

# Preparation of Nb<sub>3</sub>Al superconductor by powder metallurgy and effect of mechanical alloying on the phase formation

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**Abstract** Adoption of powder-in-tube method to fabricate superconducting wire can realize a large application of Nb<sub>3</sub>Al prepared by powder metallurgy. Powder metallurgy was used to synthesize Nb<sub>3</sub>Al under various heat-treatment conditions, annealing temperature was varied from 700 to 1,000 °C and heating time was varied from 10 to 50 h. X-ray diffraction patterns reveal that a reaction between Nb and Al took place and formed NbAl<sub>3</sub> phase. Under current heat-treatment conditions (annealing temperature was varied from 700 to 1,000 °C and heating time was varied from 10 to 50 h), NbAl<sub>3</sub> was so stable that it did not further react with the unreacted Nb and was not sensitive to the heat-treatment condition. By mechanical alloying, adoption of high-energy ball milling significantly decreases particle size and enhances surface free energy, which promotes the formation of Nb<sub>3</sub>Al phase. X-ray diffraction patterns indicate that relatively pure Nb<sub>3</sub>Al phase was obtained under the same heat-treatment condition. Energy-dispersive X-ray analysis measurement demonstrates that the obtained samples were close to the right stoichiometry of A15 structure Nb<sub>3</sub>Al.

**Keywords** Nb<sub>3</sub>Al · Superconductivity · Powder metallurgy · Mechanical alloying

## 1 Introduction

With development of modern transportation and pursuit of high speed in various vehicles, superconducting maglev is promising in taking an important role in the future transportation system. Selection of a proper superconducting wire is vital in fabrication of superconducting magnet. Nb<sub>3</sub>Al, due to its excellent superconducting properties, has drawn comprehensive attention since 1980s [1, 2]. A15 structure materials are famous for their superconductivities and Nb<sub>3</sub>Al has the higher critical temperature among all the A15 structure materials [3, 4]. Furthermore, high value of critical current density ( $J_c$ ) under high applied field makes it a promising substitution material for the fabrication of high-field magnet. The current existing fabrication method, powder-in-tube (PIT), makes it possible for a large-scale application of Nb<sub>3</sub>Al prepared by powder metallurgy.

In International Thermonuclear Experimental Reactor (ITER) [5], compared with the well-developed Nb<sub>3</sub>Sn, Nb<sub>3</sub>Al possesses better stress/strain tolerance. This makes it an ideal choice for the fabrication of the toroidal field (TF) coil in terms of the large size of the D-shape TF [6, 7]. At the moment, the relatively successful methods to prepare Nb<sub>3</sub>Al wire are restricted to high-temperature methods, because of the difficulty of the phase formation. Therefore, in order to acquire Nb<sub>3</sub>Al in the right stoichiometry, high-temperature generation specialized instruments are needed, such as RHQT [8]. In this work, powder metallurgy was used to synthesize Nb<sub>3</sub>Al and the effect of mechanical alloying on the phase formation was investigated.

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## 2 Methods

The experimental process includes into two parts. In the first part, normal hand grinding method was used to mill the Nb, Al powder. The mole ratio of Nb/Al = 3/1 was weighed, placed in an agate mortar and pestle, and mixed by gentle hand grinding for 0.5 h. The mixtures were pressed into round pellet with a diameter of 11.5 mm and a thickness of 1.5 mm using hardened steel die with uniaxial 12 MPa pressure. Then, the pellet was sealed into a vacuum-fused quartz tube with a vacuum degree of  $5.5 \times 10^{-3}$  Pa. Finally, the samples were heat treated in a tube furnace and argon was vented to avoid permeability or leakage.

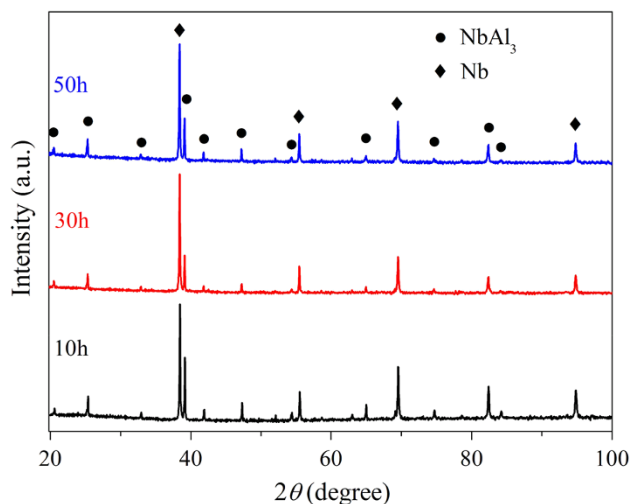
In the second part, mechanical alloying was adopted and a SPEX [9] mixer 8000 high-energy mill was used. All other experimental procedures were the same.

The crystal structure was studied by powder X-ray diffraction (XRD) using an X'Pert MRD diffractometer with Cu  $K\alpha$  radiation. All observed reflections were indexed. Lattice constants were determined from LeBail refinements. Microstructure and composition of the sample were analyzed using a field emission scanning electron microscope (FESEM) equipped with an energy-dispersive X-ray analysis (EDX). DC magnetization was measured with a SQUID magnetometer (MPMS, Quantum Design) and resistivity measurements were performed with a physical property measurement system (PPMS, Quantum Design).

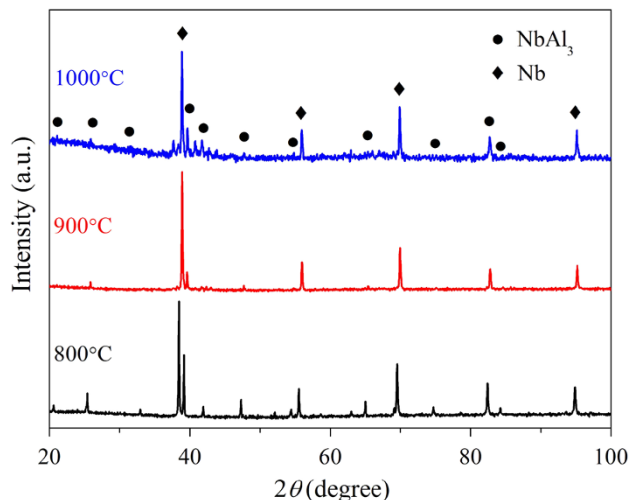
## 3 Results and discussion

Figure 1 shows the XRD patterns of Nb/Al reaction samples sintered at 800 °C for different times. It can be observed that the main phases can be indexed as NbAl<sub>3</sub> and Nb. According to the phase diagram, Nb is inferred as the  $\alpha$ -Nb which is the Nb-rich solid solution of aluminum in niobium. Figure 2 shows the XRD patterns of the samples sintered for 10 h at different sintering temperatures. Compared with the data of Fig. 1, it is obvious that both the changes of temperature and extension of heating duration make no difference to the resultant phase formation. Figure 2 shows the XRD patterns of the samples sintered for 10 h at different sintering temperatures. By comparison, it is apparent that either the change of temperature or extension of heating duration makes no difference to the resultant phase formation.

Thus, it is concluded that the reaction between Nb and Al results in the formation of NbAl<sub>3</sub> under the selected heat-treatment conditions. Furthermore, NbAl<sub>3</sub> is the most thermodynamically stable of the Nb–Al intermediate phases and so the kinetics of conversion to Nb<sub>3</sub>Al by reaction with Nb can be expected to be slow. Consequently, it is



**Fig. 1** XRD patterns of samples sintered at 800 °C

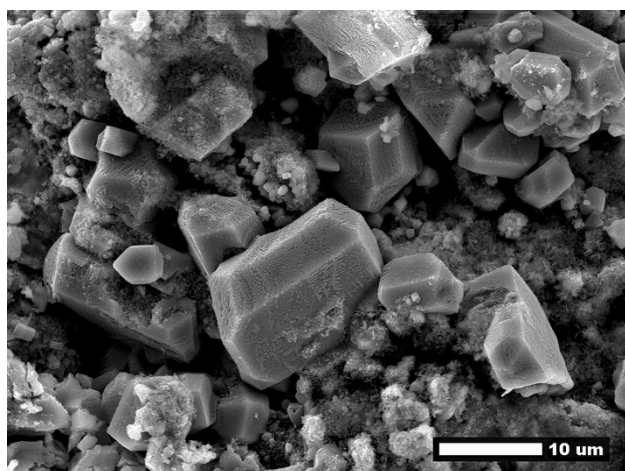


**Fig. 2** XRD pattern of samples sintered at 10 h for different temperatures

concluded that, in the range of 800–1,000 °C, the temperature and duration of heat treatment are not the controlling factors of the formation of Nb<sub>3</sub>Al.

The SEM image of sample sintered at 800 °C for 50 h is displayed in Fig. 3. It can be seen from the picture that the sample is very porous and the size of the biggest grain in this field of view is more than 10  $\mu$ m. The very coarse morphology of the sample would give the diffusion reaction a very long diffusion distance. Considering the very high formation enthalpy [9] of Nb<sub>3</sub>Al, the long diffusion distance between the two grains makes it impossible for the formation of Nb<sub>3</sub>Al using hand milling. The EDX data on grains (see Table 1) support the conclusion that the big grains are NbAl<sub>3</sub>.

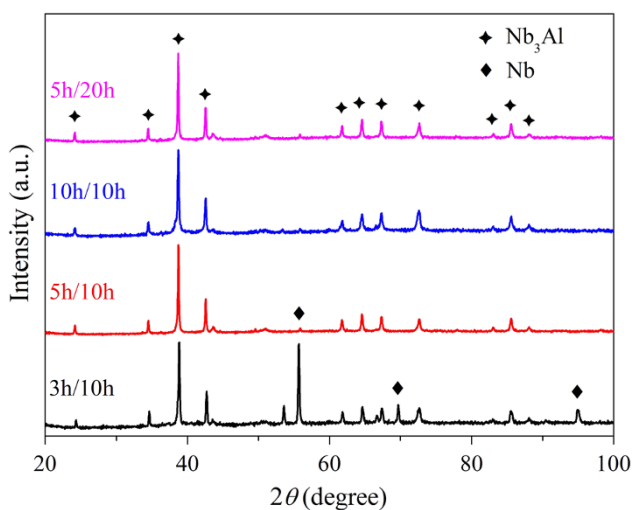
Figure 4 shows the XRD patterns of Nb<sub>3</sub>Al samples prepared for different spex milling and sintering times at



**Fig. 3** SEM image for the sample sintered at 800 °C for 50 h

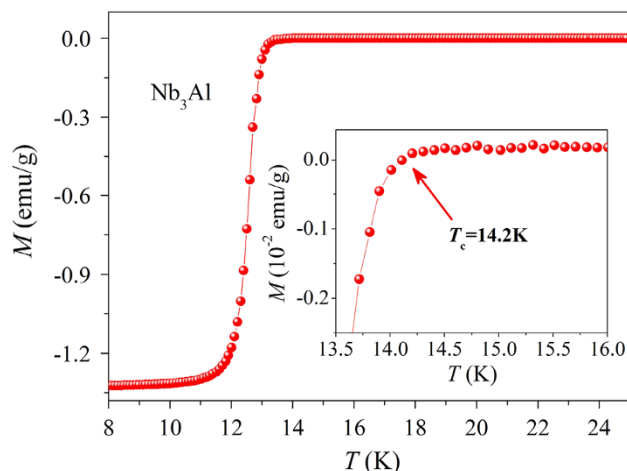
**Table 1** EDX results of a random point on the grain

Element	Weight (%)	Atom (%)
Al	44.0	73.0
Nb	56.0	27.0



**Fig. 4** XRD patterns of the samples prepared for different milling and sintering times at 900 °C

900 °C. The main phase can be indexed as the A15 structure Nb<sub>3</sub>Al. The high-purity Nb<sub>3</sub>Al sample was obtained when the spex milling time reached to 5 h, and spex milling for 10 h and sintering for 10 h gave the optimal sample. The sample that was spex milled for only 3 h contained a great quantity of Nb. This can be explained by short spex milling time; the Nb/Al powders lacked enough extra driving forces for diffusion reaction. Furthermore, it can be seen from all the four patterns that no NbAl<sub>3</sub> phase was found, thus indicating that spex milling is



**Fig. 5** The temperature dependence of magnetization for the Nb<sub>3</sub>Al sample, and *inset* shows the enlarged view of the superconducting transition

effective in increasing the activity of the two powders by improving the mixing and reducing the diffusion distance.

Figure 5 shows the temperature dependence of magnetization for the sample spex milled for 5 h and sintered for 20 h, and the critical temperature ( $T_{\text{conset}}$ ) is 14.2 K which is 4 K lower than the optimal value. The impurity phases and the porous microstructure may give rise to the poor superconducting property, although little impurity phase was indexed from the XRD patterns. It should be noted that no superconducting transition of Nb was detected, which further confirms that the Nb has sufficiently reacted. However, it is important to realize that the Nb<sub>3</sub>Al single phase range is relatively wide according to the phase diagram. In addition, the heat-treatment temperature selected in this work can only give an Nb<sub>3</sub>Al sample with the stoichiometry of only 20 at.% Al. Therefore, the deviation from the right stoichiometric concentration of Aluminum may be another reason that accounts for the low  $T_c$  of the sample, though the sample is an almost-pure single phase as the XRD reflects.

## 4 Conclusions

1. The composition of Nb/Al powder used in the experiment is not in the Nb<sub>3</sub>Al solid solution homogeneity region in phase diagram of Nb–Al binary alloy, but the as-grown sample appears to be single phase.
2. 800 °C is not adequate in terms of kinetics for the equilibration of Nb<sub>3</sub>Al phase formation.
3. Spex milling is effective in increasing activity of the powders by improving the mixing of the powders, simultaneously reducing the diffusion distance. By adoption of spex milling and the conventional PIT

method, fabrication of Nb<sub>3</sub>Al magnet under low temperature can be realized.

4. The impurities and the deviation of the right stoichiometric concentration of aluminum in Nb<sub>3</sub>Al are probably responsible for the poor quality of superconducting transition.
5. Combination of spex milling and the PIT method may be one of the solutions to prepare Nb<sub>3</sub>Al wire under low temperature in the future.

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