

Available online at www.sciencedirect.com



Procedia Engineering 31 (2012) 934 - 940

Procedia Engineering

www.elsevier.com/locate/procedia

# International Conference on Advances in Computational Modeling and Simulation

# Different Oxygen Levels of Dimethyl Ether Combustion Influence Numerical Simulation

Rong Chen<sup>a,b</sup>, Hui-tao Wang<sup>a,b\*</sup>, Hua Wang<sup>a,b</sup>

<sup>a</sup>Engineering Research Center of Metallurgical Energy Conservation and Emission Reduction, Ministry of Education, Kunming University of Science and Technology, YunnanKunming, 650093, China;

<sup>b</sup>State Key Laboratory Breeding Base of Complex Nonferrous Metal Resources Cleaning Utilization in Yunnan Province, Kunming 650093,

China.

#### Abstract

Aiming at the dimethyl ether itself with oxygen, this paper simulate that how much less oxygen quantity Dimethyl ether combustion required than liquefied petroleum gas in the same fuel quantity, and obtain optimum normoxia of dimethyl ether desired. This paper simulated dimethyl ether, liquefied petroleum gas (LPG) combustion with the air for 10%, 20%, 30%, 40%, 50%, 90% Oxygen levels. Under the different oxygen levels ,the study found that the best oxygen levels dimethyl ether combustion needed is around 30%, and the best oxygen levels liquefied petroleum gas (LPG) combustion needed is around 50%, so that Oxygen levels dimethyl ether needed is less than liquefied petroleum gas (LPG) needed in the same amount of fuel.

© 2011 Published by Elsevier Ltd. Selection and/or peer-review under responsibility of Kunming University of Science and Technology Open access under CC BY-NC-ND license.

Key words: Dimethyl ether combustion; Energy conservation and emission reduction; air normoxia; Numerical Simulation.

#### 1. Introduction

Dimethyl ether gradually replace Liquefied petroleum gas (LPG) in most of the ceramic kiln plant at present, and more and more be replaced, the main reason is the dimethyl ether own oxygen, good combustion performance, high thermal efficiency, no residue, no black smoke in the process of burning, low carbon monoxide and nitric oxide emissions, it is a kind of clean fuel [1-4]. Under the same heat condition, dimethyl ether combustion efficiency is increased 5% with natural gas, liquefied petroleum gas, and other gas phase comparison, such as shown in table 1. With liquefied petroleum gas (LPG) compared, dimethyl ether need less air, and this can avoid polluting air into influence the quality of ceramic fire, so product has good gloss with the dimethyl ether burning. Therefore, dimethyl ether instead of other fuel will become a mature technology in the near future.CH<sub>3</sub>-O-CH<sub>3</sub>

Table 1 the contrast of chemical and physical properties of Dimethyl ether and other alternative fuel contrast <sup>[5-7]</sup>

	Material	DME	Methanol	Ethanol	CNG	LPG
-	Chemical formula	CH3-O-CH3	CH3-OH	CH3- CH2OH	CH4	C3H8

\* Corresponding author. Tel.: +86-15687126075; fax: +86-0871-5153405.

*E-mail address*: energywhti@sina.com.

Low calorific value (MJ/kg)	28.43	19.5	26.8	50.0	46.5
Liquid density (g/ml)	0.668	0.79	0.784	0.43	0.51
Boiling point (°C)	-25	65	78	-162	-42
Ignition temperature ( $^\circ \mathbb{C}$ )	235	450	420	650	507
Theory air-fuel ratio (kg/kg)	9.0	6.5	9.0	17.2	15.7
Gasification latent heat	410	1110	904	-	426
Carbon content (%)	52.2	37.5	52.2	75.0	81.8
Hydrogen content (%)	13.0	12.5	13.0	25.0	18.1
Oxygen content (%)	34.8	50.0	34.8	0	0

#### 2. Turbulent combustion model

1. Control equation:

Continuity equation:

$$\frac{\partial \rho}{\partial t} + \frac{\partial (\rho u_x)}{\partial x} + \frac{\partial (\rho u_y)}{\partial y} + \frac{\partial (\rho u_z)}{\partial z} = 0$$
(1)

Momentum equations:

$$\frac{\partial(\rho u_x)}{\partial t} + \nabla \cdot \left(\rho u_x \vec{u}\right) = -\frac{\partial p}{\partial x} + \nabla \cdot \left(\mu gradu_x\right) + S_{u_x}$$
(2)

$$\frac{\partial(\rho u_y)}{\partial t} + \nabla \cdot \left(\rho u_y \vec{u}\right) = -\frac{\partial p}{\partial y} + \nabla \cdot \left(\mu gradu_y\right) + S_{u_y} \tag{3}$$

$$\frac{\partial(\rho u_z)}{\partial t} + \nabla \cdot \left(\rho u_z \vec{u}\right) = -\frac{\partial p}{\partial z} + \nabla \cdot \left(\mu gradu_z\right) + S_{u_z} \tag{4}$$

Where  $s_{u_x}$ ,  $s_{u_y}$ ,  $s_{u_z}$  is generalized source term, and  $s_{u_x} = \rho f_x + s_x$ ,  $s_{u_y} = \rho f_y + s_y$ ,  $s_{u_z} = \rho f_z + s_z$ Energy equation:

$$\frac{\partial(\rho E)}{\partial t} + \nabla \left[ \vec{u} (\rho E + p) \right] = \nabla \left[ k_{eff} \nabla T - \sum_{j} h_{j} J_{j} + \left( \tau_{eff} \cdot \vec{u} \right) \right] + S_{h}$$
(5)

Where E is total energy of micro group and contains the internal energy, energy and potential energy, namely  $\frac{\partial (\rho u_x)}{\partial t} + \nabla \cdot (\rho u_x \vec{u}) = -\frac{\partial p}{\partial x} + \nabla \cdot (\mu gradu_x) + S_{u_x}, \text{ h is effective heat enthalpy}(J/kg), h_j \text{ is enthalpy of components j, namely}$   $h_j = \prod_{\substack{ref}{T_{ref}}}^{T} C_{p,j} dT, \text{ them } T_{ref} = 298.15K; k_{eff} \text{ is effective heat conduction coefficient (W / (m K)), namely } k_{eff} = k + k_t, k_t \text{ is the}$ 

turbulence heat conduction coefficient ,according to the turbulence model used to determine;  $J_j$  is the diffusion fluxes of components j;  $s_h$  contains chemical reaction heat and other volumetric heat source user defined <sup>[8]</sup>.

#### 2. Turbulence model:

Standard k-model transport equations:

$$\frac{\partial(\rho k)}{\partial t} + \frac{\partial(\rho k u_i)}{\partial x_i} = \frac{\partial}{\partial x_j} \left[ \left( \mu + \frac{\mu_t}{\sigma_k} \right) \frac{\partial k}{\partial x_j} \right] + G_k + G_b - \rho \varepsilon - Y_M + S_k$$
(6)

$$\frac{\partial(\rho\varepsilon)}{\partial t} + \frac{\partial(\rho\varepsilon u_i)}{\partial x_i} = \frac{\partial}{\partial x_j} \left[ \left( \mu + \frac{\mu_t}{\sigma_{\varepsilon}} \right) \frac{\partial\varepsilon}{\partial x_j} \right] + C_{1\varepsilon} \frac{\varepsilon}{k} (G_k + C_{3\varepsilon} G_b) - C_{2\varepsilon} \rho \frac{\varepsilon^2}{k} + S_{\varepsilon}$$
(7)

Where  $G_k$  is the turbulence because average speed gradient produce;  $G_b$  is the turbulence because the influence of

buoyancy produce;  $r_M$  is the influence of total dissipation rate because of compressed turbulent pulse inflation; And  $c_{1\varepsilon} \,\, \, c_{2\varepsilon} \,\, c_{3\varepsilon}$  is experienced constant and a default value in FLUENT ,namely  $c_{1\varepsilon}=1.44 \,\, c_{2\varepsilon}=1.92 \,\, c_{3\varepsilon}=0.09$ ;  $\sigma_k \,\, \sigma_{\varepsilon}$  is perlong number corresponding turbulent kinetic energy and dissipation rate and a default value in FLUENT, namely  $\sigma_k=1.0 \,\, \sigma_{\varepsilon}=1.3$ ;  $Pr_t$  is turbulent kinetic perlong number, namely the default value is  $Pr_t=0.85$ ;  $g_t$  is gravity acceleration component in the *i* direction;  $\beta$  is thermal expansion coefficient;  $M_t$  is Mach number of turbulent kinetic; *a* is sound velocity <sup>[9-11]</sup>.

### 3. The simplification of geometric model and the decision of boundary condition

This paper simulation spindle ceramic kiln, as shown in figure 1, this simplified model is Shown below : ① Geometric structure construction under the foundation of the actual shuttle type furnace; ②There are no gap among the spake、 kiln wall and kiln car (kiln bottom), namely without any cold air into the furnace influencing combustion in the firing process; ③ Burner is the round entry with air and fuel concentric jet ;④ Uniform layered materials is simplified to the uniform distribution cylinder in furnace  $^{[12-13]}$ , as in figure 2 shown.





Figure 2 geometric model of spindle ceramic kiln

In the simulation process, fuel and the air turbulence intensity is significant at the entrance, so fuel by discrete phase is injected into the chamber in a fixed position, and the air by continuous phase is injected into the chamber in the burner entrance .Determine the fuel and air entry conditions, create PDF form, set the burning chemical components and fuel and air temperature, use velocity entrance boundary conditions for the entry boundary conditions <sup>[14-15]</sup>.Kiln wall, kiln crown, the kiln and materials form were used the different two types of wall; The discrete areas of grid are fluid. According to the actual calculation and field measurement, we concluded that the inlet velocity of fuel is 47.73 m/s, hydraulic diameter is 0.03 m/s; The inlet velocity of flame retardant air is100 m/s, hydraulic diameter is 0.02 m/s; The environmental temperature is 300 K, the outlet pressure is 5 Pa, the outlet hydraulic equivalent diameter is0.16 m/s; And it suppose that the material of the Kiln bottom (the kiln car), kiln wall and spake is fireclay brick, the whole simulation process ignore absorption and heat release effect from porcelain body and glaze materials of physical chemical reaction, only includes the heat transfer process of the burning of fossil fuels, kiln wall, porcelain body itself and smoke <sup>[16]</sup>, so its whole combustion process is assumed to the adiabatic combustion process.

#### 4. Dimethyl ether, liquefied petroleum gas and the different oxygen levels air Combustion

Because of the dimethyl ether itself with oxygen, through the comparison and analysis of the situation of the same volume of dimethyl ether and liquefied petroleum gas (LPG) combustion in the different oxygen levels air condition, mainly from combustion temperature, oxygen quantity and other combustion performance, it is realize the technical improvement of the dimethyl ether alternative liquefied petroleum gas (LPG).

#### 4.1 Dimethyl ether Combustion in the different oxygen levels air

It simulated the change rule of dimethyl ether combustion with the different oxygen levels air for 10%, 20%, 30%, 40%, 90%by using fluent software, the simulation results as in figure 3 to figure 7 shown. we can see when oxygen levels is 10% and 20% the average temperature of the insulation combustion is very low respectively for 1150 K and 2100 K, but it is in growth trend ; And when oxygen level is 30%, the average temperature of the insulation combustion continues to increase to 2750 K; When oxygen levels increases to 40%, the average temperature of the insulation combustion is about 2750 K as the same as oxygen levels is 30%; It is find that the average combustion temperature in whole chamber is no increase trend when we continue to increase the oxygen levels to 90%, but it drops a little, and uniformity degree of combustion temperature distribution in the whole furnace is increases, this is because the rest of the oxygen levels is 10% and 20%, in addition to vents and exit, other parts of the furnace are no oxygen; When oxygen levels increases to 30%, 40%, 90%, the average Oxygen quality score of the furnace is 5%, 15%, 60% respectively after the completion of the combustion, so the rest of the oxygen is more and more.



From the above we can conclude that when the oxygen levels is 10% and 20%, combustion temperature is low in the whole furnace, this is because oxygen quantity is insufficient and others haven't enough time to burn in the furnace and is expelled, if Only the oxygen levels increase constantly, combustion temperature will increase; When oxygen levels increase to more than 30%, the combustion temperature will no longer increase, but will decrease, thus we can conclude that the best of oxygen levels is about 30% what dimethyl ether combustion need.



From figure 3 to figure 7, we can conclude that the combustion temperature is highest when oxygen levels is 30%, and residual oxygen is the least, this is the best oxygen levels dimethyl ether combustion needed. However through

detailed calculation, the best oxygen level is 27% the fuel needed. SO it simulated the change rule of dimethyl ether combustion with air of the oxygen levels for 27%, by using fluent software, as in figure 8 shown. From the figure 9, we can see that this compared with oxygen levels for 30%, its average combustion temperature is in 2750 K, and its temperature distribution is more uniform than oxygen levels for 30% in the furnace, remaining oxygen quantity is almost the same as oxygen content for 30%. Therefore we find that oxygen level what the dimethyl ether combustion need is less than 30% slightly.

#### 4.2 Liquefied petroleum gas (LPG) Combustion in the different oxygen levels air

Most of the ceramic kiln plant still use liquefied natural gas (LPG) as fuel at present, mainly due to its high calorific value, no smoke, no carbon residue, convenient operation, etc. we can see its main composition is  $C_3H_8$  whose volume fraction is 90.7% from table 2, and it itself no own oxygen elements. The combustion process of liquefied petroleum gas (LPG) compared with dimethyl ether, dimethyl ether need the amount of oxygen more than liquefied petroleum gas when combustion effect is the best.

Table 2 liquefied gas components						
$C_3H_8$	$C_3H_6$	$C_{4}H_{10}$	$C_4H_8$	$C_{5}H_{12}$	Other	
90.7	3.5	3.8	0.1	0.5	1.4	

It simulated the change rule of liquefied petroleum gas (LPG) combustion with the different oxygen levels air for 30%, 40%, 50%, 60%, 90% by using fluent software, the simulation results as in figure 9 to figure 13 shown. we can see when oxygen levels is 30% and 40% the average temperature of the insulation combustion is very low respectively for 2750 K and 3600 K, but it is in growth trend; And when oxygen level is 50%, the average temperature of the insulation combustion continues to increase to 3800 K; When oxygen levels increases to 60%, the average temperature of the insulation combustion is about 3800 K as the same as oxygen levels is 50%; It is find that the average combustion temperature in whole chamber is no increase trend when we continue to increase the oxygen levels to 90%, but it drops a little, and uniformity degree of combustion temperature distribution in the whole furnace is increases, this is because the rest of the oxygen levels is 30% and 40%, in addition to vents and exit, other parts of the furnace are no oxygen; When oxygen levels is 50%, 60%, 90%, the average Oxygen quality score of the furnace is 5%, 10%, 60% respectively after the completion of the combustion, so the rest of the oxygen is more and more.



From the above we can conclude that when the oxygen levels is 30% and 40%, combustion temperature is low in the whole furnace, this is because oxygen quantity is insufficient and others haven't enough time to burn in the furnace and is expelled, if Only the oxygen levels increase constantly, combustion temperature will increase; When oxygen levels increase to more than 50%, the combustion temperature will no longer increase, but will decrease, thus we can conclude that the best of oxygen levels is about 50% what liquefied petroleum gas combustion need.

From figure 9 to figure 13, we can conclude that the combustion temperature is highest when oxygen levels is 50%, and residual oxygen is the least, this is the best oxygen levels liquefied petroleum gas combustion needed. However through detailed calculation, the best oxygen level is 45% the fuel needed. SO it simulated the change rule of liquefied petroleum gas combustion with air of the oxygen levels for 45%, by using fluent software, as in figure 14 shown. From the figure 14, we can see that this compared with oxygen levels for 50%, its average combustion temperature is in 3750 K, and its temperature distribution is more uniform than oxygen levels for 50% in the furnace, remaining oxygen quantity is almost the same as oxygen content for 30%. Therefore we find that oxygen level what the liquefied petroleum gas r combustion need is less than 50% slightly.

## 5. Conclusion

1. In the same oxygen levels, the burning temperature of dimethyl ether is less than the liquefied petroleum gas, as in table 3 shown. And compare the situation of the dimethyl ether and the best oxygen levels air combustion with liquefied petroleum gas, the liquefied petroleum gas (LPG) combustion temperature is higher than dimethyl ether, this is because calorific value of dimethyl ether is lower than natural gas, liquefied petroleum gas, and other gas , so the theory combustion temperature is lower than other gas. But from the economic point to see, the prices of dimethyl ether is lower than other fuel gas and can reduced by 5% when the combustion efficiency of dimethyl ether is the same as liquefied petroleum gas. It is a kind of clean fuel, no residual, no black smoke, low carbon monoxide and nitric oxide emissions, and porcelain products which use it have better gloss and higher quality.

Table 3 the adiabatic combustion temperature of Dimethyl ether, liquefied petroleum gas (LPG) with different

		02	cygen ievers				
Project	Н	Highest temperature		Ave	Average temperature		
Tiojeet	30%	40%	50%	30%	40%	50%	
DME	3102.72	3240.79	3229.96	2729.03	2652.63	2643.97	
LPG	3191.14	3918.56	4265.61	2805.65	3750.32	3699.1	

2. Compare with liquefied petroleum gas (LPG), we find that oxygen level what the dimethyl ether combustion need is less than 30% slightly, but the liquefied petroleum gas combustion need is less than 50% slightly, so amount of oxygen levels dimethyl ether needed is less than liquefied petroleum gas, and the entrance of the air can be done a bit small

#### Acknowledgments

The study presented in this paper is financially supported by National Natural Science Foundation Programs of China (Grant Nos. 51066002, U0937604), Yunnan Provincial Natural Science Foundation Programs (Grant Nos. 2008KA002, 2008CD001), and high-tech development project by the Development and Reform Commission of Yunnan province (Grant Nos 2008CD001).

#### References

[1] Mitsuru Konno, Zhili Chen, Kentaro Miki. Computatinal and Experimental Study on the influence of formaldehyde on HCCI Combustion Fueled with Dimethyl Ether. 2003 JSAE/SAE international Spring Fuels & Lubricants Meeting YoKohama, Japan May 19-22, 2003

[2]Jun Song,Zhen Huang,Xinqi Qiao,et.al.Performance of a controllable premixed combustion engine fueled with dimethyl ether.Energy Conversion and Management 45(2004)2223-2232

[3]Hiroyuki Yamada, Masataka Yoshii, Atsumu Tezaki. Chemical mechanistic analysis of additive effects in homogeneous charge compression ignition of dimethyl ether. Proceeding of the Combution institute 30(2005)2773-2780

[4] D Cipolat.Analysis of energy release and NOx emission of a CI engine fuelled on diesel and DME.Applied Thermal Engineering 27(2007)2095-2013

[5]Myung Yoon Kim, Seung Hyun Yoon, et al. Combustion and emission characteristics of DME as an alternative fuel for compression ignition engines with a high pressure injection system. Fule 87(2008)2779-2786

[6]Chen Zhili.Experimental Study of CI Natural-Gas/DME Homogeneous Charge Engine.SAE Paper,2000-01-0329

[7]Norimasa Lida, Tetsuya Igarashi. Auto-ignition and Combusition of Butane and DME/Air Mixtures in a Homogeneous Charge Compression Ignition Engine. SAE Paper, 2000-01-1832

[8] Ma Xiao-qian, Cheng Bo-hang. Analysis on the fuel and combustion characters of urban waste [J]. New Energy Sources, 1998, 20(6): 19-24.

[9] Ma Xiao-qian, Cheng Bo-hang. Analysis on the fuel and combustion characters of urban waste [J]. New Energy Sources, 1998, 20(6): 19-24.

[10] Ma Xian-qian, Lu Wei, Shen Wen-sheng. Analysis and calculate on optimization conditions of process for gas phase combustion in incinerator[J]. Shanghai Environm-

ental Science, 1999. 18(3): 135-138.

[11] Yang Y B,Yamauchi H,Nasserzadeh V,et a1.Effects of fuel devolatilisation on the combustion of wood chips and incineration of simulated municipal solid wastes in a packed bed[J].Fuel,2003,82:2205-2221

[12]Breuer.k, Han G,Bird J.C.,et a1,Infared diagnostics for measuring fluid and solid motion inside silicon microdevices, Microscale Thermophysical Engineering,8(2):169-182

[13] Fluent Inc.Fluent 6.1 User, s Guide and Gambit 2.0 User, s Guide, 2001

[14]Ma Xian-qian, Lu Wei, Shen Wen-sheng. Analysis and calculate on optimization conditions of process for gas phase combustion in incinerator[J].Shanghai Environmental Science, 1999. 18(3): 135-138.

[15] Mastorakos E, Massias A, Tsakiroglou C D, et al. CFD Predictions for cement kilns including flame modeling, heat transfer and clinker chemistry[J]. Appl Math Modeling, 1999, 23(7):55-76

[16] Yang Y B,Yamauchi H,Nasserzadeh V,et a1.Effects of fuel devolatilisation on the combustion of wood chips and incineration of simulated municipal solid wastes in a packed bed[J].Fuel,2003,82:2205-2221