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Full Length Article

Application of grey fuzzy logic for the optimization of CNC milling parameters for Al–4.5%Cu–TiC MMCs with multi-performance characteristics



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ABSTRACT

With the major application of MMCs, it is thus necessary to develop an appropriate technology for their efficient machining. Milling is the most common and versatile technology among different machining processes, characterized by an extensive range of metal cutting capacity that places it in a central role in the manufacturing industries. In the present study an attempt has been made to find out the most optimal level of process parameters for CNC milling of Al–4.5%Cu–TiC metal matrix composites using grey-fuzzy algorithm. Taguchi's L_{25} orthogonal array design is used for performing CNC milling operation on the composite plates. The Grey fuzzy optimization of CNC milling parameters consist of three different output characteristics; such as, cutting force Fc, surface roughness Ra and surface roughness Rz. It was found that a cutting speed of 600 rpm, feed of 40 mm/min and a depth of cut of 0.30 mm is the optimal combination of CNC milling parameters that has produced a high value of grey fuzzy reasoning grade of 0.8191 which is close to the reference value. ANOVA analysis is carried out and it is found that among three different process parameters, the cutting speed played a major role on the determination of GFRG.

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1. Introduction

Nowadays metal matrix composites are being used in many applications in different engineering fields, which are very significant in the recent progress in material science and hence it is acting as a substitute for several engineering materials. Particularly aircraft, automotive, and locomotive industries are replacing steel and cast iron in different mechanical components with lighter high strength alloys and composites like aluminium (Al) matrix composites. As an outcome of this trend, the machining of metal matrix composites becomes very vital in the final stage of manufacturing, which needs further research.

Abbreviations: RSM, response surface methodology; RSA, response surface analysis; GRG, grey relational grade; GFRG, grey fuzzy relational grade; TiC, titanium carbide; MMC, metal matrix composite; Ra, centre line average roughness; Rz, average maximum height of the profile; Fc, cutting force in the direction of tool travel; CNC, computer numerical control; ANOVA, analysis of variance; ANN, artificial neural network; GA, genetic algorithm; GRC, grey relation coefficient.

The first generation of aluminium based composite materials having ceramic reinforcements are found to reveal good quality strength to weight ratio and better corrosion resistance. Currently, the research consideration is directed toward the hybrid composites having more than one reinforcing phase [1]. An ample spread application of these second generation MMCs are not possible without solution to the problems related to cutting [2,3].

Manna and Bhattacharyya [4] have investigated the effect of cutting speed, feed and depth of cut on wear of the cutting tool and built-up edge formation during the turning operation of Al-SiC particulate composite, using a rhombic uncoated tool of carbide material. However, less amount of built up edge formation was found at a lower depth of cut and at higher cutting speed. Ciftci et al. [5] have examined the effect of SiC particulate size on the wear of the tool and surface finish with cubic boron nitride (CBN) tool insert at constant depth of cut, feed and at varying cutting speeds. It was suggested that for 30 µm and 45 µm size of SiC in aluminium metal matrix, optimum cutting speed was achieved at 150 m/min. For better size of SiC reinforcements (110 µm), CBN tool was not found appropriate for turning operation. Chambers [6] have found that the performance of PCD insert was significantly superior than carbides insert while turning Al-5Mg reinforced with a combination of 5 vol.% saffil and 15 vol.% SiCp. Looney et al. [7] have performed

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a series of turning operations on the Al–25%SiC metal matrix composite using CBN, carbide, and silicon nitride inserts. From these inserts, cubic boron nitride insert has formed the best cutting, and silicon nitride inserts was the worst among all. El-Gallab and Sklad [8] have determined the quality of the surface of Al–20%SiC composite in high speed turning under different cutting parameters. It was found in their investigation that the polycrystalline diamond tools (PCD) exhibited appropriate cutting tool life as when being compared with coated carbide tools and alumina.

Ding et al. [9] has investigated the machining behaviour of Al–SiC MMC using the PCBN and the PCD tools. Surface cracking was observed at the flank face surfaces of the cutting tools; intergranular fractures were observed on the rake faces. The PCD inserts performance was better than the PCBN inserts. Yanming and Zehua [10] reported the mechanism of cutting tool wear during the machining of Al–SiC composite. The cutting tool flank surface was being affected by abrasive wear and it was found that the carbide tool was appropriate for the fine size of SiC reinforced composite. It was also seen that the size of the reinforcement and the volume fraction played a great role in the cutting tool life.

Muthukrishnan et al. [11] reported that better quality of surface finish in turning of A356/SiC MMCs could be achieved by means of medium grade PCD 1500 inserts with less power utilization at the elevated cutting speed. BUE formation was seen on the tip of cutting tools at lower cutting speed. Pramanik et al. [12] have explained the effect of factors, such as tool particle connections, difference in strain, thermal softening, and work hardening, on the variation of cutting forces for metal matrix composites and its alloy. Tamer et al. [13] investigated the influence of machining parameters such as cutting speed, feed and depth of cut on the cutting tool wear and surface roughness of AlSi₇Mg₂ reinforced with 5, 10 and 15 wt.% of SiCp. Mahamani [14] has optimized the cutting parameters in machining of in situ Al-5Cu-TiB₂ composite using uncoated tungsten carbide inserts. Anandakrishnan and Mahamani [15] have studied the machinability of in situ Al-6061-TiB2 MMCs. The flank wear rate, cutting force, and surface roughness were found to be higher with a higher value of depth of cut.

Rai et al. [16] have studied the cutting force development and chip formation while doing shaping operation of Al-TiC composites and compared them with Al-TiAl₃ composite and Al-Si alloys. There was improvement in the quality of the surface machined with the increased quantity of TiC reinforcing particles in the composite. The cutting force developed while machining Al-TiC metal matrix composite was lower than the cutting force developed while machining Al-TiAl₃ composite and Al-Si alloy. Kumar et al. [17] have studied the feasibility, dry turning characteristics of Al-4.5%Cu/TiC composites using uncoated ceramic inserts. The influence of the input process parameters on the surface roughness and cutting force was observed. BUE formation was found lower at higher cutting speeds and was found higher at lower cutting speeds. Razavykia et al. [18] evaluated machining process parameters and the modifier element effects on the cutting force and the surface roughness in the dry turning of the Al-Mg₂Si in-situ MMC. The addition of the Bi element as modifier reagent results in the lower cutting force and the lower surface roughness. Kumar and Chauhan [19] also investigates the effect of the cutting speed, feed, approach angle on the surface roughness of Al7075 ceramic composite (10% SiC) and Al7075 hybrid composite (7%SiC and 3% graphite). It was found that in the turning operation of both the composite surface roughness of the hybrid, composite was less than the ceramic composite. Karabulut [20] has fabricated AA7039/Al₂O₃ MMC by using powder metallurgy technique and found that material structure was the most effective factor in affecting the cutting force, and surface roughness. The milling test was being performed based on the Taguchi design of experiment. Shoba et al. [21] also investigated the effect

of the cutting speed, feed, and depth of cut on cutting force. A comparison study was performed for the reinforced and unreinforced composites, and the result shows that cutting force decreases with the increase in the weight percentage of the reinforcements.

The multi-output optimization problems could be solved by using different methods such as grey relational analysis (GRA), genetic algorithm (GA), artificial neural network (ANN), response surface methodology (RSM) and fuzzy logic [22].

The investigation based on fuzzy-logic finds applications in unclear and undecided environment. In the recent research trends, fuzzy-logic-based multi-criteria decision making techniques have become very popular in doing optimization of different manufacturing processes. Grey system initiated by Deng [23] is a powerful tool to deal with the poor, incomplete and vague data [24,25]. In recent years, researchers have effectively used grey relational technique for solving the intricate interrelationships between the multiple objectives in a variety of fields of manufacturing [26-30]. A grey relational grade (GRG) is calculated by doing average of the grey relational coefficient of each response to convert the optimization of the complex performance characteristics into optimization of a single GRG [27]. Lin and Lin [30] researchers have done optimization of EDM process of SKD11 alloy steel with many process responses using grey-fuzzy-logic method. The theory of fuzzy logic proposed by Zadeh can successfully deal with the uncertain and vague information [31]. Therefore, the application of the fuzzy logic theory to the grey relational analysis may further develop its performance in solving multi-response problems for process parameter optimization. In the past, researchers have fruitfully employed grey fuzzy logic [24-29] for optimizing the multiple objectives of the complex manufacturing problems. They found that grey based fuzzy technique can make significant improvement in the performance characteristics of the process.

Rupajati et al. [32] has optimized several performances like recast layer thickness and surface roughness using fuzzy-logic method with Taguchi's L_{18} mixed- orthogonal array. It was found that the application of this optimization technique has significantly improved multiple output responses. Kumar et al. [33] investigated the cutting force development while performing the turning operation on unidirectional glass fibre reinforced plastics composite. Taguchi's L_{18} orthogonal array was being used for conducting the experimentations.

Soepangkat and Pramujati applied integrated approach comprising of GRA and fuzzy-logic for optimizing wire EDM of AISI D2 steel for minimizing surface roughness and layer thickness [34]. Related optimization techniques have been effectively utilized in a variety of manufacturing processes, which are mostly carried out under complex and uncertain environment [24,35–38].

Even though a very few research works have been carried out to study the influence of CNC milling parameters on different quality and productivity aspects, it is very necessary to establish optimal parametric combination with the intention of obtaining improved machined surface. Thus, the present work is focused on optimization of CNC milling machining parameters of Al–4.5%Cu–TiC metal matrix composite using grey-fuzzy analysis. The experimental work is done on the basis of Taguchi's L_{25} orthogonal array. The essential input milling parameters selected are cutting speed, feed and depth of cut, and the outputs considered are surface roughness and cutting force. For minimizing the values of all the performance characteristics, an optimal combination of input process parameters are required.

2. Experimental description

The material used for the experimentation is Al–4.5%Cu–TiC metal matrix composite prepared through the stir casting process.

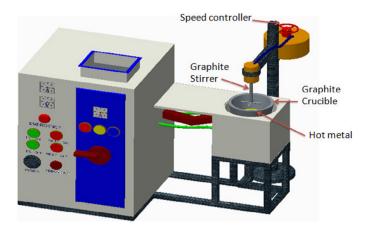


Fig. 1. Schematic diagram of a stir casting process.

It was prepared at 1250 °C by an in situ technique in an induction furnace. Titanium (99.8% purity), activated charcoal powder (average size 150 µm) and commercial pure aluminium (99.9% purity) and pure copper (99.8% pure) were used as the charge materials in the furnace. In an induction furnace (shown in Fig. 1), at first pure aluminium (Al) ingot was melted in a graphite crucible at a temperature of 685 °C, afterwards pure copper (Cu) was added to the molten aluminium at 800 °C and by the help of a graphite stirrer the mixture was endlessly stirred. Pure titanium (Ti) was then added to the liquid material at 1000 °C, and the mixture was endlessly stirred. At 1100 °C activated charcoal powder was added to the Al-Cu-Ti liquid melt and it was held for 5 minutes to permit the occurrence of the reaction thus forming TiC intermetallic particles in the melt, and the mixture was endlessly stirred. Potassium fluoride and sodium fluoride were used as a flux cover so as to remove the oxide film development from the molten metal surface and for acting as a protective barrier to gas absorption and to make possible impulsive incorporation of the particles into the melt [39,40]. Subsequently the hot liquid melt was cast into rectangular metallic mould of size $30~\text{mm}\times30~\text{mm}\times80~\text{mm}$ for carrying out the CNC milling process.

An end mill cutter of length 75 mm, diameter 8 mm, 4 number of flutes, 25 mm flute length, was used for performing machining operation of Al–4.5%Cu–5TiC metal matrix composite in CNC milling machine in dry condition, shown in Fig. 2.

The five level variations of cutting speed, feed, depth of cut chosen for this experimentation is shown in Table 1. The experiments are designed as per Taguchi's L_{25} orthogonal array of experiments.

The experimental set up for the present study is shown in Fig. 3. The experiments were carried out on a CNC end milling machine manufactured by MTAB Engineers Pvt. Ltd. The cutting force in the direction of the cutting tool travel (Fc) was measured with a dynamometer. Surface roughness parameters were measured by using a 3D profilometer at 20× magnification and at 4.7 mm cut-off distance. All the subsequent measurements were repeated 5 times.

Table 1Cutting parameters with their level.

Parameter	Notation	Unit	nit Level of factors				
			1	2	3	4	5
Cutting Speed	N	rpm	400	450	500	550	600
Feed	f	mm/min	20	25	30	35	40
Depth of Cut	d	mm	0.15	0.20	0.25	0.30	0.35

3. Methodology

3.1. Design of experiment using response surface methodology (RSM)

Response Surface Analysis focuses a renowned new approach to the optimization of the input process parameter models based on physical experiments, simulation experiments and experimental findings. These approximated models need to be assessed statistically for their competence, and then they can be used for an optimization of the initial model. The response surface analysis problems have a handy relation between responses and independent variables, and this relation can be explained by the second-order polynomial model shown below.

$$y = \beta_0 + \sum_{i=1}^{k} \beta_i X_i + \sum_{i=1}^{k} \beta_{ii} X_i^2 + \sum_{i} \sum_{i} \beta_{ij} X_i X_j + \varepsilon$$
 (1)

where y is estimated response; β_0 is the constant; and β_i , β_{ii} and β_{ij} represent the coefficients of linear, quadratic, and cross-product terms, respectively. X is the coded variables. ε is random error term. The general approach in RSM is to use regression methods based on least square methods.

3.2. *Grey relational analysis (GRA)*

As the Taguchi method is planned to optimize single response characteristic, the grey relational analysis optimizes multiple outcomes. Therefore, the grey relational analysis method is complicated [41,42]. In GRA, the optimization process is done in the following three steps.

In the first step, the measurement values of centre line average roughness (Ra), average maximum height of the profile (Rz), and cutting force (F_c) are to normalize in the range of zero to one. This is called grey relational normalization. Such normalization is required since the range and the unit in one response may vary from the others. If the response is of 'higher-the-better' characteristics, the equation for doing normalizing is as follows:

$$x_i^*(k) = \frac{x_i(k) - \min x_i(k)}{\max x_i(k) - \min x_i(k)}$$
(2)

If 'lower-the-better' condition is to be followed, in that case the following equation is to be utilized for normalizing the related data:

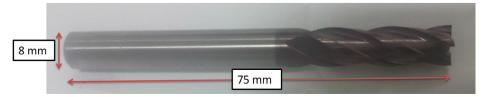


Fig. 2. Solid carbide end mill cutter.

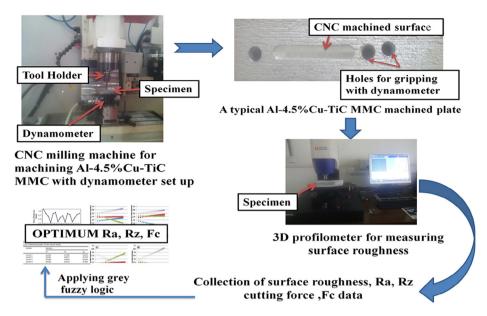


Fig. 3. Experimental set up.

$$x_i^*(k) = \frac{\max x_i(k) - x_i(k)}{\max x_i(k) - \min x_i(k)}$$
(3)

where $x_i^*(k)$ and $x_i(k)$ are normalized data and observed data respectively for the ith experiment by using kth response. After doing normalization of the responses, the next step is to calculate the grey relational coefficient (GRC). It can be calculated by using the Eq. (4).

$$\xi_i(k) = \frac{\Delta_{min} + \zeta \Delta_{max}}{\Delta_i(k) + \zeta \Delta_{max}} \tag{4}$$

where $\Delta_i(k)$ is absolute value of the difference between $x_i^0(k)$ and $x_i^*(k)$ and $\Delta_i(k) = |x_i^*(k) - x_i^0(k)|$. Δ_{max} and Δ_{min} are global maximum and global minimum values in different data series, respectively. The distinguishing coefficient (ζ) lies between 0 and 1, which is to expand or to compress the range of GRC, generally, $\zeta = 0.5$ is taken.

In third step, the grey relational grade is computed by finding the average of the grey relational coefficient corresponding to each performance characteristics. This degree is being estimated with the following equation:

$$\gamma_i = \frac{1}{n} \sum_{k=1}^n \xi_i(k) \tag{5}$$

where γ_i the grey relational grade and n is the number of process response. The optimal value of the GRG can be predicted by using Eq. (6).

$$\gamma_e = \gamma_m + \sum_{i=1}^q (\overline{\gamma}_i - \gamma_m) \tag{6}$$

where γ_m is total mean of the GRG value, q is number of input process parameters, and $\bar{\gamma}_i$ is mean GRG value at the optimal level for the ith parameter. ANOVA method is also used to find out the statistical importance of each factor and the percentage contribution of each input parameter on the responses.

3.3. Fuzzy rule based modeling

In grey relational analysis, the use of lower-the-better, higher-the-better and nominal-the-better performance

characteristics shows that there is some uncertainty in the obtained results. This vagueness can be efficiently checked by using fuzzy logic [23].

In the first step, the fuzzifier uses membership function to fuzzify inputs ($\xi 1$ = grey relation coefficient for Ra, $\xi 2$ = grey relation coefficient for Rz and $\xi 3$ = grey relation coefficient for Fc). The membership function is used defining how the values of the input ($\xi 1$, $\xi 2$ and $\xi 3$) and output (η_0 = Grey Fuzzy Relational Grade (GRFG)) are mapped to a value between 0 and 1. In the next step twenty five fuzzy rules for the three inputs and one output are developed using the Eq. (4) derived from the results obtained from experiments for inference.

Rule 1: if
$$\xi_1$$
 is A_1 , ξ_2 is B_1 , and ξ_3 is C_1 then η is D_i ; else
Rule 2: if ξ_1 is A_2 , ξ_2 is B_2 , and ξ_3 is C_2 then η is D_2 ; else
...
Rule n : if ξ_1 is A_n , ξ_2 is B_n , and ξ_3 is C_n then η is D_n

where Ai, Bi, Ci and Di are the fuzzy subsets defined by the corresponding membership functions, i.e., $\mu_{Ai}(\xi 1)$, $\mu_{Bi}(\xi 1)$, $\mu_{Ci}(\xi 1)$ and $\mu_{Di}(\eta)$. The inference engine then performs fuzzy reasoning on fuzzy rules by taking max–min inference (Eq. (8)) for generating a fuzzy value $\mu_{D0}(\eta)$.

$$\mu_{D_0}(\eta) = (\mu_{A_1}(\xi 1) \wedge \mu_{B_1}(\xi 2) \wedge \mu_{C_1}(\xi 3) \wedge \mu_{D_1}(\eta)) \\ \vee ((\mu_{A_2}(\xi 1) \wedge \mu_{B_2}(\xi 2) \wedge \mu_{C_2}(\xi 3) \wedge \mu_{D_2}(\eta)) \\ \vee (\mu_{A_3}(\xi 1) \wedge \mu_{B_3}(\xi 2) \wedge \mu_{C_3}(\xi 3) \wedge \mu_{D_3}(\eta)) \\ \vee \dots \vee (\mu_{A_n}(\xi 1) \wedge \mu_{B_n}(\xi 2) \wedge \mu_{C_n}(\xi 3) \wedge \mu_{D_n}(\eta))$$
(8)

where \land is minimum operation, and \lor is maximum operation respectively.

Finally the defuzzifier converts the fuzzy value into crisp output using the centroid defuzzification method (Eq. (9)); i.e. grey fuzzy reasoning grade (η_0) is calculated from the fuzzy multi-response output $\mu_{D_0}(\eta)$ using the following equation:

$$\eta_0 = \sum \mu_{D_0}(\eta) / \sum \mu_{D_0}(\eta) \tag{9}$$

GFRG corresponds to optimal setting of the input process parameter for multi-response characteristics.

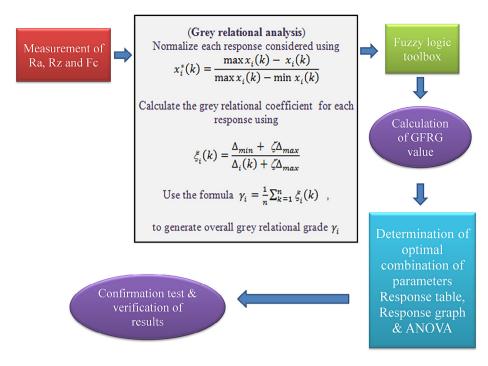


Fig. 4. Proposed grey-fuzzy-logic method.

3.4. Steps for the grey-fuzzy-logic method

The procedure adopted for determining the optimum machining parameters for the multi-response optimization is shown in Fig. 4. The methodology consists of a six step approach shown below:

Step 1: Selecting the machining parameters and their levels. Perform the experiments by using full factorial design.

Step 2: Normalization of all the responses (Data pre-processing) obtained by using Eq. (2). Calculation of the grey relational coefficient $\xi_i(k)$ for each response by using Eq. (4). Eq. (5) was used to generate the overall grey relational grade γ .

Step 3: Fuzzification of the grey relational coefficient obtained from each responses and fuzzification of the overall grey relational grade by using the membership function. Also, establishing the fuzzy rules in linguistic form relating grey relational coefficient and overall grey relational grade.

Step 4: By using max–min interface operation (Eq. (8)) calculation of the fuzzy multi-response output $\mu_{D_0}(\eta)$ and then employing centroid defuzzification (Eq. (9)) to calculate a grey-fuzzy reasoning grade η_0 .

Step 5: Selecting the optimum combination of parameters through the response table and response graph. Finding out the contribution of each factor and their interactions on the multi response output by using analysis of variance (ANOVA).

Step 6: Carrying out confirmation tests for verifying the results obtained (using Eq. (6)).

4. Results and discussion

4.1. Calculating the grey relational coefficients

The pre-processed data of experimental results, the grey relational coefficients and the overall grey relational grade for each of the combination of parameters is given in Table 2. For all the re-

sponses, 'lower-the-better' criterion is preferred. On the other hand, in order to obtain an improved quality in the performances and to decrease the vagueness in the data, grey-fuzzy logic method is additionally used for computing the GFRG.

4.2. Grey-fuzzy reasoning analysis

In this present paper, three inputs and one output (GFRG) fuzzy-logic system is used. The inference engine (Mamdani fuzzy inference system) performs fuzzy reasoning with fuzzy rules for generating a fuzzy value. These fuzzy rules are shown in the form of 'if-then' control rule. Grey relational coefficients for Ra, Rz and F_c are inputs to the fuzzy logic system. The linguistic membership function for instance Lowest, Low, Medium, High and Highest are used to represent the grey relational coefficients (GRC) of input variables R_a, R_z and F_c. Likewise the output grey relational grade is being represented by the membership functions such as Lowest (L), Very Low (VL), Medium Low (ML), Low, Medium High (MHIGH), Higher (H), Medium Higher (MH), Highest. The triangular shaped membership function, which is used in this work, is shown in Figs. 5 and 6. A total of 25 numbers of fuzzy rules are used for this purpose. The rule-based fuzzy-logic reasoning is shown in Fig. 7. Maximum-minimum compositional operation by tracking the fuzzy reasoning yields a fuzzy output. At last, the defuzzifier converts the fuzzy predicted values into a GRFG by using MATLAB (R2010b) fuzzy logic toolbox. This GFRG values are tabulated in Table 2.

The higher values of GFRG exhibits the best multiple performance characteristics. Analysis of the mean is performed for GFRG. Based on Δ (Delta) statistics, which is the difference among the highest and the lowest average of GFRG for each of the factor, the rank of the parameters, which affects the multiple performance response, is listed in Table 3. These values are plotted in Fig. 8 like the response graph for the machining parameters. The greater the inclination of the response graph, the larger the effect of the process parameters on the multiple performance response.

Table 2Data pre-processing, grey relational coefficients and grey relational grades.

	Normalized v	Normalized value of the experimental results			Grey relational coefficient			GFRG
	R _a (μm)	R _z (μm)	F _c (N)	R _a (μm)	R _z (μm)	F _c (N)	relational grade	
1	0.3220	0.3607	0	0.4244	0.5462	0.3333	0.435	0.502
2	0.3024	0.6621	0.5607	0.4175	0.3333	0.5323	0.428	0.372
3	0.3805	0.5845	0.1339	0.4466	0.5192	0.3660	0.444	0.445
4	0.4488	0	0	0.4756	0.5219	0.3333	0.444	0.559
5	0.3024	0.5369	0.5116	0.4175	0.5013	0.5059	0.475	0.294
6	0.3268	0.5419	0.5674	0.4262	0.4845	0.5361	0.482	0.339
7	0.5122	0.5025	0.4512	0.5062	0.3333	0.4767	0.439	0.406
8	0.5610	0.4680	0.2558	0.5325	0.5076	0.4019	0.481	0.837
9	0.3951	0	0.8977	0.4525	0.6516	0.8302	0.645	0.500
10	0.4976	0.5149	0.6698	0.4988	0.5127	0.6023	0.538	0.815
11	1	0.7327	0.8372	1	0.4903	0.7544	0.748	0.501
12	0.5641	0.5248	0.4605	0.5342	0.5549	0.4810	0.523	0.847
13	0.3526	0.4802	1	0.4358	0.6779	1	0.705	0.500
14	0.5128	0.5990	1	0.5065	0.4975	1	0.668	0.499
15	0.4167	0.7624	0.9760	0.4616	1	0.9542	0.805	0.954
16	0.6538	0.4950	0.2036	0.5909	0.3333	0.3857	0.437	0.537
17	0.6474	1	0.7485	0.5864	0.3491	0.6653	0.534	0.687
18	0.4167	0	1	0.4616	0.3649	1	0.609	0.571
19	0	0.0679	0.0759	0.3333	1	0.3511	0.561	0.597
20	0.9661	0.1296	0	0.9365	0.7594	0.3333	0.676	0.850
21	1	1	0.8200	1	0.5586	0.6354	0.731	0.852
22	1	0.3967	0.4700	1	0.5586	0.3718	0.643	0.857
23	0.7045	0	0.6800	1	1	0.495	0.832	0.500
24	0	0	1	0.7333	0.5461	1	0.76	0.937
25	0.4	0.6621	0.3727	1	0.3333	1	0.778	0.710

A fuzzy set \tilde{a} in a universe of discourse X is being characterized by a membership function $\mu_{\tilde{a}}(x)$, which maps every element x in X to a real number in the interval of [0, 1]. The function value $\mu_{\tilde{a}}(x)$ is termed as the grade of membership of x in \tilde{a} . The nearer value of $\mu_{\tilde{a}}(x)$ to unity, the higher the grade of membership of x in \tilde{a} .

A triangular fuzzy membership function is being represented as $\tilde{a}=(a_1,a_2,a_3)$. The membership function $\mu_{\tilde{a}}(x)$ of the triangular fuzzy number \tilde{a} is given as:

$$\mu_{\bar{a}}(x) = \begin{cases} \frac{x - a_1}{a_2 - a_1} & \text{if } a_1 \le x \le a_2 \\ 1 & \text{if } x = a_2 \\ \frac{a_3 - x}{a_3 - a_2} & \text{if } a_2 \le x \le a_3 \\ 0 & \text{Otherwise} \end{cases}$$

where a_1, a_2, a_3 are the real numbers. For a triangular fuzzy number $\tilde{a}=(a_1,a_2,a_3)$.

Fig. 5 is drawn to show the fuzzification of the three inputs e.g. Ra (taking their grey relational coefficient value). The triangular membership function graph is shown to define how the values of the input and output (Y = GFRG) are mapped to a value between 0 and 1. The linguistic membership function such as LOWEST, LOW, MEDIUM, HIGH and HIGHEST are used to represent the grey relational coefficient (GRC) of input variables. Similarly, the output grey relational grade is represented by the membership functions such as LOWEST(L), VERY LOW(VL), MEDIUM LOW(ML), LOW, MEDIUM HIGH (MHIGH), HIGHER (H), MEDIUM HIGHER(MH), HIGHEST. The triangular shaped membership function used in this work is shown in Fig. 6.

Based on Table 3 and Fig. 8, the optimum setting of the machining process parameters is found to the experimental run no. 25 i.e. with cutting speed at level five (600 m/min) (N5), feed rate at level five (40 mm/min) (f5) and depth of cut at level four (0.30 mm) (d4). This is indicated in bold font in Table 3. The use of these conditions will at the same time minimize the R₃₁.

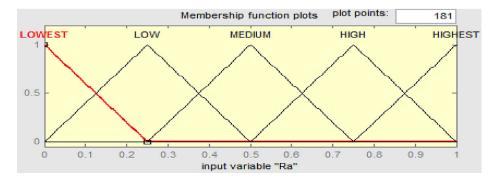


Fig. 5. Membership functions for the cutting force and surface roughness.

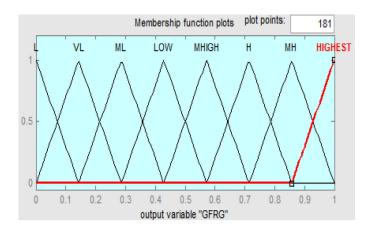


Fig. 6. Membership function for multi-response output.

 R_{z} and F_{c} throughout machining within the range of factors studied.

The response equation of the GFRG is shown in Eq. (10). The main influencing factor for multi-performance is the maximum of this value (i.e. rank 1), which is cutting speed (N). Also the same information can be obtained from Fig. 8.

$$\begin{aligned} \text{GFRG} = & (-1.90 + 0.00507 \times \text{N}) + (0.0886 \times \text{f}) - (3.95 \times \text{d}) \\ & - \left(0.000004 \times \text{N}^2\right) - \left(0.000336 \times \text{f}^2\right) - \left(7.93 \times \text{d}^2\right) \\ & - \left(0.000116 \times \text{N} \times \text{f}\right) + (0.01518 \times \text{N} \times \text{d}) \end{aligned} \tag{10}$$

ANOVA is performed for analyzing the role of each factor on the multiple performance characteristics. The analysis is done at a confidence level of 95%. Fisher's F-test is employed to find out the change

in which the process parameters have a significant effect on multiple performance characteristics. Larger F-value shows that the change of process parameters has a stronger influence on the performance characteristic. The results of the ANOVA are shown in Table 4. As in the ANOVA table of GFRG, the P value of the cutting speed is less than 0.05. This indicates that the cutting speed played a main role to determine the GFRG.

The obtained results are verified by doing the confirmatory experiment. Table 5 shows the confirmation test results of surface integrity aspects relating to initial and optimal machining conditions. It is obvious that machining with the optimum parametric combination would minimize R_a from 2.04 to 1.88 μ m, R_z from 2.57 to 1.91 μ m and decrease F_c from 600 to 499 μ m. The estimated or predicted GFRG ($\hat{\gamma}_e$) at the optimal level of the machining parameters can be calculated by using Eq. (11).

$$\hat{\gamma}_e = \gamma_m + \sum_{i=1}^q (\overline{\gamma}_i - \gamma_m) \tag{11}$$

where γ_m is total mean of the GFRG for all the experimental runs, q is number of input parameters, and $\overline{\gamma}_i$ is mean GFRG value at the optimum level for the ith parameter. Also Table 5 indicates that the machining with optimum setting would result in an improvement of GFRG of 0.2833 and 0.2100 for predicted and experimental values respectively. Hence, the present study clearly implies that grey-fuzzy-logic method can be effectively utilized for multi-characteristics optimization of process parameters.

Microscopic images of the surface before and after CNC milling machining are shown in Fig. 9(a, b).

After pouring the hot liquid material from the graphite crucible to the rectangular shaped metallic mould, the specimens were machined in shaper before performing machining operation in the CNC milling machine. The specimens were machined in the shaper for making the surfaces of the specimens free from any

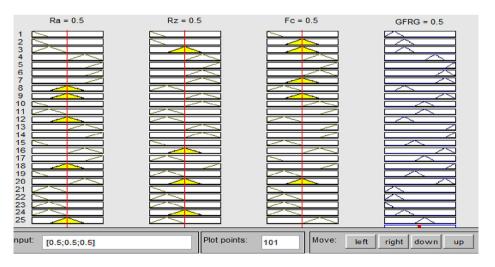


Fig. 7. Fuzzy logic rules viewer.

Table 3Response table for grey-fuzzy reasoning grade (GFRG).

Machining Parameters	Level 1	Level 2	Level 3	Level 4	Level 5	Δ(Max-Min)	Rank
Cutting speed (N)	0.4344	0.5794	0.6602	0.6484	0.7276	0.2932	1
Freed rate (f)	0.5462	0.6338	0.5706	0.6184	0.6810	0.1348	2
Depth of cut (d)	0.6488	0.5524	0.6278	0.6628	0.5666	0.1104	3

The bold values in the table indicate the level numbers which have the highest GFRG value for cutting speed, feed and depth of cut respectively. We can see that the GFRG value is higher at level 5 for cutting speed, GFRG value is higher at level 5 for feed, and GFRG value is higher at level 4 for depth of cut.

According to Table 1 in the manuscript, the value of cutting speed at level 5 is 600 rpm, the value of feed at level 5 is 40 mm/min, and the value of depth of cut at level 4 is 0.30 mm, which are the optimal combination of the said input parameters.

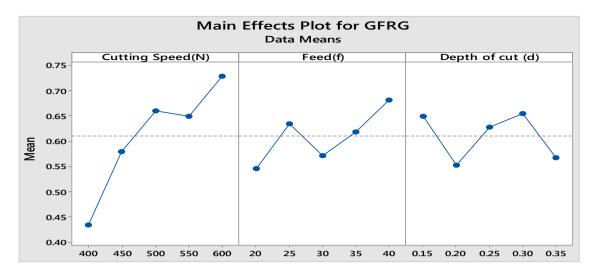


Fig. 8. Response graph for every level of machining parameters.

Table 4 ANOVA for GFRG.

Source of variance	DOF	SS	MS	F	P
Regression	3	0.249030	0.083010	2.48	0.089
Cutting Speed, N	1	0.214775	0.214775	6.41	0.019
Feed rate, f	1	0.032309	0.032309	0.96	0.337
Depth of cut, d	1	0.001947	0.001947	0.06	0.812
Error, e	21	0.703552	0.033502		
Total	24	0.952582			

casting burrs and casting defects in the surface. Fig. 9(a) shows the microscopic image of the upper surface of the specimen before performing CNC milling operation, which shows cut marks of the shaper single point cutting tool and results in more roughness in the surface, whereas Fig. 9(b) shows the image of the surface after performing CNC milling operation with end mill cutter, which shows less surface roughness as compared to shaping operation.

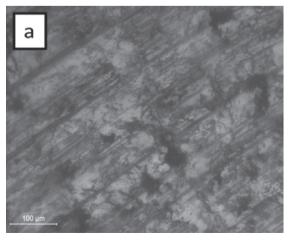
Table 5Comparison of results obtained under initial and optimum machining condition.

Levels	Initial machining parameters level	Optimum machining parameters level			
	N = 400, $f = 20$, $d = 0.15$	N = 600, f = 40, d = 0.30			
		Predicted	Experimental		
R _a ()	2.04		1.88		
$R_z()$	2.57		1.91		
$F_c()$	600		499		
GFRG	0.502	0.7853	0.7100		
Improvement in the GFRG		0.2833	0.2100		

5. Conclusion

In this present paper, machining of in situ Al–4.5%Cu/TiC metal matrix composite is carried out with input parameters considered as cutting speed, feed and depth of cut, and the response parameters as surface roughness, and cutting force in CNC milling machine. Taguchi's L_{25} orthogonal array design is used for performing CNC milling operation on the composite plates.

- It was found that a cutting speed of 600 rpm, feed of 40 mm/ min and a depth of cut of 0.30 mm is the optimal combination of input parameters.
- ANOVA statistics exposed that cutting speed is the most influencing factor in effecting the response parameters.



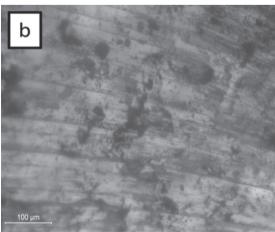


Fig. 9. Microscopic images of the surface (a) before CNC machining and (b) after CNC machining.

Therefore, it is concluded that the optimization procedure proposed in this present paper significantly improved the production of CNC milling of Al–4.5%Cu/TiC metal matrix composite.

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