470	280	32.560	142	156./lu	612	141.01	2		7				) 		

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5	183	203	300	285	268	274	277	268																								
.Ŧ	19.720	8.070	14.260	29,640	50.910	61.750	74.230	82.230																								
t	255	249	243	239	237	239	251	267	266	259	263	251	252	253	260	257	263	264														
£	156.240	148.693	150.070	152.120	154.700	146.560	124.990	133.840	147.020	141.760	144.700	152.050	146.A10	131.200	143.280	117.340	123.080	112.070														
m	272	270	258	255	264	272	259	254	260	265	259																					
4	127.070	141.110	135.410	125.500	124.280	128.010	123.150	115.440	116.940	132.510	135.750																					
N	249	242	247	258	257	254	255	261	258	549	246	248	253	256	262	292	303															
1	94.150	79.510	68.090	73.060	86.070	86.430	79.723	99.053	113.030	120.030	142.370	151.700	154.880	140.170	95.330	61.200	40.300															
1	237	235	244	254	253	249	253	258	252	248	25C	252	261	272	2 A O	262	247	544	247	255	262	549	2F1	257	262	270	277	281	300	334	342	
3	142.125	136.010	124.510	129.780	136.190	126.210	115.380	125.540	131.160	122.350	117.790	112.700	115.450	100.783	96.540	119.760	123.130	115.790	102.070	109,990	110.430	96.270	88.750	78.295	79.510	65.040	59.620	57.940	41.220	20**62	19.390	
0	277	275	271	265	26 A	212	271	270	27 F	272	26 0	273	275	273	277	274	254	271	267	260	264	259	257	262	254							
L	140.797	147.510	146.203	142.560	147.030	155.520	151.790	148.760	155.900	150.330	150.210	161. 070	154.283	160.700	151.830	143.940	154.890	157.050	153.290	151.050	145.200	139.760	129.410	109.980	106.450							
ç	250	220	062	202	290	312	287	120	334	323	312	151	240	175	253	258	231	159	351	ΣĒ												
	197.57	39.910	4.4.410	51.139	47.710	13.940	53.040	36.740	41.910	32.519	23.096	10.940	43.970	25,930	40.940	15.730	21.990	21.460	14.120	16.020												
e.	236	191	170	101	158	168	176	216	228	251	340	747	6.0	8 S	5 8	6 6	267	336														
P.	0 z 13 e	4 • 9 4 9	14.140	23.540	15.450	15.170	23.950	20.650	<b>75.</b> 900	27.470	5.573	0 6 L 6	3. 370	53.100	41.720	35.630	3.7.40	12.390														
~	₹C6	202	2 4 9	2 8 8	287	277	273	2 4 9	303	324	137	307	261																			
•	900.Jt	74.050	003.33	62.250	65.290	65.650	54.950	46.040	694°47	79. P7C	41.570	73.190	43.130																			
FLTSHT NO ALTJTUNE	<b>E1</b>	0 4	σ v	5.8	57	55	55	5 t	53	25	н 4	50	49	¥ 7	4.7	46	45	5	t 4	t 2	f 1	t 0	39	<b>6</b> F	42	35	۲. ۳	44	<b>8</b> 23	32	11	30

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1 00 60 70 70			159.320 99.550 25.483	111 120 120	188.110 F1.250	140 142	193.990 190.560 180.300 159.690	4504	147.58U 120.090 102.540 99.150	170 203 203	149.840 140.110 119.720 90.410	298 295 296 298						
9 9 9 9 9 5 9			37.940 74.440 94.350	230 295	40°230 40°230 40°2400	306 309 309	135.110 10A.410 80.480	1105	103.540 111.140 116.340	242 254 263	53.150 28.500	303 311 64						
F 6 2 6			97.470 91.470	298 297	142.240 142.720	303 298	53.990 30.180	м м Ф	119.570 121.500	269 274	33.290 56.010	107	252.170 3	12			107.560	~
16 16 10 0	70.790 53.750	2,80 2,69	84.850 74.753	294 230	136.500 126.590	285 285	19.750 29.580	96 141	120.560 117.450	278 281	73.330 85.430	115 119	220.540 2	85 85	9.170	241		306
0, 0, 6, 6,	54.703 59.100	249 225	F. P 250	0 0 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	114.350 106.950	278 257	43.890 54.840	158 165	113.339 108.590	285 289	93.150 96.870	119 119	201.630 2 180.660 2	73 12 61 16	8.880 1.190	231 223	025.520	240
		7.74	33.473	25.8	86.920 77 440	255	62°C90	171	104.430	292 296	96.340 95.300	119 118	137.016 2	50 18 40 18	10.050 15.310	216 209	102.990 110.880	224 213
	56.910	174	25.759	136	70.630	526	63.970	175	97.190	300	91.780	117	103.820		2.230	503	114.840	207
- 4 - 11 E E	55.701 55.701	150 150 8	76.84) 49.633	165 154	64.22C	1 80 8	59.840 53.880	179 193	94.470	308 308	85.510 77.200	115 115	65.389 2	07 15 07 15	9.860	196	108.690	200
32	56.550	175	57.60	677	82.420	174	45. P30	187	90.910	312	67.14D	114	51.080 1	93 12	8.210	196	97.210	200
	59.340 11.170	1135	63.42J 69.637	5 5 7 7 7 7	95.76P	164 157	38.980 31.610	195 216	90.790 91.590	314 315	55.500 41.170	112 110	37.750 1 29.119 1	101 8/ 26 10	7.520	207	66.990	212
2	14.200	102	70. 751	145	92.543	20	24.060	522	93.750	317	25.080	108	21.630 1 17.640 1		6.670	221	55.230	230 254
6 4 6 4 6 4 6 4 6 4 6 4 6 4 6 4 6 4 6 4	020.01	с, е С, е	71. 57U 69.39U	127	72.540	144	25.740	232	0 - 0 - 0 - 0 - 0 - 0 - 0 - 0 - 0 - 0 -	316 316	12.320	315			5.360	255	61.360	274
76 75 7	79.50 11.050	τ. 1 1	65.16U 54.270	124	57.350 39.330	141	32.CAO 36.870	5. 8 5. 5 6. 5	104.476 109.570	316 312	30.350	301 296	24.340 2	16 11 96 11	7.210	270	87.090	291
	re.270	1 <b>1</b> 1	45.820	121	24.309	821	77.780	293	112.410	310	70.650	285 285	39.260 2	85 13 80 14	10.550	271 269	98.503 107.820	292 288
	59.030 51.780	357	37.090	62F 172	17.41 8.590	+ + + + - + + - +	38.750	543	120.950	- 00 -	111.260	283	68.976 2	14 14	6.640	267	114.020	282
12	24.50	0 6 1	35.100	140	10.920	254	50.100	510	126.063	312	128.650	283 286	92.440 2 07 FFT 2	74 14	.7.570 6.650	264	119.830 123.270	275 268
0 4	75.850 18.420	2 F. B 2 4 G	34.940	171 85	19.170	293	52.44U	224 224	130.220	3210	142.570	291	115.570 2		6.790	259	123.830	262
	11.540	176	35.A70	27	20.970	276	42.910	224	120.950	317	148.650	262	127.840 2	59 14	-8.730	257 254	122.380	263 268
<b>1</b> 9	15.790	142	37.710	4 t 7 M	22.560 24.110	265	52.850 68.870	225	113.41U 107.850	503 301	152.570	284	130.130 2	10 10	0.420	253	125.060	274
0 U 0 0 0	41.910	145	35.150	. 40 1	52.500	252	77.900	227	102.360	299	139.730	279	123.379 2	45 16	6.600	255	128.510	273
19	35.670	127	20.150	22	46.480	256	75.420	234	96.330	301	131.940	276	117.390	54 46 46	5.010	255 256	157.51U 157.59A	002
r 0 9 9	70.F70 A.250	130	18.977 5.909	7 t 9 t	43.250	256	141.140	265	77.430	306	120.340	254	113.70	16	1.440	256	172.630	240

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	÷	236				2 0	10	241	241	540	244	251	250	252	258	256	255	263	244	245	234	230	249	246	239	, , T							
	ŝ	189.910	107.400	185.730	176.740		142.520	134.600	126.750	126.550	112.700	113.510	116.450	114.050	114.600	111.540	114.550	114.440	117.940	94.950	61.280	32,340	47.150	27.730	39.200	1							
	ю	259	26.1	26.2	2 C C		259	257	260	264	264	264	265	259	253	254	262	264	258	254	263	261			261	272	268	262	269	267	266		
	ß	160.400	159.560	167.120	171.450	169.420	176.030	172.470	172.770	175.890	179.470	179.290	180.620	176.730	167.840	167.160	161.560	155.860	146.870	137.470	117.940	110.840			95.100	92.310	89.620	067*76	80.480	85.140	84.850		
	~	279	277	271	264	260	261	265	265	264	264	265	265	268	265	264	269	564	254	271	282	280	289										
	ŝ	117.109	120.790	123.680	125.370	127.060	125.460	135.300	139.090	131.872	142.640	143.510	150.347	132.520	125.910	145.300	140.450	124.540	111.500	93.950	087.69	102.370	96.630										
	. 1	242	240	240	237	238	223	223	217	217	214	22	6	350	31	n t	119	131	132	135	46	17	113	6. 6.	113	58	341	330	304	300	309	278	289
		115.190	100.020	91.230	88.290	64.160	41.140	40-100	21.280	18°440	15.550	15.310	22.440	20.040	11.370	9.110	17.820	24.590	44.000	54.860	39.100	27.293	16.720	11.940	21.930	140	19.920	31.450	30.070	3 . 530	44.603	44.590	50.370
		PCE	314	323	344	11	e en	70	89	103	95	69	99	e C	102	102	68	29	105	163	155	158	195	223	254	255	255	253	245	254	262	261	289
	υ.	71.360	65.350	52.710	37.250	22,350	20.100	22,500	28.740	37.540	47.080	44.220	44.100	38.080	25.880	34.020	25.760	11. <sup>56</sup> C	19.670	27.930	37.550	47.010	19.590	25.4440	31.500	52.650	61.710	77.240	78.750	74.470	70.800	67.000	55.410
z	æ	255	260	265	274	271	25 A	272	271	266	251	25.0	275	279	277	252	257	275	2.16	267	273	276	27.5	5	262	278	287	249					
DIRECTIO	t	74 + 239	72.790	76.100	90.720	92.780	A1.750	179.970	95.770	87.350	98.530	88.570	74.550	68.610	76.250	82.110	63.490	70.615	60°Ca0	55.280	62.023	44.350	55.740	02	42 · 4 80	18.780	41.383	29.760					
ONV O	¢	255	257	226	227	226	219																										
ATND SPEE	4	47.520	54.733	53.500	65.420	60.190	51.830																										
-	~	199	224	249	251	231	216	177	202																								
	£	19.190	29.250	32.950	44.930	35.290	14.970	11.279	19.780																								
	ĸ	220	02	<b>r</b> 6	4	~	10 10 10	270			101																						
	ч	2.440	142.	4.619	2.650	0.4.4.0	5.300	7.830			1 T 1 T 1																						
	FLIGHT VG. Altiturg	51		59	23	1 2 4	5 U	r .	1				101		- N	- 4	р М 8 – 4		- P			4 6				25		, <b>,</b>	• •				

# TAB PRINT-OUT OF WIND SPEED AND DIRECTION

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100	153.630	129																
99	124.230	124																
£ 6	94°040	113																
44	74.250	<b>t</b> o	272.920	164														
96	67.230	የ	50d Sud	155														
95	59.720	L 8	130.240	137					187.410									
94	55.790	5	75.940	104					167.640	328	129.140	4 6						
16	44.010	20	<b>P1.</b> 530	4 4					150.710	318	131.040	50		4	158.310	0		
26	31.5 AC	~	114.130	21			8.840	270	133.530	306	131.040	51	92.100	20	105.150	<b>no</b> .		
91	18,553	8 2 E	1 27.230	11			152,540	345	118.790	292	129.390	49	92.350	63	78.350	::		
00	29.430	253	116.559	<b>P</b> <sup></sup>			116.970	101	107.490	240	120.130	40	92.690	133	61.700	<b>5</b>		2
6.4	0-1-54	226	77.579	351			110.770	285	100.500	268	102.180	41	95.130	32	38.050	13	103.150	~ ~
•	59.590	217	37.920	314			136.680	25 A	95.350	256	8.7.080	36	84.000	54	9.480	ا	041-28	2
87	72.130	214	44.033	245			172.340	544	86.970	246	62.490	29	71.080	14	18.950	205	57.800	20
25	87.130	212	74.940	221			200.010	236	77.269	235	42.170	20	47.020	2	51.560	200	38.720	29
	Q1 . 7 RU	211	94.240	244			216.570	231	67.350	221	21.160	<b>f</b> \)	21.000	330	78.380	199	33.770	5
	96.150		199.290	212			215.360	229	58.330	205	8.680	262	19.210	243	98.570	201	40.290	355
e er	100.640		112.430	210			202.170	227	53.430	185	27.130	211	35.140	208	115.810	203	47.560	340
. •			104.470				179.870	227	52.780	169	46.270	202	<b>5</b> 6.350	198	128.090	203	49.170	339
	99.670		100.440	214			152.430	822 8	56.110	154	63.240	195	73.200	194	132.650	202	44.840	359
	92.750	215	99.910	220			125.390	231	46.990	139	72.950	192	84.920	193	134.000	201	36.830	310
- C	100 - 100 -	100	75.56	240	90.350	275	102.986	240	41.920	12a	75.900	190	97.130	194	126.990	198	31.860	358
		1000		260	RC-220	010	88.130	254	33.013	110	73.950	188	93.93C	195	114.600	195	33.520	19
		510	70.250	266	72.460	. e. . w	95.420	271	23.900	74	65.143	189	94.570	199	98.640	191	37.400	t i M
		25.5	79.650	979	68.510	388	96.720	285	25.270	19	51.520	197	65.950	205	19.940	186	43.270	
-		-	01.110		69.971	293	114. P.C.D	294	42.110	778	36.170	220	71.950	219	60.280	190	49.510	<del>,</del>
-		100	102.520	246	76.850	297	134.940	297	67.670	725	36.500	259	62.220	243	39.950	172	53.810	36
, P	06.060	201	115.210	5.6	89.950	800	153.650	299	89.850	314	58.930	296	69.840	271	22.293	147	53.780	5
	110.750	289	125.470	290	107.950	296	169.790	297	109.820	70t	99.490	305	89.560	288	9.120	65	49.670	
	121.150	0 e C	135.150	274	124.460	293	178.910	295	129.910	294	114.850	306	112.550	294	25.120	555	501°10	<b>n</b> 1 <b>n</b> 1 <b>n</b> 1
• C • P	127.270	274	137.960	269	149.950	299	182.390	292	141.856	285	128.390	301	129.019	294	48.210	332	55.6/0	510
	1.70 . 1 4.0	256	131.900	267	166.739	284	194.570	290	148.070	276	129.250	290	130.240	292	68.930	318	55.000	
	127.520	25.8	124.990	266	175.470	278	186.170	287	149.540	269	124.150	277	122.550	285	<b>51.510</b>	202		100
-	128.300	271	122.990	266	179.590	270	185.480	284	142.690	264	115.530	255	109.300	275	78 . 34 U	0.07		
	120.070	269	125.520	265	176.650	262	193.190	281	130.910	259	106.350	258	102.920	262	86.910	275	4/.000	522
) U	129.010	262	131.500	259	163.490	256	165.100	279	121.770	252	101.050	249	104.590	253	85•700			+ u + u
E C	138.403	251	139.290	253	144.940	252	153.870	277	118.750	250	99.940	243	102.020	543	86.520	992	101.00	
	159.740	242	145.390	248	126.450	248	144.740	275	115.950	247	99.830	237	99.560	542		292		0.70
9	175.260	240	155.450	243	109.670	243	135 A 30	272	113.290	245	99.020	235	94.440	242	110.44	262	101.00	2

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# TAB PRINT-OUT OF WIND SPEED AND DIRECTION

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# TAB PRINT-OUT OF WIND SPEED AND DIRECTION

					UN IN	SPEFO	QNA	DIRECTION	_
FLIGHT ALTTU	40. 64 JOF		6	10		66		67	_
100									
66									
έb									
97									
96									
95									
94	141.870	328	129.510	347					
50	123.050	328	113.680	356	82	060	192		
56	104.250	6 <i>2</i> £	045.40	11	115	,551	174		
4	604.28	340	A5.630	5 0	122	330	157		
0	64.750	332	R0.260	35	113	.130	164		
	49.090	45.0	75.530	47	20	.910	153		
	40.690	35.0	69.91D	58	5.8	020	166	133.810	213
	120.05	11	64.950	<b>6</b> 6	t t	.770	190	128.170	203
9	44.950	:2	52.920	71	4	.720	215	115.930	194
	52.490	R. M.	67.440	74	44	.269	247	99.A20	135
	55,020	4	52.093	76	61	.130	258	84.060	176
r M C et	52 . 8 A C	t-	47.489	77	75	.240	261	64 • 5 0	166
	49.250	¢ 7	45.110	73	87	0ž6.	262	45.920	149
	44.0.00	t t	45.729	69	96	.550	260	36.4.30	121
	35.840	6 7	44.480	64	100	.590	258	35.150	5 0
0	36.129	47	41,919	50	103	• 52 0	256	37.500	61 I 10 I
	36.250	50	40.643	54	102	,7an	524	37.770	
	75, 201	1	36.413	43	100	.570	n uc	36.720	9 0
	74.470	t,	33.640	39	9	. مم	253	32.890	1 t 2
	34.950	27	33.370	52 5	593	. 290	553	25° a50	
74	C	12	34.750	14) 14)	91	.220	203	14.769	7 8 7
	45.100	949	76.1AD	157	0 0 0	• 4 4 0	254	2.810	167
~ ~	57.963	332	42.090	340	е. С	.100	254	17.750	202
	74.350	317	52.140	425	103	.101	252	38.790	212
	A7.91C	303	64.900	8 C F	111	.830	254	57.610	273
	96.020	004	75.410	296	121	.850	252	70.820	242
	03.700	200	966.48	2 8 8	120	.770	263	80.900	260
	01.6	57.4	91.130	284	135	110	26.8	A5.940	259
		010	93.470	28.3	139	.700	272	87.820	262
	87.660	1 U 1 U 1 A	01.865	279	140	.140	273	87.940	528
	87 . D.6.0	0.76	93.660	275	137	. 200	272	88.430	252
	A7 . 510	104	89. A 40	271	129	.260	270	<b>69.310</b>	251
0		917	A5.510	266	121	.530	267	84.670	249
30	3 \ f =C	ľ		I					

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TABLE XXVI (Concluded)

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# TAB PRINT-OUT OF WIND SPEED AND DIRECTION

					MIND SPEE		DIRECTIO	z
FLIGHT VO		54	9	tr.	Ľ	<u>م</u> `	ų	~
ALTITUR								
61	91.350	245	75.740	25 A	112.960	263	76.760	755
۹. ۲	062.42	250	64.253	248	103.250	258	71.290	263
59	70.040	250	51.530	241			71.660	257
5.A	23 510	243	66.0ª0	232			73.590	267
57	73.040	236	67.170	230			72.470	258
56	59.910	676	53.340	243			59.150	241
55	51.970	266	40.020	2 c ()			60. 570	226
54	47.590	279	36,690	750			43.780	228
5	57.730	291	43.393	273			35 . 749	251
5	67.3 20	989	55.423	2.4.5			30.600	253
51	79.710	282	69.570	275			22.540	225
50	96.700	289	77.920	979			23.560	221
4 0 4	89.850	282	79.590	220			35.751	236
8 <b>1</b>	89.690	267	77.530	255			37.060	244
47	5 <b>2.3</b> 19	248	77.140	245			42.230	285
46	67.930	240	72.530	250			002.44	260
2 U	65.540	240	57.750	248	A1.620	277	14.377	543
4	60.A10	248	076-740	260	A0.950	275	43.930	250
r 7			53.560	252	58.090	276	54.090	281
42			43.950	251	49.910	305	44.930	264
<b>6</b> 1			41.580	217	47.150	262	33.970	287
64					36.510	291	46.490	287
61					39.993	288	39.690	24.3
•					124.75	116	33.750	276
37					27.940	290	34.620	250
36					40.040	293		
35					24.490	276		
14					6.380	320		
52					17.950	301		
2					14.790	267		
31								
30								