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Mechanisms for geological carbon sequestration

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Abstract

The reduction of anthropogenic carbon dioxide (CO_2) in the atmosphere is crucial for mitigating the climate change. CO_2 capture and storage (CCS) is considered as one of the most promising options for carbon reduction. The main means is injection of CO_2 into structural reservoirs in deep, permeable geologic formations. The aim of this paper is to identify the main research needs and gaps in trapping mechanisms of geological carbon sequestration. Trapping mechanisms for geological sequestration include hydrodynamic trapping, solubility trapping, and mineral trapping. The properties of the CO_2 -water/brine system as well as the hydrodynamics, geophysics, and geochemistry of the reservoir rock/fluid system are discussed.

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1. Introduction

Climate change is one of the most significant challenges of our time. Carbon dioxide (CO₂) and other greenhouse gas emissions are believed to be the cause of the major concern. The IEA study indicates that CO₂ emissions will increase by 130% by 2050 in the absence of new policies or supply constraints as a result of increased fossil fuel usage [1]. Carbon capture and storage (CCS) is considered as one of the most promising options and the only technology available to mitigate atmospheric emissions of CO₂ from large-scale fossil fuel usage [1, 2]. Deep saline aquifers, depleted oil and gas fields, and unminable coal seams are the primary targets for the geological storage of CO₂.

In recent years, fundamental research has focused increasingly on the short and long term effects of CO₂ injection into reservoirs to assess the feasibility of CO₂ storage on a commercial scale. Sequestration processes involve different trapping mechanisms according to the hydrodynamic, physical and chemical conditions in the formation. It is common to divide these mechanisms into four different categories: hydrodynamic trapping, residual trapping, solubility trapping, and mineral trapping.

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Another major concern of all storage options is the sealing efficiency of low-permeable sequences (caprock) overlying potential storage reservoirs. It has been suggested that any technology used to geologically store CO₂ underground should store it for a minimum of 1000 years with a leakage rate of less than 0.1% per year [2–4]. The sealing capacity and long-term integrity of caprock, considering different kinds of mechanisms, is therefore an important issue for site approval and public acceptance [5]. Four different ways in which caprock can fail have been identified: diffusive loss through the caprock, leakage through pore spaces when capillary breakthrough pressure has been exceeded, leakage through faults or fractures, and well leakage when wells are degraded or inappropriately abandoned. The caprock-sealing mechanisms are recently reviewed by Song and Zhang [6], and thus not discussed in this paper.

This paper addresses the mechanisms of CO₂ trapping in the geological formations. In doing so, it both highlights key research findings and critical gaps in the current literature. For each mechanism, a brief introduction, a description of the main mechanisms or dominant factors, and its effects for storage are presented. In the end, a comprehensive conclusion as well as a summary of research gaps and needs is given.

2. Trapping mechanisms

In terms of the pore space utilization, CO₂ is preferably injected in a supercritical state (scCO₂). This is because scCO₂ is denser than gaseous CO₂ [7]. scCO₂ may undergo a phase change due to changes in pressure and/or temperature. Depending on the reservoir conditions, CO₂ can be stored as compressed gas, as liquid, or in a supercritical phase. Most of the injected CO₂ will reside in a mobile phase of CO₂, free to move laterally or migrate vertically towards the caprock. Trapping of CO₂ as residual gas occurs when formation water encroaches or invades the CO₂ plume [8]. It will also dissolve partially into the aqueous phase, leading to solubility trapping, and it can react with native minerals, resulting in mineral trapping. These trapping mechanisms are discussed in the following subsections.

2.1. Hydrodynamic trapping

Hydrodynamic trapping refers to that CO₂ is trapped as supercritical fluid or gas under a low-permeability caprock. Carbon dioxide, being less dense than the formation fluid, will rise buoyantly until it encounters a caprock that has a capillary entry pressure greater than the buoyancy or hydrodynamic force. CO₂ will accumulate in such a structural or stratigraphic feature that has both vertical and lateral seals. Trapping by such a seal is called structural or stratigraphic trapping, or hydrodynamic trapping. This mechanism is very important in that it is a prerequisite for any storage site because it prevents the leakage of CO₂ through the caprock during the time required for other trapping mechanisms to come into effect [9].

For such trapping mechanisms, the trapping efficiency is determined by the structure of the sedimentary basins, which have an intricate plumbing system defined by the location of high and low permeability strata that control the flow of fluids throughout the basin. There are numerous variations of structural and stratigraphic traps, or combinations of both structural and stratigraphic traps that can be physical traps for geological CO_2 storage. Common structural traps include anticlinal folds or sealed fault blocks (Fig. 1). CO_2 can fill to the spill point until the breakthrough pressure is exceeded.

Structural or stratigraphic traps are mostly found in reservoirs that have held oil and gas for millions of years. In these reservoirs, storage capacity mainly depends on the volume of pore space. Hydrodynamic trapping has been recognized in saline aquifers of sedimentary basins that have extremely slow flow rates. A volume of carbon dioxide injected into a deep hydrodynamic trap may take millions of years to travel by buoyancy forces up dip to reach the surface before it leaks back into the atmosphere. For this traps,

storage capacity is affected by both the volume of pore space and the reservoir permeability [11]. CO₂ sequestration by this physical trapping mechanism depends greatly on the sealing capacity of caprock, making it a big challenge for site selection [6].

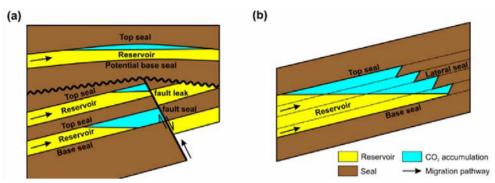


Fig. 1. Examples of (a) structural and (b) stratigraphic traps for CO₂ (modified from [10])

2.2. Residual trapping

When CO_2 is injected into the reservoir, it first displaces brine in a co-current fashion. But when the injection is stopped, due to the density difference between CO_2 and brine, the fluids flow in a counter-current fashion so that CO_2 migrates up towards and the brine flows downwards. Thus the wetting phase (brine) enters the pores by less-wetting phase (CO_2). In such a process, the brine displaces CO_2 , leading to a significant saturation of CO_2 becoming trapped in small clusters of pores, see Fig. 2. The disconnected CO_2 is then trapped as an immobile phase. This trapping mechanism is called the residual trapping or capillary trapping.

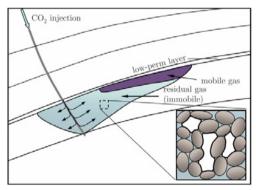


Fig. 2. Schematic of the trail of residual CO₂ that is left behind because of snap-off as the plume migrates upward during the postinjection period [12]

The capillary trapping mechanism has a huge impact on the migration and distribution of CO₂ which, in turn, affects the effectiveness of the other trapping mechanisms. This has been shown with both experiments and numerical modeling results. Suekane et al. [13] experimentally evaluated the maximum trapped CO₂ saturation for typical conditions of aquifers at a depth from 750 m to 1000 m. The trapped gas saturation is in the range from 24.8% to 28.2% for Berea sandstone core, despite the variation of CO₂ density, viscosity and interfacial tension. In addition, there are several simulation investigations

conducted to estimate the effect of capillary trapping. Two main approaches have been used in these studies of residual trapping behaviors [13]. The first isolates the effects of changes in relative permeability curves, calculating how trapped gas saturation change when the end point values such as critical gas saturation, residual gas saturation, wetting behavior, and irreducible water saturation are varied [12, 14–16]. Among these results, it is found that the residual trapping can limit significantly the movement of injected CO_2 , resulting in a significant fraction of CO_2 trapping using a hysteresis model. They concluded that the effect of residual gas on CO_2 storage can be very large. The second approach makes use of various ratios of vertical to horizontal permeability (k_v/k_h) , injection rates, formation pressure and temperature for a given set of relative permeability curves [17–19]. They found that the injection rate, heterogeneity, and the ratio of viscous to gravity force have the most significant impacts on the final immobilized saturation. Increasing the viscous to gravity force ratio and increasing the heterogeneity will enhance the sweeping efficiency, resulting in more CO_2 trapping as residual gas.

2.3. Solubility trapping

Solubility trapping refer to dissolution of CO₂ in formation fluid. CO₂ would migrate upwards to the interface between reservoir and caprock after injection and then spread laterally under caprock as a separate phase. When CO₂ contacts with the ambient formation brine and hydrocarbon, mass transfer occurs with CO₂ dissolving into the brine until an equilibrium state is reached. The solubility of CO₂ in water is dependent on the salinity, pressure and temperature of the formation water [20]. At the interface of free gas phase and formation water, CO₂ dissolves into water by molecular diffusion. The water in contact with CO₂ will be saturated with CO₂ and a concentration gradient of CO₂ would establish spatially. This process is very slow because the molecular diffusion coefficient is very small. It will take thousands of years for CO₂ to be completely dissolved in brine [21].

When diffusive CO₂ dissolves in brine, it slightly increases the brine density. The dissolution would increase the density of brine up to approximately 1% compared with the original formation brine [14, 22]. The heavier brine on the top of aquifer would flow downward due to gravity. Such convection enhances the mixing of CO₂ and brine and stimulates the diffusion process, following more dissolution of CO₂. The dissolution reduces CO₂ upward mitigation as well as increases the storage capacity. The crucial problem about the dissolution-diffusion-convection (DDC) process is the time and length scales of the onset of convection. Some approaches have been used for studying the onset of CO₂ convection in reservoir: amplification theory [23], global stability (energy) method [24], linear stability analysis [24, 25], and non-modal stability theory [26].

Modeling studies reveal that the DDC process can help to increase storage capacity in reservoir [27, 28]. Laboratory studies have been conducted that confirmed qualitative and quantitative aspects of it [29, 30]. Furthermore, as DDC process makes more CO_2 dissolve in brine, it is reasonable to expect that DDC may reduce the migration of CO_2 through caprock. It may be significant in storage capacity estimation and caprock sealing analysis.

2.4. Mineral trapping

Mineral trapping refers to the incorporation of CO₂ in a stable mineral phase via reactions with mineral and organic matter in the formation. Over time the injected CO₂ will dissolve into the local formation water and initiate a variety of geochemical reactions. Some of these reactions could be beneficial, helping to chemically contain or "trap" the CO₂ as dissolved species and by the formation of new carbonate minerals; others may be deleterious, and can actually aid in the migration of CO₂. It is important to understand the overall impact of these competing processes. However, these processes will also be dependent upon the structure, mineralogy and hydrogeology of the specific lithologies concerned [31].

Espinoza et al. [32] summarized representative chemical reactions and typical reaction rates in the literature, see Table 1.

Mineral	Typical reaction	Reaction rate (mol·m ⁻² s ⁻¹)
	$SiO_{2(s)}+2H_2O \leftrightarrow H_4SiO_4$	
Silicates [33]	\leftrightarrow H ⁺ +H ₃ SiO ₄	$1.26 \times 10^{-14} [36]$
	\leftrightarrow H ⁺ +H ₂ SiO ₄ ²⁻	
Aluminosilicates [34]	Anorthite:	Anorthite: 1.2×10^{-5}
	$CaAl_2Si_2O_{8(s)}+8H^+ \leftrightarrow Ca^{2+}+2Al^{3+}+2H_4SiO_4$	Oligiocalse: 1.2×10^{-8}
	Kaolinite:	Albite: 3.6×10^{-9}
	$Al_{2}Si_{2}O_{5}(OH)_{4(s)}+6H^{^{+}}\!\leftrightarrow\!2Al^{3+}\!+\!2H_{4}SiO_{4}\!+\!H_{2}O$	Kaolinite: 10 ⁻¹⁴ –10 ⁻¹⁵ [37]
Carbonates [35]	$CaCO3(s)+H+ \leftrightarrow Ca2++HCO3-$ $CaCO3(s)+CO2+H2O \leftrightarrow Ca2++2HCO3-$	Calcite: $1.6-3.2 \times 10^{-5}$ [38]

Table 1. Mineral reactions with CO2-acidified water

The reaction rate of minerals in CO₂-water depends on temperature, pressure, pH, and concentration of other species. Besides the aqueous reaction, water-wet scCO2 and dry scCO2 reactions may occur when a large amount of dry scCO2 flows through the reservoir. In this case, gradual displacement and dissolution of residual pore water occur and the rock comes into direct contact with dry scCO₂. Initial studies on dry scCO₂ or wet scCO₂ reactions have been conducted [39, 40]. The mineral dissolution is a very slow process as the reaction rates are usually very low and mineral trapping would only become significant at a geological time scale.

2.5. Summary

2.5.1. Relevant terminology

There are different relevant terminologies associated with CO₂ sequestration mechanisms. Definition for each one may be a little different in different literature, see Table 2.

Table 2. Mainly relevant terminology definition in the literature

Terms	Definition and references	
Static trapping	Mobile CO ₂ is trapped in stratigraphic and structural traps, or in man-made caverns [41].	
Structural trapping	Structural traps refer to geological media which precludes the upward and lateral movement of CO_2 induced by crust movement (faults and folds) [41].	
Stratigraphic trapping	Stratigraphic traps refer to geological media which precludes the upward and lateral movement of CO ₂ induced by depositional and/or diagenetic processes [41].	
Hydrodynamic trapping	 (1) The buoyant CO₂ is kept underground by an impermeable caprock [9]. (2) The injected CO₂ is primarily trapped as a gas or supercritical fluid. CO₂ will rise up due to buoyancy effect until it approaches the seals [42]. 	
Capillary trapping	 (1) It means the trapping by capillary forces in the pores on the trailing edge of the mobile CO₂ plume (typically) [43]. (2) CO₂ phase is disconnected into an immobile (trapped) fraction (or called residual trapping) [12]. 	

Residual trapping	(1) CO ₂ can be stored as an immobile form in deep saline aquifers due to the petrophysical property of
residual aupping	flow phases. CO ₂ will be left behind as trapped (residual) saturation [14].
	(2) CO ₂ is trapped in the pore space at irreducible gas saturation in which case CO ₂ is immobile
	because of the interfacial tension between CO ₂ and formation water [41].
	(3) It means the trapping by capillary forces in the pores on the trailing edge of the mobile CO ₂ plume (less commonly) [43].
	(4) Residual trapping happens when water is imbibed behind the migrating CO ₂ plume, and is caused by gas-water relative permeability hysteresis [44].
	(5) Formation of disconnected blobs of CO ₂ phase is held by capillary forces [45]
Solubility trapping	(1) CO ₂ dissolves in water and/or oil [42].
(dissolution trapping)	(2) CO ₂ dissolves in formation water, residual oil, or mixing with residual gas [43].
	(3) CO ₂ dissolves in hydrocarbons or water contained in subsurface formations [44].
	(4) CO ₂ dissolves in brine as aqueous species [45].
Mineral trapping	(1) CO_2 reacts with minerals and organic matters in the geologic formations to become a portion of the solid matrix [42].
	(2) CO ₂ is trapped by precipitation of carbonate-bearing mineral phases, such as calcite, magnesite, siderite, and dawsonite [43].
	(3) CO ₂ is trapped by the mineralization process of mineral dissolution and precipitation [44].
	(4) CO ₂ is trapped by precipitation of dissolved carbonate anions and metal cations as solids [45].
Physical trapping	(1) CO_2 is immobilized as a free gas or supercritical fluid and a process depends on the available storage volume [41].
	(2) Physical trapping (structural and stratigraphic trapping) refers to the buoyant phase trapped below a seal or within a structure that has vertical and lateral permeability barriers [43].
Chemical trapping	CO ₂ adsorbs onto organic materials contained on coals and shales, or dissolves in subsurface fluids (solubility and ionic trapping) [41].

2.5.2. Time scale

The timescales associated with each of the sequestration mechanisms are very different [46]. Hydrodynamic trapping occurs during the injection and would be a perquisite for other trapping mechanisms. For this trapping mechanism, the caprock integrity and high capillary pressure are the key factors. During and after a short term of injection, capillary trapping occurs when the displacement happens. In short to mid-term, CO₂ dissolves in brine and the solubility trapping occurs. In geological time, CO₂ would be trapped by mineralization. The timescales for the four trapping mechanisms are as follows:

$$t_{\rm hydro} < t_{\rm capi} \ll t_{\rm solu} \ll t_{\rm reac}$$
 .

2.5.3. Spatial scale

 CO_2 plume distribution changes with time when different trapping mechanisms dominate. During the hydrodynamic trapping, CO_2 accumulates under the low permeability seal and migrates laterally along it. Capillary trapping occurs all along the flow pathway, especially when the pathway has a very small pore or throat. Solubility trapping can be found at the interface of gas phase and brine along the flow pathway and under the caprock. Mineral trapping changes with the mineral distribution. The identification of dominating trapping mechanisms and CO_2 plume distribution at different time is of great importance for both the storage capacity estimation and the risk assessment.

3. Research gaps and research needs

Hydrodynamic trapping, capillary trapping, solubility trapping, and mineral trapping are four main trapping mechanisms of geologic CO₂ sequestration. Some studies have been done to investigate these mechanisms. But there are still some relevant topics that should be further investigated:

The capillary pressure of caprock and the week point of the seal should be well investigated as it decides directly the injection pressure and then the storage capacity of hydrodynamic trapping.

The relationship between geochemical reactions and their impact on porosity and permeability should be investigated in the context of CO₂ storage.

Capillary pressure curves and relative permeability curves should be obtained by CO₂ flow experiments whereas such curves were usually transferred from Hg-porosimetry or hydrocarbon systems.

Experimental methods need to be developed for imaging rocks for reconstructing three dimensional geometrics, with which flow, mineral reactions, and transport in such rocks can be studied.

Continuous effort should be invested in determining adequate kinetic rates under storage relevant conditions and characterizing reactive surface areas as well as in developing methods on how to upscale laboratory results.

A procedure has to be developed or improved to measure saturation and pH in rocks under in-situ conditions in percolation experiments.

Efforts should be made to develop adequate equations of state and solubility models when other gaseous compounds are included.

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