The Seventeenth CIRP Conference on Electro Physical and Chemical Machining (ISEM)

Electrical discharge machining of ceramic/carbon nanostructure composites

D.Hanaoka\textsuperscript{a}, Y.Fukuzawa\textsuperscript{a,*}, C. Ramirez\textsuperscript{b}, P. Miranzo\textsuperscript{b}, M.I.Osendi\textsuperscript{b}, M. Belmonte\textsuperscript{b}

\textsuperscript{a} Nagaoka University of Technology, 1603-1, Kamitomioka, Nagaoka, 940-2188 Niigata, Japan
\textsuperscript{b} Institute of Ceramics and Glass (ICV-CSIC), Kelsen 5, 28049 Madrid, Spain

* Corresponding author. Tel.: +81-258-47-9711; fax:+81-258-47-9711.E-mail address: fukuzawa@vos.nagaokaut.ac.jp.

Abstract

The miniaturization of mechanical components with complex shapes is a great challenge in emerging applications. Silicon nitride (Si\textsubscript{3}N\textsubscript{4}) ceramics are excellent candidates for such applications owing to their outstanding mechanical, thermal, and tribological properties [1]. However, due to the hardness of these ceramics, alternative machining methods to diamond grinding are required for producing complex micro components. One promising technique is electrical discharge machining (EDM), which uses a spark of electricity to blast away the unwanted material in order to create complex shapes [2]. However, EDM commonly requires the use of materials with sufficient electrical conductivity ($\geq 0.3-1$ S m$^{-1}$) [3], which limit its use on insulating ceramics such as Si\textsubscript{3}N\textsubscript{4}, SiC, and ZrO\textsubscript{2}. To overcome these difficulties, different approaches have been attempted by many researchers. Muttamara et al. [4] machined Si\textsubscript{3}N\textsubscript{4} specimens by EDM using an assisting electrode (AEM) in the form of an electrically conductive coating, although the material removal rate (MRR) was low and the electrode was considerably worn. Other researchers were focused on the addition of large amounts of electrically conductive secondary phases, mainly 40 vol.% of TiN [5], but the surface of the machined material was high in roughness and yielded a foamy structure. Malek et al. [6] have recently reported the manufacture of a Si\textsubscript{3}N\textsubscript{4} micro gear with a remarkably high MRR, low surface roughness (Ra), and low tool wear compared to Si\textsubscript{3}N\textsubscript{4}/TiN materials, introducing just 5.3 vol.% of carbon nanotubes (CNT) into the ceramic matrix. Thanks to the outstanding electrical properties of CNT, a conductive percolating network was created in the composite at low CNT

© 2013 The Authors. Published by Elsevier B.V. Selection and/or peer-review under responsibility of Professor Bert Lauwers

Keywords: Sinking EDM; insulator Si\textsubscript{3}N\textsubscript{4} ceramics; nanocomposite of Si\textsubscript{3}N\textsubscript{4}

1. Introduction

The miniaturization of mechanical components with complex shapes is a great challenge in emerging applications linked to the energy and communications sectors, such as in micro turbines or micro electro mechanical systems (MEMS). Silicon nitride (Si\textsubscript{3}N\textsubscript{4}) ceramics are excellent candidates for such applications owing to their outstanding mechanical, thermal, and tribological properties [1]. However, due to the hardness of these ceramics, alternative machining methods to diamond grinding are required for producing complex micro components. One promising technique is electrical discharge machining (EDM), which uses a spark of electricity to blast away the unwanted material in order to create complex shapes [2]. However, EDM commonly requires the use of materials with sufficient electrical conductivity ($\geq 0.3-1$ S m$^{-1}$) [3], which limit its use on insulating ceramics such as Si\textsubscript{3}N\textsubscript{4}, SiC, and ZrO\textsubscript{2}. To overcome these difficulties, different approaches have been attempted by many researchers. Muttamara et al. [4] machined Si\textsubscript{3}N\textsubscript{4} specimens by EDM using an assisting electrode (AEM) in the form of an electrically conductive coating, although the material removal rate (MRR) was low and the electrode was considerably worn. Other researchers were focused on the addition of large amounts of electrically conductive secondary phases, mainly 40 vol.% of TiN [5], but the surface of the machined material was high in roughness and yielded a foamy structure. Malek et al. [6] have recently reported the manufacture of a Si\textsubscript{3}N\textsubscript{4} micro gear with a remarkably high MRR, low surface roughness (Ra), and low tool wear compared to Si\textsubscript{3}N\textsubscript{4}/TiN materials, introducing just 5.3 vol.% of carbon nanotubes (CNT) into the ceramic matrix. Thanks to the outstanding electrical properties of CNT, a conductive percolating network was created in the composite at low CNT
contents, extraordinarily enhancing the electrical performance of Si₃N₄ [7]. Other carbon nanostructures (CNs) such as graphene present similar or even better electrical properties, and consequently, Si₃N₄ composites containing graphene nanoplatelets (GNP) have been developed with electrical conductivities as high as 4000 S·m⁻¹ [8]. In this study, to investigate the difference in the EDM properties between the insulating and conductive Si₃N₄ composites containing CNs, two different fillers (CNT and GNP) and concentrations were employed: one close to the electrical percolation threshold (pc) and one significantly greater than that limit. These were EDMed using a homemade machine, and the performance of the EDM process was evaluated as a function of the content and type of CNs. Bare Si₃N₄ specimens, which are an insulating material, were also tested for comparative purposes.

2. Machining mechanism of AEM

The mechanism of the assisting electrode method has been assumed in previous literature, but without enough theory explaining the adhesion phenomena of carbonized products [9] [10]. A schematic of the assisting electrode method is given in Fig. 1. The surface of the insulating workpiece is covered by, or attached to, the electrical discharge material and is set up in the machine under a working oil. (1) At the start of EDM, discharge occurs between the tool electrode and the covered layer, similar to EDM of conductors. (2) Discharge occurs between the electrode and the covered material at deeper levels. In this region, the electrically conductive products, which are composed of carbonized machined material, adhere to the insulating surface. (3) The carbide products come in contact with the insulating material itself. (4) The carbide products generated from the dissociation of the working oil under the discharge maintain the electrical conductivity at the discharged area, even after the assisting electrode material is removed. Many machining trials have been carried out for Si₃N₄, SiC, AlN, and ZrO₂ [9] [10].

This indicates that the electrical machining conditions depend on the physical characteristics of the workpiece. Three-dimensional precise complex shapes have been successfully machined with sinking and wire EDM methods for insulating ceramic materials such as Si₃N₄, SiC, AlN, ZrO₂, and diamond. Fig. 2 shows a typical machined sample for Si₃N₄. In this sample, a star shape was machined on a concave surface. The tip of the star was kept with a sharp corner edge. A micro-hole was also machined on the insulating Si₃N₄ using this method.

The machinable limit of electrical conductivity for normal EDM, and the effects of the carbon layer creation phenomenon on the boundary of the insulating area and electrically conductive area still require further discussion.

3. Experimental procedure

The fabrication of Si₃N₄ monolithic materials and composites containing CNs is described elsewhere [11]. In short, chemical vapor deposition (CVD) synthesized multi-walled CNTs (MWCNTs) of 9.5 nm average diameter and 1.5 μm average length (NC3100 Nanocyl S.A., Belgium) in concentrations of 0.9 and 5.3 vol.%, and GNP of nominally 200 nm diameter and 1 nm thickness (Angstrom Materials LLC, USA) in concentrations of 11.3 and 20.6 vol.% were selected as CNs. Ceramic matrix compositions containing α-Si₃N₄ powders (SN-E10, UBE Industries, Japan) plus Y₂O₃ (HC-Starck) and Al₂O₃ (SM8, Baikowski Chimie, France), were used as sintering aids. Both CNs and the ceramic powders were separately dispersed in alcohol by sonication and attrition milling, respectively, and then mixed in an ultrasonic bath under continuous stirring. The material compositions are displayed in Table 1.

Table 2 shows the fundamental EDM conditions. The EDM experiments were carried out using the assisting electrode method. The conditions were determined from previous experimental results of the insulating Si₃N₄ material using the assisting electrode method. The machining properties were estimated by the MRR, electrode wear ratio, and Ra, of the EDMed surface. The surface roughness was observed on the removed surface of the adhered, electrically conductive layer using a laser optical microscope.
4. Results and discussion

The densities of the sintered specimens were measured by water immersion. They were above 99% of the theoretical values, with the final α-phase content of the Si₃N₄ matrix ~ 50%. Furthermore, the composites exhibited an excellent CN dispersion within the matrix, avoiding CN degradation after the sintering process, as was confirmed by the micro-Raman spectroscopy shown in Fig. 4 [10]. For the monolithic Si₃N₄ material, the electrical conductivity value (Table 1) corresponded to the detection limit of our experimental set-up, 10⁻¹³ S·m⁻¹. Therefore, the real conductivity must be even lower than this value. As has been previously mentioned, the CN concentrations were selected to be close to the electrical percolation threshold, and well above that limit. In the case of 0.9 vol. % CNT composites, the electrical conductivity of σ = 4×10⁻² S·m⁻¹ became more than 10 orders of magnitude larger than the monolithic Si₃N₄. It was assumed that this value would attain the machinable limit of electrical conductivity, as well as the effects of the assisting electrode on the machining properties, the assisting electrode EDM and normal EDM methods were applied for all specimens. The discharge phenomenon was not observed on the monolithic Si₃N₄ and CNT 0.9 vol.%. This indicates that the minimum electrical conductive value was lower than 4×10⁻² S·m⁻¹. To compare the machining properties of the insulating and conductive materials, EDM was carried out using the same conditions. These were selected by considering pre-machining data as the most available conditions for the Si₃N₄. The assisting electrode method was carried out on all workpieces. The relationships between the electrical conductivity value σ and the MRR, electrode wear rate, and Ra (evaluated by a laser optical microscope) were analyzed. Results are shown in Figs. 5, 6, and 7, respectively. In these figures, the results of normal EDM data are also displayed for the machinable specimens. All data represents the average value of three experiments. Very small deviations (within 15%) were observed for each data point. With the assisting electrode method, lower discharge machining conditions of discharge open circuit voltage and current were selected than normal conditions for electrically conductive material, and a 1/10 order reduction of the MRR was observed for the AEM than for the electrically conductive materials. The same MRR values were obtained on GNP materials independent of electrical conductivity.

Table 1. Powder compositions, maximum SPS temperature (TSPS), and electrical conductivity (σ) of the materials tested by EDM

<table>
<thead>
<tr>
<th>Material</th>
<th>Si₃N₄ (wt.%)</th>
<th>Al₂O₃ (wt.%)</th>
<th>Y₂O₃ (wt.%)</th>
<th>CNs (wt.%)</th>
<th>CNs (vol.%)</th>
<th>TSPS (ºC)</th>
<th>σ (S·m⁻¹)</th>
</tr>
</thead>
<tbody>
<tr>
<td>SN</td>
<td>93.0</td>
<td>2.0</td>
<td>5.0</td>
<td>0.0</td>
<td>0.0</td>
<td>1600</td>
<td>10⁻¹³</td>
</tr>
<tr>
<td>SN/0.9 CNT</td>
<td>92.5</td>
<td>2.0</td>
<td>5.0</td>
<td>0.5</td>
<td>0.9</td>
<td>1585</td>
<td>4×10⁻²</td>
</tr>
<tr>
<td>SN/5.3 CNT</td>
<td>90.0</td>
<td>2.0</td>
<td>5.0</td>
<td>3.0</td>
<td>5.3</td>
<td>1585</td>
<td>14</td>
</tr>
<tr>
<td>SN/11.3 GNP</td>
<td>85.0</td>
<td>2.0</td>
<td>5.0</td>
<td>8.0</td>
<td>11.3</td>
<td>1625</td>
<td>1</td>
</tr>
<tr>
<td>SN/20.6 GNP</td>
<td>78.0</td>
<td>2.0</td>
<td>5.0</td>
<td>15.0</td>
<td>20.6</td>
<td>1625</td>
<td>2002</td>
</tr>
</tbody>
</table>
conductivity. In the CNT materials, the MRR decreased with increasing electrical conductivity. For the materials machinable by the normal EDM method, MRR values decreased with increasing electrical conductivity, and were lower than the assisting electrode case. The electrode wear rate values were larger on the insulating material than the other conductive materials, and decreased with increasing conductivity. Regarding the GNP materials, a lower wear rate was detected in the results of the assisting electrode method than the normal EDM method for the low conductivity composites Si3N4/11.3 vol.% GNP and CNT 5.3 vol.% However, the opposite case was shown for Si3N4/20.6 vol.% GNP, which has higher conductivity. The Ra of the insulating materials was also larger than that of the conductive materials. The rougher surfaces were observed on the assisting electrode method than the normal method. Under these machining conditions, the MRR values of the monolithic Si3N4 and CNT 0.9 vol.%, which were regarded as insulating materials, were almost identical and were larger than those of the other conditions as observed using the laser optical microscope. Results are shown in Fig. 8 for (a) Si3N4, (b) CNT 0.9 vol.%, (c) CNT 5.3 vol.%, (d) GNP 11.3 vol.%, (e) GNP 20.5 vol.%, respectively. The other surface conditions observed between the insulating and conductive material as shown in Figs. 8(c) and 8(e). With regard to the roughness of the EDMed surface, many small size discharge craters were observed as in Fig. 8. As mentioned in section 2, the electrically conductive layer, composed of carbonized products from the dissociation of the working oil under discharge, adhered to the
surface continuously. It is assumed that the roughened surface produced the large carbonized craters. On the other hand, carbonized craters were not observed on the smooth surface. It appears that the assisting electrode material could not contribute to the carbonization phenomenon in the EDM process. However, these craters were also generated on the EDMed surface of GNP 11.3 vol.% composite (Fig. 8(d)), which could be EDMed using the normal method. If some carbonization occurred in the discharge process, carbide adhesion could occur on the electrically conductive workpiece. To confirm this phenomenon, the EDMed surfaces of electrically conductive materials were observed using a laser optical microscope. The observed results are displayed in Fig. 9, for (a) CNT 5.3 vol.%, (b) GNP 11.3 vol.%, and (c) GNP 20.5 vol.%, respectively. As seen in Fig. 9(b), some carbonized craters formed on the normal EDM method. We thus consider the carbonizing phenomenon to occur at the electrically conductive area of GNP. It indicated that when the amount of GNP materials increased a little from the machinable limit for normal EDM, the carbon element adhered on the EDMed surface around the districted electrical conductive area. On the other hand, as shown in Figs. 9(a) and (c), carbonized craters are not observed on the machinable composite material. Considering the structures of CNT and GNP, the discharge phenomenon of carbonization would be different in the narrow electrically conductive area. The distribution of the conductive region in the insulating matrix was considered an important factor in controlling the carbonization phenomenon during discharge on the insulator and conductive mixed composite. To confirm the effects of the assisting electrode material on the EDM properties, the machined shape produced using the normal and assisting electrode EDM methods were compared for the GNP 11.3 vol.%
composite. The results are shown in Fig. 10 for (a) the assisting electrode method, and (b) the normal method. For the normal EDM method, a large chipping area could be observed, whereas for the assisting electrode method, a very smooth shape was detected. It appears that the continuous discharges occurred evenly on the distributed conductive element surface.

Fig. 10 EDMed surface shapes: (a) GNP 11.3 vol.% and (b) GNP 11.3 vol.% without the assisting electrode material

5. Conclusions

To investigate the discharge behavior of Si$_3$N$_4$ ceramic/carbon nanostructure composites, EDM was carried out using the assisting electrode method. The results are summarized below:

- Insulating Si$_3$N$_4$ ceramics, and Si$_3$N$_4$/CNT and Si$_3$N$_4$/GNP nanocomposites, could be machined using the assisting electrode method on EDM.
- The machinable limit of electrical conductivity was below $4 \times 10^{-2} \text{S m}^{-1}$.
- The EDM properties of electrode wear ratio and surface roughness were better on the conductive materials than insulating materials.
- Better MRRs were obtained on the insulating materials than the conductive materials.
- The same EDMed surface composed with discharge craters was detected on the electrically conductive material.
- The discharge craters were made by carbonized products and generation phenomena were controlled by the amount of the conductive element and its distribution.
- A better hole edge shape was obtained by the assisting electrode method than the normal method on a GNP composite with low conductivity.

Acknowledgements

This work was supported by the Spanish Government under the project MAT2009-09600. C. Ramirez thanks the financial support of the JAE (CSIC)

Reference