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Multi-objective optimization in the presence of practical constraints using non-dominated sorting hybrid cuckoo search algorithm

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ABSTRACT

A novel optimization algorithm is proposed to solve single and multi-objective optimization problems with generation fuel cost, emission, and total power losses as objectives. The proposed method is a hybridization of the conventional cuckoo search algorithm and arithmetic crossover operations. Thus, the non-linear, non-convex objective function can be solved under practical constraints. The effectiveness of the proposed algorithm is analyzed for various cases to illustrate the effect of practical constraints on the objectives' optimization. Two and three objective multi-objective optimization problems are formulated and solved using the proposed non-dominated sorting-based hybrid cuckoo search algorithm. The effectiveness of the proposed method in confining the Pareto front solutions in the solution region is analyzed. The results for single and multi-objective optimization problems are physically interpreted on standard test functions as well as the IEEE-30 bus test system with supporting numerical and graphical results and also validated against existing methods.

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1. Introduction

Due to the continuous increase in demand, research interest is focused towards the efficient operation and planning of power systems. Increased utilization and depletion of natural and fossil fuels means the research focus must include economic as well as environmental concerns. In general, the economic dispatch (ED) problem aims to increase utilization at the lowest cost of fuel.

Many classical and evolutionary approaches have been proposed to solve optimization problems with various power system objectives. Heuristic optimization techniques have been considered to solve constrained non-linear optimization problems. These methods are being used to solve problems such as economic dispatch, emission dispatch, optimal reactive power dispatch, etc. Some of the heuristic optimization techniques given in [1–26] are used to solve single objective and [27–42] to solve multi-objective optimization problems.

Recent focus has been towards economic-emission dispatch [43–49], where multi-objective evolutionary search strategies have been applied, such as non-dominated sorting genetic algorithm (NSGA) [50], Niche Pareto genetic algorithm [51], strong Pareto evolutionary algorithm [52], NSGA-II [53], multi-objective particle swarm optimization [54].

Reviewing the literature, hybridization of optimization algorithms may increase the effectiveness of an algorithm's performance. In this paper, a new algorithm is proposed incorporating arithmetic crossover into a conventional cuckoo search algorithm (CSA) [55,56], which we have called the hybrid cuckoo search algorithm (HCSA). The applicability and performance of the proposed method is analyzed in terms of convergence rate and the quality of the solution. The proposed method is validated against existing systems and is applied to solve electrical test systems with the objectives of minimizing generation fuel cost, emission, and total power loss. Non-dominated sorting-based methodology is adopted along with the proposed HCSA to solve the multi-objective optimization problem. The single and multi-objective optimization results for the electrical test systems are validated against existing literature methods. The multi-objective solution strategy is calibrated in terms of the confinement of the Pareto solutions. Finally,

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we assess the effectiveness of the proposed fuzzy decision making tool in selecting the compromised solution from the best Pareto for two and three objective optimization problems. The entire methodology is tested using standard test functions and the IEEE-30 bus test system with supporting numerical and graphical results.

The optimal power flow (OPF) problem is formulated in Section 2, and various system constraints, handling of practical constraints and the conversion of constrained optimization problem to unconstrained optimization problem through penalty approach are developed. The objectives are formulated in Section 3, including the methodology related to HCSA. In Section 5, we develop the multi objective solution strategy and present the various results and analyses for standard test functions and electrical test systems in Section 6. Finally, we summarize our findings and discuss future work in Section 7.

2. Problem formulation

In general, the aim of the OPF problem is to identify a set of control variables that optimize certain power system objectives while satisfying system and practical constraints.

The OPF problem can be mathematically expressed as

$$\text{Min } A_m(x, u) \quad \text{s.t.} : g(x, u) = 0 \text{ and } h(x, u) \leq 0,$$

where g and h are equality and inequality constraints, respectively; x is the state vector of dependent variables, such as slack bus active power generation (P_{G1}), load bus voltage magnitudes (V_l), generator reactive power output (Q_G), and apparent power flow (S_{line}); u is the control vector of independent variables (control variables), such as the generator active power output (P_G), generator voltage (V_G), transformer tap ratios (T), and the reactive power output of shunt compensators (Q_{sh}).

The state and control vectors can be mathematically expressed as

$$x^T = [P_{G1}, V_{l1}, \dots, V_{l_{NL}}, Q_{G1}, \dots, Q_{G_{NG}}, S_{l1}, \dots, S_{l_{nl}}]$$

$$u^T = [P_{G2}, \dots, P_{G_{NG}}, V_{G1}, \dots, V_{G_{NG}}, Q_{sh1}, \dots, Q_{sh_{nc}}, T_1, \dots, T_{nt}],$$

where NL , NG , nl , nc , and nt are the total number of load buses, generator buses, transmission lines, VAR sources, and regulating transformers, respectively.

The above problem is optimized satisfying the following constraints.

Equality constraints: These constraints are typically load flow equations:

$$P_{G,k} - P_{D,k} - \sum_{m=1}^{N_{bus}} |V_k| |V_m| |Y_{km}| \cos(\theta_{km} - \delta_k + \delta_m) = 0$$

$$Q_{G,k} - Q_{D,k} - \sum_{m=1}^{N_{bus}} |V_k| |V_m| |Y_{km}| \sin(\theta_{km} - \delta_k + \delta_m) = 0,$$

where P_{Gk} and Q_{Gk} are the active and reactive power generation at the k th bus, respectively; P_{Dk} and Q_{Dk} are the active and reactive power demands at the k th bus, respectively; N_{bus} is the number of buses; $|V_k|$ and $|V_m|$ are the voltage magnitudes at the k th and m th buses, respectively; δ_k and δ_m are the phase angles of the voltage at the k th and m th buses, respectively; and $|Y_{km}|$ and θ_{km} are the bus admittance magnitude and its angle between the k th and m th buses, respectively.

Inequality constraints

Generator bus voltage limits: $V_{G_i}^{\min} \leq V_{G_i} \leq V_{G_i}^{\max} \quad \forall i \in NG.$

Active Power Generation limits: $P_{G_i}^{\min} \leq P_{G_i} \leq P_{G_i}^{\max} \quad \forall i \in NG.$

Transformers tap setting limits: $T_i^{\min} \leq T_i \leq T_i^{\max} \quad \forall i \in nt.$

Capacitor reactive power generation limits: $Q_{sh_i}^{\min} \leq Q_{sh_i} \leq Q_{sh_i}^{\max} \quad \forall i \in nc.$

Transmission line flow limit: $S_l \leq S_l^{\max} \quad \forall i \in nl.$

Reactive Power Generation limits: $Q_{G_i}^{\min} \leq Q_{G_i} \leq Q_{G_i}^{\max} \quad \forall i \in NG.$

Load bus voltage magnitude limits: $V_i^{\min} \leq V_i \leq V_i^{\max} \quad \forall i \in NL.$

Here, P_G , V_G , T , Q_{sh} inequality constraints are self restricted constraints and can be satisfied forcibly within the OPF problem, where as the remaining three constraints and active power generation at slack bus are non-self restricted constraints and these can be handled using penalty approach [1]. With this, the generalized form of the OPF problem defined as

$$A_{aug}(x, u) = A(x, u) + R_1 \left(P_{G_1} - P_{G_1}^{\lim} \right)^2 + R_2 \sum_{i=1}^{NL} \left(V_i - V_i^{\lim} \right)^2 + R_3 \sum_{i=1}^{NG} \left(Q_{G_i} - Q_{G_i}^{\lim} \right)^2 + R_4 \sum_{i=1}^{nl} \left(S_{l_i} - S_{l_i}^{\max} \right)^2$$

where R_1 , R_2 , R_3 , and R_4 are the penalty quotients, which take large positive values. The limit values of the dependent variable x^{\lim} are

$$x^{\lim} = \begin{cases} x, & x^{\min} \leq x \leq x^{\max} \\ x^{\max}, & x \geq x^{\max} \\ x^{\min}, & x \leq x^{\min} \end{cases}$$

2.1. Practical constraints

Prohibited operating zones (POZ): In practice, when adjusting the output of a generator unit, it is important to avoid operating in prohibited zones so thermal efficiency can be maintained during vibrations in the shaft or other machine faults. This constraint can also be included in the problem formulation,

$$P_{G_i} = \begin{cases} P_{G_i}^{\min} \leq P_{G_i} \leq P_{G_i}^L & k=1 \\ P_{G_i,k-1}^U \leq P_{G_i} \leq P_{G_i,k}^L & k=2, 3, \dots, n_i \\ P_{G_i,n_i}^U \leq P_{G_i} \leq P_{G_i}^{\max} & \end{cases}$$

where n_i is the number of prohibited zones; k is the index of prohibited zones in unit i ; and $P_{G_i,k}^L$ and $P_{G_i,k}^U$ are the lower and upper limits, respectively, of the k th prohibited zone in the i th generator.

Ramp-rate limits: The operating range of the generating units is restricted by their ramp-rate limits, which force the generators to operate continuously between two adjacent periods. The inequality constraints imposed by these ramp-rate limits are

$$\max \left(P_{G_i}^{\min}, P_{G_i}^0 - DR_i \right) \leq P_{G_i} \leq \min \left(P_{G_i}^{\max}, P_{G_i}^0 + UR_i \right)$$

where $P_{G_i}^0$ is the power generation of the i th unit in the previous hour, and DR_i and UR_i are the decreasing and increasing ramp-rate limits, respectively, of the i th unit.

3. Objectives formulation

We consider the objectives generation fuel cost, emission, and total power loss for analysis.

3.1. Generation fuel cost

The total generation fuel cost for NG units is

$$A_{\text{cos } t} = \sum_{i=1}^{NG} (a_i P_{G_i}^2 + b_i P_{G_i} + c_i) \quad \$/h, \quad (1)$$

where a_i, b_i, c_i and P_{G_i} are the fuel cost coefficients and active power generation of i th unit, respectively.

3.2. Emission

The total emission for NG units is

$$A_{\text{emission}} = \sum_{i=1}^{NG} (\alpha_i P_{G_i}^2 + \beta_i P_{G_i} + \gamma_i + \varsigma_i \exp^{\lambda_i P_{G_i}}) \quad \text{ton/h}, \quad (2)$$

where $\alpha_i, \beta_i, \gamma_i, \varsigma_i, \lambda_i$ are emission coefficients of i th unit, respectively.

3.3. Total transmission loss

The total system active power loss is

$$A_{\text{TPL}} = \sum_{l=1}^{nl} g_l [V_i^2 + V_j^2 - 2V_i V_j \cos(\delta_i - \delta_j)] \quad \text{MW}, \quad (3)$$

where, g_l is the conduction of l th line which connects buses i and j ; and V_i, V_j and δ_i, δ_j are the voltage magnitude and angle of the l th and i th bus, respectively.

4. Hybrid cuckoo search algorithm (HCSA)

We develop the proposed HCSA incorporating the advantages of the CSA.

4.1. Existing cuckoo search algorithm (CSA)

CSA is a new meta-heuristic optimization method [55,56] inspired from the obligate brood parasitism of some cuckoo species by laying their eggs in the nests of other birds of other species. When the host birds discover an alien egg in their nest, they can throw it away or simply abandon their nest and build a new one elsewhere. The CSA idealized such breeding behavior in combination with Levy flights behavior of some birds and fruit flies for applying to various constrained optimization problems.

The problem control variables, u , are generated and randomly initialized between their minimum and maximum limits for a given initial population (N),

$$u_{j,i}^t = u_{j,\text{min}} + \text{rand}_{i,j}(0, 1) \cdot (u_{j,\text{max}} - u_{j,\text{min}}), \quad (4)$$

where, j represents the control variable in the i th population in t th iteration. Hence, the i th population in $(t + 1)$ th iteration is

$$u_i^{t+1} = u_i^t + S_{j,i} \times \alpha \oplus \text{Levy}(\lambda), \quad (5)$$

where, $(S_{j,i} = u_{j,i}^t - u_{\text{best}}^t)$ is the step size; $j = 1, 2, \dots, m$; m is the total number of control variables; and $i = 1, 2, \dots, N$. u_{best}^t is the global best solution in t th iteration. The levy flight operation is

$$\text{Levy}(\lambda) = \left| \frac{\Gamma(1 + \lambda) \times \sin\left(\frac{\pi \times \lambda}{2}\right)}{\Gamma\left(\frac{1+\lambda}{2}\right) \times \lambda \times 2 \left(\frac{\lambda-1}{2}\right)} \right|^{1/\lambda}; \quad 1 < \lambda \leq 3, \quad (6)$$

where, λ is the distribution factor ($0.3 \leq \lambda \leq 1.99$), and $\Gamma(\cdot)$ is the gamma distribution function.

After each iteration, the system bus and line data is updated with the new population, and load flow analysis, using the Newton Raphson (NR) method, provides the numerical solution of bus voltages, line power flows and system loss. The objectives, i.e., generation fuel cost, emission, and total power losses, are evaluated for a given population. The solution that minimizes the objective(s) is considered the best solution.

4.2. Modifications in existing CSA

Conventional optimization algorithms cannot accommodate non-linear objective functions. Meta-heuristic approaches have been developed to solve non-linear, non-continuous, and non-convex objective functions. Furthermore, hybridization has the potential to speed up exploration and find the optimum solution rapidly. Hybrid algorithms, combining two or more different methods, is a promising research field, and many satisfactory optimization results have been reported such as accuracy, convergence speed, and robustness in handling larger systems, etc. [3]. In this regard, the arithmetic crossover operation can be used to update the newly generated population and thereby the solution to speed up the convergence, which can improve exploitation of the algorithm [21].

The existing Levy flight operator in CSA can control the exploration of the solutions, to balance exploration and exploitation processes, we consider the crossover operation, which decreases the diversity of the problem and hence the final best solution will be obtained in less iterations. We call this the hybrid CSA (HCSA) optimization.

The mathematical representation of the crossover operation is [3].

$$u_{j,i}^{t+1}(\text{new}) = (1 - \lambda) \times u_{\text{best}}^t + \lambda \times u_{j,i}^{t+1}, \quad (7)$$

where λ is a random number between 0 and 1. After calculating the new population using Eq. (5), this population is modified using Eq. (7). The remaining processes of identifying the best solutions from the population and calculating a new levy flight operator are then performed for a predefined number of iterations.

4.3. HCSA procedure

We present the complete implementation procedure to solve a single objective optimization problem using the proposed HCSA in the following steps.

1. Initialize the problem parameters and read the system bus, line, and OPF data.
2. Generate the initial population for the considered problem control variables using Eq. (4).
3. Update the bus and line data with the new population and perform NR load flow.
4. Evaluate the objective function (Cost, Emission, or Loss) values for the population.
5. Identify the local best solution among all solutions, and start the iterative process.

6. Update the population using Eq. (5), ensuring use of the local best solution after calculating the Levy flight operator using Eq. (6).
7. Update this new population using Eq. (7), the crossover operation.
8. Repeat the procedure, i.e. steps from 3 to 5 in each iteration and obtain the global best solution.
9. This process from steps 1-8 is continued for a predefined number of iterations.
10. After meeting the convergence criteria, output the best solution and its respective control variables.

5. Multi-objective solution strategy

The proposed HCSA may be used to solve single-objective optimization problems but is incapable of multi-objective

optimization. In a multi-objective optimization, two or more objectives are solved simultaneously, while satisfying system and practical constraints using non-dominated HCSA (NSHCSA). Many optimum solutions are obtained rather than a single solution, and generally these solutions are contradictory [57].

The multi-objective optimization problem with different m objectives, which generally conflict with each other, can be formulated as

$$\text{Minimize } [A_1(x, u), A_2(x, u), \dots, A_m(x, u)]; \quad m = 1, 2, \dots, m, \tag{8}$$

To perform this, the initial population is randomly generated for the considered control variables for a given population. The objective functions are evaluated and a non-dominated sorting procedure is applied on the generated solutions to obtain a Pareto front set (PFS). The best PFS is obtained using a comparison procedure. Crowding sorting is applied to sort the solutions in the

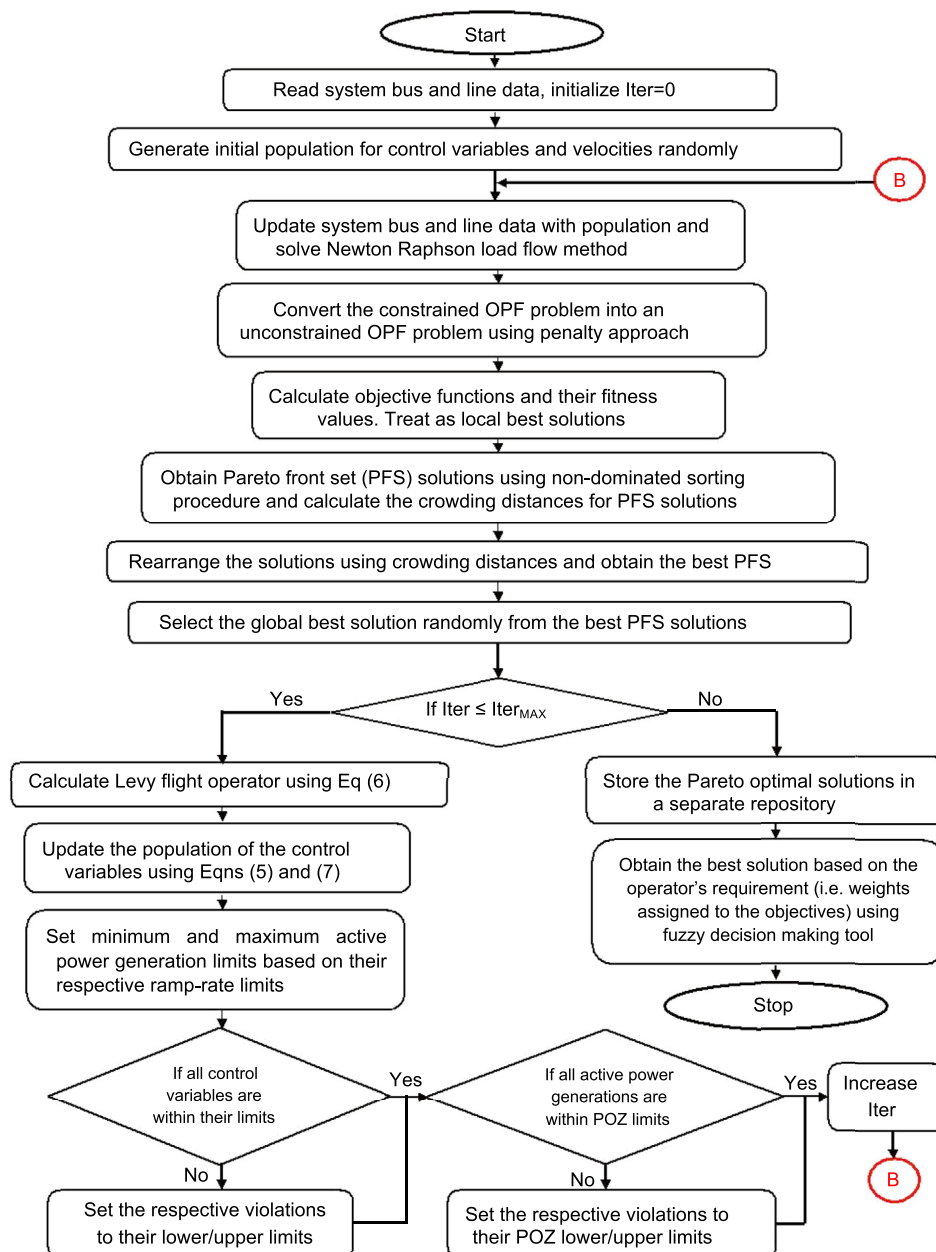


Fig. 1. Flow chart of the multi-objective solution strategy.

Table 1
Comparison of optimal parameters for Booths function.

Parameters	Existing		Proposed HCSEA
	PSO	CSA	
X	1.012698676	1.002249267	1.0043728
Y	2.989245453	2.991978006	2.9969812
Function value	0.000292035	0.000202709	3.557E-05
Time (sec)	8.232991	6.95472	4.12912

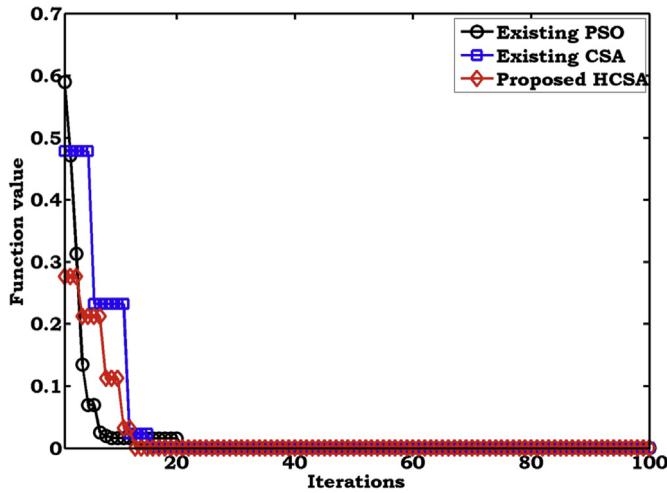


Fig. 2. Convergence characteristics of Booths function.

best PFS. Finally, a fuzzy decision making tool is applied to select the best compromised solutions as per the user requirements.

5.1. Non-dominated sorting

A non-dominated sorting procedure is applied to the multi-objective optimization solutions to obtain a PFS. Let us consider two solutions, A_1 and A_2 , in one PFS. They are checked for the following possibilities: one of them dominates the other or none of them dominates each other. A vector u_1 dominates u_2 , when the following conditions are met [58].

$$\forall i = 1, 2, \dots, m, A_i(u_1) \leq A_i(u_2)$$

$$\exists j = 1, 2, \dots, m, A_j(u_1) < A_j(u_2),$$

where, m is the total number of objective functions. Solutions that are non-dominated over the entire search space are called Pareto optimal and constitute the Pareto optimal set. We follow the sorting procedure from [59,60], based on crowding distance, to obtain the best PFS solutions.

5.2. Fuzzy decision making tool

After obtaining the best PFS solutions, we need to extract the best compromised solution based on a decision provided by the operator. We follow the fuzzy decision making mechanism proposed to obtain the optimal solution. The linear membership value, μ is initially calculated for the i th objective in the j th Pareto solution using [59,61].

$$\mu_i^j = \begin{cases} 1 & ; A_i^j \leq \min(A_i) \\ \frac{\max(A_i) - A_i^j}{\max(A_i) - \min(A_i)} & ; \min(A_i) \leq A_i^j \leq \max(A_i) \\ 0 & ; A_i^j \geq \max(A_i) \end{cases}$$

The preferred degree of the Pareto optimal solutions can be identified through normalized membership values, and this value for q th PFS solution can be calculated using

$$\mu_{opt} = \sup \frac{\sum_{p=1}^m W_p \mu_p^q}{\sum_{q=1}^{N_{PFS}} \sum_{p=1}^m W_p \mu_p^q}; \tag{9}$$

where $W_p \geq 0$; $\sum_{p=1}^m W_p = 1$; W_p is the weight of the p th objective function, and N_{PFS} is the total number of solutions in the best PFS. The PFS solution which has the highest normalized membership for the weight coefficients is considered to be the most optimal solution. The complete methodology of the proposed multi-objective optimization strategy is shown in Fig. 1.

6. Results and analysis

The effectiveness of the proposed methodology is tested for two examples.

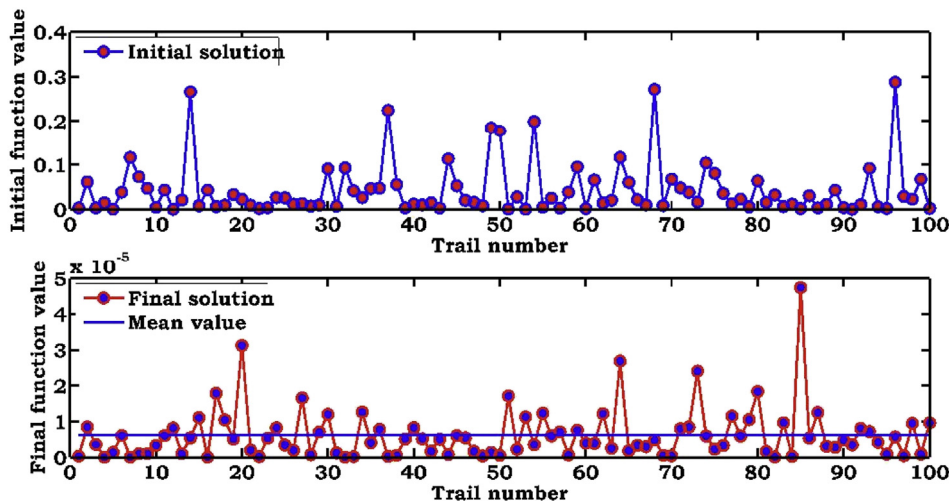


Fig. 3. Variation of the Matyas function over 100 trials using HCSEA.

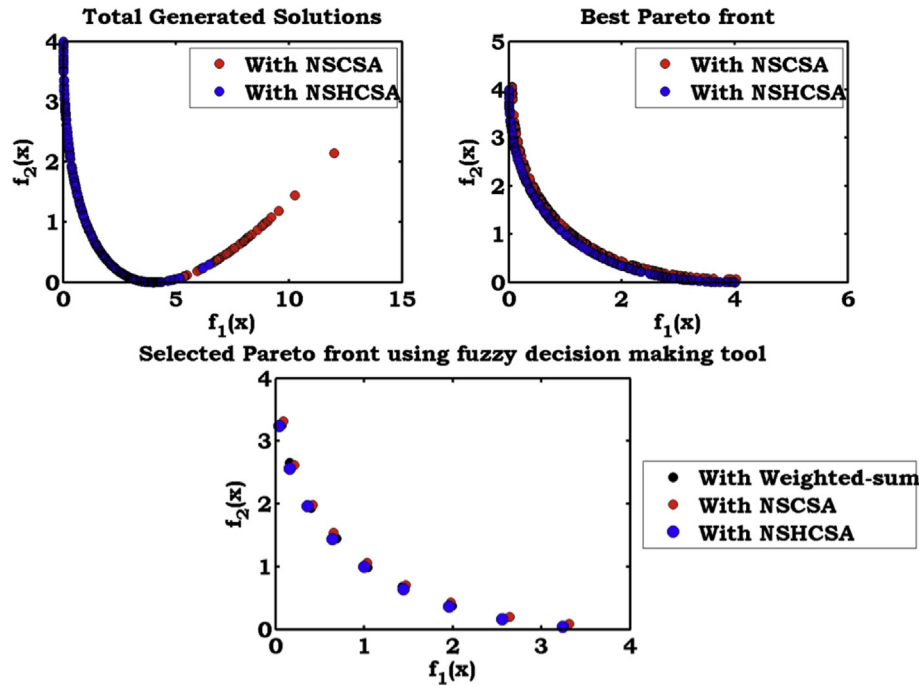


Fig. 4. Multi objective Pareto solutions for the Schaffer function.

6.1. Illustrative example

We consider Booths and Matyas functions [62] to show the effectiveness of the proposed HCSA technique over existing Particle Swarm Optimization (PSO) [10], and CSA [55] techniques in solving single objective optimization problems. The optimal parameters for the Booths function are given in Eq. (10), and the existing and proposed solution methods are shown in Table 1. The preferred solution for this function is $f(1,3) = 0$ in the operating range of $-10 \leq x, y \leq 10$. This solution is more closely matched by the proposed HCSA compared to existing methods. Furthermore, HCSA obtains the solution in less time than the other methods.

The convergence from the different methods are shown in Fig. 2. HCSA starts with a good initial value and reaches the final best value in significantly less iterations than the other methods.

$$f(x, y) = (x + 2y - 7)^2 + (2x + y - 5)^2 \tag{10}$$

To confirm the validity of the proposed HCSA algorithm, the Matyas function (Eq. (11)) was solved for 100 trials, and the

variation of initial and final function values is shown in Fig. 3. The final function value is almost zero in all trials, and most of the final function values are below its mean value. The proposed HCSA algorithm always yields the best solution.

$$f(x, y) = 0.25(x^2 + y^2) - 0.48xy \tag{11}$$

To extend the capability of the proposed NSHCSA technique to solving multi objective optimization problem, we consider the standard Schaffer (SCH) function given in functions $f_1(x)$ and $f_2(x)$ given in Eq. (12) are considered. Following the procedure of section 5, the total generated, best Pareto and selected solutions with the proposed NSHCSA and the existing NSCSA are shown in Fig. 4. The best PSF is obtained with the proposed method, and confines the entire solution region compared to existing methods.

The selected Pareto solutions obtained using the fuzzy decision making tool were also validated against the weighted sum method, as shown in Table 2. The effectiveness of the proposed fuzzy decision making tool is evident in the weight imposed on the objectives; the respective solutions are selected from the best Pareto front. The proposed NSHCSA technique yields the best results compared to existing methods.

$$\text{Minimize} = \begin{cases} f_1(x) = x^2 \\ f_2(x) = (x - 2)^2 \end{cases} \tag{12}$$

6.2. Electrical test system

We consider the IEEE-30 bus test system with forty one transmission lines [63–65] to extend the features of the proposed HCSA technique to solve single objective OPF problems and proposed NSHCSA technique to solve multi-objective OPF problems. The single line diagram of the IEEE-30 bus test system is shown in Fig. 5. There are eighteen control variables for this system, which include six active power generations and respective voltage

Table 2
Multi-objective results for the Schaffer function.

Set No	W1	W2	Existing				Proposed NSHCSA	
			Weighted sum		NSCSA		F1	F2
			F1	F2	F1	F2		
1	0.9	0.1	0.087	3.317	0.065	3.254	0.040002	3.239978
2	0.8	0.2	0.209	2.613	0.162	2.652	0.160024	2.559905
3	0.7	0.3	0.422	1.981	0.4	1.938	0.359953	1.96011
4	0.6	0.4	0.656	1.543	0.685	1.447	0.640016	1.439976
5	0.5	0.5	1.035	1.065	1.041	0.989	1	1
6	0.4	0.6	1.472	0.702	1.433	0.675	1.440345	0.639977
7	0.3	0.7	1.974	0.425	1.987	0.377	1.959544	0.360195
8	0.2	0.8	2.643	0.202	2.583	0.174	2.559729	0.160068
9	0.1	0.9	3.313	0.087	3.249	0.061	3.239934	0.040007

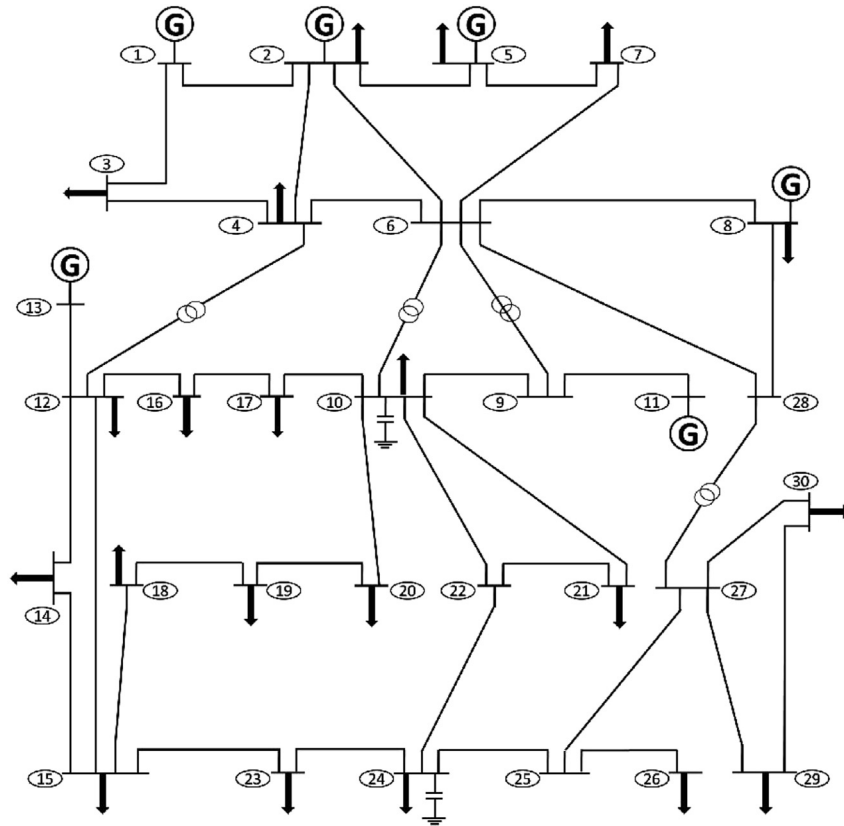


Fig. 5. Single line diagram of IEEE-30 bus system.

magnitudes, two shunt compensators and four tap setting transformers. The OPF results with generation fuel cost as an objective are shown in Table 3 for the existing and proposed methods. The proposed HCSA method produces the best generation fuel cost compared to the existing methods. The time to convergence is also

less in the proposed method. To extend the validity of the results, the comparison of the obtained generation fuel cost value was compared with literature values, as shown in Table 6. This confirms that lower generation fuel cost is obtained with the proposed method. Convergence for the existing and the proposed methods are shown in Fig. 6. The proposed method starts with a good initial value and reaches the final best value in less iteration than existing methods.

Table 3
OPF results for generation fuel cost without practical constraints.

Control variables	Existing methods			Proposed HCSA
	TS [63]	PSO	CSA	
PG1(MW)	176.04	178.5558	170.7789	176.8707
PG2(MW)	48.76	48.6032	48.3696	49.88626
PG5(MW)	21.56	21.6697	18.3135	21.61352
PG8(MW)	22.05	20.7414	32.6057	20.87963
PG11(MW)	12.44	11.7702	10	11.61685
PG13(MW)	12	12	12	12
VG1(p.u.)	1.0500	1.1	1.1	1.057
VG2(p.u.)	1.0389	0.9	1.0567	1.045622
VG5(p.u.)	1.0110	0.9642	1.0912	1.018493
VG8(p.u.)	1.0198	0.9887	1.0725	1.026591
VG11(p.u.)	1.0941	0.9403	1.0465	1.057
VG13(p.u.)	1.0898	0.9284	1.1	1.057
T6–9(p.u.)	1.0407	0.9848	1.0531	1.025462
T6–10(p.u.)	0.9218	1.0299	1.007	0.972648
T4–12(p.u.)	1.0098	0.9794	1.0395	1.006042
T28–27(p.u.)	0.9402	1.0406	0.9707	0.964443
QC10(MVAr)	–	9.0931	30	25.35913
QC24(MVAr)	–	21.665	6.7556	10.6424
Total generation (MW)	292.85	293.3403	292.0677	292.867
Generation fuel cost (\$/h)	802.29	803.4548	802.7283	802.0347
Emission (ton/h)	–	0.3701	0.3508	0.365688
Total power losses (MW)	–	9.9403	8.6677	9.466955
Time (sec)	–	30.2301	23.3948	17.9948

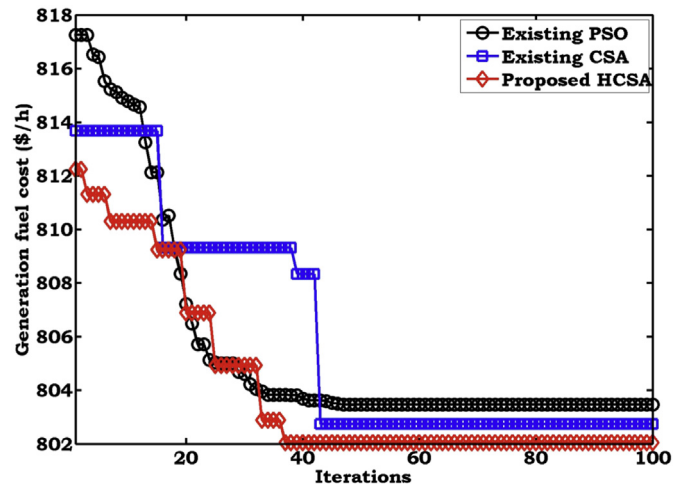


Fig. 6. Convergence for generation fuel cost.

Table 4
OPF results for generation fuel cost, emission, and total power loss objectives with and without practical constraints.

Control variables	Generation cost (\$/h)				Emission (ton/h)				Total power losses (MW)			
	Case A	Case B	Case C	Case D	Case A	Case B	Case C	Case D	Case A	Case B	Case C	Case D
PG1(MW)	176.8707	176.3404	175.4662	173.5069	63.7401	82.4821	79.6604	85.7653	51.608	82.3107	51.7177	82.521
PG2(MW)	49.8863	48.279	48.3476	50	68.2844	63	60.4497	63	80	63	80	63
PG5(MW)	21.6135	21.4978	21.5623	21.5656	50	49	50	49	50	49	50	49
PG8(MW)	20.8796	19.7378	23.0082	20.271	35	30	35	30	35	30	34.9067	30
PG11(MW)	11.6169	13	12.5634	13.5283	30	28	23.3293	25	30	28	30	28
PG13(MW)	12	14	12	14	40	35	40	35	40	35	40	35
VG1(p.u.)	1.057	1.057	1.057	1.057	1.0563	1.0566	1.0466	1.057	1.057	1.057	1.057	1.057
VG2(p.u.)	1.0456	1.0443	1.0068	1.0146	1.0082	0.9876	1.0001	1.0232	1.0562	1.0529	1.0559	1.0037
VG5(p.u.)	1.0185	1.0189	1.0188	1.0151	1.0354	1.0325	1.0004	1.0392	1.0383	1.0327	1.0339	1.0324
VG8(p.u.)	1.0266	1.0304	1.0376	1.0182	1.0393	1.0307	0.986	1.057	1.0461	1.0373	1.0434	1.057
VG11(p.u.)	1.057	1.057	0.9	1.0242	1.057	1.0504	1.057	1.0188	1.057	1.0273	1.051	1.057
VG13(p.u.)	1.057	1.0332	1.057	1.057	1.0377	1.057	0.972	1.057	1.057	1.057	1.0502	0.9308
T6–9(p.u.)	1.0255	1.0354	1.019	1.0216	1.0197	0.9414	0.9	1.1	1.0134	1.0078	0.9988	0.9624
T6–10(p.u.)	0.9726	1.0621	0.923	0.9862	0.9594	1.0402	1.0324	1.0506	0.9629	0.9665	1.0117	0.9715
T4–12(p.u.)	1.006	1.0361	0.993	1.0406	0.9196	1.014	0.9	1.1	0.9802	1.0024	0.9905	0.9
T28–27(p.u.)	0.9644	0.9937	0.9705	0.9957	0.9796	0.9744	1.041	1.049	0.9654	0.9647	0.9806	0.9349
QC10(MVAr)	25.3591	25.0745	28.4048	23.0989	22.7301	13.2467	21.4139	27.1046	21.4206	20.6	18.5121	30
QC24(MVAr)	10.6424	13.8787	14.5708	18.457	24.5998	13.6385	11.0046	5	16.5347	14.2324	11.7249	16.5028
Total generation (MW)	292.867	292.855	292.9477	292.8718	287.0245	287.4821	288.4395	287.7653	286.608	287.3107	286.6244	287.521
Generation fuel cost (\$/h)	802.0347	802.4735	802.9519	803.157	946.5282	913.4775	926.6635	909.1405	967.9202	913.0289	967.8243	913.5794
Emission (ton/h)	0.3657	0.3631	0.3613	0.3556	0.2048	0.2132	0.2112	0.216	0.2072	0.2131	0.2072	0.2133
Total power losses (MW)	9.467	9.455	9.5478	9.4718	3.6245	4.0821	5.0395	4.3653	3.208	3.9107	3.2244	4.121

Table 5
Ramp-rate and POZ limits followed by the generators for four cases.

Generators description	Minimization of											
	Generation cost				Emission				Total power losses			
	Case A	Case B	Case C	Case D	Case A	Case B	Case C	Case D	Case A	Case B	Case C	Case D
PG1	UP, 2	UP, 2	UP, 2	UP, 2	DOWN, 1	DOWN, 1	DOWN, 1	DOWN, 1	DOWN, 1	DOWN, 1	DOWN, 1	DOWN, 1
PG2	UP, 1	UP, 1	UP, 1	UP, 3	UP, 2	UP, 2	UP, 2	UP, 2	UP, 2	UP, 2	UP, 2	UP, 2
PG5	DOWN, 1	DOWN, 1	DOWN, 1	DOWN, 1	UP, 2	UP, 2	UP, 2	UP, 2	UP, 2	UP, 2	UP, 2	UP, 2
PG8	UP, 1	DOWN, 1	UP, 1	UP, 1	UP, 2	UP, 4	UP, 2	UP, 4	UP, 2	UP, 4	UP, 2	UP, 4
PG11	DOWN, 1	DOWN, 1	DOWN, 1	DOWN, 1	UP, 2	UP, 4	UP, 1	UP, 3	UP, 2	UP, 4	UP, 2	UP, 4
PG13	DOWN, 1	DOWN, 1	DOWN, 1	DOWN, 1	UP, 2	UP, 2	UP, 2	UP, 2	UP, 2	UP, 2	UP, 2	UP, 2

1-Below POZ lower limit; 2-Above POZ upper limit; 3-Equal to POZ lower limit; 4-Equal to POZ upper limit; UP-following up-ramp rate; DOWN-following down-ramp rate.

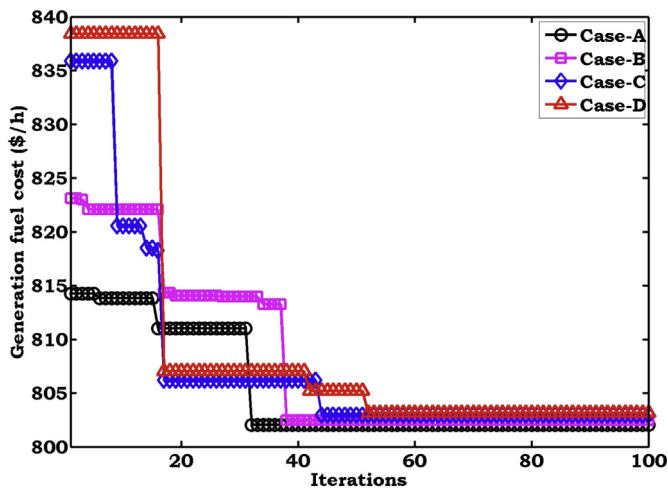


Fig. 7. Convergence of generation fuel cost for four cases.

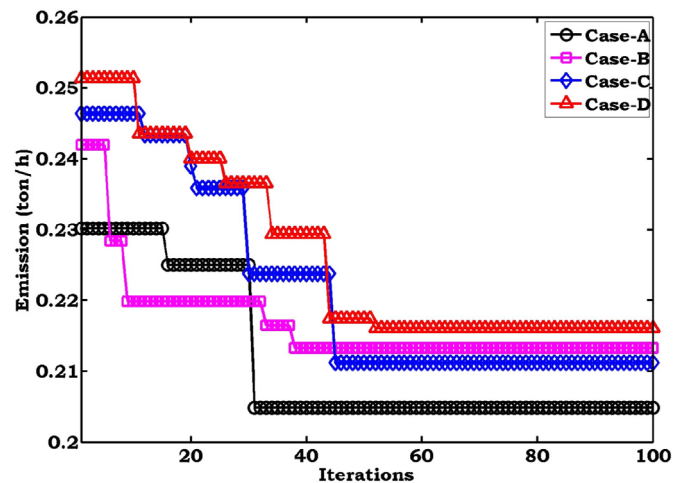


Fig. 8. Convergence of emission for four cases.

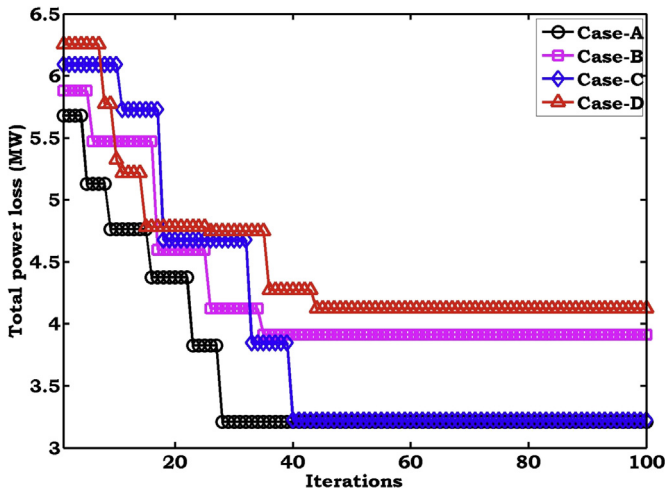


Fig. 9. Convergence of total power loss for four cases.

To show the effect of practical constraints, the OPF problem was solved for the following four cases:

- Case-A: Without ramp-rate and prohibited operating zone (POZ) limits.
- Case-B: With ramp-rate and without POZ limits.
- Case-C: Without ramp-rate and with POZ limits.
- Case-D: With ramp-rate and POZ limits.

Objectives generation fuel cost, emission, and total power losses were solved for these four cases, and the OPF results are tabulated in Table 4. As the number of constraints increase, the objective values also increase, and minimization of one objective increases the value of the other objectives. This is due to the objectives being contradictory. Due to the restrictions imposed by practical constraints on power generation, the generation is rescheduled and

some generators increase and some decrease generation. Thus, the total generation and hence the total power loss also varied from case to case. Emission and total power loss objectives for Case A are shown in Table 6, and confirmed that the proposed HCSA algorithm yields superior results than existing methods.

Note that, while minimizing generation fuel cost, the slack generator is operating at higher value and the remaining generators are operating at lesser values, whereas when minimizing emission and loss objectives, this is reversed. This is because the cost coefficients are lesser and emission coefficients are higher for the slack generator. Minimizing total power losses, all generators except the slack generator are operating at respective maximum limits to decrease the power losses in transmission lines.

The ramp-rates and POZ limits followed by the generating units for the objectives in all cases are shown in Table 5. Note that all generating units are following the respective ramp-rates and are not operating in prohibited zones.

Convergence for the objectives in the four cases are shown in Figs. 7–9. The iterative process starting value and the total number of iterations taken for final convergence increase as the number of constraints increase.

The multi-objective optimization problem with two objectives was solved for the following three combinations.

- Combination-1: Generation fuel cost and Emission objectives.
- Combination-2: Generation fuel cost and Total power loss objectives.
- Combination-3: Emission and Total power loss objectives.

Following the procedure of Section 5, the total generated, best PFS, and PFS selected using the fuzzy decision making tool for the combinations are shown in Figs. 10–12. To show the effect of practical constraints on multi-objective optimization, the selected Pareto front solutions are shown without and with practical constraints. There is a significant effect from the practical constraints on objectives, and the proposed NSHCSA algorithm provides the

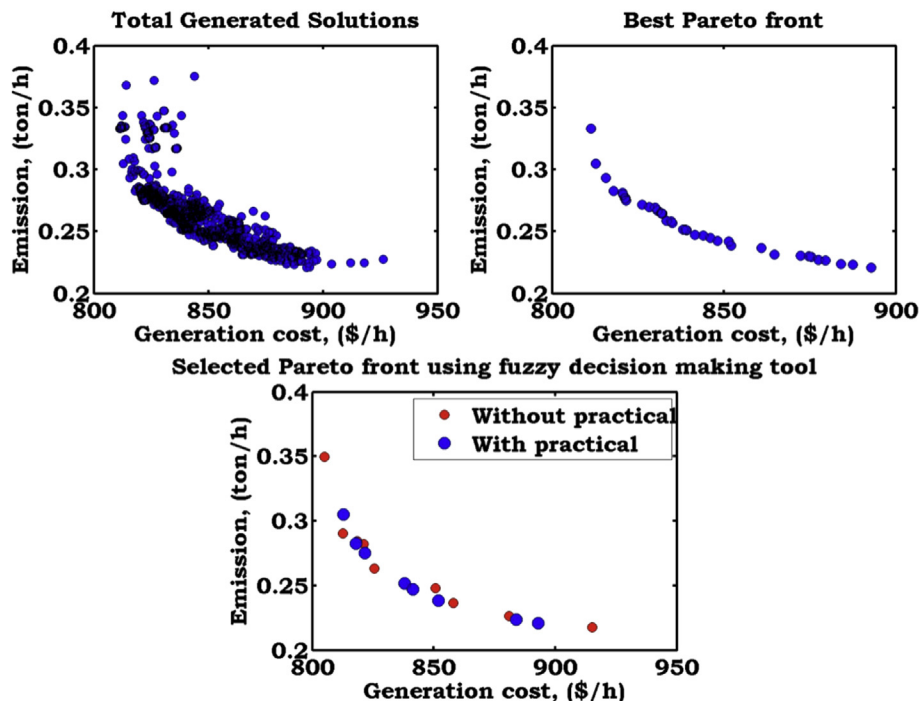


Fig. 10. Multi-objective Pareto front solutions for combination 1.

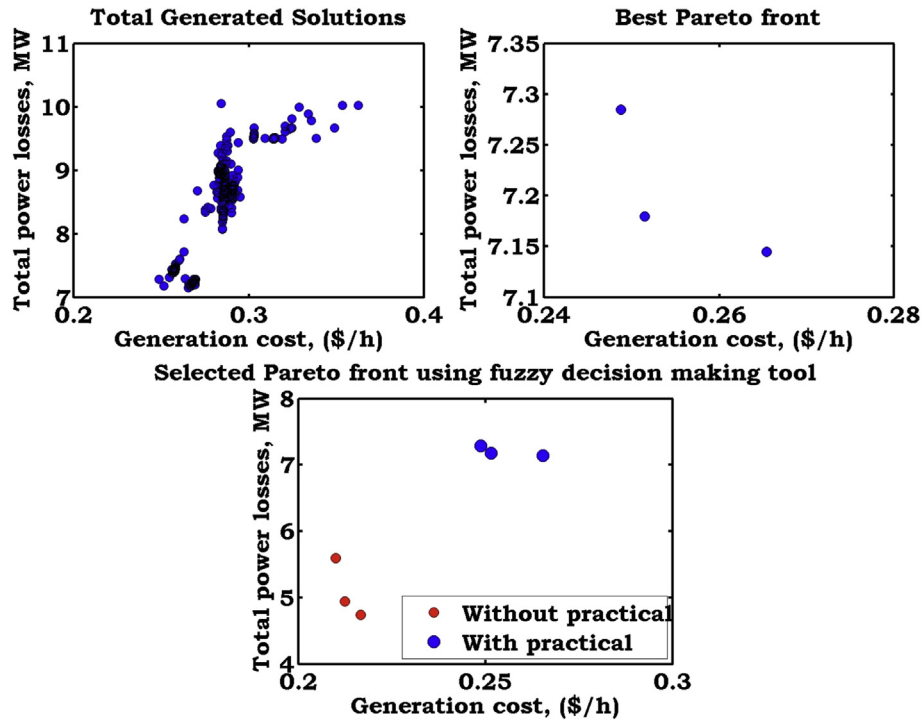


Fig. 11. Multi-objective Pareto front solutions for combination 2.

best PFS that confines the entire solutions region. The numerical results for the various weight configurations, with and without practical constraints, for the considered combinations are shown in Table 7. Based on the weights imposed on the objectives, the best compromised solution has been selected by the proposed fuzzy decision making tool. The multi-objective optimization results

were further validated against existing literature outcomes, shown in Table 8. The proposed NSHCSA technique yields superior results than existing methods.

Finally, to show the extended capability of the proposed algorithm, the multi-objective optimization problem was solved considering all three objectives simultaneously. The total

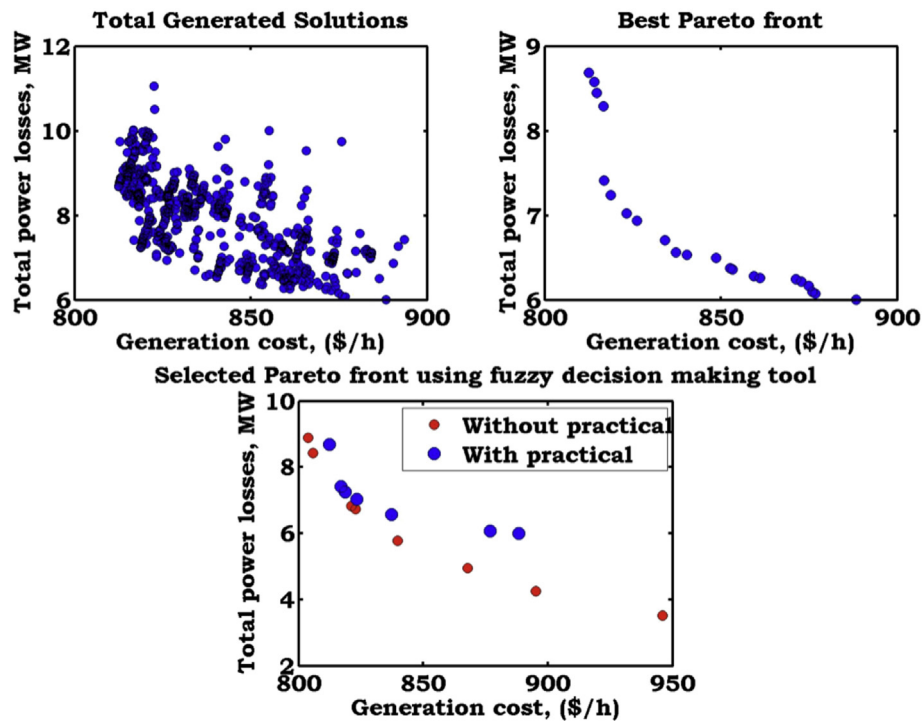


Fig. 12. Multi-objective Pareto front solutions for combination 3.

Table 6
Validation of OPF results for generation fuel cost, emission, and total power loss objectives for Cases A and D.

Methods		Generation fuel cost (\$/h)	Emission (ton/h)	Total power losses (MW)
Existing	MSFLA [27]	802.287	0.2056	–
	SFLA [27]	802.5092	0.2063	–
	PSO [28]	802.190	–	3.6294
	MDE [1]	802.376	–	–
	IEP [2]	802.465	–	–
	IPSO [29]	–	0.2058	5.0732
	PSO [29]	–	0.2063	5.1204
	RGA [3]	–	–	4.57401
	CLPSO [4]	–	–	4.6282
	DE [5]	–	–	5.011
	CMAES [6]	–	–	4.945
Proposed HCSA	HSA [7]	–	–	4.9059
		802.0347	0.204823	3.208022

Table 7
Multi-objective obtained results for three combinations for Cases A and D.

Set No	W1	W2	Combination-1				Combination-2				Combination-3			
			Case A		Case D		Case A		Case D		Case A		Case D	
			COST (\$/h)	EMISSION (ton/h)	COST (\$/h)	EMISSION (ton/h)	COST (\$/h)	LOSS (MW)	COST (\$/h)	LOSS (MW)	EMISSION (ton/h)	LOSS (MW)	EMISSION (ton/h)	LOSS (MW)
1	0.9	0.1	805.0877	0.349475	812.7527	0.304942	803.6669	8.878716	812.4517	8.684898	0.200051	5.595696	0.248776	7.284695
2	0.8	0.2	811.5777	0.290295	812.7527	0.304942	805.6669	8.421013	816.8743	7.417023	0.200051	5.595696	0.251489	7.17943
3	0.7	0.3	814.3581	0.284276	817.9518	0.28272	811.0387	6.833939	818.7925	7.242575	0.200051	5.595696	0.251489	7.17943
4	0.6	0.4	821.0646	0.282075	821.5251	0.274949	812.7463	6.729621	818.7925	7.242575	0.212441	4.939599	0.251489	7.17943
5	0.5	0.5	825.4109	0.263045	838.0356	0.251677	819.5982	5.480605	823.2176	7.0247	0.212441	4.939599	0.251489	7.17943
6	0.4	0.6	850.5875	0.241178	841.5168	0.247123	867.6758	4.943254	837.226	6.562197	0.212441	4.939599	0.251489	7.17943
7	0.3	0.7	858.0959	0.236491	851.9974	0.238557	895.0949	4.257612	837.226	6.562197	0.212441	4.939599	0.265426	7.144647
8	0.2	0.8	881.0959	0.207491	883.9444	0.223556	946.0705	3.525675	876.8383	6.073851	0.216743	4.736511	0.265426	7.144647
9	0.1	0.9	915.1892	0.203633	892.8674	0.221086	946.0705	3.525675	888.285	6.0066	0.216743	4.736511	0.265426	7.144647

Table 8
Validation of Multi-objective OPF results for three combinations, Case A.

Set No	W1	W2	Combination-1				Combination-2				Combination-3			
			Case A [27]		Case A [29]		Case A [29]		Case A [28]		Case A [29]			
			COST (\$/h)	EMISSION (ton/h)	COST (\$/h)	EMISSION (ton/h)	COST (\$/h)	LOSS (MW)	COST (\$/h)	LOSS (MW)	EMISSION (ton/h)	LOSS (MW)		
1	0.9	0.1	823.27788	0.2907778	–	–	–	–	–	–	–	–	–	–
2	0.8	0.2	857.40576	0.2360181	823.134	0.2751	839.843	8.976	–	–	–	–	0.2061	5.213
3	0.7	0.3	877.35636	0.2260597	–	–	–	–	–	–	–	–	–	–
4	0.6	0.4	890.54330	0.2226469	–	–	–	–	–	–	–	–	–	–
5	0.5	0.5	891.06507	0.2197379	841.052	0.2583	850.916	7.893	822.9	5.613	–	–	0.2063	5.179
6	0.4	0.6	898.49795	0.2185756	–	–	–	–	–	–	–	–	–	–
7	0.3	0.7	925.51651	0.2117979	–	–	–	–	–	–	–	–	–	–
8	0.2	0.8	942.24246	0.2107835	860.421	0.2383	869.731	6.775	–	–	–	–	0.2066	5.162
9	0.1	0.9	948.22649	0.2092571	–	–	–	–	–	–	–	–	–	–

generated, best, and selected PFS solutions, including the effect of practical constraints, are shown in Fig. 13. The best PFS obtained with the proposed method confines the entire trade off region. For this problem, there are 34 possible combinations based on the

weights distribution among the objectives. For space considerations, the numerical results for nine of these combinations are given in Table 9, chosen to highlight the performance of the proposed method.

Table 9
Multi objective OPF results with three objectives.

Set No	W1	W2	W3	COST(\$/h)	EMISSION(ton/h)	LOSS(MW)
1	0.1	0.1	0.8	919.8273	0.262921	4.42738
2	0.1	0.8	0.1	911.2938	0.219299	4.73920
3	0.8	0.1	0.1	811.3254	0.310293	8.177524
4	0.5	0.4	0.1	823.3849	0.239384	7.394821
5	0.5	0.1	0.4	849.3023	0.252736	5.839842
6	0.4	0.5	0.1	849.3023	0.252736	5.839842
7	0.1	0.5	0.4	911.2938	0.219299	4.73920
8	0.1	0.4	0.5	911.2938	0.219299	4.73920
9	0.4	0.1	0.5	849.3023	0.252736	5.839842

7. Conclusions

A novel hybridized optimization algorithm based on the arithmetic crossover operation and conventional CSA techniques, called HCSA, was proposed. The proposed algorithm was calibrated in terms of convergence rate and the number of iterations taken for final convergence. The HCSA method was tested on standard single and multi-objective test functions and electrical test systems, to show the advantages of incorporating the crossover operation. Single objective optimization results show the proposed method enhances the performance and applicability of the convergence

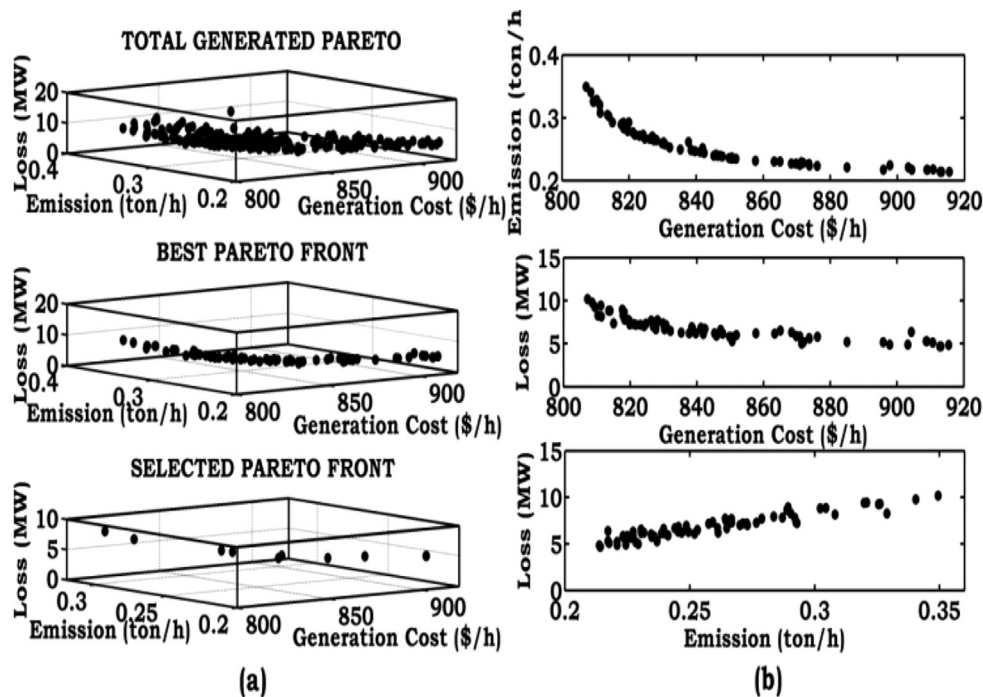


Fig. 13. Multi objective Pareto front solutions with three objectives.

and produces a superior solution compared to existing methods. The best PFS obtained with the proposed method for the multi-objective optimization problem confines the entire solutions region compared to existing methods.

The proposed new method solves single and multi-objective optimization problems with increased effectiveness for different power system objectives, such as generation fuel cost, emission, and total power loss. The effect of practical constraints on active power generation was also analyzed and the proposed HCSA method was shown to be the best when compared to existing method.

Though the proposed method is effective, the number of evolutionary operations performed during the iterative process is increased, which increases the complexity of the programming which may increase execution time. To confirm this, the future work will investigate more complicated and large scale and real time test systems.

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