

# DESIGN OF LSDS FOR ISOTOPIC FISSILE ASSAY IN SPENT FUEL

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A future nuclear energy system is being developed at Korea Atomic Energy Research Institute (KAERI), the system involves a Sodium Fast Reactor (SFR) linked with the pyro-process. The pyro-process produces a source material to fabricate a SFR fuel rod. Therefore, an isotopic fissile content assay is very important for fuel rod safety and SFR economics. A new technology for an analysis of isotopic fissile content has been proposed using a lead slowing down spectrometer (LSDS). The new technology has several features for a fissile analysis from spent fuel: direct isotopic fissile assay, no background interference, and no requirement from burnup history information. Several calculations were done on the designed spectrometer geometry: detection sensitivity, neutron energy spectrum analysis, neutron fission characteristics, self shielding analysis, and neutron production mechanism. The spectrum was well organized even at low neutron energy and the threshold fission chamber was a proper choice to get prompt fast fission neutrons. The characteristic fission signature was obtained in slowing down neutron energy from each fissile isotope. Another application of LSDS is for an optimum design of the spent fuel storage, maximization of the burnup credit and provision of the burnup code correction factor. Additionally, an isotopic fissile content assay will contribute to an increase in transparency and credibility for the utilization of spent fuel nuclear material, as internationally demanded.

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KEYWORDS : Fissile Assay, LSDS, Fission Measurement, Fissile Utilization, Neutron Source, Resolution

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## 1. INTRODUCTION

Nuclear energy is currently the most feasible option in Korea for providing for the energy demand in a sustainable manner, even though the accident at Fukushima in Japan occurred. However, an inevitable consequence is the production of high level radioactive waste during the utilization of a nuclear power reactor. In 2009, more than 10,000 tons of spent fuels were stored in nuclear power reactor site pools in Korea. Every year, about 700 tons of spent fuels are newly produced. The amount of spent fuels will soon reach the maximum storage capacity of the pools.

Nuclear spent fuel emits intense radiation. Therefore, a direct assay of fissile materials in spent fuel has many difficulties in real application. There are several existing technologies that can be used to analyze the fissile contents in spent fuel[1]; delayed neutron counting method, curium measurement, neutron die away time method, passive multiplicity counting, neutron albedo reactivity, and x-ray fluorescence. However, most technologies do not have a direct isotopic fissile analysis for spent fuel. Some technologies still need the help of burnup codes and further development for the approval to induce the fissile content. However, LSDS has a positive feature for the direct assay of isotopic fissile content in spent fuel[2,3,4,5]. It is not

influenced by the intense radiation background (neutron and gamma rays) from spent fuel.

Generally, the spent fuel from a PWR has unburned ~1 % U235, produced ~0.5 % plutonium from the decay chain, ~3 % fission products, ~ 0.1 % minor actinides (MA), and a uranium remainder[6]. About 1.5 % of the fissile materials still exist in the spent fuel. One option to reduce the volume and radiotoxicity of PWR spent fuels and to produce energy is to use an SFR linked with the pyro-process. The pyro-process produces uranium and uranium-transuranium (TRU), mainly a plutonium, neptunium, plutonium, and americium, mixture with some fission products from PWR spent fuel. The produced nuclear material is a very self resistant feature in nuclear proliferation. A SFR fuel rod is fabricated from a uranium-TRU mixture. Therefore, an assay of fissile material content in the fuel resource material is very important for safe SFR fuel development and economical reactor operation.

The new assay technology for the isotopic fissile material contents in the pyro- process is under development at KAERI[2,3]. LSDS is the most feasible technology among the non-destructive techniques to analyze isotopic fissile material content directly. LSDS is very sensitive to distinguish fission signals from each fissile isotopes. Moreover, LSDS does not need burnup history information or burnup

code help. LSDS has several features: direct fissile assay, near real time fissile assay, no influence from radiation background, fissile isotopic assay (not gross total fissile), and is applicable to spent and recycled fuel.

Several calculations were done on the designed spectrometer geometry[7]. The detection sensitivity was examined with respect to the position and distance. The neutron energy spectrum was investigated in the neutron slowing down energy. The neutron fission characteristics were analyzed in the slowing down time with the typical pyro-process materials. A self shielding and multiplication effect was investigated in the energy region. Especially, neutron production mechanism was decided and described.

An isotopic fissile assay using LSDS is also applicable for the optimum design of spent fuel storage and maximization of burnup credit. Another important application is to verify the burnup code and provide a correction factor for improving the fissile material content, fission product content and theoretical burnup. Moreover, the advanced fissile assay technology will increase the international transparency and credibility in future nuclear energy system development. The accurate fissile content of spent fuel is very important information for efficient and economical spent fuel management as well.

## 2. LEAD SLOWING DOWN SPECTROMETER

The lead spectrometer consists of several major parts: a lead slowing down spectrometer, neutron source generation, radiation detection, and data processing and analysis. An intense neutron generator is required to obtain the direct fission signal from the fissionable materials (uranium and plutonium isotopes) and receive enough detection statistics without background interference. As a source neutron,  $\sim 10^{12}$  n's/sec was proposed using a one section electron linear accelerator with a proper target design[8,9,10]. The neutrons were produced in a Tantalum or Tungsten target material which has multiple layers with different thicknesses to maximize the bremsstrahlung radiation and neutron production. A gap between layers was considered for a target material cooling.

The principle of LSDS is very simple. A source neutron slows down continuously in a lead medium. An interrogated neutron induces energy dependent characteristic fission from isotopic fissile materials in a fuel assay area. Fortunately, an individual fissile material has its own fission characteristics below an unresolved resonance energy range. A threshold fission chamber screens the prompt fast fission neutrons of fissionable materials in a complex radiation field. The fission detector is insensitive in a gamma background. The detected signals have a direct correlation with the content of each fissile material.

### 2.1 Nuclear Material Property

The pyro-process material has a spent fuel property

even though several fission products are extracted in the process. It has intense neutron emission by spontaneous fission and ( $\alpha$ , n) reaction[6]. The major neutron emission is from curium[6]. Therefore, the intense neutron emission will be a barrier in a direct content assay of isotopic fissile material. Fig. 1 shows the neutron emission rate in the major materials by burnup. As the burnup increases, the neutron emission increases as well. Especially, the neutron by Cm244 is 100 times greater than other major neutron emitters. Therefore, curium will be accumulated more at a higher burnup.

For the pyro-process material simulation, 11wt% Pu239, 8.1wt% Pu240, and 1.69wt% Pu241 are presented. The composition of the pyro-process material for simulation is summarized in Table 1. A relatively small amount of Np237 and Am241 is also presented. The fuel assay area

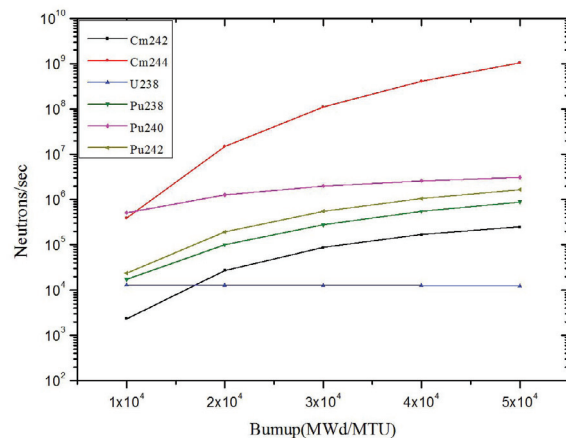


Fig. 1. Neutron Emission Rate of Different Materials by Burnup.

Table 1. Composition of Pyro-process Material for the Simulation

Nuclide	Content(wt%)
U234	0.09
U235	0.045
U236	0.036
U238	64.649
Pu238	0.74
Pu239	11
Pu240	8.1
Pu241	1.69
Pu242	1.75
Np237	0.54
Am241	1.69
Cm244	0.46
Zr90	10

is located 40cm away from the neutron source in the lead. The source neutron, having  $\sim 0.5\text{MeV}$  mean energy, slows down in the medium and induces fissile fission with respect to the slowing down energy. The fission neutron by fissile isotopes is detected at the threshold fission chamber. Fig. 2 shows the LSDS system. The neutron source is located at

the center of lead cube and the detector is above the fuel assay area.

### 2.2 Lead Spectrometer Analysis

The neutron spectrum must be well organized in the spectrometer fuel assay area from high to low energy to get the individual fissile fission signature. Therefore, in a lead spectrometer, a neutron energy spectrum was evaluated from keV to eV energy range[7]. The energy spectrum has a direct relationship with isotopic fissile fission. A narrow spectrum is preferable to discriminate isotopic nuclear fission. Fig. 3 shows the energy spectrum fitting with respect to the slowing down energy, 1keV, 100eV, 1eV, and 0.1eV. The distribution follows a Gaussian shape well. Until 1eV, the spectrum shows a good shape and resolution of  $\sim 30\%$ , however, at 0.1eV, it shows a broadened property of  $\sim 50\%$ . However, the extent of broadening is not severe. Therefore, considering the energy spectrum, 1keV to 1eV might be a good energy region.

The external neutron source slows down in a lead medium. The continuous interrogation neutron energies are obtained and the neutrons finally enter into the fuel. Prompt fast fission neutrons with respect to the fission characteristics of fissile materials(U235, Pu239 and Pu241)

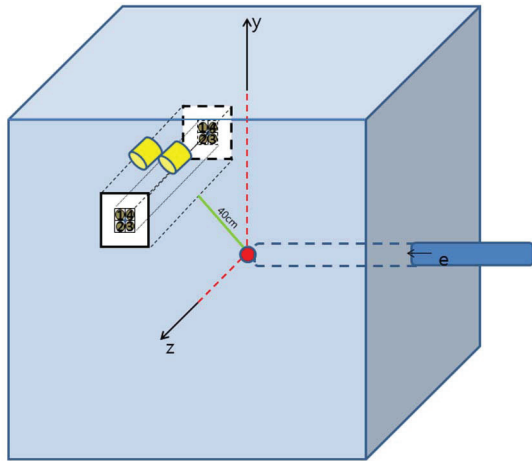


Fig. 2. Schematic View of the LSDS System.

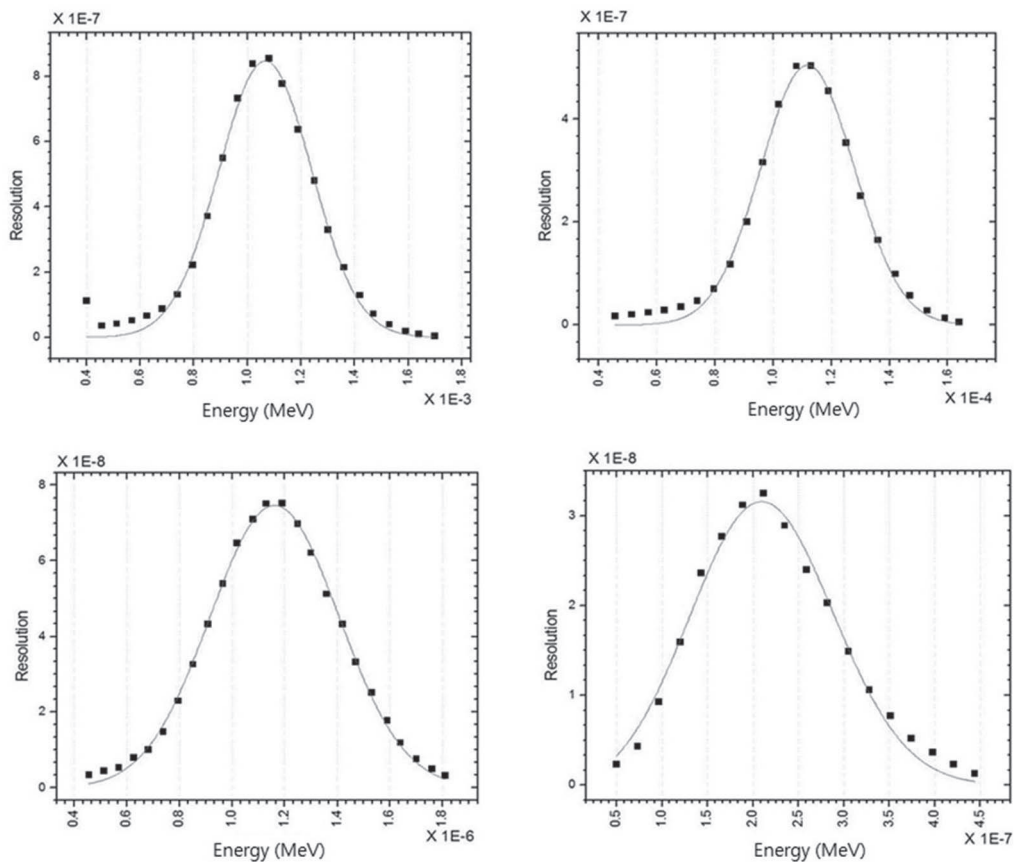


Fig. 3. Neutron Energy Spectrum of the Fuel Area(1keV, 100eV, 1eV, 0.1eV).

can be detected at the surrounding neutron detectors[7]. In the fuel area, the fission characteristics of the fissile were investigated in 2by2 fuel rods. The fissile fission in fuel is expressed as below,

$$\phi_{rod}^{fission} = \int_{t_1}^{t_2} \int_0^\infty \int_{rod} v(E)\phi(r, E, t)drdEdt, \quad (1)$$

where  $v(E)$  is the fission rate and  $\phi(E)$  is the source neutron arriving at the fuel. Fig. 4 shows the fission signature produced by each fissile material at the slowing down time. U235 has a big resonance of around 150, 250, and 400  $\mu$ sec, and 50, 130, and 600  $\mu$ sec for Pu239. Pu241 has a big resonance at 100, 170, 800  $\mu$ sec as well. After 20  $\mu$ sec, the fissile material shows its own fission property, specially, around 100  $\mu$ sec and from 500 to 600  $\mu$ sec, the fission characteristics of the isotopic fissile material are dominant. From the figure, generally, it can be seen that 20 to 600  $\mu$ sec is a good choice for a fissile assay. Therefore, LSDS is very sensitive for getting the induced fission signal from the isotopic fissile content. However, self shielding must be considered, because dominant fission has relatively large neutron absorption at the neutron energy.

A self shielding parameter was calculated at the 2by2 fuel geometry by introducing the pyro-process produced nuclear material as shown in table 1. When nuclear material is inserted into the assay area, the pyro-process recycled fuel material perturbs the spatial distribution of slowing down neutrons in lead and prompt fast fission neutrons produced by fissile materials are also perturbed. The self shielding factor is interpreted as how much of the absorption is created inside the fuel area when it is in the lead[7]. The self shielding effect provides a non-linear property in the isotopic fissile assay. When the self shielding is severe, the assay system becomes more complex and needs a special parameter to treat this non-linear effect.

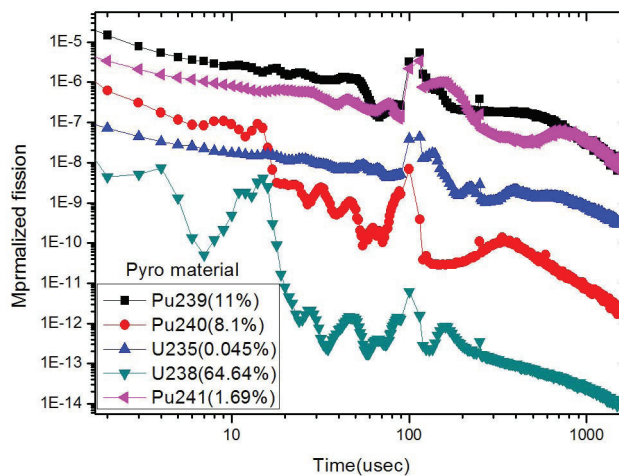
Table 2 shows the self shielding results for the pyro-process produced material. U238 is used as a base material

for fabricating SFR fuel. Therefore, the energy range in Table 2 covers the dominant absorption energy. From the results, it can be seen that the effect is relatively large at low neutron energy. In particular, at 0.3eV and 1eV, Pu239 and U235 have dominant fission characteristics. However, as the energy range becomes larger, the self shielding shows a lesser effect. In the largest energy range, the self shielding is less than 10%.

In order to understand the fission neutron contribution in the spectrometer, the multiplication effect by a fast fission neutron was investigated[7]. An induced neutron contributes to secondary fission in the fuel assembly because the pyro-process material has highly enriched plutonium isotopes with uranium. Table 3 represents the normalized fission neutrons by source neutrons at fuel rod number 1 in 2by2

**Table 2.** Self Shielding Effect with Respect to Neutron Energy for the Pyro Process Material

Energy	Self Shielding
0.1eV-1eV	1.31
0.1eV-3eV	1.19
0.6eV-8eV	1.17
5eV-30eV	1.07
40eV-100eV	1.05
3eV-300eV	1.06
20eV-600eV	1.05
3eV-1keV	1.05
0.1eV-1keV	1.05
0.1eV-10keV	1.04
0.1eV-30keV	1.04



**Fig. 4.** Neutron Fission Property of Isotopic Fissile in the Pyro-process Material.

geometry and the normalized fission neutrons at adjacent fuel rods, numbers 2 and 3, by the neutrons produced in rod number 1. From the table, it can be seen that the normalized fission neutron production at the adjacent rods by the fission

neutron in rod number 1 is very small, thousands of times less. Therefore, the multiplication effect can be neglected in 2by2 pyro assembly.

**Table 3.** Normalized Fission Neutron

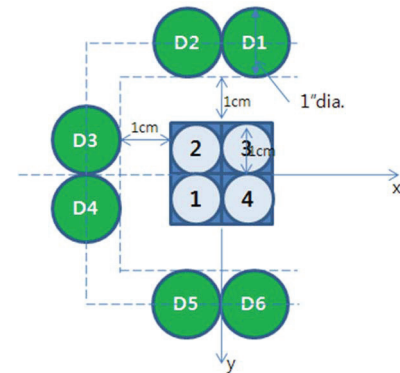
Energy (MeV)	Normalized Fission by source neutron	Normalized fission by fission neutron in fuel number 1	
	At fuel rod No. 1	At fuel rod No. 2	At fuel rod No. 3
1.0E-7	0.0	0.0	0.0
5.0E-7	5.6E-9	4.7E-9	0.0
1.0E-6	1.5E-8	2.6E-8	3.1E-8
5.0E-6	1.1E-6	1.1E-6	1.0E-6
1.0E-5	9.7E-7	1.0E-6	1.0E-6
5.0E-5	5.4E-6	6.1E-6	5.8E-6
1.0E-4	4.5E-6	4.6E-6	4.3E-6
5.0E-4	2.1E-5	2.1E-5	2.1E-5
1.0E-3	1.4E-5	1.4E-5	1.3E-5
5.0E-3	5.7E-5	5.8E-5	6.0E-5
1.0E-2	3.8E-5	4.2E-5	4.3E-5
5.0E-2	1.6E-4	2.1E-4	2.2E-4
1.0E-1	9.5E-5	1.8E-4	1.9E-4
5.0E-1	3.2E-4	9.9E-4	1.0E-3
1.0	7.6E-5	7.5E-4	8.8E-4
5.0	6.3E-5	1.9E-3	2.4E-3
10	2.5E-6	1.6E-4	2.3E-4
20	1.0E-7	6.2E-6	8.6E-6

### 2.3 Detector Sensitivity

The lead spectrometer has a very complex and intense radiation fields: from the spent fuel itself and from the neutron source generation system. Therefore, in the complex radiation field, how to collect the direct prompt fast fission neutron from fissile material is very important. Therefore, the detection sensitivity was examined at the surrounding detectors[7], as shown in Fig. 5. The fission threshold detectors are a good choice for detecting the prompt fast fission neutrons. In Fig. 5, the threshold detector is located as close as possible, 1cm away from fuel assembly surface. The detected signals are expressed as

$$\int_{S_{det}} \int_{E_1}^{E_2} \sigma_f \phi_f (r, E, t) dEdA, \tag{2}$$

where  $\sigma_f$  is the fission rate at the detector,  $\phi_f$  is the fission neutron arriving at the detector and  $S_{det}$  is the detector area. Table 4 represents the arriving neutrons at the surrounding



**Fig. 5.** Fuel Rod and Detector Geometry.

**Table 4.** Normalized Fission Neutron Arrival and Detector Response

From fuel No. 1		From fuel No. 2		From fuel No. 3	
D1	D2	D1	D2	D1	D2
2.65E-3	2.76E-3	3.01E-3	3.01E-3	2.76E-3	2.65E-3
2.32E-4	2.58E-4	3.04E-4	3.04E-4	2.54E-4	2.34E-4
D3	D4	D3	D4	D3	D4
3.00E-3	3.18E-3	3.16E-3	3.16E-3	2.62E-3	2.75E-3
3.02E-4	3.44E-4	3.46E-4	3.46E-4	2.29E-4	2.52E-4
D5	D6	D5	D6	D5	D6
3.19E-3	3.01E-3	2.74E-3	2.74E-3	2.99E-3	3.21E-3
3.48E-4	3.00E-4	2.49E-4	2.49E-4	3.02E-4	3.47E-4



detectors, and the detector threshold response. The results show the symmetrical response at the symmetrical detector position from the fuel rods. The surrounding detectors can get the fissile fission signals.

### 2.4 Neutron Source Generation

The source neutron is necessary to induce the isotopic fissile fission. Therefore, the source neutron must be intense and have good energy resolution in a wide energy range. The source neutron is produced by  $(e, \gamma)(\gamma, n)$  reaction in a multi-layer target. An electron accelerator system is selected to generate proper neutrons efficiently[8,9]. Normally, the neutron yield increases in proportion to the element mass number ( $Z$ ) with some irregularities such as nuclear deformation and the reaction threshold. The thinner target gives a good path for a high energy beam without a large loss and also provides a more positive effect to make Bremsstrahlung gamma successively. Therefore, an increasing thickness plate is a good selection for a target considering the physical phenomenon and manufacturing problems. Fig. 6 shows a scheme for accelerating electrons. The gamma energy to produce neutrons starts at around 5MeV, and the giant dipole energy for the Ta target is around 15MeV. The neutron production is shown in Fig. 7. The neutron production has a maximum 10mm target material thickness at different incident electron energies. In the figure, the produced neutron follows the evaporation spectrum and has a peak at around

1MeV. The produced neutron energy spectrum is expressed as[7]

$$N(E) = c \exp[-E/T], \tag{3}$$

where  $T$  is the photonuclear target temperature in MeV,  $E$  is the neutron energy and  $c$  is the normalization constant. The neutron is produced per  $\sim 100$  electrons at 30MeV in unit time. In order to overcome the neutron background,  $\sim 10^{12}$  n's/sec is required and an  $\sim 2$ kw beam is expected. Therefore, a high current is necessary,  $\sim 500$ mA. Fig. 8 shows the produced neutron spectrum with respect to the neutron energy. A high energy electron produces neutrons with a less broadened spectrum.

### 3. APPLICATION OF LSDS

A direct content assay of isotopic fissile materials has a good advantage in an LSDS system. The direct fissile assay is a very important key technology in the fuel cycle, similar to using PWR spent fuel for safety and economics. The LSDS is very applicable to assay isotopic fissile content in the pyro-process to fabricate an SFR fuel rod. The fissile material control must be approved for the fuel fabrication. Also, the technology is applicable to the spent fuel storage optimum design and burnup credit. Fig. 9 shows a summary

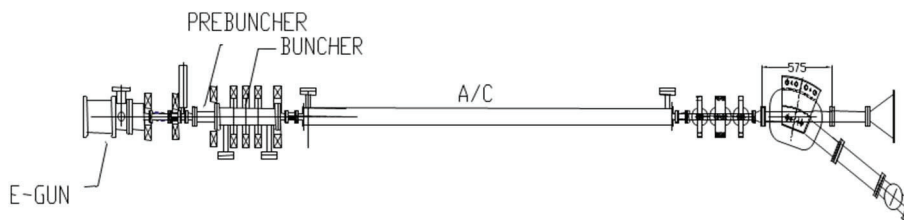


Fig. 6. Schematic View of the Electron Accelerator Column.

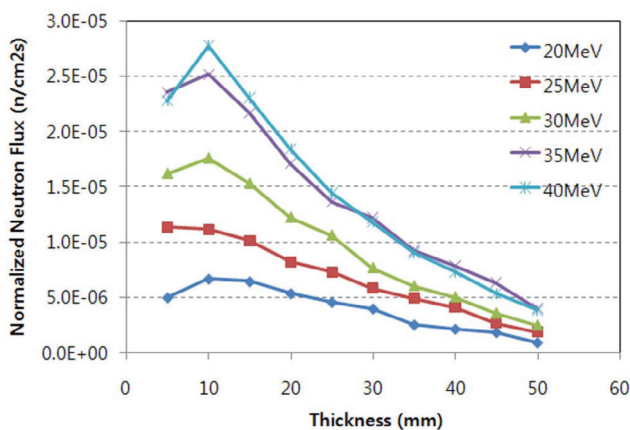


Fig. 7. Neutron Production with Different Plate Thickness.

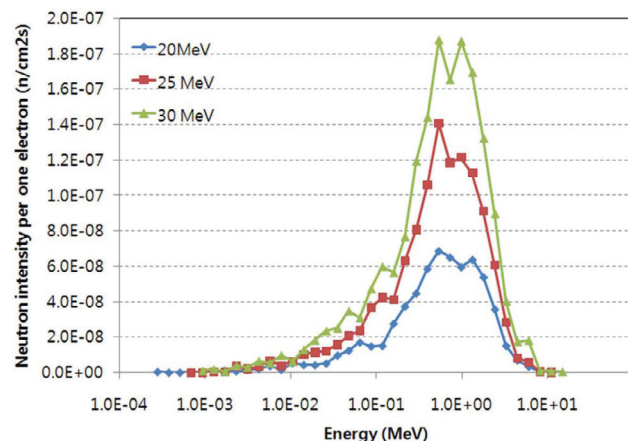


Fig. 8. Neutron Spectrum Difference with Incident Electron Energy.



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