Environment of Design Requirements Input and Preliminary Sizing for Aircraf t Conceptual Design

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Abstract: To supply a convenient and expandable tool to organize the design requirements of a new aircr aft and estimate its basic design parameters during conceptual design, the Environment of Design Requirements Input and Preliminary Sizing (EDRIPS) was developed. In this environment, the performance requirements, mission profile and payloads could be input ted or selected respectively through user -friendly int erfaces in a highly interactiv e way . Based on these requirements, it enables the designer to pick up a design point in the solution space through constraint analysis, and then conduct mission analysis either step by step or via auto iteration by using an improved method for estimating the takeoff weight. The implementation of each module and the methods utilized are described. A design example is finally presented and analyzed to validate the efficiency and reliability of applying EDRIPS to aircraft conceptual design.

Key words: aircraft design; design requirem ents; constraint analysis; mission analysis; computer aided design

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摘 要: 为了在飞机概念设计过程中给新型号的设计要求组织和基本参数估算提供便捷且可扩展 $(EDRIPS)$, \mathcal{R}

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EDRIPS

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 During the past two decades, com puter aided design technique has played an im portant role in aircraft concept ual design. T o any system for Computer Aided Aircraft Conceptual Design $(CAACD)$, the handling of design requirements, which is the yardstick for a feasible design, is always an essential problem, for the items and data structures of inputted requirements should be propitious to subsequent preliminary sizing. Correspondingly, the part of preliminary sizing, which consist s of constraint analysis and mission analysis,

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should enable the designer to get such basic design param eters as takeoff weig ht quickly , as w ell as to find out potential antinom ies and inaccuracies in requirements. The Environment of Design Requirements Input and Preliminary Sizing (EDRIPS), w hich uses such current typical CAACD codes as $\text{AAA}^{\text{[1]}}, \quad \text{ACSYNT}^{\text{[2]}}, \quad \text{AeroDYNAM IC}^{\text{[3]}} \quad \text{and}$ $RDS^{[4, 5]}$ for reference, was just developed to supply an integrated environment that embraces both of the design requirements input module and preliminary sizing module. EDRIPS also offers an ex-

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pandable framework with friendly graphical user $interface (GUI)$, so that it could not only fulfill the initial tasks of conceptual design conveniently, but also serve as the basis for further enhancement.

1 Basic F eatures and System Structure

At the beginning of aircraft design, the decision should be made that whether an absolutely novel design or a baseline one is required. One of the basic features of EDRIPS is setting tw o task modes to deal with them discriminatingly, which could im prove the design efficiency by utilizing existent design information of baseline aircraft when baseline design is conducted.

Hierarchy of data precision is a distinct t rait of engine, aerodynamic and weight fraction characteristics, which are the three kinds of primary data for sizing, with the proceeding of conceptual design. Take aerodynamic characteristics as example, statistical data for each category of aircraft, characteristics of baseline aircraft (if exists), computed characteristics for proposed config urations could be utilized at different stages of conceptual design. As for EDRIPS, the analysis is concentrated on the first stage approxim ation. How ever, it could be easily expanded to fulfill detailed sizing when more precise data are available due to the adoption of Object-O riented Prog ramm ing (OOP) technique with using $C++$ language, which also ensures the feasibility of contrasting the results of later performance analysis with well organized design requirements to evaluate a scheme-

The development environment of EDRIPS is PC platform and Windows operating system, which ensures that it could be accessed by more designers and be conveniently integrated into such av ailable systems as $\text{RCSP}\text{lus}^{[6]}$.

Fig. 1 illustrates the system structure of EDRIPS. Task selection is dedicated to select the category of aircraft and distinguish design tasks. Performance requirements input, mission profile input and payload selection belong to the design requirements input module; sizing setting, constraint

analysis and mission analysis are parts of the preliminary sizing module. Predefined data include the International Standard Atm osphere (ISA) characteristics and statistical data summarized from documents on conceptual design^[7-9], while computed data are got from subsequential analysis and could only be studied from such aspects as data structures currently.

Fig. 1 System structure of EDRIPS

2 Design Requirem ents Input M odule

2. 1 Performance requirements input

Candidate requirements are classified into t hree g roups: fundamental flight performances, such as maximum Mach num ber and m aximum range; maneuver performances, such as sea level climb rate and load factor of sustained turn; structural and material requirements, such as maximum dy namic pressure and w hether composite materials are used or not. The designer can select needed item s and input associated data, w hile EDRIPS will judge which one should not function according to the category of current aircraft. For example, it will be no use if the load factor of instantaneous turn is given to an UAV .

2. 2 Mission profile input

Because of the im portance of the mission profile to sizing and trajectory analysis, there have been m any researches on the methods for describing and utilizing it $\mathbf{t}^{[10, 11]}$. In terms of the requests for the mission profile input met hod presented in Ref. [10], the expandability of profile definition and friendliness of GUI are two of the most outstanding ones. The former is ensured by using OOP technique in EDRIPS: each optional mission

segm ent, *i.e.* takeoff, accelerated/decelerated clim b/ dive, cruise, horizontal acceleration/ deceleration, com bat turn, loiter, delivering expendables, descent and landing, is defined as an independent class that encapsulates all the associated specific data. By putting the basic information of each segment, such as its name and index in the list com posed by seg ments belonging to the sam e kind, in a mission segments information list in succession, t he w hole profile could be built. Fig . 2 illustrates such data st ructures by taking cruise and descent segm ents as ex ample.

Fig. 2 Examples of data structures for mission profile

As to the friendliness of interface, the GU I as shown in Fig. 3 was devised for EDRIPS by using such systems as $AeroDYNAMIC^{[3]}$ and $MPIS^{[10]}$ for reference. The upper zone of the interface is to represent the mission profile by a set of independent bitmaps, which could supply visual feedback to the designer. Once a segment is selected by clicking t he corresponding bitm ap or has just been added, the associated data will be shown in the list box on the left of the interface. Then the designer could m odify t hese data or even delete an existing segm ent.

In order to eliminate explicit mistakes of the inputted profile, an important measure adopted by EDRIPS is setting a plotting zone that takes rang e and altitude as abscissa and ordinate respectiv ely. Once an operation has been accomplished, EDRIPS will adjust the range of coordinate axles according to the latest profile and plot its rough trajectory. Because only the abscissas of two adjacent segments are assumed to be continuous, if the altit ude of any mission segment is unreasonable,

the trajectory will be broken along the direction of ordinate, and t he desig ner is thus notified to make some modification.

2. 3 Payl oad selection

In EDR IP S, payloads are classified into four sorts, *i.e.*, persons, weapons, equipment and others; and each sort is subdivided into several more refined groups. For instance, guns, missiles and shells are subdivisions of weapons. All the available payloads are defined and initialized in a payload base firstly, and then invoked and displayed by EDRIPS. This indicates that the key element to pay load selection is the developing of the payload base, w hile such operations as selecting, adjusting on interface are relatively conventional.

3 Preliminary Sizing M odule

3. 1 Sizing setting

Functions of this part include the following item s: determine the usable hierarchy of data for sizing according to the design requirements and information of current aircraft and its baseline (if exists), and then feed back the information to the designer via GUI; enable the designer to change the category of engine to contrast the sizing results if its type has not been fixed; update the desig n information after sizing. It also serves as the joint betw een constraint analy sis and m ission analysis: the parameters of the design point, namely, sea level thrust loading T_{SL} / W_{TO} and takeoff wing loading W To/S, picked up through the former are transferred to the latter; the weight fraction characteristics calculated through the latter are passed back to the former to get more precise constraint boundaries.

3. 2 Constraint anal ysis

Ten kinds of constraints, such as takeoff ground roll length, maximum M ach number, cruise Mach numbers, and load factor of sustained turn can be handled in EDRIPS now. When the mission analysis interface $(Fig. 4)$ is initialized, the data for each constraint item will be checked for usability based on the design requirements of the current aircraft: If usable, the corresponding

boundary could be computed^[9, 12] and the designer could control whether to display it or not; if unusable, EDRIPS will show prompts through the interface or pop-up dialogs. T he designer could use his mouse to pick up a feasible design point in the solution space form ed by different boundaries and view the values of T_{SL}/W_{TO} and W_{TO}/S of it in real time. As an assistant measure to make the selection more reasonable, the design points of existent aircraft that belong to the same category with the current design could be displayed in the constraint diag ram as references.

Fig. 4 Interface of constraint analy sis

3. 3 Mission analysis

The takeoff weight W_{TO} , sea level statistic thrust of engine T_{SL} and wing area S are the basic design parameters of an aircraft and objectives of mission analysis, in which the estimation of W ^{T O} is the key problem. When W_{TO} is calculated, T_{SL} and S could be easily got by using $T \nLly {\mathbb{Z}}$ w τ o and $W \nLly {\mathbb{Z}}$ selected in the constraint analysis.

The basic equation for estimating W To is^[9]

$$
W_{\text{TO}} = W_{\text{F}} + W_{\text{E}} + W_{\text{P}} \tag{1}
$$

where W_F is the fuel weight, W_E the empty weight, and W_F the payload weight. Both W_F and W_{E} are related to W_{TO} , so utilizing Eq. (1) to conduct analysis is an iterative process and the designer should input a guessed takeoff weight $W_{\text{T} \text{Oguess}}$ via interface firstly. W_P consists of the weight delivered during flight W PE and the w eight of fixed payload W PF, and its value is determined by payload selection^[13] and will not change during sizing.

 W_F could be calculated through analyzing the w eight fraction characteristics of each seg ment in t he mission profile, w hich includes m ission segment weight fraction Π and instantaneous weight fraction β that could be expressed as functions of propulsion characteristics and each segment's param eters $^{[9]}$. To analy ze those segments that deliver no expendables, the methods depicted in Ref. [9] are cited with modifications, $e, g,$, the minimum time-to-climb path in it will not be utilized in EDRIPS until further perform ance analysis is fulfilled.

If delivery of expendables is contained in the mission profile, the current methodologies for estimating W_F are basically considering solely the w eight loss for the fuel consumed at first, and then modifying the result according to the delivered w eight^[7-9]. In order to avoid breaking the profile into several fractions, even if there exist several scattered segments for delivering expendables, the meaning of Π is expanded in EDRIPS, *i.e.*, the equations for calculating Π and β of the segment for delivering expendables (assumed to be segm ent 'i') are m odified as follow s

$$
\Pi = \frac{W_{if}}{W_{ii}} = \frac{W_{ii} - W_{\text{iddivered}}}{W_{ii}} =
$$
\n
$$
1 - \frac{W_{\text{delivered}}}{\beta_{i-1}W_{\text{TO guess}}}
$$
\n(2)

$$
\beta_i = \beta_{i-1} \Pi_i \tag{3}
$$

where W if , W ii, W iddivered and β -1 are the final and initial weights of this segment, the delivered weight and β of the previous segment, respective- \lg .

Based on such modification, the final w eight at the end of a mission is

$$
W_{\text{land}} = \beta_{\text{and}} W_{\text{TO}} \tag{4}
$$

where β land is the instantaneous weight fraction of the landing segm ent.

Thus the fuel w eight decreased during flight

$$
W_{\text{Fused}} = W_{\text{TO}} - W_{\text{land}} - W_{\text{PE}} =
$$

$$
(1 - \beta_{\text{land}}) W_{\text{TO}} - W_{\text{PE}} \tag{5}
$$

and then

$$
W_{\rm F} = \gamma W_{\rm Fused} \tag{6}
$$

where γ is determined by the reserved fuel for m ission. Moreover, to the potential air fueling segment, this strategy also functions, once the increased fuel is counted into W_{PE} as negative expendables.

At this stage of design, W_E is estimated based on statistic relationship between $W \nvert E$ and $W \nvert D$ of existent aircraft, and a general format of estimation could be sum marized from Refs. $[7-9]$ as

$$
W_{\rm E} = \lambda (\mathcal{P}W_{\rm TO}^{\rm p} + \mathbf{\zeta}) \tag{7}
$$

where λ reflects the effect of weight saving caused by using composite materials, φ is a combined factor determined by the category of aircraft and design parameters, while both of p and ζ are determined by the category of aircraft. It should be noted that in the methods int roduced in Ref. [7] and Ref. [9] (the latter one is adopted by EDRIPS), φ is also determined by t he category of aircraft solely and ζ equals zero.

Substituting Eqs. $(5-7)$ into Eq. (1) provides $W_{\text{TO}} = \lambda \mathcal{Q} W_{\text{TO}}^P + \mathcal{Y} (1 - \beta_{\text{land}}) W_{\text{TO}} + W_{\text{P}} + \zeta$ (8)

Under the mode of 'step by step' supplied by EDRIPS, $W_{\text{Tocalculated}}$ got by substituting $W_{\text{To guess}}$ into the right hand side of Eq. (8) is just the final result. This mode could help the designer, especially those w ho are still under learning to com prehend the practical meaning of the takeoff weight. However, an evident error always exists between W TOguess and W TO calculated here, so the 'auto iteration' mode must be utilized to get such a result that could satisfy the given relative error.

When no segm ent for delivering ex pendables

exists, β and is a constant, and Eq. (8) can be written as

$$
W \text{ to} = A W_{\text{TO}}^P + B W \text{ to} + C \tag{9}
$$

where $A = \mathcal{N} \mathcal{P} B = \mathcal{Y} (1 - \beta_{\text{and}})$ and $C = W_{P} + \zeta$ all of w hich could be treated as constants for a specific aircraft if its design parameters are not changed during iteration. Then a function could be defined according to Eq. (9) as

$$
f(W_{\text{TO}}) = A W_{\text{TO}}^{\rho} + (1 - B) W_{\text{TO}} + C
$$
\n(10)

Its first derivative with respect to W_{TO gives

$$
f (WT0) = A WT0p-1 + (1 - B)
$$
 (11)

Thus by comparing the recursive rule

$$
W_{\text{TO}_{k}} = W_{\text{TO}_{k-1}} - \frac{f(W_{\text{TO}_{k-1}})}{f(W_{\text{TO}_{k-1}})}
$$

$$
k = 1, 2, ... \qquad (12)
$$

based on Newton-Raphson theorem^[14] with the w idely used

$$
W_{\text{TO}_k} = W_{\text{TO}_{k-1}} - q(W_{\text{TO}_{k-1}} - W_{\text{TO}_k})
$$

$$
k = 1, 2, ... \qquad (13)
$$

 $(q \text{ is an amending factor})$, it is seen that the former could get an convergent root far more rapidly than the latter at the least cost of computation complexity, and its range of feasible W T Oguess that makes the iteration converge is also much broader than that of the latter.

If there exists a segment for delivering expendables, it could be deduced from Eqs. (2) and (3) that β _{and} is not only related to propulsion characteristics and each seg ment' s parameters, but also has complex non-linear relations with W TOguess, so Eq. (11) is untenable strictly. However, for the variation of the values of β land is not drastic during iteration, Eq. (11) can still be utilized approximately although a new value of β and must be calcu– lated by analyzing the profile again for each step of iteration. Under this condition, it is found through enlightenm ent of previous experience^[8] and test in EDRIPS that if the result from Eq. (12) is amended following Eq. (13) with q equal to 0.75 or so, t he m ost rapid convergent speed w ill be achieved. On the contrary, the iteration sequence converges more rapidly with no amendment, namely $q=1$, if

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 β _{land} is a constant.

4 Program Validat ion

Due to the difficulty of accessing the data of real aircraft, EDRIPS w as validated by testing such designs as introduced in Refs. $[7-9]$, and the ex am ple of Air-to-Air Fighter (AAF) in Ref. [9] (renamed as $AAF - v1$ in EDRIPS) is presented here.

The performance requirements and payloads of $AAF - v1$ are absolutely the same as those of AAF, and several slight m odifications are made on the mission profile, including om itting the segments of w arm -up and takeoff rotation, setting two segments instead of one to deliver the three kinds of expendables, $etc.$, but the total number of mission segm ents remains 20. Only about a single hour was used to accomplish these modifications and input all design requirements into EDRIPS. The final status of the mission profile of AAF v^1 are shown in Fig. 3 given earlier.

Fig. 4 above illustrates the initial constraint analysis for AAF_v1 in EDRIPS. The final solution space bounded by seven kinds of available constraints quite conforms to the result given in Ref. [9] and definitely contains the design point of AAF.

Because no num erical iteration is conducted in Ref. $[9]$, the 'step by step' mode was firstly chosen to contrast the results (the fps units in Ref. [9] are conversed into m ks units). The initial parameters are as follow s

$$
T \sin W \text{ to} = 1.2 \qquad W \text{ to} S = 312.48 \text{ kg/m}^2
$$

\n
$$
W \text{ to} = 11340 \text{ kg} \qquad W \text{ to} = 1205.04 \text{ kg}
$$

\n(14)

Finally, the estimated takeoff weight of $AAF = v1$ in EDRIPS equals 11776. 60kg, which is 6. 40% heavier than the value of AAF (11067. 84kg).

As viewed from methods used for analysis, the error is mostly caused by three points except for the simplification of climb path mentioned above:

(1) T he reserved fuel for mission is not con-© 1994-2010 China Academic Journal Electronic Publishing House. Open access under [CC BY-NC-ND license.](http://creativecommons.org/licenses/by-nc-nd/4.0/) http://www.cnki.net

sidered in Ref. [9], while $\mathcal{Y} = 1.06^{8}$ in EDRIPS.

(2) Π is set to be 1 for both descent and landing in Ref. $[9]$, while equals 0. 990 and 0. 995 respectively for fighter aircraft according to the statistic data^[7,8] in EDRIPS. Moreover, a descent segment of AAF was turned to a decelerated dive of AAF_v1 for more precise calculation.

(3) Only horizontal acceleration is subdivided in Ref. [9] in practice, w hile all of climb, horizontal acceleration, cruise and loiter are refined based on preset m inimum subdivision criteria in EDRIPS.

All these modifications will increase W_F and result W ^{TO}. If they are not made, the relative error between W TO of $AAF = v1$ and that of AAF will decline to 2.40% What is more, due to the fact that no uniform methods exist for preliminary sizing, nam ely, t he results in Ref. [9] should not be regarded as absolutely standard ones, EDRIPS could be deemed as reliable.

Under 'auto iteration', if the same initial param eters are used and the relative error allowance is 0.0000001 , the results got by using different typical recursive rules (T able 1) indicate that such st rategy for iteration as argued in Section 3. 3, which is also the same as adopted in EDRIPS, is highly effective.

Table 1 Results from different typical recursive rules

Formulas U sed	Total Iteration Steps	Result W_{TO} / kg
Eq. (12) and Eq. (13) $(q=0.75)$	6	14411.6529
Eq. (12)	16	14411.6527
Eq. (13) $(q=1)$	80	14411.6451
Eq. (13) $(q=0.5)$	165	14411.6447

5 Conclusions and Future Work

EDRIPS supplies a convenient and reliable tool to the design requirements input and preliminary sizing for aircraft conceptual design. It features its highly interactive and use-friendly environment on the one hand, and the improvements on analysis methods, such as the strategy for estimate takeoff weight, on the other hand, both of which improve the efficiency and quality of conceptual design.

The emphases of future work should be placed on the follow ing tw o aspect s.

 (1) Current EDRIPS is developed for the conceptual desig n of fighter aircraft, w hose design requirement s and analy sis methods are the most complex ones. Although the expandability of its architect ure has been v alidated by taking UAV into account during system design and programming, EDRIPS should be further extended to be applied to other categories of aircraft.

(2) Based on the basic design parameters of an aircraft estimated in EDRIPS, the designer could conduct design synthesis to determine its configuration and other detail parameters, and then realize t he initial iteration of conceptual design after accomplishing a series of subsequent work, including geometric modeling, geometric characteristics analysis, aerodynamic analysis, performance analysis, comparing the results with design requirements and conducting modification^[15]. Consequently, by taking such measures as researching on more convenient modeling methods, developing engine database and integrating available sophisticated analysis codes, EDRIPS should be ultim ately enhanced to be an integ rated system for CAACD and then be utilized to solve practical engineering problem s.

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