Sintering and Microstructure of Al₂O₃ and Al₂O₃-ZrO₂ Ceramics

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Abstract

Alumina powder and two commercial 3 mol% yttria-partially stabilized zirconia powders–0.3 wt% Al₂O₃-doped (Al-Y-PSZ) and without Al₂O₃ (Y-PSZ)—were used to produce alumina-zirconia (Al₂O₃-ZrO₂) slip cast composites. The influence of the substitution of Al₂O₃ by 50 vol% of the different zirconia powders on the sintering kinetic at the intermediate stage was investigated. In addition, the microstructure of Al₂O₃ and the different composites at temperatures in the range of 1100-1600°C was studied and related to the sample hardness. An increase in the sintering rate was observed when 50 vol% Y-PSZ was substituted by 50 vol% Al-Y-PSZ. 50 vol% zirconia was effective to reduce the rate of Al₂O₃ grain growth in the final sintering stage. For 50 vol% Al-Y-PSZ a smaller ZrO₂ grain size distribution compared with 50 vol% Y-PSZ could be achieved. As the average Al₂O₃ grain size of the sintered samples became greater than about 1 μm a markedly decrease in the hardness was found; this occurred at temperatures higher than 1400°C, since de composites with 50 vol% zirconia reduced the rate of Al₂O₃ grain growth a decrease in hardness up to 1600°C was not observed.

Keywords: Al₂O₃ – ZrO₂, sintering behaviour, microstructure, hardness.

1. Introduction

The alumina (Al₂O₃) and alumina-zirconia (Al₂O₃-ZrO₂) ceramics are suitable for a variety of high demanding applications including dental screws, cutting blades, electrosurgical insulators, valve seals, body armor, pump components, oxygen sensors, dies, and prosthesis components such as hip joints, by Y. Shin et al. (1999), due to

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their attractive properties, including high-temperature mechanical strength, good thermal shock resistance, wear and oxidation resistance, low thermal conductivity, and the close match between their thermal expansion coefficients and those of metals, by J. Wan et al. (1989) and S. Olhero et al. (2009).

Colloidal processing methods allow to get green bodies with good microstructural homogeneity. Sintering of them represents great importance because it gives the microstructure and final properties of ceramics. Sintering models can be used to determine the diffusion mechanisms and activation energy. The sintering kinetics was studied measuring the contraction of the material as a function of time at different constant temperatures.

In this work, the influence of the substitution of Al₂O₃ either by 50 vol% of the different zirconia powders on the sintering kinetic at the intermediate stage was investigated. In addition, the microstructure of Al₂O₃ and the different composites at temperatures in the range of 1100-1600°C was studied and related to the sample hardness.

2. Experimental Procedure

2.1. Raw materials and powder processing

In this study, alumina powder (A16 SG, Alcoa Chemicals, USA, d₅₀=0.40 μm), and 3 mol% yttria-partially stabilized zirconia with 0.3 wt% Al₂O₃ (Saint-Gobain ZirPro, d₅₀=0.23 μm) and without Al₂O₃ (Saint-Gobain ZirPro, d₅₀=0.64 μm) powders were used. A commercial ammonium polyacrylate solution (NH₄PA) (Duramax D 3500, Rohm & Haas) was used as deflocculant. 48 vol% aqueous suspensions with different compositions (100 vol% Al₂O₃, and 50 vol% Al₂O₃ - 50 vol% zirconia powders respects to the total solid loading) with the optimum NH₄PA concentration (0.32, 0.52 and 0.11 wt% of Al₂O₃, 50vol% Al₂O₃ – 50vol% Al-YPSZ and 50vol% Al₂O₃ – 50vol% YPZ, respectively) were prepared using ultrasonic disruption; the pH was manually adjusted to 9. Slips were cast into rectangular shape plaster molds (12 x 10 x 9 mm); the consolidated samples were dried 100 °C. The green samples were sintered in air at 1100-1600 °C for 2 h (heating rate 5 °C/min).

2.2 Characterization techniques

The specific surface area (Sₐ) of the powders was measured using a Micromeritics Accusorb sorptometer. The density of the green compacts was determined by the Archimedes method using mercury sorption. The bulk density of the sintered samples was determined by water immersion (ASTM C20-00). The sintered samples were polished with a series of diamond pastes down to 1/4 μm. The Vickers hardness (Hv) was carried out using a diamond indenter (Buehler hardness tester) at a load of 3 kgf with an indentation period of 30 s. Ten Hv measurements were used to obtain an average value. The alumina and zirconia grain sizes were measured using SEM micrographs (JEOL, JSM-6360) of polished and thermally etched surfaces.

The isothermal shrinkage measurements were performed as follows: the temperature of the specimens was first increased at a constant rate of 10°C/min to 800°C, held at that temperature for 10 min, and subsequently increased rapidly at about 50°C/min to the set temperature, which was in the range of 1150-1400°C. The length shrinkage was measured as a function of time at the constant set temperature for 2h. When the time reached 2h, the specimens were cooled.

3. Results And Discussion

3.1 Densification and grain growth

The specific surface area (Sₐ) values for Al₂O₃, Y-PSZ and Al-Y-PSZ powders were 8.74, 7.84 and 12.25 m²/g, respectively.

In a previous work by Heidy L. Calambás Pulgarín et al. (2012), the present authors correlated the density of green samples with the rheological behavior of the suspensions. We noted that the suspensions of Al₂O₃ with Y-PSZ had the lowest of viscosity values and produced denser particle packing by slip casting.
Figures 1a and 1b show the change in the relative sintered density (% theoretical density) and the derivatives of sintered density with respect to temperature (d\(\rho\)/dT), versus the sintering temperature. At the intermediate sintering stage (1200-1400°C), the densification rate of Al\(_2\)O\(_3\) was higher than that of the composites Al\(_2\)O\(_3\)-ZrO\(_2\). The curves in Figure 1b showed a maximum, a higher peak temperature was found for the composites relative to that of Al\(_2\)O\(_3\) (1300°C for Al\(_2\)O\(_3\) and 1400°C for the composites) Differences between the composites were observed: 50 vol% Al-Y-PSZ (50Al-Y-PSZ) began to sinter at lower temperatures with respect to the composite with 50 vol% (50Y-PSZ), and higher sintered densities at 1250-1400 °C could be achieved.

The isothermal shrinkage behaviour of Al\(_2\)O\(_3\) and Al\(_2\)O\(_3\)-ZrO\(_2\) compacts was examined. Both values of the activation energy and the frequency-factor term in the applied sintering-rate equations were estimated from the isothermal shrinkage curves. The sintering-rate equation for isothermal shrinkage is given by K. Matsui et al. (2007):

\[
\Delta L/L_0 = \left(\frac{K\gamma\Omega a^n D}{kRTa^n}\right)t^n \tag{1}
\]

where \(\Delta L(= L_0 - L)\) is the change in the length of the specimen, \(L_0\) the initial length, \(K\) a numerical constant, \(\gamma\) the surface energy, \(\Omega\) the atomic volume, \(D\) the diffusion coefficient, \(t\) the time, \(T\) the absolute temperature, \(k\) the Boltzmann’s constant, \(a\) the spherical particle radius, and the parameters \(n\) and \(p\) the order depending on the diffusion mechanism. The values of \(p\) for grain-boundary diffusion (GBD) and volume diffusion (VD) are \(p=4\) and \(p=3\), respectively. Equation 1 is applicable to the fractional shrinkage of < 4, which satisfy the intermediate sintering stage.

On taking logarithms, the following equation is obtained:

\[
\log \frac{\Delta L}{L_0} = n\log \left(\frac{K\gamma\Omega a^n D}{kRTa^n}\right) + n\log(t) \tag{2}
\]

Moriyoshi et al. (1970) have reported that the log (\(\Delta L/L_0\)) vs log \(t\) plot of Eq. (2) does not show linear relationship when the grain growth proceeds simultaneously. Thus, the isothermal sintering experiments should be
analyzed carefully since the log-log plot of the shrinkage curve depends not only on the diffusion coefficient but also on the grain size.

![Graph showing mean grain diameters as a function of sintering temperature](image)

Fig. 2. Mean grain diameters ($d_{50}$) of Al$_2$O$_3$ and Al$_2$O$_3$-ZrO$_2$ composites as a function of the sintering temperature in the different composites

Therefore, the mean grain diameters of Al$_2$O$_3$ in the different compacts were measured as a function of the sintering temperature and are shown in Figure 2.

The Al$_2$O$_3$ grain diameter in pure alumina remained nearly constant in the temperature range 1100-1250°C, then a slightly increased in the grain diameter with increasing sintering temperature up to 1400°C was found, followed by a significant increase with further increasing in temperature up to 1600°C. The Al$_2$O$_3$ grain diameter in the composites remained virtually unchanged up to 1400°C. No significant differences in the Al$_2$O$_3$ grain diameter versus temperature curve between 50Al-Y-PSZ and 50Y-PSZ were found.

The significant Al$_2$O$_3$ grain growth in pure Al$_2$O$_3$ decreased the sintering rate at $T>1400$ °C (Equation 1) and let to a sintered density ($\rho_{sint}$) at 1600 °C lower than that observed for the composites Al$_2$O$_3$-ZrO$_2$ (Fig 1a). Similar density values at 1600 °C, 98.48 and 98.65% of the theoretical density, were measured for the composites with Al-Y-PSZ and Y-PSZ, respectively.
Figure 3 shows the microstructure of Al₂O₃, 50Al-Y-PSZ and 50Y-PSZ sintered at 1600 °C. The micrographs (b and c) show ZrO₂ grains (the brighter phase) homogeneously distributed in a fine grain Al₂O₃ matrix (the darker phase). The ZrO₂ grains inhibited the Al₂O₃ grain growth during the final sintering stage (1400-1600°C); thus, the ZrO₂ particles occupied the intergranular boundaries and often the triple points between Al₂O₃ grains. This had the effect of pinning the alumina and preventing grain growth. 50 vol% zirconia was effective inhibiting Al₂O₃ grain growth. For Al₂O₃ the rapid grain growth at 1400-1600°C led to a grain diameter at 1600°C that was 3.5 times greater than the grain diameter obtained for the composites with 50 vol% zirconia (Fig. 2).
Figure 4 presents the ZrO$_2$ grain size for the different composites at 1600 °C. The 50Al-Y-PSZ curve was slightly shifted to lower diameters with respect to that of 50Y-PSZ. The most frequent grain diameter was 0.6 and 0.8 μm for Al-Y-PSZ and Y-PSZ, respectively. The smaller ZrO$_2$ grain diameter for 50Al-Y-PSZ with respect to 50Y-PSZ was attributed to the finer Al-Y-PSZ particles relative to those of Y-PSZ.

The sintering temperature at which the Al$_2$O$_3$ grains did not change was 1150-1250 °C for Al$_2$O$_3$ and 1250-1400 °C for 50Al-Y-PSZ and 50Y-PSZ. These temperature ranges were selected to analyze the isothermal shrinkage curves of each sample.
3.2 Isothermal shrinkage analysis

Figure 5 shows the log-log plots of the isothermal shrinkage versus heating time curves for Al$_2$O$_3$, 50Al-Y-PSZ and 50Y-PSZ at four different temperatures. All the log-log plots showed linear relationships and the data satisfactory fitted to a slope of 1/3 ($n=1/3$, Eq. 2). These results indicated that the sintering rate of Al$_2$O$_3$ and the composites was controlled by grain boundary diffusion mechanism (GBD) by K. Matsui et al. (2007). The activation energy and frequency factor term of each specimen were estimated using the values of the constant term in Eq. (2). This constant term corresponded to the intercept of the straight line on the vertical axis in Figure 5 when log $t$ is 0.

Using as $\beta = \frac{K_e \Omega D_p}{T \kappa a_F}$ (Eq. 2) and using the general expression of the diffusion coefficient, $D = D_o \left( \frac{-Q}{RT} \right)$ the following equation is obtained:

$$\beta T = \beta_0 \exp \left( \frac{-Q}{RT} \right)$$

(Eq. 3)
Where \( \beta_0 = \frac{kY\Delta D_0}{k_aP} \) 

(4)

On taking natural logarithm in Eq. (3) resulted in:

\[
\ln(\beta T) = \ln \beta_0 - \frac{Q}{RT}
\]

(5)

where \( Q \) is the activation energy, \( R \) the gas constant, and \( D_0 \) the preexponential term of the diffusion coefficient.

Figure 6 shows the Arrhenius-type plots of \( \ln(\beta T) \) against \( 1/T \) for \( \text{Al}_2\text{O}_3 \) and the 50Al-Y-PSZ and 50Y-PSZ composites. The plots of all specimens showed linear relationships; the \( Q \) value of each sample was determined from the slope of the straight line by applying Eq. (5) to the Arrhenius-type plot in Figure 6. The value of \( \beta_0 \) was also determined from the intercept of the straight line on the vertical axis when \( 1/T=0 \). The \( Q \) and \( \beta_0 \) values of \( \text{Al}_2\text{O}_3 \) and the \( \text{Al}_2\text{O}_3-\text{ZrO}_2 \) composites are presented in Table 1. The activation energy of GBD in \( \text{Al}_2\text{O}_3 \) was smaller than that of the \( \text{Al}_2\text{O}_3-\text{ZrO}_2 \) composites. Thus, the greater sintering rate of \( \text{Al}_2\text{O}_3 \) with respect to that of the composites was attributed to the lower activation energy value (Eqs. 1-5).

Table 1. Activation energy and frequency for the sintering of \( \text{Al}_2\text{O}_3 \) and the composite factor.

<table>
<thead>
<tr>
<th>Muestra</th>
<th>Energía de Activación (KJ/mol)</th>
<th>Factor de Frecuencia ( \ln \beta_0 )</th>
</tr>
</thead>
<tbody>
<tr>
<td>( \text{Al}_2\text{O}_3 )</td>
<td>480±20</td>
<td>32</td>
</tr>
<tr>
<td>( \text{Al}_2\text{O}_3-\text{ZPS-dAl} )</td>
<td>690 ±20</td>
<td>50</td>
</tr>
<tr>
<td>( \text{Al}_2\text{O}_3-\text{ZPS} )</td>
<td>670 ±20</td>
<td>41</td>
</tr>
</tbody>
</table>

In the case of alumina-zirconia, our measurements of the activation energy agreed well with the work of Wakai et al. (1989) who obtained the following values for alumina-zirconia (3 mol% yttria): 723 KJ/mol for 50 vol% \( \text{Al}_2\text{O}_3 \) and 681 kJ/mol for 85.7 vol% \( \text{Al}_2\text{O}_3 \). Wang et al. (1991) also reported an activation energy of 730 ± 60 kJ/mol for alumina containing 5 vol% \( \text{ZrO}_2 \); they correlated the activation energies of alumina and alumina/zirconia with their respective interfacial energies. The alumina/zirconia interface energy was lower than that of alumina/alumina by a factor of 1.5 which was nearly the same as the ratio of the activation energies for boundary diffusion in these two types of interfaces.

Matsui et al. (2007) studied the effect of the specific surface area of different zirconia powders on the initial
sintering stage; they concluded that the increase in the specific surface area of fine zirconia powders enhanced the shrinkage rate because of an increase in $\beta_0$. In the present work, the specific surface area of the Al-Y-PSZ particles was markedly higher than that of Al$_2$O$_3$ or Y-PSZ, consequently a higher $\beta_0$ value could be expected when a large amount of Al$_2$O$_3$ or Y-PSZ was substituted by Al-Y-PSZ. Therefore, the increase in the $\beta_0$ value with the substitution of 50 vol% Y-PSZ by Al-Y-PSZ was a consequence to the increase in the specific surface area of the powders, resulting in an increasing sintering rate.

Matsui et al. (2008) also investigated the effect of Al$_2$O$_3$ concentration on the sintering of fine ZrO$_2$ powders; they demonstrated that an increase in the Al$_2$O$_3$ content from 0 to 1 wt% enhanced the densification rate because of the increase in both $n$ with the change of diffusion mechanism from grain boundary to volume diffusion and $\beta_0$ (Eq. 7). This enhanced sintering mechanism was reasonably interpreted by the segregated dissolution of Al$_2$O$_3$ at ZrO$_2$ grain boundaries. Therefore, the higher sintering rate at the intermediate stage of 50Al-Y-PSZ relative to 50Y-PSZ could be attributed to the increase in the specific surface area of the powders together with the enhanced densification produced by the Al$_2$O$_3$ doping.

3.3 Sample hardness

![Vickers hardness versus the sintering temperature for Al$_2$O$_3$ and 50Al-Y-PSZ and 50Y-PSZ composites.](image)

Figure 7 shows the vickers hardness ($H_v$) versus the sintering temperature for Al$_2$O$_3$ and the Al$_2$O$_3$-ZrO$_2$ composites. For all the samples the hardness increased with increasing sintering temperature from 1300 to 1400°C as a consequence of the increase in the relative sintered density (Fig. 1a). Thus, at 1300-1400°C the higher relative sintered density of Al$_2$O$_3$ resulted in higher $H_v$ values. Although the sintered density of Al$_2$O$_3$ increased with further increasing in temperature from 1400 to 1500 °C a maximum hardness was found at 1400°C. On the contrary, 50Al-Y-PSZ and 50Y-PSZ did not show a maximum instead the $H_v$ value increased up to 1600°C.

This behaviour was related with the Al$_2$O$_3$ grain growth versus temperature curves shown in Fig. 2. When the Al$_2$O$_3$ average grain diameter increased over about 1 μm a markedly decrease in the $H_v$ values was found; this occurred at $T > 1400°C$ for Al$_2$O$_3$. According to Rice et al (1994) the generally accepted trend was that $H_v$ increased with decreasing the grain size (G) (e.g., $H_v \propto G^{-1/2}$) at finer G. For their alumina specimens, Krell et al. (1995) attributed the increase in hardness with decreasing grain size to a reduction in dislocation mobility with decreasing grain size.

In this work, we reported a decrease in the $H_v$ values when the Al$_2$O$_3$ became greater than about 1 μm, this occurred at $T > 1400°C$ for Al$_2$O$_3$. Since 50 vol% ZrO$_2$ reduced the rate of Al$_2$O$_3$ grain growth (Fig. 2), the Al$_2$O$_3$ average grain diameter remained ≤ 1 μm up to 1600 °C and consequently a decrease in $H_v$ was not observed (Fig. 7). 50Al-Y-PSZ and 50Y-PSZ exhibited nearly the same $H_v$-T dependence in the whole range of temperatures studied. The $H_v$ value for Al$_2$O$_3$ at 1400 °C was markedly higher than that of 50Al-Y-PSZ and 50Y-PSZ at 1600 °C; since
alumina is harder than ZrO₂ by A. H. De Aza (1995), these differences in the Hᵥ values could be attributed to the greater substitution of Al₂O₃ by ZrO₂ in the composites.

4. Conclusions

Two commercial 3 mol% yttria-partially stabilized zirconia powders, 0.3 wt% Al₂O₃-doped (Al-Y-PSZ) and 100% Y-PSZ, were used to produce alumina-zirconia (Al₂O₃-ZrO₂) slip cast composites. The influence of the substitution of Al₂O₃ either by 50 vol% Al-Y-PSZ or 50 vol% Y-PSZ on the sintering kinetic at the intermediate stage was investigated. In addition, the microstructure of Al₂O₃ and the different composites at temperatures in the range of 1100-1600 °C was studied and related to the sample hardness.

The intermediate sintering stage of both alumina and the composites was controlled by a grain-boundary diffusion mechanism. The densification rate of Al₂O₃-ZrO₂ was lower than that of Al₂O₃ as a consequence of the increase in the activation energy of sintering in the presence of zirconia. An increase in the sintering rate was observed when 50 vol% Y-PSZ was substituted by 50 vol% Al-Y-PSZ. This behaviour could be attributed to the increase in the specific surface area of the Al-Y-PSZ powder together with the enhanced densification produced by the Al₂O₃ doping. For 50 vol% Al-Y-PSZ a smaller SrO₂ grain size distribution compared with 50 vol% Y-PSZ could be achieved.

As the average Al₂O₃ grain size of the sintered samples became greater than about 1 μm a markedly decrease in the hardness was found; this occurred at temperatures higher than 1400°C for Al₂O₃. Since 50 vol% 50Al-Y-PSZ and 50 vol% Y-PSZ reduced the rate of Al₂O₃ grain growth a decrease in hardness up to 1600 °C was not observed.

References