

Compendium of Current Single Event Effects Results from NASA Goddard Space Flight Center and NASA Electronic Parts and Packaging Program

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Abstract: We present the results of single event effects (SEE) testing and analysis investigating the effects of radiation on electronics. This paper is a summary of test results.



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Introduction

NASA spacecraft are subjected to a harsh space environment that includes exposure to various types of ionizing radiation. The performance of electronic devices in a space radiation environment are often limited by their susceptibility to single event effects (SEE). Ground-based testing is used to evaluate candidate spacecraft electronics to determine risk to spaceflight applications. Interpreting the results of radiation testing of complex devices is challenging. Given the rapidly changing nature of technology, radiation test data are most often application-specific and adequate understanding of the test conditions is critical.

Studies discussed herein were undertaken to establish the application-specific sensitivities of candidate spacecraft and emerging electronic devices to single-event upset (SEU), single-event latchup (SEL), single-event gate rupture (SEGR), single-event burnout (SEB), and single-event transient (SET).

For total ionizing dose (TID) results, see a companion paper submitted to the 2017 Institute of Electrical and Electronics Engineers (IEEE) Nuclear and Space Radiation Effects Conference (NSREC) Radiation Effects Data Workshop (REDW) entitled "Compendium of Current Total Ionizing Dose and Displacement Damage Results from NASA Goddard Space Flight Center and Selected NASA Electronic Parts and Packaging Program" by A. D. Topper, et al.

Test Techniques and Setup

A. Test Facilities

All tests were performed between February 2016 and February 2017. Heavy ion experiments were conducted at the Lawrence Berkeley National Laboratory (LBNL) 88-inch cyclotron [3], and at the Texas A&M University Cyclotron (TAMU) [4]. Both of these facilities provide a variety of ions over a range of energies for testing. Each device under test (DUT) was irradiated with heavy ions having linear energy transfer (LET) ranging from 0.07 to 86 MeV/cm²mg. Fluxes ranged from 1x10⁷ to 1x10¹⁰ particles/cm²s, depending on device sensitivity. Representative ions used are listed in Tables 1 and 1L. Ions in addition to the values listed were obtained by changing the angle of incidence of the ion beam with respect to the DUT, thus changing the path length of the ion through the DUT and the "effective LET" of the ion. Energies and LETs available varied slightly from one test date to another.

Proton SEE tests were performed University of California at Davis (UCD) Crocker Nuclear Laboratory (CNL) using a 76" cyclotron (maximum energy of 63 MeV) [5] and Mass General Hospital (MGH) Francis H. Burr Proton Therapy.

Laser SEE tests were performed at the pulsed laser facility at the Naval Research Laboratory (NRL) We tested with a pulsed laser at the Naval Research Laboratory using both Single-Photon Absorption (SPA) and Two-Photon Absorption (TPA) techniques with the laser light having a wavelength of 530 nm resulting in a skin depth (depth at which the light intensity decreased to 1/e – or about 37% – of its intensity at the surface) of 2 μm. A nominal pulse rate of 1 kHz was utilized. Pulse width was 1 ps, beam spot size ~1.2 μm.

Table I: LBNL Test Heavy Ions

Table with 4 columns: Ion, Energy (MeV), Surface LET in Si (MeV/cm²/mg), Range in Si (μm). Rows include 16O, 20Ne, 36Ar, 48Ca, 64Ni, 84Kr, 100Xe, 129Xe.

Table II: TAMU Test Heavy Ions

Table with 4 columns: Ion, Energy (MeV), Surface LET in Si (MeV/cm²/mg), Range in Si (μm). Rows include 14N, 20Ne, 40Ar, 60Cu, 84Kr, 108Xe, 132Xe, 156Xe, 180Kr, 208Pb, 244Pu.

Table V: Summary of SEE Test Results

Table with 9 columns: Part Number, Manufacturer, LDC or Wafer#, Device Function, Technology, Particle, Test Results, Supply Voltage, Sample Size. Rows include IRHLF87Y20, S71414DN, SQR431EP, SMHF2812D, CPM2-1200-0025B.

Table with 9 columns: Part Number, Manufacturer, LDC or Wafer#, Device Function, Technology, Particle, Test Results, Supply Voltage, Sample Size. Rows include Jetson TX1, Snapdragon 820, RT4G-150-CB1657, XCK7K325T-1F8G900.

Table with 9 columns: Part Number, Manufacturer, LDC or Wafer#, Device Function, Technology, Particle, Test Results, Supply Voltage, Sample Size. Rows include H27QDG822C8R-BCG, IMMX64M64D3DSU8AG-E125, HM268128.

Table with 9 columns: Part Number, Manufacturer, LDC or Wafer#, Device Function, Technology, Particle, Test Results, Supply Voltage, Sample Size. Rows include AD9257, LTC6268-10, LTC6103.

Diodes:

Table with 9 columns: Part Number, Manufacturer, LDC or Wafer#, Device Function, Technology, Particle, Test Results, Supply Voltage, Sample Size. Rows include JANTX1N6843CCU3, JANS1N6843CCU3, SBR10U60D1, SBR1045D1, SBR160S23, BZXR4-75, BZX84C75, HSPM-3810, BAS21-7-F.

Miscellaneous Devices:

Table with 9 columns: Part Number, Manufacturer, LDC or Wafer#, Device Function, Technology, Particle, Test Results, Supply Voltage, Sample Size. Rows include ADV212, KSW-2-46+, AD8138.

As in our past workshop compendia of NASA Goddard Space Flight Center (GSFC) test results, each DUT has a detailed test report available online at <http://radhome.gsfc.nasa.gov> describing the test method, SEE conditions/parameters, test results, and graphs of data. The Test Results and Discussion section contains summaries of testing performed on a selection of featured parts.

Test Results and Discussion

Diode Failure Summary

In the 2016 "Compendium of Single Event Effects Results from NASA Goddard Space Flight Center," we presented the top-level results of the SEE testing of a variety of diodes. One of the diodes discussed was the Diodes, Inc. SBR20A300, which is a dual 300-V, 20-A super barrier diode. A decapacitated DUT is shown in Fig. 5 mounted on a daughtercard. Five of the SBR20A300s were irradiated at LBNL with 1233 MeV Xe, which has an LET of 58.8 MeV/cm²mg. These parts experienced catastrophic failure when reverse biased at 225 V or 300 V (the parts were only biased at increments of 25% of the rated reverse voltage.) However, when biased at 50% of the rated reverse voltage, 150 V, only charge collection was observed. Fig. 6 shows the reverse current during the beam run where the diode was reverse biased at 150 V. When the SBR20A300 is reverse biased at 150 V (50% of the rated reverse voltage), only charge collection is observed after the beam is turned on at time 0s.

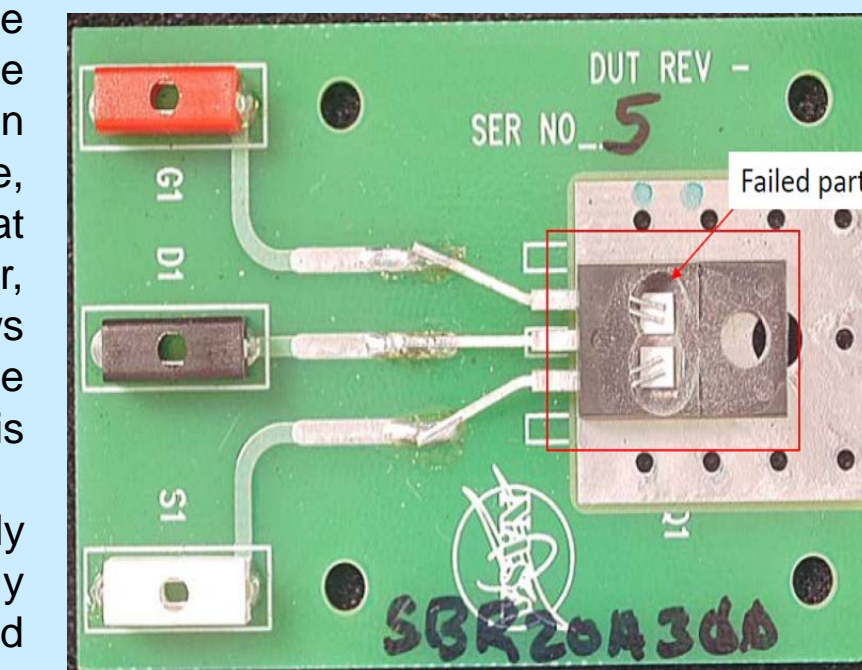


Fig 5. An example DUT of the SBR20A300 super barrier diode manufactured by Diodes, Inc. is mounted on a daughtercard for heavy-ion irradiation at LBNL.

The beam shutter was opened (beam was turned on) at time 0 s, and charge collection was immediately observed. When the shutter was closed (beam was turned off), the reverse current recovers to approximately the original value. After power was removed from the DUT, after the beam was turned off, the forward and reverse currents and voltages were measured to determine if any degradation occurred. No shifts were observed in any of these parameters. The reverse voltage on the same DUT was then increased by 25% to 225 V and irradiated. Shortly after the beam was turned on, the reverse current begins to increase and then suddenly the current increases to the point where the anode and the cathode are shorted and the amount of reverse current is limited by the compliance settings on the power supply. This is shown in Fig. 7. When the SBR20A300 is reverse biased at 225 V (75% of the rated reverse voltage), almost immediately after the beam is turned on at time 0s, the part begins to experience damage and the reverse current increases by 10s of nA. Less than 1s later, the part experiences catastrophic failure and the anode and cathode are shorted.

After the beam run is over, there were significant shifts in the electrical parameters Fig. 8 shows the reverse current as a function of the reverse voltage, and while there was little shift from the pre-rad measurements after the part was irradiated while biased at 150 V (50% of the rated reverse voltage), the part exceeded the specification for reverse current (10 μA) before the reverse voltage reached 1 V, which is well below the specification of 300 V. After the SBR20A300 is irradiated while biased at 150 V there is effectively no change in the reverse current as a function of reverse voltage when compared to the pre-irradiation values. However, when the reverse current-reverse voltage sweep is measured after the part was irradiated while biased at 225 V (75% of the rated reverse voltage), the specification for reverse current (maximum of 100 μA) was exceeded before the reverse voltage reached 1 V, indicating that the anode and cathode were shorted.

After returning to Goddard, several of these parts were taken to the Parts Analysis Lab (Code 562) for failure analysis. Two locations on the SBR20A300 show elevated temperatures when a small bias is applied and the DUT is photographed using an infrared camera. These elevated temperatures are due to high currents created by shorts between the anode and cathode that were created after irradiation with heavy ions.

The parts were photographed with a thermal infrared camera with a small reverse bias applied (Fig. 9.) The bright white spot in the upper left corner of the die along the guard ring was quickly determined to be a failure location, and a second darker spot about halfway down the left side along the guard ring was also identified, shown in the upper left corner of the thermal image in Fig. 9, this photograph taken with a camera. These locations were photographed with a high-magnification optical microscope and these images can be seen in Figs. 10 and 11. Only the brighter, upper corner failure location will be discussed in this work. The DUT was then cross-sectioned at the location of the failure. Fig. 12 shows the location of the failure in cross-section. A large void is visible, as are cracks due to stress from the excessive that resulted from the heavy ion strike. There is also a large mound directly below the void that was created after the silicon melted and then reformed. A large void is observed from the displacement of molten silicon, as is a large mound-shaped region directly below the void. In addition, cracks are observed due to stress from the excess heat created by the heavy ion as it passed through the diode.

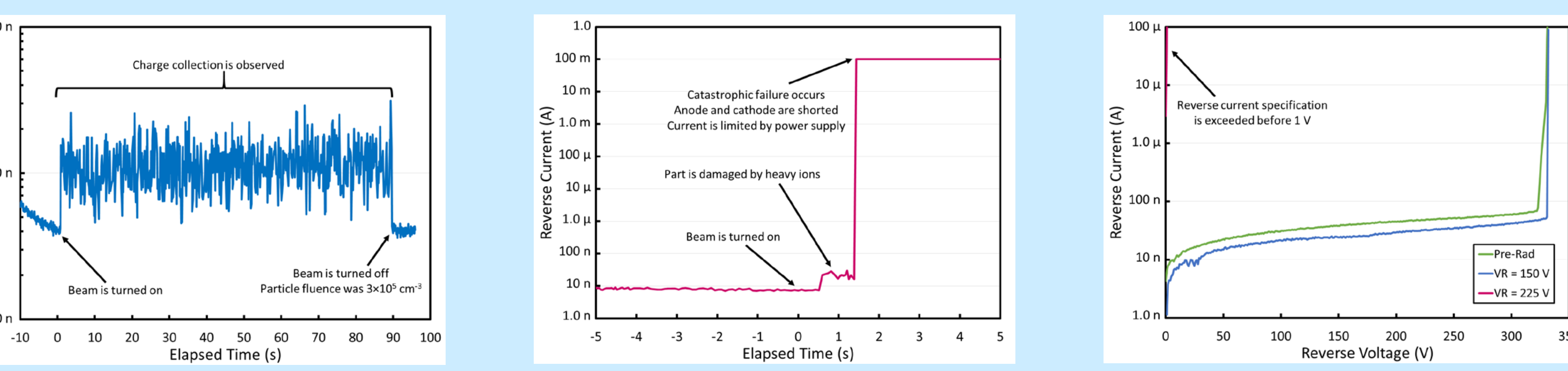


Fig 6. SBR20A300 reverse current, charge collection. Fig 7. SBR20A300 reverse current, catastrophic failure. Fig 8. SBR20A300 reverse current as a function of reverse voltage, anode – cathode short.

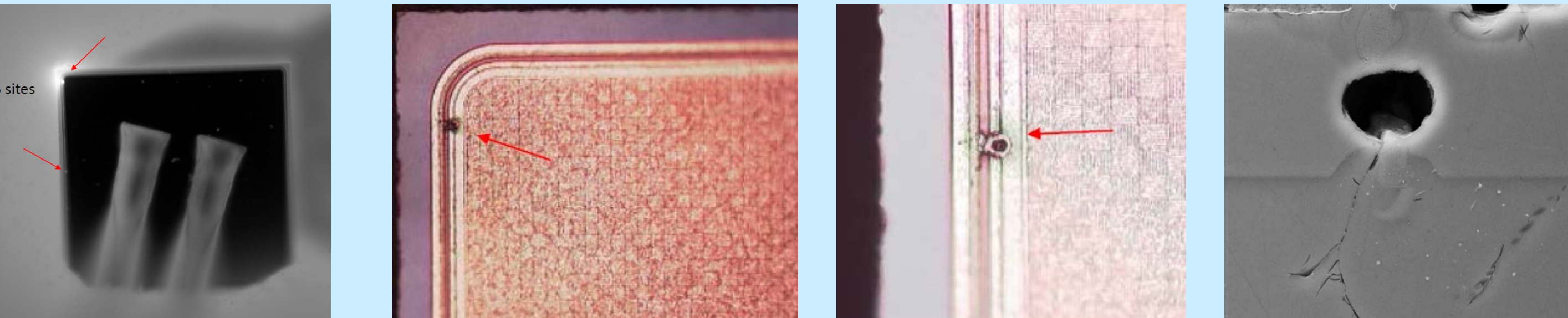


Fig 9. SBR20A300 photographed using an infrared camera. Fig 10. SBR20A300 failure location 1. Fig 11. SBR20A300 failure location 2. Fig 12. Cross sectioned view of failure.

LTC6268-10 Linear Technology Operational Amplifier

We irradiated 7 samples with 15 MeV/amu heavy ions at TAMU and with 10 MeV heavy ions at LBNL. The SEE test circuit was configured with a gain of 100 dB.

We found that the LTC6268-10 is susceptible to heavy ion-induced SET. We evaluated the SET characteristics for an input current of 10, 100, and 200 nA. The output trigger was set to 200 mVpp to compensate for the level of facility background noise.

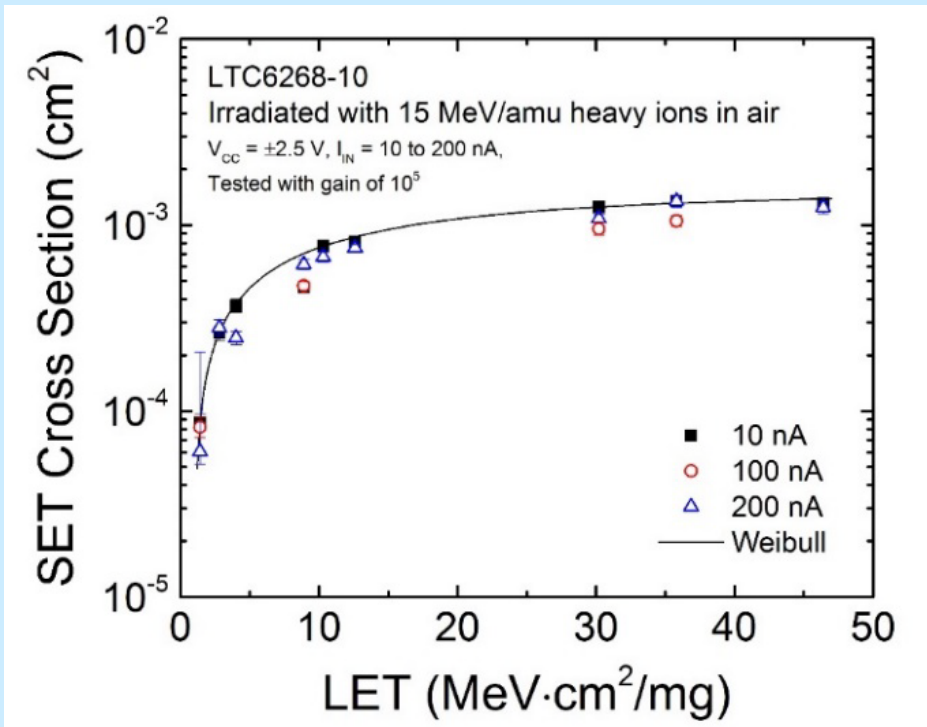


Fig. 1. SET cross section vs. effective LET for the LTC6268-10 irradiated with 15 MeV/amu heavy ions in air.

Fig. 1 shows the SET cross section vs. effective LET for various input currents. Fig. 2 shows a SET amplitude vs. duration distribution plot. The figure shows that the SETs can be generally divided into two categories: 1) SETs with a short duration on the order of microseconds, and 2) SETs with long duration on the order of milliseconds. The majority of SETs have duration less than 7 μsec. Fig. 3 shows an example of a worst case SET.

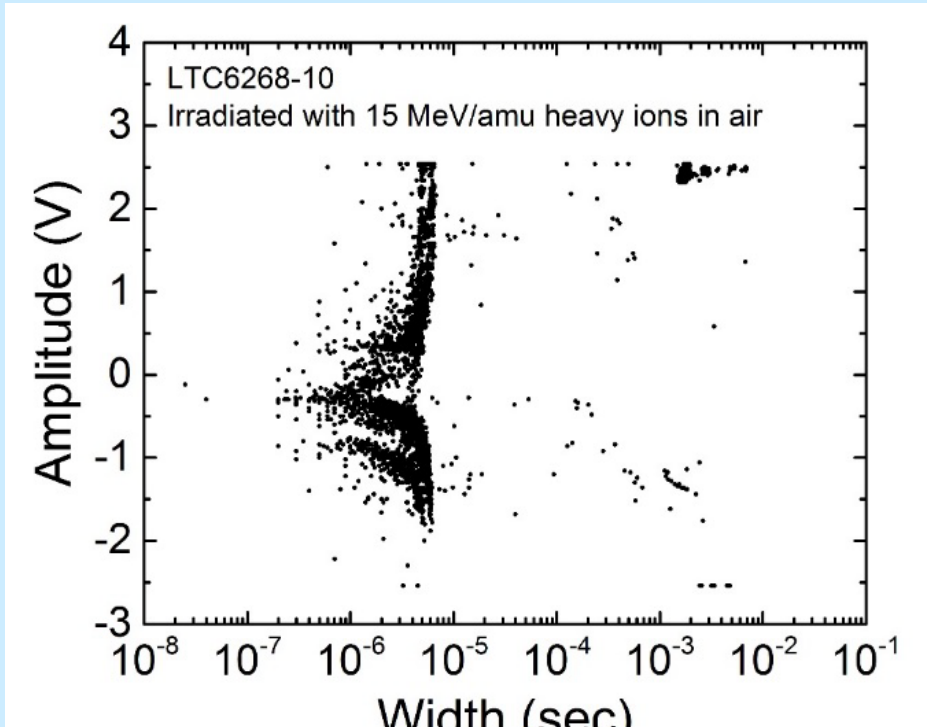


Fig. 2. SET amplitude vs. width plot for (all LETs) for the LTC6268-10 irradiated with 15 MeV/amu heavy ions in air.

Fig. 4 shows a column bar chart of the SET count for small and large events at input currents of 10, 100, and 200 nA. The SET count generally increases with decreasing input current for both small and large events.

Furthermore, the number of small events increases significantly with decreasing input current. The SET count for small events is significantly higher at 10 nA relative to 100 and 200 nA.

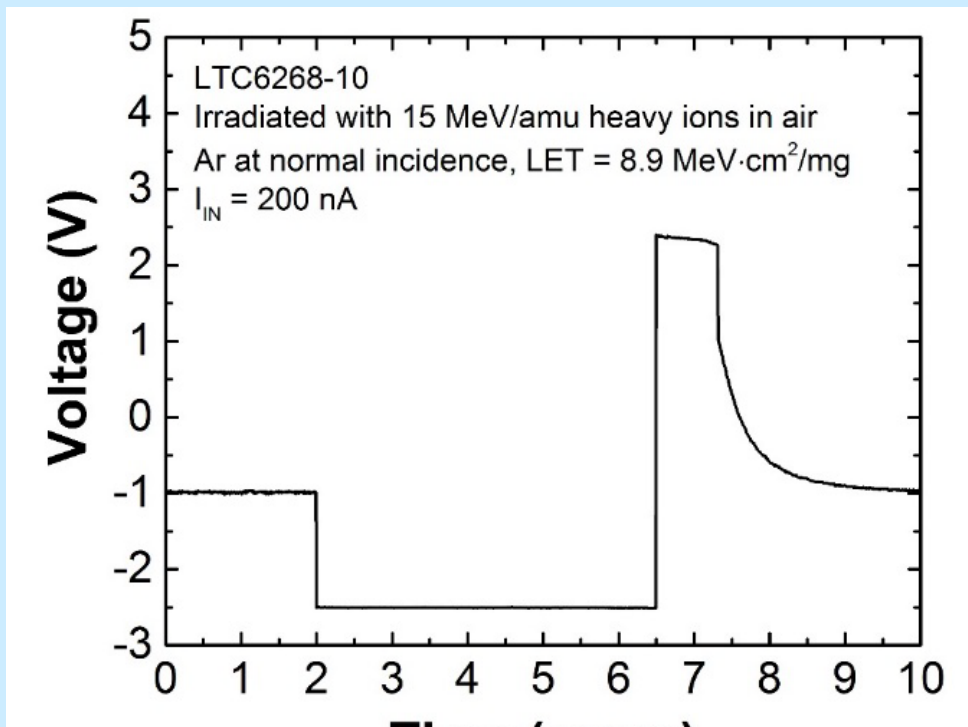


Fig. 3. SET characteristics for the LTC6268-10 (for all LETs) irradiated with 15 MeV/amu heavy ions in air.

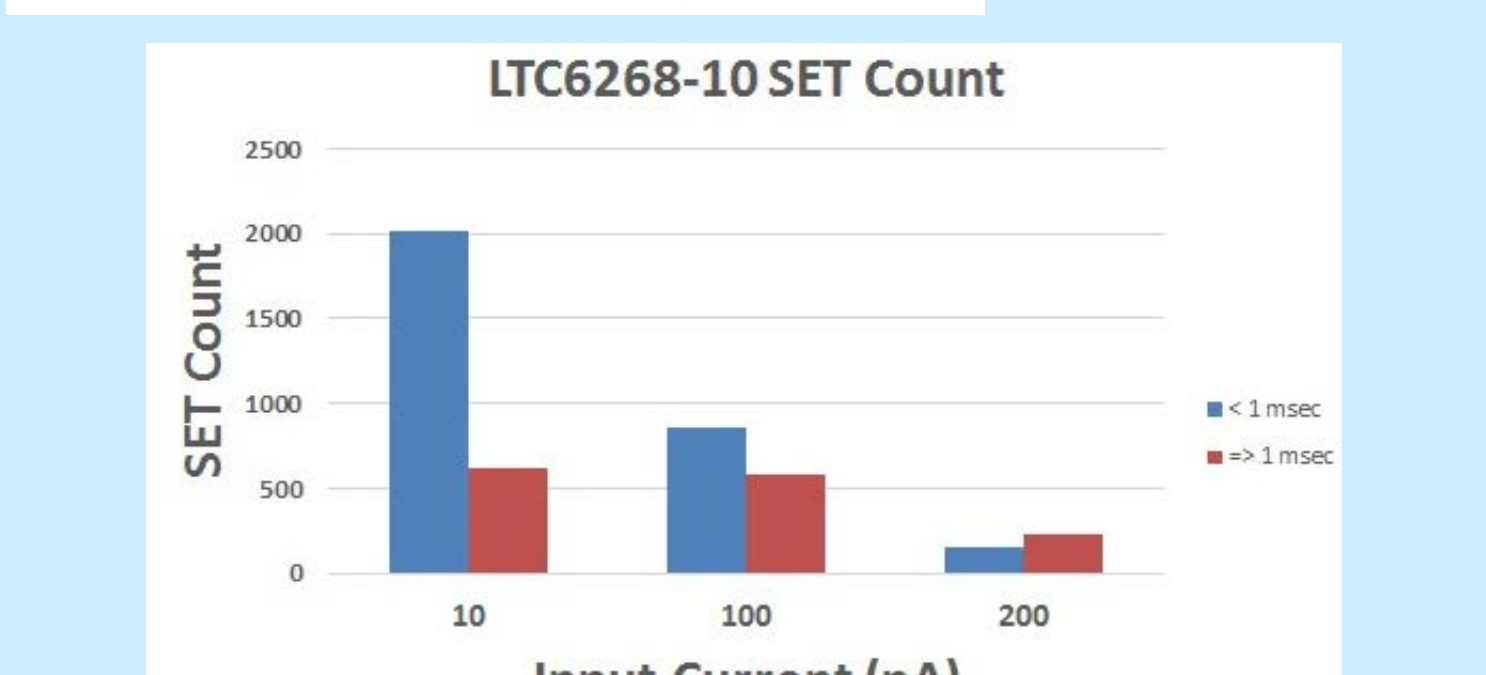


Fig. 4. SET count vs. input current for the LTC6268-10 irradiated with 15 MeV/amu heavy ions in air. The SETs are divided into two categories with respect to its duration: < 1 msec, and ≥ 1 msec. Data represents all LETs tested (Ne, Ar, Kr, and Au). The proportion of large and small SETs showed no clear dependence on LET.

Summary

We have presented current data from SEE testing on a variety of mainly commercial devices. It is the authors' recommendation that these data be used with caution. We also highly recommend that lot testing be performed on any suspect or commercial device.

Acknowledgment

This work was supported in part by the NASA Electronic Parts and Packaging (NEPP) Program, NASA Space Technology Mission Directorate Game Changing Technology Division, and NASA Flight Projects. The authors gratefully acknowledge members of the Radiation Effects and Analysis Group who contributed to the test results presented here: Hak Kim, Anthony M. Phan, Donna J. Cochran, James D. Forney, Christina M. Seidleck, and Stephen R. Cox. Special thanks go to Stephen P. Buchner and Dale McMorrow, Naval Research Laboratory for their excellent support of the laser testing.