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Comparison of Two Common Maximum Power Point Trackers by Simulating of PV Generators

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Abstract

Power point tracker algorithms play an important role in the optimization of the power and the efficiency of a photovoltaic generator (PVG). We made the comparison between two algorithms currently implemented for the power optimization of PVG. These algorithms are based on the Perturb Observe and the Conductance-Increment methods allowing the Maximum Power Point Tracking, MPPT, principle. The study leads us to conclude that these algorithms are not well adapted for PVG exposures in very unfavorable but realistic external conditions.

Keywords: Maximum Power Point Tracking, Photovoltaic Generator, Boost-converter, Microcontroller, Solar energy.

1. Introduction

The solar photovoltaic found its utility in applications for small scale, autonomic and isolated or unconnected systems but also for high power PV installations or stations. Photovoltaic energy is a source of interesting energy: it is renewable, inexhaustible and nonpolluting, so that, it is more and more intensively used as energy sources in various applications. Nevertheless, to satisfy industrial, commercial and exploiting constraints link to the cost, the system should present a good exploitation of all the photovoltaic modules and a high general efficiency [1].

For that, it is necessary to extract the maximum of power from the photovoltaic generator, i.e. the maximum of the power delivered by the PVG, not directly droved by the load. A good profitability of the PVG can be carried out if it works to the maximum of the available solar power all the time [2].

However, the maximum power point (MPP) varies according to several parameters like the solar irradiation Ψ , the temperature T , the nature of the load, the technology of the PV cells and the shadowing of the panels from various sources (falling leaves, dust...) [3],[4]. In a current solar photovoltaic system, we can consider the random existence of these parameters. Nevertheless, associated with a voltage converter, e.g. a DC-DC one as in this study, the PVG requires a permanent maximum power production [5].

Thus, whatever the weather conditions (temperature and irradiation) and whatever the load, the control system of the converter must place the system at the optimal power point (IPVopt,VPVopt). Nevertheless, the operating point of the generator on the I-V curve is dynamically modified; the MPPT must get the MPP (maximum power point) at any moment and must maintain PVG power in the neighborhoods of this point and to produce power with the higher efficiency.

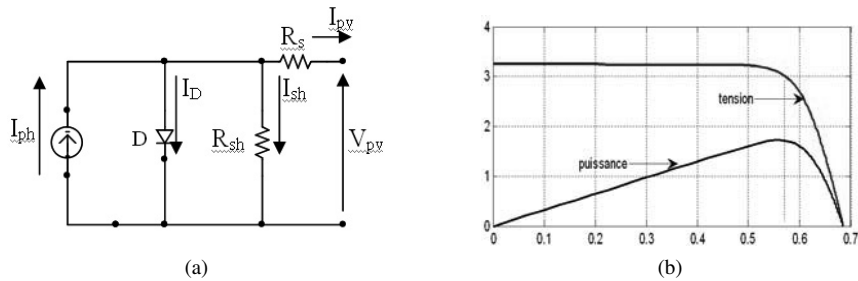


Figure 1: (a) Equivalent circuit of photovoltaic cell, (b) I-V and P-V characteristics of photovoltaic cell

Within this framework, we made a comparison between two algorithms of optimization of the power of the PVG under the Matlab/Simulink environment and test a new algorithm under the software PROTEUS and CCs compiler. The results obtained in these last simulations seem to offer the possibility of an improvement of the PVG efficiency.

2. The photovoltaic generator

2.1. The photovoltaic cell

In the literature [1],[3],[6], a photovoltaic cell is often presented as in Fig.1.a. This model includes also a serial resistance R_s , which represents the ohmic contacts between metal and the semiconductor as well as the intrinsic resistance of silicon and a shunt one R_{sh} , linked to the surface quality along the cell periphery. The cell can be described by the relation linking the photo-current of cell, I to the reverse saturation current of the diode I_{sat} and to the short circuit current I_{sc} as a function of the photovoltaic cell voltage, V , the solar radiation, Ψ (W/m^2) and the temperature of the junction, T . The characteristic equation describing the photovoltaic cell is [7]:

$$I = I_{ph} - I_{sat} \cdot \left(e^{\frac{q(V+IR_s)}{A.K.T}} - 1 \right) - \frac{V + R_s}{R_{sh}} \quad (1)$$

where I is the PV cell current, V the PV cell voltage, I_{ph} the photocurrent, I_{sat} the saturation current of the junction, q the electron charge, A the ideality factor of the P-N junction, R_s the PV cell series resistance, R_{sh} the PV cell parallel resistance, K the Boltzmann constant equal to $1,38 \cdot 10^{-23} \text{J.K}^{-1}$ and T the temperature of the junction.

The simulated I-V and P-V characteristics of such a system deduced from fig.1 with $R_s = 1\text{m}\Omega$, $R_{sh} = 15\text{k}\Omega$ are represented in Fig.1.b. We notice on these curves the MPP of the PV cell.

2.2. The photovoltaic array

Practically, a photovoltaic array results of the association of N_s photovoltaic cells in series and N_p cells in shunt. The judicious choice of N_s and N_p makes the possibility to have the desired output power for a given voltage. In Fig.2, we show the I-V characteristics for a serial association of cells, Fig.2.a., i.e. the influence of N_s and for a parallel association of cells, Fig.2.b., i.e. the influence of N_p [8].

2.3. The photovoltaic generator

To consider a real installation comprising a set of module as in [7],[8], we report in Fig.3, a practical case which is composed of three panels with thirty-six cells (not all represented) and its I-V characteristic, Fig.3.b.

This characteristic is compared with the I-V response for a string of thirty six cells, a shunt of three cells and an alone cell. Finally, the complete photovoltaic installation is represented in Fig.4. It is based on a photovoltaic generator supplying a dc load, i.e. a battery through an adaptation stage constituted by a boost converter headed by a MPPT controller for a maximum efficiency.

Controllers MPPT are usually integrated in the PVG to ensure that it operates on its maximum power point (MPP) [9]. These controllers are intended to minimize the error between the available power at MPP and the maximum power

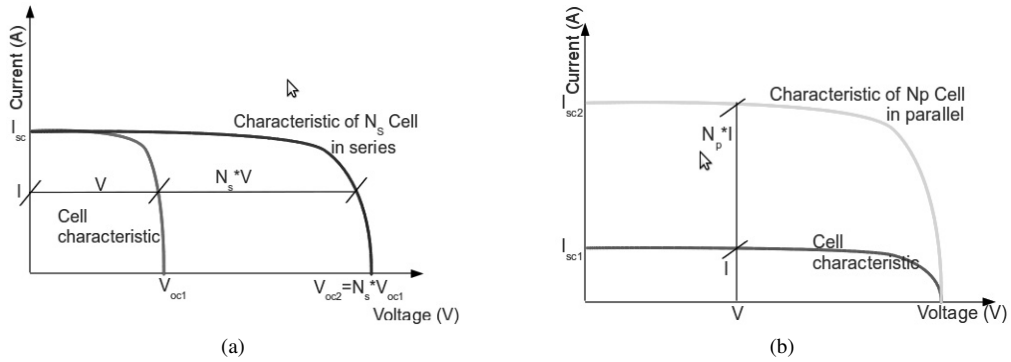


Figure 2: I-V characteristic of a photovoltaic module with cells in (a) series associating and in (b) Shunt associating.

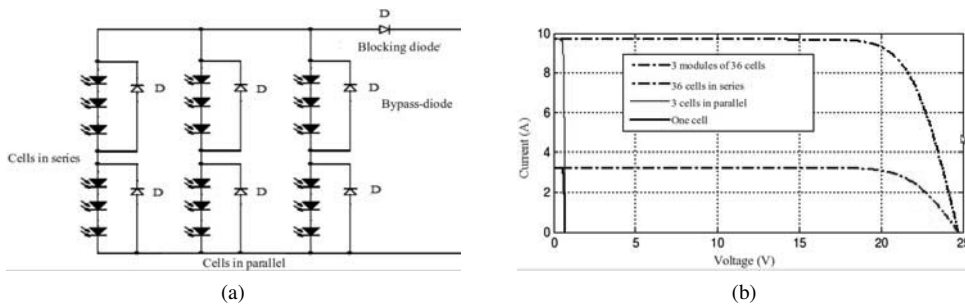


Figure 3: (a) Scheme of a photovoltaic generator and (b) its I-V curve compared with I-V curves for modules and cells.

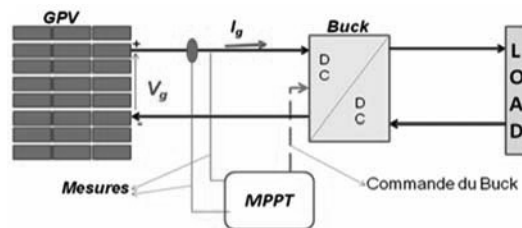


Figure 4: The complete photovoltaic installation: PVG-Boost-Load and MPPT controller.

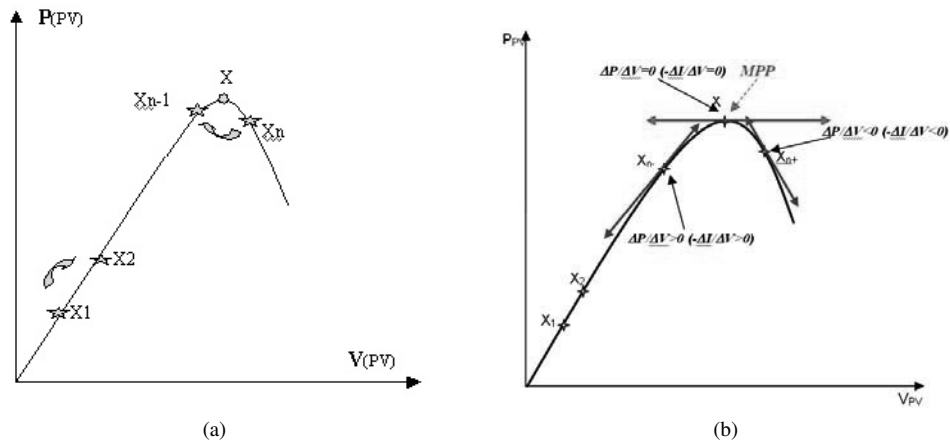


Figure 5: Principle on the P-V characteristics of (a) the Perturb and Observe (P&O) MPPT, (b) The Incremental Conductance (IncCond) MPPT.

of variable reference according to the climatic and external conditions. This MPP power value is easily calculated from the product Voltage-Current available at the output of the PVG. Nevertheless, the determination of the maximum reference power is more delicate thanks to the fact that is a function of the climatic conditions, i.e. the illumination and the temperature. This reference, being not constant is characterized by a nonlinear function, returns the high difficulties for the PVG to operate at the maximum power. In order to overcome these difficulties, several techniques are often adopted such as the analogical methods and the numerical methods using of data-processing tools.

3. Evaluation of the two MPPT algorithms

3.1. Perturb and Observe MPPT algorithm (P&O)

This method has a structure of a simple regulation, and few parameters of measurement. It operates by disturbing the voltage of the panel periodically, and by comparing the energy previously delivered with those after disturbance. This quite simple structure of the process and the few measured parameters required make that these algorithms are widely used in commercial systems [10]. With the help of an P-V characteristic, as plotted in Fig.5.a, the principle can be described as follow: If the disturbance as the addition of a positive contribution ΔV to the voltage implies an increase in the delivered power, then the operating point, e.g. X_i is in the ascending phase of the characteristic and therefore the output voltage will have to be increased up to a new point X_{i+1} and conversely. Treatments have to be in opposite direction when the additive contribution is negative. Under these conditions, the tracker seeks the maximum of power permanently. Nevertheless, the change in power is only considered as a perturbation of the output voltage and the algorithm does not compare this voltage with the present MPP voltage. At a specified insulation level I_{ph} , the desired PVG current is the solution of the following nonlinear equation:

$$\frac{dP_g}{dV_g} = \frac{d(V_g * I_g)}{dV_g} = 0 \tag{2}$$

with V_g and I_g the voltage and the current at the output of the PV generator. As a consequence of the principle of the P&O algorithms, when the MPP is reached, the tracker will oscillate around it, resulting in a loss of PV available power, especially in perturb atmospheric conditions with constant or slowly varying changes. By else, in case of rapid changes of atmospheric conditions, e.g. occurrence of clouds, it is noted that due to the change of the solar radiation, the P&O algorithm deviates from the MPP until a slow solar radiation change occurs or settles down.

3.2. Incremental Conductance MPPT algorithm (Inc Cond)

To solve the previous problem, the track of the MPP was performed with an other technique giving rise to the Incremental Conductance algorithm [11]. On the contrary to the P&O algorithms and to avoid their drawbacks, the output voltage of the generator is continuously adjusted according to its value relative to the MPP voltage. Then, the basic principle of this algorithm, represented in Fig.5.b, calculates the derivative of the power extracted of the installation. main operation done by this algorithm is to compare the dI/dV to I/V ratios and according to the result of this comparison, the reference signal will be adjusted in order to move the output voltage towards the MPP voltage. This derivative zero at the maximum power point and positive on its left and negative on its right [12]. As well as the PVG power is described by $P=VI$, the derivative as function of the voltage is then defined by:

$$\frac{dP_{PV}}{dV_{PV}} = \frac{d(V_{PV} * I_{PV})}{dV_{PV}} = V_{PV} * \frac{dI_{PV}}{dV_{PV}} + I_{PV} \quad (3)$$

which imply:

$$\frac{dP_{PV}}{dV_{PV}} > 0 \quad \text{if} \quad \frac{I_{PV}}{V_{PV}} > -\frac{dI_{PV}}{dV_{PV}}, \quad \text{on the left of MPP}; \quad (4)$$

$$\frac{dP_{PV}}{dV_{PV}} = 0 \quad \text{if} \quad \frac{I_{PV}}{V_{PV}} = -\frac{dI_{PV}}{dV_{PV}}, \quad \text{at the MPP}; \quad (5)$$

$$\frac{dP_{PV}}{dV_{PV}} < 0 \quad \text{if} \quad \frac{I_{PV}}{V_{PV}} < -\frac{dI_{PV}}{dV_{PV}}, \quad \text{on the right of MPP}; \quad (6)$$

Two other controls are included in this algorithm to take into account of a change of the atmospheric conditions when the tracker is located at the MPP. Thus, when $dV=0$, the determination of the sign of dI indicates the direction of changes. This algorithm lies a primary advantage over the P&O algorithm by the fact that he can continuously calculate the direction to reach the MPP after a perturbation of the arrays operating point and he can determine when the MPP is attained.

4. Experimental procedure and results

To compare the performance of the two common algorithms presented above, we have developed a series of tests based on a change of one functioning parameters of the PVG. For that we were implemented a microcontroller under Matlab/Simulink. To have an absolute overview of the MPPT, we have also compared the responses of a photovoltaic system without and with a tracker.

4.1. PVG response to an illumination step

To analyze and compare the performances of the algorithms of the P&O MPPT and the IncCond MPPT methods, we carried out a test in which the photovoltaic generator is exposed at the same standard environmental conditions based on the appearance of a step of illumination. In Fig.6 to Fig.13, we report the dynamic response of the PV system driven by the two algorithms.

As we can observed in the responses reported in Fig.6, the two algorithms present different response times to an illumination step. So, these characteristics curves, especially the power and voltage ones show the faster response offered by the IncCond MPPT compared to the P&O.

4.2. PVG response as function of the charges

To study the robustness and the performances of the two algorithms we carried out tests without and with the MPPT for the two following cases: (a) a dynamic resistor load and (b) a battery load [13],[14];

For the first series of test, a resistor is placed as charge and is continuously set at various values as shown in Fig.7.

The results of the variation of the resistive charge values on the power and the voltage of the generator and on the duty cycle of the system with and without MPPT are reported in Fig.8 where, in these figures, the blue, grey and red lines are related to the responses with the P&O, IncCond algorithms and without, respectively.

The PVG without MPPT controller never work at the maximum power except when the load equals the optimum value of the load impedance. On the other hand, with the both MPPT algorithms the functioning point always follows

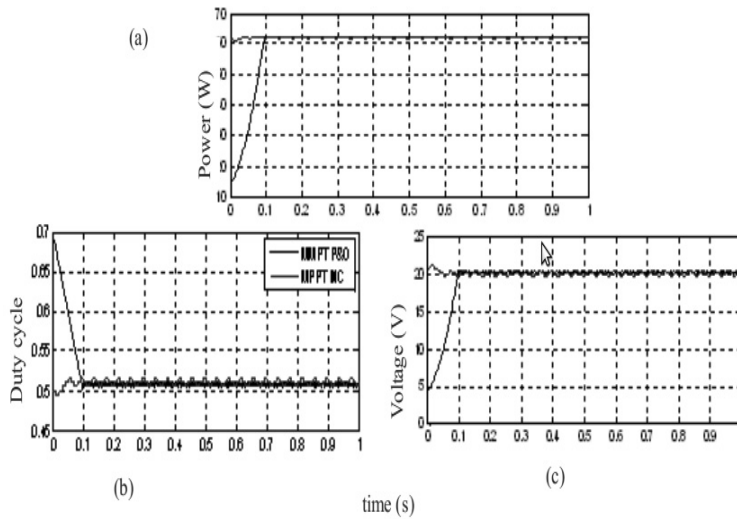


Figure 6: Variation of (a) the power, (b) the duty cycle and (c) the voltage of the module of two controllers P&O MPPT (Grey line) and IncCond MPPT (blue line) for $T=25^{\circ}\text{C}$ and $\Psi=1000\text{W}/\text{m}^2$.

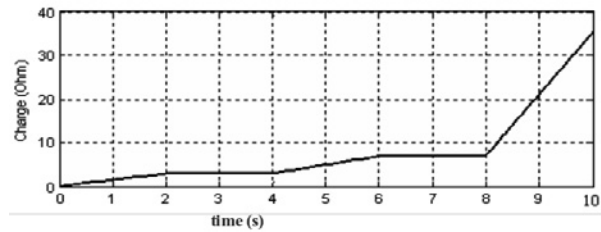


Figure 7: Dynamic resistor load. The variation of the resistor is shown according to time.

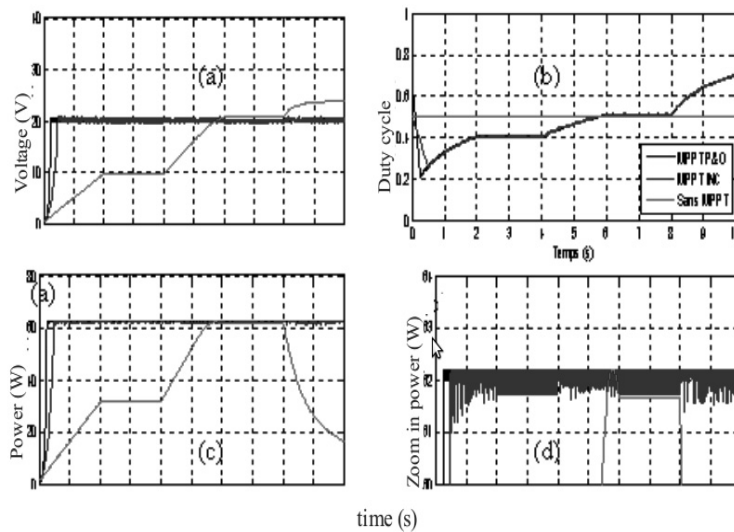


Figure 8: Influence of the resistor load value according to time on: (a) Voltage, (b) Duty cycle, (c) Power, (d) zoom on power curve of generator without (red line), with P&O (grey line) and IncCond MPPT (blue line) controllers.

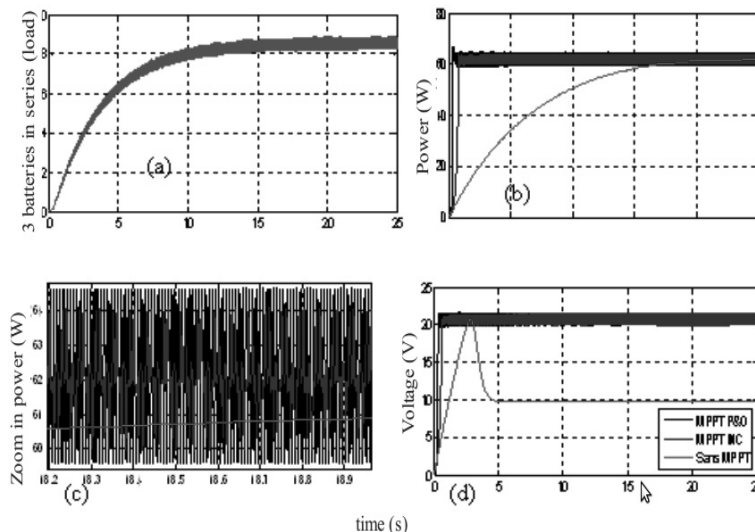


Figure 9: Influence of the load (a) of three batteries according to time on: (b) power, (c) zoom on power curve, (d) voltage, without (red line), with P&O (grey line) and IncCond MPPT (blue line) controllers.

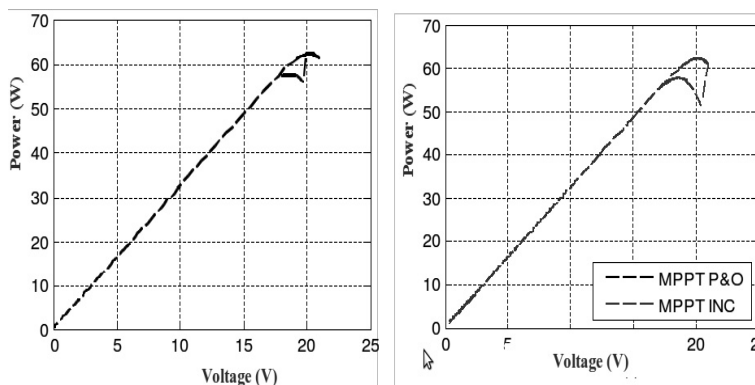


Figure 10: P-V Characteristic curves of (a) IncCond and (b) P&O MPPT controllers for a change in the temperature from 25°C to 50°C at a fixed irradiation equal to 1000 W/m².

the maximum power and does not depend on the load variation. We also notice that the PV voltage is stable in the system droved with these MPPT algorithms and, on the contrary, it is variable according to the load without them. For the second series of tests we simulated the load with three batteries. The results of the response variations of the batteries on the power and on the voltage of the generator with and without MPPT are reported in Fig.9 where, in these figures, the blue, grey and red lines are related to the responses with the P&O, IncCond algorithms and without, respectively. The maximum power point is achieved by the use of a MPPT stage and for a direct connection. The response closely approaches the optimum efficiency with both MPPT. Nevertheless, the IncCond MPPT presents smaller oscillations around the MPP. The voltage is weaker without the algorithms and the losses without regulation hugely increase.

4.3. PVG response to a temperature step

We have also analyzed the influence of the temperature on the response of the MPPT algorithms. For that, we have considered a variation of the temperature from 25°C to 50°C at a fixed irradiation equal to 1000W/m² and we have reported the response of the MPPT in Fig.10.

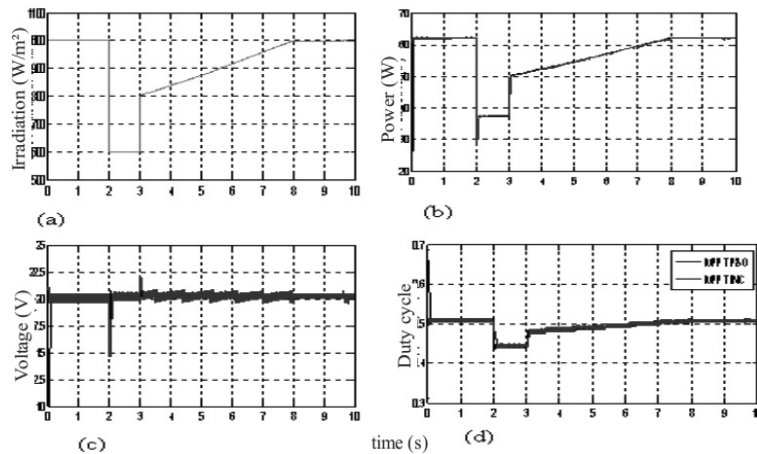


Figure 11: P&O MPPT and IncCond MPPT algorithm responses for a variation of illumination and a constant temperature of 25°C: (a) variation of the irradiation, (b) PVG power, (c) PVG voltage, (d) duty cycle.

These curves show that the P&O MPPT algorithm, see Fig.10.a, carries out variations before reaching the new MPP whereas and as shown in Fig.10.b, the IncCond MPPT one tends directly towards this MPP. Thus, with this simulation tool, we have highlight the fact that the advantages of the IncCond to the P&O algorithm by a faster achievement of the MPP which is carried out immediately in the good direction without additional oscillations when the MPP is reached in case of sudden change in temperature.

4.4. Robustness of the two algorithms

Finally, to study the robustness of the two algorithms with respect to various and randomly environmental conditions, we have defined an original set of tests and are carried out by simulations. Currently, basic tests in literature present change of parameters following a high amplitude step or a rapid change of one of the external parameter of the system. In actual conditions of exploitation of the photovoltaic energy production, i.e. when arrays and PVG are exposed to real climatic conditions, for small or unconnected installations or for installations inserted in an energy network, the changes are no so abrupt and not with a so huge amplitude as theoretically simulated. Even when shadows appears on a panel or an array or specially when temperature increase or decrease, the dynamic of the change is in order of the second which is at a minimum of two order of magnitude of the controller response. Thus, to perform test closer to the reality, we consider the system under various environmental conditions: (a) Initially the temperature is maintained constant ($T=25^{\circ}\text{C}$) and the solar radiation increases or decreases (Fig.11); (b) Then the illumination is maintained with a fixed value (1000 W/m²) and we varies the value of the temperature in the two directions of variation (Fig.12); (c) and finally, we subjected two algorithms MPPT to a random change of temperature (Fig.13);

In a first approach and at the contrary to the P&O algorithm, we can predict that the IncCond algorithm doesn't track in the wrong direction after a rapid change of the functioning conditions and doesn't present a strong oscillations about the MPP when it reaches it.

We can notice that IncCond MPPT offers a better continuation to discontinuous changes of the atmospheric conditions, but the differences in both algorithms is not drastic in case of continuous changes of the irradiation. We can also confirm with these tests that the temperature is a well-known factor that decreases the efficiency of the installation.

Finally, even if the overall better intrinsic performances of the IncCond algorithm can be shown by this study, we have to consider the simplicity of the P&O MPPT one, which makes it largely used according to the facility to implement in practical applications.

5. Conclusion

In this study, we investigated the optimal utilization of the solar energy by analyzing and comparing the two most common algorithms used for maximum power point tracking. The optimization has been targeted towards the

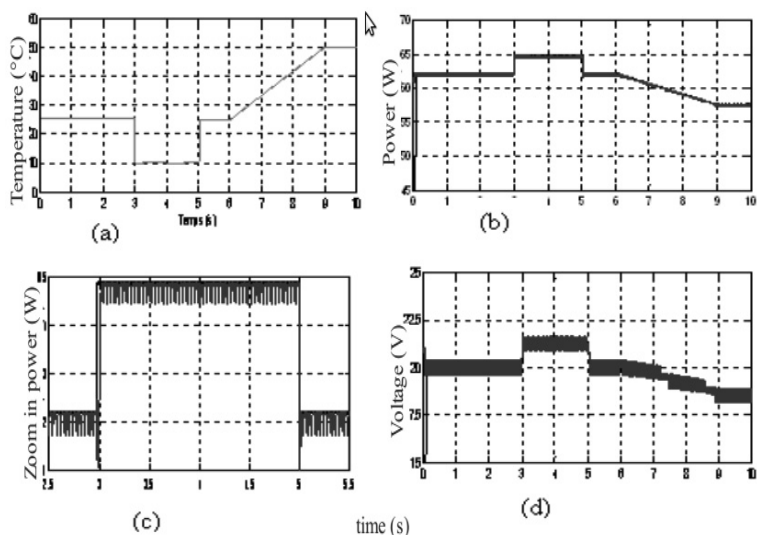


Figure 12: P&O MPPT and IncCond MPPT algorithm responses for a variation of temperature and a constant illumination of 1000W/m2: (a) variation of the temperature, (b) PVG power, (c) Zoom in PVG power, (d) PVG voltage.

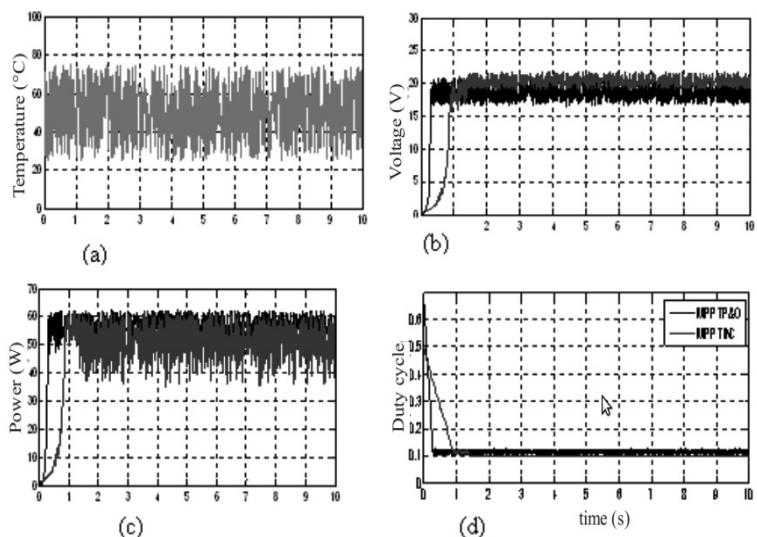


Figure 13: P&O MPPT and IncCond MPPT algorithm responses for a random variation of temperature: (a) random variation of the temperature, (b) PVG power, (c) PVG voltage, (d) duty cycle.

implementation of the maximum power point tracker algorithms in Matlab/Simulink environment. The role of the maximum power point tracker was to match the load power required with a maximum of the available power that can be generated from a photovoltaic generator (PVG), i.e. with the higher efficiency. The maximum power point will be reached by any irradiation levels and for any temperatures or variations of them. The simulation results prove positively that the P&O and the IncCond MPPTs reach the intended maximum power point. Nevertheless, the approach and the stability of the MPP are not achieved within the same manner. The IncCond MPPT presents better efficiency for rapid changes and a better stability when the MPP is achieved. However, the P&O MPPT are widely used in practice due to their simplicity. The originality and the specificity of the presented results obtain during this research reside in the fact that external parameters as irradiation and temperature were introduced, at first as linear functions and, at second as random ones describing more closely the actual applicative conditions. In cases of random functions for the simulation of external parameters, the defects and any other unfavorable conditions, which can affect the PVG are taken into considerations. We have shown that the two simulated MPPT algorithms responded with a non optimal efficiency to these functions in order to reach the MPP.

This work is the first part of a global research on MPP trackers. A novel algorithm, which was developed, recently tested and implemented in a microcontroller for the driving of DC-DC Boost converter connected to PV generator, will be presented soon. This new algorithm avoids the drawbacks of the P&O and IncCond algorithms presented in this study.

6. References

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