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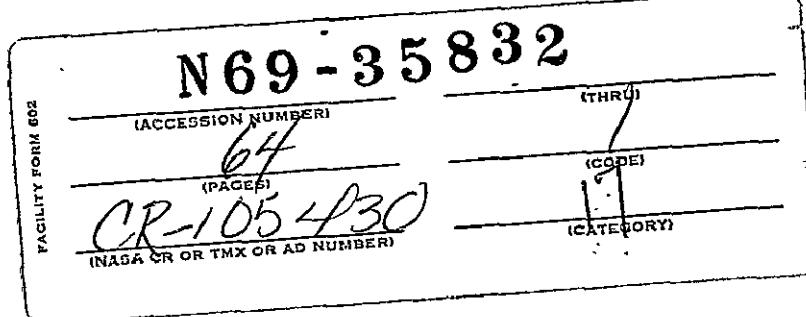
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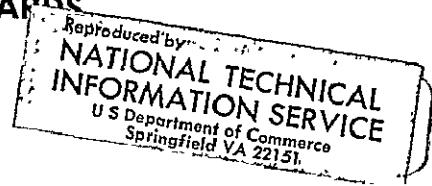
## **CRYOGENIC THERMOCOUPLE TABLES**

by

Larry L. Sparks, Robert L. Powell, and William J. Hall



**U. S. DEPARTMENT OF COMMERCE**  
**NATIONAL BUREAU OF STANDARDS**  
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## CRYOGENIC THERMOCOUPLE TABLES\*

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Experimental tests between 4 and 280 K have been completed on the following thermocouple materials: Chromel, copper, "normal" silver, platinum, silver-28 at. % gold, constantan, Alumel, and gold-(0.02, 0.03, 0.07) at. % Fe. Many thermocouple combinations can be made from the above materials — the four most important being copper vs constantan, Chromel vs constantan, Chromel vs Alumel, and Chromel vs gold-0.07 at. % iron. Results of the last combination are of particular interest for measurements near liquid hydrogen temperatures. The calibration cryostat is described briefly. Special methods of measurement and data analysis have been designed to study and minimize systematic errors. Simple illustrations of these measurement schemes are given. Interim tables and graphs of the thermoelectric voltage and thermopower are given for the four combinations listed above.

Key Words: Cryogenics, gold alloy, thermocouples.

### 1. Introduction

The rapid expansion of low temperature technology in the last 20 years has created a need for standardized thermocouple calibration tables in the cryogenic temperature range. With the cooperation of the American Society for Testing and Materials and thermocouple manufacturers throughout the country, we have now completed the experimental program that will allow establishment of acceptable standard tables for the materials commonly used at low temperatures. Later these tables will be joined smoothly to the existing high temperature standard tables at the ice point. This will then provide one continuous calibration for each thermocouple type over its entire temperature range of usefulness.

\*This work was carried out at the National Bureau of Standards under the sponsorship of the National Aeronautics and Space Administration, Space Nuclear Propulsion Office (SNPO-C), Contract R-45.

In addition to the common materials (Chromel<sup>†</sup>, copper, platinum, "normal" silver, constantan, and Alumel<sup>†</sup>), several special materials have been measured. Silver-28 at. % gold was included as a possible replacement for platinum as the reference material below liquid nitrogen temperatures. Three gold-iron alloys were included because they retain a relatively high sensitivity down to, and even below, 10 K.

In 1932 Borelius and co-workers<sup>[1]</sup> showed that small amounts of transition metals in gold cause high thermopowers at very low temperatures. In the last few years several laboratories have been using various gold-iron alloys as the negative element in thermocouples. The gold-iron alloys are preferable to the previously used gold-cobalt alloys for two

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<sup>†</sup> Authors' Note: The words Chromel and Alumel are registered trade names. The correct ASA, ASTM, ISA, designations for the relevant thermocouple combinations and materials are as follows:

Type	Elements	Materials, Trade Names
E	EP (+)	Chromel, Tophel, T-1
	EN (-)	constantan, Advance, Cupron
K	KP (+)	Chromel, Tophel, T-1
	KN (-)	Alumel, Nial, T-2
T	TP (+)	copper
	TN (-)	constantan, Advance, Cupron

Names are usually given in this article because relatively few people are familiar with the designations KP, KN, etc. However, the use of the trade names does not constitute an endorsement of one manufacturer's products. All materials manufactured in compliance with the established standards are equally suitable.

reasons: 1) they have a higher thermopower at low temperatures, and 2) they are in stable metallurgical solution (unlike the gold-cobalts) and therefore their output does not drift with time or 100 C annealing. The positive element usually has been copper, "normal" silver, or Chromel. We generally recommend the use of Chromel because it has a high positive thermopower in the upper temperature range where the gold-iron thermoelement is no longer strongly negative. This combination has sufficient sensitivity to be useful in the entire range from below 4 to 300 K. An additional advantage of Chromel over copper or "normal" silver is its relatively low thermal conductivity, as shown in table 1<sup>[2]</sup>.

Table 1.

Material	Thermal Conductivity	
	at (10 K) watts m.K	at (273 K) watts m.K
Cu	870	400
"normal" silver	200	380
Chromel	4	120

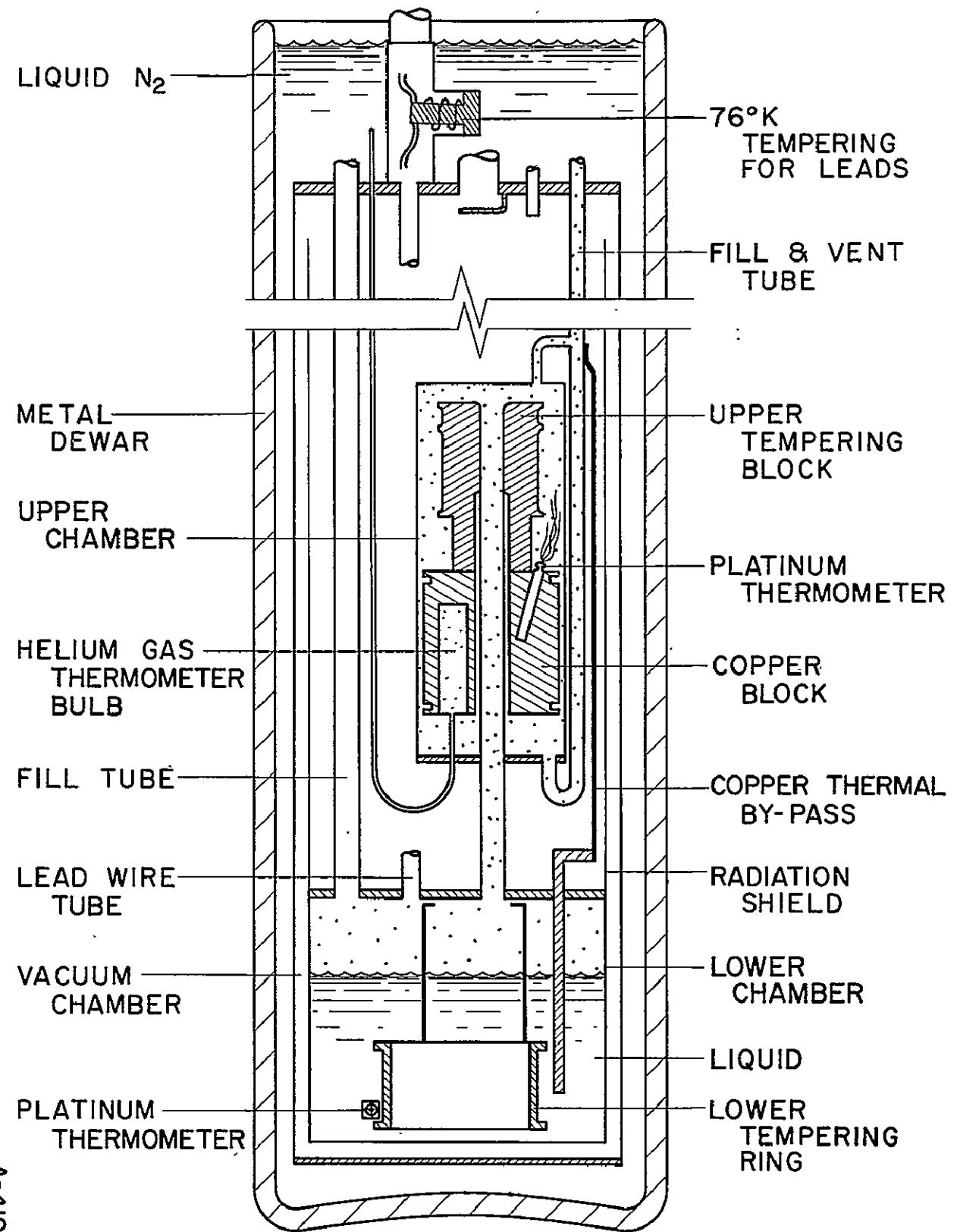
Until standardized materials and tables become available, users of the gold-iron alloys must perform their own detailed calibrations. Since this is time consuming and expensive, calibrations generally cover only the limited range of the particular experiment. We have now tested three gold-iron alloys against Chromel, platinum, and "normal" silver in the range from 4 to 280 K, but tables in the Appendix are given for only the Chromel vs gold-0.07 atomic percent iron combination.

## 2. Cryostat

A schematic of our cryostat is shown in figure 1, the critical parts of which are the two inner chambers. They are both surrounded by a high vacuum and a liquid nitrogen bath. The thermal insulation provided by this arrangement allows the use of liquid nitrogen, liquid hydrogen, or liquid helium as the thermocouple reference junction bath. The reference junction for the thermocouples is in the lower chamber. In addition to providing a reference temperature, this bath serves both as a heat sink for all incoming wires and as a source of refrigeration for the upper chamber.

The upper and lower chambers are connected by a tube which provides a wire duct and allows gas conduction between the lower and upper chambers. The variable junctions of the thermocouples are thermally anchored to a large copper block contained in the upper chamber. Refrigeration for the copper block is supplied by gas conduction from the lower chamber and also by conduction along the wires connecting the upper and lower chambers. A stable temperature difference is established between the two thermocouple junctions by balancing the refrigerator power with the power supplied to a heater coil wound on the copper block. Temperature drift of the block during a one-hour run is less than 3 mK.

In order to reduce the heat leak into the upper chamber as much as possible, all incoming wires are thermally tempered at liquid nitrogen temperatures before going into the lower chamber. All wires going into the upper chamber are of course also tempered in the reference cryogen. A thermal shield is between the copper block and the side walls of the upper chamber. An automatic heater control, operating from the output of a thermopile between the block and the shield, controls the temperature of the shield to be within 0.01 K of the block during all runs.



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Figure 1 Thermocouple calibration cryostat.

Temperature determinations for the variable junction are made with platinum resistance thermometers when operating between 20 and 280 K and with germanium resistance thermometers when operating between 4 and 20 K. Three of each type of thermometer are actually installed in the upper copper block to provide a check on the primary thermometer and for use in the temperature control system. The temperature of the reference bath is calculated from readings of a single calibrated platinum thermometer whenever liquid hydrogen or liquid nitrogen are being used. The pressure of the inner system is manostatically controlled when these cryogens are used. Whenever liquid helium is being used, the inner system is at normal atmospheric pressure, and the bath temperature is then calculated from readings of the vapor pressure.

### 3. Instrumentation, Measurement and Materials

A block diagram of the measurement system is given in figure 2. The instrumentation is similar to many low level d. c. measurement systems. A six dial potentiometer is used to measure the thermocouple and germanium thermometer voltages. A G2 Mueller bridge that has been thermally isolated from room temperature fluctuations is used to determine the resistance of the platinum thermometers.

Our method of data analysis requires that we be able to intercompare any of the nineteen thermocouple wires. Out of the many possible combinations, 37 were of special importance. They fall into three groups: 1) four primary thermocouple combinations — i. e., Chromel vs constantan, Chromel vs Alumel, copper vs constantan, and Chromel vs gold-0.07 at. % iron; 2) eleven calibration combinations — e. g., constantan vs reference platinum; and 3) twenty-two intercomparison combinations — e. g., constantan from one manufacturer vs constantan from another manufacturer.

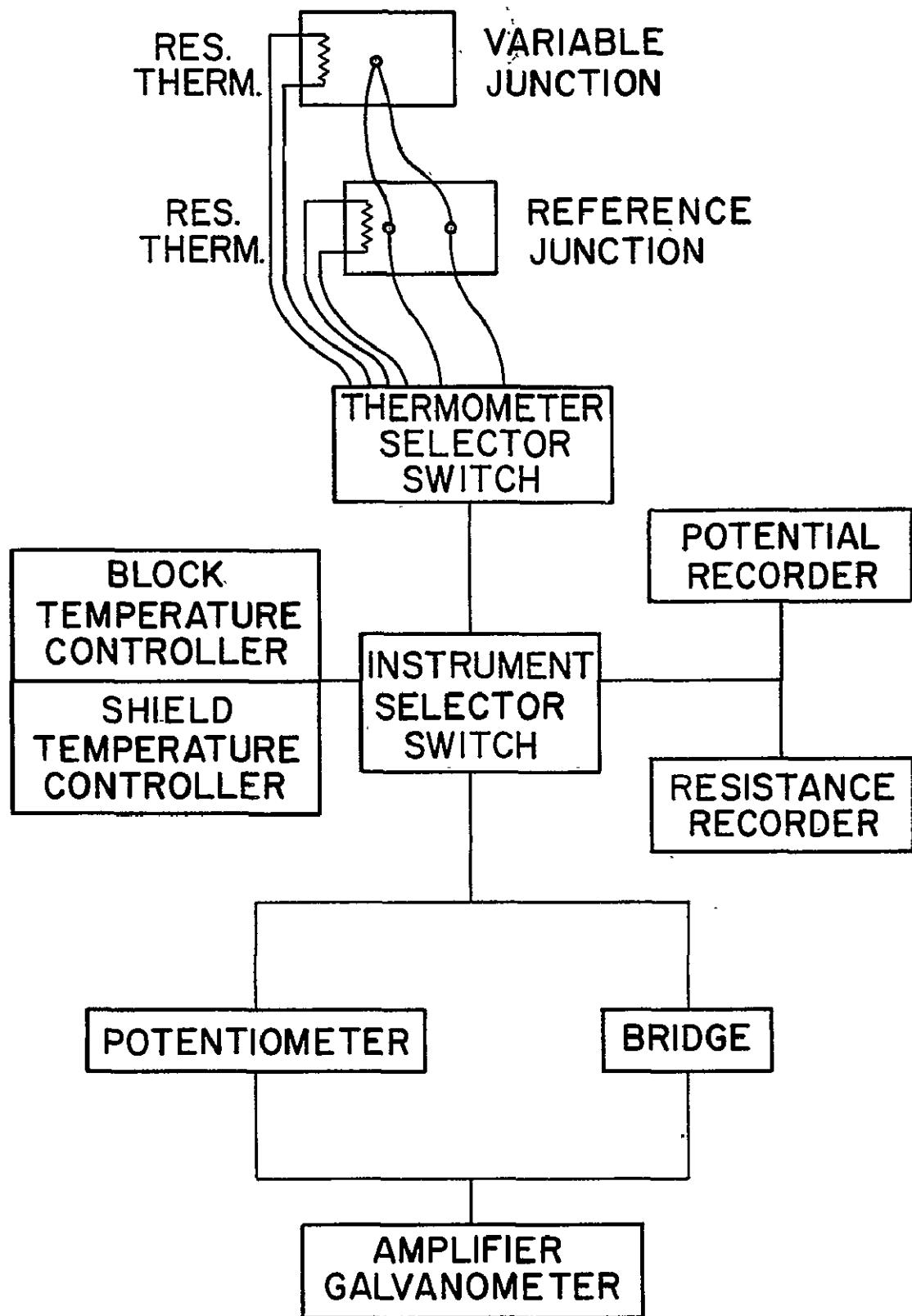


Figure 2      Thermocouple instrumentation system.

Figure 3 is an illustration of a typical set of voltage measurements used to determine the value of a single thermocouple pair - Chromel vs Au-0.07 at. % Fe in this example. In this figure, the letters represent actual voltage measurement paths, e.g., (A) represents the direct reading of Chromel vs gold-iron, (B) represents Chromel vs platinum, etc. The five voltage determinations are combined as follows to yield the calculated value of Chromel vs gold-iron;

$$\text{Calculated voltage} = \{ 2(A) + [(B) + (C)] + [(D) + (E)] \} / 4.$$

The (A) reading is given a weight of 2 since it involves only one reading while the others require two readings.

This measurement scheme enables us to convert at least three types of systematic error into random errors. The random errors from these sources can then be included with the other scatter present in the experimental data. The sources of errors accounted for in this manner are operator prejudice, potentiometer dial inconsistencies, and spurious thermal voltages in the lead wires. The effect of any subconscious tendency of the operator to make the data appear repeatable in a sequence of measurements is eliminated from the final calculated value because computation of the final result involves the algebraic combination of five different voltages whose values vary considerably. In addition to eliminating operator prejudice, the five diverse measurements randomize errors associated with inconsistencies in potentiometer dial readings. Inhomogeneities in extension wires cause small spurious voltages that will change whenever temperature gradients along the wires change. Since a set of voltage readings takes many minutes to complete, variations in spurious voltages tend to be randomized by our method of calculation.

Materials included in this set of calibration wires are Chromel, copper, "normal" silver, platinum, silver-28 at. % gold, constantan,

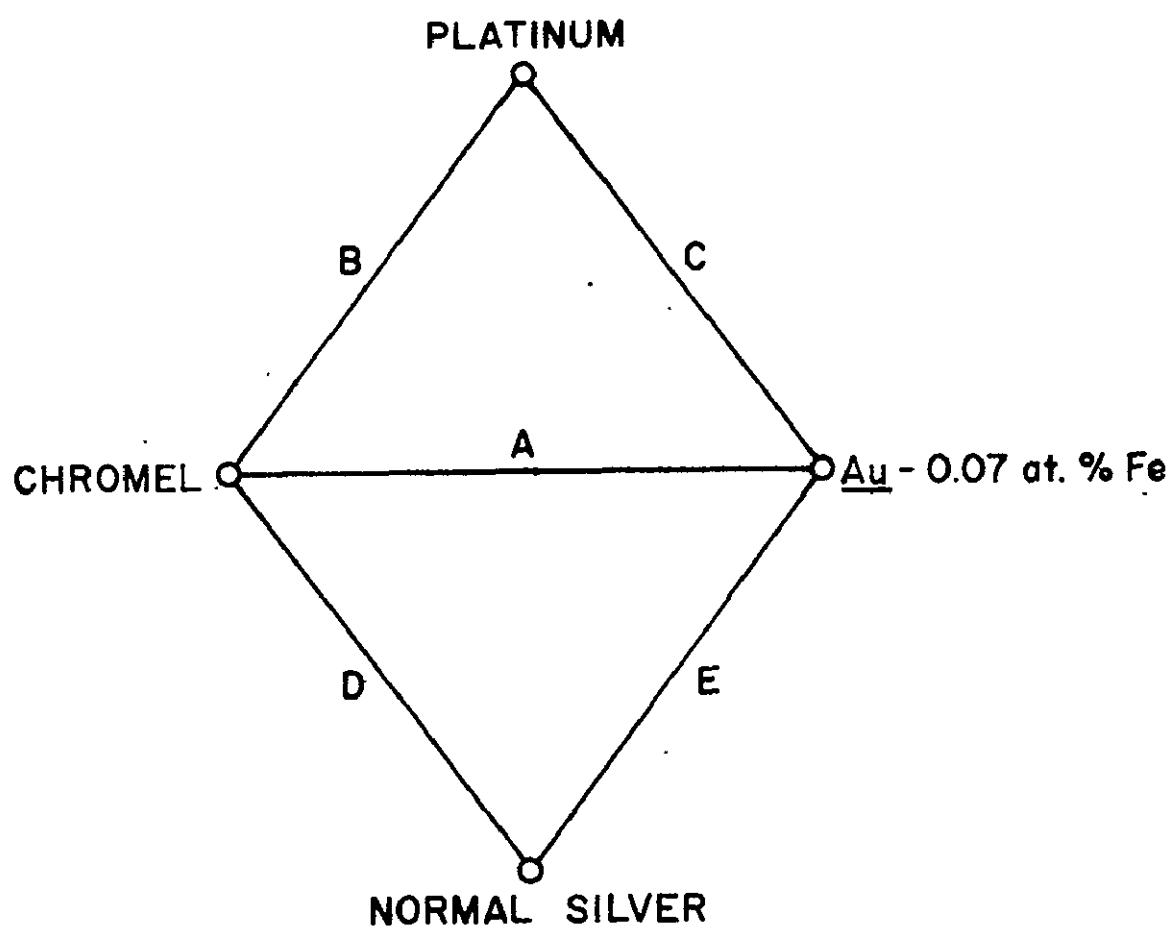


Figure 3      Typical Calibration measurement graph.

Alumel, and three gold-iron alloys (0.02, 0.03, 0.07 at. % Fe in Au). An industry wide sampling was available for the regular commercial materials; therefore, the results for these materials will be acceptable as standards. An industry-wide sampling for the gold-iron alloys was not available, so the results for these alloys must be considered interim.

#### 4. Data Analysis and Results

As mentioned previously, our data are taken using three different liquids in the reference bath. This allows us to cover the range from 4 to 280 K and still maintain temperature control in the upper block. The following temperature spans were used: liquid helium (4 to 26 K), liquid hydrogen (20 to 90 K), and liquid nitrogen (75 to 280 K). Figure 4 shows a least squares approximation to the experimental data for Chromel vs Au-0.07 at. % Fe before the "range shift constants" are applied. The Law of Successive Temperatures<sup>[3]</sup> for thermocouples states: "If two dissimilar homogeneous metals produce a thermal voltage of  $E_1$  when the junctions are at temperatures  $T_1$  and  $T_2$  and a thermal voltage of  $E_2$  when the junctions are at  $T_2$  and  $T_3$ , the thermal voltage generated when the junctions are at  $T_1$  and  $T_3$  will be  $E_1 + E_2$ ." This law allows all of the voltages to be shifted to a common reference temperature. We call those shifts in voltages the "range shift constants," and they are treated as unknown constants in the least squares computer program. The calibration table is made continuous over the entire range by including the necessary shift constants. The final curves for the temperature dependence of the thermal voltage and thermopower of Chromel vs Au-0.07 at. % Fe are shown in figures 5 and 6 respectively.

Since our method of data analysis is quite different from the usual power series expansion, it will be described briefly. The adjusted

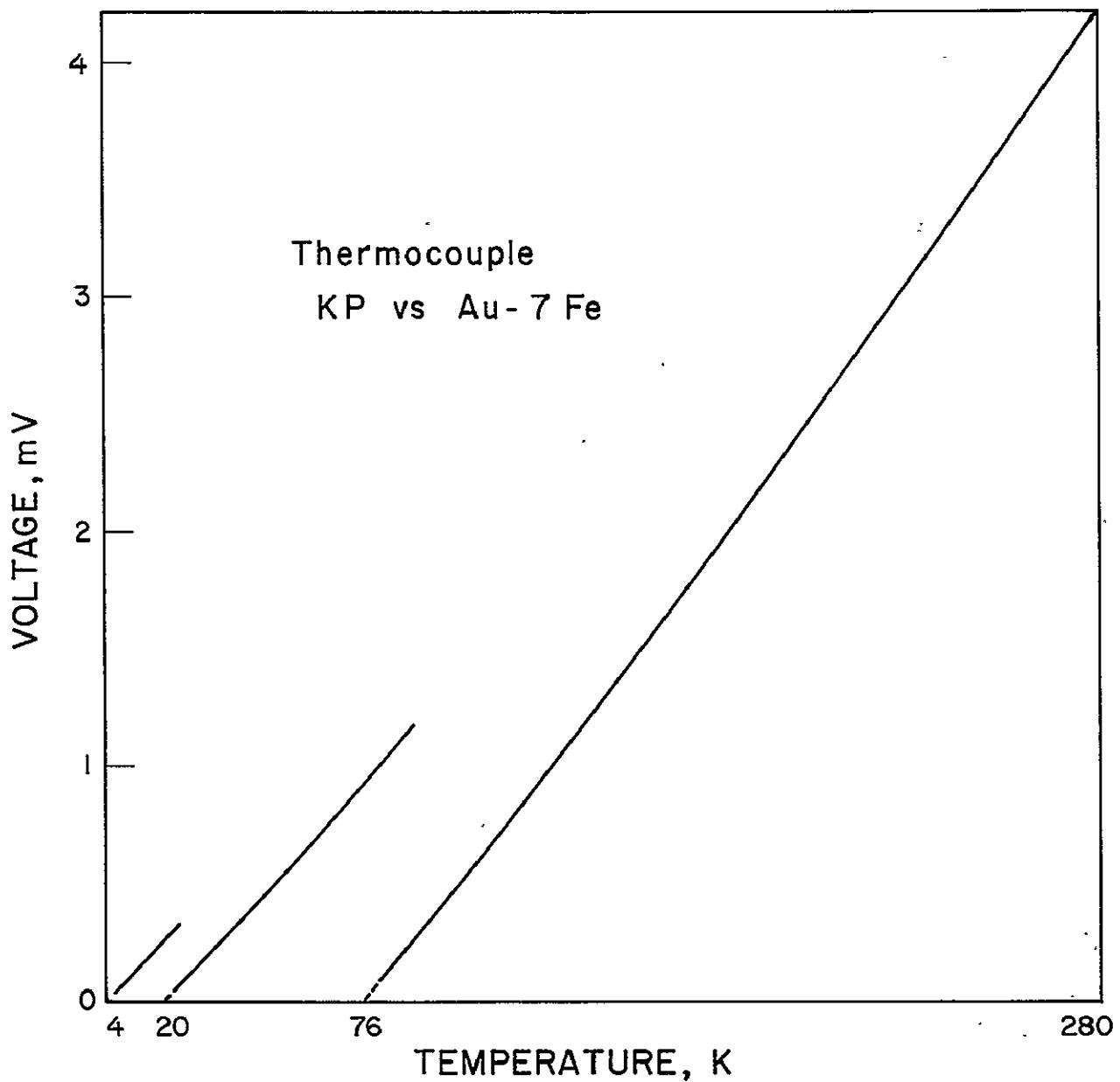


Figure 4      Thermoelectric voltage of Chromel versus.  
gold-0.07 atomic % Fe. Reference junctions  
at 4, 20, and 76 K.

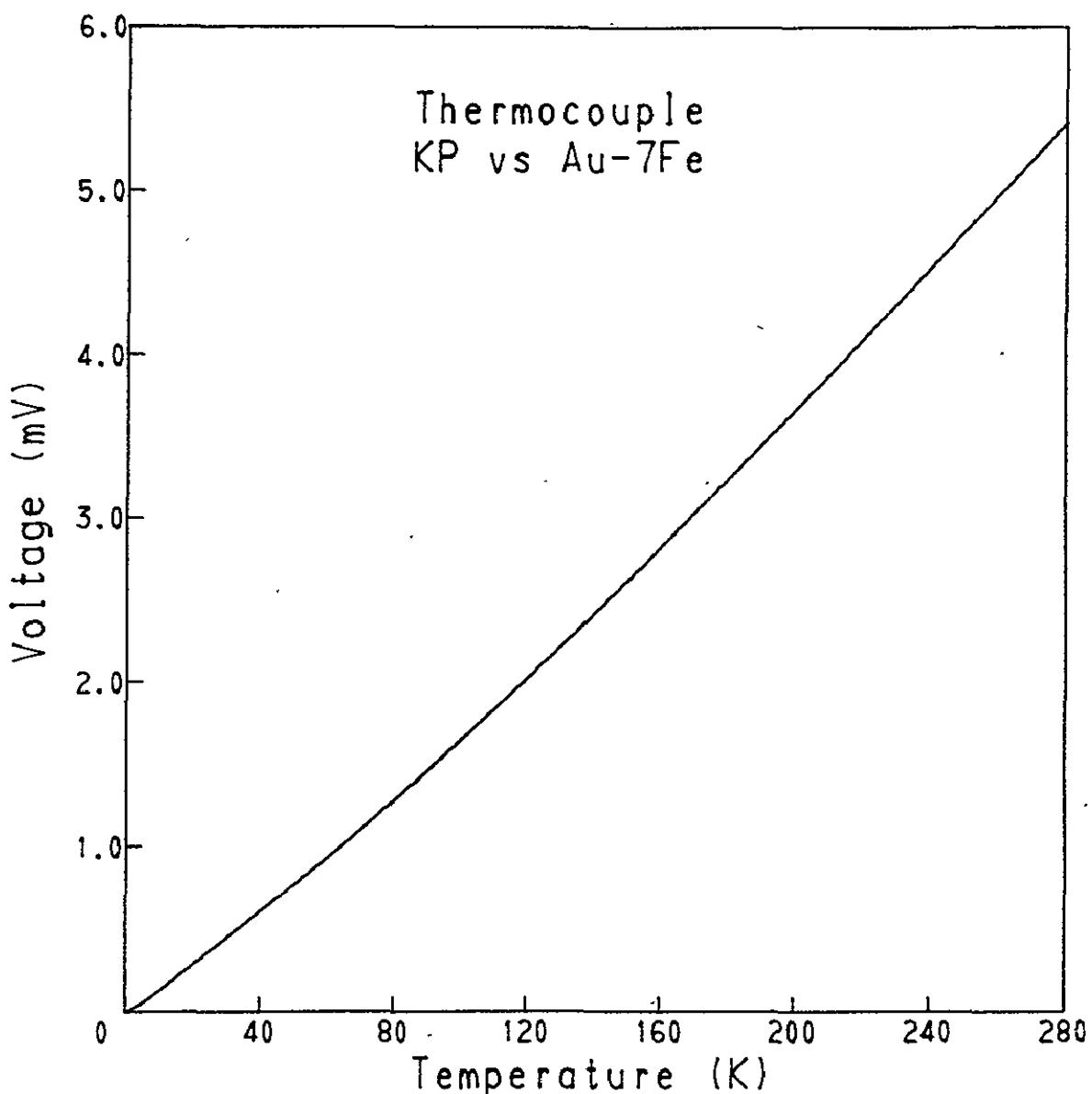


Figure 5      Thermoelectric voltage of Chromel versus  
gold-0.07 atomic % Fe. A common reference  
temperature of zero K.

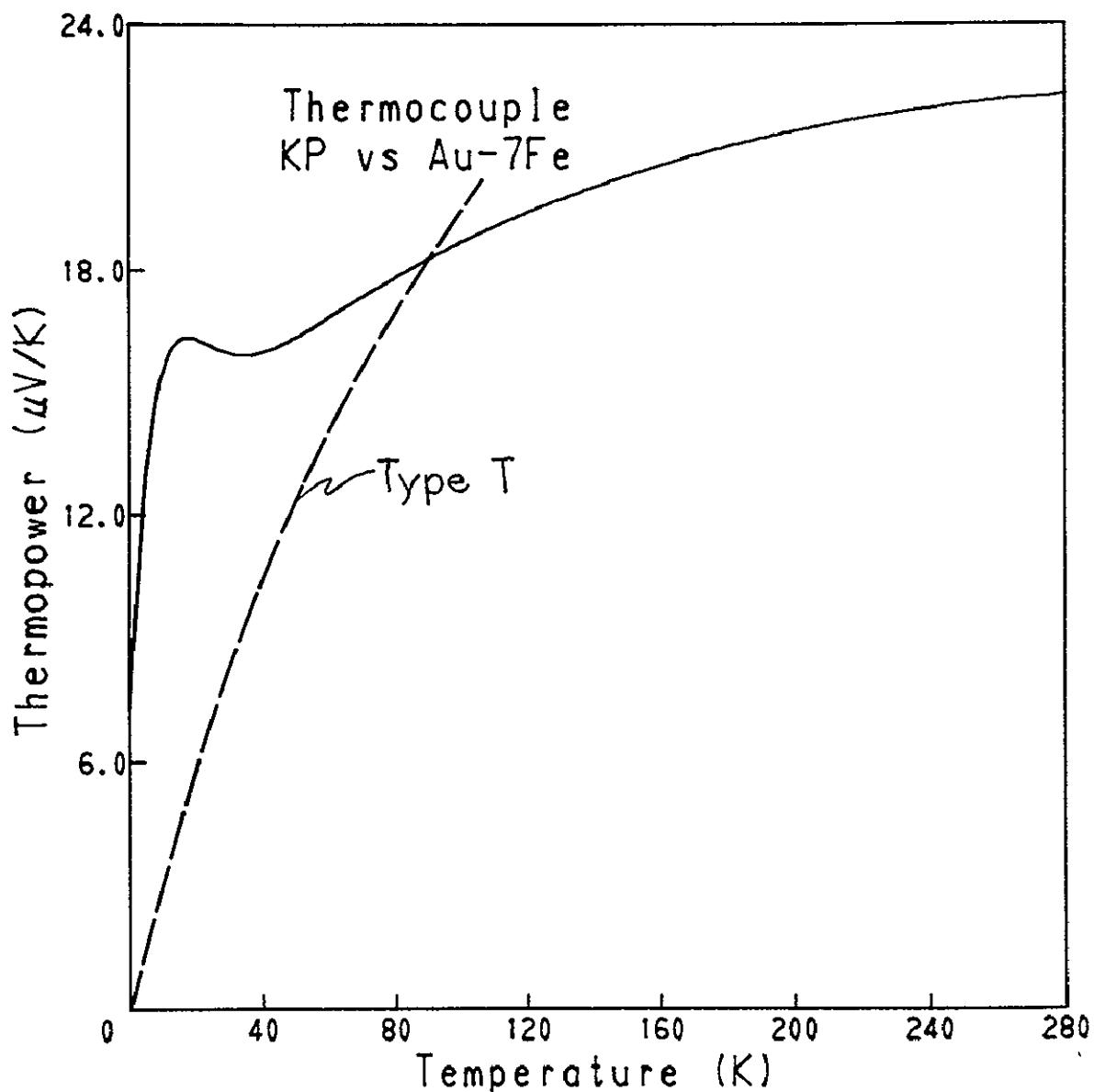


Figure 6 Thermopower of Chromel versus gold-0.07 atomic % Fe. A comparison curve for type T is included.

experimental values for the voltages of each thermocouple combination are approximated by a series of orthonormal polynomials in the  $L_2$  norm (least squares), that is,

$$E(T) = \sum_{n=1}^L A_n F_n(T)$$

where

- $E$  = thermocouple potential in microvolts;
- $T$  = temperature in degrees kelvin;
- $L$  = the highest order for a best fit, different for different combinations;
- $A_n$  = constants to be determined by the fitting approximation; and
- $F_n(T)$  = orthonormal polynomials, orthonormal on the data points over the range of variation of the independent variable,  $T$ .

The conditions for orthonormality of  $F_n(T)$  are

$$\sum_{i=1}^N F_m(T) F_n(T) = \delta_{mn}$$

$\delta_{mn}$	= 0 if $m \neq n$
	= 1 if $m = n$ ;

where i is summed over the total number of experimental points, N.

It should be stressed that the orthonormal polynomials  $F_n(T)$  are determined by values of the independent variable  $T$  only. The  $F_n(T)$  are generated from a truncated power series

$$F_n(T) = \sum_{j=1}^n C_{jn} T^j.$$

Once the  $F_n(T)$  are determined, the coefficients  $A_n$  are determined by values of the dependent variable  $E$ . Therefore, the  $F_n(T)$  are the same

for all combinations, but the  $A_n$  are different for each thermocouple combination. The highest order,  $L$ , necessary for a best fit is also different for each combination.

A common problem in the numerical analysis of data fitting by polynomials is selection of the proper order for a best fit—an order high enough to represent the data with no loss of precision, but not so high as to introduce mathematical oscillations. This problem is well solved by our method of fitting by orthonormal polynomials. For true physical phenomena, the absolute values of the coefficients  $A_n$  decrease with increasing  $n$  as  $1/n$  or  $1/n^2$ . However, for noise, the coefficients are random. Therefore, an inspection of a graph of  $|A_n|$  vs  $n$  shows the noise level and the maximum value of  $n$  that is useable. In figure 7 such a graph is shown for the thermocouple KP vs Au-0.07 at. % Fe. The first three points are range shift constants. The coefficient for order 7 is accidentally below the noise level of  $2 \times 10^{-1}$ .

The general polynomials  $F_n(T)$  and the  $A_n$  and  $L$  for each thermocouple combination are given in Appendix E. An error analysis is also included in that appendix.

Thermopowers and thermopower derivatives are calculated from the differentiated expressions for thermal voltage.

Calibration tables for the four primary thermocouple systems result from our experimental research and analysis. These include types T, E, K, and Chromel vs Au-0.07 at. % Fe. The tables for types T, E, and K are only minor modifications of the interim internal standard tables by Sparks and Powell, which were in turn modified versions of earlier<sup>[4, 5]</sup> work. The analyzed results are given in graphs and tables in Appendices A through D. The three graphs in each appendix represent the thermal voltage  $E$ , thermopower  $S \equiv dE/dT$ , and thermopower

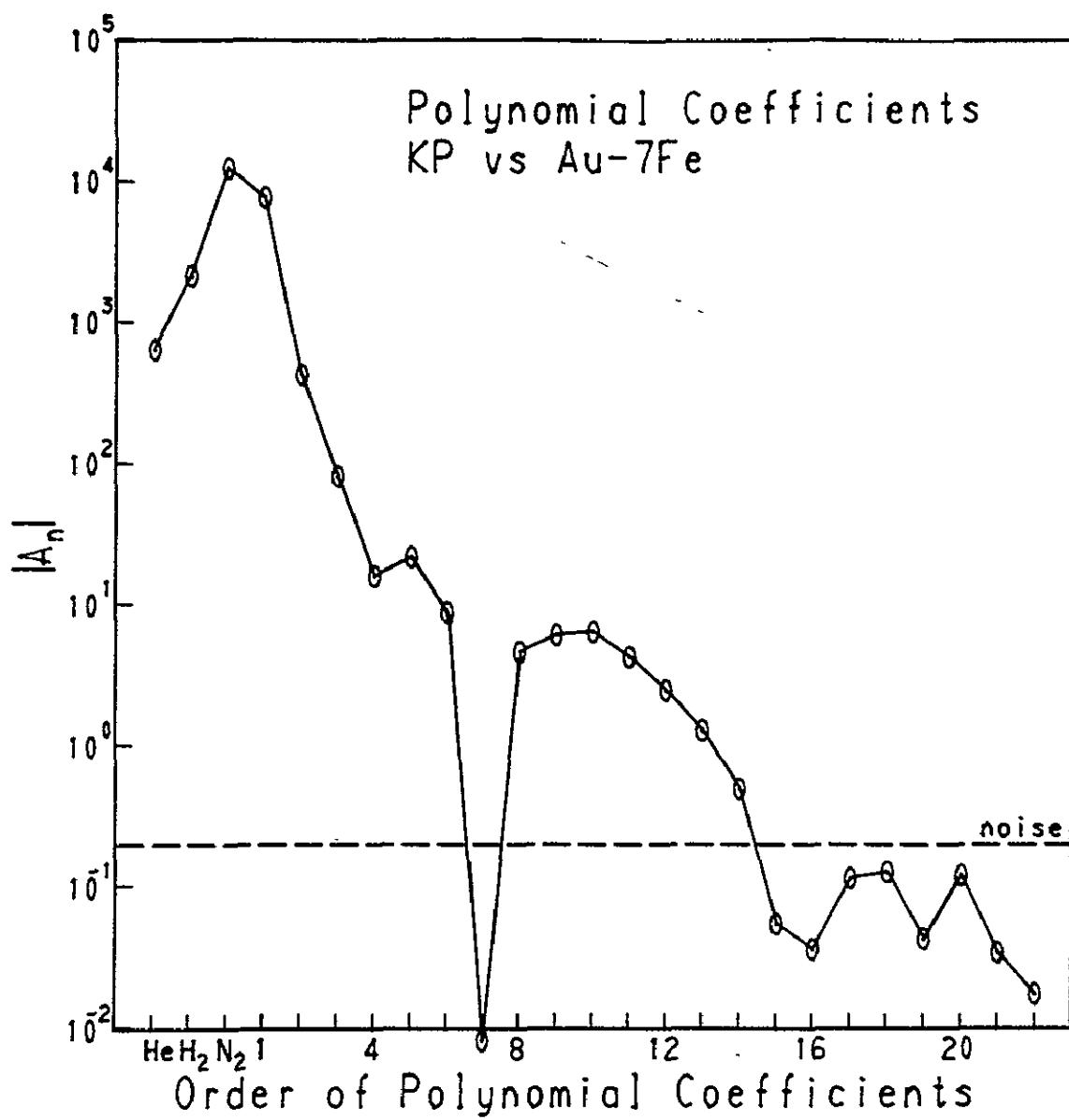


Figure 7      Polynomial coefficients for KP versus  
                Au-0.07 atomic % Fe.

derivative  $dS/dT$ . Most of them are straightforward and need no explanation. However, the bump in the thermopower derivative for type T (fig. A-3) above 270 K causes an exception. The sudden upturn is probably not a true physical phenomenon, but rather a peculiarity of the data fitting caused by a slight error in voltage at the highest experimental temperature. Deviation plots for each type are included in Appendix E.

Since the essential information on the T, E, and K systems is in the literature,<sup>[4,5]</sup> the remainder of the discussion will be primarily concerned with the Chromel vs Au-0.07 at.% Fe system. The principal reason for the interest shown in the gold-iron alloys has been their relatively high sensitivity in the liquid hydrogen and liquid helium ranges. Another significant property of the Chromel vs Au-0.07 at.% Fe system is its linearity, clearly seen in figure 5. The maximum voltage deviation from linearity is approximately 5 percent of the full scale voltage. This property is very important in applications where a reliable temperature difference is needed, but it is difficult to maintain a suitable reference temperature. Figure 6 represents the thermopower of the Chromel vs Au-0.07 at.% Fe combination. For purposes of comparison the thermopower of type T is shown by the dashed line. The hump in the thermopower is characteristic of all Au-Fe alloys. The position of the hump is affected by the solute concentration and, in general, the high temperature sensitivity increases and the low temperature sensitivity decreases as the iron concentration is increased.<sup>[6,7]</sup> A theoretical explanation of the high thermoelectric power at low temperatures has not been fully developed. However, the theories of Kasuya, Bailyn, and de Vroomen<sup>[8]</sup> appear to offer the most reasonable explanations at present.

The estimated inaccuracies in the independent variable (temperature) for our calibrations are 2.2 mK in the helium range, 2.5 mK in the hydrogen range, and 2.0 mK in the nitrogen range. Inaccuracy of the dependent variable (voltage) varies with the thermocouple being used. For example,

for the Chromel vs Au-0.07 at. % Fe system the inaccuracies are 0.034  $\mu$ V in the liquid helium range, 0.135  $\mu$ V in the hydrogen range, and 0.218  $\mu$ V in the nitrogen range. A conservative estimate of the total inaccuracies to be found in the calibration of our particular Chromel vs Au-0.07 at. % Fe combination is as follows:  $\pm$  10 mK in the range from 4 to 20 K,  $\pm$  12 mK in the range from 20 to 75 K, and  $\pm$  15 mK in the range from 75 to 280 K. The temperature scales being used are the latest proposed international scale<sup>[9]</sup> above 20 K and the NBS acoustical scale below 20 K. The inaccuracies given do not include deviations of these temperature scales from the true thermodynamic scale.

### 5. Summary

We recommend type E (Chromel vs constantan) thermocouples for general engineering use above liquid hydrogen temperatures. Both elements of this thermocouple have low thermal conductivity and reasonably good homogeneity. This combination may be used over the wide temperature range from the normal boiling point of liquid hydrogen 20 K (the sensitivity is marginal in this region) up to approximately 1000C. For operation below 20 K, Chromel vs Au-0.07 at. % Fe is the most sensitive combination available. The usefulness of this combination is further enhanced by its linear characteristics.

The experimental research done on types T, E, and K qualify the calibration results to be acceptable as national standards; consequently, they will soon be joined to the existing high temperature standard tables to provide calibrations over the entire temperature range of usefulness for each material. The tests on Au-Fe alloys must be continued in order to establish the degree of uniformity between samples of materials from different producers.

An NBS Monograph will be published later with full details on the experimental apparatus, measurement methods, numerical analysis techniques, and thermocouple material characterizations. At that time the tables in the following appendices will be slightly altered so that they will join smoothly at the ice point to the high temperature tables already published.<sup>[10]</sup>

## 6. References

1. G. Borelius, W. H. Keesom, C. H. Johansson and J. O. Linde, Proc. Kon. Akad. Amsterdam 35, 10 (1932).
2. G. A. Slack, "Thermal Conductivity of  $\text{CaF}_2$ ,  $\text{MnF}_2$ ,  $\text{CoF}_2$ , and  $\text{ZnF}_2$  Crystals", Phys. Rev. 122, No. 5, 1451 (1961).
3. D. I. Finch, "General Principles of Thermoelectric Thermometry", Temperature—Its Measurement and Control in Science and Industry (Reinhold, New York, N. Y., 1962), Vol. 3, Part 2.
4. R. L. Powell, L. P. Caywood, Jr., and M. D. Bunch, "Low-Temperature Thermocouples", Temperature—Its Measurement and Control in Science and Industry (Reinhold, New York, N. Y., 1962), Vol. 3, Part 2.
5. Unpublished data by R. L. Powell and M. D. Bunch, National Bureau of Standards.
6. R. Berman, J. C. F. Brock and D. J. Huntley, "Properties of Gold + 0.03 percent (at.) Iron Thermoelements Between 1 and 300 °K and Behavior in a Magnetic Field", Cryogenics 4, 233 (1964).
7. D. K. Finnemore, J. E. Ostenson and T. F. Stromberg, "Secondary Thermometer for the 4 to 20 °K Range", Rev. Sci. Instr. 36, No. 9, 1369 (Sept. 1965).
8. D. K. C. McDonald, Thermoelectricity: An Introduction to the Principles (John Wiley & Sons, New York, N. Y., 1962), p. 80.
9. Private correspondence from Preston-Thomas, NRC, Canada. Also see: H. Preston-Thomas and R. E. Bedford, "Practical Temperature Scales Between 11K and 273K", Metrologia 4, No. 1 (1968).

References continued

10. H. Shenker, et al., Reference Tables for Thermocouples, NBS Circular 561, (Gov't. Printing Office, Wash., D.C., 1955); American Standards Assoc., American Standard for Temperature Measurement Thermocouples, C 96.1-1964, (Am. Stand. Assoc., Pittsburgh, 1964); American Society for Testing and Materials, Temperature Electromotive Force (EMF) Tables for Thermocouples, E 230-63, (Am. Soc. Test. Mat., Philadelphia, 1963).

Appendix A.

Interim Tables and Graphs for Thermocouple Type T,  
Copper vs Constantan.

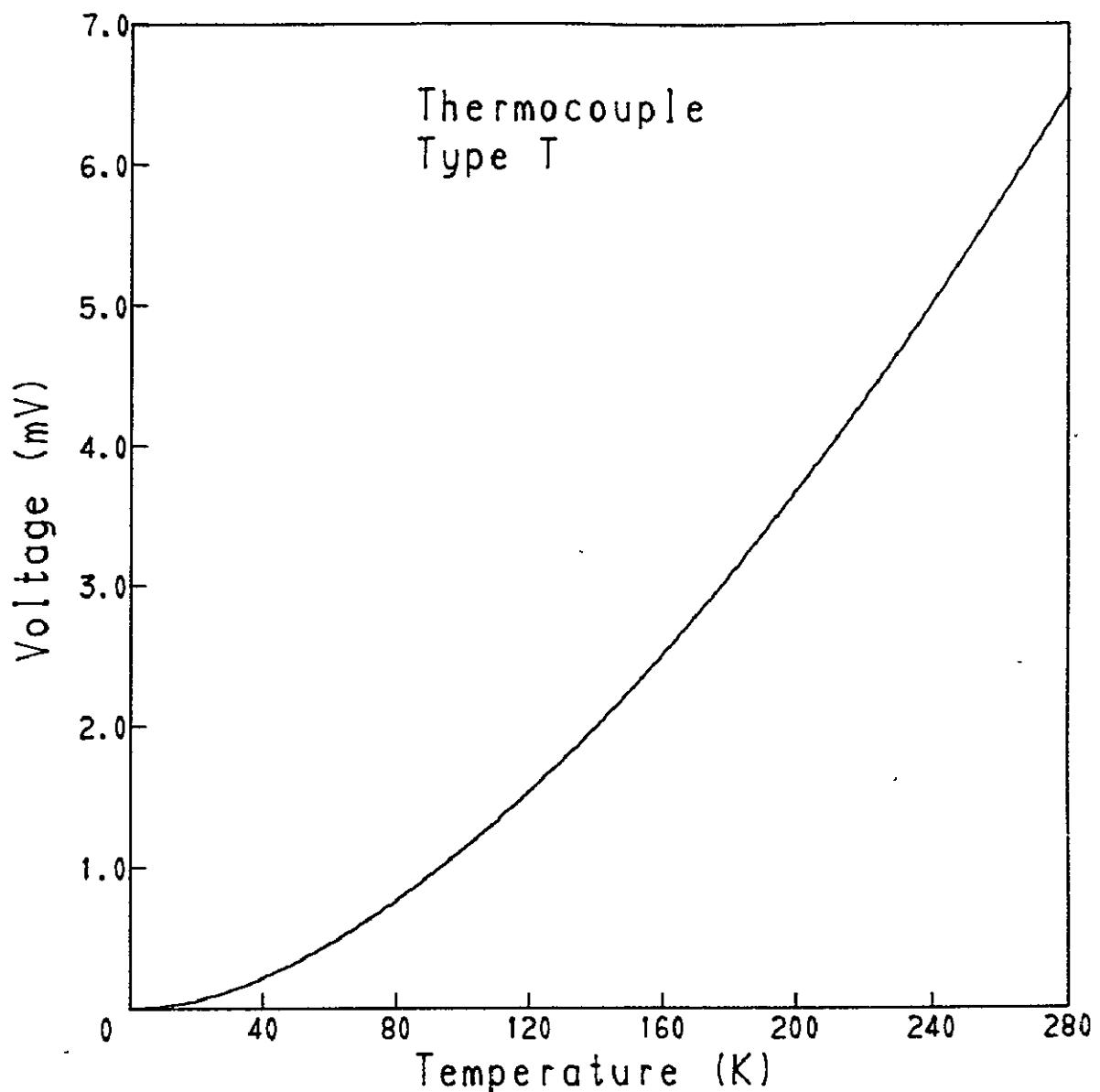


Figure A-1 Thermoelectric voltage of thermocouple type T, copper versus constantan.

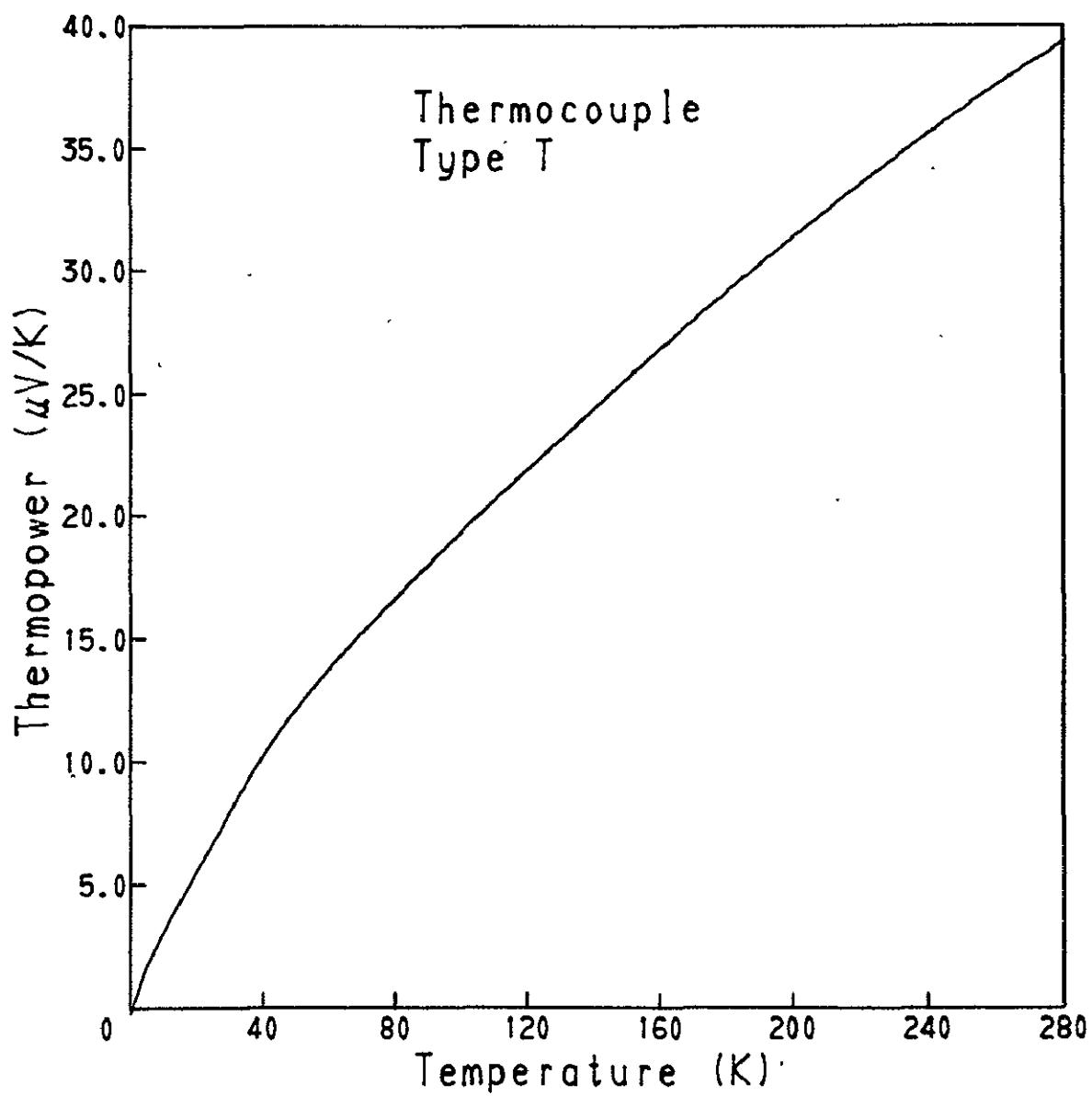


Figure A-2 Thermopower of thermocouple type T,  
copper versus constantan.

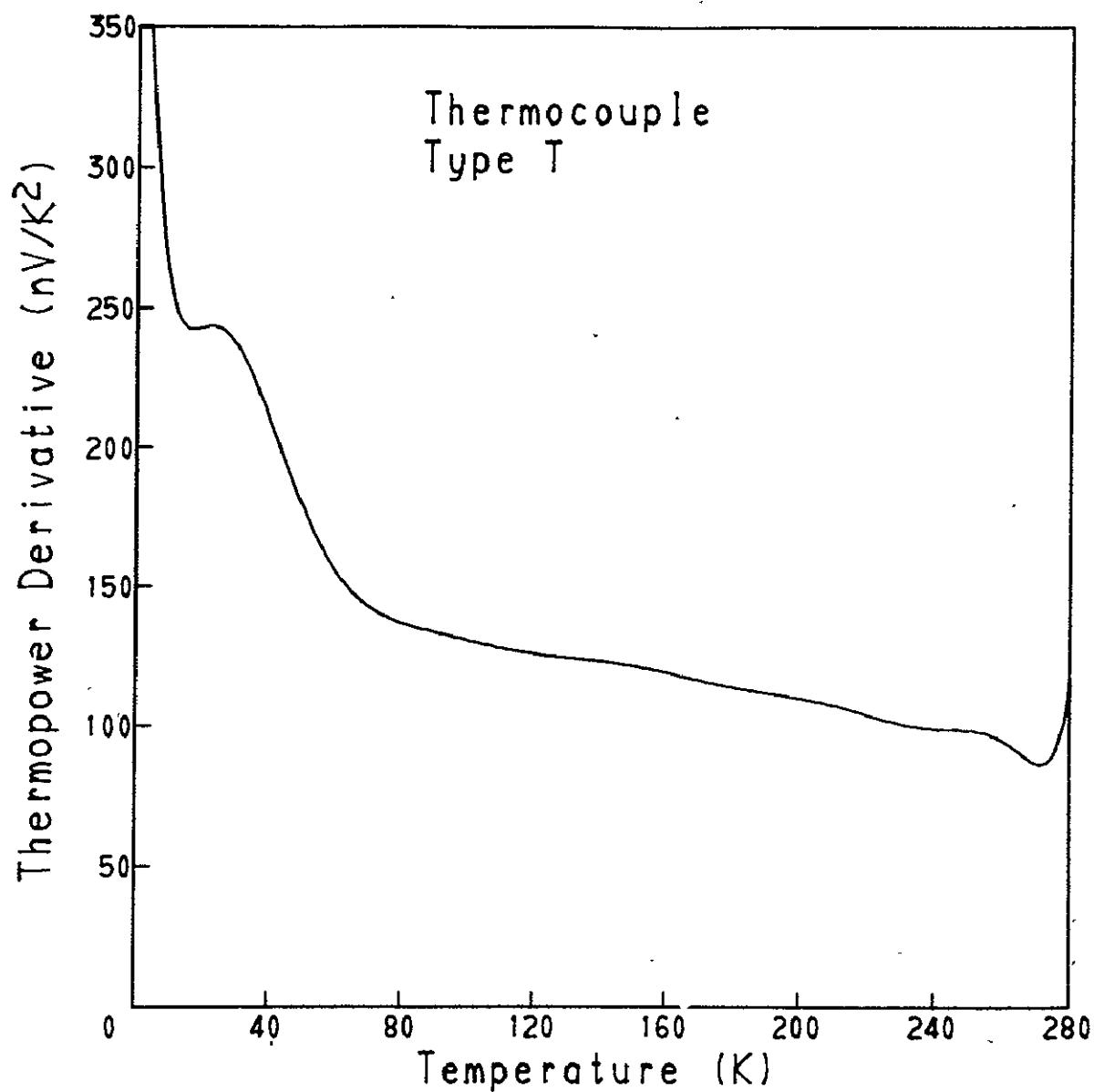


Figure A-3 Thermopower derivative of thermocouple type T, copper versus constantan.

Temp. K	Voltage=E mV	$\frac{dE}{dT}=S$ mV/K	$\frac{dS}{dT}$ mV/K <sup>2</sup>	Temp. K	Voltage=E mV	$\frac{dE}{dT}=S$ mV/K	$\frac{dS}{dT}$ mV/K <sup>2</sup>
1	-0.09	0.147	0.4611	51	343.30	12.345	0.1752
2	0.28	0.586	0.4179	52	355.73	12.519	0.1725
3	1.07	0.985	0.3816	53	368.33	12.690	0.1699
4	2.24	1.351	0.3515	54	381.11	12.859	0.1674
5	3.76	1.690	0.3266	55	394.05	13.025	0.1650
6	5.61	2.006	0.3064	56	407.16	13.189	0.1628
7	7.77	2.304	0.2900	57	420.43	13.350	0.1607
8	10.21	2.587	0.2770	58	433.86	13.510	0.1586
9	12.94	2.859	0.2668	59	447.44	13.668	0.1567
10	15.93	3.121	0.2590	60	461.19	13.824	0.1549
11	19.18	3.377	0.2531	61	475.09	13.978	0.1533
12	22.68	3.628	0.2489	62	489.15	14.130	0.1517
13	26.43	3.876	0.2459	63	503.35	14.281	0.1502
14	30.43	4.120	0.2440	64	517.71	14.431	0.1489
15	34.67	4.364	0.2428	65	532.21	14.579	0.1476
16	39.16	4.606	0.2423	66	546.86	14.726	0.1464
17	43.89	4.848	0.2421	67	561.66	14.872	0.1453
18	48.85	5.091	0.2422	68	576.61	15.017	0.1443
19	54.07	5.335	0.2425	69	591.70	15.160	0.1434
20	59.52	5.576	0.2428	70	606.93	15.303	0.1425
21	65.22	5.818	0.2431	71	622.30	15.445	0.1417
22	71.16	6.062	0.2432	72	637.82	15.587	0.1410
23	77.34	6.305	0.2432	73	653.48	15.727	0.1403
24	83.77	6.548	0.2430	74	669.27	15.868	0.1397
25	90.44	6.791	0.2426	75	685.21	16.007	0.1391
26	97.35	7.033	0.2419	76	701.29	16.146	0.1386
27	104.50	7.274	0.2409	77	717.50	16.284	0.1381
28	111.90	7.515	0.2398	78	733.86	16.422	0.1376
29	119.55	7.754	0.2383	79	750.35	16.559	0.1372
30	127.40	7.991	0.2366	80	766.97	16.696	0.1368
31	135.51	8.227	0.2347	81	783.74	16.833	0.1364
32	143.86	8.461	0.2325	82	800.64	16.969	0.1360
33	152.43	8.692	0.2302	83	817.68	17.105	0.1357
34	161.24	8.921	0.2276	84	834.85	17.241	0.1354
35	170.27	9.147	0.2249	85	852.16	17.376	0.1350
36	179.53	9.371	0.2220	86	869.60	17.511	0.1347
37	189.01	9.591	0.2190	87	887.18	17.645	0.1344
38	198.72	9.809	0.2160	88	904.89	17.779	0.1341
39	208.63	10.023	0.2128	89	922.74	17.913	0.1338
40	218.76	10.234	0.2096	90	940.72	18.047	0.1335
41	229.10	10.442	0.2063	91	958.85	18.180	0.1332
42	239.64	10.647	0.2030	92	977.08	18.314	0.1329
43	250.39	10.848	0.1997	93	995.46	18.446	0.1326
44	261.34	11.046	0.1965	94	1013.97	18.579	0.1324
45	272.48	11.241	0.1932	95	1032.62	18.711	0.1321
46	283.82	11.433	0.1901	96	1051.39	18.843	0.1318
47	295.35	11.621	0.1869	97	1070.30	18.975	0.1315
48	307.06	11.807	0.1839	98	1089.34	19.106	0.1312
49	318.96	11.989	0.1809	99	1108.51	19.237	0.1309
50	331.04	12.168	0.1780	100	1127.82	19.368	0.1306

Table A-1 Thermal voltage, thermopower, and thermopower derivative for thermocouple type T, copper vs constantan.

Temp. K	Voltage=E mV	$\frac{dE}{dT}=\bar{S}$	$\frac{dS}{dT}$		Temp. K	Voltage=E mV	$\frac{dE}{dT}=\bar{S}$	$\frac{dS}{dT}$
		mV/K	mV/K <sup>2</sup>				mV/K	mV/K <sup>2</sup>
101	1147.25	19.498	0.1304		151	2280.58	25.767	0.1214
102	1166.81	19.629	0.1301		152	2306.40	25.889	0.1212
103	1186.51	19.758	0.1298		153	2332.35	26.010	0.1209
104	1206.33	19.888	0.1295		154	2358.42	26.130	0.1207
105	1226.28	20.017	0.1292		155	2384.61	26.251	0.1205
106	1246.37	20.147	0.1290		156	2410.93	26.371	0.1202
107	1266.58	20.275	0.1287		157	2437.36	26.491	0.1200
108	1286.92	20.404	0.1285		158	2463.91	26.611	0.1197
109	1307.38	20.532	0.1282		159	2490.58	26.731	0.1194
110	1327.98	20.660	0.1280		160	2517.37	26.850	0.1192
111	1348.71	20.788	0.1277		161	2544.28	26.969	0.1189
112	1369.56	20.916	0.1275		162	2571.31	27.088	0.1186
113	1390.54	21.043	0.1273		163	2598.46	27.206	0.1183
114	1411.64	21.170	0.1270		164	2625.72	27.325	0.1181
115	1432.88	21.297	0.1268		165	2653.10	27.442	0.1178
116	1454.24	21.424	0.1266		166	2680.61	27.560	0.1175
117	1475.73	21.551	0.1264		167	2708.22	27.677	0.1172
118	1497.34	21.677	0.1263		168	2735.96	27.795	0.1169
119	1519.08	21.803	0.1261		169	2763.81	27.911	0.1167
120	1540.95	21.929	0.1259		170	2791.78	28.028	0.1164
121	1562.94	22.055	0.1257		171	2819.87	28.144	0.1161
122	1585.06	22.181	0.1256		172	2848.07	28.260	0.1158
123	1607.30	22.306	0.1254		173	2876.39	28.376	0.1156
124	1629.67	22.431	0.1253		174	2904.82	28.491	0.1153
125	1652.16	22.557	0.1252		175	2933.37	28.606	0.1151
126	1674.78	22.682	0.1250		176	2962.04	28.721	0.1148
127	1697.53	22.807	0.1249		177	2990.81	28.836	0.1146
128	1720.39	22.932	0.1248		178	3019.71	28.950	0.1143
129	1743.39	23.056	0.1247		179	3048.71	29.065	0.1141
130	1766.51	23.181	0.1245		180	3077.84	29.179	0.1139
131	1789.75	23.305	0.1244		181	3107.07	29.292	0.1136
132	1813.12	23.430	0.1243		182	3136.42	29.406	0.1134
133	1836.61	23.554	0.1242		183	3165.88	29.519	0.1132
134	1860.23	23.678	0.1241		184	3195.46	29.632	0.1130
135	1883.97	23.802	0.1240		185	3225.15	29.745	0.1128
136	1907.83	23.926	0.1238		186	3254.95	29.858	0.1126
137	1931.82	24.050	0.1237		187	3284.86	29.971	0.1124
138	1955.93	24.174	0.1236		188	3314.89	30.083	0.1123
139	1980.17	24.297	0.1235		189	3345.03	30.195	0.1121
140	2004.52	24.420	0.1233		190	3375.28	30.307	0.1119
141	2029.01	24.544	0.1232		191	3405.64	30.419	0.1117
142	2053.61	24.667	0.1230		192	3436.12	30.531	0.1116
143	2078.34	24.790	0.1229		193	3466.71	30.642	0.1114
144	2103.19	24.913	0.1227		194	3497.40	30.753	0.1112
145	2128.17	25.035	0.1226		195	3528.21	30.864	0.1110
146	2153.26	25.158	0.1224		196	3559.13	30.975	0.1108
147	2178.48	25.280	0.1222		197	3590.16	31.086	0.1107
148	2203.82	25.402	0.1220		198	3621.30	31.197	0.1105
149	2229.28	25.524	0.1218		199	3652.56	31.307	0.1103
150	2254.87	25.646	0.1216		200	3683.92	31.417	0.1101

Table A-1 (Cont.) Thermal voltage, thermopower, and thermopower derivative for thermocouple type T, copper vs constantan.

Temp. K	Voltage=E mV	$\frac{dE}{dT}=S$ mV/K	$\frac{dS}{dT}$ mV/K <sup>2</sup>	Temp. K	Voltage=E mV	$\frac{dE}{dT}=S$ mV/K	$\frac{dS}{dT}$ mV/K <sup>2</sup>
201	3715.39	31.527	0.1099	251	5423.15	36.677	0.0985
202	3746.97	31.637	0.1097	252	5459.87	36.776	0.0983
203	3778.66	31.746	0.1094	253	5496.69	36.874	0.0981
204	3810.46	31.856	0.1092	254	5533.52	36.972	0.0978
205	3842.38	31.965	0.1090	255	5570.34	37.070	0.0975
206	3874.39	32.074	0.1087	256	5607.75	37.167	0.0971
207	3906.52	32.182	0.1084	257	5644.97	37.264	0.0966
208	3938.76	32.291	0.1082	258	5682.28	37.360	0.0960
209	3971.10	32.399	0.1079	259	5719.69	37.456	0.0954
210	4003.56	32.506	0.1076	260	5757.20	37.551	0.0947
211	4036.12	32.614	0.1073	261	5794.79	37.645	0.0939
212	4068.78	32.721	0.1070	262	5832.49	37.739	0.0931
213	4101.56	32.828	0.1067	263	5870.27	37.831	0.0922
214	4134.44	32.934	0.1063	264	5908.15	37.923	0.0913
215	4167.43	33.040	0.1060	265	5946.12	38.014	0.0903
216	4200.52	33.146	0.1056	266	5984.17	38.103	0.0894
217	4233.72	33.252	0.1053	267	6022.32	38.193	0.0885
218	4267.02	33.357	0.1049	268	6060.56	38.281	0.0877
219	4300.43	33.462	0.1046	269	6098.88	38.368	0.0870
220	4333.95	33.566	0.1042	270	6137.30	38.455	0.0865
221	4367.56	33.670	0.1038	271	6175.79	38.541	0.0863
222	4401.29	33.774	0.1035	272	6214.37	38.627	0.0865
223	4435.11	33.877	0.1031	273	6253.05	38.714	0.0871
224	4469.04	33.980	0.1028	274	6291.80	38.802	0.0884
225	4503.07	34.083	0.1024	275	6330.65	38.891	0.0903
226	4537.21	34.185	0.1021	276	6369.59	38.983	0.0932
227	4571.44	34.287	0.1018	277	6408.62	39.078	0.0972
228	4605.78	34.388	0.1015	278	6447.74	39.178	0.1024
229	4640.22	34.490	0.1012	279	6486.97	39.283	0.1092
230	4674.76	34.591	0.1009	280	6526.31	39.397	0.1178
231	4709.40	34.691	0.1006				
232	4744.14	34.792	0.1004				
233	4778.98	34.892	0.1001				
234	4813.93	34.992	0.0999				
235	4848.97	35.092	0.0998				
236	4884.11	35.192	0.0996				
237	4919.35	35.291	0.0995				
238	4954.69	35.391	0.0994				
239	4990.13	35.490	0.0993				
240	5025.67	35.589	0.0992				
241	5061.31	35.688	0.0991				
242	5097.05	35.787	0.0991				
243	5132.89	35.886	0.0990				
244	5168.82	35.986	0.0990				
245	5204.86	36.084	0.0990				
246	5240.99	36.183	0.0989				
247	5277.22	36.282	0.0989				
248	5313.55	36.381	0.0988				
249	5349.99	36.480	0.0987				
250	5386.51	36.579	0.0986				

Table A-1 (Cont.) Thermal voltage, thermopower, and thermopower derivative for thermocouple type T, copper vs constantan.

**Appendix B.**

**Interim Tables and Graphs for Thermocouple Type E,  
Chromel vs Constantan.**

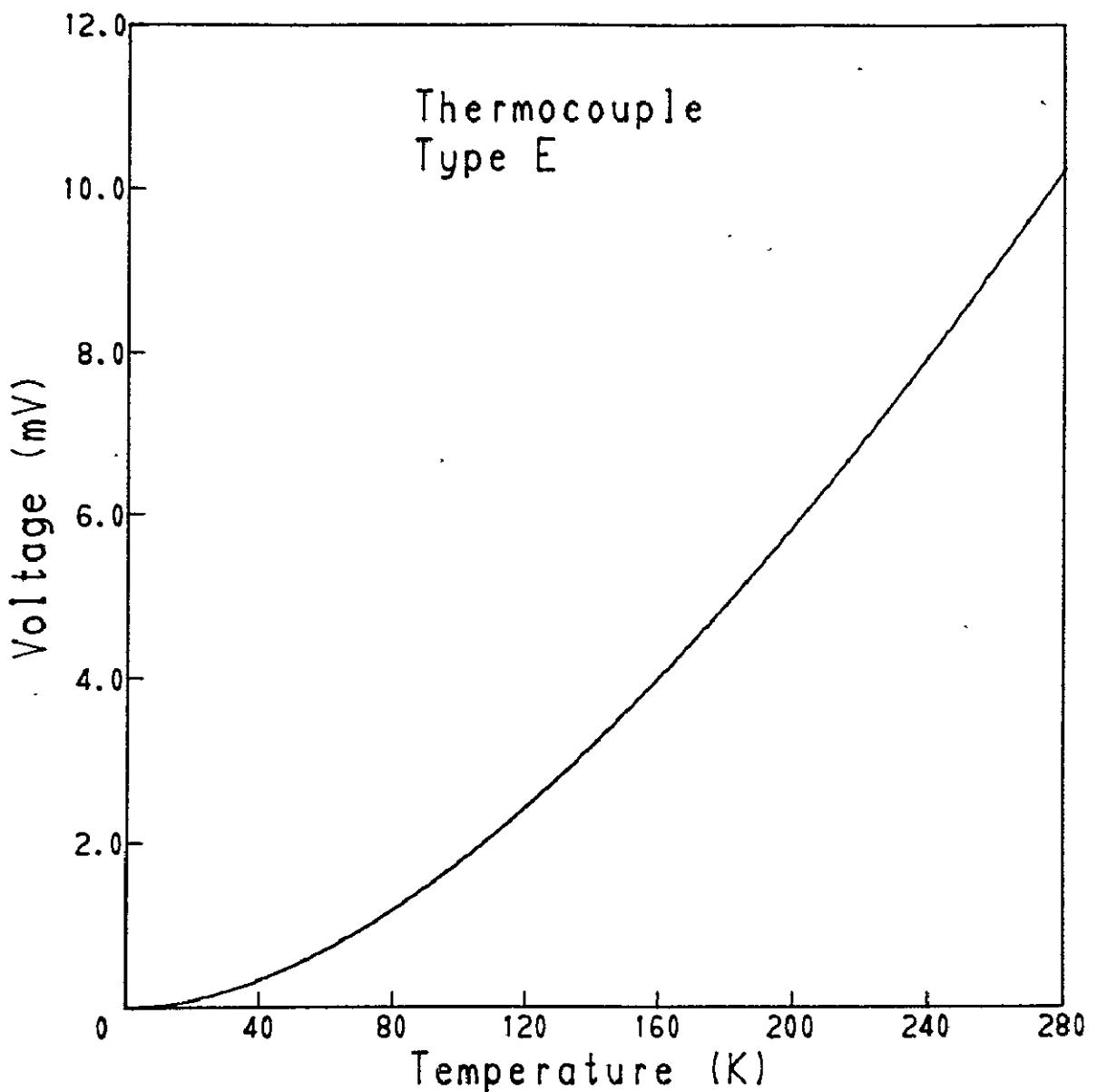


Figure B-1 Thermoelectric voltage of thermocouple type E, Chromel versus constantan.

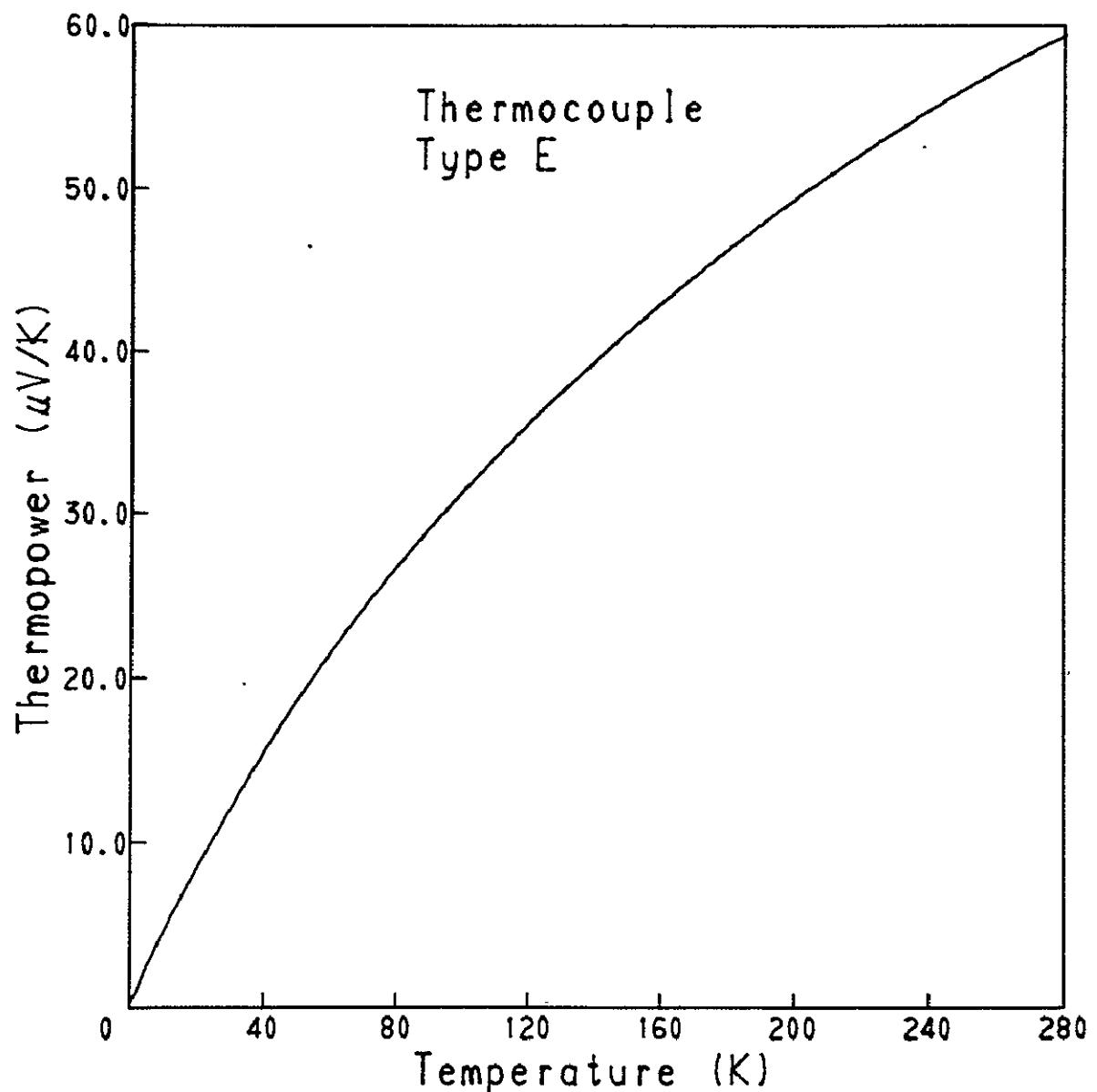


Figure B-2 Thermopower of thermocouple type E,  
Chromel versus constantan.

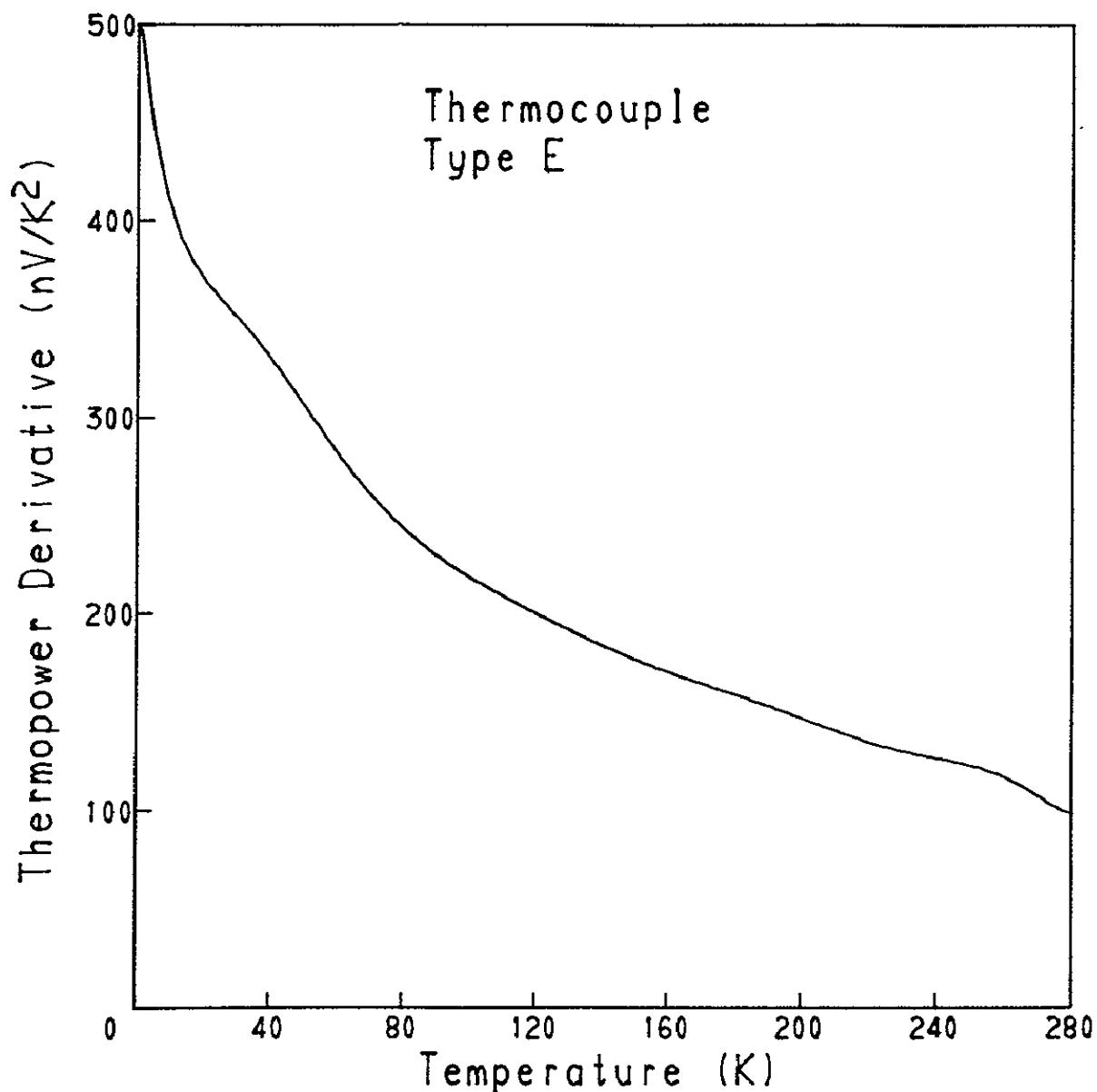


Figure B-3 Thermopower derivative of thermocouple  
type E, Chromel versus constantan.

Temp. K	Voltage E uV	$\frac{dE}{dT} \times S$ uV/K	$\frac{dS}{dT}$ uV/K <sup>2</sup>	Temp. K	Voltage E uV	$\frac{dE}{dT} \times S$ uV/K	$\frac{dS}{dT}$ uV/K <sup>2</sup>
1	0.41	0.660	0.4962	51	522.68	19.001	0.3032
2	1.31	1.149	0.4812	52	541.83	19.303	0.3007
3	2.70	1.623	0.4678	53	561.28	19.603	0.2982
4	4.56	2.085	0.4557	54	581.04	19.900	0.2957
5	6.87	2.535	0.4449	55	601.08	20.194	0.2933
6	9.62	2.975	0.4353	56	621.42	20.486	0.2908
7	12.81	3.406	0.4267	57	642.05	20.776	0.2884
8	16.43	3.829	0.4190	58	662.97	21.063	0.2860
9	20.47	4.244	0.4122	59	684.18	21.348	0.2836
10	24.92	4.653	0.4061	60	705.67	21.630	0.2813
11	29.77	5.057	0.4006	61	727.44	21.911	0.2790
12	35.03	5.455	0.3957	62	749.49	22.188	0.2767
13	40.68	5.848	0.3914	63	771.82	22.464	0.2745
14	46.72	6.238	0.3875	64	794.42	22.737	0.2722
15	53.15	6.623	0.3839	65	817.29	23.008	0.2701
16	59.97	7.005	0.3807	66	840.43	23.277	0.2679
17	67.16	7.385	0.3778	67	863.84	23.544	0.2658
18	74.74	7.761	0.3751	68	887.52	23.809	0.2638
19	82.69	8.135	0.3726	69	911.46	24.072	0.2618
20	91.01	8.506	0.3703	70	935.66	24.333	0.2598
21	99.70	8.876	0.3681	71	960.13	24.592	0.2579
22	108.76	9.243	0.3660	72	984.85	24.849	0.2560
23	118.18	9.608	0.3640	73	1009.82	25.104	0.2542
24	127.97	9.971	0.3621	74	1035.05	25.357	0.2524
25	138.12	10.332	0.3602	75	1060.54	25.608	0.2506
26	148.64	10.691	0.3584	76	1086.27	25.858	0.2489
27	159.51	11.049	0.3565	77	1112.25	26.106	0.2473
28	170.73	11.404	0.3546	78	1138.48	26.353	0.2456
29	182.31	11.758	0.3528	79	1164.96	26.598	0.2441
30	194.25	12.110	0.3509	80	1191.68	26.841	0.2425
31	206.53	12.460	0.3490	81	1218.64	27.083	0.2410
32	219.17	12.808	0.3470	82	1245.84	27.323	0.2395
33	232.15	13.154	0.3450	83	1273.28	27.562	0.2381
34	245.47	13.498	0.3430	84	1300.96	27.799	0.2367
35	259.14	13.840	0.3409	85	1328.88	28.035	0.2354
36	273.15	14.179	0.3388	86	1357.03	28.270	0.2340
37	287.50	14.517	0.3366	87	1385.42	28.503	0.2327
38	302.19	14.853	0.3344	88	1414.04	28.735	0.2315
39	317.20	15.186	0.3322	89	1442.89	28.966	0.2302
40	332.56	15.517	0.3299	90	1471.97	29.196	0.2290
41	348.24	15.846	0.3276	91	1501.28	29.424	0.2279
42	364.25	16.172	0.3253	92	1530.82	29.652	0.2267
43	380.58	16.496	0.3229	93	1560.59	29.878	0.2256
44	397.24	16.818	0.3205	94	1590.58	30.103	0.2245
45	414.22	17.137	0.3181	95	1620.79	30.327	0.2234
46	431.51	17.454	0.3156	96	1651.23	30.549	0.2223
47	449.13	17.769	0.3131	97	1681.89	30.771	0.2213
48	467.05	18.081	0.3107	98	1712.77	30.992	0.2202
49	485.29	18.390	0.3082	99	1743.87	31.212	0.2192
50	503.83	18.697	0.3057	100	1775.19	31.430	0.2182

Table B-1 Thermal voltage, thermopower, and thermopower derivative for thermocouple type E, Chromel vs constantan.

Temp. K	Voltage=E uV	$\frac{dE}{dT}=S$ uV/K	$\frac{dS}{dT}$ uV/K <sup>2</sup>	Temp. K	Voltage=E uV	$\frac{dE}{dT}=S$ uV/K	$\frac{dS}{dT}$ uV/K <sup>2</sup>
101	1806.73	31.648	0.2172	151	3642.12	41.423	0.1760
102	1838.49	31.865	0.2162	152	3683.63	41.599	0.1754
103	1870.46	32.081	0.2153	153	3725.31	41.774	0.1747
104	1902.65	32.295	0.2143	154	3767.18	41.948	0.1741
105	1935.05	32.509	0.2134	155	3809.21	42.122	0.1734
106	1967.67	32.722	0.2125	156	3851.42	42.295	0.1728
107	2000.50	32.934	0.2115	157	3893.80	42.467	0.1722
108	2033.54	33.145	0.2106	158	3936.35	42.639	0.1716
109	2066.79	33.355	0.2097	159	3979.08	42.811	0.1709
110	2100.25	33.565	0.2088	160	4021.97	42.981	0.1703
111	2133.92	33.773	0.2079	161	4065.04	43.151	0.1697
112	2167.79	33.981	0.2070	162	4108.28	43.321	0.1692
113	2201.88	34.187	0.2062	163	4151.68	43.490	0.1686
114	2236.17	34.393	0.2053	164	4195.26	43.658	0.1680
115	2270.66	34.598	0.2044	165	4239.00	43.825	0.1674
116	2305.36	34.802	0.2035	166	4282.91	43.993	0.1668
117	2340.27	35.005	0.2027	167	4326.98	44.159	0.1663
118	2375.37	35.207	0.2018	168	4371.22	44.325	0.1657
119	2410.68	35.408	0.2009	169	4415.63	44.491	0.1651
120	2446.19	35.609	0.2001	170	4460.21	44.655	0.1646
121	2481.90	35.809	0.1992	171	4504.94	44.820	0.1640
122	2517.81	36.007	0.1984	172	4549.84	44.984	0.1635
123	2553.91	36.205	0.1975	173	4594.91	45.147	0.1629
124	2590.22	36.402	0.1967	174	4640.14	45.309	0.1624
125	2626.72	36.599	0.1958	175	4685.53	45.471	0.1618
126	2663.41	36.794	0.1950	176	4731.08	45.633	0.1613
127	2700.30	36.989	0.1942	177	4776.79	45.794	0.1607
128	2737.39	37.182	0.1933	178	4822.67	45.954	0.1601
129	2774.67	37.375	0.1925	179	4868.70	46.114	0.1596
130	2812.14	37.567	0.1917	180	4914.90	46.274	0.1590
131	2849.80	37.759	0.1909	181	4961.25	46.432	0.1585
132	2887.66	37.949	0.1901	182	5007.76	46.590	0.1579
133	2925.70	38.139	0.1893	183	5054.43	46.748	0.1573
134	2963.94	38.328	0.1885	184	5101.26	46.905	0.1567
135	3002.36	38.516	0.1877	185	5148.24	47.061	0.1562
136	3040.97	38.703	0.1869	186	5195.38	47.217	0.1556
137	3079.76	38.890	0.1861	187	5242.67	47.373	0.1550
138	3118.75	39.075	0.1854	188	5290.12	47.527	0.1544
139	3157.91	39.260	0.1846	189	5337.73	47.681	0.1538
140	3197.27	39.445	0.1838	190	5385.49	47.835	0.1532
141	3236.80	39.628	0.1831	191	5433.40	47.988	0.1526
142	3276.52	39.811	0.1823	192	5481.46	48.140	0.1520
143	3316.42	39.993	0.1816	193	5529.68	48.292	0.1514
144	3356.51	40.174	0.1809	194	5578.05	48.443	0.1508
145	3396.77	40.355	0.1802	195	5626.56	48.593	0.1502
146	3437.22	40.534	0.1795	196	5675.23	48.743	0.1495
147	3477.84	40.713	0.1787	197	5724.05	48.893	0.1489
148	3518.64	40.892	0.1781	198	5773.02	49.041	0.1483
149	3559.62	41.070	0.1774	199	5822.13	49.189	0.1477
150	3600.78	41.247	0.1767	200	5871.40	49.336	0.1470

Table B-1 (Cont.) Thermal voltage, thermopower, and thermopower derivative for thermocouple type E, Chromel vs constantan.

Temp. K	Voltage E mV	$\frac{dE}{dT} \# S$ mV/K	$\frac{dS}{dT}$ mV/K <sup>2</sup>	Temp. K	Voltage E mV	$\frac{dE}{dT} \# S$ mV/K	$\frac{dS}{dT}$ mV/K <sup>2</sup>
201	5920.81	49.483	0.1464	251	8566.06	56.133	0.1225
202	5970.36	49.629	0.1458	252	8622.25	56.255	0.1220
203	6020.06	49.775	0.1451	253	8678.57	56.377	0.1215
204	6069.91	49.919	0.1445	254	8735.01	56.498	0.1210
205	6119.90	50.064	0.1439	255	8791.56	56.619	0.1204
206	6170.04	50.207	0.1432	256	8848.24	56.739	0.1198
207	6220.32	50.350	0.1426	257	8905.04	56.858	0.1191
208	6270.74	50.492	0.1420	258	8961.96	56.977	0.1184
209	6321.30	50.634	0.1413	259	9019.00	57.095	0.1177
210	6372.01	50.775	0.1407	260	9076.15	57.212	0.1169
211	6422.85	50.915	0.1401	261	9133.42	57.329	0.1161
212	6473.84	51.055	0.1395	262	9190.81	57.445	0.1152
213	6524.96	51.194	0.1389	263	9248.31	57.559	0.1143
214	6576.22	51.333	0.1383	264	9305.93	57.673	0.1134
215	6627.63	51.471	0.1377	265	9363.66	57.786	0.1124
216	6679.17	51.608	0.1371	266	9421.50	57.898	0.1114
217	6730.84	51.745	0.1366	267	9479.45	58.009	0.1103
218	6782.66	51.882	0.1360	268	9537.51	58.119	0.1093
219	6834.61	52.017	0.1355	269	9595.69	58.227	0.1082
220	6886.69	52.152	0.1349	270	9653.97	58.335	0.1071
221	6938.91	52.287	0.1344	271	9712.36	58.442	0.1060
222	6991.27	52.421	0.1339	272	9770.85	58.547	0.1049
223	7043.75	52.555	0.1334	273	9829.45	58.651	0.1038
224	7096.38	52.688	0.1329	274	9888.15	58.755	0.1028
225	7149.13	52.821	0.1324	275	9946.96	58.857	0.1018
226	7202.02	52.953	0.1320	276	10005.87	58.958	0.1009
227	7255.04	53.085	0.1315	277	10064.88	59.059	0.1001
228	7308.19	53.216	0.1311	278	10123.98	59.159	0.0994
229	7361.47	53.347	0.1306	279	10183.19	59.258	0.0989
230	7414.88	53.477	0.1302	280	10242.50	59.356	0.0985
231	7468.42	53.607	0.1298				
232	7522.09	53.737	0.1295				
233	7575.89	53.866	0.1291				
234	7629.83	53.995	0.1287				
235	7683.88	54.124	0.1284				
236	7738.07	54.252	0.1280				
237	7792.39	54.380	0.1277				
238	7846.83	54.507	0.1273				
239	7901.40	54.634	0.1270				
240	7956.10	54.761	0.1267				
241	8010.92	54.888	0.1263				
242	8065.87	55.014	0.1260				
243	8120.95	55.140	0.1257				
244	8176.15	55.265	0.1253				
245	8231.48	55.390	0.1250				
246	8286.93	55.515	0.1246				
247	8342.51	55.639	0.1242				
248	8398.21	55.763	0.1238				
249	8454.04	55.887	0.1234				
250	8509.99	56.010	0.1230				

Table B-1 (Cont.) Thermal voltage, thermopower, and thermopower derivative for thermocouple type E, Chromel vs constantan.

**Appendix C.**

**Interim Tables and Graphs for Thermocouple Type K,  
Chromel vs Alumel.**

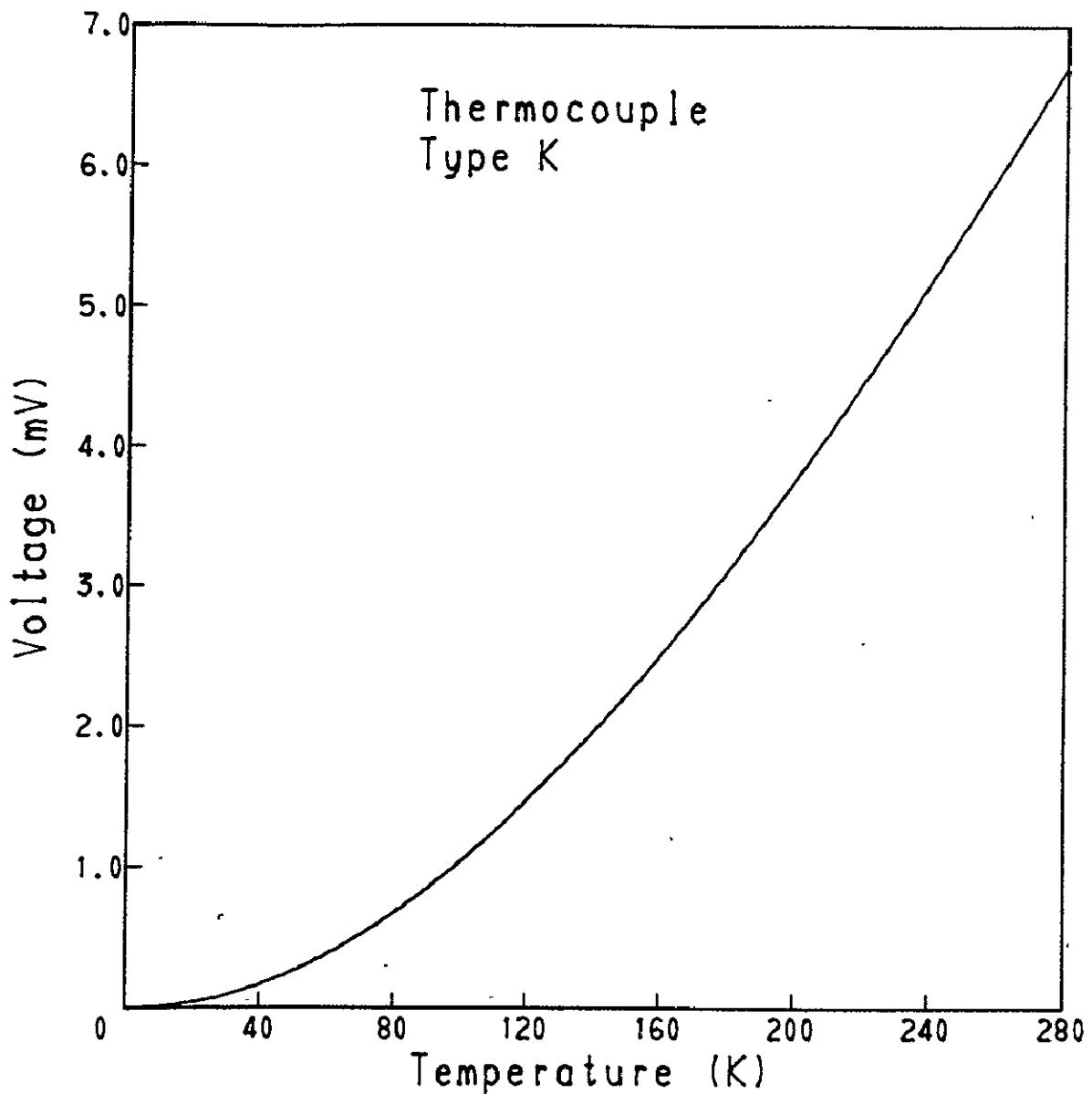


Figure C-1 Thermoelectric voltage of thermocouple type K, Chromel versus Alumel.

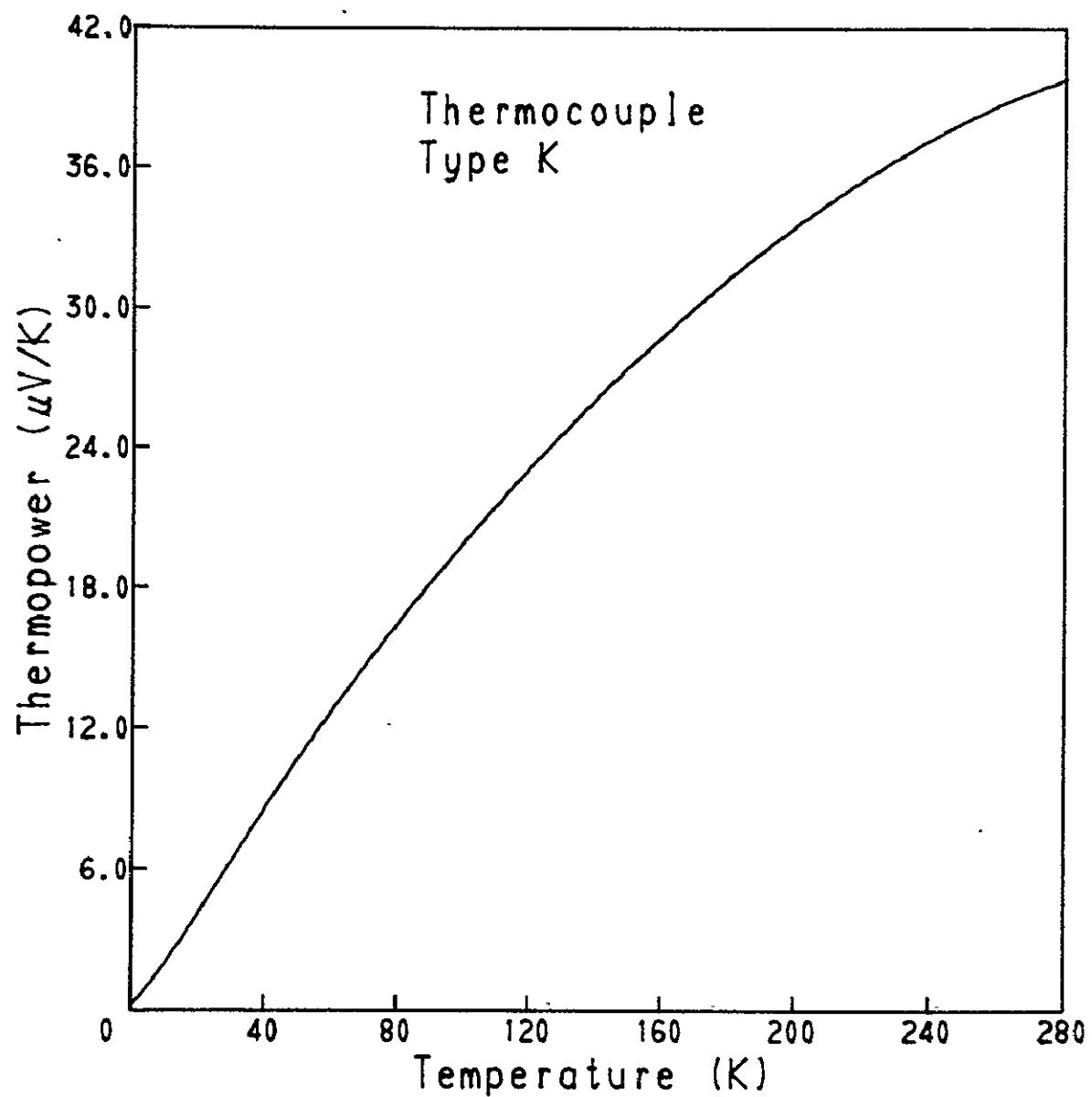


Figure C-2 Thermopower of thermocouple type K,  
Chromel versus Alumel.

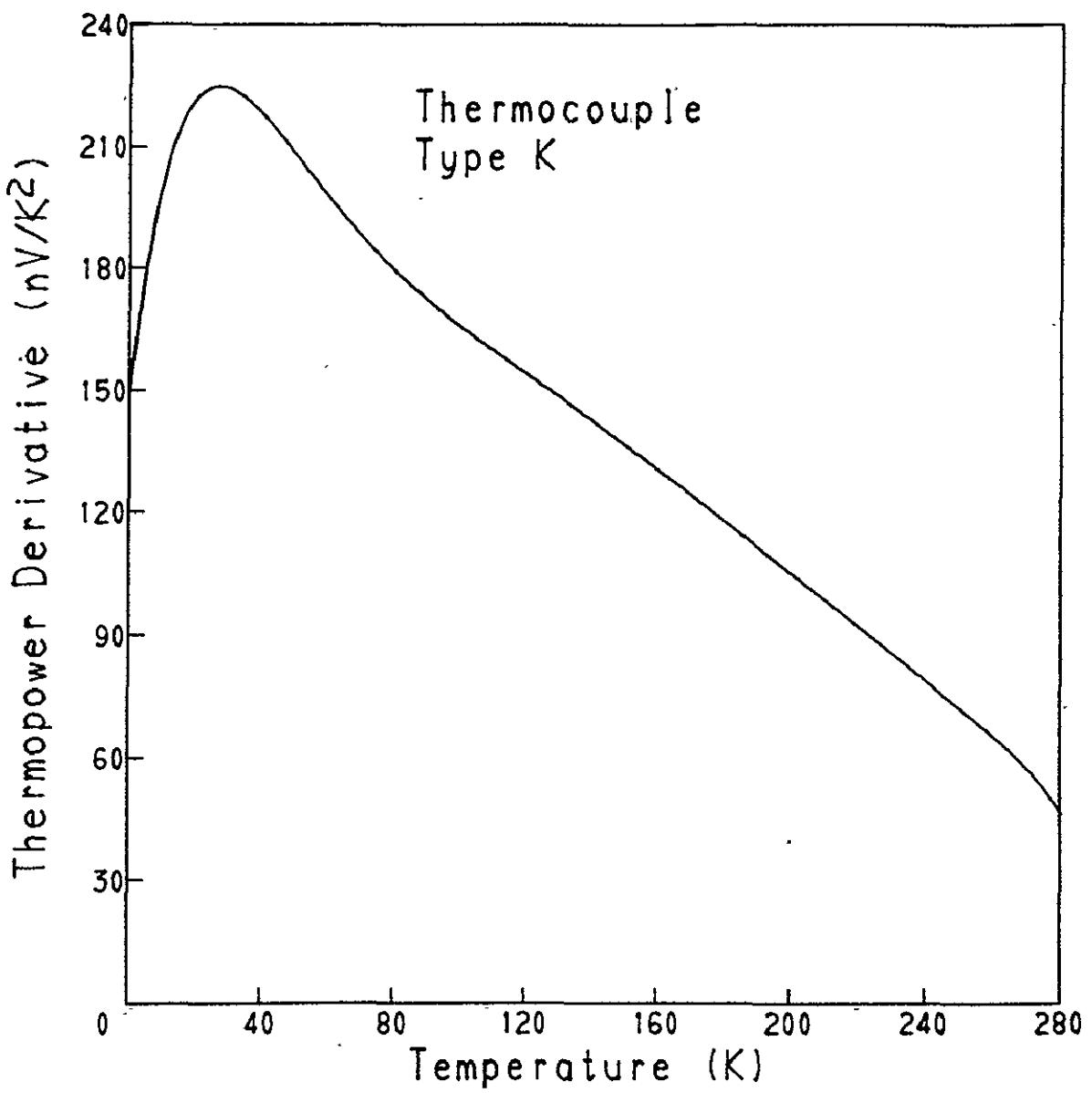


Figure C-3 Thermopower derivative of thermocouple  
type K, Chromel versus Alumel.

Temp. K	Voltage=E mV	$\frac{dE}{dT} = S$ mV/K	$\frac{dS}{dT}$ mV/K <sup>2</sup>	Temp. K	Voltage=E mV	$\frac{dE}{dT} = S$ mV/K	$\frac{dS}{dT}$ mV/K <sup>2</sup>
1	0.30	0.382	0.1559	51	276.73	10.940	0.2066
2	0.77	0.541	0.1627	52	287.77	11.146	0.2056
3	1.39	0.707	0.1689	53	299.02	11.351	0.2045
4	2.18	0.879	0.1748	54	310.47	11.555	0.2035
5	3.15	1.056	0.1801	55	322.13	11.758	0.2024
6	4.30	1.239	0.1851	56	333.99	11.960	0.2013
7	5.63	1.426	0.1897	57	346.05	12.161	0.2003
8	7.15	1.618	0.1939	58	358.31	12.360	0.1993
9	8.86	1.814	0.1978	59	370.77	12.559	0.1982
10	10.78	2.014	0.2013	60	383.43	12.757	0.1972
11	12.89	2.217	0.2045	61	396.28	12.953	0.1962
12	15.21	2.423	0.2075	62	409.33	13.149	0.1952
13	17.74	2.631	0.2101	63	422.58	13.344	0.1942
14	20.48	2.843	0.2124	64	436.02	13.537	0.1932
15	23.42	3.056	0.2146	65	449.65	13.730	0.1922
16	26.59	3.272	0.2164	66	463.48	13.922	0.1912
17	29.97	3.489	0.2181	67	477.50	14.113	0.1903
18	33.57	3.708	0.2195	68	491.70	14.302	0.1894
19	37.38	3.928	0.2207	69	506.10	14.491	0.1884
20	41.42	4.149	0.2218	70	520.69	14.679	0.1875
21	45.68	4.371	0.2227	71	535.46	14.866	0.1866
22	50.17	4.594	0.2234	72	550.42	15.053	0.1857
23	54.87	4.818	0.2239	73	565.56	15.238	0.1849
24	59.80	5.042	0.2243	74	580.89	15.422	0.1840
25	64.96	5.267	0.2246	75	596.41	15.606	0.1832
26	70.34	5.491	0.2247	76	612.11	15.789	0.1823
27	75.94	5.716	0.2248	77	627.99	15.971	0.1815
28	81.77	5.941	0.2247	78	644.05	16.152	0.1807
29	87.82	6.165	0.2245	79	660.29	16.332	0.1799
30	94.10	6.390	0.2242	80	676.71	16.512	0.1791
31	100.60	6.614	0.2239	81	693.31	16.690	0.1784
32	107.33	6.837	0.2234	82	710.09	16.868	0.1776
33	114.28	7.061	0.2229	83	727.05	17.046	0.1769
34	121.45	7.283	0.2223	84	744.18	17.222	0.1761
35	128.84	7.505	0.2217	85	761.49	17.398	0.1754
36	136.46	7.727	0.2210	86	778.98	17.573	0.1747
37	144.29	7.947	0.2202	87	796.64	17.747	0.1740
38	152.35	8.167	0.2194	88	814.47	17.921	0.1733
39	160.63	8.386	0.2186	89	832.48	18.094	0.1726
40	169.12	8.604	0.2177	90	850.66	18.266	0.1719
41	177.84	8.821	0.2168	91	869.01	18.438	0.1712
42	186.77	9.038	0.2159	92	887.53	18.608	0.1706
43	195.91	9.253	0.2149	93	906.23	18.779	0.1699
44	205.27	9.468	0.2139	94	925.09	18.948	0.1693
45	214.85	9.681	0.2129	95	944.13	19.117	0.1686
46	224.63	9.893	0.2119	96	963.33	19.286	0.1680
47	234.63	10.105	0.2109	97	982.70	19.453	0.1674
48	244.84	10.315	0.2098	98	1002.23	19.620	0.1667
49	255.26	10.524	0.2088	99	1021.94	19.787	0.1661
50	265.89	10.733	0.2077	100	1041.81	19.952	0.1655

Table C-1 Thermal voltage, thermopower, and thermopower derivative for thermocouple type K, Chromel vs Alumel.

Temp. K	Voltage=E mV	$\frac{dE}{dT} = S$ mV/K	$\frac{dS}{dT}$ mV/K <sup>2</sup>	Temp. K	Voltage=E mV	$\frac{dE}{dT} = S$ mV/K	$\frac{dS}{dT}$ mV/K <sup>2</sup>
101	1061.84	20.118	0.1649	151	2261.72	27.636	0.1357
102	1082.04	20.282	0.1643	152	2289.42	27.772	0.1351
103	1102.41	20.446	0.1637	153	2317.26	27.906	0.1345
104	1122.93	20.610	0.1631	154	2345.23	28.041	0.1339
105	1143.62	20.772	0.1625	155	2373.34	28.174	0.1333
106	1164.48	20.935	-0.1619	156	2401.58	28.307	0.1327
107	1185.49	21.096	0.1613	157	2429.96	28.440	0.1321
108	1206.67	21.257	0.1607	158	2458.46	28.572	0.1315
109	1228.01	21.418	0.1602	159	2487.10	28.703	0.1309
110	1249.51	21.578	0.1596	160	2515.87	28.833	0.1303
111	1271.16	21.737	0.1590	161	2544.77	28.963	0.1297
112	1292.98	21.896	0.1584	162	2573.79	29.093	0.1291
113	1314.95	22.054	0.1579	163	2602.95	29.222	0.1285
114	1337.09	22.211	0.1573	164	2632.24	29.350	0.1278
115	1359.38	22.368	0.1567	165	2661.65	29.477	0.1272
116	1381.82	22.525	0.1561	166	2691.19	29.604	0.1266
117	1404.43	22.681	0.1556	167	2720.86	29.730	0.1260
118	1427.18	22.836	0.1550	168	2750.65	29.856	0.1254
119	1450.10	22.991	0.1544	169	2780.57	29.981	0.1248
120	1473.16	23.145	0.1538	170	2810.61	30.106	0.1241
121	1496.39	23.298	0.1533	171	2840.78	30.229	0.1235
122	1519.76	23.451	0.1527	172	2871.07	30.353	0.1229
123	1543.29	23.604	0.1521	173	2901.49	30.475	0.1223
124	1566.97	23.756	0.1516	174	2932.02	30.597	0.1217
125	1590.80	23.907	0.1510	175	2962.68	30.719	0.1210
126	1614.78	24.058	0.1504	176	2993.46	30.839	0.1204
127	1638.91	24.208	0.1498	177	3024.36	30.959	0.1198
128	1663.20	24.357	0.1493	178	3055.38	31.079	0.1192
129	1687.63	24.506	0.1487	179	3086.52	31.198	0.1185
130	1712.21	24.655	0.1481	180	3117.77	31.316	0.1179
131	1736.94	24.802	0.1475	181	3149.15	31.433	0.1173
132	1761.81	24.950	0.1470	182	3180.64	31.550	0.1166
133	1786.84	25.096	0.1464	183	3212.25	31.667	0.1160
134	1812.01	25.242	0.1458	184	3243.97	31.782	0.1154
135	1837.32	25.388	0.1452	185	3275.81	31.898	0.1147
136	1862.78	25.533	0.1446	186	3307.77	32.012	0.1141
137	1888.39	25.677	0.1441	187	3339.84	32.126	0.1135
138	1914.14	25.821	0.1435	188	3372.02	32.239	0.1128
139	1940.03	25.964	0.1429	189	3404.32	32.351	0.1122
140	1966.06	26.107	0.1423	190	3436.72	32.463	0.1116
141	1992.24	26.249	0.1417	191	3469.24	32.575	0.1109
142	2018.56	26.390	0.1411	192	3501.87	32.685	0.1103
143	2045.02	26.531	0.1405	193	3534.61	32.795	0.1097
144	2071.62	26.671	0.1399	194	3567.46	32.905	0.1090
145	2098.37	26.811	0.1393	195	3600.42	33.013	0.1084
146	2125.25	26.950	0.1387	196	3633.49	33.121	0.1077
147	2152.26	27.088	0.1381	197	3666.66	33.229	0.1071
148	2179.42	27.226	0.1375	198	3699.95	33.335	0.1064
149	2206.72	27.363	0.1370	199	3733.33	33.442	0.1058
150	2234.15	27.500	0.1364	200	3766.83	33.547	0.1052

Table C-1 (Cont.) Thermal voltage, thermopower, and thermopower derivative for thermocouple type K, Chromel vs Alumel.

Temp. K	Voltage=E μV	$\frac{dE}{dT}=S$ μV/K	$\frac{dS}{dT}$ μV/K <sup>2</sup>	Temp. K	Voltage=E μV	$\frac{dE}{dT}=S$ μV/K	$\frac{dS}{dT}$ μV/K <sup>2</sup>
201	3800.43	33.652	0.1045	251	5600.01	38.058	0.0717
202	3834.13	33.756	0.1039	252	5638.10	38.129	0.0710
203	3867.94	33.860	0.1032	253	5676.26	38.200	0.0703
204	3901.85	33.962	0.1026	254	5714.50	38.270	0.0696
205	3935.86	34.065	0.1019	255	5752.80	38.339	0.0690
206	3969.98	34.166	0.1013	256	5791.18	38.407	0.0683
207	4004.20	34.267	0.1006	257	5829.62	38.475	0.0676
208	4038.51	34.367	0.0999	258	5868.13	38.543	0.0669
209	4072.93	34.467	0.0993	259	5906.70	38.609	0.0661
210	4107.45	34.566	0.0986	260	5945.34	38.675	0.0654
211	4142.06	34.664	0.0980	261	5984.05	38.740	0.0647
212	4176.78	34.762	0.0973	262	6022.82	38.804	0.0639
213	4211.59	34.859	0.0967	263	6061.66	38.868	0.0632
214	4246.49	34.955	0.0960	264	6100.56	38.931	0.0624
215	4281.50	35.051	0.0954	265	6139.52	38.993	0.0616
216	4316.60	35.146	0.0947	266	6178.54	39.054	0.0608
217	4351.79	35.240	0.0940	267	6217.63	39.114	0.0600
218	4387.08	35.334	0.0934	268	6256.77	39.174	0.0591
219	4422.46	35.427	0.0927	269	6295.97	39.232	0.0582
220	4457.93	35.520	0.0921	270	6335.24	39.290	0.0573
221	4493.50	35.611	0.0914	271	6374.55	39.347	0.0564
222	4529.15	35.702	0.0907	272	6413.93	39.403	0.0554
223	4564.90	35.793	0.0901	273	6453.36	39.458	0.0544
224	4600.74	35.883	0.0894	274	6492.84	39.512	0.0534
225	4636.67	35.972	0.0888	275	6532.38	39.565	0.0523
226	4672.68	36.060	0.0881	276	6571.97	39.616	0.0512
227	4708.79	36.148	0.0874	277	6611.62	39.667	0.0501
228	4744.98	36.235	0.0868	278	6651.31	39.716	0.0489
229	4781.25	36.321	0.0861	279	6691.05	39.765	0.0476
230	4817.62	36.407	0.0855	280	6730.84	39.812	0.0463
231	4854.07	36.492	0.0848				
232	4890.60	36.577	0.0842				
233	4927.22	36.661	0.0835				
234	4963.93	36.744	0.0828				
235	5000.71	36.826	0.0822				
236	5037.58	36.908	0.0815				
237	5074.53	36.989	0.0809				
238	5111.56	37.070	0.0802				
239	5148.67	37.150	0.0796				
240	5185.86	37.229	0.0789				
241	5223.12	37.308	0.0783				
242	5260.47	37.386	0.0776				
243	5297.90	37.463	0.0770				
244	5335.40	37.540	0.0763				
245	5372.97	37.616	0.0756				
246	5410.63	37.691	0.0750				
247	5448.36	37.766	0.0743				
248	5486.16	37.840	0.0737				
249	5524.04	37.913	0.0730				
250	5561.98	37.986	0.0723				

Table C-1 (Cont.) Thermal voltage, thermopower, and thermopower derivative for thermocouple type K, Chromel vs Alumel.

Appendix D.

Preliminary Tables and Graphs for Chromel vs Gold-0.07  
Atomic Percent Iron

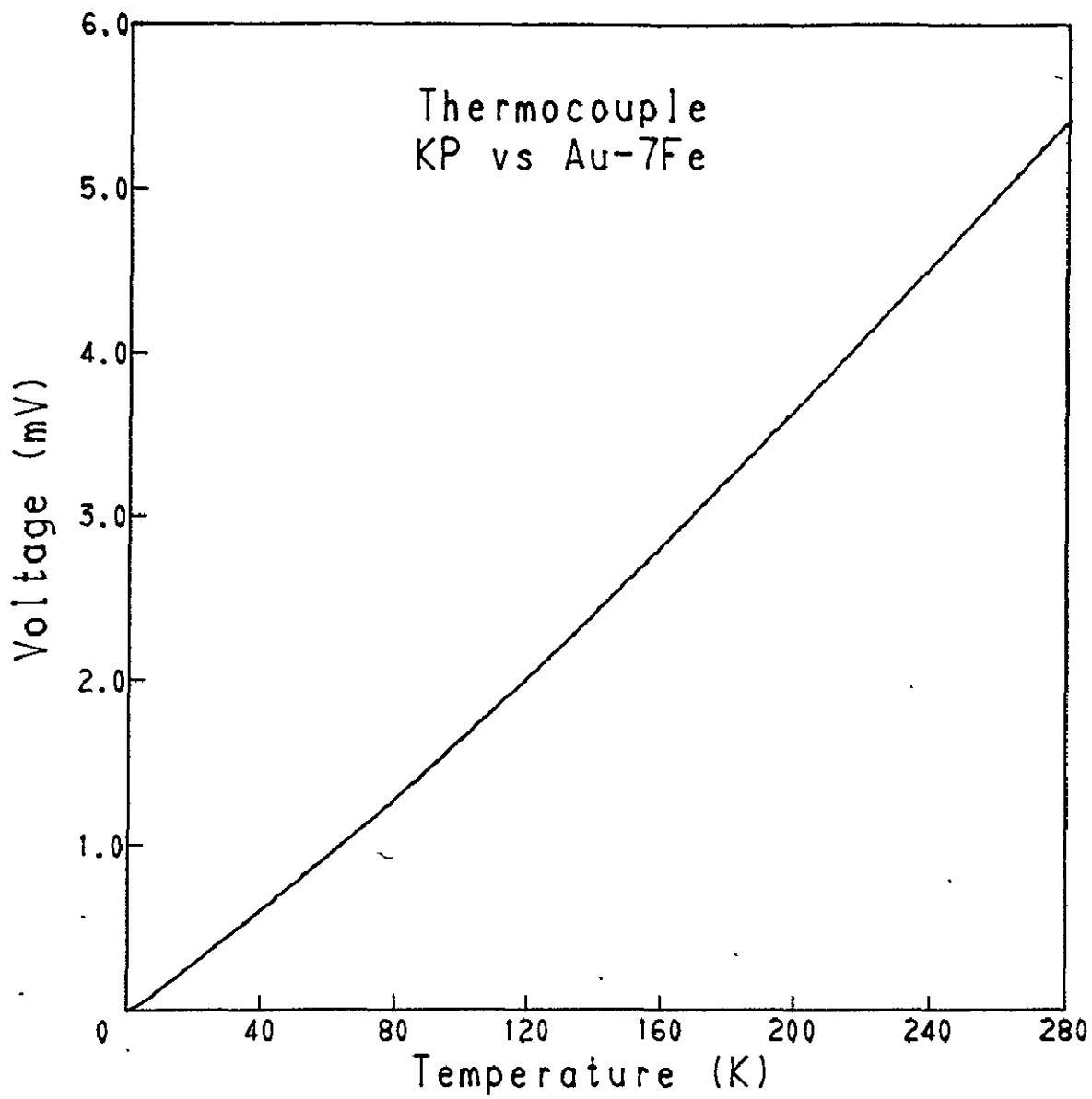


Figure D-1 Thermoelectric voltage of Chromel versus  
gold-0.07 at. % Fe.

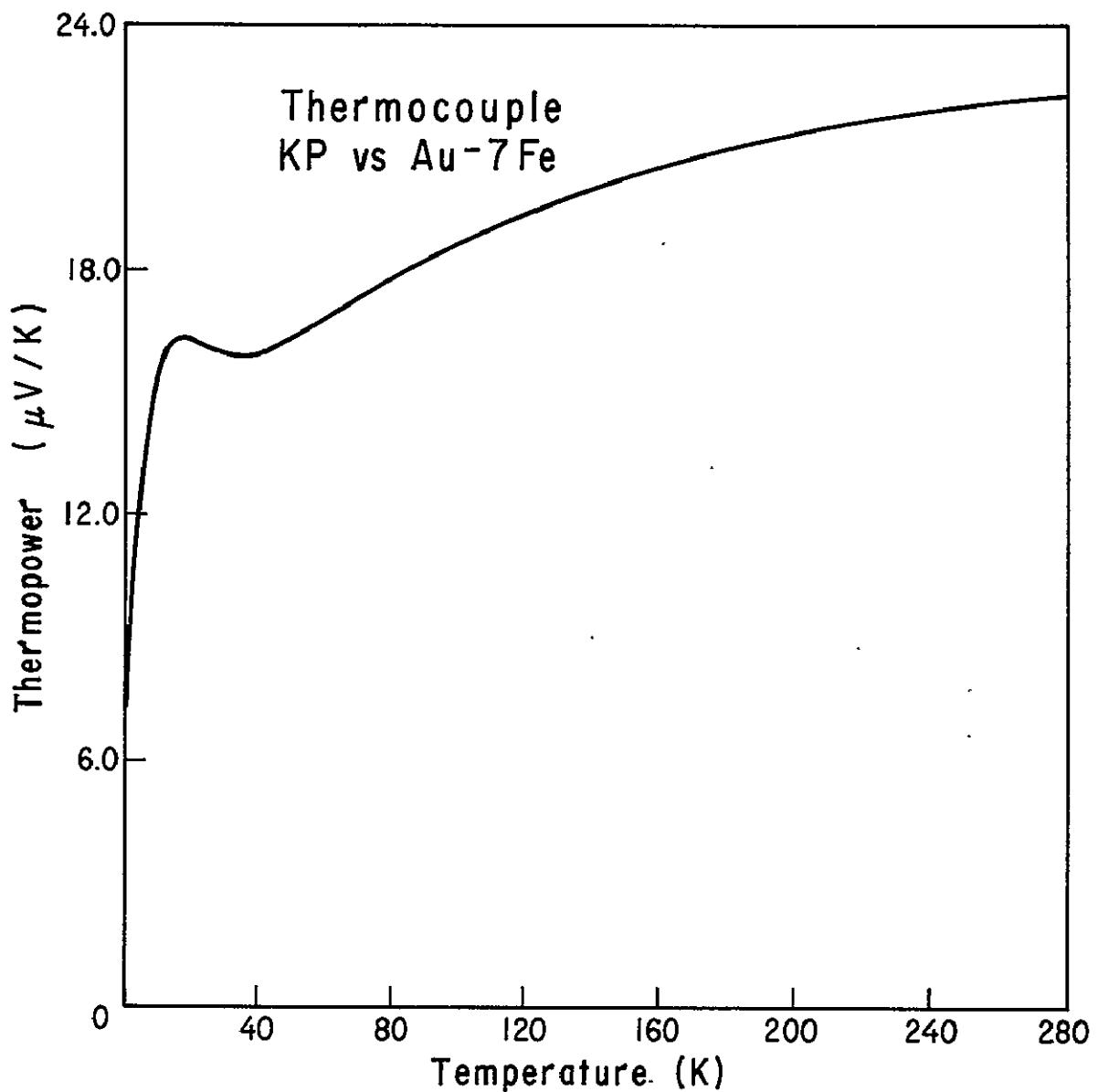


Figure D-2 Thermopower of Chromel versus  
gold-0.07 at. % Fe.

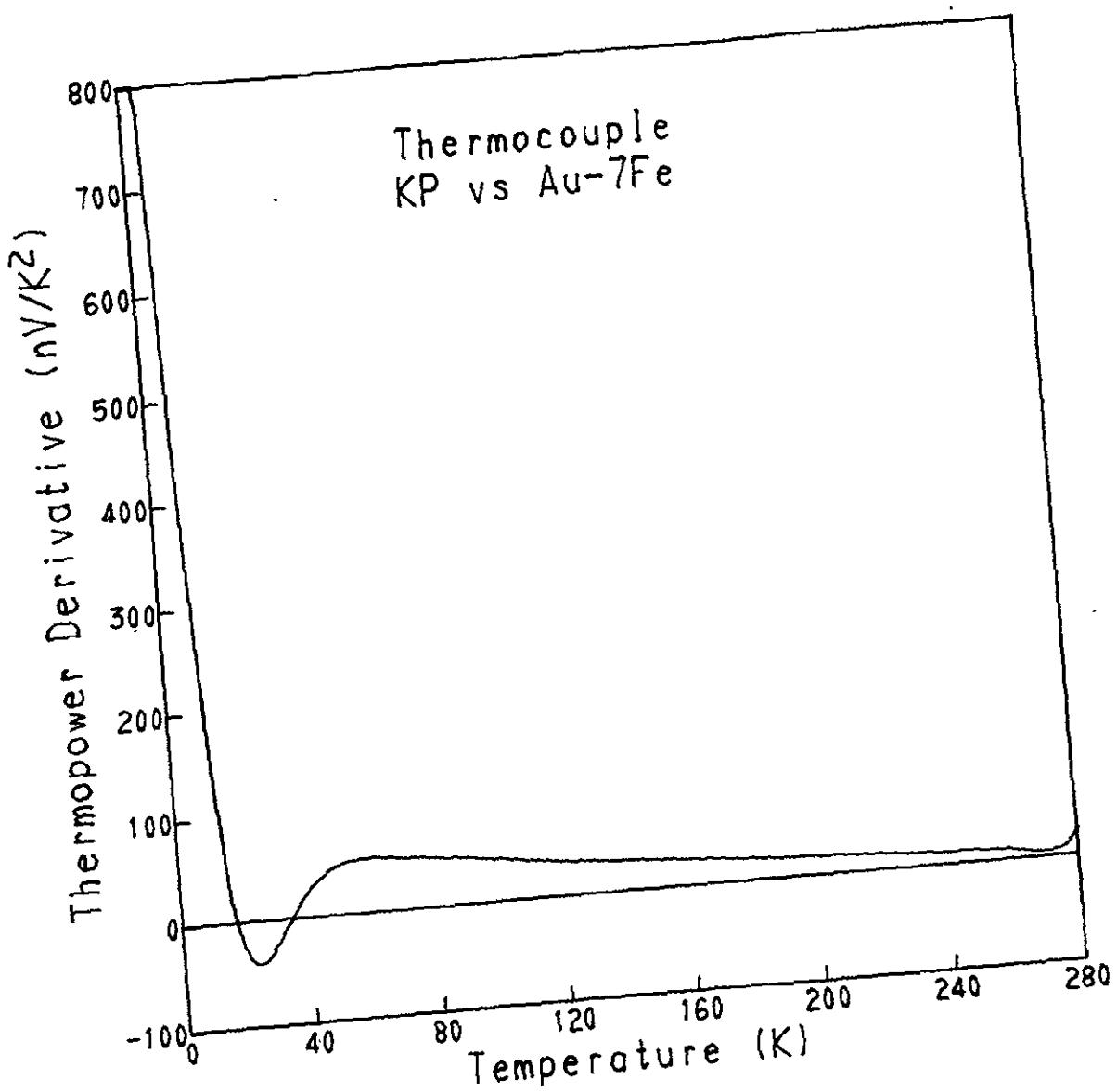


Figure D-3 Thermopower derivative of Chromel  
versus gold-0.07 at.% Fe.

D-4

Temp. K	Voltage mV	$\frac{dE}{dT} \times S$ mV/K	$\frac{dS}{dT}$ mV/K <sup>2</sup>	Temp. K	Voltage mV	$\frac{dE}{dT} \times S$ mV/K	$\frac{dS}{dT}$ mV/K <sup>2</sup>
1	7.86	8.645	1.5000	51	785.00	16.402	0.0476
2	17.21	10.035	1.2833	52	801.42	16.450	0.0484
3	27.86	11.220	1.0917	53	817.89	16.498	0.0492
4	39.59	12.226	0.9231	54	834.42	16.548	0.0497
5	52.26	13.073	0.7749	55	850.99	16.598	0.0502
6	65.69	13.782	0.6454	56	867.61	16.648	0.0505
7	79.78	14.369	0.5325	57	884.29	16.699	0.0508
8	94.40	14.852	0.4345	58	901.01	16.750	0.0509
9	109.45	15.243	0.3499	59	917.79	16.801	0.0510
10	124.86	15.555	0.2772	60	934.61	16.852	0.0510
11	140.54	15.801	0.2151	61	951.49	16.903	0.0509
12	156.44	15.989	0.1625	62	968.42	16.953	0.0508
13	172.50	16.128	0.1183	63	985.40	17.004	0.0507
14	188.68	16.228	0.0814	64	1002.43	17.055	0.0505
15	204.94	16.293	0.0509	65	1019.51	17.105	0.0503
16	221.26	16.331	0.0262	66	1036.64	17.155	0.0501
17	237.60	16.347	0.0064	67	1053.82	17.205	0.0498
18	253.95	16.346	-0.0091	68	1071.05	17.255	0.0495
19	270.29	16.330	-0.0209	69	1088.33	17.304	0.0493
20	286.60	16.305	-0.0295	70	1105.66	17.354	0.0490
21	302.89	16.272	-0.0354	71	1123.03	17.402	0.0487
22	319.15	16.235	-0.0389	72	1140.46	17.451	0.0484
23	335.36	16.195	-0.0406	73	1157.94	17.499	0.0481
24	351.54	16.154	-0.0406	74	1175.46	17.547	0.0478
25	367.67	16.114	-0.0394	75	1193.03	17.595	0.0476
26	383.77	16.076	-0.0371	76	1210.65	17.642	0.0473
27	399.82	16.040	-0.0339	77	1228.31	17.689	0.0470
28	415.85	16.008	-0.0301	78	1246.03	17.736	0.0467
29	431.84	15.980	-0.0258	79	1263.79	17.783	0.0464
30	447.81	15.957	-0.0212	80	1281.59	17.829	0.0461
31	463.76	15.938	-0.0164	81	1299.44	17.875	0.0458
32	479.69	15.924	-0.0115	82	1317.34	17.921	0.0456
33	495.61	15.915	-0.0065	83	1335.29	17.966	0.0453
34	511.52	15.911	-0.0017	84	1353.28	18.011	0.0450
35	527.43	15.912	0.0031	85	1371.31	18.056	0.0447
36	543.35	15.917	0.0077	86	1389.39	18.101	0.0444
37	559.27	15.927	0.0121	87	1407.51	18.145	0.0441
38	575.20	15.941	0.0163	88	1425.68	18.189	0.0438
39	591.15	15.960	0.0203	89	1443.89	18.233	0.0435
40	607.12	15.982	0.0239	90	1462.14	18.276	0.0432
41	623.12	16.007	0.0273	91	1480.44	18.319	0.0429
42	639.14	16.036	0.0305	92	1498.78	18.362	0.0426
43	655.19	16.068	0.0334	93	1517.16	18.404	0.0422
44	671.28	16.103	0.0360	94	1535.59	18.446	0.0419
45	687.40	16.140	0.0383	95	1554.06	18.488	0.0416
46	703.56	16.180	0.0404	96	1572.56	18.529	0.0412
47	719.76	16.221	0.0422	97	1591.11	18.570	0.0409
48	736.00	16.264	0.0439	98	1609.70	18.611	0.0405
49	752.29	16.309	0.0453	99	1628.34	18.651	0.0402
50	768.62	16.355	0.0465	100	1647.01	18.691	0.0398

Table D-1 Thermal voltage, thermopower, and thermopower derivative for thermocouple Chromel vs gold-0.07 at. % iron.

Temp. K	Voltage=E mV	$\frac{dE}{dT} = S$	$\frac{dS}{dT}$	Temp. K	Voltage=E mV	$\frac{dE}{dT} = S$	$\frac{dS}{dT}$
		mV/K	$mV/K^2$			mV/K	$mV/K^2$
101	1665.72	18.731	0.0394	151	2644.69	20.320	0.0263
102	1684.47	18.770	0.0391	152	2665.02	20.346	0.0261
103	1703.26	18.809	0.0387	153	2685.38	20.372	0.0259
104	1722.09	18.848	0.0383	154	2705.76	20.398	0.0257
105	1740.95	18.886	0.0380	155	2726.18	20.423	0.0255
106	1759.86	18.924	0.0376	156	2746.61	20.449	0.0253
107	1778.80	18.961	0.0372	157	2767.07	20.474	0.0251
108	1797.78	18.998	0.0368	158	2787.56	20.499	0.0249
109	1816.80	19.035	0.0365	159	2808.07	20.524	0.0246
110	1835.85	19.071	0.0361	160	2828.61	20.548	0.0244
111	1854.94	19.107	0.0357	161	2849.17	20.573	0.0242
112	1874.06	19.143	0.0354	162	2869.75	20.597	0.0240
113	1893.22	19.178	0.0350	163	2890.36	20.621	0.0237
114	1912.42	19.213	0.0347	164	2910.99	20.644	0.0235
115	1931.65	19.247	0.0343	165	2931.65	20.668	0.0233
116	1950.91	19.281	0.0340	166	2952.33	20.691	0.0230
117	1970.21	19.315	0.0337	167	2973.03	20.714	0.0228
118	1989.54	19.349	0.0333	168	2993.76	20.736	0.0226
119	2008.91	19.382	0.0330	169	3014.50	20.759	0.0223
120	2028.31	19.415	0.0327	170	3035.27	20.781	0.0221
121	2047.74	19.447	0.0324	171	3056.06	20.803	0.0219
122	2067.20	19.480	0.0321	172	3076.88	20.825	0.0216
123	2086.70	19.512	0.0319	173	3097.71	20.846	0.0214
124	2106.23	19.543	0.0316	174	3118.57	20.867	0.0212
125	2125.78	19.575	0.0313	175	3139.45	20.888	0.0209
126	2145.37	19.606	0.0311	176	3160.35	20.909	0.0207
127	2165.00	19.637	0.0308	177	3181.27	20.930	0.0205
128	2184.65	19.668	0.0306	178	3202.21	20.950	0.0203
129	2204.33	19.698	0.0304	179	3223.17	20.970	0.0201
130	2224.04	19.728	0.0301	180	3244.15	20.990	0.0199
131	2243.79	19.758	0.0299	181	3265.15	21.010	0.0197
132	2263.56	19.788	0.0297	182	3286.17	21.030	0.0195
133	2283.36	19.818	0.0295	183	3307.21	21.049	0.0193
134	2303.20	19.847	0.0293	184	3328.27	21.068	0.0191
135	2323.06	19.876	0.0291	185	3349.34	21.088	0.0190
136	2342.95	19.905	0.0289	186	3370.44	21.106	0.0188
137	2362.87	19.934	0.0288	187	3391.56	21.125	0.0187
138	2382.82	19.963	0.0286	188	3412.69	21.144	0.0185
139	2402.80	19.991	0.0284	189	3433.85	21.162	0.0184
140	2422.80	20.020	0.0282	190	3455.02	21.180	0.0182
141	2442.83	20.048	0.0281	191	3476.21	21.199	0.0181
142	2462.90	20.076	0.0279	192	3497.41	21.217	0.0180
143	2482.99	20.104	0.0277	193	3518.64	21.235	0.0178
144	2503.10	20.131	0.0275	194	3539.88	21.252	0.0177
145	2523.25	20.159	0.0274	195	3561.14	21.270	0.0176
146	2543.42	20.186	0.0272	196	3582.42	21.288	0.0175
147	2563.62	20.213	0.0270	197	3603.72	21.305	0.0174
148	2583.85	20.240	0.0268	198	3625.03	21.322	0.0173
149	2604.10	20.267	0.0267	199	3646.36	21.340	0.0172
150	2624.38	20.293	0.0265	200	3667.71	21.357	0.0171

Table D-1 (Cont.) Thermal voltage, thermopower, and thermopower derivative for thermocouple Chromel vs gold-0.07 at.% iron.

Temp. K	Voltage*E μV	$\frac{dE}{dT} = S$ μV/K	$\frac{dS}{dT}$ μV/K <sup>2</sup>	Temp. K	Voltage*E μV	$\frac{dE}{dT} = S$ μV/K	$\frac{dS}{dT}$ μV/K <sup>2</sup>
201	3689.08	21.374	0.0170	251	4775.99	22.040	0.0104
202	3710.46	21.391	0.0169	252	4798.03	22.050	0.0103
203	3731.86	21.408	0.0168	253	4820.09	22.060	0.0102
204	3753.27	21.424	0.0167	254	4842.15	22.071	0.0100
205	3774.71	21.441	0.0166	255	4864.23	22.081	0.0099
206	3796.16	21.457	0.0164	256	4886.31	22.090	0.0097
207	3817.62	21.474	0.0163	257	4908.41	22.100	0.0094
208	3839.10	21.490	0.0162	258	4930.51	22.109	0.0091
209	3860.60	21.506	0.0161	259	4952.63	22.118	0.0088
210	3882.12	21.522	0.0159	260	4974.75	22.127	0.0085
211	3903.65	21.538	0.0158	261	4996.88	22.135	0.0081
212	3925.19	21.554	0.0157	262	5019.03	22.143	0.0076
213	3946.75	21.569	0.0155	263	5041.17	22.150	0.0072
214	3968.33	21.585	0.0154	264	5063.32	22.157	0.0067
215	3989.92	21.600	0.0152	265	5085.48	22.164	0.0062
216	4011.53	21.615	0.0150	266	5107.64	22.170	0.0057
217	4033.15	21.630	0.0148	267	5129.82	22.175	0.0053
218	4054.79	21.645	0.0147	268	5152.00	22.180	0.0049
219	4076.44	21.659	0.0145	269	5174.18	22.185	0.0046
220	4098.11	21.674	0.0143	270	5196.37	22.190	0.0044
221	4119.79	21.688	0.0141	271	5218.56	22.194	0.0044
222	4141.49	21.702	0.0139	272	5240.75	22.198	0.0046
223	4163.19	21.716	0.0137	273	5262.96	22.203	0.0052
224	4184.92	21.729	0.0135	274	5285.16	22.209	0.0061
225	4206.65	21.743	0.0133	275	5307.37	22.216	0.0075
226	4228.40	21.756	0.0131	276	5329.59	22.224	0.0095
227	4250.17	21.769	0.0129	277	5351.83	22.235	0.0122
228	4271.94	21.782	0.0127	278	5374.06	22.248	0.0157
229	4293.73	21.794	0.0125	279	5396.32	22.266	0.0204
230	4315.53	21.807	0.0123	280	5418.60	22.290	0.0262
231	4337.34	21.819	0.0121				
232	4359.17	21.831	0.0120				
233	4381.00	21.843	0.0118				
234	4402.85	21.855	0.0117				
235	4424.71	21.866	0.0115				
236	4446.59	21.878	0.0114				
237	4468.47	21.889	0.0113				
238	4490.36	21.900	0.0112				
239	4512.27	21.911	0.0111				
240	4534.19	21.922	0.0110				
241	4556.11	21.933	0.0109				
242	4578.05	21.944	0.0109				
243	4600.00	21.955	0.0108				
244	4621.96	21.966	0.0107				
245	4643.94	21.977	0.0107				
246	4665.92	21.987	0.0107				
247	4687.91	21.998	0.0106				
248	4709.91	22.009	0.0106				
249	4731.93	22.019	0.0105				
250	4753.95	22.030	0.0105				

Table D-1 (Cont.) Thermal voltage, thermopower, and thermopower derivative for thermocouple Chromel vs gold-0.07 at.% iron.

## Appendix E.

### Functional Representations and Error Analyses

As described in the "Data Analysis and Results" section, the thermal voltage can be represented by

$$E(T) = \sum_{n=1}^L A_n F_n(T),$$

where the orthonormal polynomials  $F_n(T)$  are given by

$$F_n(T) = \sum_{j=1}^n C_{jn} T^j.$$

The  $F_n(T)$  (up to  $n = 14$ ) are given in table E-1 to twelve significant figures and are in a form convenient for rapid computation and minimum round-off error. Sometimes, but not always (as explained next), all fourteen functions are required to obtain a best fit.

In general, the more complex the shape of a curve, the more terms are required in an expansion. The curve for type K is relatively simple; only 10 polynomials are required. Curves for type T and KP vs Au-7 Fe are more complex; they require 14 polynomials. Type E is intermediate; 12 polynomials are needed. All of the necessary coefficients,  $A_n$ , for each of the four thermocouple combinations are given in table E-2. The numbers are all given with sufficient digits so that no significant precision is lost in the final calculation.

For most computers, double precision constants and software are required in the program if the final calculations are to retain all of the precision inherent in the experimental data. If the full array of functions and constants are used with a double precision program, then the resultant standard deviation of the data fits are 0.06, 0.11, 0.07, and 0.10 microvolts for Types T, E, K, and KP vs Au-7 Fe respectively.

$$F(1) = 2.62699813461 \times 10^{-3} T$$

$$F(2) = [3.21644939212 \times 10^{-5} T - 1.11693281748 \times 10^{-2}]T$$

$$\begin{aligned} F(3) = & [(3.58986173360 \times 10^{-7} T - 1.55665286232 \times 10^{-4})T \\ & + 1.81137186628 \times 10^{-2}]T \end{aligned}$$

$$\begin{aligned} F(4) = & [(5.34727798756 \times 10^{-9} T - 3.04978248031 \times 10^{-6})T \\ & + 5.54625790795 \times 10^{-4})T - 3.34631223797 \times 10^{-2}]T \end{aligned}$$

$$\begin{aligned} F(5) = & [(6.07093013715 \times 10^{-11} T - 4.27373422008 \times 10^{-8})T \\ & + 1.07117698644 \times 10^{-5})T - 1.13757942812 \times 10^{-3})T + 4.64537228886 \times 10^{-2}]T \end{aligned}$$

$$\begin{aligned} F(6) = & [(8.82359212161 \times 10^{-13} T - 7.28186199261 \times 10^{-10})T \\ & + 2.24765904282 \times 10^{-7})T - 3.18943408270 \times 10^{-5})T + 2.05429286434 \times 10^{-3})T \\ & - 5.17871198112 \times 10^{-2}]T \end{aligned}$$

$$\begin{aligned} F(7) = & [(1.33824082457 \times 10^{-14} T - 1.32030883347 \times 10^{-11})T \\ & + 5.13280189141 \times 10^{-9})T - 9.93378385912 \times 10^{-7})T + 9.92080547172 \times 10^{-5})T \\ & - 4.75674883206 \times 10^{-3})T + 8.88149787156 \times 10^{-2}]T \end{aligned}$$

$$\begin{aligned} F(8) = & [(1.91122488586 \times 10^{-16} T - 2.16756712456 \times 10^{-13})T \\ & + 1.00341211234 \times 10^{-10})T - 2.43627392132 \times 10^{-8})T + 3.31519537388 \times 10^{-6})T \\ & - 2.49826333327 \times 10^{-4})T + 9.57847982898 \times 10^{-3})T - 1.50658460622 \times 10^{-1})T \end{aligned}$$

$$\begin{aligned} F(9) = & [(2.92664884243 \times 10^{-18} T - 3.70219405097 \times 10^{-15})T \\ & + 1.95708484602 \times 10^{-12})T - 5.60572545443 \times 10^{-10})T + 9.43371886071 \times 10^{-8})T \\ & - 9.45983561819 \times 10^{-6})T + 5.47473023495 \times 10^{-4})T - 1.67836957950 \times 10^{-2})T \\ & + 2.24869753823 \times 10^{-1})T \end{aligned}$$

Table E-1 The orthonormal polynomials  $F_n(T)$ .

$$\begin{aligned}
 F(10) &= (((((((((3.95801534382*10^{-20})T - 5.60568859106*10^{-17})T \\
 &+ 3.38786223933*10^{-14})T - 1.13998063262*10^{-11})T + 2.33700771017*10^{-9})T \\
 &- 3.00187384267*10^{-7})T + 2.39434643671*10^{-5})T - 1.13590924597*10^{-3})T \\
 &+ 2.93458112010*10^{-2})T - 3.46535708754*10^{-1})T \\
 F(11) &= (((((((((5.38516736601*10^{-22})T - 8.32331470995*10^{-19})T \\
 &+ 5.56674670636*10^{-16})T - 2.11051706773*10^{-13})T + 4.99234280040*10^{-11})T \\
 &- 7.64420856213*10^{-9})T + 7.61267444043*10^{-7})T - 4.83150710271*10^{-5})T \\
 &+ 1.86327527031*10^{-3})T - 4.00410161322*10^{-2})T + 4.09499105085*10^{-1})T \\
 F(12) &= (((((((((8.26232811079*10^{-24})T - 1.39942629861*10^{-20})T \\
 &+ 1.03886749337*10^{-17})T - 4.44101985907*10^{-15})T + 1.20800316490*10^{-12})T \\
 &- 2.18094014408*10^{-10})T + 2.64618560604*10^{-8})T - 2.13895663004*10^{-6})T \\
 &+ 1.11909300262*10^{-4})T - 3.59443137275*10^{-3})T + 6.49353202556*10^{-2})T \\
 &- 5.70479386855*10^{-1})T \\
 F(13) &= (((((((((1.25461027145*10^{-25})T - 2.30105779284*10^{-22})T \\
 &+ 1.87043885148*10^{-19})T - 8.87601372259*10^{-17})T + 2.72632243976*10^{-14})T \\
 &- 5.67999046167*10^{-12})T + 8.17908913314*10^{-10})T - 8.14274313875*10^{-8})T \\
 &+ 5.51731174858*10^{-6})T - 2.46158777788*10^{-4})T + 6.84002302040*10^{-3})T \\
 &- 1.08288591279*10^{-1})T + 8.46075126398*10^{-1})T \\
 F(14) &= (((((((((1.85341453474*10^{-27})T - 3.66081814236*10^{-24})T \\
 &+ 3.23482126555*10^{-21})T - 1.68761557726*10^{-18})T + 5.77754988256*10^{-16})T \\
 &- 1.36460361321*10^{-13})T + 2.27598282316*10^{-11})T - 2.69808964571*10^{-9})T \\
 &+ 2.25818509834*10^{-7})T - 1.30847059620*10^{-5})T + 5.06916388647*10^{-4})T \\
 &- 1.24180968293*10^{-2})T + 1.76154785795*10^{-1})T - 1.25353229615)T
 \end{aligned}$$

Table E-1 (Cont.) The orthonormal polynomials  $F_n(T)$ .

COEFFICIENT	TYPE T	TYPE E	TYPE K	KP VS AU-7FE
A(1)	10673.443	16803.061	11244.712	7823.267
A(2)	1947.355	2969.647	2175.001	433.939
A(3)	-158.544	-405.095	-297.946	-82.121
A(4)	44.522	65.071	5.299	-16.055
A(5)	-34.697	-22.933	-4.617	21.929
A(6)	10.896	3.050	-0.622	-8.975
A(7)	-0.253	1.794	2.145	0.008
A(8)	-2.966	-1.910	-1.907	4.704
A(9)	2.053	0.284	0.745	-6.097
A(10)	-1.085	0.131	-0.271	6.441
A(11)	-0.055	-0.720		-4.328
A(12)	0.467	0.437		2.494
A(13)	-0.568			-1.283
A(14)	0.464			0.496

Table E-2 Coefficients for a polynomial expansion representation of the thermocouple data.

However, any functional representation can be simplified at the cost of an increased standard deviation for the data fit. Again the standard deviation for any given order depends on the thermocouple type. In table E-3 are listed the approximate standard deviations for each order of polynomial expansion between 4 and the maximum number (14, 12, 10, or 14 respectively). It can be clearly seen that if, for example, only 1 microvolt precision is desired, then the order is usually about halved, to 7, 6, 5, or 11 respectively.

Computer economies can also be obtained by reducing the number of digits carried, by changing from double to single precision. Since there is no uniformity in what constitutes single or double precision (single can mean from about 8 to 12 decimal digits), we have tabulated the errors caused by using various different numbers of digits in computations. For full table reproduction precision (0.01 microvolt), 38 binary bits (12 decimal digits) must be carried for type T or KP vs Au-7 Fe thermocouples; 33 binary bits (10 decimal) for type E; and 26 binary (8 decimal) for type K. Table E-4 indicates the number of binary bits and decimal digits necessary to obtain various given precisions. The values in the table presume, of course, that a sufficient number of polynomials are used to eliminate any error that would be caused by using too low an order of fit. Since all large computers carry at least 24 binary bits in single precision, errors were not calculated for any fewer bits than that. The tables in Appendices A through D were calculated using 72 binary bits (22 decimals).

The deviations between calculated and experimental values of voltage are given in figures E-1 through E-4. Note that the deviations are in nanovolts.

NUMBER OF COEFFICIENTS	APPROXIMATE STANDARD DEVIATION			
	TYPE T	TYPE E	TYPE K	KP VS AU-7EE
4	9	13	1.5	6
5	7	5	0.9	5
6	2	0.6	0.5	2
7	0.8	0.5	0.4	1.9
8	0.6	0.4	0.38	1.7
9	0.4	0.2	0.15	1.5
10	0.2	0.17	0.07	1.4
11	0.15	0.15		1.0
12	0.13	0.11		0.6
13	0.10			0.3
14	0.06			0.10

Table E-3 Approximate standard deviations (in microvolts) for various orders of polynomial expansions.

Table E-4

Number of digits necessary in computations to reduce  
round-off errors below certain limits

Error Criteria	Number of Digits Necessary for Thermocouple							
	Type T		Type E		Type K		KP vs Au-7 Fe	
	binary	decimal	binary	decimal	binary	decimal	binary	decimal
Full table precision $<0.01\mu V$	38	12	33	10	26	8	38	12
Approx. exp. error $<0.1\mu V$	35	11	29	9	24	8	35	11
$<1\mu V$	32	10	24	8	24	8	32	10
$<50\mu V$	24	8					24	8

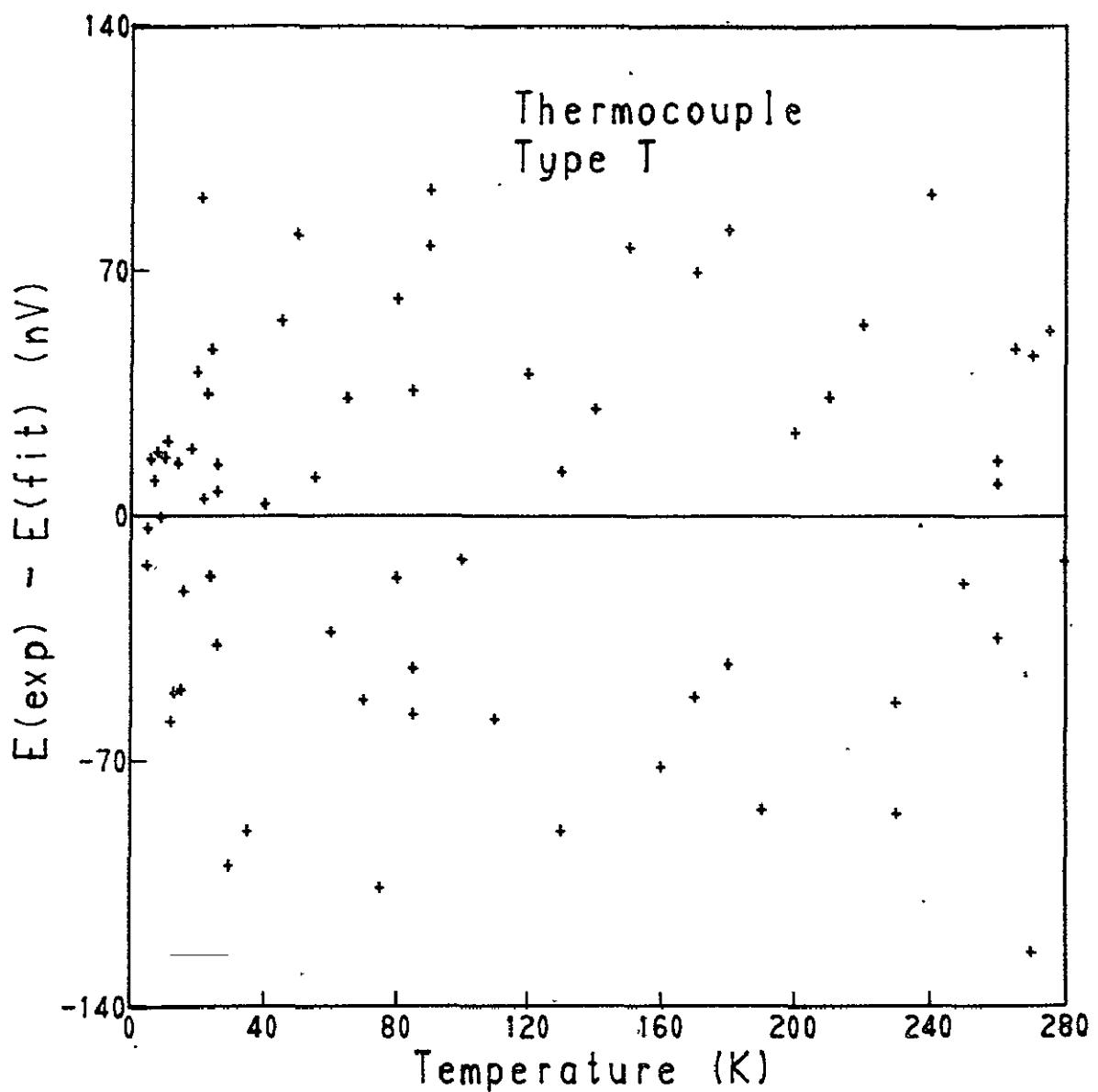


Figure E-1 Deviations between calculated and experimental values for thermocouple type T.

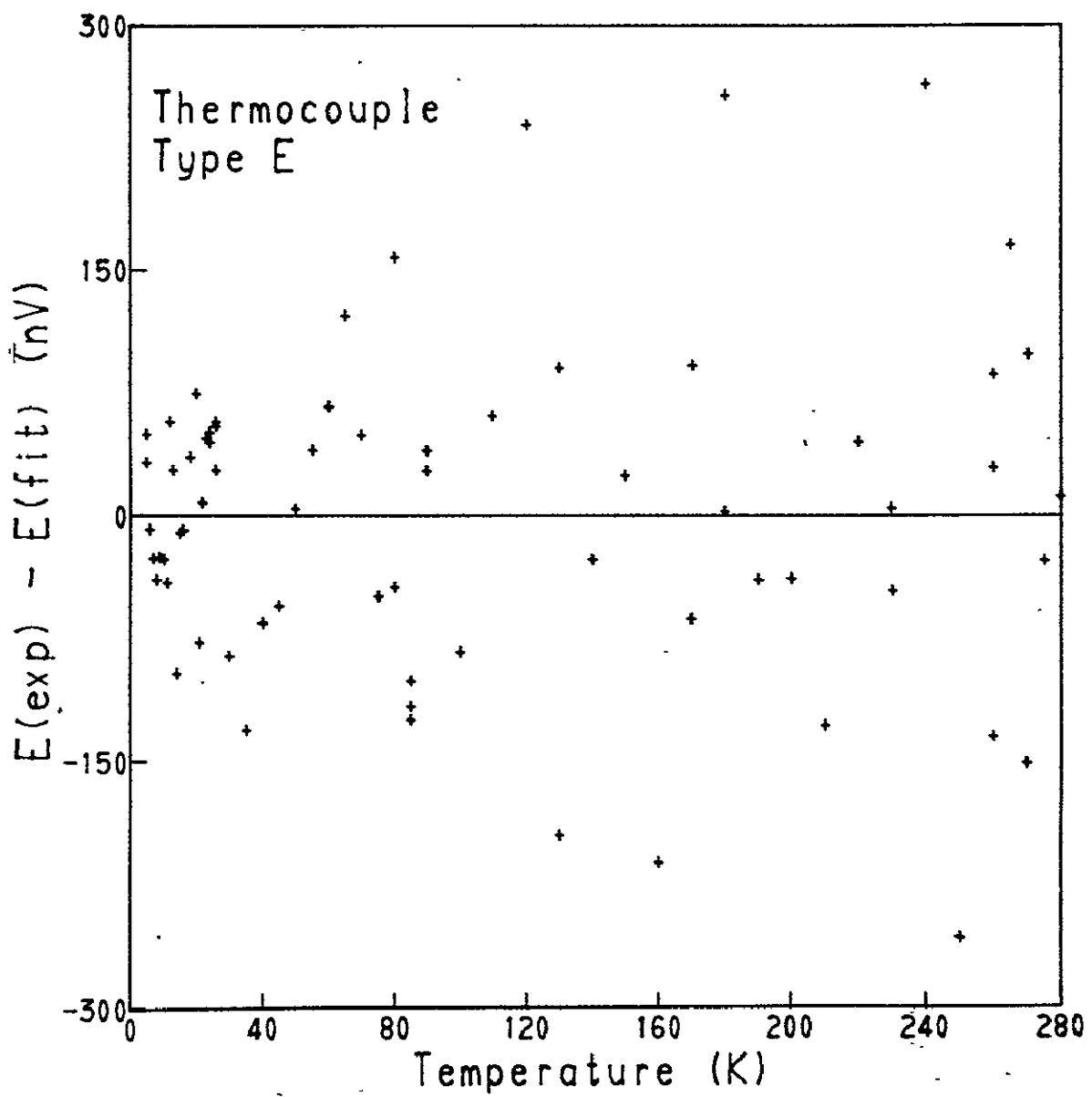


Figure E-2 Deviations between calculated and experimental values for thermocouple type E.

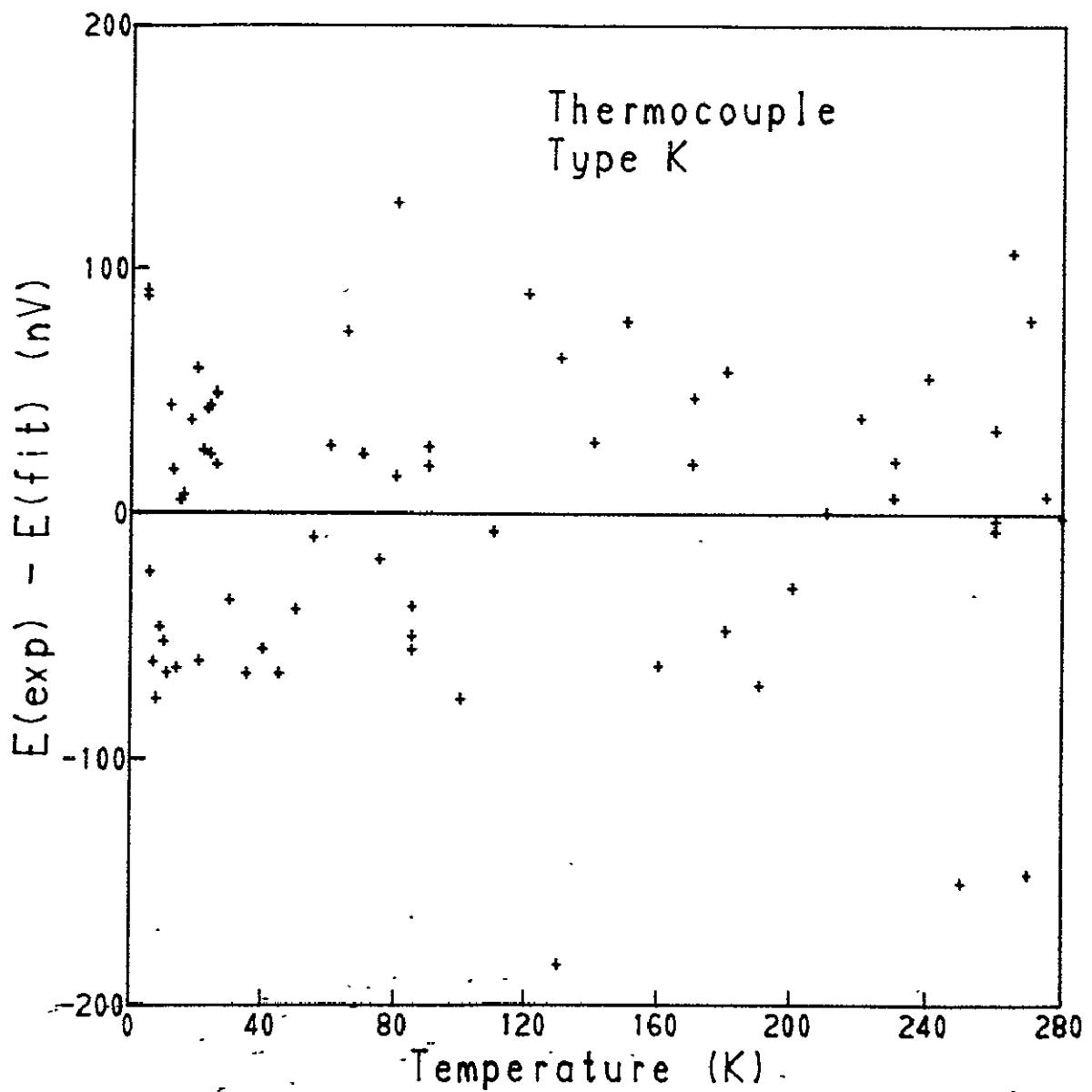


Figure E-3 Deviations between calculated and experimental values for thermocouple type K.

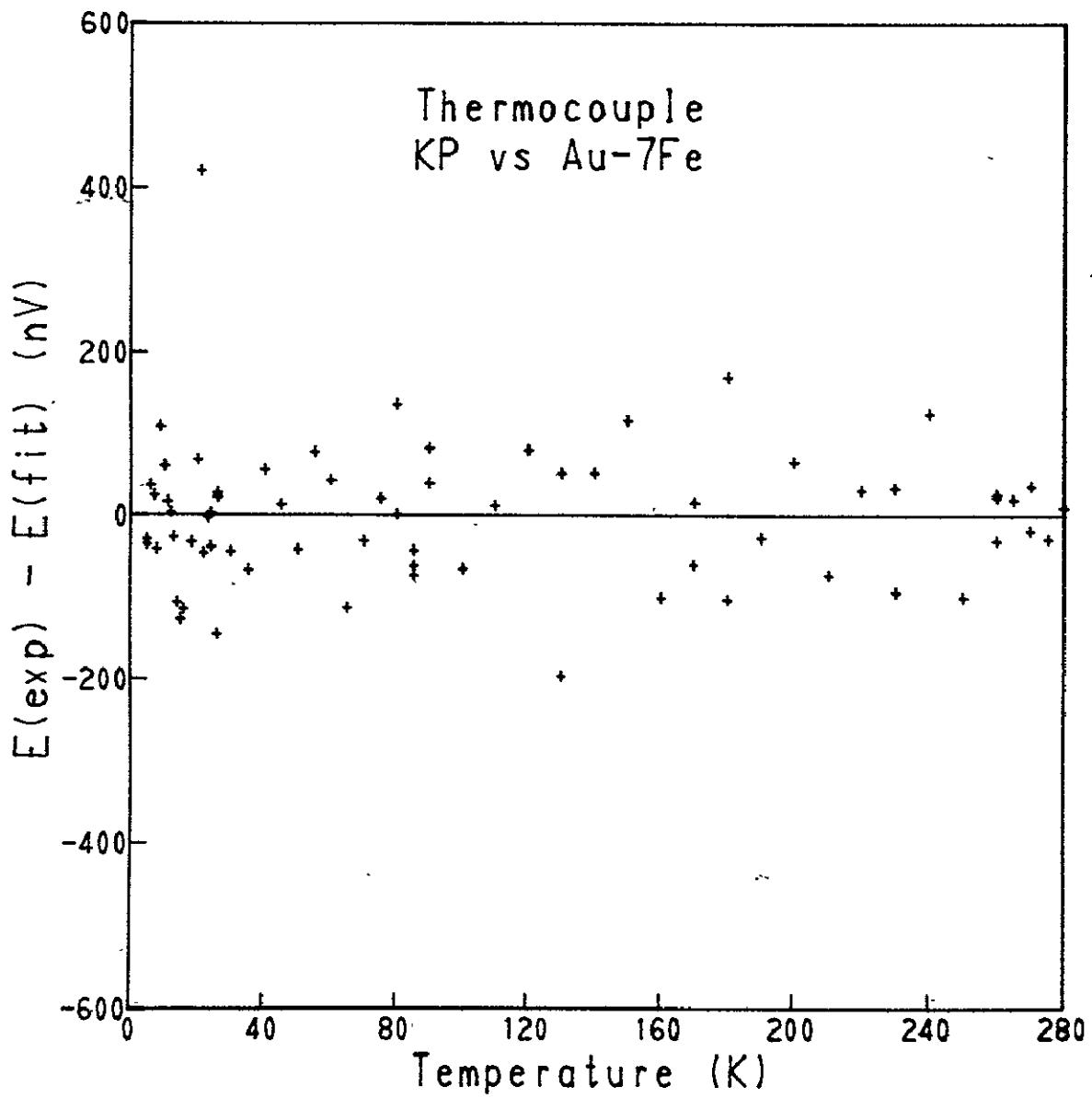


Figure E-4 Deviations between calculated and experimental values for Chromel versus Au-0.07 at.% Fe.

In addition to the errors caused by imprecisions of data fitting, other errors can be introduced by inaccuracies in measurement of the independent variable, temperature. These are approximately 2.2 mK between 4 and 20 K, 2.5 mK between 20 and 75 K, and 2.0 mK between 75 and 280 K. The equivalent voltage inaccuracies, given in table E-5, will depend on the sensitivities of each thermocouple type in each temperature range. Only above about 80 K do the temperature errors cause greater equivalent voltage errors than does the curve fitting.

Table E-5

Equivalent voltage errors caused by temperature inaccuracies

Temperature Range	Voltage Inaccuracies (in microvolts) for Thermocouple			
	Type T	Type E	Type K	KP vs Au-7Fe
LHe	0.01	0.02	0.01	0.03
LH <sub>2</sub>	0.06	0.09	0.06	0.14
LN <sub>2</sub>	0.30	0.46	0.31	0.22

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