



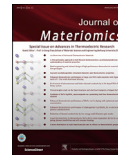
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# Enhanced thermoelectric performance of MnTe *via* Cu doping with optimized carrier concentration

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## Abstract

Polycrystalline  $\text{Mn}_{1-x}\text{Cu}_x\text{Te}$  ( $x = 0, 0.025, 0.05, 0.075$ ) thermoelectric materials were prepared by a combined method of melt-quenching and hot press. The effect of Cu doping on the electrical resistivity, band gap, the Seebeck coefficient and thermal conductivity was investigated. The power factors of the Cu-doped samples increase greatly due to the decrease of electrical resistivity and the higher Seebeck coefficient in high temperatures. In addition, the thermal conductivities of the Cu-doped samples also reduce due to the extra phonon scattering from the point defects introduced by Cu doping. As a result, the thermoelectric performance of MnTe is greatly enhanced, and a maximum  $ZT$  value of  $\sim 0.55$  in the  $\text{Mn}_{0.925}\text{Cu}_{0.075}\text{Te}$  sample at 773 K is achieved, which is 35% greater than that of the pristine MnTe sample.

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**Keywords:** MnTe; Thermoelectric materials; Doping; Carrier concentration

## 1. Introduction

Thermoelectric (TE) materials have attracted much attention due to their ability to convert heat directly into electricity [1–3]. In general, the conversion efficiency of a TE device depends on the dimensionless figure of merit  $ZT$  of the TE materials employed, i.e.,  $ZT = S^2T/\rho\kappa$ , where  $S$  is the Seebeck coefficient,  $\rho$  is the electrical resistivity,  $\kappa$  is the thermal conductivity and  $T$  is the absolute temperature. Therefore, effective TE materials should have a high power factor ( $S^2\sigma$ ) as well as a low thermal conductivity ( $\kappa$ ). However, it is challenging for researchers to decouple these parameters and achieve high  $ZT$  values due to the interdependent relationship between the electrical and thermal parameters [4]. Many efforts have been made to improve the  $ZT$  value of TE materials

through two main approaches so far. One approach is to increase the power factor by carrier engineering [5] or band engineering [6], and the another is to reduce the lattice thermal conductivity *via* nano-inclusions [7] or point defects [8]. Consequently, some encouraging results have been achieved in some material systems, such as  $\text{Bi}_2\text{Te}_3$ -based [9], PbTe-based [10],  $\text{CoSb}_3$ -based [11], etc.

Chalcogenide MnTe compound [12] has a typical hexagonal NiAs crystal structure with a large indirect band gap of 1.27 eV and a relatively low hole concentration ( $p = 10^{18} \text{ cm}^{-3}$ ) at room temperature. Recently, wide band gap semiconductors are frequently employed as potential TE materials due to their intrinsic large Seebeck coefficient and low thermal conductivity [13], which can work at a relatively high temperature. Thus, MnTe can be a potential candidate for middle-temperature thermoelectric application. Some studies have focused on the low-temperature electrical, magnetic and optical properties of MnTe compound [14–17], and MnTe has also been incorporated into PbTe, GeTe and SnTe thermoelectric materials [18–20] to improve their thermoelectric

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performance. However, less attention has been paid to its own intrinsic thermoelectric performance. More recently, Kim, et al. [21] prepared bulk non-stoichiometric MnTe materials by a melt-quenching plus spark plasma sintering method, and achieved a high Seebeck coefficient of over 600  $\mu\text{V/K}$  at room temperature and a promising  $ZT$  value of  $\sim 0.41$  in the  $\text{Mn}_{0.51}\text{Te}_{0.49}$  sample at 773 K. In the light of the band structure of MnTe, the large Seebeck coefficient is closely related to the large band gap and the  $p$ - $d$  overlap induced van Hove singularity in the electron density of states near the valence band edge [22]. Xie et al. [23] reported an enhanced TE performance in a sulfur doped MnTe in a low temperature range as a consequence of the increase of electrical properties and the decrease of thermal conductivity, however, the TE performance at a high temperature has no improvement at all. In general, the large electrical resistivity hinders the compound from achieving a high  $ZT$  value. Therefore, tuning its electrical properties is a key issue to improve the TE performance of the compound. Clearly, there are two possible doping sites in MnTe, i.e., the cation and anion sites. Some work on anion doping have already been tried, however, little work on cation doping in MnTe have ever been reported yet.

In this paper, Cu was doped into MnTe to substitute Mn cations for the improvement of its hole concentration and electrical properties. The samples of Cu-doped  $\text{Mn}_{1-x}\text{Cu}_x\text{Te}$  ( $x = 0, 0.025, 0.05, 0.075$ ) were prepared *via* a combined method of melt-quenching and hot press. The effect of Cu doping on the electrical and thermal transport properties the  $\text{Mn}_{1-x}\text{Cu}_x\text{Te}$  samples was investigated.

## 2. Experimental

### 2.1. Preparation

Cu-doped  $\text{Mn}_{1-x}\text{Cu}_x\text{Te}$  ( $x = 0, 0.025, 0.05, 0.075$ ) ingots were prepared *via* a vacuum melting method. The powders of Mn (99.9%), Te (99.99%) and Cu (99.9%) were weighed and loaded into quartz tubes after mixing, then the quartz tubes were evacuated and sealed to ensure a vacuum atmosphere ( $10^{-3}$  Pa). The sealed quartz tubes were slowly heated up to 1273 K, held at this temperature for 2 days followed by water quenching. The obtained ingots were ground to fine powders in an agate mortar and re-consolidated by a hot press under an axial pressure of 120 MPa in a purified argon atmosphere at 923 K for 2 h. The relative density is above 95% for all the hot pressed samples.

### 2.2. Characterization

The structure and phase purity of samples were characterized by a powder X-ray diffraction (XRD) in a model X'Pert PRO diffractometer with Cu  $K\alpha$  radiation ( $\lambda = 0.15418$  nm) (Philips Co. Ltd., the Netherlands). The fracture morphologies of the samples were observed by a model NanoSEM 450 field-emission scanning electron microscope (FSEM). The Seebeck coefficient and electrical resistivity were simultaneously measured using a model Namicro-III thermoelectric

measurement system. Thermal conductivity ( $\kappa$ ) is calculated according to  $\kappa = DC_p\lambda$ , where  $D$  is the density, which was determined by the Archimedes method,  $C_p$  is the specific heat capacity and the literature value of  $C_p$  [23] for MnTe compound was used for all the samples, and  $\lambda$  is the thermal diffusivity measured by a model LFA-427 laserflash diffusivity instrument (Netzsch Co. Ltd., Germany). The Hall measurements were accomplished by van der Pauw method in a model HMS 5500 Hall effect measurement system.

## 3. Results and discussion

### 3.1. Phase identification

Fig. 1a shows the X-ray diffraction patterns (XRD) of the  $\text{Mn}_{1-x}\text{Cu}_x\text{Te}$  ( $x = 0, 0.025, 0.05, 0.075, 0.1$ ) samples. For  $x$  from 0 to 0.075, all the XRD peaks can be well indexed as a hexagonal MnTe phase (space group, P63/mmc), and no peak of secondary phase is detected, indicating that single phase MnTe-based compounds can be obtained within the composition range of doping. However,  $\text{MnTe}_2$  impurity phase was clearly found in  $\text{Mn}_{0.9}\text{Cu}_{0.1}\text{Te}$  sample, which is negative to the electrical transport property of MnTe. In Fig. 1b, the XRD peaks shift toward a low angle direction due to the larger ionic radius of  $\text{Cu}^+$  (77 pm) compared to  $\text{Mn}^{2+}$  (66 pm). This shift further confirms that  $\text{Cu}^+$  has substituted the  $\text{Mn}^{2+}$  of the MnTe lattice. The lattice parameters of the samples were  $a = 4.1438, c = 6.7039$ ;  $a = 4.1448, c = 6.7048$ ;  $a = 4.1459, c = 6.7058$ ;  $a = 4.1468, c = 6.7075$ ;  $a = 4.1446, c = 6.7045$ , respectively. This increased lattice parameters are consistent with the shift of the XRD peaks.

Fig. 2 shows the SEM images of  $\text{Mn}_{1-x}\text{Cu}_x\text{Te}$  ( $x = 0, 0.025, 0.05, 0.075$ ) samples. Clearly, there is no evident difference among the hot-pressed samples. In addition, no crack and pore appear in the samples, indicating that they are a dense polycrystalline microstructure.

### 3.2. Electrical properties

Fig. 3a shows the temperature dependence of the electrical resistivity ( $\rho$ ) of  $\text{Mn}_{1-x}\text{Cu}_x\text{Te}$  ( $x = 0, 0.025, 0.05, 0.075$ ) samples. The electrical resistivity of all samples decreases with increasing the temperature generally except an un conspicuous peak at 323 K. This characteristic should be attributed to the transition from antiferromagnetism to paramagnetism of MnTe at the Neel temperature [12]. The Seebeck coefficient (see Fig. 5a) and thermal conductivity (see Fig. 6a) also have such a characteristic at the same temperature. The  $\rho$  of  $\text{Mn}_{1-x}\text{Cu}_x\text{Te}$  compounds exhibits a decrease within the exhaustion range from room temperature to 523 K, and it decreases rapidly with increasing the temperature due to the intrinsic excitation [23]. Besides, the  $\rho$  of all the samples decreases distinctly with increasing Cu doping content in the whole measured temperature range. Assuming a single parabolic band conduction process at 300 K, we estimated the carrier concentration ( $n$ ) from the formula  $n = 1/eR_{\text{H}}$ , where  $e$  is the electronic charge. The measured carrier concentrations are  $\sim 6.8 \times 10^{18} \text{ cm}^{-3}$ ,

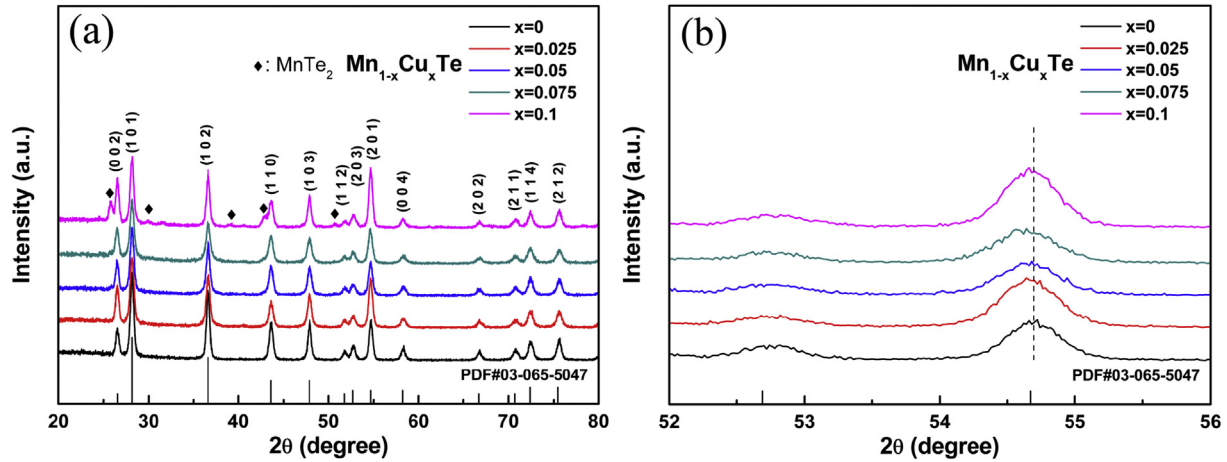


Fig. 1. (a) XRD patterns of  $\text{Mn}_{1-x}\text{Cu}_x\text{Te}$  samples with different Cu doping content. (b) high angle XRD peak position comparison of the samples.

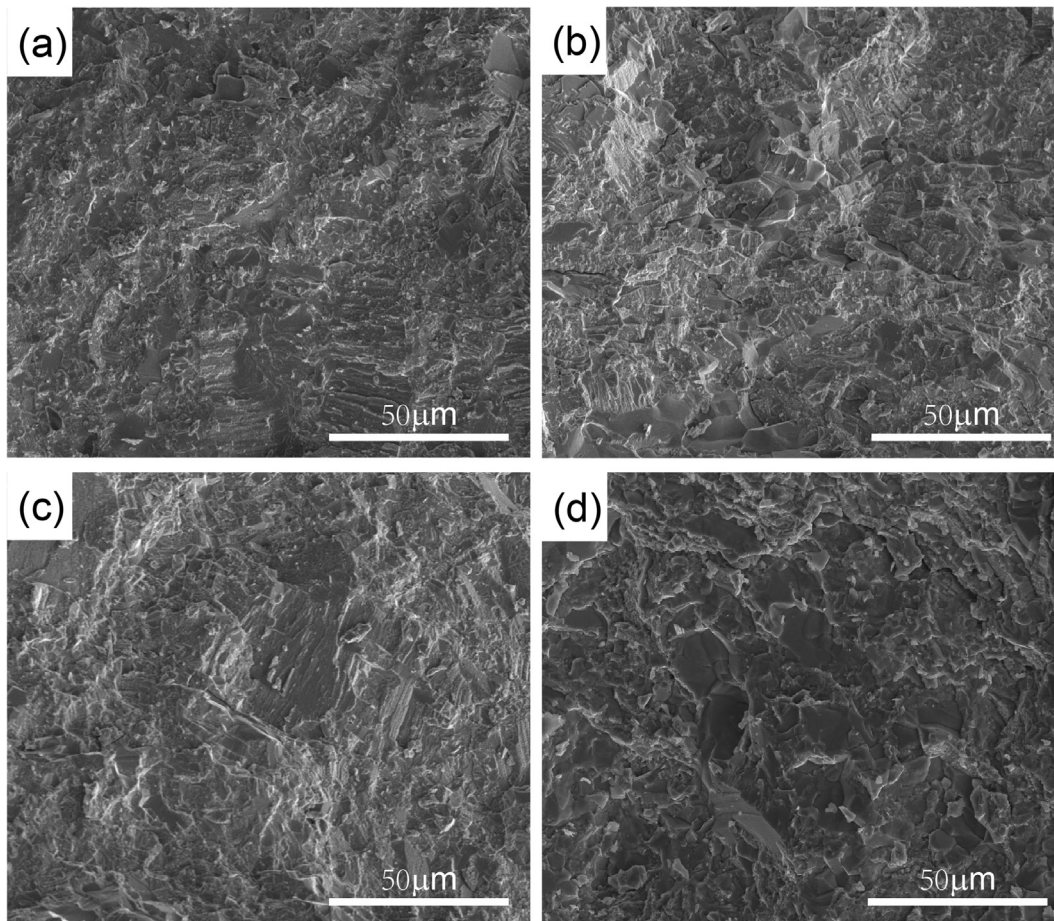


Fig. 2. SEM images of the samples with different contents of Cu doping (a)  $\text{MnTe}$ , (b)  $\text{Mn}_{0.975}\text{Cu}_{0.025}\text{Te}$ , (c)  $\text{Mn}_{0.95}\text{Cu}_{0.05}\text{Te}$ , (d)  $\text{Mn}_{0.925}\text{Cu}_{0.075}\text{Te}$ .

$\sim 1.7 \times 10^{19} \text{ cm}^{-3}$ ,  $\sim 5.2 \times 10^{19} \text{ cm}^{-3}$ , and  $\sim 1.8 \times 10^{20} \text{ cm}^{-3}$  for the pristine  $\text{MnTe}$ ,  $\text{Mn}_{0.975}\text{Cu}_{0.025}\text{Te}$ ,  $\text{Mn}_{0.95}\text{Cu}_{0.05}\text{Te}$ , and  $\text{Mn}_{0.925}\text{Cu}_{0.075}\text{Te}$  samples, respectively (see Table 1). Clearly, the carrier concentration increases rapidly with increasing Cu doping content, while the  $\mu$  decreases due to the impurity scattering by dopants (see Fig. 3b). Thus, this decrease in electrical resistivity should be attributed to the increased carrier

concentration by Cu doping, despite of the slight decrease in Hall mobility.

To further investigate the influence of Cu doping, the band gap was estimated from the slope of  $\ln \rho$  vs.  $1000/T$  curve (see Fig. 4a) according to the Arrhenius formula:

$$\rho = \rho_0 \exp(E_g/2k_B T) \quad (1)$$

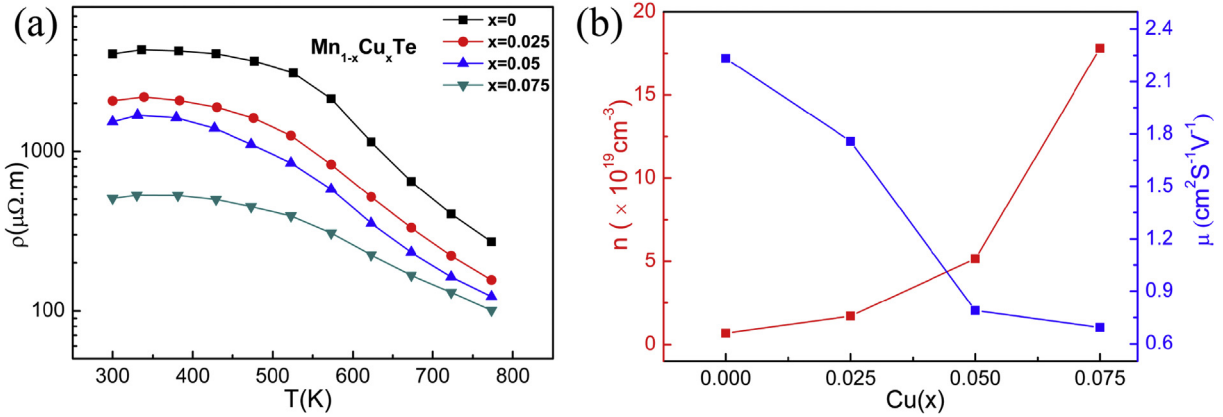


Fig. 3. (a) Temperature-dependent electrical resistivity ( $\rho$ ) of  $\text{Mn}_{1-x}\text{Cu}_x\text{Te}$  samples, (b) carrier concentration ( $n$ ) and carrier mobility ( $\mu$ ) at room temperature with respect to Cu doping concentration ( $x$ ) in  $\text{Mn}_{1-x}\text{Cu}_x\text{Te}$  samples.

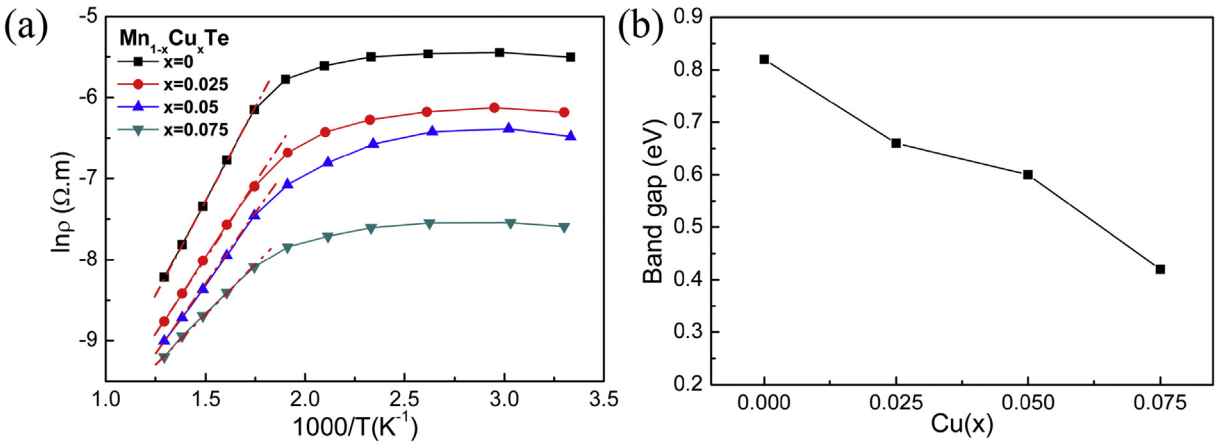


Fig. 4. (a)  $\ln \rho$  vs.  $1000/T$  plot, (b) the calculated intrinsic band gap of  $\text{Mn}_{1-x}\text{Cu}_x\text{Te}$  ( $x = 0, 0.025, 0.05, 0.075$ ).

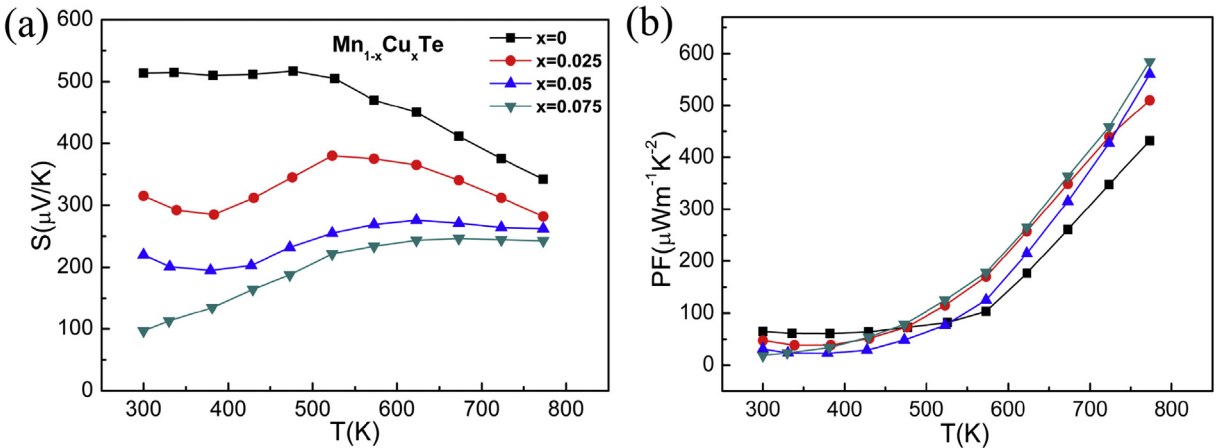


Fig. 5. (a) and (b) Temperature-dependent Seebeck coefficient ( $S$ ) and power factor ( $\sigma S^2$ ), respectively.

where  $\rho$  is the electrical resistivity, and  $\rho_0$  is a constant. The calculated intrinsic band gap values are 0.82, 0.66, 0.6 and 0.42 eV for the pristine MnTe,  $\text{Mn}_{0.975}\text{Cu}_{0.025}\text{Te}$ ,  $\text{Mn}_{0.95}\text{Cu}_{0.05}\text{Te}$ , and  $\text{Mn}_{0.925}\text{Cu}_{0.075}\text{Te}$  samples, respectively (see Fig. 4b). In which, the estimated band gap value of the pristine MnTe is similar to the theoretical result (0.8 eV) [24].

It can thus be concluded that the band gap of the samples narrows with increasing Cu content. This is consistent with the increase in carrier concentration and electrical conductivity.

Fig. 5a shows the temperature-dependent Seebeck coefficient of  $\text{Mn}_{1-x}\text{Cu}_x\text{Te}$  ( $x = 0, 0.025, 0.05, 0.075$ ) samples. At 300 K, the room-temperature Seebeck coefficient ( $S$ ) of the



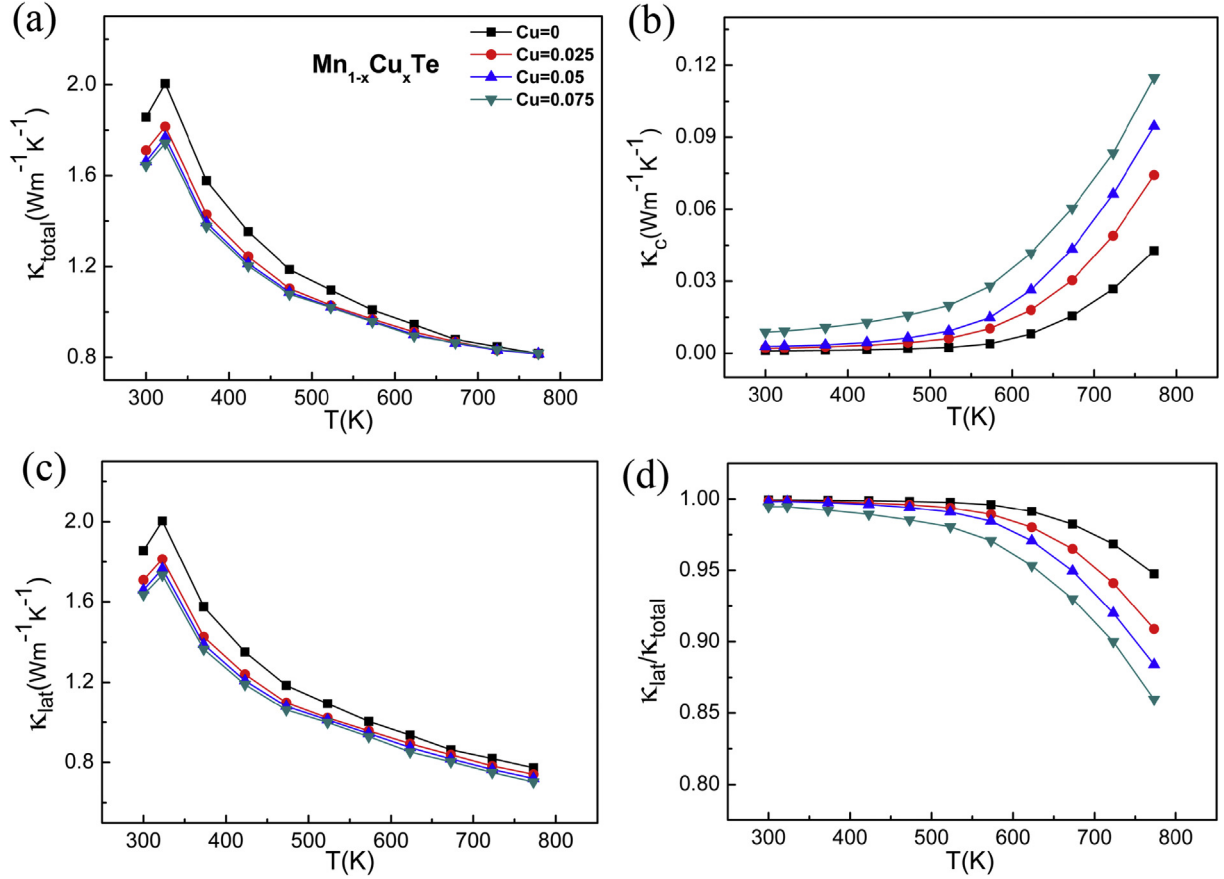


Fig. 6. Temperature-dependent (a) total thermal conductivity ( $\kappa_{\text{total}}$ ), (b) carrier thermal conductivity ( $\kappa_c$ ), (c) lattice thermal conductivity ( $\kappa_{\text{lat}}$ ) and (d)  $\kappa_{\text{lat}}/\kappa_{\text{total}}$  of the  $\text{Mn}_{1-x}\text{Cu}_x\text{Te}$  ( $x = 0, 0.025, 0.05, 0.075$ ) samples.

Table 1

Carrier concentration  $n_h$ , effect mass  $m^*$  of all the samples at room temperature.

| Sample  | $n_h$ ( $10^{19} \text{ cm}^{-3}$ ) | $m^*(m_0)$ |
|---|-------------------------------------|------------|
| MnTe  | 0.68                                | 5.58       |
| $\text{Mn}_{0.975}\text{Cu}_{0.025}\text{Te}$ | 1.71                                | 2.38       |
| $\text{Mn}_{0.95}\text{Cu}_{0.05}\text{Te}$   | 5.15                                | 2.1        |
| $\text{Mn}_{0.925}\text{Cu}_{0.075}\text{Te}$ | 17.8                                | 1.45       |

pristine MnTe is  $513.9 \mu\text{V/K}$ , and it decreases dramatically after doping Cu into Mn sites, displaying a similar trend with the electrical resistivity. In addition, the  $S$  for all the samples reduces with the increase of temperature at a high temperature, and the temperature factor of the  $S$  reduces gradually with the content of Cu. When the point defect is the top change in the samples with different contents of Cu, it should also be the main effect on the  $S$  for the samples. Assuming a single parabolic band model with acoustic phonon scattering for nondegenerate semiconductor, we estimate the effective mass  $m^*$  according to the following equation (2) using the measured  $S$  and Hall carrier concentrations ( $n$ ):

$$S = \frac{k_B}{e} \left\{ 2 + \lambda + \ln \left[ \frac{2(2\pi m^* k_B T / h^2)^{3/2}}{n} \right] \right\} \quad (2)$$

where  $m^*$  is the effective mass of carrier,  $e$  is the electronic charge,  $k_B$  is the Boltzmann constant,  $h$  is the Planck constant, and  $\lambda$  is the scattering parameter [23]. Considering  $\lambda = 0, 2$  for the acoustic phonon scattering and ionized impurity scattering, respectively.  $m^*$  is calculated when  $\lambda = 0$  and the acoustic phonon scattering is the dominant scattering mechanism in MnTe compound. The calculated  $m^*$  for the pristine,  $\text{Mn}_{0.975}\text{Cu}_{0.025}\text{Te}$ ,  $\text{Mn}_{0.95}\text{Cu}_{0.05}\text{Te}$ , and  $\text{Mn}_{0.925}\text{Cu}_{0.075}\text{Te}$  samples are  $5.58m_0$ ,  $2.38m_0$ ,  $2.1m_0$  and  $1.45m_0$ , respectively (see Table 1). Therefore, the Seebeck coefficient of the doped samples is greatly lower than that of the undoped MnTe as a consequence of the increase in carrier concentration and the decrease in effective mass  $m^*$ .

Fig. 5b shows the temperature dependence of the power factor of  $\text{Mn}_{1-x}\text{Cu}_x\text{Te}$  ( $x = 0, 0.025, 0.05, 0.075$ ) samples. Typically, at room temperature, the power factor value for MnTe is  $64.8 \mu\text{W m}^{-1} \text{K}^{-2}$ , which increases to a maximum of  $431.7 \mu\text{W m}^{-1} \text{K}^{-2}$  at 773 K. With the increase of the Cu content, the power factor decreases from  $64.8 \mu\text{W m}^{-1} \text{K}^{-2}$  for the pristine MnTe to  $18.4 \mu\text{W m}^{-1} \text{K}^{-2}$  for  $\text{Mn}_{0.925}\text{Cu}_{0.075}\text{Te}$  at room temperature, mainly due to the great decrease of the Seebeck coefficient. After 500 K, the power factor values for the doped samples exceed that of the pristine MnTe because of the increased electrical conductivity, then reach a maximum at 773 K. The power factor of

$\text{Mn}_{0.925}\text{Cu}_{0.075}\text{Te}$  becomes the maximum of  $584.2 \mu\text{W m}^{-1}\text{K}^{-2}$  at 773 K due to the decrease of the electrical resistivity and the relative high Seebeck coefficient at elevated temperature, which is 35.3% greater than that of the un-doped MnTe sample.

### 3.3. Thermal transport properties

Fig. 6a shows the total thermal conductivity ( $\kappa_{\text{total}}$ ) of all  $\text{Mn}_{1-x}\text{Cu}_x\text{Te}$  ( $x = 0, 0.025, 0.05, 0.075$ ) samples. The  $\kappa_{\text{total}}$  of  $\text{Mn}_{1-x}\text{Cu}_x\text{Te}$  samples generally decreases with increasing temperature except the transition point at 320 K. It is seen that the Cu-doped samples have lower  $\kappa_{\text{total}}$  than the pristine MnTe when the temperature is lower than 673 K, and the influence of Cu doping on the  $\kappa_{\text{total}}$  becomes slight at a high temperature. Generally, the  $\kappa_{\text{total}}$  consists of two parts, i.e., the lattice thermal conductivity ( $\kappa_{\text{lat}}$ ) and the carrier thermal conductivity ( $\kappa_{\text{c}}$ ). The  $\kappa_{\text{c}}$  was calculated using the Wiedemann-Franz law,  $\kappa_{\text{c}} = L\sigma T$ , where  $L$  is the Lorenz number,  $\sigma$  is the electrical conductivity and  $T$  is the absolute temperature. Here, when  $L = 1.5 \times 10^{-8} \text{ V}^2 \text{ K}^{-2}$ , this value is usually suitable for nondegenerate semiconductors [25]. Thus, the temperature-dependent  $\kappa_{\text{lat}}$  values can be obtained by subtracting the  $\kappa_{\text{c}}$  from the  $\kappa_{\text{total}}$ . In Fig. 6b, the  $\kappa_{\text{c}}$  of the  $\text{Mn}_{1-x}\text{Cu}_x\text{Te}$  samples increases largely with the increase of Cu doping content over the whole temperature range due to the enhanced electrical conductivity of samples. The  $\kappa_{\text{lat}}$  in Fig. 6c shows a slight decrease with increasing Cu doping concentration. This decrease in  $\kappa_{\text{lat}}$  can be ascribed to the extra point defects scattering for phonons, which is due to the mass fluctuation and strain field fluctuation by the substitution of Mn by Cu. In this case, we can conclude that the Cu doping has a slight effect on the  $\kappa_{\text{total}}$  at a high temperature due to the sharply increase in the  $\kappa_{\text{c}}$  of the Cu doped samples (see Fig. 6b). In addition, Xie, et al. [23] also reported that the bipolar effect could be an important factor.

Fig. 6d shows the calculated ratio of  $\kappa_{\text{lat}}$  in  $\kappa_{\text{total}}$  for all the  $\text{Mn}_{1-x}\text{Cu}_x\text{Te}$  samples. Clearly, the  $\kappa_{\text{lat}}/\kappa_{\text{total}}$  of the pristine MnTe sample decreases with increasing temperature, but it is greater than 90% over the whole temperature range. Moreover, the  $\kappa_{\text{lat}}/\kappa_{\text{total}}$  of Cu-doped samples is lower than that of pristine MnTe sample due to the significantly enhanced electrical conductivity, but it can remain above 85% over the entire temperature range. Consequently, the  $\kappa_{\text{total}}$  in  $\text{Mn}_{1-x}\text{Cu}_x\text{Te}$  system is mainly dominated by  $\kappa_{\text{lat}}$ , which conducts heat through lattice vibrations.

### 3.4. The dimensionless figure of merit $ZT$

Fig. 7 shows the dimensionless thermoelectric figure of merit ( $ZT$ ) of the  $\text{Mn}_{1-x}\text{Cu}_x\text{Te}$  ( $x = 0, 0.025, 0.05, 0.075$ ) samples. Clearly, the  $ZT$  value of all the samples monotonously increases with the increase of temperature. Note that the  $ZT$  values of the Cu-doped samples are greater than that of the undoped MnTe due to the remarkably decreased electrical resistivity and slightly suppressed thermal conductivity as aforementioned, and the maximum  $ZT$  value of 0.55 at 773 K

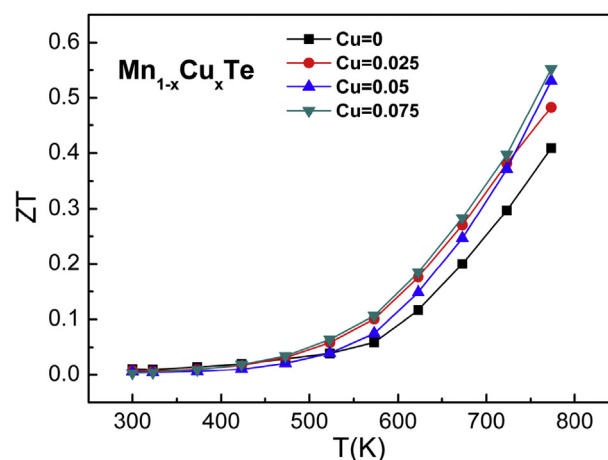


Fig. 7. Temperature-dependent thermoelectric figure of merit ( $ZT$ ) of the  $\text{Mn}_{1-x}\text{Cu}_x\text{Te}$ .

is achieved in the  $\text{Mn}_{0.925}\text{Cu}_{0.075}\text{Te}$  sample, which is approximately 35% greater than that of the pristine MnTe sample.

## 4. Conclusions

A series of p-type Cu-doped  $\text{Mn}_{1-x}\text{Cu}_x\text{Te}$  ( $x = 0, 0.025, 0.05, 0.075$ ) samples were prepared by a combined method of melt-quenching and hot press. The band gap of  $\text{Mn}_{1-x}\text{Cu}_x\text{Te}$  samples decreased correspondingly, and the electrical conductivity and power factor of the  $\text{Mn}_{1-x}\text{Cu}_x\text{Te}$  samples increased with increasing the Cu doping concentration due to the increase of carrier concentration. In addition, the thermal conductivity was reduced due to the intensive scattering of phonons by the extra point defects introduced by Cu doping. As a consequence, a maximum  $ZT$  value of  $\sim 0.55$  was obtained in the  $\text{Mn}_{0.925}\text{Cu}_{0.075}\text{Te}$  sample at 773 K, which was approximately 35% greater than that of the pristine MnTe sample.

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