

X-547-65-222

NASA TMX-55271

FACILITY FORM 602

165-29805 (ACCESSION NUMBER)	(THRU)
114 (PAGES)	(CODE)
(NASA OR OR TMX OR AD NUMBER)	08 (CATEGORY)

A MUTUAL VISIBILITY COMPUTER PROGRAM FOR COMMUNICATION SATELLITES

GPO PRICE \$ _____

CFSTI PRICE(S) \$ _____

Hard copy (HC) 4.00

Microfiche (MF) .75

BY
G. D. REPASS
R. G. CHAPLICK

ff 653 July 65

MAY 1965



GODDARD SPACE FLIGHT CENTER
GREENBELT, MARYLAND

Reproduced by
NATIONAL TECHNICAL
INFORMATION SERVICE
U S Department of Commerce
Springfield VA 22151

1229

CLASS FILE
G00007

A MUTUAL VISIBILITY COMPUTER PROGRAM FOR
COMMUNICATION SATELLITES

by

G. D. Repass and R. G. Chaplick

May 1965

Goddard Space Flight Center
Greenbelt, Maryland

A MUTUAL VISIBILITY COMPUTER PROGRAM FOR COMMUNICATION SATELLITES

INTRODUCTION

As more and more ground stations are constructed around the world to operate with communication satellites, the problems of scheduling the experiments become more complex. Many factors, e.g., is the attitude of the satellite correct, must be considered simultaneously in order for decisions to be made. Although many pieces of data were on hand during tests with Telstar I and Relay I, the information was presented randomly in three or more books, and much human effort was needed to extract and analyze the pertinent data. The obvious solution was to compute only the necessary data and to present them as concisely as possible. This report will describe such a program which has been developed by members of the Theory and Analysis Office.

PROGRAM CRITERIA

The following criteria were used to design the program:

(a) Data should be printed only for passes during which the spacecraft was visible to a "control" station. Because the Relay spacecraft can be operated by only two or three stations, it must be visible to one of those stations when experiments are made.

(b) Data should be presented in two books, one graphs of mutual visibility and the other the actual numerical data.

MUTUAL VISIBILITY

Bar graphs appeared to be the most legible form for presentation of time intervals of mutual visibility. In addition, indications of elevation angles from 0° to 5° , from 5° to 10° , and from 10° to 90° ; of ranges higher or lower than a prescribed input value; of spacecraft look angle; and of orbit number were necessary.

NUMERICAL DATA

This volume consists of all the numerical data used to produce the mutual visibility graphs. These data are spacecraft longitude, latitude, height and sun-light indicator; and for each station the spacecraft look angle (the angle between the spin axis and the slant range), azimuth, elevation, and slant range. The last set of data in this book is a complete time history of entry into and exit from the earth's shadow.

THEORY

The program can be described simply as an orbit generator with associated subroutines necessary to perform needed calculations. Experience at Goddard has indicated that the theory developed by Brouwer (1959) is adaptable for the purposes of this program. The American Institute of Physics has granted permission to the authors to reproduce certain pages of Brouwer (1959) herein. Appendix I consists of pages 393 to 396. To aid the reader the pertinent equations have been rewritten and the equivalent Fortran II variable names for some of the terms have been superimposed on the equations. These equations are reproduced in Appendix II.

A brief explanation of how the orbit generator has been programmed will help the reader.

Secular terms. These equations were rewritten as:

$$l'' = l_0'' + S_1 t + S_{1,2} t^2$$

$$g'' = g_0'' + S_2 t$$

$$h'' = h_0'' + S_3 t$$

where S_1 , S_2 , S_3 are constant for any given set of a_0'' , e_0'' , I_0'' , and earth constants and $S_{1,2}$ is the anomalistic acceleration computed by the GSFC differential correction programs. If $S_{1,2}$ is unavailable, the added term can be dropped by inputting it as zero.

Long Period terms. These equations were rewritten as:

$$\ell' = \ell'' + L_1 \sin 2g'' + L_2 \cos g'' + L_3 \cos 3g''$$

$$g' = g'' + L_4 \sin 2g'' + L_5 \cos g'' + L_6 \cos 3g''$$

$$h' = h'' + L_7 \sin 2g'' + L_8 \cos g'' + L_9 \cos 3g''$$

$$\delta_1 e = L_{10} \cos 2g'' + L_{11} \sin g'' + L_{12} \sin 3g''$$

$$\delta_1 I = L_{13} \delta_1 e$$

where L_i , $1 \leq i \leq 13$ are constant for any given set of a_0'' , e_0'' , I_0'' , and earth constants.

EARTH'S GRAVITATIONAL POTENTIAL

The force function used is that of Brouwer, page 393, where k_2 , k_3 , k_4 , k_5 represent the zonal harmonics. However, Vinti's notation of J_n should be adopted. Either set of harmonics can be used by means of the following equations:

$$k_2 = + \frac{1}{2} J_2 R_e^2$$

$$k_3 = - J_3 R_e^3$$

$$k_4 = - \frac{3}{8} J_4 R_e^4$$

$$k_5 = - J_5 R_e^5$$

The program has been designed either to use constants stored in memory or to read new constants along with other input data.

COMPUTER PROGRAM

The computer program, written in Fortran II for the IBM 7094, was designed typically is a main program with subroutines called when needed. The orbit generator has been designed to compute in one subroutine all quantities which are functions of mean elements and earth constants. Another subroutine computes only those quantities which are either explicit or implicit functions of time. Terms that occur at least twice in the equations are assigned a variable name and actually are computed only once.

Main Program. The requirement that data be printed only for passes when the spacecraft is visible at a control station implies, unfortunately, that data must be computed and stored before a decision can be made to discard the data. The authors recognize that "shortcuts" were available to avoid computing data which were to be thrown away. However, the requirement for an accurate eclipse history did not allow such methods to be used.

Main Program One. This program fulfills the requirements described previously herein. Its characteristics are (a) an IBM 7094 with a 65K memory is required and (b) the complete sunlight history is computed. Computer running time could be reduced if (a) and (b) can be eliminated.

Main Program Two. This program is similar to Main Program One except that the control station requirements, the complete sunlight history, and the numerical data on bar graphs were deleted. A computer with at least a 20K memory (dependent on memory needed for library subroutines) is required.

Subroutines. The subroutines for each of the main programs are identical.

Operation Instructions. Instructions for operating the two programs are given in Appendix III.

Input deck instructions. Instructions for punching the input deck for each program are given in Appendix III.

Flow Charts. The flow chart for Main Program Two is contained in Appendix IV.

Source Decks. Source decks for Main Program One, Main Program Two, and Subroutines are reproduced in Appendices V, VI, and VII respectively.

Sample Problems. Inputs to and outputs of each program are given in Appendix VIII. The outputs have been abbreviated.

Results

Main Program One has been used extensively and successfully for planning experiments with Relay I and II and Echo I and II. Main program Two, which is less sophisticated and is easy to change, has been used for a variety of special studies, e.g., travel time of light from station to spacecraft back to station; angles between slant ranges from a single station to two different spacecraft, etc.

REFERENCE

1. "Solution of the Problem of Artificial Satellite Theory without Drag," D. Brouwer, *Astronomical Journal* 64, 9, Nov. 1959, pp. 393-396.

APPENDIX I

Reproduction of Pages 393 to 396 of Brouwer (1959)

Formulas for Computation. For convenience of computation the perturbations in the Keplerian elements a , e , I are given instead of those in L , G , H .

The adopted force function is

$$\begin{aligned}
 U = & \frac{\mu}{r} + \frac{\mu k_2}{r^2} (1 - 3 \sin^2 \beta) + \frac{\mu k_4}{r^6} \left(1 - 10 \sin^2 \beta + \frac{35}{3} \sin^4 \beta \right) \\
 & + \frac{\mu A_{3,0}}{r^4} \left(-\frac{3}{2} \sin \beta + \frac{5}{2} \sin^3 \beta \right) + \frac{\mu A_{5,0}}{r^6} \left(\frac{15}{8} \sin \beta - \frac{35}{4} \sin^3 \beta + \frac{63}{8} \sin^5 \beta \right),
 \end{aligned}$$

in which k_2 is a small quantity, and k_4 , $A_{3,0}$, $A_{5,0}$ are assumed to be of order k_2^2 .

The secular motions have been computed to $O(k_2^2)$, the coefficients of periodic terms to $O(k_2)$.

Basic constants:

a'' = semi-major axis constant

e'' = eccentricity constant

I'' = inclination constant

$n_0 = \mu^{1/2} a''^{-3/2} = 17.04337 (a''/R)^{-3/2}$ rev./day

R = equatorial radius

Abbreviations:

$$\eta = (1 - e'^2)^{1/2} \quad \theta = \cos I''$$

$$\gamma_2 = \frac{k_2}{a'^2} \quad \gamma_4 = \frac{k_4}{a'^4} \quad \gamma_3 = \frac{.13 \ 0}{a'^8} \quad \gamma_5 = \frac{.15 \ 0}{a'^8}$$

$$\gamma_2' = \gamma_2 \eta^{-4} \quad \gamma_4' = \gamma_4 \eta^{-8} \quad \gamma_3' = \gamma_3 \eta^{-6} \quad \gamma_5' = \gamma_5 \eta^{-10}$$

It is customary to use for the second harmonic the coefficient J; Jeffreys (1954) used for the fourth harmonic the coefficient D. The relations between J, D and γ_2, γ_4 are

$$\gamma_2 = \frac{1}{3} J \left(\frac{R}{a''} \right)^2, \quad \gamma_4 = \frac{3}{35} D \left(\frac{R}{a''} \right)^4.$$

Strictly speaking, $e'' + \delta_1 e$, $\theta' = \cos(I'' + \delta_1 I)$, $\eta' = [1 - (e'' + \delta_1 e)^2]^{1/2}$ should be used in the computation of the periodic terms, but since the short-period terms are obtained to $O(k_2)$, it is of no consequence if contributions of $O(k_2)$ are omitted in expressions that have γ_2 as a factor. Similarly, ℓ'' , g'' might be used in computing f' , r' ; but since ℓ' , γ' are available, their use does not complicate the calculation.

The formulas are applicable for any eccentricity $e < 1$ and any inclination with the exception of inclinations near the critical inclination, for which $1 - 5 \cos^2 I$ appears as a small divisor.

The appearance of e'' as a divisor in the short-period terms in e is apparent only. The expressions that are multiplied by e''^{-1} contain e'' as a factor, either implicitly or explicitly.

In the short-period terms in ℓ and g a divisor e'' occurs also, but for the calculation of the position only $g + \ell$ + equation of the center is needed. In $g + \ell$ the divisor e'' is not present.

Singularities in some of the elements also occur for very small inclinations; again, no singularity is present in the coordinates. In such cases it may be found convenient to modify the formulas and obtain expressions for the perturbations in coordinates.

Secular terms:

l'' = "mean" mean anomaly

$$= n_0 t \left\{ 1 + \frac{3}{2} \gamma_2' \eta (-1 + 3\theta^2) + \frac{3}{32} \gamma_2'^2 \eta [-15 + 16\eta + 25\eta^2 + (30 - 96\eta - 90\eta^2)\theta^2] \right. \\ \left. + (105 + 144\eta + 25\eta^2)\theta^4 \right\} + \frac{15}{16} \gamma_4' \eta e''^2 [3 - 30\theta^2 + 35\theta^4] + l_0''$$

g'' = mean argument of perigee

$$= n_0 t \left\{ \frac{3}{2} \gamma_2' (-1 + 5\theta^2) + \frac{3}{32} \gamma_2'^2 [-35 + 24\eta + 25\eta^2 + (90 - 192\eta - 126\eta^2)\theta^2] \right. \\ \left. + (385 + 360\eta + 45\eta^2)\theta^4 \right\} + \frac{5}{16} \gamma_4' [21 - 9\eta^2 + (-270 + 126\eta^2)\theta^2 + (385 - 189\eta^2)\theta^4] + g_0''$$

h'' = mean longitude of ascending node

$$= n_0 t \left\{ -3\gamma_2' \theta + \frac{3}{8} \gamma_2'^2 [(-5 + 12\eta + 9\eta^2)\theta + (-35 - 36\eta - 5\eta^2)\theta^2] \right. \\ \left. + \frac{5}{4} \gamma_4' (5 - 3\eta^2)\theta(3 - 7\theta^2) \right\} + h_0''$$

Long-period terms:

$$\begin{aligned} \delta_{1e} = & \left\{ \frac{1}{8} \gamma_2' e'' \eta^3 [I - 11\theta^2 - 40\theta^4 (I - 5\theta^2)^{-1}] - \frac{5}{12} \frac{\gamma_4'}{\gamma_2'} e'' \eta^3 [I - 3\theta^2 - 8\theta^4 (I - 5\theta^2)^{-1}] \right\} \cos 2g'' \\ & + \left\{ \frac{1}{4} \frac{\gamma_3'}{\gamma_2'} \eta^3 \sin I'' + \frac{5}{64} \frac{\gamma_6'}{\gamma_2' \eta^2} \sin I'' (4 + 3e''^2) [I - 9\theta^2 - 24\theta^4 (I - 5\theta^2)^{-1}] \right\} \sin g'' \\ & - \frac{35}{384} \frac{\gamma_6'}{\gamma_2'} e''^2 \eta^3 \sin I'' [I - 5\theta^2 - 16\theta^4 (I - 5\theta^2)^{-1}] \sin 3g'' \end{aligned}$$

$$\delta_{1I} = -\frac{e'' \delta_{1e}}{\eta^2 \tan I''}$$

$$\begin{aligned} I' = I'' + & \left\{ \frac{1}{8} \gamma_2' \eta^3 [I - 11\theta^2 - 40\theta^4 (I - 5\theta^2)^{-1}] - \frac{5}{12} \frac{\gamma_4'}{\gamma_2'} \eta^3 [I - 3\theta^2 - 8\theta^4 (I - 5\theta^2)^{-1}] \right\} \sin 2g'' \\ & + \left\{ -\frac{1}{4} \frac{\gamma_3'}{\gamma_2'} \frac{\eta^3}{e''} \sin I'' - \frac{5}{64} \frac{\gamma_6'}{\gamma_2' e''} \eta^3 \sin I'' (4 + 9e''^2) [I - 9\theta^2 - 24\theta^4 (I - 5\theta^2)^{-1}] \right\} \cos g'' \\ & + \frac{35}{384} \frac{\gamma_6'}{\gamma_2'} \eta^3 e'' \sin I'' [I - 5\theta^2 - 16\theta^4 (I - 5\theta^2)^{-1}] \cos 3g'' \end{aligned}$$

$$\begin{aligned} g' = g'' + & \left\{ -\frac{1}{16} \gamma_2' [(2 + e''^2) - 11(2 + 3e''^2)\theta^2 - 40(2 + 5e''^2)\theta^4 (I - 5\theta^2)^{-1}] \right. \\ & - 400e''^2 \theta^6 (I - 5\theta^2)^{-2}] + \frac{5}{24} \frac{\gamma_4'}{\gamma_2'} [2 + e''^2 - 3(2 + 3e''^2)\theta^2 - 8(2 + 5e''^2)\theta^4 (I - 5\theta^2)^{-1}] \\ & \left. - 80e''^2 \theta^6 (I - 5\theta^2)^{-2}] \right\} \sin 2g'' + \left\{ \frac{1}{4} \frac{\gamma_3'}{\gamma_2'} \left(\frac{\sin I''}{e''} - \frac{e'' \theta^2}{\sin I''} \right) + \frac{5}{64} \frac{\gamma_6'}{\gamma_2'} \right. \\ & \times \left[\left(\frac{\eta^2 \sin I''}{e''} - \frac{e'' \theta^2}{\sin I''} \right) (4 + 3e''^2) + e'' \sin I'' (26 + 9e''^2) \right] [I - 9\theta^2 - 24\theta^4 (I - 5\theta^2)^{-1}] \\ & - \frac{15}{32} \frac{\gamma_6'}{\gamma_2'} e'' \theta^2 \sin I'' (4 + 3e''^2) [3 + 16\theta^2 (I - 5\theta^2)^{-1} + 40\theta^4 (I - 5\theta^2)^{-2}] \left. \right\} \cos g'' \\ & + \left\{ -\frac{35}{1152} \frac{\gamma_6'}{\gamma_2'} [e'' \sin I'' (3 + 2e''^2) - \frac{e''^2 \theta^2}{\sin I''}] [I - 5\theta^2 - 16\theta^4 (I - 5\theta^2)^{-1}] \right. \\ & \left. + \frac{35}{576} \frac{\gamma_6'}{\gamma_2'} e''^2 \theta^2 \sin I'' [5 + 32\theta^2 (I - 5\theta^2)^{-1} + 80\theta^4 (I - 5\theta^2)^{-2}] \right\} \cos 3g'' \end{aligned}$$

$$\begin{aligned}
h' = h'' + & \left\{ -\frac{1}{8} \gamma_2 e'' \theta [11 + 80\theta^2(1 - 5\theta^2)^{-1} + 200\theta^4(1 - 5\theta^2)^{-2}] \right. \\
& + \frac{5}{12} \frac{\gamma_4'}{\gamma_2'} e'' \theta [3 + 16\theta^2(1 - 5\theta^2)^{-1} + 40\theta^4(1 - 5\theta^2)^{-2}] \left. \right\} \sin 2g'' \\
& + \left\{ \frac{1}{4} \frac{\gamma_2'}{\gamma_2'} \frac{e'' \theta}{\sin I''} + \frac{5}{64} \frac{\gamma_6'}{\gamma_2'} \frac{e'' \theta}{\sin I''} (4 + 3e'' \theta) [1 - 9\theta^2 - 24\theta^4(1 - 5\theta^2)^{-1}] \right. \\
& + \left. \frac{15}{32} \frac{\gamma_6'}{\gamma_2'} e'' \theta \sin I'' (4 + 3e'' \theta) [3 + 16\theta^2(1 - 5\theta^2)^{-1} + 40\theta^4(1 - 5\theta^2)^{-2}] \right\} \cos g'' \\
& + \left\{ -\frac{35}{1152} \frac{\gamma_6'}{\gamma_2'} \frac{e'' \theta}{\sin I''} [1 - 5\theta^2 - 16\theta^4(1 - 5\theta^2)^{-1}] \right. \\
& \quad \left. - \frac{35}{576} \frac{\gamma_2'}{\gamma_2'} e'' \theta \sin I'' [5 + 32\theta^2(1 - 5\theta^2)^{-1} + 80\theta^4(1 - 5\theta^2)^{-2}] \right\} \cos 3g''
\end{aligned}$$

Short-period terms included:

$$\begin{aligned}
a &= a'' \left\{ 1 + \gamma_2 \left[(-1 + 3\theta^2) \left(\frac{a'' \theta}{r' \theta} - \eta^{-3} \right) + 3(1 - \theta^2) \frac{a'' \theta}{r'} \cos (2g' + 2f') \right] \right\} \\
e &= e'' + \delta_1 e + \frac{\eta^2}{2e''} \left\{ \gamma_2 \left[(-1 + 3\theta^2) \left(\frac{a'' \theta}{r' \theta} - \eta^{-3} \right) + 3(1 - \theta^2) \left(\frac{a'' \theta}{r' \theta} - \eta^{-4} \right) \cos (2g' + 2f') \right] \right. \\
& \quad \left. - \gamma_2' (1 - \theta^2) [3e'' \cos (2g' + f') + e'' \cos (2g' + 3f')] \right\} \\
I &= I'' + \delta_1 I + \frac{1}{2} \gamma_2' \theta (1 - \theta^2)^{\frac{1}{2}} [3 \cos (2g' + 2f') + 3e'' \cos (2g' + f') + e'' \cos (2g' + 3f')] \\
l &= l' - \frac{\eta^2}{4e''} \gamma_2' \left\{ 2(-1 + 3\theta^2) \left(\frac{a'' \theta}{r' \theta} \eta^2 + \frac{a''}{r'} + 1 \right) \sin f' \right. \\
& \quad \left. + 3(1 - \theta^2) \left[\left(-\frac{a'' \theta}{r' \theta} \eta^2 - \frac{a''}{r'} + 1 \right) \sin (2g' + f') + \left(\frac{a'' \theta}{r' \theta} \eta^2 + \frac{a''}{r'} + \frac{1}{3} \right) \sin (2g' + 3f') \right] \right\} \\
g &= g' + \frac{\eta^2}{4e''} \gamma_2' \left\{ 2(-1 + 3\theta^2) \left(\frac{a'' \theta}{r' \theta} \eta^2 + \frac{a''}{r'} + 1 \right) \sin f' \right. \\
& \quad \left. + 3(1 - \theta^2) \left[\left(-\frac{a'' \theta}{r' \theta} \eta^2 - \frac{a''}{r'} + 1 \right) \sin (2g' + f') + \left(\frac{a'' \theta}{r' \theta} \eta^2 + \frac{a''}{r'} + \frac{1}{3} \right) \sin (2g' + 3f') \right] \right\} \\
& \quad + \frac{1}{2} \gamma_2' \{ 6(-1 + 5\theta^2)(f' - l' + e'' \sin f') \\
& \quad \quad + (3 - 5\theta^2)[3 \sin (2g' + 2f') + 3e'' \sin (2g' + f') + e'' \sin (2g' + 3f')] \} \\
h &= h' - \frac{1}{2} \gamma_2' \theta [6(f' - l' + e'' \sin f') - 3 \sin (2g' + 2f') \\
& \quad \quad - 3e'' \sin (2g' + f') - e'' \sin (2g' + 3f')].
\end{aligned}$$

f', r' are to be computed from

$$\begin{aligned}
E' - e'' \sin E' &= l' \\
\tan \frac{1}{2} f' &= \left(\frac{1 + e''}{1 - e''} \right)^{\frac{1}{2}} \tan \frac{1}{2} E' & \frac{r'}{a''} \sin f' &= (1 - e''^2)^{\frac{1}{2}} \sin E' \\
\frac{a''}{r'} &= \frac{1 + e'' \cos f'}{1 - e''^2} & \text{or} & \frac{r'}{a''} \cos f' &= \cos E' - e'' \\
& & & \frac{r'}{a''} &= 1 - e'' \cos E'
\end{aligned}$$

For the calculation of the coordinates at any time the complete values of e and l should be used for the solution of Kepler's equation,

$$E - e \sin E = l$$

and subsequently r and f , which may then be used in the formulas:

$$x = r[\cos(g + f) \cos h - \sin(g + f) \sin h \cos I]$$

$$y = r[\cos(g + f) \sin h + \sin(g + f) \cos h \cos I]$$

$$z = r \sin(g + f) \sin I$$

A convenient alternative form is:

$$x = A_x (\cos E - e) + B_x \sin E$$

$$y = A_y (\cos E - e) + B_y \sin E$$

$$z = A_z (\cos E - e) + B_z \sin E$$

$$A_x = a [\cos g \cos h - \sin g \sin h \cos I]$$

$$B_x = -a(1 - e^2)^{\frac{1}{2}} [\sin g \cos h$$

$$+ \cos g \sin h \cos I]$$

$$A_y = a [\sin g \cos h \cos I + \cos g \sin h]$$

$$B_y = a(1 - e^2)^{\frac{1}{2}} [\cos g \cos h \cos I - \sin g \sin h]$$

$$A_z = a \sin g \sin I$$

$$B_z = a(1 - e^2)^{\frac{1}{2}} \cos g \sin I$$

Noted added in proof. The lack of uniformity in notation of the coefficients of the second and fourth harmonics of the earth's potential in papers dealing with the motion of artificial satellites calls for a comment on this subject.

The table below contains a listing of some of the designations used and their relations to the coefficients B_p in the expression of the force function of a body with rotational symmetry,

$$F = \frac{\mu}{r} \left[1 + \sum_{p=2}^{\infty} \frac{B_p P_p(\sin \beta)}{r^p} \right],$$

in which B_p are Legendre polynomials and $\mu = GM$. The expression is an adaptation of the Laplacian expression given by Tisserand.

In addition to the equivalents of B_2 and B_4 the table gives those of the ratio B_4/B_2^2 , which is unity for the special case treated by Vinti (1959), in which the terms with small divisors near the critical inclination vanish. No effort has been made to make the tabulation complete.

Laplace	B_2	B_4	B_4/B_2^2	Tisserand, <i>Mé. Ch.</i> 11, 320, 1890
H. Struve	$-\frac{2}{3}k$	$\frac{2}{3}l$	$\frac{3}{2}l/k^2$	<i>Suppl. I, Obs. Pulkovo</i> 1888
W. de Sitter	$-\frac{2}{3}JK^2$	$\frac{4}{15}KR^2$	$\frac{3}{5}K/J^2$	<i>B. A. N.</i> 2, 97, 1924
D. Brouwer	$-2k_2$	$\frac{8}{3}k_4$	$\frac{2}{3}k_4/k_2^2$	<i>J. J.</i> 51, 223, 1946
H. Jeffreys	$-\frac{2}{3}JK^2$	$\frac{8}{35}DK^2$	$\frac{18}{35}D/J^2$	<i>M. N.</i> 14, 433, 1954
Y. Kozai	$-\frac{2}{3}A_2$	$\frac{8}{35}A_4$	$\frac{18}{35}A_4/A_2^2$	
P. Herget and P. Mussen	$-2k_2$	$8k_4$	$2k_4/k_2^2$	<i>J. J.</i> 63, 430, 1958
J. O'Keefe et al.	$+ .12\omega/\mu$	$+ .14\omega/\mu$	$\mu .14\omega/A_2\omega^2$	<i>J. J.</i> 64, 235, 1959
B. Garfinkel	$-2k$	k'	$\frac{1}{4}k'/k^2$	This issue
J. Vinti	$-J_2R^2$	$-J_4R^4$	J_4/J_2^2	<i>J. of Res. Nat. Bureau of Standards</i> 62B, 105, 1959

In the table R represents the earth's equatorial radius. Ignoring the presence of R^2 and differences in sign, essentially three different coefficients for the second

harmonic have been used in recent papers. For the coefficients of the fourth harmonic six different choices are listed. I now regret that I introduced k_2 , k_4 in my paper in 1946. The principal reason was that they give a particularly simple form for the expression of the potential in the equatorial plane. If I could have foreseen the increase in interest in the subject and the confusion to which I was contributing, I would have chosen the coefficients B_p or the alternative form

$$V = \frac{\mu}{r} \left[1 - \sum_{p=2}^{\infty} J_p \left(\frac{R}{r} \right)^p P_p(\sin \beta) \right],$$

which was used by Vinti (1959). I intend to revert to this form and recommend this to other authors.

APPENDIX II

Short Period Term for a

From Brouwer, SPT is

$$1 + \gamma_2 \left[(-1 + 3\theta^2) \left(\frac{a^{n3}}{r'^3} - \eta^{-3} \right) + 3(1 - \theta^2) \frac{a^{n3}}{r'^3} \cos(2g' + 2f') \right]$$

Rewrite

$$1 + \gamma_2 \left[\underbrace{(-1 + 3\theta^2)}_{D(6)} \underbrace{\left(\frac{a^{n3}}{r'^3} - \eta^{-3} \right)}_{\substack{X(11) \\ B(8)}} + \frac{a^{n3}}{r'^3} \underbrace{3(1 - \theta^2)}_{D(19)} \underbrace{\cos(2g' + 2f')}_{X(21)} \right]$$

$\underbrace{\hspace{10em}}_{X(22)} \qquad \underbrace{\hspace{10em}}_{X(23)}$

$$SPT = 1. + C(1) * (X(22) + X(11) * X(23))$$

Short Period Term for e

$$\frac{\eta^2}{2e''} \left\{ \gamma_2 \left[\underbrace{(-1 + 3\theta^2)}_{C(1)} \underbrace{\left(\frac{a^{n3}}{r'^3} - \eta^{-3} \right)}_{X(22)} + \underbrace{\left(\frac{a^{n3}}{r'^3} - \eta^{-4} \right)}_{\substack{X(11) \\ B(9)}} \underbrace{3(1 - \theta^2) \cos(2g' + 2f')}_{X(23)} \right] - \gamma_2' (1 - \theta^2) \underbrace{[3e'' \cos(2g' + f') + e'' \cos(2g' + 3f')]}_{X(24)} \right\}$$

$\underbrace{\hspace{10em}}_{D(23)} \qquad \underbrace{\hspace{10em}}_{X(24)}$

$$SPT_e = G(12) * (C(1) * (X(22) + X(23)) * (X(11) - B(9))) - D(23) * X(24)$$

Short Period Term for Inclination

$$\frac{1}{2} \gamma_2' \theta (1 - \theta^2)^{1/2} \underbrace{[3 \cos(2g' + 2f')]}_{D(22)} + e'' \underbrace{[3 \cos(2g' + f') + \cos(2g' + 3f')]}_{X(24)}$$

$\underbrace{\hspace{10em}}_{X(21)}$

$$SPT_i = D(22) * (3 * X(21) + X(24))$$

Short Period Term for l

$$\begin{array}{c}
 \frac{\eta^2}{4e^{f'}} \gamma_2' \left\{ 2(-1 + 3\theta^2) \left(\frac{a''^2}{r'^2} \eta^2 + \frac{a''}{r'} + 1 \right) \sin f' + 3(1 - \theta^2) \left[\left(-\frac{a''^2}{r'^2} \eta^2 - \frac{a''}{r'} + 1 \right) \sin (2g' + f') + \left(\frac{a''^2}{r'^2} \eta^2 + \frac{a''}{r'} + \frac{1}{3} \right) \sin (2g' + 3f') \right] \right\} \\
 \begin{array}{cccccccc}
 \uparrow & & & & \uparrow & & & \uparrow \\
 \text{B(2)*G(13)} & \text{D(20)} & \text{X(25)} & \text{X(12)} & \text{D(19)} & \text{X(25)} & \text{X(19)} & \text{X(25)} & \text{X(20)} \\
 & & & & & & & & \vdots \\
 & & & & & & & & \text{X(26)}
 \end{array}
 \end{array}$$

$$\text{SPT}_M = \text{B(2)*X(26)}$$

Short Period Term for g

$$\begin{array}{c}
 + \frac{\eta^2}{4e^{f'}} \gamma_2' \left\{ 2(-1 + 3\theta^2) \left(\frac{a''^2}{r'^2} \eta^2 + \frac{a''}{r'} + 1 \right) \sin f' \right. \\
 \left. + 3(1 - \theta^2) \left[\left(-\frac{a''^2}{r'^2} \eta^2 - \frac{a''}{r'} + 1 \right) \sin (2g' + f') + \left(\frac{a''^2}{r'^2} \eta^2 + \frac{a''}{r'} + \frac{1}{3} \right) \sin (2g' + 3f') \right] \right\} \\
 \text{X(26)} \\
 + \frac{1}{4} \gamma_2' \left\{ 6(-1 + 5\theta^2) (f' - l' + e'' \sin f') + (3 - 5\theta^2) [3 \sin (2g' + 2f') + 3e'' \sin (2g' + f') + e'' \sin (2g' + 3f')] \right\} \\
 \begin{array}{cccccccc}
 \uparrow & & & & & & & \uparrow \\
 \text{C(9)} & \text{D(7)} & \text{X(27)/6} & \text{D(21)} & \text{X(17)} & \text{X(19)} & \text{X(20)} & \text{X(28)}
 \end{array}
 \end{array}$$

$$\text{SPT} = \text{X(26)} + \text{C(9)} * (\text{D(7)} * \text{X(27)} + \text{D(21)} * \text{X(28)})$$

Short Period Terms for h

$$\frac{1}{2}\gamma_2'\theta[6(f' - l' + e'' \sin f') - 3 \sin(2g' + 2f') - 3e'' \sin(2g' + f') - e'' \sin(2g' + 3f')], \quad (27)$$

\uparrow X(27) X(28)

C(10)

$$\text{SPT} = \text{C}(10) * (\text{X}(27) - \text{X}(28))$$

Secular terms:

$l'' =$ "mean" mean anomaly

$$= n_0 \left\{ 1 + \frac{3}{2}\gamma_2'\eta(-1 + 3\theta^2) + \frac{3}{32}\gamma_2'^2\eta[-15 + 16\eta + 25\eta^2 + (30 - 96\eta - 90\eta^2)\theta^2] + (105 + 144\eta + 25\eta^2)\theta^4 + \frac{15}{16}\gamma_4'\eta e''^2[3 - 30\theta^2 + 35\theta^4] \right\} t + l_0''$$

S(1)

$g'' =$ mean argument of perigee

$$= n_0 \left\{ \frac{3}{2}\gamma_2'\eta(-1 + 5\theta^2) + \frac{3}{32}\gamma_2'^2\eta[-35 + 24\eta + 25\eta^2 + (90 - 192\eta - 126\eta^2)\theta^2] + (385 + 360\eta + 45\eta^2)\theta^4 + \frac{5}{16}\gamma_4'\eta[21 - 9\eta^2 + (-270 + 126\eta^2)\theta^2 + (385 - 189\eta^2)\theta^4] \right\} t + g_0''$$

S(2)

$h'' =$ mean longitude of ascending node

$$= n_0 \left\{ -3\gamma_2'\theta + \frac{3}{8}\gamma_2'^2\eta[(-5 + 12\eta + 9\eta^2)\theta + (-35 - 36\eta - 5\eta^2)\theta^2] + \frac{5}{4}\gamma_4'\eta(5 - 3\eta^2)\theta(3 - 7\theta^2) \right\} t + h_0''$$

S(3)

Long-period terms:

EL(10)

$$\delta_1 e = \left\{ \frac{1}{8}\gamma_2'e''\eta^2[1 - 11\theta^2 - 40\theta^4(1 - 5\theta^2)^{-1}] - \frac{5}{12}\frac{\gamma_4'}{\gamma_2'}e''\eta^2[1 - 3\theta^2 - 8\theta^4(1 - 5\theta^2)^{-1}] \right\} \cos 2g'' + \left\{ \frac{1}{4}\frac{\gamma_6'}{\gamma_2'}\eta^2 \sin I'' + \frac{5}{64}\frac{\gamma_6'}{\gamma_2'\eta^2} \sin I'' (4 + 3e''^2)[1 - 9\theta^2 - 24\theta^4(1 - 5\theta^2)^{-1}] \right\} \sin g''$$

EL(11)

$$- \frac{35}{384}\frac{\gamma_6'}{\gamma_2'}e''^2\eta^2 \sin I'' [1 - 5\theta^2 - 16\theta^4(1 - 5\theta^2)^{-1}] \sin 3g''$$

EL(12)

$$\delta_1 I = -\frac{e'' \delta_1 e}{\eta^2 \tan I''} = \text{EL}(13) * \delta_1 e$$

Long Period Terms

$$l' = l'' + \left\{ \frac{1}{8} \gamma_2' \eta' [1 - 11\theta^2 - 40\theta^4(1 - 5\theta^2)^{-1}] - \frac{5}{12} \frac{\gamma_4'}{\gamma_2'} \eta^2 [1 - 3\theta^2 - 8\theta^4(1 - 5\theta^2)^{-1}] \right\} \sin 2g'' + \left\{ -\frac{1}{4} \frac{\gamma_2'}{\gamma_2'} \frac{\eta^2}{e''} \sin I'' - \frac{5}{64} \frac{\gamma_6'}{\gamma_2'} \frac{\eta^2}{e''} \sin I'' (4 + 9e''^2) [1 - 9\theta^2 - 24\theta^4(1 - 5\theta^2)^{-1}] \right\} \cos g'' + \frac{35}{384} \frac{\gamma_6'}{\gamma_2'} \eta^2 e'' \sin I'' [1 - 5\theta^2 - 16\theta^4(1 - 5\theta^2)^{-1}] \cos 3g''$$

\uparrow A11(6) \uparrow C(5) \uparrow B(3) \uparrow D(10) \uparrow X(3) \uparrow C(7) \uparrow F(5) \uparrow X(4) \uparrow X(5)

$\underbrace{\hspace{15em}}_{D(11)} \quad \underbrace{\hspace{15em}}_{EL(2)} \quad \underbrace{\hspace{15em}}_{EL(3)}$

$\underbrace{\hspace{15em}}_{B(3) * D(11)} \quad \underbrace{\hspace{15em}}_{EL(1)}$

$$l' = l'' + EL(1) * X(3) + EL(2) * X(4) + EL(3) * X(5)$$

$$g' = g'' + \left[\begin{array}{l} -\frac{1}{16} \gamma_2' [(2 + e''^2) - 11(2 + 3e''^2)\theta^2 - 40(2 + 5e''^2)\theta^4(1 - 5\theta^2)^{-1}] \\ -400e''^2\theta^6(1 - 5\theta^2)^{-2} + \frac{5}{24} \frac{\gamma_4'}{\gamma_2'} [2 + e''^2 - 3(2 + 3e''^2)\theta^2 - 8(2 + 5e''^2)\theta^4(1 - 5\theta^2)^{-1}] \\ -80e''^2\theta^6(1 - 5\theta^2)^{-2} \end{array} \right] \sin 2g'' + \left[\begin{array}{l} \frac{1}{4} \frac{\gamma_2'}{\gamma_2'} \left(\frac{\sin I''}{e''} - \frac{e''\theta^2}{\sin I''} \right) + \frac{5}{64} \frac{\gamma_6'}{\gamma_2'} \\ \left(\frac{\eta^2 \sin I''}{e''} - \frac{e''\theta^2}{\sin I''} \right) (4 + 3e''^2) + e'' \sin I'' (26 + 9e''^2) [1 - 9\theta^2 - 24\theta^4(1 - 5\theta^2)^{-1}] \\ -\frac{15}{32} \frac{\gamma_6'}{\gamma_2'} e''\theta^2 \sin I'' (4 + 3e''^2) [3 + 16\theta^2(1 - 5\theta^2)^{-1} + 40\theta^4(1 - 5\theta^2)^{-2}] \end{array} \right] \cos g''$$

\uparrow EL(4) \uparrow X(3) \uparrow EL(5) \uparrow X(4)

$$g' = g'' + EL(4) * X(3) + EL(5) * X(4) + EL(6) * X(5)$$

$$\uparrow \quad \uparrow \quad \uparrow$$

A1(5) A11(5) \uparrow X(5)

$$h' = h'' + \left\{ -\frac{1}{8} \gamma_2' e''^2 \theta [11 + 80\theta^2(1 - 5\theta^2)^{-1} + 200\theta^4(1 - 5\theta^2)^{-2}] + \frac{5}{12} \frac{\gamma_4'}{\gamma_2'} e''^2 \theta [3 + 16\theta^2(1 - 5\theta^2)^{-1} + 40\theta^4(1 - 5\theta^2)^{-2}] \right\} \sin 2g'' + \left\{ \frac{1}{4} \frac{\gamma_2'}{\gamma_2'} \frac{e''\theta}{\sin I''} + \frac{5}{64} \frac{\gamma_6'}{\gamma_2'} \frac{e''\theta}{\sin I''} (4 + 3e''^2) [1 - 9\theta^2 - 24\theta^4(1 - 5\theta^2)^{-1}] + \frac{15}{32} \frac{\gamma_6'}{\gamma_2'} e''\theta \sin I'' (4 + 3e''^2) [3 + 16\theta^2(1 - 5\theta^2)^{-1} + 40\theta^4(1 - 5\theta^2)^{-2}] \right\} \cos g'' + \left\{ -\frac{35}{1152} \frac{\gamma_6'}{\gamma_2'} \frac{e''^2 \theta}{\sin I''} [1 - 5\theta^2 - 16\theta^4(1 - 5\theta^2)^{-1}] - \frac{35}{576} \frac{\gamma_6'}{\gamma_2'} e''^2 \theta \sin I'' [5 + 32\theta^2(1 - 5\theta^2)^{-1} + 80\theta^4(1 - 5\theta^2)^{-2}] \right\} \cos 3g''$$

\uparrow EL(7) \uparrow X(3) \uparrow EL(8) \uparrow X(4) \uparrow EL(9) \uparrow X(5)

$$h' = h'' + EL(7) * X(3) + EL(8) * X(4) + EL(9) * X(5)$$

APPENDIX III (PART A)

PROGRAM OPERATING INSTRUCTIONS
FOR MAIN PROGRAM ONE

```

@PPRATING INSTRUCTIONS
      FOR
      MUSTAP PROGRAM
@PPRATING NOTES FOR MUSTAP PROGRAM.
PURPOSES--
      THE MUSTAP PROGRAM IS ONE DESIGNED TO COMPUTE MUTUAL VISIBILITY
, LOCAL STATION PREDICTIONS, SPACECRAFT LOOK ANGLES, AND WORLD MAPS OF
COMMUNICATION SATELLITES.
INPUT--
      INPUT TO THE PROGRAM CONSISTS OF CONTROL OPTIONS, TEST CRITERIA,
EPOCH, ORBITAL ELEMENTS OR POSITION AND VELOCITY VECTORS, START AND STOP
TIMES WITH PREDICTION INTERVAL, ATTITUDE DATA, AND STATION COORDINATES.
METHOD--
      THE PATH OF THE SATELLITE IS COMPUTED BY AN INTERNAL ORBIT
GENERATOR. THE POSITION OF THE SPACECRAFT WITH RESPECT TO EACH STATION
IS COMPUTED AND TESTED AGAINST THE SPECIFIED CRITERIA. OUTPUT STATEMENTS
ARE ARRANGED TO PRESENT THE DATA IN THE MOST USEFUL MANNER TO THE PROJECT.
OUTPUT--
      OUTPUT DATA ARE WRITTEN ON TWO MAGNETIC TAPES--(1) MUTUAL VISIBILITY
(2) WORLD MAP, PREDICTIONS AND TIME THE SATELLITE IS IN SHADOW. THE MUTUAL
VISIBILITY DATA ARE PRESENTED IN GRAPHICAL FORM. THE OTHER DATA ARE S/C
LATITUDE, LONGITUDE, HEIGHT, AZIMUTH, ELEVATION, RANGE, AND SPACECRAFT
LOOK ANGLE (THE ANGLE BETWEEN THE S/C SPIN AXIS AND THE LINE TO THE STATION).
FOR CHECKOUT PURPOSES A SENSE SWITCH CAN BE DOWN AND THE INPUT WILL BE
WRITTEN ON--LINE.
PROGRAM INPUT DATA INSTRUCTIONS.
INPUT DATA--
      ALL INPUT DATA ARE ON CARDS (READ ON--LINE).
CARD 1-- IDENTIFICATION CARD (FORMAT 2(6A6))--ANY DESCRIPTIVE DATA
NOTE ---
      THIS IDENTIFICATION IS OUTPUT ON 2 LINES --
      LINE 1 -CONTENTS OF COLUMNS 1-36
      LINE 2 -CONTENTS OF COLUMNS 37-72
CARD 2--CONTROL CARD (FORMAT 8(3,F10,1))
COLUMN
1-3 TYPE OF INPUT +01 = OSCULATING ORBITAL ELEMENTS
+03 = INERTIAL R AND V VECTORS, CANONICAL UNITS
+04 = BROUWER MEAN ELEMENTS
4-6 WORLD MAP +01 = COMPUTE WORLD MAP AND PREDICTIONS
+00 = DO NOT COMPUTE WORLD MAP AND PREDICTIONS
-01 = DO NOT COMPUTE WORLD MAP AND PREDICTIONS
7-9 LOOK ANGLE +01 ALWAYS
10-12 EARTH CONST. -03 = USE INTERNATIONAL CONSTANTS WITH
HARMONICS EQUAL TO ZERO.
-02 = USE GODDARD EARTH CONSTANTS WITH
HARMONICS EQUAL TO ZERO.
-01 = USE SIRY PACKAGE CONSTANTS
+00 = USE GODDARD EARTH CONSTANTS
+01 = READ A NEW SET OF EARTH CONSTANTS
([INPUT ON CARDS 4-5])
13-15 TRUNCATION -01 = USE INTERNAL VALUE
+00 = USE INTERNAL VALUE
+01 = READ NEW TRUNCATION FACTOR -- CARD 3
(USED AS CRITERIA TO SOLVE KPFLER'S EQ.)
16-18 BRWR TRUNCATION -01 = USE INTERNAL VALUES
+00 = USE INTERNAL VALUES
+01 = READ NEW TRUNCATION FACTORS FOR
SUBROUTINE BRWR -- CARD 6
19-21 BLANK -- USED INTERNALLY
22-24 POSITIVE N -- N CONTROL STATIONS (THEY ARE THE FIRST N

```

STATIONS.)
N MUST BE LFSS THAN OR EQUAL TO THE NUMBER OF STATIONS GIVEN
ON CARD 11.

25-34 MAXIMUM RANGE FOR STATIONS IN NAUTICAL MILES. A T IS PRINTED
ON THE MUTUAL VISIBILITY OUTPUT,WHFN THE RANGE IS LARGER
THAN THIS VALUF.

CARD 3 -- NEW TRUNCATION FACTØR (ØMIT THIS CARD UNLESS CØLUMNS 13-15
OF CARD 2 ARF = +01) (FØRMT FØ.2)

CØLUMN
1-8 NFW TRUNCATION FACTØR

CARD 4 -- EARTH CØNSTANTS (ØMIT UNLESS CØLUMNS 10-12 ØF
CARD 2 = +01) (FØRMT F12.6,F12.5)

CØLUMN
1-12 NFW G⁴ ØF THE EARTH (KM. CUBFD/ SFCØNDS SQUARD)
13-24 J₂)
25-36 J₃) HARMØNICS ØF THE GRAVITATIONAL PØTENTIAL ØF
37-48 J₄) THE EARTH
49-60 J₅)

CARD 5 -- EARTH CØNSTANTS CØNTINUED (ØMIT UNLESS CØLUMNS 10-12
ØF CARD 2 = +01) (FØRMT 2F12.4)

CØLUMN
1-12 INVFRSE ØF FLATTENING
13-24 EQUATØRIAL RADIUS ØF THE EARTH IN KM

CARD 6 -- NEW TRUNCATION FACTØRS FOR SUBRØUTINE BØRNR (ØMIT UNLESS
CØLUMNS 10-18 ØF CARD 2 ARE = +01) (FØRMT 6F12.8)
TRUNCATION FACTØRS USED IN CØMPUTING BRØUWER MEAN
ELEMENTS FRØM ØSCULATING ELFHNENTS ---

CØLUMN
1-12 (SEMI-MAJØR AXIS - KM
13-24 (ECCFNTPICITY - KM
25-36 FACTØR FOR (INCLINATION - DEGRFES
37-48 (R.A. ASC. NØDF - DEGRFES
49-60 (ARG. ØF PFRIGFF - DEGRFES
61-72 (MEAN ANØVALY - DEGRFES

CARD 7 -- EPOCH CARD (TIME AT WHICH PARAMETERS APPLY)
FØRMT 1X,A5,X,3I2,X,2I2,X,F4.2,39X,15)

CØLUMN
1 PLANK
2-6 SATELLITE IDENTIFICATION NUMBER
8-9 VFAP (ABBFRVIATF)
10-11 MONTH
12-13 DAY
15-16 HOUR)
17-18 MINUTE) UNIVFRSAL TIME
20-24 SFCØNDS)
63-67 ØRBIT NUMBER AT THE START TIME GIVEN ØN CARD 10

CARD 8 -- PARAMETER CARD (THFSE DATA MUST BE CØHØEN IN ACCØRDANCE
WITH THE INSTRUCTION ØN CARD 2, CØLUMNS 1-3)
(FØRMT 6F12.8) +XXXXXXXXXX

--ØØ NØT LEAVE THE SIGN ØF THE EXPØNENT BLANK--

VECTØRS (+Ø3) REQUIRF THE FØLLØIING

CØL
1-12 X VUL
13-24 Y VUL
25-36 Z VUL
37-48 X-DØT VUL/VUT
49-60 Y-DØT VUL/VUT
61-72 Z-DØT VUL/VUT

ELFHNENTS (+Ø1 AND +Ø4) REQUIRF THE FØLLØIING

CØL
1-12 SEMI-MAJØR AXIS VUL
13-24 ECCFNTPICITY
25-36 INCLINATION RADIANS
37-48 MEAN ANØVALY RADIANS
49-60 ARGUMENT ØF PFRIGFF RADIANS
61-72 R.A. ØF ASCENDING NØDF RADIANS

ØNE VUL = 6378.388 KILØMETERS
ØNE VUL/VUT = 6378.388 KM / 806.832 SEC
RECTANGULAR CØØRDINATES ARE ØFFINED TO BE IN AN INERTIAL,
EQUATØRIAL, GØCØNTRIC SYSTEM. X GØES THROUGH ARIES, Y IS
IN EQUATØRIAL PLANE, Z IS ALØNG PØLAR AXIS TØ FØRM A RIGHT
HANDED SYSTEM.

CARD 9 -- DRAG CARD (FØRMT A46.1X,E12.8)

CØL
1-24 SAME AS EPOCH CARD
25 PLANK
26-37 ACCELERATION ØF MEAN ANØVALY(N2 DRAG TERM AT GSFC) IN
UNITS ØF RADIANS / VUT SQUARFD. +XXXXXXXXXX

CARD 10 -- PREDICTION AND MUTUAL VISIBILITY REQUEST CARD
(FØRMT 2I1I2,1X,14,2I3,F7.3,13,1X,12,1X,1,2I3,
F7.3,F11,3)

CØL FØRMT
2-3 MONTH IZ

5-6 DAY)) I2
 8-11 YEAR (DO NOT ABRFVIATF)) START I4
 13-14 HOUR)) TIME I2
 16-17 MINUTE) UNIVERSAL TIME) I2
 19-24 SECOND)) F6.3
 26-27 MONTH)) I2
 29-30 DAY)) I2
 32-35 YEAR (DO NOT ABRFVIATF)) END I4
 37-38 HOUR)) TIME I2
 40-41 MINUTE) UNIVERSAL TIME) I2
 43-48 SECOND)) F6.3
 49-59 PREDICTION INTERVAL, SECOND) F11.3

CARD 11--STATION CONTROL CARD (FORMAT 313,F10,0,51X,I2)

COL
 1-3 NO. OF STATION COORDINATE CARDS TO BE LOADED
 N.B., THE MAXIMUM NUMBER OF STATIONS THAT CAN BE CONSIDERED IS NINETY (19).
 4-6 = BLANK OR +00
 7-9 = +XX LOWEST ELEVATION ANGLE FOR WHICH THE STATIONS CAN OBSERVE THE SPACECRAFT.
 10-19= BLANK (READ BUT NOT USED)
 20-70= BLANK (NOT READ)
 71-72= BLANK FOR NORMAL RUNS. OUTPUT FOR A PASS IS GIVEN WHEN THERE IS MUTUAL VISIBILITY BETWEEN AT LEAST TWO STATIONS (ONE OF WHICH IS A CONTROL STATION) DURING THE PASS.
 +XX UNEQUAL TO ZERO -- KILLS MUTUAL VISIBILITY REQUIREMENT-- GIVES OUTPUT ANYTIME THE SPACECRAFT IS VISIBLE TO ANY OF THE STATIONS.

(WHEN COLUMNS 1-3 OF THIS CARD ARE LESS THAN OR EQUAL TO ZERO, A NEW JOB IS STARTED BY READING CARD 1.)

CARD 12--ATTITUDE DATA CARD (FORMAT 4F6,1,I6)

COL
 1-12 READ BUT NOT USED
 13-18 RIGHT ASCENSION OF S/C SPIN AXIS, DEGREES
 19-24 DECLINATION OF S/C SPIN AXIS, DEGREES
 25-30 +00 USE THE INPUT VALUES OF RT, ASCENSION AND DECLINATION TO DEFINE SPIN AXIS DIRECTION
 +XX (POSITIVE) ASSUME SPIN AXIS IS ALONG THE INITIAL INERTIAL VELOCITY VECTOR

N.B., RIGHT ASCENSION AND DECLINATION ARE AT THE EPOCH GIVEN ON CARD 3. THESE ANGLES ARE ASSUMED CONSTANT.

CARD 13 -- STATION COORDINATE CARD (S)

COL	NAME	FORMAT
2-7	LONGITUDE, DEGREES (+FAST)	A6
9-12	LONGITUDE, MINUTES	I4
14-15	LONGITUDE, SECONDS	I2
17-22	LATITUDE, DEGREES (+NORTH)	F6.3
24-26	LATITUDE, MINUTES	I3
28-29	LATITUDE, SECONDS	I2
31-36	ALTITUDE, METERS	F6.3
37-47	ALTITUDE, METERS	F11.2

N.B., THERE MUST BE AS MANY STATION COORDINATE CARDS AS INDICATED BY CARD 11.

THE STATION COORDINATE CARDS ARE FOLLOWED BY ANOTHER STATION CONTROL CARD OR BY A BLANK. IF THE NUMBER IN COLUMNS 1-3 OF THIS CARD IS NEGATIVE OR ZERO, A NEW JOB IS STARTED BY READING CARD 1. IF THE NUMBER IN COLUMNS 1-3 OF THIS CARD IS POSITIVE, NEW ATTITUDE DATA AND COORDINATE CARDS ARE READ. MUTUAL VISIBILITY AND PREDICTIONS ARE THEN COMPUTED FOR THE NEW STATIONS AND ATTITUDE FOR TIMES GIVEN ON CARD 10.

JOB'S MAY BE STACKED BY PLACING A BLANK CARD AFTER THE LAST STATION COORDINATE CARD. CARD 1 OF THE NEW JOB THEN FOLLOWS THIS BLANK CARD.

PLACE 3 BLANK CARDS AFTER THE LAST STATION COORDINATE CARD IN THE LAST INPUT DECK OF THE JOB. THIS WILL RESULT IN THE CORRECT FINAL HALT -- HPR 77777.

PUT SENSE SWITCH 3 DOWN TO TERMINATE RUN BEFORE THE END TIME IS REACHED.

VALUF	EARTH CONSTANTS STORED IN THE PROGRAM		
	INTERNATIONAL	GOODARD	SIRY
GM	+3.986268730E+05	+3.986032000E+05	+3.986268800E+05
J2	0.0	+1.0823E-03	+1.08219E-03
J3	0.0	+2.3F-06	-2.88E-06
J4	0.0	-1.8E-06	-2.123F-06
J5	0.0	0.0	-2.32F-07
F	297.0	298.3	297.0
A	6378.388	6378.165	6378.388

RUNNING INSTRUCTIONS.

0
0
0
0
0
0
0

Mount PROGRAM SYSTEM TAPF ON A1
Mount BLANK TAPFS ON A3, A5, A8
No KEYS ON SENSE SWITCHES.
PUT INPUT CARDS IN READER AND READER READER.
CLEAR AND LOAD TAPF.
FINAL STOP IS HPR 77777

HALTS --

HPR 00010 MACHINE IS NOT IN 65K
HPR 54321 MORE THAN 19 CONTROL STATIONS ARE BEING USED. THE
PROGRAM CAN NOT RUN.
HPR 54333 THE NUMBER OF CONTROL STATIONS IS LARGER THAN THE NUMBER
OF STATIONS.
HPR 66666 MORE THAN 19 STATIONS ARE BEING USED. THE PROGRAM
CAN NOT RUN.
HPR 77774 SENSE SWITCH 2 IS DOWN FOR TIMING PURPOSES -- END OF
PREDICTIONS. HIT START TO CONTINUE.
HPR 77775 SENSE SWITCH 2 IS DOWN FOR TIMING PURPOSES -- BEGINNING
OF PREDICTIONS. HIT START TO CONTINUE.
HPR 77777 FINAL (END OF JOB)

PRINT OUTPUT TAPF A3
(1) NARROW PAPER WHEN THERE ARE 15 OR LESS STATIONS
(2) WIDE PAPER WHEN THERE ARE 16 TO 19 STATIONS
PRINT OUTPUT TAPF A8 ON NARROW PAPER.

APPENDIX III (PART B)
PROGRAM OPERATING INSTRUCTIONS
FOR MAIN PROGRAM TWO

OPERATING INSTRUCTIONS

FOR

MUSTAP PROGRAM

```

0
0 OPERATING NOTES FOR MUSTAP PROGRAM.
0
0 PURPOSE--
0 THE MUSTAP PROGRAM IS ONE DESIGNED TO COMPUTE MUTUAL VISIBILITY,
LOCAL STATION PREDICTIONS, SPACECRAFT LOOK ANGLES, AND WORLD MAPS OF
COMMUNICATION SATELLITES.
0
0 INPUT--
0 INPUT TO THE PROGRAM CONSISTS OF CONTROL OPTIONS, TEST CRITERIA,
EPOCH, ORBITAL ELEMENTS OR POSITION AND VELOCITY VECTORS, START AND STOP
TIMES WITH PREDICTION INTERVAL, ATTITUDE DATA, AND STATION COORDINATES.
0
0 METHOD--
0 THE PATH OF THE SATELLITE IS COMPUTED BY AN INTERNAL ORBIT
GENERATOR. THE POSITION OF THE SPACECRAFT WITH RESPECT TO EACH STATION
IS COMPUTED AND TESTED AGAINST THE SPECIFIED CRITERIA. OUTPUT STATEMENTS
ARE ARRANGED TO PRESENT THE DATA IN THE MOST USEFUL MANNER TO THE PROJECT.
0
0 OUTPUT--
0 OUTPUT DATA ARE WRITTEN ON TWO MAGNETIC TAPES--(1) MUTUAL VISIBILITY
AND WORLD MAP (2) PREDICTIONS. FOR CHECKOUT PURPOSES A SENSE SWITCH CAN BE
DOWN AND ALL DATA WILL BE WRITTEN ON-LINE. THE MUTUAL VISIBILITY DATA ARE
PRESENTED IN GRAPHICAL FORM. THE OTHER DATA ARE S/C LATITUDE, LONGITUDE,
AND HEIGHT FOR EACH TIME STEP, AZIMUTH, ELEVATION, RANGE, AND SPACECRAFT
LOOK ANGLE (THE ANGLE BETWEEN THE S/C SPIN AXIS AND THE LINE TO THE STATION)
FOR EACH STATION.
0
0 PROGRAM INPUT DATA INSTRUCTIONS.
0
0 INPUT DATA--
0 ALL INPUT DATA ARE ON CARDS (READ ON-LINE).
0
0 CARD 1--IDENTIFICATION CARD (FORMAT 12A6)--ANY DESCRIPTIVE DATA
0
0 CARD 2--CONTROL CARD (FORMAT 713)
0
0 COLUMN
0 1-3 TYPE OF INPUT +01 = OSCILLATING ORBITAL ELEMENTS
+02 = INERTIAL R AND V VECTORS, KGS SYSTEM
+03 = INERTIAL R AND V VECTORS, CANONICAL UNITS
+04 = BROWNER MEAN ELEMENTS
0 4-6 WORLD MAP +01 = COMPUTE WORLD MAP
+00 = DO NOT COMPUTE MAP
-01 = DO NOT COMPUTE MAP
0 7-9 LOOK ANGLE +01 = COMPUTE MUTUAL VISIBILITY
+00 = DO NOT COMPUTE MUTUAL VISIBILITY
-01 = DO NOT COMPUTE MUTUAL VISIBILITY
0 10-12 EARTH CONST. -03 = USE INTERNATIONAL CONSTANTS WITH
HARMONICS EQUAL TO ZERO.
-02 = USE GODDARD EARTH CONSTANTS WITH
HARMONICS EQUAL TO ZERO.
-01 = USE SIRY PACKAGE CONSTANTS
+00 = USE GODDARD EARTH CONSTANTS
+01 = READ A NEW SET OF EARTH CONSTANTS
(INPUT ON CARDS 4-5)
0 13-15 TRUNCATION -01 = USE INTERNAL VALUE
+00 = USE INTERNAL VALUE
+01 = READ NEW TRUNCATION FACTOR -- CARD 3
(USED AS CRITERIA TO SOLVE KEPLER'S EQ.)
0 16-18 BBRWR TRUNCATION -01 = USE INTERNAL VALUES
+00 = USE INTERNAL VALUES
+01 = READ NEW TRUNCATION FACTORS FOR
SUBROUTINE BBRWR -- CARD 6
0
0 CARD 3 -- NEW TRUNCATION FACTOR ( OMIT THIS CARD UNLESS COLUMNS 13-15
OF CARD 2 ARE = +01 ) (FORMAT E8.2)

```

COLUMN
1-8 NFW TRUNCATION FACTOR

CARD 4 -- EARTH CONSTANTS (OMIT UNLESS COLUMNS 10-12 OF
CARD 2 = +01) (FORMAT F12.6,4E12.5)

COLUMN
1-12 NEW GM OF THE EARTH (KM. CUBED/ SECONDS SQUARED)
13-24 J2)
25-36 J3) HARMONICS OF THE GRAVITATIONAL POTENTIAL OF
37-48 J4) THE EARTH
49-60 J5)

CARD 5 -- EARTH CONSTANTS CONTINUED (OMIT UNLESS COLUMNS 10-12
OF CARD 2 = +01) (FORMAT 2F12.4)

COLUMN
1-12 INVERSE OF FLATTENING
13-24 EQUATORIAL RADIUS OF THE EARTH IN KM

CARD 6 -- NEW TRUNCATION FACTORS FOR SUBROUTINE BBRWR (OMIT UNLESS
COLUMNS 16-18 OF CARD 2 ARE = +01) (FORMAT 6F12.8)
TRUNCATION FACTORS USED IN COMPUTING BROUWER MEAN
ELEMENTS FROM OSCULATING ELEMENTS ---

COLUMN
1-12 (SEMI-MAJOR AXIS - KM
13-24 (ECCENTRICITY
25-36 FACTOR FOR (INCLINATION - DEGREES
37-48 (R.A. ASC. NODE - DEGREES
49-60 (ARG. OF PERIGEE - DEGREES
61-72 (MEAN ANOMALY - DEGREES

CARD 7 -- EP@CH CARD (TIME AT WHICH PARAMETERS APPLY)

COL.	MONTH	DAY	YEAR (DO NOT ABBREVIATE)	HOUR	MINUTE	SECOND
2-3						
5-6						
8-11						
13-14						
16-17						
19-24						

FORMAT
12
12
14
12
12
F5.3

CARD 8 -- PARAMETER CARD (THESE DATA MUST BE CHOSEN IN ACCORDANCE
WITH THE INSTRUCTION ON CARD 2, COLUMNS 1-3) (FORMAT 6F12.6)
ELEMENTS (+01 OR +04) REQUIRE THE FOLLOWING

COL	SEMI-MAJOR AXIS, KILOMETERS	ECCENTRICITY	INCLINATION	R.A. OF ASCENDING NODE	ARGUMENT OF PERIGEE	MEAN ANOMALY
1-12						
13-24						
25-36						
37-48						
49-60						
61-72						

VECTORS (+02 OR +03) REQUIRE THE FOLLOWING

COL	X	Y	Z	X-DOT	Y-DOT	Z-DOT
1-12						
13-24						
25-36						
37-48						
49-60						
61-72						

ONE VUL = 6378.388 KILOMETERS
ONE VUL/VUT = 6378.388 KM/ 806.832 SEC
RECTANGULAR COORDINATES ARE DEFINED TO BE IN AN INERTIAL,
EQUATORIAL, GEOCENTRIC SYSTEM. X GOES THROUGH ARIES, Y IS
IN EQUATORIAL PLANE, Z IS ALONG POLAR AXIS TO FORM A RIGHT
HANDED SYSTEM.

CARD 9 -- WORLD MAP REQUEST CARD.
THIS CARD IS NEEDED ONLY WHEN THE NUMBER IN COLUMNS 4-6
OF CARD 2 IS GREATER THAN ZERO.
(FORMAT 21X12,1X,14+213,F7.3,13,1X,12+1X,14+213,
F7.3,F11.3)

COL	MONTH	DAY	YEAR (DO NOT ABBREVIATE)	HOUR	MINUTE	SECOND	MONTH	DAY	YEAR (DO NOT ABBREVIATE)	HOUR	MINUTE	SECOND	PREDICTION INTERVAL, SECOND
7-9													
11-13													
15-17													
19-24													
26-27													
29-30													
32-35													
37-38													
40-41													
43-48													
49-59													

FORMAT
12
12
14
12
12
F6.3
12
12
14
12
12
F6.3
F11.3

N.B., IF THE NUMBER IN COLUMNS 7-9 OF CARD 2 IS ZERO OR
NEGATIVE, A NEW JOB IS STARTED BY PEADING CARD 1.

N.B., IF CONTROL ON CARD 2 REQUESTS BOTH MAP AND PREDICTIONS,
TWO REQUEST CARDS ARE NECESSARY.

CARD 10 -- PREDICTION AND MUTUAL VISIBILITY REQUEST CARD
THIS CARD IS NEEDED ONLY WHEN THE NUMBER IN COLUMNS 7-9
OF CARD 2 IS GREATER THAN ZERO.

(SAME FORMAT AS CARD 9)

CARD 11 -- STATION CONTROL CARD (FORMAT 313,F10,0)

COL.
1-3 NO. OF STATION COORDINATE CARDS TO BE LOADED

N.B., THE MAXIMUM NUMBER OF STATIONS THAT CAN BE CONSIDERED IS TWELVE (12).
4-6 = +1 COMPUTE PREDICTIONS, OUTPUT WILL BE ON TAPE A6.
+00 DO NOT OUTPUT PREDICTIONS (ON TAPE A6)
7-9 = MINIMUM ELEVATION ANGLE (DEGREES). NO OUTPUT IS GIVEN IF ELEVATION IS LESS THAN THIS VALUE.
10-20 = MAXIMUM RANGE (KILOMETERS). NO OUTPUT IS GIVEN WHEN THE RANGE IS LARGER THAN THIS VALUE.

(WHEN COLUMNS 1-3 OF THIS CARD ARE LESS THAN OR EQUAL TO ZERO A NEW JOB IS STARTED BY READING CARD 1.)

CARD 12 -- ATTITUDE DATA CARD (FORMAT 4F6,1)

COL.
1-6 MAXIMUM SPACECRAFT LOOK ANGLE, DEGREES
7-12 MINIMUM SPACECRAFT LOOK ANGLE, DEGREES
13-18 RIGHT ASCENSION OF S/C SPIN AXIS, DEGREES
19-24 DECLINATION OF S/C SPIN AXIS, DEGREES

NO MUTUAL VISIBILITY OUTPUT IS GIVEN WHEN THE SPACECRAFT LOOK ANGLE IS OUTSIDE THE LIMITS OF THE MAXIMUM AND MINIMUM VALUES ON THIS CARD.

N.B., MAXIMUM AND MINIMUM LOOK ANGLES, RIGHT ASCENSION, AND DECLINATION ARE CONSTANTS.

CARD 13 -- STATION COORDINATE CARD (S)

COL	NAME	FORMAT
2-7	NAME	A6
9-12	LONGITUDE, DEGREES (+EAST)	I4
14-15	LONGITUDE, MINUTES	I2
17-22	LONGITUDE, SECONDS	F6.3
24-26	LATITUDE, DEGREES (+NORTH)	I3
28-29	LATITUDE, MINUTES	I2
31-36	LATITUDE, SECONDS	F6.3
37-47.	ALTITUDE, METERS	F11.2

N.B., THERE MUST BE AS MANY STATION COORDINATE CARDS AS INDICATED BY CARD 11.

THE STATION COORDINATE CARDS ARE FOLLOWED BY ANOTHER STATION CONTROL CARD OR BY A BLANK. IF THE NUMBER IN COLUMNS 1-3 OF THIS CARD IS NEGATIVE OR ZERO, A NEW JOB IS STARTED BY READING CARD 1. IF THE NUMBER IN COLUMNS 1-3 OF THIS CARD IS POSITIVE, NEW ATTITUDE DATA AND COORDINATE CARDS ARE READ. MUTUAL VISIBILITY AND PREDICTIONS ARE THEN COMPUTED FOR THE NEW STATIONS AND ATTITUDE FOR TIMES GIVEN ON CARD 10.

JOBS MAY BE STACKED BY PLACING A BLANK CARD AFTER THE LAST STATION COORDINATE CARD. CARD 1 OF THE NEW JOB THEN FOLLOWS THIS BLANK CARD.

PLACE 3 BLANK CARDS AFTER THE LAST STATION COORDINATE CARD IN THE LAST INPUT DECK OF THE JOB. THIS WILL RESULT IN THE CORRECT FINAL HALT -- HPR 77777.

EARTH CONSTANTS STORED IN THE PROGRAM

VALUF	INTERNATIONAL	GODDARD	SIRY
GH	+3.986268730E+05	+3.986032000E+05	+3.986268800E+05
J2	0.0	+1.0823E-03	+1.08219E-03
J3	0.0	-2.3E-06	-2.285E-06
J4	0.0	-1.8E-06	-2.123E-06
J5	0.0	0.0	-2.32E-07
F	297.0	298.3	297.0
A	6370.388	6370.165	6370.388

RUNNING INSTRUCTIONS.

RUN UNDER MONITOR SYSTEM
MOUNT BLANK TAPES ON A3 AND A6. IF CONTROL ON CARD 6 CALLS FOR A6

NO KEYS OR SPNSE SWITCHES.

PUT INPUT CARDS IN READER AND READY READER.

FINAL STOP IS -- HPR 77777

PRINT OUTPUT TAPES A3 AND A6 ON NARROW PAPER WITH PROGRAM CONTROL

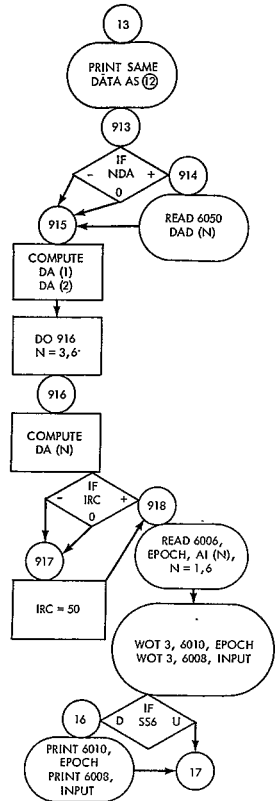
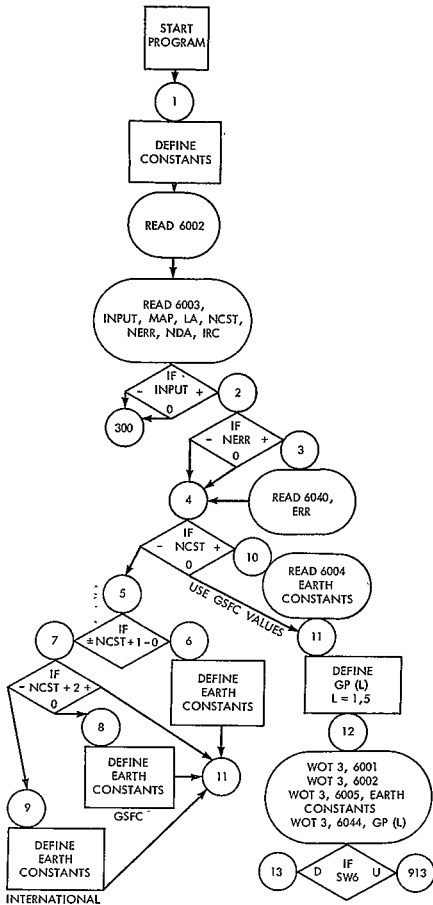
SAMPLE PROGRAM INPUT DECK FOLLOWS. THE DECK WILL COMPUTE THE MUTUAL VISIBILITY OF 12 STATIONS FOR ABOUT ONE DAY. SOME OF THE

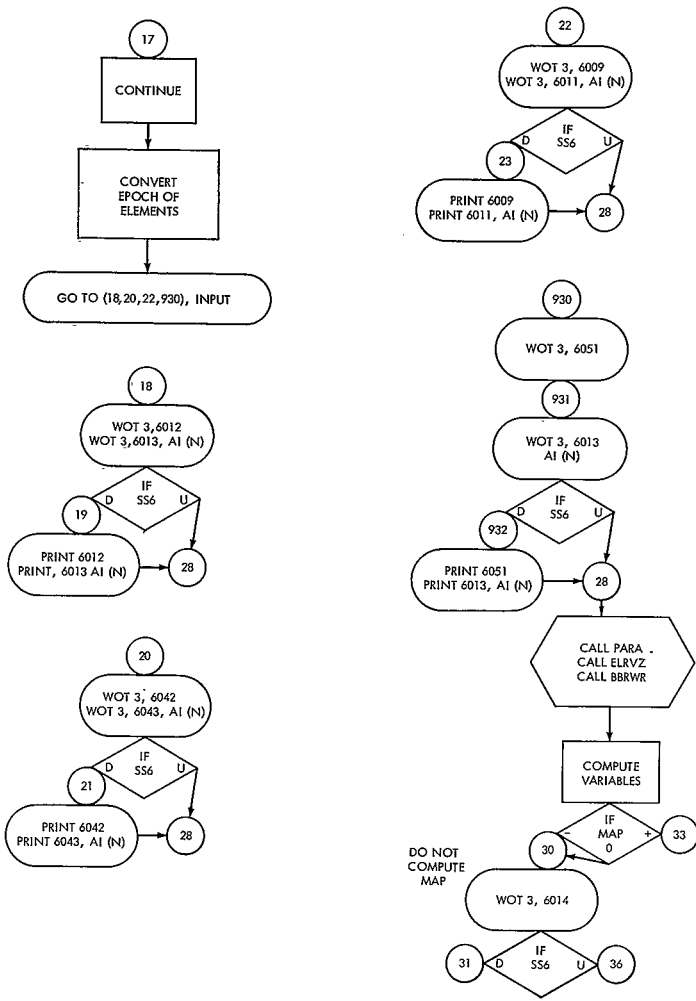
STATIONS WILL BE DUPLICATED. NOTE THAT BOTH MUTUAL VISIBILITY AND
 A WORLD MAP ARE REQUESTED.

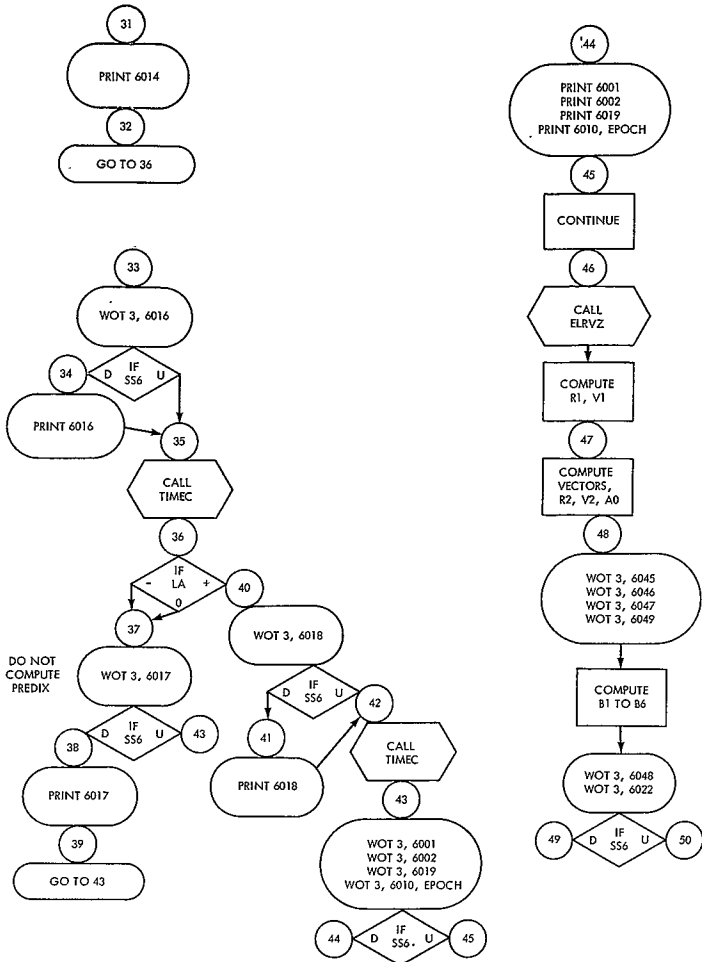
RELAY TEST 12 STATIONS
 +04+01+01-01
 01/14/1964 21 57
 +11143.084 +0.23653052 +46.497757 +220.62688 +186.36665 +359.95097
 01/15/1964 20 00 00.000 01/16/1964 20 00 00.000 +120.
 01/15/1964 19 00 00.000 01/16/1964 19 00 00.000 +120.
 +12+01+00
 90.0 0.0 178. 25.
 CCMNUT -75 00 0.000 +40 00 0.000 0.0
 CCMAND -068 40 00.000 +44 54 00.000 38.
 CCMHIL -05 10 29.0 +50 02 58.0 350.0
 CCMGFR +10 00 00.000 +51 00 00.000 50.
 CCMTEL +13 36 5.000 +41 58 41.000 2168.6
 CCMRIP -43 22 7.000 -22 57 9.000 0.8
 CCMNUT -75 00 0.000 +40 00 0.000 0.0
 CCMAND -068 40 00.000 +44 54 00.000 38.
 CCMHIL -05 10 29.0 +50 02 58.0 350.0
 CCMNUT -75 00 0.000 +40 00 0.000 0.0
 CCMAND -068 40 00.000 +44 54 00.000 38.
 CCMHIL -05 10 29.0 +50 02 58.0 350.0

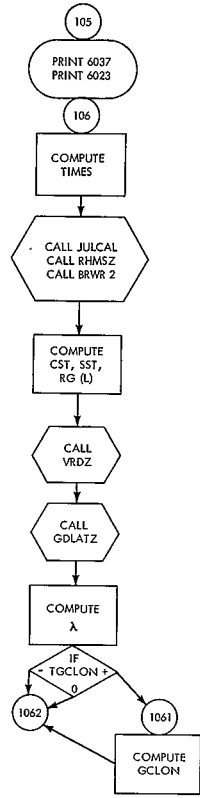
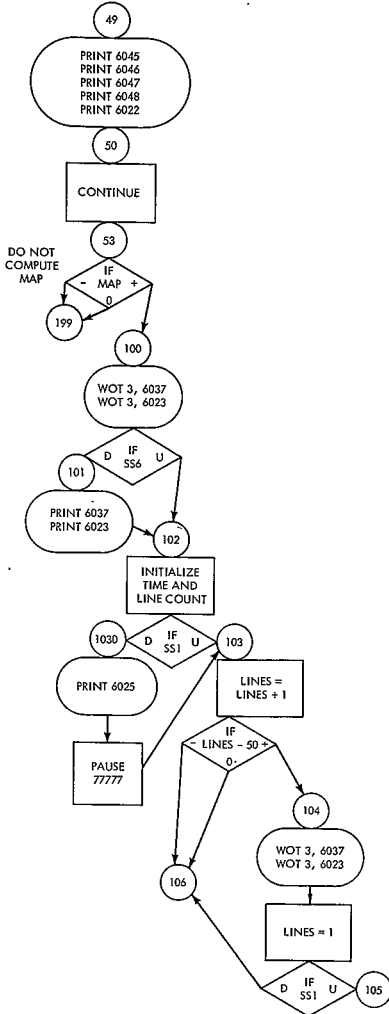
APPENDIX IV

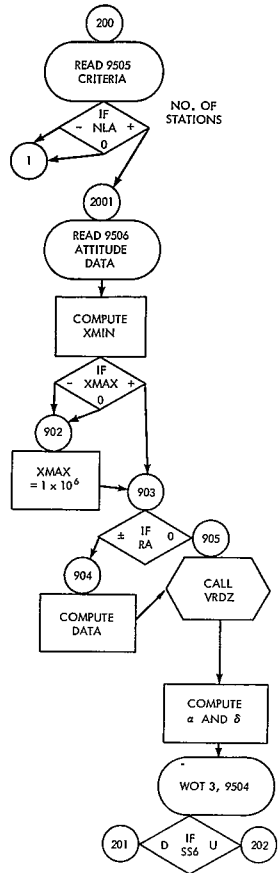
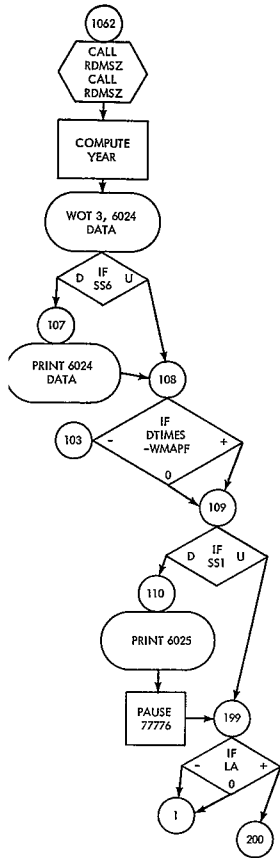
FLOW CHART FOR MAIN PROGRAM TWO

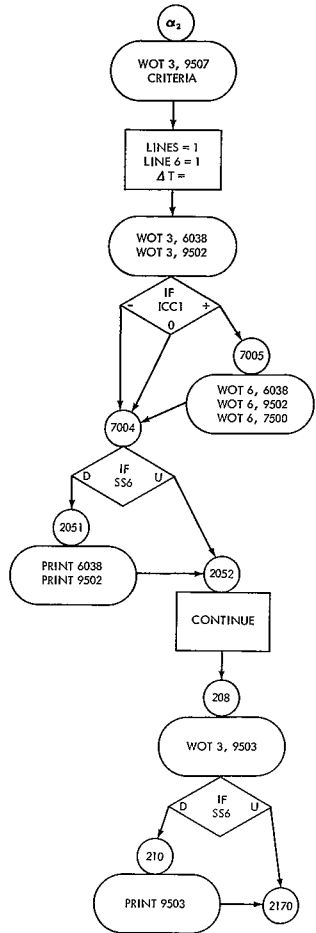
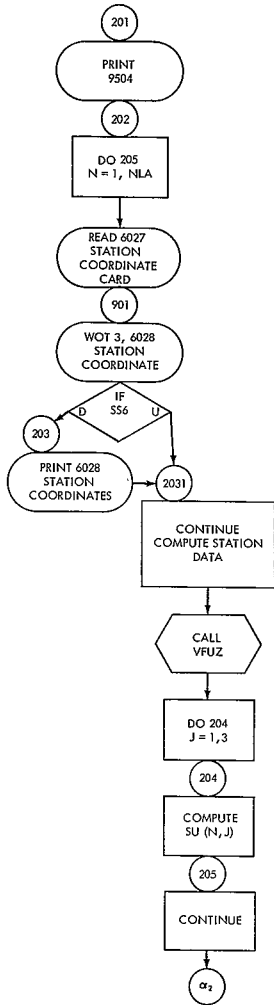


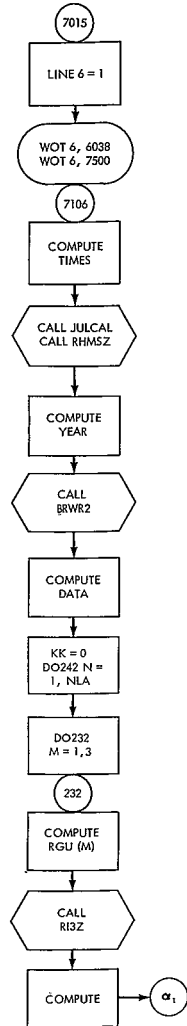
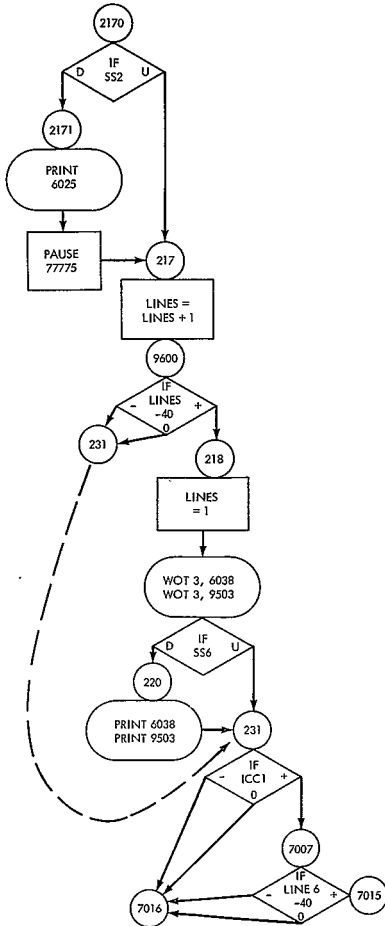


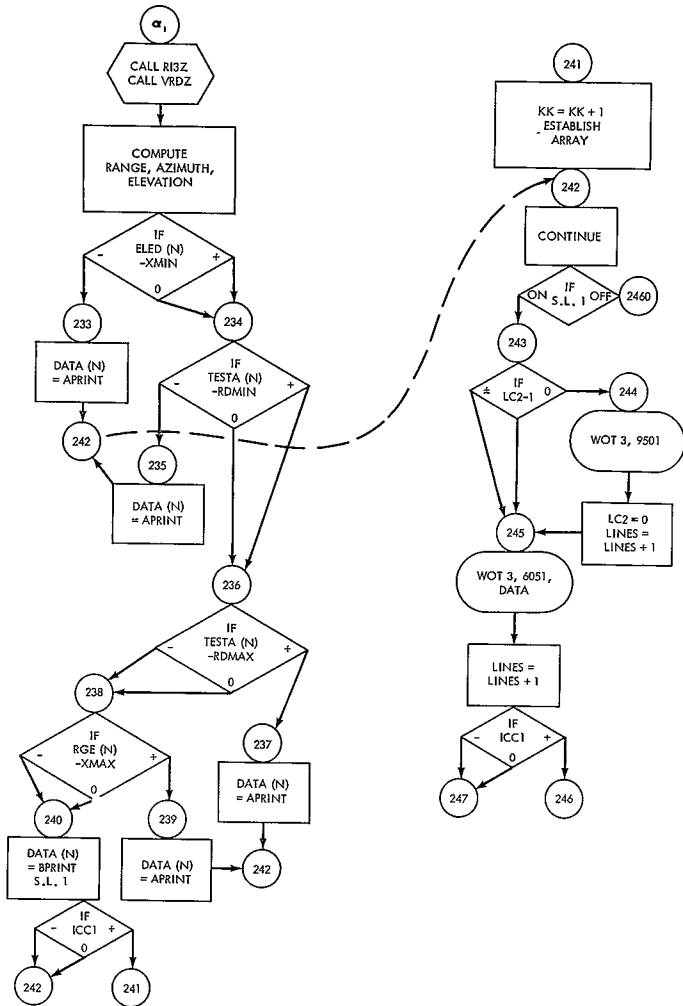


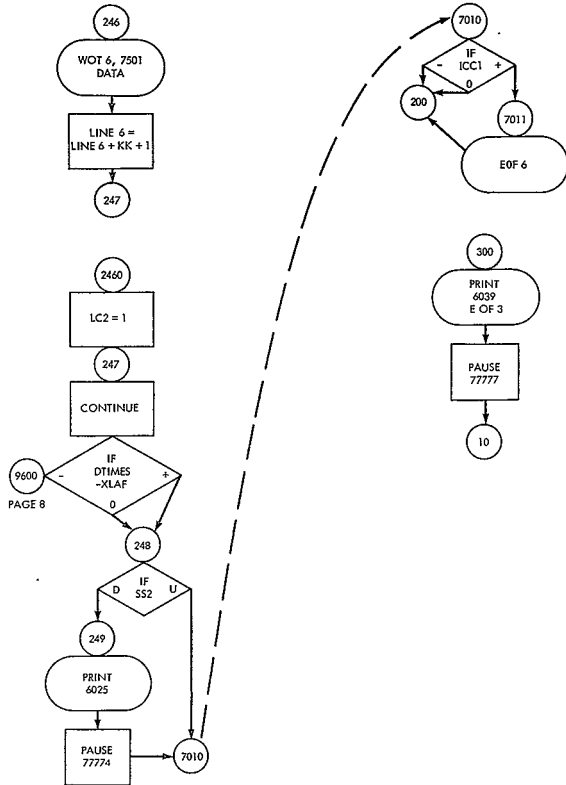












APPENDIX V
SOURCE DECK FOR MAIN PROGRAM ONE

```

*      DATE 9/6/65
*      C N RPPASC
*      DATE
*      CARD# COLUMN
*      LIST#
*      LABEL
*      MUSTAP PROGRAM VERSION 2 THEORY AND ANALYSIS OFFICE - GSFC
C
C      GENERALIZED WORLD MAP AND LOCAL STATION PREDICTIONS PROGRAM.
C
C      1A. CONVERTS OSCILLATING ORBITAL ELEMENTS TO INERTIAL POSITION
C           AND VELOCITY RECTANGULAR COORDINATES.
C      1B. CONVERTS INERTIAL POSITION AND VELOCITY RECTANGULAR
C           COORDINATES TO OSCILLATING ORBITAL ELEMENTS.
C      2.  COMPUTES WORLD MAP ON REQUEST.
C      3.  COMPUTES LOCAL STATION PREDICTIONS (LOOK ANGLES) ON REQUEST.
C
C      ALL INTERNAL CALCULATIONS ARE PERFORMED USING THE KILOMETER AS
C      THE UNIT OF LENGTH AND THE SECOND AS THE UNIT OF TIME. IF ANY
C      OF THE OPTIONAL INPUT PARAMETERS ARE DEFINED IN OTHER UNITS,
C      THEY ARE CONVERTED TO THESE UNITS AS SOON AS THEY ARE READ IN
C      AND ARE SUBSEQUENTLY USED IN THE CALCULATIONS IN KILOMETERS
C      AND SECONDS.
C
C      THE ORBIT REQUIRED FOR THE WORLD MAP AND LOCAL STATION PREDICTIONS
C      IS GENERATED BY SUBROUTINES BRW1 AND BRW2 (DIRK BRUGNER -
C      SOLUTION OF THE PROBLEM OF ARTIFICIAL SATELLITE THEORY WITHOUT
C      MAPS)
C
C      REQUIRED SUBROUTINES AND FUNCTIONS
C
C      ALL0T
C      ALL0TZ
C      ARKTAN
C      ATANQ
C      ATAN7
C      RAC
C      RACNR
C      RRWR1
C      RRWR2
C      CH65C
C      DJUL
C      DMSR2
C      D0TZ
C      FLRV
C      FLRVZ
C      FQN
C      GASTZ
C      GDLATZ
C      HNSPZ
C      JULCAL
C      PARA
C      PM6Z
C      RM6Z
C      RVFZ
C      R137
C      TFSOV
C      TIMFC
C      TIMF4
C      STASH
C      SIN
C      VFI7
C      VPD7
C      XKFP
C      XKFPZ
C
C      Z END OF NAME OF FUNCTION OR SUBROUTINE INDICATES THAT INPUT,
C      OUTPUT, AND INTERNAL ARITHMETIC ARE PERFORMED IN DOUBLE PRECISION.
C
C      DEFINITION OF SYMBOLS
C
C      ERR = TRUNCATION FACTOR (IN RADIANS) USED IN SOLUTION OF
C      KPFLR5 EQUATION
C      GM = PRODUCT OF G (=GAUSSIAN CONSTANT SQUARED) AND M, THE MASS OF
C      THE EARTH, IN UNITS OF KM. CUBED/SEC SQUARED
C      FJ2=J2 )
C      FJ3=J3 ) HARMONICS OF EARTH'S GRAVITATIONAL POTENTIAL
C      FJ4=J4 ) (DIMENSIONLESS)
C      FJ5=J5 )
C      FL=INVERSE OF FLATTENING
C      RE= EQUATORIAL RADIUS OF EARTH IN KM.
C
C      SENSE SWITCH 6 IS USED IN THE MAIN PROGRAM TO PROVIDE AN OPTION TO
C      GET THE INPUT PRINTED ON LINE.
C
C      ALL FORMATS USED IN PROGRAM FOLLOW IMMEDIATELY.
C
C      6002 FORMAT (12A6)
C      6003 FORMAT (8I3,F10.1)
C      6004 FORMAT (E12.6,4E12.5/2F12.4)
C      6005 FORMAT (/ 1X1PE14.8,9X23H FFET PER NAUTICAL MILE//
C      1XDP9.3,9X33H EQUATORIAL RADIUS OF EARTH IN KM /2XFS.1,11X22H IN
C      2VERSE OF FLATTENING/1X,1PE14.8,3X31H GM (KM, CUBED/SECONDS SQUARED

```



```

C
C   TEST FOR 65K SFTTING.
5041 CALL CH65K(NP)
      IF(NW)5038,5042,5038
5038 PRINT 5040
      WRITE OUTPUT TAPE 3,5040
5040 FORMAT (15H0 NOTE TO OPERATOR / 72H PUT MACHINE IN 65K + REWIND AL
      1L TAPFS , AND START JOB FROM BEGINNING . )
      REWIND 1
      PAUSE 00010
      GO TO 5038
5042 IF(SFNSF LIGHT 2) 1,1
      N 1 FRR=1,OF-8
          FRRB=1,OF-7
          ITAPP4 = 8
          LPAS = 0
          NPAG3 = 0
C
C   DEFINE TRUNCATION FACTORS FOR SUBROUTINE BRUNFR ( USED TO CONVERT
C   OSCILLATING FLPMENTS TO BRUNFR MFA4 ELEMNTS)
C
      NAD(1)=5,OF-4
      NAD(2)=5,OF-6
      NAD(3)=5,OF-6
      NAD(4)=5,OF-6
      NAD(5)=5,OF-6
      NAD(6)=5,OF-6
C
C   LCF=0
      LCF=0
      I9FD = 0
      APRINT=60 60 60 60 60 60
      RPRINT = 60 21 60 60 60 60
      BPRINT = 60 05 60 60 60 60
      RPRINT = 60 11 60 60 60 60
      R      XRX = 74 77 77 77 77 77
      XNET = 60B.
      NUMNUM = 0
      XST00 = 0.
      IZWI = 0
      DO 4002 I = 1,12
R4002 XHP(1) = 60452612760
C   ASSUMF VFHICLF STARTS OFF IN SHADOW
      IVA = 0
      IFCY = 0
      IFCSM = 0
      IFSO = 0
      IFSH = 0
      IFSM = 0
C
C   DFFINF GENDARD EARTH CONSTANTS
C
      GM=3.986032F+5
      FJ2=1.4873F-3
      FJ3=-7,7F-6
      FJ4=-1,8F-6
      FJ5=0.0
      FL=298.165
      RF=6378.165
C
C   CARD 1 - READ IN I.D. CARD - ANY INFORMATION IN COLS. 2 - 72
C
      RFAD 6002,(XHFAD(1),I = 1,12)
C
C   CARD 2 - READ IN CONTROL CARD
C
      COLS. 1-3 TYPE OF INPUT (+03 = INERTIAL POSITION AND VELOCITY
      IN VANGUARD UNITS
      +01 = OSCILLATING ELEMENTS-CU AND RAD
      +04 = BRUNFR VFA4 FLPMENTS )
      COLS. 4-6 COMPUTE WORLD MAP AND PREDICTIONS - YES OR NO
      ( YES IF MAP=XX, NO IF MAP=+00 OR -XX )
      COLS. 7-9 +XX ALWAYS
      COLS. 10-12 CHANGE EARTH CONSTANTS
      COLS. 13-15 CHANGE TRUNCATION FACTOR
      COLS. 16-18 BRUNFR TRUNCATION CONTROL
      COLS. 19-21 BLANK - USED INTERNALLY
      COLS. 22-24 NUMBER OF CONTROL STATIONS
      COLS. 25-34 MAXIMUM RANGE TEST VALUF NAUTICAL MILES
      READ 6003,INPUT,MAP,LA,NCST,NERR,NDA,IRC,I2CT,RGMA
C
C   I2CT IS THE NUMBER OF CONTROL STATIONS.
C   TEST - HAVE ALL CASES BEEN RUN - YES OR NO
C
      IF(I2CT - 19) 5034,5034,3010
3010 PRINT 5033,I2CT
      WRITE OUTPUT TAPE 3,5033,I2CT
5033 FORMAT(15H0YOU ARE USING 16,60H CONTROL STATIONS. THE PROGRAM CAN
      1ONLY HANDLE 19 STATIONS. )
      68 PAUSE 54321
      GO TO 68
5034 IF(1INPUT)300,300+2
C   IF INPUT=+00 OR -XX, ALL CASES HAVE BFEN RUN. GO TO 300 (END

```

```

C
C   TEST - CHANGE TRUNCATION FACTOR - YES OR NO
C
C   2 IF (NFRF) 4,4,3
C
C   CARD 2A- (OPTIONAL) READ IN NEW VALUE OF TRUNCATION FACTOR IF
C   NERR=XX. IF NERR=+00 OR -XX, PROCEED TO NEXT
C   OPTION TFST.
C
C   3 READ          6040,ERR
C
C   TEST - CHANGE EARTH CONSTANTS - YES OR NO
C
C   4 IF (NCST) 5,11,10
C
C   TO NEXT STEP.
C
C   5 IF (NCST+1) 7,6,7
C
C   USE SJRY PACKAGE CONSTANTS IF NCST = -1
C
C   6 GM=3.9862688F+05
C   FJ2=1.0F219F-03
C   FJ3=-2.285F-06
C   FJ4=-2.123F-06
C   FJ5=-2.32F-07
C   FL=297.0
C   RF=6374.388
C   GM TQ 11
C
C   7 IF (NCST+2) 9,8,11
C
C   USE GODDARD EARTH CONSTANTS WITH HARMONICS = 0 IF NCST = -2
C
C   8 FJ2=0.0
C   FJ3=0.0
C   FJ4=0.0
C   FJ5=0.0
C   GM TQ 11
C
C   USE INTERNATIONAL CONSTANTS WITH HARMONICS = 0 IF NCST = -3
C
C   9 GM=3.98626873F+5
C   FJ2=0.0
C   FJ3=0.0
C   FJ4=0.0
C   FJ5=0.0
C   FL=297.0
C   RF=6374.388
C   GM TQ 11
C
C   CARDS 2B AND 2C- (OPTIONAL) READ IN NEW SET OF EARTH CONSTANTS
C   IF NCST=+XX.
C
C   10 READ          6004,GM,FJ2,FJ3,FJ4,FJ5,FL,RF
C
C   CONVERT EARTH CONSTANTS
C
C   11 GP(1)=GM
C   GP(2)=-.5*FJ2*RF**2
C   GP(3)=-FJ3*RF**3
C   GP(4)=-.375*FJ4*RF**4
C   GP(5)=-FJ5*RF**5
C
C   PRINT ALL QUANTITIES ON OUTPUT TAPE A3.
C
C   12 WRITE OUTPUT TAPE 3,3089
C   WRITE OUTPUT TAPE ITAPF4,3089
C   WRITE OUTPUT TAPE 3,3087,(IXHFAD(1),I = 1,12)
C   WRITE OUTPUT TAPE ITAPF4,3087,(IXHFAD(1), I = 1,12)
C   WRITE OUTPUT TAPE 3,3089
C   WRITE OUTPUT TAPE 3,5025,(IXHFAD(1),I = 1,12)
3087 F8RMAT (////////// ?(21X6A6/))
3088 F8RMAT (1HP)
5025 F8RMAT (////////// 2(54X,6A6/))
WRITE OUTPUT TAPE 3,3089
3089 F8RMAT (1H1)
WRITE OUTPUT TAPE 3,3088
WRITE OUTPUT TAPE ITAPF4,3088
WRITE OUTPUT TAPE ITAPF4,3088
WRITE OUTPUT TAPE 3,6C05,XNMFT,RE,FL,GM,FJ2,FJ3,FJ4,FJ5
WRITE OUTPUT TAPE ITAPF4,6C05,XNMFT,RE,FL,GM,FJ2,FJ3,FJ4,FJ5
IF (SFNSF SWITCH 6) 13,915
C
C   PRINT SAVE INFORMATION ON LINE IF SENSE SWITCH 6 IS DOWN.
C
C   13 PRINT 6002
C   PRINT 6005,XNMFT,RE,FL,GM,FJ2,FJ3,FJ4,FJ5
913 IF (NDA) 915,915,914
914 READ          6050, (PAD(N), N=1,6)
915 PA(1)=PAD(1)
PA(2)=PAD(2)
DA 916 N=3,6

```

```

916 NAI(N)=NAD(N)*0.017453292
IF (IRC) 917,917,918
917 IRC=50
CARD 4 - READ IN PARAMETERS
TAKES STANDARD EP0CH AND ELEMENT CARDS
ALL PARAMETERS USE STANDARD FORMAT (6E12,8)
918 READ 6006,IDSAT,NYE,NME,NDE,NHE,NMNE,TSE,NORBIT,(AI(N), N = 1,6)
NYE = 1900 + NYE
PRINT FP0CH AND INPUT OPTI0N 0N OUTPUT TAPF A3
15 WRITE OUTPUT TAPE 3,6010,NYE,NME,NDE,NHE,NMF,NMNE,TSF
WRITE OUTPUT TAPE ITAPE4,6010,NYE,NME,NDE,NHE,NMNE,TSE
IF (SFNSF SWITCH 6) 16,17
PRINT SAME INFORMATION 0N-LINE IF SENSE SWITCH 6 IS 00WN
16 PRINT 6010,NYE,NME,NDE,NHE,NMNE,TSE
17 CONTINUE
READ THE FP0CH AND DRAG TERM. THE UNITS 0F THE DRAG TERM ARE
RADIAN5 PER CUT**2.
CHANGE DRAG TO RADIAN5 PER SECOND**2 BY DIVIDING BY 806.832**2.
READ 5028,IDG1,IDG2,IDG3,IDG4,IDG5,IDG6,ENZ
5028 FORMAT (7X,3I2,X,2I2,X,1I2,4X,E12.8)
CONVERT EP0CH UNIVERSAL TIME IN HOURS, MINUTES, AND SECONDS
TO FP0CH UNIVERSAL TIME IN RADIAN5.
TIME0=HMSRZ(NHF,NMNE,TSE)
CONVERT EP0CH CALENDAR DATE TO FP0CH JULIAN DATE AT 0 HOURS
UNIVERSAL TIME.
NJO=NJUL(NME,NDF,NYE)
CONVERT EP0CH UNIVERSAL TIME IN HOURS, MINUTES, AND SECONDS
TO SFC0NDS.
THF=NHF*3600
TMNF=NMNF*60
TSFP=THF+TMNF+TSE
GO TO (18,1,22,930), INPUT
18 WRITE OUTPUT TAPF 3,6012
INPUT OPTI0N 1 - OSCILLATING ELEMENTS IN VANGUARD UNITS AND RADIAN5
WRITE OUTPUT TAPE ITAPE4,6012
WRITE OUTPUT TAPE 3,6051
WRITE OUTPUT TAPE ITAPE4,6051
WRITE OUTPUT TAPE 3,6011, (AI(N),N = 1,6)
WRITE OUTPUT TAPF ITAPE4,6011,(AI(N),N = 1,6)
IF (SFNSF SWITCH 6) 19,3002
19 PRINT 6012
PRINT 6051
PRINT 6011, (AI(N),N=1,6)
GO TO 3002
PRINT INPUT PARAMETERS 0N OUTPUT TAPE A3 - INPUT OPTI0N 3
INERTIAL POSITION AND VELOCITY RECTANGULAR COORDINATES -
IN VANGUARD UNITS.
22 WRITE OUTPUT TAPE 3,6009
WRITE OUTPUT TAPE ITAPE4,6009
WRITE OUTPUT TAPE 3,6011,(AI(N),N=1,6)
WRITE OUTPUT TAPE ITAPE4,6011,(AI(N),N = 1,6)
IF (SFNSF SWITCH 6) 23,28
PRINT SAME INFORMATION 0N-LINE IF SENSE SWITCH 6 IS 00WN
23 PRINT 6009
PRINT 6011,(AI(N),N=1,6)
GO TO 24
PRINT INPUT PARAMETERS - INPUT OPTI0N 4 - BROUWER MEAN ELEMENTS
930 WRITE OUTPUT TAPE 3,6051
WRITE OUTPUT TAPE ITAPE4,6051
931 WRITE OUTPUT TAPE 3,6011,(AI(N),N = 1,6)
WRITE OUTPUT TAPE ITAPE4,6011,(AI(N),N = 1,6)
IF (SFNSF SWITCH 6) 932,3002
PRINT SAME INFORMATION 0N-LINE IF SENSE SWITCH 6 IS 00WN
932 PRINT 6051
PRINT 6011,(AI(N),N = 1,6)
CONVERT TO KM AND DGRFFS
N0002 A1(1) = A1(1) * 6378.388
AAMA = A1(4) * 57.2957795130823
A1(4) = A1(6) * 57.2957795130823
A1(5) = A1(5) * 57.2957795130823
A1(6) = AAMA * 57.2957795130823

```

```

C
C      CONVERT INPUT PARAMETERS TO OSCILLATING ELEMENTS
C
C 28 CALL PARA(INPUT,AT+A,GN)
5027 FORMAT(13HODRAG EFFECTS ,6X,7H(P,0),8X,7H(N(2,0),9X,7H(N(3,0)
      1 14X,2(X,3)2I,2(3X+E15,8I)
      WRITE OUTPUT TAPE ITAPE4,5027,1DG1,1DG2,1DG3,1DG4,1DG5,1DG6,EN2
      WRITE OUTPUT TAPE          3,5027,1DG1,1DG2,1DG3,1DG4,1DG5,1DG6,EN2
n      FN2 = FN2 / 806.832**2
D      CALL FLRVZ(RX,VX,A,PER,FM,GM,ERR)
      CALL BRNR(DA,A,IRC,MN)
n      VX(1)=VX(1)
n      VX(2)=VX(2)
n      VX(3)=VX(3)
      FN=S*(1)
      DP=S*(2)
      DN=S*(3)
n      PFR=6.2831853*718/EN
n      PFRM=PFR/60.0
n      PFRH=PFR/3600.0
n      FN1=FN*206264.806247096
n      DNPF=DN*4950355.3499303
n      DPFJ=DP*4950355.3499303
C
C      TFST = I4 WRPLD MAP DFS1PFD
C
C
C 29 IF (MAP) 30,30,33
30 WRITE OUTPUT TAPE 3,6014
      IF (SFNSF SWITCH 6) 31,36
31 PRINT 6014
32 GO TO 36
33 CONTINUE
C
C
C 36 CONTINUE
C
C      CARD 10 - STATION PREDICTIONS AND WORLD MAP ARE REQUIRED, READ
C      CALENDAR DATE AND UNIVERSAL TIME AT WHICH THE START
C      OF THE CALCULATION IS DESIRED, CALENDAR DATE AND
C      UNIVERSAL TIME AT WHICH THE TERMINATION OF THE
C      CALCULATION IS DESIRED, AND THE DESIRED TIME INCREMENT
C      OF THE CALCULATION IN SECONDS.
C
C 40 WRITE OUTPUT TAPE 3,6018
      WRITE OUTPUT TAPE ITAPF4,6018
C
C      PRINT SAME INFORMATION ON-LINE IF SENSE SWITCH 6 IS DOWN
C
C      IF (SFNSF SWITCH 6) 41,42
41 PRINT 6018
42 CALL TIME4(IDJ0,TSEP,XLAS,XLAF,DTLA)
C
C      PRINT SAME INFORMATION ON-LINE IF SENSE SWITCH 6 IS DOWN
C
C 43 CONTINUE
C
C      CONVERT OSCILLATING ORBITAL ELEMENTS TO INERTIAL POSITION AND
C      VELOCITY CORRELINATES IN KM AND KV/SEC
C
C 46 CALL FLRVZ(RX,VX,A,PER,EN,GM,ERR)
      R1=SQRT(RX(1)**2+RX(2)**2+RX(3)**2)
      V1=SQRT(VX(1)**2+VX(2)**2+VX(3)**2)
C
C      CONVERT TO VANGUARD UNITS OF LENGTH AND VELOCITY
C
C 47 X01=RX(1)/6378.388
n      X02=RX(2)/6378.388
n      X03=RX(3)/6378.388
n      V01=VX(1)/7.9054722668
n      V02=VX(2)/7.9054722668
n      V03=VX(3)/7.9054722668
n      P2=SQRT(X01**2+X02**2+X03**2)
n      V2=SQRT(V01**2+V02**2+V03**2)
C
C      CONVERT ANGLFS (RADIAN) TO ANGLFS (DEGREES)
C
C      A01=A(1)
n      A02=A(2)
n      A03=A(3)*57.2957795130923
n      A04=A(4)*57.2957795130923
n      A05=A(5)*57.2957795130923
n      A06=A(6)*57.2957795130923
n      R1=110(1)
n      R2=110(2)
n      R3=110(3)*57.2957795
n      R4=110(4)*57.2957795
n      R5=110(5)*57.2957795
n      R6=110(6)*57.2957795
C
C      BEGIN LOCAL STATION PREDICTIONS CALCULATION

```



```

200 IF(IIRD)13001,3000,3001
3000 READ 9505,NLA,ICCL1,MINV,XMAX,MUTE
      IRFD = 5
      IF(NLA - 18) 73,73,70
70 PRINT 71,NLA
  WRITE OUTPUT TAPE 3,71,NLA
71 FORMAT(16H0 YOU ARE USING 19,
  1 47H STATIONS. PROGRAM CAN ONLY HANDLE 19 STATIONS.
72 PAUSE 66666
  GO TO 72
C   WIDE PAPER FORM IF MBRF THAN 15 STATIONS ARE USED
73 IF(NLA - 15) 60,60,61
60 NLSPP = 40
  GO TO 62
61 NLSPP = 58
62 IF (NLA) 1,1,2001
C   MAKE ISVEL POSITIVE IF SPIN AXIS IS ALONG INERTIAL VELOCITY VECTOR
2001 READ 9506,RDMAX,RDMIN,RA,DEC,ISVEL
C   STORE BLANKS
      IF(NLA - 12CT) 5035,5037,5037
5035 PRINT 5036
      WRITE OUTPUT TAPE 3,5036
5036 FORMAT(72H0THE NUMBER OF CONTROL STATIONS IS LARGER THAN THE NUMBE
  1FR OF STATIONS.
67 PAUSE 54333
  GO TO 67
5047 IF(NLA - 18) 5004,5004,5006
5004 NFL = (NLA*2) + 7
  DO 5005 I = NFL,44
5005 MUV(I) = APRINT
5006 CONTINUE
      XMIN=MINV
      XMAX = RGMA * XMMET * 0.30480061F-03
  903 IF(ISVEL)905,904,905
  9004 RAR=RA*,0176532925
  D   DECR=DFC*.0176532925
  D   VXF(1) = COSF(DFCR) * COSF(IRAR)
  D   VXF(2) = COSF(DFCR) * SINF(IRAR)
  D   VXF(3) = SINF(DFCR)
  GO TO 5026
  9905 CALL VRDZ(1,VXF,DECR,RAR,XXX)
      S4 = RAR*57.2957795
      DFC=DFCR*57.2957795
5026 WRITE OUTPUT TAPE 3,9504
      IF (SFNSF SWITCH 6) 201,202
201 PRINT 9504
202 DO 205 N=1,NLA
  READ 6027,STAT(N),STAT1(N),LOND,LONM,XLONS,LATD,LATM,
  1 XLATS,HGT
  901 WRITE OUTPUT TAPE 3,6028,STAT(N),STAT1(N),LOND,LONM,XLONS,LATD,
  1LATM,XLATS,HGT
      IF (SFNSF SWITCH 6) 203,2031
203 PRINT 6028,STAT(N),LOND,LONM,XLONS,LATD,LATM,XLATS,HGT
2031 CONTINUE
  D   C@ORD(1)=DMSRZ(LATD,LATM,XLATS)
  D   C@ORD(2)=DMSRZ(LOND,LONM,XLONS)
  D   C@ORD(3)=HGT/1000.0
  D   RLAT(N)=C@ORD(1)
  D   RLON(N)=C@ORD(2)
  D   CALL VFUZ(C@ORD,RE,FL,U)
  DO 204 J=1,3
204 SU(N,J)=U(J)
205 CONTINUE
      N = 1
      IF(12CT) 3095,3095,3094
3094 N= 17CT
3095 WRITE OUTPUT TAPE 3,3093,(STAT(J),STAT1(J),J = 1,N)
      WRITE OUTPUT TAPE 1TAPE4,3093,(STAT(J),STAT1(J), J = 1,N)
3093 FORMAT(//15X21H CONTROL STATIONS ARE /+4(20X23/1)
      WRITE OUTPUT TAPE 3,9507,MINV,MINV,RGMA
      WRITE OUTPUT TAPE 3,3013,RA,DEC
      WRITE OUTPUT TAPE 3,3091
3091 FORMAT(54H0 S IS PRINTED WHEN THE SATELLITE IS IN THE SUNLIGHT )
      WRITE OUTPUT TAPE 3,3092
3092 FORMAT(80H0 THE 3 DIGIT NUMBERS UNDER THE STATION NAMES ARE THE S
  1PACRCRAFT LOOK ANGLES.
)
)
C   INITIALIZE LINE COUNT AND DELTA T (DIFFERENCE BETWEEN
  LOCAL STATION PREDICTIONS STARTING TIME AND EPOCH OF INPUT
  PARAMETERS IN SECONDS)
C
C
3001 LINF5 = 1
  LINF6=1
  D   DTIMF=XLAS-DTLA
C
C
2170 IF (SFNSF SWITCH 2) 2171,217
2171 PRINT 6025
      PAUSE 77775
217 LINF5=LINF5+1
C
C   SKIP A PAGE AND PRINT HEADING IF 50 LINES OF CALCULATION

```

```

C      HAVF BFFN PPINTED
C
0601 JJ = 1
      NPPRFD = 0
      LIN11 = 0
      LIN12 = 0
      IALAX = 0
      IMRS = '2767'
0600 CONTINUE
07016 DTIMES = DTIMFS + DTLA
D      TIME=TIME0+DTIMES*0.727220521664304E-4
D      DDJO=INT( (TIME/6.283185307179586)
D      DJ=DDJO*DDJO
D      TIME=ALLDTZ(TIME)
C
C      COMPUTE GFRENWICH APPARENT SIDEREAL TIME AT TO + DELTA T
C
D      UT = TIME * 2.81071863471
D      FOR = FON(DJ,UT,XDX,XDX,FCOM)
D      ST = GAST7(DJ,UT,EOR)
D      CALL JULCAL(DJ,NR,ND,NY)
C
C      CONVERT UNIVERSAL TIME IN RADIANS TO HOURS, MINUTES, AND SECONDS
C
D      CALL RHP5Z(TIME,II,II,14,TS)
D      NYM19=NY-1900
C
C      CALL RRWR2(DTIMES,ENZ)
C      CST=SIGN(*T)
C      R(1)=RXR(1)*FCST+RXR(2)*SST
C      R(2)=RXB(2)*CST-RX(1)*SST
C      R(3)=RXB(3)
D      CALL VRN2(1,RG,GCLAT,GCLON,R)
C
C      COMPUTE GEOPTIC LATITUDE OF SUBSATELLITE POINT
C
D      GDLAT = GDLATZ(GCLAT,R,RE,FL,ALTT)
C
C      COMPUTE HEIGHT OF SATELLITE ABOVE COMPUTATIONAL ELLIPSOID ALONG
C      NORMAL FROM SATELLITE TO FLLIPSOID
C
C      CONVERT LATITUDE AND LONGITUDE IN RADIANS TO DEGREES, MINUTES,
C      AND SECONDS
C
D      TGCLON=GCLON-3.141592653589793
D      IF (TGCLON) 1062,1062,1061
01061 GCLON=TGCLON-3.141592653589793
C
C      1062 CONTINUE
C      TEST FOR VEHICLE IN SUNLIGHT
C      AN S WILL BE PRINTED IF IN SUNLIGHT
C      IF(SFNSFLIGHT 2) 3000,3011
03011 CALL SUN(DJ,TIME,SLC)
D      SLC = SLC - 0.99241E-04
D      CFCO = COS(FCOM)
D      SFCO = SIN(FCOM)
D      SSLC = SIN(SLC)
C      COMPUTE COMPONENTS OF SUN
D      XSU = COS(SLC)
D      YSU = SSLC * CFCO
D      ZSU = SFCO * SFCO
D      RINTO = RXB(1)**2 + RXB(2)**2 + RXB(3)**2
D      RINT = SORTF(RINTO)
D      IF(RINT)3015,3015,3016
3015 IFR = 0
D      PRINT 3024,IFR,I
3024 FORMAT(2I6)
D      GO TO 3007
3016 CPSI = (XSU*RXB(1) + YSU*RXB(2) + ZSU*RXB(3)) / RINT
3017 IF(CPSI)3005,3006,3006
3005 DFMX = RINTO - RF**2
D      DFMX = SORTF(DFMX)
D      IF(DFMX)3018,3018,3019
3018 IFR = 1
D      PRINT 3024,IFR,I
D      GO TO 3007
03019 TNN = RF / DFMX
D      CALL ARKTAN(RE,DFMX,XNU,1)
D      SPS1 = 1.-CPSI**2
D      IF(SPS1)3020,3021,3021
3020 IFR = 2
D      PRINT 3024,IFR,I
D      GO TO 3007
3021 SPS1 = SORTF(SPS1)
D      CPS1 =-CPS1
D      CALL ARKTAN(SPS1,CPS1,PSVA,1)
D      X90DG = 1.5707963
D      GULX = X90DG - PSVA
D      TFNN = GULX + XNU - X90DG
D      IF(TFNN) 3006,3006,3007
R3006 SUNN = 62 60 60 60 60 60

```

```

      IGDR = 2
C     VFHICLF IN SUN
      NUMSUN = NUMSUN + 1
      GR TO 3008
93007 SUNN = 60 60 60 60 60 60
      IGDR = 1
C     VFHICLF IN SHAD0W
900R  CONTINUE
      IF(1VA) 3026,3025,3026
9025  IVA = 2
      DTFSH = DTIMFS
      GR TO 3030
3026  IF(IGDR - (IGM)3027,3030,3028
3027  IFSY = NY419
      IFSM0 = NY
      IFSN = ND
      IFSM = IH
      IFSM = IV
      DTFSH = DTIMFS
      GR TO 3030
93028 PERCENT = 100. - (DTIMFS - DTFSH) / (36. * PPRH)
      DRAT = DTIMFS - DTFSH / 60.
      WRITE OUTPUT TAPE 5,3029,IESY,IESM0,IESD,IFSH,IESM,NY19,NY,ND,
      IIM,IM,DRAT,PERCENT
3029  FORMAT (5X,312,X,212,13X,312,X,212,5X,FT,1,11X,FT,2)
3031  FORMAT (11X,20X,22H SUNLIGHT HISTORY OF A57/5X63HSATELLITE WILL BE
      11N SUNLIGHT AT ALL TIMFS EXCEPT WHEN IT WILL /5X,
      24DHENTER SHAD0W AT AND LEAVE SHAD0W AT /5X,
      37SHYMNDD HHMM          YMNDD HHMM DURATION (MIN) PERCENT IN
      4, SUNLIGHT )
9030  IGDM = IGDR
C     .
      IF(XS700)3070,3069,3079
3069  XGLAST = 6DLT
      GR TO 3074
9070  IF(GDLAT)3073,3071,3071
3071  IF(XGLAST)3072,3073,3073
3072  NDRAT = NDRAT + 1
3073  XGLAST = GDLAT
9074  XS700 = X5700 + 1
      IF(IJJ - 113078,3077,3078
9077  IREGDR = NDRAT
9078  CONTINUE
      IF(XS700 - 300.)3064,3063,3063
9063  X5700 = 1.
      PRINT 5050,NY419,NM,ND,IH,IV
5050  FORMAT (3X,312,2X,212)
3064  KK = 0
      DO 3081 I = 1,19
9081  XPESTA(I) = APRINT
      DO 242 K=1,NLA
      DO 232 M=1,5
      232  QGU(M) = RG(M) - SU(N,M)
      CALL R13Z(RTX,0,-ST,QGU)
      NDRAT = NDRAT + 1
      TESTA(N) = NUM*57.295780
      R13A1 = 1.57079632679 - RLAT(N)
      R13A2 = 1.57079632679 + RLON(N)
      CALL R13Z(I,R13A1,R13A2,RGU)
      CALL WRZ(I,2,2,ELEVAT,AZ,INUT,RANG)
      FLFD(N) = 57.29578 * ELEVAT
      AZID(N) = 57.29578 * AZINUT
      RGF(N) = PANG
      DATA(N) = APRINT
      IF(FLFD(N))1293,319,318
318  IF(FLFD(N) - 5.0) 319,321,320
319  DATA(N) = DPRINT
      GR TO 238
320  IF(FLFD(N) - 10.1321,238,238
321  DATA(N) = FPRINT
328  IF(RGF(N) - XMAX)239,239,902
233  DATA(N) = APRINT
      GR TO 242
      902  DATA(N) = DATA(N) + (- XRRX)
240  IDATA = APRINT
3004  FNEF LIGHT 1
4009  FRRMAT (1515,F16,R)
4001  FRRMAT (4F16,R,215)
322  IF(NPRFD) 241,310,241
310  DO 309 I11 = 1,12CT
      IDAT = DATA(I11)
      IF(IDAT - IDATA)311,3009,311
9009  CONTINUE
      GR TO 241
311  NPRFD = 1
241  KK = KK + 1
      IF(IALAX - 1) 3061,3061,3062
9061  IALAX = KK
9062  CONTINUE
      XRG(KK) = QGF(N)
      XAZ(KK) = AZID(N)
      XFL(KK) = FLFD(N)

```

```

Y0(KK) = TFSTA(N)
STAT3(KK) = STAT(N)
STAT4(KK) = STAT1(N)
IN(KK) = N
IZ(KK) = TFSTA(N)
242 CONTINUE
C CONVERT S/C ANGLE TO BCD
I*(KK)3090,3090,3082
3082 DO 3083 I = 1,KK
CALL TFSCBVI(IZ(I),XZ(I))
3083 CONTINUE
DO 3085 I = 1,KK
INVA = IN(I)
3085 XSTAT(INVA) = XZ(I)
3090 GCLN = GCLRN * 57.29577951
N GOLT = GDLAT * 57.29577951
243 IF (SPNSF LIGHT 1) 243,2460
244 LC2 = 0
245 JJ = JJ + 1
17N1 = 10
C SET UP WPIV APPRY
WPIV(1) = NV*19
UPIV(2) = NM
WPIV(3) = ND
WPIV(4) = IH
WPIV(5) = IM
VPIV(6) = NFRQIT
DO 5003 I = 1,NLA
NXD = (I*2) * 5
WPIV(NXD) = XSTAT(I)
NXD = 4*ND + 1
5003 WPIV(NXD) = DATA(I)
C STORF WPIV
IPRS = 12000 - LIN11 * 44
IF (IPRS - 44)5019,5021,5021
5019 DTIMFS = DTIMFS - DTLA
SFNSF LIGHT 3
GO TO 2460
5021 CALL STASH(WPIV+44,IPRS)
IF(MAP)3079,3079,3080
C SET UP FOR 65 K.
3080 PRF(1) = KK
PRF(2) = STAT3(I)
PRF(3) = STAT4(I)
PRF(4) = XPG(I)
PRF(5) = XZ(I)
PRF(6) = XFL(I)
PRF(7) = XR(I)
PRF(8) = GOLT
PRF(9) = GCLN
PRF(10) = ALIT
PRF(11) = SINW
LIN12 = LIN12 + 1
NXD = 11
IF(KK - 1)5002,5002,5000
5000 DO 5001 K = 2,KK
NXD = (K*7) - 2
PRF(NXD) = STAT3(K)
NXD = NXD + 1
PRF(NXD) = STAT4(K)
NXD = NXD + 1
PRF(NXD) = XRG(K)
NXD = NXD + 1
PRF(NXD) = XAZ(K)
NXD = NXD + 1
PRF(NXD) = XFL(K)
NXD = NXD + 1
PRF(NXD) = XR(K)
NXD = NXD + 1
5001 PRF(NXD) = SINW
5002 IF(IMBS - 12000 - NXD) 5020,5022,5022
5020 DTIMFS = DTIMFS - DTLA
LL11 = LL11 - 1
SFNSF LIGHT 4
GO TO 2460
C STORF PRF
5022 CALL STASH(PRF+NXD,IMFS)
IMFS = IMFS - NXD
IX = IX + 1
3051 FFORMAT (13X,2A3,F9.1,2F6.1,F7.1,5A6)
3070 LFN1 = LIN11 + 1
GO TO 247
2460 IF(INLA - 1)3059,3060+63
63 IF(IMUTF)313,5031,313
5031 IF(IJLAK - 1)3059,3059+3060
3060 IF(INPRED) 313,3059,313
313 JWX = JJ - 1
LPAS = 10
WRITE OUTPUT TAPE 3,3076,1BG5RB
3076 FFORMAT (1H1,27X,13H ORBIT NUMBER 16)
WRITE OUTPUT TAPE 3,330,1NSAT

```

```

      LL11 = 2
      LASORR = JRGORB
C   RETURN WPUV
      DR 3054 K = 1,LL11
      LOK = I2000 - (K-1) * 44
      CALL BACK(WPUV,44,LOK)
      DA 5007 I = 1,5
5007 MVI(1) = WPUV(1)
      IF(LL11 = 2) 5032,64,5032
      64 IF(NPAG2)65,5029,65
      65 NPAG3 = 0
      LL11 = LL11 + 1
      MVI(7) = WPUV(6)
      WRITE OUTPUT TAPE 3,66,MVI(7)
      66 FORMAT (2RX,13H ORBIT NUMBR 16 )
5029 WRITE OUTPUT TAPE 3,5030,MVI(2),MVI(3),MVI(1)
5030 FORMAT (2RX,18H DATE(MV,DD,YY) = 2(12,1H),12)
      WRITE OUTPUT TAPE 3,331,(STAT(1)),I = 1,4LA)
5032 MVI(7) = WPUV(6)
      IF(LASORR = MVI(7)) 5016,5017,5017
5016 LASORR = MVI(7)
      WRITE OUTPUT TAPE 3,5018,LASORR
      WRITE OUTPUT TAPE ITAPF4,5018,LASORR
5018 FORMAT (1H0,27X13H ORBIT NUMBR 16)
      WRITE OUTPUT TAPE 3,4006,APRINT
      LL11 = LL11 + 3
      LL12 = LL12 + 2
5017 NFND = (NLA*2) + 6
      WRITE OUTPUT TAPE 3,6052,(MVI(1)),I = 4,5),(MVI(1)),I = 7,NEND)
      IF(MAP) 5014,5014,102
      102 LINF4 = 1
      IF(K-1) 5009,5008,5009
5008 IMOS = 32767
      WRITE OUTPUT TAPE ITAPF4,3076,IBGORB
      WRITE OUTPUT TAPE ITAPF4,332,IDSAT
      LL12 = 3
5009 CALL BACK(PRF,11,IMOS)
C   RETURN PRF
      IMOS = IMOS - 11
      MVI(6) = PRF(1)
      WRITE OUTPUT TAPE ITAPF4,4006,APRINT
      4006 FORMAT (114X,A6)
      WRITE OUTPUT TAPE ITAPF4,323,(MVI(K),K = 1,5),(PRE(K),K = 2,11)
      LL12 = LL12 + 2
      IF(LL12 = 40) 5024,5024,5023
5023 WRITE OUTPUT TAPE ITAPF4,3076,MVI(7)
      WRITE OUTPUT TAPE ITAPF4,4005
      LL12 = 3
5024 IF(MVI(6) - 1) 5014,5014,5010
5010 IPPP = MVI(6)
      DR 3056 I = 2,IPPP
      CALL BACK(PRF,7,IPPS)
      IMOS = IMOS - 7
      WRITE OUTPUT TAPE ITAPF4,3051,(PRF(K), K = 1,6)
      LINF2 = LINF2 + 1
      LL12 = LL12 + 1
      IF(LL12 = 40)3056,3056,4004
4004 WRITE OUTPUT TAPE ITAPF4,3076,MVI(7)
      WRITE OUTPUT TAPE ITAPF4,4005
4005 FORMAT ( 20XSHRANG,4X,4HAZ1,2X,5HELEV,2X,8HSC/L 00K,2X,4HLAT,
      1,2X,5HLONG,2X6HFHEIGHT /
      210H YYMMDD HHHM STAT,3X,4H(K),4X,35H-----DEGREES-----
      3-----,3X,4H(K) )
      LL12 = 2
3056 CONTINUE
5014 LL11 = LL11 + 1
      IF(LL11 = NLSPP) 3054,3054,4003
4003 WRITE OUTPUT TAPE 3,3089
      LL11 = 2
      NPAGF = 10
3054 CONTINUE
      WRITE OUTPUT TAPE 3,9501
      WRITE OUTPUT TAPE ITAPF4,9501
      LC2 = 3
C
C   PUT SENSF SWITCH 3 DOWN TO TERMINATE RUN BEFORE THE END TIME.
C
      IF(SFNSF SWITCH 3)5012,3059
3059 CONTINUE
      323 FORMAT(1X,31Z,X,21Z,X,2A3,F9.1,2F6.1,F7.1,F10.1,F7.1,F9.1,X,A3)
      332 FORMAT (15H LOCAL STATION PREDICTIONS AND SATELLITE WORLD MAP FOR
      1A5/20XSHRANG,4X,4HAZ1,2X,5HELEV,2X,8HSC/L 00K,2X,4HLAT,2X,
      25HLONG,2X6HFHEIGHT /
      310H YYMMDD HHHM STAT,3X,4H(K),4X,35H-----DEGREES-----
      4-----,3X,4H(K) )
      317 IF(OTIMFS = XLAF)9601,248,248
      247 CONTINUE
      IF(OTIMFS = XLAF) 9600,5015,5C15
      5015 IF(LL11 = 2) 1,248,248,2460
      248 IF (SPNSF SWITCH 2) 249,7C10
      249 PRINT 6025
      PAUSE 77774

```

```

7010 IF(LPAS) 5012,5011,5012
5011 LPAS = 10
GO TO 2460
5012 JMX = 9
WRITE OUTPUT TAPE ITAPF4,3031,IDSAT
WRITE OUTPUT TAPE 5,3032,JMX
END FILE 5
REWIND 5
3033 READ INPUT TAPF 5,3032,JMX,(SA(I),I = 1,12)
3032 FORMAT (11,11(A6),A3)
IF(JMX - 9)3036,3035,3034
3034 WRITE OUTPUT TAPE ITAPF5,3036,(SA(I),I = 1,12)
3036 FORMAT (11,11(A6),A3)
GO TO 3033
3035 REWIND 5
GO TO 3000
C
C FND LOCAL STATION PRFDICTIONS CALCULATION
C
390 PRINT 6039
END FILE 3
PAUSE 77777
GO TO 10
END

```

APPENDIX VI
SOURCE DECK FOR MAIN PROGRAM TWO

```

* DATE 10/19/64
* GDR
* PAUSE
* XEQ
* CARDS COLUMN
* LIST8
* LABEL
* FORMAP
C HWAPLA
C
C GENERALIZED WORLD MAP AND LOCAL STATION PREDICTIONS PROGRAM.
C
C 1A. CONVERTS OSCULATING ORBITAL ELEMENTS TO INERTIAL POSITION
C AND VELOCITY RECTANGULAR COORDINATES.
C 1B. CONVERTS INERTIAL POSITION AND VELOCITY RECTANGULAR
C COORDINATES TO OSCULATING ORBITAL ELEMENTS.
C 2. COMPUTES WORLD MAP ON REQUEST.
C 3. COMPUTES LOCAL STATION PREDICTIONS (LOOK ANGLES) ON REQUEST.
C PROCESSES 1, 2, 3, OR 4 STATIONS SIMULTANEOUSLY ON REQUEST.
C
C ALL INTERNAL CALCULATIONS ARE PERFORMED USING THE KILOMETER AS
C THE UNIT OF LENGTH AND THE SECOND AS THE UNIT OF TIME. IF ANY
C OF THE OPTIONAL INPUT PARAMETERS ARE DEFINED IN OTHER UNITS,
C THEY ARE CONVERTED TO THESE UNITS AS SOON AS THEY ARE READ IN
C AND ARE SUBSEQUENTLY USED IN THE CALCULATIONS IN KILOMETERS
C AND SECONDS.
C
C
C REQUIRED SUBROUTINES AND FUNCTIONS
C
C ALLOT
C ALL0TZ
C ATANO
C ATANZ
C BRWR
C BRWR1
C BRWR2
C DJUL
C DMSRZ
C DOTZ
C ELRV
C ELRVZ
C FON
C GASTZ
C GOLATZ
C HMSRZ
C JULCAL
C PARA
C RDMSZ
C RHMSZ
C RVELZ
C R13Z
C TIMEC
C VFUZ
C VRDZ
C XKEP
C XKEPZ
C
C Z END OF NAME OF FUNCTION OR SUBROUTINE INDICATES THAT INPUT,
C OUTPUT, AND INTERNAL ARITHMETIC ARE PERFORMED IN DOUBLE PRECISION.
C
C DEFINITION OF SYMBOLS
C
C ERR = TRUNCATION FACTOR (IN RADIAN) USED IN SOLUTION OF
C KEPLER'S EQUATION
C GM = PRODUCT OF G (=GAUSSIAN CONSTANT SQUARED) AND M, THE MASS OF
C THE EARTH, IN UNITS OF KM. CUBED/SEC SQUARED
C FJ2=J2 )
C FJ3=J3 ) HARMONICS OF EARTH'S GRAVITATIONAL POTENTIAL
C FJ4=J4 ) (DIMENSIONLESS)
C FJ5=J5 )
C FL=INVERSE OF FLATTENING
C RE= EQUATORIAL RADIUS OF EARTH IN KM.
C
C SENSE SWITCH 6 IS USED IN THE MAIN PROGRAM TO PROVIDE AN OPTIONAL
C OUTPUT ON LINE. IF SENSE SWITCH 6 IS DOWN, THE SAME INFORMATION
C WHICH IS PRINTED ON TAPE A3 IS ALSO PRINTED ON LINE. IF SENSE
C SWITCH 6 IS UP, OUTPUT IS PRINTED ON A3 ONLY.
C
C ALL FORMATS USED IN PROGRAM FOLLOW IMMEDIATELY.
C
C 6001 FORMAT (36HISANDTRACKS ORBITAL COMPUTING SYSTEM //)
C 6002 FORMAT (72H
C 1
C 6003 FORMAT (713)
C 6004 FORMAT (E12.6,4E12.5/2F12.4)
C 6005 FORMAT (/ IX1PE8.1,9X39H TOLERANCE REQUIRED FOR KEPZ SUBROUTINE//
C 1 X0PF8.3,9X39H EQUATORIAL RADIUS OF EARTH IN KM /2XF5.1,11X22H IN
C 2VERSE OF FLATTENING/1X,1PE14.8,3X31H GM (KM. CUBED/SECONDS SQUARED
C 3 /18X44H HARMONICS OF EARTH'S GRAVITATIONAL POTENTIAL /1XE19.6,
C 4 4X3H J2/1X,E13.6,4X3H J3/1X,E13.6,4X3H J4 /1X,E13.6,4X3H J5 )
C 6006 FORMAT (21X12,1X14,213,F7.3/6F12.6)
C 6008 FORMAT (/1X13,14X20H INPUT @PT10N NUMBER/18X24H INPUT PARAMETERS A

```



```

1RF--- //)
6009 FORMAT (46H GEOCENTRIC EQUATORIAL RECTANGULAR COORDINATES/70H REQU
IRED UNITS - CENY MIXED UP VANGUARD UNITS OF LENGTH AND VELOCITY)
6010 FORMAT ( // 1X12+21H/12,1H/14,7X29H EPOCH DATE OF PARAMETERS,21X12),
1 F7.3,5X29H EPOCH TIME OF PARAMETERS-UT2 )
6011 FORMAT (16X,F12.9, 20H X1 - VANGUARD UNITS/6X,F12.9, 3H X2/
1 6X,F12.9, 3H X3/6X,F12.9, 20H VX1- VANGUARD UNITS/6X,F12.9,
2 4H VX2/6X,F12.9, 4H VX3 )
6012 FORMAT (30H ORBITAL ELEMENTS - OSCULATING/69H PEQUIRED UNITS - ALL
1 ANGLES IN DEGREES,SEMI-MAJOR AXIS IN KILOMETERS )
6013 FORMAT ( // 2X,F11.4,5X,27H SEMI-MAJOR AXIS-KILOMETERS/6X,F11.8,
1 14H ECCENTRICITY/6X,F12.6,3X,12H INCLINATION,3X,9H -DEGREES/3X,
2 F12.6,3X,24H R.A. ASC. NODE -DEGREES/3X,F12.6,3X,24H ARG. OF PERI
3 GEE-DEGREES/3X,F12.6,3X,24H MEAN ANOMALY -DEGREES )
6014 FORMAT ( //18X,25H NO WORLD MAP CALCULATION )
6016 FORMAT ( //45H WORLD MAP CALCULATIONS - START AND END TIMES//)
6017 FORMAT ( //18X,26H NO LOOK ANGLE CALCULATION )
6018 FORMAT ( //46H LOOK ANGLE CALCULATIONS - START AND END TIMES//)
6019 FORMAT ( // 32H QUANTITIES COMPUTED FROM INPUT )
6020 FORMAT ( // 1X,F13.5,4X,16H X1 - KILOMETERS/1X,F13.5,4X,3H X2/1X,
1 F13.5,4X,3H X3/5X,F12.8,22H VX1- KILOMETERS/SEC./5X,F12.8,
2 5H VX2/5X,F12.8,5H VX3 )
6021 FORMAT ( // 2X,F11.4,5X,27H SEMI-MAJOR AXIS-KILOMETERS/6X,F11.8,
1 14H ECCENTRICITY/3X,F12.6,3X,12H INCLINATION,3X,9H -DEGREES/3X,
2 F12.6,3X,24H R.A. ASC. NODE -DEGREES/3X,F12.6,3X,24H ARG. OF PERI
3 GEE-DEGREES/3X,F12.6,3X,24H MEAN ANOMALY -DEGREES )
6022 FORMAT ( // 4X,F11.6,3X,7H PERIOD,8X,7H -HOURS/2X,F11.4,20X,9H -MINUT
1 ES/4X,F11.6,3X,12H MEAN MOTION,3X,14H -DEGREES/HOUR/4X,F11.6,3X,
2 15H MOTION OF NODE,8X,14H -DEGREES/DAY/4X,F11.6,3X,18H NOTION OF
3 PERIGEE,5X,14H -DEGREES/DAY )
6023 FORMAT (5H DATE,6X,14H UNIVERSAL TIME,16X,20H GEODETIC COORDINATES/
1 9H MO/DY/YR,3X,4HH M,3X,4HSEC.,9X,39H LATITUDE-DMS LONGITUDE-DMS H
2 FIGHT-KM, //)
6024 FORMAT ( //1X12+1H/,12+1H/,12,2X213+P7.3,8X213+P6.2,2X14+,13+P6.2,
1 F11.3 )
6025 FORMAT (11H PUSH START //)
6026 FORMAT (11H//15X,39H LOCAL STATION PREDICTIONS FOR -- //8H STATION,
1 5X,10H LONGITUDE,5X,10H LATITUDE,4X,16H HEIGHT (METERS) //)
6027 FORMAT (1X,2A3,15,13,F7.3,14,13,F7.3,F11.2 )
6028 FORMAT (1X,2A3,5X14,13,F7.3,15,13,F7.3,4XF10.2 )
6037 FORMAT (11H//4510H WORLD MAP //)
6038 FORMAT (27HLOCAL STATION PREDICTIONS )
6039 FORMAT (13H JOB FINISHED //)
6040 FORMAT (E8.2)
6041 FORMAT (28HIEXCUTE MAIN PROGRAM-WMAPLA/1H)
6042 FORMAT (1C EQUATORIAL INERTIAL COORDINATES/
1 90H REQUIRED UNITS - KILOMETERS AND KILOMETERS/SECOND)
6043 FORMAT (1X,F13.5,4X,17H X1 - KILOMETERS/1X,F13.5,4X,
1 17H X2 - KILOMETERS/1X,F13.5,4X,17H X3 - KILOMETERS//5X,F12.8,
2 1X,13H VX1 - KM/SEC/5X,F12.8,1X,13H VX2 - KM/SEC/5X,F12.8,1X,
3 13H VX3 - KM/SEC)
6044 FORMAT ( //18X,50H BROUWER HARMONICS COMPUTED FROM J2,J3,J4, AND J5
1 /1X,1PE14+8,3X,24H K2 (KILOMETERS SQUARED)/1X,E14+8,3X,
2 22H K3 (KILOMETERS CUBED)/1X,E14+8,3X,
3 29H K4 (KILOMETERS FOURTH POWER)/1X,E14+8,3X,
4 28H K5 (KILOMETERS FIFTH POWER) //)
6045 FORMAT ( //4X,63H POSITION AND VELOCITY VECTORS - GEOCENTRIC EQUATOR
1 IAL INERTIAL )
6046 FORMAT ( //1X,F13.5,4X,17H X1 - KILOMETERS,3X,F12.8,1X,
1 21H X1 - VANGUARD UNITS/1X,F13.5,4X,17H X2 - KILOMETERS,3X,
2 F12.8,1X,21H X2 - VANGUARD UNITS/1X,F13.5,4X,
3 17H X3 - KILOMETERS,3X,F12.8,1X,21H X3 - VANGUARD UNITS)
6047 FORMAT ( //5X,F13.5,4X,17H X1 - KM/SEC,7X,F12.8,1X,
1 21H VX1 - VANGUARD UNITS/5X,F12.8,1X,13H VX2 - KM/SEC,7X,F12.8,
2 1X,21H VX2 - VANGUARD UNITS/5X,F12.8,1X,13H VX3 - KM/SEC,7X,
3 F12.8,1X,21H VX3 - VANGUARD UNITS//1X,F13.5,4X,
4 17H R - KILOMETERS,3X,F12.8,1X,21H R - VANGUARD UNITS/5X,
5 F12.8,1X,13H V - KM/SEC,7X,F12.8,1X,
6 21H V - VANGUARD UNITS)
6048 FORMAT ( //26X,17H ORBITAL ELEMENTS/20H OSCULATING ELEMENTS,2X,
1 22H BROUWER MEAN ELEMENTS//1X,F12.4,11X,F12.4,7X,
2 29H SEMI-MAJOR AXIS - KILOMETERS/6X,F11.8,12X,F11.8,3X,
3 13H ECCENTRICITY/4X,F11.6,12X,F11.6,5X,
4 26H INCLINATION - DEGREES/4X,F11.6,12X,F11.6,5X,
5 26H R.A. ASC. NODE - DEGREES/4X,F11.6,12X,F11.6,5X,
6 26H ARG. OF PERIGEE - DEGREES/4X,F11.6,12X,F11.6,5X,
7 26H MEAN ANOMALY - DEGREES)
6049 FORMAT ( //45H TRUNCATION FACTORS USED IN COMPUTING BROUWER /
1 39H MEAN ELEMENTS FROM OSCULATING ELEMENTS//1X,1PE8+1,9X,
2 29H SEMI-MAJOR AXIS - KILOMETERS/1X,E8.1,9X,13H ECCENTRICITY/1X,
3 E8.1,9X,26H INCLINATION - DEGREES/1X,E8.1,9X,
4 26H R.A. ASC. NODE - DEGREES/1X,E8.1,9X,
5 26H ARG. OF PERIGEE - DEGREES/1X,E8.1,9X,
6 26H MEAN ANOMALY - DEGREES )
6050 FORMAT ( //F12.8)
6051 FORMAT (22H BROUWER MEAN ELEMENTS/69H REQUIRED UNITS - ALL ANGLES
1 IN DEGREES,SEMI-MAJOR AXIS IN KILOMETERS )
6052 FORMAT ( //1X12+21H/12,1X,213/,F7.3,5X,12(ZXA3))
9501 FORMAT (11H,8H *****)
9502 FORMAT (11H,07H MUTUAL VISIBILITY//)
9503 FORMAT ( //SHDATE,5X15H UNIVERSAL TIME/23H MO/DY/YR H M SEC.,
1 5X,12(ZXA3))

```

```

9504 FORMAT(1H1//15X33H LOCAL STATION PREDICTIONS FOR -- //8H STATION,
15X10H LONGITUDE ,6X9H LATITUDE,4X16H HEIGHT (METERS)//)
9505 FORMAT (3I3,F10.0)
9506 FORMAT(A#6.1)
9507 FORMAT(1//17X26HNO STATION PRINT OUT IF ---//
11X,25H1. ELEVATION IS LESS THAN,14X,13. 8H DEGREES/
21X,25H2. RANGE IS GREATER THAN ,7X,F9.0,12H KILOMETERS/
31X,30H3. RADAR ANGLE IS GREATER THAN,6X,F6.1,8H DEGREES/
419X,12HOR LESS THAN,6X,F6.1,8H DEGREES//)
54X,25H5HIN AXIS COORDINATES ARE,8X,F6.1,24H DEGREE RIGHT ASCENSIN@
6N/37X,F6.1,20H DEGREE DECLINATION )
7500 FORMAT(5HODATE,7X3HUTZ,15X5HRRANGE,3X2HAZ,3X2HEL,3X5HRRADAR/
1 9H M@D@Y/YR,16H . H M STATION,6X4H(KM),12H (DEG) (DEG) .
2 12H ANGLE F (DEG) //)
7501 FORMAT(XI2,2(1H/12),1X,2(13),2X,2A3,3XF8.1,1XF5.1,XF4.1,2XF5.1/
118X,2A3,3XF8.1,XF5.1,XF4.1,2XF5.1/18X,2A3,3XF8.1,XF5.1,XF4.1,2X
2F5.1/18X,2A3,3XF8.1,XF5.1,XF4.1,2XF5.1/18X,2A3,3XF8.1,XF5.1,XF4.1
3 , 2XF5.1/18X,2A3,3XF8.1,XF5.1,XF4.1,2XF5.1/18X,2A3,3XF8.1,XF5.1
4 ,XF4.1,2XF5.1/18X,2A3,3XF8.1,XF5.1,XF4.1,2XF5.1/18X,2A3,3XF8.1
5 ,XF5.1,XF4.1,2XF5.1/18X,2A3,3XF8.1,XF5.1,XF4.1,2XF5.1/18X,2A3,3X
6 F8.1,XF5.1,XF4.1,2XF5.1/
718X,2A3,3XF8.1,XF5.1,XF4.1,2XF5.1)
C
C ALL DIMENSION STATEMENTS FOLLOW IMMEDIATELY.
C
C DIMENSION RX(3),VX(3),A(6),A(16),RG(3),VG(3),RLAT(12),RLON(12)
D
D DIMENSION RGU(3),Z(3),C@GRD(3),U(3),SU(12,3)
D DIMENSION ELED(12),AZID(12),RGE(12),TESTA(12),STAT1(12),STAT2(12)
D DIMENSION RGE1(12),ELED1(12),AZID1(12),TESTA1(12),STAT3(12)
D DIMENSION GP(5),DA(6),DAD(6),A1(10),XX(12),AD(6),RXB(3)
D
D DIMENSION VXE(3),RTX(3)
D DIMENSION STATA(12),DATA(12),VXB(3),XXX(10),SS(3)
D DIMENSION DUM1(100)
COMMON DUM1,A110,GP,ERRB,XX,AB,RXB,VXB,XXX,SS
C
C PRINT 6041
C
C DEFINE TRUNCATION FACTOR (RADIAN)
C
C 1 FRR=1,DE-8
D FRRB=3,DE-7
D EN2 = 0.0
C
C DEFINE TRUNCATION FACTORS FOR SUBROUTINE BBRWR I USED TO CONVERT
C OSCILLATING ELEMENTS TO BROWNER MEAN ELEMENTS)
C
DAD(1)=5,OF-4
DAD(2)=5,OF-6
DAD(3)=5,OF-6
DAD(4)=5,OE-6
DAD(5)=5,OF-6
DAD(6)=5,OE-6
C
C LC2=0
B APRINT=60 60 60 60 60 60
B BPRINT = 60 60 54 60 60 60
C
C DEFINE GODDARD EARTH CONSTANTS
C
D GM=3.986032E+5
D FJ2=1.0823E-3
D FJ3=-2.3E-6
D FJ4=-1.8E-6
D FJ5=0.0
D FL=298.3
D RE=6378.165
C
C CARD 1 - READ IN I.D. CARD - ANY INFORMATION IN COLS. 2 - 72
C
C RFDAD 6002
C
C CARD 2 - READ IN CONTROL CARD
C
C COLS. 1- 3 TYPE OF INPUT +01 = OSCILLATING ORBITAL ELEMENTS
C +02 = INERTIAL POSITION AND VELOCITY
C IN KILOMETERS AND KM/SEC
C +03 = INERTIAL POSITION AND VELOCITY
C IN VANGUARD UNITS
C +04 = BROWNER MEAN ELEMENTS )
C
C COLS. 4- 6 COMPUTE WORLD MAP - YES OR NO ( YES IF MAP=+XX, NO IF
C MAP=+00 OR -XX)
C COLS. 7- 9 COMPUTE LOOK ANGLES - YES OR NO (YES IF LA=+XX, NO IF
C LA=+00 OR -XX)
C
C COLS. 10-12 CHANGE EARTH CONSTANTS
C COLS. 13-16 CHANGE TRUNCATION FACTOR
C
C READ 6003,INPUT,MAP,LA,MCST,NERR,HDA,IRC
C
C TEST - HAVE ALL CASES BEEN RUN - YES OR NO
C
C IF (INPUT) 300,300,Z

```

```

C      IF INPUT=+00 OR -XX, ALL CASES HAVE BEEN RUN. GO TO 300 (END
C      FILE, REWIND AND UNLOAD A3). IF INPUT =+XX, PROCEED TO NEXT CASE.
C
C      TEST - CHANGE TRUNCATION FACTOR - YES OR NO
C
C      2 IF (NERR) 4,4,3
C
C      CARD 2A- (OPTIONAL) READ IN NEW VALUE OF TRUNCATION FACTOR IF
C      NERR=+XX. IF NERR=+00 OR -XX, PROCEED TO NEXT
C      OPTION TEST.
C
C      3 READ          6040,ERR
C
C      TEST - CHANGE EARTH CONSTANTS - YES OR NO
C
C      4 IF (NCST) 5,11,10
C
C      IF NCST=+00, RETAIN STANDARD GODDARD EARTH CONSTANTS AND PROCEED
C      TO NEXT STEP.
C
C      5 IF (NCST+1) 7,6,7
C
C      USE S1RY PACKAGE CONSTANTS IF NCST = -1
C
C      6 GM=3,9862688E+05
C      D FJ2=1,08219E-03
C      D FJ3=-2,285E-06
C      D FJ4=-2,123F-06
C      D FJ5=-2,32F-07
C      D FL=297,0
C      D RE=6378,388
C      GO TO 11
C      7 IF (NCST+2) 9,8,11
C
C      USE GODDARD EARTH CONSTANTS WITH HARMONICS = 0 IF NCST = -2
C
C      8 FJ2=0,0
C      D FJ3=0,0
C      D FJ4=0,0
C      D FJ5=0,0
C      GO TO 11
C
C      USE INTERNATIONAL CONSTANTS WITH HARMONICS = 0 IF NCST = -3
C
C      9 GM=3,98626873E+5
C      D FJ2=0,0
C      D FJ3=0,0
C      D FJ4=0,0
C      D FJ5=0,0
C      D FL=297,0
C      D RF=6378,388
C      GO TO 11
C
C      CARDS 2B AND 2C- (OPTIONAL) READ IN NEW SET OF EARTH CONSTANTS
C      IF NCST=+XX.
C
C      10 READ          6004,GM,FJ2,FJ3,FJ4,FJ5,FL,RE
C
C      CONVERT EARTH CONSTANTS
C
C      11 GP(1)=GM
C      GP(2)=.5*FJ2*RE**2
C      GP(3)=-FJ3*RE**3
C      GP(4)=-.375*FJ4*RE**4
C      GP(5)=-FJ5*RE**5
C
C      PRINT ALL QUANTITIES ON OUTPUT TAPE A3.
C
C      12 WRITE OUTPUT TAPE 3,6001
C      WRITE OUTPUT TAPE 3,6002
C      WRITE OUTPUT TAPE 3,6005,ERR,RE,FL,GM,FJ2,FJ3,FJ4,FJ5
C      WRITE OUTPUT TAPE 3,6044,GP(2),GP(3),GP(4),GP(5)
C      IF (SFNSF SWITCH 6) 13,913
C
C      PRINT SAME INFORMATION ON LINE IF SENSE SWITCH 6 IS DOWN.
C
C      13 PRINT 6001
C      PRINT 6002
C      PRINT 6005,ERR,RE,FL,GM,FJ2,FJ3,FJ4,FJ5
C      PRINT 6044,GP(2),GP(3),GP(4),GP(5)
C      913 IF (NDA) 915,915,914
C      914 READ          6050, (DAD(N), N=1,6)
C      915 DA(1)=DAD(1)
C      DA(2)=DAD(2)
C      DO 916 N=3,6
C      916 DA(N)=DAD(N)*0.017453292
C      IF (IRCI 917,917,918
C      917 IRC=50 -
C
C      CARD 3 - READ IN EPOCH OF INPUT PARAMETERS-CALENDAR DATE (MONTH,
C      DAY, AND YEAR) AND UNIVERSAL TIME (HOURS, MINUTES, AND
C      SECONDS TO 3 DECIMALS OF A SECOND).

```

```

C   CARD 4 - READ IN PARAMETERS
C
C   918 READ          6006,NME,NDE,NYE,NHE,NMNE,TSE,(AI(N),N=1,6)
C
C   PRINT EP0CH AND INPUT OPTION 0N OUTPUT TAPE A3
C
C   15 WRITE OUTPUT TAPE 3,6010,NME,NDE,NYE,NHE,NMNE,TSE
C   WRITE OUTPUT TAPE 3,6008,INPUT
C   IF (SENSE SWITCH 6) 16,17
C
C   PRINT SAME INFORMATION 0N-LINE IF SENSE SWITCH 6 IS DOWN
C
C   16 PRINT 6010,NME,NDE,NYE,NHE,NMNE,TSE
C   PRINT 6008,INPUT
C   17 CONTINUE
C
C   CONVERT EP0CH UNIVERSAL TIME IN HOURS, MINUTES, AND SECONDS
C   TO EP0CH UNIVERSAL TIME IN RADIANs.
C
C   TIME0=HMSRZ(NHE,NMNE,TSE)
C
C   CONVERT EP0CH CALENDAR DATE TO EP0CH JULIAN DATE AT 0 HOURS
C   UNIVERSAL TIME.
C   DJ0=DJUL(NME,NDE,NYE)
C
C   CONVERT EP0CH UNIVERSAL TIME IN HOURS, MINUTES, AND SECONDS
C   TO SECONDS.
C
C   THE=NHE*3600
C   TMNE=NMNE*60
C   TSEP=THE+TMNE+TSE
C   GO TO (18,20,22,930) , INPUT
C
C   PRINT INPUT PARAMETERS 0N OUTPUT TAPE A3 - INPUT OPTION 1
C   OSCULATING ORBITAL ELEMENTS -
C   1. SEMI-MAJOR AXIS IN KM 2. ECCENTRICITY 3. INCLINATION 4. RIGHT
C   ASCENSION OF ASCENDING NODE 5. ARGUMENT OF PERIGEE 6. MEAN ANOMALY
C   (ALL ANGLES I.E. 3,4,5, AND 6 ARE IN DEGREES).
C
C   18 WRITE OUTPUT TAPE 3,6012
C   WRITE OUTPUT TAPE 3,6013,(AI(N),N=1,6)
C   IF (SENSE SWITCH 6) 19,28
C
C   PRINT SAME INFORMATION 0N-LINE IF SENSE SWITCH 6 IS DOWN
C
C   19 PRINT 6012
C   PRINT 6013,(AI(N),N=1,6)
C   GO TO 28
C
C   PRINT INPUT PARAMETERS 0N OUTPUT TAPE A3 - INPUT OPTION 2
C   INERTIAL POSITION AND VELOCITY RECTANGULAR COORDINATES -
C   IN KILOMETERS AND KILOMETERS PER SECOND.
C
C   20 WRITE OUTPUT TAPE 3,6042
C   WRITE OUTPUT TAPE 3,6043,(AI(N),N=1,6)
C   IF (SENSE SWITCH 6) 21,28
C
C   PRINT SAME INFORMATION 0N-LINE IF SENSE SWITCH 6 IS DOWN
C
C   21 PRINT 6042
C   PRINT 6043,(AI(N),N=1,6)
C   GO TO 28
C
C   PRINT INPUT PARAMETERS 0N OUTPUT TAPE A3 - INPUT OPTION 3
C   INERTIAL POSITION AND VELOCITY RECTANGULAR COORDINATES -
C   IN VANGUARD UNITS.
C
C   22 WRITE OUTPUT TAPE 3,6009
C   WRITE OUTPUT TAPE 3,6011,(AI(N),N=1,6)
C   IF (SENSE SWITCH 6) 23,28
C
C   PRINT SAME INFORMATION 0N-LINE IF SENSE SWITCH 6 IS DOWN
C
C   23 PRINT 6009
C   PRINT 6011,(AI(N),N=1,6)
C   GO TO 28
C
C   PRINT INPUT PARAMETERS - INPUT OPTION 4 - BROUWER MEAN ELEMENTS
C
C   930 WRITE OUTPUT TAPE 3,6051
C   931 WRITE OUTPUT TAPE 3,6013,(AI(N),N = 1,6)
C   IF (SENSE SWITCH 6) 932,28
C
C   PRINT SAME INFORMATION 0N-LINE IF SENSE SWITCH 6 IS DOWN
C
C   932 PRINT 6051
C   PRINT 6013,(AI(N), N = 1,6)
C
C   CONVERT INPUT PARAMETERS TO OSCULATING ELEMENTS

```

```

D 28 CALL PARA (INPUT ,AI ,A ,GM)
D CALL ELRVZ (RX ,VX ,A ,PER ,EN ,GM ,ERR)
D CALL BBRWR (DA ,A ,IRC ,NN)
D VXE (1) =VX (1)
D VXE (2) =VX (2)
D VXE (3) =VX (3)
D FN =SS (1)
D DP =SS (2)
D DN =SS (3)
D PER =6.28318530718 /EN
D PERM =PER /60.0
D PERH =PER /3600.0
D EN1 =EN *206264.806247096
D DN0DE =DN *4950355.3499303
D DPERI =DP *4950355.3499303
C
C TEST - IS WORLD MAP DESIRFO
C
D 29 IF (MAP) 30,30,33
D 30 WRITE OUTPUT TAPE 3,6014
D IF (SENSE SWITCH 6) 31,36
D 31 PRINT 6014
D 32 GO TO 36
C
C CARD 5A - WORLD MAP IS DESIRED. READ IN CALENDAR DATE (DAY,
C MONTH, AND YEAR) AND UNIVERSAL TIME (HOURS, MINUTES,
C AND SECONDS TO 3 DECIMALS OF A SECOND) AT WHICH THE
C START OF CALCULATION IS DESIRED, CALENDAR DATE AND
C UNIVERSAL TIME AT WHICH THE TERMINATION OF THE
C CALCULATION IS DESIRED, AND THE DESIRED TIME INCREMENT
C OF THE CALCULATION IN SECONDS TO 3 DECIMALS OF A SECOND.
C
D 33 WRITE OUTPUT TAPE 3,6016
C
C PRINT SAME INFORMATION ON-LINE IF SENSE SWITCH 6 IS DOWN
C
D IF (SENSE SWITCH 6) 34,35
D 34 PRINT 6016
D 35 CALL TIMEC (DJO ,TSEP ,WMAPS ,WMAPF ,WMAFDT)
C
C TEST - ARE STATION PREDICTIONS (LOOK ANGLES) DESIRED
C
D 36 IF (LA) 37,37,40
D 37 WRITE OUTPUT TAPE 3,6017
D IF (SENSE SWITCH 6) 38,43
D 38 PRINT 6017
D 39 GO TO 43
C
C CARD 5B - STATION PREDICTIONS (LOOK ANGLES) ARE REQUIRED. READ
C IN CALENDAR DATE AND UNIVERSAL TIME AT WHICH THE START
C OF THE CALCULATION IS DESIRED, CALENDAR DATE AND
C UNIVERSAL TIME AT WHICH THE TERMINATION OF THE
C CALCULATION IS DESIRED, AND THE DESIRED TIME INCREMENT
C OF THE CALCULATION IN SECONDS.
C
D 40 WRITE OUTPUT TAPE 3,6018
C
C PRINT SAME INFORMATION ON-LINE IF SENSE SWITCH 6 IS DOWN
C
D IF (SENSE SWITCH 6) 41,42
D 41 PRINT 6018
D 42 CALL TIMEC (DJO ,TSEP ,XLAS ,XLAF ,DTLA)
D 43 WRITE OUTPUT TAPE 3,6001
D WRITE OUTPUT TAPE 3,6002
D WRITE OUTPUT TAPE 3,6019
D WRITE OUTPUT TAPE 3,6010,NME,NDE,NYE,NHE,NMNE,TSE
C
C PRINT SAME INFORMATION ON-LINE IF SENSE SWITCH 6 IS DOWN
C
D IF (SENSE SWITCH 6) 44,45
D 44 PRINT 6001
D PRINT 6002
D PRINT 6019
D PRINT 6010,NME,NDE,NYE,NHE,NMNE,TSE
D 45 CONTINUE
C
C CONVERT OSCILLATING ORBITAL ELEMENTS TO INERTIAL POSITION AND
C VELOCITY COORDINATES IN KM AND KM/SEC
C
D 46 CALL ELRVZ (RX ,VX ,A ,PER ,EN ,GM ,ERR)
D R1 =SORTF (RX (1) **2 +RX (2) **2 +RX (3) **2)
D V1 =SORTF (VX (1) **2 +VX (2) **2 +VX (3) **2)
C
C CONVERT TO VANGUARD UNITS OF LENGTH AND VELOCITY
C
D 47 X01 =RX (1) /6378.388
D X02 =RX (2) /6378.388
D X03 =RX (3) /6378.388
D V01 =VX (1) /7.9054722668
D V02 =VX (2) /7.9054722668
D V03 =VX (3) /7.9054722668

```

```

D      R2=SQRT(X01**2+X02**2+X03**2)
D      V2=SQRT(V01**2+V02**2+V03**2)
C
C      CONVERT ANGLES (RADIAN) TO ANGLES (DEGREES)
C
D      A01=A(1)
D      A02=A(2)
D      A03=A(3)*57.2957795130823
D      A04=A(4)*57.2957795130823
D      A05=A(5)*57.2957795130823
D      A06=A(6)*57.2957795130823
48 WRITE OUTPUT TAPE 3,6045
   WRITE OUTPUT TAPE 3,6046,RX(1),X01,RX(2),X02,RX(3),X03
   WRITE OUTPUT TAPE 3,6047,VX(1),V01,VX(2),V02,VX(3),V03,R1,R2,V1,V2
   WRITE OUTPUT TAPE 3,6049,(DAD(I) , I = 1,6)
   B1=A110(1)
   B2=A110(2)
   B3=A110(3)*57.2957795
   B4=A110(4)*57.2957795
   B5=A110(5)*57.2957795
   B6=A110(6)*57.2957795
   WRITE OUTPUT TAPE 3,6048,A01,B1,A02,B2,A03,B3,A04,B4,A05,B5,A06,B6
   WRITE OUTPUT TAPE 3,6022,PERH,PERM,EN1,DNODE,DPERI
   IF (SENSE SWITCH 6) 49,50
C
C      PRINT SAME INFORMATION ON-LINE IF SENSE SWITCH 6 IS DOWN
C
C
49 PRINT 6045
   PRINT 6046,RX(1),X01,RX(2),X02,RX(3),X03
   PRINT 6047,VX(1),V01,VX(2),V02,VX(3),V03,R1,R2,V1,V2
   PRINT 6048,A01,B1,A02,B2,A03,B3,A04,B4,A05,B5,A06,B6
   PRINT 6022,PERH,PERM,EN1,DNODE,DPERI
50 CONTINUE
53 IF (MAP) 199,199,100
C
C      BEGIN WORLD MAP CALCULATION (NO CALCULATION IF MAP = 0)
C      SKIP A PAGE AND PRINT HEADING FOR WORLD MAP CALCULATIONS
C
100 WRITE OUTPUT TAPE 3,6037
   WRITE OUTPUT TAPE 3,6023
   IF (SENSE SWITCH 6) 101,102
101 PRINT 6037
   PRINT 6023
C
C      INITIALIZE LINE COUNT AND DELTA T (DIFFERENCE BETWEEN
C      WORLD MAP STARTING TIME AND EPOCH OF INPUT PARAMETERS IN SECONDS)
C
C
102 LINES=1
   DTIMES=WMAPS-WMAPDT
   IF (SENSE SWITCH 1) 1030,103
1030 PRINT 6025
   PAUSE 7777
103 LINES=LINES+1
C
C      SKIP A PAGE AND PRINT HEADING IF 50 LINES OF CALCULATION
C      HAVE BEEN PRINTED
C
   IF (LINES-50) 106,106,104
104 WRITE OUTPUT TAPE 3,6037
   WRITE OUTPUT TAPE 3,6023
   LINES=1
105 IF (SENSE SWITCH 6) 105,106
105 PRINT 6037
   PRINT 6023
D 106 DTIMES=DTIMES+WMAPDT
   TIME=TIME+DTIMES*0.727220521664304E-4
D DDJO=INTF(TIME/6.283185307179586)
D DJ=DJO+DDJO
   TIME=ALL0TZ(TIME)
C
C      COMPUTE GREENWICH APPARENT SIDEREAL TIME AT TO + DELTA T
C
C
   EPHR = TIME * 3.81971863421
D   EQR=EON(DJ,EPHR,XX,XX,XX)
D   ST=GASTZ(DJ,EPHR,EQR)
D   CALL JULCAL(DJ,NM,ND,NY)
C
C      CONVERT UNIVERSAL TIME IN RADIAN TO HOURS, MINUTES, AND SECONDS
C
C
   CALL RHMSZ(TIME,II,IH,IM,IS).
C
   CALL BRWR2(DTIMES,EN2)
   SST=SINF(ST)
   CST=COSF(ST)
   RG(1)=RXB(1)*CST+RXB(2)*SST
   RG(2)=RXB(2)*CST-RXB(1)*SST
   RG(3)=RXB(3)
   CALL VROZ(I,RG,GCLAT,GCLON,R)
C
C      COMPUTE GEODETIC LATITUDE OF SUBSATELLITE POINT
C

```

```

C      COMPUTE HEIGHT OF SATELLITE ABOVE COMPUTATIONAL ELLIPSOID ALONG
C      NORMAL FROM SATELLITE TO ELLIPSOID
C
C      GDLAT = GDLATZ(GCLAT,R,RE,FL,ALT)
C
C      CONVERT LATITUDE AND LONGITUDE IN RADIANS TO DEGREES, MINUTES,
C      AND SECONDS
C
C      TGCLON=GCLON-3,141592653589793
C      IF (TGCLON) 1062,1062,1061
D1061 GCLON=TGCLON-3,141592653589793
C      1062 CONTINUE
D      CALL RDMSZ(GDLAT,I,IPD,IPM,TPS)
D      CALL RDMSZ(GCLON,II,ILD,ILM,TLS)
C
C      OUTPUT PREPARATION
C
C      NYM19=NY-1900
C      WRITE OUTPUT TAPE 3,6024,NM,ND,NYM19,IH,IM,TS,IPD,IPM,TPS,ILD,
C      1 ILM,TLS,ALT
C      IF (SENSE SWITCH 6) 107,108
107 PRINT 6024,NM,ND,NYM19,IH,IM,TS,IPD,IPM,TPS,ILD,ILM,TLS,ALT
108 IF (DTIMES-WMAPF) 103,109,109
109 IF (SENSE SWITCH 1) 110,199
110 PRINT 6025
C      PAUSE 77776
C
C      END WORLD MAP CALCULATION
C
C      199 IF (LA) 1,1,200
C
C      BEGIN LOCAL STATION PREDICTIONS CALCULATION
C      (NO CALCULATION IF LA=0)
C
C      200 READ          9505,NLA,ICCI,MINV,XMAX
C      IF (NLA) 1,1,2001
2001 READ          9506,RDMAX,RDMIN,RA,DEC
C      XMIN=MINV
C      IF(XMAX) 902,902,903
902 XMAX=1000000.0
903 IF(RA) 904,905,904
D904 RAR=RA*.0174532925
D      DECR=DEC*.0174532925
D      VXE(1) = COSF(DECR) * COSF(RAR)
D      VXF(2) = COSF(DECR) * SINF(RAR)
D      VWF(3) = SINF(DECR)
D905 CALL VRDZ(1,VXE+DECR,RAR,XXX)
C      RA = RAR*57.2957795
C      DECR=DECR*57.2957795
C      WRITE OUTPUT TAPE 3,9504
C      IF (SENSE SWITCH 6) 201,202
201 PRINT 9504
202 DO 205 N=1,NLA
C      READ          6027,STAT1(N),STAT2(N),LOND,LONM,XLONS,LATD,
901  LATM,XLATS,HGT
C      WRITE OUTPUT TAPE 3,6028,STAT1(N),STAT2(N),LOND,LONM,XLONS,LATD,
C      1LATM,XLATS,HGT
C      IF (SENSE SWITCH 6) 203,2031
203 PRINT 6028,STAT1(N),STAT2(N),LOND,LONM,XLONS,LATD,LATM,XLATS,HGT
2031 CONTINUE
D      CCOORD(1) = DMSRZ(LATD,LATM,XLATS)
D      CCOORD(2) = DMSRZ(LOND,LONM,XLONS)
D      CCOORD(3) = HGT/1000.0
D      RLAT(N)=CCOORD(1)
D      RLON(N)=CCOORD(2)
D      CALL VFUZ(CCOORD,RE,FL,U)
D      DO 204 J=1,J
204 SUIN(J)=I(J)
205 CONTINUE
C      WRITE OUTPUT TAPE 3,9507,MINV,XMAX,RDMAX,RDMIN,RA,DEC
C
C      INITIALIZE LINE COUNT AND DELTA T DIFFERENCE BETWEEN
C      LOCAL STATION PREDICTIONS STARTING TIME AND EPOCH OF INPUT
C      PARAMETERS IN SECONDS)
C
C      LINES=1
C      LINE6=1
D      DTIMES=XLAS-DTIA
C
C      SKIP A PAGE AND PRINT HEADING FOR LOCAL STATION PREDICTIONS
C      PRINT 607
C
C      WRITE OUTPUT TAPE 3,6038
C      WRITE OUTPUT TAPE 3,9502
C      IF(ICCI) 7004,7004,7005
7005 WRITE OUTPUT TAPE 6,6038
C      WRITE OUTPUT TAPE 6,9502
C      WRITE OUTPUT TAPE 6,7500
7004 IF(SENSE SWITCH 6) 2051,2052
2051 PRINT 6038
207 PRINT 9502
2052 CONTINUE

```

```

208 WRITE OUTPUT TAPE 3,9503,(STAT2(I),I = 1,NLA)
    IF (SENSE SWITCH 6) 210,2170
210 PRINT          9503,(STAT2(I),I = 1,NLA)
2170 IF (SENSE SWITCH 2) 2171,217
2171 PRINT 6025
    PAUSE 77775
217 LINES=LINFS+1
C
C   SKIP A PAGE AND PRINT HEADING IF 50 LINES OF CALCULATION
C   HAVE BEEN PRINTED
C
9600 IF (LINES-40) 231,231,218
218 LINFS=1
    WRITE OUTPUT TAPE 3,6038
    WRITE OUTPUT TAPE 3,9503,(STAT2(I),I = 1,NLA)
    IF (SENSE SWITCH 6) 220,231
220 PRINT 6038
    PRINT          9503,(STAT2(I),I = 1,NLA)
231 IF (ICCL) 7016,7016,7007
7007 IF (LINE6-40) 7016,7016,7015
7015 LINE6=1
    WRITE OUTPUT TAPE 6,6038
    WRITE OUTPUT TAPE 6,7500
D7016 DTIMES=DTIMFS+DTLA
D   TIME=TIME0+DTIMES*0.727220521664304E-4
D   DJO=INT(F TIME/6.283185307179586)
D   DJ=DJ0+ND*10
D   TIME=ALL0TZ(TIME)
C
C   COMPUTE GREENWICH APPARENT SIDEREAL TIME AT TO + DELTA T
C
D   EPHR = TIME * 3.81971863421
D   EOR=EON(DJ,EPHR,XX,XX,XX)
D   ST = GAST7(DJ,EPHR,EOR)
D   CALL JULCAL(DJ,NM,ND,NY)
C
C   CONVERT UNIVERSAL TIME IN RADIAN TO HOURS, MINUTES, AND SECONDS
C
C   CALL RHMSZ(TIME,II,IH,IM,TS)
C   NYM19=NY-1900
C
C   CALL BRWR2(DTIMES,EN2)
    SST=SNP(ST)
    CST=COSF(ST)
    RG(1)=RXB(1)*CST+RXB(2)*SST
    RG(2)=RXB(2)*CST-RXB(1)*SST
    RG(3)=RXB(3)
C
C   KK=0
D0 242 N=1,NLA
D0 232 M=1,3
D232 PCU(N)=RG(N)-SU(N,M)
D   CALL R13Z(RTX,0,-ST,RGU)
D   DUMX=DOTZ(RTX,VXE)
D   TESTA(N)=DJM*57.295780
D   R13A1=1.57079632679-RLAT(N)
D   R13A2=1.57079632679+RLON(N)
D   CALL R13Z(Z,R13A1,R13A2,RGU)
D   CALL VRDZ(Z,Z,ELEVAT,AZIMUT,RANG)
D   ELED(N)=57.29578*ELEVAT
D   AZID(N)=57.29578*AZIMUT
D   RGE(N)=RANG
    IF (ELED(N)-XMIN) 233,234,234
B 233 DATA(N)=APRINT
    G0 T0 242
234 IF (TESTA(N)-RDMIN) 235,236,236
B 235 DATA(N)=APRINT
    G0 T0 242
236 IF (TESTA(N)-RDMAX) 238,238,237
B 237 DATA(N)=APRINT
    G0 T0 242
238 IF (RGE(N)-XMAX) 240,240,239
B 239 DATA(N)=APRINT
    G0 T0 242
B 240 DATA(N)=BPRINT
    SENSE LIGHT 1
    IF (ICCL) 242,242,241
241 KK=KK+1
    RGE1(KK)=RGE(N)
    ELED1(KK)=ELED(N)
    AZID1(KK)=AZID(N)
    TESTA1(KK)=TESTA(N)
B   STAT3(KK) = STAT1(N)
B   STAT4(KK) = STAT2(N)
242 CONTINUE
    IF (SENSE LIGHT 1) 243,2460
243 IF (LC2-1) 245,244,245
244 WRITE OUTPUT TAPE 3,9501
    LC2=0
    LINES =LINES+1
245 WRITE OUTPUT TAPE 3,6052,NM,ND,NYM19,IH,IM,TS, (DATA(N), N=1,NLA)
    LINES= LINES+1

```



```

      IF (ICCL) 247,247,246
246  WRITE OUTPUT TAPE 6,7501,NM,NO,NYM19,IH,IM,(STAT3(I),STAT4(I),
      IRGF1(I),AZ101(I),ELED1(I),TESTA1(I), I =1,KK)
      LINE6=LINE6+KK+1
      GO TO 247
2460 LC2=1
247  CONTINUE
      IF (DTIMFS-XLAF) 9600,248,248
248  IF (SENSF SWITCH 2) 249,7010
249  PRINT 6025
      PAUSE 77774
7010 IF (ICCL) 200,200,7011
7011 FND FILF 6
      GO TO 200
C
      END LOCAL STATION PREDICTIONS CALCULATION
C
300 PRINT 6039
      FND FILE 3
      PAUSE 77777
      GO TO 10
      END

```

APPENDIX VII
SOURCE DECKS OF SUBROUTINES

```

* DATE 2/25/65
* FUNCTION ALLOT FORTRAN SOURCE PROGRAM
* CARDS COLUMN
* LISTS
* LABEL
* FUNCTION ALLOT(X)
VERSION OF 07/22/63
FORTRAN FUNCTION
FOR USE WITH FORTRAN 2 MONITOR ON IBM 7090, 7094
PURPOSE
REDUCES AN ANGLE OF ANY MAGNITUDE AND SIGN BY MODULUS 2 PI
AND ADDS 2 PI IF ANGLE IS NEGATIVE. THE RESULTING ANGLE IS
POSITIVE BETWEEN 0 AND +2 PI RADIANS.
CALLING SEQUENCE
NAME = ALLOT(X)
INPUT
X = ANGLE IN RADIANS
OUTPUT
NAME = ANGLE IN RADIANS BETWEEN 0 AND + 2 PI RADIANS
REFERENCE
*****
METHOD
*****
RESTRICTIONS
*****
ACCURACY
*****
REQUIRED SUBPROGRAMS - FORTRAN 2 MONITOR
NONE
REQUIRED SUBPROGRAMS - OTHER
NONE
STORAGE REQUIREMENTS
41
TIMING
NO ESTIMATE AVAILABLE
PROGRAM MODIFICATIONS
NO MODIFICATIONS TO DATE
***** START PROGRAM *****
2 ALLOT=MODF(X,6.2831853)
3 IF (ALLOT) 4,5,5
4 ALLOT=ALLOT+6.2831853
5 RETURN
END
* FUNCTION ALLJZ FORTRAN SOURCE PROGRAM
* CARDS COLUMN
* LISTS
* LABEL
* FUNCTION ALLJZ(X)
VERSION OF 07/22/63
FORTRAN FUNCTION
FOR USE WITH FORTRAN 2 MONITOR ON IBM 7090, 7094
PURPOSE
REDUCES AN ANGLE OF ANY MAGNITUDE AND SIGN BY MODULUS 2 PI
AND ADDS 2 PI IF ANGLE IS NEGATIVE. THE RESULTING ANGLE IS
POSITIVE BETWEEN 0 AND +2 PI RADIANS.
CALLING SEQUENCE
D NAME = ALLJZ(X)
INPUT
X = ANGLE IN RADIANS
X MUST BE AVAILABLE IN CALLING PROGRAM IN DOUBLE PRECISION
FORM.
OUTPUT
NAME = ANGLE IN RADIANS BETWEEN 0 AND + 2 PI RADIANS
NAME IS RETURNED TO CALLING PROGRAM IN DOUBLE PRECISION
FORM.
REFERENCE
*****

```

```

ALLJ7000
ALLJ7001
ALLJ7002
ALLJ7003
ALLJ7004
ALLJ7005
ALLJ7006
ALLJ7007
ALLJ7008
ALLJ7009
ALLJ7010
ALLJ7011
ALLJ7012
ALLJ7013
ALLJ7014
ALLJ7015
ALLJ7016
ALLJ7017
ALLJ7018
ALLJ7019
ALLJ7020
ALLJ7021
ALLJ7022
ALLJ7023
ALLJ7024
ALLJ7025
ALLJ7026
ALLJ7027
ALLJ7028
ALLJ7029
ALLJ7030
ALLJ7031
ALLJ7032
ALLJ7033
ALLJ7034
ALLJ7035
ALLJ7036
ALLJ7037
ALLJ7038
ALLJ7039
ALLJ7040
ALLJ7041
ALLJ7042
ALLJ7043
ALLJ7044
ALLJ7045
ALLJ7046
ALLJ7047
ALLJ7048
ALLJ7049
ALLJ7050
ALLJ7051
ALLJ7052
ALLJ7053
ALLJ7054
ALLJ7055
ALLJ7056
ALLJ7057
ALLJ7058
ALLJ7059
ALLJ7060
ALLJ7061
ALLJ7062
ALLJ7063
ALLJ7064
ALLJ7065
ALLJ7066
ALLJ7067
ALLJ7068
ALLJ7069
ALLJ7070
ALLJ7071
ALLJ7072
ALLJ7073
ALLJ7074
ALLJ7075
ALLJ7076
ALLJ7077
ALLJ7078
ALLJ7079
ALLJ7080
ALLJ7081
ALLJ7082
ALLJ7083
ALLJ7084
ALLJ7085
ALLJ7086
ALLJ7087
ALLJ7088
ALLJ7089
ALLJ7090
ALLJ7091
ALLJ7092
ALLJ7093
ALLJ7094
ALLJ7095
ALLJ7096
ALLJ7097
ALLJ7098
ALLJ7099
ALLJ7100

```



```

100 IF (S) 102,104,106
102 ATANQ=4.712 388 98
RETURN
104 ATANQ=0.0
RETURN
-----
106 ATANQ=1.570 796 33
RETURN
108 IF (S) 110,112,114
110 ADD=3.141 592 65
GO TO 124
112 ATANQ=3.141 592 65
RETURN
114 ADD=3.141 592 65
GO TO 132
-----
116 IF (S) 118,120,122
118 ADD=6.283 185 31
GO TO 132
-----
120 ATANQ=0.0
RETURN
122 ADD=0.0
124 IF (ABS(F(S)-ABS(F(C))) 126,128,130
126 ATANQ=ATANF(S/C)+ADD
RETURN
128 ATANQ=0.785 398 163+ADD
RETURN
130 ATANQ=1.570 796 33-ATANF(C/S)+ADD
RETURN
132 IF (ABS(F(S)-ABS(F(C))) 126,134,136
134 ATANQ=-0.785 398 163+ADD
RETURN
136 ATANQ=-1.57079633-ATANF(C/S)+ADD
RETURN
END
FUNCTION ATANZ FURTRAN SOURCE PROGRAM
CARDS COLUMN
LISTB
LABEL
FUNCTION ATANZ(S,C)
VERSION OF 07/22/63
FORTRAN FUNCTION
FOR USE WITH FORTRAN 2 MONITOR ON IBM 7090, 7094
PURPOSE
COMPUTES AN ANGLE FROM ITS SINE AND COSINE AND PLACES THE
THE ANGLE IN A POSITIVE QUADRANT BETWEEN 0 AND + 2 PI
RADIANS.
CALLING SEQUENCE
D NAME = ATANZ(S,C)
INPUT
S = SINE OF ANGLE (+ OR -)
C = COSINE OF ANGLE (+ OR -)
INPUT ARGUMENTS MUST BE AVAILABLE IN CALLING PROGRAM IN
DOUBLE PRECISION FORM.
OUTPUT
NAME = ANGLE IN RADIANS BETWEEN 0 AND + 2 PI RADIANS
NAME IS RETURNED TO CALLING PROGRAM IN DOUBLE PRECISION
FORM.
REFERENCE
*****
METHOD
USES FORTRAN MONITOR FUNCTION ATANZF. IF ARGUMENT
RETURNED BY ATANZF IS -, 2 PI RADIANS ARE ADDED .
RESTRICTIONS
*****
ACCURACY
INTERNAL ARITHMETIC IS PERFORMED IN DOUBLE PRECISION.
REQUIRED SUBPROGRAMS - FORTRAN 2 MONITOR
DATANZ,DFAD)
REQUIRED SUBPROGRAMS - OTHER
NONE
STORAGE REQUIREMENTS
67 WITHOUT REQUIRED SUBPROGRAMS
TIMING
NO ESTIMATE AVAILABLE
PROGRAM MODIFICATIONS
NO MODIFICATIONS TO DATE

```

```

ATANQ058
ATANQ059
ATANQ070
ATANQ071
ATANQ072
ATANQ073
ATANQ074
ATANQ075
ATANQ076
ATANQ077
ATANQ078
ATANQ079
ATANQ080
ATANQ081
ATANQ082
ATANQ083
ATANQ084
ATANQ085
ATANQ086
ATANQ087
ATANQ088
ATANQ089
ATANQ090
ATANQ091
ATANQ092
ATANQ093
ATANQ094
ATANQ095
ATANQ096
ATANQ097
ATANQ098
ATANQ099
ATANQ100
ATANZ000
ATANZ001
ATANZ002
ATANZ003
ATANZ004
ATANZ005
ATANZ006
ATANZ007
ATANZ008
ATANZ009
ATANZ010
ATANZ011
ATANZ012
ATANZ013
ATANZ014
ATANZ015
ATANZ016
ATANZ017
ATANZ018
ATANZ019
ATANZ020
ATANZ021
ATANZ022
ATANZ023
ATANZ024
ATANZ025
ATANZ026
ATANZ027
ATANZ028
ATANZ029
ATANZ030
ATANZ031
ATANZ032
ATANZ033
ATANZ034
ATANZ035
ATANZ036
ATANZ037
ATANZ038
ATANZ039
ATANZ040
ATANZ041
ATANZ042
ATANZ043
ATANZ044
ATANZ045
ATANZ046
ATANZ047
ATANZ048
ATANZ049
ATANZ050
ATANZ051
ATANZ052
ATANZ053
ATANZ054
ATANZ055
ATANZ056
ATANZ057
ATANZ058
ATANZ059

```

```

C
C ***** START PROGRAM *****
D 2 ATANZ=ATANZ(S,C)
D 3 IF (ATANZ1,4,5,6)
D 4 ATANZ=ATANZ+6.283185307179586
D 5 RETURN
END
SUBROUTINE BBRWR FORTRAN SOURCE PROGRAM
*
* PAUSE
* CARDS COLUMN
* LISTB
* LABEL
SUBROUTINE BBRWR(DA,AT,J,K)
VERSION OF 10/02/63
FORTRAN SUBROUTINE
FOR USE WITH FORTRAN 2 MONITOR ON IBM 7090, 7094
PURPOSE
COMPUTES BROUWER MEAN ORBITAL ELEMENTS FROM OSCULATING
ORBITAL ELEMENTS BY MEANS OF AN ITERATIVE PROCESS.
CALLING SEQUENCE
DIMENSION DA(6),AT(6)
CALL BBRWR(DA,AT,J,K)
INPUT
J = MAXIMUM NUMBER OF ITERATIONS ALLOWED
DA(1) = TRUNCATION FACTOR FOR SEMI-MAJOR AXIS - KILOMETERS
DA(2) = TRUNCATION FACTOR FOR ECCENTRICITY - DIMENSIONLESS
DA(3) = TRUNCATION FACTOR FOR INCLINATION - RADIANS
DA(4) = TRUNCATION FACTOR FOR RIGHT ASCENSION OF ASCENDING
NODE - RADIANS
DA(5) = TRUNCATION FACTOR FOR ARGUMENT OF PERIGEE - RADIANS
DA(6) = TRUNCATION FACTOR FOR MEAN ANOMALY - RADIANS
TRUE VALUES OF OSCULATING ORBITAL ELEMENTS
AT(1) = SEMI-MAJOR AXIS - KILOMETERS
AT(2) = ECCENTRICITY - DIMENSIONLESS
AT(3) = INCLINATION - RADIANS
AT(4) = RIGHT ASCENSION OF ASCENDING NODE - RADIANS
AT(5) = ARGUMENT OF PERIGEE - RADIANS
AT(6) = MEAN ANOMALY - RADIANS
OUTPUT
K = NUMBER OF ITERATIONS REQUIRED FOR CONVERGENCE
OUTPUT VIA COMMON
BROUWER MEAN ELEMENTS
ALL(1) = SEMI-MAJOR AXIS - KILOMETERS
ALL(2) = ECCENTRICITY - DIMENSIONLESS
ALL(3) = INCLINATION - RADIANS
ALL(4) = RIGHT ASCENSION OF ASCENDING NODE - RADIANS
ALL(5) = ARGUMENT OF PERIGEE - RADIANS
ALL(6) = MEAN ANOMALY - RADIANS
REFERENCE
REFER TO MATHEMATICAL DESCRIPTION IN SUBPROGRAM WRITEUP
METHOD
FOR THE 1ST APPROXIMATION, THE MEAN ELEMENTS ARE ASSUMED
TO BE EQUAL TO THE TRUE OSCULATING ELEMENTS. IN SUBSEQUENT
APPROXIMATIONS, THE MEAN ELEMENTS ARE SET EQUAL TO THE
MEAN ELEMENTS OF THE PREVIOUS APPROXIMATION PLUS THE
ALGEBRAIC DIFFERENCE BETWEEN THE VALUES OF THE TRUE
OSCULATING ELEMENTS MINUS THE VALUES OF THE OSCULATING
ELEMENTS COMPUTED BY SUBROUTINES BRWR1 AND BRWR2.
SUBROUTINES BRWR1 AND BRWR2 COMPUTE OSCULATING ELEMENTS
ACCORDING TO DIRK BROWDER'S ARTIFICIAL SATELLITE THEORY
WITHOUT DRAG.
THIS METHOD SUGGESTED BY DR. HANS HERTZ, DATA SYSTEMS
DIVISION, GODDARD SPACE FLIGHT CENTER.
RESTRICTIONS
FOR SMALL ECCENTRICITIES, THIS SUBROUTINE WILL NOT
CONVERGE. ERROR WARNING IS PRINTED IN LINE AND IN TAPE
UNIT 43 BEFORE RETURNING TO CALLING PROGRAM IF CONVERGENCE
IS NOT OBTAINED AFTER J ITERATIONS.
ACCURACY
SEVERAL TEST CASES WERE RUN WITH ECCENTRICITIES IN THE
NEIGHBORHOOD OF 1 AND CONVERGENCE WAS REACHED AFTER 4 OR
5 ITERATIONS.
REQUIRED SUBPROGRAMS - FORTRAN 2 MONITOR
(ISTH),(FIL),(SPH)
REQUIRED SUBPROGRAMS - OTHER
07/22/63 ALLOT
07/22/63 ALLOTZ
ATANZ066
ATANZ067
ATANZ068
ATANZ069
ATANZ070
ATANZ071
ATANZ072
ATANZ073
BBRW000
BBRW001
BBRW002
BBRW003
BBRW004
BBRW005
BBRW006
BBRW007
BBRW008
BBRW009
BBRW010
BBRW011
BBRW012
BBRW013
BBRW014
BBRW015
BBRW016
BBRW017
BBRW018
BBRW019
BBRW020
BBRW021
BBRW022
BBRW023
BBRW024
BBRW025
BBRW026
BBRW027
BBRW028
BBRW029
BBRW030
BBRW031
BBRW032
BBRW033
BBRW034
BBRW035
BBRW036
BBRW037
BBRW038
BBRW039
BBRW040
BBRW041
BBRW042
BBRW043
BBRW044
BBRW045
BBRW046
BBRW047
BBRW048
BBRW049
BBRW050
BBRW051
BBRW052
BBRW053
BBRW054
BBRW055
BBRW056
BBRW057
BBRW058
BBRW059
BBRW060
BBRW061
BBRW062
BBRW063
BBRW064
BBRW065
BBRW066
BBRW067
BBRW068
BBRW069
BBRW070
BBRW071
BBRW072
BBRW073
BBRW074
BBRW075
BBRW076
BBRW077
BBRW078
BBRW079
BBRW080
BBRW081
BBRW082
BBRW083

```

```

C      03/03/64. ATANQ      BBRW086
C      07/17/63. BRWR1     BBRW085
C      01/31/64 BRWR2     BBRW086
C      03/02/64. ELRV     BBRW087
C      09/12/63. XKPE     BBRW088
C      -----           BBRW089
C      STORAGE REQUIREMENTS BBRW090
C      . . . 146 WITHOUT REQUIRED SUBPROGRAMS. BBRW091
C      -----           BBRW092
C      TITING             BBRW093
C      . . . NO ESTIMATE AVAILABLE. BBRW094
C      -----           BBRW095
C      PROGRAM MODIFICATIONS BBRW099
C      -----           BBRW102
C      ***** START PROGRAM ***** BBRW103
C      100 FORMAT (//24H ***** WARNING ***** //7TH NO CONVERGENCE IN BBRWBWR109 BBRW106
C      1R SUBROUTINE, BROWWER MEAN ELEMENTS ARE NOT ACCURATE...//11//). BBRW107
C      -----           BBRW108
C      DIMENSION DUML(100) BBRW111
C      DIMENSION DA(6),AT(6),AL(6),A1(6),DUML(100),AF(6),DA(16),DTAT(6) BBRW112
C      -----           BBRW113
C      COMMON DUML,A110,DUHX,AC BBRW114
C      -----           BBRW115
C      K = 0 BBRW116
C      DO 10 N=1,6 BBRW117
C      10 A110(N) = AT(N) BBRW118
C      -----           BBRW119
C      1 CALL BRWR1 BBRW120
C      CALL BRWR2(0.0,0.0) BBRW121
C      -----           BBRW122
C      K = K + 1 BBRW123
C      IF (K-J) 4,4,3 BBRW124
C      3 WRITE OUTPUT TAPE 3,100 BBRW125
C      PRINT 100 BBRW126
C      RETURN BBRW127
C      -----           BBRW128
C      4 DO 5 N=1,6 BBRW129
C      DAT(N) = AT(N) - AC(N) BBRW130
C      5 TDAT(N) = ABSF(DAT(N)) BBRW131
C      -----           BBRW132
C      DO 6 N=1,6 BBRW133
C      IF (TDAT(N)-DAT(N)) 6,6,8 BBRW134
C      6 CONTINUE BBRW135
C      7 RETURN BBRW136
C      -----           BBRW137
C      8 DO 9 N=1,6 BBRW138
C      9 A110(N) = A110(N) + DAT(N) BBRW139
C      A110(3) = ALL0T(A110(3)) BBRW140
C      A110(4) = ALL0T(A110(4)) BBRW141
C      A110(5) = ALL0T(A110(5)) BBRW142
C      A110(6) = ALL0T(A110(6)) BBRW143
C      GO TO 1 BBRW144
C      END BBRW145
C      SUBROUTINE BRWR1 BBRW146
C      * CARDS COLUMN BRWR1001
C      * LIST8 BRWR1002
C      * LABEL BRWR1003
C      SUBROUTINE BRWR1 BRWR1004
C      -----           BRWR1005
C      VERSION OF 07/17/63 BRWR1006
C      FORTRAN SUBROUTINE BRWR1009
C      FOR USE WITH FORTRAN 2 MONITOR ON IBM 7090, 7094 BRWR1007
C      -----           BRWR1008
C      PURPOSE BRWR1009
C      BRWR1 AND BRWR2 CONVERT BROWWER MEAN ORBITAL ELEMENTS TO BRWR1010
C      OSCILLATING ORBITAL ELEMENTS AND TO POSITION AND VELOCITY BRWR1011
C      COMPONENTS. SECULAR AND LONG PERIOD COEFFICIENTS AND OTHER BRWR1012
C      INTERMEDIATE QUANTITIES WHICH ARE FUNCTIONS OF THE MEAN BRWR1013
C      ELEMENTS AND THE EARTH'S GRAVITATIONAL HARMONICS ONLY (I.E., DO NOT BRWR1014
C      VARY WITH TIME AND ARE CONSTANT FOR ANY GIVEN SET OF MEAN BRWR1015
C      ELEMENTS) ARE COMPUTED IN BRWR1 AND PLACED IN COMMON. BRWR2 CAN BRWR1016
C      THEN BE USED TO CALCULATE OSCILLATING ORBITAL ELEMENTS FOR ANY BRWR1017
C      SPECIFIED VALUE OF DT (TIME ELAPSED FROM EPOCH OF MEAN BRWR1018
C      ELEMENTS). COMMON IS USED TO TRANSFER INPUT TO SUBROUTINE BRWR1 BRWR1019
C      FROM CALLING PROGRAM, CONSTANTS AND INTERMEDIATE CALCULATIONS FROM BRWR1020
C      BRWR1 TO BRWR2, AND TO RETURN OUTPUT FROM BRWR2 TO CALLING PROGRAM BRWR1021
C      -----           BRWR1022
C      DUML IS A DUMMY VARIABLE INSERTED AS FIRST VARIABLE IN COMMON IN BRWR1023
C      BRWR1 AND BRWR2 TO PERMIT SHIFTING OF VARIABLES IN COMMON AREA IF BRWR1024
C      DESIRED. THE DIMENSION OF DUML MAY BE CHANGED BUT SHOULD BE THE BRWR1025
C      SAME IN SUBROUTINES BRWR1,BRWR2, AND THE CALLING PROGRAM. BRWR1026
C      -----           BRWR1027
C      CALLING SEQUENCE BRWR1028
C      CALL BRWR1 BRWR1029
C      -----           BRWR1030
C      INPUT VIA COMMON BRWR1031
C      BROWWER MEAN ELEMENTS BRWR1032
C      A110(1) = SEMI-MAJOR AXIS - KILOMETERS BRWR1033
C      A110(2) = ECCENTRICITY BRWR1034
C      A110(3) = INCLINATION - RADIANS BRWR1035
C      A110(4) = RIGHT ASCENSION OF ASCENDING NODE - RADIANS BRWR1036

```



```

C
D DIMENSION X(3), VX(3), A(6) ELRVZ215
D CALL ELRVZ(A, VX, A, P, EN, GH, ERR) ELRVZ216
C ELRVZ217
C ELRVZ218
C INPUT ELRVZ219
C A(1) = SEMI-MAJOR AXIS ELRVZ220
C A(2) = ECCENTRICITY, DIMENSIONLESS ELRVZ221
C A(3) = INCLINATION, RADIANS ELRVZ222
C A(4) = RIGHT ASCENSION OF ASCENDING NODE, RADIANS ELRVZ223
C A(5) = ARGUMENT OF PERIGEE, RADIANS ELRVZ224
C A(6) = MEAN ANOMALY, RADIANS ELRVZ225
C GH = THE PRODUCT OF G, THE GAUSSIAN CONSTANT SQUARED, ELRVZ226
C AND H, THE MASS OF THE EARTH ELRVZ227
C ERR = TRUNCATION FACTOR REQUIRED IN XKEPZ FUNCTION ELRVZ229
C IN RADIANS ELRVZ230
C ELRVZ231
C UNITS OF INPUT ARGUMENTS A(1) AND GH ARE ARBITRARY ELRVZ232
C BUT MUST BE MUTUALLY CONSISTENT. ELRVZ233
C INPUT ARGUMENTS MUST BE AVAILABLE IN CALLING PROGRAM IN ELRVZ234
C DOUBLE PRECISION FORM. ELRVZ235
C OUTPUT ELRVZ237
C X(1) ELRVZ238
C X(2) THE 3 RECTANGULAR COORDINATES OF POSITION ELRVZ239
C X(3) ELRVZ240
C ELRVZ241
C VX(1) ELRVZ242
C VX(2) THE 3 RECTANGULAR COMPONENTS OF VELOCITY ELRVZ243
C VX(3) ELRVZ244
C ELRVZ245
C P = ANOMALISTIC PERIOD ELRVZ246
C EN = MEAN ANGULAR MOTION ELRVZ247
C ELRVZ248
C UNITS OF OUTPUT ARGUMENTS X, VX, P, AND EN WILL DEPEND ELRVZ249
C UPON THE UNITS EMPLOYED FOR A(1) AND GH. ELRVZ250
C OUTPUT ARGUMENTS ARE RETURNED TO CALLING PROGRAM IN DOUBLE ELRVZ251
C FORM. ELRVZ252
C ELRVZ253
C REFERENCE ELRVZ254
C REFER TO MATHEMATICAL DESCRIPTION IN SUBPROGRAM WRITEUP ELRVZ255
C ELRVZ256
C METHOD ELRVZ257
C REFER TO MATHEMATICAL DESCRIPTION IN SUBPROGRAM WRITEUP ELRVZ258
C ELRVZ259
C RESTRICTIONS ELRVZ260
C ECCENTRICITY MUST BE LESS THAN 1.0. ELRVZ261
C ELRVZ262
C ACCURACY ELRVZ263
C REFER TO ACCURACY TESTS IN SUBPROGRAM WRITEUP. ELRVZ264
C INTERNAL ARITHMETIC IS PERFORMED IN DOUBLE PRECISION. ELRVZ265
C ELRVZ266
C REQUIRED SUBPROGRAMS - FORTRAN 2 MONITOR ELRVZ267
C (DFMP), (DFAD), (DFOP), DEXPT2, DSORT, DSTN, DCOS, (DFSB) ELRVZ268
C ELRVZ269
C REQUIRED SUBPROGRAMS - OTHER ELRVZ270
C 09/12/63 XKEPZ ELRVZ271
C ELRVZ272
C STORAGE REQUIREMENTS ELRVZ273
C 843 WITHOUT REQUIRED SUBPROGRAMS ELRVZ274
C ELRVZ275
C TIMING ELRVZ276
C NO ESTIMATE AVAILABLE ELRVZ277
C ELRVZ278
C PROGRAM MODIFICATIONS ELRVZ279
C ELRVZ280
C ELRVZ281
C ***** START PROGRAM ***** ELRVZ282
C ELRVZ283
C DIMENSION V(3), VX(3), A(6) ELRVZ284
C ELRVZ285
C A1=A(1) ELRVZ286
C A2=A(2) ELRVZ287
C A3=A(3) ELRVZ288
C A4=A(4) ELRVZ289
C A5=A(5) ELRVZ290
C A6=A(6) ELRVZ291
C 4 E=XKEPZ(A6, A2, SE, CE, ERR) ELRVZ292
C 7 X1=1.0-A(2)*CE ELRVZ293
C 8 X2=1.0/X1 ELRVZ294
C 9 R=A(1)*X1 ELRVZ295
C 10 DUM(1)=3-A2**2 ELRVZ296
C 11 RTGMA=SQRTF(GMA*1) ELRVZ297
C SA = SINP(A5) ELRVZ298
C SB = SINP(A3) ELRVZ299
C SC = SINP(A4) ELRVZ300
C CA = COSF(A5) ELRVZ301
C CB = COSF(A3) ELRVZ302
C CC = COSF(A4) ELRVZ303
C COMPUTE POSITION COORDINATES ELRVZ304
C ELRVZ305

```

```

D Q1 = A(1)*(CE-A(2))
D Q2 = A(1)*X3+SE
D V = Q1*CA - Q2*SA
D W = Q2*CA + Q1*SA
D Z = CB*W
D X(1) = CC*V - SC*Z
D X(2) = CC*Z + SC*V
D X(3) = SB*W
C
C COMPUTE VELOCITY COMPONENTS
C
D QD1 = -RTGMA*SE/R
D QD2 = RTGMA*X3+CE/R
D V = QD1*CA - QD2*SA
D W = QD2*CA + QD1*SA
D Z = CB*W
D VX(1) = CC*V - SC*Z
D VX(2) = CC*Z + SC*V
D VX(3) = SB*W
C
C RTGM=SQRTF(GM)
C RTA=SQRTF(A1)
C ENH=RTGM/RTA*A(1)
D P=6.283185307179586/EN
C RETURN
C
* FUNCTION EQN FORTRAN SOURCE PROGRAM
* CARDS COLUMN
* LISTB
* LABEL
* FUNCTION EQN(DJ,ET,DPSI,DE,E)
C
C VERSION OF 02/27/64
C FORTRAN FUNCTION
C FOR USE WITH FORTRAN 2 MONITOR ON IBM 7090, 7094
C
C PURPOSE
C COMPUTES NUTATION IN LONGITUDE, NUTATION
C IN OBLIQUITY, TRUE OBLIQUITY OF DATE AND NUTATION
C IN RIGHT ASCENSION (EQUATION OF THE EQUINOXES).
C
C CALLING SEQUENCE
C NAME = EQN(DJ,ET,DPSI,DE,E)
C
C INPUT
C DJ = JULIAN DATE AT 0 HOURS EPHEMERIS TIME
C ET = EPHEMERIS TIME IN HOURS
C
C OUTPUT
C DPSI = NUTATION IN LONGITUDE - RADIANS
C DE = NUTATION IN OBLIQUITY - RADIANS
C C = TRUE OBLIQUITY OF DATE - RADIANS
C .NAME = NUTATION IN RIGHT ASCENSION - RADIANS
C (EQUATION OF THE EQUINOXES)
C
C REFERENCE
C THE FORMULATION BY EDGAR W. WOOLARD MAY BE FOUND IN
C 4 PUBLICATIONS -
C
C 1. ASTRONOMICAL PAPERS PREPARED FOR THE USE OF THE
C AMERICAN EPHEMERIS AND NAUTICAL ALMANAC - VOLUME 15,
C PART 1, PAGE 153 (THEORY OF THE ROTATION OF THE
C EARTH AROUND ITS CENTER OF MASS - BY FOSAR H.
C WOOLARD)
C
C 2. IMPROVED LUNAR EPHEMERIS 1952-1959 - A JOINT
C SUPPLEMENT TO THE AMERICAN EPHEMERIS AND THE
C (BRITISH) NAUTICAL ALMANAC - PAGES IX AND X.
C
C AND THE AMERICAN EPHEMERIS AND NAUTICAL ALMANAC -
C PAGES 44 AND 45.
C
C 3. ASTRONOMICAL JOURNAL, 1953 FEBRUARY, VOL. 58, NO. 1
C PAGES 1-3 (A DEVELOPMENT OF THE THEORY OF NUTATION)
C - BY EDGAR W. WOOLARD)
C
C METHOD
C
C RESTRICTIONS
C ALL PERIODIC TERMS IN WOOLARD'S THEORY WITH COEFFICIENTS
C LESS THAN 0.001 SECONDS OF ARC HAVE BEEN NEGLECTED. ALL
C SECULAR PORTIONS OF THE COEFFICIENTS HAVE BEEN NEGLECTED
C WHENEVER THE SECULAR COEFFICIENTS ARE LESS THAN 0.001
C SECONDS OF ARC.
C
C REQUIRED SUBPROGRAMS - FORTRAN 2 MONITOR
C (DFAD), (DFSH), (DFHP), (DFDP), DADD, COS, SIN
C
C REQUIRED SUBPROGRAMS - OTHER
C NONE
C
C TIMING
C 9.4 MILLISECONDS ON 7094
C
C STORAGE REQUIREMENTS

```

```

ELRVZ118
ELRVZ119
ELRVZ120
ELRVZ121
ELRVZ122
ELRVZ123
ELRVZ124
ELRVZ125
ELRVZ126
ELRVZ127
ELRVZ128
ELRVZ129
ELRVZ130
ELRVZ131
ELRVZ132
ELRVZ133
ELRVZ134
ELRVZ135
ELRVZ136
ELRVZ137
ELRVZ138
ELRVZ139
ELRVZ140
ELRVZ141
ELRVZ142
ELRVZ143
EQV 000
EQV 001
EQV 002
EQV 003
EQV 004
EQV 005
EQV 006
EQV 007
EQV 008
EQV 009
EQV 010
EQV 011
EQV 012
EQV 013
EQV 014
EQV 015
EQV 016
EQV 017
EQV 018
EQV 019
EQV 020
EQV 021
EQV 022
EQV 023
EQV 024
EQV 025
EQV 026
EQV 027
EQV 028
EQV 029
EQV 030
EQV 031
EQV 032
EQV 033
EQV 034
EQV 035
EQV 036
EQV 037
EQV 038
EQV 039
EQV 040
EQV 041
EQV 042
EQV 043
EQV 044
EQV 045
EQV 046
EQV 047
EQV 048
EQV 049
EQV 050
EQV 051
EQV 052
EQV 053
EQV 054
EQV 055
EQV 056

```



```

----- EQN 367
1096 WITHOUT REQUIRED SUBPROGRAMS EQN 368
1329 WITH REQUIRED SUBPROGRAMS EQN 369
----- EQN 370
PROGRAM MODIFICATIONS EQN 371
----- EQN 372
NOTE: A 7094 FAP VERSION OF EQN IS AVAILABLE USING THE SAME EQN 384
CALLING SEQUENCE AS THE FORTRAN VERSION. THE FAP VERSION EQN 385
REQUIRES 725 STORAGE LOCATIONS WITHOUT REQUIRED SUBPROGRAMS EQN 386
AND 830 LOCATIONS WITH REQUIRED SUBPROGRAMS. COMPUTING EQN 388
TIME FOR THE FAP VERSION IS 6.6 MILLISECOND ON 7094. EQN 389
----- EQN 390
***** START PROGRAM ***** EQN 391
----- EQN 392
DIMENSION SCF(36),S(36),CCE(19),C(19) EQN 393
----- EQN 394
COMPUTE NUMBER OF JULIAN CENTURIES OF 36525.0 DAYS EXACTLY WHICH EQN 395
HAVE ELAPSED FROM 1900 JAN. 0.5 DAYS EPHEMERIS TIME. EQN 396
----- EQN 397
PRT1=DJ-2415020.0 EQN 398
PRT2=ET/24.0 EQN 399
T=(PRT1+PRT2)/36525.0 EQN 400
T2=T*T EQN 401
T3=T*T2 EQN 402
----- EQN 403
COMPUTE FUNDAMENTAL ARGUMENTS EQN 404
----- EQN 405
MEAN ANOMALY - MOON EQN 406
----- EQN 407
X = 0.160 424 847 E-3 *T2 + 0.251 133 E-6 * T3 EQN 408
EL = 5.168 000 345 745 + X + 8328.691 103 668 024 * T EQN 409
EQN 410
MEAN ANOMALY - SUN EQN 411
----- EQN 412
X = 0.261 799 4 E-5 *T2 + 0.581 78 E-7 * T3 EQN 413
ELL = 6.256 583 580 497 - X + 628.301 945 726 742 * T EQN 414
EQN 415
MEAN ARGUMENT OF LATITUDE - HDON EQN 416
----- EQN 417
X = 0.560 444 62 E-4 *T2 + 0.581 8 E-8 * T3 EQN 418
F = 0.196 365 054 887 - X + 8433.466 291 171 947 * T EQN 419
EQN 420
MEAN ELONGATION OF MOON FROM SUN EQN 421
----- EQN 422
X = 0.250 648 67 E-4 *T2 - 0.329 67 E-7 * T3 EQN 423
O = 6.121 523 942 807 - X + 7771.377 193 934 485 * T EQN 424
EQN 425
LONGITUDE OF MEAN ASCENDING NODE - HDON EQN 426
----- EQN 427
X = 0.362 640 63 E-4 *T2 + 0.387 85 E-7 * T3 EQN 428
O = 4.523 601 514 852 + X - 33.757 146 246 552 * T EQN 429
EQN 430
REDUCE ALL ANGLES BY MODULUS 2 PI. EQN 431
EQN 432
EL = MODF(EL,6.283 185 307 179 586) EQN 433
ELL = MODF(ELL,6.283 185 307 179 586) EQN 434
F = MODF(F,6.283 185 307 179 586) EQN 435
O = MODF(O,6.283 185 307 179 586) EQN 436
O = MODF(O,6.283 185 307 179 586) EQN 437
COMPUTE SINES AND COSINES OF FUNDAMENTAL ARGUMENTS AND EQN 438
AND COMBINATIONS OF THE FUNDAMENTAL ARGUMENTS. EQN 439
----- EQN 440
S(1) = SIN(F) EQN 441
C(1) = COS(F) EQN 442
S(3) = 2.0*S(1)*C(1) EQN 443
C(3) = C(1)**2-S(1)**2 EQN 444
SF = SIN(F) EQN 445
CF = COS(F) EQN 446
S(25) = 2.0*SF*CF EQN 447
C2F = CF**2-SF**2 EQN 448
SD = SIN(O) EQN 449
CD = COS(O) EQN 450
S(14) = 2.0*SD*CD EQN 451
C2D = CD**2-SD**2 EQN 452
S(4) = S(25)*C(3)+C2F *S(3) EQN 453
C(4) = C2F *C(3)-S(25)*S(3) EQN 454
AL = S(4)*C2D EQN 455
AL1 = C(4)*S(14) EQN 456
AL2 = S(4)*S(14) EQN 457
AL3 = C(4)*C2D EQN 458
S(2) = AL -AL1 EQN 459
C(2) = AL3*AL2 EQN 460
S(21) = AL +AL1 EQN 461
C(16) = AL3-AL2 EQN 462
S(5) = SIN(ELL) EQN 463
CL1 = COS(ELL) EQN 464
S(28) = 2.0*S(5)*CL1 EQN 465
C2L1 = CL1**2-S(5)**2 EQN 466
S(6) = SIN(EL) EQN 467
CL = COS(EL) EQN 468
S(22) = 2.0*S(6)*CL EQN 469
EQN 470

```

```

C2L = CL**2-S(6)**2
S(8) = S(25)*C(11)+C2F *S(11)
C(6) = C2F *C(11)-S(25)*S(11)
BE = S(2)*CL1
BE1 = C(2)+S(5) --
BE2 = S(2)+S(5)
BE3 = C(2)+C1
S(7) = BE +BE1
C(5) = BE3-BE2
S(10) = BE -BE1
C(8) = BE3+BE2
GA = S(4)*CL
GA1 = C(4)+S(6)
GA2 = S(4)+S(6) --
GA3 = C(4)+CL
S(9) = GA +GA1
C(7) = GA3-GA2
S(13) = GA -GA1
C(10) = GA3+GA2
S(11) = S(6)*C2D-CL *S(14)
CT = CL *C2D+S(6)*S(14)
S(12) = S(8)*C2D-C(6)*S(14)
C(9) = C(6)*C2D+S(8)*S(14)
DE = S(1)*CL
DE1 = C(1)*S(6)
DE2 = S(1)*S(6)
DE3 = C(1)*CL
S(15) = DE +DE1
C(11) = DE3-DE2
S(16) = DE -DE1
C(12) = DE3+DE2
S(17) = S(21)*CL -C(16)*S(6)
C(15) = C(16)*CL +S(21)*S(6)
S(18) = S(8)*C2L-C(6)*S(22)
C(13) = C(6)*C2L+S(8)*S(22)
S(19) = S(22)*C2D-C2L *S(14)
EP = S(8)*CL
EP1 = C(6)*S(6)
EP2 = S(8)*S(6)
EP3 = C(6)*CL
S(20) = EP +EP1
C(14) = EP3-EP2
S(27) = EP -EP1
C(19) = EP3+EP2
S(23) = S(2)*CL +C(2)*S(6)
C(17) = C(2)*CL -S(2)*S(6)
S(26) = S(4)*C2L +C(4)*S(22)
C(18) = C(4)*C2L -S(4)*S(22)
S(26) = S(25)*C2D-S(14)*C2F
S(29) = S(2)*C2L+C(2)*S(26)
ZE = S(11)*CL
ZE1 = C(11)*S(5)
S(30) = ZE+ZE1
S(13) = ZE-ZE1
AMU = S(11)*CT
AMU1 = C(11)*S(11)
S(31) = AMU-AMU1
S(32) = AMU+AMU1
S(34) = S(22)*C2F-C2L*S(25)

```

C
P
C

DEFINE C,H,STANT COEFFICIENTS OF SINE AND COSINE TERMS ON FIRST
PASS ONLY

```

IF (TEST) 2,1,2
1 TEST = + 1.0
SCF(2) = - 1.2729
SCF(3) = + 0.2088
SCF(4) = - 0.2037
SCF(5) = + 0.1261
SCF(6) = + 0.0675
SCF(7) = - 0.0497
SCF(8) = - 0.0342
SCF(9) = - 0.0261
SCF(10) = + 0.0214
SCF(11) = - 0.0149
SCF(12) = + 0.0124
SCF(13) = + 0.0114
SCF(14) = + 0.0060
SCF(15) = + 0.0058
SCF(16) = - 0.0057
SCF(17) = - 0.0052
SCF(18) = + 0.0045
SCF(19) = + 0.0045
SCF(20) = - 0.0044
SCF(21) = - 0.0032
SCF(22) = + 0.0028
SCF(23) = + 0.0026
SCF(24) = - 0.0026
SCF(25) = + 0.0025
SCF(26) = - 0.0021
SCF(27) = + 0.0019
SCF(28) = + 0.0016
SCF(29) = - 0.0015
SCF(30) = - 0.0015

```

EQN 171
EQN 172
EQN 173
EQN 176
EQN 175
EQN 176
EQN 177
EQN 178
EQN 179
EQN 180
EQN 181
EQN 182
EQN 183
EQN 184
EQN 185
EQN 186
EQN 187
EQN 188
EQN 189
EQN 190
EQN 191
EQN 192
EQN 193
EQN 194
EQN 195
EQN 196
EQN 197
EQN 198
EQN 199
EQN 200
EQN 201
EQN 202
EQN 203
EQN 204
EQN 205
EQN 206
EQN 207
EQN 208
EQN 209
EQN 210
EQN 211
EQN 212
EQN 213
EQN 214
EQN 215
EQN 216
EQN 217
EQN 218
EQN 219
EQN 220
EQN 221
EQN 222
EQN 223
EQN 224
EQN 225
EQN 226
EQN 227
EQN 228
EQN 229
EQN 230
EQN 231
EQN 232
EQN 233
EQN 234
EQN 235
EQN 236
EQN 237
EQN 238
EQN 239
EQN 240
EQN 241
EQN 242
EQN 243
EQN 244
EQN 245
EQN 246
EQN 247
EQN 248
EQN 249
EQN 250
EQN 251
EQN 252
EQN 253
EQN 254
EQN 255
EQN 256
EQN 257
EQN 258
EQN 259
EQN 250
EQN 261
EQN 262
EQN 263
EQN 264

```

SCF(31) = + 0.0014 EQN 265
SCF(32) = - 0.0013 EQN 266
SCF(33) = - 0.0010 EQN 267
SCF(34) = + 0.0010 EQN 268
CCF(1) = + 0.2100 EQN 269
CCF(2) = + 0.3522 EQN 270
CCF(3) = - 0.0904 EQN 271
CCF(4) = + 0.0884 EQN 272
CCF(5) = + 0.0216 EQN 273
CCF(6) = + 0.0183 EQN 274
CCF(7) = - 0.1313 EQN 275
CCF(8) = - 0.0093 EQN 276
CCF(9) = - 0.0066 EQN 277
CCF(10) = - 0.0050 EQN 278
CCF(11) = - 0.0031 EQN 279
CCF(12) = + 0.0030 EQN 280
CCF(13) = - 0.0024 EQN 281
CCF(14) = + 0.0023 EQN 282
CCF(15) = + 0.0022 EQN 283
CCF(16) = + 0.0014 EQN 284
CCF(17) = - 0.0011 EQN 285
CCF(18) = + 0.0011 EQN 286
CCF(19) = - 0.0010 EQN 287
2 CONTINUE EQN 288
EQN 289
EQN 290
EQN 291
EQN 292
EQN 293
EQN 294
EQN 295
EQN 296
EQN 297
EQN 298
EQN 299
EQN 300
EQN 301
EQN 302
EQN 303
EQN 304
EQN 305
EQN 306
EQN 307
EQN 308
EQN 309
EQN 310
EQN 311
EQN 312
EQN 313
EQN 314
EQN 315
EQN 316
EQN 317
EQN 318
EQN 319
EQN 320
EQN 321
EQN 322
EQN 323
EQN 324
EQN 325
EQN 326
EQN 327
EQN 328
EQN 329
EQN 330
EQN 331
EQN 332
EQN 333
EQN 334
EQN 335
EQN 336
EQN 337
EQN 338
EQN 339
EQN 340
EQN 341
EQN 342
EQN 343
EQN 344
EQN 345
EQN 346
EQN 347
EQN 348
EQN 349
EQN 350
EQN 351
EQN 352
EQN 353
EQN 354
EQN 355
EQN 356
EQN 357
EQN 358
EQN 359
EQN 360
EQN 361
EQN 362
EQN 363
EQN 364
EQN 365
EQN 366
EQN 367
EQN 368
EQN 369
EQN 370
EQN 371
EQN 372
EQN 373
EQN 374
EQN 375
EQN 376
EQN 377
EQN 378
EQN 379
EQN 380
EQN 381
EQN 382
EQN 383
EQN 384
EQN 385
EQN 386
EQN 387
EQN 388
EQN 389
EQN 390
EQN 391
EQN 392
EQN 393
EQN 394
EQN 395
EQN 396
EQN 397
EQN 398
EQN 399
EQN 400
EQN 401
EQN 402
EQN 403
EQN 404
EQN 405
EQN 406
EQN 407
EQN 408
EQN 409
EQN 410
EQN 411
EQN 412
EQN 413
EQN 414
EQN 415
EQN 416
EQN 417
EQN 418
EQN 419
EQN 420
EQN 421
EQN 422
EQN 423
EQN 424
EQN 425
EQN 426
EQN 427
EQN 428
EQN 429
EQN 430
EQN 431
EQN 432
EQN 433
EQN 434
EQN 435
EQN 436
EQN 437
EQN 438
EQN 439
EQN 440
EQN 441
EQN 442
EQN 443
EQN 444
EQN 445
EQN 446
EQN 447
EQN 448
EQN 449
EQN 450
EQN 451
EQN 452
EQN 453
EQN 454
EQN 455
EQN 456
EQN 457
EQN 458
EQN 459
EQN 460
EQN 461
EQN 462
EQN 463
EQN 464
EQN 465
EQN 466
EQN 467
EQN 468
EQN 469
EQN 470
EQN 471
EQN 472
EQN 473
EQN 474
EQN 475
EQN 476
EQN 477
EQN 478
EQN 479
EQN 480
EQN 481
EQN 482
EQN 483
EQN 484
EQN 485
EQN 486
EQN 487
EQN 488
EQN 489
EQN 490
EQN 491
EQN 492
EQN 493
EQN 494
EQN 495
EQN 496
EQN 497
EQN 498
EQN 499
EQN 500

```



```

..... (24 HOURS = 2 PI RADIANS).....
CALLING SEQUENCE
D NAME = HMSRZ(IH, TH, TS)
INPUT
IH = NUMBER OF HOURS IN TIME
TH = NUMBER OF MINUTES IN TIME
TS = NUMBER OF SECONDS IN TIME
SIGN OF THE INPUT TIME NEED ONLY BE ASSOCIATED WITH
THE NUMBER OF HOURS (IHL)
OUTPUT
NAME = TIME IN RADIANS
NAME IS RETURNED TO CALLING PROGRAM IN DOUBLE
PRECISION FORM.
REFERENCE
*****
METHOD
*****
RESTRICTIONS:
*****
ACCURACY
WHEN NECESSARY, INTERNAL ARITHMETIC IS PERFORMED IN DOUBLE
PRECISION SO THAT THE VALUE OF THE OUTPUT ARGUMENT IS
AVAILABLE TO CALLING PROGRAM IN DOUBLE PRECISION.
REQUIRED SUBPROGRAMS - FORTRAN 2 MONITOR
(DFMB), (DFAD)
REQUIRED SUBPROGRAMS - OTHER
NONE
STORAGE REQUIREMENTS
125 WITHOUT REQUIRED SUBPROGRAMS.
TIMING
NO ESTIMATE AVAILABLE.
PROGRAM MODIFICATIONS
NO MODIFICATIONS TO DATE
***** START PROGRAM *****
2 TH=IH
3 TH=TH
4 TH=SIGNF(TH,TH)
5 TRS=SIGNF(TS,TH)
0 6 HMSRZ=TH*.2617993877991494 + TH*4.363323129985824E-3
1 RETURN
END
SUBROUTINE JULCAL(FURTRAN SOURCE PROGRAM)
CARDS COLUMN
LISTB
LABEL
SUBROUTINE JULCAL(DJ, NM, ND, NY)
VERSION OF 07/22/63
FORTRAN SUBROUTINE
FOR USE WITH FORTRAN 2 MONITOR ON IBM 7090, 7094
PURPOSE
COMPUTES CALENDAR DATE FROM JULIAN DATE AT 0 HOURS
UNIVERSAL TIME (OR 0 HOURS EPHEMERIS TIME).
CALLING SEQUENCE
CALL JULCAL(DJ, NM, ND, NY)
INPUT
DJ = JULIAN DATE AT 0 HOURS UNIVERSAL TIME
OUTPUT
NM = CALENDAR MONTH
ND = CALENDAR DAY
NY = CALENDAR YEAR
REFERENCE
REFER TO MATHEMATICAL DESCRIPTION IN SUBPROGRAM WRITEUP
METHOD
THE NUMBER OF DAYS FROM 12 HOURS UNIVERSAL TIME JAN. 0,
1800 IS CALCULATED. THE INTEGRAL NUMBER OF YEARS IN THIS
NUMBER IS ADDED TO 1800 TO GIVE THE CURRENT CALENDAR YEAR
AND THE NUMBER OF DAYS CONTAINED IN THE INTEGRAL NUMBER
OF YEARS ELAPSED SINCE JAN. 0, 1800 IS SUBTRACTED FROM THE

```

```

HMSRZ011
HMSRZ012
HMSRZ013
HMSRZ014
HMSRZ015
HMSRZ016
HMSRZ017
HMSRZ018
HMSRZ019
HMSRZ020
HMSRZ021
HMSRZ022
HMSRZ023
HMSRZ024
HMSRZ025
HMSRZ026
HMSRZ027
HMSRZ028
HMSRZ029
HMSRZ030
HMSRZ031
HMSRZ032
HMSRZ033
HMSRZ034
HMSRZ035
HMSRZ036
HMSRZ037
HMSRZ038
HMSRZ039
HMSRZ040
HMSRZ041
HMSRZ042
HMSRZ043
HMSRZ044
HMSRZ045
HMSRZ046
HMSRZ047
HMSRZ048
HMSRZ049
HMSRZ050
HMSRZ051
HMSRZ052
HMSRZ053
HMSRZ054
HMSRZ055
HMSRZ056
HMSRZ057
HMSRZ058
HMSRZ059
HMSRZ070
HMSRZ071
HMSRZ072
HMSRZ073
HMSRZ074
HMSRZ075
HMSRZ076
HMSRZ077
HMSRZ078
HMSRZ079
HMSRZ080
HMSRZ081
HMSRZ082
HMSRZ083
HMSRZ084
HMSRZ085
HMSRZ086
HMSRZ087
HMSRZ088
HMSRZ089
HMSRZ090
HMSRZ091
HMSRZ092
HMSRZ093
HMSRZ094
HMSRZ095
HMSRZ096
HMSRZ097
HMSRZ098
HMSRZ099
HMSRZ100
HMSRZ101
HMSRZ102
HMSRZ103
HMSRZ104
HMSRZ105
HMSRZ106
HMSRZ107
HMSRZ108
HMSRZ109
HMSRZ110
HMSRZ111
HMSRZ112
HMSRZ113
HMSRZ114
HMSRZ115
HMSRZ116
HMSRZ117
HMSRZ118
HMSRZ119
HMSRZ120
HMSRZ121
HMSRZ122
HMSRZ123
HMSRZ124
HMSRZ125
HMSRZ126
HMSRZ127
HMSRZ128
HMSRZ129
HMSRZ130
HMSRZ131
HMSRZ132
HMSRZ133
HMSRZ134
HMSRZ135
HMSRZ136
HMSRZ137
HMSRZ138
HMSRZ139
HMSRZ140
HMSRZ141
HMSRZ142
HMSRZ143
HMSRZ144
HMSRZ145
HMSRZ146
HMSRZ147
HMSRZ148
HMSRZ149
HMSRZ150
HMSRZ151
HMSRZ152
HMSRZ153
HMSRZ154
HMSRZ155
HMSRZ156
HMSRZ157
HMSRZ158
HMSRZ159
HMSRZ160
HMSRZ161
HMSRZ162
HMSRZ163
HMSRZ164
HMSRZ165
HMSRZ166
HMSRZ167
HMSRZ168
HMSRZ169
HMSRZ170
HMSRZ171
HMSRZ172
HMSRZ173
HMSRZ174
HMSRZ175
HMSRZ176
HMSRZ177
HMSRZ178
HMSRZ179
HMSRZ180
HMSRZ181
HMSRZ182
HMSRZ183
HMSRZ184
HMSRZ185
HMSRZ186
HMSRZ187
HMSRZ188
HMSRZ189
HMSRZ190
HMSRZ191
HMSRZ192
HMSRZ193
HMSRZ194
HMSRZ195
HMSRZ196
HMSRZ197
HMSRZ198
HMSRZ199
HMSRZ200
HMSRZ201
HMSRZ202
HMSRZ203
HMSRZ204
HMSRZ205
HMSRZ206
HMSRZ207
HMSRZ208
HMSRZ209
HMSRZ210
HMSRZ211
HMSRZ212
HMSRZ213
HMSRZ214
HMSRZ215
HMSRZ216
HMSRZ217
HMSRZ218
HMSRZ219
HMSRZ220
HMSRZ221
HMSRZ222
HMSRZ223
HMSRZ224
HMSRZ225
HMSRZ226
HMSRZ227
HMSRZ228
HMSRZ229
HMSRZ230
HMSRZ231
HMSRZ232
HMSRZ233
HMSRZ234
HMSRZ235
HMSRZ236
HMSRZ237
HMSRZ238
HMSRZ239
HMSRZ240
HMSRZ241
HMSRZ242
HMSRZ243
HMSRZ244
HMSRZ245
HMSRZ246
HMSRZ247
HMSRZ248
HMSRZ249
HMSRZ250
HMSRZ251
HMSRZ252
HMSRZ253
HMSRZ254
HMSRZ255
HMSRZ256
HMSRZ257
HMSRZ258
HMSRZ259
HMSRZ260
HMSRZ261
HMSRZ262
HMSRZ263
HMSRZ264
HMSRZ265
HMSRZ266
HMSRZ267
HMSRZ268
HMSRZ269
HMSRZ270
HMSRZ271
HMSRZ272
HMSRZ273
HMSRZ274
HMSRZ275
HMSRZ276
HMSRZ277
HMSRZ278
HMSRZ279
HMSRZ280
HMSRZ281
HMSRZ282
HMSRZ283
HMSRZ284
HMSRZ285
HMSRZ286
HMSRZ287
HMSRZ288
HMSRZ289
HMSRZ290
HMSRZ291
HMSRZ292
HMSRZ293
HMSRZ294
HMSRZ295
HMSRZ296
HMSRZ297
HMSRZ298
HMSRZ299
HMSRZ300
HMSRZ301
HMSRZ302
HMSRZ303
HMSRZ304
HMSRZ305
HMSRZ306
HMSRZ307
HMSRZ308
HMSRZ309
HMSRZ310
HMSRZ311
HMSRZ312
HMSRZ313
HMSRZ314
HMSRZ315
HMSRZ316
HMSRZ317
HMSRZ318
HMSRZ319
HMSRZ320
HMSRZ321
HMSRZ322
HMSRZ323
HMSRZ324
HMSRZ325
HMSRZ326
HMSRZ327
HMSRZ328
HMSRZ329
HMSRZ330
HMSRZ331
HMSRZ332
HMSRZ333
HMSRZ334
HMSRZ335
HMSRZ336
HMSRZ337
HMSRZ338
HMSRZ339
HMSRZ340
HMSRZ341
HMSRZ342
HMSRZ343
HMSRZ344
HMSRZ345
HMSRZ346
HMSRZ347
HMSRZ348
HMSRZ349
HMSRZ350
HMSRZ351
HMSRZ352
HMSRZ353
HMSRZ354
HMSRZ355
HMSRZ356
HMSRZ357
HMSRZ358
HMSRZ359
HMSRZ360
HMSRZ361
HMSRZ362
HMSRZ363
HMSRZ364
HMSRZ365
HMSRZ366
HMSRZ367
HMSRZ368
HMSRZ369
HMSRZ370
HMSRZ371
HMSRZ372
HMSRZ373
HMSRZ374
HMSRZ375
HMSRZ376
HMSRZ377
HMSRZ378
HMSRZ379
HMSRZ380
HMSRZ381
HMSRZ382
HMSRZ383
HMSRZ384
HMSRZ385
HMSRZ386
HMSRZ387
HMSRZ388
HMSRZ389
HMSRZ390
HMSRZ391
HMSRZ392
HMSRZ393
HMSRZ394
HMSRZ395
HMSRZ396
HMSRZ397
HMSRZ398
HMSRZ399
HMSRZ400
HMSRZ401
HMSRZ402
HMSRZ403
HMSRZ404
HMSRZ405
HMSRZ406
HMSRZ407
HMSRZ408
HMSRZ409
HMSRZ410
HMSRZ411
HMSRZ412
HMSRZ413
HMSRZ414
HMSRZ415
HMSRZ416
HMSRZ417
HMSRZ418
HMSRZ419
HMSRZ420
HMSRZ421
HMSRZ422
HMSRZ423
HMSRZ424
HMSRZ425
HMSRZ426
HMSRZ427
HMSRZ428
HMSRZ429
HMSRZ430
HMSRZ431
HMSRZ432
HMSRZ433
HMSRZ434
HMSRZ435
HMSRZ436
HMSRZ437
HMSRZ438
HMSRZ439
HMSRZ440
HMSRZ441
HMSRZ442
HMSRZ443
HMSRZ444
HMSRZ445
HMSRZ446
HMSRZ447
HMSRZ448
HMSRZ449
HMSRZ450
HMSRZ451
HMSRZ452
HMSRZ453
HMSRZ454
HMSRZ455
HMSRZ456
HMSRZ457
HMSRZ458
HMSRZ459
HMSRZ460
HMSRZ461
HMSRZ462
HMSRZ463
HMSRZ464
HMSRZ465
HMSRZ466
HMSRZ467
HMSRZ468
HMSRZ469
HMSRZ470
HMSRZ471
HMSRZ472
HMSRZ473
HMSRZ474
HMSRZ475
HMSRZ476
HMSRZ477
HMSRZ478
HMSRZ479
HMSRZ480
HMSRZ481
HMSRZ482
HMSRZ483
HMSRZ484
HMSRZ485
HMSRZ486
HMSRZ487
HMSRZ488
HMSRZ489
HMSRZ490
HMSRZ491
HMSRZ492
HMSRZ493
HMSRZ494
HMSRZ495
HMSRZ496
HMSRZ497
HMSRZ498
HMSRZ499
HMSRZ500

```



```

AND, M.L. THE MASS OF THE EARTH. . . . . PARA 324
----- PARA 325
OUTPUT OSCULATING ORBITAL ELEMENTS . . . . . PARA 326
----- PARA 327
A(1) = SEMI-MAJOR AXIS . . . . . PARA 328
A(2) = ECCENTRICITY . . . . . - DIMENSIONLESS PARA 329
A(3) = INCLINATION . . . . . - RADIANS . . . . . PARA 330
A(4) = RIGHT ASCENSION OF ASCENDING NODE . . . . . - RADIANS PARA 331
A(5) = ARGUMENT OF PERIGEE . . . . . - RADIANS PARA 333
A(6) = MEAN ANOMALY . . . . . - RADIANS . . . . . PARA 334
----- PARA 335
REFERENCE . . . . . PARA 336
***** PARA 337
METHOD . . . . . PARA 338
***** PARA 339
RESTRICTIONS . . . . . PARA 340
***** PARA 341
ACCURACY . . . . . PARA 342
***** PARA 343
REQUIRED SUBPROGRAMS - FORTRAN 2 MONITOR
. . . . . {DEMP} PARA 344
. . . . . PARA 345
. . . . . PARA 346
. . . . . PARA 347
. . . . . PARA 348
. . . . . PARA 349
. . . . . PARA 350
. . . . . PARA 351
. . . . . PARA 352
. . . . . PARA 353
. . . . . PARA 354
. . . . . PARA 355
. . . . . PARA 356
. . . . . PARA 357
. . . . . PARA 358
. . . . . PARA 359
. . . . . PARA 360
. . . . . PARA 361
. . . . . PARA 362
. . . . . PARA 363
. . . . . PARA 364
. . . . . PARA 365
. . . . . PARA 366
. . . . . PARA 367
. . . . . PARA 368
. . . . . PARA 369
. . . . . PARA 370
. . . . . PARA 371
. . . . . PARA 372
. . . . . PARA 373
. . . . . PARA 374
. . . . . PARA 375
. . . . . PARA 376
. . . . . PARA 377
. . . . . PARA 378
. . . . . PARA 379
***** START PROGRAM *****
D DIMENSION A(6),A(6),RX(3),VX(3) PARA 381
D DIMENSION DUM1(100),A1(6) PARA 382
D DIMENSION XX(18),AB(6) PARA 383
C COMMON DUM1,A1(6),XX,AB PARA 384
C GO TO (1,2,3,4), INPUT PARA 385
C INPUT OPTION 1. AI = OSCULATING ORBITAL ELEMENTS, ALL ANGLES IN PARA 386
C DEGREES PARA 387
D 1 A(1)=A(1) PARA 388
D A(2)=A(2) PARA 389
D DD 101 N=3,6 PARA 390
D 101 A(N)=A1(N)+0.0174532925199433 PARA 391
D GO TO 9999 PARA 392
C INPUT OPTION 2. AI = POSITION AND VELOCITY VECTORS IN PARA 393
C KILOMETERS AND KILOMETERS/SEC^2) PARA 394
D 2 DD 201 N=1,3 PARA 395
D RX(N)=A1(N) PARA 396
D 201 VX(N)=A1(N+3) PARA 397
D CALL RVELZ(RX,VX,A,PER,EN,GM) PARA 398
D GO TO 9999 PARA 399
C INPUT OPTION 2. AI = POSITION AND VELOCITY VECTORS IN PARA 400
C VANGUARD UNITS PARA 401
D 3 DD 301 N=1,3 PARA 402
D RX(N)=A1(N)+6378.388 PARA 403
D 301 VX(N)=A1(N+3)+7.905472668 PARA 404
D CALL RVELZ(RX,VX,A,PER,EN,GM) PARA 405
D GO TO 9999 PARA 406
C INPUT OPTION 4. AI = BROWER MEAN ELEMENTS, ALL ANGLES IN DEGREES PARA 407
D 4 A1(0(1))=A(1) PARA 408
D A1(0(2))=A(2) PARA 409
D DD 401 N=3,6 PARA 410
D BA=A1(N)+0.0174532925199433 PARA 411
D 401 A1(0(N))=BA PARA 412

```


CALL BRHR1	PARA 123
D DT=0.0	PARA 124
D CALL BRHR2(0Y,0.0)	
DD 402 N=1,6	PARA 126
402 SIN=ABIN)	PARA 127
9999 RETURN	PARA 128
END	PARA 129
* SUBROUTINE RDMSZ...EDTRAN_SOURCE_PROGRAM	RDMSZ000
* CARDS COLUMN	RDMSZ001
* LISTS	RDMSZ002
* LABEL	
SUBROUTINE RDMSZ(AR,IR,JD,IM,AS)	RDMSZ003
C	RDMSZ004
C VERSION OF 03/02/64	RDMSZ005
C FORTRAN SUBROUTINE	RDMSZ006
C FOR USE WITH FORTRAN 2 MONITOR ON IBM 7090, 7094	RDMSZ007
C	RDMSZ008
C PURPOSE	RDMSZ009
CONVERTS AN ANGLE OR ARC IN RADIANS INTO THE INTEGRAL	RDMSZ010
NUMBER OF REVOLUTIONS, NUMBER OF DEGREES, NUMBER OF	RDMSZ011
MINUTES, AND NUMBER OF SECONDS AND DECIMALS OF A SECOND	RDMSZ012
CONTAINED IN THE ANGLE OR ARC.	RDMSZ013
CALLING SEQUENCE	RDMSZ014
D CALL RDMSZ(AR,IR,JD,IM,AS)	RDMSZ015
INPUT	RDMSZ016
AR = ANGLE OR ARC IN RADIANS	RDMSZ017
AR MUST BE AVAILABLE IN CALLING PROGRAM IN DOUBLE PRECISION	RDMSZ018
FORM.	RDMSZ019
OUTPUT	RDMSZ020
IR = INTEGRAL NUMBER OF REVOLUTIONS IN THE ANGLE OR ARC	RDMSZ021
JD = NUMBER OF DEGREES	RDMSZ022
IM = NUMBER OF MINUTES	RDMSZ023
AS = NUMBER OF SECONDS AND DECIMALS OF A SECOND	RDMSZ024
REFERENCE	RDMSZ025
*****	RDMSZ026
METHOD	RDMSZ027
*****	RDMSZ028
RESTRICTIONS	RDMSZ029
*****	RDMSZ030
ACCURACY	RDMSZ031
CONVERSION IS ACCURATE TO AT LEAST .001 SECONDS OF ARC.	RDMSZ032
REQUIRED SUBPROGRAMS - FORTRAN 2 MONITOR	RDMSZ033
(DFDP),DMDD,(DFMP),(DFSB)	RDMSZ034
REQUIRED SUBPROGRAMS - OTHER	RDMSZ035
NONE	RDMSZ036
STORAGE REQUIREMENTS	RDMSZ037
337 WITHOUT REQUIRED SUBPROGRAMS	RDMSZ038
TIMING	RDMSZ039
NO ESTIMATE AVAILABLE	RDMSZ040
ANALYSIS	RDMSZ041
PROGRAM MODIFICATIONS	RDMSZ042
03/02/64 MOD. 1 BY S. STATEV - CHANGED UPPER LIMIT OF	RDMSZ043
AS FROM 99.0005 TO 59.9995	RDMSZ044
***** START PROGRAM *****	RDMSZ045
D 5 IR=AR/6.283185307179586	RDMSZ046
D 6 AR=MODF(AR,6.283185307179586)	RDMSZ047
D 7 JD=AR*57.2957795130823	RDMSZ048
D 8 AI=JD	RDMSZ049
D 9 A=AI/57.2957795130823	RDMSZ050
D 10 B=AR-A	RDMSZ051
D 11 IM=B*3437.746770784938	RDMSZ052
D 12 A2=IM	RDMSZ053
D 13 IM=XABSF(IM)	RDMSZ054
D 14 C=A2/3437.746770784938	RDMSZ055
D 15 D=B-C	RDMSZ056
D 16 AS=ABSF(D+206.264.806247096)	RDMSZ057
D 17 IF (AS=99.9995) 20,18,18	RDMSZ058
D 18 AS=ABSF(AS-63.)	RDMSZ059
D 19 IM=IM-1	RDMSZ060
D 20 IF (IM=63) 23,21,21	RDMSZ061
D 21 IM=IM-60	RDMSZ062
D 22 ID=ID+XSIGNF(1,JD)	RDMSZ063
D 23 IF (XABSF(ID)=360) 26,24,24	RDMSZ064
D 24 ID=ID+XSIGNF(360,JD)	RDMSZ065
D 25 IR=IR+XSIGNF(1,IR)	RDMSZ066
D 26 RETURN	RDMSZ067

END	R0HSZ090
• SUBROUTINE RHMSZ FORTRAN SOURCE PROGRAM	R4HSZ091
• CARDS COLUMN	R4HSZ092
• LISTB	
• LABEL	
SUBROUTINE RHMSZ(TR,IO,IM,TS)	R4HSZ093
VERSION OF 03/02/64	R4HSZ094
FORTRAN SUBROUTINE	R4HSZ095
FOR USE WITH FORTRAN 2 MONITOR ON IBM 7090, 7094	R4HSZ096
PURPOSE	R4HSZ097
CONVERTS TIME IN RADIANs (24 HOURS = 2 PI RADIANs) INTO	R4HSZ098
THE INTEGRAL NUMBER OF DAYS, NUMBER OF HOURS, NUMBER OF	R4HSZ099
MINUTES, AND NUMBER OF SECONDS AND DECIMALS OF A SECOND	R4HSZ100
CONTAINED IN THE TIME.	R4HSZ101
CALLING SEQUENCE	R4HSZ102
D CALL RHMSZ(TR,IO,IM,TS)	R4HSZ103
INPUT	R4HSZ104
TR = TIME IN RADIANs	R4HSZ105
TIME MUST BE AVAILABLE IN CALLING PROGRAM IN	R4HSZ106
DOUBLE PRECISION FORM.	R4HSZ107
OUTPUT	R4HSZ108
IO = INTEGRAL NUMBER OF DAYS CONTAINED IN THE	R4HSZ109
IM = NUMBER OF HOURS	R4HSZ110
IM = NUMBER OF MINUTES	R4HSZ111
TS = NUMBER OF SECONDS AND DECIMALS OF A SECOND	R4HSZ112
REFERENCE	R4HSZ113
*****	R4HSZ114
METHOD	R4HSZ115
*****	R4HSZ116
RESTRICTIONS	R4HSZ117
*****	R4HSZ118
ACCURACY	R4HSZ119
CONVERSION IS ACCURATE TO AT LEAST .001 SECONDS OF TIME.	R4HSZ120
REQUIRED SUBPROGRAMS - FORTRAN 2 MONITOR	R4HSZ121
(DFDP),DMDD,(DFHP),(DFSB)	R4HSZ122
REQUIRED SUBPROGRAMS - OTHER	R4HSZ123
NONE	R4HSZ124
STORAGE REQUIREMENTS	R4HSZ125
316 WITHOUT REQUIRED SUBPROGRAMS	R4HSZ126
TIMING	R4HSZ127
NO ESTIMATE AVAILABLE	R4HSZ128
ANALYSIS	R4HSZ129
PROGRAM MODIFICATIONS	R4HSZ130
03/02/64 MOD. 1 BY S. STATEN - CHANGED UPPER LIMIT OF	R4HSZ131
TS FROM 59.0005 TO 59.9995	R4HSZ132
***** START PROGRAM *****	R4HSZ133
D 5 IO=TR/6.283185307179586	R4HSZ134
D 6 TR=MODF(TR,6.283185307179586)	R4HSZ135
D 7 IM=TR-5.91771863420548	R4HSZ136
D 8 T1=IM	R4HSZ137
D 9 A=1/3.81971863420548	R4HSZ138
D 10 B=TK-A	R4HSZ139
D 11 IM=B+229.183118052329	R4HSZ140
D 12 T2=IM	R4HSZ141
D 13 IM=XBSF(IM)	R4HSZ142
D 14 C=T2/229.183118052329	R4HSZ143
D 15 D=B-C	R4HSZ144
D 16 TS=BSF(D+13750.98700831397)	R4HSZ145
D 17 IF (TS-59.9995) 20,18,18	R4HSZ146
D 18 TS=BSF(TS-62.)	R4HSZ147
D 19 IM=IM+1	R4HSZ148
D 20 IF (IM-62) 23,21,21	R4HSZ149
D 21 IM=IM-60	R4HSZ150
D 22 IM=IM*SIGNF(1,IM)	R4HSZ151
D 23 IF (XBSF(IM)-24) 26,24,24	R4HSZ152
D 24 IM=IM*XSIGNF(24,IM)	R4HSZ153
D 25 IO=IO*XSIGNF(1,IO)	R4HSZ154
D 26 RETURN	R4HSZ155
END	R4HSZ156
• SUBROUTINE RVELZ FORTRAN SOURCE PROGRAM	R4HSZ157
• CARDS COLUMN	R4HSZ158
• LISTB	R4HSZ159
• LABEL	R4HSZ160
• SUBROUTINE RVELZ(X,VX,A,P,EY,GH)	R4HSZ161
	R4HSZ162
	R4HSZ163
	R4HSZ164
	R4HSZ165
	R4HSZ166
	R4HSZ167
	R4HSZ168
	R4HSZ169
	R4HSZ170
	R4HSZ171
	R4HSZ172
	R4HSZ173
	R4HSZ174
	R4HSZ175
	R4HSZ176
	R4HSZ177
	R4HSZ178
	R4HSZ179
	R4HSZ180
	R4HSZ181
	R4HSZ182
	R4HSZ183
	R4HSZ184
	R4HSZ185
	R4HSZ186
	R4HSZ187
	R4HSZ188
	R4HSZ189
	R4HSZ190
	R4HSZ191
	R4HSZ192
	R4HSZ193
	R4HSZ194
	R4HSZ195
	R4HSZ196
	R4HSZ197
	R4HSZ198
	R4HSZ199
	R4HSZ200
	R4HSZ201
	R4HSZ202
	R4HSZ203
	R4HSZ204

```

VERSION OF 07/22/63
FORTRAN SUBROUTINE
FOR USE WITH FORTRAN 2 MONITOR ON IBM 7090, 7094
RVELZ005
RVELZ006
RVELZ007
RVELZ008
RVELZ009

PURPOSE
CONVERTS GEOCENTRIC EQUATORIAL INERTIAL RECTANGULAR
COORDINATES OF POSITION AND COMPONENTS OF VELOCITY INTO
OSCILLATING ORBITAL ELEMENTS
RVELZ010
RVELZ011
RVELZ012
RVELZ013

CALLING SEQUENCE
D DIMENSION X(3),VX(3),A(6)
D CALL RVELZ(X,VX,A,P,EH,GH)
RVELZ014
RVELZ015
RVELZ016
RVELZ017
RVELZ018

INPUT
X(1)
X(2) THE 3 RECTANGULAR COORDINATES OF POSITION
X(3)
RVELZ019
RVELZ020
RVELZ021
RVELZ022
RVELZ023
RVELZ024
RVELZ025
RVELZ026
RVELZ027
RVELZ028
RVELZ029
RVELZ030
RVELZ031
RVELZ032
RVELZ033
RVELZ034
RVELZ035
RVELZ036
RVELZ037
RVELZ038
RVELZ039
RVELZ040
RVELZ041
RVELZ042
RVELZ043
RVELZ044
RVELZ045
RVELZ046
RVELZ047
RVELZ048
RVELZ049
RVELZ050
RVELZ051
RVELZ052
RVELZ053
RVELZ054
RVELZ055
RVELZ056
RVELZ057
RVELZ058
RVELZ059
RVELZ060
RVELZ061
RVELZ062
RVELZ063
RVELZ064
RVELZ065
RVELZ066
RVELZ067
RVELZ068
RVELZ069
RVELZ070
RVELZ071
RVELZ072
RVELZ073
RVELZ074
RVELZ075
RVELZ076
RVELZ077
RVELZ078
RVELZ079
RVELZ080
RVELZ081
RVELZ082
RVELZ083
RVELZ084
RVELZ085
RVELZ086
RVELZ087
RVELZ088
RVELZ089
RVELZ090
RVELZ091
RVELZ092
RVELZ093
RVELZ094
RVELZ095
RVELZ096
RVELZ097
RVELZ098
RVELZ099
RVELZ100
RVELZ101
RVELZ102
RVELZ103
RVELZ104
RVELZ105
RVELZ106
RVELZ107
RVELZ108
RVELZ109
RVELZ110
RVELZ111
RVELZ112
RVELZ113
RVELZ114

UNITS OF INPUT ARGUMENTS X, VX, AND GH ARE ARBITRARY BUT
MUST BE MUTUALLY CONSISTENT
INPUT ARGUMENTS MUST BE AVAILABLE IN CALLING PROGRAM IN
DOUBLE PRECISION FORM.

OUTPUT
A(1) = SEMI-MAJOR AXIS - DIMENSIONLESS
A(2) = ECCENTRICITY - RADIANS
A(3) = INCLINATION - RADIANS
A(4) = RIGHT ASCENSION OF ASCENDING NODE - RADIANS
A(5) = ARGUMENT OF PERIGEE - RADIANS
A(6) = MEAN ANOMALY - RADIANS
P = ANOMALISTIC PERIOD
EV = MEAN ANGULAR MOTION
UNITS OF OUTPUT ARGUMENTS A(1), P, AND EV WILL DEPEND UPON
THE UNITS EMPLOYED FOR X, VX, AND GH.
ALL ANGLES ARE IN RADIANS.
OUTPUT ARGUMENTS ARE RETURNED TO CALLING PROGRAM IN DOUBLE
FORM.

REFERENCE
REFER TO MATHEMATICAL DESCRIPTION IN SUBPROGRAM WRITEUP

METHOD
REFER TO MATHEMATICAL DESCRIPTION IN SUBPROGRAM WRITEUP

RESTRICTIONS
ECCENTRICITY MUST BE LESS THAN 1.0.

ACCURACY
REFER TO ACCURACY TESTS IN SUBPROGRAM WRITEUP.
INTERNAL ARITHMETIC IS PERFORMED IN DOUBLE PRECISION.

REQUIRED SUBPROGRAMS - FORTRAN 2 MONITOR
DEXPT2, (DFAD), DSQRT, (DFMP), (DFSB), (DFDP)

REQUIRED SUBPROGRAMS - OTHER
07/22/63 ALLOTZ
07/22/63 ATANZ

STORAGE REQUIREMENTS
1015 WITHOUT REQUIRED SUBPROGRAMS

TIMING
NO ESTIMATE AVAILABLE

PROGRAM MODIFICATIONS
NO MODIFICATIONS TO DATE

***** START PROGRAM *****
D DIMENSION X(3),VX(3),A(6),Y(3),VY(3)
500 DO 502 N=1,3
D 501 Y(N)=X(N)
D 502 VY(N)=VX(N)
D 3 R=SQRTF(R2)
D 4 VZ=VY(1)**2+VY(2)**2+VY(3)**2
D 5 V1=SQRTF(VZ)
D 6 RDOT=Y(1)*VY(1)+Y(2)*VY(2)+Y(3)*VY(3)
D 7 H1=Y(2)*VY(3)-Y(3)*VY(2)
D 8 H2=Y(3)*VY(1)-Y(1)*VY(3)
D 9 H3=Y(1)*VY(2)-Y(2)*VY(1)

```

```

D 10 C2=H1**2+H2**2 . RVELZ105
D 11 C1=SQRTF(C2) RVELZ106
D 12 H=SQRTF(H3**2+C2) RVELZ107
D 13 RCI=R*CI RVELZ108
D 14 RTGM=SQRTF(GH) RVELZ109
D 15 A(1)=GM*R/(GM+GM-R*V2) RVELZ110
D 16 RTA=SQRTF(A(1)) RVELZ111
D 17 FI=RODOTZ(RTGM*RTA) RVELZ112
D 18 AR=A(1)/R RVELZ113
D 19 F2=1.0-R/A(1) RVELZ114
D 20 F2=F1**2+F2**2 RVELZ115
D 21 A(2)=SQRTF(E2) RVELZ116
D 22 S1=C1/H RVELZ117
D 23 C1=H3/H RVELZ118
D 24 SN=H1/C1 RVELZ119
D 25 CN=H2/C1 RVELZ120
D 26 SU=H*Y(3)/RC1 RVELZ121
D 27 CU= (Y(2)*H1-Y(1)*H2)/RC1 RVELZ122
D 28 SE=F1/A(2) RVELZ123
D 29 CE=F2/A(2) RVELZ124
D SF=AR+SE*SQRTF(1.0-E2) RVELZ125
D CF=AR*(CE-A(2)) RVELZ126
D 30 A(3)=ATANZ(S1,CI) RVELZ127
D 31 A(4)=ATANZ(SN,CN) RVELZ128
D 32 U=ATANZ(SU,CU) RVELZ129
D F=ATANZ(SF,CF) RVELZ130
D 33 E=ATANZ(SE,CE) RVELZ131
D AS=U-F RVELZ132
D A(5)=ALLOTZ(A5) RVELZ133
D 34 A6=E-A(2)*SE RVELZ134
D 35 A(6)=ALLOTZ(A6) RVELZ135
D 36 EN=RTGM/(RTA*A(1)) RVELZ136
D 37 P=6.283185307179586/EN RVELZ137
RETURN RVELZ138
END RVELZ139
* SUBROUTINE R13Z 'FORTRAN SOURCE PROGRAM' R13Z 000
* CARDS COLUMN R13Z 001
* .LISTB R13Z 002
* LABEL R13Z 003
* SUBROUTINE R13Z(Y,B,A,X) R13Z 004
C
VERSION OF 07/10/63 R13Z 005
FORTRAN SUBROUTINE R13Z 006
FOR USE WITH FORTRAN 2 MONITOR ON IBM 7090, 7094 R13Z 007
C
PURPOSE R13Z 008
SOLVES THE MATRIX EQUATION - R13Z 009
Y = R1(B) R3(A) X R13Z 010
WHERE - R13Z 011
R3(A)= COS A SIN A 0 R13Z 012
-SIN A COS A 0 R13Z 013
0 0 1 R13Z 014
R1(B)= 1 0 0 R13Z 015
0 COS B SIN B R13Z 016
0 -SIN B COS B R13Z 017
C
CALLING SEQUENCE R13Z 018
D DIMENSION Y(3),X(3) R13Z 019
D CALL R13Z(Y,B,A,X) R13Z 020
C
INPUT R13Z 021
VECTOR X IN ANY UNITS R13Z 022
ROTATION ANGLES A AND B IN RADIANS R13Z 023
INPUT ARGUMENTS MUST BE AVAILABLE IN CALLING PROGRAM IN R13Z 024
DOUBLE PRECISION FORM. R13Z 025
C
OUTPUT R13Z 026
VECTOR Y IN SAME UNITS AS VECTOR X R13Z 027
OUTPUT ARGUMENTS ARE RETURNED TO CALLING PROGRAM IN DOUBLE R13Z 028
FORM. R13Z 029
C
REFERENCE R13Z 030
REFER TO MATHEMATICAL DESCRIPTION IN SUBPROGRAM WRITEUP R13Z 031
C
METHOD R13Z 032
REFER TO MATHEMATICAL DESCRIPTION IN SUBPROGRAM WRITEUP R13Z 033
C
RESTRICTIONS R13Z 034
***** R13Z 035
C
ACCURACY R13Z 036
INTERNAL ARITHMETIC IS PERFORMED IN DOUBLE PRECISION. R13Z 037
C
REQUIRED SUBPROGRAMS - FORTRAN 2 MONITOR R13Z 038
DSIN,DCOS,(DFMP),(DFSB),(DFAD). R13Z 039
C
REQUIRED SUBPROGRAMS - OTHER R13Z 040
NONE R13Z 041

```

```

C
C----- STORAGE REQUIREMENTS ----- R13Z 058
C----- 248 WITHOUT REQUIRED SUBPROGRAMS ----- R13Z 059
C----- TIMING ----- R13Z 060
C----- NO ESTIMATE AVAILABLE. ----- R13Z 061
C----- ANALYSIS ----- R13Z 062
C----- PROGRAM MODIFICATIONS ----- R13Z 063
C----- NO MODIFICATIONS TO DATE ----- R13Z 064
C----- START PROGRAM ----- R13Z 065
C----- R13Z 066
C----- R13Z 067
C----- R13Z 068
C----- R13Z 069
C----- R13Z 070
C----- R13Z 071
C----- R13Z 072
C----- R13Z 073
C----- R13Z 074
C----- R13Z 075
C----- R13Z 076
C----- R13Z 077
C----- R13Z 078
C----- R13Z 079
C----- R13Z 080
C----- R13Z 081
C----- R13Z 082
C----- R13Z 083
C----- R13Z 084
C----- R13Z 085
C----- R13Z 086
C----- R13Z 087
C----- R13Z 088
C----- R13Z 089
C----- TIMEC
* SUBROUTINE TIMEC FORTRAN SOURCE PROGRAM
* CARDS COLUMN
* LISTB
* LABEL
* SUBROUTINE TIMEC(DJO,TSEP,S,E,DT)
* USES TAPE A3
C
C----- VERSION OF 7/22/63 -----
C----- READS A CARD FROM CARD READER CONTAINING CALENDAR DATE AND UT2 OF
C----- DESIRED START AND END TIMES FOR CALCULATION OF AN EPHEMERIS, AND
C----- THE TIME INCREMENT OF THE EPHEMERIS IN SECONDS. CALCULATES TIME
C----- INTERVAL IN SECONDS FROM SOME EPOCH (DJO,TSEP) TO THE START AND
C----- END TIMES.
C----- WRITES CALENDAR DATE AND UT2 ON TAPE UNIT A3.
C----- INPUT FROM CALLING SEQUENCE
C----- DJO = EPOCH JULIAN DATE AT 0 HOURS UT2.
C----- TSEP = EPOCH UT2 IN SECONDS
C----- INPUT FROM CARD READER
C----- NMS,NDS,NYS = MONTH, DAY, YEAR OF START DATE
C----- NMF,NDF,NYF = MONTH, DAY, AND YEAR OF END DATE
C----- NMS,NMNS,TSS = HOUR, MINUTE, SECOND (UT2) OF START TIME
C----- NMF,NMNF,TSF = HOUR, MINUTE, SECOND (UT2) OF END DATE
C----- DT = TIME INCREMENT OF EPHEMERIS IN SECONDS
C----- OUTPUT
C----- S = TIME IN SECONDS FROM EPOCH TO START TIME
C----- F = TIME IN SECONDS FROM EPOCH TO END TIME
C----- DT = TIME INCREMENT OF EPHEMERIS IN SECONDS
C----- REQUIRED SUBPROGRAMS
C----- DJUL, JULCAL 37/22/60 - FAP DOUBLE ENTRY PROGRAM
C-----
5015 FORNAT (2(1X)I2) ,1X,14,2I3,F7.3,I3,1X,12,1X,14,2I3,F7.3,F11.3 )
6016 FORNAT (1X)I2,1H)I2,1H)I4,7X)I1H START DATE(1X)I2,I3,F7.3,2X,
1 15H START TIME-UT2(1X)F12.3,5X)23H TIME INCREMENT-SECONDS(1X)I2,
2 1H)I2,1H)I4,7X)9H END DATE(1X)I2,I3,F7.3,5X)13H END TIME-UT2
READ 6015,NMS,NDS,NYS,NMS,NMNS,TSS,NMF,NDF,NYF,NMF,NDF,NYF,
1,NMNF,TSF,DT
WRITE OUTPUT TAPE 3,6016,NMS,NDS,NYS,NMS,NMNS,TSS,DT,NMF,NDF,NYF,
1,NMF,NMNF,TSF
IF (SENSE SWITCH 6) 1,2
PRHT 6016,NMS,NDS,NYS,NMS,NMNS,TSS,DT,NMF,NDF,NYF,NMF,NDF,NYF,TSF
D JDSO=DJUL(NMS,NDS,NYS)
DJFO=DJUL(NMF,NDF,NYF)
TSS=NMS*3600
TMNS=NMNS*60
TS=TS+TMNS+TSS-TSEP
THF=NMF*3600
TMNF=NMNF*60
TF=THF+TMNF+TSF-TSEP
DJS=DJSO-DJO
DJF=DJFO-DJO
S=DJS+86400.+TS
F=DJF+86400.+TF
RETURN
END
* SUBROUTINE VFUZ FORTRAN SOURCE PROGRAM
* CARDS COLUMN
* LISTB
* LABEL
* SUBROUTINE VFUZ(ISC,RE,F,U)
C----- R13Z 090
C----- R13Z 091
C----- R13Z 092
C----- R13Z 093
C----- R13Z 094
C----- R13Z 095

```

```

VERSION OF 07/22/63.....VFUZ 005
FORTRAN SUBROUTINE.....VFUZ 006
FOR USE WITH FORTRAN 2 MONITOR ON IBM 7090, 7094VFUZ 007
VFUZ 008
PURPOSE.....VFUZ 009
CONVERTS GEODETIC LATITUDE, LONGITUDE, AND HEIGHT OF A
STATION ABOVE A COMPUTATIONAL SPHEROID (ALONG A NORMAL TO
THE SPHEROID) INTO GEOCENTRIC RECTANGULAR COORDINATES OF
POSITION. THE ORIGIN OF THE RECTANGULAR COORDINATE SYSTEM
(THE U SYSTEM) IS LOCATED AT THE GEOMETRICAL CENTER OF THE
COMPUTATIONAL SPHEROID. THE U1 AXIS IS DIRECTED INWARDS
THE INTERSECTION OF THE GREENWICH MERIDIAN AND THE
EQUATORIAL PLANE. THE U3 AXIS IS PERPENDICULAR TO THE
EQUATORIAL PLANE AND IS DIRECTED NORTH. THE U2 AXIS IS
LOCATED IN THE EQUATORIAL PLANE 90 DEGREES EAST OF THE U1
AXIS.
VFUZ 010
VFUZ 011
VFUZ 012
VFUZ 013
VFUZ 014
VFUZ 015
VFUZ 016
VFUZ 017
VFUZ 018
VFUZ 019
VFUZ 020
VFUZ 021
VFUZ 022
CALLING SEQUENCE.....VFUZ 023
0 DIMENSION SC(3),U(3)VFUZ 024
0 CALL VEUZ(SC,RE,F,UI)VFUZ 025
VFUZ 026
INPUT.....VFUZ 027
SC(1)= GEODETIC LATITUDE - RADIANSVFUZ 028
SC(2)= GEODETIC LONGITUDE - RADIANSVFUZ 029
SC(3)= HEIGHT ABOVE COMPUTATIONAL SPHEROID ALONG A NORMAL
TO THE SPHEROID.VFUZ 030
VFUZ 031
RE = EQUATORIAL RADIUS OF COMPUTATIONAL SPHEROIDVFUZ 032
F = [INVERSE OF FLATTENING OF COMPUTATIONAL SPHEROID]VFUZ 033
(DIMENSIONLESS) - E.G. IF FLATTENING = 1/298.3,
THEN F = 298.3VFUZ 034
VFUZ 035
VFUZ 036
UNITS OF INPUT ARGUMENTS SC(3) AND RE ARE ARBITRARY BUT
MUST BE MUTUALLY CONSISTENT.VFUZ 037
INPUT ARGUMENTS MUST BE AVAILABLE IN CALLING PROGRAM IN
DOUBLE PRECISION FORM.VFUZ 038
VFUZ 039
VFUZ 040
VFUZ 041
OUTPUT.....VFUZ 042
U(1)VFUZ 043
U(2) THE 3 RECTANGULAR COORDINATES OF POSITIONVFUZ 044
U(3)VFUZ 045
VFUZ 046
UNITS OF OUTPUT ARGUMENTS, U WILL DEPEND UPON THE UNITS
EMPLOYED FOR SC(3) AND RE.VFUZ 047
VFUZ 048
OUTPUT ARGUMENTS ARE RETURNED TO CALLING PROGRAM IN DOUBLE
FORM.VFUZ 049
VFUZ 050
VFUZ 051
VFUZ 052
REFERENCE.....VFUZ 053
REFER TO MATHEMATICAL DESCRIPTION IN SUBPROGRAM WRITEUPVFUZ 054
VFUZ 055
METHOD.....VFUZ 056
REFER TO MATHEMATICAL DESCRIPTION IN SUBPROGRAM WRITEUPVFUZ 057
VFUZ 058
RESTRICTIONS.....VFUZ 059
*****VFUZ 060
VFUZ 061
ACCURACY.....VFUZ 062
INTERNAL ARITHMETIC IS PERFORMED IN DOUBLE PRECISION.VFUZ 063
VFUZ 064
REQUIRED SUBPROGRAMS - FORTRAN 2 MONITORVFUZ 065
DSIN,DCOS,(DFOP),(DFS8),DEXP(2,DSQRT,(DFMB),(DFAD)VFUZ 066
VFUZ 067
REQUIRED SUBPROGRAMS - OTHERVFUZ 068
NONEVFUZ 069
VFUZ 070
STORAGE REQUIREMENTS.....VFUZ 071
305 WITHOUT REQUIRED SUBPROGRAMSVFUZ 072
VFUZ 073
TIMING.....VFUZ 074
NO ESTIMATE AVAILABLEVFUZ 075
VFUZ 076
VFUZ 077
VFUZ 078
VFUZ 079
PROGRAM MODIFICATIONS.....VFUZ 080
NO MODIFICATIONS TO DATEVFUZ 081
VFUZ 082
***** START PROGRAM *****VFUZ 083
VFUZ 084
VFUZ 085
VFUZ 086
VFUZ 087
VFUZ 088
VFUZ 089
VFUZ 090
VFUZ 091
VFUZ 092
VFUZ 093
VFUZ 094
VFUZ 095
VFUZ 096
VFUZ 097
VFUZ 098
VFUZ 099
VFUZ 100
VFUZ 101
VFUZ 102
VFUZ 103
VFUZ 104
VFUZ 105
VFUZ 106
VFUZ 107
VFUZ 108
VFUZ 109
VFUZ 110
VFUZ 111
VFUZ 112
VFUZ 113
VFUZ 114
VFUZ 115
VFUZ 116
VFUZ 117
VFUZ 118
VFUZ 119
VFUZ 120
VFUZ 121
VFUZ 122
VFUZ 123
VFUZ 124
VFUZ 125
VFUZ 126
VFUZ 127
VFUZ 128
VFUZ 129
VFUZ 130
VFUZ 131
VFUZ 132
VFUZ 133
VFUZ 134
VFUZ 135
VFUZ 136
VFUZ 137
VFUZ 138
VFUZ 139
VFUZ 140
VFUZ 141
VFUZ 142
VFUZ 143
VFUZ 144
VFUZ 145
VFUZ 146
VFUZ 147
VFUZ 148
VFUZ 149
VFUZ 150
VFUZ 151
VFUZ 152
VFUZ 153
VFUZ 154
VFUZ 155
VFUZ 156
VFUZ 157
VFUZ 158
VFUZ 159
VFUZ 160
VFUZ 161
VFUZ 162
VFUZ 163
VFUZ 164
VFUZ 165
VFUZ 166
VFUZ 167
VFUZ 168
VFUZ 169
VFUZ 170
VFUZ 171
VFUZ 172
VFUZ 173
VFUZ 174
VFUZ 175
VFUZ 176
VFUZ 177
VFUZ 178
VFUZ 179
VFUZ 180
VFUZ 181
VFUZ 182
VFUZ 183
VFUZ 184
VFUZ 185
VFUZ 186
VFUZ 187
VFUZ 188
VFUZ 189
VFUZ 190
VFUZ 191
VFUZ 192
VFUZ 193
VFUZ 194
VFUZ 195
VFUZ 196
VFUZ 197
VFUZ 198
VFUZ 199
VFUZ 200
VFUZ 201
VFUZ 202
VFUZ 203
VFUZ 204
VFUZ 205
VFUZ 206
VFUZ 207
VFUZ 208
VFUZ 209
VFUZ 210
VFUZ 211
VFUZ 212
VFUZ 213
VFUZ 214
VFUZ 215
VFUZ 216
VFUZ 217
VFUZ 218
VFUZ 219
VFUZ 220
VFUZ 221
VFUZ 222
VFUZ 223
VFUZ 224
VFUZ 225
VFUZ 226
VFUZ 227
VFUZ 228
VFUZ 229
VFUZ 230
VFUZ 231
VFUZ 232
VFUZ 233
VFUZ 234
VFUZ 235
VFUZ 236
VFUZ 237
VFUZ 238
VFUZ 239
VFUZ 240
VFUZ 241
VFUZ 242
VFUZ 243
VFUZ 244
VFUZ 245
VFUZ 246
VFUZ 247
VFUZ 248
VFUZ 249
VFUZ 250
VFUZ 251
VFUZ 252
VFUZ 253
VFUZ 254
VFUZ 255
VFUZ 256
VFUZ 257
VFUZ 258
VFUZ 259
VFUZ 260
VFUZ 261
VFUZ 262
VFUZ 263
VFUZ 264
VFUZ 265
VFUZ 266
VFUZ 267
VFUZ 268
VFUZ 269
VFUZ 270
VFUZ 271
VFUZ 272
VFUZ 273
VFUZ 274
VFUZ 275
VFUZ 276
VFUZ 277
VFUZ 278
VFUZ 279
VFUZ 280
VFUZ 281
VFUZ 282
VFUZ 283
VFUZ 284
VFUZ 285
VFUZ 286
VFUZ 287
VFUZ 288
VFUZ 289
VFUZ 290
VFUZ 291
VFUZ 292
VFUZ 293
VFUZ 294
VFUZ 295
VFUZ 296
VFUZ 297
VFUZ 298
VFUZ 299
VFUZ 300
VFUZ 301
VFUZ 302
VFUZ 303
VFUZ 304
VFUZ 305
VFUZ 306
VFUZ 307
VFUZ 308
VFUZ 309
VFUZ 310
VFUZ 311
VFUZ 312
VFUZ 313
VFUZ 314
VFUZ 315
VFUZ 316
VFUZ 317
VFUZ 318
VFUZ 319
VFUZ 320
VFUZ 321
VFUZ 322
VFUZ 323
VFUZ 324
VFUZ 325
VFUZ 326
VFUZ 327
VFUZ 328
VFUZ 329
VFUZ 330
VFUZ 331
VFUZ 332
VFUZ 333
VFUZ 334
VFUZ 335
VFUZ 336
VFUZ 337
VFUZ 338
VFUZ 339
VFUZ 340
VFUZ 341
VFUZ 342
VFUZ 343
VFUZ 344
VFUZ 345
VFUZ 346
VFUZ 347
VFUZ 348
VFUZ 349
VFUZ 350
VFUZ 351
VFUZ 352
VFUZ 353
VFUZ 354
VFUZ 355
VFUZ 356
VFUZ 357
VFUZ 358
VFUZ 359
VFUZ 360
VFUZ 361
VFUZ 362
VFUZ 363
VFUZ 364
VFUZ 365
VFUZ 366
VFUZ 367
VFUZ 368
VFUZ 369
VFUZ 370
VFUZ 371
VFUZ 372
VFUZ 373
VFUZ 374
VFUZ 375
VFUZ 376
VFUZ 377
VFUZ 378
VFUZ 379
VFUZ 380
VFUZ 381
VFUZ 382
VFUZ 383
VFUZ 384
VFUZ 385
VFUZ 386
VFUZ 387
VFUZ 388
VFUZ 389
VFUZ 390
VFUZ 391
VFUZ 392
VFUZ 393
VFUZ 394
VFUZ 395
VFUZ 396
VFUZ 397
VFUZ 398
VFUZ 399
VFUZ 400
VFUZ 401
VFUZ 402
VFUZ 403
VFUZ 404
VFUZ 405
VFUZ 406
VFUZ 407
VFUZ 408
VFUZ 409
VFUZ 410
VFUZ 411
VFUZ 412
VFUZ 413
VFUZ 414
VFUZ 415
VFUZ 416
VFUZ 417
VFUZ 418
VFUZ 419
VFUZ 420
VFUZ 421
VFUZ 422
VFUZ 423
VFUZ 424
VFUZ 425
VFUZ 426
VFUZ 427
VFUZ 428
VFUZ 429
VFUZ 430
VFUZ 431
VFUZ 432
VFUZ 433
VFUZ 434
VFUZ 435
VFUZ 436
VFUZ 437
VFUZ 438
VFUZ 439
VFUZ 440
VFUZ 441
VFUZ 442
VFUZ 443
VFUZ 444
VFUZ 445
VFUZ 446
VFUZ 447
VFUZ 448
VFUZ 449
VFUZ 450
VFUZ 451
VFUZ 452
VFUZ 453
VFUZ 454
VFUZ 455
VFUZ 456
VFUZ 457
VFUZ 458
VFUZ 459
VFUZ 460
VFUZ 461
VFUZ 462
VFUZ 463
VFUZ 464
VFUZ 465
VFUZ 466
VFUZ 467
VFUZ 468
VFUZ 469
VFUZ 470
VFUZ 471
VFUZ 472
VFUZ 473
VFUZ 474
VFUZ 475
VFUZ 476
VFUZ 477
VFUZ 478
VFUZ 479
VFUZ 480
VFUZ 481
VFUZ 482
VFUZ 483
VFUZ 484
VFUZ 485
VFUZ 486
VFUZ 487
VFUZ 488
VFUZ 489
VFUZ 490
VFUZ 491
VFUZ 492
VFUZ 493
VFUZ 494
VFUZ 495
VFUZ 496
VFUZ 497
VFUZ 498
VFUZ 499
VFUZ 500
VFUZ 501
VFUZ 502
VFUZ 503
VFUZ 504
VFUZ 505
VFUZ 506
VFUZ 507
VFUZ 508
VFUZ 509
VFUZ 510
VFUZ 511
VFUZ 512
VFUZ 513
VFUZ 514
VFUZ 515
VFUZ 516
VFUZ 517
VFUZ 518
VFUZ 519
VFUZ 520
VFUZ 521
VFUZ 522
VFUZ 523
VFUZ 524
VFUZ 525
VFUZ 526
VFUZ 527
VFUZ 528
VFUZ 529
VFUZ 530
VFUZ 531
VFUZ 532
VFUZ 533
VFUZ 534
VFUZ 535
VFUZ 536
VFUZ 537
VFUZ 538
VFUZ 539
VFUZ 540
VFUZ 541
VFUZ 542
VFUZ 543
VFUZ 544
VFUZ 545
VFUZ 546
VFUZ 547
VFUZ 548
VFUZ 549
VFUZ 550
VFUZ 551
VFUZ 552
VFUZ 553
VFUZ 554
VFUZ 555
VFUZ 556
VFUZ 557
VFUZ 558
VFUZ 559
VFUZ 560
VFUZ 561
VFUZ 562
VFUZ 563
VFUZ 564
VFUZ 565
VFUZ 566
VFUZ 567
VFUZ 568
VFUZ 569
VFUZ 570
VFUZ 571
VFUZ 572
VFUZ 573
VFUZ 574
VFUZ 575
VFUZ 576
VFUZ 577
VFUZ 578
VFUZ 579
VFUZ 580
VFUZ 581
VFUZ 582
VFUZ 583
VFUZ 584
VFUZ 585
VFUZ 586
VFUZ 587
VFUZ 588
VFUZ 589
VFUZ 590
VFUZ 591
VFUZ 592
VFUZ 593
VFUZ 594
VFUZ 595
VFUZ 596
VFUZ 597
VFUZ 598
VFUZ 599
VFUZ 600
VFUZ 601
VFUZ 602
VFUZ 603
VFUZ 604
VFUZ 605
VFUZ 606
VFUZ 607
VFUZ 608
VFUZ 609
VFUZ 610
VFUZ 611
VFUZ 612
VFUZ 613
VFUZ 614
VFUZ 615
VFUZ 616
VFUZ 617
VFUZ 618
VFUZ 619
VFUZ 620
VFUZ 621
VFUZ 622
VFUZ 623
VFUZ 624
VFUZ 625
VFUZ 626
VFUZ 627
VFUZ 628
VFUZ 629
VFUZ 630
VFUZ 631
VFUZ 632
VFUZ 633
VFUZ 634
VFUZ 635
VFUZ 636
VFUZ 637
VFUZ 638
VFUZ 639
VFUZ 640
VFUZ 641
VFUZ 642
VFUZ 643
VFUZ 644
VFUZ 645
VFUZ 646
VFUZ 647
VFUZ 648
VFUZ 649
VFUZ 650
VFUZ 651
VFUZ 652
VFUZ 653
VFUZ 654
VFUZ 655
VFUZ 656
VFUZ 657
VFUZ 658
VFUZ 659
VFUZ 660
VFUZ 661
VFUZ 662
VFUZ 663
VFUZ 664
VFUZ 665
VFUZ 666
VFUZ 667
VFUZ 668
VFUZ 669
VFUZ 670
VFUZ 671
VFUZ 672
VFUZ 673
VFUZ 674
VFUZ 675
VFUZ 676
VFUZ 677
VFUZ 678
VFUZ 679
VFUZ 680
VFUZ 681
VFUZ 682
VFUZ 683
VFUZ 684
VFUZ 685
VFUZ 686
VFUZ 687
VFUZ 688
VFUZ 689
VFUZ 690
VFUZ 691
VFUZ 692
VFUZ 693
VFUZ 694
VFUZ 695
VFUZ 696
VFUZ 697
VFUZ 698
VFUZ 699
VFUZ 700
VFUZ 701
VFUZ 702
VFUZ 703
VFUZ 704
VFUZ 705
VFUZ 706
VFUZ 707
VFUZ 708
VFUZ 709
VFUZ 710
VFUZ 711
VFUZ 712
VFUZ 713
VFUZ 714
VFUZ 715
VFUZ 716
VFUZ 717
VFUZ 718
VFUZ 719
VFUZ 720
VFUZ 721
VFUZ 722
VFUZ 723
VFUZ 724
VFUZ 725
VFUZ 726
VFUZ 727
VFUZ 728
VFUZ 729
VFUZ 730
VFUZ 731
VFUZ 732
VFUZ 733
VFUZ 734
VFUZ 735
VFUZ 736
VFUZ 737
VFUZ 738
VFUZ 739
VFUZ 740
VFUZ 741
VFUZ 742
VFUZ 743
VFUZ 744
VFUZ 745
VFUZ 746
VFUZ 747
VFUZ 748
VFUZ 749
VFUZ 750
VFUZ 751
VFUZ 752
VFUZ 753
VFUZ 754
VFUZ 755
VFUZ 756
VFUZ 757
VFUZ 758
VFUZ 759
VFUZ 760
VFUZ 761
VFUZ 762
VFUZ 763
VFUZ 764
VFUZ 765
VFUZ 766
VFUZ 767
VFUZ 768
VFUZ 769
VFUZ 770
VFUZ 771
VFUZ 772
VFUZ 773
VFUZ 774
VFUZ 775
VFUZ 776
VFUZ 777
VFUZ 778
VFUZ 779
VFUZ 780
VFUZ 781
VFUZ 782
VFUZ 783
VFUZ 784
VFUZ 785
VFUZ 786
VFUZ 787
VFUZ 788
VFUZ 789
VFUZ 790
VFUZ 791
VFUZ 792
VFUZ 793
VFUZ 794
VFUZ 795
VFUZ 796
VFUZ 797
VFUZ 798
VFUZ 799
VFUZ 800
VFUZ 801
VFUZ 802
VFUZ 803
VFUZ 804
VFUZ 805
VFUZ 806
VFUZ 807
VFUZ 808
VFUZ 809
VFUZ 810
VFUZ 811
VFUZ 812
VFUZ 813
VFUZ 814
VFUZ 815
VFUZ 816
VFUZ 817
VFUZ 818
VFUZ 819
VFUZ 820
VFUZ 821
VFUZ 822
VFUZ 823
VFUZ 824
VFUZ 825
VFUZ 826
VFUZ 827
VFUZ 828
VFUZ 829
VFUZ 830
VFUZ 831
VFUZ 832
VFUZ 833
VFUZ 834
VFUZ 835
VFUZ 836
VFUZ 837
VFUZ 838
VFUZ 839
VFUZ 840
VFUZ 841
VFUZ 842
VFUZ 843
VFUZ 844
VFUZ 845
VFUZ 846
VFUZ 847
VFUZ 848
VFUZ 849
VFUZ 850
VFUZ 851
VFUZ 852
VFUZ 853
VFUZ 854
VFUZ 855
VFUZ 856
VFUZ 857
VFUZ 858
VFUZ 859
VFUZ 860
VFUZ 861
VFUZ 862
VFUZ 863
VFUZ 864
VFUZ 865
VFUZ 866
VFUZ 867
VFUZ 868
VFUZ 869
VFUZ 870
VFUZ 871
VFUZ 872
VFUZ 873
VFUZ 874
VFUZ 875
VFUZ 876
VFUZ 877
VFUZ 878
VFUZ 879
VFUZ 880
VFUZ 881
VFUZ 882
VFUZ 883
VFUZ 884
VFUZ 885
VFUZ 886
VFUZ 887
VFUZ 888
VFUZ 889
VFUZ 890
VFUZ 891
VFUZ 892
VFUZ 893
VFUZ 894
VFUZ 895
VFUZ 896
VFUZ 897
VFUZ 898
VFUZ 899
VFUZ 900
VFUZ 901
VFUZ 902
VFUZ 903
VFUZ 904
VFUZ 905
VFUZ 906
VFUZ 907
VFUZ 908
VFUZ 909
VFUZ 910
VFUZ 911
VFUZ 912
VFUZ 913
VFUZ 914
VFUZ 915
VFUZ 916
VFUZ 917
VFUZ 918
VFUZ 919
VFUZ 920
VFUZ 921
VFUZ 922
VFUZ 923
VFUZ 924
VFUZ 925
VFUZ 926
VFUZ 927
VFUZ 928
VFUZ 929
VFUZ 930
VFUZ 931
VFUZ 932
VFUZ 933
VFUZ 934
VFUZ 935
VFUZ 936
VFUZ 937
VFUZ 938
VFUZ 939
VFUZ 940
VFUZ 941
VFUZ 942
VFUZ 943
VFUZ 944
VFUZ 945
VFUZ 946
VFUZ 947
VFUZ 948
VFUZ 949
VFUZ 950
VFUZ 951
VFUZ 952
VFUZ 953
VFUZ 954
VFUZ 955
VFUZ 956
VFUZ 957
VFUZ 958
VFUZ 959
VFUZ 960
VFUZ 961
VFUZ 962
VFUZ 963
VFUZ 964
VFUZ 965
VFUZ 966
VFUZ 967
VFUZ 968
VFUZ 969
VFUZ 970
VFUZ 971
VFUZ 972
VFUZ 973
VFUZ 974
VFUZ 975
VFUZ 976
VFUZ 977
VFUZ 978
VFUZ 979
VFUZ 980
VFUZ 981
VFUZ 982
VFUZ 983
VFUZ 984
VFUZ 985
VFUZ 986
VFUZ 987
VFUZ 988
VFUZ 989
VFUZ 990
VFUZ 991
VFUZ 992
VFUZ 993
VFUZ 994
VFUZ 995
VFUZ 996
VFUZ 997
VFUZ 998
VFUZ 999
VFUZ 1000
VFUZ 1001
VFUZ 1002
VFUZ 1003
VFUZ 1004
VFUZ 1005
VFUZ 1006
VFUZ 1007
VFUZ 1008
VFUZ 1009
VFUZ 1010
VFUZ 1011
VFUZ 1012
VFUZ 1013
VFUZ 1014
VFUZ 1015
VFUZ 1016
VFUZ 1017
VFUZ 1018
VFUZ 1019
VFUZ 1020
VFUZ 1021
VFUZ 1022
VFUZ 1023
VFUZ 1024
VFUZ 1025
VFUZ 1026
VFUZ 1027
VFUZ 1028
VFUZ 1029
VFUZ 1030
VFUZ 1031
VFUZ 1032
VFUZ 1033
VFUZ 1034
VFUZ 1035
VFUZ 1036
VFUZ 1037
VFUZ 1038
VFUZ 1039
VFUZ 1040
VFUZ 1041
VFUZ 1042
VFUZ 1043
VFUZ 1044
VFUZ 1045
VFUZ 1046
VFUZ 1047
VFUZ 1048
VFUZ 1049
VFUZ 1050
VFUZ 1051
VFUZ 1052
VFUZ 1053
VFUZ 1054
VFUZ 1055
VFUZ 1056
VFUZ 1057
VFUZ 1058
VFUZ 1059
VFUZ 1060
VFUZ 1061
VFUZ 1062
VFUZ 1063
VFUZ 1064
VFUZ 1065
VFUZ 1066
VFUZ 1067
VFUZ 1068
VFUZ 1069
VFUZ 1070
VFUZ 1071
VFUZ 1072
VFUZ 1073
VFUZ 1074
VFUZ 1075
VFUZ 1076
VFUZ 1077
VFUZ 1078
VFUZ 1079
VFUZ 1080
VFUZ 1081
VFUZ 1082
VFUZ 1083
VFUZ 1084
VFUZ 1085
VFUZ 1086
VFUZ 1087
VFUZ 1088
VFUZ 1089
VFUZ 1090
VFUZ 1091
VFUZ 1092
VFUZ 1093
VFUZ 1094
VFUZ 1095
VFUZ 1096
VFUZ 1097
VFUZ 1098
VFUZ 1099
VFUZ 1100
VFUZ 1101
VFUZ 1102
VFUZ 1103
VFUZ 1104
VFUZ 1105
VFUZ 1106
VFUZ 1107
VFUZ 1108
VFUZ 1109
VFUZ 1110
VFUZ 1111
VFUZ 1112
VFUZ 1113
VFUZ 1114
VFUZ 1115
VFUZ 1116
VFUZ 1117
VFUZ 1118
VFUZ 1119
VFUZ 1120
VFUZ 1121
VFUZ 1122
VFUZ 1123
VFUZ 1124
VFUZ 1125
VFUZ 1126
VFUZ 1127
VFUZ 1128
VFUZ 1129
VFUZ 1130
VFUZ 1131
VFUZ 1132
VFUZ 1133
VFUZ 1134
VFUZ 1135
VFUZ 1136
VFUZ 1137
VFUZ 1138
VFUZ 1139
VFUZ 1140
VFUZ 1141
VFUZ 1142
VFUZ 1143
VFUZ 1144
VFUZ 1145
VFUZ 1146
VFUZ 1147
VFUZ 1148
VFUZ 1149
VFUZ 1150
VFUZ 1151
VFUZ 1152
VFUZ 1153
VFUZ 1154
VFUZ 1155
VFUZ 1156
VFUZ 1157
VFUZ 1158
VFUZ 1159
VFUZ 1160
VFUZ 1161
VFUZ 1162
VFUZ 1163
VFUZ 1164
VFUZ 1165
VFUZ 1166
VFUZ 1167
VFUZ 1168
VFUZ 1169
VFUZ 1170
VFUZ 1171
VFUZ 1172
VFUZ 1173
VFUZ 1174
VFUZ 1175
VFUZ 1176
VFUZ 1177
VFUZ 1178
VFUZ 1179
VFUZ 1180
VFUZ 1181
VFUZ 1182
VFUZ 1183
VFUZ 1184
VFUZ 1185
VFUZ 1186
VFUZ 1187
VFUZ 1188
VFUZ 1189
VFUZ 1190
VFUZ 1191
VFUZ 1192
VFUZ 1193
VFUZ 1194
VFUZ 1195
VFUZ 1196
VFUZ 1197
VFUZ 1198
VFUZ 1199
VFUZ 1200
VFUZ 1201
VFUZ 1202
VFUZ 1203
VFUZ 1204
VFUZ 1205
VFUZ 1206
VFUZ 1207
VFUZ 1208
VFUZ 1209
VFUZ 1210
VFUZ 1211
VFUZ 1212
VFUZ 1213
VFUZ 1214
VFUZ 1215
VFUZ 1216
VFUZ 1217
VFUZ 1218
VFUZ 1219
VFUZ 1220
VFUZ 1221
VFUZ 1222
VFUZ 1223
VFUZ 1224
VFUZ 1225
VFUZ 1226
VFUZ 1227
VFUZ 1228
VFUZ 1229
VFUZ 1230
VFUZ 1231
VFUZ 1232
VFUZ 1233
VFUZ 1234
VFUZ 1235
VFUZ 1236
VFUZ 1237
VFUZ 1238
VFUZ 1239
VFUZ 1240
VFUZ 1241
VFUZ 1242
VFUZ 1243
VFUZ 1244
VFUZ 1245
VFUZ 1246
VFUZ 1247
VFUZ 1248
VFUZ 1249
VFUZ 1250
VFUZ 1251
VFUZ 1252
VFUZ 1253
VFUZ 1254
VFUZ 1255
VFUZ 1256
VFUZ 1257
VFUZ 1258
VFUZ 1259
VFUZ 1260
VFUZ 1261
VFUZ 1262
VFUZ 1263
VFUZ 1264
VFUZ 1265
VFUZ 1266
VFUZ 1267
VFUZ 1268
VFUZ 1269
VFUZ 1270
VFUZ 1271
VFUZ 1272
VFUZ 1273
VFUZ 1274
VFUZ 1275
VFUZ 1276
VFUZ 1277
VFUZ 1278
VFUZ 1279
VFUZ 1280
VFUZ 1281
VFUZ 1282
VFUZ 1283
VFUZ 1284
VFUZ 1285
VFUZ 1286
VFUZ 1287
VFUZ 1288
VFUZ 1289
VFUZ 1290
VFUZ 1291
VFUZ 1292
VFUZ 1293
VFUZ 1294
VFUZ 1295
VFUZ 1296
VFUZ 1297
VFUZ 1298
VFUZ 1299
VFUZ 1300
VFUZ 1301
VFUZ 1302
VFUZ 1303
VFUZ 1304
VFUZ 1305
VFUZ 1306
VFUZ 1307
VFUZ 1308
VFUZ 1309
VFUZ 1310
VFUZ 1311
VFUZ 1312
VFUZ 1313
VFUZ 1314
VFUZ 1315
VFUZ 1316
VFUZ 1317
VFUZ 1318
VFUZ 1319
VFUZ 1320
VFUZ 1321
VFUZ 1322
VFUZ 1323
VFUZ 1324
VFUZ 1325
VFUZ 1326
VFUZ 1327
VFUZ 1328
VFUZ 1329
VFUZ 1330
VFUZ 1331
VFUZ 1332
VFUZ 1333
VFUZ 1334
VFUZ 1335
VFUZ 1336
VFUZ 1337
VFUZ 1338
VFUZ 1339
VFUZ 1340
VFUZ 1341
VFUZ 1342
VFUZ 1343
VFUZ 1344
VFUZ 1345
VFUZ 1346
VFUZ 1347
VFUZ 1348
VFUZ 1349
VFUZ 1350
VFUZ 1351
VFUZ 1352
VFUZ 1353
VFUZ 1354
VFUZ 1355
VFUZ 1356
VFUZ 1357
VFUZ 1358
VFUZ 1359
VFUZ 1360
VFUZ 1361
VFUZ 1362
VFUZ 1363
VFUZ 1364
VFUZ 1365
VFUZ 1366
VFUZ 1367
VFUZ 1368
VFUZ 1369
VFUZ 1370
VFUZ 1371
VFUZ 1372
VFUZ 1373
VFUZ 1374
VFUZ 1375
VFUZ 1376
VFUZ 1377
VFUZ 1378
VFUZ 1379
VFUZ 1380
VFUZ 1381
VFUZ 1382
VFUZ 1383
VFUZ 1384
VFUZ 1385
VFUZ 1386
VFUZ 1387
VFUZ 1388
VFUZ 1389
VFUZ 1390
VFUZ 1391
VFUZ 1392
VFUZ 1393
VFUZ 1394
VFUZ 1395
VFUZ 1396
VFUZ 1397
VFUZ 1398
VFUZ 1399
VFUZ 1400
VFUZ 1401
VFUZ 1402
VFUZ 1403
VFUZ 1404
VFUZ 1405
VFUZ 1406
VFUZ 1407
VFUZ 1408
VFUZ 1409
VFUZ 1410
VFUZ 1411
VFUZ 1412
VFUZ 1413
VFUZ 1414
VFUZ 1415
VFUZ 1416
VFUZ 1417
VFUZ 1418
VFUZ 1419
VFUZ 1420
VFUZ 1421
VFUZ 1422
VFUZ 1423
VFUZ 1424
VFUZ 1425
VFUZ 1426
VFUZ 1427
VFUZ 1428
VFUZ 1429
VFUZ 1430
VFUZ 1431
VFUZ 1432
VFUZ 1433
VFUZ 1434
VFUZ 1435
VFUZ 1436
VFUZ 1437
VFUZ 1438
VFUZ 1439
VFUZ 1440
VFUZ 1441
VFUZ 1442
VFUZ 1443
VFUZ 1444
VFUZ 1445
VFUZ 1446
VFUZ 1447
VFUZ 1448
VFUZ 1449
VFUZ 1450
VFUZ 1451
VFUZ 1452
VFUZ 1453
VFUZ 1454
VFUZ 1455
VFUZ 1456
VFUZ 1457
VFUZ 1458
VFUZ 1459
VFUZ 1460
VFUZ 1461
VFUZ 1462
VFUZ 1463
VFUZ 1464
VFUZ 1465
VFUZ 1466
VFUZ 1467
VFUZ 1468
VFUZ 1469
VFUZ 1470
VFUZ 1471
VFUZ 1472
VFUZ 1473
VFUZ 1474
VFUZ 1475
VFUZ 1476
VFUZ 1477
VFUZ 1478
VFUZ 1479
VFUZ 1480
VFUZ 1481
VFUZ 1482
VFUZ 1483
VFUZ 1484
VFUZ 1485
VFUZ 1486
VFUZ 1487
VFUZ 1488
VFUZ 1489
VFUZ 1490
VFUZ 1491
VFUZ 1492
VFUZ 1493
VFUZ 1494
VFUZ 1495
VFUZ 1496
VFUZ 1497
VFUZ 1498
VFUZ 1499
VFUZ 1500
VFUZ 1501
VFUZ 1502
VFUZ 1503
VFUZ 1504
VFUZ 1505
VFUZ 1506
VFUZ 1507
VFUZ 1508
VFUZ 1509
VFUZ 1510
VFUZ 1511
VFUZ 1512
VFUZ 1513
VFUZ 1514
VFUZ 1515
VFUZ 1516
VFUZ 1517
VFUZ 1518
VFUZ 1519
VFUZ 1520
VFUZ 1521
VFUZ 1522
VFUZ 1523
VFUZ 1524
VFUZ 1525
VFUZ 1526
VFUZ 1527
VFUZ 1528
VFUZ 1529
VFUZ 1530
VFUZ 1531
VFUZ 1532
VFUZ 1533
VFUZ 1534
VFUZ 1535
VFUZ 1536
VFUZ 1537
VFUZ 1538
VFUZ 1539
VFUZ 1540
VFUZ 1541
VFUZ 1542
VFUZ 1543
VFUZ 1544
VFUZ 1545
VFUZ 1546
VFUZ 1547
VFUZ 1548
VFUZ 1549
VFUZ 1550
VFUZ 1551
VFUZ 1552
VFUZ 1553
VFUZ 1554
VFUZ 1555
VFUZ 1556
VFUZ 1557
VFUZ 1558
VFUZ 1559
VFUZ 1560
VFUZ 1561
VFUZ 1562
VFUZ 1563
VFUZ 1564
VFUZ 1565
VFUZ 1566
VFUZ 1567
VFUZ 1568
VFUZ 1569
VFUZ 1570
VFUZ 1571
VFUZ 1572
VFUZ 1573
VFUZ 1574
VFUZ 1575
VFUZ 1576
VFUZ 1577
VFUZ 1578
VFUZ 1579
VFUZ 1580
VFUZ 1581
VFUZ 1582
VFUZ 1583
VFUZ 1584
VFUZ 1585
VFUZ 1586
VFUZ 1587
VFUZ 1588
VFUZ 1589
VFUZ 1590
VFUZ 1591
VFUZ 1592
VFUZ 1593
VFUZ 1594
VFUZ 1595
VFUZ 15
```

```

SUBROUTINE VRDZ(N,Z,E,A,R) VRDZ 003
C----- VRDZ 006
VERSION OF 07/16/63 VRDZ 005
FORTRAN SUBROUTINE VRDZ 004
FOR USE WITH FORTRAN 2 MONITOR ON IBM 7090, 7094 VRDZ 007
C----- VRDZ 008
PURPOSE VRDZ 009
C----- VRDZ 010
CONVERTS RECTANGULAR POSITION COORDINATES OF A POINT TO THE
SPHERICAL COORDINATES OF THE POINT. VRDZ 011
C----- VRDZ 012
C----- VRDZ 013
CALLING SEQUENCE VRDZ 014
D DIMENSION Z(3) VRDZ 015
D CALL VRDZ(1,Z,E,A,R) VRDZ 016
D CALL VRDZ(2,Z,E,A,R) VRDZ 017
C----- VRDZ 018
INPUT VRDZ 019
Z(1) VRDZ 020
Z(2) THE 3 RECTANGULAR COORDINATES OF POSITION VRDZ 021
Z(3) VRDZ 022
N = OPTION NUMBER TO DETERMINE TYPE OF SPHERICAL
COORDINATE DESIRED. VRDZ 024
VRDZ 025
OUTPUT VRDZ 027
R = MAGNITUDE OF POSITION VECTOR VRDZ 028
E = ANGULAR DISTANCE IN RADIANs OF VECTOR FROM Z1-Z2 VRDZ 029
PLANE (E.G. ELEVATION, DECLINATION, LATITUDE) VRDZ 030
E IS RESTRICTED TO LIE BETWEEN 0 AND + PI/2 RADIANs
OR BETWEEN 0 AND - PI/2 RADIANs VRDZ 031
VRDZ 032
N=1 A = ANGULAR DISTANCE IN RADIANs OF PROJECTION OF VECTOR VRDZ 033
ONTO THE Z1-Z2 PLANE, MEASURED POSITIVELY COUNTER- VRDZ 035
CLOCKWISE FROM THE Z1 AXIS (E.G. RIGHT ASCENSION, VRDZ 036
LONGITUDE MEASURED POSITIVE EAST FROM GREENWICH) VRDZ 037
VRDZ 038
N=2 A = ANGULAR DISTANCE IN RADIANs OF PROJECTION OF VECTOR VRDZ 039
ONTO THE Z1-Z2 PLANE, MEASURED POSITIVELY CLOCKWISE VRDZ 040
FROM THE Z2 AXIS (E.G. AZIMUTH MEASURED POSITIVE VRDZ 041
CLOCKWISE FROM NORTH) VRDZ 042
VRDZ 043
A IS RESTRICTED TO LIE BETWEEN 0 AND + 2 PI RADIANs VRDZ 044
VRDZ 045
OUTPUT ARGUMENTS ARE RETURNED TO CALLING PROGRAM IN DOUBLE
FORM. VRDZ 046
VRDZ 047
VRDZ 048
VRDZ 049
REFERENCE VRDZ 050
REFER TO MATHEMATICAL DESCRIPTION IN SUBPROGRAM WRITEUP VRDZ 051
VRDZ 052
METHOD VRDZ 053
REFER TO MATHEMATICAL DESCRIPTION IN SUBPROGRAM WRITEUP VRDZ 054
VRDZ 055
RESTRICTIONS VRDZ 056
***** VRDZ 057
VRDZ 058
ACCURACY VRDZ 059
INTERNAL ARITHMETIC IS PERFORMED IN DOUBLE PRECISION. VRDZ 060
VRDZ 061
REQUIRED SUBPROGRAMS - FORTRAN 2 MONITOR VRDZ 062
DSQRT,DEXP(2),(DFA0),(DFDP),(DFMP),DATAN VRDZ 063
VRDZ 064
REQUIRED SUBPROGRAMS - OTHER VRDZ 065
07/22/63 ATANZ VRDZ 066
VRDZ 067
STORAGE REQUIREMENTS VRDZ 068
298 WITHOUT REQUIRED SUBPROGRAMS VRDZ 069
VRDZ 070
TIMING VRDZ 071
NO ESTIMATE AVAILABLE VRDZ 072
VRDZ 073
VRDZ 074
VRDZ 075
PROGRAM MODIFICATIONS VRDZ 081
NO MODIFICATIONS TO DATE VRDZ 082
VRDZ 083
***** START PROGRAM ***** VRDZ 085
C----- VRDZ 086
2 DIMENSION Z(3) VRDZ 087
C----- VRDZ 088
3 R=SQRT(Z(1)**2+Z(2)**2+Z(3)**2) VRDZ 089
4 SE=Z(3)/R VRDZ 090
5 CE=SQRT(1.0-SE**2) VRDZ 091
6 C=R*CE VRDZ 092
GO TO (7,9), N VRDZ 093
7 CA=Z(1)/C VRDZ 094
8 SA=Z(2)/C VRDZ 095
GO TO 11 VRDZ 096
9 SA=Z(1)/C VRDZ 097
10 CA=Z(2)/C VRDZ 098
11 E=ATAN2(SE,CF) VRDZ 099
12 A=ATANZ(SA,CA) VRDZ 100
RETURN VRDZ 101
END VRDZ 102

```

```

* FUNCTION XKEP                                     XKEP
* CARDS COLUMN
* LISTB
* LABEL
* FUNCTION XKEP(AM,ECC,SE,CE,ERR)
  E1 = AM + (ECC * SINP(AM) )
  N = 0
1 E2 = E1
  N = N + 1
  SE = SINP(E1)
  CE = COSP(E1)
  E1 = E1 + ((AM - E1 + ECC*SE) / (1.0 - ECC*CE))
  G = ABSF(E1 - E2) / E1
  IF( N = 20 ) 2,2,3
  IF( G = ERR ) 5,5,1
  3 PRINT 4
  PRINT 6,AM,E1,E2,G,N
  4 FORMAT (36H0D CONVERGENCE IN KEPLERS EQUATION
  6 FORMAT (4E16,8,I5)
  SENSE LIGHT 2
  5 XKEP = E1
  RETURN
  END
* FUNCTION XKCP2                                     XKEPZ
* CARDS COLUMN
* LISTB
* LABEL
* FUNCTION XKCP2(AM,ECC,SE,CE,ERR)
D .. E1 = AM + (ECC * SINP(AM) )
  N = 0
D 1 E2 = E1
  N = N + 1
D SE = SINP(E1)
D CE = COSP(E1)
D .. E1 = E1 + ((AM - E1 + ECC*SE) / (1.0 - ECC*CE))
D G = ABSF(E1 - E2) / E1
D IF( N = 20 ) 2,2,3
D 2 IF( G = ERR ) 5,5,1
  3 PRINT 4
  PRINT 6,AM,E1,E2,G,N
  4 FORMAT (36H0D CONVERGENCE IN KEPLERS EQUATION
  6 FORMAT (4E16,8,I5)
  SENSE LIGHT 2
D 5 XKCP2 = E1
  RETURN
  END
* SUBROUTINE BACK
* CARDS COLUMN
* LISTB
* FAP
COUNT 82
LBL BACK,X
REM SUBROUTINE BACK
REM PROGRAM IN CORE A. MOVES AN ARRAY FROM CORE B TO
REM DESIGNATED LOCATIONS CORE A.
ENTRY BACK
BACK EFT TEST FOR A OR B CORE
TRA ERROR ERROR - B CORE
SXA STORA,1 STORE MACHINE CONDITIONS
SXO STORA,2 X
STI STOIND X
AXT 0,2 ZERO I.R. 2
CAL* 2,4 FORTRAN ADDRESS BLOCK FROM CORE B
ARS 18 SHIFT TO ADDRESS PORTION OF WORD
STA ARRAY STORED FOR REFERENCE
SUB ADDR1 SETTING UP TRANSFER OF THREE WORDS
STA ARRAY+1 AT A TIME
SUB ADDR1 X
STA ARRAY+2 X
CAL* 2,4 ARRAY LENGTH
PDX 0,1 PLACED IN I.R. 1
TXL SHLARY,1,2 SMALL ARRAY, LENGTH EQUAL TO 1 OR 2
CAL 1,4 FORTRAN ADDRESS BLOCK IN CORE A
STA STORE STORED FOR REFERENCE
SUB ADDR1 WILL BE STORING THREE WORDS AT A TIME
STA STORE+1 X
SUB ADDR1 X
STA STORE+2 X
RESET SEB X
ARRAY CLA **2 TRANSFER OF WORDS
LDO **2 X
LDI **2 X
SEA X
STORE STO **2 STORED
STO **2 X
STI **2 X
TXL **1,2,3 MOVE DOWN THROUGH BLOCK
TIX RESET,1,3 REDUCE BLOCK BY 3
TXH ARRAY3,1,2 IF 3 WORDS, SET I.R. 1 = 0
TXH THWDS,1,1 TEST FOR REMAINING (1 OR 2) WORDS
TXL RETURN,1,0 X
ONEWD CAL* 3,4 TRANSFERRING TOTAL OF 1 WORD, OR
ARS 18 REMAINING WORD FROM A TO B CORE
STA ARRAY1 REMAINING WORD FROM A TO B CORE

```


	CAL	1,4	X
	STA	STORE1	X
	SEB		X
ARRAY1	CLA	**,2	X
	SEB		X
STORE1	STO	**,2	X
RETURN	LXA	STOIR,1	RETURN TO FORTRAN
	LXD	STOIR,2	X
	LDI	STOIND	X
	TRA	4,4	X
SMLARY	TXL	ONEWD,1,2	TEST FOR 1 OR 2 WORDS IN ARRAY
TWOADS	CAL*	3,4	TRANSFERRING TOTAL OF 2 WORDS, OR
	ARS	18	REMAINING 2 WORDS FROM A TO B CORE
	STA	ARRAY2	X
	SUB	ADDR1	X
	STA	ARRAY2+1	X
	CLA	1,4	X
	STA	STORE2	X
	SUB	ADDR1	X
	STA	SJOBZ+1	X
	SEB		X
ARRAY2	CLA	**,2	X
	LQ	**,2	X
	SEA		X
STORE2	STO	**,2	X
	STQ	**,2	X
	TRA	RETURN	X
ARRAY3	AXT	0,1	3 WORDS, ZERO I.R. 1
	TRA	RESET	X
ERROR	WTOA	3	
	RCHA	READ	
	TGOA	*	
	TRA	4,4	
READ	IDCD	WORDS,1,9	
	WORDS	BCI	9,1** SUBROUTINE BACK CANNOT BE EXECUTED FROM B CORE **
	ADDR1	OCT	1
STOIND	BSS	1	
STOIR	BSS	1	
	END		
	*	SUBROUTINE STASH	
	*	CARDS COLUMN	
	*	LIST8	
	*	FAP	
	COUNT	80	
	LBL	STASH,X	
	REM	SUBROUTINE STASH	
	REM	PROGRAM IN CORE A, MOVES AN ARRAY FROM CORE A TO	
	REM	DESIGNATED LOCATIONS CORE B.	
	ENTRY	STASH	
STASH	FT	STASH	TEST FOR A OR B CORE
	TRA	ERROR	ERROR - B CORE
	SXA	STOIR,1	STORE MACHINE CONDITIONS
	SXD	STOIR,2	X
	STI	STOIND	X
	AXT	0,2	ZERO I.R. 2
	CAL	1,4	FORTRAN ADDRESS BLOCK FROM
	STA	ARRAY	STORED FOR REFERENCE
	SUB	ADDR1	SETTING UP TRANSFER OF THREE WORDS
	STA	ARRAY+1	AT A TIME
	SUB	ADDR1	X
	STA	ARRAY+2	X
	CAL*	2,4	ARRAY LENGTH
	PDX	0,1	PLACED IN I.R. 1
	TXL	SMLARY,1,2	SMALL ARRAY, LENGTH EQUAL TO 1 OR 2
	CAL*	3,4	FORTRAN ADDRESS BLOCK TO
	ARS	18	SHIFT TO ADDRESS PORTION OF WORD
	STA	STORE	STORED FOR REFERENCE
	SUB	ADDR1	WILL BE STORING THREE WORDS AT A TIME
	STA	STORE+1	X
	SUB	ADDR1	X
	STA	STORE+2	X
ARRAY	CLA	**,2	TRANSFER OF WORDS
	LQ	**,2	X
	LDI	**,2	X
	SEB		X
STORE	STO	**,2	STORED
	STQ	**,2	X
	STI	**,2	X
	TXI	**1,2,3	MOVE DOWN THROUGH BLOCK
	SEA		X
	TXH	ARRAY,1,3	REDUCE BLOCK BY 3
	TXH	ARRAY3,1,2	IF 3 WORDS, SET I.R. 1 = 0
	TXH	TWOADS,1,1	TEST FOR REMAINING (1 OR 2) WORDS
	TXL	RETURN,1,0	X
ONEWD	CAL	1,4	TRANSFERRING TOTAL OF 1 WORD, OR
	STA	ARRAY1	REMAINING WORD FROM A TO B CORE
	CAL*	3,4	X
	ARS	18	X
	STA	STORE1	X
ARRAY1	CLA	**,2	X
	SEB		X
STORE1	STO	**,2	X
	RESET	SEA	X
	RETURN	LXA	STOIR,1
			RETURN TO FORTRAN

```

LXD STOR1+2 .....X
LDL STOR1D .....X
TRA 4,4 .....X
SMARY TXL ONEHD;L;J ..... TEST FOR 1 OR 2 WORDS IN ARRAY
TWODS CAL 1,4 ..... TRANSFERRING TOTAL OF 2 WORDS; DR
STA ARRAY2 ..... REMAINING 2 WORDS FROM A TO B CORE
SUB ADDR1 .....X
STA ARRAY2+1 .....X
CLA# 3,4 .....X
ARS 18 .....X
STA STOREZ .....X
SUB ADDR1 .....X
STA STORE2+1 .....X
ARRAY2 CLA ##;2 .....X
LDQ ##;2 .....X
SEB .....X
STOREZ STO ##;2 .....X
STQ ##;2 .....X
TRA RESET .....X
ARRAY3 AXT 0,1 ..... 3 WORDS; ZERO I,R, 1
TRA ARRAY .....X
ERROR WTD A 3
RCHR READ
TCOA *
TRA 4,4
READ JDCD .....WORDS;L;R
WORDS BCI 9,1+ SUBROUTINE STASH CANNOT BE EXECUTED FROM B CORE
ADDR1 OCT 1
STOIN BSS 1
STOIN BSS 1
END
* SUBROUTINE TIMC4
* CARDS COLUMN
* LISTB
* LABEL
C SUBROUTINE TIMC4(DJO,TSEP,S;F,DT)
C USES SUBROUTINE TIMEC AND GIVES OUTPUT ON
C TAPES A3 AND A8.
C
C VERSION OF 7/22/63
C
C READS A CARD FROM CARD READER CONTAINING CALENDAR DATE AND UT2 OF
C DESIRED START AND END TIMES FOR CALCULATION OF AN EPHEMERIS, AND
C THE TIME INCREMENT OF THE EPHEMERIS IN SECONDS. CALCULATES TIME
C INTERVAL IN SECONDS FROM SOME EPOCH (DJO,TSEP) TO THE START AND
C END TIMES.
C WRITES CALENDAR DATE AND UT2 ON TAPE UNIT A3.
C
C INPUT FROM CALLING SEQUENCE
C DJO = EPOCH JULIAN DATE AT 0 HOURS UT2.
C TSEP = EPOCH UT2 IN SECONDS
C
C INPUT FROM CARD READER
C NMS,NDS,NYS = MONTH, DAY, YEAR OF START DATE
C NMF,NDF,NYF = MONTH, DAY, AND YEAR OF END DATE
C
C NMS,NMNS,TSS = HOUR, MINUTE, SECOND (UT2) OF START TIME
C NMF,NMNF,TSF = HOUR, MINUTE, SECOND (UT2) OF END DATE
C DT = TIME INCREMENT OF EPHEMERIS IN SECONDS
C
C OUTPUT
C S = TIME IN SECONDS FROM EPOCH TO START TIME
C F = TIME IN SECONDS FROM EPOCH TO END TIME
C DT = TIME INCREMENT OF EPHEMERIS IN SECONDS
C
C REQUIRED SUBPROGRAMS
C
C DJUL, JULCAL 07/22/60 - FAP DOUBLE ENTRY PROGRAM
C
6015 FORMAT (2I1X12), 1X, I4, 2I3, F7.3, 13, 1X, I2, 1X, I4, 2I3, F7.3, F11.3 )
6016 FORMAT (1X12, 1H/12, 1H/14, 7X11H START DATE/1X12, 13, F7.3, 5X,
1 15H START TIME-UT2/1X12, 3, 5X23H TIME INCREMENT-SECONDS//1X12,
2 1H/12, 1H/14, 7X9H END DATE/1X12, 13, F7.3, 5X13H END TIME-UT2 )
READ 6015, NMS, NDS, NYS, NMS, NMNS, TSS, NMF, NDF, NYF, NMF
1 NMF, TSF, DT
WRITE OUTPUT TAPE 3, 6016, NMS, NDS, NYS, NMS, NMNS, TSS, DT, NMF, NDF, NYF,
1 NMF, NMNF, TSF
WRITE OUTPUT TAPE 8, 6016, NMS, NDS, NYS, NMS, NMNS, TSS, DT, NMF, NDF, NYF,
1 NMF, NMNF, TSF
PRINT 6016, NMS, NDS, NYS, NMS, NMNS, TSS, DT, NMF, NDF, NYF, NMF, NMNF, TSF
IF ISENSE SWITCH 0) 1+2
1 PRINT 6016, NMS, NDS, NYS, NMS, NMNS, TSS, DT, NMF, NDF, NYF, NMF, NMNF, TSF
2 DJSO=DJUL(NMS,NDS,NYS)
DJFO=DJUL(NMF,NDF,NYF)
THS=NMS*3600
TMNS=NMNS*60
TS=THS+TMNS+TSS-TSEP
THF=NMF*3600
TMNF=NMNF*60
TF=THF+TMNF+TSF-TSEP
DJS=DJSO-DJO
DJF=DJFO-DJO
S=DJS+86400.*TS
F=DJF+86400.*TF

```

```

RETURN
END
SUBROUTINE SUN
  CARDS COLUMN
  LISTB
  LABEL
  SUBROUTINE SUN(DJ,ET,CL)

```

```

THEORY AND ANALYSIS OFFICE - GSEC
ONLY COMPUTES LONGITUDE IN RADIANs - ECLIPTIC
VERSION OF 9/15/64

```

```

WOOLARD'S ABBREVIATED VERSION OF NEWCOMB'S THEORY OF THE SUN.

```

```

INPUT
  DJ = JULIAN DATE AT 0 HOUR'S EPHEMERIS TIME.
  ET = EPHEMERIS TIME IN RADIANs [24 HOURS = 2 PI RADIANs].
  ET IS RESTRICTED TO LIE BETWEEN 0 AND +2 PI RADIANs.

```

```

OUTPUT
  GEOMETRIC COORDINATES OF THE SUN, TRUE EQUINOX
  AND ECLIPTIC OF DATE.
  CL = LONGITUDE IN RADIANs.

```

```

REFERENCES
  ASTRONOMICAL PAPERS PREPARED FOR THE USE OF THE AMERICAN
  EPHEMERIS AND NAUTICAL ALMANAC. VOLUME 15, PART 1 (THEORY
  OF THE ROTATION OF THE EARTH AROUND ITS CENTER OF MASS -
  BY EDGAR N. WOOLARD - PAGES 53, 64 - 66 ).

```

```

RESTRICTIONS
  WOOLARD HAS USED NEWCOMB'S THEORY OF THE SUN, NEGLECTING
  ALL PERIODIC TERMS WITH COEFFICIENTS GREATER THAN .001
  SECONDS OF ARC IN LONGITUDE AND LATITUDE, AND GREATER
  THAN 7 UNITS IN THE 8TH DECIMAL OF THE LOGARITHM
  OF THE RADIUS VECTOR.

```

```

COMPUTE TIME IN JULIAN CENTURIES ELAPSED SINCE 1900 JAN. 0.5 ET

```

```

DIMENSION S(35),C(35),C(123),E(23),S(28),H(28),C(41),G(45)
PRT1=DJ-2419020.0
PRT2=ET/6.28318531
T=PRT1+PRT2/36525.0
T2=T*T
T3=T2*T

```

```

COMPUTE FUNDAMENTAL ARGUMENTS

```

```

MEAN LONGITUDE - SUN
  X = 3.5284469 E-5 *T2
  CL1 = 4.881627934112 + 628.331950990909*T + X

```

```

MEAN ANOMALY - VENUS
  X = 0.22446873 E-4 *T2
  G1 = 3.710626228126 + 1021.328348655046*T + X

```

```

MEAN ANOMALY - EARTH
  X = 0.2617994 E-5 *T2 + 0.58178 E-7 *T3
  G2 = 6.256583580497 + 628.301945726741*T - X

```

```

MEAN ANOMALY - MARS
  X = 0.3156137 E-5 *T2
  G3 = 5.57684377809 + 334.053549190822*T + X

```

```

MEAN ANOMALY - JUPITER
  G4 = 3.932889060231 + 52.965367620264*T

```

```

MEAN ANOMALY - SATURN
  G5 = 3.062637351924 + 21.320095075899*T

```

```

MEAN ANOMALY - MOON
  X = 0.163424846 E-3 *T2 + 0.251133 E-6 *T3
  SL = 5.158000345744 + 8328.691103668024*T + X

```

```

MEAN ANOMALY - SUN
  X = 0.2617994 E-5 *T2 + 0.58178 E-7 *T3
  SL1 = 6.256583590497 + 628.301945726741*T - X

```

```

MEAN ARGUMENT OF LATITUDE - MOON
  X = 0.56344461E-4*T2 + 0.5818E-8*T3
  F = 0.196365054887 + 8433.466291171947*T - X

```

```

MEAN ELONGATION OF MOON FROM SUN
  X = 0.32967E-7*T3 - 0.25064867E-4*T2

```

```

D. D = 6.121523942807 ± 777L377193934895 *T+X
C
C LONGITUDE OF MEAN ASCENDING NODE - PDDN
C
C X = 0.36284063E-4+T2 + 0.38785E-7+T3
C W = 4.523601514852 - 33.757146246651T + X
C
C REDUCE ALL ANGLES BY MODULUS 2 PI
C
C
C CL1 = MODF (CL1,6.283185307179586)
D G1 = MODF (G1,6.283185307179586)
D G3 = MODF (G3,6.283185307179586)
D G4 = MODF (G4,6.283185307179586)
D G5 = MODF (G5,6.283185307179586)
D SL = MODF (SL,6.283185307179586)
D SL1 = MODF (SL1,6.283185307179586)
D D = MODF (D,6.283185307179586)
D F = MODF (F,6.283185307179586)
D W = MODF (W,6.283185307179586)
C
C COMPUTE EXCEPTIONAL ARGUMENTS
C
1400 EA1 = 8.0*S11-15.0*G3
EA2 = 3.0*G4-3.0*G3+4.0*S11
EA3 = .785398163327446E-1+T-R*0*G1+13.0*S11
EA4 = 7.0*S11-(3.0*G1+4.0*G3)
EA5 = (F+W)+(F+W)
EA6 = EA5-(D*2)
C COMPUTE SINES AND/OR COSINES OF 16 ARGUMENTS
1500 S11 = SINP(SL1)
CS11 = COSP(SL1)
S1L = SINP(SL)
CSL = COSP(SL)
S01 = SINE(G1)
C01 = COSP(G1)
S03 = SINP(G3)
C03 = COSP(G3)
S04 = SINP(G4)
C04 = COSP(G4)
S05 = SINP(G5)
C05 = COSP(G5)
SF = SINP(F)
SD = SINP(D)
CD = COSP(D)
SW = SINP(W)
CW = COSP(W)
C28 = COSP(EA1)
S49 = SINP(EA2)
C49 = COSP(EA2)
S51 = SINP(EA3)
C51 = COSP(EA3)
S52 = COSP(EA4)
S46 = SINP(EA5)
S47 = SINP(EA6)
S44A = S1L*CD
S44B = CSL*SD
S44 = S44A+S44B
S45 = S44A-S44B
C45A = CSL*CD
C45B = S1L*SD
C45 = C45A+C45B
C75 = C45A-C45B
C76 = C45A*(4.0*CD+CD-3.0)+C45B*(3.0-4.0*SD*SD)
C EVALUATE ALL OTHER SINES AND COSINES IN TERMS OF ABOVE
X = 2.0*CS11
S01 = X *S11
C01 = X *CS11-1.0
X = 2.0*C01
S02 = (X +1.0)*S11
C02 = (X -1.0)*CS11
S03 = 2.0*S01*C01
S04 = S11*(C01-CS11)+S01
C04 = CS11*(C01+S11)+S01
S05 = S04 *C01-C04 *S01
C05 = C04 *C01+S04 *S01
X = 2.0*C04
S06 = X *S04
C06 = X *C04-1.0
S07 = S11*(C06+CS11)+S06
C07 = CS11*(C06-S11)+S06
X = 2.0*C06
S08 = (X +1.0)*S04
C08 = (X -1.0)*C04
S09 = S11*(C08+CS11)+S08
C09 = CS11*(C08-S11)+S08
S10 = S61*(C09+CS11)+S09
C10 = CS11*(C09-S11)+S09
X = 2.0*C08
S11 = X *S06
C11 = X *C06-1.0
S12 = S11*(C11+CS11)+S11
S13 = S01 *(C11+C01)+S11
C13 = C01 *C11-S01 *S11

```

```

S14 =S11 *CG4+C11 *S04.
C14 =C11 *CG4-C11 *S04.
S15 =S01 *C14+C01 *S14
C16 =CG2 *C14-S02 *S14
C17 =CG4 *C14-S04 *S14
S18 =SS11*CG3-C20*S02
C18 =C011*CG3+SS11*S03
S19 =S18 *CG3-C18 *SG3
C19 =C18 *CG3+S18 *SG3
X =2.0*C18
S20 =X *S18
C20 =X *C18-1.0
S21 =S20*CG3-C20*S03
C21 =CG29*CG3-C20*S02
C22 =C18*C20-S18*S20
S23 =S21*CG3-C21*S03
C23 =C21*CG3+S21*S03
S24 =SS11*CG3-C21*S03
C24 =C011*CG3-SS11*S23
S25 =S24 *CG3-C24 *SG3
C25 =C24 *CG3+S24 *SG3
C26 =C011*CG3-SS11*S25
S27 =S18*CG3+C18*S25
C27 =C18*C25-S18*S25
S29 =SS11*CG4-C511*S04
C29 =C511*CG4+SS11*S04
S30 =SS11*CG9-C511*S29
C30 =C511*CG9-SS11*S29
S31 =S29 *CG4-C29 *S04
C31 =CG9 *CG4+S29 *S04
X =2.0 *C29
S32 =X *S29
C32 =X *C29-1.0
C33 =C011*CG3-SS11*S32
S34 =S31 *CG4-C31 *S04
C34 =C31 *CG4+S31 *S04
S35 =S32 *CG4-C32 *S04
C35 =C32 *CG4+S32 *S04
S36 =S29 *CG3-C29 *S32
C36 =C29 *CG3-S29 *S32
C37 =C35 *CG4+S35 *S04
S38 =S35 *CG4-C36 *S04
C39 =C511*CG4-SS11*S04
S40 =SS11*CG5-C511*S05
C40 =C511*CG5+SS11*S05
C41 =C40 *CG5+S40 *SG5
X =2.0 *C40
C42 =X *C40-1.0
S43 =SS11*CG -C511*S0
C77A =C511*CG
C77B =S511*S0
C77 =C77A-C77B
C78 =C77A+C77B
X =C511*CG9
Y =SS11*S49
C48 =X +Y
C50 =X -Y

```

C COMPUTE LOG11JDE OF SUN (HEAN LUNG. + TABLE 8) 4000LD 2P1

```

1800 C11 J=S511*(+33502.E-6)
C12 J=S01 *(+ 351.E-6)
C13 J=S02 *(+ 5.E-6)
C14 J=S49 *(+ 25.E-6)
C15 J=S04 *(+ 20.E-6)
C16 J=S05 *(+ 14.E-6)
C17 J=S07 *(+ 9.E-6)
C18 J=S09 *(+ 2.E-6)
C19 J=S12 *(+ 3.E-6)
C110)=S51 *(+ 7.E-6)
C111)=S19 *(+ 1.E-6)
C112)=S23 *(+ 3.E-6)
C113)=S19 *(+ 3.E-6)
C114)=S21 *(+ 1.E-6)
C115)=S24 *(+ 2.E-6)
C116)=S23 *(+ 1.E-6)
C117)=S29 *(+ 1.E-6)
C118)=S04 *(+ 13.E-6)
C119)=S32 *(+ 13.E-6)
C120)=S31 *(+ 7.E-6)
C121)=S35 *(+ 3.E-6)
C122)=S34 *(+ 1.E-6)
C123)=S40 *(+ 2.E-6)
C124)=S05 *(+ 2.E-6)
C125)=SS11*(+ 8358.E-8)*T
C126)=S01 *(+ 175.E-8)*T
C127)=SS11*(+ 29.E-8)*T*T
C128)=S0 *(+ 31.E-6)
C129)=S44 *(+ 1.E-6)
C130)=S45 *(+ 2.E-6)
C131)=S43 *(+ 1.E-6)
C132)=S0 *(+ 84.E-6)
C133)=S03 *(+ 1.E-6)
C134)=S47 *(+ 6.E-6)
C135)=S45 *(+ 1.E-6)
1900 C11 J=C04 *(+ 11.E-6)

```

```

E(2 )=C06 *(- 23.E-6)
E(3 )=C07 *(+ 9.E-6)
E(4 )=C08 *(- 3.E-6)
E(5 )=C09 *(+ 7.L-6)
E(6 )=C10 *(+ 4.E-6)
E(7 )=C11 *(- 1.E-6)
E(8 )=C13 *(+ 1.E-6)
E(9 )=C15 *(+ 1.E-6)
E(10)=C51 *(+ 6.E-6)
E(11)=C49 *(+ 18.E-6)
E(12)=C18 *(- 1.E-6)
E(13)=C20 *(+ 10.E-6)
E(14)=C13 *(- 8.E-6)
E(15)=C21 *(+ 2.E-6)
E(16)=C23 *(+ 3.E-6)
E(17)=C28 *(+ 1.E-6)
E(18)=C30 *(- 1.E-6)
E(19)=C29 *(- 35.E-6)
E(20)=C04 *(- 1.E-6)
E(21)=C31 *(- 3.E-6)
E(22)=C36 *(- 1.E-6)
E(23)=C52 *(- 1.E-6)
T8S = C(1)
DO 1930 J=2,35
1930 T8S = T8S+C(J)
      T8C = E(1)
1940 T8C = T8C+E(J)
      T488 = T8S + T8C
1950 CL =M00F(T488*CL1, 6.283185307179586)
9000 RETURN
      END
      * SUBROUTINE ARKTAN
      * CARDS COLUMN
      * LIST8
      * LABEL
      * SUBROUTINE ARKTAN(Y,X,Z,N)
      * IF (X) 6,5,6
      * 5 IF (Y) 7,8,9
      * 7 IF (N) 10,11,10
      * 11 Z = -90.
      * GO TO 502
      * 10 Z = -1.5707964
      * GO TO 502
      * 8 Z = 0.
      * GO TO 502
      * 9 IF (Y) 12,13,12
      * 13 Z = 90.
      * GO TO 502
      * 12 Z = 1.5707964
      * GO TO 502
      * 6 IF (Y) 15,15,14
      * 15 IF (X) 15,17,17
      * 16 IF (N) 18,19,18
      * 19 Z = 180.
      * GO TO 502
      * 18 Z = 3.1415927
      * GO TO 502
      * 17 Z = 0.
      * GO TO 502
      * 14 IF ACCUMULATOR OVERFLOW 30,30
      * 30 IF JOTIEVF JVERFLOW 31,31
      * 31 IF DIVIDE CHECK 32,32
      * 32 A = ARSF (Y)
      * B = ARSF (X)
      * Z = A/B
      * IF DIVIDE CHECK 33,34
      * 33 Z = 0.
      * GO TO 502
      * 34 Z = ATANF(Z)
      * IF (Y) 50,51,51
      * 50 IF (X) 52,53,53
      * 52 Z = Z-3.1415927
      * GO TO 502
      * 53 Z = -Z
      * GO TO 600
      * 51 IF (X) 54,600,600.
      * 54 Z = 3.1415927-Z
      * GO TO 600
      * 600 IF (N) 500,55,500
      * 55 Z = (180./3.1415927)*Z
      * 500 RETURN
      * END
      * SUBROUTINE TESCOV CONVERTS 3 DIGIT INTEGER INTO BCD FORM
      * CARDS COLUMN
      * LIST8
      * FAP
      * COUNT 20
      * LBL TESCOV,X
      * ENTRY TESCOV
      * TESCOV CLA= 1,4
      * RCYDEC ARS= 18
      * ANA, IBADR
      * LDQ BLNKS

```

ALLOT001
ALLOT002

```

VDP      RCVDI+6
VDP      BCVDI+1,6
VDP      BCVDI+3,6
VDP      BCVDI+3,6
VDP      BCVDI+3,6
VDP      BCVDI+3,6
RQL      18
STQ*     2,4
TRA      3,4
BCVDI DEC -840000,-6096000,-26214400,-167772160,-1073741824
ISADR DCT 00000007777
BLNKS BCL 1
END
* SUBROUTINE CH65K      TESTS FOR 65K.
* CARDS COLUMNS
* LISTB
* FAP
COUNT 20
LBL CH65K
ENTRY CH65K
CH65K SEB
EFT
TRA ***
XN32K CLA B32
STQ* 1,4
TRA 2,4
SEA
EFT
TRA XN32K
STQ* 1,4
TRA 2,4
B32 DCT 00000400000

```

```

-----
_FORTRAN CALLING SEQUENCE =
CALL CH65K(N)

```

```

MACHINE IS IN 32K -- N

```

```

MACHINE IS IN 65K -- N = 0

```

APPENDIX VIII (PART A)
SAMPLE INPUT
FOR MAIN PROGRAM ONE

RELAY 2 12 STATION TEST

+04+01+01-01 +4 5000.
 33333 640114 2157 00000 00000
 +17470063+01+23653052+00+81153895+00+62823296+01+32527117+01+38506655+01 TEST
 33333 640114 2157 00000 +00000000+00
 01/15/1964 20 00 00,000 01/16/1964 20 00 00,000 +120.
 +12+00+00
 90.0 0.0 178. 25.
 C8MNUIT -75 00 0.000 +40 00 0.000 0.0
 C8MAND -068 40 00.000 +44 54 00.000 38.
 C8MHIL -05 10 29.0 +50 02 58.0 350.0
 C8MGER +10 00 00.000 +51 00 00.000 50.
 C8MTEL +13 36 5.000 +41 58 41.000 2168.6
 C8MRI8 -43 22 7.000 -22 57 9.000 0.0
 C8MNUIT -75 00 0.000 +40 00 0.000 0.0
 C8MAND -068 40 00.000 +44 54 00.000 38.
 C8MHIL -05 10 29.0 +50 02 58.0 350.0
 C8MNUIT -75 00 0.000 +40 00 0.000 0.0
 C8MAND -068 40 00.000 +44 54 00.000 38.
 C8MHIL -05 10 29.0 +50 02 58.0 350.0

APPENDIX VIII (PART B)
MAIN PROGRAM ONE OUTPUT

BAR GRAPHS
TAPE A3

RELAY 2 12 STATION TEST

RELAY 2 12 STATION TEST

5.0799999E 03 FEET PER NAUTICAL MILE

5376.388 EQUATORIAL RADIUS OF EARTH IN KM
297.0 INVERSE OF FLATTENING
3.98626870E 05 GM (KM. CUBED/SECONDS SQUARED)

HARMONICS OF EARTHS GRAVITATIONAL POTENTIAL

1.082190E-03 J2
-2.285000E-06 J3
-2.123000E-06 J4
-2.320000E-07 J5

EPOCH 54 1 14 21 57 .00

A E I M OMEGA THETA
1.7470063E 00 2.3693052E-01 8.1153895E-01 6.2823295E 00 3.2527117E 00 3.8505655E 00

DRAG EFFECTS T (P,0) N (2,0) N (3,0)
64 114 2157 0 0.

LOOK ANGLE CALCULATIONS - START AND END TIMES

1/15/1964 START DATE
20 0 0. START TIME-UT2
120.000 TIME INCREMENT-SECONDS

1/16/1964 END DATE
20 0 0. END TIME-UT2

LOCAL STATION PREDICTIONS FOR --

STATION	LONGITUDE	LATITUDE	HEIGHT (METERS)
COMNUT	-75 0 0.	40 0 0.	0.
COMAND	-68 40 0.	44 54 0.	38.00
COMHIL	-5 10 29.000	50 2 58.000	350.00
COMGER	10 0 0.	51 0 0.	50.00
COMTEL	13 36 54.000	41 58 41.000	2168.50
COMRIO	-43 22 7.000	-22 57 9.000	0.
COMNUT	-75 0 0.	40 0 0.	0.
COMAND	-68 40 0.	44 54 0.	38.00
COMHIL	-5 10 29.000	50 2 58.000	350.00
COMNUT	-75 0 0.	40 0 0.	0.
COMAND	-68 40 0.	44 54 0.	38.00
COMHIL	-5 10 29.000	50 2 58.000	350.00

CONTROL STATIONS ARE

COMNUT
COMAND
COMHIL
COMGER

NO STATION PRINT OUT IF --

ELEVATION IS LESS THAN 0 DEGREES

5 IS PRINTED IF THE ELEVATION IS GREATER THAN OR EQUAL TO 0 AND LESS THAN 5 DEGREES
9 IS PRINTED IF THE ELEVATION IS GREATER THAN OR EQUAL TO 5 AND LESS THAN 10 DEGREES
A IS PRINTED IF THE ELEVATION IS GREATER THAN OR EQUAL TO 10 DEGREES

A T IS PRINTED OF RANGE IS GREATER THAN 0.50300000E 00NAUTICAL MILES

SPIN AXIS COORDINATES ARE
178.0 DEGREES RIGHT ASCENSION
25.0 DEGREES DECLINATION

THE 3 DIGIT NUMBERS UNDER THE STATION NAMES ARE THE SPACECRAFT LOOK ANGLES.

ORBIT NUMBER 0

MUTUAL VISIBILITY OF 33333 FOR THE FOLLOWING STATIONS

DATE(EHH/00/YY) = 1/15/64

HHMM	NUT	AND	HIL	GER	TEL	RIO	NUT	AND	HIL	NUT	AND	HIL
20 0	068	A	072	A			068	A	072	A		
20 2	071	A	075	A			071	A	075	A		
20 4	075	A	079	A			075	A	079	A		
20 6	078	A	083	A			078	A	083	A		
20 8	083	A	087	A			083	A	087	A		
20 10	088	A	093	A			088	A	093	A		
20 12	094	A	099	A			094	A	099	A		
20 14	101	A	106	A	114	5	101	A	106	A	114	5
20 16	108	A	114	A	119	5	108	A	114	A	119	5
20 18	116	A	123	A	124	5	116	A	123	A	124	5
20 20	123	A	132	A	131	5	123	A	132	A	131	5
20 22	128	A	139	A	137	5	128	A	139	A	137	5
20 24	131	A	142	A	144	5	131	A	142	A	144	5
20 26	132	A	143	A	152	5	132	A	143	A	152	5
20 28	131	A	141	A	160	5	131	A	141	A	160	5
20 30	128	A	137	A	168	5	128	A	137	A	168	5
20 32	126	9	133	9	177	5	126	9	133	9	177	5
20 34			129	5			087	5	126	9	133	9
20 36							088	9				
20 38							088	A				
20 40							087	A				
20 42							086	A				
20 44							083	A				
20 46							081	A				
20 48							078	A				
20 50							075	9				
20 52							072	5				
20 54							070	5				

TAPE A8
WORLD MAP
LOCAL STATION PREDICTIONS
SUN LIGHT HISTORY

RELAY 2 12 STATION TEST

5.07999998E 03 FEET PER NAUTICAL MI.±

5378.388 EQUATORIAL RADIUS OF EARTH IN KM
297.0 INVERSE OF FLATTENING
3.98626876E 05 GM (KM. CUBED/SECONDS SQUARED)

HARMONICS OF EARTHS GRAVITATIONAL POTENTIAL

1.082190E-03 J2
-2.285000E-06 J3
-2.123000E-06 J4
-2.320000E-07 J5

EPOCH 64 1 14 21 57 0.

A E I H OMEGA THETA
1.7470063E 00 2.3653052E-01 8.1193895E-01 6.2823296E 00 3.2527117E 00 3.8506655E 00

DRAG EFFECTS I (P.0) N (2.0) N (3.0)
64 114 2157 0 0.

LOOK ANGLE CALCULATIONS - START AND END TIMES

1/15/1964 START DATE
20 0 0. START TIME-UT2
120.000 TIME INCREMENT-SECONDS

1/16/1964 END DATE
20 0 0. END TIME-UT2

CONTROL STATIONS ARE
COMNUT
COMAND
COMHIL
COMGER

S IS PRINTED WHEN THE SATELLITE IS IN THE SUNLIGHT

ORBIT NUMBER 0									
LOCAL STATION PREDICTIONS AND SATELLITE WORLD MAP FOR 33333									
YKMD	HMM	STAT.	RANGE (KM)	AZI.	ELEV.	S/C LOOK -----DEGREES-----	LAT.	LONG.	HEIGHT (KM)
64	115	20	0	CONNUT	6619.0	295.1	29.8	68.9	46.0 -116.7 4853.8 S
				COMAND	6854.6	289.3	26.2	72.9	
				CONNUT	6619.0	295.1	29.8	68.9	
				COMAND	6854.6	289.3	26.2	72.9	
				CONNUT	6619.0	295.1	29.8	68.9	
				COMAND	6854.6	289.3	26.2	72.9	
64	115	20	2	CONNUT	6166.2	295.8	33.9	71.9	46.4 -112.1 4594.3 S
				COMAND	6402.8	288.6	30.1	76.0	
				CONNUT	6166.2	295.8	33.9	71.9	
				COMAND	6402.8	288.6	30.1	76.0	
				CONNUT	6166.2	295.8	33.9	71.9	
				COMAND	6402.8	288.6	30.1	76.0	
64	115	20	4	CONNUT	5715.0	296.5	38.6	75.2	46.5 -107.2 4522.5 S
				COMAND	5941.3	287.5	34.4	79.5	
				CONNUT	5715.0	296.5	38.6	75.2	
				COMAND	5941.3	287.5	34.4	79.5	
				CONNUT	5715.0	296.5	38.6	75.2	
				COMAND	5941.3	287.5	34.4	79.5	
64	115	20	6	CONNUT	5270.4	297.3	43.9	79.0	46.5 -102.2 4348.9 S
				COMAND	5484.4	286.0	39.3	83.4	
				CONNUT	5270.4	297.3	43.9	79.0	
				COMAND	5484.4	286.0	39.3	83.4	
				CONNUT	5270.4	297.3	43.9	79.0	
				COMAND	5484.4	286.0	39.3	83.4	
64	115	20	8	CONNUT	4839.1	298.4	50.0	83.4	46.2 -97.0 4174.3 S
				COMAND	5038.4	283.9	44.8	88.0	
				CONNUT	4839.1	298.4	50.0	83.4	
				COMAND	5038.4	283.9	44.8	88.0	
				CONNUT	4839.1	298.4	50.0	83.4	
				COMAND	5038.4	283.9	44.8	88.0	
64	115	20	10	CONNUT	4430.5	299.8	57.0	88.4	45.6 -91.7 3999.5 S
				COMAND	4611.7	280.5	51.1	93.3	

SUNLIGHT HISTORY OF 33333

SATELLITE WILL BE IN SUNLIGHT AT ALL TIMES EXCEPT WHEN IT WILL
ENTER SHADOW AT AND LEAVE SHADOW AT

YKMD HMM YKMD HMM DURATION (MIN) PERCENT IN SUNLIGHT

NO OUTPUT INDICATES THAT SPACECRAFT IS IN SUNLIGHT 100% OF TIME

APPENDIX VIII

PART C

OUTPUT OF MAIN PROGRAM TWO

TAPE A3
WORLD MAP AND BAR GRAPHS

SANDTRACKS, ORBITAL COMPUTING SYSTEM

DELAY TEST 12 STATIONS

```

10.0E-09      TOLERANCE REQUIRED FOR KEPLER SUBROUTINE
6378.388      EQUATORIAL RADIUS OF EARTH IN KM
297.0        INVERSE OF FLATTENING
3.98626876E 05 GM (KM. CUBED/SECONDS SQUARED)

             HARMONICS OF EARTHS GRAVITATIONAL POTENTIAL
1.082190E-03 J2
-2.285000E-06 J3
-2.123000E-06 J4
-2.320000E-07 J5

2.20138180E 04 BRUWER HARMONICS COMPUTED FROM J2, J3, J4, AND J5
5.92951238E 05 K2 (KILOMETERS SQUARED)
1.31772552E 09 K3 (KILOMETERS CUBED)
2.44950354E 12 K4 (KILOMETERS FOURTH POWER)
                K5 (KILOMETERS FIFTH POWER)

1/14/1964     EPOCH DATE OF PARAMETERS
21 57 -0.    EPOCH TIME OF PARAMETERS-UT2
                INPUT OPTION NUMBER
                INPUT PARAMETERS ARE---

BRUWER MEAN ELEMENTS
REQUIRED UNITS - ALL ANGLES IN DEGREES, SEMI-MAJOR AXIS IN KILOMETERS
11143.3840    SEMI-MAJOR AXIS-KILOMETERS
0.23653051    ECCENTRICITY
46.497756     INCLINATION -DEGREES
220.526879    RA. ASC. NODE -DEGREES
166.386648    ARC. OF PERIGEE-DEGREES
359.950966    MEAN ANOMALY -DEGREES

WORLD MAP CALCULATIONS - START AND END TIMES
1/15/1964     START DATE
20 0 0.       START TIME-LT2
120.000       TIME INCREMENT-SECONDS

1/16/1964     END DATE
20 0 0.       END TIME-UT2

LECK ANGLE CALCULATIONS - START AND END TIMES
1/15/1964     START DATE
10 0 0.       START TIME-LT2
120.000       TIME INCREMENT-SECONDS

1/16/1964     END DATE
10 0 0.       END TIME-UT2

```

SANDTRACKS ORBITAL COMPUTING SYSTEM

RELAY TEST 12 STATIONS

QUANTITIES COMPUTED FROM INPUT

1/14/1964	EPOCH DATE OF PARAMETERS	---
21 57 -0.	EPOCH TIME OF PARAMETERS	UT2
POSITION AND VELOCITY VECTORS - GEOCENTRIC EQUATORIAL INERTIAL		
5986.52051	X1 - KILOMETERS	0.94013103 X1 - VANGUARD UNITS
5986.32159	X2 - KILOMETERS	0.94009985 X2 - VANGUARD UNITS
-682.69296	X3 - KILOMETERS	-0.10703221 X3 - VANGUARD UNITS
-4.02792885	VX1 - KM/SEC	-0.50951149 VX1 - VANGUARD UNITS
3.40607376	VX2 - KM/SEC	-0.43085013 VX2 - VANGUARD UNITS
-5.48964036	VX3 - KM/SEC	-0.69441018 VX3 - VANGUARD UNITS
8507.65540	R - KILOMETERS	1.33382532 R - VANGUARD UNITS
7.61325824	V - KM/SEC	0.96303649 V - VANGUARD UNITS

TRUNCATION FACTORS USED IN COMPUTING BROWNER
MEAN ELEMENTS FROM OSCILLATING ELEMENTS

5.0E-04	SEMI-MAJOR AXIS - KILOMETERS
5.0E-06	ECCENTRICITY
5.0E-06	INCLINATION - DEGREES
5.0E-06	R.A. ASC. NODE - DEGREES
5.0E-06	ARC. OF PERIGEE - DEGREES
5.0E-06	MEAN ANOMALY - DEGREES

CRITICAL ELEMENTS

OSCILLATING ELEMENTS BROWNER MEAN ELEMENTS

11150.8829	11143.0640	SEMI-MAJOR AXIS - KILOMETERS
0.23704214	0.23653051	ECCENTRICITY
46.509814	46.497756	INCLINATION - DEGREES
220.619161	220.626875	R.A. ASC. NODE - DEGREES
186.266777	186.366640	ARC. OF PERIGEE - DEGREES
0.050050	359.950958	MEAN ANOMALY - DEGREES
3.251240	PERIOD	-HOURS
155.0744		-MINUTES
110.726969	MEAN MOTION	-DEGREES/HOUR
-1.042296	MOTION OF NODE	- DEGREES/DAY
1.085400	MOTION OF PERIGEE	- DEGREES/DAY
		WORLD MAP

DATE MO/DY/YR	UNIVERSAL TIME		GEODEIC COORDINATES		
	H	M SEC.	LATITUDE-DMS	LONGITUDE-DMS	HEIGHT-KM.
1/15/64	20	0 C.CCC	45 58 3.44	-116 41 9.76	4863.764
1/15/64	20	1 C.CCC	46 23 44.15	-112 3 20.31	4694.303
1/15/64	20	4 0.CCC	46 35 36.75	-107 12 31.30	4522.467
1/15/64	20	6 C.CCC	46 32 5.89	-102 10 21.52	4348.900
1/15/64	20	8 C.CCC	46 11 43.08	-76 59 43.31	4174.323
1/15/64	20	10 C.CCC	45 33 11.46	-91 43 48.92	3999.537
1/15/64	20	12 0.CCC	44 35 30.19	-96 26 5.46	3825.429
1/15/64	20	14 C.CCC	43 17 57.62	-81 9 58.17	3652.979
1/15/64	20	16 0.CCC	41 40 12.74	-75 58 33.43	3483.259
1/15/64	20	18 C.CCC	39 62 15.16	-70 54 25.40	3317.437
1/15/64	20	20 C.CCC	37 24 23.77	-65 59 27.44	3156.770
1/15/64	20	22 0.CCC	34 47 14.74	-61 14 49.10	3002.603
1/15/64	20	24 C.CCC	31 51 39.51	-56 40 58.13	2856.350
1/15/64	20	26 0.CCC	28 38 43.12	-52 17 45.57	2719.480
1/15/64	20	28 C.CCC	25 9 43.10	-48 4 32.26	2593.492
1/15/64	20	30 C.CCC	21 26 9.20	-44 0 15.90	2479.878
1/15/64	20	32 C.CCC	17 25 43.00	-40 3 35.58	2380.086
1/15/64	20	34 0.CCC	13 22 18.25	-36 13 2.11	2295.473
1/15/64	20	36 C.CCC	9 6 0.61	-32 26 51.37	2227.256
1/15/64	20	38 0.CCC	4 43 7.11	-28 43 16.92	2176.462
1/15/64	20	40 C.CCC	0 16 5.05	-25 0 26.26	2143.803
1/15/64	20	42 0.CCC	-4 12 30.38	-21 16 23.33	2130.034
1/15/64	20	44 0.CCC	-8 39 57.52	-17 29 9.25	2135.135
1/15/64	20	46 0.CCC	-13 3 31.88	-13 36 42.88	2159.090
1/15/64	20	48 C.CCC	-17 25 28.68	-9 37 2.52	2201.505
1/15/64	20	50 C.CCC	-21 28 5.68	-5 28 0.20	2261.690
1/15/64	20	52 0.CCC	-25 23 45.58	-1 8 5.78	2338.718
1/15/64	20	54 C.CCC	-29 4 58.28	3 24 47.24	2431.448
1/15/64	20	56 0.CCC	-32 29 23.01	6 11 52.97	2536.579
1/15/64	20	58 0.CCC	-35 34 56.78	13 14 2.16	2658.705
1/15/64	21	0 C.CCC	-38 19 27.46	18 31 21.17	2790.355
1/15/64	21	2 0.CCC	-40 41 37.96	24 2 59.79	2932.042
1/15/64	21	4 C.CCC	-42 46 11.25	29 46 56.24	3082.288
1/15/64	21	6 C.CCC	-44 14 25.80	35 40 4.06	3239.665

1/15/64	21 8	0.000	-45 24 14.38	41 38 0.97	3402.803
1/15/64	21 10	0.000	-46 10 6.21	47 36 18.24	3570.416
1/15/64	21 12	0.000	-46 33 7.64	53 29 18.83	3741.303
1/15/64	21 14	0.000	-46 34 54.49	59 12 19.32	3914.355
1/15/64	21 16	0.000	-46 17 27.11	64 41 12.54	4088.586
1/15/64	21 18	0.000	-45 52 35.28	69 52 53.88	4262.983
1/15/64	21 20	0.000	-44 53 45.54	74 45 26.98	4436.798
1/15/64	21 22	0.000	-43 52 12.25	79 17 58.76	4609.247
1/15/64	21 24	0.000	-42 40 12.84	83 30 28.57	4779.653
1/15/64	21 26	0.000	-41 19 58.53	87 23 34.53	4947.410
1/15/64	21 28	0.000	-39 52 23.97	90 58 20.69	5111.977
1/15/64	21 30	0.000	-38 19 36.97	94 16 6.06	5272.871
1/15/64	21 32	0.000	-36 42 33.88	97 18 16.56	5429.663
1/15/64	21 34	0.000	-35 2 13.38	100 6 18.94	5581.974
1/15/64	21 36	0.000	-33 19 23.70	102 41 37.30	5729.465

LOCAL STATION PREDICTIONS FOR

STATION	LONGITUDE	LATITUDE	HEIGHT (METERS)
COMNUT	-75 0 0	40 0 0	0
COMANC	-68 40 0	44 54 0	350.00
COMHIL	-5 10 25.000	50 2 58.000	350.00
COMGEF	10 0 0	51 0 0	50.00
COMTEL	13 26 5.000	41 56 41.000	2168.60
COMRKC	-43 22 7.000	-22 57 5.000	0
COMNUT	-75 0 0	40 0 0	0
COMANC	-68 40 0	44 54 0	350.00
COMHIL	-5 10 25.000	50 2 58.000	350.00
COMNUT	-75 0 0	40 0 0	0
COMANC	-68 40 0	44 54 0	350.00
COMHIL	-5 10 25.000	50 2 58.000	350.00

NO STATION PRINT OUT IF --

- ELEVATION IS LESS THAN 0 DEGREES
- RANGE IS GREATER THAN 100000. KILOMETERS
- RADAR ANGLE IS GREATER THAN 50.0 DEGREES OR LESS THAN 0. DEGREES

SPIN AXIS COORDINATES ARE 175.0 DEGREES RIGHT ASCENSION
25.0 DEGREES DECLINATION

LOCAL STATION PREDICTIONS

MUTUAL VISIBILITY

DATE	UNIVERSAL TIME	NUT	AND	HIL	GER	TEL	RID	NUT	AND	HIL	NUT	AND	HIL
1/15/64	10 0 C.000	*	*	*	*	*	*	*	*	*	*	*	*
1/15/64	10 2 C.000	*	*	*	*	*	*	*	*	*	*	*	*
1/15/64	10 4 C.000	*	*	*	*	*	*	*	*	*	*	*	*
1/15/64	10 6 C.000	*	*	*	*	*	*	*	*	*	*	*	*
1/15/64	10 8 C.000	*	*	*	*	*	*	*	*	*	*	*	*
1/15/64	10 10 C.000	*	*	*	*	*	*	*	*	*	*	*	*

1/15/64	11 52 0.000	*	*	*	*	*	*	*	*	*	*	*	*
1/15/64	11 54 C.000	*	*	*	*	*	*	*	*	*	*	*	*
1/15/64	11 56 C.000	*	*	*	*	*	*	*	*	*	*	*	*
1/15/64	11 58 C.000	*	*	*	*	*	*	*	*	*	*	*	*
1/15/64	12 0 C.000	*	*	*	*	*	*	*	*	*	*	*	*
1/15/64	12 2 C.000	*	*	*	*	*	*	*	*	*	*	*	*
1/15/64	12 4 0.000	*	*	*	*	*	*	*	*	*	*	*	*
1/15/64	12 6 C.000	*	*	*	*	*	*	*	*	*	*	*	*
1/15/64	12 8 C.000	*	*	*	*	*	*	*	*	*	*	*	*
1/15/64	12 10 C.000	*	*	*	*	*	*	*	*	*	*	*	*
1/15/64	12 12 C.000	*	*	*	*	*	*	*	*	*	*	*	*
1/15/64	12 14 C.000	*	*	*	*	*	*	*	*	*	*	*	*
1/15/64	12 16 C.000	*	*	*	*	*	*	*	*	*	*	*	*
1/15/64	12 18 C.000	*	*	*	*	*	*	*	*	*	*	*	*
1/15/64	12 20 C.000	*	*	*	*	*	*	*	*	*	*	*	*
1/15/64	12 22 C.000	*	*	*	*	*	*	*	*	*	*	*	*
1/15/64	12 24 C.000	*	*	*	*	*	*	*	*	*	*	*	*
1/15/64	12 26 C.000	*	*	*	*	*	*	*	*	*	*	*	*
1/15/64	12 28 C.000	*	*	*	*	*	*	*	*	*	*	*	*
1/15/64	12 30 C.000	*	*	*	*	*	*	*	*	*	*	*	*
1/15/64	12 32 C.000	*	*	*	*	*	*	*	*	*	*	*	*
1/15/64	12 34 C.000	*	*	*	*	*	*	*	*	*	*	*	*
1/15/64	12 36 C.000	*	*	*	*	*	*	*	*	*	*	*	*

1/15/64	12 38	0.000	*	*						*	*
1/15/64	12 40	0.000	*	*						*	*
1/15/64	12 42	0.000	*	*						*	*
1/15/64	12 44	0.000	*	*						*	*
1/15/64	12 46	0.000	*	*						*	*
1/15/64	12 48	0.000	*	*						*	*
1/15/64	12 50	0.000	*	*						*	*
1/15/64	12 52	0.000	*	*						*	*
1/15/64	12 54	0.000	*	*						*	*

LOCAL STATION PRECISIONS

DATE			UNIVERSAL TIME													
MO/DY/YR	H	M	SEC.	NUT	AND	HIL	GER	TEL	RIO	NIT	AND	HIL	NUT	AND	HIL	
1/15/64	12	56	0.000	*	*	*	*	*	*	*	*	*	*	*	*	
1/15/64	12	58	0.000	*	*	*	*	*	*	*	*	*	*	*	*	
1/15/64	13	0	0.000	*	*	*	*	*	*	*	*	*	*	*	*	
1/15/64	13	2	0.000	*	*	*	*	*	*	*	*	*	*	*	*	
1/15/64	13	4	0.000	*	*	*	*	*	*	*	*	*	*	*	*	
1/15/64	13	6	0.000	*	*	*	*	*	*	*	*	*	*	*	*	
1/15/64	13	8	0.000	*	*	*	*	*	*	*	*	*	*	*	*	
1/15/64	13	10	0.000	*	*	*	*	*	*	*	*	*	*	*	*	
1/15/64	13	12	0.000	*	*	*	*	*	*	*	*	*	*	*	*	
1/15/64	13	14	0.000	*	*	*	*	*	*	*	*	*	*	*	*	
1/15/64	13	16	0.000	*	*	*	*	*	*	*	*	*	*	*	*	
1/15/64	13	18	0.000	*	*	*	*	*	*	*	*	*	*	*	*	
1/15/64	13	20	0.000	*	*	*	*	*	*	*	*	*	*	*	*	
1/15/64	13	22	0.000	*	*	*	*	*	*	*	*	*	*	*	*	
1/15/64	13	24	0.000	*	*	*	*	*	*	*	*	*	*	*	*	
1/15/64	13	26	0.000	*	*	*	*	*	*	*	*	*	*	*	*	
1/15/64	13	28	0.000	*	*	*	*	*	*	*	*	*	*	*	*	
1/15/64	13	30	0.000	*	*	*	*	*	*	*	*	*	*	*	*	
1/15/64	13	32	0.000	*	*	*	*	*	*	*	*	*	*	*	*	
1/15/64	13	34	0.000	*	*	*	*	*	*	*	*	*	*	*	*	
1/15/64	13	36	0.000	*	*	*	*	*	*	*	*	*	*	*	*	
1/15/64	13	38	0.000	*	*	*	*	*	*	*	*	*	*	*	*	

1/15/64	15	46	0.000	*	*	*	*	*	*	*	*	*	*	*	*	
1/15/64	15	48	0.000	*	*	*	*	*	*	*	*	*	*	*	*	
1/15/64	15	50	0.000	*	*	*	*	*	*	*	*	*	*	*	*	
1/15/64	15	52	0.000	*	*	*	*	*	*	*	*	*	*	*	*	
1/15/64	15	54	0.000	*	*	*	*	*	*	*	*	*	*	*	*	
1/15/64	15	56	0.000	*	*	*	*	*	*	*	*	*	*	*	*	
1/15/64	15	58	0.000	*	*	*	*	*	*	*	*	*	*	*	*	
1/15/64	16	0	0.000	*	*	*	*	*	*	*	*	*	*	*	*	
1/15/64	16	2	0.000	*	*	*	*	*	*	*	*	*	*	*	*	
1/15/64	16	4	0.000	*	*	*	*	*	*	*	*	*	*	*	*	
1/15/64	16	6	0.000	*	*	*	*	*	*	*	*	*	*	*	*	
1/15/64	16	8	0.000	*	*	*	*	*	*	*	*	*	*	*	*	
1/15/64	16	10	0.000	*	*	*	*	*	*	*	*	*	*	*	*	
1/15/64	16	12	0.000	*	*	*	*	*	*	*	*	*	*	*	*	
1/15/64	16	14	0.000	*	*	*	*	*	*	*	*	*	*	*	*	
1/15/64	16	16	0.000	*	*	*	*	*	*	*	*	*	*	*	*	
1/15/64	16	18	0.000	*	*	*	*	*	*	*	*	*	*	*	*	

TAPE A6
LOCAL STATION PREDICTIONS

LOCAL STATION PREDICTIONS
MUTUAL VISIBILITY

DATE MO/DY/YR	UTZ		STATION	RANGE AZ EL RADAR			
	H	M		(KM)	(DEG)	(DEG)	(DEG)
1/15/64	10	0	COMFIL	6356.7	149.6	62.6	84.3
			CONCER	6368.5	201.7	62.2	75.7
			CONTEL	6144.1	249.3	72.2	69.0
			COMHIL	6356.7	149.6	62.6	84.3
COMFIL	6356.7	149.6	62.6	84.3			
1/15/64	10	2	COMHIL	6214.4	138.5	62.6	87.9
			CONCER	6141.3	193.8	65.5	79.0
			CONTEL	5931.2	246.3	77.3	72.3
			COMHIL	6214.4	138.5	62.6	87.9
COMHIL	6214.4	138.5	62.6	87.9			
1/15/64	10	4	CONCER	5931.5	182.7	68.4	82.6
			CONTEL	5736.9	248.2	82.7	75.9
1/15/64	10	6	CONCER	5743.3	167.9	70.3	86.6
			CONTEL	5565.1	261.2	88.4	79.8
1/15/64	10	8	CONTEL	5420.3	59.9	85.4	84.0
1/15/64	10	10	CONTEL	5307.1	63.6	79.0	88.5
1/15/64	11	52	COMRIC	10353.6	244.9	0.4	55.9
1/15/64	11	54	COMRIC	10285.1	247.3	2.5	53.0
1/15/64	11	56	COMRIC	10225.0	249.8	4.5	50.2
1/15/64	11	58	COMRIC	10173.0	252.3	6.4	47.4
1/15/64	12	0	COMRIO	10128.8	254.9	8.2	44.7
1/15/64	12	2	COMRIO	10092.0	257.5	9.9	42.0
1/15/64	12	4	COMRIO	10062.2	260.2	11.5	39.5
1/15/64	12	6	COMRIC	10038.9	262.9	13.0	37.0
1/15/64	12	8	COMNUI	11465.3	201.0	0.1	71.4
			COMRIO	10021.8	265.7	14.3	34.6
			COMNUT	11465.3	201.0	0.1	71.4
			COMNUT	11465.3	201.0	0.1	71.4

119.

N65-30479

URBAN EMPLOYMENT MULTIPLIERS AND THEIR
APPLICATION TO THE AEROSPACE INDUSTRY IN
ST. LOUIS

Se-Hark Park

Washington University
St. Louis, Missouri

June 1965