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# TIME VARYING SOLAR CYCLE PROTONS PROGRAM MANUAL

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BY  
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OCTOBER 1964

NASA

GODDARD SPACE FLIGHT CENTER

GREENBELT, MD.

**TIME VARYING SOLAR CYCLE PROTONS  
PROGRAM MANUAL**

by

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## TABLE OF CONTENTS

	<u>Page</u>
INTRODUCTION . . . . .	1
I. DIURNAL AVERAGED ATMOSPHERE . . . . .	3
II. B-L SEARCH . . . . .	9
A. Introduction . . . . .	9
B. Mnemonics . . . . .	10
C. Flow Charts . . . . .	11
1. Main Program . . . . .	11
2. Subroutine RING . . . . .	13
D. Fortran Listing . . . . .	15
E. Restrictions . . . . .	36
F. Input . . . . .	36
1. Card Description . . . . .	36
2. Sample . . . . .	37
G. Output . . . . .	38
1. Tape 3 Sample . . . . .	39
2. Tape 5 . . . . .	40
a. Card Description . . . . .	41
b. Sample . . . . .	42
H. Running Time . . . . .	43
III. LONGITUDINAL AVERAGING PROCESSOR . . . . .	45
A. Introduction . . . . .	45
B. Mnemonics . . . . .	45
C. Flow Chart . . . . .	48
D. Fortran Listing . . . . .	49
E. Restrictions . . . . .	54
F. Input . . . . .	54
1. Tape 2 . . . . .	54
a. Card Description . . . . .	54
b. Sample . . . . .	55

	<u>Page</u>
2. Tape 5 . . . . .	56
a. Card Description . . . . .	56
b. Sample . . . . .	57
G. Output . . . . .	58
1. Tape 3 Sample . . . . .	59
2. Tape 10 . . . . .	64
a. Card Description . . . . .	64
b. Sample . . . . .	65
H. Running Time . . . . .	66
 IV. LAMBDA PUNCH . . . . .	67
A. Introduction . . . . .	67
B. Mnemonics . . . . .	67
C. Flow Chart . . . . .	69
D. Fortran Listing . . . . .	71
E. Restrictions . . . . .	75
F. Input . . . . .	75
1. Card Description . . . . .	75
2. Sample . . . . .	76
G. Output . . . . .	77
1. Tape 3 Sample . . . . .	78
2. Tape 5 . . . . .	80
a. Card Description . . . . .	80
b. Sample . . . . .	81
H. Running Time . . . . .	82
 V. "BOUNCE" AVERAGE CALCULATION . . . . .	83
A. Introduction . . . . .	83
B. Equations . . . . .	83
C. Mnemonics . . . . .	87
D. Flow Charts . . . . .	89
1. Main Program . . . . .	89
2. Subroutine TABLE . . . . .	90
E. Fortran Listing . . . . .	91

	<u>Page</u>
F. Input . . . . .	99
1. Card Description . . . . .	99
2. Sample . . . . .	100
G. Output . . . . .	101
1. Tape 3 Sample . . . . .	102
2. Tape 5 . . . . .	104
a. Card Description . . . . .	104
b. Sample . . . . .	105
H. Running Time . . . . .	106
 VI. R, $\Sigma$ CALCULATION AND FLUX ELIMINATION . . . . .	107
A. Introduction . . . . .	107
B. Equations . . . . .	107
C. Mnemonics . . . . .	108
D. Flow Charts . . . . .	110
1. Main Program . . . . .	110
2. Subroutine ELIM . . . . .	111
E. Fortran Listing . . . . .	112
F. Input . . . . .	119
1. Card Description . . . . .	119
2. Sample . . . . .	120
G. Output . . . . .	121
1. Tape 3 Sample . . . . .	122
2. Tape 5 . . . . .	127
a. Card Description . . . . .	127
b. Sample . . . . .	129
H. Running Time . . . . .	130
 VII. CONSERVATION EQUATION CALCULATION . . . . .	131
A. Introduction . . . . .	131
B. Equations . . . . .	131
C. Mnemonics . . . . .	133
D. Flow Charts . . . . .	138
1. Main Program . . . . .	138

	<u>Page</u>
2. Subroutine RUNGE . . . . .	139
3. Subroutine DERIV . . . . .	140
4. Subroutine TABLE . . . . .	141
E. Fortran Listing . . . . .	142
F. Restrictions . . . . .	157
G. Input . . . . .	157
1. Card Description . . . . .	158
2. Sample . . . . .	160
H. Output . . . . .	161
1. Transient Steady-State Sample . . . . .	162
2. Tape 5 Time History Sample . . . . .	164
3. Time-Averaged Steady-State Sample . . . . .	166
I. Running Time . . . . .	168
<b>VIII. STEADY-STATE CALCULATION . . . . .</b>	<b>169</b>
A. Introduction . . . . .	169
B. Equations . . . . .	169
C. Mnemonics . . . . .	170
D. Flow Charts . . . . .	174
1. Main Program . . . . .	174
2. Subroutine TABLE . . . . .	175
E. Fortran Listing . . . . .	176
F. Input . . . . .	182
1. Card Description . . . . .	182
2. Sample . . . . .	184
G. Output . . . . .	185
H. Running Time . . . . .	189
<b>IX. REFERENCES . . . . .</b>	<b>191</b>
<b>X. ILLUSTRATIONS . . . . .</b>	<b>193</b>

## LIST OF FIGURES

<u>Figure</u>		<u>Page</u>
1.	A time history of the 10.7 cm solar flux according to the measurements of the National Research Council of Canada for the recent past. The heavy dotted line indicates the approximate yearly average. . . . .	193
2.	A mapping of the polar coordinates $R$ and $\lambda$ onto the B-L plane where $R = (h + 6378.2)$ . . . . .	194
3.	B-L contours for the northern hemisphere at an $L$ of 1.25 earth radii. . . . .	195
4.	B-L contours for the southern hemisphere at an $L$ of 1.25 earth radii. . . . .	196
5.	Schematic of a trapped particle's north-south motion. . . . .	197
6.	The weighing factor, $A(\lambda)$ , versus latitude for various mirror latitudes, $\lambda_0$ , where $\lambda_0$ are the asymptotes of each curve. . . . .	198
7.	A time history of the atmosphere scale factor, $R$ , as a function of $B$ at $L = 1.25$ e.r. . . . .	199
8.	A time history of the atmospheric loss parameter, $\Sigma$ , as a function of $B$ at $L = 1.25$ e.r. . . . .	200
9.	A time history of the constructed mean solar cycle variation of the 10.7 cm solar flux with reference time $t_0$ of Jan., 1954. .	201
10.	A time history of the relative inner belt source strength. . .	202
11.	The proton energy loss spectrum for an oxygen target. . . .	203
12.	The slope of proton energy loss versus energy for an oxygen target. . . . .	204
13.	A comparison of the steady-state and transient proton flux energy spectrums for $L = 1.25$ , $B = .199$ at solar minimum and solar maximum. . . . .	205

<u>Figure</u>		<u>Page</u>
14.	The time required in terms of solar cycles to build steady-state conditions versus energy as a function of B. . . . .	206
15.	A time history of proton flux as a function of energy at L = 1.25, B = .209 for the first and tenth solar cycles. . . . .	207

### LIST OF TABLES

<u>Table</u>		<u>Page</u>
1.	Diurnal averaged number densities of Helium (He) as a function of altitude for five solar flux numbers. . . . .	4
2.	Diurnal averaged number densities of Oxygen (O) as a function of altitude for five solar flux numbers. . . . .	5
3.	Diurnal averaged number densities of Molecular Oxygen ( $O_2$ ) as a function of altitude for five solar flux numbers. . . . .	6
4.	Diurnal averaged number densities of Nitrogen ( $N_2$ ) as a function of altitude for five solar flux numbers. . . . .	7
5.	Diurnal averaged number densities of Hydrogen (H) as a function of altitude for five solar flux numbers. . . . .	8

## TIME VARYING SOLAR CYCLE PROTONS PROGRAM MANUAL

### INTRODUCTION

The purpose of this manual is to provide a detailed description of the programs employed in calculating the variation of the proton population in the earth's radiation belt due to solar cycle atmospheric and source changes. This report makes no attempt to make detail explanations of the theory involved in the calculations. An adequate list of references is provided for those interested in the explanation of the methods and the results to be expected. The entire process involves several interdependent steps. For example, the diurnal averaged atmosphere and the rings output from the B-L search routine are input to the longitudinal averaging processor. The output from this program is then used as input to the "bounce" average program and so forth. Each program description includes the equations used, a flow chart and Fortran listing of the program, input and output specifications, card descriptions, sample input and output data and running time. The code is written in Fortran II language and assembled under GSFC-NASA Theoretical Division monitor system on the IBM-7094 computer.

## I. DIURNAL AVERAGED ATMOSPHERE

Contained here are tables of number density vs. altitude and solar flux number. Separate tables of He, O, O<sub>2</sub>, N<sub>2</sub> and H are contained in Tables 1-5. The models are those generated by Harris and Priester.<sup>(2)</sup> Each model refers to a given solar radiation flux in units of  $10^{-22}$  watts/m<sup>2</sup>/cycle/sec. The link between solar flux, S, and time is given by Figure 1 (reproduced from reference 2 with the permission of Harris and Priester). This data is included for continuity and is used as input for the longitudinal averaging processor. The Harris and Priester atmosphere and solar flux vs. time curve is the data used and is subject to change as soon as better data becomes available. Such changes can be performed without effecting the logic of the following programs.

Table 1  
 Diurnal Averaged Number Densities of He as a  
 Function of Altitude for Five Solar Flux Numbers.

S h(km.)	250	200	150	100	70
120	2.500E07	2.500E07	2.500E07	2.500E07	2.500E07
200	4.413E06	4.872E06	5.484E06	6.319E06	6.982E06
300	2.642E06	2.843E06	3.050E06	3.205E06	3.212E06
400	1.945E06	2.007E06	2.012E06	1.885E06	1.689E06
500	1.499E06	1.477E06	1.390E06	1.154E06	9.272E05
600	1.176E06	1.107E06	9.646E05	7.236E05	5.231E05
700	9.327E05	8.387E05	6.842E05	4.607E05	3.021E05
800	7.461E05	6.422E05	4.916E05	3.004E05	1.783E05
900	6.016E05	4.964E05	3.574E05	1.984E05	1.074E05
1000	4.886E05	3.871E05	2.628E05	1.331E05	6.593E04
1100	3.995E05	3.044E05	1.953E05	9.050E04	4.119E04
1200	3.287E05	2.411E05	1.466E05	6.238E04	2.616E04
1300	2.721E05	1.925E05	1.110E05	4.353E04	1.687E04
1400	2.265E05	1.547E05	8.482E04	3.074E04	1.104E04
1500	1.895E05	1.251E05	6.537E04	2.195E04	7.328E03
1600	1.595E05	1.019E05	5.078E04	1.584E04	4.925E03
1700	1.348E05	8.346E04	3.974E04	1.155E04	3.351E03
1800	1.145E05	6.875E04	3.133E04	8.497E03	2.306E03
1900	9.774E04	5.696E04	2.487E04	6.308E03	1.605E03
2000	8.378E04	4.743E04	1.988E04	4.724E03	1.128E04

Table 2  
 Diurnal Averaged Number Densities of O as a  
 Function of Altitude for Five Solar Flux Numbers.

S h(km.)	250	200	150	100	70
120	7.600E10	7.600E10	7.600E10	7.600E10	7.600E10
200	3.600E09	3.457E09	3.209E09	2.795E09	2.416E09
300	8.870E08	7.134E08	5.124E08	2.809E08	1.564E08
400	3.054E08	2.054E08	1.112E08	4.025E07	1.471E07
500	1.168E08	6.616E07	2.788E07	6.771E06	1.675E06
600	4.749E07	2.287E07	7.708E06	1.273E06	2.183E05
700	2.024E07	8.364E06	2.232E06	2.611E05	3.153E04
800	8.983E06	3.207E06	6.918E05	5.747E04	4.946E03
900	4.130E06	1.282E06	2.252E05	1.342E04	8.320E02
1000	1.960E06	5.312E05	7.645E04	3.301E03	1.488E02
1100	9.567E05	2.275E05	2.696E04	8.502E02	2.810E01
1200	4.791E05	1.003E05	9.834E03	2.284E02	5.381E00
1300	2.456E05	4.538E04	3.701E03	6.379E01	1.162E00
1400	1.287E05	2.106E04	1.434E03	1.848E01	2.527E-1
1500	6.878E04	9.997E03	5.706E02	5.541E00	5.729E-2
1600	3.746E04	4.849E03	2.330E02	1.717E00	1.352E-2
1700	2.077E04	2.399E03	9.744E01	5.486E-1	3.312E-3
1800	1.170E04	1.210E03	4.170E01	1.806E-1	8.412E-4
1900	6.700E03	6.216E02	1.824E01	6.079E-2	2.212E-4
2000	3.893E03	3.247E02	8.149E00	2.128E-2	6.010E-5

Table 3  
 Diurnal Averaged Number Densities of O<sub>2</sub> as a  
 Function of Altitude for Five Solar Flux Numbers.

S h(km.)	250	200	150	100	70
120	1.200E11	1.200E11	1.200E11	1.200E11	1.200E11
200	9.900E08	7.910E08	5.699E08	3.438E08	2.151E08
300	7.683E07	4.269E07	1.791E07	4.503E06	1.188E06
400	1.020E07	4.069E06	1.048E06	1.191E05	1.427E04
500	1.217E06	4.886E05	7.983E04	4.808E03	2.444E02
600	3.142E05	6.758E04	7.106E03	1.857E02	5.155E00
700	6.428E04	1.033E03	7.062E02	9.135E00	1.265E-1
800	1.364E04	1.714E03	7.688E01	5.002E-1	3.528E-3
900	3.242E03	3.031E02	8.962E00	3.010E-2	1.102E-4
1000	7.981E02	5.682E01	1.122E00	1.975E-3	3.821E-6
1100	2.056E02	1.122E01	1.493E-1	1.403E-4	1.459E-7
1200	5.526E01	2.322E00	2.106E-2	1.074E-5	5.274E-9
1300	1.544E01	5.028E-1	3.139E-3	8.835E-7	2.788E-10
1400	4.474E00	1.136E-1	4.927E-4	7.772E-8	1.382E-11
1500	1.342E00	2.778E-2	8.124E-5	7.292E-9	7.412E-13
1600	4.157E-1	6.520E-3	1.405E-5	7.277E-10	4.288E-14
1700	1.328E-1	1.653E-3	2.541E-6	7.702E-11	2.667E-15
1800	4.370E-2	4.342E-4	4.800E-7	8.627E-12	1.777E-16
1900	1.478E-2	1.177E-4	9.452E-8	1.200E-12	1.267E-17
2000	5.142E-3	2.906E-5	1.937E-8	1.270E-13	9.626E-19

Table 4  
 Diurnal Averaged Number Densities of N<sub>2</sub> as a  
 Function of Altitude for Five Solar Flux Numbers.

S h(km.) \	250	200	150	100	70
120	5.800E11	5.800E11	5.800E11	5.800E11	5.800E11
200	7.393E09	6.180E09	4.743E09	3.136E09	2.124E09
300	7.630E08	4.639E08	2.210E08	6.739E07	2.113E07
400	1.278E08	5.777E07	2.151E07	2.682E06	4.225E05
500	2.562E07	8.798E06	1.810E06	1.407E05	1.156E04
600	5.730E06	1.521E06	3.239E05	8.800E03	3.844E02
700	1.403E06	2.884E05	2.763E04	6.190E02	1.471E01
800	3.664E05	5.883E04	3.899E03	4.802E01	6.320E-1
900	1.012E05	1.276E04	5.894E02	4.057E00	3.006E-2
1000	2.932E04	2.918E03	9.470E01	3.702E-1	1.570E-3
1100	8.862E03	6.994E02	1.609E01	3.627E-2	8.936E-5
1200	2.783E03	1.725E02	2.878E00	3.798E-3	1.016E-5
1300	9.053E02	4.558E01	5.404E-1	4.237E-4	3.674E-7
1400	3.041E02	1.233E01	1.063E-1	5.017E-5	2.633E-8
1500	1.075E02	3.456E00	2.183E-2	6.287E-6	2.023E-9
1600	3.768E01	1.002E00	4.677E-3	8.321E-7	1.661E-10
1700	1.380E01	3.001E-1	1.042E-3	1.160E-7	1.454E-11
1800	5.211E00	9.268E-2	2.313E-4	1.699E-8	1.353E-12
1900	2.005E00	2.949E-2	5.746E-5	2.612E-9	1.334E-13
2000	7.927E-1	9.654E-3	1.431E-5	4.619E-10	1.393E-14

Table 5  
 Diurnal Averaged Number Densities of H as a  
 Function of Altitude for Five Solar Flux Numbers.

S h(km.) \	250	200	150	100	70
120	4.356E04	4.356E04	4.356E04	4.356E04	4.356E04
200	1.071E04	1.224E04	1.447E04	1.790E04	2.104E04
300	8.035E03	9.323E03	1.114E04	1.380E04	1.611E04
400	7.205E03	8.328E03	9.837E03	1.189E04	1.352E04
500	6.690E03	7.660E03	8.898E03	1.046E04	1.157E04
600	6.272E03	7.102E03	8.107E03	9.263E03	9.974E03
700	5.904E03	6.609E03	7.415E03	8.214E03	8.638E03
800	5.573E03	6.168E03	6.803E03	7.360E03	7.518E03
900	5.272E03	5.769E03	6.260E03	6.597E03	6.571E03
1000	4.996E03	5.408E03	5.774E03	5.933E03	5.768E03
1100	4.742E03	5.079E03	5.339E03	5.352E03	5.083E03
1200	4.502E03	4.778E03	4.947E03	4.843E03	4.495E03
1300	4.291E03	4.503E03	4.594E03	4.395E03	3.989E03
1400	4.090E03	4.250E03	4.275E03	3.998E03	3.552E03
1500	3.903E03	4.018E03	3.986E03	3.647E03	3.173E03
1600	3.730E03	3.804E03	3.723E03	3.335E03	2.843E03
1700	3.568E03	3.606E03	3.484E03	3.057E03	2.555E03
1800	3.417E03	3.424E03	3.266E03	2.809E03	2.303E03
1900	3.276E03	3.255E03	3.066E03	2.587E03	2.081E03
2000	3.144E03	3.098E03	2.884E03	2.387E03	1.886E03

## II. B-L SEARCH

### A. Introduction

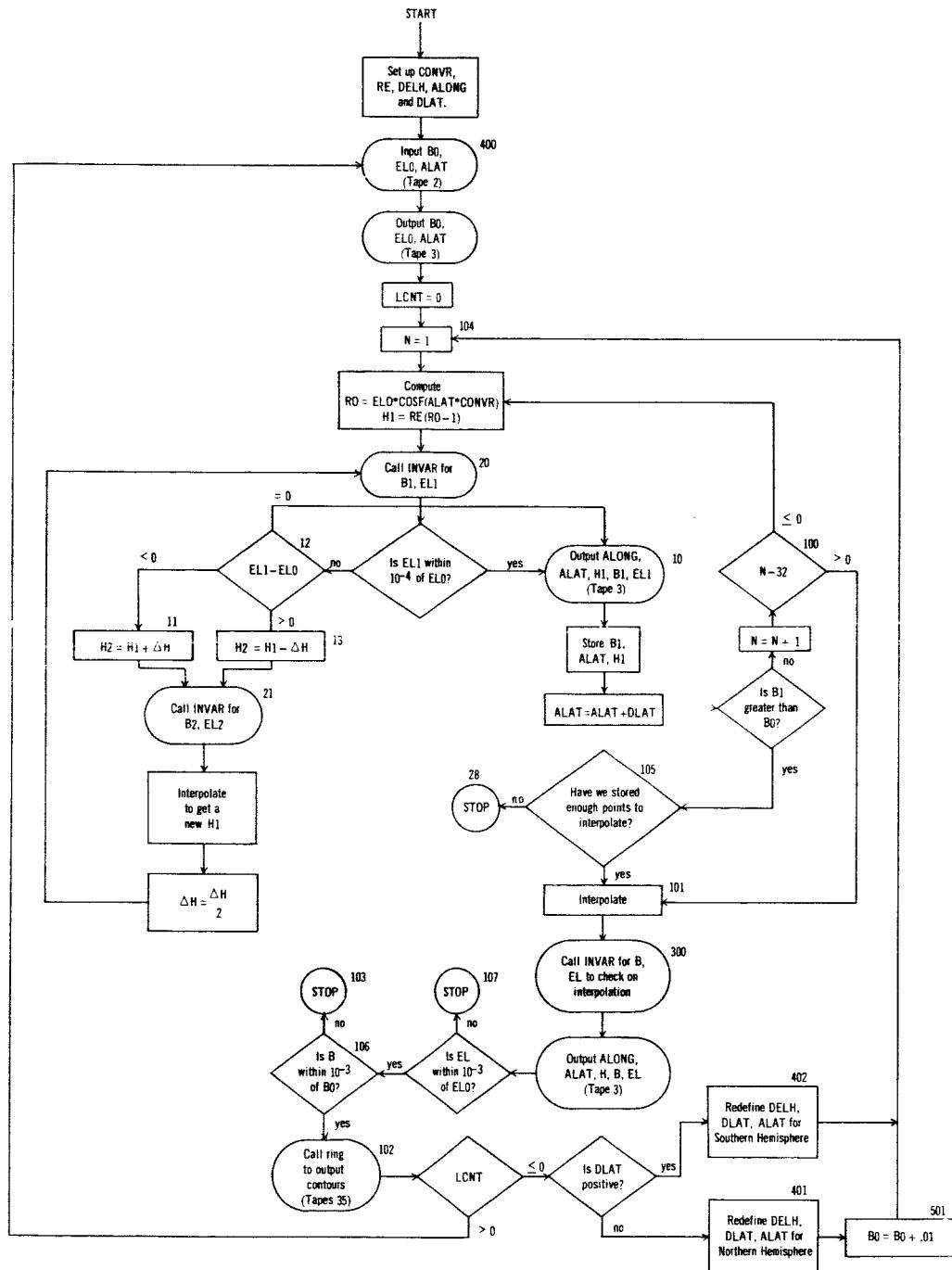
This program produces contours of constant B and L as a function of longitude, latitude and altitude in both the northern and southern hemispheres. The desired initial values of B and L are read into the program along with an approximate corresponding latitude,  $\lambda$ , which can easily be obtained by the use of Figure 2. The dipole equation  $r_0 = L_0 \cos^2 \lambda$  relating the initial L and the geocentric distance  $r_0$  is used with the radius of the earth,  $r_e$ , and the equation  $h_1 = r_e (r_0 - 1)$  to provide an approximation of the altitude. This is fed, together with a longitude of 180 degrees and latitude  $\lambda$ , into subroutine INVAR which calculates B and L for a given longitude, latitude and altitude. This subroutine makes use of the transformation developed by McIlwain<sup>(3)</sup> using the 48 spherical harmonic coefficients of Jenson and Cain<sup>(4)</sup>. INVAR numerically integrates the longitudinal invariant I using a series expansion for the magnetic field. Then L is calculated as a function of both B and I by using a dipole representation of the earth. The B and L obtained in this manner are returned to the main program. Here the accuracy of the initial approximation is checked. If the computed L is found to be within an accuracy of  $10^{-4}$  of the initial L the program will enter into a search routine with linear interpolation in latitude and altitude in order to arrive at a correct B. The search parameters  $\Delta h$  (increment in altitude) and  $\Delta \lambda$  (increment in latitude) are prefixed and must remain small in order that interpolation may hold. Once B is found, it is checked, together with the value of L, to insure an accuracy of  $10^{-3}$  in comparison with the initial values. If the accuracy is sufficient the subroutine RING will be called for the northern hemisphere. This subroutine takes a given latitude and altitude and computes the B and L contour map for longitudes of 10 degree increment for the full 360 degrees. The program then computes the contour map for the southern hemisphere at the same B and L, increments B by .01 gauss and returns to the northern hemisphere. It will continue in this manner until the altitude drops below 100 kilometers, at which point the next initial B, L and  $\lambda$  will be read until input data is exhausted. The entire process prepares input for the longitudinal averaging processor.

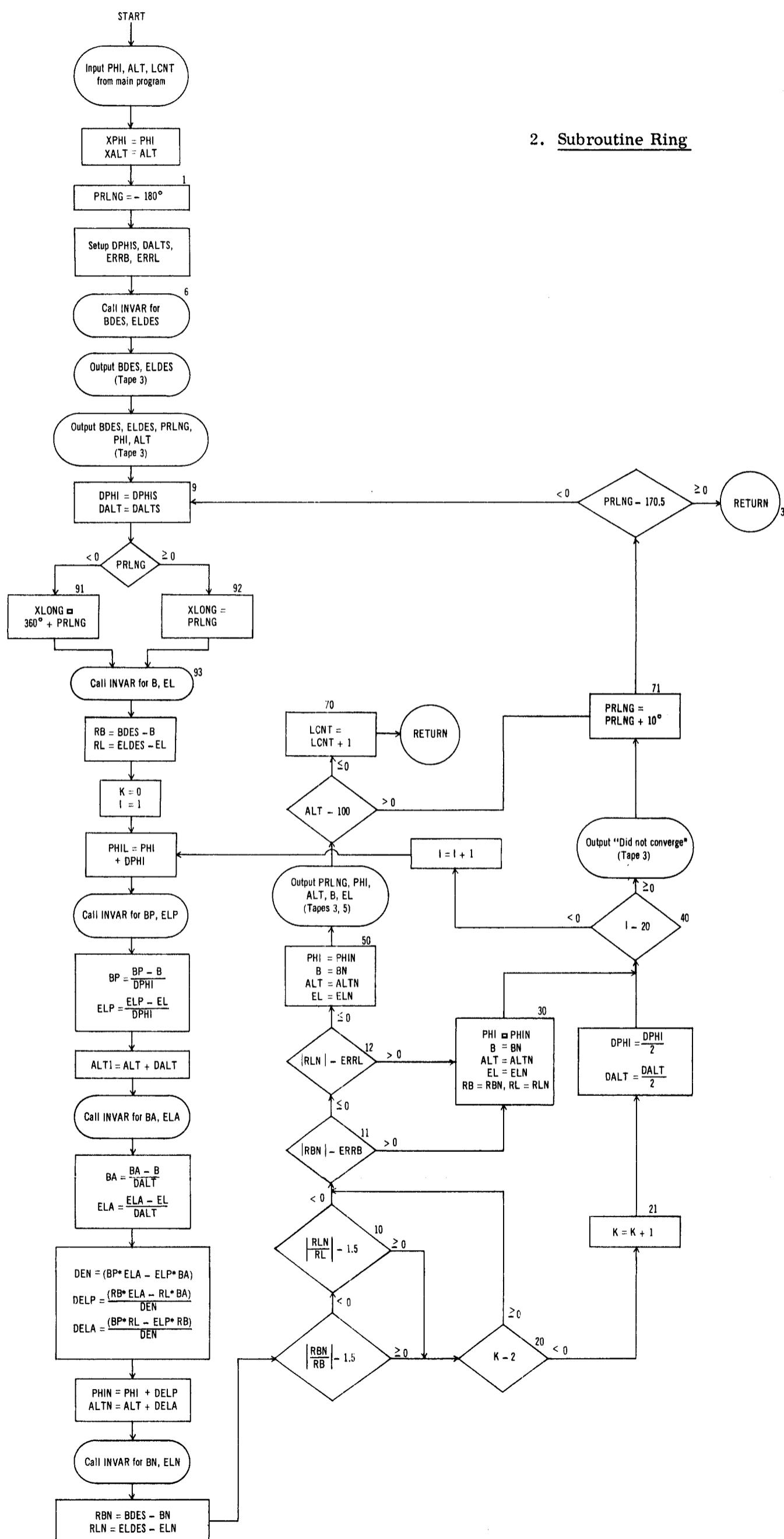
## B. Mnemonics

Quantity	Description	Units
CONVR	conversion factor - degrees to radians	--
RE	radius of the earth	km.
DELH	delta altitude	km.
ALONG	geocentric longitude	degrees
DLAT	delta latitude	"
ALAT	geocentric latitude	"
B	magnetic induction	gauss
EL	magnetic field line	earth radii
R	geocentric distance	"
H	altitude	km.
SAVB	temporary storage of B	gauss
SAVH	temporary storage of H	km.
SAVLAT	temporary storage of ALAT	degrees
LCNT	an indicator used to indicate when the altitude has dropped below 100 km.	--

## C. Flow Charts

### 1. Main Program





## 2. Subroutine Ring

#### D. Fortran Listing

```

C   B-L SEARCH
C   DIMENSION SAVB(32),SAVLAT(32),SAVH(32)
1  FORMAT(2F12.5,F8.5)
2  FORMAT(5X,42H INTERMEDIATE RESULTS--NORTHERN HEMISPHERE)
3  FORMAT(5X,42H INTERMEDIATE RESULTS--SOUTHERN HEMISPHERE)
4  FORMAT(8X,4H LONG,BX,3BLAT,9X,3BLAT,10X,1HB11X,1HB1)
5  FORMAT(4H1B0=1F8.5,4X,4H LO=1F8.5,4X,13H INITIAL LAT=1F8.5)
6  FORMAT(1HL,5X,42H INTERMEDIATE RESULTS--NORTHERN HEMISPHERE)
7  FORMAT(1HL,5X,42H INTERMEDIATE RESULTS--SOUTHERN HEMISPHERE)
8  FORMAT(36H0VALUE OF B IS NOT WITHIN •COL OF R0)
9  FORMAT(60HINTERPOLATION CANNOT PROCEED--MAKE INITIAL LATITUDE SM
      ALLER)
10 FORMAT(37H0VALUE OF L IS NOT WITHIN •COL OF E0)
400 READ INPUT TAPE 2,1,B0,E0,ALAT
      WRITE OUTPUT TAPE 3,5,B0,E0,ALAT
      WRITE OUTPUT TAPE 3,3
      WRITE OUTPUT TAPE 3,4
      CONVR=.01745333
      RE=6370.2
      DELH=100.
      ALONG=180.
      CLAT=2.
      ALATO=ALAT
      LCNT=C
1C4  DU 100 N=1,32
      K0=E0,*COSF(ALAT*CONVR)**2
      H1=RE*(R0-1.)
      CALL INVAR(ALAT,ALONG,H1,.01,E1,EL1)
      CKEL=EL1-EL0
      IF(ABS(CKEL)-1.E-4)>14,14,12
12  IF(CKEL) 11,14,13
13  H2=H1-DELH
      H1=H1-(EL1-EL0)*(H1-H2)/(EL1-EL2)
      DELH=DELH/2.
      GU TO 20
11  H2=H1+DELH
      GU TO 21
14  WRITE OUTPUT TAPE 3,2,ALONG,ALAT,H1,B1,tL1
      SAVB(N)=b1
      SAVLAT(N)=ALAT
      ALAT=ALAT+ULAT
      I+(R1-B0) 100,100,105
1C0  CONTINUE
1C5  IF (N-1) 28,29,101
      28  WRITE OUTPUT TAPE 3,9
      CALL EXIT
101 DO 200 I=1,32
      1F(SAVB(I)-B0) 200,30,31
      31  AL2=SAVLAT(I)
      02=SAVb(I)
      H2=SAVH(I)
      AL1=SAVLAT(I-1)
      b1=SAVb(I-1)

```

```

H1=SAYF((1-1)
ALAT=AL2-(AL2-AL1)*(H1-H2)/(H2-H1)
GC TO JCU
50 H=SVN((1)
ALAT=SAVLAT((1)
H=SAVH((1)
GC TO JCU
260 CCNT TUE
360 CALL INVARI(LAT,ALUNG,H,01,B,E)
WRITE OUTPUT TAPE 3,2,ALUNG,ALAT,R,U,EL
GUE=EL-ELO
IF (AB,F(GKL)-1.E-3) 106,1U6,1U7
137 WRITE OUTPUT TAPE 3,1G
CALL E(XI)
166 GRB=B-B0
IF (AC3(FGRB)-1.E-3) 102,1G2,1O3
163 WRITE OUTPUT TAPE 3,8
CALL E(XI)
102 CALL 3ING(ALAT,H,LCNT)
IF (LC,1) 403,403,4C0
4C3 IF (ALAT) 401,401,402
402 EUE=1G.
GLAT=-E
IF (ALAT<-1.) 5CC,501,5G1
5G0 ALAT=-1.
GC TO JCU
5G1 ALAT=-ALATG+11.
5G2 WRITE OUTPUT TAPE 3,6
WRITE OUTPUT TAPE 3,4
GL TO 104
DLH=100.
DLAT=2.
ALAT=ALAT0+1.
ALAT0=ALAT
DU=60.*CL
WRITE OUTPUT TAPE 3,7
WRITE OUTPUT TAPE 3,4
GC TO 104
E:D1,1,U,C,O,O,1,U,C,G,C,U,O)

```

## STORAGE NOT USED BY PROGRAM

	DEC	OCT	DEC	OCT
624	01160	32561	77461	

## STORAGE LOCATIONS FOR VARIABLES APPEARING IN DIMENSION AND EQUIVALENCE STATEMENTS

S A V B	DEC	OCT	DEC	OCT	DEC	OCT	DEC	OCT	DEC	OCT
	623	01157	SAVH	559 01057	SAVAT	591 01117				

## STORAGE LOCATIONS FOR VARIABLES NOT APPEARING IN COMMON, DIMENSION, OR EQUIVALENCE STATEMENT

	DEC	OCT	DEC	OCT	DEC	OCT	DEC	OCT	DEC	OCT
AL1	527	11017	AL2	526 01016	ALATO	525 01015	ALAT	524 C1C14	ALONG	523 01013
B0	522	01012	B1	521 C1011	H2	520 01010	B	519 C1CC7	CkB	518 01CC6
CKEL	517	01005	CKL	516 C1004	CUNVR	515 01003	DLBLH	514 01002	DLAT	513 01001
LLO	512	01000	L1	511 01077	LL2	510 00776	EL	509 C0775	H1	508 C0774
H2	507	01773	H	506 C0172	I	505 00771	LCNT	504 C0770	N	503 00767
R0	502	C0765	RE	5C1 C0765						

## SYMBOLS AND LOCATIONS FOR SOURCE PROGRAM FORMAT STATEMENTS

	EFN	DEC	EFN	DEC	EFN	DEC	EFN	DEC	EFN	LOC
01	1	C0157	012	2	00754	013	3	00752	014	00741
016	c	C0720	017	f	0106	018	b	00674	019	9 C0665

## LOCATIONS FOR OTHER SYMBOLS NOT APPEARING IN SOURCE PROGRAM

	DEC	OCT	DEC	OCT	DEC	OCT	DEC	OCT	DEC	OCT
1)	496	C0760	2)	399 00617	3)	403 00623	4)	32767 77777	6)	413 00635
C)G0	459	C0763	C)G1	3C0 00164	D)IGF	204 00314	D)20L	266 00412	D)4C1	15 CC017
C)401	164	C0275	D)G01	14 00016	E)5	110 00156	E)8	145 00221	L)S	15C 00226
C)C	188	C0274	E)F	202 C0312	E)H	211 00323	E)J	263 C04C7	E)N	311 C0467
C)P	330	C0512	E)R	345 00531	E)101	17 00021				

## LOCATIONS OF NAMES IN TRANSFER VECTOR

	DEC	OCT	DEC	OCT	DEC	OCT	DEC	OCT	DEC	OCT
C)S	0EC	CC1	EXIT	7 C007	INVAR	6 00006	RING	8 C0010	(FILE)	4 CCC04
(FPT)	0	CC000	(RTN)	2 C0002	(STH)	3 00003	(TSH)	1 C0011		

## ENTRY POINTS TO SUBROUTINES NOT OUTPUT FROM LIBRARY

C)S	LSTF	INVAR	RING	(FILE)	(FPT)	(RTN)	(STH)	(TSF)

## EXTERNAL FORMULA NUMBERS WITH CORRESPONDING INTERNAL FORMULA NUMBERS AND OCTAL LOCATIONS

	EFN	IFN	LLC	EFN	IFN	LLC	EFN	IFN	LLC	EFN	IFN	LLC
400	1	C0G23	1C4	26 C0011	20	2y 00134	12	33 00160	13	34 00164	13	34 00164
21	3	C0167	11	4C C0222	14	4z 00227	1C	49 C0272	1C5	50 C0276		
28	51	C0102	101	53 C0013	31	5z 00325	30	64 C0316	2C	68 CC410		
300	59	C0413	107	65 C0457	106	7f 00471	103	79 C0502	102	81 C0514		
403	84	C0225	402	d5 C0533	5C0	8b 00543	501	90 C0546	502	91 C0551		
401	94	C0566										

```

Subroutine XING(PHI,ALI,LGNT)
101  FLR=AT(2,X,14H FINAL RESULTS)
102  FORK(I,I1P,I2D,NCT CONVERGE)
103  FORK(I(3),I2,2,2,I2,I2)
104  FORK(I(3),I3,I4X,3H L=1F8.5)
105  DPH,I3=4,G
CALTS=5,G
LXRH=1.0E-4
LXR=1.G-3
XPHI = PHI
XALI = ALI
1  PRNG=-150.C
CALL INVAR(PHI,18C.,ALI,G.C1,BUS,ELNS)
6  WRITE OUTPUT TAPE 3,107,BUES,ELNS
WRITE OUTPUT TAPE 3,101,BUES,ELNS
9  WRITE OUTPUT TAPE 3,162,PRNG,PHI,ALI,BUes,BLDES
DPHI=DPHS
ALAI=ALIS
IF (PRNG) 91,92,92
91  XLONG = 36C. + PRNG
92  TO 93
93  CUNITLE
C COMPUTE d AND L
CALL INVAR(PHI,XLONG,ALI,G.C1,d,LL)
KB=BLCSUB
RL=ELDES-EL
COMPUTE PARTIALS
K=0
DO 40 I=1,20
PHII=PHI+EP*I
CALL INVAK(PHI,XLONG,ALI,G.C1,EP,ELP)
EP=(EP-B)/DPHI
ELP=(ELP-EL)/DPHI
ALTI=ALI+CALT
CALL INVAR(PHI,XLONG,ALI,G.C1,BA,ELA)
ELA=(ELA-EL)/CALT
ELA=(ELA-EL)/CALT
COMPUTE CORRECTIONS
DEN=EP*ELA-ELP*DA
UDLP=(RD*ELA-RL*BA)/DEN
UELA=(UP*RL-ELP*RB)/DEN
PHN=PHI-DEL P
ALTN=ALI+DELA
CALL INVAK(PHI,XLONG,ALTN,0.01,BN,ELN)
BN=BUes-BN
RN=ELDES-ELN
IF (AUSF(KBN/RB)-1.5) 10,20,20
20  IF (K<-2) 21,11,11
21  K=K+1
DPHI=DPHI/2.
LALT=CALV/2.
GO TO 40
10  IF (AUSF(RLN/RL)-1.5) 11,20,20
11  IF (AUSF(RBN)-ERR) 12,12,3C

```

```

12 IF (ABS(F(RLN)-ERRRL) .GT. .5C,50,30
30 PHI=PHIN
L=BN
ALT=ALIN
EL=ELIN
RL=RLIN
RH=RHIN
KL=RLIN
40 GOTO 100
      WRITE (UNIT TAPE 3,102
      PRLNG=PRLNG+1C.
      IF (PRLNG-18G.*5) 9,3,3
      PHI=PHIN
50 b=BN
ALT=ALIN
EL=ELIN
      WRITE (UNIT TAPE 3,103,PRLNG,PHI,AL1,b,LL
      WRITE (UNIT TAPE 5,103,PRLNG,PHI,AL1,b,C_L
      IF (AL1-100.) 70,7C,71
      PRLNG=PRLNG+10.
      71 IF (PRLNG-17C.*5) 9,3,3
      72 GOTO 40
      LCN=LCN+1
      RETURN
      END(1,1,0,0,0,0,1,0,0,0,0,0)

```

## STORAGE NC1 USED BY PROGRAM

DEC CCI  
423 CC647

DEC CCT  
3561 17461

## STORAGE LOCATIONS FOR VARIABLES NOT APPEARING IN COMMON, DIMENSION, OR EQUIVALENCE STATEMENT

	DEC	LCT	DEC	OCT	DEC	OCT	DEC	CCT	DEC	OCT
ALTI	422	CC646	ALIN	421 00645	RA	420 00644	BUES	419 CC643	BN	418 00642
BP	417	CC641	B	416 00640	DALT	415 00637	CALTS	414 00636	DELA	413 00635
BLIP	412	CC634	BLN	411 00633	DPHI	410 00632	DPHS	409 00631	ELA	408 CC630
BLUES	407	CC627	BLN	406 00626	ELP	405 00625	EL	404 CC624	ERRB	403 CC623
ERRL	402	CC622	I	401 00621	K	400 00620	PHI	399 CC617	PHIN	398 00616
FRNG	397	00615	RBN	396 00614	R6	395 00613	RLN	394 00612	RL	393 00611
XALT	392	CC610	XLONG	391 00607	XPHI	390 00606				

## SYMBOLS AND LOCATIONS FOR SOURCE PROGRAM FORMAT STATEMENTS

	EFN	LCC	EFN	LCC	EFN	LCC	EFN	LCC
8)35	101	CC6C2	8)36	102 CC576	8)37	103 0072	8)38	107 CC567

## LOCATIONS FOR OTHER SYMBOLS NOT APPEARING IN SOURCE PROGRAM

	DEC	CCT	DEC	CCT	DEC	CCT	DEC	CCT
1)	387	00603	2)	347 CC533	3)	352 00540	6)	365 CC555
1)201	88	00130	0)401	335 00517	E)9	231 00347	C)8	243 00363
E)H	326	00506						

## LOCATIONS OF NAMES IN TRANSFER VECTOR

	DEC	OCT	DEC	OCT	DEC	CCT	DEC	CCT
INVAR	DEC CCI 6 CC6C0	(FILE)	DEC 2 CC0C2	(STH)	DEC 1 00001			

## ENTRY POINTS TO SUBROUTINES NOT OUTPUT FROM LIBRARY

INVAR (FILE) (STH)

## EXTERNAL FORMULA NUMBERS WITH CORRESPONDING INTERNAL FORMULA NUMBERS AND OCTAL LOCATIONS

	EFN	LCC	EFN	LCC	EFN	LCC	EFN	LCC
1	13	CC664	6	16 CC75	9	21 00131	91	24 CC140
93	27	00146	20	54 00322	21	55 00326	10	59 CC340
12	61	CC355	30	62 00373	40	68 00407	50	72 CC425
3	83	00520	70	85 CC524			71	81 CC507

```

C      SUBROUTINE INVAR (FLAT,FLNG,ALT,ERR,FLN)
C      NULC   ERROR IN L IS TYPICALLY LESS THAN 0.1*ERR
C      FLAT=LATITUDE IN DEGREES   FLNG=LNGITUDE IN DEGREES
C      ALT=ALTITUDE=INSTANCE FROM SURFACE OF EARTH IN KILOMETERS
C      DIMENSION VN(3),VN(200),ARC(200),VN(3),VP(3),BEND(200),
C      1BLG(200),FLC(200),SL(3),R(3),VN(3),VP(3),BEG(200),
C      V(1,2)=ALT/6371.2
C      V(2,2)=(90.-FLAT)/57.*2957795
C      V(3,2)=FLNG/57.*2957795
C      ARC(1)=0.
C      ARC(2)=(1.0+V(1,2))*SIN(FLNG)*0.3
C      DCL=1.5/(8-C*200)*COS(V(3,2))+1.239
C      IF(V(2,2)-DCL)>10.10,11
C      11  ARC(2)=ARC(2)
C      10  CALL START (R1,R2,R3,R,ARC,ERR,V)
C      DC 12  I=1,5
C      VP(I)=V(I,2)
C      12  VN(I)=V(I,3)
C      CALL LINES (R1,R2,R3,R,ARC,ERR,V,P,VN)
C      IF(J=200)16,17,17
C      17  FL=-1.0
C      GC  FG 18
C      16  JUP=J
C      DC 40  J=1,JUP
C      ARC(J)=ABSF(ARC(J))
C      40  BL0G(J)=EGR(B(J))
C      JLP=JUP-1
C      DC 21  J=2,JLP
C      DC 22  J=JLP+1
C      ASUM=ARC(J)+ARC(J+1)
C      DX=RL(L(J)-RL(L(J-1))-RLG(J)
C      DN=ASUM*ARC(J)*ARC(J+1)
C      BCG=((RLG(J-1)-RLG(J+1))*ARC(J)*2.0*ASUM*#2)/DN
C      CCO=(1.0*ARC(J+1)-(RLG(J)-RLG(J+1))*ARC(J+1))*ARC(J)/DN
C      SA=7.0*ARC(J)
C      SC=SA*2.0*ASUM
C      DCD=RLG(J-1)-CCC *SA*SC
C      CGH(J)=BCG + CCG *(SC+SC)
C      BFG(J)=EGR((LCG+CC(J))*5*ARC(J))
C      21  BNCE(J)=EGR((CCG+CC(J))*5*(ASUM+ARC(J)))
C      BCG(JP)=EGR((CCG+CC(J))*5*(ASUM+ARC(J)))
C      BFG(JP)=EGR((CCG+CC(J))*5*(ASUM+ARC(J)))
C      BCF(JP)=EGR((CCG+CC(J))*5*(ASUM+ARC(J)))
C      BCF(JP)=((2.0*ARC(JP))*LCGF(BND(JP))/BLG(JP))
C      CALL INTG (arc,flg,B,N,D,B,JP,CC,FLINT)
C      27  CALL CARBEL (R12,FL18,FL)
C      18  ER=H(C)
C      END(1,L,U,U,C,O,C,1.0,O,C,C,C,O,O)

```

STRUCTURE NOT USED BY PROGRAM

DEC	LCT	DEC	DEC
1507	C2743	32561	77461

STRUCTURE LOCATIONS FOR VARIABLES APPEARING IN DIMENSION AND EQUIVALENCE STATEMENTS

DEC	LCT	DEC	DEC
1306	C2432	11C0	C2114
ARC	5C0	3C0	00454
LCO	CC764	R1	R2
V	1103	C2117	V
VP		291	C0445

STRUCTURE LOCATIONS FOR VARIABLES NOT APPEARING IN COMMON, DIMENSION, OR EQUIVALENCE STATEMENT

DEC	LCT	DEC	DEC
282	C0432	281	C0431
DN	277	276	CC24
JUP	272	271	C0417
	C0420	SA	SC
		270	00416

LOCATIONS FOR OTHER SYMBOLS NOT APPEARING IN SOURCE PROGRAM

DEC	LCT	DEC	DEC
1)	264	242	C0362
C164	265	31	245
	00410	00362	00365
	C0415		

LOCATIONS OF NAMES IN TRANSFER VECTOR

DEC	LCT	DEC	DEC
22	7	1	5
CARTEL	CCCC7	CCCC01	00005
LOG	4	00004	00006
	SQRT	0	2
		CCCC	CCCC
		START	CCCC
			CCCC

ENTRY POINTS TO SUBROUTINES NOT OUTPUT FROM LIBRARY

CARTEL	CCS	EXP	INTG	LINE	LOG	SCR1
--------	-----	-----	------	------	-----	------

EXTERNAL FORMULA NUMBERS WITH CARRY SPACING INTERNAL FORMULA NUMBERS AND OCTAL LOCATIONS

EFN	IFN	LCC	IFN	LCC	FFN	IFN	LOC
11	11	CC105	10	12	12	17	20
40	25	C0164	21	3H	3H	18	C0152
					44	46	C0354

```

SUBROUTINE LINES (R1,R2,R3,B,ARC,ERR,J,VP,VN)
DIMENSION B(200),ARC(200),R1(3),R2(3),R3(3),VN(3),VP(3),RA(3)
CRE=0.25
IF (ERR<0.15625) 74,75,75
74 CRE= ((ERR*40.333333333)
75 A3=ARC(3)
AAB=AH*SF(A3)
SNA=A3*AB
A1=ARC(1)
A2=ARC(1)
AC6=A3*A3/6.0
J=3
1LP=1
1S=1
GO TO 87
66 1S=1
J=J+1
AU6=A3*A3/6.0
AKCJ=A1+A2+A3
AD=(ASUM+A1)/AA
BD=ASUM/BB
CU=A1/CC
36 DO 5 I=1,3
DU=R1(I)/AA-R2(I)/BB+R3(I)/CC
GU TO 6,8,1S
6 RT=R1(I)-(AD*R1(I)-BD*R2(I)+CD*R3(I))-DD*ARC(J)*ARCJ
RA(I)=R1(I)
R1(I)=R2(I)
R2(I)=R3(I)
R3(I)=RT
VPL(I)=VN(I)
VP(I)=VP(I)+3*RBAR
8 RLAR=(R2(I)+R3(I))/2.-DD*A06
5 VN(I)=VP(I)+3*RBAR
87 IF (VN(2)>VN(1)) 76,77,77
76 VN(2)=VN(2)
77 IF (VN(2)-3.141592653178+79,79
79 VN(2)=0.283185307-VN(2)
GO TO 77
78 IF (VN(3)>VN(2)) 80,81,81
80 VN(3)=VN(3)+6.283183307
GU TO 78
81 IF (VN(3)-6.283185307182,82,83
83 VN(3)=VN(3)-6.283185307
84 GU TO 81
82 GU TO 9,10,1S
9 SIT=AUSF(SINF(VN(2)))
PRE1=VN(L)
PRE2=PRE1*SIT*VN(3)
PRE3=PRE1*SIT*VN(3)
SSQ=SIT*SIT
10 DER=16356.912+SSQ*(21.36774+.106*SSQ)/6371.2
AER=VN(1)-DER
CALL MAGNET(ARC,SIT,VN(3),BR,BT,BP,B(J),VN(2))
R3(1)=BR/B(J)
DN=B(J)*VN(1)

```

```

R3(2)=V1/DN
RJ(3)=D/V(DN*SIT)
ASUM=A+A^2
AA=ASUM*A2
Hd=AA*2
CC=ASUF*A3
IS=2
60 1C 36
10 SIT=ABSF(SIN(VN(2)))
B(J)=S(J)*((PH1/VN(1))*3)
59 QRT=.2*ABSF(.3*11)/(.1+ABSF(R3(2)*VN(11)))
X=(ABSF(V(1)-PRE1)*QRT*ABSF(VN(1)*VN(2)-PRE2)+ABSF(VN(11)*SIT*VN(3LINES05
1)-PRE3))/((AAB*RR*SGTF(1.+QRT*CR1))
GC TO (96,93,90),LP
73 IF(X-.3)>0,3G
69 A3=A3*.2*(18.*C+X)/(C.*3+X)
J=J-1
1LP=3
ASUM=A+A1
AA=ASUF*A1
Hb=AA*2
CC=ASUM*A2
DC=91 I=1,J
VN(I)=P(I)
R3(I)=K2(I)
R2(I)=K1(I)
91 R1(I)=RA(I)
60 TU /3
90 IF((J-2,C)>I+.CC,60
67 AI=A2
IF(TB(J)-B(Z))49,45,60
49 1LP=2
A2=A3
A3=A3*.2*(8.*X)/(8.*X)
AM=(2.-R3(2)*VN(1))*VN(1)*CRE
IF(ABSF(A3)-AM)>84,84,72
72 A3=SNA*A M
84 IF(SNA*AR3(1)+.5)85,85,73
85 AM=-.5*SN(A*VN(1))/R3(1)
IF(ABSF(A3)-AM)>73,73,86
86 A3=SNA*A M
73 ARC(J+1)=A3
AAB=ABSF(A3)
60 GU TO 66
60 RETURN
END(1,0,0,0,0,1,0,0,C,C,C,0,0)

```

STANDARD OCTAL USED BY PROGRAM

DEC OCT  
65C 61212

#### STORAGE LOCATIONS FOR VARIABLES APPEARING IN DIMENSION AND EQUIVALENCE STATEMENTS

	DEC	OCT	DEC	OCT	DEC	OCT	DEC	OCT	DEC	OCT
R4	644	C1211								

#### STORAGE LOCATIONS FOR VARIABLES NOT APPEARING IN COMMON, DIMENSION, OR EQUIVALENCE STATEMENT

	DEC	OCT	DEC	OCT	DEC	OCT	DEC	OCT	DEC	OCT
A1	646	01206	A2	C1205	A3	644 01204	A4H	643 01203	AA	642 01202
AD	641	01201	AER	640 C11C0	AP	639 01177	AC6	638 C1176	ARCJ	637 01175
ASUM	636	C1174	BB	635 01173	PB	634 01172	BP	633 C1171	BR	632 01170
BT	631	C1167	CC	630 C1166	CC	629 01165	CR4	628 01164	DC	627 01163
DN	627	C1162	ILP	625 C1161	IS	624 01160	OLR	623 C1157	PRI	622 01156
PRE2	621	C1155	PRL3	620 C1154	CRT	619 01153	RBAR	618 C1152	RT	617 01151
SIT	616	C1150	SNA	615 01147	SSG	614 01146	X	613 01145		

#### LOCATIONS FOR OTHER SYMBOLS NOT APPEARING IN SCURRE PROGRAM

	DEC	OCT	DEC	OCT	DEC	OCT	DEC	OCT	DEC	OCT
I1	604	01134	2)	572 C1674	3)	576 01100	6)	594 01122	9)	600 01130
C162	610	01142	C163	611 C1143	C164	612 01144	E01	155 02233	E1A	277 00425
t.E	292	CC444	E1K	444 0C674	E1G	493 00755	EIP	498 CC762		

#### LOCATIONS OF NAMES IN TRANSFER VECTOR

	DEC	OCT	DEC	OCT	DEC	OCT	DEC	OCT	DEC	OCT
EXP(3)	DEC	OCT	MAGNET	DEC	SIN	DEC	1 C0001	SQRT	DEC	OCT
	1.	CCC00	2	CC002						

#### ENTRY POINTS TO SUBROUTINES NOT OUTPUT FROM LIBRARY

EXP(3) MAGNET SIN SQRT

#### EXTERNAL FORMULA NUMBERS WITH CARRIERS PUNCTUATING INTERNAL FORMULA NUMBERS AND OCTAL LOCATIONS

	IFN	LCC	FFN	IFN	LLC	FFN	IFN	LLC	FFN	IFN	LOC
F74	0 C0234	75	7	0024C	66	17	00274	36	24 00327	6	27 00346
8	2 0 C0463	5	34	C0414	87	35	00422	76	36 00426	77	37 00430
79	3 0 C0435	78	40	C0441	80	41	00445	81	43 00451	83	44 00456
82	4 0 C0462	9	47	C0464	10	66	00574	29	68 00614	93	71 00675
89	7 2 C0702	91	83	C075C	90	85	00556	67	86 0C764	49	88 CC772
72	9 3 C1033	84	94	01L36	85	93	01043	86	97 01057	73	98 01062
60	1C1 01C7C										

```

SUBROUTINE START (R1,R2,R3,B,ARC,ERR,V)
DIMENSION b(200),ARC(200),V(3,3),R1(3),R2(3),R3(3)
SIT=ABS(SIN(F(V(2,2)))
AR=v(1,2)
SSQ=SIT*SIT
UER=(656.912+SSQ*(121.3677+108*SSQ))/6371.2
V(1,2)=AR*ERR
10 IF(V(3,2))11,12,12
11 V(3,2)=V(3,2)+6.*2E3185307
GC TG LC
12 CALL MAGNE ((AEP),SIT,V(3,2),BR,BT,DP,B(2),V(2,2))
R2(1)=BR/B(2)
DN=B(2)*V(1,2)
R2(2)=BT/DN
R2(3)=DP/(DN*SIT)
IS=0
1 DO 2 I=1,3
2 V(1,1)=V(1,2)-ARC(2)*R2(I)
SIT=AESF(SINF(V(2,1)))
3 SSC=SIT*SIT
GER=(656.912+SSQ*(121.3677+108*SSQ))/6371.2
AER=V(1,1)-OER
CALL MAGNET(AEK,SIT,V(3,1),ER,BT,DP,B(1),V(2,1))
IF(B(1)-B(2))4,5,5
4 ARC(2)=-ARC(2)
5 GO TG 1
R1(1)=BR/B(1)
ARC(3)=ARC(2)
DN=B(1)*V(1,1)
R1(2)=BT/DN
R1(3)=BP/(LN*SIT)
DO 6 I=1,3
6 V(1,1)=V(1,2)-ARC(2)*(R1(I)+R2(I))/2.
SIT=ABS(F(SINF(V(2,1)))
IS=IS+1
GO TO 7,IS
7 DO 8 I=1,3
8 V(1,3)=V(1,2)+ARC(3)*((1.5)*R2(I)-.5*R1(I))
RETURN
END(L,I,U,C,O,C,L,O,C,C,O,C,O,O)

```

STORAGE OCTAL USED BY PROGRAM

DEC	UCI	DEC	OCT
297	C0445	32561	17461

STORAGE LOCATIONS FOR VARIABLES NOT APPEARING IN COMMON, DIMENSION, OR EQUIVALENCE STATEMENT

DEC	UCI	DEC	OCT
292	CC444	291	00443
AER	286	BP	00442
FS	CC437	286	00436

LOCATIONS FOR OTHER SYMBOLS NOT APPEARING IN SOURCE PROGRAM

DEC	UCI	DEC	OCT
11	280	21	00401
162	283	193	00301

LOCATIONS OF NAMES IN TRANSFER VECTOR

DEC	UCI	DEC	OCT
MAGNET	1	SIN	0 0000

ENTRY POINTS TO SUBROUTINES NOT OUTPUT FROM LIBRARY

MAGNET →IN

INTERNAL FORMULA NUMBERS WITH CORRESPONDING INTERNAL FORMULA NUMBERS AND OCTAL LOCATIONS

IFN	IFN	IFN	IFN	IFN	IFN	IFN	IFN	IFN	IFN	IFN	IFN
10	9	10	10	12	12	19	19	20	20	20	20
3	00164	00167	00173	00173	00173	00227	00227	00231	00231	00231	00231
22	CC245	4	5	5	5	6	6	7	7	7	7
6	41	28	30	30	30	36	36	40	40	40	40
		00302	00305	00330	00330			00355	00355		

SURFACE LINE MAGNET (R, PHI, PR, DHIT, BPHI, OB, THET)  
 DIRECTIONS (P(4,9), P(4,9), G(1,9), H(4,9), CONST(4,9), ACR(7), SP(7), CP(7))  
 IF(KIP)151,15C,15C  
 1;0 KIP=-1  
 DL 15C  
 N=1,4,  
 G(N)=C  
 G(N)=C  
 152 H(N)=C  
 JNSC<sub>N</sub> AND CAIN COEFFICIENTS FOR LSEC (JUN E 1962)  
 C G(1) = G(N,M) AND H(1) = H(N,M) WHERE 1 = N+7\*(M-1)  
 G(1,2) = 3.0411205CL-C1  
 G(1,3) = 2.1435858E-C2  
 G(1,4) = 2.40353671E-C2  
 G(1,5) = -5.1253379E-C2  
 G(1,6) = -1.33811969E-C2  
 G(1,7) = -3.15178651E-C2  
 G(1,8) = 6.2130C9C6E-C2  
 G(1,9) = -2.48941333E-C2  
 G(1,10) = -6.49965905E-C3  
 G(1,11) = -4.17941639E-C2  
 G(1,12) = -4.5293366CE-C2  
 G(1,13) = -2.17937447E-C2  
 G(1,14) = 7.00025405CL-C3  
 G(1,15) = -2.64355562E-C3  
 G(1,16) = 1.6256271L-C2  
 G(1,17) = -3.44087606E-C2  
 G(1,18) = -1.9444C026E-C2  
 G(1,19) = -6.08211374E-C4  
 G(1,20) = 2.77533549E-03  
 G(1,21) = 6.96882467L-C2  
 G(1,22) = -1.9521736E-C2  
 G(1,23) = -4.85326147E-C3  
 G(1,24) = 3.21122428E-03  
 G(1,25) = 2.14128328E-02  
 G(1,26) = 1.05051275E-03  
 G(1,27) = 2.26822448E-C4  
 G(1,28) = 1.1147358E-03  
 G(1,29) = 5.79890501E-02  
 H(1,0) = 3.3124C114L-C2  
 H(1,1) = -1.37893822E-C3  
 H(1,2) = 1.48666943E-02  
 H(1,3) = 1.3885C349CE-03  
 H(1,4) = -4.67459458E-C3  
 H(1,5) = -1.95864466E-C4  
 H(1,6) = 2.1C31235E-C4  
 H(1,7) = -1.18215456E-C2  
 H(1,8) = 1.CC057732L-C2  
 H(1,9) = 4.3036038631E-04  
 H(1,10) = -2.18063925E-C3  
 H(1,11) = -5.75830293E-03  
 H(1,12) = -8.73461401E-03  
 H(1,13) = -3.466C4013E-C3  
 H(1,14) = -1.13162456E-04

MAGNTCC0  
 MAGNTCC1  
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 MAGNTCC4  
 MAGNTCC5  
 MAGNTCC6  
 MAGNTCC7  
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 MAGNTCC50  
 MAGNTCC51  
 MAGNTCC52  
 MAGNTCC53  
 MAGNTCC54

```

H(42)=-1.14023013E-03
H(49)=-3.24831891E-04
P(1)=0.0
DP(1)=0.0
SP(1)=0.0
CP(1)=1.0
CONST(1)=0.0
CONST(16)=0.0
DO 80 N=3,7
FN=N
DO 80 M=1,N
FM=M
I=N+7*(M-1)
H(UNST(I))=((FN-2.0)**2-(FM-1.0)**2)/((FN+FN-3.0)*(FN+FN-5.0))
151 C=SQRT(FABS(F(1.0-S*S)))
IF(THET-1.57C796327) 154,154,156
156 C=-C
154 AR=1.0/(1.0+K)
155 SP(2)=SINF(PHI)
CP(2)=COSF(PHI)
AUR(1)=AR*AR
ACR(2)=AR*AOR(1)
DO 90 M=3,7
N=M-1
SP(M)=SP(2)*CP(N)+CP(2)*SP(N)
CP(M)=CP(2)*CP(N)-SP(2)*SP(N)
90 ACR(M)=AR*AOR(N)
BK=0.0
BTHT=T=U=0
BPHI=0.0
DO 32 N=2,7
FN=N
SUMR=0.0
SUMT=0.0
SUMP=0.0
DO 33 M=1,N
IF(N-M)87,88,87
88 I=B-N-7
L=I-8
P(L)=S*P(L)
DP(L)=S*DP(L)+C*P(L)
GO TO 89
87 I=N+7*(M-1)
J=I-1
K=I-2
P(1)=C*P(J)-CONST(1)*P(K)
DP(1)=C*DP(J)-SP(J)-CONST(1)*DP(K)
89 FM=M-1
TS=G(1)*CP(M)+H(1)*SP(M)
SUMR=SUMR+P(1)*TS
SUMT=SUMT+DP(1)*TS
33 SUMP=SUMP+FM*P(1))-(-G(1)*SP(M)+H(1)*CP(M))
BR=BR+AOR(N)*FN*SUMR
BTHET=BTHET-AOR(N)*SUMT
32 BPHI=BPHI-AOR(N)*SUMP
BPHI=BPHI/S

```

```
Bb=SQRFF(BR**2+RTHET**2+BPHI**2)
RETURN
END(1,0,C,O,O,O,O,O,O,O,O,O,O,O,O,O,O,O)
```

```
MAGNT111
MAGNT112
```

## STORAGE LOCATIONS BY PROGRAM

	DEC	OCT	DEC	OCT
	830	01476	32561	77461

## STORAGE LOCATIONS FOR VARIABLES APPEARING IN DIMENSION AND EQUIVALENCE STATEMENTS

	DEC	OCT	DEC	OCT	DEC	OCT	DEC	OCT
AOR	584	01110	CONST	633 01171	CP	570 01012	DP	829 01475
H	682	01252	P	780 01414	SP	577 01101		6 731 01333

## STORAGE LOCATIONS FOR VARIABLES NOT APPEARING IN COMMON, DIMENSION, OR EQUIVALENCE STATEMENT

	DEC	OCT	DEC	OCT	DEC	OCT	DEC	OCT
AR	563	01063	C	562 01C62	FM	561 01061	FN	560 01C6C
J	558	01056	KIP	551 01C55	K	556 01054	L	555 C1C53
N	553	01051	SUMP	552 01C5C	SUMR	551 01047	SUMT	55C 01046

## LOCATIONS FOR OTHER SYMBOLS NOT APPEARING IN SOURCE PROGRAM

	DEC	OCT	DEC	OCT	DEC	OCT	DEC	OCT
I	537	01031	2)	472 01730	3)	477 00735	6)	531 01023
C1G2	543	01037	C)63	544 01040	C)G4	545 01041	C)G5	546 01042
C1201	548	01044	0120D	3C7 00463	D)404	173 00255	C)408	230 C0346

## LOCATIONS OF NAMES IN TRANSFER VECTOR

	DEC	OCT	DEC	OCT	DEC	OCT	DEC	OCT
COS	DEC 2	UGT C0002	SIN 1	CC001	SQRT 0	OCC00		CC1

## ENTRY POINTS TO SUBROUTINES NOT OUTPUT FROM LIBRARY

	CCS	SIN	SQRT					
31								

EXTERNAL FORMULA NUMBERS WITH CORRESPONDING INTERNAL FORMULA NUMBERS AND OCTAL LOCATIONS

EFN	IFN	LCC	EFN	IFN	LCC	EFN	IFN	LCC	EFN	IFN	LCC
150	152	8 CCC71	80	68	00107	151	69	C0347	156	71	00365
154	155	73 C0375	90	81	00443	88	92	C0512	87	97	00541
89	33	1C6 00635	32	109	00572						

```
SUBROUTINE INTEG (ARC,BEG,BEND,B,JEP,ECC,F1)
DIMENSION ARC(200),BEG(200),BEND(200),B(200),ECC(200)
4 KK=JEP
6 IF (KK=4) 14,11,20
11 KK=KK-1
14 A=B*(KK-1)/B(12)
X2=B*(KK) ) B(12)
X3=B*(KK+1)/B(12)
ASUM=ARC(IKK)*ARCI(KK)+ARC(IKK+1)
DN=ARC(IKK)*ARCIKK+1)*ASUM+
BB=( -A*ARC(IKK+1)*(ARC(IKK)+ASUM)+X2*ASUM**2-X3*ARC(KK))/CN
C=(A*ARC(IKK+1)*X2*ASUM+X3*ARC(KK))/CN
F1=1.570796326*(1.-A+BB*BB/(4.*C))/SQR(F(ABS(F(C)))
RETURN
20 T=SQRT(F(1.-BEND(2)/B(2))
F1=(2.*T-LOGF((1.+T)/(1.-T)))/ECC(2)
1 F(B(2)-BEND(KK))21,21,25
25 KK=KK+1
21 T=SQRT(F(ABS(F(1.-BEG(KK)/B(2)))
F1=F1-(2.*T-LOGF((1.+T)/(1.-T)))/ECC(KK)
KK=KK-1
22 DO 5 I=3,KK
ARG1=1.-BEND(I)/B(2)
IF(ARG1)26,26,27
26 TE=1.-t-5
GO TO 28
27 TE=SQRT(F(ARG1)
28 ARG1=1.-DEG(I)/B(2)
IF(ARG1)29,29,31
31 TB=SQRT(F(ARG1)
GO TO 32
29 TB=1.E-5
32 IF(ABS(F(ECO(I))-2.E-5) .GT. 23.E-24
23 F1=F1+(1.E+TB)*(ARC(11)+ARC(11+1))/4.
GO TO 5
24 F1=F1+(1.E-TB)-LOGF((1.+TE)*(1.-TB)/(1.-TE)*(1.+TB)))/ECO(1)
5 CONTINUE
30 RETURN
END1.1.0.0,0.0.0.1.0.0.0.0.0.0.0.0.0.0.0.0.0.0
```

STORAGE LOC USED BY PROGRAM

DEC	UCI	DEC	UCI
371	C0563	32561	77461

STORAGE LOCATIONS FOR VARIABLES NOT APPEARING IN COMMON, DIMENSION, OR EQUIVALENCE STATEMENT

DEC	UCI	DEC	UCI
A\$G1	370 C0562	^	369 00561
DN	365 C0555	K	364 00554
X2	366 C0550	X3	359 00547

LOCATIONS FOR OTHER SYMBOLS NOT APPEARING IN SOURCE PROGRAM

DEC	UCI	DEC	UCI
1)	350 C0536	2)	329 C0511
C160	358 00546	3)	323 00515
		4)	315 202 00312

LOCATIONS OF NAMES IN TRANSFER VECTOR

DEC	UCI	DEC	UCI
LOG	1 CCC01	SQRT	0 C0CCC

ENTRY POINTS TO SUBROUTINES NOT OUTPUT FROM LIBRARY

LOC	SIGN	EFN	IFN	LOC	EFN	IFN	LOC

EXTERNAL FORMULA NUMBERS WITH CORRESPONDING INTERNAL FORMULA NUMBERS AND OCTAL LOCATIONS

CFN	IFN	LOC	EFN	IFN	LOC	EFN	IFN	LOC
4	4 C0117	5	C0122	6	C0127	14	7 CC135	17 00246
25	20 C0355	21	C0313	22	C0355	26	27 CC371	29 00374
28	36 C0401	31	C0411	29	00421	32	35 CC423	23 00430
24	36 C0445	35	C0503	30	00505			

SUBROUTINE CARMEL (B,X1,V1)

COMPUTE L

XX=LG05 F((X1+3)\*E)/0.311E53

If((XX+2,-1),1,1,B

8 IF((XX+3,-2),2,S

9 IF((XX-3),3,10

10 IF((XX-12),4,11

11 IF((XX-23),5,6

12 IF((XX-23),5,6

13 G5=333233\*XX+3CC621C2

14 TU /

2 G6=((((((-d+1.537735E-14\*XX+d+3232531E-15)\*XX+1.006C562E-9)\*XX+

1.3+1.0456d5,-6)\*XX+2.2916354E-6\*XX+8.2711G56i,-5)\*XX+1.371467E-3)\*

2XX+0.15G17245)\*XX+4.3632642)\*XX+c.2331691

GC TC /

3 G6=(((((2.6677C23E-10\*XX+2.302567E-9)\*XX+2.19975d3E-8)\*XX-

1.5.397764,-7)\*XX-3.34088222E-6)\*XX+3.8374917E-2)\*XX+1.1784234E-3)\*

2XX+1.445244L,-2)\*XX+4.335278E1\*XX+6.228644

GU TC /

4 G6=(((((6.3271Lc65L-10\*XX-3.95d56E-8)\*XX+3.5766148L-07)\*XX-

11.253132E-5)\*XX+7.9451313E-5)\*XX-3.2077032E-4)\*XX+2.1680398E-3)\*

2XX+1.2e17956L,-2)\*XX+4.35105261\*XX+6.222353

GU TU /

> G6=(((((2.3212035E-8\*XX-3.8049276L-6)\*XX+2.17G224E-4)\*XX+6.73103239GAKn1022

1E-3)\*XX+1.2038224)\*XX+1.84e1796)\*XX+2.CCG137

GU TC /

6 GU=-3.5C460C81

7 VL=((1.10+exp F(G6))\*C.311E53)/R)\*(1./3.)

C END CFPLT L

RETURN

END(1.1.0,G,C,0,0,1.0,0,C,0,C,0,0)

## STORAGE OCT USED BY PROGRAM

DEC	OCT	DEC	OCT
25C	00372	325E1	77461

## STORAGE LOCATIONS FOR VARIABLES NOT APPEARING IN COMMON, DIMENSION, OR EQUIVALENCE STATEMENT

DEC	OCT	DEC	OCT
249	00371	XX	248 00370

## LOCATIONS FOR OTHER SYMBOLS NOT APPEARING IN SOURCE PROGRAM

DEC	OCT	DEC	OCT
244	00364	2)	191 00277

## LOCATIONS OF NAMES IN TRANSFER VECTOR

DEC	OCT	DEC	OCT
1	00001	EXP(3	2 CCC02

## ENTRY POINTS TO SUBROUTINES NOT OUTPUT FROM LIBRARY

EXP	EXP(3	LOG
-----	-------	-----

## EXTERNAL FORMULA NUMBERS WITH CORRESPONDING INTERNAL FORMULA NUMBERS AND OCTAL LOCATIONS

EFN	IFN	LCC	EFN	IFN	LCC	EFN	IFN	LCC	EFN	IFN	LOC
8	5	00045	9	6	C0052	10	7	00027	11	8	CCC64
2	11	C0076	3	13	00134	4	15	00171	15	17	C0226
7	2C	C0255							e	e	C0252

#### E. Restrictions

ALAT must be remotely close to the correct latitude corresponding to the initial B in order to save machine time and to insure the accuracy of the answers. ALAT must always be positive and greater than the geomagnetic equator at geocentric longitude of  $180^\circ$ . This means that ALAT must be greater than  $4^\circ$ .

#### F. Input

Cards containing the initial values of B, L and  $\lambda$  are all the data necessary for the execution of this program. This data is entered on logical tape number two. Each card represents a single case.

##### 1. Card Description

Columns	Mode	Quantity	Units	Description
1-12	F	BO	gauss	initial magnetic induction
13-24	F	ELO	earth radii	initial magnetic field line
25-32	F	ALAT	degrees	initial latitude

2. Sample

**GENERAL PURPOSE DATA SHEET**

Problem Spanner	INPUT B-L SEARCH (INITIAL B, L, $\lambda$ )		P <sub>ave</sub>	SAMPLE	P <sub>ave</sub> of ef
	TAPE 1	TAPE 2			
1					
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4					
5					
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100					

## G. Output

Output from this program appears on logical tapes 3 and 5. Both tapes contain the same information with the exception that tape 3 also contains the intermediate results of the search routine. Tape 5 is the output to be used in the longitudinal averaging processor. This tape is punched onto cards which can be combined with similar output from other runs. All this data can then be used as input to the longitudinal averaging processor, but it is important that a blank card follow the last of the data cards. This arrangement is discussed in the next section.

**1. Tape 3 Sample**

BO= 0.11000	LO= 1.75000	INITIAL LAT=26.00000		
INTERMEDIATE RESULTS--NORTHERN HEMISPHERE				
LCNG	LAT	ALT	B	L
180.00000	26.00000	3533.22839	0.10159	1.75000
180.00000	28.00000	3257.93344	0.11298	1.75000
180.00000	27.47628	3330.02185	0.10985	1.74955
B= 0.10985	L= 1.74955	FINAL RESULTS		
-180.00	27.48	3330.02	0.10985	1.74955
-180.00	27.48	3330.02	0.10985	1.74955
-170.00	25.79	3309.07	0.10987	1.75027
-160.00	23.86	3298.23	0.10987	1.75043
-150.00	21.82	3293.89	0.10987	1.75049
-140.00	19.74	3290.96	0.10986	1.74966
-130.00	17.71	3287.41	0.10986	1.74966
-120.00	15.73	3279.11	0.10986	1.74966
-110.00	13.83	3263.27	0.10987	1.75054
-100.00	11.97	3234.47	0.10987	1.75049
-90.00	10.27	3190.87	0.10987	1.75052
-80.00	8.93	3132.92	0.10986	1.75014
-70.00	8.27	3067.73	0.10986	1.74978
-60.00	8.66	3009.01	0.10985	1.74947
-50.00	10.36	2972.82	0.10985	1.74926
-40.00	13.12	2964.85	0.10985	1.74926
-30.00	16.35	2979.89	0.10985	1.74933
-20.00	19.48	3011.16	0.10985	1.74939
-10.00	22.19	3052.95	0.10985	1.74927
-0.	24.34	3101.34	0.10985	1.74913
10.00	25.90	3153.89	0.10985	1.74914
20.00	26.92	3210.03	0.10985	1.74922
30.00	27.49	3269.30	0.10985	1.74940
40.00	27.80	3331.19	0.10986	1.74874
50.00	28.10	3397.64	0.10987	1.74857
60.00	28.53	3466.52	0.10985	1.74941
70.00	29.03	3528.77	0.10985	1.74939
80.00	29.55	3579.90	0.10985	1.74936
90.00	29.99	3614.76	0.10985	1.74941
100.00	30.27	3629.99	0.10985	1.74857
110.00	30.48	3626.67	0.10985	1.74880
120.00	30.63	3605.07	0.10986	1.74932
130.00	30.67	3566.43	0.10987	1.74938
140.00	30.64	3517.70	0.10987	1.74968
150.00	30.42	3464.00	0.10988	1.75053
160.00	29.83	3410.37	0.10986	1.74985
170.00	28.87	3364.67	0.10986	1.75002

2. Tape 5

INTERMEDIATE RESULTS--SOUTHERN HEMISPHERE

LONG	LAT	ALT	B	L
180.00000	-15.00000	3695.08514	0.10030	1.74998
180.00000	-17.00000	3433.09256	0.11171	1.74995
180.00000	-16.70013	3472.37378	0.10990	1.74989
B = 0.10990	L = 1.74989			

FINAL RESULTS

-180.00	-16.70	3472.37	0.10990	1.74989
-180.00	-16.70	3472.37	0.10990	1.74989
-170.00	-18.67	3441.67	0.10990	1.75006
-160.00	-20.70	3407.85	0.10990	1.75001
-150.00	-22.78	3370.58	0.10990	1.75002
-140.00	-24.86	3327.75	0.10990	1.75005
-130.00	-26.87	3277.04	0.10988	1.74890
-120.00	-28.92	3219.97	0.10987	1.74896
-110.00	-30.96	3153.88	0.10987	1.74892
-100.00	-32.95	3077.77	0.10987	1.74908
-90.00	-34.76	2990.94	0.10987	1.74901
-80.00	-36.23	2895.15	0.10988	1.74917
-70.00	-37.17	2794.22	0.10989	1.74943
-60.00	-37.39	2694.25	0.10990	1.74975
-50.00	-36.73	2603.75	0.10991	1.75009
-40.00	-35.09	2533.92	0.10991	1.75021
-30.00	-32.47	2497.69	0.10991	1.75013
-20.00	-29.06	2503.03	0.10987	1.74902
-10.00	-25.47	2545.84	0.10990	1.74915
-0.	-22.21	2615.13	0.10990	1.74996
10.00	-19.60	2695.72	0.10990	1.75003
20.00	-17.80	2780.87	0.10990	1.75013
30.00	-16.70	2870.66	0.10990	1.75012
40.00	-15.98	2969.88	0.10990	1.75012
50.00	-15.29	3079.53	0.11000	1.74901
60.00	-14.53	3205.88	0.10990	1.75006
70.00	-13.64	3328.53	0.10990	1.75010
80.00	-12.77	3437.57	0.10990	1.75010
90.00	-12.08	3524.42	0.10990	1.75011
100.00	-11.65	3585.00	0.10990	1.75007
110.00	-11.42	3618.98	0.10990	1.74908
120.00	-11.44	3631.77	0.10990	1.74995
130.00	-11.60	3624.71	0.10991	1.75053
140.00	-11.89	3601.71	0.10990	1.74967
150.00	-12.51	3570.65	0.10989	1.74957
160.00	-13.51	3536.55	0.10989	1.74939
170.00	-14.92	3503.21	0.10988	1.74915

a. Card Description

Columns	Mode	Quantity	Units	Description
1-12	F	PRLNG	degrees	geocentric longitude
13-24	F	PHI	degrees	geocentric latitude
25-36	F	ALT	km.	altitude
37-48	F	B	gauss	magnetic induction
49-60	F	EL	earth radii	magnetic field line

b. Sample

GENERAL PURPOSE DATA SHEET

Problem	OUTPUT - B-L SEARCH (B-L CONTOURS)	Date	SAMPLE	Page	of
Spanner	TAPE 5				
1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 31 32 33 34 35 36 37 38 39 40 41 42 43 44 45 46 47 48 49 50 51 52 53 54 55 56 57 58 59 60 61 62 63 64 65 66 67 68 69 70 71 72 73 74 75 76 77 78 79 80					
-1 8 0 . 0 0	2 5 . 6 3	3 5 8 0 . 6 8	0 . 0 9 9 7 4	1 . 7 4 9 6 8	
-1 7 0 . 0 0	2 3 . 9 4	3 5 5 8 . 7 7	0 . 0 9 9 7 5	1 . 7 5 0 4 7	
-1 6 0 . 0 0	2 2 . 0 1	3 5 4 6 . 1 2	0 . 0 9 9 7 6	1 . 7 5 0 6 0	
-1 5 0 . 0 0	1 9 . 9 9	3 5 3 9 . 2 4	0 . 0 9 9 7 6	1 . 7 5 0 6 2	
-1 4 0 . 0 0	1 7 . 9 1	3 5 3 3 . 4 2	0 . 0 9 9 7 4	1 . 7 4 9 7 9	
-1 3 0 . 0 0	1 5 . 9 3	3 5 2 7 . 4 8	0 . 0 9 9 7 6	1 . 7 5 0 5 7	
-1 2 0 . 0 0	1 3 . 9 5	3 5 1 5 . 4 6	0 . 0 9 9 7 6	1 . 7 5 0 5 8	
-1 1 0 . 0 0	1 2 . 0 2	3 4 9 4 . 9 0	0 . 0 9 9 7 6	1 . 7 5 0 5 6	
-1 0 0 . 0 0	1 0 . 1 6	3 4 6 2 . 3 4	0 . 0 9 9 7 6	1 . 7 5 0 4 7	
-9 0 . 0 0	8 . 4 7	3 4 1 5 . 3 5	0 . 0 9 9 7 5	1 . 7 5 0 3 1	
-8 0 . 0 0	7 . 1 2	3 3 5 4 . 4 2	0 . 0 9 9 7 4	1 . 7 4 9 7 1	
-7 0 . 0 0	6 . 4 6	3 2 8 7 . 5 9	0 . 0 9 9 7 4	1 . 7 4 9 8 3	
-6 0 . 0 0	6 . 8 1	3 2 2 6 . 1 6	0 . 0 9 9 7 6	1 . 7 4 8 9 8	
-5 0 . 0 0	8 . 4 5	3 1 9 0 . 3 8	0 . 0 9 9 7 4	1 . 7 4 9 4 9	
-4 0 . 0 0	1 1 . 1 4	3 1 8 2 . 4 9	0 . 0 9 9 7 4	1 . 7 4 9 4 5	
-3 0 . 0 0	1 4 . 3 5	3 1 9 9 . 3 3	0 . 0 9 9 7 4	1 . 7 4 9 4 9	
-2 0 . 0 0	1 7 . 5 0	3 2 3 2 . 5 1	0 . 0 9 9 7 4	1 . 7 4 9 4 5	
-1 0 . 0 0	2 0 . 2 4	3 2 7 6 . 2 0	0 . 0 9 9 7 4	1 . 7 4 9 3 7	
-0 0 . 0 0	2 2 . 4 2	3 3 2 6 . 2 8	0 . 0 9 9 7 3	1 . 7 4 9 2 9	
1 0 . 0 0	2 4 . 0 1	3 3 8 0 . 0 7	0 . 0 9 9 7 4	1 . 7 4 9 4 1	
2 0 . 0 0	2 5 . 0 5	3 4 3 7 . 1 1	0 . 0 9 9 7 4	1 . 7 4 9 4 2	
3 0 . 0 0	2 5 . 6 7	3 4 9 7 . 8 1	0 . 0 9 9 7 4	1 . 7 4 9 4 7	
4 0 . 0 0	2 6 . 0 5	3 5 6 2 . 5 7	0 . 0 9 9 7 4	1 . 7 4 9 3 2	
5 0 . 0 0	2 6 . 3 9	3 6 3 1 . 1 2	0 . 0 9 9 7 4	1 . 7 4 9 5 7	

#### H. Running Time

This program takes about ten minutes for each 100 kilometers in altitude. The initial minimum altitude is required in order to estimate the number of kilometers for a particular run. Use Figure 2 and the initial values of B, L and  $\lambda$  to arrive at an estimate of the initial altitude  $h$ . Subtracting 800 kilometers from this value will give the approximate initial minimum altitude of the first ring. This is the altitude used in figuring the running time.

### III. LONGITUDINAL AVERAGING PROCESSOR

#### A. Introduction

Input to this program are the five diurnal average number density tables (Tables 1-5) and the B-L contour rings output from the B-L search routine. The tables are interpolated (extrapolated) in order to obtain a density value for every ten degrees of longitude in the B-L contours. The densities are then added together for each of the five flux models, and the resulting sum is divided by 36 to arrive at the longitudinally averaged number density. This is done for the northern and southern hemispheres separately and then these values are added together and divided by two in order to obtain one number density for each B and L and each of the five flux models. These final values are used as input to the lambda punch program.

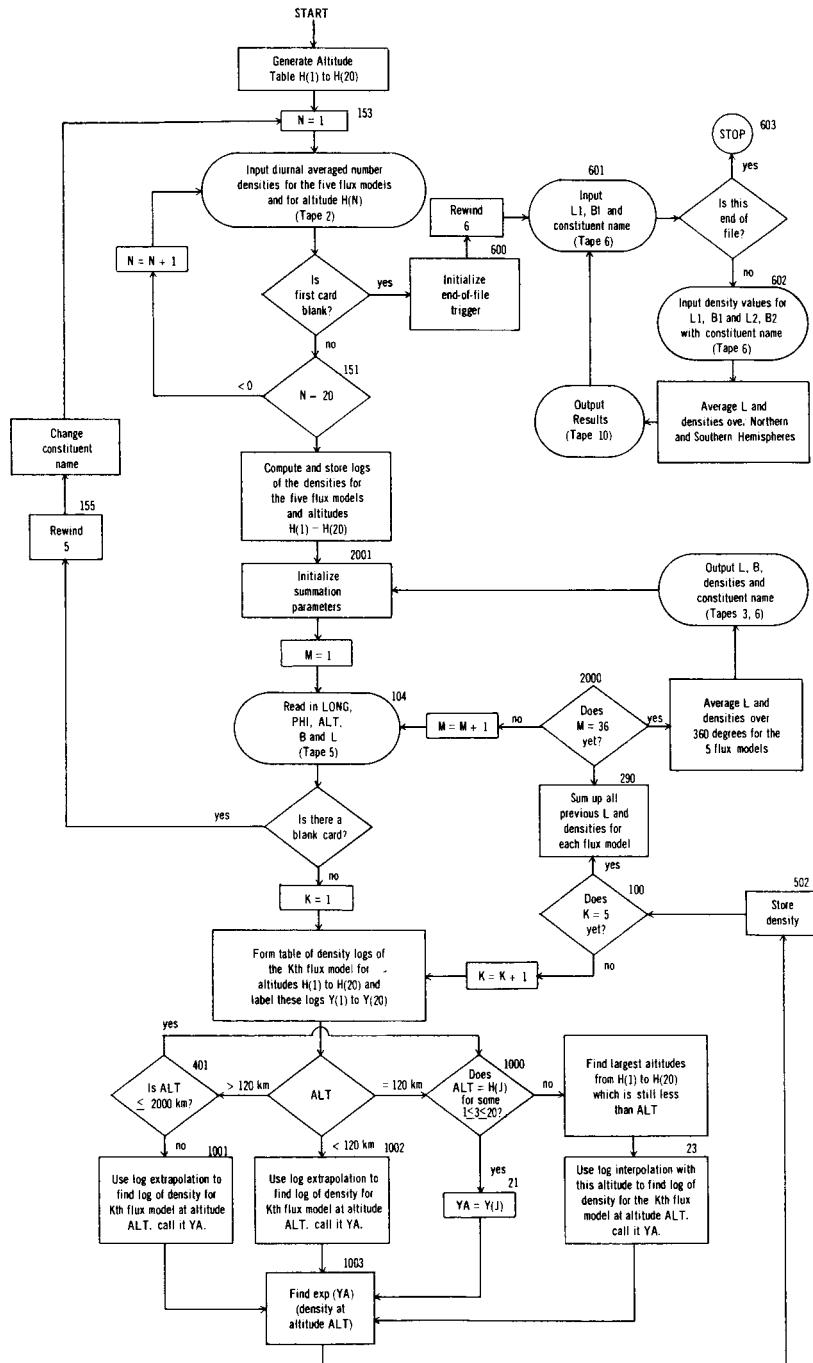
#### B. Mnemonics

<u>Quantity</u>	<u>Description</u>	<u>Units</u>
H(J)	J <sup>th</sup> altitude from the diurnal averaged atmosphere tables, Tables 1-5	km.
S1(J), . . . , S5(J)	diurnal averaged atmosphere densities for the J <sup>th</sup> altitude and fluxes of 250, 200, 150, 100 and $70 \times 10^{-22}$ watts/m <sup>2</sup> /cycle/sec from Tables 1-5	atoms/cm <sup>3</sup>
A1, . . . , A5	temporary storage of S1(J), . . . , S5(J)	"
SS1(J), . . . , SS5(J)	natural logarithms of S1(J), . . . , S5(J)	--
AVHA	sum of EL	earth radii
AVBN1, . . . , AVBN5	density summation for the five flux models	atoms/cm <sup>3</sup>
LONG	geocentric longitude	degrees
PHI	geocentric latitude	degrees

<u>Quantity</u>	<u>Description</u>	<u>Units</u>
ALT	altitude	km.
B	magnetic induction	gauss
EL	magnetic field line	earth radii
Y(I)	temporary storage of SSK(J) at altitude I = J depending on whether K = 1, 2, 3, 4 or 5	--
HA	temporary storage of altitude	km.
YA	natural logarithm of density at altitude ALT	--
BARN	density at altitude ALT	atoms/cm <sup>3</sup>
BARNAV(K)	temporary storage of BARN for flux model K	"
JUNK	temporary storage of K	--
AVERH1	average longitudinal value of EL for only one hemisphere	earth radii
AVERN1, . . . , AVERN5	averaged densities for the five flux models and one hemisphere	atoms/cm <sup>3</sup>
FINI	end of file trigger for tape 6	--
EL1	EL for northern hemisphere	earth radii
EL2	EL for southern hemisphere	"
B1	B for northern hemisphere	gauss
B2	B for southern hemisphere	"

<u>Quantity</u>	<u>Description</u>	<u>Units</u>
EN1, . . . , EN5	the first time this designation appears it represents the northern hemisphere densities for the five flux models. The second time it appears it represents the densities for the north and south averaged together.	atoms/cm <sup>3</sup>
EN12, . . . , EN52	averaged southern hemisphere densities for the five flux models	"
ITT	counter to keep track of which hemisphere is being considered	--
ITTI	counter to keep track of which atmospheric constituent is being considered	--
XLA(ITTI)	first six letters of the constituent name designated by ITTI	--
XLB(ITTI)	last two letters of the constituent name designated by ITTI	--
TSA	first six letters of constituent name	--
TSB	last two letters of constituent name	--

### C. Flow Chart



## D. Fortran Listing

```

C LONGITUDINAL AVERAGING PROCESSOR
DIMENSION S1(20),S2(20),S3(20),S4(20),S5(20),H(20),SS1(20),SS2(20)
1,SS3(20),SS4(20),SS5(20),Y(20),HARNAV(5),ALA(5),XLA(5)
1 FORMATH(8,35)AVERAGE NUMBER DENSITIES FCK DIFF S / IX,
119HSOUTHERN HEMISPHERE)
2 FORMAT(8,12)AVERAGE L=1+6,3,X,2HB=1+6,5)
3 FORMAT(8,35)AVERAGE NUMBER DENSITIES FCK DIFF S / IX,
119HNORTHERN HEMISPHERE)
4 FORMAT(12.4,12X,A6,A2)
5 FORMAT(1H1,8X,25HATMOSPHERIC CONSTITUENT--,A6,A2///)
6 FORMAT(1H0)
7 FORMAT(2F8.5,56X,A6,A2)
8 FORMAT(15E12.4)
1C3 FORMAT(3F12.2,2F12.5)
152 FORMAT(15E12.6)
XLA(1)=6+ELIUM
XLA(2)=6+CXGEN
XLA(3)=6+ C 2
XLA(4)=6+VIRGO
XLA(5)=6+HYDUG
XLB(1)=2h
XLB(2)=2h
XLB(3)=2h
XLB(4)=2h
XLB(5)=2h
LIT=1
LIT=1
153 WRITE OUTPUT TAPE 3,5,XLA(LIT),XLB(LIT)
H(1)=1.0
H(2)=2.0.
UL 15G N=2,1S
H(N+1)=F(N)+10.0.
150 CONTINUE
UC 15I N=1,2C
9tAD INPUT TAPE 2,15Z,S1(N),S2(N),S3(N),S4(N),S5(N)
1F-(S1(I)) 15I,CC,15I
151 COUNT
DC 10 I=1,20
A1=S1(I)
A2=S2(I)
A3=S3(I)
A4=S4(I)
A5=S5(I)
SS1(I)= LGCF(A1)
SS2(I)= LGCF(A2)
SS3(I)= LGCF(A3)
SS4(I)= LGCF(A4)
SS5(I)= LGCF(A5)
1C COUNT
2C1 AVHA=0.
AVB1=0.
AVB2=0.
AVB3=0.
AVB4=0.
AVB5=0.

```

```

1C4   EC 26G0 K=1,36
      READD 1,PLT,TAPE 5, 103,LCNG,PHI,ALT,2,EL
      LF (48) 155,155,505
      REWIN 5
      ITTI=ITTI+1
      LF (ITTI-5) 157,157,153
      1,7 WRITE OUTPUF TAPE 3,5,XLAT(1111),XLH(1111)
      GL TC 123
      DC 1CC K=1,5
      GL TC (2CC,201,2G2,203,2G4),K
      2G0 DC 3C0 I=1,2C
      Y(1)=>S1(1)
      3C1 CCN1NUC
      6G TC 4CC
      2C1 DC 301 I=1,2Q
      Y(1)=>S2(1)
      201 CCN1NUC
      6G TC 4CC
      2G2 DC 302 I=1,2C
      Y(1)=>S3(1)
      3C2 CCN1NUC
      GG TC 4CC
      2G3 DC 3C3 I=1,2C
      Y(1)=>S4(1)
      3C3 CCN1NUC
      GC TC 4CC
      2G4 DC 3C4 I=1,2C
      Y(1)=>S5(1)
      3C4 CCN1NUC
      HA=ALT
      IF (HA-L2G.) 1CC2,1CC0,4C1
      4G1 IF (HA-<CC0.) 1CCC,1CC,1CC1
      1C0 DC 2G J=1,20
      IF ( H(J)-HA ) 2G,21,22
      21 YA=Y(J)
      6G TC 3C
      22 H1=H(J)
      Y1=Y(J)
      HG=H(J-1)
      YG=Y(J-1)
      GU TC <3
      20 CCN1NUC
      23 YA=Y1-(Y1-YG)*(H1-HA)/(H1-HC)
      2G GL TC 1CC3
      1C1 YA=Y(2)+H-A+F(2C)*(Y(2C)-Y(19))/(H-(2C)-F(19))
      GL TC 1CC3
      1C02 YA=Y(2)-(H(2)-HA)*(Y(2)-Y(1))/(H-(2)-F(1))
      1CC3 BARN=EPF(YA)
      5G2 BARNAV(K)=BARN
      JUNK=K
      IF (JUNK=5) 1CC,29C,1C0
      29G AVBA=&LAVFA
      AVBN1 = BARNAV(1)+AVBN1
      AVBN2 = BARNAV(2)+AVBN2
      AVBN3 = BARNAV(3)+AVBN3
      AVBN4 = BARNAV(4)+AVBN4

```

```

LCO  CUNTRUE
2CO  CUNTRUE
AVERH1=AVERH/26.
AVERN1 = AVERN1/36.
AVERN2 = AVERN2/36.
AVERN3 = AVERN3/36.
AVERN4 = AVERN4/36.
AVERN5 = AVERN5/36.
WRITE UCPUT TAPE 3,2,AVERH1,B
IF (ITI=1) 36,05,36
WRITE UCPUT TAPE 3,3
ITI=ITI+1
GO TO 37
36  WRITE UCPUT TAPE 3,1
ITI=1
37  WRITE UCPUT TAPE 3,8,AVERN1,AVERN2,AVERN3,AVERN4,AVERN5
      WRITE UCPUT TAPE 6,7,AVERH1,B,XLA(LIT1)*XLA(LIT1)
      WRITE UCPUT TAPE 6,4,AVERN1,AVERN2,AVERN3,AVERN4,AVERN5,XLA(LIT1)
      1,XLB(LIT1)
      WRITE UCPUT TAPE 3,6
      GO TO 2001
FINI=0,
      WRITE UCPUT TAPE 6,7,FINI,FINI
      RCVINI 6
      READ INPUT TAPE 6,7,ELL,B1,ISA,TSC
      IF (ELL) 602,6C2,6C2
      602  RFLAG INPUT TAPE 6,4,EN1,EN2,EN3,EN4,EN5,ISA,ISE
      READ INPUT TAPE 6,7,ELL,B2,ISA,TSC
      READ INPUT TAPE 6,4,EN12,EN22,EN32,EN42,EN52,ISA,ISE
      EL=(ELL+LL2)/2,
      d=(B1+d2)/2.
      E3=(EN1+EN12)/2.
      EN2=(EN2+EN22)/2.
      EN3=(E3+EN32)/2.
      EN4=(E4+EN42)/2.
      EN5=(EN5+EN52)/2.
      WRITE UCPUT TAPE 10,I,ELL,B,ISA,TSC
      WRITE UCPUT TAPE 1C,4,FN1,EN2,EN3,EN4,EN5,ISA,ISE
      GO TO 601
      CALL F411
END1,L0,0,C,C,C,1,0,C,0,C,C,C,C

```

STRUCTURE NET USE IN PROGRAM

DEC LCT CCT  
1041 C2021  
2251 77461

STORAGE LOCATIONS FOR VARIABLES APPEARING IN CIVILISATION AND EQUIVALENCE STATEMENTS

	DEC	LCT	CCT
EAVG	DEC C1440	94C C1654	S1 C1440
S4	980 01424	SS6 C17CC	S2 C1774
S5	860 01334	SS5 C151C	S2 C16560
S54		XLA 79C 01433	S2 C1426

STORAGE LOCATIONS FOR VARIABLES NOT APPEARING IN COMMON, DIMENSION, OR EQUIVALENCE STATEMENTS

	DEC	LCT	CCT	DEC	LCT	CCT
A1	783 01421	A2 784 0142C	A3 783 01417	A4 782 01416	A5 781 01415	
A1T	78C C1414	AVCN1 775 C1413	AVRN2 776 01412	AVRN3 777 C1411	AVRN4 778 C1410	
AVBN5	775 C1407	AVERN1 774 C1406	AVERN2 775 01405	AVERN3 776 C1404	AVERN4 777 C1403	
AVERN4	776 C1402	AVRN5 765 C1401	AVRN6 768 01400	B1 767 C1377	B2 766 01376	
BARN	765 C1375	B7 764 C1374	BLL 763 01373	EL2 762 C1372	EL 761 01371	
EN112	76C C1376	EN1 759 C1367	EN2 757 C1365	EN2 756 C1364	EN3 755 C1366	
EN3	755 C1365	EN42 754 C1362	EN4 753 01361	EN52 752 C1360	EN5 751 01357	
FIN1	75C C1356	H0 749 C1355	H1 748 01354	H4 747 C1353	H11 746 01352	
ITT	745 01351	J 744 C135C	JUNK 743 01347	K 742 C1346	LONG 741 01345	
W	74C C1344	N 739 C1343	PFI 738 01342	TSA 737 C1341	TSA 736 01340	
Y0	735 01337	Y1 734 C1336	YA 733 01335			

SYMBOLS AND LOCATIONS FOR SOURCE PROGRAM FORMAT STATEMENTS

	EFN	LCC	LCC	EFN	LCC	LCC
EF1	1 01329	EF12 2 01306	EF13 3 01277	EF14 4 01261	EF15 5 01256	
e16	6 01246	e17 7 01245	e18 8 0 01242	e19 9 01240	e14C 8 01235	

LOCATIONS FOR OTHER SYMBOLS NOT APPEARING IN SOURCE PROGRAM

	DEC	CCT	DEC	CCT	DEC	CCT
I1	DEC D1325	62 C165	63 C165	63 C167	41 32761 7777	61 662 01226
H1	63C 01173	C161 724 C133C	C163 729 C1331	C164 730 C1332	C165 731 01333	
C1200	732 01334	C1215 265 CC411	C1219 <92 00445	C1220 143 C0217	D1201 142 C0216	
L17	63 CC122	C1218 66 C013C	C1218 141 C0215	C1221 178 CC262	E120 205 C0215	
L1K	212 CC324	C1219 215 C0333	C1219 226 0042	C1221 257 C04C1	E115 264 00410	
E112	25C CC372					

LOCATIONS OF NAMES IN TRANSFER VECTOR

	DEC	CCT	DEC	CCT	DEC	CCT
(TRN)	8 C0014	EXP (TRN)	7 CCCC7 (TRN)	6 CCCC6 (TRN)	5 CCCC5 (TRN)	4 CCCC4 (TRN)
	4 C0014		1 C0005 (TRN)		3 CCCC3 (TRN)	

ENTRY POINTS TO SUBROUTINES NOT OUTPUT FROM LIBRARY

	DEC	CCT	DEC	CCT
EXI1	zAP	LCC	(FPT)	(RTN)

(TSF)

(TSF)

INTERNAL FORMULA NUMBERS WITH CORRESPONDING INTERNAL FORMULA NUMBERS AND OCTAL LOCATIONS

IFN	LLOC	IFN	LLOC	IFN	LLOC	IFN	LLOC	IFN	LLOC	IFN	LLOC
150	31 CG67	153	32 CCC71	151	36 00123	10	48 00174	2001	49 00176		
154	56 CG20	155	55 CG245	157	62 00766	505	65 00305	200	67 00316		
160	65 CG321	<C1	71 CG325	3C1	73 00330	202	75 00334	302	77 00337		
203	79 CG43	303	81 CG346	204	83 00351	304	85 00354	4CC	86 00356		
401	88 CG369	1CCG	85 CG373	21	91 00403	22	93 00412	2C	98 00425		
21	95 CG427	J0	1C0 CG446	10C1	101 00447	1002	103 00464	10C3	104 00501		
502	1C5 CG566	290	1C8 CG517	1C0	114 00541	2000	115 00544	35	125 00606		
36	128 CG116	J7	130 CGc24	6C0	138 00706	601	142 CC130	602	145 00752		
cC4	1e3 CG151										

## E. Restrictions

Input tables must have densities for altitudes starting at 120 kilometers and followed by each 100-kilometer level up to 2000 kilometers. If the tables are changed then the program must be modified. The tables must be input in the following order:

- (1) helium,
- (2) oxygen,
- (3) molecular oxygen,
- (4) nitrogen,
- (5) hydrogen.

## F. Input

Input to this program is handled by two tapes. On tape 2 are entered the diurnal averaged atmosphere tables (Tables 1-5). These tables are punched on cards and placed one behind the other at the end of the Fortran deck. These tables must be input in the following order: helium, oxygen, molecular oxygen, nitrogen and hydrogen. This is necessary in order that the constituent names may be correctly punched on the output. It is also important that a blank card follow the last table in order to notify the program when it has reached the end of the file.

On tape 5 are placed the B-L contours which were produced by the B-L search program. As with the tables, the last card must be blank in order to designate an end of file.

### 1. Tape 2

#### a. Input Card Description

#### ATMOSPHERE TABLES

<u>Columns</u>	<u>Mode</u>	<u>Quantity</u>	<u>Units</u>	<u>Description</u>		
1-12	E	S1(N)	atoms/cm <sup>3</sup>	density for flux model 1, altitude N		
13-24	E	S2(N)	"	"	"	2, "
25-36	E	S3(N)	"	"	"	3, "
37-48	E	S4(N)	"	"	"	4, "
49-60	E	S5(N)	"	"	"	5, "

**b. Sample GENERAL PURPOSE DATA SHEET**

Problem Spirator	INPUT - LONGITUDINAL AVERAGING PROCESSOR (DENSITY TABLES)		Page SAMPLE	Page (TABLES 1-5)
	TAPE 2	TAPE 1		
1	2	3	4	5
6	7	8	9	10
11	12	13	14	15
16	17	18	19	20
21	22	23	24	25
26	27	28	29	30
31	32	33	34	35
36	37	38	39	40
41	42	43	44	45
46	47	48	49	50
51	52	53	54	55
56	57	58	59	60
61	62	63	64	65
66	67	68	69	70
71	72	73	74	75
76	77	78	79	80
81	82	83	84	85
86	87	88	89	90
91	92	93	94	95
96	97	98	99	100
5.800E+11	5.800E+11	5.800E+11	5.800E+11	5.800E+11
7.393E+69	6.180E+09	4.743E+09	3.136E+09	2.112E+09
7.630E+08	4.639E+08	2.210E+08	6.739E+07	2.113E+07
1.278E+08	5.777E+07	2.151E+07	2.682E+06	4.225E+05
2.562E+07	8.798E+06	1.810E+06	1.407E+05	1.156E+04
5.730E+06	1.521E+06	3.239E+05	8.800E+03	3.844E+02
1.403E+06	2.884E+05	2.763E+04	6.190E+02	1.471E+01
3.664E+05	5.883E+04	3.899E+03	4.802E+01	6.320E-01
1.012E+05	1.276E+04	5.894E+02	4.057E+00	3.006E-02
2.932E+04	2.918E+03	9.470E+01	3.702E-01	1.570E-03
8.862E+03	6.994E+02	1.609E+01	3.627E-02	8.936E-05
2.783E+03	1.752E+02	2.878E+00	3.798E-03	1.016E-05
9.053E+02	4.558E+01	5.404E-01	4.237E-04	3.674E-07
3.041E+02	1.233E+01	1.063E-01	5.017E-05	2.633E-08
1.075E+02	3.456E+00	2.183E-02	6.287E-06	2.023E-09
3.768E+01	1.002E+00	4.677E-03	8.321E-07	1.661E-10
1.380E+01	3.001E-01	1.042E-03	1.160E-07	1.454E-11
5.211E+00	9.268E-02	2.414E-04	1.699E-08	1.353E-12
2.005E+00	2.949E-02	5.746E-05	2.612E-09	1.334E-13
7.927E-01	9.654E-03	1.431E-05	4.619E-10	1.393E-14
7.600E+10	7.600E+10	7.600E+10	7.600E+10	7.600E+10
3.600E+09	3.457E+09	3.209E+09	2.795E+09	2.416E+09
8.870E+08	7.134E+08	5.124E+08	2.809E+08	1.564E+08
3.054E+08	2.054E+08	1.112E+08	4.025E+07	1.471E+07

2. Tape 5

a. Input Card Description

B-L CONTOURS

<u>Columns</u>	<u>Mode</u>	<u>Quantity</u>	<u>Units</u>	<u>Description</u>
1-12	F	LONG	degrees	geocentric longitude
13-24	F	PHI	degrees	geocentric latitude
25-36	F	ALT	km	altitude
37-48	F	B	gauss	magnetic induction
49-60	F	EL	earth radii	magnetic field line

b. Sample

**GENERAL PURPOSE DATA SHEET**

Problem Sponsor	INPUT - LONGITUDINAL AVERAGING PROCESSOR (B-L CONTOURS)		Page of
	TAPE 5	SAMPLE	
1	2	3	4
5	6	7	8
9	10	11	12
13	14	15	16
17	18	19	20
21	22	23	24
25	26	27	28
29	30	31	32
33	34	35	36
37	38	39	40
41	42	43	44
45	46	47	48
49	50	51	52
53	54	55	56
57	58	59	60
61	62	63	64
65	66	67	68
69	70	71	72
73	74	75	76
77	78	79	80
81	82	83	84
85	86	87	88
89	90	91	92
93	94	95	96
97	98	99	100
-18.0	0.0	2.5	6.3
-17.0	0.0	2.3	9.4
-16.0	0.0	2.2	0.1
-15.0	0.0	1.9	9.9
-14.0	0.0	1.7	9.1
-13.0	0.0	1.5	9.3
-12.0	0.0	1.3	9.5
-11.0	0.0	1.2	0.2
-10.0	0.0	1.0	1.6
-9.0	0.0	8.4	7
-8.0	0.0	7.1	2
-7.0	0.0	6.4	6
-6.0	0.0	6.8	1
-5.0	0.0	8.4	5
-4.0	0.0	11.1	14
-3.0	0.0	14.3	5
-2.0	0.0	17.5	0
-1.0	0.0	20.0	24
-0.0	0.0	22.4	2
1.0	0.0	24.0	1
2.0	0.0	25.0	5
3.0	0.0	25.6	7
4.0	0.0	26.0	5
5.0	0.0	26.3	9
1.2	3	4	5
5	6	7	8
8	9	10	11
11	12	13	14
14	15	16	17
17	18	19	20
20	21	22	23
23	24	25	26
26	27	28	29
29	30	31	32
32	33	34	35
35	36	37	38
38	39	40	41
41	42	43	44
44	45	46	47
47	48	49	50
50	51	52	53
53	54	55	56
56	57	58	59
59	60	61	62
62	63	64	65
65	66	67	68
68	69	70	71
71	72	73	74
74	75	76	77
77	78	79	80
80	81	82	83
83	84	85	86
86	87	88	89
89	90	91	92
92	93	94	95
95	96	97	98
98	99	100	101

## G. Output

Output for this program appears on logical tapes 3 and 10. Tape 3 will contain the averaged densities for each of the five flux models at a particular B and L for both northern and southern hemispheres and for each of the five constituents. The constituents (He, O, O<sub>2</sub>, N<sub>2</sub>, H) follow each other in the same order as they exist in the tables which are input on tape 2. Tape 3 is printed with appropriate headings.

Tape 10 also contains densities for the five flux models at each B and L but here the northern and southern hemispheres are averaged together to give one final value for each B and L. Tape 10 contains no headings but each card is labeled with the appropriate constituent name. This tape is punched in order to be used as input to the lambda punch.

A scratch tape must be set up on logical tape unit 6. Although no data appears on this tape at the completion of the program it is used in intermediate steps to store data.

**1. Tape 3 Sample**

ATMOSPHERIC CONSTITUENT--HELIUM

AVERAGE L= 1.142 B=.23891  
AVERAGE NUMBER DENSITIES FOR DIFF S  
NORTHERN HEMISPHERE  
0.8300E 06 0.7508E 06 0.6289E 06 0.4600E 06 0.3382E 06

AVERAGE L= 1.142 B=.23890  
AVERAGE NUMBER DENSITIES FOR DIFF S  
SOUTHERN HEMISPHERE  
0.1346E 08 0.1210E 08 0.1064E 08 0.9134E 07 0.8207E 07

AVERAGE L= 1.142 B=.22741  
AVERAGE NUMBER DENSITIES FOR DIFF S  
NORTHERN HEMISPHERE  
0.7137E 06 0.6282E 06 0.5063E 06 0.3493E 06 0.2433E 06

AVERAGE L= 1.142 B=.22736  
AVERAGE NUMBER DENSITIES FOR DIFF S  
SOUTHERN HEMISPHERE  
0.1428E 07 0.1402E 07 0.1357E 07 0.1293E 07 0.1250E 07

AVERAGE L= 1.142 B=.23465  
AVERAGE NUMBER DENSITIES FOR DIFF S  
NORTHERN HEMISPHERE  
0.7842E 06 0.7021E 06 0.5795E 06 0.4145E 06 0.2984E 06

AVERAGE L= 1.142 B=.23466  
AVERAGE NUMBER DENSITIES FOR DIFF S  
SOUTHERN HEMISPHERE  
0.5205E 07 0.4932E 07 0.4608E 07 0.4235E 07 0.3986E 07

AVERAGE L= 1.142 B=.21968  
AVERAGE NUMBER DENSITIES FOR DIFF S  
NORTHERN HEMISPHERE  
0.6485E 06 0.5615E 06 0.4423E 06 0.2952E 06 0.1996E 06

AVERAGE L= 1.142 B=.21968  
AVERAGE NUMBER DENSITIES FOR DIFF S  
SOUTHERN HEMISPHERE  
0.8665E 06 0.8125E 06 0.7325E 06 0.6253E 06 0.5477E 06

AVERAGE L= 1.170 B=.23992  
AVERAGE NUMBER DENSITIES FOR DIFF S  
NORTHERN HEMISPHERE  
0.7300E 06 0.6415E 06 0.5134E 06 0.3472E 06 0.2351E 06

AVERAGE L= 1.170 B=.23991  
AVERAGE NUMBER DENSITIES FOR DIFF S  
SOUTHERN HEMISPHERE  
0.1571E 08 0.1399E 08 0.1217E 08 0.1032E 08 0.9197E 07

AVERAGE L= 1.170 B=.23468  
AVERAGE NUMBER DENSITIES FOR DIFF S  
NORTHERN HEMISPHERE  
0.6785E 06 0.5881E 06 0.4614E 06 0.3026E 06 0.1990E 06

AVERAGE L= 1.170 B=.23467  
AVERAGE NUMBER DENSITIES FOR DIFF S  
SOUTHERN HEMISPHERE  
0.5025E 07 0.4766E 07 0.4459E 07 0.4106E 07 0.3874E 07

AVERAGE L= 1.170 B=.22957  
AVERAGE NUMBER DENSITIES FOR DIFF S  
NORTHERN HEMISPHERE  
0.6319E 06 0.5403E 06 0.4158E 06 0.2647E 06 0.1693E 06

AVERAGE L= 1.170 B=.22956  
AVERAGE NUMBER DENSITIES FOR DIFF S  
SOUTHERN HEMISPHERE  
0.1975E 07 0.1940E 07 0.1885E 07 0.1810E 07 0.1758E 07

AVERAGE L= 1.170 B=.21976  
AVERAGE NUMBER DENSITIES FOR DIFF S  
NORTHERN HEMISPHERE  
0.5513E 06 0.4595E 06 0.3410E 06 0.2052E 06 0.1246E 06

AVERAGE L= 1.170 B=.21977  
AVERAGE NUMBER DENSITIES FOR DIFF S  
SOUTHERN HEMISPHERE  
0.8559E 06 0.8062E 06 0.7343E 06 0.6406E 06 0.5740E 06

AVERAGE L= 1.170 B=.20975  
AVERAGE NUMBER DENSITIES FOR DIFF S  
NORTHERN HEMISPHERE  
0.4812E 06 0.3913E 06 0.2804E 06 0.1600E 06 0.9249E 05

AVERAGE L= 1.170 B=.20972  
AVERAGE NUMBER DENSITIES FOR DIFF S  
SOUTHERN HEMISPHERE  
0.6456E 06 0.5736E 06 0.4764E 06 0.3555E 06 0.2730E 06

AVERAGE L= 1.170 B=.20474  
AVERAGE NUMBER DENSITIES FOR DIFF S  
NORTHERN HEMISPHERE  
0.4513E 06 0.3629E 06 0.2560E 06 0.1428E 06 0.8090E 05

AVERAGE L= 1.170 B=.20475  
AVERAGE NUMBER DENSITIES FOR DIFF S  
SOUTHERN HEMISPHERE  
0.5692E 06 0.4911E 06 0.3896E 06 0.2688E 06 0.1907E 06

AVERAGE L= 1.170 B=.20141  
AVERAGE NUMBER DENSITIES FOR DIFF S  
NORTHERN HEMISPHERE  
0.4332E 06 0.3460E 06 0.2419E 06 0.1333E 06 0.7469E 05

AVERAGE L= 1.170 B=.20134  
 AVERAGE NUMBER DENSITIES FOR DIFF S  
 SOUTHERN HEMISPHERE  
 0.5207E 06 0.4399E 06 0.3375E 06 0.2199E 06 0.1474E 06

AVERAGE L= 1.188 B=.23382  
 AVERAGE NUMBER DENSITIES FOR DIFF S  
 NORTHERN HEMISPHERE  
 0.6179E 06 0.5248E 06 0.3992E 06 0.2485E 06 0.1550E 06

AVERAGE L= 1.188 B=.23383  
 AVERAGE NUMBER DENSITIES FOR DIFF S  
 SOUTHERN HEMISPHERE  
 0.3782E 07 0.3632E 07 0.3447E 07 0.3229E 07 0.3084E 07

AVERAGE L= 1.188 B=.21177  
 AVERAGE NUMBER DENSITIES FOR DIFF S  
 NORTHERN HEMISPHERE  
 0.4507E 06 0.3605E 06 0.2517E 06 0.1373E 06 0.7561E 05

AVERAGE L= 1.188 B=.21175  
 AVERAGE NUMBER DENSITIES FOR DIFF S  
 SOUTHERN HEMISPHERE  
 0.6639E 06 0.5964E 06 0.5050E 06 0.3904E 06 0.3108E 06

AVERAGE L= 1.188 B=.25851  
 AVERAGE NUMBER DENSITIES FOR DIFF S  
 NORTHERN HEMISPHERE  
 0.8776E 06 0.7972E 06 0.6687E 06 0.4846E 06 0.3495E 06

AVERAGE L= 1.188 B=.25853  
 AVERAGE NUMBER DENSITIES FOR DIFF S  
 SOUTHERN HEMISPHERE  
 0.8554E 09 0.6005E 09 0.3943E 09 0.2397E 09 0.1695E 09

AVERAGE L= 1.188 B=.24959  
 AVERAGE NUMBER DENSITIES FOR DIFF S  
 NORTHERN HEMISPHERE  
 0.7733E 06 0.6856E 06 0.5550E 06 0.3807E 06 0.2603E 06

AVERAGE L= 1.188 B=.24954  
 AVERAGE NUMBER DENSITIES FOR DIFF S  
 SOUTHERN HEMISPHERE  
 0.1175E 09 0.9275E 08 0.7004E 08 0.5030E 08 0.3995E 08

AVERAGE L= 1.188 B=.23938  
 AVERAGE NUMBER DENSITIES FOR DIFF S  
 NORTHERN HEMISPHERE  
 0.6690E 06 0.5769E 06 0.4486E 06 0.2890E 06 0.1862E 06

AVERAGE L= 1.188 B=.23934  
 AVERAGE NUMBER DENSITIES FOR DIFF S  
 SOUTHERN HEMISPHERE  
 0.1212E 08 0.1095E 08 0.9695E 07 0.8383E 07 0.7571E 07

AVERAGE L= 1.188 B=.21981  
AVERAGE NUMBER DENSITIES FOR DIFF S  
NORTHERN HEMISPHERE  
0.5056E 06 0.4133E 06 0.2976E 06 0.1702E 06 0.9799E 05

AVERAGE L= 1.188 B=.21981  
AVERAGE NUMBER DENSITIES FOR DIFF S  
SOUTHERN HEMISPHERE  
0.8335E 06 0.7838E 06 0.7133E 06 0.6223E 06 0.5579E 06

AVERAGE L= 1.188 B=.20482  
AVERAGE NUMBER DENSITIES FOR DIFF S  
NORTHERN HEMISPHERE  
0.4087E 06 0.3211E 06 0.2185E 06 0.1146E 06 0.6086E 05

AVERAGE L= 1.188 B=.20481  
AVERAGE NUMBER DENSITIES FOR DIFF S  
SOUTHERN HEMISPHERE  
0.5597E 06 0.4837E 06 0.3855E 06 0.2689E 06 0.1932E 06

AVERAGE L= 1.200 B=.24991  
AVERAGE NUMBER DENSITIES FOR DIFF S  
NORTHERN HEMISPHERE  
0.7400E 06 0.6498E 06 0.5184E 06 0.3469E 06 0.2312E 06

AVERAGE L= 1.200 B=.24992  
AVERAGE NUMBER DENSITIES FOR DIFF S  
SOUTHERN HEMISPHERE  
0.1125E 09 0.8896E 08 0.6733E 08 0.4849E 08 0.3861E 08

AVERAGE L= 1.200 B=.23952  
AVERAGE NUMBER DENSITIES FOR DIFF S  
NORTHERN HEMISPHERE  
0.6373E 06 0.5438E 06 0.4160E 06 0.2608E 06 0.1634E 06

AVERAGE L= 1.200 B=.23948  
AVERAGE NUMBER DENSITIES FOR DIFF S  
SOUTHERN HEMISPHERE  
0.1122E 08 0.1018E 08 0.9049E 07 0.7866E 07 0.7131E 07

AVERAGE L= 1.200 B=.22940  
AVERAGE NUMBER DENSITIES FOR DIFF S  
NORTHERN HEMISPHERE  
0.5508E 06 0.4569E 06 0.3357E 06 0.1976E 06 0.1166E 06

AVERAGE L= 1.200 B=.22938  
AVERAGE NUMBER DENSITIES FOR DIFF S  
SOUTHERN HEMISPHERE  
0.1666E 07 0.1638E 07 0.1594E 07 0.1536E 07 0.1496E 07

AVERAGE L= 1.200 B=.21979  
AVERAGE NUMBER DENSITIES FOR DIFF S  
NORTHERN HEMISPHERE  
0.4790E 06 0.3869E 06 0.2735E 06 0.1516E 06 0.8459E 05

AVERAGE L= 1.200 B=.21980  
AVERAGE NUMBER DENSITIES FOR DIFF S  
SOUTHERN HEMISPHERE  
0.8144E 06 0.7642E 06 0.6936E 06 0.6031E 06 0.5390E 06

AVERAGE L= 1.200 B=.20970  
AVERAGE NUMBER DENSITIES FOR DIFF S  
NORTHERN HEMISPHERE  
0.4136E 06 0.3249E 06 0.2207E 06 0.1151E 06 0.6061E 05

AVERAGE L= 1.200 B=.20971  
AVERAGE NUMBER DENSITIES FOR DIFF S  
SOUTHERN HEMISPHERE  
0.6189E 06 0.5489E 06 0.4559E 06 0.3416E 06 0.2637E 06

AVERAGE L= 1.200 B=.18974  
AVERAGE NUMBER DENSITIES FOR DIFF S  
NORTHERN HEMISPHERE  
0.3116E 06 0.2325E 06 0.1468E 06 0.6859E 05 0.3260E 05

AVERAGE L= 1.200 B=.18975  
AVERAGE NUMBER DENSITIES FOR DIFF S  
SOUTHERN HEMISPHERE  
0.3818E 06 0.3026E 06 0.2112E 06 0.1179E 06 0.6790E 05

2. Tape 10

a. Output card description

	<u>Columns</u>	<u>Mode</u>	<u>Quantity</u>	<u>Units</u>	<u>Description</u>		
B, L Card	1-8	F	EL	earth radii	averaged magnetic field line		
	9-16	F	B	gauss	magnetic induction		
	72-80	-	-	-	constituent name		
Density Card	1-12	E	EN1	atoms/cm <sup>3</sup>	density for flux model 1		
	13-24	E	EN2	atoms/cm <sup>3</sup>	den	"	2
	25-36	E	EN3	"	"	"	3
	37-48	E	EN4	"	"	"	4
	49-60	E	EN5	"	"	"	5
	72-80	-	-	-	constituent name		

b. Sample

## GENERAL PURPOSE DATA SHEET

Problem Sponsor	OUTPUT - LONGITUDINAL AVERAGING PROCESSOR (NORTH-SOUTH AVERAGE)		Page of
	TAPE 10	DATA SAMPLE	
1. 2. 3. 4. 5. 6. 7. 8. 9. 10. 11. 12. 13. 14. 15. 16. 17. 18. 19. 20. 21. 22. 23. 24. 25. 26. 27. 28. 29. 30. 31. 32. 33. 34. 35. 36. 37. 38. 39. 40.			NITROGEN
1. 1. 4. 1. 9. 6. 0. . 2. 3. 8. 9. 0.			NITROGEN
0. . 3. 8. 8. 1. E. 1. 3. 0. . 4. 9. 1. 4. E. 1. 3. 0. . 6. 9. 7. 5. E. 1. 3. 0. . 1. 2. 0. 9. E. 1. 4. 0. . 2. 0. 3. 6. E. 1. 4.			NITROGEN
1. 1. 4. 1. 9. 7. 0. . 2. 2. 7. 3. 8.			NITROGEN
0. . 2. 4. 3. 0. E. 1. 0. 0. . 2. 2. 5. 8. E. 1. 0. 0. . 2. 0. 3. 8. E. 1. 0. 0. . 1. 7. 4. 8. E. 1. 0. 0. . 1. 5. 2. 1. E. 1. 0.			NITROGEN
1. 1. 4. 1. 9. 8. 0. . 2. 3. 4. 6. 5.			NITROGEN
0. . 2. 7. 4. 5. E. 1. 2. 0. . 3. 1. 1. 9. E. 1. 2. 0. . 3. 7. 7. 1. E. 1. 2. 0. . 5. 0. 9. 5. E. 1. 2. 0. . 6. 7. 8. 0. E. 1. 2.			NITROGEN
1. 1. 4. 2. 0. 0. 0. . 2. 1. 9. 6. 8.			NITROGEN
0. . 6. 7. 8. 4. E. 0. 8. 0. . 4. 4. 8. 8. E. 0. 8. 0. . 2. 5. 3. 3. E. 0. 8. 0. . 1. 0. 5. 7. E. 0. 8. 0. . 4. 7. 2. 0. E. 0. 7.			NITROGEN
1. 1. 7. 0. 0. 1. 0. . 2. 3. 9. 9. 1.			NITROGEN
0. . 5. 1. 8. 0. E. 1. 3. 0. . 6. 5. 6. 5. E. 1. 3. 0. . 9. 3. 3. 0. E. 1. 3. 0. . 1. 6. 1. 5. E. 1. 4. 0. . 2. 7. 1. 1. E. 1. 4.			NITROGEN
1. 1. 7. 0. 0. 0. 0. . 2. 3. 4. 6. 7.			NITROGEN
0. . 2. 2. 5. 8. E. 1. 2. 0. . 2. 5. 1. 9. E. 1. 2. 0. . 2. 9. 6. 2. E. 1. 2. 0. . 3. 8. 1. 9. E. 1. 2. 0. . 4. 8. 5. 8. E. 1. 2.			NITROGEN
1. 1. 6. 9. 9. 4. 0. . 2. 2. 9. 5. 6.			NITROGEN
0. . 9. 9. 5. 6. E. 1. 0. 0. . 9. 7. 5. 5. E. 1. 0. 0. . 9. 4. 9. 0. E. 1. 0. 0. . 9. 1. 1. 0. E. 1. 0. 0. . 8. 7. 8. 5. E. 1. 0.			NITROGEN
1. 1. 1. 7. 0. 0. 2. 0. . 2. 1. 9. 7. 6.			NITROGEN
0. . 8. 7. 4. 2. E. 0. 8. 0. . 6. 0. 8. 9. E. 0. 8. 0. . 3. 6. 6. 2. E. 0. 8. 0. . 1. 6. 6. 7. E. 0. 8. 0. . 8. 0. 1. 5. E. 0. 7.			NITROGEN
1. 1. 1. 7. 0. 0. 6. 0. . 2. 0. 9. 7. 3.			NITROGEN
0. . 7. 8. 5. 3. E. 0. 7. 0. . 3. 6. 0. 2. E. 0. 7. 0. . 1. 3. 4. 3. E. 0. 7. 0. . 2. 0. 6. 0. E. 0. 6. 0. . 3. 8. 8. 6. E. 0. 5.			NITROGEN
1. 1. 1. 7. 0. 0. 0. 0. . 2. 0. 4. 7. 4.			NITROGEN
0. . 2. 6. 8. 7. E. 0. 7. 0. . 9. 9. 8. 7. E. 0. 6. 0. . 2. 7. 0. 2. E. 0. 6. 0. . 2. 6. 1. 5. E. 0. 5. 0. . 3. 0. 9. 9. E. 0. 4.			NITROGEN
1. 1. 1. 7. 0. 0. 5. 0. . 2. 0. 1. 3. 7.			NITROGEN
0. . 1. 2. 8. 1. E. 0. 7. 0. . 4. 0. 7. 9. E. 0. 6. 0. . 8. 5. 5. 8. E. 0. 5. 0. . 5. 9. 9. 5. E. 0. 4. 0. . 5. 0. 5. 9. E. 0. 3.			NITROGEN
1. 1. 1. 8. 7. 9. 5. 0. . 2. 3. 3. 8. 2.			NITROGEN
0. . 9. 7. 2. 5. E. 1. 1. 0. . 1. 0. 4. 7. E. 1. 2. 0. . 1. 1. 6. 6. E. 1. 2. 0. . 1. 3. 8. 2. E. 1. 2. 0. . 1. 6. 2. 3. E. 1. 2.			NITROGEN

#### H. Running Time

An allowance of 8 seconds for each B-L line will give a close estimate of the running time for this program.

## IV. LAMBDA PUNCH

### A. Introduction

This program takes the cards from the longitudinal averaging processor and punches the latitude in degrees on every B-L card. This value is necessary in the execution of the "bounce" average calculation.

Computing the latitude is done by the method of false position using the equation.

$$B = \frac{M}{r_e^3} \frac{\sqrt{4 - 3 \cos^2 \lambda}}{L^3 \cos^6 \lambda} \quad (1)$$

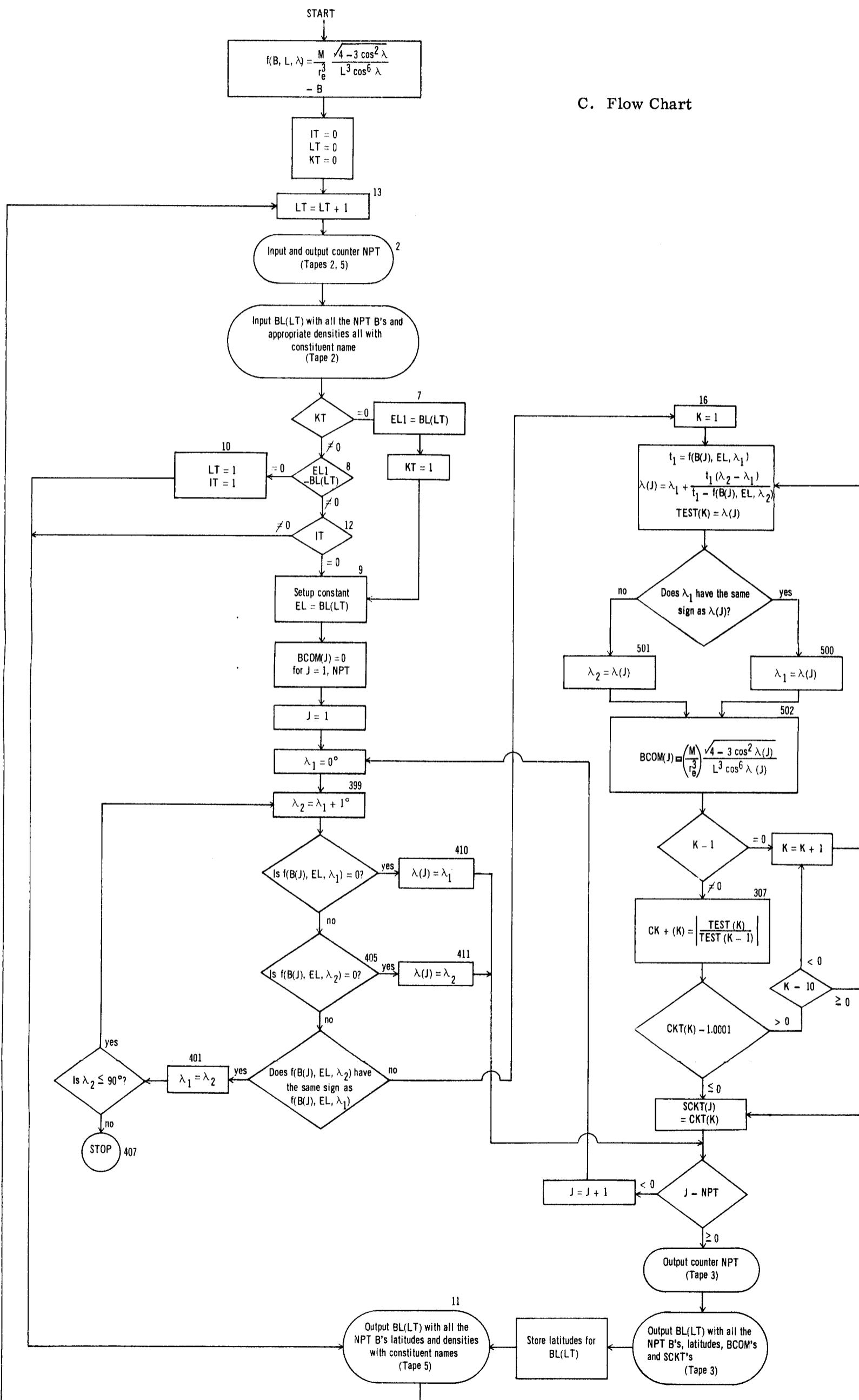
where  $M$  is the earth's magnetic dipole moment,  $r_e$  is the radius of the earth and  $\lambda$  is the latitude.  $B$  is traded to the right hand side of equation (1) and the resulting function is evaluated for zero at a fixed  $B$  and  $L$ :

$$BFUNF(B, L, \lambda) = \frac{M}{r_e^3} \frac{\sqrt{4 - 3 \cos^2 \lambda}}{L^3 \cos^6 \lambda} - B$$

### B. Mnemonics

<u>Quantity</u>	<u>Description</u>	<u>Units</u>
IT	counter to eliminate repetition in computation	-
LT	L counter	-
KT	counter to determine whether a particular L is the first L considered	-
RTD	conversion factor - radians to degrees	-
DTR	" " - degrees to radians	-

<u>Quantity</u>	<u>Description</u>	<u>Units</u>
RE	radius of the earth ( $6378.16 \times 10^5$ )	cm
EM	the earth's magnetic dipole moment ( $8.1 \times 10^{25}$ gauss cm <sup>3</sup> ) divided by the radius of the earth cubed	gauss
NPT	count of the number of B's to a given L	-
BL(J)	J <sup>th</sup> magnetic field line	earth radii
B(I)	I <sup>th</sup> magnetic induction for a given L	gauss
SS1(I),..., SS5(I)	longitudinally averaged number densities for the five flux models and the I <sup>th</sup> B.	atoms/cm <sup>3</sup>
RATIO(I)	ratio of the upper limit on the latitude XLW2 to the lower limit on the latitude XLW1 for the I <sup>th</sup> B.	-
BCOM(I)	B computed for the final latitude XLAMP(I) at B(I)	gauss
XLW1	lower limit on the latitude	radians
XLW2	upper limit on the latitude	"
FXLW1	BFUNF computed for XLW1	-
FXLW2	" " " XLW2	-
XLAMP(I)	final selected latitude for B(I)	radians/ degrees
TERM 1	BFUNF computed for XLW1	-
TBLAM(J, I)	latitude for the I <sup>th</sup> B of the J <sup>th</sup> L	degrees
TEST(K)	temporary storage of XLAMP(J)	radians
CKT(K)	the absolute value of TEST(K)/TEST(K-1)	-
SCKT(J)	temporary storage of final CKT(K)	-



C. Flow Chart

#### D. Fortran Listing

```

LAPBUN
C  LAPBUN BUNCH
      DIMENSION BL(25),EL(25),EL(25),SS1(5),SS2(5),SS3(5),SS4(5),
      ISSS(25),CC(25),CL(25),TSL(25),CKT(25),SLNP(25),
      BFUNFL,IM,EL,XLMF=EM*SCRF(4.0-3.0*CCSF(XLMF)**21/(1-L**2))*
      ICSE(XLMF)*6)-3
      -RRC4_1 = LAMBDA GREATER THAN 9.0 DEG.
C  FORMATS
      ICO FORMAT(I2)
      I01 FORMAT(12F-5.5,56A,A6,A2)
      I02 FORMAT(5C16.4,1X,A6,A6,A2)
      I03 FORMAT(6F ERROR,I2)
      I04 FORMAT(1H NPI,5X,1HL,9X,1HB,6X,6HLAMBCN,4X,9H CEMP.,16A,5I RATI
      I05 FORMAT(14)
      I06 FORMAT(4X,2E10.5,F10.4,2E15.7)
      I07 FORMAT(2F8.5,F8.3,4E8.6,A2/5E12.4,12X,A6,A2)
      IT=0
      LI=0
      KT=0
      K=1
      GU TC Y
      8 IF (TEL-BL(LT)) 12,1G,12
      12 IF (LT) 11,9,11
      11 IF (LT) 10,10,10
      9  READ INPUT TAPE 2,ICO,NPT
      10 WRITE OUTPUT TAPE 5,ICO,NPT
      DU 18 L=1,NPT
      READ INPUT TAPE 2,IC1,BL(L)*d(L),XL,XLB
      18 READ INPUT TAPE 2,102,SS1(L),SS2(L),SS3(L),SS4(L),SS5(L),XL,A,ALB
      IF(KT) 8,7,8
      7 EL=LBL(LT)
      K=1
      GU TC Y
      8 IF (TEL-BL(LT)) 12,1G,12
      12 IF (LT) 11,9,11
      11 IF (LT) 10,10,10
      9  READ INPUT TAPE 2,IC1,BL(L)*d(L),XL,XLB
      10 WRITE OUTPUT TAPE 5,ICO,NPT
      DU 199 BCOM(11)=0.0
      DC 200 J=1,NP1
      XLW1=0.0
      399 XLW2=XLW1+CTR
      FALW1=BFUNF(B(J1),EL,XLMF)
      FALW2=BFUNF(B(J2),EL,XLMF)
      IF (FALW1) 405,410,405
      405 IF (FALW2) 406,411,406
      406 IF (FALW1-SIGN(FALW1,FALW2)) 16,4C1,16
      401 XLW1=XLW2
      IF (XLW2-1.5707961) 399,399,4C7
      4C7 IERR=1
      WRITE OUTPUT TAPE 3,103,IERR
      CALL EXIT
      410 XLMAMP(j)=XLW1
      GU TO 200

```

```

411 XLAHP(J)=XLWZ
  GC TC ZCG
  N>TUE UF FALSE POSITION
C
16 GL L5; K=1,1C
  TTKL=JL+H(S(J),S(L),XLWZ)
  XLAHP(J)=XLW+TURS(L)/TEW+EFUNF(C(J),EN,EL+AL,EL)
17 (XLWZ-AL)
  TEST(K:=XLADP(J))
  IF(XLAHP(J)=XLADP(J)-SLUF(XLAHP(J),XLWZ)) E(L,SL,SC1
500 XLW=XLADP(J)
502 BCDF(J)=EN*SCRF(4-C-3.0*CLSFXLAHP(J))**2/((EL**2)*
  LCSE(XLAHP(J))**6)
  IF(K=2,307,15G,4G)
  CKT(K)=abs(FILEST(K))/S1(K-1)
  If TCKT(K)-1.GOC1) 4G,209,15C
501 XLW2=XLAHP(J)
  GC TC ZCG
150 CONTINUE
309 SCKT(J)=CKT(K)
200 CONTINUE
  WRITE OUTPUT TAPE 3,1C4
  WRITE OUTPUT TAPE 3,1G5,NP1
  DC 201 L=1,NP1
  XLAHP(L)=XLAHP(L)*R1C
201 WRITE OUTPUT TAPE 3,1G6,BL(LT),B(L),XLAHP(L),GCCP(L),SCKT(L)
15 TGLAP(L,J)=XLADP(J)
  GC TC 11
10 LT=1
11 DC 17 L=1,NP1
17 WLT=OUTPUT TAPE 5,1G7,BL(LT),B(L),TGLAP(L,L),XLAP(L,L),S1(L),
  1352(L),SS3(L),SS4(L),SS5(L),XL,A,XLE
  G1,TC 13
  EN,D1,1,C,C,0,C,1,O,C,C,0,C,0

```

## STORAGE NC1 USED BY PROGRAM

DEC LCF  
1440 C2646DEC OCT  
32561 17461

## STORAGE LOCATIONS FOR VARIABLES APPEARING IN DIMENSION AND EQUIVALENCE STATEMENTS

DEC LCF	BL	DEC OCT	DEC OCT	DEC CCT	DEC CCT
BCOM 1295 02417	SS2	1395 C2563	1449 C2545	CRT 1225 C2311	SUR 12C5 C2245
SS1 1420 02261	TSST	1245 02355	1370 C2532	SS4 1345 C2301	SS5 1326 C2436
TBLW 1155 02203			XLAMP 1180 C2234		

## STORAGE LOCATIONS FOR VARIABLES NOT APPEARING IN DIMENSION, EQUIVALENCE, OR EQUIVALENCE STATEMENTS

DEC LCF	EL1	DEC OCT	DEC OCT	DEC CCT	DEC CCT
DTA 530 C1022	52S 01021	EL	528 01026	E 227 C1617	F XLW 1
XLW2 525 C1015	TERR	524 01014	11 523 01013	K 522 C1612	K 521 C1011
L1 520 01010	NPT	519 01027	RT	RTU 518 C1606	TEM 1
XL4 515 C1003	XLB	514 01022	XWL	XLW2 513 01021	SL 01004

## SYMBOLS AND LOCATIONS FOR SOURCE PROGRAM FORMAT STATEMENTS

EFN LCC					
8134 100 CC154	8135 1C1 00153	8136 1C2 CC150	8137 1C3 CC145	8138 1C4 CC142	8139 104 CC142
8139 105 CC127	813A 1C6 00126	813B 1C7 CC122			

## LOCATIONS FOR CIPHER SYMBOLS NOT APPEARING IN SOURCE PROGRAM

DEC CCT	DEC OCT	DEC OCT	DEC CCT	DEC CCT	DEC CCT
1 494 CC155	111 495 CC173	21 454 00167	31 508 CC174	41 505 CC175	41 32767 11117
+11 511 CC171	61 454 00166	71 544 00161	14 76 CC114	510 CC125	
C1G4 151 CC177	D140A 116 C0164	D140C 234 00152	E1H 183 CC267	E1K 291 CC443	116 85 C0125
L1F 152 CC226					11P 296 00450
11S 3C5 CC456					

## LOCATIONS OF NAMES IN TRANSFER VECTOR

DEC CCT	DEC OCT	DEC CCT	DEC CCT	DEC CCT	DEC CCT
LDS 1 C0001	EXIT 7 00001	SCRT 2 00002	(FILE) 6 00006	(FILE) 0 00000	(FILE) 0 00000
(TRN) 4 C0004	5 C0005	(1ST)			

## ENTRY POINTS TO SUBROUTINES NOT OUTPUT FROM LIBRARY

CRS EXIT (FILE) (FILE) (TRN) (1ST)

## NAMES AND LOCATIONS OF ARITHMETIC STATEMENT FUNCTIONS

DEC CCT	DEC CCT	DEC CCT	DEC CCT	DEC CCT
EFUN 4C CCT21				

## INTERNAL FORMULA NUMBERS WITH CURRENT SPECIFYING INTERNAL FORMULA NUMBERS AND OCIAL LOCATIONS

IFN	IFN	LUC	IFN	LUC	IFN	LUC	IFN	LUC	IFN	LUC
13	13	C0129	16	C0131	16	C0164	23	C0164	26	C0115
12	31	C0126	9	C0132	159	C0159	37	C0159	399	C0167
106	46	C026	401	C0247	401	C0247	90	C0247	410	C0264
16	56	C0273	51	C0354	52	C0356	62	C0356	307	C0426
13C	63	C0342	3C9	C0452	2CC	70	C0354	84	C0355	2C1
1C	81	C0343	11	C0351	17	C0355	11	C0355	76	C0305

## E. Restrictions

Before the first card of a new L line section a counter card must be inserted in order to inform the computer of the number of B's connected with that L.

## F. Input

There are three different cards in the input deck for this program. A counter card is followed by the designated number of card pairs for each L line of every constituent. The card pairs consist of a B-L card and a density card in that order. These are the cards output from the longitudinal averaging processor.

### 1. (Tape 2)

#### CARD DESCRIPTION

	<u>Columns</u>	<u>Mode</u>	<u>Quantity</u>	<u>Units</u>	<u>Description</u>						
Counter Card	1-2	I	NPT	-	B-L, density card pair counter						
B-L Card	1-8	F	EL	earth radii	mag	field	line				
	9-16	F	B	gauss							magnetic induction
	73-80	-	-	-							constituent name
Density Card	1-12	E	SS1	atoms/cm <sup>3</sup>	den	sity	for	flux	mod	el	1
	13-24	E	SS2	"	"	"	"	"	"	"	2
	25-36	E	SS3	"	"	"	"	"	"	"	3
	37-48	E	SS4	"	"	"	"	"	"	"	4
	49-60	E	SS5	"	"	"	"	"	"	"	5
	73-80	-	-	-							constituent name

2. Sample

GENERAL PURPOSE DATA SHEET

Problem	INPUT - LAMBDA PUNCH		Date	SAMPLE	Page	of
	Sponsor	TAPE 2				
1	1.14196	0.23890				NITROGEN
4	0.3881E	13	0.4914E	13	0.6975E	13
	1.14196	0.22738				NITROGEN
	0.2430E	10	0.2258E	10	0.2038E	10
	1.14198	0.23465				NITROGEN
	0.2745E	12	0.3119E	12	0.3771E	12
	1.14200	0.21968				NITROGEN
	0.6784E	08	0.4488E	08	0.2533E	08
7						NITROGEN
	1.17001	0.23991				NITROGEN
	0.5180E	13	0.6565E	13	0.9330E	13
	1.17000	0.23467				NITROGEN
	0.2258E	12	0.2519E	12	0.2962E	12
	1.16994	0.22956				NITROGEN
	0.9956E	10	0.9755E	10	0.9490E	10
	1.17002	0.21976				NITROGEN
	0.8742E	08	0.6089E	08	0.3662E	08
	1.17006	0.20973				NITROGEN
	0.7853E	07	0.3602E	07	0.1343E	07
	1.17000	0.20474				NITROGEN
	0.2687E	07	0.9987E	06	0.2702E	06
	1.17005	0.20137				NITROGEN
	0.1281E	07	0.4079E	06	0.8558E	05
	0.1281E	07	0.4079E	04	0.5995E	04
						NITROGEN
						NITROGEN

## G. Output

Output for this program occurs on logical tapes 3 and 5. Tape 3 contains the results of the latitude calculation. The counter NPT is printed along with L, B,  $\lambda$ , BCOMP and the ratio RATIO. BCOMP is the new B computed by inserting the values of L and  $\lambda$  into equation (1). It should compare with the initial B. RATIO is the ratio of  $\lambda$  to a former value of the latitude computed in the intermediate steps. It is the same as SCKT (refer to the mnemonics listing). RATIO should be within .0001 of unity.

Tape 5 contains the same data that was input on tape 2 with the exception that latitudes were added. This tape is punched and used as input for the "bounce" average calculation.

1. Tape 3 Sample

NPT	L	B	LAMBDA	B COMP.	RATIO
4					
	1.14200	0.23890	9.836	0.2389000E-00	0.1000009E 01
	1.14200	0.22738	7.740	0.2273800E-00	0.1000034E 01
	1.14200	0.23465	9.129	0.2346499E-00	0.1000039E 01
	1.14200	0.21968	5.867	0.2196800E-00	0.1000023E 01

NPT	L	B	LAMBDA	B CUMP.	RATIO
7					
1.17005	0.23991	12.444	0.2399099E-00	0.1000030E 01	
1.17005	0.23467	11.752	0.2346700E-00	0.1000012E 01	
1.17005	0.22956	11.022	0.2295600E-00	0.1000005E 01	
1.17005	0.21976	9.420	0.2197599E-00	0.1000056E 01	
1.17005	0.20973	7.346	0.2097300E-00	0.1000005E 01	
1.17005	0.20474	6.014	0.2047400E-00	0.1000015E 01	
1.17005	0.20137	4.894	0.2013700E-00	0.1000025E 01	

2. Tape 5

a. Output card description

	<u>Columns</u>	<u>Mode</u>	<u>Quantity</u>	<u>Units</u>	<u>Description</u>						
Counter Card	1-2	I	NPT	-	B-L-λ and density card pair counter						
B-L-λ Card	1-8	F	EL	earth radii	mag	field	line				
	9-16	F	B	gauss	magn	etic	induction				
	17-24	F	XLAM	degrees	lati	tude					
	73-80	-	-	-	constituent	name					
Density Card	1-12	E	SS1	atoms/cm <sup>3</sup>	density for flux model 1						
	13-24	E	SS2	"	"	"	"	"	"	"	2
	25-36	E	SS3	"	"	"	"	"	"	"	3
	37-48	E	SS4	"	"	"	"	"	"	"	4
	49-60	E	SS5	"	"	"	"	"	"	"	5
	73-80	-	-	-	constituent	name					

b. Sample

**GENERAL PURPOSE DATA SHEET**

Problem	OUTPUT-LAMBDA PUNCH		Date	SAMPLE	Page
Sponsor	TAPE	5	of		
1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 31 32 33 34 35 36 37 38 39 40 41 42 43 44 45 46 47 48 49 50 51 52 53 54 55 56 57 58 59 60 61 62 63 64 65 66 67 68 69 69 70 71 72 73 74 75 77 78 79 80					
4					
1. 1 4 2 0 0 0 . 2 3 8 9 0 9 . 8 3 6					NITROGEN
0 . 3 8 8 1 E 1 3 0 . 4 9 1 4 E 1 3 0 . 6 9 7 5 E 1 3 0 . 1 2 0 9 E 1 4 0 . 2 0 3 6 E 1 4					NITROGEN
1. 1 4 2 0 0 0 . 2 2 7 3 8 7 . 7 4 0					NITROGEN
0 . 2 4 3 0 E 1 0 0 . 2 2 5 8 E 1 0 0 . 2 0 3 8 E 1 0 0 . 1 7 4 8 E 1 0 0 . 1 5 2 1 E 1 0					NITROGEN
1. 1 4 2 0 0 0 . 2 3 4 6 5 9 . 1 2 9					NITROGEN
0 . 2 7 4 5 E 1 2 0 . 3 1 1 9 E 1 2 0 . 3 7 7 1 E 1 2 0 . 5 0 9 5 E 1 2 0 . 6 7 8 0 E 1 2					NITROGEN
1. 1 4 2 0 0 0 . 2 1 9 6 8 5 . 8 6 7					NITROGEN
0 . 6 7 8 4 E 0 8 0 . 4 4 8 8 E 0 8 0 . 2 5 3 3 E 0 8 0 . 1 0 5 7 E 0 8 0 . 4 7 2 0 E 0 7					NITROGEN
7					
1. 1 7 0 0 5 0 . 2 3 9 9 1 1 2 . 4 4 4					NITROGEN
0 . 5 1 8 0 E 1 3 0 . 6 5 6 5 E 1 3 0 . 9 3 3 0 E 1 3 0 . 1 6 1 5 E 1 4 0 . 2 7 1 1 E 1 4					NITROGEN
1. 1 7 0 0 5 0 . 2 3 4 6 7 1 1 . 7 5 2					NITROGEN
0 . 2 2 5 8 E 1 2 0 . 2 5 1 9 E 1 2 0 . 2 9 6 2 E 1 2 0 . 3 8 1 9 E 1 2 0 . 4 8 5 8 E 1 2					NITROGEN
1. 1 7 0 0 5 0 . 2 2 9 5 6 1 1 . 0 2 2					NITROGEN
0 . 9 9 5 6 E 1 0 0 . 9 7 5 5 E 1 0 0 . 9 4 9 0 E 1 0 0 . 9 1 1 0 E 1 0 0 . 8 7 8 5 E 1 0					NITROGEN
1. 1 7 0 0 5 0 . 2 1 9 7 6 9 . 4 2 0					NITROGEN
0 . 8 7 4 2 E 0 8 0 . 6 0 8 9 E 0 8 0 . 3 6 6 2 E 0 8 0 . 1 6 6 7 E 0 8 0 . 8 0 1 5 E 0 7					NITROGEN
1. 1 7 0 0 5 0 . 2 0 9 7 3 7 . 3 4 6					NITROGEN
0 . 7 8 5 3 E 0 7 0 . 3 6 0 2 E 0 7 0 . 1 3 4 3 E 0 7 0 . 2 0 6 0 E 0 6 0 . 3 8 8 6 E 0 5					NITROGEN
1. 1 7 0 0 5 0 . 2 0 4 7 4 6 . 0 1 4					NITROGEN
0 . 2 6 8 7 E 0 7 0 . 9 9 8 7 E 0 6 0 . 2 7 0 2 E 0 6 0 . 2 6 1 5 E 0 5 0 . 3 0 9 9 E 0 4					NITROGEN
1. 1 7 0 0 5 0 . 2 0 1 3 7 4 . 8 9 4					NITROGEN
0 . 1 2 8 1 E 0 7 0 . 4 0 7 9 E 0 6 0 . 8 5 5 8 E 0 5 0 . 5 9 9 5 E 0 4 0 . 5 0 5 9 E 0 3					NITROGEN

#### H. Running Time

This program will take close to a minute for every two L lines evaluated.

## V. "BOUNCE" AVERAGE CALCULATION

### A. Introduction

The "bounce" average of the number density is defined<sup>(5)</sup> by the equation

$$\bar{\rho} = \frac{\int_{\lambda_s}^{\lambda_n} \rho(B, L) ds}{\int_{\lambda_s}^{\lambda_n} ds} \quad (1)$$

In other words, for a given mirror point  $\lambda_0$  and a given field line L, the "bounce" average of the number density is the average number of atoms/cm<sup>3</sup> that a particle encounters while spiraling about a field line from the northern to the southern mirror points (see Figure 5). The earth is assumed to be a dipole. This gives symmetry to the magnetic field, permitting the integrals in equation (1) to be evaluated over a fourth of a complete oscillation (see page 189, reference 1, for a discussion of the motion of trapped particles in a magnetic field.)

The output from the lambda punch becomes input to this program. Results are printed and punched for use in later programs. Subroutine TABLE is included to interpolate (extrapolate) the density table to supply the appropriate density at any latitude specified by the main program.

### B. Equations

To calculate equation (1) we project the element of arc length ds onto the field line L. Next we eliminate L from the equation and use the dipole representation

$$B = \frac{M}{r^3} (1 + 3 \sin^2 \lambda)^{1/2} \quad (2)$$

to express B in terms of  $\lambda$ . This gives the "bounce" average  $\bar{\rho}$  weighted over latitude for a given field line as

$$\text{RHOAV} = \frac{\int_0^{\lambda_0} \rho(\lambda) A(\lambda) d\lambda}{\int_0^{\lambda_0} A(\lambda) d\lambda} \quad (3)$$

where the "weighing" factor is

$$A(\lambda) = \frac{\cos^4 \lambda \sqrt{4 - 3 \cos^2 \lambda}}{\sqrt{\cos^6 \lambda \sqrt{4 - 3 \cos^2 \lambda_0} - \cos^6 \lambda_0 \sqrt{4 - 3 \cos^2 \lambda}}}$$

This factor allows for the fact that particles spiraling about the field line stay longer at the mirror latitudes  $\lambda_0$  (see page 189, reference 1, for a complete treatment of the derivation). Figure 6 is a plot of  $A(\lambda)$  versus  $\lambda$  for different mirror latitudes. Since  $A(\lambda)$  becomes undefined at  $\lambda_0$  we divided equation (3) into two cases:

$$\text{RHOAV} = \frac{\int_0^{\lambda_0 - 2h} \rho(\lambda) A(\lambda) d\lambda + \int_{\lambda_0 - 2h}^{\lambda_0} \rho(\lambda) A(\lambda) d\lambda}{\int_0^{\lambda_0 - 2h} A(\lambda) d\lambda + \int_{\lambda_0 - 2h}^{\lambda_0} A(\lambda) d\lambda}$$

Next we designate the square of the denominator of  $A(\lambda)$  by  $q(\lambda)$ . Expanding about  $\lambda_0$  by Taylor's series gives us

$$g(\lambda) = (\lambda - \lambda_0) \sum_{i=1}^{\infty} \frac{q^{(i)}(\lambda_0)}{i!} (\lambda - \lambda_0)^{i-1}$$

where  $q^{(i)}(\lambda_0)$  is the  $i^{\text{th}}$  derivative of  $q$  evaluated at  $\lambda_0$ . To approximate the infinite series we define

$$S(\lambda) = \text{SLAMF}(\lambda, \lambda_0) = - \sum_{i=1}^3 \frac{q^{(i)}(\lambda_0)}{i!} (\lambda - \lambda_0)^{i-1}$$

where the minus sign is inserted in order to avoid the square root of a negative number. In the program we let  $S1LAMF(\lambda, \lambda_0)$ ,  $S2LAMF(\lambda, \lambda_0)$  and  $S3LAMF(\lambda, \lambda_0)$  represent the first, second and third terms of  $SLAMF(\lambda, \lambda_0)$  respectively and we define

$$WLAMF(\lambda, \lambda_0) = \frac{\cos^4 \lambda \sqrt{4 - 3 \cos^2 \lambda}}{\sqrt{SLAMF(\lambda, \lambda_0)}}$$

This gives

$$\int_{\lambda_0 - 2h}^{\lambda_0} \rho(\lambda) A(\lambda) d\lambda = \int_{\lambda_0 - 2h}^{\lambda_0} \frac{\rho(\lambda) WLAMF(\lambda, \lambda_0)}{\sqrt{\lambda_0 - \lambda}} d\lambda \quad (4)$$

and

$$\int_{\lambda_0 - 2h}^{\lambda_0} A(\lambda) d\lambda = \int_{\lambda_0 - 2h}^{\lambda_0} \frac{WLAMF(\lambda, \lambda_0)}{\sqrt{\lambda_0 - \lambda}} d\lambda \quad (5)$$

which are linearly approximated by the equations

$$ADNUM = \sqrt{2h} \left[ \frac{4}{5} \rho(\lambda_0) WLAMF(\lambda_0, \lambda_0) + \frac{16}{15} \rho(\lambda_0 - h) WLAMF(\lambda_0 - h, \lambda_0) \right]$$

$$+ \frac{2}{15} \rho(\lambda_0 - 2h) WLAMF(\lambda_0 - 2h, \lambda_0) \right]$$

and

$$ADDEN = \sqrt{2h} \left[ \frac{4}{5} WLAMF(\lambda_0, \lambda_0) + \frac{16}{15} WLAMF(\lambda_0 - h, \lambda_0) + \frac{2}{15} WLAMF(\lambda_0 - 2h, \lambda_0) \right]$$

respectively. The final step is to integrate by Simpson's rule<sup>(6)</sup> and add on ADDNUM and ADDDEN to get the correct density  $\bar{\rho}$ .

Additional equations used in this program are listed below:

$$\text{AAAF}(\lambda) = \sqrt{4 - 3 \cos^2 \lambda}$$

$$\text{BBBF}(\lambda) = \cos^6 \lambda$$

$$\text{MONEF}(\lambda) = 3 \cos^4 \lambda \sin 2\lambda \quad \text{the first derivative of BBBF}(\lambda) \text{ used in computing } \text{S1LAMF}(\lambda, \lambda_0)$$

$$\text{MTWOF}(\lambda) = \frac{15}{2} (\cos \lambda \sin 2\lambda)^2 - 6 \cos^6 \lambda \quad \text{the second derivative of BBBF}(\lambda) \text{ used in computing S2LAMF}(\lambda, \lambda_0)$$

$$\text{MTHRF}(\lambda) = 48 \cos^4 \lambda \sin 2\lambda - 15 \sin^3 2\lambda \quad \text{the third derivative of BBBF}(\lambda), \text{ used in computing S3LAMF}(\lambda, \lambda_0)$$

$$\text{ETAF}(\lambda) = 10 \cos 2\lambda - 3 \sin^2 2\lambda - 6 \cos^2 2\lambda \quad \text{a factor which appears in the second and third derivatives of AAAF}(\lambda)$$

$$\text{NONEF}(\lambda) = \frac{3 \sin 2\lambda}{2 \text{AAAF}(\lambda)} \quad \text{the first derivative of AAAF}(\lambda) \text{ used in computing S1LAMF}(\lambda, \lambda_0).$$

$$\text{NTWOF}(\lambda) = \frac{3 \text{ETAF}(\lambda)}{4(4 - 3 \cos^2 \lambda)^{3/2}} \quad \text{the second derivative of AAAF}(\lambda) \text{ used in computing S2LAMF}(\lambda, \lambda_0).$$

$$\text{NTHRF}(\lambda) = \frac{3}{4} \frac{\frac{9 \text{ETAF}(\lambda) \sin 2\lambda}{-20 \sin \lambda - 6 \sin 4\lambda - 4 - 3 \cos^2 \lambda}}{(4 - 3 \cos^2 \lambda)^{3/2}} \quad \text{the third derivative of AAAF}(\lambda), \text{ used in computing S3LAMF}(\lambda, \lambda_0)$$

WGTF( $\lambda, \lambda_0$ ) the designation for A( $\lambda$ ) when integrating by Simpson's rule

ALAM the value of the denominator in equation (3) but without equation (5)

RHOAS the value of the numerator in equation (3) but without equation (4)

BSUBO  $B_0$  computed by equation (2) for  $\lambda_0$ .

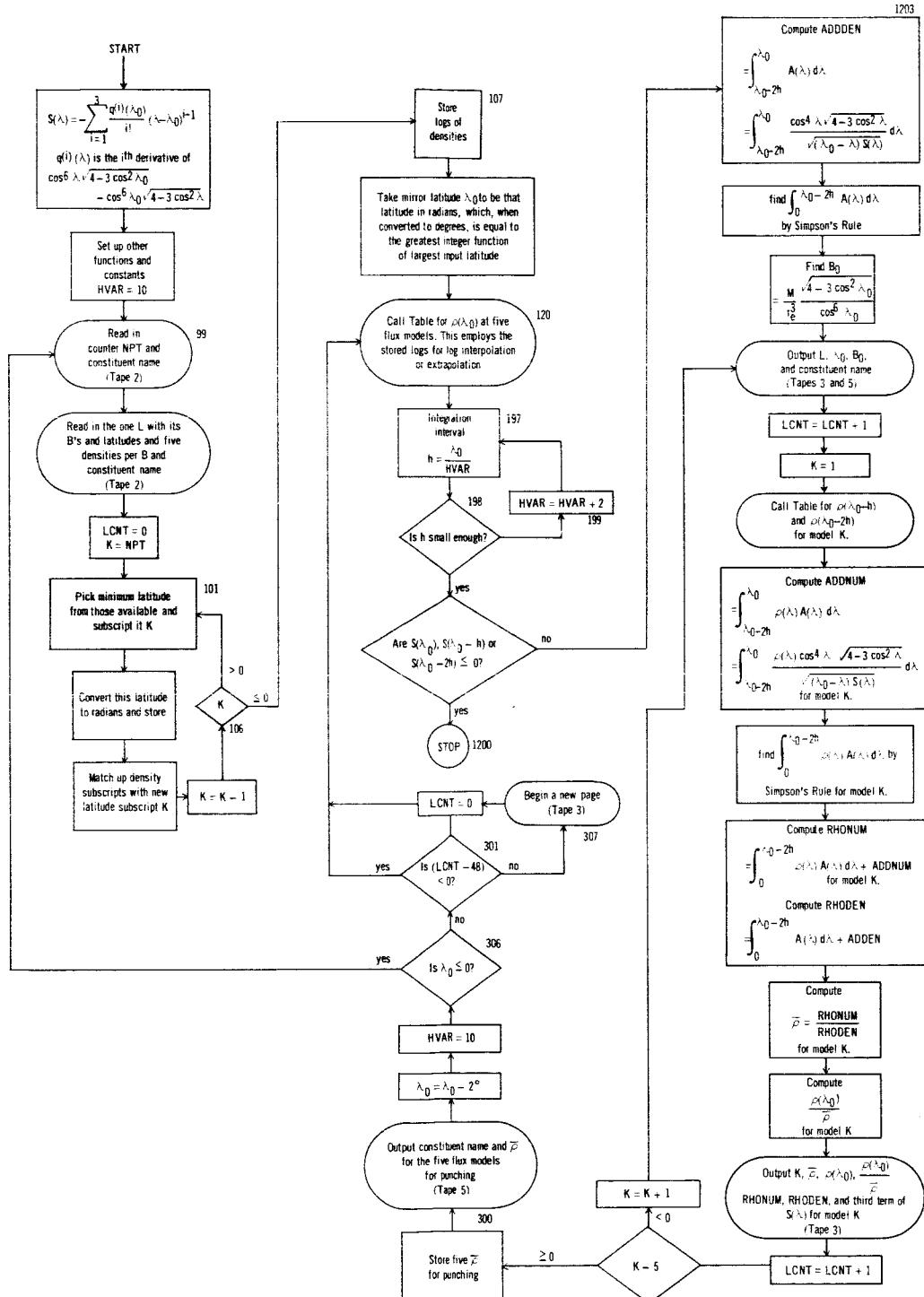
### C. Mnemonics

<u>Quantity</u>	<u>Description</u>	<u>Units</u>
DTR	Conversion factor - degrees to radians	-
RTD	Conversion factor - radians to degrees	-
RE	radius of the earth, $6378.165 \times 10^5$ cm.	cm.
EM	earth's magnetic dipole moment, $8.1 \times 10^{25}$ gauss cm <sup>3</sup> , divided by the radius of the earth cubed.	gauss
HVAR	number of partitions in Simpson's rule	-
NPT	counter of the B's for a given L	-
XLAB1	first six letters of constituent identification name	-
XLAB2	remaining two letters of constituent identification name	-
EL	magnetic field line L	earth radii
B(I)	I <sup>th</sup> magnetic induction for a given L	gauss
SS(I,J)	(a) the first time this designation is used it represents the longitudinally averaged density for the I <sup>th</sup> solar flux model and the J <sup>th</sup> magnetic induction  (b) the second time this designation is used it represents the log of the densities in (a)	atoms/cm <sup>3</sup>
LCNT	line counter for output on tape 3	-
XMIN	storage of the smallest available latitude	degrees
XLAMW(K)	latitude in radians, sorted in decreasing order	radians
XLAMRF	storage of maximum value of the latitude	radians

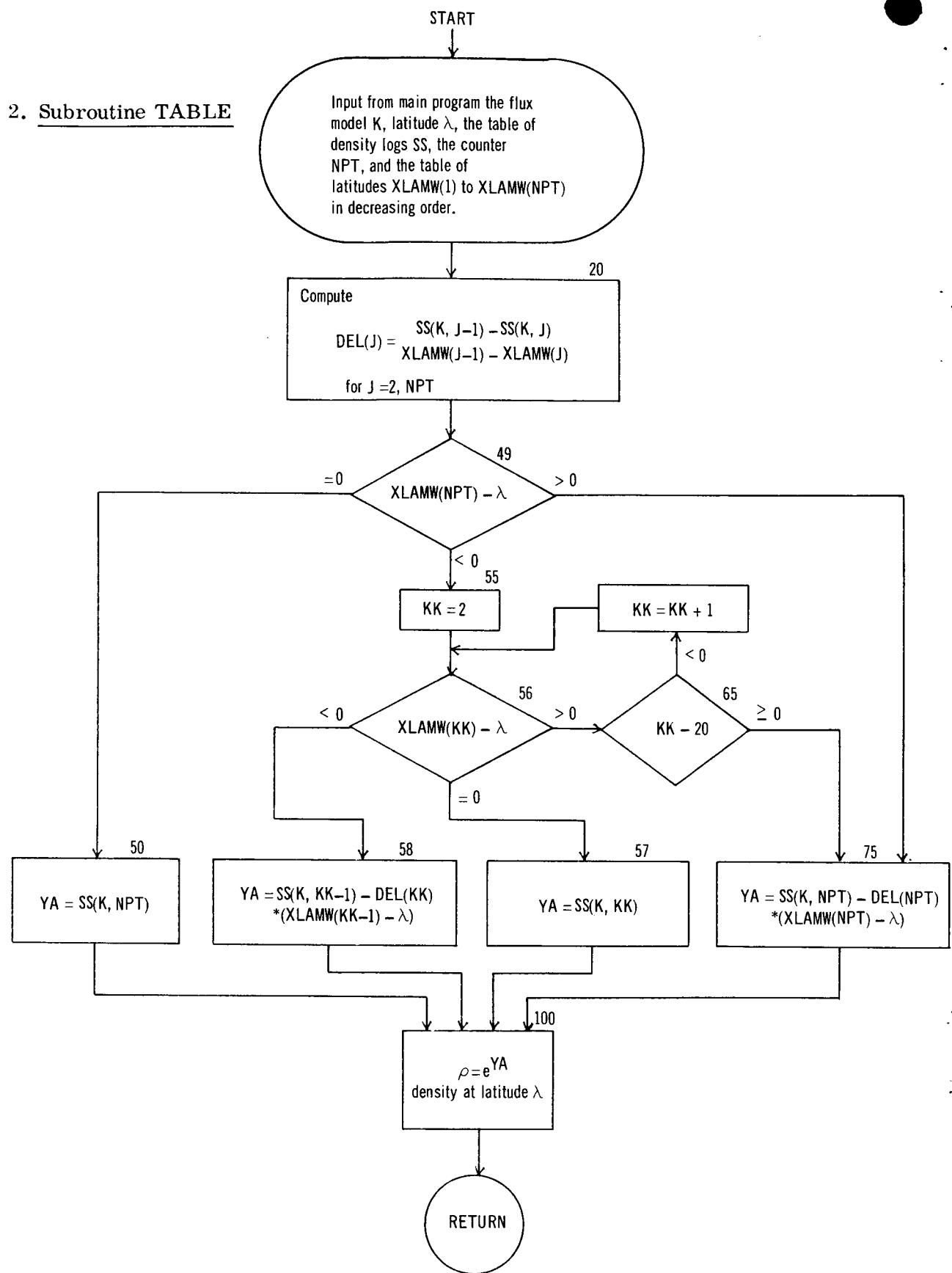
<u>Quantity</u>	<u>Description</u>	<u>Units</u>
XLAMO	mirror latitude $\lambda_0$	radians
RHOLO(I)	density for I <sup>th</sup> flux model at mirror latitude	atoms/cm <sup>3</sup>
HS	integration interval h for Simpson's rule	radians
RHOAV	"bounce" average density	atoms/cm <sup>3</sup>
RATRHO	ratio of density at mirror latitude to density RHOAV	-
RHOLOP	density at mirror latitude	atoms/cm <sup>3</sup>
DENB(K)	temporary storage of "bounce" average density at K <sup>th</sup> flux model for tape 5 punch	atoms/cm <sup>3</sup>

## D. Flow Chart

### 1. Main Program



## 2. Subroutine TABLE



## E. Fortran Listing

```

      BOUNCE
C   BLUNGF AVERAGE CALCULATION
C   PROGRAM TO COMPUTE RHC TRIPLE BAR AS FUNCTION OF L,LAMBDA AND FLUX
      DIMENSION S(LC),XL(NCO),SS(5,20),DEN(20),HOLC(15),CELLS
      IXLAMF(LC),S15(20),DEN(20),HOLC(15),CELLS
      FREQUENCY 102100,106100,107100,107100,108100,109100
      1,30115,1,0,1,0,05610,0,IC,126110,0,51,265110,1,211(99),259(100),
      226159,1,159(C,1,IC),1201(C,1,IC),12C2(C,1,IC),
      C FORMATS
      1 FORMAT(1Z, /GX, #, #, A2)
      2 FORMAT(2F4.5,F8.3,4F8.6,A2)
      3 FORMAT(5L12,4,12X,A6,A2)
      4 FORMAT(1B10,I11,1P10R, 1P,4*X,UFLUX AVERAGE
      1H, RHO AT MEDIUM RHO/AV. RTG, INTEGRAL OF S3 (LA
      2N,1, FNU/22X,4HLAT.,3IX,dHLATITUDE,15X,21H,RCA CLR,
      312INT. INTERVAL //)
      5 FORMAT(3X,A6,A2,Ft,4,F8.3,F8.4)
      6 FORMAT(36A12,12,1P6E14.4)
      7 FORMAT(3HRC ERROR - S(LAM) IS NEG. CR ZERO/BH SLL = E15.5,
      16F SL2 = E15.5,OH SL3 = E15.5,8H XLM0 = E15.5,5H HS = E15.5)
      8 FORMAT(25HILVICE CHLCK HAS OCCURRED)
      9 FORMAT(30HILVICE OVERFLW HAS OCCURRED)
      C ARITHMETIC FUNCTIONS
      AaSF(XL)=5CRTF(4,C-3.0*(CCSF(XL)**21)
      BbSF(XL)=CCSF(XL)**6
      EIAF(XL)=10.*CCSF(2.*XL))-3.*0.*SINF(2.*XL)**2)
      1-6.0*(CCSF(2.*XL))**2)
      WANG(XL)=-3.0*(CCSF(XL))**4)*SINF(2.*XL)
      NWCF(XL)=T-5.*CCSF(XL)*SINF(2.*XL))**2-6.0*(CCSF(XL))**6)
      NHRF(XL)=4.0*(CCSF(XL))**4)*(SINF(2.*XL))
      1-15.0*(SINF(2.*XL))**3)
      NCUF(XL)=1.5*SINF(2.*XL))/AAAF(XL)
      NIWCF(XL)=0.75*ETAF(XL)/(14.C-3.0*(CCSF(XL))**2)**1.5)
      NHRF(XL)=(0.*T**(-20.0)*(SINF(2.*XL))-6.G*(SINF(4.0.*XL))
      1-19.C-7.TAF(XL)*(SINF(2.*XL))/((4.-0.-3.C*(CCSF(XL))**2)))
      2/(14.-3.0*(CCSF(XL))**2)**1.5)
      SLAMF(XL,XLC)=1.0*(AAAF(XLC)*NGNE(XLC)-BHF(XLC)*NFF(XLC))
      SLAMF(XL,XLC)=1.0*(AAAF(XLC)*NGNE(XLC)-BHF(XLC)*NFF(XLC))
      2*(XL-XLC)/(-2.0)
      SLLAV(XL,XLC)=(AAAF(XLC)*KHF(XLC)-BHF(XLC)*NFF(XLC))
      2*((XL-XLC)**2)/(-6.0)
      SLAMF(XL,XLC)=SLAMF(XL,XLC)+S2LAMF(XL,XLC)+3LAMF(XL,XLC)
      1XL0))
      WGF(XL,XLC)=(CCSF(XL)**4)*AAAF(XL)/SQRTF(1
      JAAAF(XLC)*BHF(XL)-BHF(XLC)*AAAF(XL))
      C TURN OFF LINEAR CHECK LIGHT
      C AND QUOTIENT OVERFLOW LIGHT
      IF CIVICE CHECK 3C,30
      30 IF (CIVICE CONSTANT IS
      PROGRAM CIVICE
      31 DTR=1/454352
      K10=57.297795
      R=637000000
      E=0.1627353
      FVAR=1.0

```

```

99 IF CIVILL CHECK 32,98
98 IF SUFFICIENT VEREICK 34,32
33 WRITE OUTPUT TAPE 3,6
CALL EXIT
34 WRITE OUTPUT TAPE 3,9
CALL EXIT
REAL IN TABLES OF DENSITY FOR GIVEN L AND VARIOUS LAMBDA-S
C DENSITY - FIRST SUBSCRIPT = FLUX NO., SECOND SUBSCRIPT = LATITUDE NC.
32 READ INPUT TAPE 2,1,NP1,XLAB1,XLAB2
DO 100 I=1,NP1
READ INPUT TAPE 2,2,ELB(I),XLB(I),XLAB1,XLAB2
100 READ INPUT TAPE 2,3,(SS(IF,I),IF=1,5),XLAB1,XLAB2
WRITE OUTPUT TAPE 3,4
LCNT=0
ELB=ELB*ELB*ELB
C SORT LAMBDA-S IN DECREASING ORDER
SUBSCRIPT = 1 = MAX VALUE UP TO SUBSCRIPT = NP1 = MIN VALUE
K=NP1
101 XMIN=LG.0
102 LG DC 103 I=1,NP1
103 IF(XMIN-XL N(I)) 105,104
104 XMIN=XL N(I)
JJ=1
105 CONTINUE
C XAMWK(K)=WORKING VALUE OF LAMBDA (IN RAD.) SORTED IN DECREASING ORDER
C LENGTH SUBSCRIPTS MATCHED UP WITH SORTED LAMBDA-S
XAMWK(K)=XAMWK(LTR
DC 1105 KF=1,5
1105 S(KF,K)=S(KF,JJ)
XL N(JJ)=CC.C
K=K-1
106 II(K) LG7,107,1G1
C SGETL LG5 CF CENSURIT
107 CL LG5 I=1,NP1
   EC 1106 IL=1,5
1108 SS(II,J)=LG(I,S(II,J))
108 CONTINUE
C PICKR LATITUDE
XAMWF(XAMWF)
XAMWF=CL174
1300 IF(XAMWF-XLAMWF) 1301,120,1302
1301 XLWF=ALWF+CL174
CL LG 1302
1302 XLWF=ALWF-C(.174
C LINEAR INTERP. (EXTRAP.) TO FIND DENSITY (FROM TABLE) ASSOCIATED WITH
C PICKR LATITUDE
120 UL 114G RI=1,5
CALL Table.(K1,XLAMWF,SS,RHCS,NP1,XAMWF)
1140 RHOL(K1)=RHOL
C FIND INTERSECTION INTERVAL FOR SIMPSON-S RULE (HS)
197 HS=XLAB1/1-VAP
T0H=-C*HS
SFUN=S2LANT(XLAB1+T0H,XLAB2)
198 IF(SFUN>SFUN(XLAB1+T0H)-1.CE-7) 200,2CG,199
199 FV43=FV43+Z.C
200 GIC 1G7

```

```

C COMPUTE AUGUST FUNCTION FOR FINAL INTEGRATION STEPS
200 S2H=S2H(TWCH)
H=H-S
TWA=TWCH
H03=3/3*C

C TEST IF SLAMF ALG.
SL1=SLAMF(XLAMC,XLAMO)
SL2=SLAMF(XLAMC-HS,XLAMC)
SL3=SLAMF(XLAMC-TWCH,XLAMC)

1159 IF(SL1) 1200,1201,1201
1200 WRITE OUTPU TAPE 3,7,SL1,SL2,SL3,XLAMC+HS
CALL TWCH

1201 IF(SL2) 1200,1202
1202 IF(SL3) 1200,1200,1202
1203 ADDDEN(SL2)*C-B*SLAMF(XLAMC,XLAMC)+1.0666667*
    XLAMF(XLAMC+HS,XLAMC)+C,1333333*SLAMF(XLAMC-TWA,
    2XLAMC)

C INTEGRATE CROWDATOR BY SIMPSON-S RULE (XLAM) FUNCTION
XLIM1=XLAMC-TWCH
XLIM2=XLAMC-TWCH+C
N=NN
N=N+1
NW2=N-1
A4=0.C
A2=C.C
XLAM=XLAM+TS
XLAM=XLAM+TAC+
209 DC 210 TS=1,NM1
XLAM=XLAM+TAC+
210 A4=A4+TGIF(XLAM,XLAMO)
XLAM=0.C
211 DU 212 TS=1,NW2
XLAM=XLAM+TAC+
212 A2=A2+TGIF(XLAM,XLAMO)
XLAM=XLAM+TS
XLAM=XLAM+TGIF(XLAM+0.0,XLAM)+4.*C*A4+2.*A2+TGIF(XLIMIT,
XLAM))
LNGR=LN+1
LNGR=LNGR+S RULE FOR ALAMBA)
SUBC=M*AAA(XLAMC)/(EL3*BPF(XLAMO))
XLAMP=ALAMC*G
WRITE OUTPU TAPE 3,5,XLAB1*XLAB2,EL,XLABP,HSUEC
WRITE OUTPU TAPE 5,2,EL,BSUEC,XLAMP,XLAB1,XLAB2
LCNT=LN+1
C INTEGRATE FIVE DENSITY MUELS
DC 300 K=1,5
C ADDEND FUNCTION FOR NUMERICAL
RHOA1=RFLG(K)
CALL TABLE (K,XLAMC-HA,S,KHC1,NP1,XLAP)
CALL TABLE (K,XLAMC-TWCH,S,RHUM3,NP1,XLAMW)
ALDNP=S/2H*(C.0*HCW1*BLANF(XLAM,XLAMC)+1.0666667*
    2XLAMF(XLAMC-TWA,XLAMC))+C.13333333*RHM3
C INTEGRATE NUMBERATOR BY SIMPSON-S RULE
RHC(XLAM)+ALAM
RHOA4=U.G
RHOA2=G.O
XLAM=XLAM+TWCH
259 DC 260 K=1,NM1
XLAM=XLAM+TWCH

```

```

C ALL TABLE (K,XLAN,SS,RHCTAB,NPT,XLANW)
250 RHDIA4,RFLA4+RHUDE4,RFLA4,XLAN,XLANW)

251 06 262 K3=LNW
XLAN=XLM+LNW
C ALL TABLE (K,XLAN,SS,RHCTAB,NPT,XLANW)
252 RHDIAZ=RFLAZ,RHOTAZ,RGT(XLAN,XLANL)
C ALL TABLE (K,O,CSS,RGASC,NPT,XLANW)
RHDAS=RSUZ*(RHDASWGT(O,O,XLAN)+4.0*RFLA4+2.0*RHDIAZ
1+RHDIAZ*RGT(XLMIT,XLANC))
END SIMPSON'S RULE FOR RHUDE4(LAMBDA)
C COMPUTE AVERAGE RHUDE4
RHUDE4=RFLA4+RHDIAZ
RHUDE4=RFLA4+RHDIAZ
RHUDE4=RFLA4+RHDIAZ
C COMPUTE RATIO OF BOUNCE DENSITY TO INITIAL
RHUDE=RFLD(K)/RFLAV
RHUDE=RFLD(K)
WRITE OUTPUT TAPE 3,6,K,RFLAV,RHUDE,RFLD,RFLAV,RHUDE,N3FLA
LNFLD=LNFLD+1
C STORE BOUNCE AVERAGE DENSITIES FOR 4-5 PLANCH
300 DECNE(4)=RFLAV
WRITE OUTPUT TAPE 5,3,DECNE(1),DECNE(2),DECNE(3),DECNE(4),DECNE(5),
XLAN,XLANL
C DECREMENT PLANC LATITUDE BY 2 DEGREES
XLAN=XLANP-G-C*0.345G653
NVAR=15,6
306 IF(XLANP) 59,99,301
301 IF(LCN1=4,) 120,307,307
307 WRITE OUTPUT TAPE 3,4
LCN1=0
60 UC 120
END1,1,C,C,C,C,L,C,C,C,C,O

```

## STRUCTURE AND USE OF PROGRAM

DEC LCT  
173 C33C5

STRUCTURE AND USE OF PROGRAM

DEC OCT  
32561 77461

## STRUCTURE AND USE OF PROGRAM

DEC LCT	DEC CCT
173 C33C4	1647 C3157
SS 1642 C3152	1652 C3234

## STRUCTURE AND USE OF PROGRAM

A2 1442 0<442	A4 1441 0<441	CCT 1440 0<440	CCT 1440 0<440
ESUBC 1437 0<435	GTR 1436 0<434	ALUEN 1435 0<433	ACNUM 1435 0<433
HJ 1432 0<430	H-SUB 1431 0<429	CL3 1430 0<428	EL 1434 0<428
JJ 1427 0<423	K1 1426 0<422	H2 1430 0<426	HVAR 1429 0<425
AM2 1422 0<416	JPT 1421 0<415	K 1425 0<421	LCNT 1429 0<421
RHGR2 1417 0<411	QFIA4 1416 0<410	N 1420 0<414	RATKG 1415 0<413
RHGRV 1412 0<404	PHDUN 1411 0<403	LN 1412 0<407	RF-CASG 1414 0<406
RHTTAB 1407 0<407	RHMW1 1405 0<406	LLP 1410 0<402	RHDOS 1409 0<401
S3PUN 1402 0<402	SL1 1401 0<571	R-FW2 1405 0<575	RHMW3 1404 0<574
TWHA 1397 0<405	WCH 1396 0<564	SL2 1404 0<570	SL3 1399 0<567
XLAMP 1392 0<406	ALARF 1391 0<557	ALU1 1395 0<563	XLAB2 1394 0<562
XN 1387 C2553		ALAM 1390 0<566	XLIMIT 1395 0<556

## SYMBOLS AND LOCATIONS FOR SOURCE PROGRAM FORMAT STATEMENTS

EFN 1 02467	LCT 2 02464	EFN 3 02466	FFN 4 02465
EFN 6 024C4	LCT 7 02401	EFN 8 02355	FFN 9 02347

## LOCATIONS FOR OTHER SYMBOLS AND APPEARANCE IN SOURCE PROGRAM

DEC LCT	DEC CCT	DEC CCT	DEC CCT
1) 1336 0<470	1) 1 1343 0<471	1) 2 1343 0<255	1) 3 1356 0<516
1) 1365 0<526	2) 12C9 0<271	2) 1217 0<261	4) 22767 7777
4) 2 1369 0<531	4) 13 1371 0<253	4) 14 1373 0<235	4) 1375 0<537
7) 1377 0<541	7) 1 1378 0<2542	7) 2 1379 0<2543	6) 1380 0<544
C161 1382 0<546	C162 1383 0<547	C161 1384 0<2550	7) 3 1381 0<545
C110C 1116 0<167	D10R 223 0<337	C162 0<336	C12CC 1386 0<551
C15CH 167 0<247	E1C 118 0<166	L140U 217 0<324	0) 14CF 168 0<252

## LOCATIONS OF NAMES IN TRANSFER VECTOR

DEC CCT	DEC CCT	DEC CCT	DEC CCT
CC001 1 EXIT 7 CCC07	CC004 4 CCC04	CC012 10 CCC06	CC003 3 CCC03
CC002 2 TABLE 11 CCC13	(FILE) 6 00006	(FILE) 0 CCC00	(FILE) 9 CCC011
(STH) 5 CCC05	8 CCC10	E1C	E12

## ENTRY POINTS TO SUBROUTINES AND OUTPUT FROM LIBRARY

CCS (15r)	$\text{exp}(z)$	$\text{exp}(z)$	$\text{LCC}$	$\text{sin}$	$\text{cos}$	$\text{tan}$	$\text{cot}$	$\text{sec}$	$\text{csc}$	$\text{erf}$	$\text{erfc}$
NAMES AND LOCATIONS OF ARITHMETIC STANDARD FUNCTIONS											
$\text{DEC}$	$\text{CCT}$	$\text{LCC}$	$\text{LCC}$	$\text{LCC}$	$\text{CCT}$	$\text{LCC}$	$\text{LCC}$	$\text{LCC}$	$\text{CCT}$	$\text{DEC}$	$\text{CCT}$
$\text{AAA}$	$74_5$	$01324$	$I64$	$C1374$	$T_A$	$I64$	$0114$	$\text{MCN}$	$01452$	$670$	$01546$
$\text{MAC}$	$034$	$01364$	$\text{MCN}$	$\text{C1364}$	$\text{INT}_X$	$94_2$	$01626$	$\text{INT}_X$	$01625$	$958$	$01746$
$\text{SALW}$	$131$	$02007$	$\text{INT}_Y$	$C2053$	$\text{SLW}$	$116_2$	$02122$	$\text{INT}_Y$	$02123$	$1132$	$02154$
INTERNAL FORMULA NAMES WITH CCRS, SPACING INTERNAL FORMULA NUMBERS AND OCTAL LOCATIONS											
$\text{EFN}$	$\text{LCC}$	$\text{LCC}$	$\text{LCC}$	$\text{LCC}$	$\text{LCC}$	$\text{LCC}$	$\text{LCC}$	$\text{LCC}$	$\text{LCC}$	$\text{EFN}$	$\text{LCC}$
$3_0$	$2_5$	$00023$	$3_1$	$00022$	$5_9$	$36$	$00346$	$5_8$	$37$	$CCG50$	$33$
$3_4$	$4_1$	$00001$	$2_2$	$00066$	$1C0$	$48$	$00124$	$1C1$	$57$	$CC170$	$1C2$
$1C3$	$5_5$	$00200$	$1C4$	$00205$	$1C5$	$62$	$00213$	$116_3$	$65$	$CC251$	$1C6$
$1C7$	$6_5$	$00211$	$110_8$	$00300$	$108$	$72$	$00210$	$13C0$	$75$	$CC320$	$13C1$
$1C2$	$7_5$	$00432$	$120$	$00340$	$1140$	$82$	$00354$	$197$	$83$	$CC361$	$198$
$1C9$	$8_7$	$00454$	$89$	$00410$	$1199$	$96$	$00446$	$12C0$	$97$	$CC451$	$12C1$
$1D2$	$1C1$	$00470$	$1203$	$00502$	$2C9$	$111$	$00576$	$210$	$113$	$CC6C4$	$211$
$212$	$117$	$00627$	$259$	$136$	$01061$	$260$	$140$	$01100$	$261$	$142$	$CC120$
$3C0$	$16C$	$C13CC$	$3C6$	$165$	$01334$	$3C1$	$166$	$01340$	$3C7$	$167$	$CC345$

```

C SUBROUTINE TABLE
C SUBROUTINE TO INTERP. (EXTRAP.) IN CLSITFY TABLE FOR GIVEN S
DIMENSION SS(520),RHUS,NPT,XLAM
FREQUENCIES(11111,44110,0,5),SE(5,0,5)
15 DG 20 J=2,NPT
20 DEL(J)=(SS(K,J-1)-SS(K,J))/(XLAM(K,J-1)-XLAM(K,J))
49 IF(XLAM(K,NPT)-XLAM) 55,56,75
50 YA=SS(K,NP1)
51 GO TO 1CU
55 UC 65 KK=2,2C
56 IF(XLAM(KK)-XLAM) 58,57,65
57 YA=SS(K,KK)
58 YA=SS(K,KK-1)-DEL(KK)*(XLAM(KK-1)-XLAM)
59 GO TO 1CU
60 CCNTINUE
65 CCNTINUE
C EXTRAPOLATE
75 YA=SS(K,NPT)-DEL(NPT)*(XLAM(NPT)-XLAM)
100 RHUS=EXP(YA)
RETURN
END 1,1,U,C,C,O,O,O,O,C,O,O

```

STORAGE ACT USED BY PROGRAM

	DEC	UCI	DEC	CCT
	204	0C14	32561	77461

STORAGE LOCATIONS FOR VARIABLES APPEARING IN DIMENSION AND EQUIVALENCE STATEMENTS

	DEC	UCI	DEC	CCT
LEL	183	CC261	Y	2C3 C0313

STORAGE LOCATIONS FOR VARIABLES NOT APPEARING IN COMMON, DIMENSION, OR EQUIVALENCE STATEMENT

	DEC	UCI	DEC	CCT
KK	163	CC243	YA	162 CC242

LOCATIONS FOR OTHER SYMBOLS NOT APPEARING IN SOURCE PROGRAM

	DEC	UCI	DEC	CCT
1)	154	CC232	2)	142 CC216
C)G1	158	CC236	159 CC237	144 CC220
L)108	121	CC171	133	12 CC116

LOCATIONS OF NAMES IN TRANSFER VECTOR

	DEC	UCI	DEC	CCT
LX4	0	CC261		

ENTRY POINTS TO SUBROUTINES NOT OUTPUT FROM LIBRARY

LXP

INTERNAL FORMULA NUMBERS WITH CORRESPONDING INTERNAL FORMULA NUMBERS AND OCIAL LOCATIONS

	IFN	UCI	IFN	UCI	IFN	UCI	IFN	LOC
15	9	CC062	20	6	49	7	50	55
56	11	CC125	57	12	CC132	58	14	10 00116
106	13	CC172					65	16 CC152

## F. Input

The input to this program are simply the cards output from the lambda punch. Each constituent can be run separately or they can all be run at the same time. Any number of L lines may be run also. A counter card must state the number of points to each L line which is run. Counter cards are included in the output from the lambda punch but they must be corrected if the number of points per L line are changed before running this program. Input occurs on tape 2.

### 1. Input card description

	<u>Columns</u>	<u>Mode</u>	<u>Quantity</u>	<u>Units</u>	<u>Description</u>
Counter Card	1-2	I	NPT	-	B-L- $\lambda$ , density card pair counter
B-L- $\lambda$ Card	1-8	F	EL	earth radii	magnetic field line
	9-16	F	B(I)	gauss	magnetic induction
	17-24	F	XLAM(I)	degrees	latitude
	73-80	-	-	-	constituent name
Density Card	1-12	E	SS(1,I)	atoms/cm <sup>3</sup>	density for flux model 1
	13-24	E	SS(2,I)	"	" "
	25-36	E	SS(3,I)	"	" "
	37-48	E	SS(4,I)	"	" "
	49-60	E	SS(5,I)	"	" "
	73-80	-	-	-	constituent name

2. Sample

**GENERAL PURPOSE DATA SHEET**

Problem Sponsor	INPUT - "BOUNCE" AVERAGE CALCULATION		Date	Page	of
	TAPE 2	SAMPLE			
1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 31 32 33 34 35 36 37 38 39 40 41 42 43 44 45 46 47 48 49 50 51 52 53 54 55 56 57 58 59 60 61 62 63 64 65 66 67 68 69 70 71 72 73 74 75 76 77 78 79 80					
4					OXYGEN
1. 14200 0 . 23890 9 . 836					OXYGEN
0 . 9347E 11 0 . 9836E 11			0 . 1081E 12	0 . 1288E 12	OXYGEN
1. 14200 0 . 22738 7 . 740					OXYGEN
0 . 5882E 09 0 . 5626E 09			0 . 5318E 09	0 . 4901E 09	OXYGEN
1. 14200 0 . 23465 9 . 129					OXYGEN
0 . 1471E 11 0 . 1508E 11			0 . 1582E 11	0 . 1733E 11	OXYGEN
1. 14200 0 . 21968 5 . 867					OXYGEN
0 . 7599E 08 0 . 5826E 08			0 . 4130E 08	0 . 2470E 08	OXYGEN
7					OXYGEN
1. 17005 0 . 23991 12 . 444					OXYGEN
0 . 1205E 12 0 . 1270E 12			0 . 1400E 12	0 . 1677E 12	OXYGEN
1. 17005 0 . 23467 11 . 752					OXYGEN
0 . 1349E 11 0 . 1380E 11			0 . 1441E 11	0 . 1562E 11	OXYGEN
1. 17005 0 . 22956 11 . 022					OXYGEN
0 . 1563E 10 0 . 1541E 10			0 . 1513E 10	0 . 1476E 10	OXYGEN
1. 17005 0 . 21976 9 . 420					OXYGEN
0 . 8147E 08 0 . 6556E 08			0 . 4948E 08	0 . 3218E 08	OXYGEN
1. 17005 0 . 20973 7 . 346					OXYGEN
0 . 2206E 08 0 . 1353E 08			0 . 6905E 07	0 . 2469E 07	OXYGEN
1. 17005 0 . 20474 6 . 014					OXYGEN
0 . 1256E 08 0 . 6731E 07			0 . 2815E 07	0 . 7430E 06	OXYGEN
1. 17005 0 . 20137 4 . 894					OXYGEN
0 . 8589E 07 0 . 4184E 07			0 . 1520E 07	0 . 3201E 06	OXYGEN
0 . 8589E 07 0 . 4184E 07			0 . 7391E 05		OXYGEN

## G. Output

Output from this program appears on logical tapes 3 and 5. Tape 3 gives results which are to be printed. Each page is devoted to a single L line for a specific constituent. Of the eleven columns which cross the page, the first contains the constituent name. This is followed by the value of L, the mirror latitude  $\lambda_0$ , the corresponding value of B, the flux model number, the "bounce" average number density, the longitudinally averaged number density, the ratio of the longitudinally averaged number density to the "bounce" averaged number density, the value of  $\int_0^{\lambda_0} \rho(\lambda)A(\lambda) d\lambda$ , the value of  $\int_0^{\lambda_0} A(\lambda)d\lambda$  and the third term of  $SLAMF(\lambda_0 + 2h, \lambda_0)$ . All these additional values are included as an intermediate check on the process.

Tape 5 contains the data to be punched. The counter card has been eliminated and all that remains are the B-L- $\lambda$  card and the "bounce" average density card with constituent names punched to the right of each card.

1. Tape 3 Sample

CONSTITUENT	L	FLUX	AVERAGE RHO	RHO AT MIRROR LATITUDE	RHO/AV.	RHO	INTEGRAL CF RHO*A	INTEGRAL CF A ELAM	S3 (ELAM*) FCR INT. INTERVAL
HELIUM	1.1420	6.973	C.2338	1	1.9423E 06	2.6747E 06	2.4419E 00	8.2198E 05	1.5248E-01
		2	1.0698E 06	2.5110E 00	2.4866E 00	7.5985E 05	7.5248E-01	-9.9948E-08	
	3	8.9101E 05	2.3147E 06	2.5071E 00	5.5248E 05	5.1656E 05	7.5248E-01	-9.9948E-08	
	4	7.6346E 05	2.0673E 06	2.7684E 00	5.7449E 05	7.5248E-01	-9.9948E-08		
	5	6.7422E 05	1.9022E 06	2.8213E 00	6.0734E 05	7.5248E-01	-9.9948E-08		
HELIUM	1.1420	6.973	C.2239	1	8.2564E 05	9.2931E 02	1.4654E 00	4.6187E 05	1.4783F-01
	2	6.5096E 05	8.6498E 05	1.5474E 00	4.1802E 05	7.4783E-01	-9.9891E-08		
	3	4.6631E 05	7.7118E 02	1.6461E 00	3.5022E 05	7.4783E-01	-9.9891E-08		
	4	3.5860E 05	6.4768E 05	1.8686E 00	2.6778E 05	7.4783E-01	-9.9891E-08		
	5	2.8677E 05	5.6219E 02	1.9046E 00	2.1446E 05	7.4783E-01	-9.9891E-08		
HELIUM	1.1420	6.973	C.2168	1	4.7743E 05	8.4203E 02	1.3446E 00	3.5538E 05	7.4428E-01
	2	4.1045E 05	5.7017E 05	1.3691E 00	3.0549E 05	7.4428E-01	-9.9846E-08		
	3	3.2262E 05	4.7128E 02	1.4568E 00	2.4012E 05	7.4428E-01	-9.9846E-08		
	4	2.2101E 05	3.4903E 05	1.5793E 00	1.6449E 05	7.4428E-01	-9.9846E-08		
	5	1.5864E 05	2.6842E 05	1.6920E 00	1.1807E 05	7.4428E-01	-9.9846E-08		
HELIUM	1.1420	2.973	C.2122	1	3.6833E 05	4.43956E 05	1.2042E 00	2.7425E 05	7.4185F-01
	2	3.0540E 05	3.7534E 05	1.2306E 00	2.2656E 05	7.4185E-01	-9.9703E-08		
	3	2.2619E 05	2.8801E 05	1.2732E 00	1.6780E 05	7.4185E-01	-9.9703E-08		
	4	1.3593E 05	1.8869E 05	1.3445E 00	1.0378E 05	7.4185E-01	-9.9703E-08		
	5	9.0997E 04	1.2814E 05	1.4130E 00	6.7283E 04	7.4185E-01	-9.9703E-08		
HELIUM	1.1420	0.973	C.2039	1	2.8749E 05	3.0644E 05	1.0659E 00	2.1293E 05	7.4664E-C1
	2	2.3666E 05	2.4774E 05	1.0743E 00	1.7079E 05	7.4664E-C1	-9.5805E-08		
	3	1.6117E 05	1.7661E 05	1.0880E 00	1.1981E 05	7.4664E-C1	-9.5805E-08		
	4	9.1554E 04	1.0136E 05	1.1107E 00	6.7586E 04	7.4664E-C	-9.5805E-08		
	5	5.4019E 04	6.1169E 04	1.1327E 00	4.0009E 04	7.4664E-C	-9.5805E-08		

CONSTITUENT	L	MIRROR LAT.	E	FLUX	AVERAGE RH <sub>O</sub>	RH <sub>O</sub> AT MIRRUR LATITUDE	RHO/AV. RH <sub>O</sub>	INTEGRAL OF RH <sub>O</sub> *A DALM	INTEGRAL CF A DALM	S3 (LAM.) FCR INT. INTERVAL
HELIUM	1.1700	11.963	C.2362	1 1.1605E 06 2 1.0524E 06 3 9.2613E 05 4 7.7353E 05 5 6.7968E 05	3.9406E 06 3.6392E 06 3.2852E 06 2.8870E 06 2.6315E 06	3.3955E 06 3.4480E 06 3.5549E 06 3.7323E 06 3.8716E 06	8.8337E 05 8.0388E 05 7.0342E 05 5.8879E 05 5.1736E 05	7.6118E-01 7.6118E-01 7.6118E-01 7.6118E-01 7.6118E-01	-9.9974E-08 -9.9974E-08 -9.9974E-08 -9.9974E-08 -9.9974E-08	
HELIUM	1.1700	9.963	C.2229	1 5.7759E 05 2 4.9657E 05 3 3.9651E 05 4 2.8489E 05 5 2.1614E 05	8.6715E 05 7.9498E 05 6.9577E 05 5.7327E 05 4.9288E 05	1.5013E 06 1.5945E 06 1.7460E 06 <.0123E 06 2.2680E 06	4.3617E 05 3.7650E 05 3.0093E 05 2.1513E 05 1.6322E 05	7.5516E-01 7.5516E-01 7.5516E-01 7.5516E-01 7.5516E-01	-9.9922E-08 -9.9922E-08 -9.9922E-08 -9.9922E-08 -9.9922E-08	
HELIUM	1.1700	10.963	C.2124	1 4.9387E 05 2 4.1153E 05 3 3.0989E 05 4 1.9167E 05 5 1.3185E 05	6.0193E 05 5.2229E 05 4.2009E 05 2.9864E 05 2.2157E 05	1.2188E 05 1.2708E 05 1.3559E 05 1.5108E 05 1.6609E 05	3.7041E 05 3.0865E 05 2.3242E 05 1.4826E 05 9.8892E 04	7.5001E-01 7.5001E-01 7.5001E-01 7.5001E-01 7.5001E-01	-9.9847E-08 -9.9847E-08 -9.9847E-08 -9.9847E-08 -9.9847E-08	
HELIUM	1.1700	5.963	C.2046	1 4.4908E 05 2 3.6244E 05 3 2.6457E 05 4 1.9665E 05 5 0.5689E 04	5.0365E 05 4.2540E 05 3.2122E 05 2.6438E 05 1.3457E 05	1.1326E 05 1.1641E 05 1.2142E 05 1.3047E 05 1.4034E 05	3.3497E 05 2.759E 05 1.9734E 05 1.684E 05 7.1524E 04	7.4590E-01 7.4590E-01 7.4590E-01 7.4590E-01 7.4590E-01	-9.9919E-08 -9.9919E-08 -9.9919E-08 -9.9919E-08 -9.9919E-08	
HELIUM	1.1700	3.963	C.1971	1 4.1452E 05 2 3.3077E 05 3 2.3198E 05 4 1.2947E 05 5 1.4132E 04	4.5059E 05 3.6669E 05 2.6479E 05 1.5551E 05 9.3876E 04	1.0678E 05 1.1082E 05 1.1414E 05 1.2011E 05 1.2663E 05	3.0794E 05 2.4573E 05 1.7234E 05 9.6186E 04 5.5073E 04	7.4290E-01 7.4290E-01 7.4290E-01 7.4290E-01 7.4290E-01	-9.9457E-08 -9.9457E-08 -9.9457E-08 -9.9457E-08 -9.9457E-08	
HELIUM	1.1700	1.963	0.1999	1 3.8312E 05 2 2.5999E 05 3 2.0408E 05 4 1.0700E 05 5 5.7930E 04	3.5969E 05 3.1601E 05 2.1828E 05 1.1833E 05 6.5489E 04	1.0432E 05 1.0534E 05 1.0695E 05 1.0987E 05 1.1305E 05	2.8393E 05 2.2335E 05 1.5125E 05 7.9820E 04 4.2932E 04	7.4110E-01 7.4110E-01 7.4110E-01 7.4110E-01 7.4110E-01	-9.9592E-08 -9.9592E-08 -9.9592E-08 -9.9592E-08 -9.9592E-08	

2. Tape 5

a. Output card description

	<u>Columns</u>	<u>Mode</u>	<u>Quantity</u>	<u>Units</u>	<u>Description</u>
B-L-\` Card	1-8	F	EL	earth radii	magnetic field line
	9-16	F	BSUBO	gauss	magnetic induction
	17-24	F	XLAMP	degrees	latitude
	73-80	-	-	-	constituent name
Density Card	1-12	E	DENB(1)	atoms/cm <sup>3</sup>	density for flux model 1
	13-24	E	DENB(2)	"	" " 2
	25-36	E	DENB(3)	"	" " 3
	37-48	E	DENB(4)	"	" " 4
	49-60	E	DENB(5)	"	" " 5
	73-80	-	-	-	constituent name

b. Sample

**GENERAL PURPOSE DATA SHEET**

OUTPUT - "BOUNCE" AVERAGE CALCULATION

Problem	Spencer	TAPE 5	Page	SAMPLE	Page	of
1	1.14200	0 . 2 3 3 7 6	8 . 9 7 3			OXYGEN
2	0 . 1 8 3 3 E	1 0 . 0 . 1 8 3 8 E	1 0 . 0 . 1 8 7 0 E	1 0 . 0 . 1 9 5 2 E	1 0 . 0 . 2 0 5 8 E	1 0 .
3	1 . 1 4 2 0 0	0 . 2 2 3 9 4	6 . 9 7 3			OXYGEN
4	0 . 7 4 8 4 E	0 8 . 0 . 6 2 0 0 E	0 8 . 0 . 4 8 9 8 E	0 8 . 0 . 3 4 8 9 E	0 8 . 0 . 2 6 1 3 E	0 8 .
5	1 . 1 4 2 0 0	0 . 2 1 6 8 0	4 . 9 7 3			OXYGEN
6	0 . 1 0 0 3 E	0 8 . 0 . 6 5 6 0 E	0 7 . 0 . 3 8 0 9 E	0 7 . 0 . 1 7 0 9 E	0 7 . 0 . 8 5 3 1 E	0 6 .
7	1 . 1 4 2 0 0	0 . 2 1 2 1 5	2 . 9 7 3			OXYGEN
8	0 . 1 4 6 8 E	0 7 . 0 . 7 5 9 5 E	0 6 . 0 . 3 2 4 8 E	0 6 . 0 . 9 1 8 6 E	0 5 . 0 . 3 0 5 7 E	0 5 .
9	1 . 1 4 2 0 0	0 . 2 0 9 8 8	0 . 9 7 3			OXYGEN
10	0 . 2 5 8 4 E	0 6 . 0 . 1 0 7 8 E	0 6 . 0 . 3 4 6 6 E	0 5 . 0 . 6 3 3 7 E	0 4 . 0 . 1 4 3 0 E	0 4 .
11	1 . 1 7 0 0 5	0 . 2 3 6 2 3	1 1 . 9 6 3			OXYGEN
12	0 . 3 5 1 1 E	1 0 . 0 . 3 5 8 8 E	1 0 . 0 . 3 7 5 1 E	1 0 . 0 . 4 0 8 9 E	1 0 . 0 . 4 4 9 4 E	1 0 .
13	1 . 1 7 0 0 5	0 . 2 2 2 8 7	9 . 9 6 3			OXYGEN
14	0 . 5 1 9 9 E	0 8 . 0 . 4 1 2 1 E	0 8 . 0 . 3 1 0 9 E	0 8 . 0 . 2 0 9 7 E	0 8 . 0 . 1 5 0 0 E	0 8 .
15	1 . 1 7 0 0 5	0 . 2 1 2 4 2	7 . 9 6 3			OXYGEN
16	0 . 1 3 8 9 E	0 8 . 0 . 8 1 8 6 E	0 7 . 0 . 4 0 6 8 E	0 7 . 0 . 1 4 7 0 E	0 7 . 0 . 5 9 0 9 E	0 6 .
17	1 . 1 7 0 0 5	0 . 2 0 4 5 7	5 . 9 6 3			OXYGEN
18	0 . 7 0 1 3 E	0 7 . 0 . 3 3 8 8 E	0 7 . 0 . 1 2 4 3 E	0 7 . 0 . 2 7 7 2 E	0 6 . 0 . 6 9 8 6 E	0 5 .
19	1 . 1 7 0 0 5	0 . 1 9 9 1 2	1 . 9 6 3			OXYGEN
20	0 . 4 1 5 7 E	0 7 . 0 . 1 7 2 5 E	0 7 . 0 . 5 0 1 0 E	0 6 . 0 . 7 5 7 0 E	0 5 . 0 . 1 3 0 5 E	0 5 .
21	1 . 1 7 0 0 5	0 . 1 9 5 9 2	1 . 9 6 3			OXYGEN
22	0 . 2 5 4 5 E	0 7 . 0 . 9 1 9 1 E	0 6 . 0 . 2 1 5 6 E	0 6 . 0 . 2 2 7 1 E	0 5 . 0 . 2 7 3 5 E	0 4 .

#### H. Running Time

This program will take about twenty minutes for every two L lines if five constituents are run together.

## VI. R, $\Sigma$ CALCULATION AND FLUX ELIMINATION

### A. Introduction

This program computes the atmospheric scale factor R and the atmospheric loss parameter  $\Sigma$ . The scale factor is used in the next program in order to relate the energy loss of the atmosphere with the measured energy loss data.<sup>(7)</sup> The atmospheric loss parameter appears in the calculation of the proton loss term of the conservation equation in the next section. Solar flux S is eliminated from both R and  $\Sigma$  by subroutine ELIM. This subroutine logarithmically interpolates Figure 9 to yield R and  $\Sigma$  as functions of time rather than solar flux S. B, L, and  $\lambda$  and the "bounce" averaged number densities are input to this program. B, L,  $\lambda$ , R and  $\Sigma$  are output for use in the conservation equation calculation.

### B. Equations

For a given B and solar flux model, the "bounce" average number densities of the five constituents are put together to form an average number of equivalent oxygen atoms/cm<sup>3</sup> by the equation OXY = RHO/8 where

$$RHO = 14\bar{n}(N_2) + 8\bar{n}(O) + 2\bar{n}(He) + 16\bar{n}(O_2) + \bar{n}(H)$$

and  $\bar{n}^{(J)}$  is the "bounce" average number density for the J<sup>th</sup> constituent.

The scale factor R is given by the equation

$$R(L, B, t) = \frac{(OXYGEN\ ATOMS/CM^3)ATMOS}{(OXYGEN\ ATOMS/CM^3)NTP}$$

where (oxygen atoms/cm<sup>3</sup>) ATMOS is OXY and (oxygen atoms/cm<sup>3</sup>) NTP comes from the following relationship of an ideal gas:

$$22414\ cm^3/Kmole = .60249 \times 10^{24}\ atoms/Kmole$$

or  $(OXYGEN\ ATOMS/CM^3)_{NTP} = 2.69 \times 10^{19}$ . Figure 7 is an example of the output from this program. It shows the time dependence of the atmosphere in terms of the scale factor R.

Sigma is given by the equation

$$\sum = \frac{\bar{n}(\text{He})}{2} \sigma(\text{He}) + \left[ \frac{\frac{\bar{n}(^0)}{8} + 2\bar{n}(^0_2)}{8} + \frac{2\bar{n}(^N_2)}{7} \right] \sigma(0) \text{ atoms/cm.}$$

where  $\sigma(\text{He})$  and  $\sigma(0)$  are the interaction cross sections of helium and oxygen respectively. Figure 8 again illustrates output from this program. It shows  $\log_e \Sigma$  as a function of time for various values of B at an L of 1.25 earth radii.

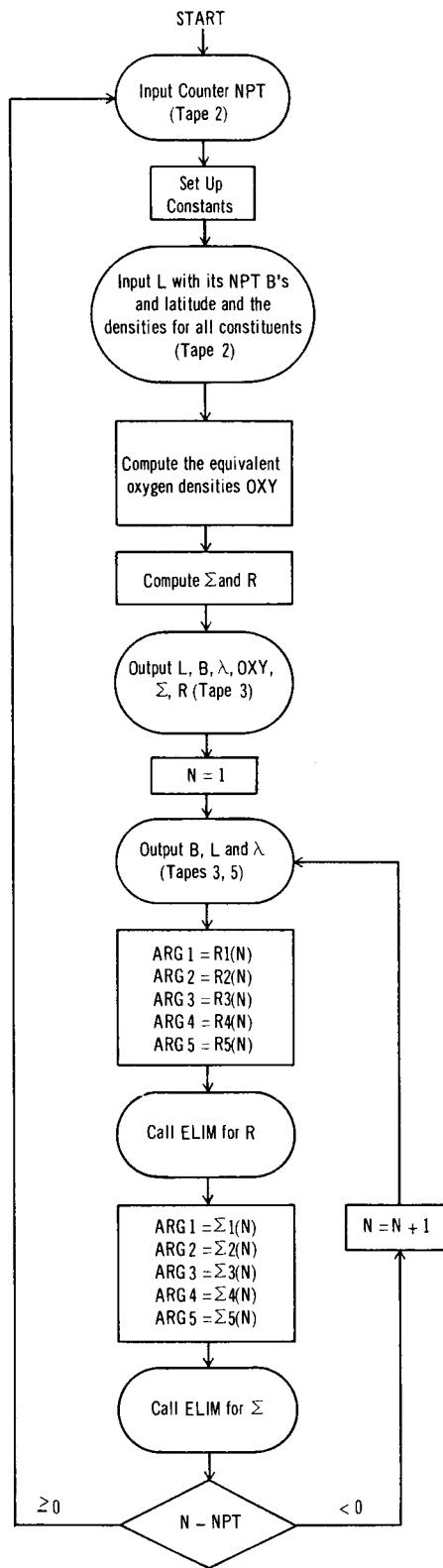
### C. Mnemonics

<u>Quantity</u>	<u>Description</u>	<u>Units</u>
NPT	counter of the number of B's to a given L	-
C	(oxygen atoms/cm <sup>3</sup> ) NTP = $2.69 \times 10^{19}$	atoms/cm <sup>3</sup>
SIGHE	$\sigma(\text{He}) = .143 \times 10^{-24}$	cm <sup>2</sup>
SIGO	$\sigma(0) = .36 \times 10^{-24}$	"
EL	magnetic field line L	earth radii
B(N)	N <sup>th</sup> magnetic induction B for a given L line	gauss
ALATO(N)	latitude corresponding to B(N)	degrees
HE1(N), ..., HE5(N)	helium "bounce" averaged densities for B(N) and the five flux models	atoms/cm <sup>3</sup>
O1(N), ..., O5(N)	oxygen "bounce" averaged densities for B(N) and the five flux models	atoms/cm <sup>3</sup>
O21(N), ..., O25(N)	molecular oxygen "bounce" averaged densities for B(N) and the five flux models	atoms/cm <sup>3</sup>
AN21(N), ..., AN25(N)	nitrogen "bounce" averaged densities for B(N) and the five flux models	atoms/cm <sup>3</sup>

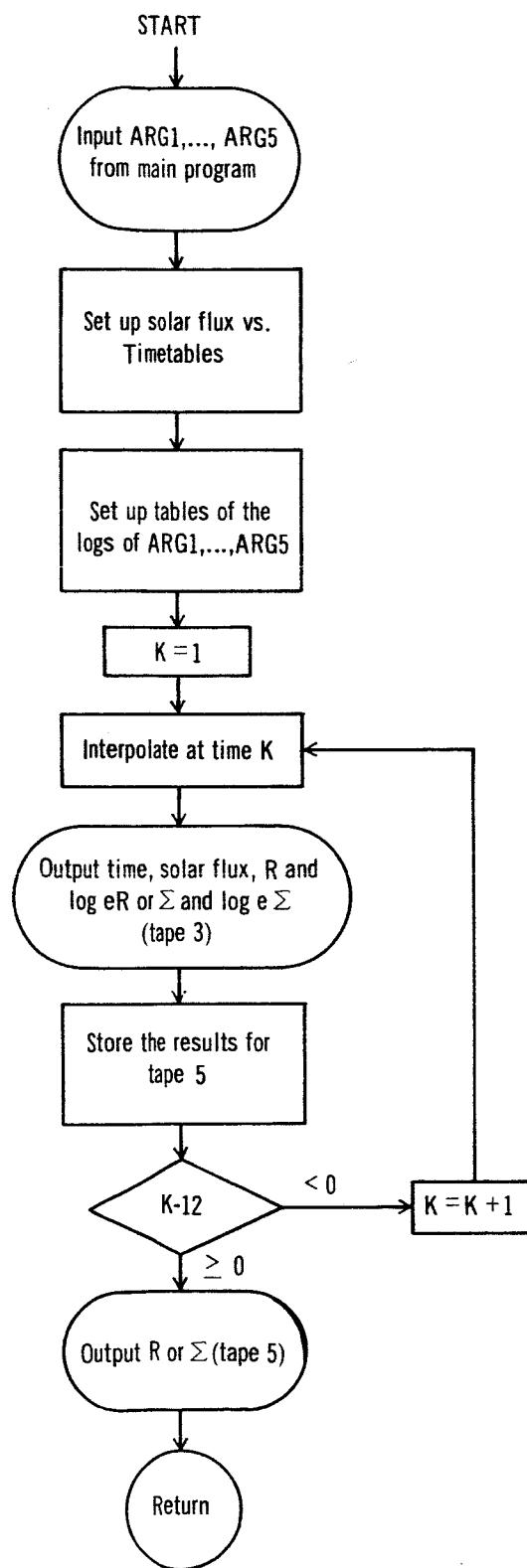
<u>Quantity</u>	<u>Description</u>	<u>Units</u>
H1(N), ..., H5(N)	hydrogen "bounce" averaged densities for B(N) and the five flux models	atoms/cm <sup>3</sup>
RHO1(N), ..., RHO5(N)	RHO for B(N) and the five flux models (see equation on page 105)	atoms/cm <sup>3</sup>
OXY1(N), ..., OXY5(N)	OXY for B(N) and the five flux models (see equation on page 105)	atoms/cm <sup>3</sup>
SIG1(N), ..., SIG5(N)	atmospheric loss parameter $\Sigma$ for B(N) and the five flux models	atoms/cm
RAT1(N), ..., RAT5(N)	scale factor R for B(N) and the five flux models	-
LCNT	counter to notify subroutine whether it is working with R or $\Sigma$	-
ARG1	temporary storage of RAT1 or SIG1 depending on LCNT	depends on LCNT
ARG2	temporary storage of RAT2 or SIG2 depending on LCNT	depends on LCNT
ARG3	temporary storage of RAT3 or SIG3 depending on LCNT	depends on LCNT
ARG4	temporary storage of RAT4 or SIG4 depending on LCNT	depends on LCNT
ARG5	temporary storage of RAT5 or SIG5 depending on LCNT	depends on LCNT

## D. Flow Charts

### 1. Main program



2. Subroutine Elim.



## E. Fortran Listing

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      RATIO,STOMA CALCULATION AND FLUX ELIMINATION
      DIMENSION B(12),RHG(112),RHG2(112),RH03(12),RH05(112),RH06(112),RH07(12),RH08(12)
      1(12),CXY(112),CX(12),CX(4)(12),CX(4)(112),CX(4)(112),CX(4)(112),CX(4)(112),CX(4)(112)
      2)RAT4(112),RAT5(112),RAT6(112)
      DIMENSION S(112),R(5),Y(5),S(5)
      DIMENSION C1(112),C2(112),AN23(112),AN24(112),AN25(112)
      DIMENSION C3(112),C4(112),C5(112),E(5)
      DIMENSION E(112),F(112),HE3(112),HE4(112),HE5(112)
      DIMENSION G21(112),G22(112),G23(112),G24(112),G25(112)
      DIMENSION H(112),H2(112),H3(112),H4(112),H5(112)
      DIMENSION SIG1(112),SIG2(112),SIG3(112),SIG4(112),SIG5(112)
      COMMON LUN,IARG,ARG3,ARG4,ARG5
      1 FORMAT (2F8.5,F8.3)
      2 FORMAT (4F8.0,X,5E12.4)
      3 FORMAT (1H1)
      4 FORMAT (1SF12.6)
      5 FORMAT (12X,2HL-Fd.5,4X,2HL-Fd.5,4X,4HLAT=F6.*3)
      6 FORMAT (6H RATE0,4X,5E12.4)
      7 FORMAT (6P SIGMA,4X,5E12.4//)
      8 FORMAT (5E12.4)
      9 FORMAT (1L2)
      10 FORMAT (14X,B5=250,7X,5HS=2C0,7X,5HS=15C,7X,5HS=1CC,1X,4HS=7C)
      11 FORMAT (5HCLAT=F8.4,4X,2HL-F8.4,4X,2HL-F8.4)
      12 FORMAT (3FE.4)
      13 FORMAT (//)
      14 READ INPUT TAPE 2,9,NPT
      READ INPUT TAPE 2,3,HU1(N),HE2(N),HE3(N),HE4(N),HE5(N)
      READ INPUT TAPE 2,3,HU1(N),HE2(N),HE3(N),HE4(N),HE5(N)
      15 CONTINUE
      DC 17 N=1,NPI
      READ INPUT TAPE 2,1,EL8(N),ALATO(N)
      READ INPUT TAPE 2,8,01(N),G2(N),G3(N),G4(N),G5(N)
      16 CONTINUE
      DC 18 N=1,NPI
      READ INPUT TAPE 2,1,EL8(N),ALATO(N)
      READ INPUT TAPE 2,8,G21(N),G22(N),G23(N),G24(N),G25(N)
      17 CONTINUE
      DC 19 N=1,NPI
      READ INPUT TAPE 2,1,EL8(N),ALATO(N)
      READ INPUT TAPE 2,8,A21(N),AN22(N),AN23(N),AN24(N),AN25(N)
      18 CONTINUE
      DC 14 N=1,NPI
      READ INPUT TAPE 2,1,EL8(N),ALATO(N)
      READ INPUT TAPE 2,8,E1(N),E2(N),E3(N),E4(N),E5(N)
      19 CONTINUE
      DC 15 N=1,NPI
      RF01(N)=14.**4C21(N)+8.**C1(N)+Z.**HE1(N)+16.*C21(N)+H1(N)
      RF02(N)=14.**AN22(N)+6.**G2(N)+Z.**HE2(N)+16.*C22(N)+H2(N)
      RF03(N)=14.**AN23(N)+E.**C2(N)+Z.**F13(N)+16.*C23(N)+H3(N)

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RH04(N)=14.*AN24(N)+8.*C04(N)*2.*H4(N)+2.*H4(N)+H4(N)
RH05(N)=14.*AN25(N)+8.*C05(N)*2.*H5(N)+16.*C24(N)+H4(N)
CONTINUE
DC 20 N=1,NPT
 0XY1(N)=RHO1(N)/8.
 0XY2(N)=RHO2(N)/8.
 0XY3(N)=RHO3(N)/8.
 0XY4(N)=RHO4(N)/8.
 0XY5(N)=RHO5(N)/8.
CONTINUE
DC 25 J=1,NPT
SIG1(J)=F1(J)*SIGE/J+((G1(J)+2.*G21(J))/8.+2.*AN1(J)/J)*SIGC
SIG2(J)=F2(J)*SIGE/J+((G2(J)+2.*G22(J))/8.+2.*AN22(J)/J)*SIGC
SIG3(J)=F3(J)*SIGE/J+((G3(J)+2.*G23(J))/8.+2.*AN23(J)/J)*SIGC
SIG4(J)=F4(J)*SIGE/J+((G4(J)+2.*G24(J))/8.+2.*AN24(J)/J)*SIGC
SIG5(J)=F5(J)*SIGE/J+((G5(J)+2.*G25(J))/8.+2.*AN25(J)/J)*SIGC
CONTINUE
DC 3C N=1,NPT
RAT1(N)=LAY1(N)/C
RAT2(N)=LAY2(N)/C
RAT3(N)=LAY3(N)/C
RAT4(N)=LAY4(N)/C
RAT5(N)=LAY5(N)/C
CONTINUE
DC 40 I=1,NPI
  WRITE OUTPUT TAPE 3,5,EL,B(N),ALATO(N)
  WRITE OUTPUT TAPE 3,2,GAY1(N),0XY2(N),CXY1(N),CXY4(N)
  WRITE OUTPUT TAPE 3,6,RAT1(N),RAT2(N),RAT3(N),RAT4(N),RAT5(N)
  WRITE OUTPUT TAPE 3,7,SIG1(N),SIG2(N),SIG3(N),SIG4(N),SIG5(N)
CONTINUE
  WRITE OUTPUT TAPE 3,3
DC 50 N=1,NPT
LNFT=C
  WRITE CUIPL TAPE 3,11,ALATC(N),EL,B(N)
  WRITE CUIPL TAPE 5,12,ALATO(N),EL,E(N)
  ARG1=F1(N)
  ARG2=F2(N)
  ARG3=F3(N)
  ARG4=F4(N)
  ARG5=F5(N)
  CALL LIP
  LNFT=1
  WRITE CUIPL TAPE 3,1,
  ARG1=5,I1(N)
  ARG2=5,I2(N)
  ARG3=5,I3(N)
  ARG4=5,I4(N)
  ARG5=5,I5(N)
  CALL LIP
CONTINUE
END(1,1,C,C,G,C,1,0,0,0,C,0,C)

```

## STORAGE-NCT USED BY PROGRAM

DEC	UCI			DEC	OCT		
1194	02252			32555	77453		

## STORAGE LOCATIONS FOR VARIABLES APPEARING IN COMMON STATEMENTS

DEC	UCI			DEC	OCT		
32561	02260			32559	77457		
A:G1	UCI			ARG3	32558	77456	
LCNT	32561	77461		ARG4	32557	77455	

## STORAGE LOCATIONS FOR VARIABLES APPEARING IN DIMENSION AND EQUIVALENCE STATEMENTS

DEC	UCI			DEC	OCT		
ALATO	1091	01751		AN21	950	01666	
A:25	914	01622		G62	01762		
H4	686	01256		1153	02251		
H:E4	806	01446		H5	674	01242	
U23	758	01366		H5	794	01432	
U4	866	01542		J24	746	01552	
C:V4	1084	02075		05	854	01526	
RAT4	1025	02001		CXY5	1073	02061	
R:U4	1145	02171		RAT5	1013	0165	
S163	622	01162		RH5	805	1133	
X5	652	01226		SIG5	614	01446	
				Y	972	0114	

## STORAGE LOCATIONS FOR VARIABLES NOT APPEARING IN COMMON, DIMENSION, OR EQUIVALENCE STATEMENT

DEC	UCI			DEC	OCT		
C	590	01116		EL	589	01115	
				NPT	588	01114	

SYMBOLS AND LOCATIONS FOR SOURCE PROGRAM FORMAT STATEMENTS

EFN	LCC	LFC		EFN	LCC		
011	1	01104		012	2	C101	
016	6	01063		017	7	C1057	
018	11	01035		01C	12	C1026	

## LOCATIONS FOR OTHER SYMBOLS NOT APPEARING IN SOURCE PROGRAM

DEC	CCF	CCT		DEC	OCT		
1)	581	01105		513	C101	31	
					518	0106	
					13	0104	

LOCATIONS OF NAMES IN TRANSFER VECTOR

DEC	OCT			DEC	OCT		
DCT	'S	OCT5		(FILE)	CC4	OCT	
ELIM	1	CCCC1		(FP)	OCT4	OCT	
(TSF)					(RIN)	2	CCCC2

ENTRY POINTS TO SOURCE LINES NOT OUTPUT FROM LIBRARY  
 L:LIB (FILE) (FP) (RIN) (TSF) (TSI)

## INTERNAL FORMULA NUMBERS WITH CCRK-SPLICING INTERNAL FORMULA NUMBERS AND OCTAL LOCATIONS

EFN	LUC	EFN	IFN	LCC	EFN	IFN	LCC	EFN	IFN	LCC
100	24	16	26	C0C72	17	42	CC164	15	54	C0221
14	6C	15	67	004G3	20	74	00427	25	81	C0566
40	98	50	12C	C0176				20	88	C0012

```

C SUBROUTINE TO ELIMINATE SOLAR FLUX
SUBROUTINE ELIM
DIMENSION ST(12),R(5),Y(5),S(12)
COMMON LCNT,ARG1,ARG2,ARG3,ARG4,ARGS
1 FORMAT (//,15E12.6)
2 FORMAT (15E12.6)
3 FORMAT (13,4X,1F10.2,2E20.5)
4 FORMAT (5H TIME,7A,5HSCLAR,12X,6HLOG OF,15X,5H RATIO/6H (YR5),6X,4H
IFLUX,1X,5H RATIO)
5 FORMAT (5H TIME,7A,5HSCLAR,12X,6HLOG OF,15X,5H SIGMA/6H (YR5),6X,4H
IFLUX,1X,5HSIG MA)
6 FORMAT (6E10.4)
R(1) = ARG1
R(2) = ARG2
R(3) = ARG3
R(4) = ARG4
R(5) = ARG5
ST(1) = 7C.
ST(2) = 75.
ST(3) = 130.
ST(4) = 230.
ST(5) = 250.
ST(6) = 220.
ST(7) = 165.
ST(8) = 14C.
ST(9) = 105.
ST(10)=90.
ST(11)=75.
ST(12)=7C.
S(1)=250.
S(2)=200.
S(3)=150.
S(4)=100.
S(5)=0.
1 IF (LCNT) 14,14,17
14 WRITE OUTPUT TAPE 3,4
   GO TO 18
17 WRITE OUTPUT TAPE 3,5
18 DO 20 J=1,5
      A=R(JJ)
      Y(JJ)=LGCF(A)
20  COUNTNEC
      DO 30 K=1,12
         HA=S(K)
         IF (HA>250.) 40,40,41,41
         IF (HA<-10.) 42,42,43
41  ANS=Y(1)
        GO TO 1C00
42  ANS=Y(5)
        GO TO 1C00
43  DO 50 J=1,5
         IF (HA-S(J)) 50,51,52
51  ANS=Y(J)
        GO TO 1C00
52  H1=S(J)

```

```

Y1=Y(J)
H0=S(J-1)
Y0=Y(J-1)
ANS=Y1-(Y1-Y0)*(H1-HA)/(H1-HC)
GU TG LCCE
CONTINUE
50 CONTINUE
ICCO X=EXP((AN5))
ITIME=K-1
WRITE OUTPUT TAPE 3,3,ITIME,HA,ANS,X
X(1)=X
CONTINUE
30 CONTINUE
WRITE OUTPUT TAPE 3,1
WRITE OUTPUT TAPE 5,6,XS(11),XS(3),A2(4),XS(5),XS(6)
WRITE OUTPUT TAPE 5,6,XS(7),XS(8),XS(9),XS(1C),XS(11),XS(1c)
RETURN
END(1,0,C,0,C,1,C,C,G,C,0)

```

STORAGE: NOT USED BY PROGRAM

DEC	LCT	DEC	CCT
321	CC,C4	32555	77453

STORAGE LOCATIONS FOR VARIABLES APPEARING IN COMMON STATEMENTS

DEC	LCT	DEC	OCT
32560	1746C	ARG2	32559 77457
LUNT	32561	ARG3	32556 77456

STORAGE LOCATIONS FOR VARIABLES APPEARING IN DIMENSION AND EQUIVALENCE STATEMENTS

DEC	LCT	DEC	OCT
R	311 CC467	S	3C1 00455

STORAGE LOCATIONS FOR VARIABLES NOT APPEARING IN COMMON, DIMENSION, OR EQUIVALENCE STATEMENT

DEC	LCT	DEC	CCT
ANS	284 CC434	A	283 00433
TIME	273 CC427	J	278 C0426

SYMBOLS AND LOCATIONS FOR SOURCE PROGRAM FORMAT STATEMENTS

EFN	LCC	EFN	LCC
011	1 CC414	012	2 CC412
016	6 CC352		

LOCATIONS FOR EITHER SYMBOLS NOT APPEARING IN SOURCE PROGRAM

DEC	OCT	DEC	OCT
11	263 CC415	211 00323	214 00326
C)G2	271 CC421	0)2C6	0)2CG
		E2 C0122	141 00125
			E1C 107 C0153

LOCATIONS OF NAMES IN TRANSFER VECTOR

DEC	OCT	DEC	OCT
EXP	3 CC003	LOG	2 CC002
		(FILE)	(FILE)

ENTRY POINTS TO SUBROUTINES NOT OUTPUT FROM LIBRARY

LLG (FILE) (STH)

EXTERNAL FORMULA NUMBERS WITH CORRESPONDING INTERNAL FORMULA NUMBERS AND OCTAL LOCATIONS

EFN	LCC	EFN	LCC	EFN	LCC	EFN	I FN	LOC
14	34 CC074	17	36 CC011	18	37 00105	20	40 CC115	4C 44 C0131
41	42 CC136	42	47 CC141	43	49 00144	51	51 CC0154	52 53 CC0161
50	55 CC212	1CCG	6C CC116	3G	65 CC250			

## F. Input

Input to this program are the "bounce" average density cards together with the B-L- $\lambda$  cards output from the last program. The cards are rearranged by L line rather than by constituent as they have been arranged in previous programs. A counter card must again be inserted in order to inform the computer of the number of card pairs per constituent for a given L-line. All input is on tape 2. For a given L-line the constituents must be in the following order:

- (1) helium,
- (2) oxygen,
- (3) molecular oxygen,
- (4) nitrogen,
- (5) hydrogen.

### 1. Input Card Description

	<u>Columns</u>	<u>Mode</u>	<u>Quantity</u>	<u>Units</u>	<u>Description</u>
Counter Card	1-2	I	NPT	-	B-L- $\lambda$ and density card pair counter
B-L- $\lambda$ Card	1-8	F	EL	earth radii	magnetic field line
	9-16	F	B	gauss	magnetic induction
	17-24	F	ALATO	degrees	latitude
	73-80	-	-	-	constituent name
Density Card	1-12	E	*	atoms/cm <sup>3</sup>	density for flux model 1
	13-24	E	*	"	density for flux model 2
	25-36	E	*	"	density for flux model 3
	37-48	E	*	"	density for flux model 4
	49-60	E	*	"	density for flux model 5
	73-80	-	-	-	constituent name

\* All of the five constituents use the same card format here. Therefore the quantity on a given density card (HE, O, O<sub>2</sub> N<sub>2</sub> or H) will depend on the constituent name listed in columns 73-80 of that same card.

## 2. Sample

## GENERAL PURPOSE DATA SHEET

Problem INPUT - R,  $\Sigma$  CALCULATION AND FLUX ELIMINATION

Sponsor TAPE 2

Problem	INPUT - R, $\Sigma$	CALCULATION AND FLUX ELIMINATION	Date	SAMPLE	Page	of
1. 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 31 32 33 34 35 36 37 38 39 40 41 42 43 44 45 46 47 48 49 50 51 52 53 54 55 56 57 58 59 60 61 62 63 64 65 66 67 68 69 70 71 72 73 74 75 76 77 78 79 80						
5						HEL IUM
1. 1 4 2 0 0 0 . 2 3 3 7 6 . 8 . 9 7 3						HEL IUM
0 . 1 0 9 2 E 0 7 0 . 1 0 1 0 E 0 7 0 . 8 9 9 1 E 0 6 0 . 7 6 3 5 E 0 6 0 . 6 7 4 2 E 0 6						HEL IUM
1. 1 4 2 0 0 0 . 2 2 3 9 4 6 . 9 7 3						HEL IUM
0 . 6 2 5 6 E 0 6 0 . 5 5 9 0 E 0 6 0 . 4 6 8 3 E 0 6 0 . 3 5 8 1 E 0 6 0 . 2 8 6 8 E 0 6						HEL IUM
1. 1 4 2 0 0 0 . 2 1 6 8 0 1 . 4 . 9 7 3						HEL IUM
0 . 4 7 7 5 E 0 6 0 . 4 1 0 5 E 0 6 0 . 3 2 2 6 E 0 6 0 . 2 2 1 0 E 0 6 0 . 1 5 8 6 E 0 6						HEL IUM
1. 1 4 2 0 0 0 . 2 1 2 1 5 2 . 9 7 3						HEL IUM
0 . 3 6 8 3 E 0 6 0 . 3 0 5 4 E 0 6 0 . 2 2 6 2 E 0 6 0 . 1 3 9 9 E 0 6 0 . 9 0 7 0 E 0 5						HEL IUM
1. 1 4 2 0 0 0 . 2 0 9 8 8 0 . 9 7 3						HEL IUM
0 . 2 8 7 5 E 0 6 0 . 2 3 0 6 E 0 6 0 . 1 6 1 8 E 0 6 0 . 9 1 2 5 E 0 5 0 . 5 4 0 2 E 0 5						HEL IUM
1. 1 4 2 0 0 0 . 2 3 3 7 6 8 . 9 7 3						OXYGEN
0 . 1 8 3 3 E 1 0 0 . 1 8 3 8 E 1 0 0 . 1 8 7 0 E 1 0 0 . 1 9 5 2 E 1 0 0 . 2 0 5 8 E 1 0						OXYGEN
1. 1 4 2 0 0 0 . 2 3 9 4 6 . 9 7 3						OXYGEN
0 . 7 4 8 4 E 0 8 0 . 6 2 0 0 E 0 8 0 . 4 8 9 8 E 0 8 0 . 3 4 8 9 E 0 8 0 . 2 6 1 3 E 0 8						OXYGEN
1. 1 4 2 0 0 0 . 2 1 6 8 0 4 . 9 7 3						OXYGEN
0 . 1 0 0 3 E 0 8 0 . 6 5 6 0 E 0 7 0 . 3 8 0 9 E 0 7 0 . 1 7 0 9 E 0 7 0 . 8 5 3 1 E 0 6						OXYGEN
1. 1 4 2 0 0 0 . 2 1 2 1 5 2 . 9 7 3						OXYGEN
0 . 1 4 6 8 E 0 7 0 . 7 5 9 5 E 0 6 0 . 3 2 4 8 E 0 6 0 . 9 1 8 6 E 0 5 0 . 3 0 5 7 E 0 5						OXYGEN
1. 1 4 2 0 0 0 . 2 0 9 8 8 0 . 9 7 3						OXYGEN
0 . 2 5 8 4 E 0 6 0 . 2 3 3 7 6 8 . 9 7 3						OXYGEN
1. 1 4 2 0 0 0 . 6 6 6 5 E 1 0 0 . 7 8 7 2 E 1 0 0 . 1 0 2 6 E 1 1 0 . 1 3 2 0 E 1 1						OXYGEN
1. 1 4 2 0 0 0 . 2 2 3 9 4 6 . 9 7 3						OXYGEN

## G. Output

Output for this program occurs on tapes 3 and 5. Tape 3 contains two groups of data for each L. The first group lists the values of R,  $\Sigma$  and OXY as functions of position and flux model. The second group contains R,  $\log_e R$ ,  $\Sigma$ ,  $\log_e \Sigma$  and solar flux as functions of position and time.

On tape 5 is the data to be punched for use in the conservation equation calculation. Each B-L- $\lambda$  card is followed by two R cards which are followed in turn by two  $\Sigma$  cards.

### **1. Tape 3 Sample**

	S=250	S=200	S=150	S=100	S=70
L	1.14200	0.23376	LAT= 8.973		
OXY	0.5479E-11	0.5975E-11	0.6624E-11	0.8475E-11	0.1046E-12
RATIO	0.2037E-08	0.2221E-08	0.2537E-08	0.3151E-08	0.3889E-08
SIGMA	0.3331E-14	0.3303E-14	0.3766E-14	0.4672E-14	0.5757E-14

L	1.14200	B= 0.22394	LAT= 6.973		
OXY	0.3259E-09	0.2545E-09	0.1635E-09	0.1138E-09	0.7492E-09
RATIO	0.1208E-10	0.9452E-11	0.6622E-11	0.4231E-11	0.2765E-11
SIGMA	0.1765E-16	0.1379E-16	0.9906E-17	0.6101E-17	0.3984E-17

L	1.14200	B= 0.21680	LAT= 4.973		
OXY	0.1631E-08	0.9054E-07	0.5278E-07	0.2141E-07	0.1007E-07
RATIO	0.6065E-12	0.3700E-12	0.1962E-12	0.7958E-13	0.3744E-13
SIGMA	0.8406E-18	0.5144E-18	0.2747E-18	0.1145E-18	0.5633E-19

L	1.14200	B= 0.21215	LAT= 2.973		
OXY	0.1731E-07	0.8997E-06	0.3982E-06	0.1296E-06	0.5424E-05
RATIO	0.6435E-13	0.3345E-13	0.1480E-13	0.4816E-14	0.2016E-14
SIGMA	0.1023E-16	0.5969E-17	0.3173E-19	0.1425E-19	0.7875E-20

L	1.14200	B= 0.20985	LAT= 0.973		
OXY	0.3371E-06	0.1677E-06	0.7598E-06	0.2981E-05	0.1557E-05
RATIO	0.1253E-13	0.6232E-14	0.2624E-14	0.1198E-14	0.5789E-15
SIGMA	0.3255E-19	0.2143E-19	0.1314E-19	0.6810E-20	0.3927E-20

LAT= 8.9730 L= 1.1420 B= 0.2338

TIME (YRS)	SOLAR FLUX	LOG OF RATIO	RATIO
0	70.00	-0.19365E 02	0.38892E-08
1	75.00	-0.19400E 02	0.37550E-08
2	130.00	-0.19706E 02	0.27666E-08
3	230.00	-0.19977E 02	0.21087E-08
4	250.00	-0.20012E 02	0.20368E-08
5	220.00	-0.19960E 02	0.21457E-08
6	185.00	-0.19885E 02	0.23118E-08
7	140.00	-0.19749E 02	0.26492E-08
8	105.00	-0.19597E 02	0.30832E-08
9	90.00	-0.19505E 02	0.33798E-08
10	75.00	-0.19400E 02	0.37550E-08
11	70.00	-0.19365E 02	0.38892E-08

TIME (YRS)	SOLAR FLUX	LOG OF SIGMA	SIGMA
0	70.00	-0.32788E 02	0.57570E-14
1	75.00	-0.32823E 02	0.55601E-14
2	130.00	-0.33126E 02	0.41067E-14
3	230.00	-0.33396E 02	0.31370E-14
4	250.00	-0.33430E 02	0.30307E-14
5	220.00	-0.33378E 02	0.31915E-14
6	185.00	-0.33304E 02	0.34365E-14
7	140.00	-0.33169E 02	0.39339E-14
8	105.00	-0.33019E 02	0.45726E-14
9	90.00	-0.32928E 02	0.50088E-14
10	75.00	-0.32823E 02	0.55601E-14
11	70.00	-0.32788E 02	0.57570E-14

LAT= 6.9730 L= 1.1420 B= 0.2239

TIME (YRS)	SOLAR FLUX	LOG OF RATIO	RATIO
0	70.00	-0.26607E 02	0.27852E-11
1	75.00	-0.26537E 02	0.29862E-11
2	130.00	-0.25902E 02	0.56356E-11
3	230.00	-0.25237E 02	0.10957E-10
4	250.00	-0.25139E 02	0.12083E-10
5	220.00	-0.25286E 02	0.13434E-10
6	185.00	-0.25482E 02	0.85774E-11
7	140.00	-0.25806E 02	0.62006E-11
8	105.00	-0.26141E 02	0.44381E-11
9	90.00	-0.26328E 02	0.36806E-11
10	75.00	-0.26537E 02	0.29862E-11
11	70.00	-0.26607E 02	0.27852E-11

TIME (YRS)	SOLAR FLUX	LOG OF SIGMA	SIGMA
0	70.00	-0.40064E 02	0.39844E-17
1	75.00	-0.39993E 02	0.42776E-17
2	130.00	-0.39347E 02	0.81603E-17
3	230.00	-0.38675E 02	0.15991E-16
4	250.00	-0.38576E 02	0.17648E-16
5	220.00	-0.38724E 02	0.15221E-16
6	185.00	-0.38922E 02	0.12488E-16
7	140.00	-0.39250E 02	0.89911E-17
8	105.00	-0.39590E 02	0.64039E-17
9	90.00	-0.39780E 02	0.52931E-17
10	75.00	-0.39993E 02	0.42776E-17
11	70.00	-0.40064E 02	0.39844E-17

LAT= 4.9730 L= 1.1420 E= 0.2168

TIME (YRS)	SOLAR FLUX	LOG OF RATIO	RATIO
0	70.00	-0.30916E 02	0.37441E-13
1	75.00	-0.30790E 02	0.42455E-13
2	130.00	-0.29620E 02	0.13677E-12
3	230.00	-0.28329E 02	0.49772E-12
4	250.00	-0.28131E 02	0.60649E-12
5	220.00	-0.28428E 02	0.45089E-12
6	185.00	-0.28815E 02	0.30591E-12
7	140.00	-0.29440E 02	0.16382E-12
8	105.00	-0.30072E 02	0.87100E-13
9	90.00	-0.30413E 02	0.61897E-13
10	75.00	-0.30790E 02	0.42455E-13
11	70.00	-0.30916E 02	0.37441E-13

TIME (YRS)	SOLAR FLUX	LOG OF SIGMA	SIGMA
0	70.00	-0.44323E 02	0.56327E-19
1	75.00	-0.44205E 02	0.63395E-19
2	130.00	-0.43089E 02	0.19356E-18
3	230.00	-0.41817E 02	0.69067E-18
4	250.00	-0.41620E 02	0.84064E-18
5	220.00	-0.41915E 02	0.62604E-18
6	185.00	-0.42300E 02	0.42613E-18
7	140.00	-0.42914E 02	0.23059E-18
8	105.00	-0.43526E 02	0.12495E-18
9	90.00	-0.43850E 02	0.90378E-19
10	75.00	-0.44205E 02	0.63395E-19
11	70.00	-0.44323E 02	0.56327E-19

LAT= 2.9730 L= 1.1420 B= 0.2121

TIME (YRS)	SOLAR FLUX	LOG OF RATIO	RATIO
0	70.00	-0.33838E 02	0.20163E-14
1	75.00	-0.33692E 02	0.23311E-14
2	130.00	-0.32293E 02	0.94462E-14
3	230.00	-0.30636E 02	0.49528E-13
4	250.00	-0.30374E 02	0.64346E-13
5	220.00	-0.30767E 02	0.43452E-13
6	185.00	-0.31273E 02	0.26189E-13
7	140.00	-0.32069E 02	0.11824E-13
8	105.00	-0.32855E 02	0.53884E-14
9	90.00	-0.33257E 02	0.36028E-14
10	75.00	-0.33692E 02	0.23311E-14
11	70.00	-0.33838E 02	0.20163E-14

TIME (YRS)	SOLAR FLUX	LOG OF SIGMA	SIGMA
0	70.00	-0.46290E 02	0.78783E-20
1	75.00	-0.46191E 02	0.86967E-20
2	130.00	-0.45217E 02	0.23039E-19
3	230.00	-0.43942E 02	0.82457E-19
4	250.00	-0.43727E 02	0.10228E-18
5	220.00	-0.44050E 02	0.74037E-19
6	185.00	-0.44455E 02	0.49381E-19
7	140.00	-0.45057E 02	0.27037E-19
8	105.00	-0.45617E 02	0.15442E-19
9	90.00	-0.45895E 02	0.11698E-19
10	75.00	-0.46191E 02	0.86967E-20
11	70.00	-0.46290E 02	0.78783E-20

LAT= 0.9730 L= 1.1420 B= 0.2099

TIME (YRS)	SOLAR FLUX	LOG OF RATIO	RATIO
0	70.00	-0.35085E 02	0.57888E-15
1	75.00	-0.34977E 02	0.64504E-15
2	130.00	-0.33875E 02	0.19426E-14
3	230.00	-0.32290E 02	0.94762E-14
4	250.00	-0.32011E 02	0.12530E-13
5	220.00	-0.32430E 02	0.82409E-14
6	185.00	-0.32946E 02	0.49151E-14
7	140.00	-0.33688E 02	0.23424E-14
8	105.00	-0.34343E 02	0.12167E-14
9	90.00	-0.34653E 02	0.89241E-15
10	75.00	-0.34277E 02	0.64504E-15
11	70.00	-0.35085E 02	0.57888E-15

TIME YRS)	SOLAR FLUX	LOG OF SIGMA	SIGMA
0	70.00	-0.46986E-02	0.39268E-20
1	75.00	-0.46895E-02	0.43043E-20
2	130.00	-0.46041E-02	0.19104E-19
3	230.00	-0.45039E-02	0.27541E-19
4	250.00	-0.44872E-02	0.32550E-19
5	220.00	-0.45122E-02	0.29333E-19
6	185.00	-0.45436E-02	0.18509E-19
7	140.00	-0.45910E-02	0.11524E-19
8	100.00	-0.46370E-02	0.72732E-20
9	90.00	-0.46619E-02	0.56685E-20
10	75.00	-0.46895E-02	0.43043E-20
11	70.00	-0.46986E-02	0.39268E-20

2. Tape 5

a. Output Card Description

	<u>Columns</u>	<u>Mode</u>	<u>Quantity</u>	<u>Units</u>	<u>Description</u>
B-L-λ	1-8	F	ALATO	degrees	latitude
	9-16	F	EL	earth radii	magnetic field line
	17-24	F	B	gauss	magnetic induction
1st R Card	1-10	E	XS(1)	-	R for time 0
	11-20	E	XS(2)	-	R for time 1
	21-30	E	XS(3)	-	R for time 2
	31-40	E	XS(4)	-	R for time 3
	41-50	E	XS(5)	-	R for time 4
	51-60	E	XS(6)	-	R for time 5
2nd R Card	1-10	E	XS(7)	-	R for time 6
	11-20	E	XS(8)	-	R for time 7
	21-30	E	XS(9)	-	R for time 8
	31-40	E	XS(10)	-	R for time 9
	41-50	E	XS(11)	-	R for time 10
	51-60	E	XS(12)	-	R for time 11
1st Σ Card	1-10	E	XS(1)	atoms/cm	Σ for time 0
	11-20	E	XS(2)	"	Σ for time 1
	21-30	E	XS(3)	"	Σ for time 2
	31-40	E	XS(4)	"	Σ for time 3
	41-50	E	XS(5)	"	Σ for time 4
	51-60	E	XS(6)	"	Σ for time 5

	<u>Columns</u>	<u>Mode</u>	<u>Quantity</u>	<u>Units</u>	<u>Description</u>
2nd $\Sigma$ Card	1-10	E	XS(7)	atoms/cm	$\Sigma$ for time 6
	11-20	E	XS(8)	"	$\Sigma$ for time 7
	21-30	E	XS(9)	"	$\Sigma$ for time 8
	31-40	E	XS(10)	"	$\Sigma$ for time 9
	41-50	E	XS(11)	"	$\Sigma$ for time 10
	51-60	E	XS(12)	"	$\Sigma$ for time 11

This five card group is repeated for each new B and L.

b. Sample

GENERAL PURPOSE DATA SHEET

Problem Sponsor	OUTPUT-R, $\Sigma$ CALCULATION AND FLUX ELIMINATION		Page of
	TAPE 5	SAMPLE	
1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 31 32 33 34 35 36 37 38 39 40 41 42 43 44 45 46 47 48 49 50 51 52 53 54 55 56 57 58 59 60 61 62 63 64 65 66 67 68 69 70 71 72 73 74 75 76 77 78 79 80			
8 . 973 0	1 . 142 0	0 . 233 8	
0 . 3889E - 080 . 3755E - 080 . 2767E - 080 . 2109E - 080 . 2037E - 080 . 2146E - 08			
0 . 2312E - 080 . 2649E - 080 . 3083E - 080 . 3380E - 080 . 3755E - 080 . 3889E - 08			
0 . 5757E - 140 . 5560E - 140 . 4107E - 140 . 3137E - 140 . 3031E - 140 . 3191E - 14			
0 . 3437E - 140 . 3934E - 140 . 4573E - 140 . 5009E - 140 . 5560E - 140 . 5757E - 14			
6 . 973 0	1 . 142 0	0 . 223 9	
0 . 2785E - 110 . 2986E - 110 . 5636E - 110 . 1096E - 110 . 1208E - 110 . 1043E - 10			
0 . 8577E - 110 . 6201E - 110 . 4438E - 110 . 3681E - 110 . 2986E - 110 . 2785E - 11			
0 . 3984E - 117 . 0 . 4278E - 170 . 8160E - 170 . 1599E - 160 . 1765E - 160 . 1522E - 16			
0 . 1249E - 160 . 8991E - 170 . 6404E - 170 . 5293E - 170 . 4278E - 170 . 3984E - 17			
4 . 973 0	1 . 142 0	0 . 216 8	
0 . 3744E - 130 . 4245E - 130 . 1368E - 120 . 4977E - 120 . 6065E - 120 . 4509E - 12			
0 . 3059E - 120 . 1638E - 120 . 8710E - 130 . 6190E - 130 . 4245E - 130 . 3744E - 13			
0 . 5633E - 190 . 6339E - 190 . 1936E - 180 . 6907E - 180 . 8406E - 180 . 6260E - 18			
0 . 4261E - 180 . 2306E - 180 . 1250E - 180 . 9038E - 190 . 6339E - 190 . 5633E - 19			
2 . 973 0	1 . 142 0	0 . 212 1	
0 . 2016E - 140 . 2331E - 140 . 9446E - 140 . 4953E - 130 . 6435E - 130 . 4345E - 13			
0 . 2619E - 130 . 1182E - 130 . 5388E - 140 . 3603E - 140 . 2331E - 140 . 2016E - 14			
0 . 7878E - 200 . 8697E - 200 . 2304E - 190 . 8246E - 190 . 1023E - 180 . 7404E - 19			
0 . 4938E - 190 . 2704E - 190 . 1544E - 190 . 1170E - 190 . 8697E - 200 . 7878E - 20			
0 . 973 0	1 . 142 0	0 . 209 9	
0 . 5789E - 150 . 6450E - 150 . 1943E - 140 . 9476E - 140 . 1253E - 130 . 8241E - 14			
0 . 4915E - 140 . 2342E - 140 . 1217E - 140 . 8924E - 150 . 6450E - 150 . 5789E - 15			
0 . 3927E - 200 . 4304E - 200 . 1010E - 190 . 2754E - 190 . 3255E - 190 . 2533E - 19			

#### H. Running Time

The running time for this program will be about three minutes for every L line.

## VII. CONSERVATION EQUATION CALCULATION

### A. Introduction

This program studies the build-up of proton density by use of the conservation equation (see equation (1)). Several lines of action are available. Either a transient or a time-averaged steady state solution can be calculated for any of 15 desired energy levels without altering the program.

In the transient steady-state solution the conservation equation is integrated as a function of time for a particular energy level until maximum and minimum values of the densities start repeating from one solar cycle to another. At this point the cycle number is recorded together with the time of the maximum and minimum densities. These values are printed with the maximum and minimum density and flux values as well as with the ratio of the maximum flux to the minimum flux. In addition, when calculating the transient steady-state solution, one may have the time history of any one of the energy levels printed on tape 5 with as many points as desired.

In the time-averaged steady-state solution the condition  $dN_p/dt = 0$  yields a density equation for density  $N_p$  which is solved using the relative neutron source strength  $\Phi$  together with  $\Sigma$  and  $R$  from the last program. All these values are averaged over time for this solution of the conservation equation.

Three subroutines assist the main program: subroutine RUNGE is used in integrating by the Runge Kutta technique, subroutine DERIV is used to evaluate  $dN_p/dt$  for a given  $t$  and  $N_p$  and subroutine TABLE interpolates any given table either logarithmically or linearly.

### B. Equations

The form of the particle conservation equation used for the study of the proton population as a function of time is given by

$$\frac{dN_p}{dt} = C_0 \Phi - C_1 N_p \left( \frac{dE}{dx} \right) - C_2 N_p \frac{d}{dE} \left( \frac{dE}{dx} \right) - C_2 N_p \Sigma \quad (1)$$

where  $\frac{dE}{dx}$ ,  $\frac{d}{dE} \left( \frac{dE}{dx} \right)$ ,  $\Phi$  and  $\Sigma$  are the quantities to be supplied and where:

$N_p$  = density

$$C_0 = A_0 / L^2 E^{B_0} \cos^4 \lambda_0$$

$$C_1 = A_1 / E^{B_1}$$

$$C_2 = A_2 E^{B_2}$$

E = Energy

$A_0, \dots, A_2$  = high or low energy conservation equation coefficients depending on whether  $E > 80$  Mev. or  $E \leq 80$  Mev. respectively

$$B_0, \dots, B_2 = " " " " " " " " " " " " " "$$

$\lambda_0$  = mirror latitude

The condition  $dN_p/dt = 0$  yields the equation for the time averaged steady state proton density:

$$N_p = \frac{A_0 \Phi}{L^2 E^{B_0} \left[ \frac{A_1}{E^{B_1}} \left( \frac{dE}{dX} \right) + A_2 E^{B_2} \frac{d}{dE} \left( \frac{dE}{dX} \right) + A_2 E^{B_2} \Sigma \right] \cos^4 \lambda_0}$$

where  $\Phi$ ,  $\Sigma$  and the scale factor  $R$  used in calculating  $dE/dx$  and  $d/dE$  ( $dE/dx$ ) are all averaged over time.

The density  $N_p$  gives a flux by the equation:

$$\text{Flux} = 2C_2 N_p = N_p v$$

where  $v$  is the neutron velocity factor.

### C. Mnemonics

<u>Quantity</u>	<u>Description</u>	<u>Units</u>
TIME(J)	Abscissa of time in increments of years for 12 years	years
ELOSS(J)	$dE/dk$ corresponding to E(J) (see Figure 11)	Mev/cm.
E(J)	energy corresponding to ELOSS(J) "	Mev.
CONVM	conversion factor - months to seconds	-
AL0	$A_0$ for $E \leq 80$ Mev. (see page 130)	# protons cm. sec. Mev.
AL1	$A_1$ " " "	cm./sec.
AL2	$A_2$ " " "	cm./Mev <sup>2</sup> /sec.
AH0	$A_0$ for $E > 80$ Mev. (see page 130)	# protons cm. sec. Mev.
AH1	$A_1$ " " "	cm./sec.
AH2	$A_2$ " " "	cm./Mev <sup>2</sup> /sec.
BL0	$B_0$ for $E \leq 80$ Mev. (see page 130)	-
BL1	$B_1$ " " "	-
BL2	$B_2$ " " "	-
BH0	$B_0$ for $E > 80$ Mev. (see page 130)	-
BH1	$B_1$ " " "	-
BH2	$B_2$ " " "	-
DELOSS(J)	$d(dE/dx)/dE$ corresponding to DE(J) (see Figure 12)	cm. <sup>-1</sup>
DE(J)	energy corresponding to DELOSS(J) (see Figure 12)	Mev.

<u>Quantity</u>	<u>Description</u>	<u>Units</u>
PREL(J)	$\phi$ for TIME(J) (see page 130 and Figure 11)	-
AVPRL	simple average of PREL(1), ..., PREL(12)	-
ALAT	mirror latitude $\lambda_0$	degrees
EL	magnetic field line L	earth radii
B	magnetic induction B	gauss
CONVR	conversion factor - degrees to radians	-
ALATO	ALAT in radians	radians
CSLAT4	$\cos^4(\text{ALATO})$	-
EEL	$L^2$	(earth radii) <sup>2</sup>
R(I)	atmospheric scale factor R for TIME(I)	-
SIG(I)	atmospheric loss parameter $\Sigma$ for TIME(I)	atoms/cm.
ENO	initial density $N_{p_0}$ for integration	# protons/cm <sup>3</sup>
TSUBO	initial time $t_0$ for integration	months
DT1	integration interval for ICSUBO	months
DT2	integration interval for all other cycles	months
TEND	end limit on integration	months
IEST	initial energy level subscript	-
IEDEL	increment for energy level subscript	-
IEEND	final energy level subscript	-
IEPR	subscript of energy level whose time history is desired	-

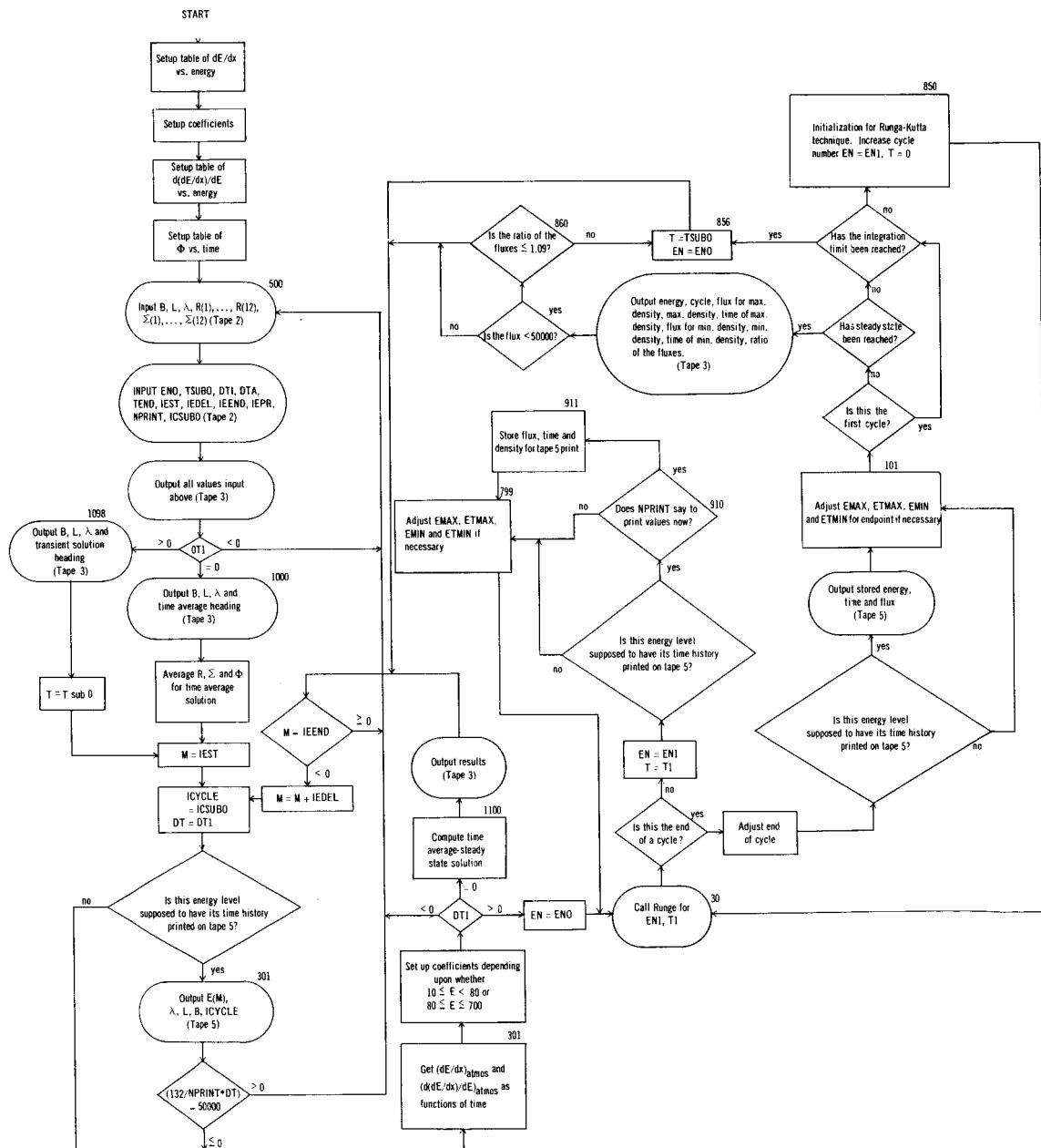
<u>Quantity</u>	<u>Description</u>	<u>Units</u>
NPRINT	a control factor for the time history print on tape 5. Density and flux are given for every NPRINT increments in time. (See Restriction (1)).	-
ICSUBO	initial cycle number corresponding to ENO and TSUBO	-
SUMR	sum of R(1), ..., R(12)	-
AVR	simple average of R(1), ..., R(12)	-
SUMSIG	sum of SIG(1), ..., SIG(12)	atoms/cm
AVSIG	simple average of SIG(1), ..., SIG(12)	atoms/cm
T	time	months
TMAX	time of an eleven year cycle - 132 months	months
TCK	time check to see if TEND has been reached	months
DT	increment in time	months
ICYCLE	cycle number	-
EMAX(J)	maximum density for cycle J	atoms/cm <sup>3</sup>
EMIN(J)	minimum density for cycle J	atoms/cm <sup>3</sup>
ETMAX(J)	time at EMAX(J)	months
ETMIN(J)	time at EMIN(J)	months
M	subscript to indicate the energy level which is under consideration	-
ENER	energy level M under consideration	Mev.
ITEST3	test value to see if the energy level under consideration is to have its time history printed on tape 5	-

<u>Quantity</u>	<u>Description</u>	<u>Units</u>
ALOSS	temporary storage of ELOSS(M)	Mev./cm.
X(1), ...,		
X(15)	temporary storage of DE(1), ..., DE(15)	Mev
Y(1), ...,		
Y(15)	temporary storage of DELOSS(1), ..., DELOSS(15)	cm <sup>-1</sup>
ALOSSA(J)	(dE/dx) × R(J) for energy ENER	Mev./cm.
DLOSSA(J)	(d(dE/dx)/dE) × R(J) for energy ENER	cm <sup>-1</sup>
A0	temporary storage of ALO or AHO	# protons cm. sec. Mev.
A1	temporary storage of AL1 or AH1	cm/sec
A2	temporary storage of AL2 or AH2	cm/Mev <sup>2</sup> sec
B0	temporary storage of BL0 or BH0	-
B1	temporary storage of BL1 or BH1	-
B2	temporary storage of BL2 or BH2	-
C0	conservation equation coefficient (see page 129)	# protons/cm <sup>3</sup> sec Mev.
C1	conservation equation coefficient (see page 129)	cm/sec. Mev.
C2	conservation equation coefficient (see page 129)	cm/sec. Mev.
DEDX	temporary storage of ALOSSA(J)	Mev./cm.
DDEDX	temporary storage of DLOSSA(J)	cm <sup>-1</sup>

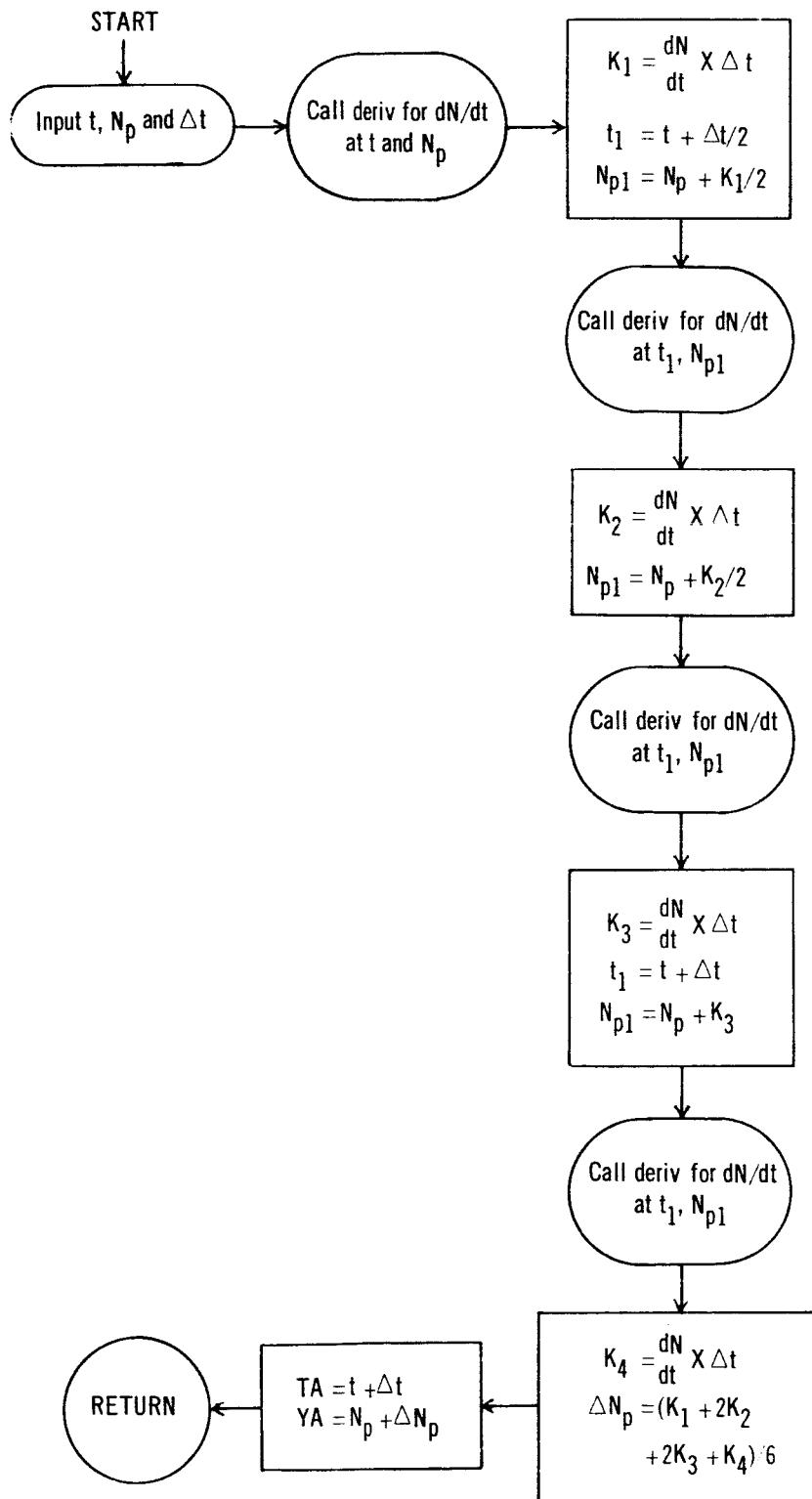
<u>Quantity</u>	<u>Description</u>	<u>Units</u>
DENS	proton density $N_p$	# protons/cm <sup>3</sup> Mev.
FLUX	proton flux	# protons/cm <sup>2</sup> sec. Mev.
NP	counter of the increments in time; used as a check for NPRINT	-
N5	counter of the number of prints on tape 5	-
EN	proton density $N_p$	atoms/cm <sup>3</sup> Mev
ICYM1	the value ICYCLE-1 used in testing for steady-state	-
TEST1	test to see if steady state has been reached	-
TEST2	test to see if steady state has been reached	-
EPR1	minimum density in cycle ICYM1	# protons/cm <sup>3</sup> Mev.
FLPR1	flux for EPR1	# protons/cm <sup>2</sup> sec. Mev.
TPR1	time of EPR1	months
EPR2	maximum density in cycle ICYM1	# protons/cm <sup>3</sup> Mev.
FLPR2	flux for EPR2	# protons/cm <sup>2</sup> sec. Mev.
TPR2	time of EPR2	months
RATIO	ratio of FLPR2 to FLPR1	-

## D. Flow Chart

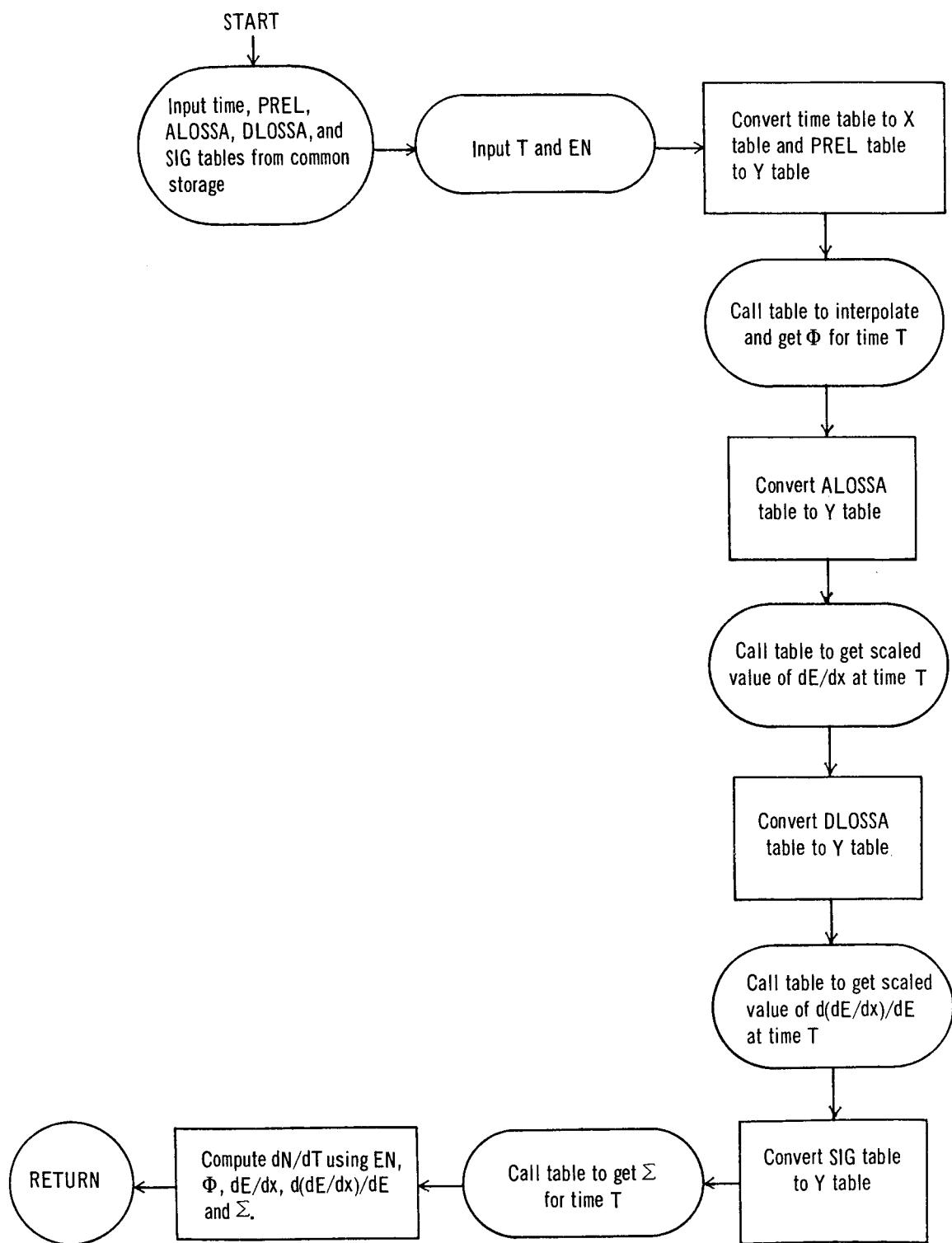
### 1. Main Program



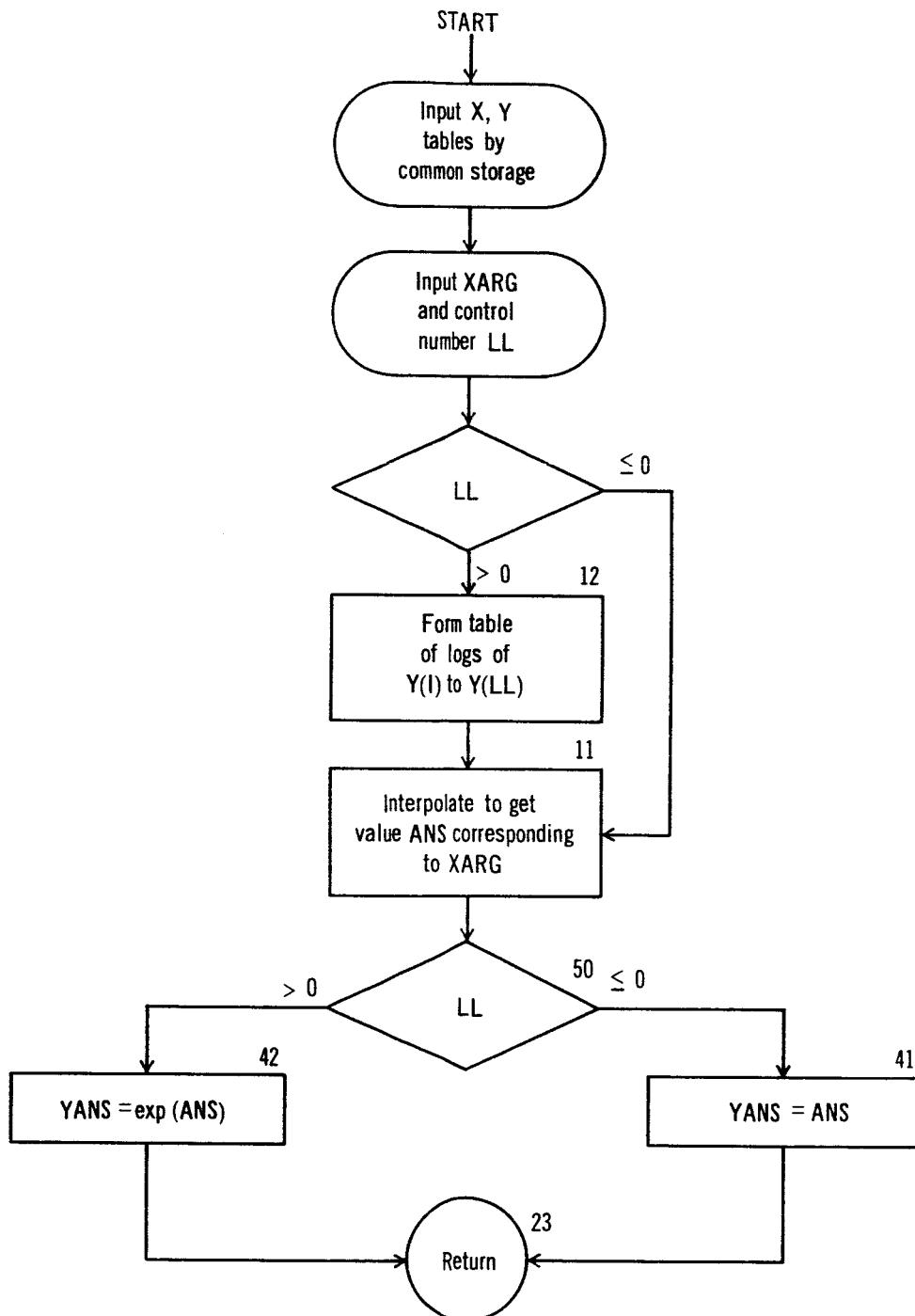
## 2. Subroutine RUNGE



### 3. Subroutine DERIV



4. Subroutine TABLE



## E. Fortran Listing

1C/C1/64

```

CCS:SER
C CONSERVATION EQUATION CALCULATION
C IF O11=0, THEN BRANCH TO TIME AVERAGE STEADY STATE SOLUTION.
C OTHERWISE, INTEGRATE STEADY STATE SOLUTION AVERAGED OVER TIME.
C
DIMENSION C(15),ELLOSS(15),TIME(12),R(12),DELLOSS(15),DE(15),PRCL(12)
I1,ALOSSA(12),LOSSA(12),X(15),Y(15),SIG(12),
IEAX(2CC),IEAY(2CC),LMIN(2CC),ETMIN(2CC),T5(5CC0),E5(5CC0),
IFL(5CC),
COMCN(C1,C2,X,Y,TIME,PREL,ALOSSA,LOSSA,SIG
FREQUENCY 716(5,C,10)
1 FORMAT(0E+0)
2 FORMAT(0E+0)
3 FORMAT(1F15.3,1E22C4,F20.3)
720 FORMAT(2E0.4/3F8.4/3I3/3I5)
TIME(1)=0.0
DC 11 J=1,1
11 TIME(J+1)=TIME(J)+12.0
ELLOSS(1)=5.3985E-2
ELLOSS(2)=2.5732E-2
ELLOSS(3)=1.4755E-2
ELLOSS(4)=1.0754E-2
ELLOSS(5)=8.6553E-2
ELLOSS(6)=7.3567E-2
ELLOSS(7)=6.4720E-3
ELLOSS(8)=5.3435E-2
ELLOSS(9)=4.6543E-3
ELLOSS(10)=4.1914E-3
ELLOSS(11)=3.8602E-3
ELLOSS(12)=3.6127E-3
ELLOSS(13)=3.2701E-3
ELLOSS(14)=3.0476E-3
ELLOSS(15)=2.8942E-3
E(1)=10.
E(2)=25.
E(3)=50.
E(4)=75.
E(5)=100.
E(6)=125.
E(7)=120.
E(8)=200.
E(9)=250.
E(10)=300.
E(11)=350.
E(12)=400.
E(13)=500.
E(14)=600.
E(15)=700.
C CONVERT IMC= 36CC*24*30 SEC
CCNVP= 2.592E6
19-F=20 MeV
C
AL0=CCNVP* 2.564E-13
AL1=CCNVP* 3.463E+6
AL2=CCNVP* 7.255E+6
BL0=2.*CC,
BL1=.*4.*2
BL2=.*4.*7

```

```

C   80-E-F0 REV
AH0=CNVNM*3.4792E-13
AH1=CNVNM*4.617E+8
AH2=CNVNM*1.343E+5
BH0=2.549
BH1=.626
BH2=.244
Dt(1)=10.
Dt(2)=10.5
Dt(3)=16.5
Dt(4)=27.5
Dt(5)=52.5
Dt(6)=12.5
Dt(7)=92.5
Dt(8)=137.5
Dt(9)=212.5
Dt(10)=262.5
Dt(11)=312.5
Dt(12)=412.5
Dt(13)=525.5
Dt(14)=625.5
Dt(15)=700.
DLGCS(1)=-.4CE-2
DLGCS(2)=-.3985E-2
DLGCS(3)=-.1710E-2
DLGCS(4)=-.1C51E-3
DLGCS(5)=-.2173E-3
DLGCS(6)=-.1172E-3
DLGCS(7)=-.743E-4
DLGCS(8)=-.354E-4
DLGCS(9)=-.153E-4
DLGCS(10)=-.101E-4
DLGCS(11)=-.713E-5
DLGCS(12)=-.410E-5
DLGCS(13)=-.244E-5
DLGCS(14)=-.166E-5
DLGCS(15)=-.131E-5
PREL(1)=1.25
PREL(2)=1.25
PREL(3)=1.22
PREL(4)=1.13
PREL(5)=1.16
PREL(6)=1.20
PREL(7)=1.25
AVPL=1.14e25
RLAD INPUT TAPE 2,1,ALAT,L,B
CNVNR=6.11453292E-1
ALATO=ALAT*CNVNR
CSLAT4=CSLF(ALATO)**4
ELET=L*EL
READ INPUT TAPE 2,2,((R(I),I=1,12),(SIG(J),J=1,L))

```

```

400 READ TAPE 2,72C,ENC,TSLUO,D11,LT2,ENC,TEST,FILEL,LENL,
L1EPL,4PL1,I1SUBC
C INPUT P1INP1U1
C WRITE OUTPUT TAPE 3,72C
        WRITE OUTPUT TAPE 3,72C,ENC,TSLUO,DT1,UT2,
72C FURMAT(2#) **** PROGRAM INPUT **** //
        WRITE OUTPUT TAPE 3,701,ALAT,EL,B,ENC,TSLUO,DT1,UT2,
1TNGD1,1TLEL,1FEND,1CSUB,1NPRT
    1T21 FURMAT(3#) LATC *** =F8.4/13H L ***** =F8.4/13H B **** =
    1F8.4/13H NP SUB C =E12.4/13H T SUB C =E12.4/
    113H DELTA EL =F8.4/13H DELTA T2 =F8.4
    2 /13H T ENL ***
2F5.1V/23H ENERGY LEVEL START =1.3/23H DELTA ENERGY LEVEL =1.3/
323H ENERGY LEVEL END =1.3//30H ENERGY LEVEL TIME HISTORY =1.3,
47X,92P INDICATES ENERGY LEVEL AT WHICH TIME HISTORY OF ENERGY AND
5FLUX WILL BE PRINTED ON TAPE 5. /4CX,43H HERE INDICATES NO TIME HI
6STORY ON TAPE 5 //30H CYCLE AT SUB ZERO ***** =15//35H PRI
7INITIUS TAPE 5 AFTER EVERY 16.5H DELTA T./)
    WRITE OUTPUT TAPE 3,7C2,R11,TIG(1)*=1.12)
    702 FURMAT(CA,4HRL1,10X,CHSIG(1)/(2E14.4))
C HEADING AND R,SIG,PREL, AVERAGED FOR TIME AVERAGE SI-SI. SOLUTION
C IF(D11) 500,1CC,1CH
      IF(D11) 500,1CC,1CH
1CC0 WRITE OUTPUT TAPE 3,1C01,ALAT,EL,1#
1CC1 FURMAT(48H1 TIME AVERAGE STEADY STATE SOLUTION FOR LATC =F8.4,
16H * L =F7.4,6H * B =F7.4//)
280H ENERGY PROTON- PROTON-
3 (DE/DX) D(CEDDX)/DE/ PHIBAR SIG BAK
434H (KtEV) FLUX DENSITY)
SUMR0.0 J
DU 106.2 NN=1.12
1CC2 SUMRSUMR+R(NN)
AVR=SUMR/12.6
DC 10G2 NN=1.12
1CC3 R(NN)=AVR
SUMS1=C.0
DC 10G5 NN=1.12
1CC5 SUMS1=SUMSIG+SIG(NN)
AVSIG=SUMSIG/12.6
DU 10G6 NN=1.12
1CC6 SIG(NN)=AVSIG
DU 10G7 NN=1.12
1CC8 PREL(NN)=APRL
GL FG 1059
1C98 WRITE OUTPUT TAPE 3,705,ALAT,EL,B
7C5 FURMAT(45#) TRANSIENT STATION STATE SOLUTION FOR LATC =F8.4,
16H * L =F7.4,6H * B =F7.4//)
24CH ENERGY CYCLE 1 MINIMUM - PRCTCN-6X,22HPRCTCN- I MAX
31#UM -,5X,7HPRCTCN-,6X,7HPRCTCN-,3X,13H FLUX RATE/C
3 4X,33H(MEV) NO. 1 TIME (MC)
4 FLUX,9X,31#DENSITY 1 TIME (MC)
53X,1.3#E1 (MAX/MIN)
510X,1F1,37X,1H1,35X,1H1
T=TSLUO
TMAX=132.
TCK=6.0
C FILEN MUST BE LESS THAN OR EQUAL TO 15, BUT GREATER THAN 0

```

```

1C'9 DU 3CG, M=TEST, TEEAC, ITTEL
DT=DTI
ICYCLE=ICSUBC
EMAX(1)=EBC
ETMAX(1)=0.0
EMIN(1)=NG
EMIN(1)=0.0
ENER=L(M)

C TIME HISTORY HEADING ON TAPE 5
ITEST=M-1LPR
IF(IUT<13) 31C,101,31C
301 WRITE OUTPUT TAPE 5,302,ENER,ALAT,EL,B
302 FORMAT(4SH1 TIME HISTORY OF ENERGY AND FLUX FOR ENERGY =F6.1,
1 9H , LAU0 =F8.4, 6H , B =F7.4/24X.95H TIME FLUX
2  DENSITY 1 TIME FLUX DENSITY 1 TIME
3UX  DENSITY)
WRITE OUTPUT TAPE 5,900,1CYCLE
900 FORMAT(14H CYCLE NO. =14,35,1H1,33X,1H1)
IF(I13>0/FLCATE(NPRINT)*CT)->CC0.C) 31C,310,9C1
901 WRITE OUTPUT TAPE 3,902
902 FORMAT(6HONPRINT WILL CAUSE TS,ED,AND FL TO EXCEED DIMENSION CF
15000.)
```

145

```

GG TC 3C0
310 ALLOSS=ALLOSS(M)
DC 201 K=1,15
X(K)=U(K)
2C1 Y(K)=DLOSS(K)
CALL TABLE(ENER,EANS,15)
DO 20 J=1,12
ALLOSS(J)=K(J)*ALLOSS
20 DLOSS(J)=R(J)*EANS
C NOW HAVE (GE/GX) AMOS AND (D(GE/DX)/DE)ATCS AS FUNCTIONS
C OF TIME FOR A GIVEN ENERGY AND L
710 IF(LUNCH-B0.) 21,21,22
21 AU=ALC
AU=A1L
A1=A1L
A2=A1Z
B0=BLC
B1=B1L
B2=B2L
GU TO 23
22 A0=A0H
A1=AH1
A2=AH2
B0=BH0
B1=BH
B2=BH?
23 C=AG(1ELE*ENER**UC*CSL*14)
C1=AV((ENER*B1)
C2=A2*LNC*B2
C COMPUTE THE AVERAGE STEADY STATE SOLUTION
1+LUT) 50,L1C,1959
IF(DDX=ALLOSS(1))
DDEDX=ALLOSS(1)
DENS=AU*AVPL/(LAC(CO)*(C1*DEDX+C2*(LDEDX+AVSIG)))
FLUX=2.0*DENS*C2/CNV
```

```

      WRITE, OUTPUT TAPE 3, 1101, ENER, FLUX, DENS, AVPRL, AVSIG,
      IDEDX, CDEDX
1101 FORMAT(1HC, F6.2, 1P6E13.4)
      GO TO 360
C BEGIN RUNGE KUTTA TECHNIQUE
1599 NP=0
      N5=0
      EN=ENO
      30 CALL RANGE(T, SN, CI, DEN, T1, EN1)
      IF(T1-TMAX) 31, JCC, 1CC
31 EN=EN1
      T=T1

C TEST/STORE LINE HISTORY
      IF(TLE1.5) 750, 91C, 79J
910 NP=NP+1
      IF(NP-NPAINT) 799, S11, 911
      N5=N5+1
      NP=0

      TS(N5)=T1
      E5(N5)=EN1
      FLS(N5)=EN1*2.0*C2/CCNVM
      TEST AND STORE P'IN-MAX
      759 IF(EMAX(1CYCLE)-EN1) 800, 30, 801
      800 EMX(1CYCLE)=EN1
      EMAX(1CYCLE)=T1
      GC TO 30
      801 IF(EMIN(1CYCLE)-EN1) 30, 3C, 8C2
      8C2 EMIN(1CYCLE)=EN1
      EMIN(1CYCLE)=T1
      GL TO 3C

C ADJUST END OF 11 YEAR CYCLE
      1C0 EN1=EN*(TMAX-T)/CT1*GEN
      IF(TLE1.5) 1C1, 915, 1C1
      C PRINT P'IN-HISTORY ON 5
      915 N5=N5+1
      TS(N5)=TMAX
      E5(N5)=EN1
      FLS(N5)=EN1*2.0*C2/CCNVM
      WRITE, OUTPUT TAPE 5, 916, (TS(I), FLS(I), E5(I), I=1,N5)
916 FURPA(12CX,OPF9.3,OPF1.1,1PE12.4,2H 1,CPF9.3,CPF11.4,1PE12.4)
      12H 1,CPF5.3,CPF11.4,1PE12.4)
      ICY5=1CYCLE+1
      WRITE, OUTPUT TAPE 5, 9C0, ICY5
      N5=0
      NP=0

C CHECK END POINT FOR *IN-MAX
      1C1 IF(EMAX(1CYCLE)-EN1) 1C0, 815, 811
      810 EMAX(1CYCLE)=EN1
      CTMAX(1CYCLE)=TMAX
      GC TO 812
      811 IF(EMIN(1CYCLE)-EN1) 815, 815, 812
      812 EMIN(1CYCLE)=EN1
      CTMIN(1CYCLE)=TMAX
      C TEST STEADY STATE SOLUTION
      d15 TCK=TCK+132.0
      IF(ICYCLE-ICSECI) 813, 849, 82C

```

```

319 STOP //////
820 ICYMI=ICYCLE-1
TEST1=LMAX(ICYCLE)/FMAX(ICYMI )-1.0
TEST2=LMIN(ICYCLE)/EMIN(ICYMI )-1.0
IF(LAHS(1,TEST1)-1.0,CE-4) 821,821,849
821 IF(LAHS(1,TEST2)-1.0,CE-4) 822,822,849
822 TPRI=EMIN(ICYMI )
EPR1=EPRI*MIN(ICYMI )
FLPRI=FLPRI*2*CC2/CCNVM
TPR2=EMAX(ICYMI )
EPR2=EMAX(ICYMI )
FLPR2=EPRI*2*CC2/CCNVM
RATIO=FLPRI/FLPR1
WRITE OUTPUT TAPE 3,823,ENER,ICYMI ,TPR1,FLPRI,EPRI,TPR2,fLPR2
1 EPRI2,KALIU
WRITE OUTPUT TAPE 3,823,ENER,ICYMI ,TPR1,FLPRI,EPRI,TPR2,fLPR2
823 FORMAT(10H9.2,3X,13.4H 1,0PF9.4,0PF13.4,1PF13.4,3H 1,0PF13.4,
10PF14.4,1PF13.4,3H 1,0PF13.4)
11 TAB5*(FLPRI-5CC0.) 86C,831,831
12HNC 1.0PF13.4,3H 1,0PF13.4
96G IFRATIO=1.09C1 861,861,81C
861 WRITE OUTPUT TAPE 3,862
862 FORMAT(1//96H ALL HIGHER ENERGY LEVELS ARE BEING NEGLECTED SINCE
LE THE FLUX RATIO HAS BECOME LESS THAN 1.0-C.)
GO TO 300
831 WRITE OUTPUT TAPE 3,832
832 FORMAT(1//,52H 1 BLCW UP. RERUN THIS CASE WITH SMALLER DELTA 1
1.)
833 GO TO 300
834 WRITE OUTPUT TAPE 3,834
FORMAT(10H1.1,37X,1H1,39X,1H1)
GU TU 856
849 IF(TCK-TENC) 850,855,855
850 T=0.0
EN=EN1
DT=DT2
ICYCL=ICYCLE+1
EMAX(ICYCL)=EMI
EMIN(ICYCL)=EMI
EMAX(ICYCLE)=0.0
EMIN(ICYCLE)=0.0
GL TO 30
C NO TRANSIENT STEADY STATE SOLUTION AS YET
855 TPRI=EMIN(ICYCLE)
EPRI1=EPRI*MIN(ICYCLE)
FLPRI1=FLPRI*2*CC2/CCNVM
TPR2=EMAX(ICYCLE)
EPR2=EMAX(ICYCLE)
FLPR2=FLPRI*2*CC2/CCNVM
RATIO=FLPRI*2/FLPR2
WRITE OUTPUT TAPE 3,857,ENER,ICYCLE,TPR1,FLPRI,EPRI,TPR2,fLPR2,
1EPRI2,PAU
857 FORMAT(10H9.2,3X,13.4H 1,0PF9.4,0PF13.4,1PF13.4,3H 1,0PF13.4,
10PF14.4,1PF13.4,3H 1,0PF13.4)
12HNC 1.05-S SCRN. AS YET
858 WRITE OUTPUT TAPE 3,858
856 T=TSMIN
TCK=0.0

```

CNSER

EN=ENC  
3CO CONTINUE  
GU TO 3CO  
END(1,0,C,C,0,0,1,0,0,0,0,C,0,0)

1C/01/64

## LOCATIONS OF NAMES IN TRANSFER VECTOR

COS (FPT)	DEC 3 0	LCT CCC03 CCCC0	DEC EXP(3 (RIN)	OCT 7 2	OCT 00C7 CCUC2	DEC RUNGE (STH)	OCT b 4	DEC 00010 00004	DEC TABLE (TSI)	OCT 6 1	CCC06 CCCO1
--------------	---------------	-----------------------	-----------------------	---------------	----------------------	-----------------------	---------------	-----------------------	-----------------------	---------------	----------------

## ENTRY POINTS TO SUBROUTINES NOT OUTPUT FROM LIBRARY

CCS	LXP(3	RUNGE	TABLE	(FIL)	(FPT)	(RTN)	(STH)	(TSI)	(TSI)	(TSI)
-----	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------

## EXTERNAL FORMULA NUMBERS WITH CORRESPONDING INTERNAL FORMULA NUMBERS AND OCTAL LOCATIONS

EFN	IFN	LCC									
11	26	00021	500	113	00315	4C0	130	00401	1000	141	00534
LC03	148	00566	1005	151	00575	1006	154	00606	1008	156	00613
1099	163	00646	301	173	00705	9C1	178	00755	310	180	00764
20	18H	010C7	710	189	C1C14	21	190	01020	22	197	C1C37
H100	2C7	01120	1599	214	01204	30	217	01213	31	220	C1231
911	225	01251	799	230	01271	800	231	01275	801	234	01302
100	236	01314	915	240	01326	101	254	01414	810	255	C1420
812	259	01432	815	261	01436	819	263	01445	820	264	C1447
H22	269	01500	860	279	01564	861	280	01570	831	282	01577
349	286	01616	850	287	01622	855	296	01646	856	306	C1735

## STORAGE NOT USED BY PROGRAM

DEC UCT  
17467 42CT5DEC CCT  
32468 77324

## STORAGE LOCATIONS FOR VARIABLES APPEARING IN COMMON STATEMENTS

DEC	UCT	DEC	CCT
ALGSSA	17304	CO	32561
PKEL	32516	SIG	32480
EMIN	16994	DE	17465
R 17436	42034	E	17466
		T5	16554

## STORAGE LOCATIONS FOR VARIABLES APPEARING IN DIMENSION AND EQUIVALENCE STATEMENTS

DEC	UCT	DEC	CCT
CLCSS	17424	DE	17465
EMIN	42020	E	42C01
R 17436	41142	T5	42C72
			16554
			40322

## STORAGE LOCATIONS FOR VARIABLES NOT APPEARING IN COMMON, DIMENSION, OR EQUIVALENCE STATEMENT

DEC	UCT	DEC	CCT
A0	1594	A1	1553
AH2	1585	AL0	1568
ALAT	1584	ALCSS	1583
BC	1579	B1	1578
BH2	1574	BLG	1573
CCNVM	1569	CGNVR	1566
EANS	1564	CG34	1563
ENR	1559	EEL	1558
ENER	1554	EN	1553
FLPR2	1549	FLUX	1548
ICYMI	1544	I EDEL	1547
ITEST3	1535	M	1538
RATIC	1534	SUMR	1533
TENU	1529	TEST1	1528
TPR2	1524	TEST2	1527
		T	1523
			02764

DEC	CCT	DEC	CCT
AI	33C71	A2	1592
AL1	03C64	AL1	1587
AVPRL	03C57	AVR	1582
B2	15C52	B2	1577
BL1	15D45	BL1	1572
CSLATA	15E40	CSLATA	1567
C3C33	15E3	C3C33	1562
EL	03C26	EL	1557
C3C21	15C2	EPR1	1552
ICSUBO	03C14	ICSUBO	1547
IEEND	15C07	IEEND	1542
NS	15C02	NS	1537
SUMSIG	1532	SUMSIG	1532
TEST2	02775	TEST2	1527
TSUBO	02767	TSUBO	1522
			02763
			1

## SYMBOLS AND LOCATIONS FOR SOURCE FORMAT STATEMENTS

EFN	LCC	EFN	LCC
811	1 C2750	812	2 C2746
81LT	701 02726	81LU	7C2
81PO	824 C2160	81QC	832 C2173
81S6	902 C2272	81SK	916 C2253

DEC	CCT	DEC	CCT
2)	1CC0	3)	1CC7
C1G6	1519	C1G7	1520
D1G3	01220	D1G3	2CC
E110	541 01035	E112	591 01117
E1503	203 CC313		

## LOCATIONS FOR OTHER SYMBOLS NOT APPEARING IN SOURCE PROGRAM

DEC	OCT	DEC	OCT
1)	1513 02751	2)	1CC7 01757
C1G4	1518 02756	C1G6	1519 C2757
C121T	909 C1615	D1G3	00310
E110	541 01035	E112	591 01117
E1503	203 CC313		

EFN	LCC	EFN	LCC
819t	302 C2344	81PS	7CC 02734
81PG	12C C2740	81PN	823 02234
81Q	862 C2215	81Q	9CC 02301
	1101 C2257		

DEC	OCT	DEC	OCT
1)	1513 02751	2)	1CC7 01757
C1G4	1518 02756	C1G6	1519 C2757
C121T	909 C1615	D1G3	00310
E110	541 01035	E112	591 01117
E1503	203 CC313		

EFN	LCC	EFN	LCC
61	32767 77777	61	11C0 02114
D12C3	1521 C2761	D12C3	201 00311
E1C	4CC C062C	E1C	451 OC703
E11G	664 C1230	E11G	779 01413

RANGE

```
C SUBROUTINE FOR RANGE KUTIA TECHNIQUE
SUBROUTINE RUNGTE(10,Y0,H,DELY,T,A)
CUMPCN C0,C1,C2,X,Y,TIME,PREL,ALCSA,DLCSA,SIG
CALL DERIV(10,Y0,DER)
C0=1.D-8
T1 = T0+H/2.
Y1 = Y0+C0*V1/2.
CALL DERIV(T1,Y1,DER)
C0=1.D-8
Y1 = Y0+C0*T2/2.
CALL DERIV(T1,Y1,DER)
C0=1.D-8
T1=T0+H
Y1=Y0+C0*T3
CALL DERIV(T1,Y1,DER)
C0=1.D-8
DLY=(C0*T1+Z.*CCN12+Z.*CCN13+C0*N14)/6.
TA= T0+H
YA= Y0+CELY
RETURN
END(1,1,0,0,0,0,1,0,0,C,G,C,O,O,O)
```

10/61/64

## STRUCTURE NOT USED BY PROGRAM

DEC OCT  
12, OCT  
115 OCT4

## STORAGE LOCATIONS FOR VARIABLES APPEARING IN COMMON STATEMENTS

DEC	OCT
ALGOSA 22554 77452	CC 32561 77461
P,PL 22555 77453	SIG 32552 77455

## STRUCTURE LOCATIONS FOR VARIABLES NOT APPEARING IN COMMON, DIMENSION, OR EQUIVALENCE STATEMENT

DEC	OCT
OCT11 124 OCT4	CC 412 CC173
Y1 115 OCT4	116 OCT6

## LOCATIONS FOR C1HLR SYMBOLS NOT APPEARING IN SOURCE PROGRAM

DEC	OCT
1) 111 OCT4	3) 1C8 OCT54

## LOCATIONS OF NAMES IN TRANSFER VECTOR

DEC	OCT
DERIV DEC OCT	DEC OCT

## ENTRY POINTS TO SUBROUTINES NOT OUTPUT FROM LIBRARY

LIBRIV

```
C SUBROUTINE IC EVALUATE (EN/C1) FOR A GIVEN T AND EN
SUBROUTINE DERIV(11,EN,DER)
DIMENSION TIME(12),PREL(12),ALOSSA(12),CLSSA(12),X(15),Y(15),SIG(112)
COMMON CC,C1,C2,X,Y,TIME,PREL,ALOSSA,CLSSA,SIG
CC=1 K=1,12
X(K)=TINF(K)
CONTINUE
DO 2 K=1,12
Y(K)=PSLT(K)
CONTINUE
CALL TABLE(1,TANS,O)
P=TANS
DO 3 K=1,12
Y(K)=ALCSSA(K)
CONTINUE
CALL TABLE(1,ANS,12)
EX=ANS
DO 4 K=1,12
Y(K)=CLSSA(K)
CONTINUE
CALL TABLE(T,ANS,12)
EXX=ANS
DO 5 K=1,12
Y(K)=SIG(K)
CONTINUE
CALL TABLE(T,ANS,12)
SIGANS
C EVALUATE (Dv/ET1)
DER=CC*p-C1*EN*EX-C2*EN*EXX-SIGMA*EN*C2
RETURN
END 11,10,C,0,C,1,C,0,0,C,0,0,C,0,0
```

## STORAGE NOT USED BY PROGRAM

DEC OCT  
114 CC162

## STORAGE LOCATIONS FOR VARIABLES APPEARING IN COMMON STATEMENTS

DEC OCT	CC1	DEC OCT	DEC CCT	DEC CCT	DEC CCT
ALC-SA 32564 77370	32561 77461	32560 77480	32559 77457	32492 77354	
PTEL 32516 77464	SIG 32480 77340	TIM 32528 77420	X 32558 77456	Y 32543 77437	

## STORAGE LOCATIONS FOR VARIABLES NOT APPEARING IN COMMON, DIMENSION, OR EQUIVALENCE STATEMENT

DEC OCT	CC1	DEC CCT	DEC OCT	DEC CCT
ANS 113 CC161	EX 112 00160	EXX 111 00157	P 110 00156	SIGNA 105 CC155
FNS 104 CC154				

## LOCATIONS FOR OTHER SYMBOLS NOT APPEARING IN SOURCE PROGRAM

DEC OCT	OCT	DEC OCT	DEC OCT	DEC CCT
1) 1C4 0C150	2) 98 0137	1) 98 00142		

## LOCATIONS OF NAMES IN TRANSFER VECTOR

DEC OCT	OCT	DEC OCT	DEC OCT	DEC CCT
TAUDE DEC CCT				
TAUDE 0 CCCCC				

## ENTRY POINTS TO SUBROUTINES NOT OUTPUT FROM LIBRARY

TABLE

## EXTERNAL FORMULA NUMBERS WITH CORR-SPACING INTERNAL FORMULA NUMBERS AND OCTAL LOCATIONS

EFN 1	LOC 7 CCO30	EFN 2	LOC 10 CCC35	EFN 3	LOC 16 00050	EFN 4	LOC 22 CCO63	EFN 5	LOC 28 CCC76

## TABLE

1C/01/64

```

C SUBROUTINE TO INTERPOLATE A GIVEN TABLE
SUBROUTINE TABLE(XARG,YANS,LL)
DIMENSION X(15),Y(15)
COMMON CO,C1,C2,X,Y,TIME,PREL,ALCSA,SIG
IF(LL)11,11,12
12 DC 10 K=1,LL
      A=Y(K)
      Y(K)=LCGF(A)
      LO CNTTRUE
      DO 20 J=1,15
      IF(X(J)-XARG)>20,21,22
21 ANS=Y(J)
      GC T0 >G
      22 H1=X(J)
      Y1=Y(J)
      H0=X(J-1)
      Y0=Y(J-1)
      ANS=Y1-(Y1-YC)*(H1-XARG)/(H1-HG)
      GC TC >C
      20 CLNTINC
      50 IF(LL)1,41,42
      41 YANS=ANS
      42 GC TC 23
      23 YANS=APF(ANS)
      23 RETURN
      END(1,1,U,U,C,O,C,1,O,C,C,C,O,O)

```

## STACKAGE AND USED BY PROGRAM

DEC OCT  
LIC C0156  
LCC 32523 77412

## STRUCTURE LOCATIONS FOR VARIABLES APPEARING IN COMMON STATEMENTS

DEC	LIC	DEC	LIC	DEC	OCT
32523	77416	CO 32561	17461	C1 32560	77457
PHLL	32521 77417	SIG 32524	77414	11PC 32523	X 77420

## STRUCTURE LOCATIONS FOR VARIABLES NOT APPEARING IN COMMON, DIMENSION, OR EQUIVALENCE STATEMENT

DEC	LIC	DEC	OCT	DEC	OCT
ANS	103 C0155	A 1CH	C0154	H0 1C7	00153
Y0	104 C015C	Y1 1C3	C0147		

## LOCATIONS FOR OTHER SYMBOLS NOT APPEARING IN SOURCE PROGRAM

DEC	LIC	DEC	OCT	DEC	OCT
1)	99 C0143	2) S2 C0134	6) 93 00135	C0141	00146
2)	40 C0060	8) C0122			

## LOCATIONS OF NAMES IN TRANSFER VECTOR

DEC	LIC	DEC	OCT	DEC	OCT
EXP	1 C0001	LCG 0 CCCCC			

## ENTRY POINTS TO SUBROUTINES NOT OUTPUT FROM LIBRARY

EXP LCG

## EXTERNAL FORMULA NUMBERS WITH CORRESPONDING INTERNAL FORMULA NUMBERS AND OCTAL LOCATIONS

EFN	IFN	LCC	EFN	IFN	LCC	EFN	IFN	LCC
12	6 C0031	1C 9 CCC43	11 1G 00045	21 12 CC053		22	14 C0061	
20	20 C0111	5C 21 00114	41 22 00117	42 24 CC123		23	25 C0130	

## F. Restrictions

- (1)  $132 / (\text{NPRINT} \times \text{DT1})$  must be less than 5000 in order that T5, E5 and FL5 subscripts do not exceed their dimension specifications.
- (2) IEEND cannot exceed 15 since the table of energy levels contains only 15 values (see energy level table below)

## G. Input

Input to this program consists of five data cards and four control cards for every B-L line considered. The data cards are those output by the preceding program. The control cards are those that handle the selection of the many available calculations in this program. The first control card contains the initial density (END) and the initial time (TSUBO) for integration. The second card contains the integration interval for the first cycle (DT1), the integration interval for all other cycles (DT2) and the end limit of integration (TEND). Setting DT1 equal to zero will give a time averaged steady state solution of the equation. The next control card defines the energy level(s) to be used. It gives the initial energy level subscript (IEST), the increment in energy level subscripts (IEDEL) and the final energy level subscript (IEEND). Energy levels are as follows:

E(1) = 10 Mev	E(6) = 125 Mev	E(11) = 350 Mev.
E(2) = 25 Mev	E(8) = 150 Mev	E(12) = 400 Mev.
E(3) = 50 Mev	E(8) = 200 Mev	E(13) = 500 Mev.
E(4) = 75 Mev	E(9) = 250 Mev	E(14) = 600 Mev.
E(5) = 100 Mev	E(10) = 300 Mev	E(15) = 700 Mev.

Note that IEST, IEEND and IEDEL must be greater than zero and that IEND cannot be greater than 15. The fourth control card contains three numbers (1) IEPR is the subscript of that energy level whose time history is to be printed on tape 5. If IEPR = 0 then no time history will be printed. (2) NPRINT tells the computer how often to print density, flux and time values on tape 5 if IEPR  $\neq$  0. Values will be given for every NPRINT increments in time. However, if  $132 / (\text{NPRINT} \times \text{DT1})$  is greater than 5000 the computer will print an error message and go on to the next case. This is done in order to prevent time, energy and flux subscripts from exceeding their dimension statement capacities. (3) ICSUBO is the cycle number at initial density (ENO) and initial time (TSUBO). ICSUBO is always greater than or equal to 1. All input occurs on tape 2.

### 1. Input Card Description

	<u>Columns</u>	<u>Mode</u>	<u>Quantity</u>	<u>Units</u>	<u>Description</u>
<u>Card 1</u>	1-8	F	ALAT	degrees	latitude
	9-16	F	EL	earth radii	magnetic field line
	17-24	F	B	gauss	magnetic induction
<u>Card 2</u>	1-10	E	R(1)	-	scale factor R for TIME(1)
	11-20	E	R(2)	-	scale factor R for TIME(2)
	21-30	E	R(3)	-	scale factor R for TIME(3)
	31-40	E	R(4)	-	scale factor R for TIME(4)
	41-50	E	R(5)	-	scale factor R for TIME(5)
	51-60	E	R(6)	-	scale factor R for TIME(6)
<u>Card 3</u>	1-10	E	R(7)	-	scale factor R for TIME(7)
	11-20	E	R(8)	-	scale factor R for TIME(8)
	21-30	E	R(9)	-	scale factor R for TIME(9)
	31-40	E	R(10)	-	scale factor R for TIME(10)
	41-50	E	R(11)	-	scale factor R for TIME(11)
	51-60	E	R(12)	-	scale factor R for TIME(12)
<u>Card 4</u>	1-10	E	SIG(1)	atoms/cm	atmospheric loss parameter $\Sigma$ for TIME(1)
	11-20	E	SIG(2)	atoms/cm	atmospheric loss parameter $\Sigma$ for TIME(2)
	21-30	E	SIG(3)	atoms/cm	atmospheric loss parameter $\Sigma$ for TIME(3)
	31-40	E	SIG(4)	atoms/cm	atmospheric loss parameter $\Sigma$ for TIME(4)
	41-50	E	SIG(5)	atoms/cm	atmospheric loss parameter $\Sigma$ for TIME(5)
	51-60	E	SIG(6)	atoms/cm	atmospheric loss parameter $\Sigma$ for TIME(6)

<u>Columns</u>	<u>Mode</u>	<u>Quantity</u>	<u>Units</u>	<u>Description</u>
<u>Card 5</u>	1-10	E SIG(7)	atoms/cm	atmospheric loss parameter $\Sigma$ for TIME(7)
	11-20	E SIG(8)	atoms/cm	atmospheric loss parameter $\Sigma$ for TIME(8)
	21-30	E SIG(9)	atoms/cm	atmospheric loss parameter $\Sigma$ for TIME(9)
	31-40	E SIG(10)	atoms/cm	atmospheric loss parameter $\Sigma$ for TIME(10)
	41-50	E SIG(11)	atoms/cm	atmospheric loss parameter $\Sigma$ for TIME(11)
	51-60	E SIG(12)	atoms/cm	atmospheric loss parameter $\Sigma$ for TIME(12)
<u>Card 6</u>	1-10	E ENO	# protons/ cm <sup>3</sup>	initial proton density
	11-20	E TSUBO	months	initial time
<u>Card 7</u>	1-8	F DT1	months	first cycle integration interval
	9-16	F DT2	months	remaining cycle integration interval
	17-24	F TEND	months	limit of integration
<u>Card 8</u>	1-3	I IEST	-	initial energy level subscript*
	4-6	I IEDEL	-	energy level subscript increment*
	7-9	I IEEND	-	final energy level subscript*
<u>Card 9</u>	1-5	I IEPR	-	subscript of energy level to be printed on tape 5
	6-10	I NPRINT	-	print on tape 5 after so many increments in time
	11-15	I ICSUBO		cycle corresponding to ENO and TSUBO

\* see table of energy levels in INPUT.

2. Sample

**GENERAL PURPOSE DATA SHEET**

**INPUT - CONSERVATION EQUATION CALCULATION**

Problem Sponsor	TAPE 2	Date	SAMPLE	Page of
1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 17 16 18 20 21 22 23 24 25 26 27 28 29 30 31 32 33 34 35 36 37 38 39 40 41 42 43 44 45 46 47 48 49 50 51 52 53 54 55 56 57 58 59 60 61 62 63 64 65 66 67 68 69 70 71 72 73 74 75 76 77 78 79				
2 8 . 9 0 5 0 1 . 6 0 0 0 0 . 2 2 0 8				
0 . 1 6 7 9 E - 1 5 0 . 2 0 7 8 E - 1 5 0 . 1 6 2 8 E - 1 4 0 . 1 6 7 4 E - 1 3 0 . 2 3 7 0 E - 1 3 0 . 1 4 0 7 E - 1 3				
0 . 7 0 4 6 E - 1 4 0 . 2 2 6 7 E - 1 4 0 . 7 1 1 6 E - 1 5 0 . 3 9 3 8 E - 1 5 0 . 2 0 7 8 E - 1 5 0 . 1 6 7 9 E - 1 5				
0 . 7 2 0 8 E - 2 1 0 . 8 3 0 9 E - 2 1 0 . 3 5 7 1 E - 2 0 0 . 2 5 1 8 E - 1 9 0 . 3 4 7 9 E - 1 9 0 . 2 1 4 2 E - 1 9				
0 . 1 1 5 9 E - 1 9 0 . 4 5 8 1 E - 2 0 0 . 1 9 1 5 E - 2 0 0 . 1 2 7 3 E - 2 0 0 . 8 3 0 9 E - 2 1 0 . 7 2 0 8 E - 2 1				
0 . 0 E 0 0 . 0 E 0				
0 . 1 0 0 0 0 . 5 0 0 0 1 3 2 0 0 0 . 0				
2 2 2 1 4				
0 0 0 1				
1 5 . 9 4 5 0 1 . 2 5 0 0 0 . 2 2 4 0				
0 . 3 5 2 9 E - 1 2 0 . 3 8 8 0 E - 1 2 0 . 9 2 3 9 E - 1 2 0 . 2 2 8 9 E - 1 1 0 . 2 6 1 7 E - 1 1 0 . 2 1 4 1 E - 1 1				
0 . 1 6 3 9 E - 1 1 0 . 1 0 5 4 E - 1 1 0 . 6 6 5 3 E - 1 2 0 . 5 1 5 5 E - 1 2 0 . 3 8 8 0 E - 1 2 0 . 3 5 2 9 E - 1 2				
0 . 4 9 0 2 E - 1 8 0 . 5 4 0 1 E - 1 8 0 . 1 3 1 1 E - 1 7 0 . 3 2 9 9 E - 1 7 0 . 3 7 8 0 E - 1 7 0 . 3 0 8 2 E - 1 7				
0 . 2 3 5 0 E - 1 7 0 . 1 4 9 9 E - 1 7 0 . 9 3 7 7 E - 1 8 0 . 7 2 2 4 E - 1 8 0 . 5 4 0 1 E - 1 8 0 . 4 9 0 2 E - 1 8				
0 . 0 E 0 0 . 0 E 0				
0 . 0 1 0 0 0 . 1 0 0 0 1 3 2 0 0 0 . 0				
2 2 2 1 4		1		
4 1 0				

## H. Output

Output from this program exists in several forms. First of all there is the output from the transient steady-state solution. In this solution there are two pages of printout for each case (each B-L line considered). The first page merely lists the input with explanatory headings. The second page lists each energy level and the cycle number at which steady-state was reached for that energy level. It also gives the maximum and minimum density and flux for that cycle with the times at which they appear within the cycle. Finally it lists the ratio of the maximum to the minimum flux. If, for any energy level, the absolute value of the minimum flux becomes greater than 50,000 protons/cm<sup>2</sup> sec. mev. then the program will ask that a smaller integration interval be used and go on to the next case. On the other hand, if the ratio of the maximum to the minimum flux becomes less than 1.09 for any energy level the program will neglect all higher energy levels and pass on to the next case since there will be no solar cycle variations in higher energy levels. This output occurs on tape 3.

The time-averaged steady-state solution has the same output with the exception that on the second page for a given B-L line  $\bar{\Phi}$ ,  $\bar{\Sigma}$ ,  $dE/dx$  and  $d/dE(dE/dx)$  are printed along with the flux and density for each energy level.

Time histories for energy levels are printed on tape 5 if requested during the steady-state solution. Here time, flux and density are printed for each cycle at the intervals indicated by NPRINT. See figure 13 for an idea of the results to be expected from the transient steady-state solution. Figure 15 shows output from several time history runs.

1. Transient Steady-State Sample

\*\*\*\*\* PROGRAM INPUT \*\*\*\*\*

LATO \*\*\* = 15.9450  
L \*\*\*\*\* = 1.2500  
B \*\*\*\*\* = 0.2<4C  
NP SUB 0 = 0.  
T SUB 0 = 0.  
DELTA T1 = 0.  
DELTA T2 = 0.1UC0  
T ENC \*\* = 1320G.C

ENERGY LEVEL START = 2  
DELTA ENERGY LEVEL = 2  
ENERGY LEVEL END = 14

ENERGY LEVEL TIME HISTORY = 0

CYCLE AT T SUB ZERO \*\*\*\* = 1

PRINTING ON TAPE A-5 AFTER EVERY 1C DELTA T.

R(11) SIG(11)  
C.3529E-12 C.4902E-18  
C.3880E-12 U.3601E-18  
C.9239E-12 U.1311E-17  
C.2289E-11 U.2299E-17  
C.2611E-11 U.3780E-17  
U.2141E-11 U.3082E-17  
U.1639E-11 U.2350E-17  
C.1054E-11 U.1499E-17  
C.6653E-12 U.9377E-18  
C.5155E-12 U.7224E-18  
C.3880E-12 U.5401E-18  
C.3529E-12 U.4902E-18

INDICATES ENERGY LEVEL AT WHICH TIME HISTORY OF DENSITY AND FLUX WILL BE PRINTED ON TAPE A5.  
ZERO INDICATES NO TIME HISTORY ON TAPE A-5.

## TIME AVERAGE STEADY STATE SOLUTION FOR LAT0 = 15.9450 • L = 1.2500 • B = 0.2240

ENERGY (MEV)	PROTON- FLUX	PROTON- DENSITY	PHI BAR	SIG BAR	(DE/DX)	(DDE/DX)/DE
25.00	1.0451E-01	1.5521E-11	1.1462E 00	1.5868E-18	2.8576E-14	9.6523E-16
75.00	5.0094E-02	4.4027E-12	1.1462E 00	1.5868E-18	1.1943E-14	1.2295E-16
125.00	3.7291E-02	2.6373E-12	1.1462E 00	1.5868E-18	8.1699E-15	4.8304E-17
200.00	2.5994E-02	1.5639E-12	1.1462E 00	1.5868E-18	5.9342E-15	1.9541E-17
300.00	1.8619E-02	9.7436E-13	1.1462E 00	1.5868E-18	4.0554E-15	8.6384E-18
400.00	1.4037E-02	6.6527E-13	1.1462E 00	1.5868E-18	4.0121E-15	4.8793E-18
600.00	8.9035E-03	3.6709E-13	1.1462E 00	1.5868E-18	3.3845E-15	2.0338E-18

## 2. Tape 5 Time History Sample

\*\*\*\*\* PROGRAM INPUT \*\*\*\*\*

```
LAT0 *** = 28.0050
L *** = 1.5000
B *** = 0.2238
NP SUB S =
NP SUB C =
DELTA T1 = 0.1000
DELTA T2 = 0.5000
T END ** =132.0000
ENERGY LEVEL START = 2
DELTA ENERGY LEVEL = 2
ENERGY LEVEL END = 14
ENERGY LEVEL TIME HISTORY = 1
PRINTING ON TAPE A-5 AFTER EVERY 10000 TIME HISTORY
```

) DELTA T.

```
R(1)      SIG(1)
0.1679E-15 0.7238E-21
0.2078E-15 0.8309E-21
0.1629E-14 0.3571E-21
0.1674E-13 0.2518E-19
0.2373E-13 0.3479E-19
0.1457E-13 0.2142E-19
0.7046E-14 0.1159E-19
0.2267E-14 0.4531E-21
0.7115E-15 0.1915E-21
0.3938E-15 0.1273E-21
0.2078E-15 0.8309E-21
0.1679E-15 0.7238E-21
```

## TRANSIENT STEADY STATE SOLUTION FOR LAT0 = 28.9050 , L = 1.525 , H = 1.2238

ENERGY (MEV)	CYCLE NO.	MINIMUM- TIME (μs)	PROTON- FLUX	PROTON- DENSITY	MAXIMUM- TIME (μs)	PROTON- FLUX	PROTON- DENSITY	FLUX RATIO (MAX/MIN)
25.07	2	54.500	4.9453	7.3402E-10	22.5777	87.7665	1.3533E-39	17.7515
75.00	6	68.500	5.2627	4.6253E-10	28.3770	15.7626	1.3238E-39	2.8521
125.07	11	72.500	5.0683	3.5847E-10	29.5577	8.3703	5.8914E-10	1.5435
200.00	19	74.500	3.9392	2.3705E-10	35.3700	5.7201	3.3624E-10	1.2922
300.00	31	74.500	2.9495	1.5636E-10	37.4200	3.4172	1.7883E-10	1.1585
400.00	41	74.500	2.2517	1.3673E-10	35.0100	2.4980	1.1841E-10	1.1134
600.00	59	75.300	1.4299	5.6954E-11	37.4300	1.5293	6.3054E-11	1.0595

3. Time Averaged Steady State Sample

\*\*\*\*\* PROGRAM INPUT \*\*\*\*\*

LAI0 \*\*\* = 28.2050  
L \*\*\*\*\* = 1.6000  
B \*\*\*\*\* = 0.2208  
NP SUB 0 = 0.  
T SUB 0 = 0.  
DETA 11 = 0.1000  
DETA 12 = 0.1000  
T END \*\* = 1.3200.0  
  
ENERGY LEVEL START = 3  
DELTA :: ENERGY LEVEL = 8  
ENERGY LEVEL END = 8  
ENERGY LEVEL TIME HISTORY = 3  
  
CYCLE AT T SUB ZERO \*\*\* = 1  
PRINTING ON TAPE A-5 AFTER EVERY 50 DELTA T.  
  
R(1) SIG(1)  
0.1679E-15 0.7208E-21  
0.2074E-15 0.8309E-21  
0.1628E-14 0.3571E-20  
0.1674E-13 0.2510E-19  
0.2370E-13 0.3479E-19  
0.1407E-13 0.2144E-19  
0.7046E-14 0.1159E-19  
0.2226E-14 0.4581E-20  
0.7116E-15 0.1915E-20  
0.3936E-15 0.1275E-20  
0.2078E-15 0.8309E-21  
0.1679E-15 0.7208E-21

INDICATES ENERGY LEVEL AT WHICH TIME HISTORY OF DENSITY AND FLUX WILL BE PRINTED ON TAPE A-5.  
ZERO INDICATES NO TIME HISTORY ON TAPE A-5.

TIME HISTORY OF DENSITY AND FLUX FOR ENERGY = 200.0 , LATO = 28.905C , L = 1.0000 , B = 0.2208							
CYCLE NO. =	1	TIME	FLUX	DENSITY	TIME	FLUX	DENSITY
1	5.000	0.0849	5.1059E-12	1.0.000	0.1695	1.0200E-11	1.5.000
	20.000	0.3372	2.0286E-11	25.000	0.4187	2.5191E-11	30.000
	35.000	3.2645E-11	40.000	0.6042	3.6359E-11	45.000	
	50.000	0.6117	3.8011E-11	55.000	0.6901	4.1517E-11	60.000
	65.000	0.7672	4.6161E-11	70.000	0.8157	4.9078E-11	75.000
	80.000	0.9306	5.5990E-11	85.000	0.9960	5.9921E-11	90.000
	95.000	1.1388	6.5616E-11	1.10.000	1.2145	7.3072E-11	1.105.000
	110.000	1.3681	8.2313E-11	115.000	1.4466	8.7032E-11	120.000
	125.000	1.6076	9.4672E-11	130.000	1.6703	1.0170E-10	132.000
CYCLE NO. =	2	5.000	1.8077	1.0676E-10	10.000	1.8792	1.1379E-10
	20.000	2.0545	1.2361E-10	25.000	2.1290	1.2809E-10	30.000
	35.000	2.2068	1.3277E-10	40.000	2.1675	1.3044E-10	45.000
	50.000	2.0335	1.2234E-10	55.000	1.9827	1.1922E-10	60.000
	65.000	1.9543	1.1758E-10	70.000	1.9700	1.1852E-10	75.000
	80.000	2.0469	1.2315E-10	85.000	2.1032	1.2634E-10	90.000
	95.000	2.2369	1.3458E-10	100.000	2.3103	1.3900E-10	105.000
	110.000	2.4667	1.4805E-10	115.000	2.5380	1.5270E-10	120.000
	125.000	2.6975	1.6229E-10	130.000	2.7795	1.6723E-10	132.000
CYCLE NO. =	3	5.000	2.8960	1.7424E-10	10.000	2.9789	1.7924E-10
	20.000	3.1393	1.8881E-10	25.000	3.2094	1.9309E-10	30.000
	35.000	3.2476	1.9239E-10	40.000	3.4551	1.8984E-10	45.000
	50.000	2.9001	1.7448E-10	55.000	2.7992	1.6848E-10	60.000
	65.000	2.7042	1.6227E-10	70.000	2.6992	1.6240E-10	75.000
	80.000	2.7521	1.6538E-10	85.000	2.8627	1.6866E-10	90.000
	95.000	2.9306	1.7632E-10	100.000	3.0026	1.8056E-10	105.000
	110.000	3.1909	1.8957E-10	115.000	3.2275	1.9418E-10	120.000
	125.000	3.3860	2.0372E-10	130.000	3.4676	2.0863E-10	132.000
CYCLE NO. =	4	6.000	3.5835	2.1566E-10	10.000	3.6659	2.2056E-10
	20.000	3.8446	2.3011E-10	25.000	3.6917	2.3416E-10	30.000
	35.000	3.9051	2.3495E-10	40.000	3.7789	2.2736E-10	45.000
	50.000	3.4476	2.0742E-10	55.000	3.1511	1.9945E-10	60.000
	65.000	3.1976	1.9120E-10	70.000	3.1598	1.9011E-10	75.000
	80.000	3.1976	1.9239E-10	85.000	3.2445	1.9521E-10	90.000
	95.000	3.3869	2.0269E-10	100.000	3.4399	2.0696E-10	105.000
	110.000	3.5869	2.1580E-10	115.000	3.6631	2.2039E-10	120.000
	125.000	3.8209	2.2398E-10	130.000	3.9023	2.3478E-10	132.000
CYCLE NO. =	5	5.000	4.0178	2.4173E-10	10.000	4.1000	2.4667E-10
	20.000	4.2275	2.5612E-10	25.000	4.2321	2.6916E-10	30.000
	35.000	4.3204	2.5994E-10	40.000	4.1730	2.5110E-10	45.000
	50.000	3.7934	2.2823E-10	55.000	3.6416	2.1096E-10	60.000
	65.000	3.4772	2.0922E-10	70.000	3.4508	2.0762E-10	75.000
	80.000	3.4790	2.0931E-10	85.000	3.5237	2.1200E-10	90.000
	95.000	3.6457	2.1934E-10	100.000	3.7161	2.2558E-10	105.000
	110.000	3.8623	2.3223E-10	115.000	3.8382	2.3694E-10	120.000
	125.000	4.0957	2.4041E-10	130.000	4.1769	2.5130E-10	132.000
CYCLE NO. =	6	5.000	4.2922	2.5624E-10	10.000	4.3742	2.6317E-10
	20.000	4.5310	2.7261E-10	25.000	4.5954	2.7668E-10	30.000
	35.000	4.5828	2.7522E-10	40.000	4.4220	2.6655E-10	45.000
	50.000	4.0118	2.4137E-10	55.000	3.9468	2.3144E-10	60.000
	65.000	3.6662	2.2053E-10	70.000	3.6346	2.1668E-10	75.000
	80.000	3.6668	2.2051E-10	85.000	3.7000	2.2261E-10	90.000
	95.000	3.8206	2.2986E-10	100.000	3.8906	2.3696E-10	105.000
	110.000	4.0363	2.4284E-10	115.000	4.1120	2.4740E-10	120.000
	125.000	4.2693	2.5686E-10	130.000	4.3503	2.6173E-10	132.000

## I. Running Time

Transient steady-state solutions where DT1 = .5 and DT2 = 1.0 will cover eleven cycles per minute. See figure 14 for an idea of how many cycles are necessary to reach steady-state for various B's at an L of 1.25 earth radii.

Runs requesting a time history print on tape 5 take about twice as long.

Time averaged steady state solutions take about a quarter of a minute for each B-L line.

## VIII. STEADY-STATE CALCULATION

### A. Introduction

This program evaluates the solar maximum and solar minimum steady state conditions of the conservation equation. That is, with  $dN_p/dt$  set equal to zero, the flux and density are studied at solar minimum (time = 0.0 years, see Figure 1) and solar maximum (time = 4.0 years). The mean lifetimes of the protons are also calculated as well as  $dE/dx$ ,  $d/dE(dE/dx)$ , the three coefficients of the conservation equation  $C_0$ ,  $C_1$  and  $C_2$  and the source and loss terms. This is all printed together with the appropriate  $\Sigma$  for a given  $B$ ,  $L$ ,  $\lambda$  and energy level. All 15 energy levels of the preceding program are evaluated for each  $B$  and  $L$ .

### B. Equations

The equations used in this program are listed below:

$$\text{SOURCE} = XX = A_0 \Phi / L^2 E^{B_0} \cos^4 \lambda_0$$

$$\text{LOSS} = YY = \frac{A_1 N_p}{E^{B_1}} \left( \frac{dE}{dx} \right) + A_2 N_p E^{B_2} \frac{d}{dE} \left( \frac{dE}{dx} \right) + A_2 N_p E^{B_2} \Sigma$$

$$\text{MEAN LIFETIME} = TAU = N_p / XX$$

$$\text{FLUX} = \text{FLUXP} = N_p (\text{EXT}) E^{B_2} C = N_p \beta C = N_p V$$

$$\text{DENSITY} = EN1 = \frac{A_0 \Phi}{L^2 E^{B_0} \cos^4 \lambda_0 \left[ \frac{A_1}{E^{B_1}} \left( \frac{dE}{dx} \right) + A_2 E^{B_2} \left( \frac{d}{dE} \left( \frac{dE}{dx} \right) + \Sigma \right) \right]}$$

where  $C$  = speed of light

$\Phi$  = PREL = relative neutron source strength

$\Sigma$  = SIG = atmospheric loss parameter

$A_0, \dots, A_2$  = high or low energy conservation equation coefficients depending upon whether  $E > 80$  Mev. or  $E \leq 80$  Mev respectively

$B_0, \dots, B_2$  = high or low energy conservation equation coefficients depending upon whether  $E > 80$  Mev. or  $E \leq 80$  Mev. respectively

$\lambda_0$  = Mirror latitude

$N_p$  = proton number density

$v$  = neutron velocity

$\beta$  =  $v/C$

$$EXT = \beta/E^{B2}$$

### C. Mnemonics

<u>Quantity</u>	<u>Description</u>			<u>Units</u>
TIME(J)	abscissa of time in increments of years for 12 years			years
ELOSS(J)	$dE/dX$ corresponding to E(J) (see Figure 11)			Mev./cm.
E(J)	energy corresponding to ELOSS(J) (see Figure 11)			Mev
AL0	$A_0$ for $E \leq 80$ Mev. (see preceding page)			# protons cm. sec. Mev.
AL1	$A_1$ "	"	"	cm/sec
AL2	$A_2$ "	"	"	cm./Mev <sup>2</sup> sec.
AH0	$A_0$ for $E > 80$ Mev. (see preceding page)			# protons cm. sec. Mev.
AH1	$A_1$ "	"	"	cm. sec.
AH2	$A_2$ "	"	"	cm/Mev <sup>2</sup> sec.

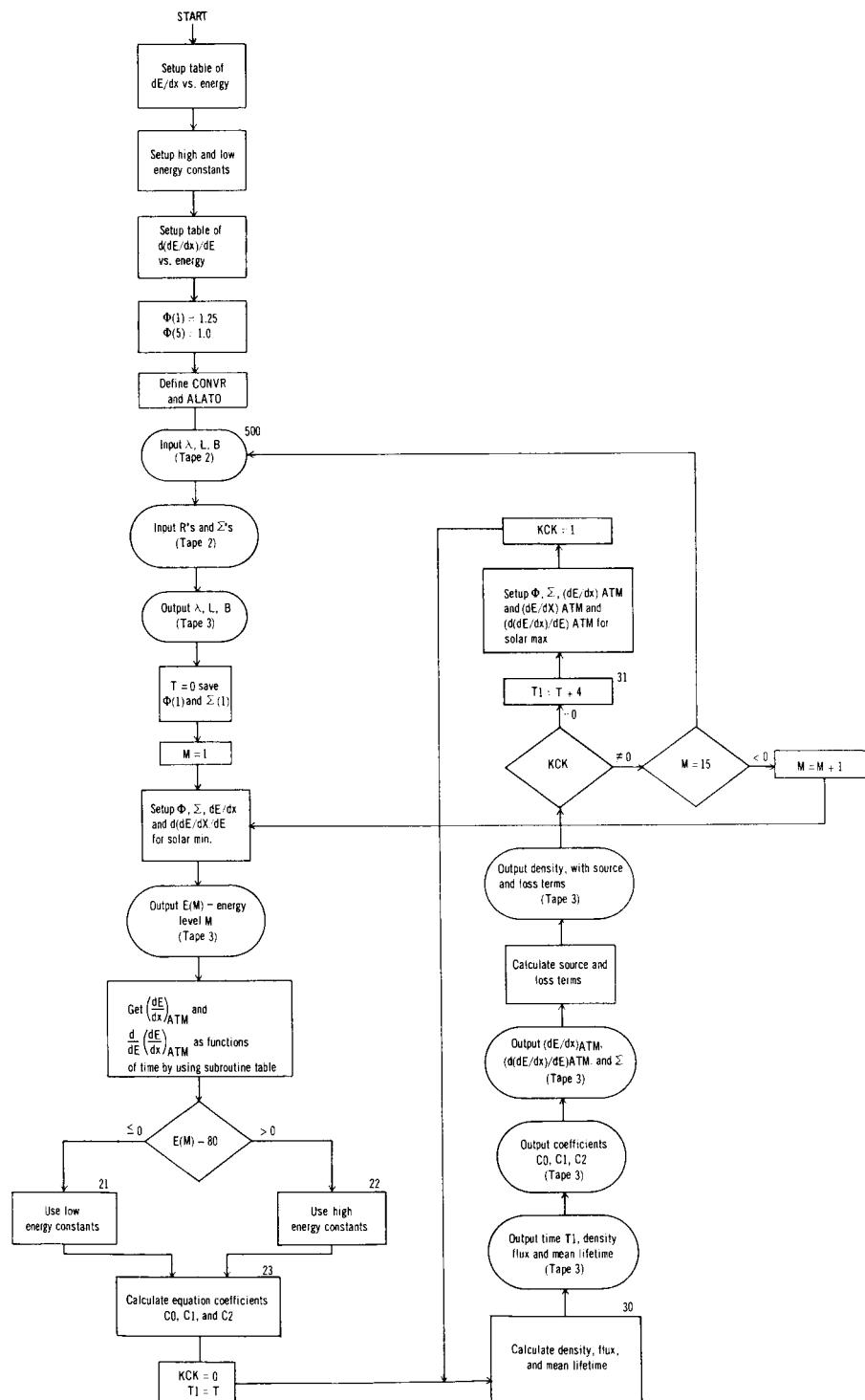
<u>Quantity</u>	<u>Description</u>	<u>Units</u>
BL0	$B_0$ for $E \leq 80$ Mev. (see preceding page)	-
BL1	$B_1$ " " "	-
BL2	$B_2$ " " "	-
BH0	$B_0$ for $E > 80$ Mev. (see preceding page)	-
BH1	$B_1$ " " "	-
BH2	$B_2$ " " "	-
DELOSS(J)	$d(dE/dX)/dE$ corresponding to DE(J) (see Figure 12)	$\text{cm.}^{-1}$
DE(J)	energy corresponding to DELOSS(J) (see Figure 12)	Mev.
PREL(J)	$\Phi$ for TIME(J) (see Figure 11 and page 167)	-
CONVR	conversion factor - degrees to radians	-
ALAT	mirror latitude $\lambda_0$	degrees
EL	magnetic field line L	earth radii
B	magnetic induction B	gauss
R(J)	atmospheric scale factor R for TIME(J)	-
SIG(J)	atmospheric loss parameter $\Sigma$ for TIME(J)	atoms/cm
ALATO	ALAT in radians	radians
SVPR	temporary storage of PREL(1)	-
SVSG	temporary storage of SIG(1)	atoms/cm
t	time	years

<u>Quantity</u>	<u>Description</u>	<u>Units</u>
M	energy level subscript	-
ENER	energy level E(M)	Mev.
ALOSS	dE/dX for E(M)	Mev/cm
X(k)	temporary storage of DE(k)	Mev.
Y(k)	temporary storage of DELOSS(k)	cm <sup>-1</sup>
EANS	d(dE/dX)/dE for E(M)	cm <sup>-1</sup>
ALOSSA(J)	(dE/dX) X R(J) for E(M)	Mev/cm
DLOSSA(J)	(d(dE/dX)/dE) X R(J) for E(M)	cm <sup>-1</sup>
A0	temporary storage of AL0 or AH0	# protons cm. sec. Mev.
A1	temporary storage of AL1 or AH1	cm./sec.
A2	temporary storage of AL2 or AH2	cm/Mev <sup>2</sup> sec.
B0	temporary storage of BL0 or BH0	-
B1	temporary storage of BL1 or BH1	-
B2	temporary storage of BL2 or BH2	-
EXT	(see page 168)	-
C0	conservation equation coefficient $c_0$ where $c_0 = A_0 / L^2 E^{B_0} \cos^4 \lambda_0$	# protons cm <sup>2</sup> sec. Mev.
C1	conservation equation coefficient $c_1$ where $c_1 = A_1 / E^{B_1}$	cm/sec. Mev.
C2	conservation equation coefficient $c_2$ where $c_2 = A_2 E^{B_2}$	cm/sec. Mev.

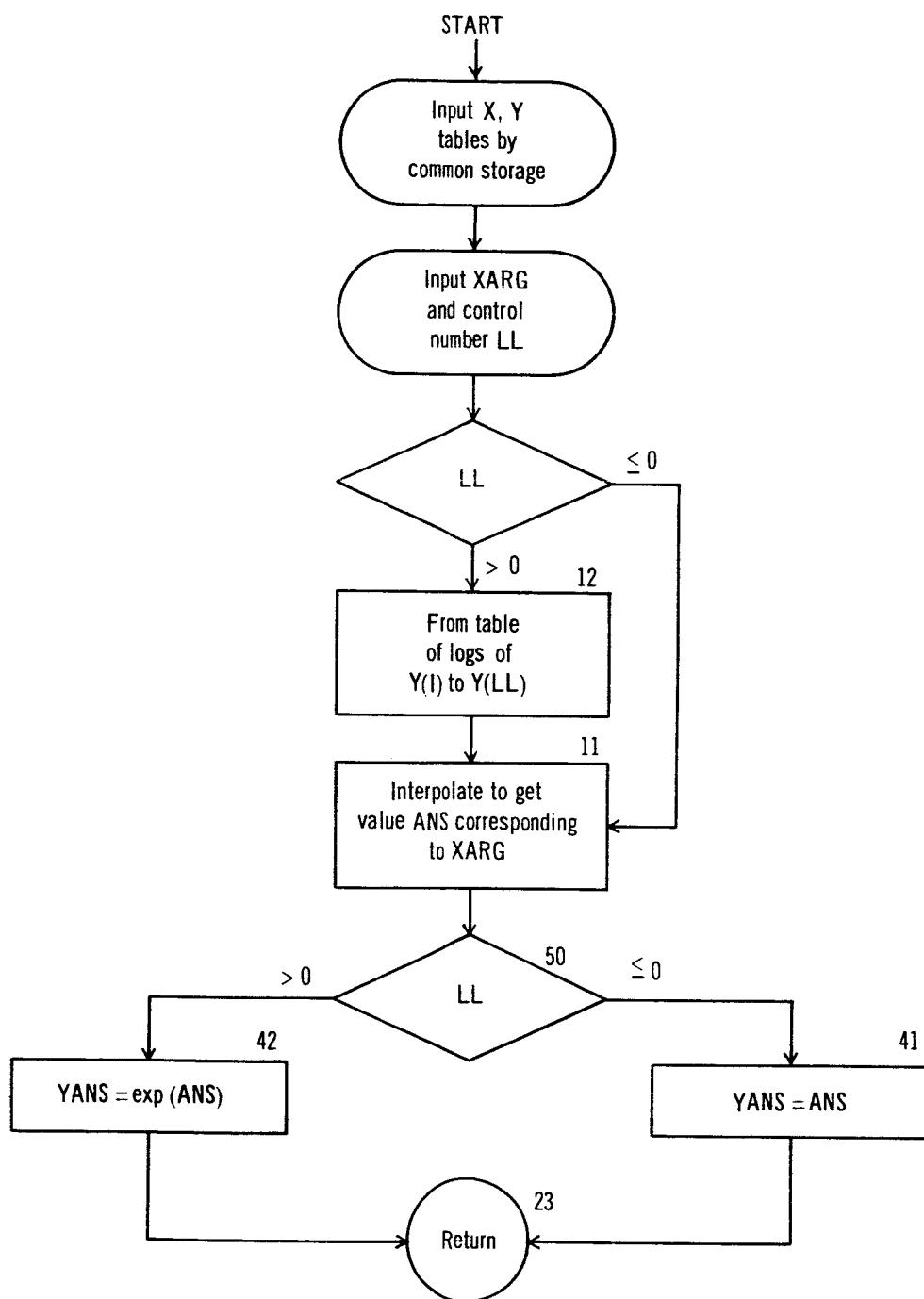
<u>Quantity</u>	<u>Description</u>	<u>Units</u>
KCK	counter to determine if solar maximum or solar minimum is being evaluated	-
T1	particular time under consideration	years
EN1	proton density	# protons Mev. cm
FLUXP	proton flux	# protons cm <sup>2</sup> sec. Mev.
TAU	mean proton lifetime	sec
XX	conservation equation source term (see page 167)	# protons cm <sup>2</sup> sec.
YY	conservation equation loss term (see page 167)	# protons cm <sup>2</sup> sec.

## D. Flow Charts

### 1. Main Program



## 2. Subroutine Table



## E. Fortran Listing

STACY

10/01/64

```

C      STEACY STATE
C      DIMENSION L(15),ELCSS(15),TIME(12),R(12),DELCSS(15),RL(15),PRLL(5)
1,ALUSSA(12),DLUSSA(12),X(15),Y(15),SIG(12)
COMMON XY
1      FORMAT(3E8.4)
2      FORMAT(6E0.4)
3      FORMAT(1F15.3,1E20.5,1E20.5)
4      FORMAT(1I1,2X,5HLATG=1F8.3,2X,2HL=1F6.3,3X,2hd=F7.4)
5      FORMAT(1CX,7HENERGY=1F8.2,3HEV)
6      FORMAT(9X,4+TIME,15X,4HN(t),17X,4FFLUX,1LA,13HFAN LIFETIME)
7      FORMAT(5,3HC1-E12.5,X,3HC1-E12.5,X,3FC=12.5)
8      FORMAT(1A,7HLOSSA=E12.5,1X,7HDLCSA=E12.5,1X,7HSIG=E12.5)
9      FORMAT(3,5HN(E)=t12.5,1X,7HSOURCE=E12.5,X,5HLCSS=E12.5)
TIME(1)=0.0
DO 11 J=1,11
TIME(J+1)=TIME(J)+12.0
11 CONTINUE
ELoss(1)=5.39251E-2
ELoss(2)=2.5732E-2
ELoss(3)=1.4755E-2
ELoss(4)=1.0754E-2
ELoss(5)=8.6531E-3
ELoss(6)=7.3567E-3
ELoss(7)=6.4720E-3
ELoss(8)=5.3435E-3
ELoss(9)=4.6543E-3
ELoss(10)=4.1916E-3
ELoss(11)=3.8607E-3
ELoss(12)=3.6121E-3
ELoss(13)=3.2701E-3
ELoss(14)=3.0476E-3
ELoss(15)=2.8542E-3
E(1)=10.
E(2)=25.
E(3)=50.
E(4)=75.
E(5)=100.
E(6)=125.
E(7)=150.
E(8)=200.
E(9)=250.
E(10)=300.
E(11)=350.
E(12)=400.
E(13)=500.
E(14)=600.
E(15)=700.
IC=-iu MEV
AL0=          2.964F-13
AL1=          3.463Cv
AL2=          7.255t+C
BL0=2.3C9
BL1=5.23
BL2=4.17
BL3=1.00 MEV
C

```

```

AH0=      3.4792E-13
AH1=      4.671E+0
AH2=      1.343E+9
BH0=2.349
BH1=.656
BH2=.344
Dt(1)=10.
Dt(2)=10.5
Dt(3)=16.5
Dt(4)=21.5
Dt(5)=25.5
Dt(6)=32.5
Dt(7)=42.5
Dt(8)=52.5
Dt(9)=62.5
Dt(10)=700.
Dt(11)=312.5
Dt(12)=412.5
Dt(13)=525.5
Dt(14)=625.5
Dt(15)=700.

DELOSS(1)=-.4CE-2
DELOSS(2)=-.3985E-2
DELOSS(3)=-.1770E-2
DELOSS(4)=-.1C51E-3
DELOSS(5)=-.2173E-3
DELOSS(6)=-.1172E-3
DELOSS(7)=-.743E-4
DELOSS(8)=-.354E-4
DELOSS(9)=-.153E-4
DELOSS(10)=-.101E-4
DELOSS(11)=-.713E-5
DELOSS(12)=-.410E-5
DELOSS(13)=-.244E-5
DELOSS(14)=-.166E-5
DELOSS(15)=-.131E-5
PREL(1)=1.2,
PREL(2)=1.0

CLNR=1/57.29577
READ INPUT TAPE 2,1,ALAT,EL,B
READ INPUT TAPE 2,2,R(1),R(2),R(3),R(4),R(5),R(6)
READ INPUT TAPE 2,2,R(7),R(8),R(9),R(10),R(11),R(12)
READ INPUT TAPE 2,2,SIG(1),SIG(2),SIG(3),SIG(4),SIG(5),SIG(6)
READ INPUT TAPE 2,2,SIG(7),SIG(8),SIG(9),SIG(10),SIG(11),SIG(12)
WRITE OUTPUT TAPE 3,4,ALAT,EL,B
ALAT=ALAT*CLNR
SVP=R*PREL(1)
SVSIG(SIG(1))
T=0.0
DU .3CU M=1,15
ENER=E(M)
WRITE OUTPUT TAPE 3,5,ENER
WRITE OUTPUT TAPE 3,6
ALUSS=CLLOSS(M)
DU 201 K=1,15
X(K)=U(K)

```

Y(K)=ALLOSSA(K)  
CONTINUE  
CALL TABL..(C1,KA,FANS,1D)  
DC 20,J=1,12  
ALLOSSA(J)=K(J)\*ALCSS  
BLOSSA(J)=K(J)\*EANS  
20 CONTINUE  
NEW F-AZ (COMPLEXATES AND G(EVEX) ENERGY AND T  
FUNCTIONS  
C UP-TIME FOR A GIVE ENERGY AND G(EVEX)/G(EV) MUS AS FUNCTIONS  
TENSORS  
21 AG=ALC  
A1=AL1  
A2=AL2  
J0=HLC  
H1=BL1  
H2=BL2  
EXT=.0454  
GL 1C 23  
22 AG=AH0  
A1=AH1  
A2=AH2  
B0=BH0  
B1=BH1  
B2=BH2  
EXT=.0556  
23 C0=A0/(GL\*Z\*ENCL\*\*RC\*CCSF(ALATU)\*\*4)  
C1=AL1/(ENCR\*\*EL)  
C2=A2\*LNEK\*\*EL2  
KCK=0  
T1=T  
EN1=C0\*PREL(1)/(C1\*ALCSSA(1)+C2\*BLOSSA(1)+C2\*SIG(1))  
FLUXP=EN1\*ENCR\*EL(R2\*975E1C  
TAU=EN1/(C0\*PREL(1)\*2.592E6)  
WRITE OUTPUT TAPE 3,3,T1,A1,FLUXP,IAU  
WRITE OUTPUT TAPE 3,7,CC,C1,C2  
WRITE OUTPUT TAPE 3,8,BLOSSA(1),SIG(1)  
XA=CO\*PAUL(1)  
YY=C1\*BLOSSA(1)+C2\*BLOSSA(1)+C2\*SIG(1)  
WRITE OUTPUT TAPE 3,S,EN1,XX,YY  
IF(KCK) 3C1,B1,3C1  
24 T1=T+4.  
ALLOSSA(1)=ALCSSA(1)  
BLOSSA(1)=BLOSSA(1)  
PREL(1)=PREL(5)  
SIG(1)=SIG(5)  
KCK=1  
WRITE OUTPUT TAPE 3,6  
GC TO 30  
3C1 PREL(1)=SYPR  
SIG(1)=SYSG  
CONTINUE  
GC TO 3C0  
END(1,C,O,C,G,C,C,C,C,C,C,C)

## STORAGE NOT USEC BY PROGRAM

	DEC	UCI	DEC	CCT
811	01461			

	DEC	OCT	DEC	CCT
	32331	77423		

## STORAGE LOCATIONS FOR VARIABLES APPEARING IN COMMON STATEMENTS

	DEC	OCT	DEC	CCT
X	32561	77461	Y	32546

## STORAGE LOCATIONS FOR VARIABLES APPEARING IN DIMENSION AND EQUIVALENCE STATEMENTS

	DEC	UCI	DEC	CCT	DEC	CCT	DEC	CCT			
ALOSSA	727	01327	LFLSS	762	C1372	E	747	01353	CLOSSA	715	C1313
F	816	01460	PREL	732	C1334	R	774	01406	SIG	703	C1277

## STORAGE LOCATIONS FOR VARIABLES NOT APPEARING IN COMMON, DIMENSION, OR EQUIVALENCE STATEMENT

	DEC	UCI	DEC	CCT	DEC	CCT	DEC	CCT	DEC	CCT	
AU	691	C1263	A1	690	01262	A2	689	01261	AHO	688	C126C
AH2	686	01226	ALO	685	01255	ALL	684	01254	AL2	683	C1253
ALAT	681	01251	ALUSS	680	0125C	B0	679	01247	B1	678	C1246
BH0	676	01244	BH1	675	C1243	BH2	674	01242	BLO	673	C1241
BL2	671	C1237	B	670	01236	CO	669	01235	C1	668	01234
CNVRK	666	01232	CANS	665	C1231	EL	664	01230	EN1	663	01227
EXT	661	C1225	FLUXP	660	01224	KCK	659	01223	SVR	658	C1222
T1	656	01220	TAU	655	01217	T	654	01216	XX	653	C1215

## SYMBOLS AND LOCATIONS FOR SOURCE PROGRAM FORMAT STATEMENTS

	EFN	LCC	EFN	LOC	EFN	LCC	EFN	LOC
811	1	01206	812	2	01204	813	3	01202
816	6	01160	817	7	01147	818	6	01137

## LOCATIONS FOR OTHER SYMBOLS NOT APPEARING IN SOURCE PROGRAM

	DEC	UCI	DEC	CCT	DEC	OCT	DEC	OCT
1)	647	01271	21	496	0C76	3)	502	CC766

## LOCATIONS OF NAMES IN TRANSFER VECTOR

	DEC	CCT	DEC	OCT	DEC	CCT	DEC	CCT
COS	6	UCF	EXP(3)	7	00007	TABLE	111	00432
(RTN)	2	CCC06	(STH)	3	CCC03	(FILE)	145	00431

## ENTRY POINTS TO SUBROUTINES NOT OUTPUT FROM LIBRARY

	CCS	EXP(3)	TABLE	(FILE)	(FP1)	(RTN)	(STL)	(TSR)
--	-----	--------	-------	--------	-------	-------	-------	-------

## EXTERNAL FORMULA NUMBERS WITH CORRESPONDING INTERNAL FORMULA NUMBERS AND OCTAL LOCATIONS

	EFN	LCC	EFN	LCC	EFN	LOC	EFN	LCC
11	16	C0023	500	52	C0234	2C1	111	00432
22	133	C0477	23	140	C0515	30	145	00431
300	164	C0755					155	00727

```

C   SUBROUTINE TO INTERPOLATE A GIVEN TABLE
      SUBROUTINE TABLE(XA,YA,NLL)
      DIMENSION X(15),Y(15)
      COMMON X,Y
      IF(NLL)11,11,12
12    DC 10 K=1,LL
      A=Y(K)
      Y(K)=JGF(A)
10    CONTINUE
11    DO 20 J=1,15
      IF(X(J)-XARG)>20,21,22
21    ANS=Y(J)
22    GO TO 50
22    H1=X(J)
      Y1=Y(J)
      H0=X(J-1)
      Y0=Y(J-1)
      ANS=1-(Y1-YC)*(H1-XARG)/(H1-H0)
      GO TO 20
20    CONTINUE
      50 IF(NLL)41,41,42
41    YANS=ANS
      GO TO 23
42    YANS=EXP(ANS)
23    RETURN
      END(1,0,0,0,0,0,0,C,0,C,C,0,0)

```

## STORAGE AND USE BY PROGRAM

	DEC	LLC	LOC	DEC	LOC	DEC	LOC	DEC	LOC
	110	C016	32531 77423						
<b>STORAGE LOCATIONS FOR VARIABLES APPEARING IN COMMON STATEMENTS</b>									
X	DEC	LLC	DEC	DEC	OCT	DEC	OCT	DEC	OCT
X 32561 77461			Y 32546 7745						
<b>STORAGE LOCATIONS FOR VARIABLES NOT APPEARING IN COMMON, DIMENSION, OR EQUIVALENCE STATEMENT</b>									
ANS	DEC	LLC	DEC	DEC	OCT	DEC	OCT	DEC	OCT
109 CC155		A	1C8 C0154		40 1C7 00153	H1	106 C0152	J	105 C0151
Y0	104	C0150	Y1	1C3 C0147					
<b>LOCATIONS FOR OTHER SYMBOLS NOT APPEARING IN SOURCE PROGRAM</b>									
I)	DEC	LLC	DEC	DEC	OCT	DEC	OCT	DEC	OCT
99 CC143		21	92 00134		61	93 C0135	C14	102 C0146	D14CA
E)7	43	CC060	E)C	82	00122				
<b>LOCATIONS OF NAMES IN TRANSFER VECTOR</b>									
EXP	DEC	LLC	LCG	DEC	OCT	DEC	OCT	DEC	OCT
		I	0 CCCCC						
<b>ENTRY POINTS TO SUBROUTINES NOT OUTPUT FROM LIBRARY</b>									
EXP		LLC							
<b>EXTERNAL FORMULA NUMBERS WITH CORRESPONDING INTERNAL FORMULA NUMBERS AND OCTAL LOCATIONS</b>									
EFN	IFN	LLC	IFN	IFN	LLC	IFN	LLC	IFN	LOC
12	10	5 C0043	11	1C C0145	21	12 C0053	22	14 C0061	
c	5C	21 C0114	41	2C C0117	42	24 C0123	23	25 C0130	

## F. Input

Input to this program occurs on logical tape 2 and consists of B, L,  $\lambda$ , R(1), ..., R(12)  $\Sigma$  (1), ...,  $\Sigma$  (12) for each case under consideration. As with the conservation equation calculation the B-L- $\lambda$  card is followed by two R cards which are followed in turn by two  $\Sigma$  cards. The control cards are left out of this program since there is only one method of computation available here.

### 1. Input Card Description

	<u>Columns</u>	<u>Mode</u>	<u>Quantity</u>	<u>Units</u>	<u>Description</u>
B-L- $\lambda$ Card	1-8 9-16 17-24	F F F	ALAT EL B	degrees earth radii gauss	latitude magnetic field line magnetic induction
First R Card	1-10 11-20 21-30 31-40 41-50 51-60	E E E E E E	R(1) R(2) R(3) R(4) R(5) R(6)	- - - - - -	scale factor R for TIME(1) scale factor R for TIME(2) scale factor R for TIME(3) scale factor R for TIME(4) scale factor R for TIME(5) scale factor R for TIME(6)
Second R Card	1-10 11-20 21-30 31-40 41-50 51-60	E E E E E E	R(7) R(8) R(9) R(10) R(11) R(12)	- - - - - -	scale factor R for TIME(7) scale factor R for TIME(8) scale factor R for TIME(9) scale factor R for TIME(10) scale factor R for TIME(11) scale factor R for TIME(12)
First $\Sigma$ Card	1-10 11-20 21-30 31-40	E E E E	SIG(1) SIG(2) SIG(3) SIG(4)	atoms/cm atoms/cm atoms/cm atoms/cm	atmospheric loss parameter $\Sigma$ for TIME(1) atmospheric loss parameter $\Sigma$ for TIME(2) atmospheric loss parameter $\Sigma$ for TIME(3) atmospheric loss parameter $\Sigma$ for TIME(4)

<u>Columns</u>	<u>Mode</u>	<u>Quantity</u>	<u>Units</u>	<u>Description</u>
41-50	E	SIG(5)	atoms/cm	atmospheric loss parameter $\Sigma$ for TIME(5)
51-60	E	SIG(6)	atoms/cm	atmospheric loss parameter $\Sigma$ for TIME(6)

<u>Second <math>\Sigma</math> Card</u>	<u>1-10</u>	<u>E</u>	<u>SIG(7)</u>	<u>atoms/cm</u>	<u>atmospheric loss parameter <math>\Sigma</math> for TIME(7)</u>
	11-20	E	SIG(8)	atoms/cm	atmospheric loss parameter $\Sigma$ for TIME(8)
	21-30	E	SIG(9)	atoms/cm	atmospheric loss parameter $\Sigma$ for TIME(9)
	31-40	E	SIG(10)	atoms/cm	atmospheric loss parameter $\Sigma$ for TIME(10)
	41-50	E	SIG(11)	atoms/cm	atmospheric loss parameter $\Sigma$ for TIME(11)
	51-60	E	SIG(12)	atoms/cm	atmospheric loss parameter $\Sigma$ for TIME(12)

2. Sample

**GENERAL PURPOSE DATA SHEET**

Problem Sponsor	INPUT - STEADY STATE TAPE 2		Date	SAMPLE	Page	of
1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 31 32 33 34 35 36 37 38 39 40						
6 . 9 7 3 0 1 . 1 4 2 0 0 . 2 2 3 9						
0 . 2 7 8 5 E - 1 1 0 . 2 9 8 6 E - 1 1 0 . 5 6 3 6 E - 1 1 0 . 1 0 9 6 E - 1 0 0 . 1 2 0 8 E - 1 0 0 . 1 0 4 3 E - 1 0						
0 . 8 5 7 7 E - 1 1 0 . 6 2 0 1 E - 1 1 0 . 4 4 3 8 E - 1 1 0 . 3 6 8 1 E - 1 1 0 . 2 9 8 6 E - 1 1 0 . 2 7 8 5 E - 1 1						
0 . 3 9 8 4 E - 1 7 0 . 4 2 7 8 E - 1 7 0 . 8 1 6 0 E - 1 7 0 . 1 5 9 9 E - 1 6 0 . 1 7 6 5 E - 1 6 0 . 1 5 2 2 E - 1 6						
0 . 1 2 4 9 E - 1 6 0 . 8 9 9 1 E - 1 7 0 . 6 4 0 4 E - 1 7 0 . 5 2 9 3 E - 1 7 0 . 4 2 7 8 E - 1 7 0 . 3 9 8 4 E - 1 7						
4 . 9 7 3 0 1 . 1 4 2 0 0 . 2 1 6 8						
0 . 3 7 4 4 E - 1 3 0 . 4 2 4 5 E - 1 3 0 . 1 3 6 8 E - 1 2 0 . 4 9 7 7 E - 1 2 0 . 6 0 6 5 E - 1 2 0 . 4 5 0 9 E - 1 2						
0 . 3 0 5 9 E - 1 2 0 . 1 6 3 8 E - 1 2 0 . 8 7 1 0 E - 1 3 0 . 6 1 9 0 E - 1 3 0 . 4 2 4 5 E - 1 3 0 . 3 7 4 4 E - 1 3						
0 . 5 6 3 3 E - 1 9 0 . 6 3 3 9 E - 1 9 0 . 1 9 3 6 E - 1 8 0 . 6 9 0 7 E - 1 8 0 . 8 4 0 6 E - 1 8 0 . 6 2 6 0 E - 1 8						
0 . 4 2 6 1 E - 1 8 0 . 2 3 0 6 E - 1 8 0 . 1 2 5 0 E - 1 8 0 . 9 0 3 8 E - 1 9 0 . 6 3 3 9 E - 1 9 0 . 5 6 3 3 E - 1 9						
2 . 9 7 3 0 1 . 1 4 2 0 0 . 2 1 2 1						
0 . 2 0 1 6 E - 1 4 0 . 2 3 3 1 E - 1 4 0 . 9 4 4 6 E - 1 4 0 . 4 9 5 3 E - 1 3 0 . 6 4 3 5 E - 1 3 0 . 4 3 4 5 E - 1 3						
0 . 2 6 1 9 E - 1 3 0 . 1 1 8 2 E - 1 3 0 . 5 3 8 8 E - 1 4 0 . 3 6 0 3 E - 1 4 0 . 2 3 3 1 E - 1 4 0 . 2 0 1 6 E - 1 4						
0 . 7 8 7 8 E - 2 0 0 . 8 6 9 7 E - 2 0 0 . 2 3 0 4 E - 1 9 0 . 8 2 4 6 E - 1 9 0 . 1 0 2 3 E - 1 8 0 . 7 4 0 4 E - 1 9						
0 . 4 9 3 8 E - 1 9 0 . 2 7 0 4 E - 1 9 0 . 1 5 4 4 E - 1 9 0 . 1 1 7 0 E - 1 9 0 . 8 6 9 7 E - 2 0 0 . 7 8 7 8 E - 2 0						
0 . 9 7 3 0 1 . 1 4 2 0 0 . 2 0 9 9						
0 . 5 7 8 9 E - 1 5 0 . 6 4 5 0 E - 1 5 0 . 1 9 4 3 E - 1 4 0 . 9 4 7 6 E - 1 4 0 . 1 2 5 3 E - 1 3 0 . 8 2 4 1 E - 1 4						
0 . 4 9 1 5 E - 1 4 0 . 2 3 4 2 E - 1 4 0 . 1 2 1 7 E - 1 4 0 . 8 9 2 4 E - 1 5 0 . 6 4 5 0 E - 1 5 0 . 5 7 8 9 E - 1 5						
0 . 3 9 2 7 E - 2 0 0 . 4 3 0 4 E - 2 0 0 . 1 0 1 0 E - 1 9 0 . 2 7 5 4 E - 1 9 0 . 3 2 5 5 E - 1 9 0 . 2 5 3 3 E - 1 9						
0 . 1 8 5 1 E - 1 9 0 . 1 1 5 2 E - 1 9 0 . 7 2 7 3 E - 2 0 0 . 5 6 6 8 E - 2 0 0 . 4 3 0 4 E - 2 0 0 . 3 9 2 7 E - 2 0						

## G. Output

Output for this program occurs on tape 3. Time, density, flux, mean lifetime,  $dE/dX$ ,  $d(dE/dX)/dE$ ,  $\Sigma$ , source and loss are all printed for each energy level at a given B, L and latitude. The headings are listed below with explanations and dimensions:

TIME - time - years

N(E) - density - # protons/cm<sup>3</sup> Mev.

FLUX - flux - # protons/cm<sup>2</sup> sec. Mev.

MEAN LIFETIME - proton mean lifetime - sec.

C0 - C<sub>0</sub> (see MNEMONICS) - # protons/cm<sup>3</sup> sec. Mev.

C1 - C<sub>1</sub> (see MNEMONICS) - cm/sec. Mev.

C2 - C<sub>2</sub> (see MNEMONICS) - cm/sec. Mev.

ALOSSA - (dE/dX) ATMOS - Mev./cm.

DLOSSA - (d(dE/dX)/dE) ATMOS - cm<sup>-1</sup>

SIG -  $\Sigma$  - atoms/cm

SOURCE - conservation equation source term - # protons/cm<sup>3</sup> Mev.

LOSS - conservation equation loss term - # protons/cm<sup>3</sup> Mev.

ENERGY - energy - Mev.

LATO - latitude - degrees

L - magnetic field line - earth radii

B - magnetic induction - gauss

LATO= 12.954 L= 1.188 B= 0.2331  
 ENERGY= 10.00MEV  
 TIME N(E) FLUX MEAN LIFETIME  
 0. 0.7172E-13 0.00031 0.30695E-04  
 CO= 0.72115E-15 C1= 0.10386E 09 C2= 0.21759E 10  
 ALOSSA= 0.47404E-10 DLOSSA= 0.35124E-11 SIG= 0.13080E-14  
 N(E)= 0.71720E-13 SOURCE= 0.90144E-15 LOSS= 0.12569E-01  
 TIME N(E) FLUX MEAN LIFETIME  
 4.000 0.7083E-13 0.00031 0.37893E-04  
 CO= 0.72115E-15 C1= 0.10386E 09 C2= 0.21759E 10  
 ALOSSA= 0.38400E-10 DLOSSA= 0.28452E-11 SIG= 0.10610E-14  
 N(E)= 0.70831E-13 SOURCE= 0.72115E-15 LOSS= 0.10131E-01  
 ENERGY= 25.00MEV  
 TIME N(E) FLUX MEAN LIFETIME  
 0. 0.2246E-13 0.00015 0.95765E-04  
 CO= 0.72376E-16 C1= 0.64318E 08 C2= 0.33686E 10  
 ALOSSA= 0.22595E-10 DLOSSA= 0.76320E-12 SIG= 0.13080E-14  
 N(E)= 0.22457E-13 SOURCE= 0.90470E-16 LOSS= 0.40286E-02  
 TIME N(E) FLUX MEAN LIFETIME  
 4.000 0.2218E-13 0.00015 0.11822E-03  
 CO= 0.72376E-16 C1= 0.64318E 08 C2= 0.33686E 10  
 ALOSSA= 0.18303E-10 DLOSSA= 0.61623E-12 SIG= 0.10610E-14  
 N(E)= 0.22178E-13 SOURCE= 0.72376E-16 LOSS= 0.32634E-02  
 ENERGY= 50.00MEV  
 TIME N(E) FLUX MEAN LIFETIME  
 0. 0.9981E-14 0.00009 0.24227E-03  
 CO= 0.12715E-16 C1= 0.44760E 08 C2= 0.46686E 10  
 ALOSSA= 0.12956E-10 DLOSSA= 0.21465E-12 SIG= 0.13080E-14  
 N(E)= 0.99806E-14 SOURCE= 0.15894E-16 LOSS= 0.15925E-02  
 TIME N(E) FLUX MEAN LIFETIME  
 4.000 0.9857E-14 0.00009 0.29908E-03  
 CO= 0.12715E-16 C1= 0.44760E 08 C2= 0.46686E 10  
 ALOSSA= 0.10495E-10 DLOSSA= 0.17387E-12 SIG= 0.10610E-14  
 N(E)= 0.98567E-14 SOURCE= 0.12715E-16 LOSS= 0.12900E-02  
 ENERGY= 75.00MEV  
 TIME N(E) FLUX MEAN LIFETIME  
 0. 0.6368E-14 0.00007 0.42753E-03  
 CO= 0.45973E-17 C1= 0.36207E 08 C2= 0.56691E 10  
 ALOSSA= 0.94431E-11 DLOSSA= 0.97214E-13 SIG= 0.13080E-14  
 N(E)= 0.63681E-14 SOURCE= 0.57466E-17 LOSS= 0.90241E-03  
 TIME N(E) FLUX MEAN LIFETIME  
 4.000 0.6289E-14 0.00007 0.52777E-03  
 CO= 0.45973E-17 C1= 0.36207E 08 C2= 0.56691E 10  
 ALOSSA= 0.76493E-11 DLOSSA= 0.78748E-13 SIG= 0.10610E-14  
 N(E)= 0.62890E-14 SOURCE= 0.45973E-17 LOSS= 0.73100E-03  
 ENERGY= 100.00MEV  
 TIME N(E) FLUX MEAN LIFETIME  
 0. 0.4893E-14 0.00006 0.69244E-03  
 CO= 0.21809E-17 C1= 0.22509E 08 C2= 0.65475E 10  
 ALOSSA= 0.76002E-11 DLOSSA= 0.57659E-13 SIG= 0.13080E-14  
 N(E)= 0.48928E-14 SOURCE= 0.27261E-17 LOSS= 0.55716E-03  
 TIME N(E) FLUX MEAN LIFETIME  
 4.000 0.4832E-14 0.00006 0.85460E-03  
 CO= 0.21509E-17 C1= 0.22509E 08 C2= 0.65475E 10  
 ALOSSA= 0.61565E-11 DLOSSA= 0.46707E-13 SIG= 0.10610E-14  
 N(E)= 0.48320E-14 SOURCE= 0.21309E-17 LOSS= 0.45134E-03  
 ENERGY= 125.00MEV  
 TIME N(E) FLUX MEAN LIFETIME  
 0. 0.3812E-14 0.00005 0.95289E-03  
 CO= 0.12348E-17 C1= 0.19444E 08 C2= 0.76699E 10  
 ALOSSA= 0.64599E-11 DLOSSA= 0.38193E-13 SIG= 0.13080E-14  
 N(E)= 0.38123E-14 SOURCE= 0.15435E-17 LOSS= 0.40488E-03  
 TIME N(E) FLUX MEAN LIFETIME  
 4.000 0.3765E-14 0.00005 0.11763E-02

CO= 0.12348E-17	C1= 0.19444E 08	C2= 0.70599E 10	
ALOSSA= 0.52328E-11	DLOSSA= 0.3093HE-13	SIG= 0.10610E-14	
N(E)= 0.37650E-14	SOURCE= 0.12348E-17	LOSS= 0.32798E-03	
ENERGY= 150.00MEV			
TIME	N(E)	FLUX	MEAN LIFETIME
0.	0.3115E-14	0.00005	0.12391E-02
CO= 0.77584E-18	C1= 0.17252E 08	C2= 0.75275E 10	
A SSA= 0.56631E-11	DLOSSA= 0.27629E-13	SIG= 0.13080E-14	
N(E)= 0.31148E-14	SOURCE= 0.96980E-18	LOSS= 0.31135E-03	
TIME	N(E)	FLUX	MEAN LIFETIME
4.000	0.3076E-14	0.00005	0.15296E-02
CO= 0.77584E-18	C1= 0.17252E 08	C2= 0.75275E 10	
ALOSSA= 0.46035E-11	DLOSSA= 0.21895E-13	SIG= 0.10610E-14	
N(E)= 0.30761E-14	SOURCE= 0.77584E-18	LOSS= 0.25222E-03	
ENERGY= 200.00MEV			
TIME	N(E)	FLUX	MEAN LIFETIME
0.	0.2258E-14	0.00004	0.18701E-02
CO= 0.37265E-18	C1= 0.14285E 08	C2= 0.83106E 10	
ALOSSA= 0.46921E-11	DLOSSA= 0.15451E-13	SIG= 0.13080E-14	
N(E)= 0.22579E-14	SOURCE= 0.46928E-18	LOSS= 0.20630E-03	
TIME	N(E)	FLUX	MEAN LIFETIME
4.000	0.2230E-14	0.00004	0.23084E-02
CO= 0.37265E-18	C1= 0.14285E 08	C2= 0.83106E 10	
ALOSSA= 0.38008E-11	DLOSSA= 0.12516E-13	SIG= 0.10610E-14	
N(E)= 0.22298E-14	SOURCE= 0.37265E-18	LOSS= 0.16713E-03	
ENERGY= 250.00MEV			
TIME	N(E)	FLUX	MEAN LIFETIME
0.	0.1753E-14	0.00003	0.25641E-02
CO= 0.21100E-18	C1= 0.12340E 08	C2= 0.89736E 10	
ALOSSA= 0.40869E-11	DLOSSA= 0.98392E-14	SIG= 0.13080E-14	
N(E)= 0.17529E-14	SOURCE= 0.26375E-18	LOSS= 0.15046E-03	
TIME	N(E)	FLUX	MEAN LIFETIME
4.000	0.1731E-14	0.00003	0.31651E-02
CO= 0.21100E-18	C1= 0.12340E 08	C2= 0.89736E 10	
ALOSSA= 0.33106E-11	DLOSSA= 0.79702E-14	SIG= 0.10610E-14	
N(E)= 0.17310E-14	SOURCE= 0.21100E-18	LOSS= 0.12189E-03	
ENERGY= 300.00MEV			
TIME	N(E)	FLUX	MEAN LIFETIME
0.	0.1404E-14	0.00003	0.32680E-02
CO= 0.13257E-18	C1= 0.10949E 08	C2= 0.95545E 10	
ALOSSA= 0.36805E-11	DLOSSA= 0.68303E-14	SIG= 0.13080E-14	
N(E)= 0.14037E-14	SOURCE= 0.16571E-18	LOSS= 0.11805E-03	
TIME	N(E)	FLUX	MEAN LIFETIME
4.000	0.1386E-14	0.00003	0.40338E-02
CO= 0.13257E-18	C1= 0.10949E 08	C2= 0.95545E 10	
ALOSSA= 0.29813E-11	DLOSSA= 0.55329E-14	SIG= 0.10610E-14	
N(E)= 0.13861E-14	SOURCE= 0.13257E-18	LOSS= 0.95643E-04	
ENERGY= 350.00MEV			
TIME	N(E)	FLUX	MEAN LIFETIME
0.	0.1142E-14	0.00002	0.39376E-02
CO= 0.89495E-19	C1= 0.98958E 07	C2= 0.10075E 11	
ALOSSA= 0.33896E-11	DLOSSA= 0.50877E-14	SIG= 0.13080E-14	
N(E)= 0.11418E-14	SOURCE= 0.11187E-18	LOSS= 0.97978E-04	
TIME	N(E)	FLUX	MEAN LIFETIME
4.000	0.1127E-14	0.00002	0.48601E-02
CO= 0.89495E-19	C1= 0.98958E 07	C2= 0.10075E 11	
ALOSSA= 0.27458E-11	DLOSSA= 0.41212E-14	SIG= 0.10610E-14	
N(E)= 0.11274E-14	SOURCE= 0.89495E-19	LOSS= 0.79381E-04	
ENERGY= 400.00MEV			
TIME	N(E)	FLUX	MEAN LIFETIME
0.	0.9561E-15	0.00002	0.46341E-02
CO= 0.63676E-19	C1= 0.90659E 07	C2= 0.10548E 11	
ALOSSA= 0.31723E-11	DLOSSA= 0.38580E-14	SIG= 0.13080E-14	
N(E)= 0.95607E-15	SOURCE= 0.79596E-19	LOSS= 0.83253E-04	
TIME	N(E)	FLUX	MEAN LIFETIME
4.000	0.9440E-15	0.00002	0.57195E-02

$C0 = 0.63676E-19$	$C1 = 0.90659E-07$	$C2 = 0.10548E-11$	MEAN LIFETIME
$ALOSSA = 0.25697E-11$	$DLOSSA = 0.31252E-14$	$SIG = 0.10610E-14$	$0.59518E-02$
$N(E) = 0.94400E-15$	$SOURCE = 0.63576E-19$	$LOSS = 0.67454E-04$	
ENERGY = 500.00MEV			
TIME	$N(E)$	FLUX	MEAN LIFETIME
0.	$0.6953E-15$	0.00002	$0.59518E-02$
$C0 = 0.36054E-19$	$C1 = 0.78313E-07$	$C2 = 0.11390E-11$	MEAN LIFETIME
$SSA = 0.28715E-11$	$DLOSSA = 0.24089E-14$	$SIG = 0.13080E-14$	$0.73451E-02$
$N(E) = 0.69526E-15$	$SOURCE = 0.45068E-19$	$LOSS = 0.64821E-04$	
TIME	$N(E)$	FLUX	MEAN LIFETIME
4.000	$0.6864E-15$	0.00002	$0.73451E-02$
$C0 = 0.36054E-19$	$C1 = 0.78313E-07$	$C2 = 0.11390E-11$	
$ALOSSA = 0.23260E-11$	$DLOSSA = 0.19512E-14$	$SIG = 0.10610E-14$	
$N(E) = 0.68642E-15$	$SOURCE = 0.36054E-19$	$LOSS = 0.52525E-04$	
ENERGY = 600.00MEV			
TIME	$N(E)$	FLUX	MEAN LIFETIME
0.	$0.5248E-15$	0.00001	$0.71499E-02$
$C0 = 0.22653E-19$	$C1 = 0.69485E-07$	$C2 = 0.12127E-11$	MEAN LIFETIME
$ALOSSA = 0.26761E-11$	$DLOSSA = 0.16081E-14$	$SIG = 0.13080E-14$	$0.88230E-02$
$N(E) = 0.52477E-15$	$SOURCE = 0.28316E-19$	$LOSS = 0.53959E-04$	
TIME	$N(E)$	FLUX	MEAN LIFETIME
4.000	$0.5181E-15$	0.00001	$0.88230E-02$
$C0 = 0.22653E-19$	$C1 = 0.69485E-07$	$C2 = 0.12127E-11$	
$ALOSSA = 0.21678E-11$	$DLOSSA = 0.13026E-14$	$SIG = 0.10610E-14$	
$N(E) = 0.51805E-15$	$SOURCE = 0.22653E-19$	$LOSS = 0.43727E-04$	
ENERGY = 700.00MEV			
TIME	$N(E)$	FLUX	MEAN LIFETIME
0.	$0.4033E-15$	0.00001	$0.81399E-02$
$C0 = 0.15292E-19$	$C1 = 0.62302E-07$	$C2 = 0.12788E-11$	MEAN LIFETIME
$ALOSSA = 0.25414E-11$	$DLOSSA = 0.11503E-14$	$SIG = 0.13080E-14$	$0.10044E-01$
$N(E) = 0.40331E-15$	$SOURCE = 0.19115E-19$	$LOSS = 0.47397E-04$	
TIME	$N(E)$	FLUX	MEAN LIFETIME
4.000	$0.3981E-15$	0.00001	$0.10044E-01$
$C0 = 0.15292E-19$	$C1 = 0.62302E-07$	$C2 = 0.12788E-11$	
$ALOSSA = 0.20586E-11$	$DLOSSA = 0.93180E-15$	$SIG = 0.10610E-14$	
$N(E) = 0.39811E-15$	$SOURCE = 0.15292E-19$	$LOSS = 0.38412E-04$	

## H. Running Time

This program will do eleven cases in a minute and a half.

## IX. REFERENCES

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3. McIlwain, C.E., "Coordinates for Mapping the Distribution of Magnetically Trapped Particles," Journal of Geophysical Research, vol. 66, (1961), pp. 3681-3691.
4. Jensen, D.C., and Cain, J.C., unpublished, presented at April, 1962, meeting of the American Geophysical Union, Washington, D.C.
5. Ray, Ernest, C., "On the Theory of Protons Trapped in the Earth's Magnetic Field," Journal of Geophysical Research, vol. 65, no. 4, April, 1960, pp. 1125-1133.
6. Scarborough, J.B., Numerical Mathematical Analysis, 3rd Edition, Oxford University Press, copyright, 1955.
7. Aron, W.A., Hoffman, B.C., Williams, F.C., "Range-Energy Curves" (2nd Rev. 1949) U.S.A.E.C., Univ. of Calif. Rad. Lab.

## X. ILLUSTRATIONS

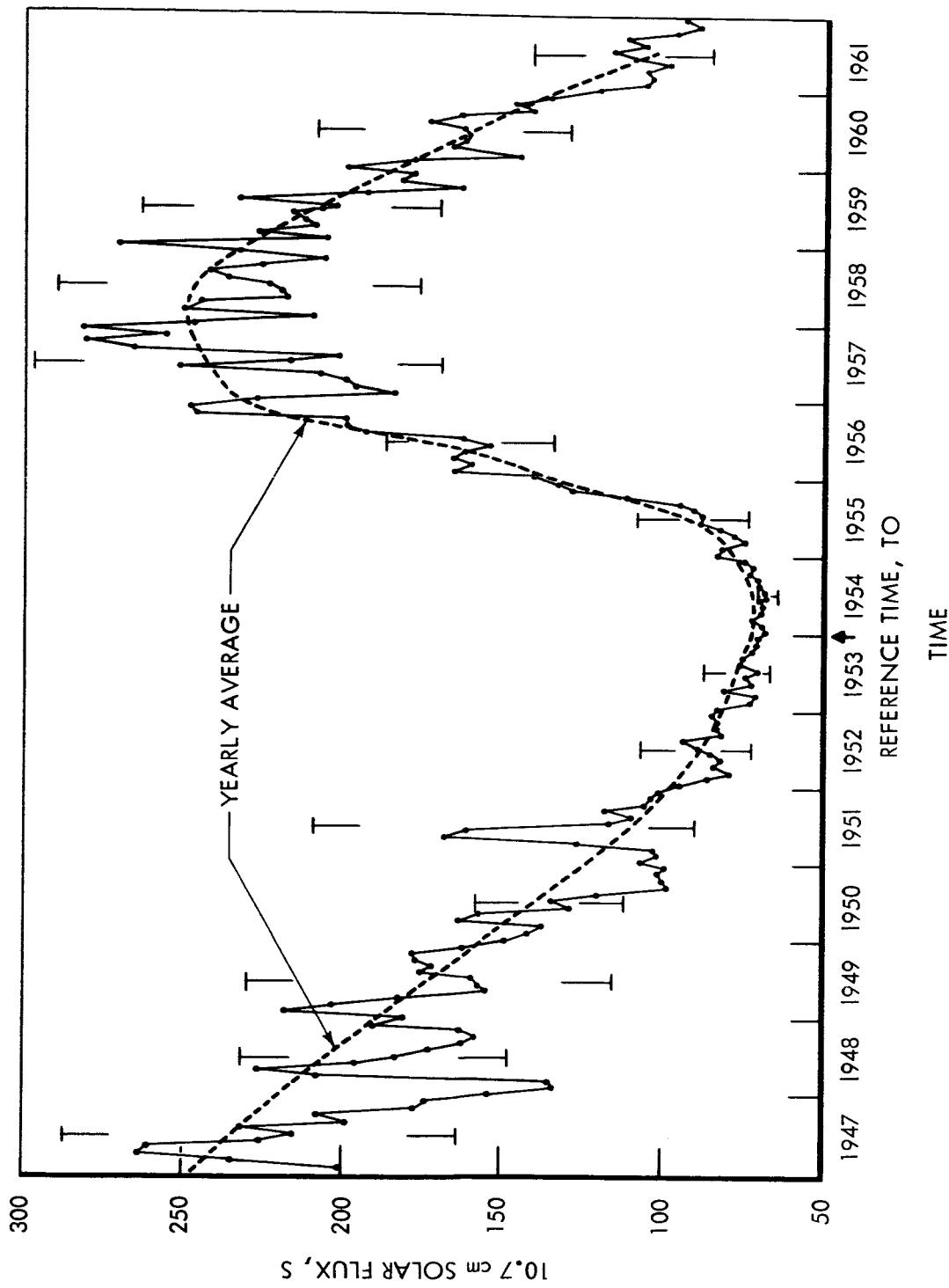


Figure 1-A time history of the 10.7 cm solar flux according to the measurements of the National Research Council of Canada for the recent past. The heavy dotted line indicates the approximate yearly average.

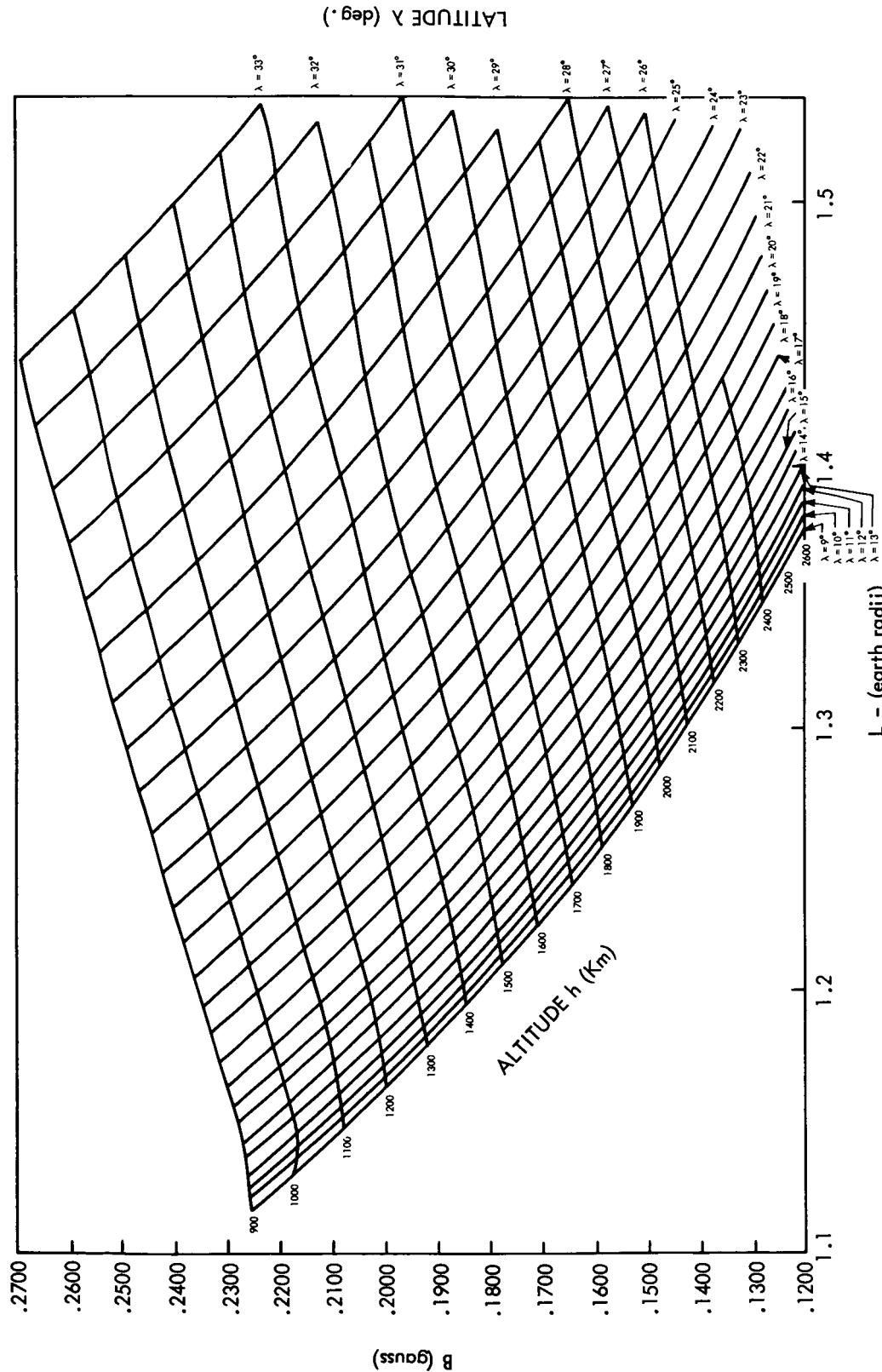


Figure 2-A mapping of the polar coordinates  $R$  and  $\lambda$  onto the B-L plane  
where  $R = (h + 6378.2)$

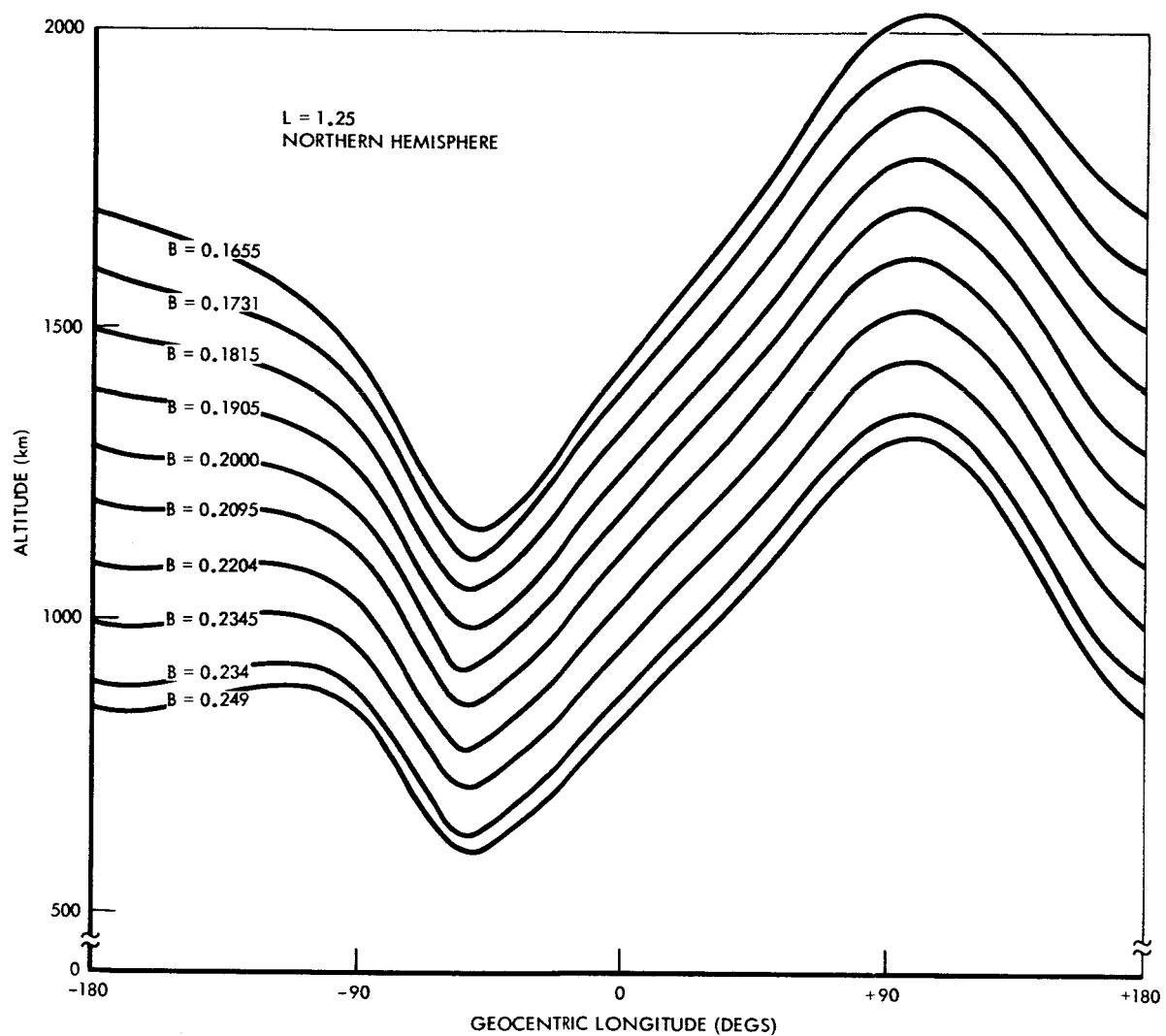


Figure 3-B-L contours for the northern hemisphere at an  $L$  of 1.25 earth radii

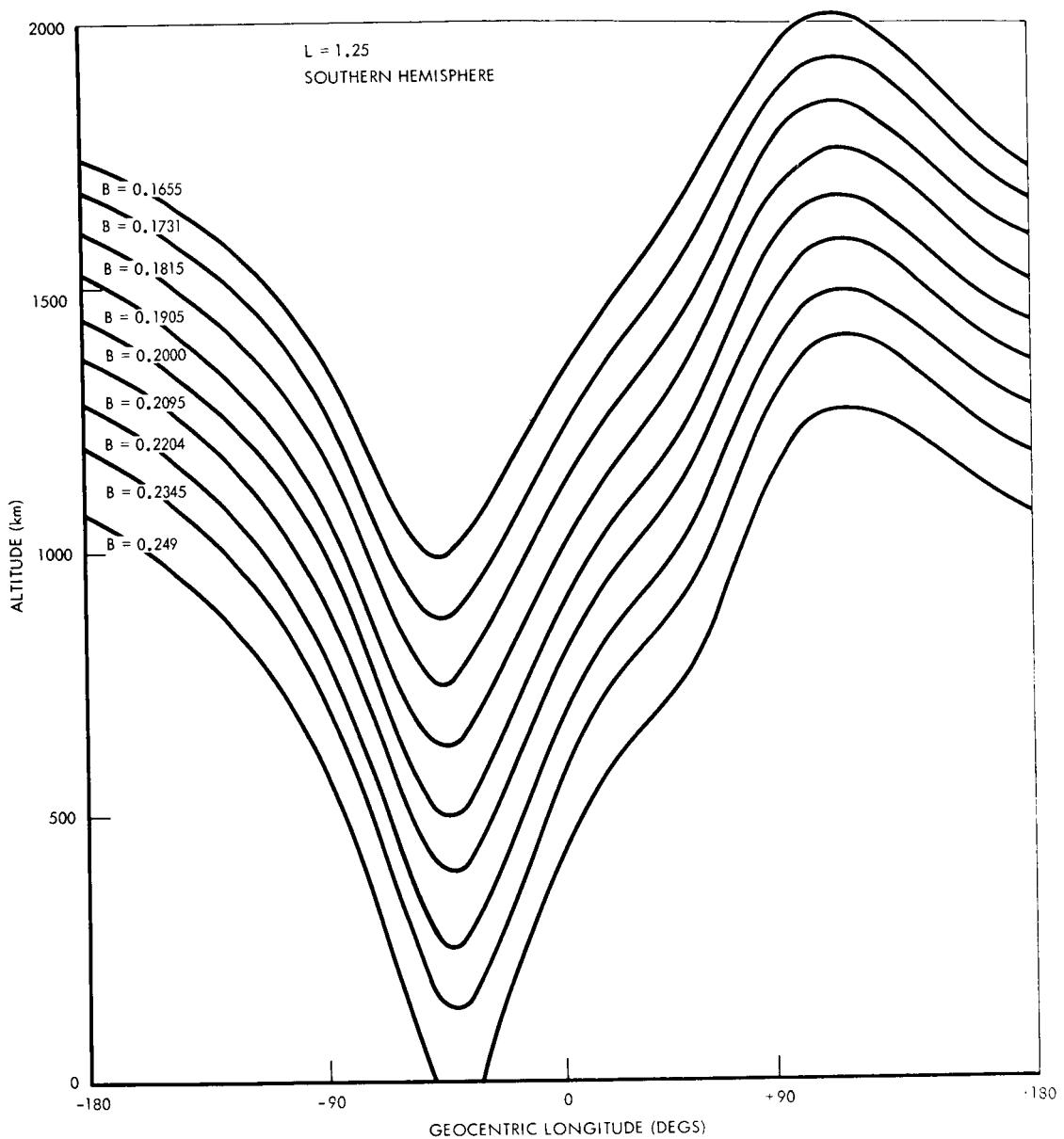
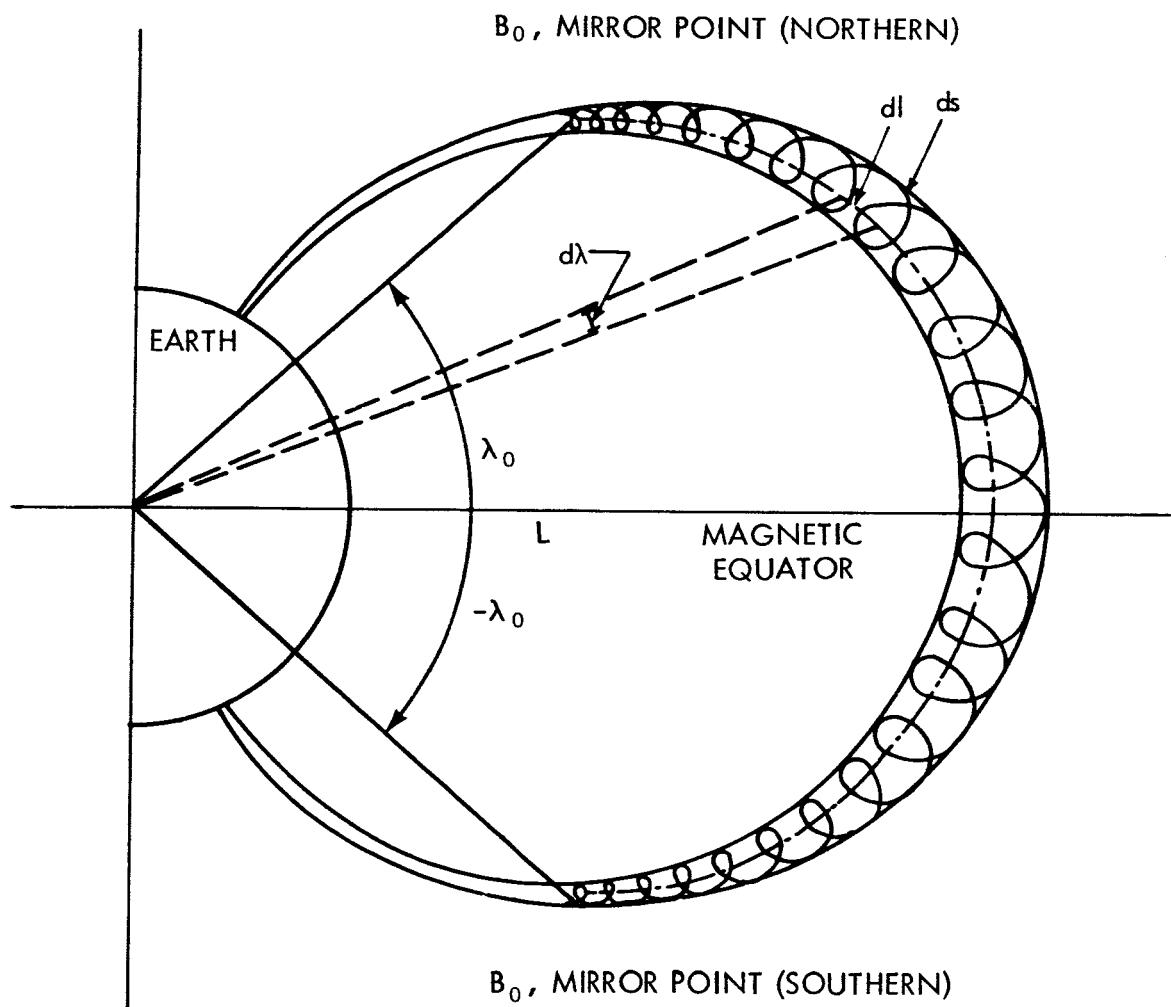


Figure 4-B-L contours for the southern hemisphere at an L of 1.25 earth radii



WHERE:

- $ds$  - Element of Arc along the particle's helical trajectory
- $dl$  - Element of Arc along the field line

Figure 5-Schematic of a trapped particle's north-south motion

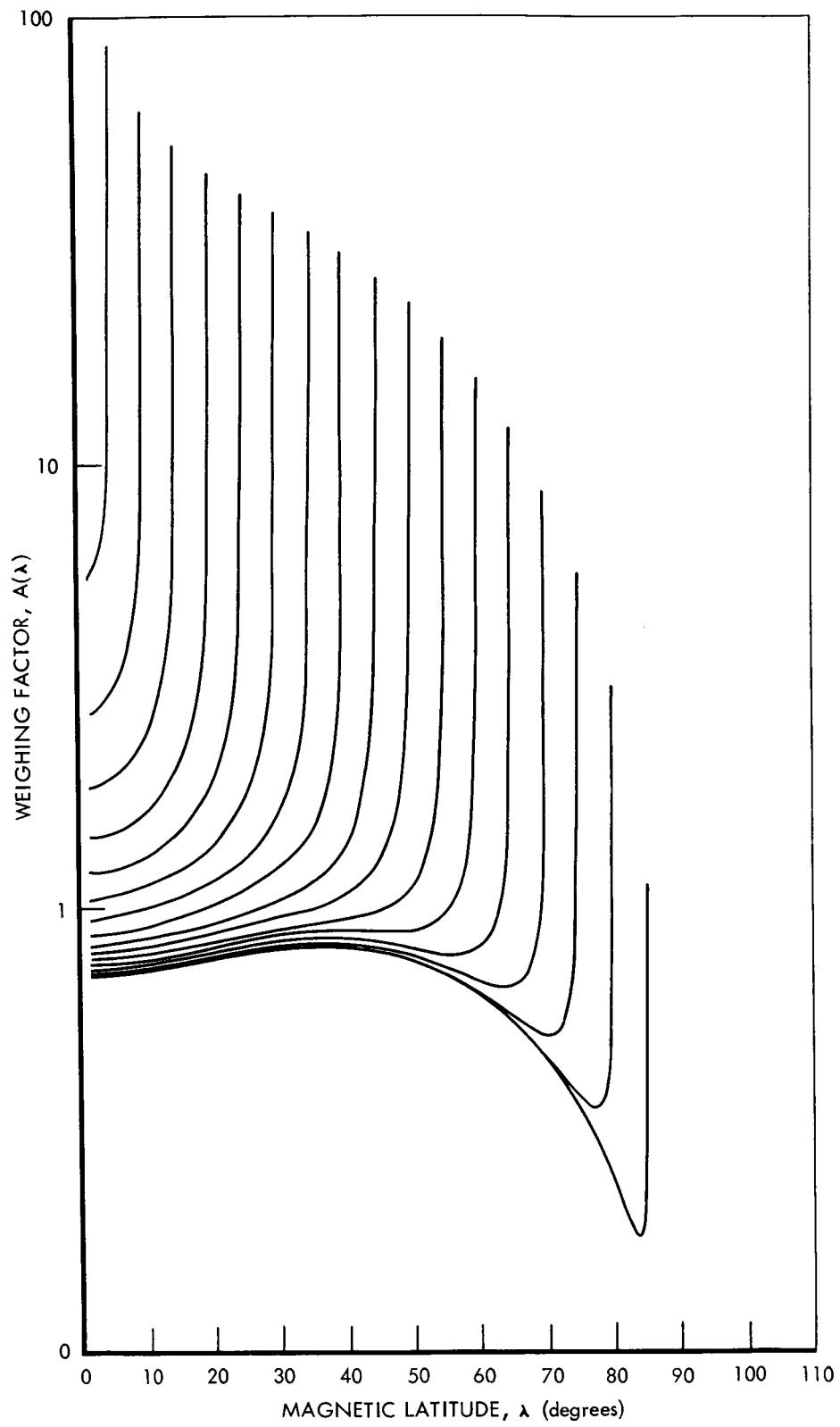


Figure 6-The weighing factor,  $A(\lambda)$ , versus latitude for various mirror latitudes,  $\lambda_0$ , where  $\lambda_0$  are the asymptotes of each curve

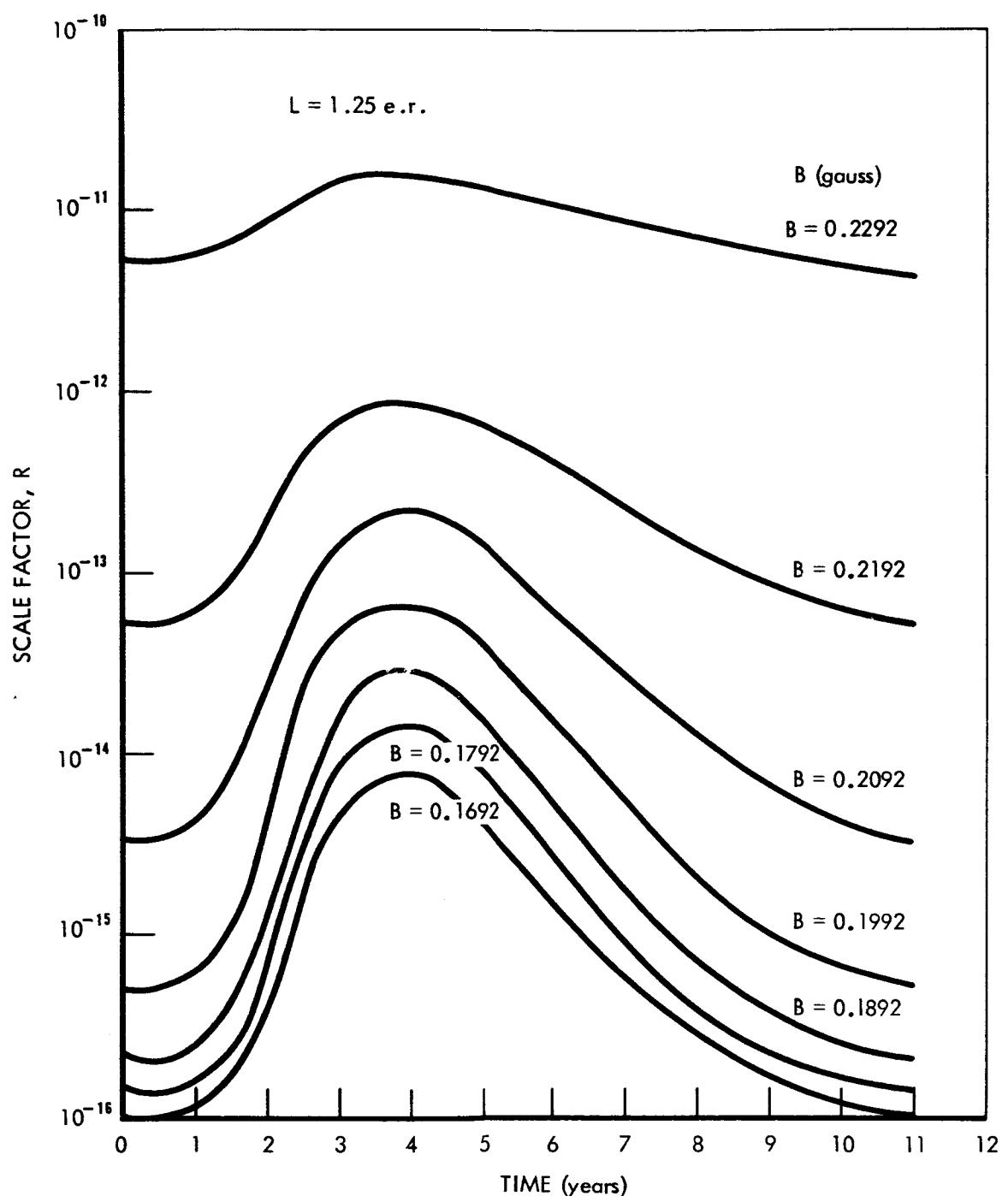


Figure 7-A time history of the atmosphere scale factor,  $R$ , as a function of  $B$  at  $L = 1.25$  e.r.

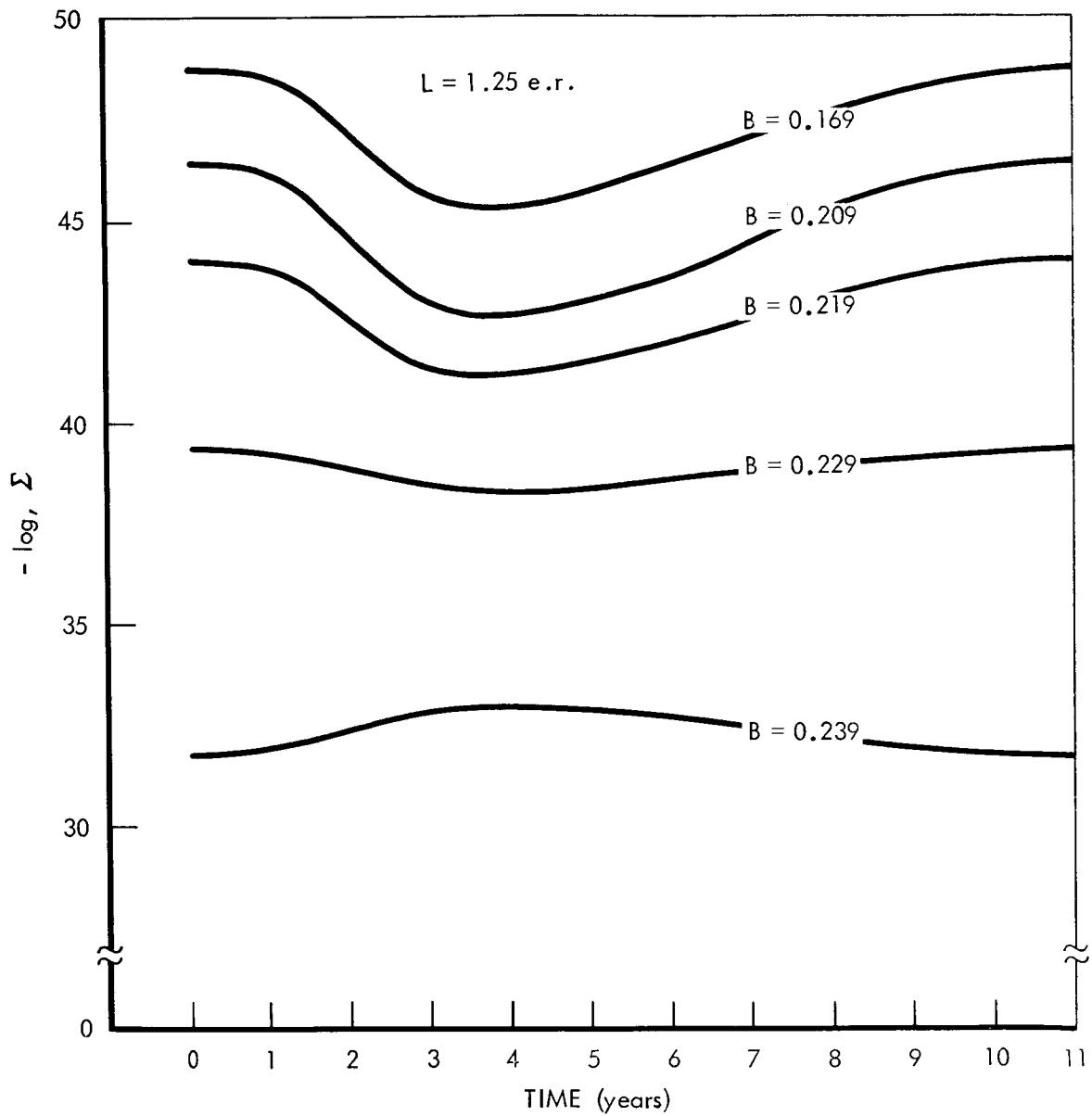


Figure 8-A time history of the atmospheric loss parameter  $\Sigma$ , as a function of  $B$  at  $L = 1.25$  e.r.

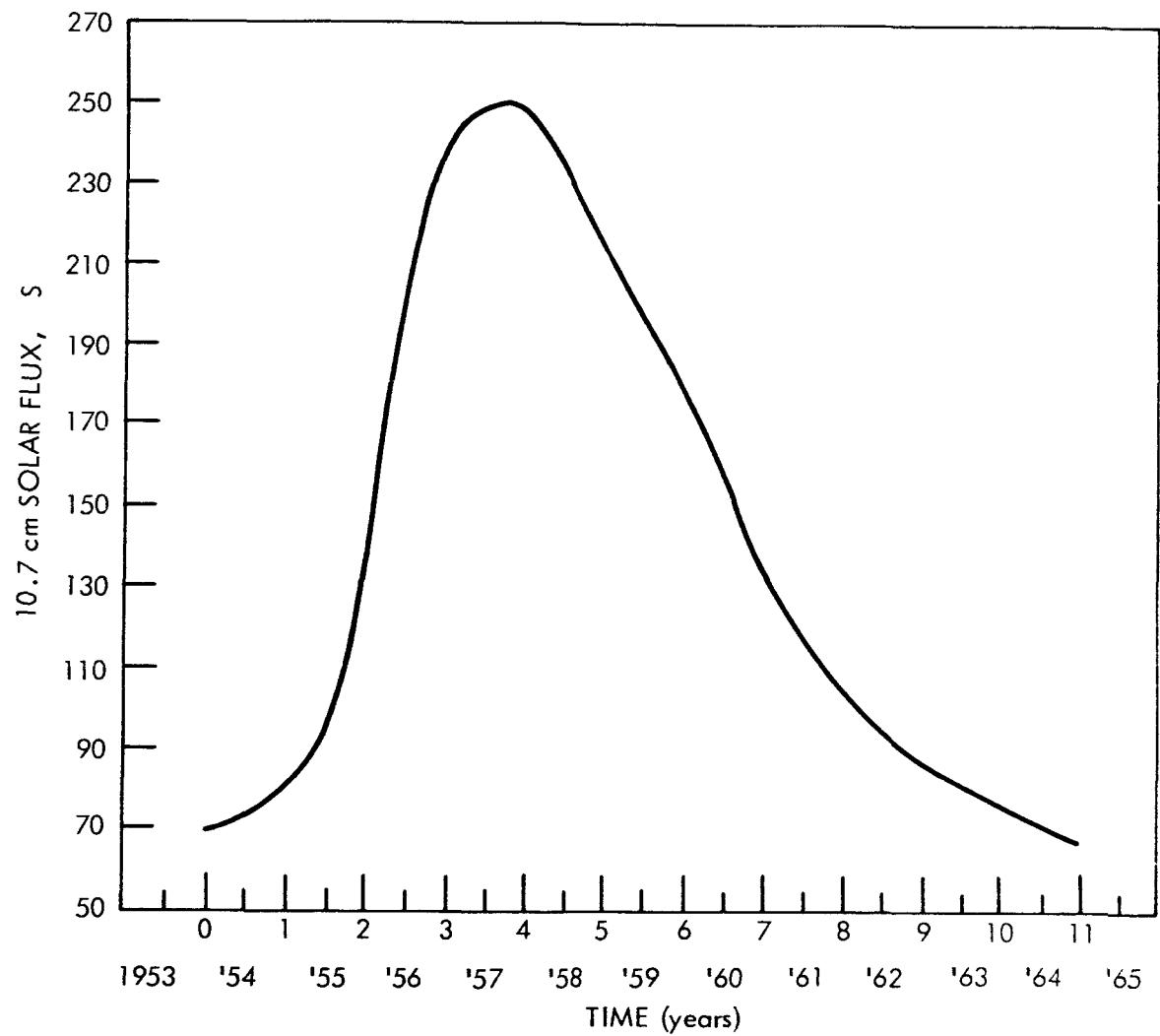


Figure 9-A time history of the constructed mean solar cycle variation of the 10.7 cm. solar flux with reference time  $t_0$  of Jan., 1954

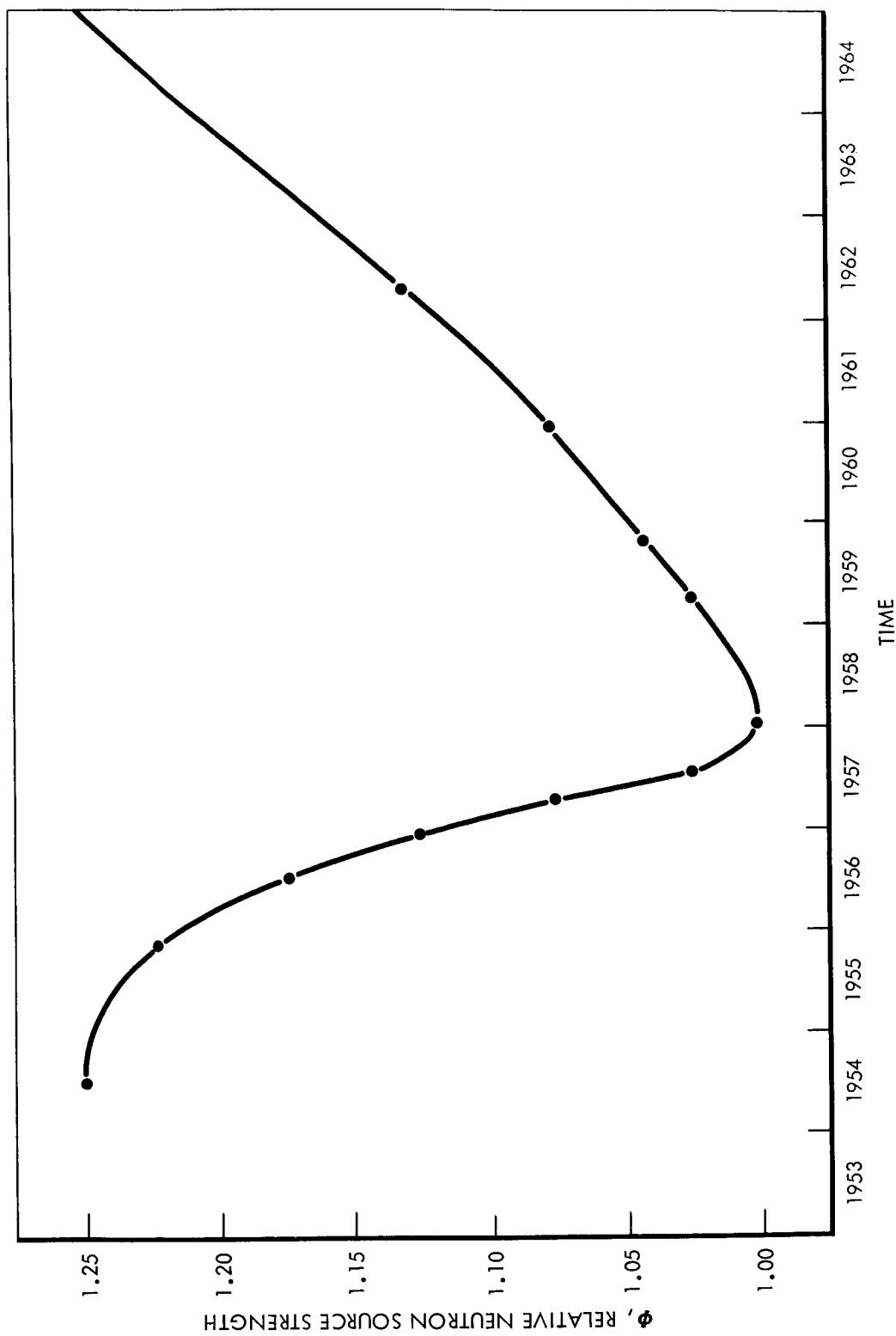


Figure 10-A time history of the relative inner belt source strength

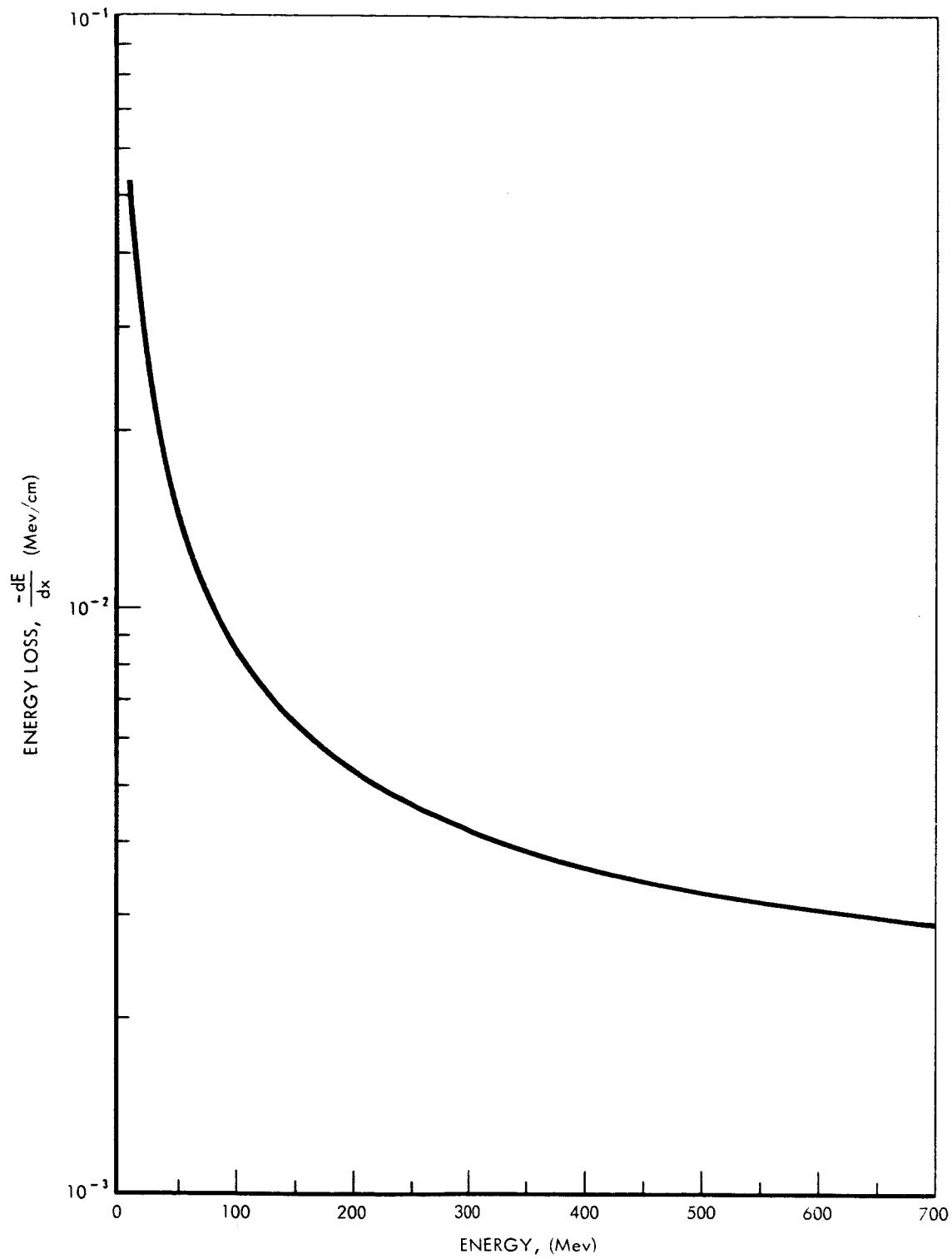


Figure 11-The proton energy loss spectrum for an oxygen target

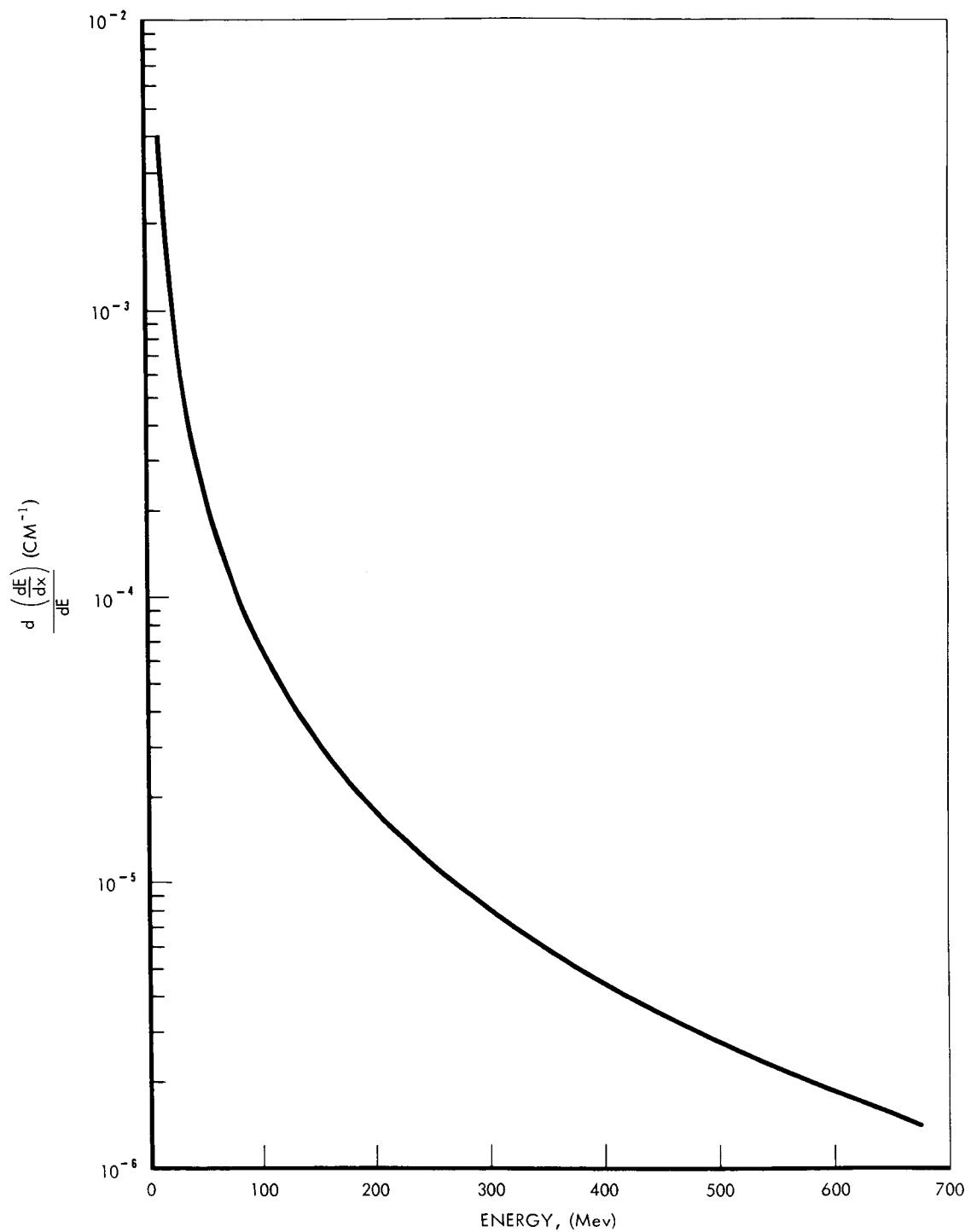


Figure 12-The slope of proton energy loss versus energy for an oxygen target

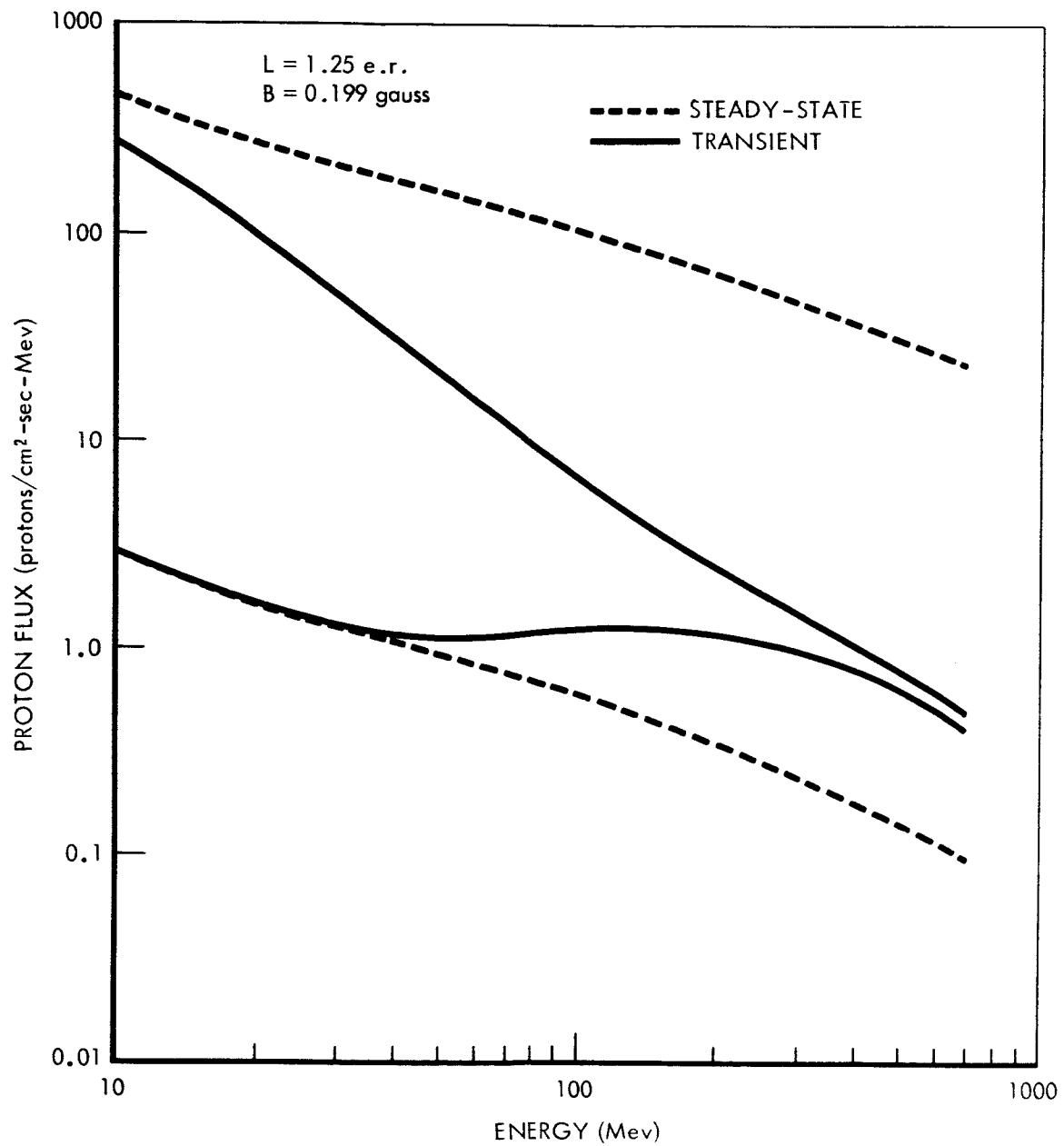


Figure 13-A comparison of the steady-state and transient proton flux energy spectrums for  $L = 1.25$ ,  $B^* = .199$  at solar minimum and solar maximum

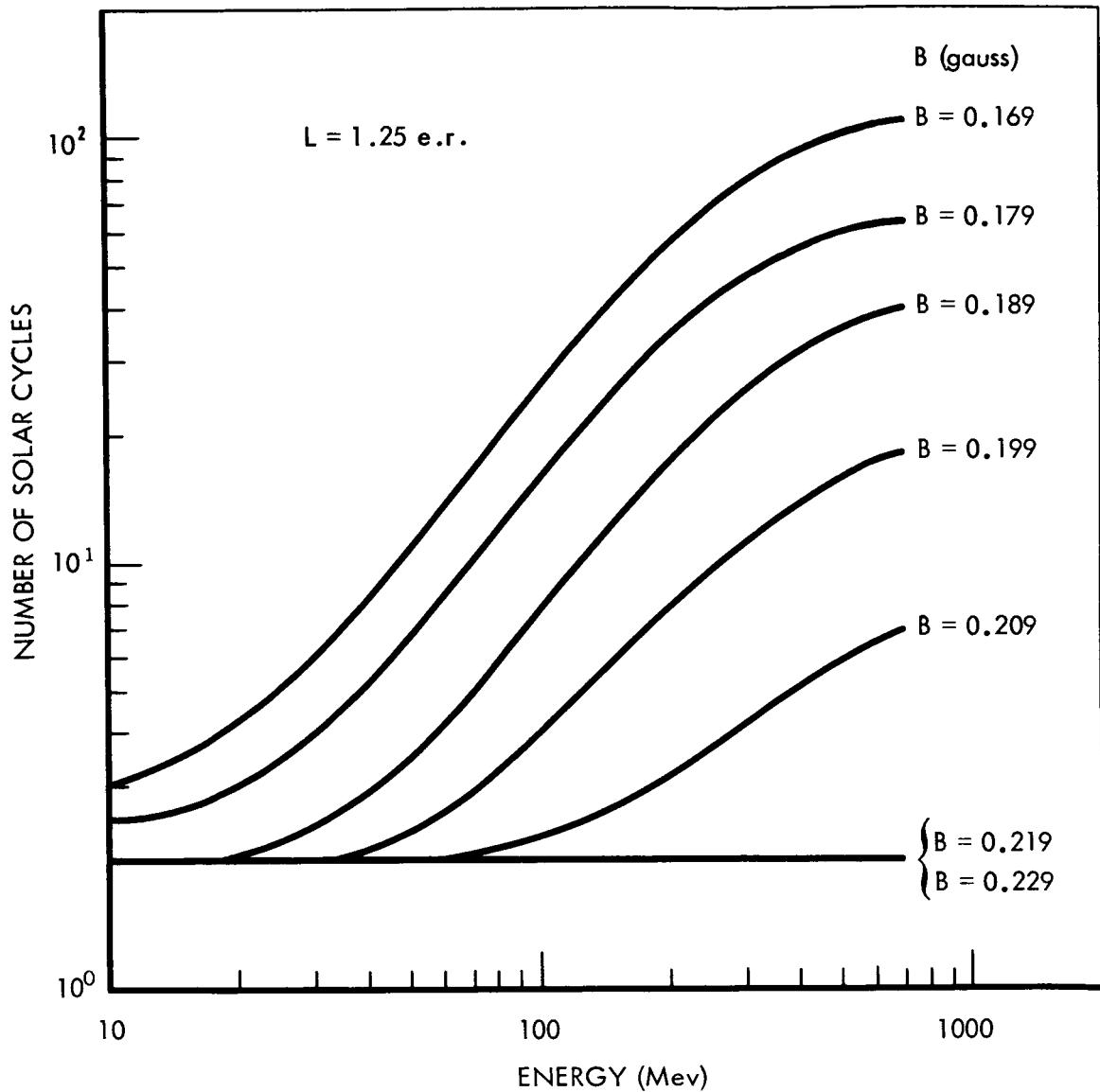


Figure 14-The time required in terms of solar cycles to build steady state conditions versus energy as a function of  $B$

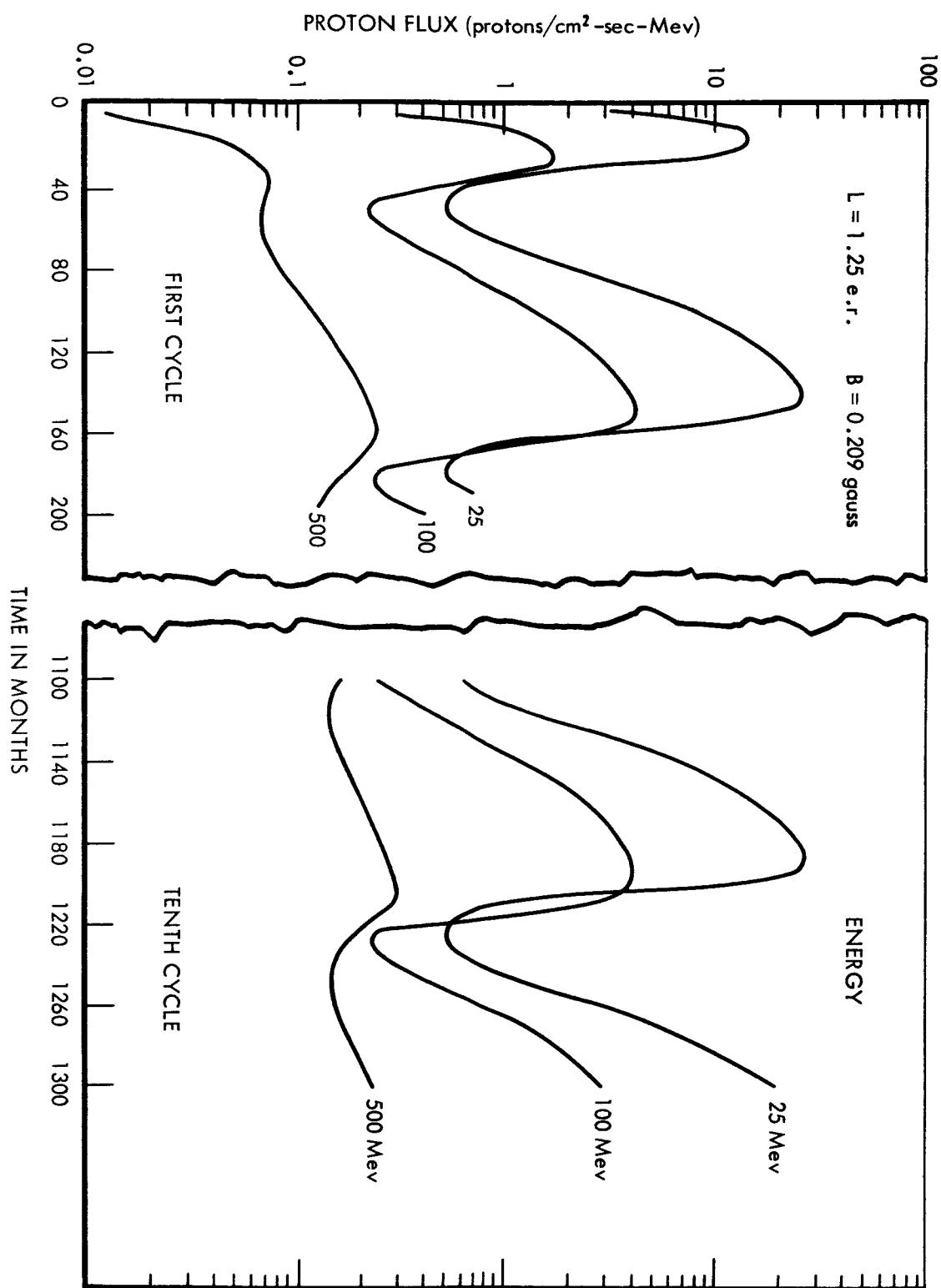


Figure 15-A time history of proton flux as a function of energy at  $L = 1.25$ ,  
 $B = .209$  for the first and tenth solar cycles