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## Operating cost for CO<sub>2</sub> capture process using aqueous ammonia

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### Abstract

In the present paper, we report the result of cost analysis associated with the operation of CO<sub>2</sub> capture pilot facility using aqueous ammonia. The facility treating 1,000 Nm<sup>3</sup>/hr of BFG (blast furnace gas) is in operation with the production capacity of 10 t-CO<sub>2</sub>/d. From the pilot plant operation we found that the CO<sub>2</sub> recovery was 90% and the purity of product CO<sub>2</sub> was over 98%. Waste heat recovery system for steam generation was installed and integrated with the CO<sub>2</sub> capture facility successfully. Operating cost analysis based on the running data of the facility has been performed based on the consumptions of steam, electricity, water, and chemical. Since the process uses waste heat recovery system, the majority of operating cost is the electricity consumption. Excluding the steam cost generated by the waste heat recovery system, the operating cost for the process was estimated under \$20/t-CO<sub>2</sub>.

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### 1. Introduction

As an attempt to mitigate the anthropogenic concentration of carbon dioxide (CO<sub>2</sub>), absorption-based CO<sub>2</sub> capture technologies have been developed at large stationary point sources such as power generation and iron and steel-making plants. Two exemplary absorption solutions are the aqueous amines (advanced amine) and ammonia. Besides superior features such as low chemical cost and corrosiveness, the ammonia solution exhibits at relatively low regeneration temperature /energy rendering a competitive option for CO<sub>2</sub> capture, i.e. it is the most important factor when selecting the absorption solution for CO<sub>2</sub>

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capture. Due to the advantages of the above-mentioned characteristics, researchers have been developing ammonia-based CO<sub>2</sub> capture technologies [1-3].

Iron and steel industry is known to be one of the large CO<sub>2</sub> emitting industry, thus there is a strong need to mitigate the CO<sub>2</sub> emissions. Efforts have been made to develop steel-industry specific CO<sub>2</sub> capture technology removing CO<sub>2</sub> from blast furnace gas (BFG) [3,4]. Recalling the fact that ammonia solution can be regenerated at relatively low regeneration temperature, ammonia-based CO<sub>2</sub> capture technology can utilize low-grade steam which can be generated by recovering waste heat at low temperatures. Therefore, the ammonia-based CO<sub>2</sub> capture process can be very attractive in the iron and steel industry since there are lots of available waste heats at the low temperature range.

Depending on the calculation method, the application sector, location, and time, the operating cost of CO<sub>2</sub> capture facilities can vary considerably. For a pulverized coal-fired power plant, a cost analysis for CO<sub>2</sub> capture using monoethanolamine (MEA) has been performed and the CO<sub>2</sub> capture cost was estimated at \$50-75/t-CO<sub>2</sub> avoided using a process simulator [5]. More recently, a report was released dealing with the commercial & finance topics and the CO<sub>2</sub> avoidance cost range was €30-35/t-CO<sub>2</sub> [6].

In this paper, we report the test result of ammonia-based CO<sub>2</sub> capture technology at POSCO-Pohang Works. A rough estimation of the operating cost of the process has been made based on the pilot plant operation data together with a brief technical performance.

## 2. Method

### 2.1. Process Description

An aqueous ammonia-based CO<sub>2</sub> capture pilot facility has been constructed and in operation at POSCO-Pohang Works since mid-2011. The facility can process BFG at 1,000 Nm<sup>3</sup>/hr resulting in the production of 10 t-CO<sub>2</sub>/d. It is integrated with other sub-facility which comprises an exemplary CO<sub>2</sub> emissions reduction concept in iron and steel industry. After leaving the CO<sub>2</sub> capture facility, the captured CO<sub>2</sub> is converted into CO, a reducing agent, and then fed into BF to reduce the cokes consumption in iron-making process. In the meantime, the thermal energy or steam required for the regeneration of absorbent solution is provided by the waste heat recovery system.

The overall process concept for the CO<sub>2</sub> capture process combined with the waste heat recovery system is depicted in Fig. 1. BFG containing about 20% of CO<sub>2</sub> is processed by the rich solution and product CO<sub>2</sub> is obtained at the top of regenerator or stripper, while the waste heat from flue gas leaving a boiler stack has been recovered and used to generate steam for reboiling. The details of the ammonia-based CO<sub>2</sub> process can be found in the literature [3]. The ammonia-based CO<sub>2</sub> capture process is composed of three columns; absorber, stripper or regenerator, and concentrator. The basic concept for capturing CO<sub>2</sub> is similar to the typical amine-based CO<sub>2</sub> capture system. However, instead of a reclaimer unit for the decomposition of the heat stable salt, the process adopted a concentrator or recovery unit of ammonia. In the concentrator column, the partially carbonated aqueous ammonia from the tops of absorber and stripper is reboiled at ~ 105 °C so that theoretically all the ammonia molecules are vaporized and then fed into the stripper. Washing water is supplied to the tops of regenerator and absorber and to be recycled via concentration column.

CO<sub>2</sub> concentrations in the inlet and outlet of BFG and that in the product stream were measured by NDIR (non-dispersive infrared) CO<sub>2</sub> analyzer. Based on the concentration data, the CO<sub>2</sub> removal efficiency has been calculated.

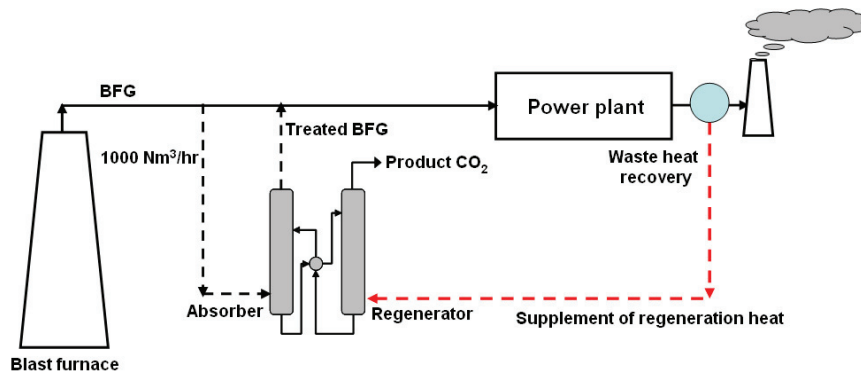


Fig. 1. Process schematic of an ammonia-based CO<sub>2</sub> capture process at POSCO-Pohang Works [7].

## 2.2. Cost evaluation scheme

Total production cost for a chemical plant can be divided by the manufacturing costs and general expenses. The former contains direct production costs, fixed charges, and plant overhead costs, while the latter comprises of administrative expenses and distribution and marketing expenses [8]. The detailed cost analysis should be backed up by process simulation and long-term operation data at a larger scale facility. Moreover, more accurate financial and engineering data are mandatory. However, note that the scope of the work is not to thoroughly investigate the detailed analysis, but rather to provide a rule-thumb figure for process developers.

Accepting the limitations of this work, we can provide a rough estimate of an operating cost based on the current test results. While the operating cost of the CO<sub>2</sub> capture facility is affected by many parameters such as steam requirement, electricity consumption for pumps and cooling tower operation, process water consumption, and chemical loss (make-up cost of chemicals), etc., the majority of operating cost comes from the steam requirement for regeneration and concentration.

Thermal energy consumption (t-steam/t-CO<sub>2</sub>) has been calculated by measuring the steam consumption. The quantity was obtained by the steam consumption flow rate (t-steam/hr) multiplied by 2.2 GJ/t-steam, the heat of vaporization of saturated steam at 1.0 kgf/cm<sup>2</sup>\_g. Typically, the electricity consumption has been measured at every two hours during the run.

## 3. Results and Discussion

### 3.1. Technical performance

The profile of CO<sub>2</sub> removal efficiency is shown in Fig.2. The steam generated by the waste heat recovery is designated as G steam. The efficiency of the CO<sub>2</sub> removal was about 90% and the concentration of CO<sub>2</sub> in the product stream is over 98% (figure not shown). The calorific value of BFG would be increased by 30% due to the selective removal of CO<sub>2</sub> from the supplied BFG. The increase in

calorific value will increase the energy density; therefore, the process volume of BFG for combustion in the power plant could be significantly decreased, which, in turn, will lead to a cost benefit.

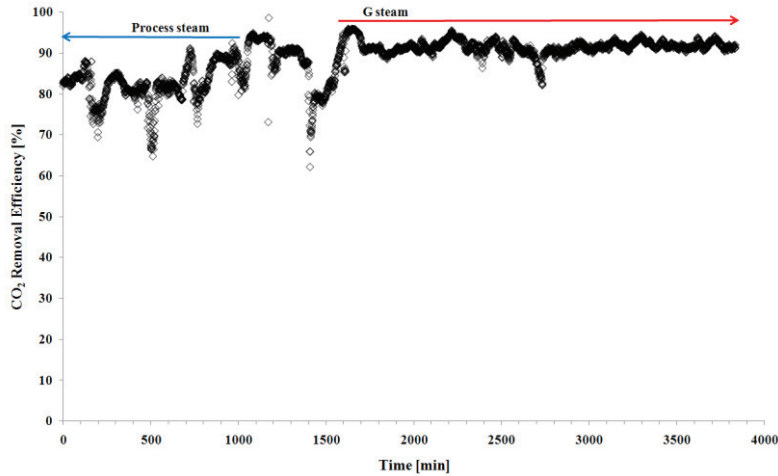


Fig. 2. Profile of CO<sub>2</sub> removal ratio during a test run of the pilot plant operation [7].

### 3.2. Cost analysis using field pilot operation results

Following the previous method for obtaining the operating cost of the process, we obtained the figures in the Table 1. For the process, the largest portion of the CO<sub>2</sub> capture cost was the electricity comprising 60-70%. The cost of electricity and make-up water to operate the waste heat recovery system comprises 20% of the cost. The cost for make-up water for the cooling tower and ammonia makeup due to ammonia loss was 10-15% of total CO<sub>2</sub> capture cost. Based on the pilot plant operation results, CO<sub>2</sub> capture cost was estimated under \$20/t-CO<sub>2</sub> because the process economics were greatly improved by using waste heat to provide the regeneration and concentration energy.

• Table 1. Operating cost of the ammonia-based CO<sub>2</sub> capture pilot plant from this work.

Cost components	Energy/Utility	Cost (\$)	Remark
Steam	~ 5 GJ/t-CO <sub>2</sub>	0	For stripper and concentrator In case of the utilization waste heat
Electricity	~160 kWh/t-CO <sub>2</sub>	~11	
Water	~3 m <sup>3</sup> /t-CO <sub>2</sub>	~1	
Ammonia	~2 kg/t-CO <sub>2</sub>	~1	
Waste heat recovery		~3	Electricity and steam cost
Other expenses		~2	
Total operating cost		<20	

Considering the potential of electricity production by the waste heat, the opportunity cost is about \$ 10/t-CO<sub>2</sub>. It was calculated by considering the sales of the electricity produced by using the Organic Rankine Cycle (ORC). The cycle is one of the efficient electric generation systems in low temperature

range (70~350 °C). The efficiency was assumed to be 10%. Therefore, it can be insisted that the total operating cost is lower than \$ 30/t-CO<sub>2</sub>, even with the opportunity cost of the waste heat.

The steam requirement for the regeneration of aqueous ammonia is somewhat higher than that of amines [4]. However, recall that the steam for CO<sub>2</sub> production can be solely provided by the waste heat recovery system, which makes the process economically outstanding when there is available waste heat at mid and low temperatures.

### *3.3. Potentials to improve the process economics*

From the results and discussion regarding the cost calculation of the CO<sub>2</sub> capture process, it should be stressed that even though the energy consumption is relatively larger than that of other competing technologies, the cost for the operation may not be; Available resources such as waste heat can drastically reduce the energy cost.

Suggestions can be made for the cost reduction of the ammonia-based CO<sub>2</sub> capture processes; ammonia slip prevention, heat integration within the system, process optimization and improvement, etc. Suppression of ammonia slip is of great importance for the commercialization of the ammonia-based CO<sub>2</sub> capture process. Replacing current structured packings with cheaper random packings in the column may be taken into consideration for the reduction of capital investment. Process improvement such as pressurized absorption/regeneration and recycle/reuse of waste stream is quite critical to the process economics. To reduce the operating cost, the process monitoring could be an effective tool. This can be done either by direct sensing of the process and control variables or by statistical and soft-sensing technology since the chemical process is quite complicated.

As discussed earlier, various factors determining the cost of CO<sub>2</sub> capture have to be taken into consideration to reasonably support the decision making process. Some of them are the following: time and duration, location(country) of the plant, fuel cost (for power generation sector) and other financial factors. Lots of financial factors including equipment, facility, utility, and human are affected by the choice of time and location. The following can be suggested for the cost analysis of CO<sub>2</sub> capture technology. Field operation data should be verified by another independent authorized organization. An economic analysis tool can be also applied to accurately deduce the cost analysis.

## **4. Conclusion**

We have confirmed that the ammonia-based CO<sub>2</sub> capture technology can be successfully applied in the iron and steel industry. The CO<sub>2</sub> capture ratio was ~90% and the purity of product CO<sub>2</sub> was over 98%. Moreover, the CO<sub>2</sub> capture system can be successfully integrated with the waste heat recovery system. From a rough estimation on the process economics, we found that the majority of the energy consumption comes from the thermal energy or steam for absorbent regeneration and ammonia recovery. Although the energy consumption at current development status is relatively larger compared to the advanced amine system, the operating cost can be drastically lower than that. If thermal energy could be supplied from the waste heat for stripping and concentration energy, the CO<sub>2</sub> capture cost from BFG can be reduced to less than \$ 20/t-CO<sub>2</sub>. Conclusively, the ammonia-based CO<sub>2</sub> capture technology is extremely functional if there is unrecovered waste heat at low temperature like the iron and steel industry. The detailed process simulation data at larger scale, at least ~100,000 t-CO<sub>2</sub>/yr basis and long-term operation data are prerequisite to the more realistic estimate of the process economics.

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