



# Development of stable, low resistance solder joints for space-flight HTS lead assemblies

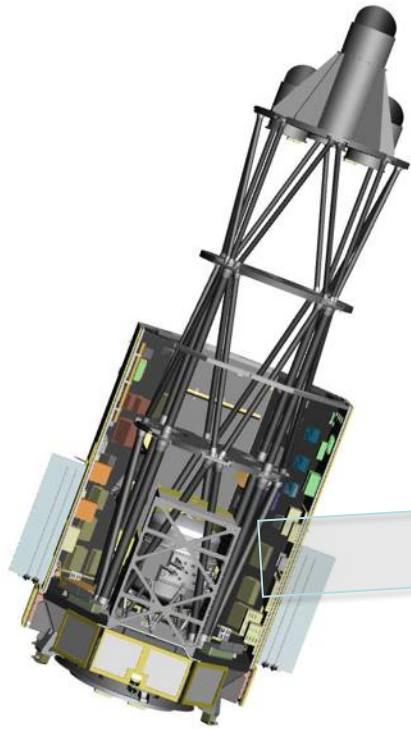
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<sup>1</sup> NASA – Goddard Space Flight Center

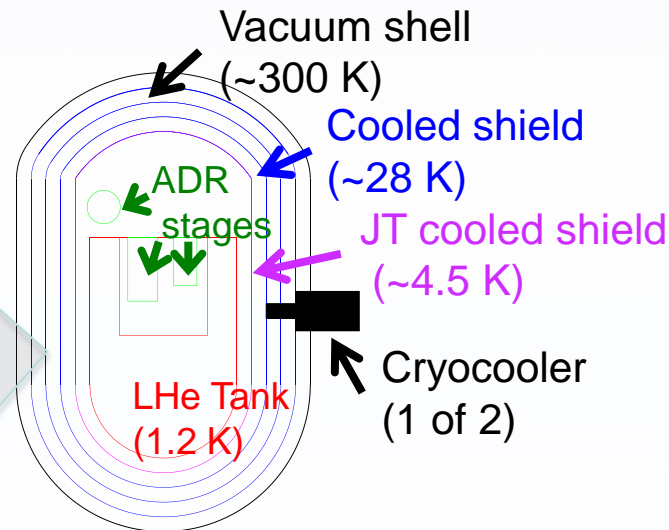
<sup>2</sup> Alcyon Technical Services, LLC

<sup>3</sup> SGT, Inc

# Background: Astro-H (Hitomi)/SXS



Soft X-ray Spectrometer used a microcalorimeter array operating at 50 mK



SXS Thermal System:

- (2x) 2 stage Stirling coolers
- JT cooler (4.5 K)
- 40 l LHe tank (1.2 K)
- 3 stage ADR ( 50 mK )

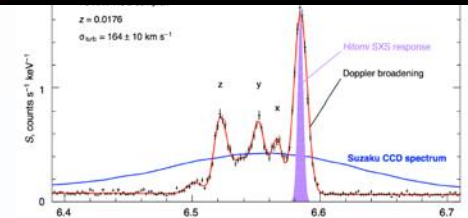
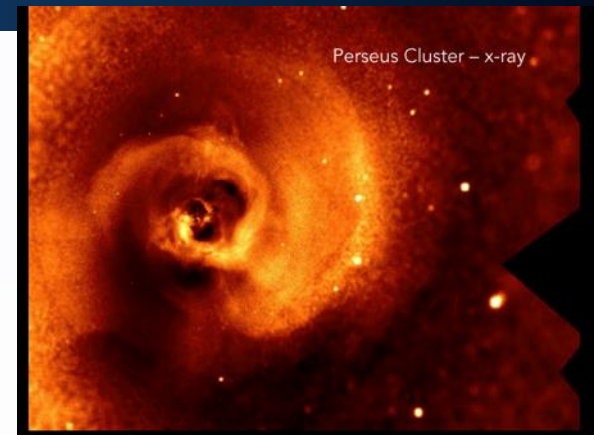
HTS leads for ADR magnet current (2 A) needed to meet stringent parasitic heat load requirements

- HTS allocation: 10  $\mu$ W @ 1.2 K; 670  $\mu$ W @ 4.5 K

17 February 2016: Hitomi launched; SXS performs flawlessly

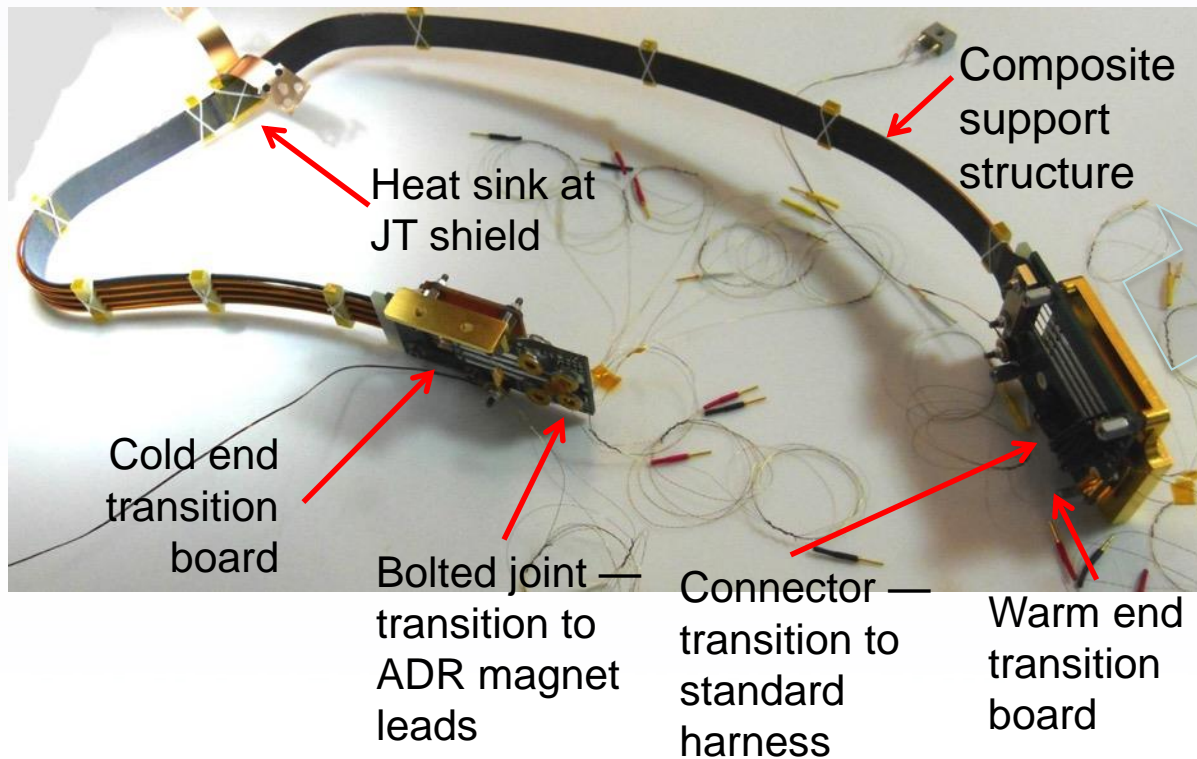
# Background: XARM/RESOLVE

- In first few weeks, SXS demonstrated unprecedented resolution & discovered important new results
- 26 March, 2016: Attitude control system incident disables spacecraft
- 2017 — Start recovery mission
  - RESOLVE instrument – identical to SXS
  - Rapid turn around (2019 delivery to JAXA)
  - “build to print” with very few exceptions

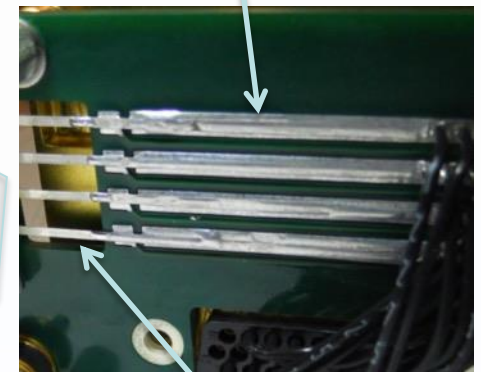


# RESOLVE HTS Lead Assemblies — Approach

- Physical structure identical to Astro-H



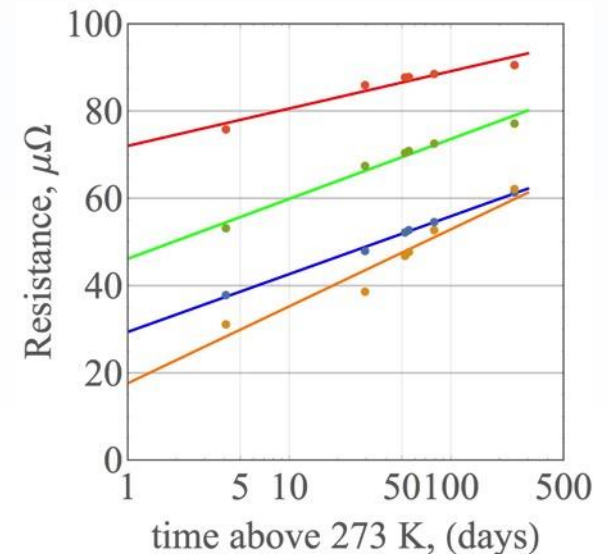
Solder pads:  
100  $\mu\text{m}$  cu /immersion Ag



1 mm Ag5%Au coated  
REBCO tape

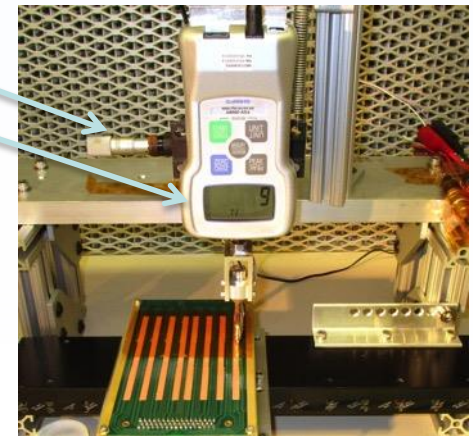
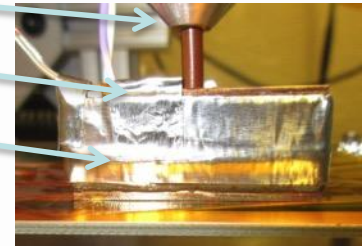
# RESOLVE HTS Lead Assemblies – Changes

- Changes driven by issues encountered in Astro-H
  - $I_c$  degradation, esp. in humid environment
    - SXS: REBCO 2G conductor, Ag/Au coated, slit to 1 mm after
    - Concern over lateral H<sub>2</sub>O & CO<sub>2</sub> transport from exposed edges
    - RESOLVE: same conductor, coated after slitting
  - Solder joint degradation
    - SXS: measurements showed  $R \propto \log(t)$  at ambient  $T$
    - Slow consumption of 2  $\mu\text{m}$  AgAu layer by In3%Ag solder
    - RESOLVE: 20  $\mu\text{m}$  Cu plating over HTS at solder joints
  - Variability of void density & joint R



# Updates to HTS/PCB solder process

- Prototype solder rig
  - Motivation: tight control of process parameters
  - Ball joint for uniform force
  - Diode for accurate temperature control
  - Wrapped tip heater uniform heating
  - Fine position adjustment
  - Accurate control of force
  - Typical parameters (for In48%Sn):
    - Apply 10 N (80 mm<sup>2</sup> area)
    - Controller on; set point = 150 C
    - Wait 30 s after T = set point; controller off
    - When T < 100 C, remove force
- Production solder rig
  - Miniaturized to fit flight assemblies



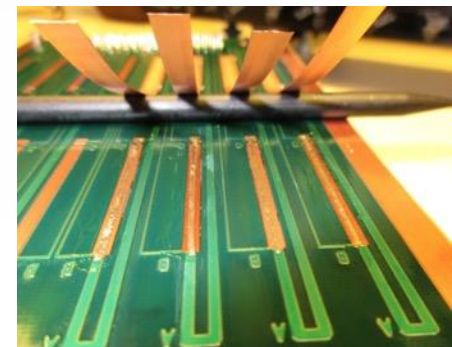
# Solder Tests – Materials

- Test boards

- Solder pads similar to flight boards (2 x 40 mm)
- Separate voltage tap points
- 16 joints / board
- Plating types:
  - Bare copper
  - Immersion tin
  - Electroless Ni/immersion gold

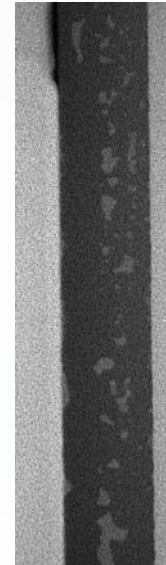
- Solder

- In48%Sn (m.p.118 C, eutectic)
- 1 mm preforms



# Measurements and Early Results

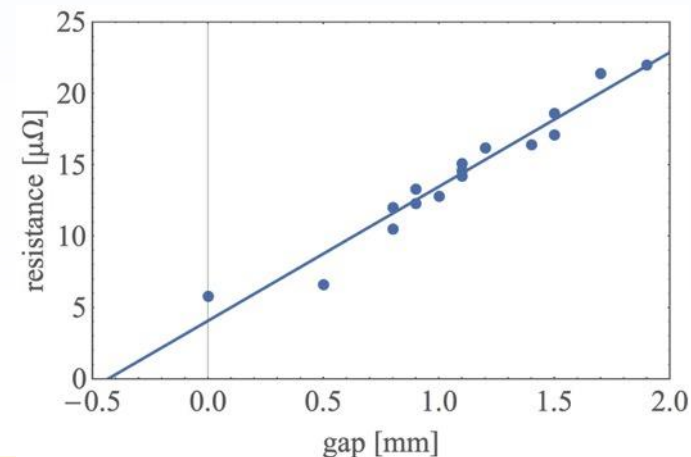
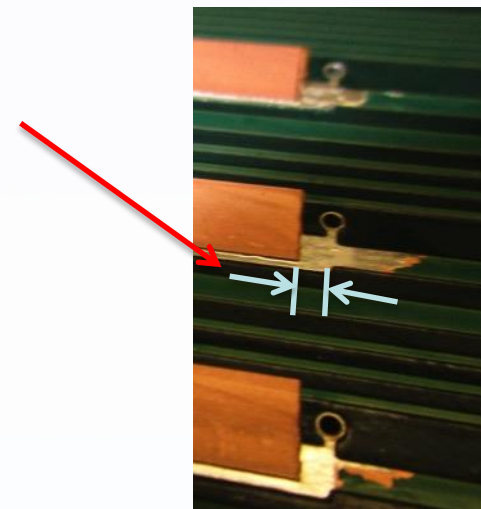
- X-ray images to determine void fraction, wetting
- Joint resistances at 77 K
- Joint  $R$  vs  $T$  (3 K – 300 K)
- Early development test
  - Varied  $T_{solder}$  150 – 165 K, Force 5 – 20 N, hold time 30 – 90 s
  - no obvious patterns in x-ray images or  $R(77\text{ K})$
- Cycled 20 x (300 K  $\rightarrow$  77 K); no change in any  $R(77\text{ K})$
- Comparison of surface treatment in process
  - Best results so far with manual pre-tinning of solder pads





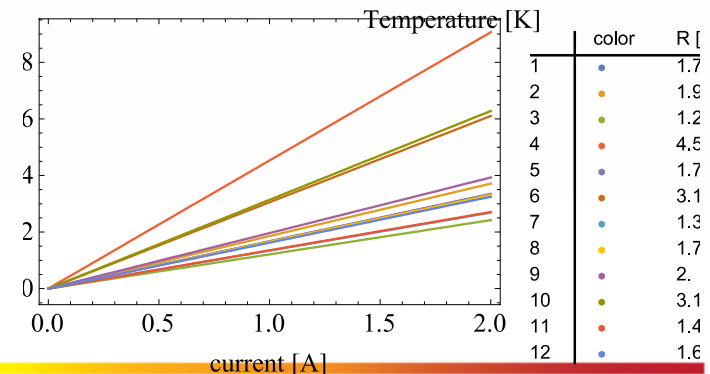
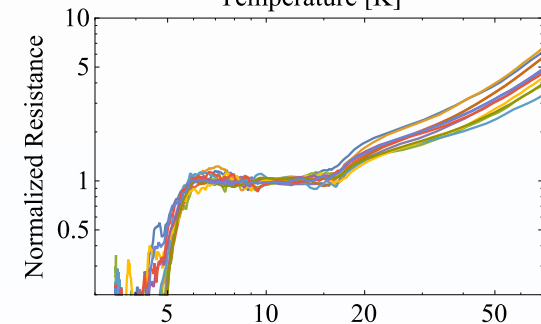
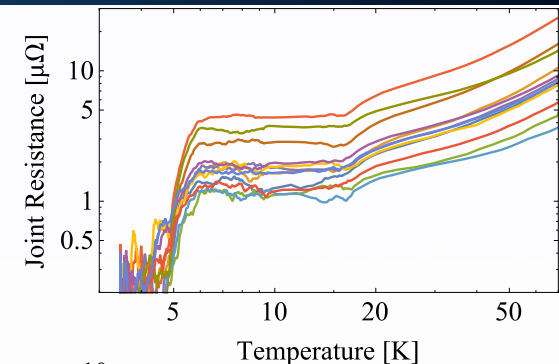
# Current Transfer Length

- Serendipitous measurement:
  - $x$  = HTS end to voltage tap distance
  - In early boards,  $x$  varied
  - Measure joint  $R$  at 77K
  - $dR/dx$  = trace resistivity =  $9.4 \mu\Omega/\text{mm}$
  - AstroH samples: trace resistivity =  $8 \mu\Omega/\text{mm}$
  - Intercept = average current transfer length,  $\lambda = 0.43 \text{ mm}$
  - In Astro-H samples,  $\lambda = 2 - 4 \text{ mm}$
- For subsequent boards,  $x = 0$



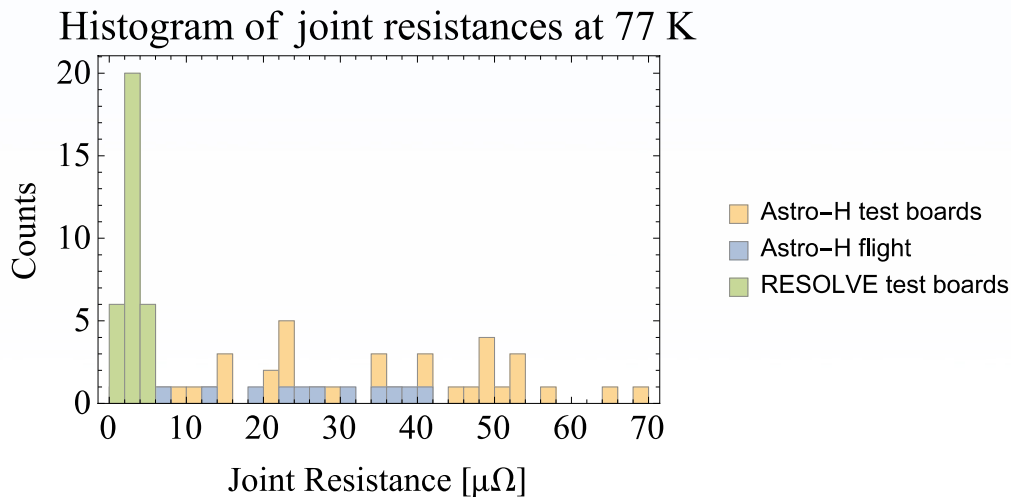
# Low Temperature Resistance

- Measured  $R$  vs  $T$  (3 – 300 K)
  - Plateau 5 K  $< T <$  16 K
  - $R \approx 0$  for  $T \lesssim 5$  K ( $T_c$  InSn 7.1 – 7.5 K)
- Normalized by mean (8 – 16 K)
  - Still  $\sim 2$  x variation at 70 K  $\rightarrow$  not a simple geometric effect
- Measure  $I$ - $V$  at 10 K
  - $I$  up to full operating current (2A)
  - Linear  $\rightarrow$  ohmic behavior
  - Derived  $R$  matches those measured at low  $I$



# Distribution of Joint Resistances at 77 K

- Allows convenient comparison
- Astro-H
  - Test board & prototype measurements
  - Flight units (from post-vibe functional cool-down)
- 4 recent boards produced with same protocol



- Results

- Values not directly comparable, but distributions are
- Astro-H measurements all had wide distribution
- Boards produced under new protocol show much tighter distribution

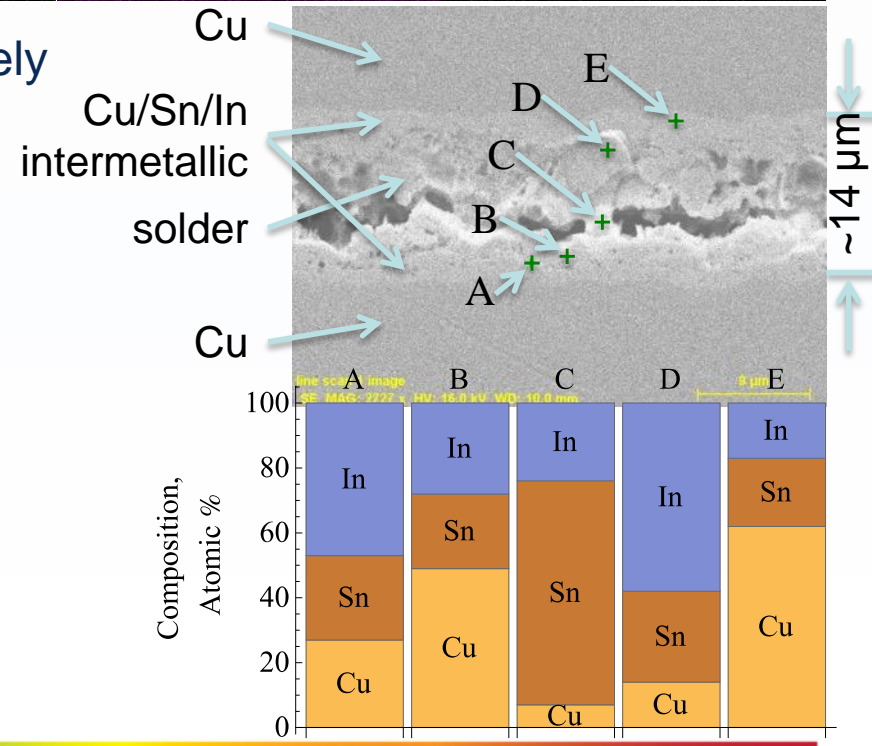
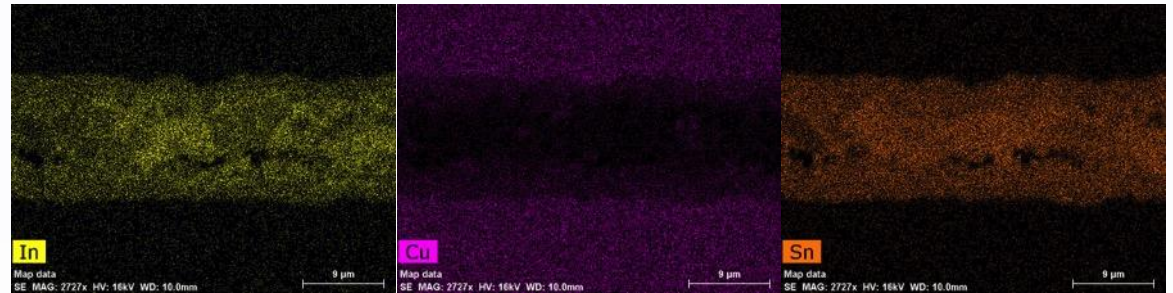
# SEM/EDS of Cross-Sections

- EDS

- Provides map of joint composition
- Shows formation of inter-metallics at boundaries, largely unreacted solder in center

- Vianco, et al.:

- CuIn growth rate follows
 
$$Dy = At^n e^{-Q/RT}$$
- Predicts  $\Delta y \approx 2.5 \mu\text{m}$  in 4 yr
  - ➔ will maintain compliant InSn layer



# Conclusions

- RESOLVE: Rapid rebuild of Soft X-ray Spectrometer
- RESOLVE HTS lead assemblies to “build to print” except
  - Improved HTS material
  - New solder joint material & process
    - Plating protects Au layer from slow consumption by solder
    - New rig gives tight control of process parameters
- Solder process qualification tests
  - Good wetting and void levels (x-ray image)
  - Acceptable intermetallic layers at boundary
  - Ohmic behavior to full operating current
  - Excellent sample-to-sample variation in 77 K resistance
- Path forward
  - I-V testing to 5 A in prototype
  - Environmental degradation testing of joints an HTS tape