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Experimental and Computational Study of a Micro Vertical Axis Wind Turbine

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Abstract

With recent surge in fossil fuel prices and demand for cleaner renewable energy sources, wind turbines have become an alternative technology for power generation. Greenhouse gases such as carbon dioxide (CO₂) emitted into the atmosphere contribute to the global climate change. This paper investigates the design of a Savonius type vertical axis wind turbine and its potential to generate power. To enhance the performance of the turbine, a flow restricting cowl is incorporated into the turbine. The airflow behavior of the turbine was investigated both experimentally and computationally. Three different configurations were studied (open position, centred position and a closed position). It is found that a partially cowed turbine in a centred and closed position resulted in a better performance of the turbine than a fully cowed turbine with the same configuration.

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Nomenclature

V	Velocity
A	Area
m	Mass
P	Power
ρ	Density
VAWT	Vertical Axis Wind Turbine
HAWT	Horizontal Axis Wind Turbine
CFD	Computational Fluid Dynamics
CO ₂	Carbon Dioxide

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1. Introduction

Wind energy is fast becoming an alternative source of energy to generate power. With the current state of the world development, our demand for energy has increased exponentially and as a result, more fossil fuel such as coal are burnt resulting in CO₂ emissions into the atmosphere. The emission of CO₂ into the atmosphere contributes to the global climate change. To tackle this problem, many of the developed nations are continuing to invest heavily in renewable energy sources. As part of the global CO₂ emission reduction strategy, Australia has developed policies to generate power from renewable energy of at least 20% by the year 2020 [1].

Harnessing the energy of the wind is a clean and reliable way of reducing our dependency on fossil fuel thereby decreasing the CO₂ emission into the atmosphere. Wind turbines allow the conversion of wind energy to kinetic energy for electricity generation. While there are currently a range of wind turbines being used for power generation, the bulk of these wind turbines are extremely large and used for large scale power producing (up to 4 MW) [2]. These large wind turbines are required to be placed in non-populated areas where there is minimal flow disturbance from nearby objects as well as to minimise discomfort to surrounding dwellings. The type of wind turbines available today, the horizontal axis wind turbine (HAWT) is the most common type of wind turbine both commercially and domestically [3]. The geometrical shape and size of the blades are very critical as they ultimately determine the amount of energy that can be extracted from the wind. Unlike HAWTs, which requires a yaw mechanism to align itself at the direction of the wind, vertical axis wind turbines (VAWTs) are less sensitive to a change in wind direction. This is particularly an important advantage for the effective use of VAWTs in urban and suburban environments [4]. VAWTs are typically classified into two categories: a Darrieus and a Savonius. A Darrieus turbine rotor relies on lift to generate torque, whereas a Savonius turbine rotor relies on drag. Both of this type design have a single purpose that is to, generate power [5]. Regardless of the type of wind turbine, the main goal of a wind turbine is to extract as much energy as possible from the wind. Every object, including air, in motion will have some amount of kinetic energy. The kinetic energy of air passing through the turbines is converted into mechanical energy and ultimately into electrical energy. To determine the amount of power available in the wind, the following equations are used.

$$E_K = \frac{1}{2} m V^2 \quad (1)$$

$$\dot{m} = \rho AV \quad (2)$$

Substituting Eq. (2) into Eq. (1), the idealized equation for power generated from wind by the turbine is obtained as shown in Eq. (3):

$$P = \frac{1}{2} \rho AV^3 \quad (3)$$

The maximum theoretical coefficient of performance or otherwise known as Betz limit is defined as 16/27 or 0.59 [6]. What this actually means is that for any given wind turbine, the maximum energy it can extract from the wind is 59 per cent of the wind's energy. In practice however, the best modern wind turbine can achieve a coefficient of performance of about 40 per cent. This is the maximum value, achievable over a narrow band of wind speeds. The actual coefficient of performance will vary with wind speeds.

Small scale wind turbines can generate electricity for households and in turn reduce the power bill and carbon footprint. However, a residential wind turbine needs to be small and inexpensive to mount and install as well as to operate efficiently. The small scale wind turbine can be installed on roofs of houses and on buildings [7]. It is well known that there are a large number of small scale wind turbines in the market that can be implemented in a domestic environment, however, their power generation efficiencies are questionable. Small scale wind turbines face complex wind conditions at the height at which they operate. Due to the complexity of wind conditions in built up areas, where the atmospheric wind is highly turbulent, small wind turbines need a smart design that can operate more efficiently and generate more power at low wind speeds.

A major disadvantage for VAWTs is that, as the airflow moves through the rotor, it has to come in to contact with the rotating blades as it exits the rear. This creates a negative torque on the rotor and the exiting air stream is directed back in to the incoming free stream. A turbulent region is produced due to the interaction of the exiting air stream and incoming free stream which not only introduces losses minimising efficiency, but also creates a pressure fluctuations that produce vibrations in the turbine [8]. This unstable flow restricts the rotor from accelerating to higher torque producing speeds. In order for VAWTs to extract maximum energy and reduces losses due to turbulence, it is important to have a good understanding of the flow behaviour on VAWTs. Several flow enhancing devices have been proposed in the past to minimise the airflow on the non-torque side of the rotor and the majority of them have proven to be ineffective as they

have the adverse effect of causing a high pressure zone and very little additional air is directed onto the actual rotor.

In this paper, we propose a new concept of vertical axis wind turbine that can generate more power under turbulent wind environment. To reduce the turbulence of the VAWTs we propose simultaneously shielding parts of the rotor from the wind, whilst directing to those parts where it can more efficiently impart momentum to the rotor.

Figure 1 shows a new vertical axis wind turbine with cowling concept that can potentially extract more power from the wind and on the trailing blades of a vertical axis wind turbine and allow for higher resultant torques produced by the wind turbine

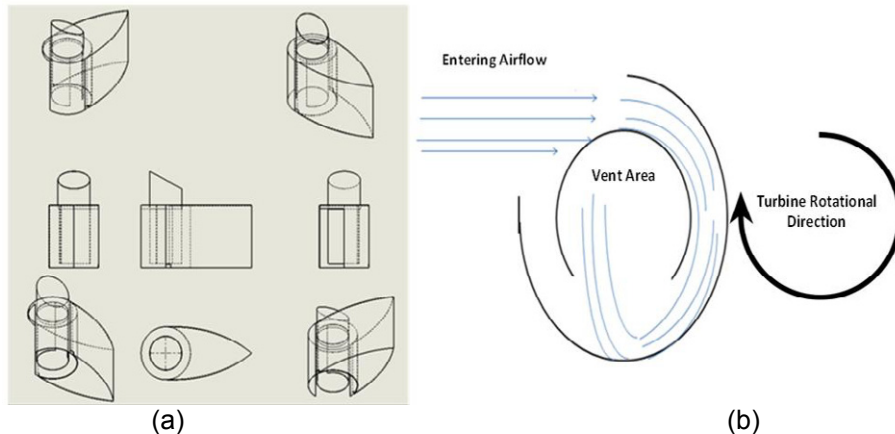


Fig.1. (a) Concept cowling; (b) Cross section of the wind turbine and visualization of the flow direction

The concept of cowling, developed by Wind Energy Technology Pty Ltd Australia, incorporates an outer cowling with a tail section. The tail section of the outer cowling allows even flow over both sides of the cowling when the cowling is in line with the airflow. When the cowling is not in line with the airflow there will be a pressure differential between the two sides of the turbine cowling, and if the cowling is mounted on a bearing, the cowling will yaw to an in line with the flow position. The concept cowling also incorporates a vent tube in the center of the turbine rotor and an induction chimney. The inner vent tube has the main purpose of allowing the flow over the turbine blades and to recirculate the flow in the turbine as seen in Figure 1 (b). The chimney is one of the critical features of the cowling. The main purpose of the chimney is to allow the airflow to exit the cowling. The secondary effect of the chimney is to create a pressure differential in the vent tube and induce a flow swirling in the middle of the turbine. This flow swirling induces a flow rotation which will create a low pressure at the entrance to the vent tube and from this increase the driving force of the turbine. The primary objective of this paper is to undertake an experimental and computational investigation of the concept and explore its potential for power generation.

2. Methodology

2.1. Wind Tunnel Test

To investigate the concept of cowling, a wind tunnel test was conducted at RMIT University industrial wind tunnel. The wind tunnel was used to evaluate the performance of the wind turbine over a range of wind speeds. The data obtained from these tests would determine if a flow restricting device improves the performance of a wind turbine and at which speeds the turbines operate most efficiently and can provide data that would allow the optimisation. Three configurations have been tested. These configurations are:

- a) Bare rotor (no cowl)
- b) Cowled with no induction vent tube
- c) Fully cowled

The bare rotor is the control configuration for benchmarking. The bare rotor is not cowled and has no features that would enhance or degrade the performance of the turbine. The results obtained from the testing of this configuration were used to determine whether the other configurations would have a positive or negative effect on the performance. The second

configuration to be tested is the cowed configuration without induction vent tube. This configuration consists of a turbine rotor being covered only by the external wall of the cowl which should allow large amounts of flow to circulate within the cowling. This configuration is not a part of the induction chimney and would allow to determine if the induction chimney and flow restricting vent tube have a major effect on the performance of the prototype wind turbine. The last major configuration is the fully cowed configuration. The Fully cowed configuration consists of external cowling walls, induction vent tube and chimney. The tail section would allow the testing of the pivot feature of the turbine. The testing of all three configurations allows the performance increase or decrease caused by separate cowling features.

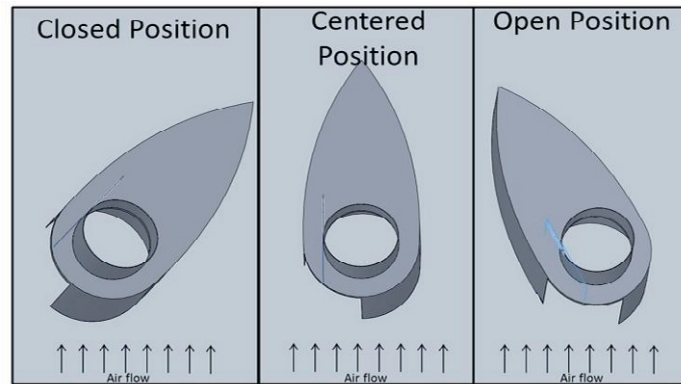


Fig.2. Test configurations

During the testing, the orientation of the cowling was considered. The cowling utilises a 90° opening to restrict flow over the turbine rotor. Depending on the orientation of the cowling the airflow can be directed over the driving more than the forward moving blades or oppositely over the forward moving blades that causes high resistance. As the turbine cowl is designed to pivot in the wind it is was decided to test different opening positions to determine the best possible opening position with respect to the airflow that would result in a better performance of the wind turbine. The closed position was expected to direct flow predominantly over the driving blades and should reduce any back flow over the forward moving blades that would cause resistance. The closed position should however allow less flow over the entire rotor than any of the other positions. The centred position was used for the main flow entrance position of the turbine cowl. This position should allow a large air flow over the driving section of the turbine, while it is expected to reduce flow over the forward moving, resistance producing blades. The open position should allow the largest possible airflow over the turbine rotor; however this position is most likely to have high flows over the forward moving blades which should result in a high drag on the turbine rotor. While the drag load has the potential to be high the potential for high flows over the driving turbine blades could be large enough to drive the rotor.

Figure 3 shows the experimental setup of the wind turbine in RMIT University wind tunnel at zero degree yaw angle. The full scale turbine was tested for wind speeds up to 30km/h. The initial wind speed at which the turbine began to rotate was recorded. It was noted during the test that, if the wind tunnel speed was reduced, the rotor would continue to spin at lower wind speeds than which it began to rotate initially.



Fig.3. Wind turbine prototype made from stainless steel.

2.2 Computational modelling

Computational Fluid Dynamics (CFD) modeling is a common practice in engineering to understand airflow behaviour around an object. To aid this investigation, CFD modeling was undertaken to understand the airflow velocities and air pressure distribution around the turbines. The turbine model varies from the full scale wind tunnel tested model in several ways. The main critical difference is that the CFD model has a very small clearance (less than 1mm) between the edges of the turbine blades and the cowling walls. Because of this there is less flow through the turbine than that of the real model. While this is a major difference, the small wall clearance coincides with the ideas and concepts when the turbine as initially designed. Because of this the CFD is valid for a proof of concept and will also allow the concept to be simulated in its most idealised state. Another major point that needs to be noted is that the airflow over the turbine is modelled to be for one particular wind speed of 36km/h and the turbine is specified to be spinning at a constant revolution per minute (RPM) of 100. This will allow the flow to be visualised for a particular case and allow of a general idea to be formed about the flow through the turbine, however the flow pattern is expected to vary with wind speed and RPM. The CFD analysis is used for comparison purpose.

3. Results

3.1 Full Scale Prototype

Full scale prototype made of stainless steel was manufactured. The turbine configurations results were compared to each other with respect to the cowling inlet positions. The cowling inlet position is used to separate the comparisons as each position would allow a different mass flow through the turbine rotor and a varying potential energy of the turbine. Each position is compared to the bare rotor configuration to validate the effect of a cowl. Therefore all results were compared to the uncowed configuration to determine the effect of the cowl.

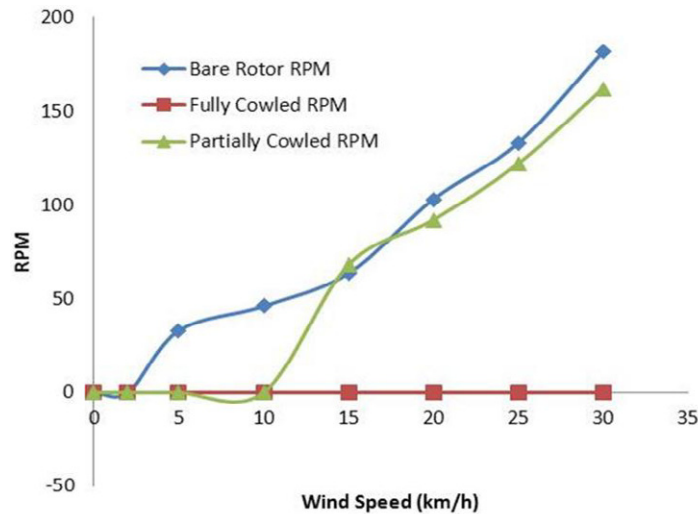


Fig.4. Comparison of configurations for centred position.

It can be seen from Figure 4 that the highest RPMs are reached by the bare rotor and that the fully cowled configuration does not allow rotation. The partially cowled configuration generates rotational speeds that are close to that of the bare rotor for wind speeds of 15km/h and 20km/h, but after that it begins to drop off. It can also be seen that the bare rotor is significantly more effective at wind speeds below the 15km/h. Overall it can be said that the best performance was achieved by the bare rotor for the centred position over the entire range of wind speeds. At 15km/h wind speed, the rotational speed of the partially cowled turbine configuration had slightly higher rotational speeds than fully closed configuration. The rotational behaviour of these two configurations was considered to be very similar.

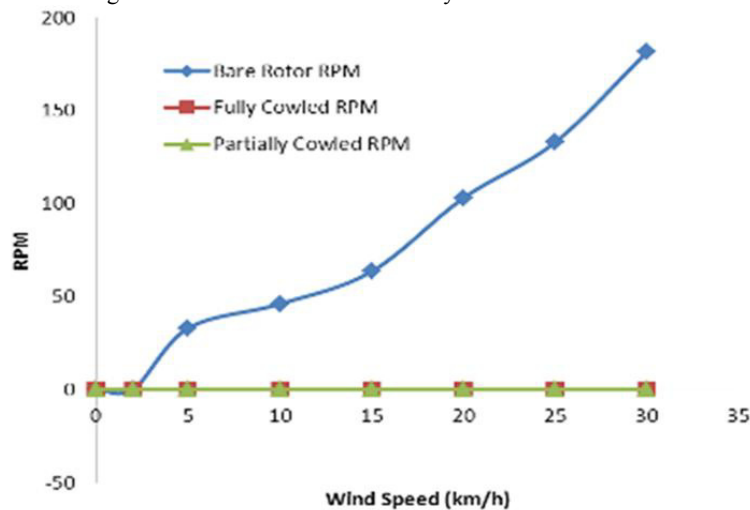


Fig.5. Comparison of configurations for open position.

For the open position, neither partially cowled nor fully cowled configurations produce any rotational motion due to the restricted flow over the turbine. The design of the cowl should allow self-alignment with the wind direction in order to increase the rotational speeds.

Figure 6 shows that the bare rotor is most efficient configuration as no rotational motion was noted below 15 km/h under partially and fully cowled closed positions. The fully cowled turbine started rotating at speeds over 20 km/h. The frequency of rotational motion is still lower than frequencies of partially cowled and the bare rotor configurations. At wind speeds

exceeding 20 km/h, no variation in RPM readings for the partially cowled turbine and bare rotor was observed (Figure 6).

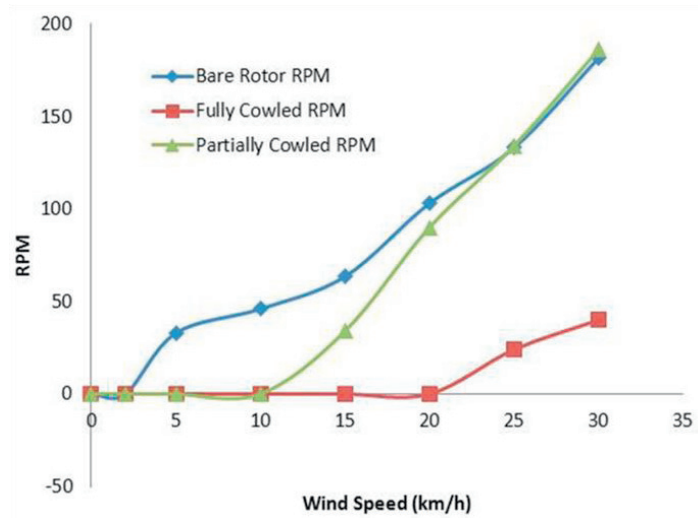


Fig.6. Comparison of configurations for closed position.

3.2 Small Scale Prototype

A small scale prototype wind turbine was manufactured using cardboard. This prototype is significantly lighter and smaller than the stainless steel made prototype. The cardboard made prototype has less inertia compared to the steel prototype. It is expected that the cardboard made prototype will start rotating at lower wind speeds. The prototype is shown in Figure 7. The cardboard model was tested under a range of wind speeds. However, the maximum speed was restricted due to the fragility of the model. The primary purpose was to see whether the model's susceptibility to the lower wind speeds.

The results obtained from the wind tunnel showed that the bare rotor started rotating at very low wind speed (below 1 m/s). The rotational speed was almost linearly increased at wind speeds 10 m/s and above. In contrast, the rotational speed increased significantly when the cowl was introduced. As shown in Figure 8, the rotation speed of the turbine with cowl was increased at speeds tested and the variation in RPM is more than doubled.

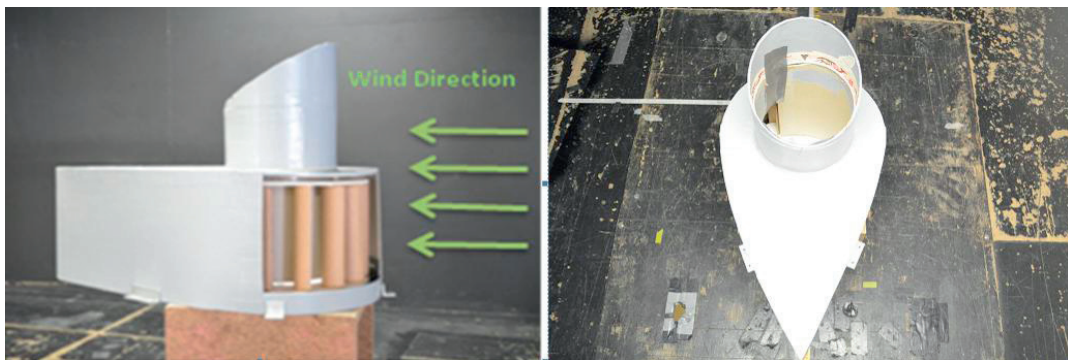


Fig.7. Wind turbine made from cardboard.

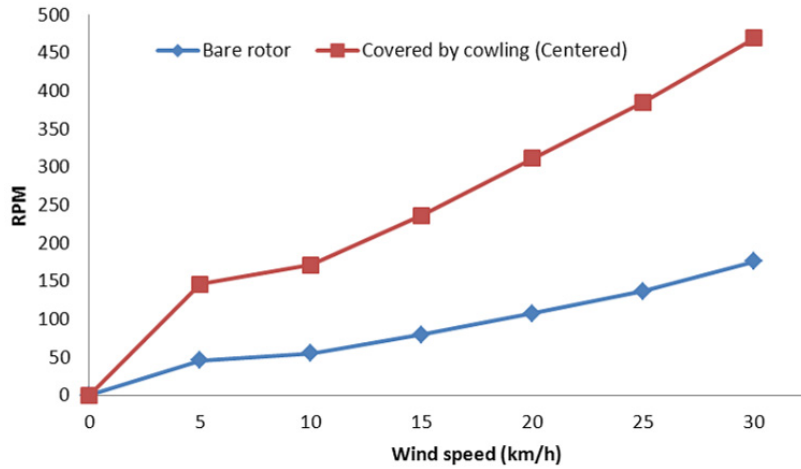


Fig. 8. Wind tunnel results for bare rotor and cowling wind turbine.

2.2 Computational Modelling

The computational modelling of the wind turbine was undertaken to determine and visualise the airflow direction, pressure contours and velocity profiles. At first the flow through the bare rotor was modelled. In the modelling, the rotor was purely exposed to the oncoming airflow and no restriction was applied to it. A single reference frame condition was applied for this analysis in order to predict the flow behaviour. The model geometry is based on cardboard prototype model.

The static pressure distributions on the bare rotor and the cowl are shown in Figures 9 and 10 respectively. The simulated results indicate that there is significant variation in static pressure distribution in and around the blades. The variation is especially larger between front and rear blades. The variation of pressure difference is causing the rotational motion of the rotor.

Figure 10 shows the static pressure distribution on the cowl surface. One side of the cowl experiences higher pressure than the other side resulting in the self-regulated alignment of the cowl with the wind direction. Blades near the opening of the cowl are exposed to low pressure zone thus allowing higher air velocity through the opening which drives the blades. The blades at the rear do not experience any resistive air pressure. As a result, they need to perform significantly less work.

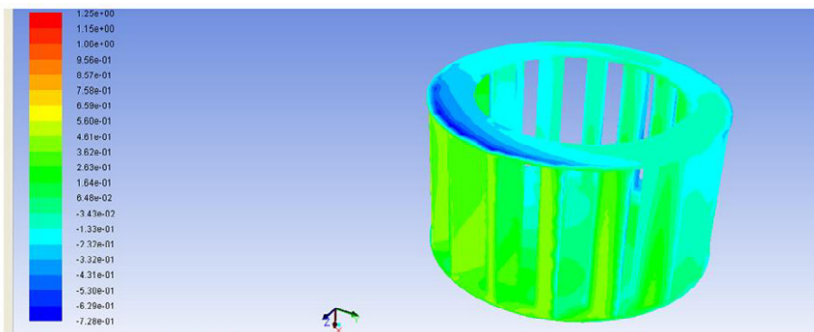


Fig.9. Pressure distribution around the blades.

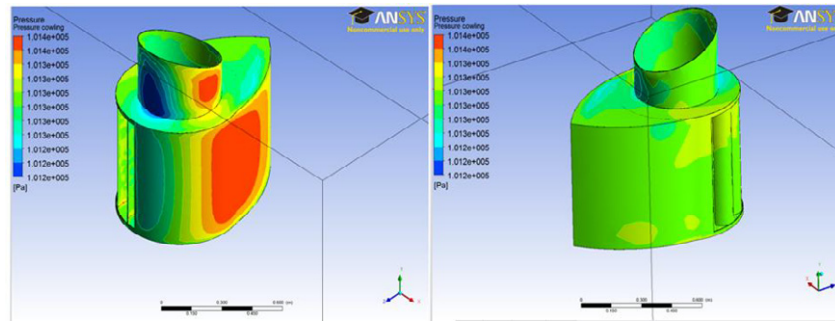


Fig.10. Side pressure difference of cowled turbine.

4. Conclusion

A vertical axis scale wind turbine was investigated under three different configurations to enhance its performance. Two prototype wind turbines (steel made and cardboard made) were studied. For the steel prototype, the fully cowled configuration in closed position is the least efficient of all the turbine configurations. The fully cowled configuration only produced a rotation in closed position for high wind speeds. The Partially cowled configuration showed relatively better performance compared to fully cowled for the centred and closed positions. The open position did not produce any rotational motion for the partially cowled and fully cowled configurations. The partially cowled configuration generated similar RPMs as the bare rotor for high wind speeds; however at low wind speeds this configuration did not perform well. The open position induces high resistance on the turbine resulting in no rotational motion. However, the closed position reduces the resistance and significantly increases the rotational motion.

For cardboard made wind turbine, the cowling showed a significant improvement over the bare rotor at all speeds. The cowling position proved to be a major factor for the turbine. The heavier the turbine, the higher the wind speed is required to generate motion at the beginning. The lighter turbine is shown to be better at all speeds.

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