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ENTRY TRAJECTORY, ENTRY ENVIRONMENT, AND ANALYSIS OF SPACECRAFT MOTION FOR THE RAM C-III FLIGHT EXPERIMENT

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SUMMARY

The RAM C-III flight experiment was launched from NASA Wallops Station on September 30, 1970, to study the problem of radiofrequency blackout at an entry velocity 7.407 km/sec (24 300 ft/sec). The flight is described, and data for the entry trajectory and environment, which include the effects of actual temperature measured the day of launch, are presented. An analysis of entry spacecraft motions was performed. This analysis included the determination of wind angles from measured accelerations and estimates of wind angles at high altitudes from gyro-measured rotation rates. The maximum wind angles were found to be less than 5° to the point of pitch-roll resonance (an altitude of 35.052 km (115 000 ft)), where the total wind angle increased to 8.5° and the roll rate started decreasing. A plausible cause for the decrease in roll rate was shown to be a combination of trim angle and an offset center of gravity.

INTRODUCTION

RAM C-III was one in a series of flight experiments conducted by Project RAM (Radio Attenuation Measurements) at the Langley Research Center to study the problem of radiofrequency blackout associated with high-speed entry into the earth's atmosphere. Some results of previous flight experiments are reported in references 1 to 7, and a summary of the RAM Program is presented in reference 8.

The RAM C-III spacecraft was launched from NASA Wallops Station, Wallops Island, Virginia, by a Scout vehicle September 30, 1970. Several experiments were included with the objectives of comparing the effectiveness of electrophilic liquids with that of water in reducing radiofrequency blackout and of obtaining measurements of ion and electron concentrations in the plasma sheath. Some results of this flight are presented in references 9 to 12.

In the present paper the RAM C-III flight is described, and comprehensive data for the entry trajectory and environment are presented. The results reported will serve as

a base-line source for trajectory and environmental data required in the continuing analyses of flight data. All of the experimental data showed effects of spacecraft rotational motions and wind-angle changes. This paper contains an analysis of these data which can be used in the evaluation of the experimental data.

The analysis includes determination of the wind angles from measured accelerations in the region of substantial aerodynamic effects and the determination of inertial rotations and estimates of maximum wind angles from gyro-measured rotation rates in the high-altitude, low-density region. A computer simulation was used to demonstrate a plausible cause for the significant decrease in spacecraft roll rate.

SYMBOLS

Measurements and calculations were made in the U.S. Customary Units. (See appendix for further explanation and factors for conversion to SI Units.)

^a N	normal acceleration, $-a_Z$
^a x, ^a y, ^a Z	accelerations along body axes (nondimensionalized by earth gravitational acceleration)
c _{m,o}	static pitching-moment coefficient at $\alpha = 0$
$c_{m_{\eta}}$	slope of pitching-moment coefficient at $\eta = 0$
c _{n,o}	static yawing-moment coefficient at $\alpha = 0$
C_N	normal-force coefficient
c _Y	side-force coefficient
D	diameter of base of spacecraft, 0.67 m (2.2 ft)
f()	function of quantity in parentheses
١	lateral moment of inertia, $(I_Y + I_Z)/2$
$\mathbf{I}_{\mathbf{X}}, \mathbf{I}_{\mathbf{Y}}, \mathbf{I}_{\mathbf{Z}}$	spacecraft moments of inertia

- \mathbf{L} geodetic latitude; angle between the equatorial plane and the altitude vector (positive north) rotation rates about X-, Y-, and Z-axes p,q,r dynamic pressure, $\frac{1}{2}\rho_{\rm m}V^2$ \mathbf{q}_{∞} area of base of spacecraft, 0.35 m^2 (3.8 ft²) S time t time at beginning of interval for rotation and α,β cross plots tp time interval defined in equation (15) Δt magnitude of earth-relative velocity vector, $\sqrt{u^2 + v^2 + w^2}$ V magnitude of lateral velocity, $\sqrt{v^2 + w^2}$ V' W spacecraft weight components of relative velocity along spacecraft X-, Y-, and Z-axes u,v,w spacecraft body axes X,Y,Zaxis defined in figure 9 $\mathbf{X}_{\mathbf{b}}$ measurements along X_{b} -, Y-, and Z-axes in figure 9 x_{h}, y, z $\Delta y, \Delta z$ displacements of center of gravity from X-axis of spacecraft wind angles (angle of attack, angle of sideslip, and total wind angle) α,β,η angle between gyro spin axis and spacecraft roll angular velocity vector δ η
 - ' uncertainty in direction of relative velocity with respect to inertial frame at 405 seconds

λ	longitude; angle between Greenwich meridian and the spacecraft meridian (positive east)
$ ho_{ m m}$	atmospheric density computed on basis of temperature measurements the day of launch
ρ _o	atmospheric density based on 1962 Standard Atmosphere model (ref. 13)
au ,	resultant inertial angle in ψ, θ plane, $\sqrt{\psi^2 + \theta^2}$
ϕ '	angle between negative Z-axis and V' (positive clockwise looking forward), $\tan^{-1}\left(\!-a_Y\!\!\left/\!-a_N\!\right)$
$\psi, heta, \phi$	inertial or Euler angles
ά	total angular rate of change of earth-relative coordinates with respect to inertial frame
ω_{0}	spacecraft natural oscillation frequency
$\Delta \omega$	modified roll frequency
$\omega_0/\Delta\omega$	resonance parameter
Subscripts	s:
max	maximum value
0	value for beginning of integration
A do	t over a quantity represents differentiation with respect to time.
	NOMENCLATURE
Altitude	magnitude of geodetic altitude vector; geodetic height above earth
Earth rang	ge great-circle distance along earth between launch site and projected spacecraft position

Flight azimuth	angle between spacecraft meridian and projection of relative veloc- ity vector onto spacecraft horizon (positive clockwise from north)
Flight elevation	angle between spacecraft horizon and relative velocity vector (positive up)
Mach number	ratio of spacecraft velocity to velocity of sound
Radar azimuth	angle between radar meridian and projection of range vector on radar horizon (positive clockwise from north)
Radar elevation	angle between radar horizon and range vector (positive up)
Radar range	magnitude of range vector from radar to spacecraft

LAUNCH VEHICLE AND TRAJECTORY

A photograph of the RAM C-III launch vehicle on the launch pad at Wallops Station is shown in figure 1. The vehicle was launched at 20:06:29.1 GMT September 30, 1970. The lift-off was vertical, and the vehicle was pitched down on a flight azimuth of 109^o. Table I lists some of the important flight events, and figure 2 shows plots of flight parameters. The time scale is based on time elapsed after lift-off. The plots show the overlapping of the data from the principal tracking radars.

The second-stage motor was ignited at zero angle of attack, and during the long coast between second burnout and third ignition (see fig. 2(a)), the vehicle was pitched down; the third stage was ignited just prior to apogee at a negative angle of attack. Therefore, the trajectory for the data period was uprange about 185 km (100 nautical miles) from that of a nominal ballistic trajectory. The indicated roll-up took place after third-stage burnout and just prior to fourth ignition. The purpose of rolling the space-craft was to minimize anomalies due to separation and thrust misalinement for the unguided fourth stage. A few seconds after fourth-stage burnout (an altitude of about 141.732 km (465 000 ft)), a command signal from Bermuda initiated the start of an onboard programer which controlled several subsequent spacecraft events (separation, liquid injection, probe retraction, etc.). Separation of the fourth-stage motor case from the spacecraft was produced initially by a spring-loaded device. This system was augmented by a system of two small rocket motors designed to produce permanent separation.

ENTRY TRAJECTORY AND ENVIRONMENT

The Bermuda AN/FPS-16 radar which was tracking the C-band beacon in the spacecraft lost signal because of plasma at about 400 seconds; the Bermuda AN/FPQ-6 radar, however, switched to the skin-track mode at onset of attenuation and tracked throughout the entire period of interest. Trajectory data obtained by the two radars prior to loss of signal by the FPS-16 (see fig. 2(c), for instance) are in very good agreement. All the data for entry trajectory and environment presented or used in this paper are taken from the FPQ-6 radar. The coordinates of the FPQ-6 radar at Bermuda are

Latitude, 32.348⁰

Longitude, -64.654⁰

Radar data showing the spacecraft position relative to Bermuda are shown in figure 3.

Entry-trajectory parameters (altitude, latitude, longitude, earth range, velocity, flight azimuth, and flight elevation) are presented in figure 4. All parameters except flight azimuth and flight elevation vary smoothly and indicate no anomalies. The behavior of these parameters after about 420 seconds probably reflects inaccuracies in differentiating the position data obtained by the radar. It can be seen in figure 3, for instance, that the elevation angle from Bermuda is quite low at 420 seconds. Table II gives the entrytrajectory parameters in 0.1-second intervals.

Dynamic pressure and Mach number are plotted in figure 5. In computing these parameters, the atmospheric density was corrected for the temperature measured at Bermuda within a few hours after the entry. The temperatures to 182.88 km (60 000 ft) were obtained with a radiosonde, and above that altitude they were obtained with an Arcasonde. The variation in density from the 1962 Standard Atmosphere (ref. 13) is given in figure 6, and the actual correction factor used is also shown. The velocity of the wind relative to the earth was not considered in the computations. During the data period the spacecraft velocity is large, and wind effects could be expected to have a negligible effect on dynamic pressure. At the lower altitudes the effect may be more significant. Table III presents atmospheric density, dynamic pressure, and Mach number for the entry trajectory in 0.1-second intervals. For convenience the spacecraft altitude and velocity are also tabulated.

SPACECRAFT DESCRIPTION AND INSTRUMENTATION

The spacecraft consisted of a hemispherical nose with a radius of 15.95 cm (6.28 in.) faired into a cone frustum with a half-angle of 9° . A sketch of the geometry is

shown in figure 7(a). The fins at the base of the spacecraft contained the probe rakes used to measure electron and positive-ion densities. They were retracted at 401.3 seconds (an altitude of about 60.808 km (199 500 ft)) to prevent adverse aerodynamic and heating effects on the spacecraft at lower altitudes. The nose of the spacecraft was covered with phenolic-graphite (see sketch in fig. 1), a hard, charring ablative material which permitted the drilling of holes for liquid injection. The remainder of the frustum was covered with teflon, and the base was protected by cork. Figure 7(b) lists the preflight-measured weight and moments of inertia of the spacecraft, and figure 7(c) shows plots of the preflight-computed histories of the weight and moments of inertia. The computations accounted for mass loss due to ablation and liquid injection. The sketches of figure 8 illustrate the axis systems and nomenclature employed.

A list of the performance instruments is shown in table IV. Shown also are the response of each instrument, its Inter-Range Instrumentation Group (IRIG) channel assignment, and the range and estimated error of each instrument. Note that the total ranges of the accelerometers measuring normal and side accelerations are divided into three subranges to improve the accuracy of their measurements at the lower end of the scale. The locations of the instruments on the spacecraft are shown in figure 9.

MEASURED SPACECRAFT-MOTION DATA

Spacecraft rotation rates measured by the gyros are presented in figure 10, and lateral (side and normal) accelerations measured by the accelerometers are presented in figure 11. All data have been smoothed. The data from 315 to 325 seconds are presented to illustrate the effects at roll-up, and the data from 370 to 380 seconds are presented to show the effects at separation of the fourth stage. From 380 to 440 seconds the acceleration which was due to the displacement of the accelerometers from the spacecraft center of gravity has been removed. The most significant component of that acceleration is shown in figure 11(a) and results from displacements of the lateral accelerometers from the spacecraft X-axis. (See fig. 9.) Figure 11(b) shows that separation of the fourth stage leaves this rotational component of measured acceleration essentially unchanged.

DETERMINATION OF WIND ANGLES FROM ACCELERATION DATA

Wind angles were determined from the following relationships:

$$C_{N} = \frac{Wa_{N}}{q_{\infty}S}$$
(1)

$$C_{Y} = \frac{Wa_{Y}}{q_{\infty}S}$$
(2)

$$\alpha = f(C_N)$$
(3)

$$\beta = f(C_Y)$$
(4)

$$\eta = \sqrt{\alpha^2 + \beta^2} \tag{5}$$

$$\phi' = \tan^{-1} \frac{-a_Y}{-a_N} \tag{6}$$

The quadrant of ϕ' was determined by testing the sign of the numerator and denominator of equation (6). The values of a_N and a_Y used in equations (1) and (2) were those shown in figure 11; values of W were taken from figure 7(b); and values of q_{∞} were taken from table III. Aerodynamic-force coefficients were obtained in wind-tunnel tests from Mach 1.5 to Mach 20.3. Typical curves of the coefficients as a function of wind angles are shown in figure 12. All acceleration was assumed to be due to static aerodynamic forces, and cross coupling between α and β was considered negligible.

Wind angles determined from the acceleration data and equations (3) to (6) are presented in figures 13 and 14 from 400 seconds to 440 seconds. Wind angles determined by this method are not considered reliable prior to 400 seconds because of the very low measured accelerations. The maximum possible error in the absolute values of the wind angles from 400 to 405 seconds based on the instrument errors of table IV is about 3° . The consistent behavior of the angles, however, suggests that the errors are probably less than the maximum possible values. Between 405 and 410 seconds the maximum error in wind angles based on instrument measurement error goes to about 1.0° . The reason for presenting the roll rate with the total wind angle and phase angle is the relationship between these three quantities during the period when roll rate was decreasing.

INERTIAL ROTATIONS AND WIND ANGLES AT HIGH ALTITUDES

Integration and Analysis of Gyro Data

The data periods for most of the experiments began prior to 400 seconds, and additional analysis was required to determine spacecraft motions and to estimate maximum wind angles in the high-altitude, low-dynamic-pressure region. In reference 7, measured spacecraft rotation rates were used in the equations for the force-free motions of a symmetrical gyro to determine inertial rotations of the RAM C-I and C-II spacecraft. These were then utilized to estimate maximum wind angles on the assumption that the X-axis of each spacecraft was alined with its velocity vector at fourth-stage separation. In the present analysis measured spacecraft rotation rates were numerically integrated to obtain inertial rotations of the spacecraft. These rotations and the uncertainties in the direction of the relative velocity vector were used to estimate conservative maximum wind angles from 380 to 410 seconds.

Inertial rotations were determined from the following relationships:

$$\psi = \int_{t} \dot{\psi} \, dt + \psi_0 \tag{7}$$

$$\theta = \int_{t} \dot{\theta} \, dt + \theta_0 \tag{8}$$

$$\phi = \int_{t} \dot{\phi} \, dt + \phi_0 \tag{9}$$

$$\dot{\psi} = \frac{q \sin \phi + r \cos \phi}{\cos \theta} \tag{10}$$

$$\dot{\theta} = q \cos \phi - r \sin \phi \tag{11}$$

$$\dot{\phi} = p + q \tan \theta \sin \phi + r \tan \theta \cos \phi$$
 (12)

The lateral (pitch and yaw) gyros are measuring components of the roll angular velocity, as can be seen from figure 10(a). These components are due to misalinements between the gyro axes and the roll angular velocity vector. The values of angular misalinement required to produce these measured values were found to be

> $\delta = 0.35^{\circ}$ (yaw gyro) $\delta = 0.02^{\circ}$ (pitch gyro)

Whether these misalinements were due to an inertial unbalance (principal-axis misalinement) of the spacecraft or to a geometric misalinement of the instruments cannot be precisely established. However, the fact that values of roll rate measured by the lateral gyros were essentially the same after fourth-stage separation as before suggests an instrument misalinement. This was concluded since it is improbable that the same inertial unbalance would have been present in the fourth-stage—spacecraft configuration as in the spacecraft alone because of the significant differences in their moments of inertia.

Inertial rotations of the spacecraft obtained by integrating equations (7) to (9) over two different time intervals are shown in figure 15. Over each of these time intervals a comparison is made between the rotations obtained by using rotation rates corrected for the roll components (instrument misalinement) and the measured rotation rates (assumes inertial misalinement). The inclusion of the roll components can be seen in figure 15(a) to produce nutation and to increase the rotation angles over those obtained with the modified rotation rates. The differences are not as apparent from 405 to 410 seconds (fig. 15(b)), probably because of the increased effect of aerodynamics. Because the main use of the inertial rotations will be to estimate conservative maximum wind angles, inertial rotation obtained by using the measured lateral rotation rates will be employed.

In figure 8 it can be seen that the total wind angle η is the angle between the direction of the relative wind velocity and the spacecraft X-axis. Figure 16 illustrates the relationship between the total wind angle and the resultant inertial angle τ . For simplicity the X-axis of the spacecraft, the X-axis of the inertial frame, and the relative velocity vector are shown in the same plane. It can be seen in figure 16 that if the inertial X-axis and the relative velocity vector have the same direction, then $\tau \equiv \eta$. Thus, values of η determined from inertial rotations will be in error because of the uncertainty in the direction of the relative velocity vector with respect to the inertial frame. This uncertainty results from two factors: (1) the initial misalinement between the relative velocity and the inertial frame at the time that integration of the gyro data is started, and (2) the change with time in the direction of the relative velocity vector due to the rotation of the earth.

Figure 15(b) indicates conelike angular motion of the spacecraft from 405 to 410 seconds. When the cross plot of α and β over the same time interval in figure 17 is compared with the inertial rotations, it is apparent that the relative velocity vector was inside the inertial cone. The proximity of the relative velocity vector to the angular momentum vector at this time make it a good time to initiate integration of the gyro data to obtain inertial rotations. The origin of the inertial coordinate system was chosen as the approximate center of the rotation in figure 15(b) and integration was started at 405 seconds. Equations (7) to (9) were integrated forward to 410 seconds and backward to 380 seconds. Plots of the inertial rotation in 5-second intervals are shown in figure 18. The arrows indicate the direction of rotation and the solid circular symbols approximate the average direction of the angular momentum vector during the time interval. These plots show that the variation in inertial angle increased from about 3^o in the interval from 380 to 385 seconds to about 6.5° in the interval from 405 to 410 seconds and that the average direction of the angular momentum changed about 1.0° from 380 to 410 seconds.

Determinations of Conservative Maximum Wind Angles

First a resultant inertial angle τ was determined from each 5-second-interval plot by graphically measuring the distance from the origin to the outside rotation along a line passing through the angular momentum vector. A maximum value of η was then determined by adding linearly to this value of τ the initial uncertainty of the relative velocity assumed at 405 seconds η' and the total angular change in the relative frame with respect to the inertial frame. The equation for η_{max} is

$$\eta_{\max} = \tau_{\max} + \eta' + \hat{\Omega} \Delta t \tag{13}$$

where

ł

$$\dot{\Omega} = \sqrt{\dot{L}^2 + \dot{\lambda}^2} \tag{14}$$

$$\Delta t = 405 - t_{\rm p} \tag{15}$$

An initial uncertainty of 1^{0} was assumed on the basis of the error in the determination of wind angles at 405 seconds. The rotation of the relative frame was nearly constant over the entire time interval:

$$\dot{\mathbf{L}} = -0.028 \text{ deg/sec}$$

 $\dot{\lambda} = 0.068 \text{ deg/sec}$
 $\dot{\Omega} = 0.074 \text{ deg/sec}$

Figure 19 graphically illustrates the technique for obtaining conservative maximum total wind angles from the inertial plots. Figure 20 is a plot of the values of η_{max} from 380 to 410 seconds. The values were plotted at a time halfway through the time interval of the inertial-rotation plot. Shown also in this figure are the maximum total wind angles determined from acceleration data. It was shown in reference 7 that the cyclic changes in ion density measured by the electrostatic probes on the RAM C-II and C-II spacecraft were due to changes in the angle of attack. The locations of the RAM C-III probes relative to the angle-of-attack plane were identical with the probe locations on the RAM C-I and C-I and C-II and C-II spacecraft, and hence, the cyclic changes in ion density measured during the RAM C-III entry (see ref. 12) can be attributed to changes in angle of attack. The varia-

tion in angle of attack was shown in reference 7 to be $\alpha = \pm \eta_{\text{max}}$. The maximum wind angles are seen to be less than 5^o prior to resonance.

PITCH ROLL RESONANCE AND ROLL ANOMALY

Determination of Pitch Roll Resonance

It can be seen in figures 13 and 14 that the spacecraft continued to cone about the velocity vector until about 413 seconds, when the motions started to amplify. The resonance parameter

$$\frac{\omega_{O}}{\Delta\omega} = \frac{\sqrt{\frac{-C_{m}\eta^{Q_{\infty}}SD}{I_{l}} + \left(\frac{pI_{X}}{2I_{l}}\right)^{2}}}{p\left(1 - \frac{I_{X}}{2I_{l}}\right)}$$
(16)

was computed by using q_{∞} from table III and the measured roll rate p. The plot of the resonance parameter in figure 21 indicates that resonance amplification should have started at 415 seconds. The actual onset of amplification occurred 1 to 2 seconds prior to 415 seconds, as can be seen in figures 10, 11, 13, and 14. This early occurrence may have been because the total wind angle η was greater than zero for several seconds prior to resonance, and the effective moment coefficient may have been greater than C_{m_n} .

After 415 seconds both the oscillation and trim are greater in the β -plane than that in the α -plane. (See fig. 13.) It can be seen in figure 14 that the orientation of the lateral velocity ϕ' is essentially oscillating between 270° and 360° (0° to -90°). That is, the spacecraft is presenting only its fourth quadrant to the wind vector. The times of maximum roll deceleration can be seen in figure 14 to correspond to the times when η is about maximum and when ϕ' is increasing. At around 425 seconds, the spacecraft was undergoing small oscillations about a trim angle of approximately 2°. Thus the spacecraft X-axis coned about the relative velocity vector while the spacecraft presented only a few degrees of its circumference to the wind vector. The maximum wind angle of 8.5° which occurred at about 414.7 seconds is slightly greater than the maximum values reached during the resonance periods of the RAM C-I and C-II spacecraft.

Computer Simulation of Roll Anomaly

Unpublished studies by the authors indicated that the changes in roll rate which occurred during and after resonance conditions on the RAM C-I and C-II entries could be

attributed to a combination of an aerodynamic trim and an offset center of gravity. Therefore, a set of equations in six degrees of freedom were computer-programed with the capability to simulate an aerodynamic trim and an offset center of gravity. Because the location of the center of gravity and an aerodynamic trim could have varied as a result of unsymmetrical ablation of the heat shield, a period of time after most of the ablation had occurred was chosen for simulation of the RAM C-III spacecraft motions. The simulation period was 433 to 440 seconds. Angular motions were small during this period. (See figs. 10, 11, 13, and 14.) The trim angle was slightly greater than 1° , and the changes in orientation of the lateral velocity vector were small. It is during this period that the roll rate passes through zero. (See fig. 14.) Figure 22 shows the computed simulation of roll rate and the wind angles. Values of static moment coefficients at $\alpha = 0$ and center-of-gravity displacement required were

 $C_{m,0} = -0.0030$ $C_{n,0} = 0.0025$ $\Delta y = 1.22 \text{ mm} (0.004 \text{ ft})$ $\Delta z = 0$

The average value of roll is simulated well even though the small oscillations are not. The wind angles are simulated in magnitude and frequency at certain times, but the main point is that the general trends in the angles are matched up fairly well. This type of simulation demonstrates the plausibility that a combination of trim angle and offset center of gravity caused the roll deceleration experienced by the spacecraft.

CONCLUDING REMARKS

The RAM C-III flight experiment was launched from NASA Wallops Station September 30, 1970, to study the problem of radiofrequency blackout at an entry velocity of 7.407 km/sec (24 300 ft/sec). The flight is described, and data for the entry trajectory and environment, which include the effects of actual temperature measured the day of launch, are presented. An analysis of entry spacecraft motions was performed. This analysis included the determination of wind angles from measured accelerations and estimates of wind angles at high altitudes from gyro-measured rotation rates. The maximum wind angles were found to be less than 5° to the point of pitch roll resonance (an altitude of 35.052 km (115 000 ft)), where the total wind angle went to 8.5° and the roll rate started decreasing. A plausible cause for the decrease in roll rate was shown to be a combination of trim angle and an offset center of gravity.

Langley Research Center,

National Aeronautics and Space Administration, Hampton, Va., May 9, 1972.

APPENDIX

WORKING UNITS AND CONVERSION TO SI UNITS

The RAM C-III spacecraft was designed and fabricated to specifications in the U.S. Customary Units. All measurements (ground and flight) pertinent to the present paper were made in the U.S. Customary Units, and all data reduction and computations were made in that system. Graphical data were therefore plotted in the U.S. Customary Units. The final data were converted to SI Units, and a secondary SI scale is presented on each of the graphical figures. In other cases where numerical data are presented or discussed the value of each quantity is presented first in the SI Units followed by its value in the U.S. Customary Units. A list of the conversion factors used is given below. The conversion factors were taken from or derived from values given in reference 14. (1 n. mi. = 6080 ft herein.)

Physical quantity	U.S. Customary Unit	Conversion factor (*)	SI Unit
Length	feet feet inches inches	3.048×10^{-1} 3.048×10^{-4} 2.54 25.4	meters (m) kilometers (km) centimeters (cm) millimeters (mm)
Velocity		3.048 × 10-4 47.88	kilometers per second (km/sec) newtons per square meter (N/m ²)
Density	slugs/ft ³ pounds	515.379 4.536 × 10-1 1.357	kilograms per cubic meter (kg/m ³) kilograms (kg) kilogram-meters ² (kg-m ²)

^{*}Multiply value given in U.S. Customary Units by conversion factor to obtain equivalent value in SI Units.

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Event	Time, sec
Launch	0
First-stage burnout	76.70
Second-stage ignition	81.40
Second-stage burnout	123.50
Heat-shield ejection	262.40
Third-stage ignition	264.00
Third-stage burnout	299.00
Fourth-stage roll-up	319.60
Fourth-stage ignition	325.00
Fourth-stage burnout	359.00
Command signal to programer	362.24
Fourth-stage separation	372.56
Begin liquid injection	389.24
Begin VHF blackout	390.10
Probe retraction	401.30
End liquid injection	413.46
End VHF blackout	419.80
Impact	520.00

TABLE I.- TRAJECTORY EVENTS

TABLE II.- ENTRY-TRAJECTORY PARAMETERS

RANGE	NAUT. MI.	532.614 532.007	533.370	533 . 748	534.126	534.504	534.882	102.050	535.037 536 017	536.345	536.774	537.152	537.530	537.908	538.287	538.665	539.043	124.420	008.666	8/1°046	540.035	512 133	541.691	542.070	542.448	542.826	543.205	543.583	543.962	544 340	544°114	545.476	545.854	546.233	546.612	546.490	541.309 547 748	548-126	548-505	548.884	549.263	549.642	550.020	S.	50	101-100	Ŷ
HOP I ZONT AL		587.031	901.102 988.433	989.133	989.834	990.535	. 23	γι γ	992.631 003 338	ŝ	044 . 740	995.441	996.142	996.843	997.544	998.245	• 6*	999.641	1000.348	1001-049	1001-1001	1010-1011	1003 854	1004.555	1005.256	1005.957	1006.659	1007.360	1008.061	1008.162		1010-367	1011-568	1012.270	1012.972	1013-6/3	1014.373	1015.779	1016.481	1017.183	1017.885	1016.587	1019.289		1020.694	1021.396	1022.070
FLIGHT FLEVATION	DE	ភំម	-10.444		-15.443	-15.443	\$.			-15.447	-15.448	-15.450	-15.451	-15.453	-15.455	-15.457	-15.459	-15.462	-15.464	-15.466	-13.400	-15.470	-15.474	-15.476	-15.477	-15.478	-15.480	-15.481	-15.482	-15-482	-15-483	-15.483	-15.483	-15.482	-15.482	-15.481	-15.470	-15 477	-1476	-15.474	-15.473	-15.471	-15.469	ŝ	-15.465	-15.463
FI IGHT AZIMUTH	nëG	115.701	115 110	212-211	115.723	115.728	115.734	115.739	115.744	115 755	115.761	115.760	115.771	115.776	115.782	115.787	115.792	115.797	115.802	115.807	115.812	118.011	115 027	115.831	115.830	115.841	115.845	0	115.854	115.859	115.864	115 273	115.877	115.881	115.386	115.890	115.895	115 0/2	115 006	115.017	115.910	115-921	115.925	115.929	•	٠	115.942
YT I	FT/SEC	24218	81242	24210 24219	24219	24220	24221	24221	24221	22242	12212	24221	24221	24221	24221	24222	24222	24222	24272	24222	24222	77767	57747	52525	24224	24224	24224	24225	24226	24226	24227	24228	94224	24231	24232	24233	24234	26242	24230	076762	04242	24240	24242	24243	24244	24240	24247
VELUCITY	KM/ SEC	1.382	1.382	7 282	7.382	7.382	7.383	7.383	7.383	(999) 1 242		7.383	7.383	7. 383	7.383	1.383	1.383	7.383	7.383	7.383	1.383	1. 383	1.383	7. 184	7.383	7 383	7. 383	7.384	7.384	7.384	7. 384	7.385	7.345	7.346	7.380	1.386	7.381	1. 38/	196.1	1. 333 9.00	1 194	1997 - L	7.389	7.389	7.390	7.390	1.390
LUNGITUDE	DEG	-65.133	-65.326	617 - CO-	-65.305	-65.298	-65.291	-65.285	-65.278	1/2-69-	107°C0-	-63-250	-65.243	-65.236	-65.230	-65.223	-65.216	-65.209	- 65.202	-65.195	-65.188	-0,182	-65.175	-03-140			-05.140	-05.133	-65.127	-65.120	-65.113	-65.106	-00.044	-65.086	-65.079	-63.072	-65.065	-65.058	100.00-		÷.	100-00-			-65.003	- 64.956	-94-990
LATITUDE	UEG	34.440	54-443	34-440		34.432	34.424	34.421	34.424	34-421	014.410	14•47C	014.45	34.407	34.405	34.402	665-45	34.396	34.394	196.46	34.348	246.45	54.183		474.46	110000	1691.94	34.366	54.303	102.45	34.158	565.45 55	54• J2C	34.347	4+1+52	34.341	34.335	34.336	555.45	000.40 000 00	4.52		270.470 014.440	010.46	34.314	34.311	34.308
AL Í ITUJÉ	F T	330960	215022 2	010666	134381	133730	1933091	332440	1181155	741165	110000		173526	327931	321230	325041	325945	325345	224734	524058	323412	322706	122120	521414	130020		51 0000	213242	666115	51094d	115515	515054	500c15	102410	313067	512420	51173	311120	310475	209852	3051905	2000 C C C C C C C C C C C C C C C C C C	501092	100598	305952	دُل 3 د ل و	304059
ALFI	ž	202.7 05	102.509	102.512	101-914	101.123	101.520	101.330	cc1.101	100.937		240.00T	041-001	6 C Q . 6 Q	161.66	100.64	94. Joj	99.160	010.85	98.775	98 . 576	96.319	98.142	CDY.15	001-16	110.10	191-19	000-79	96.303	90.000	96.409	96.211	96.014	110.025	95.469	95.260	95.028	94.a3L	34.034	94.457	0+2-44	94.045	47° 440	010.040	93.254	7cv.c6	92 . đuỳ
7 I ME	SEC	S	380.10	340.20		380.50	380.60	3 80.70	380.80	380 - 90	00-18c	361-10	112 - 1 PC	131.40	341.50	381.60	381.70	U8.182	06.162	UU.286	942.LU	332.20	JUE. JUE	382.40	00.200		07-30C	387.94	38.00	01.685	33.20	بار. 185	343.40	00.005 112 145	383.70	10.00	02.205	384.00	3d4.lu	304.24	<u>0</u> 5.482	774.40	344.00	904+00	334.80	584.9U	00.485

HUPIZUNTAL RANGE	KM NALLT MI	000 651		-166	2.244 6	0 0 0 1	•						1029.829 555.708		5 556.	38 556.84	1 557.	1033.345 557.605	1 557	558		559	961 55	<u>u</u> 1	38.268 56	-1			ŝ	1041.786 562.160	ŝ	4 562.92	563.79	1044-001 303-079 1045 205 544 050	59-995	564.81	565	1		1049.529 566.338	4		567.4	567.85	3.050 568.23	5 568.61	9 568-99	1055.164 569.379	
FL TGHT ELEVATION	DEG	-15 463	u	÷.,	ດ ເ 4 ເ			•	1 1 1	1 4 1 4	• •	ع ۲	5		ċ		-15.440	-15.440	-15.440	-15.440	-15.440	<u>ئ</u> ،	-15.440	-15.440	-15.441	.	-15.442	• 4 4			Å .	Å.,	14461-	•	-15.450	-15.451	-15.452	-15.453	-15.455	-15.456	-15.458		-13-461	Å.,	۰° ۱	.	-15.469	-15.471	
FL I GHT AZI MUTH	016				110.420	115 959	96.5	96.5	179.411	115-976	116.980	115-984	• •	115.992	115.996	116.001	116.005	116.009	116.013	110.017	116.021	116.025	•		٥	.	116.046		116.055	116.059	116.063	o,	116.072	116.081	116.085	116.090	116.094	116.099	116.104	116.108	116.113	6•11 ·	110-122	21.	116.132	110.136		110.146	
VELOCITY	F1/SEC	3	94748	24.24.0	26250	24251	24251	24253	24253	24254	24255	24255	24256	24257	24257	24258	24258	24259	24260	24260	24260	24261	24261	24262	24263	24264	24264	24265	24200	19242	24208	0767C	24270	24271	24272	24272	24274	24274	24275	24276	24216	23	11242	61242	24219	61242	61242	4 4 4	
VELT	KM/SEC	7.390	105.7	102.7	101 1	7.392	1.392	1.392	7.392	1.393	1.143	1.353	7.393	7.394	1.394	٠	1.394	6٤.	7.394	7.394	7.394	7.355	1.355	7.395	(65 · /	1.396	1.396	955-1	0/6.1	166.1	1.25.1	146 -1	1.46.1	7.398	1.398	1.398	7.349	. 19	1.399	5	555 · 1	1.400			33		- + UU		107 6
LUNG IT UDE	DEG	-64.550	-64.583		44	1	64.		-04.541		÷	-64.921	-64.914	-64.907	-64.900	-64.893	-64.887	÷	-64.873	-64.866	-64.659	-04.852	-04.845	•••	-04.832 -66 035	0 4	-04-818	-04.511	-04.804	-64.191	-64.784 -64.784	-64.177	-64.770	-64.163	-64.756	-64.749	-64.742	-64.136	-64.129	-64.722	C11.40-	-04.100	-64 665		-04.088	100-10-			-66 660
LATITUDE	ULG	34. JUB	34.305	14.403	34-300	34.297	34.294	34.292	34.285	34-280	34.283	34\$ 280	34.278	34.275	34.272	34.265	34.266	34.204	34.20l	34.258	34.255	54.253	94.2.96	04-74 L	112.00 120 02	34• 24 T		002440			1 - 7 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 -	2 4 - V V V	34.215	34.216	34.214	112.46	34.208	34.205	34.202	34.200	141.40	101 76	34.182	701 77	2007-40 241-72		007 • LC		44.174
1 JUE	ЕT	94654 9465	304012	103360	302720	302073	301427	187005	dE100 L	584657	256843	298197	297551	296906	240260	2 556 14	294968	525452	293677	243031	685762	251739	560162	2 70448	20002	0616086	016207	210297	112102	11002	245279	784633	280986	C45282	282693	232047	231400	261082	20100	5C+612	210012 773165	27718	276871	216224	215576	214030	274241		14644
AL FIT JUE	× X	92-800	92.063	92.466	92.209	92.072	91.875	9178	91.48I	91.234	11.347	90.890	90.094	90.497	90.300	Э,	7 (89.110	610.48	.	87°179	8.4Z	00.120 00 0.00		200.000 28.1.58	2 C T - D D D D D D D D D D D D D D D D D D	177 28	1 - 2 - 2 - 2 - 2 - 2 - 2 - 2 - 2 - 2 -	87.347	87.150	5 C 7 O 9	30.75b	36.559	86.302	86.165	606.50	d5.171	4) C • C 8	00.01C	60 T • C 0	797 - 707 777	2	4 - 50	84.102	100-68	201.00	83-011		H 4.404
T I ME) EC	טט. כֿ8 כ	385.10	385.20	Uc.485	382.40	04.485	00.085	385.70	385.80	J 85.90	386.00	æ	530 - ZU	106.JU	380-40	00.000	280.00	000.000	Jdu. 80	100.000		01-100	287.54	387.41	16-785	187.60	487.70	387-80	387.90	386.00	388.10	383.20	344.30	388.40	388.50	386.60	288.7U		100-000 100-086	10.102	389.20	UC.98c	189-40	04 . 986	384.60	389.70		00.200

AL RANGE	NAUT. MI.	570.519	570.899	571.279	571.659	572.040	572.420	572.800	573.180	573.560	573.940	574.320	574.700	575.081	575.461	575.841	576-221	576-601	576.982		577.742						580.024	580.40			94C*18C	581.927	106°286	000.500	000000		584.211	584.592	¢.	585.354	585.734		580.49	586.87	62.1 86	581.63	588.021	588.402	200	101•101 575	4C • A 8
HOR I ZONT AL	5	27	1057.981	1058.686	1059.390		1060.799	1061.503	1062.208	1062.912	1063.617	1064-321	1065.026	1065.730	1066-435	1067.139	1067 .844	1068-548	1069.253	1069.958	1070.662	1071-367	1072.072	1072.777	1073.482	1074.186	1074.891	1075.596	1076.302	1077.007	1077.112	1078.417	1019-122	1040 533	020 1001	1081.945	1082.650	1083.356	1084.062	1084.768	85.47	86.18	1086.886	1087.592	1088.298	1089-004	2	- (1091.123	470°T60T	cfc•2601
FLIGHT ELEVATION	DEG	-15.478	-15.480	-15.482		ഹ	5	5	15.	6			, u		-15 500	-15,500	-15 500		-15.500	-15.499	-15-498	-15.497	-15.495	-15.493	-15.492	-15.490	-15.488	-15.485	-15.483	-15.480	-15.478	-15.475	-15.473	-12.4/1	-10.400	-15.464	-15.462	-15.460	-15.459	-15.457	-15.456	-15.455	-15.455	-15.454	-15.454	-15.455	-15.455	5. 45	ה ו	* •	-15.458
FL IGHT AZIMUTH	DEG	116.160	116.165	116.170	116.174	116.179	116-184	116.188	116.193	116.197	116.202	116 206	116-211	116 215	16	116 224	116 278	116.233	116.237	116.241	116.245	116 240	116.254	116.258	116-262	116.266	116.270	116.274	116.278	116.282	116.286	116.290	so .	116.298	116.302	CUC.011	5.31 15.31	116.318	116.322	6.32	116.329	116.334	116.338	116.342	116.346	35	35	6.35	116.363	116.367	116.371
LTY CITY	FT/SEC	5	24280	24279	24278	24278	24277	24277	24277	24270	24215	01313	21252	72070	01747	21212	34040	26275	24275	26.70	22272	26.275	74778	24278	24280	24281	24281	24282	24284	24288	24286	24285	24289	24290	24291	24242	24295	24296	24300	24298	24296	24300	24300	24301	24302	24302	24303	24303	24306	24303	24300
VFLOCITY	KM/ SEC	-	104-1	1.400	7-400	7.400	7.400	7-400	2.400		004.1	776 - 1 202 - 5	046.1	1111-1111-1111-1111-1111-1111-1111-1111-1111	556 · 1	666 ° 1	666°'	0.15 5	107 L		004 2		66C°2	•	104-1	7.401	7.401	7.401	7.402	7.403	7.402	7.402	7.403	7.404	7.404	; ;	C0+•/	2 405	7.407	7.406	7.405	7.407	1.407	7.407	7.407	7.407	7.408	7.408	7.408	7.408	1.4.07
LUNGITUDE	046			-66 433			-04-612	-64.605	-04-500		74C • + O -		+0+•) / 0		+00°+01		DCC •+0-	**C **Q		÷ .			-04.502		-64.490		-64.475	-64.468	-64.461	-64.455	-64.448	-64.441	-64.434	-04.427	-64.420	-64.414	-04*40-		-64-386	975-94-	-64.472	-64.306	-64.359	-64.352	-64.345	-64.338	-64.331	-64.325	-64.318	-64.311	-64.304
LATITUDE	nř.G	140	34 144		07.75		141 15		201.40	6 + T + T O	34.140	34.144	34.141	54.138	54.135	34-132	14.1.50	4 • • •	34-124	121.40	54° 11 0	011-40	011.40	011.40	34.101	101-46	34, 099	34.096	54.093	34.090	34.087	34.085	34.082	34.079	34.076	34.073	34.011		00- 1 0	14.050	24.025	34.054	34-051	34-048	34.045	34.042	34.040	14.037	54.034	34.031	34•028
AL LITUNE	1			040140	70117	172017	04160703	160607	C00447	201000	201102	6650	265824	262200	199407	263908	263234	262010	T96197	CICI07	260664	< 1002	005652	211862	253069	254777	750123	755475	754827	254178	055552	252882	252234	251586	250938	250291	249643	666872	040047	1301143	241033	04040	1111111	244463	4381	243168	24/520	241873	4122	240577	
ALFI	r N				410-20	v -	γr	170-78	670.10	670.18	81.428	81.230	8 L • U 32	60.835	•	80.439	80.241	80.0+4	19.846	2+0-61	15.450	662.61	540°6/	1 68 . 8 1	78.659	10.402	74.056	77-869	77.671	77.473	dL 11	77.078	70.331	70.083	76.480	16.289	160.091	469.41	060.01	55+°C)	200.001	10.104	74.701		74.315	74.118	73.920	73.723		73.328	
TIME	ل ا ا	300 10	00.020	01-066	02-065	05.075	190.40	06.065	390.60	390.10	390.80	390.90	00.196	91.1	391.20	UE.192	391.40	04.195	391.60	191.10	391.80	391.90	392.00	392.10	392.20		04•760 201 PU	200-200 200-60	00.366	347.80	3 92 . 91	393,00	393.10	343.20	05.592	393.4U	UZ.29ć	393.00	393. /0	08.646	06.595	5 94 • UU	54 4.10	07*560		201-102 202 ED	00.460	00+460 11-11-11-11-11-11-11-11-11-11-11-11-11-	14 - 46 C	194.90	UC.482

RANGE	NAUT. MI.	589.545	589.926	590.307	590.688	600 · 160	•	268.140	C12.24C	+6C*26C	C16.26C	943.356 202 202	543. [3]	611°+66	594.500	188°94°881	202.024 505.202	140°040	500.020	004-04C	101.070	201 - 102	046-146	164.140	216.075	149°846	C10.660	064 • 666	188.666	600-219	600-600	600.982	601.363	601-176	603 507	005 • 200 6 0 2 - 88 B	603.270	603.651	604.033	604.414	604.795	605.177	605.558	605.940	606.321	606.702	607.084	607.465	• 84	608.228	608.610
HOR I ZONTAL	¥	1092.535	1093.241		1094.654	095-0401	100.071	1096.113	104 - 407	1098.180	7 64 ° 86 0 7	1099.505	CUE.UU11	110.1011	1101.718	1102.424	161.6011		1104.044	1105.051		1106.065	1101.510	1108-0703	CO1 *0011	1104.484	1110.003	1110.905	1111-609	2.31	3.02	1113.129	1116 1436	പ്	1116 556	066 00 111	026-2111	1118.677	1119.383	0	1120.797	1121.504	1122.211	1122.918	1123.624	24.33	5.03	1125.745	26.45	1127.159	27.86
FLIGHT ELEVATION	DEG	-15.458	-15.459	-15.461	ທໍາ	+0+•11	-19-407	104-61-	-12.408	-15.472	å 1	÷.		÷.	-10.4/4			214.01-	-12-4/1	-15.410		-15-400	404°CT-	-15.40Z	-12.400	-13.428	-13.436	-15-454	-15.452	064.61-	-15.448	-15-445	-15 444	-15.444	• •••	5	-15.442	-15.442	-15.442	-15.443	- 15.444	•	•	٠	•	-15.453	45	-15.458	-15.461
FL I GHT AZI MUTH	DEG	116.371	116.376	116.380	110.384	110.387	110.345	110.398	110.403	104-011	110.412	116.416	110.421	116.426	116.430	116.435	1 16 - 44U	1 10 • 444	5+++ OII	110.454	864-011	110-463	110.408	714-011	114.011	184-011	110.480	110-491	110.449	116.500	116.505		116.014	116.574	116 578	116.533	116-537	116.541	116.545	116.549	116.552	116.556	116.560	116.563	116.566	9	116.570	116.572	6.57	116.575	6.57
YTT.	F1/SEC	24300	24303	24303	24303	24303	24303	24302	20242	24303	24302	24298	24301	24301	24301	24301	24300	24300	24300	24302	66767	24240	24242	86747	04747	86767	16747	16767	96747	24299	24245	26242	24294	20070	20275	CDC7C	24292	24291	24293	24290	24287	24289	428	24287	24287	24286	24286	24285	24288	24285	24281
VELOCITY	KM/ SEC	1.407	7.408	7.408	7.408	1.408	1.408	104-1		1.408	104.1	1.406	1.401	1.407	1.401	104-1	104-1			104-1	- +00	1.405	- +00	1.400		1.405	-+10	1.400	- 405	1.406	407 · /	10404	C04 - 1	204.7	7 405	1.404	7-404	7.404	7.405	7.404	7.403	7.403	7.403	1.403	7.403	7.402	1.402	7.402	7.403	7.402	40
LUNGITUDE	DEG	-64.304	-64.297	-64.250	-64.283	017+00-	-64.210	-64.263	067 **0-	647.49-	242.40-	-64.235	-04.229	-64.222	-64.215	-64.208	-64.201	+6T • 60 -	-04-18/		+J T • + 0 -	-04.101	-04-100	-04•133 -44 144	041-40-		CC1 • + 0 -	04.120	-04.114	-04-112	o、	660°+9-	-64.092	-64- (78		-64-064	;	4	-64.044	-64.037	-64.030	-64.023	-64.017	-64.010	-64.003	÷		'n	2	-63.569	-63.562
LATITUDE	ÜĒĠ	34.028	34.025	34.023	34.020		54°D 74	34-011			54°UU3	54.000	144.55	47.4.6.0	33.991	33.988	55.400 507 55		000.000	116.55	+14.00	216.66	202.00	006-5C		00-40C	330 66	004.00	33.922	242.55	345.346	242.25	55.940	450.65	C C C C C C C C C C C C C C C C C C C	9 Ch - F E	33.926	33.923	33.920	33.918	33.915	33.912	13.909	33.906	33.903	33.900	33 . 898	.89	33.892	33.889	33.880
ruue	17	233930	239282	233634	237986	10,,00	160052	240042	+60007	2 34 7 40	234038	233450	77877	661262	404152	068052	230201	666677	116072	797977	+T0177	C06077	116077	1000077	120622	616422	071677	010522	064222	221183	221130	220488	148412	218548	100210	217254	216607	196617	212314	214667	214021	213374	212727	212081	211434		210140	505464	208846	206199	207552
ALT ITUUE	ΣX	73.131	72.933	72.736	72.538	140.21	C+T*7/	11.940	1 1 - 1 - 1 - 1	100-11	1. L. J.J.	11.150	866.01	101.07	10.502	10.305	101-101	.	04.112	4) C * 6 0	116.40	611.60	0 201	0 8 • 1 0 t		00°07	00.172		161.10	c (. 244	01.402	CU2.10	6 / • UUS	66-614	55 415 55 415	64.219	66.022	65.825	05.623	65.431	462.60	utt.da	04.839	64.042	64.445	64.24B	140.40	63.854	5	03.454	63.202
TIME	SEC	395.00	U1.495	395.20	395.30	040.40	00.040	00°066	01.040		04.040	5 40.00	01-045	070010	06.955	5 46.40	596°50	00.040	01.045	540-BU	04.046	00-165	01-165	07.145 107 101	02 162	04-166	00.140	00-145 00-20C	591.10	391.80	391.90	00°875	598.1U	07-06 C	1.4 4.04	04.040	398.60	394.70	346.80	398.90	00.496	399.10	399.20	UE-99E	399.40	04.995	399.60	U7.99£	399.80	399.90	4 00.00

L RANGE	NAUT. MI.	608.610	608.991	609.372	609-754	010.130 410 614	010.010	010-070 611 270	6120110	100-110	7404710	624•210 208 Cly	101 217	613 567	107°610	017 330	112 - 119	615.002	615.673	615.854	616.235	616-616	616.998	617.379	617.760	618.141	618.522	618.903	619.284	619.664	620.045	620+426	620.807	621.188	621.569	621.950	166.229	622.712	623.093	623.474	623.854	624.235		624.997	625.378	625.759	626.139	626.520	626.901	242-120	621.662
HOR I ZONTAL	X	\sim	28.57	1129.279	1129.986	760.1511	740°1011	210 CTT	101 101 101	726 7211	07704611	1135 430	776 7611	1127 052	200.1211	1130 //5	C11 0211	01130 870	1140.585	106-1711	1141.998	1142.704	1143.410	1144.116	1144.822	1145.528	1146.234	1146.940	1147.646	1148.352	1149.058	1149.764	1150.470	1151.176	1151.882	1152.587	1153.293	1153.999	1154.705	1155.411	1156.117	1156.823	876./611	1158.234	1158.940	1159.646	1160.352	1161.057	9.	۰	1163.174
FLIGHT ELEVATION	<u> </u>	-15.461	ŝ	-15.467	-15.470	ດ 1		•	•	•	064°CT-	•		n u	-15 507	•		•	ي	•	-15-521	-15.522	-15.573	-15.523	-15.524	-15.523	-15.523	-15.521	-15.520	-15.517	-15.515	-15.512	-15.508	-15.505	-15.501	-		-15.488	• : -	۳	<u>.</u>	-15.470	-12.466	-15.462	-15.459	-15.455	-	-15.451	4	•	-15.447
FL LGHT AZI M'JTH	DEG	116.576	116.577	116.579	116.580	196.011	COC.011	116 504	114 500	007.011	114 507	116 596	110 507	116 500	116.604	116 407	019 911	116 613	116.617	116-620	116-624	116-627	116-630	116.634	116.637	116.640	116-643	116.646	116.648	116.650	116.652	116.654	116.655	116.657	116.659	116.661	116.664	116.666	116.668	116.671	116.674	116.677	116.680	116.684	116.689	116.694	116.699	116.705	116.711	:	116.725
VELOCITY	FT/SEC	24281	24284	24282	24280	08242	04242	61242 24278	0/247	00747	11242	21242	61343	12070	11252	27277	24201	24763	24265	24260	24255	24256	24254	24252	24249	24247	24246	24243	24244	24239	24235	24236	24234	24233	24231	24229	24228	24226	24227	24223	24219	24220	61262	24218	24215	24213	24211	24209	420	24204	24198
VELO	KM/SFC	104.1	7.402	7.401	7.401	104.1				104.1	000 0	7 202	0000 6	1.270			105.1	7 305	1. 196	405.1	595.7	7. 493	1.103	7.392	196.7	7.390	7.390	7.389	1.390	7.388	7.387	1.387	7.387	7.386	7.386	1.385	7.385	7.384	7.384	7.383	7.382	7.382	7.382	7.382	7.381	7.380	7.380	1.379	2	2	7.376
LCNGTTUDE	DEG	-63.962	-63.955	-63.548	-63.941	CCV+CO-	-63.520	126.60-	-15.00 c 7	106.60-	006 ° C0-	-63-894		-63-873		000.07-	-63 853	475 E4-	013 129 -	-63.63-	-63.825	-63-819	-63.812	-63.805	-63.798	-63.791	-63.784	-63.178	-63.771	-63.764	-63.757	-63.750	-63.744	-63.737	-63.730	-63.723	-63.716	-63.710	-63.703	-63•ö96	-63.689	-63.682	-63.676	-63.669	-63.662	-63.635	-63.648	-63.641	-63.635	.	-63.621
LATITUDE	DEG	33.386	33. 483	3.84	33.478	C 10.CC	210.00	200.00 240 65		130 000		00.000 2000 2000		200.00	640°CC		040.00	å r	2000 - 100 2007 - 100 2007 - 100		200°00	33.826	23.22	33.821	33.818	33.015	33.812	33.809	33.806	33.803	33.801	33.798	33.795	33.792	33.789	33.786	33.784	33.781	33.178	33.175	33.172	33.769	33.766	33.764		33.758	33.155	33.752	3.74	٠	33.744
ALTITUJE	1 1	201552	206904	200257	205609	204402	+ 7 C+O Z	200000 200000	010002		771107	2 010 2 5	C24002	199197	121661		191190	1 2 4 2 4 4		195733	1 44784	750571	10225	192635	191986	1661937	1 50688	6 2005 1	1893-30	188742	188093	187445	186796	1 do 1 4 8	185500	184853	184205	1 83558	182912	182265	181619	1 80973	180327	179681	179036	178340	177746	177101	L76456	58	175107
ALTI	Σ	v 3. 262	63.004	02.807	02.070	214.20	C17+70		000 • 1 0	1.000	01.400	107•10	01-040	00.072 40.494	140°01		047.00		50.7.03		000°04		1 0 X X	58.715	58.517	U26.84	58.122	57.924	57.720	57.529	155.74	57.133	56.935	56.738	56.24U	54.343	56.140	55 . 948	55.752	+cc.5c	5.357	55.161	54.964	54.107		64.375		Э•9	m.	3 . 5	196.63
TIME	SEC	400.30	400.10	400.20	400-30	400.40		00° 004		400-60 200 00	400-90	00*10 *		401.40	00.104		06-10+	00-104	CP 107		00.004	402.10	4.02 . 20	402.30	402.40	402.50	402.60	402.70	402.60	402.90	403.30	403.10	403.20	403.30	403.40	4.03.50	403.60	403.70	403.80	403.90	404-00	404.10	404.20	404.30	404.40	404.20	404.60	404.70	404.80	404.90	405.00

RANGE		NAUI . MI.	90 BC	10.01 20.01	908	0		40.00	30.23	20.00		00.01C		10.11.		632 007 632 007	h n	796.669		034.120	016.450	034.883 775 377	697.669 	033.044	636.023	636.402	636.781	631.16U	021.039 010 TC	816.160	038.296	679.85d	539.053 55.55	639.432	039.81U	040.188	040.000	110 - 744	176-140	041.033	010-240		160.24	80/*04	696 . 545	10.000	44.338	5 I 5 I	Ś.	• 40	45.84	46.218 46.594	
HOP I ZONT AL	3		53		ŝ	5	66-70	7 40	1168-111		60.07 60 62	70.00	170.07	1 V V V	55 - C L	20.57		1174 . 440	176 15	_	176 550		111-202	. 07.		1,5.6						295.5811			2000		87 786	001-10				. .		0 COV-14					472	0.108	90.809 51.55	1197.561 6 1198.257 6	
FLIGHT ELEVATION		-15.447		-15.447	-15.448	-15.450	-15.452	5 45	ŝ	5	2				5	-15.481	-15.485	15.48		-15 405	503	-15 503	-15 504		-15 500	• u	n .	-15 512		• • •	, u		- - -		, .		-15.508		5	, .	5.		5	• u	-15 487	, u		1	-10°4/9	i u		-15.468	
FL I GHT A ZI MUT H	050	116.725	· •	0	116.746	116.753	116.761		116.776	116.783	5	116.797	116.803	6.80	.81	ŝ	116.825		116-834	6 8 3) (116.847	116-851	116.855	116.859	116.863	116-867	116.870	116.874	116-879	5			116.897	116.902	116.907	116.912	116.918	116.923	116.928	116.934	16.93	116.945	16.95		•	ۍ (• • •	- 8 - 8		6.6	
VELACITY	F1/SEC	; 4	24198	24194	24191	24187	24183	24179	24174	24173	24165	24158	24155	24149	24145	24139	24133	24127	24122	11	24110	24102	24098	24042	24080	24079	24073	24066	24059	24055	24045	24035	24030	24022	24014	400	23997	23988	23978	397	23958	23946	23938	23926	23915	23903	23890	23878	386	385	283	382	
VELD	KM/SFC	1.376	7.376	•	7.373	7.372	7.371	1.370	• 36	7.368	. 36	.36	7.362	.36	7.359	7.358	7.356	7.354	7.352	7.351	7.349	.34	.34	7.343	.34	7.339	7.337	7.335	1.333	7.332	7.329	7.326	.32	7.322	7.319	31	7.314	7.312	7.308	7.306	7.302	7.299	7.296		28	7.286	1.282	N	12	27	1	26	
LUNGITUDE	DEG	-63.621	-63.614	-63.608	63.	m.	÷	÷	 .	o3 .	-63.560	-63.553	-63.546	-63.540	-63.533		-63.519	-63.513	-63.506	-63.499		-63.486		-63.472	-63.465	3.45	-63.452	-63.445	-63.438	-63.431	-63.425	÷.	-63.411	-	-63.398	-63.391	-63.384	-63.378	-63.371	-63.364		-63.351	~	-63.337	-63.331	-63.324	-63.317	-63.311	-63.304	-63.297	-63.290	÷.	
LATITUDE	DEG	33.744	33.741	33.738	33.735	55.132	33.129	33.726	53.123	3.72	3.71	33.715	33.712	33.709	33.706	£01.Eć	33.700	33.098	33.695	33.092	33.089	33.086	33.083	33.680	33.078	33.675	23.072	33.665	33.066	33.063	33.660	e.	e.	m.	33.049	33.046	33.043	40.5	m.	3.03	3.63	3.02	3- 62	3.62	3.02	3.61	33.015	33.612	3.60	3.60	33.603	33.601	
lUDE	FT	171671	174523	1/3879	1 13235	1667/1	146717	1/1302	1 10058	1/0014	169370	1 66 7 2 6	166081	107437	L 6793	100143	1 62504	1 ö486Ü	164216	163571	162921	162232	loló3J	160994	1 60350	159705	159061	154418	157774	157130	150487	155844	155201	L54558	153916	153273	152631	066141	151349	1207J8	10068	149428	148788	143149	147510	140871	146233	145596	144959	144322	143686	143051	
ALTITUDE	КM	192.53	291.5C	864°26	208-20		504 ° 7 C	57°713	110-20	51-82U	470.1c	51.42B	162.16	260.1c	50.d39	240.00	50.440	50.249	50.02	49.856	49.060	40404	49.207	49.071	48.875	48.678	48.482	48.230	48.090	47.d95	47.047	47.501	47.305	47.109	40.914	46.718	å.	46.321	46.131	4 2. 430	å .	4 3. 546	146.4*	45 . 150	44.961	+4.700	44.572	44.518	44.184	43.989	43.795	43.002	
TIME	SEC	405.00	405.10	403.20		412 PU		400°004		405-00		400.00	4 UO • L U	10.004	400.30		400.00	400.00	406.70	400-80	400.90	407.00	407.10	407.20	401.30	407.40	UC.TU4	407.60	407.70	401.80	401.90	404.00	408-10	408.20	404.30	404.40	408.50	408.00		408.80	408.90	404-00	404-10	409.20	409.30	C4.04	404.5U	409.00	409.70	409.80	06*60+	410.00	

TAL RANGE	NAUT . M	646.59	646.96	647.34	49	648-	648	648.84	64	64	649.96	\$	ç	\$	9	9		9	652.			0					625-894				657-728		658	658	659	659					001.002				200 663			664.22	1999 1999		
HOR I ZUNTAL	T T	1198.257	1198.952	1199.647	1200.341	1201.036	1201.729	1202.423	1203.115	1203.808	1204.499	1205.190	1205.881	1206.572	1207.261	1207-950	1208.639	1209.327	1210-012	1210-702	1211.388	1212.073	1212.58	1213 443	121+4121	1214-809	1215.692	1216.252	1217.534	51C-1121	1218-842	1219-569	1220.246	1220-922	1221.596	1222.270	1222.94	1223.61	1224.280	1225 4370	1226-234	1226 055	1227-627	1228.286	1228-951	14.00			31.58	40.00	7.75
FLIGHT ELEVATION	066	ໍ	-15.465	-15.463	-15.461	-15.459	5.4	-15.456	5.4	-15.454	-15.453	-15.453	-15.453	-15.453	-15.454	-15.454	-15.455	.	"	ئ	-15.462	-15.464	ئ ،	-15.469	ໍ.		-15.476	-15 401	-15.484	• •	ŝ	-15.491	-15.494	-15.496	-15.498	-15.500	-15.502	-15.504	-15.507 55 55	106.61-	-15 510	-12.910	-12.011	210.01-	-15.515	-16 -11 - 11 - 11 - 11 - 11 - 11 - 11 -		, i			20.
FL I GHT AZIMUTH	DEG	116.994	116.999	117.004	117.009	117	117	-	117	117	117	117.040	117.044	117.048	117.052	117.056	117.059		117	117	117	117	117	117	11/	117	117			2 T T			111	111	1	117	117	-	117	,					117 186	111	-	161-111	117 200	12.11	11/
VELOCITY	Ē	~		~	~			ه ۳				1 23658		2	2	~	~					0 23457			~	~	4 23340	~ ~	~ ~	v (2	40				CA CA	14 23012		~		~ ~	.	*•					6672	22		
VE	KM/ SEC	7.26	7.25	7.25	7.24	7.243	1.23	7.23	7.22	1.22	1.21	7.211	7.206	7.201	7.195	7.18	7.18	7.177	7.170	7.165	7.15	7.15	7.14	7.136	~		~ 1	1.105	1-098	160 1	180.7	7.063	7-054	7.045	7-034	7.02	~		9	• •	6.961 2.051	• 0·	••	• Q.	• •	- 0 - 0	0.891	0.010		÷ n • 0	6.9
L ONG LT UDE	DEG	-63.284	-63.277	-63.270	- 6	9-	-63.2	9-		9-	10	1	9	91	9-	9	4	10	٩ ١		9-	- 6	-6	9-	1	ł	1	,	1	1		-63-070	,	,	1	1	-63	-63.041	- 63. 034	63	m	63.	-63.	-63-	-62.	-62.	-62.	-62.	-62.		-62.958
LATITUDE	DEG	33.601	33.598	33. 595	33.592	33.585	33.586	33.583	33.581	33.57B	33.575	33.572	90c-55	33.506	33.564					942.65	33.547	33.544	33. 541	33.238	33.535	554.62	33.530					55. 510 52 512			33.505	33.502		.66	-55°	33.	33.	33.48	ι, m	~1			רד ,	33.465	33.466	33.464	33-461
ALT ITUNË	FT	143051	147416		141147		13988					130723	135093	135463	134834	134206	133578	132950	132323	131696	131070	130444	121819	123194	-	12794	٦	-	120079	~	124837							119897		118671			TT		1	310311	3	11380	11320	<u>∼</u> ∎.	100/11
ALT	κ.Χ.	43-602) ~	43.215	43.022	42-329	42.030	42.443	42.250	42-058	4 L - X - 5	41.673	41-481	41.289	41.097	40.900	c11.04	624.04	40.332	40.141	39.950	39.759	39.269	39.378	39.188	38.998	38.408	38.018	38.42 9	38.240	040.85	37.861	(10.10 717 fc	27 206	101 7 5 C	36.420	36.132	26.245	36.358	36.171	5 . 98	35.798	10.c	35.427	s5.242	35.057	34.872	34.088	•	34.521	4 4
TIME	SFC.	410.00		01-014	410.30	410-40	05 014	410.60	02-015	111-HU	00.014	00.114		411-20	411-50	411-40	114-114	411.60	411.70	411.80	411.90	412.00	412.10	412-20	412.30	412.40	412.50	412.60	412.70	412.80	412.90	413.00	413.10	413+20			413-60	413.70	413.80	413.90	414.00	414.10	414.20	414.30	414.40	414.50	414.00	414.70	414.80	414.90	-

L RANGE	Σ.	4.93	5.28	000.000	N 3	69	667.039	38	667.734	08	668.425	668.769	669.112	669.454	669.795	670.135	670.473	670.811	671.147	671.482	671.816	672.149	672.480	672.811	673.139	673.467	613.193	674.118	674.441	674.763	675.084	675.403	675.720	676.036	0 1 6 . 6 . 9 . 9 . 0	610-003	010.414	671.284	166-119	677-897	678.ZUZ	678.504	678.805	679.104	679.401	619.697	679.990	80.	680.571	٠	681.145
HURIZONTAL	¥		m 1	י וי	1234.202	1 1	16		1237.434	. 60	38.71	1239.352	1239.988	1240-621	1241.253	1241.883	1242.510	1243.136	1243.759	1244.380	1244.999	1245.615	1246.230	1246.842	1247.451	1248.058	1248.663	1249.264	1249.864	1250.460	1251.054	1251.645	1252.234	1252.819	1253.401	186.5621	166.4621	1255.131	01.00	1256.269	1256.832	1251.393	7.95	1258.505	1259.055	1259.603	1260.147	•68	• 22	1261.757	1262.286
FLIGHT ELEVATION	DEG	15.52	15.	-15. 52 	•	5	5	15.	15.	15.			-15.549	•	-15.555	-15.557	-15.560	-15.562	5.56	-15.565	•	-15.567	٠	ŝ	°.	-15.566	•	-15.502	5	\$	5.	15.	-	1 2	<u>.</u>	<u>, '</u>	•	<u>.</u>	<u>.</u>	-	-15.492	.	-15.480	ŝ	15.	-15.466	15	٠	• 46	-15.460	-15.461
FL I GHT AZI MUTH	EG	117.215	117.221	117.227	667•111 066 111	1 2 2 2 2	117.250	7.2	2	117.267	117.273	117.279	117.285	117.291	117.296	117.302	117.308	117.314		117.325		117.337	117.343	117.349	117.355	117.361	~	117.373	~	117.385	117.392	117.399			117.419	•	11/.433	٠	**		•			48			5	٠	.53	ŝ	117.548
ΙTY	FT/SEC	22409	22360	22307	22223	22141	800	22023	21965	10612	21834	21773	21707	21639	21571	21500	21428	21355	21284	21204	21123	21047	20966	20884	20798	20712	20624	20535	20447	20351	20254	20160	20062	19962	15860	96/51	26951	19545	04451	15327	15213	15102	18988	16873	18755	18636	3		16275	÷.	18022
VELOCITY	KM/ SEC	•	6.815	٠	0.183		•	6.713	6.695	6.675	59	63	01	59	6.575	6.553	6.531		6.437	6.463	6.438	6.415	39	6.365	6.339	6.313	6.286	6•259	6.232	6.203	6.173	6.145	6.115	6.084	6.053	6.022	066.4	5.957	624 ° C	5.891		• 82	. 78	5.752	11.	. 68	• 64	• 60		5.532	5.493
LUNGITUDE		-62.558	-62.952	-62.946	454.20- 550 Cir	0.00	10	62.91		-62-902	1		-62.884	~	-62.872	- 62 . E 6 6	-62.860	-62.654	-62.648	-62.842	-62.836	-62.830	-62.824	-62.819	-67.813	-62.807	-62.801	-62.795	-62.790	-62.784	-62.178	-62.773	-62.767	-62.762	-62.750	-62.150	-62.145	-62.139	-62.134	-62.129	-62.123	-62.718	-62.713	-62.707	-62.702	-62.697	62.69	2.¢	2.68		-62.671
LATITUDE	UEG	33.461	33.458	33.45 6	53.455 53. 55	004.00 844.44		33-442	14.440	33.437	13 434	33.432	33.429	33.427	33.424	33.421	33.415	33.416	33.414	33.411	33.40 U	33.406	33.403	33.401	33.398	33.396	33.393	195.55	33.388	33.386	33.383	33.381	33.379	33.376	33.374	33.371	33.369	33.367	33.364	33.362	33.159	n.	33.355	÷.	÷.	.	33.346	'n	ŝ	53	ŝ
TUDE	FΤ	100711	111402	110804	110208	100010	10801	107837	847101	100000	106074	105490	104907	104326	103747	103169	102593	102020	101447	1 3087 7	100309	64762	61165	93617	98058	97501	96946	56393	65843	95296	54751	94209	93670	93134	92600	. 52070	5154.5	51018	16406	89979	89464	88953	.+	41934	87438	m -	80444	c¢668	· •	84979	84438
ALT ITUDE	κx	34.138	33.955	33.773	190.55	00.410	677°CC	202.56	20-30 27-580	32.10	37.331	32-153	31.976	31.799	51.022	31.440	31.270	31.096	30.921	30.747	30.074	30.402	30.230	30.058	29.835	29.718	29.549	29.38L	29.213	29-046	28.480	28.715	28.551	28.387	28.224	28.005	27.902	27.742	27.583	27.423	27.209	27.115	26.958	2 6 . 804	26.051	5		6.13	, o	25.902	25.755
TIME	SEC	415.00	415.10	415.ZU	415-3U	410.40		415.70	415-40	12.14	4 1 a - 00	410-10	415.20	410.00	416.40	410.00	416.00	416.70	410.00	410.90	417.00	417.10	417.20	417.30	417.40	417.50	417.00	417.70	411.80	417.90	418.00	418.10	418.20	418.30	418.40	418.50	418.0U	418.70	418.80	418.90	419.JU	419.10	419.20	419.30	419.40	419.50	419.00	419.70	٠	419.90	420.00

. RANGE		688.293 688.516 688.516 689.172 689.172 689.807 689.807 689.807 690.819 690.621 690.622 691.208 691.208 691.208 691.538 691.774 691.588 691.774 692.140 692.140 692.140
HOR I ZONTAL	1262.286 1262.812 1263.813 1263.853 1264.879 1264.879 1264.879 1264.879 1264.879 1266.889 1266.884 1266.884 1266.884 1266.884 1266.884 1266.884 1266.884 1266.884 1266.884 1266.884 1266.884 1266.884 1270.706 1270.706 1277.953 1277.955 1277.555 1277.955 1277.555 127	1275,533 1276,767 1276,767 1276,761 12776,761 1277,559 1277,559 1277,559 1277,559 1277,559 1277,559 1277,559 1277,559 1277,559 1277,559 1278,239 1280,521 1281,985 1281,985 1281,985 1282,997 1282,997 1283,326 1283,326 1283,551
FLIGHT FLEVATION	$\begin{array}{c} -15.661\\ -15.662\\ -15.662\\ -15.662\\ -15.662\\ -15.662\\ -15.668\\ -15.668\\ -15.553\\ -15.553\\ -15.653\\ -15.653\\ -15.653\\ -15.668\\ -15.668\\ -15.668\\ -15.668\\ -15.668\\ -15.739\\ -15.7$	-15.793 -15.805 -15.805 -15.805 -15.818 -15.829 -15.861 -15.861 -15.861 -15.861 -15.861 -15.890 -15.908 -15.925 -15.001
FL IGHT AZIMUTH	117.548 117.5567 117.5567 117.5567 117.557 117.557 117.6507 117.651 117.653 117.653 117.653 117.653 117.653 117.653 117.659 117.659 117.757 117.757 117.754 117.757 117.759 117.759 117.759 117.751 117.881 117.881 117.881 117.8820 117.8820 117.8820 117.8820 117.8820	117.845 117.845 117.859 117.859 117.865 117.876 117.876 117.878 117.878 117.878 117.878 117.878 117.855 117.855 117.855 117.853 117.820 117.820 117.820 117.815 117.815
LTY	17902 17900 17900 17643 17643 175645 175645 17388 175645 165755 1757555 1757555 1757555 1757555 17575555 1757555 1757555555 175755555555	14220 14220 13926 13636 13636 13691 13692 13696 12615
VELOCITY		→ → → → → → → → → → → → → →
LONGITUDE	- 62, 651 - 62, 651 - 62, 656 - 62, 656 - 62, 656 - 62, 655 - 62, 6337 - 62, 6337 - 62, 6337 - 62, 6337 - 62, 6337 - 62, 5378 - 62, 53788 - 62, 53788 - 62, 53788 - 62, 53788 - 62, 53788 - 62, 53788	6 6 6 7 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5
LATITUDE		222222 222222 222222 222222 222222 22222
υE	844498 8454498 8454498 845072 8256072 8226072 8226072 8325647 745969 7755662 7755662 7755662 7755965 775562 775562 7755153 7755555 77555555 77555555 7755555555 77555555	72338 71571 71571 71571 708193 70818 708193 69309 669395 669395 66225 66225 66225 66726 657360 652346 657360 657360 657360 657360 657360 657360 657360 657360 657260 77727272727272727272727272727272727272
ALT ITUDE	25, 464 25, 464 25, 464 25, 464 25, 177 25, 177 25, 177 25, 177 25, 177 25, 177 24, 205 24, 205 24, 205 23, 934 23, 176 23, 176 23, 176 23, 176 22, 407 22, 40	21.919 21.919 21.919 21.919 21.919 21.919 21.919 21.919 21.919 20
TIME	4 4 2 2 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	**************************************

NAUT. MI. 692.673 692.673 693.017 693.017 693.186 693.518 693.518 693.518 693.518 693.4155 694.155 694.461 694.612 694.760 694.760 694.906 695.193 695.334 695.473 695.610 695.745 695.878 696.010 696.140 696.268 696.395 696.520 696.644 696.886 696.886 697.005 697.239 697.353 697.466 697.678 697.578 697.798 698.012 698.117 698.221 698.324 698.425 698.525 698.525 698.625 698.722 698.819 598.914 600.669 699.102 RANGE HOR I ZONTAL KM [283.65] [283.65] [284.289 [284.289 [284.91] [284.91] [284.91] [285.517 [285.814 [285.814 [285.814 [286.825] [286.8243 [286.963 [286.963 [286.963 [286.963 [286.963 [286.963 [286.963 [286.963 [286.963 [286.963 [286.963 [286.963 [286.963 [286.963 [286.963 [286.963 [286.963 [286.963 [286.953] [297.649 [297.546 [297.546 [297.640 [297.660 [297.660 [297.660 [297.660 [297.660 [297.660 [297.660 [297.660 [297.660 [297.660 [297.660 [297.660 [297.660 [297.660 [297.660 [297.660 [297.660 [295.060] [295.060] [295.060] [295.060] [295.060] [295.060] [295.217 295.392 FLIGHT ELEVATION -16.987 -17.030 -17.071 -17.110 -17.145 -17.145 -17.205 -17.205 -17.227 -16.617 -16.653 -16.691 -16.731 -16.731 -16.772 -16.857 -16.900 -16.944 FI. IGHT AZIMUTH () EG 117.808 117.808 117.808 117.808 117.808 117.810 117.819 117.819 117.819 117.827 117.927 117.932 117.993 117.993 117.993 117.993 117.993 117.962 117.9 117.836 117.803 117.769 117.734 117.629 117.597 117.566 117.539 117.516 17.472 117.467 17.663 17.482 17.483 VELOCITY 3.367 3.3267 3.22455 3.22455 3.22455 3.22456 3.22456 3.225962 2.9622 2.9486 2.9486 2.9486 2.9482 2.9482 2.9570 2.6704 2.6704 2.6704 2.599 2.5567 2.533 2.501 2.469 2.459 2.3478 2.3478 2.3478 2.348 2.348 2.348 2.348 2.348 2.348 2.252 2.252 2.181 2.169 2.103 2.1 M/ SEC .889 .866 .844 .821 .758 -62.445 -62.442 -62.439 -62.429 -62.429 -62.426 -62.424 -62.419 -62.416 -62.414 -62,412 -62,409 -62,407 -62,403 -62,403 -62,403 -62,403 -62,398 -62,398 -62,388 -62,388 -62,388 -62,388 -62,388 -62,378 -62,378 -62,378 UEG -62.468 -62.465 -62.465 -62.459 -62.459 -62.434 -62.431 -62.453 LUNGITUDE -62.370 -62.365 -02.363 -62.362 -62.360 -62.358 -62.358 -62.447 -62.437 -62.372 -62.367 -62.355 83.216 83.216 83.215 83.214 83.212 83.212 83.210 83.209 83.209 LATITUDE 33.207 33.207 33.206 33.206 33.204 53.204 53.204 33.202 33.202 33.200 33.200 33.199 33.198 33.197 ALT ITUDE 6.949 6.889 6.829 6.770 6.771 6.053 6.053 6.538 6.538 6.482 6.370 6.370 6.261 6.201 S EL 425-10 45-10 45-1 429.60 429.70 429.80 429.90 429.90 TIME

IL RANGE	NAUT. MI.	699.102	699.194	699.284	694°314	400 400	163 003	100.7004	271.660	44 . 80	644°864	770 0E2			212.007	100.240	700.368	100.444	700.519	700-594	700.667	700.740	700.811	700.882	700.952	701.021	701.089	701.156	701.223	701.288	701.353	701.417	701.480	701.543	701.604	701.665	czi • 10/	701.784	701.843	101.900	701.958	702.014	702.070	702.125	702.179	702.232	702.285	702.338	38			702.541
HOR I ZONT AL	¥	1295.564	1295.734	1295.903	1205 205	1204 205	1206.073	CCC.0721	C 1 / 0 6 7 1	80	1291.024	9/1-/671	126+1721	1291.419	1291-922	101 - 1671	1297.910	86	1298.191	1 29 8 • 32 9	1298.465	1298.599	1298.732	1298.863	1298.993	1299.121	1299.247	9.37	1299.495	1299.616	1299.736	1299.855	1299.972	1300.088	1300.202	1300.314	1300.425	1300.535	1300.643	1300.751	1300.857	1300.961	1301.064	1301.166	1301.266	1301.366	1301.464	1301.561	1301.657	1301.752	.84	1301.938
FLIGHT Elevation	DEG	-17.243	-17.253	-17.255	162-11-	-17 210	817 1 1-	-12 153	-11- 521 -11-	-1/-109	•	-10-94	• •	-		••	_	-16.540	-16.457	-16.376	-16.296	-16.221	-16.152	-16.089	-16.034	-15.989	-15.955	ŝ	-15.921	ŝ	-15.939	-15.968	-16.010	-16.066	-16.135	-16.218	-16.312	-16.419	-16.537	÷	-16.800	9	-17.094	-17.250	-17.410	-17.573	-17.739	-17.905	-18.073		-18.406	-18.571
FL I GHT A Z I MUT H	DEG	117.483	117.499	٠	4	010-111		040-111	6	111.734	11/ 18/	111.831		111.930	166.111	118.040	118.101	118.156	118.210	118.263	118.315	118.366	118.414	118.458	æ	8.53	118.573	118.605	118.633	118.658	118.680	118.700	118.716	118.729	118.739	118.747	118.753	118.757	118.760	118.761	œ	118.763	118.763	118.763	118.763	118.764	118.766	118.769	118.773	•	• 78	118.798
ITY	FT/SEC	5899	5829	5758	1895	0100			8040	5343	5125	5026		61 NG	6005	6464	4881	4818	4755	4696	4633	4571	4514	4456	4399	4343	4287	4232	4179	4129	4014	4021	3974	3925	3877	3830	3783	3738	3693	3653	3607	3563	3525	3484	3445	3407	3369	3332	3295	3262	3224	3186
VELCCITY	KM/ SEC	1.798	1.777	1.755	1.733	717.1	169-1	1 1 1 1 0		1.629	1.001	1.586	100.1	1.041	1.521	100.1	1.468	I.469	1.449	1.431	1.412	1.393	1.376	1.358	1.341	1.324	1.307	1.290	1.274	1.259	1.242	1.226	1.211	1.196	1.182	1.167	1.153	1.139	1.126	1.113	1.099	1.086	1.074	1.062	1.050	1.038	1.027	1.016	1.304	* 66 *	.983	116.
LONGITUDE	DEG	-62.355	-62.353	-62.352	-62.350	645 • 70-	-02.341	C+C • 79-	-02.344	-62.342	-62.341	-62.340	DCC-70-	-02.331	-62.335	-62.334	-62.333	-62.331	33	-62.329	-62.327	-62.326	-62.325	-62.324	-62.322	-62.321	-62.320	-62.319	-62.318	-62.316	-62.315	-62.314	-62.313	-62.312	-62.311	-62.310	-62.309	-62.308	-62.307	-62.306	-62.305	-62.304	-62.303	-62.302		-62.300	-62.299	~	-62.297	-62.296	-62.295	-62.295
LATIUDE	ÚEG	33.197	761.66	33.196	33.196	641.66	53. L94	541.CC	53.195	33.192	33.191	33.191	061.00	191.55	33.149	33.188	33.188	33.187	33.187	33.186	33.185	33.185	33.184	33.184	33.183	681.6 5	34.182	33.181	33.181	13.180	33.140	33.179	33.179	33.178	33.178	33.177	33.177	33.177	33.176	33.176	33.175	33.175	33.174	3.17	3.17	¿71.č£	33.172	33.172	33.172	33.171	33.171	33.170
UDE	FΤ	53173	96925	52825	52655	08426	02520	06126	C 6 6 1 C	51836	6/91c	6751C	11012	67719	51078	65406	5,1793	くぐらしく	51513	50385	50255	50126	50000	49876	49755	49635	49517	10464	4 9287	49174	49062	48352	44843	43735	48628	48521	48415	4.3310	43200	44101	1997	41894	16174	47688	47585	41482	47379	47276	41174	47072	46970	46868
ALTIUDE	ЖX	16.207	16.154	16.101	16.049	866°C1	n (.	'n.	ŝ	15.752	. .	10.07	15.613	15.269	224.41	15.482	15.440	15.398	15.357	15.318	15.278	15.240	15.202	15.105	15.129	15.095	15.057	15.023	14.988	14.954	14.921	14.387	14.854	14.422	14.789	14.727	1 4. 725	14.093	14.001	14.629	14.548	14.507	465.41	14.004	14.473	14.441	14 410	14.379	14.548	14.310	14.282
TIME	SEC	430.00	430 . lù	430.20	430.30	430.40	430-50	430.00	430.70	430.8U	430.90	431.00	431.10	431.20	431.50	431.40	431.50	431.60	431.70	431-80	431.90	432.00	432.LU	02.264	432.33	432.40	432.50	432.60	432.70	432.83	432.90	433.00	433.lu	433.20	433.53	433.40	433.50	433.00	433.70	433.60	433.90	434.00	434.10	434-20	434-30	434-40		434.60	434.70	434.80	434.90	30.

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RANGE		707 E.1	146.201			702.735	702.782		702.875	92	702.965	703.009	703.053	703.097	703.140	703.182	703.224	703.266	703.307	703.348	703.388	703.427	703.467	703.506	703.544	703.582	703.620	703.657	703.694	703.731	703.767	703.802	703.838	703.873	703.907	703.941	103.975	104-009	104.042		704 130	121.401	101-101	704 233		202 - 202	704.373	704.353	704.382		
HOR I ZONTAL				12021001	1302-2001	1302.297	1302.384	1302.471	1302.556	1302 • 640	1302.724	1302 . 806	1302.887	1302.968	1303.047	1303.126	1303.204	1303.281	1303.357	1303.432	1303.507	1303.581	1303.654	1303.726	1303.797	1303.868	1303.937	1304.006	1304.075	1304.142	1304.209	1304.275	1304.341	1304.405				1204 • 058								1305.186	1305.241	1305.296		5.403	1305.456
FLIGHT ELEVATION		010	110.01-	-18 800	-19-061-	-19.222	-19.384	6	-19.712	-19-879	-20.049	-20.223	-20.402	-20.586	-20.776	-20.971	-21.171	-21.376	-21.586	-21.798	-22.010	-22.221	-22.430	-22.634	-22.830	-23.017	-23.192	-23.351	-23.492	-23.613	-23.709	-23.779	-23.822	-23.833	-23.812	-23.758	800*67-	44C *C 2-	191.52-	-22 062	22.	-22.410	10) r~	-21.398	-21.028	-20.651	-20.273	9.90	-19.537	19.19
FL IGHT AZI MUTH	DEC	118 798	a	118.873	8.83	118.852	118.868	118.885	118.902	œ	118.939	118.958	118.975	118.991	119.004	119.016	119.026	119.034	119.040	119.043	119.045	119.045	119•042	119.035	119.026	119.014	• 00	88	118.969	118.951	θ	118.918	118.901	118.883	118.865	118-849	+C0 * 01 1	118.808	118.797	118.790	118.785	118-780	118.776	118.773	8.76	118.766	œ	118.758	118.752	118.744	118.736
117	ET/CEC	3186	3155	3121	3087	3055	3023	1662	5557	2931	2898	2866	2840	2810	2783	2755	2728	2701	2676	2653	2626	2600	2579	2555	2531	2509	2486	2463	2439	2417	2351	2365	2344	2321	96.77	2210	2210	1912	2166	2136	2104	2078	2048	2020	1661	1961	1532	1904	~	1848	
VELACITY	KM/CEC		296-		.941	166.	.921	-912	• 902	• 893	.883	.874	• 866	.856	.848	.840	.831	.823	.816	.809	. 800	. 792	. 786	. 779	• 771	. 165	. 758	.751	. 743	. 737	. 729	. 721	• 714	101.	001.	760.	- DD -	. 668	.060	160.	. 641	.633	.024	.616	.007	.598	• 589	084.	.572	. 563	• 554
LONGITUDE	DEG	-62.295	-62-244	-62.293	-62.292	-62.291	-62.291	-62.290	-62.289	-62.288	-62.287	-62.286	-62.286	-62.285	-62.284	-62.284	-62.283	-02.282	-62.281	-62.281	-62.280	-62.279	-62.278	-62.278	-62.277	-02.276	62 .	-62.275	-62.275	62 .	-62.273	62.	-62.212	212-29-	112.20-	-62.270	-42.249	-62.268	- 02.268	-62.267	-62.267	-62.266	-02.206	-62.265	-62.265	-62.264	-62.264	-62.263	-62.263	-62.762	-62.262
LATITUDE	ut G	33.170	33.170	33.170	33.165	33.165	33.168	33.168	33.168	53.167	33.167	33.167	33.166	33 . 166	33.166	33.165	33.165	33.165	33.164	33.164	JJ. 104	33.163	53.163	591.5C	33.162	33.162	33.162	13.161	33.161	33.161	33.161	33.160	101-55	33.10U	601•00 091 70		33.159	33.158	33.158	33.158	33.158	33.157	33.157	33.157	33.157	33.156	33.156	33.156	ςŢ.	• T 5	33.155
UVE.	FT	46808	46766	40665	40564	40463	46363	46263	46163	40063	45964	45865	45766	45668	45569	17 464	61664	47244	42177	42078	44 480	44862	44 / 83	44045	44000	15444	44589	66755	26154	44044	19954	43900	40804	43108	11011	4 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 -	43337	43248	43160	43075	42991	42910	42831	42754	42680	42608	42533	12474	42436	42344	42284
ALTITUUE	КM	14.285	14-254	14.223	14.153	14.102	14.131	14.101	14.070	14.040	14.010	13.480	13-949	13.920	15.889		12.030		13.110	13.140	13.110	13.660	13.030	13.020			13.53U	000-01		10++01	10°410	195.51	100001	770-01	13.265	13.137	13.209	13.182	13.155	13.129	13.104	13.079	13.005	13.031	13.009	12.987	12.960	12.945	12.925		12+088
TIME	SEC	435.00	435.10	U 2.564	435.30	435.40	435.JU	435.60	4.35.70	435.0U	435.90	436.JU	4 30• LU	430-20	430.30	430.40	400.00	430.60	420.10	430-80	100.400	431.UU	01-164	421.40	101-104 123 - 50		431.30	431.60	431.10	491.00	4.0 F • 40		4.20.10	4 48 - 40	438.40	Uč 854	438.00	438.70	438.80	438.50	434.00	439.10	439.20	439.30	439.40	439.50	439.6U	439.7U	439.dU	434.40	440-00

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TABLE III.- ENTRY-ENVIRONMENT PARAMETERS

MACH	2	27.07	2	27.07	27.	27.07	27.07	27.07	27.	27.07	27.07	27.	27.07	27.07	27.0	27.07	27.07	27.07	27-0	21.0.12	27.07	27.0	21.01	-12	12		10		-12	00°12	27.08	27.	27.08	27.	27.08	27.08	4 27.	5 27 . 09	8 21.09	1 27.		17 0	70°17 00	50°17 7				1.12 0	7 21.110
DYNAMIC PRESSURE	LBS/FT:	8.62 .18								• 49	• 49		.45	.93	.41	• 39	•36	• 84	• 32	• 28	. 76	• 24		8.67	9.15	4.03 202	PC . U	1.0.1	2002	2.70 2.46	3.40 4 42	25.38 .53	6.33	1.29	8.25	9.21	0.64 .6	50 .5	2.56 .6	3.99			1.e.) 	4. 20 2. 20 2. 20		2•01 •3	4•00 4•4	5.96	* *
DENSITY	S/FT**	355~	•4564E~	6.6776E-10	- 9070F-	.1458F	.39395-1	.65195~1	.9201F-1	•1990F…1	.4886F-1	.7908	.1047F-1	.4309F-1	709F-	01205-0	04695-0	08300	12055-	5955 -	19995-0	2418F-0	2854F-	33065~	3776E-0	42631-0	4 / /1 - 1 5 - 2 - 2 - 0	0 Z Y - 7 - 9	5643F-0	04111-0 70011 0	1 13	8252F-0	8915F-0	504F-0	3195-0	•1064E-	•1838	•2644F	• 3482F-	•4353F-	•5260F-	- 62 U3 F-	- 11851.	• # 2 0 4 t **	• 9268F •	• 03 75 - 0	.15%/1-0	727F-	C1 7 C .
DEN	ETER*	1	.3275E-	•44155-	•5597 ⊡ -	.6828	-31075-	-36165-	•0819 ^c -	.22565-	.37485-	.5306	•6924E-	 8605E- 	•0357E-	•21565-	•3955E-	.58165	•77485-	.97586-	.18406-	-40001-	•62475	.8576E-	-106660-	-3509E-	1.61215-01		-1601.	8.45795-07			!.	-01035-	1	•0856ē-	•12555-	.1670F-	•21025-	5516-	• 3018"-	.35048-	4011.4	-19864.	50845-	56555-	248	6867E	
ΛΕΓ UC Ι ΤΥ	FT/SEC	24218	24219	-	-	24219	24220	24221	24221	24221	24222	24221	24221	24221	24221	24221	24221	24222	24222	24222	24222	24222	24222	24222	24223	24223	24223	47747	24224	24224	24725	24220	24227	24228	24229	24229	24231	24232	24233	24234	24235	24236	24238	24240	24240	24240	24242	24243	14/44
VELG	KM/ SEC	7.382	7.382	7.382	7.382	7.382	7.382	7.383	7.383	7.383	7.383	7.383	7.383	7.383	7.383	7.383	7.383	7.383	7.383	7.383	7.383	7.383	7.383	7.383	7.383	7.383	7.383	1.383	7.383	7.383	1.384	1.284	7.384	7.385	7.385	7.395	7.386	7.386	7.386	7.397	7.387	7.387	Ωn -	100	• 38 • 38	• 38	.38	m i	7
TUDE	F T		31	335670	502	38	573	333091	332446	331801	331157	330511	329866	329222	328577	327931	327286	326641	325995	325349	324704	324058	323412	322766	322120	321474	320827	320181	319535	3188888	318242	242715 214040	316301	315654	315008	314361	313714	313067	312420	311773	311126	310479	309832	309186	308539	307892	307245	306598	505
ALTI	Σ ¥	. 70	02.50	02.31	02.11	16.10	01.72	01.52	01.33	01.13	00.93	0.74	00.54	00.34	00.15	.95	.75	3 . 56	9.36	9.16	1.6.8	3.77	3.57	3.37	3.18	7.98	7.78	7.59	7.39	7.19	00.1	96.8U3			5.01	5.81	5.62	5.42	5.22	5.02	4 • 83	4.63	6 • 4 3	4.24	4 . 04	3.84	3.64	3.45	ה ה
TIME	LL.	Q		2	ŝ	4	ŝ	Ŷ	~	œ	o	0	1	2	ŝ	4	ŝ	ð	~	æ	σ	0	-	~	G) -	4	ഹ	5	~ '	ωi	σ, e	333.00		16	14	un.	-0	1.	æ	<u>.</u>	0	-	14	Ľ.	×.	<u>ب</u>	~	· .	"

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Continued
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PARAMETERS
ENTRY-ENVIRONMENT
TABLE III

ACH		27.10		27.10	27	27.111	212	21	27	27	27	27.		27.	27.	27.	27.	27.	27.	27.44	27.44	27.44	27.44	27.	-	•	27.448	÷.	÷.	÷.	27.453		27.454	27.455		20	27.4	27.4	27.	27.46	1.46	.46	.46	.46	1.46	.46		.46	27.469	~
DYNAMIC PRESSURE	2 LBS/FT**	1.0	1.1	1.1	1.2	-	. .	1.3	1.4	1.4	1.5	1.5	1.6	1.7	1.7	1.3	1.9	1.9	2		~	2	2	2	2•5	2.6	2.7	2	2.9	3 ° 0	3•1	1911	4 I 4 I	ы т т	• •			•	•	•	-	۰.	7	"	5.51	1.	۰,	6.15	6.38	4
DYNAM IC						59.85	62.24	64.64	67.03	69.90	72.78	75.65	78.52	81.40	84.75	88.10	61.93	95.28	98.63	102.46	106.29	110.12	113.95		122.57	127.36	~	136.94	142.20	*	$\sim c$	158.48	164•23	170.45	10.01		7.2	204.45	212.11	219.77	227.91	236.53	245.15	<u>ع</u>	3.8	3.8	283.93	294.46	305.47	316.49
DENSITY	SLUGS/FT**3	3.66305-	•8042F	9511F	.1042E-	2640F-	• 4 3 035 - 0	6036F-	7843E-	9728F-	16935-	3743F-	881F-	3107E-0	0435"-0	2863F-	5295F-0	7703F-	02 03 F- 0	- 196	5485 - 0	8273F-0	1165E-	1585-	68F-0	492F0	836E-0	9.7303 ^E -0	1.0090F-0	I.0463F-0			1.166/4-03	1.2099t-08	•	34915		1.4509E-08	1.5047E-08			6	2	œ	an i	1.9412F-08	315-	878F-	52E~ 0	2.24565-08
DEN	KG/METER**3		-9606F-	۱.	1	.19765-	- 2833	.37265-	•46575-	• 5629F-	-66415-	.7698F-	800 ^E -	-97496.	•1147 <u>5</u> -	2398 ^E -	• 3652F-	-366	.61815-	5136-	903E-	3405-	.1831E-	• 33 73 E-	• 4976E-	4.6638F-06	4.83615-06	5.01485-06	5.2002F-06	5.3924E-06	5.5919E-06	00-36861.6	6.0129E-06	0662.		-9530F-	.2107E-			.04205-	• 3399 ⁶ -	•6491E-	-31696	• 3016E-	•6463E-	005E-	755-	-:09	597-	1.15735-05
VELOCITY	FT/SEC	24247	24248	24249	24250	24251	16242	24253	24253	24254	24255	24255	24256	24257	24257	24258	24258	2425a	24260	24260	24260	24261	24261	24262	24263	24264	5	426	24266	24267	24268	24/42	54242	24210	• •	24272	· .+	÷27	427	+27	24276	24277	24277	24279	427	427	24279	24279	428	24279
Ve L	KM/SEC	ŝ		7.391	1.391	7.392	1. 592	1. 392	7.392	7.393	7.393	7.393	7.393	7.394	m.	7.394	7.394	99	7.394	7.394	7.394	7.395	7.395	7.395	7.395	7.396	7.396	~ (с. С.	5		- 500 - 1		1.591		50	68	7.399	33			• •0	• •0		7.400	4		• +0	7.401	7.400
TUDE	F T	304659	304012	303366	302720	302073	301421	300781	300135	299483	298343	299197	297551	296906	· •	295614	294968	294323	293677	293031	292385	291739	291093	290448	289802	289156	288510	287864	287217	286571	285925	617687	201000	2834582	282693	282047	291400	280753	280106	279459	278812	278165	277518	276871	276224	275576	92	28	Q	272986
ALTITUD	¥	A 1	<u>~</u> 1	N	Ai	92.072			. .		_	\sim	\sim	0	0	\sim	C.	m.	-	~	~	~	-	-	<u> </u>	÷.,					•	Ξ.	2	Ξ.							•				•	•	٠	•	•	•
TI MF		35.	35.	32	35.	385.40		5	چ	5	35.	36.	36.	36.	36.	36.	36.	36.1		 20.	0			-	-	-	N 1			-		20	x x	2	α		8.6	8.	8° 8	8.9	0°6	9.1	6 •2	6 .	9 • 4	6°2	9.6	89.7	339.80	89.9

TABLE III.- ENTRY-ENVIRONMENT PARAMETERS - Continued

MACH		46	27.466	9	27.464	27.464	27.463	27.463	27.463	27.465	27.462	27.458	27.462	21.462	21.462	27.462	27.461	27.417	27.359	27.305		27.186	77.133	27.076	27.023	26.968	26.913	26.859	26.806	26.756	26.700	26.645	•	26.545	26.493	ŝ	6.3	6.3	26.291	~				740°07					•	5.5	201.02	co•c		
SSURE	S/FT	م	11.7	ŝ	7.65	ح	~	ŝ	α?	9.19	9.52			10.63	11-02	11.43	11.86	12.26	12.56	13.08	13.50	19.93	14.28	14.84	- 4	15.80		. 8. 9	17.34	7.8	18-44	19.00	19.60	20.20	20.82	21.45	22.10	22.77	23.45	24.16	24.88	25.61	26.38	27.16	27.99	28.11		30.41	٠	•	٠	34.12		
DYNAMIC PRESSUR	**2 LB	328.46	F4-045	362.35	366-28	11.085	304.05	40 B - 40	423-74	440-02	455.87			501 0V	521.64		17.1 HC				17.070		000	n i	10.01			180.44	80.4°00 810.76		10 000	000 72	21.000 21.000	01.140	906.86) r	058	1090-23	1122.79	156	1191.25	1226.21	1263.07	1300.42	1338.25	1377.51	1417.73	1458.30	1501.04	1544.61	38.	1633.67		
1 1 4		*	01468	547-0	2.5051E*-U8	- 18		1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	2.89865-08	1.10	816-	1	446-	190E~ 0	- 1680	-285-	51F-	- 199 -	4.1629F-08	-16862.	.43816-	•5817F-	2935	3075	367F	ò	5.3613E-08	5.5305F-08	5.7040F-08	5.882208	6.0655F-08	6.25355-08	4466	,	8483	7.05725-08	2112	C 1 6 4 4	7 0/ 055-08	36781	10001	1001	31720	0.1993	9-46888	0.7455	1.00281	1.03195-	1.06175-	1.09235-	1.1236F-	1.15575-		
DE NSI TY		S**3	20036-	.24485-	1.29115-05	.33905-	.38875-	-34045-	- 4939F-	.54945	.60705-	-66685-	.72985-	0-3069	126315-	-306Z	2.00085-05	152	2.14555-05	2154	2873	361	4371	2.5154 - 05	2.5958F-05	2.6784F-05	7.76315-05	2.8503 - 05	2.93975-05	3.03165-05	3.1260F-05			3.42465-05	52955-	6371E-	74745-	.86095-	97725-0	•	-21905-	344011	•				1 4 9 7 5	-: 7001.		4 11 801		55		
117		FT/SEC	~	24280	24279	24278	24278	24277	24277	24277	24279	24276	54273	24276	24276	24275	24276	24275	24275	24275	01070	24277	26.275	24278	81040	08696	18676	24281	24282	24284	24288	24286	24285	24289	24290	24291	24292	24294	24295	24296	24300	24298	24296	24300	24300	24301	24302			2430	24	2	24	
VFL0C11			1999	10	7.400	00		00	00	00	00	500	808	000	000	000	000	000	000	200							104.1	7 401		7.402	204-1	204 - 2	204 4	1.403	7.404		4		7.405			7.406	.40	7.407	7.407	1.407	4	7.407	7.409	7.408	•40	7.408	7.407	
30					0-01/2	701017	77207F	100070	140407			261107	200303	+C8C9/	207602	26433	263408	667697	262010	106107	11197	260664	260015	259366	258718	258069	257420	256772	256123	C1 4007	254821	254178	253530	252882	+C2/C2	250230	066062	5		5	, ñ	i ñ	ñ,	Ň	N	2	N	2		10	. ~			
3011111	ALIIG		WX	83.009	82.811	82.014	82.416	82.219	120-28	81.423	629.18	81.4 28	81.230	81.032	80.835	80.637	80.439	80.241	80.044	79.846	79.648	79.450	79.253	79.055	78.857	78.659	78.462	78.264	78.066	17.869	77.671	77.473	77.276	17.078	16.841	76.683	76.435	x (7 0	r 0	0	ç	2 5	2		5			0				151.57	•
	TIME		SEC	390.00	ŏ	390.20	390.30	390.40	õ	õ.	9	σ	390.90	α	391.10	391.20	391.30	or.	391.50	391.60	391.70	391.80	391.90	392.00	392.10	397.20	392.30	392.40	392.50	392.60	392.70	392.80	392.90	393.00	393.10	393.20	393.30	393.40	393.50	393.60	393. /0	393.80	393.90	394.00		07*+65	544*20 207 20	344°40	944 20	394.60	394.10	394.80	394.90	00 ° 66 §

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Continued
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PARAMETERS
- ENTRY-ENVIRONMENT
TABLE III

MACH		ŝ	.	5.56	5.51	25.466	5.41	5.37	ů,	5.28	5.23	.18	5.14	5.09	5.05	<u>°</u>	÷	°,		÷	÷	÷	24.701	+										- 24			24.119	:		•		16.	. 88	.84	.80	.76	. 72	- 68	3.6	3.61	3.57	
PRESSURE	L8S/FT**2	34.12	5.1	36.09	7.1	8.1	N.		÷.	2.6	m	44.97	46.21	47.48	80	50.10	51.45	52.84	54.26	55.73	~	5	0	ъ.	\$	5.1	6.8	8.6	0	22.27	74.06	75.94	06-11			3.9	•	8.2	90.47	N	95 • 04	97.37	θ.	102.25	104.76	3	۰,	•	115.35	118.18	1.0	en en
DYNAMIC P	NEWTONS/M**2	1633.67	80	7.9	6.8	27.	78.3	930.5	984 . 6		5.7	~ 1	2212.53	.		÷.	463.4	529.	7.9	۳° ۳	738	•	886.2	962.	ς.	20.	.10	35.0	3369.79	57.8	5.9	36.0	3729.85	*	_		4122.47	.8	331.	440.8	550.	s.	78.	895.	÷.	13	263.9	392.7	•	658.4	79	
DËNSITY	S/FT*	557F-0		2223F-	22685-	• 29 22 2-	.32841-	3 0 0 0 1	.4037F	44/011	• 4825F-	52345-	- 36036-	6081F-	6 5 2 UF-	69695-	7429E	78995-	83805-	• 88745-	.9377E-0	•9894F-	.0421F-	-0961F-	.1513F-	•2077E-0	-2654E-	• 3244F- 0	.38485-0	.4464E-0	.5095E-	.5740E-0	63995-	. 7071E-	-7759F-	• 8 4	2.9182F-07	-99166-	•0666F-0	.1433F-0	2217F-	0165-	•3834E-	- 4669E-	521F-	.6393F-	.7283E-	.3192E-	- 9118E -	-3890+	4.1035E-07	023
DËN	METER**	.95625-	•1258E-	• 2 9 9 5 5 - 0	-41135-	- J/ 60.	840971	10260.	• < 34411 • < 34411	しいりょうよ	-04020-	-35135-	-10100.	-28/82-	• 2 1 4 1 1 - •	140001		• 2 2 4 8 E -	-41215-	.72735-	-9865E-	•0253E-	0525E-	803F-	1.1087E-04	•1378F-	6756-		2915-	1.26082-04	1.2933 ^c -04	- u 9	.36055-	1.3952E-04	.4306	669E-	5040E-	418E-	58055-	6200E-	<u>.</u>	19	1	- 80	83075-	7565-	215°-	83E-	161	.0650	149E-	2 .16 585-04
VELOCITY	FT/SEC	2	20			24303			24305			24242	10642	24301	10642	24301	24300	24300	÷.	24302	24299	24296	24298	24299	24298	2429R	ح	24297	4	24299	24295	24292	24294	24293	24293	429	24292	429	3	24293	Y (¥	Υ.	÷.	24287	€.	42	42	428		24285	428
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MACH		23.609	23.461	23.422	23.386	23.349	23.312	23.276	23.242	23.213	23.190	23.173	23.156	23.136	23.117	790.44	23.078	23.058	23-043	23 020	27.008	600 66	201.022	770 22	++6-77	22.423	22.886 22.886	22.000 23 RAA	13 050	020 22	070°77	000.27	261.22	211.22	261.22	25.130	911°77	001.22	999 CC	2000000	22.4042	019 22	22.592	32.575	22 57 5 5 5 6 5 5 5 5 5 5 5 5 5 5 5 5 5 5	163 66	166.22	216-22	307 66	204.27	+0+•72	*			
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DYNAMIC PRES	/M**2 LB	5930	6075.01	6219.61	6361.UB	00100	1000	000000		1157.10	7328.99	1509.	1691.01	7889.67	8085.02	8284.68	8489.12	8698.36	8912.38	9134.07	9355.75	9582.70	9420.19	10059.59	10305-69	10555.62	10812.26	11075.60	11343.25	11620.95	11898.18	12183.54	12479.92	12780.13	13088.00	13401.61	13721.45	14050.86	14385.55	14730.76	15077.89	15432.68	15801.36	16175.78	16558.87	16946.65	17345.01	17751.03	18166.63	18594.68	19023.20	19460.35	•		
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VFL	S.F.	m	7.376	7.374	7.373	7.372	7.371	7.370	7.368	•	7.365	7.363	7.362	7.361	7.359	7.358	7.356	7.354	7.352	7.351	7.349	7.346	7.345	7.343	7.341	7.339	7.337	7.335	7.333	7.332	7.329	7.32.6	7.324	7.322	7.017	- 31 -	1.314				1.502	7 206	202.7	7. 289	7 286	7.282	7 370		+12 ·1	v (1.261	10101
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PRESSURE	1 DC/ET## 7	1390	57.3	14		2			- '		1 102 - 14	1/42.00	20.6811	20			4 • 7 6 7 6 6	۰ o	7.600	102.2	2122 • 84	204	262	225	686	100 40 40	2510-04	5		86-21/2		v u	8C*6767	4 900	10.000	610401C	06 0225	3415.96	9. 6	593.9	84.4	6.9	873.5	3971.19	m	4173.18	277.0	<u>م</u>	°	209		4821.33
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174	*****				•		-12004-	• • • • • • •	7683F-0	- 6136	• 06295	• 2160E-0	.3731E-	•5345E-	10035-	8704 ^E -		22435-	7.4086E-06	1. 59/85-06	7.7921E-06	7.59695-06	285-	153E-	-3676	+15F-	9.19565-06		.7261F-	•0003r-		1.0583F-05	1.08855-05	1.11975-05	1.1518101	1.18495-05 1.21201 25	L.2189F-U5	1	1.32735-05	1.3655F-05	- 495-0	1.4455E-05	1.48725-05	302 ^E -	455-	1.6200F-05	1		1.7648E-05	1 10-1	85	1.9226E-05
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CITY		71040	5 r	23809	23794	23//9	23763	23746	23730	23714	23700	23679	23658	23643	23624	23605	23585	23565	23546	23524	23507	23482	23457	23437	23413	23389	23365	23340	23314	23288	23263	23233	23200	23174	23143	23112	23079	23046	71067	61677	20002	22860	22823	778	22741	22693	22 653	~	22559	22514	22462	22409
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ΓΤΙΤΙΟΕ	,		143051	142416	141791	141147	140514	139881	139248	138616	137984	137353	136723	136793	135463	134834	134206	133578	132°50	132323	131696	131070	130444	129819	129194	128570	127946	127323	126701	126079	125458	124837	124217	123598	172979	122361	121744	121127	216071	168611	119671	118050			116229	_	1501	1441	1320	-	112671	112001
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PRE SSURE		ž	4827	. <			1 80.	6E.905c	435.7	563.7	ŝ	827.3	061.1		7	< 30.4	8	-	٠,	6773.82			1.0		20.1001	76•11+1	1010.42	1760.59	4	048.6	8193.53	338.5	8484-37	20		n (7	9062.90	2.00.2	48°Z	с.	°.5	9768.04	9905.19	10044.02	5	80	4	10563.49	89.6	811.1	931	048.5	0 6 7 1		0 0 0	5.6	11486.26
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45471 .840 2755 2.4975-01 4.83666-04 85781-04 85781-04 85781-69 85754.65 1807-56 45777 .813 7701 2.50475-01 4.97476-04 85781-64 8558.96 17786.0 45077 .813 7701 2.55375-01 4.97476-04 80501.61 17756.0 45078 .800 2655 2.55365-01 4.97476-04 80501.61 17756.0 44082 .771 2553 2.55365-01 4.97476-04 80501.61 1681.3 44787 .771 2553 2.55365-01 4.9776-04 80501.61 1681.3 44787 .771 2553 2.60775-04 73475.02 1573.8 44787 .771 2531 2.6176-01 5.03567-04 73475.32 1693.37 44787 .7751 256075-04 7731.45 7737.69 1573.8 44787 .775 2.60775-04 7347.62 1573.8 44787 .7751 2.60775-04 7347.64 1747	w	45569	. 848	2783	•4807	 8134E- 	249.7	64.0	.8.
7577 .331 7728 7.50445-01 .455465 1807.9 4577 .816 .5719 .55156-01 .455165-04 8554.96 1780.45 4517 .816 .571 .55156-01 4.9716-04 81051.45 1774.5 4517 .816 .5579 .55195-01 4.9716-04 81051.60 1681.3 45078 .800 2553 .253975-01 4.9716-04 8175.32 1774.5 44980 .779 .25516-01 4.97475-04 8175.340 1615.3 44487 .765 .2591 .2.53775-01 77373.40 1615.3 44487 .765 .26475-01 5.04325-04 7635.40 1692.15 44487 .765 .26475-01 5.04325-04 75354.02 1552.1 44487 .765 .26475-01 5.1175-04 75354.02 1552.1 44487 .765 .26475-04 5.1175-04 76394.42 15234.86 44487 .765 .26475-04 17147.24	÷	45471	. 840	2755	•49245-	-8360E-	873.6	35.2	•84
45775 .813 2701 2.5155-01 4.9816E-04 89525.96 17806 45078 .809 2651 2.5277E-01 4.9977E-04 84081.11 1756.0 45078 .809 2651 2.5277E-01 4.9778F-04 80931.45 1734.2 44980 .809 2651 2.55795-01 4.9778F-04 80931.45 1774.2 44887 .772 2557 2.55785-01 4.9778E-04 8052.1 8052.1 44487 .771 2555 2.55785-01 4.9778-04 8093.47 1776.2 44487 .771 2557 2.6077-01 5.04975-04 77318.57 15529.2 74487 .771 2557 2.6077-01 5.04975-04 77318.57 15529.2 74487 .773 2.5439 2.6477-01 5.14137-42 15959.37 14417.2 74484 .773 2.5476-04 5.14135-04 77318.57 15529.2 74484 .773 2.5476-04 5.14135-04 713218.57	30	45373	.831	2728	• 50415-	- 8588E-	564.6	01.9	2.818
45177 .816 2676 2.5277E-01 4.9045F-04 84081.11 1756.0 45078 .809 2653 2.5516E-01 4.9738F-04 8175.47 1707.0 44882 .772 2600 2.5516E-01 4.9718F-04 8175.47 1707.0 44882 .778 25516E-01 4.9718F-04 8175.32 1662.1 44783 .771 2531 2.5536E-01 4.9718F-04 8175.32 1662.1 44788 .771 2531 2.5536E-01 5.04257-04 73737.60 1615.9 44489 .771 2531 2.60075-01 5.04257-04 73318.67 1573.12 44489 .771 2543 2.6477-01 5.04557-04 74317.42 1552.1 44489 .771 2417 2.6622E-01 5.04557-04 74317.42 1552.1 44499 .771 2417 2.6622E-01 5.04557-04 74317.42 1552.1 44994 .771 2463 2.6622E-01 5.14176-04 73241.82 1552.1 44994 .771 2463 2.6622E-01	300	45275	. 82 3	2701	•5159E-	.8816E-	258.	80.6	• 79
\$6778 .009 2653 2.53975-01 4.9778-04 83034.45 1773.2 44783 .779 260.5 2.553975-01 4.9778-04 80501.60 1881.3 44783 .779 260.5 2.553975-01 4.97475-04 80501.60 1862.1 44783 .779 2500 2.553975-01 5.04575-04 7373.60 1681.3 4488 .771 2555 2.553975-01 5.04575-04 75374.02 1653.63 44936 .771 2553 2.663775-01 5.04575-04 75374.02 1573.43 44094 .753 2463 2.662265-01 5.04575-04 75374.02 1573.42 44094 .773 2343 2.662275-01 5.14135-04 7321.42 1573.42 44094 .773 2443 2.662275-01 5.14435-04 16417.2 1573.42 44094 .772 2444 2.645275-04 7224.1.82 1593.42 44094 .772 234.4 2.645275-04 7237.1.92	770	45177	.816	2676	- 52 77E-	-9045E-	4081.	56.0	•
110 44980 580 2.55165-01 4.95105-04 81735.47 1707.0 680 44783 778 25595-01 4.95795-04 79532.78 1681.3 650 44783 778 25595-01 4.97795-04 75372.69 1661.59 650 44783 778 25595-01 5.004227-04 75372.60 1691.59 650 44487 758 250 2.61265-01 5.094227-04 75374.02 1573.48 650 44487 758 250 2.61265-01 5.094227-04 75374.02 1573.48 650 44487 758 2669 2.61265-01 5.09376-04 75374.02 1573.48 650 44197 751 250 2.6173.60 16115.91 1493.47 670 44197 753 264975-01 5.11725-04 73214.92 1552.11 670 44197 771 2.664975-01 5.1435-04 71025.19 1493.43 670 44197 771 <t< td=""><td>12</td><td>45078</td><td>.809</td><td>2653</td><td>-3791E-</td><td>-9278F-</td><td>3034.</td><td>734.2</td><td>•14</td></t<>	12	45078	.809	2653	-3791E-	-9278F-	3034.	734.2	•14
680 44882 .772 256367-01 4.974F-04 80501.60 1681.3 650 44885 .773 2557 255957-01 5.0214F-04 70575.32 1615.95 650 44485 .771 7531 2.60075-01 5.04975-04 70375.40 1615.95 650 44487 .776 2559 2.60075-01 5.04975-04 7337.42 1657.32 650 44487 .7763 25487 2.60375F-01 7.11725-04 7337.42 1573.40 650 44997 .773 2439 2.654775-01 5.117725-04 7337.42 1573.42 670 44094 .773 2437 2.64376-01 5.144357 1573.42 670 44094 .773 2.64376-01 5.144357 1573.42 1573.42 741 2.743 2.64376-01 5.144357 17241.82 1573.42 741 2.264376-01 5.144356-04 73241.82 1431.42 1593.40 741 2.233 2.64376-01 5.144356-04 73241.82 1574.82 741 2.6543	7	44980	. 800	2626	.55165-	-9510E-	1735.	01.0	
650 44783 778 2579 2.5788F-01 4.6979E-04 79582.78 16622.1 650 44487 775 2555 2.58797-01 5.0457E-04 77375.62 16595.95 650 44487 775 2557 2.62467-01 5.0457E-04 7537.60 15573.8 1652.1 650 44487 775 2463 2.62467-01 5.1177.42 2595.29 1573.8 15533.8 1573.8 1573.8 1573.8 1573.8 1573.8 1573.8 1573.8 1573.8	39	44882	. 792	2600	-5636E-	-9743F-	0501	81.3	
620 44685 .779 2555 2.58995-01 5.0627E-04 77373.60 1615.9 590 44437 .7531 2.60072-01 5.0627E-04 77373.60 1615.9 560 44437 .753 2.60072-01 5.0627E-04 75354.02 1573.3 560 44437 .751 2463 2.60072-01 5.0930E-04 7537.40 1595.3 570 44297 .751 2446 2.6077-01 5.0930E-04 75354.02 1573.3 670 4497 .773 243 2.6622E-01 5.1413E-04 73218.57 1508.3 6710 44947 .773 2541 2.6622E-01 5.1413E-04 73218.57 1592.3 6710 4797 .773 2557-04 77241.87 15522.3 371 4717.2 2571.04 7241.87 1367.42 15522.3 372 43804 .710 2331 2.66947-04 65930.402 14780.43 372 43804 .710 2.71496-01 5.14957-04 69801.91.91 14717.2 374 436	5	44783	. 786	2579	-38515.	-36165	9582	62.1	2.664
590 4458 .771 7531 2.60075-01 5.04525-04 7737.60 1615-9 560 44487 .755 2580 2.6475-01 5.0393.57.04 7337.60 1615-9 560 44487 .751 2548 2.64775-01 5.0393.57.04 7534.02 1573.60 570 44192 .751 2549 2.64775-01 5.0393.57.04 73241.82 1573.43 571 44192 .773 2439 2.64775-01 5.1175-04 74317.42 1573.42 571 4700 .771 2343 2.662275-01 5.118555-04 71025.19 1493.63 331 43001 .771 2344 2.64765-01 5.18555-04 71025.19 1493.63 3321 43104 .771 2344 2.64765-01 5.18555-04 7102.42 1550.93.57 3321 43104 .771 2314 2.64375-01 67494.91 1441.25 3321 43176 6518 2.74065-01 5.1356-04	53	44685	.179	2555	-36795-	02145-	8475	9	. 63
560 44487 .765 2503 2.61265-01 5.0692F-04 75354.02 1573.69 530 44197 .751 2.64367-01 5.01135-04 73354.02 15534.02 501 44197 .751 2.463 2.64377-01 5.01137-04 73318.57 1553-02 670 44197 .751 2.463 2.64376-01 5.11125-04 73318.57 1553-02 610 43977 .723 2.417 2.66226-01 5.14137-04 73218.57 1529.23 351 43904 .721 2.344 2.66976-01 5.143669 73218.57 1493.48 3322 43104 .714 2344 2.66976-01 5.21366-04 6599.37 1443.47 2537 43104 .714 2344 2.66976-01 5.14356-04 65993.37 1447.2 2537 43304 .710 22321 2.73386-04 65993.37 1417.2 254 2549166-01 5.1186-04 659993.77 14570.2 1371.42	5	44586	. 171	2531	.60025-	04525-	7373	S.	.61
530 44389 .758 2486 2.62487-01 5.093057-04 75354.02 15523.1 640 44197 .751 2.643757-01 5.11475-04 74317.42 15523.1 640 44197 .731 2.463 2.64375-01 5.11475-04 72311.82 15523.1 640 44097 .731 2.417 2.66476-01 5.11475-04 72241.82 15523.1 641 373 2.391 2.64376-01 5.11475-04 71025.19 1493.4 710 43907 .771 2.351 2.64376-01 5.21895-04 69811.91 1458.03 332 43708 .714 2344 2.73356-04 6789.37 1417.2 254 43520 .667 2.73356-04 5.23776-04 6789.37 1417.2 254 43520 .677 2.37356-04 5.23376-04 6789.37 1417.2 254 4351 2.7406-01 5.23776-04 5710.97 1307.9 1417.2 254 4364 2.74066-01 5.23767-04 6799.13 1417.2 254	56	44487	. 765	2509	.61265-	926-	6395	ŝ	٠
500 44290 771 2463 2.63735-01 5.11726-04 74317.42 1529.2 410 4797 773 2433 2.64577-01 5.11655-04 72241.82 1559.2 410 4730 772 2.433 2.64577-01 5.11655-04 72241.82 1559.2 410 4730 771 2345 2.6557-04 72241.82 1493.4 351 4300 714 2344 2.654570 5.11657-04 72241.82 1493.4 325 43708 771 2344 2.66947-01 5.21657-04 6704.98 1307.9 255 4350 .692 2270 2.71186-01 5.23557-04 67859.37 1417.2 255 4351 .707 2321 2.7496-01 5.33587-04 67981.191 1478.0 255 4352 .692 2244 2.7496-01 5.33286-04 6704.98 1307.9 256 4352 .684 2740 273657-04 669893.57 1417.2 1307.9 259 4356 .684 2740 2668	3	44389	. 758	2486	.62485-	-306	5354	æ.	• 56
4107 44197 743 2439 2.64975-01 5.14135-04 73218.57 1559.2 440 44094 773 2417 2.66475-01 5.16135-04 72241.82 1508.8 351 4300 .721 2355 2.66745-01 5.1675-04 72241.82 1508.8 351 4300 .721 2345 2.6976-01 5.16755-04 71025.19 1458.0 352 43708 .710 2344 2.6945-01 5.2186-04 69811.91 1458.0 255 43520 .697 2270 2.774065-01 5.21367-04 67893.57 1438.8 255 43520 .697 2.27740 68893.57 1438.8 1357.9 255 43708 .678 2218 2.774045-01 5.23776-04 65893.57 1417.2 267 4352 .676 2218 2.776046-01 5.33586-04 65887.52 1347.4 274 .676 2218 2.77259-01 5.3586-04 65887.52 1347.4 284 .6764 2848666 .772264 66887.57	8	44290	.751	2463	.6373E-	725-	4317	-	• 54
4400 44094 737 2417 $2.6622E-01$ $5.1655-04$ 72241.82 1508.8 381 43907 772 2345 $2.6762-01$ $5.1855-04$ 71025.19 1493.4 381 43907 $.772$ 2345 $2.65942E-01$ $5.2377E-04$ 61859.37 1417.2 381 43807 $.714$ 2345 $2.65942E-01$ $5.2377E-04$ 61859.37 1417.2 255 43814 $.707$ 2321 $2.7740E-01$ $5.2618E-04$ 68993.57 1472.2 255 43614 $.700$ 2294 $2.7740E-01$ $5.2385E-04$ 657064.98 1397.1 255 43327 $.6692$ 22770 $2.7740E-01$ $5.3395E-04$ 657064.98 1397.1 207 43377 $.676$ 2270 $2.7722E-01$ $5.3395E-04$ 65906.46 1317.4 208 43377 $.6671$ 22136 $2.7722E-01$ $5.3789E-04$ 65900.46 1317.4 207 4377 $.6661$ $2.7722E-01$ $5.3789E-04$ 65900.46 1291.0 129 4377 $.6602$ 2136 $2.7722E-01$ $5.4236E-04$ 65900.46 1291.0 129 4377 $.6601$ 2136 $2.7722E-01$ $5.4256E-04$ 65900.46 1291.0 129 4377 $.6611$ 2104 $2.7722E-01$ $5.4256E-04$ 65090.46 1291.0 129 42910 $.6601$ 21366 $2.7722E-01$ $5.4256E-04$ 65091.02 $1291.$	3	44192	. 743	2439	•6497 <u>5</u> -	137-	3218	~	
410 43997 .729 2391 2.61465-01 5.11855-04 71025.19 1458.0 351 43804 .714 2344 2.68705-01 5.21365 69811.91 1458.0 355 43708 .701 2344 2.68705-01 5.21365 64873.57 1417.2 255 4350 .701 2321 2.71186-01 5.21365 6474.98 1367.9 255 43520 .684 2700 2.72446-01 5.30357-04 6681.91 137.2 255 4337 .676 2244 2.770645-01 5.330957-04 6592.231 1417.2 269 4337 .676 2244 2.77065-01 5.330957-04 66911.91 1291.0 279 4337 .676 2244 2.77065-01 5.33286-04 66704.98 1347.5 284 4337 .666 2191 2.77225-01 5.33286-04 661816.91 1291.0 115 43075 .676 22144 2.77225-01 5.42365-04 661816.91 1291.0 1129 43075 .660	4	44094	. 737	2417	•6622E-	55° -	2241	Φ.	• 49
381 43°00 .721 2365 2.68305-01 5.21365-04 69811.91 1438.9 351 43804 .714 2344 2.69945-01 5.21365-04 66993.57 1417.2 324 43614 .700 22321 2.71495-01 5.25185-04 667859.37 1417.2 255 43514 .700 2226 2.77496-01 5.231385-04 6579.49 1367.9 255 43520 .697 2.2710 2.73635-01 5.23188-04 6579.37 1417.2 265 43526 .697 .5710.72 1367.9 1367.9 1367.9 209 43337 .668 2191 2.772645-01 5.33285-04 64287.52 1342.56 209 43337 .668 2191 2.772645-01 5.317895-04 6599.37 126711 1182 43248 .668 2191 2.77225-01 5.317895-04 6599.49 1317.4 1182 43075 .651 2.77226-01 5.37895-04 6660.23 1267.11 1199 .651 2191 2.77226-01 <td< td=""><td>3</td><td>43997</td><td>.729</td><td>2391</td><td>•6746^c-</td><td>955-</td><td>1025</td><td>4</td><td>•</td></td<>	3	43997	.729	2391	•6746 ^c -	955-	1025	4	•
351 43804 .714 2344 2.69945-01 5.2377F-04 68893.57 1417.2 259 43708 .707 2321 2.71186-01 5.2357E-04 667859.37 1417.2 259 43514 .700 22796 2.77146-01 5.2355F-04 667859.37 1417.2 259 43520 .692 22700 2.7748F-01 5.2355F-04 657859.37 1417.2 269 43520 .692 22700 2.7748F-01 5.2355F-04 65486152 1347.4 209 43377 .676 2.7789F-01 5.3328F-04 64287.52 1347.4 1129 43248 .668 2191 2.7604F-01 5.3328F-04 64287.52 1347.4 1129 43248 .668 2191 2.77604F-01 5.4316F-04 61816.91 1297.0 1129 43248 .668 2191 2.77504F-01 5.4016F-04 61816.91 1297.1 1129 4291 .661 217325F-01 5.4176F-04 55511.81 1180.2 1129 4281 .651 21665F-04	m	43900	. 721	2365	•6870 ⁵ -	365-	9811	58.0	•
322 43708 .707 2321 2.71185-01 5.256185-04 667859.37 1417.2 294 43614 .700 2296 2.772405-01 5.23955-04 66704.98 1303.1 205 43520 .684 2274 2.77645-01 5.33957-04 66796.49 1347.6 205 43428 .684 2244 2.77604E-01 5.33585-04 64287.52 1347.6 205 43428 .668 2191 2.77604E-01 5.35605-04 64287.52 1347.6 1155 43160 .668 2191 2.77604E-01 5.35605-04 64069.23 1291.0 1155 43160 .668 2191 2.772255-01 5.473655-04 65660.923 1291.0 1159 4291 .661 2136 2.772255-01 5.473655-04 656511.81 1120.2 1164 42991 .641 2.172456-01 5.473655-04 55510.72 1205.3 1164 42991 .641 2.17226-01 5.42365-04 56511.81 1180.2 1104 4291 .660 2164865	5	43804	.714	2344	-34669.	77E-	8893.	38.8	2.421
294 43614 .700 2296 2.7240E-01 5.2355E-04 66704.98 13679 265 43520 .684 .770 2.7363F-01 5.3303E-04 65496.49 13679 285 4337 .676 .2770 2.7363F-01 5.3303E-04 65496.49 13679 289 4337 .676 .2218 2.77604E-01 5.33037E-04 65496.49 1374 182 4337 .676 .2218 2.77046E-01 5.33080-46 1291.0 185 43160 .660 2166 2.77225-01 5.4016F-04 61816.91 1291.0 129 43075 .651 2136 2.77225-01 5.4236E-04 65640.93 1291.0 129 43075 .660 2166 2.77225-01 5.4236E-04 65611.81 1180.2 129 42910 .661 2104 2.8135E-01 5.4236E-04 56511.81 1180.2 129 42911 .674 2.04665-04 56511.81 1180.2 207 4291 .661 2.046655-04 56511.81 1180.2<	3	43708	. 107	2321	.71185-	185-	7859.	17.2	
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Instrument	Measurement	Response, Hz	IRIG channel number	Range	Error
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Gyro	Roll velocity, p	8.4 96	2	0 to 20 rad/sec 3 to -3 rad/sec	±0.06 rad/sec
Gyro Gwro	Pitch velocity, q Yaw velocity, r	11) m	3 to -3 rad/sec	±0.06 rad/sec
Accelerometer	্র	59	6	1 to -2	±0.03
Accelerometer	Axial acceleration, ax	160.	12	25 to -60	±0.85
Accelerometer	Side acceleration, $a_{\mathbf{Y}}$	45	ω	$\left\{\begin{array}{ll} (1) \ 1 \ \text{to} \ -1 \\ (2) \ \pm1 \ \text{to} \ \pm5 \\ (3) \ \pm5 \ \text{to} \ \pm30 \end{array}\right.$	± 0.06 ± 0.24 ± 1.50
Accelerometer	Normal acceleration, a _N	35	۲-	$\begin{cases} (1) \ 1 \ to \ -1 \\ (2) \ \pm 1 \ to \ \pm 5 \\ (3) \ \pm 5 \ to \ \pm 30 \end{cases}$	±0.06 ±0.24 ±1.50

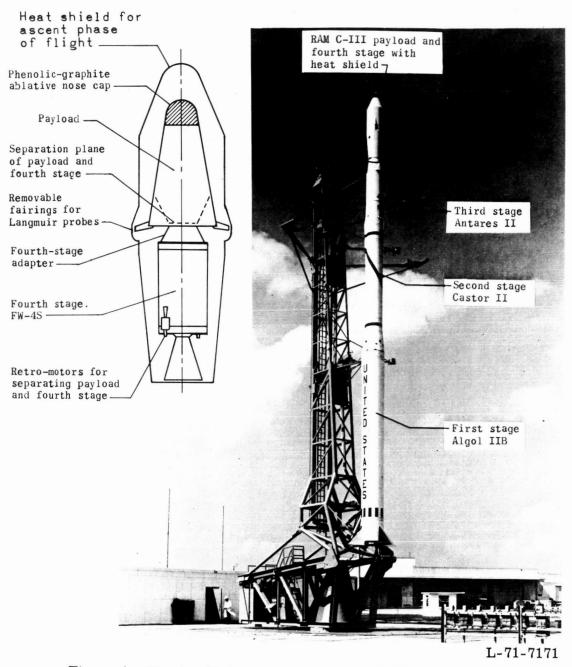


Figure 1.- Boost vehicle and spacecraft for RAM C-III flight.

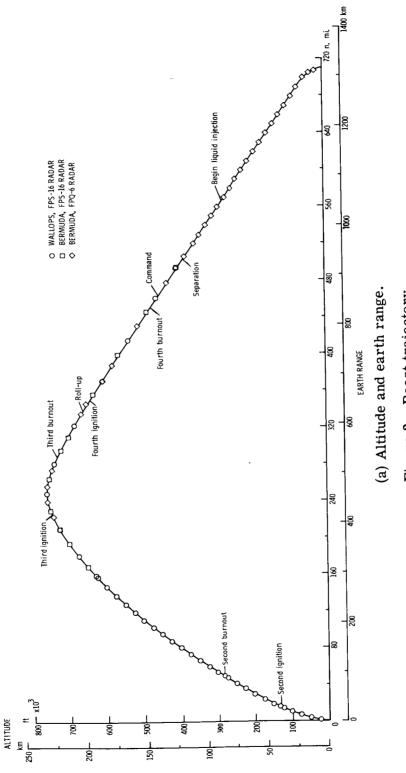
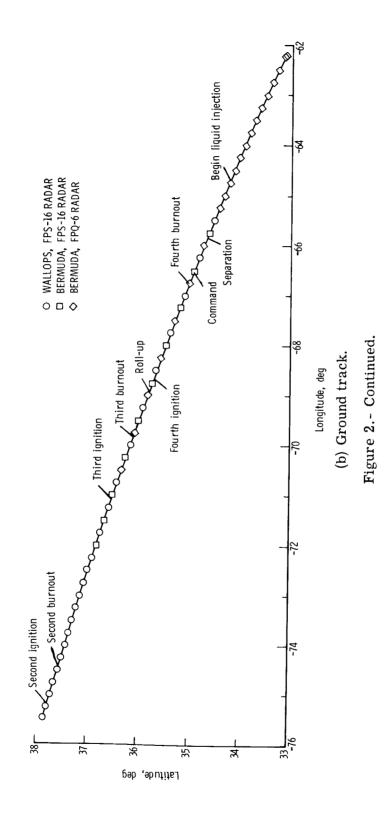
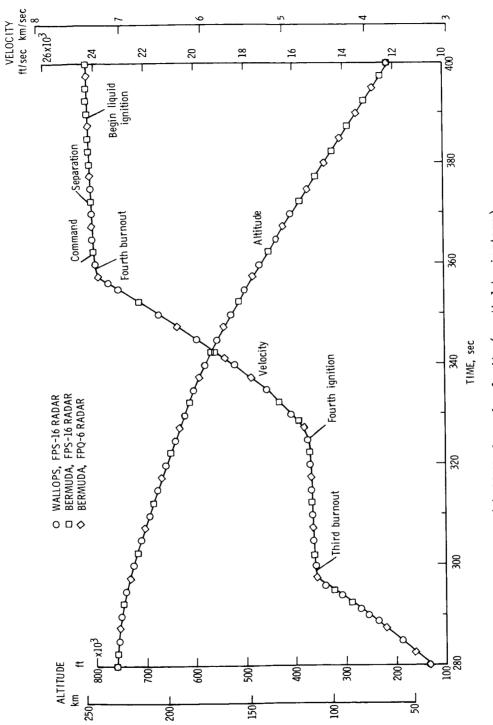


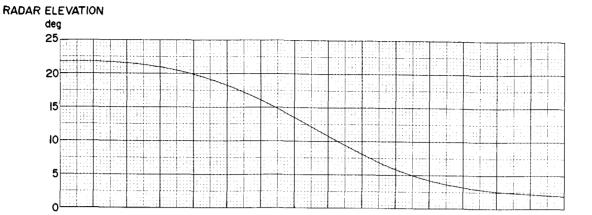
Figure 2.- Boost trajectory.

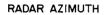


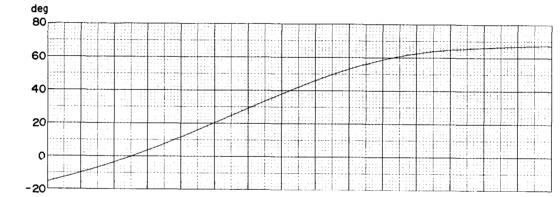


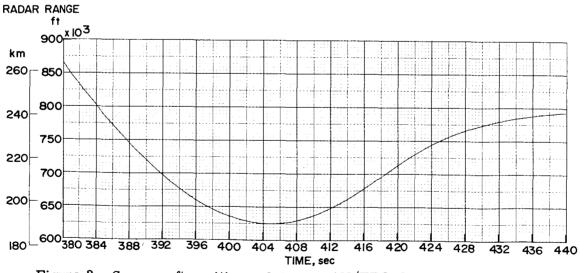


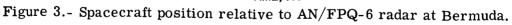
(c) Altitude and velocity (partial trajectory).











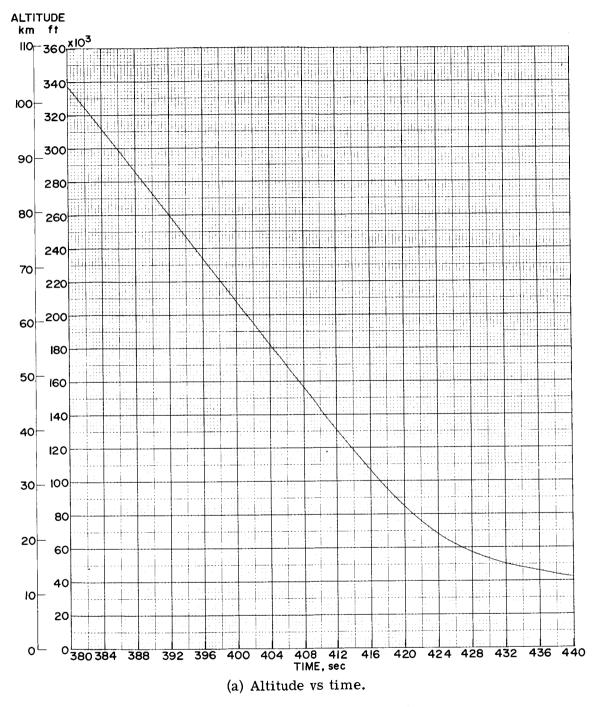


Figure 4.- Entry trajectory parameters.

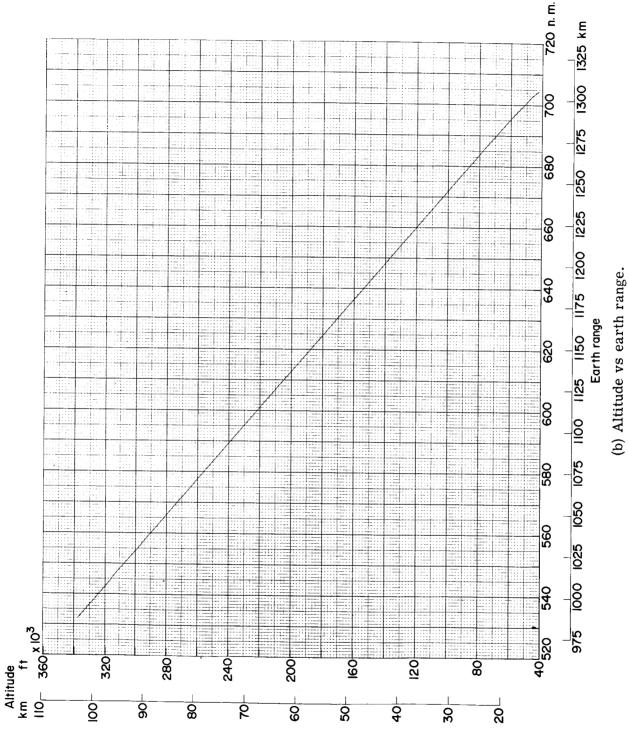


Figure 4. - Continued.

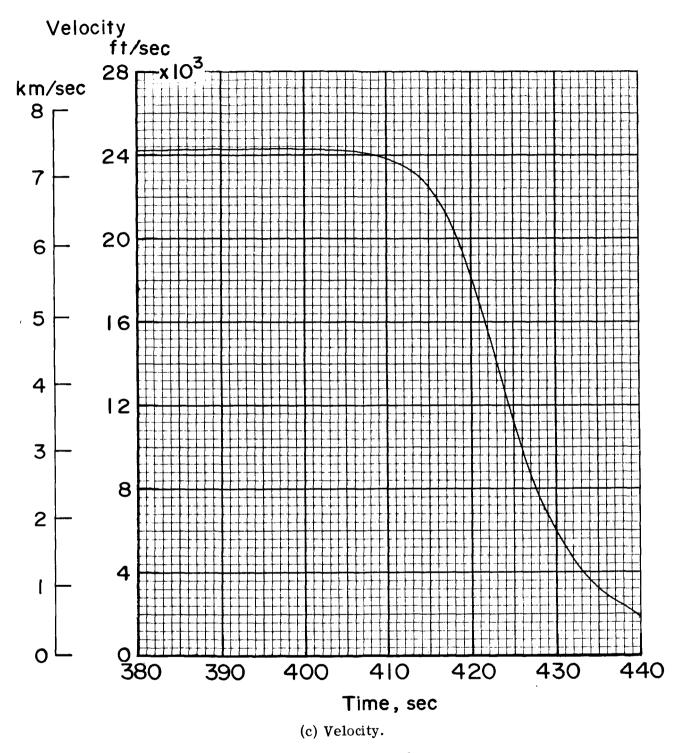
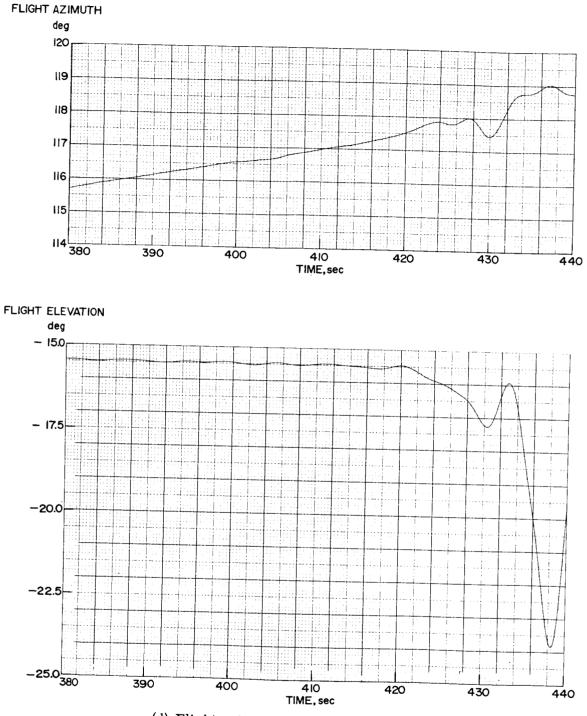


Figure 4.- Continued.



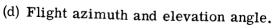


Figure 4.- Continued.

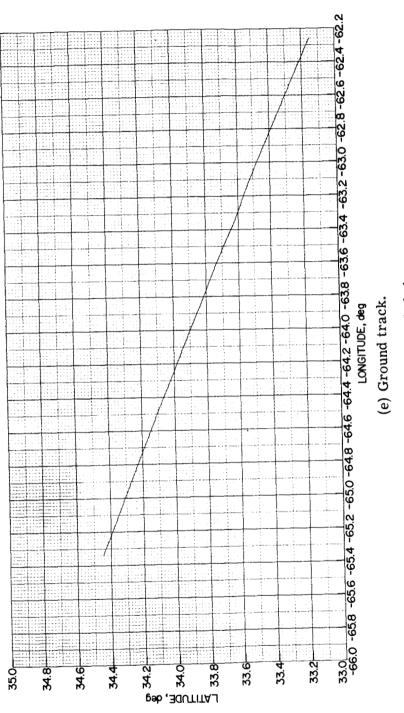
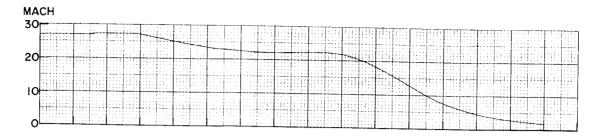


Figure 4.- Concluded.



DYNAMIC PRESSURE

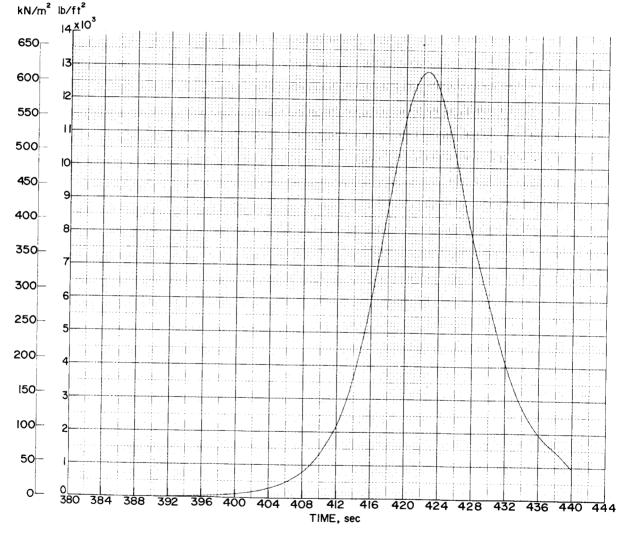


Figure 5.- Dynamic pressure and Mach number.

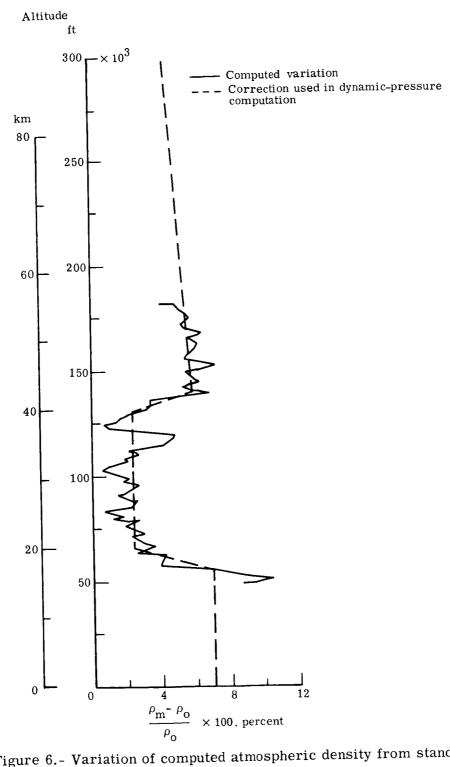
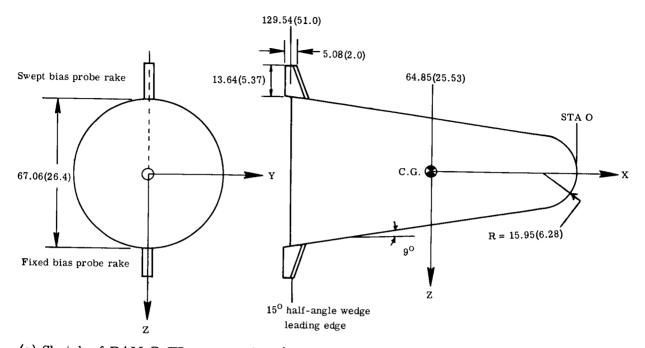


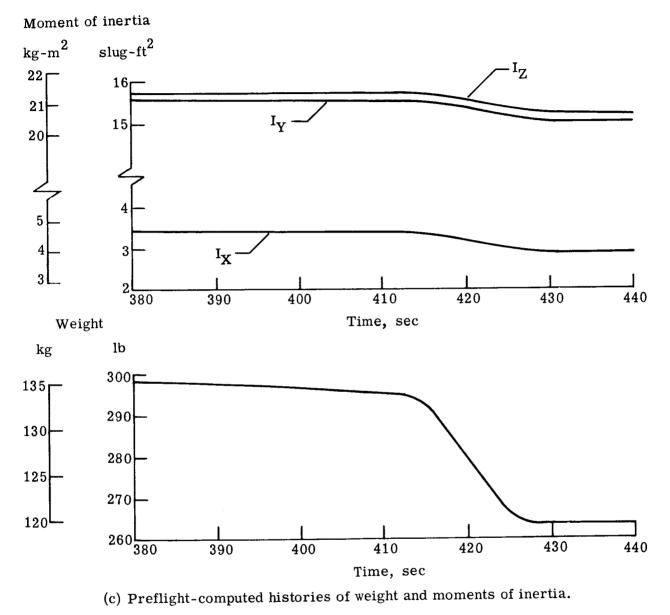
Figure 6.- Variation of computed atmospheric density from standard. $\left(\begin{array}{c} \rho_{\mathrm{O}} & \mathrm{from \ 1962 \ Standard \ Atmosphere; \ \rho_{\mathrm{m}} & \mathrm{based \ on \ temperature} \\ \mathrm{measured \ the \ day \ of \ launch.} \end{array} \right)$

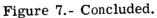


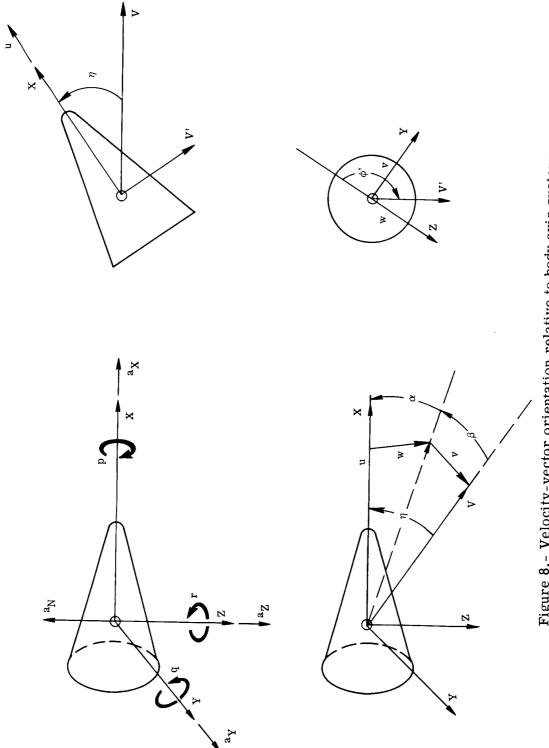
(a) Sketch of RAM C-III spacecraft. (Dimensions in cm and parenthetically in inches.)

v	V		^I x		I _Y		^I z
kg	lb	kg-m2	slug-ft2	kg-m2	slug-ft ²	kg-m ²	slug-ft ²
135	298	4.7	3.5	21.2	15.6	21.3	15.7

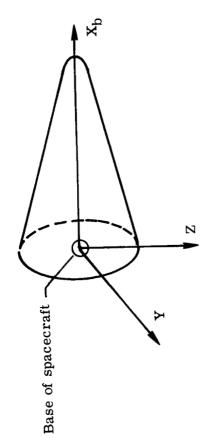
(b) Preflight-measured weight and moments of inertia at entry. Figure 7.- Spacecraft geometry, weight, and moments of inertia.











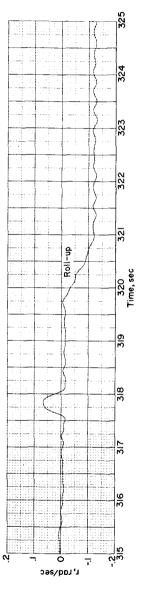
Axis system

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		in	cm	in.	cm	.111.
	CIII	• • • • •				
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Roll gyro	00.01	+0.+0			60 V	1.90
	76 84	30.25	0	D	4.00	
Pitch gvro	10.01				1 0 0	-1 90
	76 84	30.25	0	D	-4.00	00.1
Vaw gvro	10.01				C C L	00 6
(63 32	24.93	0	0	80°C	4.00
Axial accelerometer (10%)	10.00				200	-2 00
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Side accelerometer	10.00				19.0	-0.24
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Figure 9

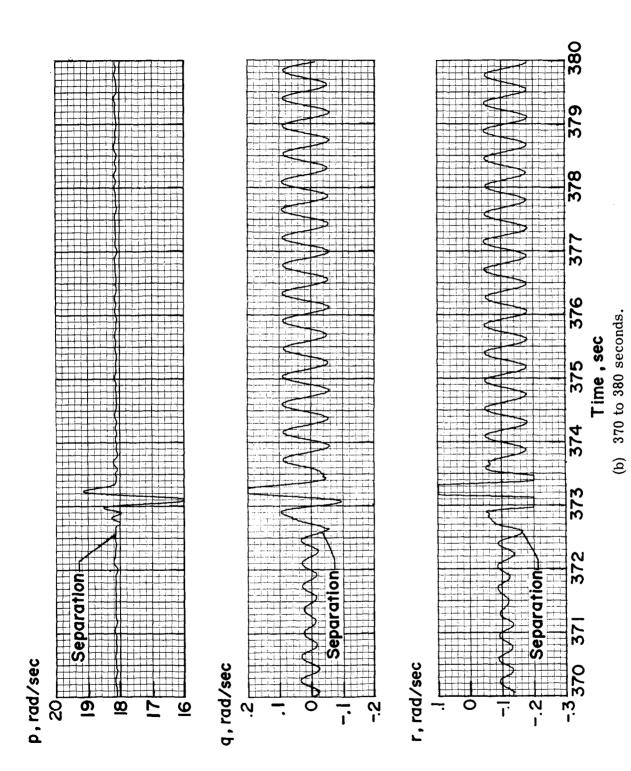
Figure 10.- Spacecraft rotation rates.



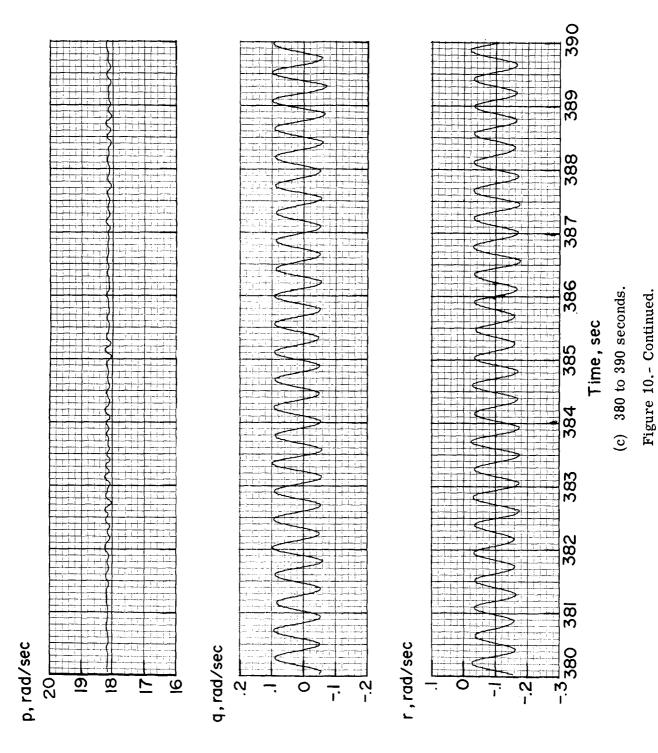


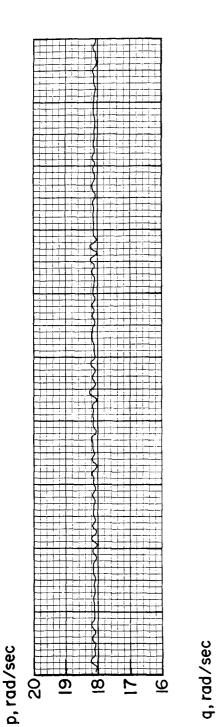
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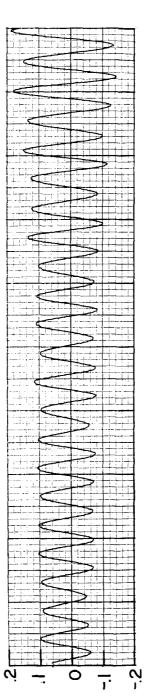












r, rad/sec

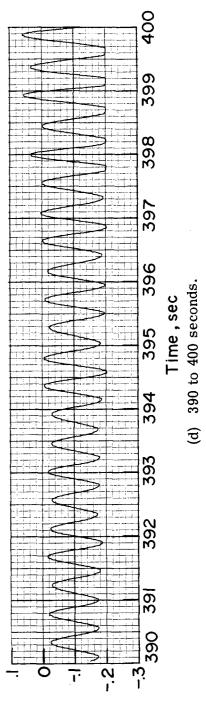
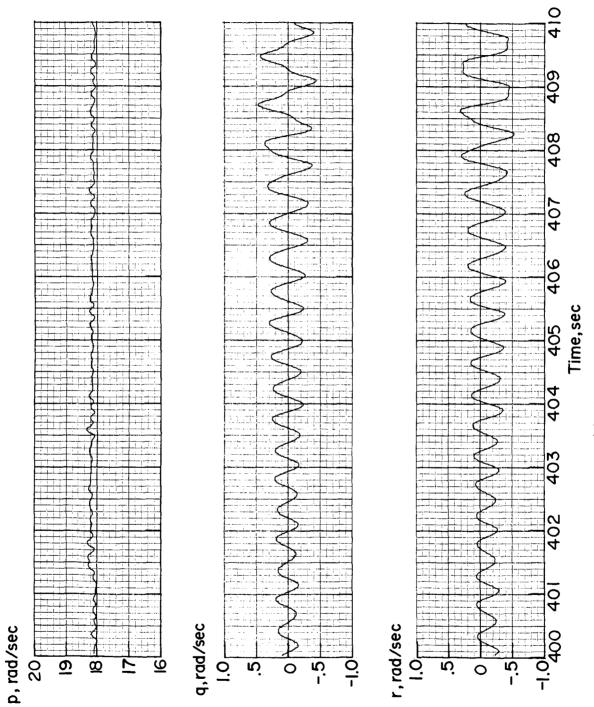
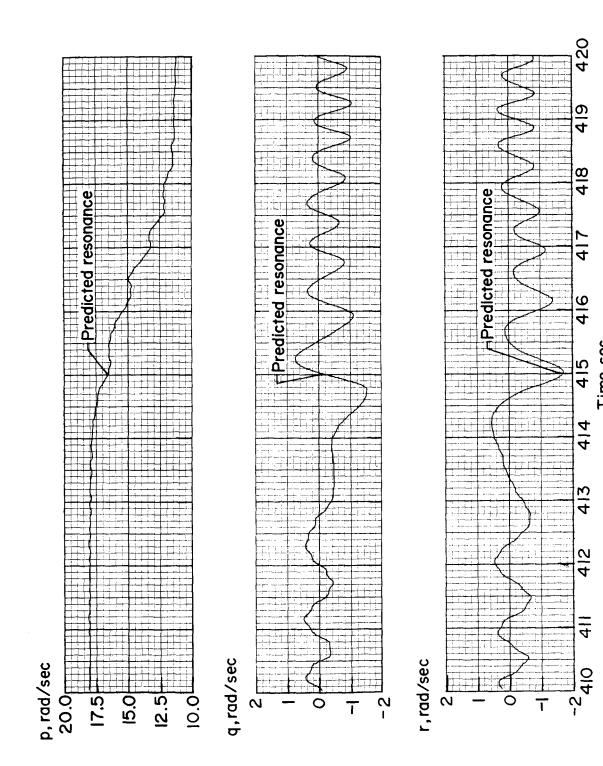


Figure 10. - Continued.



(e) 400 to 410 seconds.

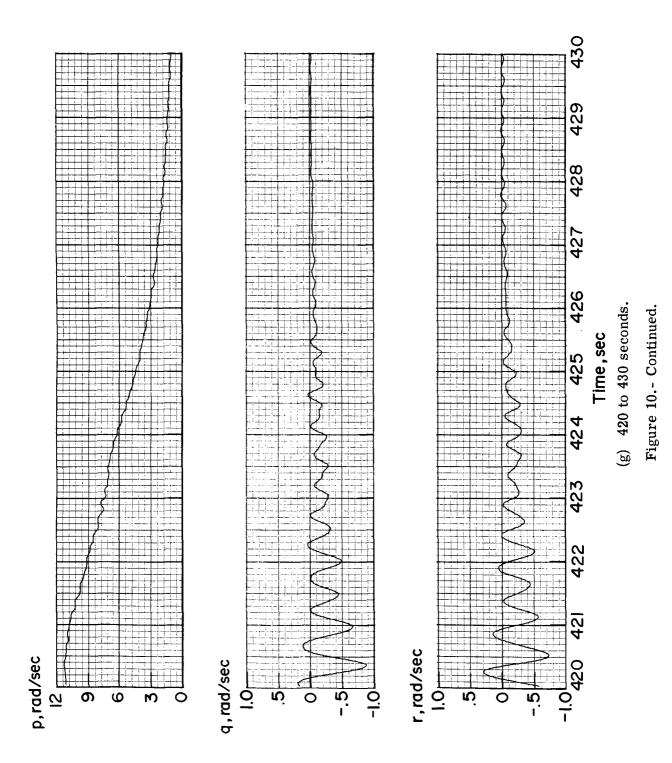




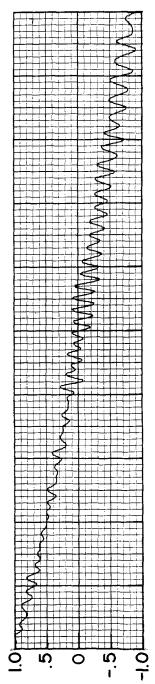


(f) 410 to 420 seconds.

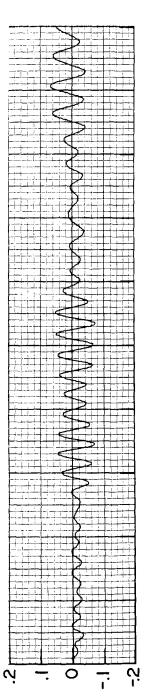
Time, sec













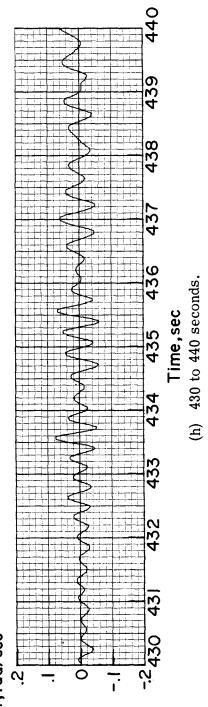


Figure 10.- Concluded.

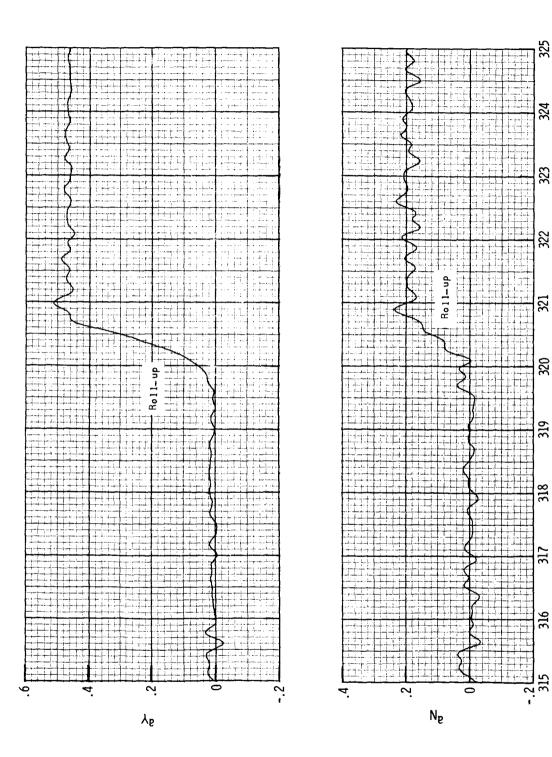
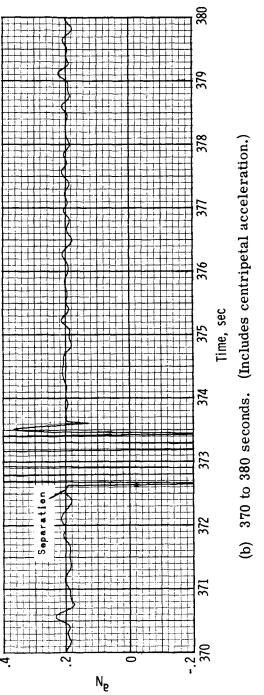


Figure 11.- Measured side and normal acceleration.

315 to 325 seconds. (Includes centripetal acceleration.)

(a)

Time, sec





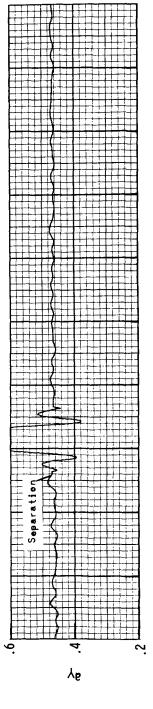
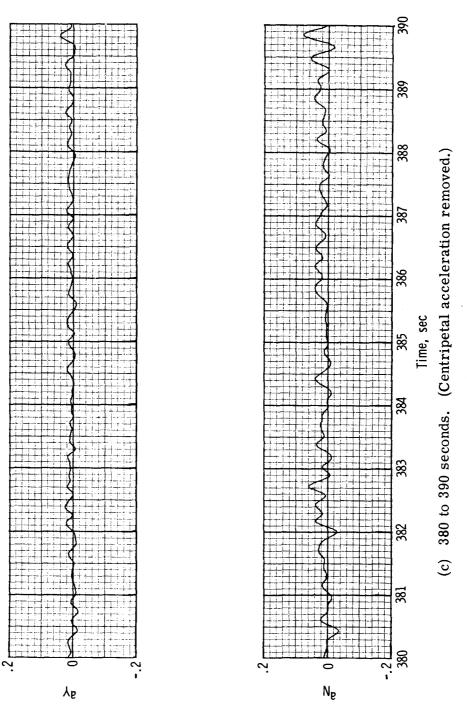
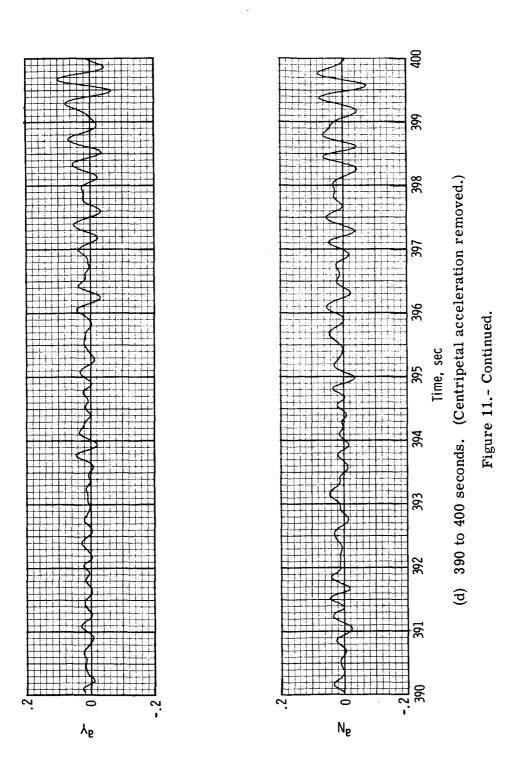
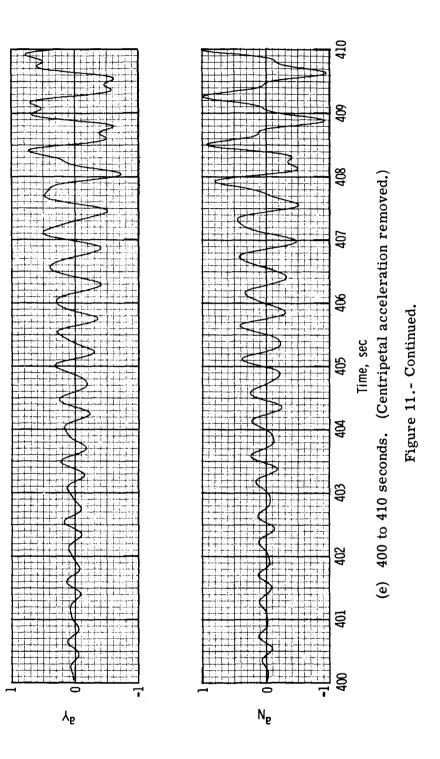


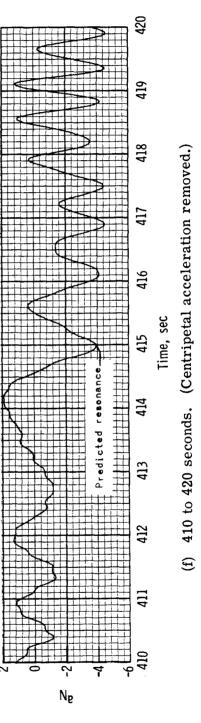
Figure 11.- Continued.

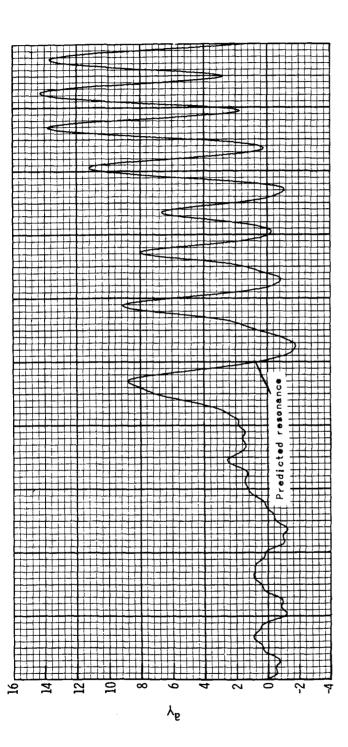












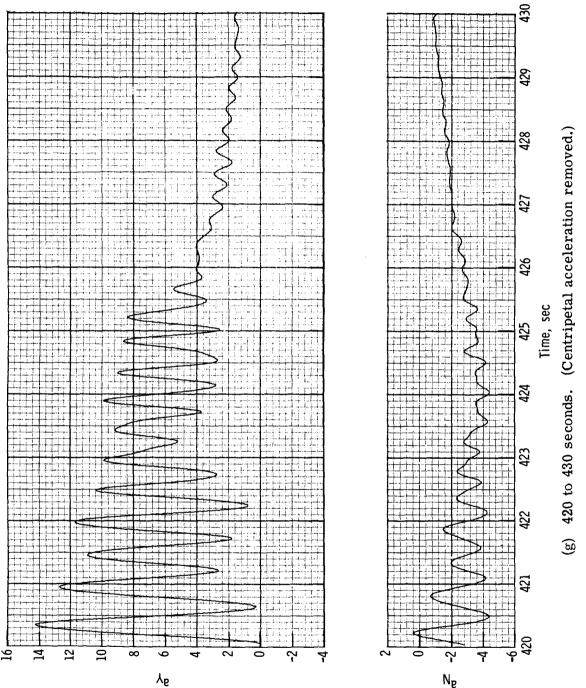


Figure 11.- Continued.

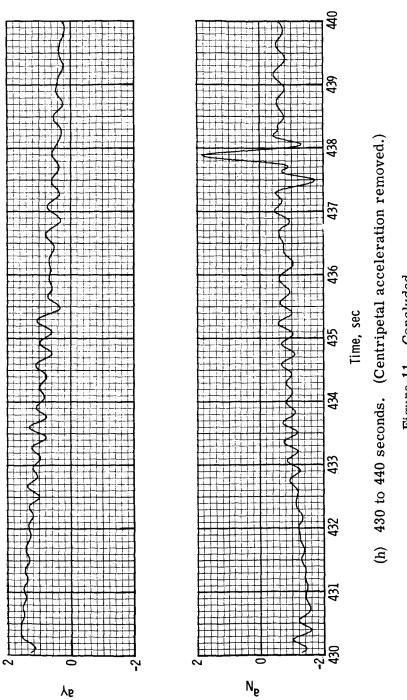
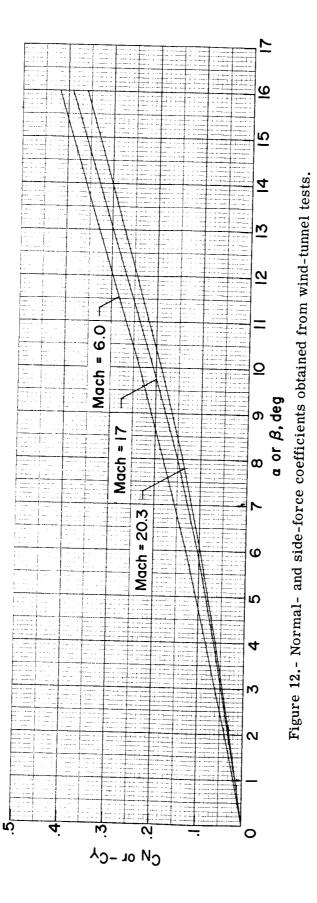
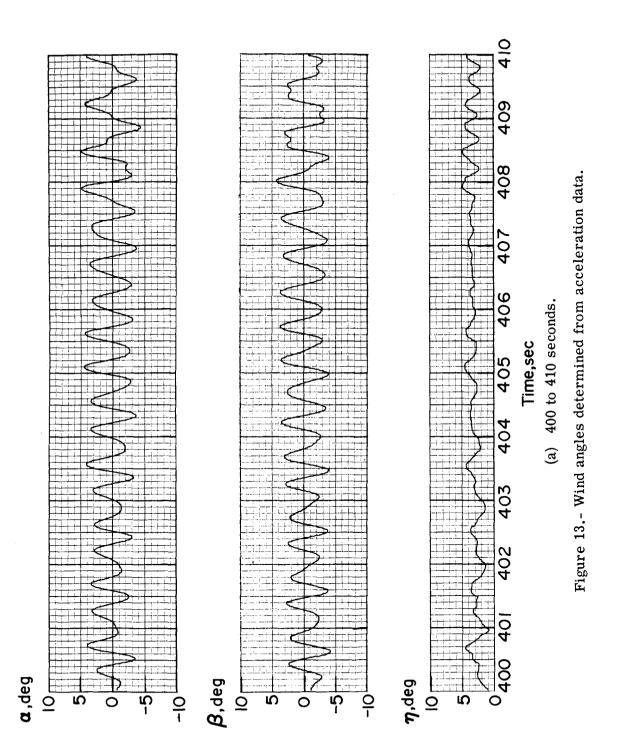
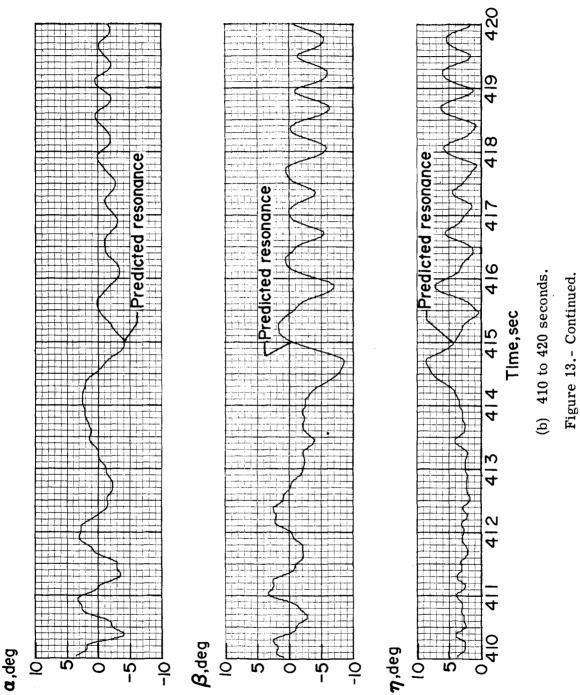


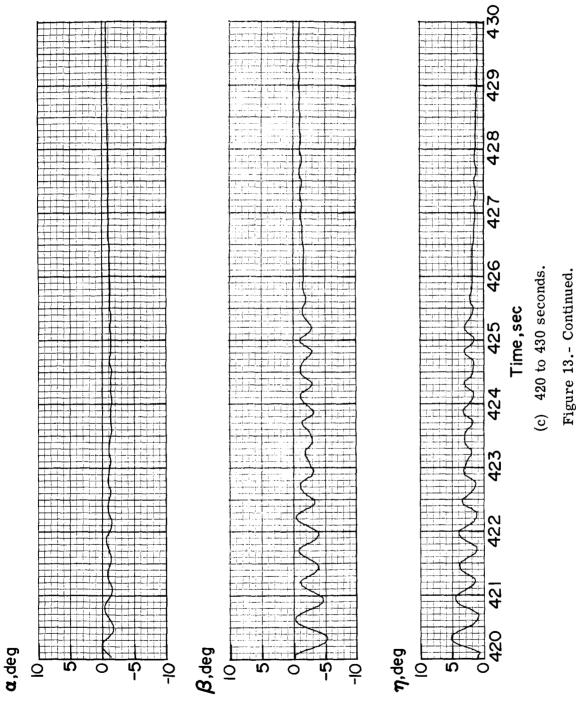
Figure 11.- Concluded.

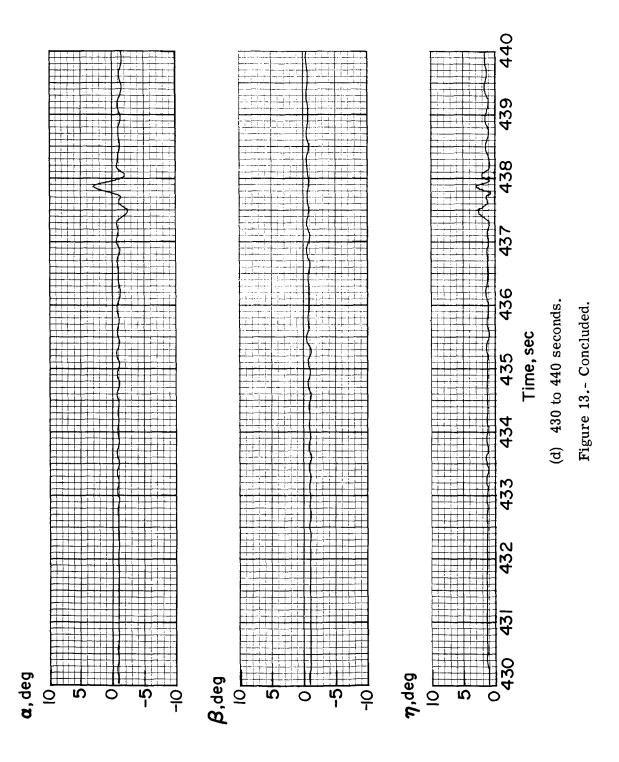








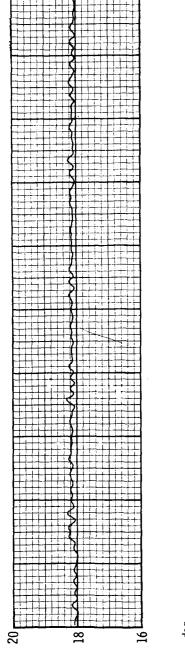




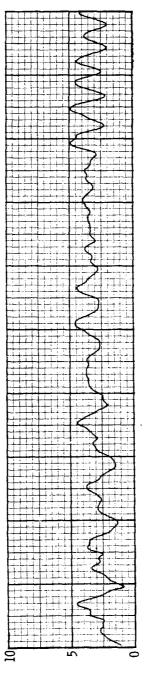


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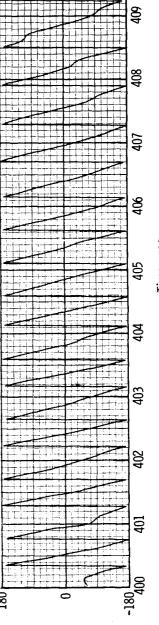


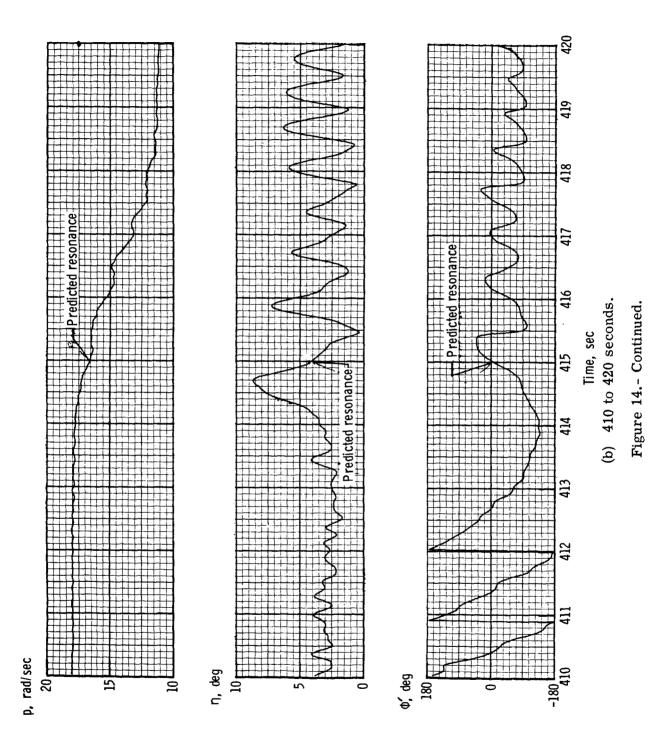


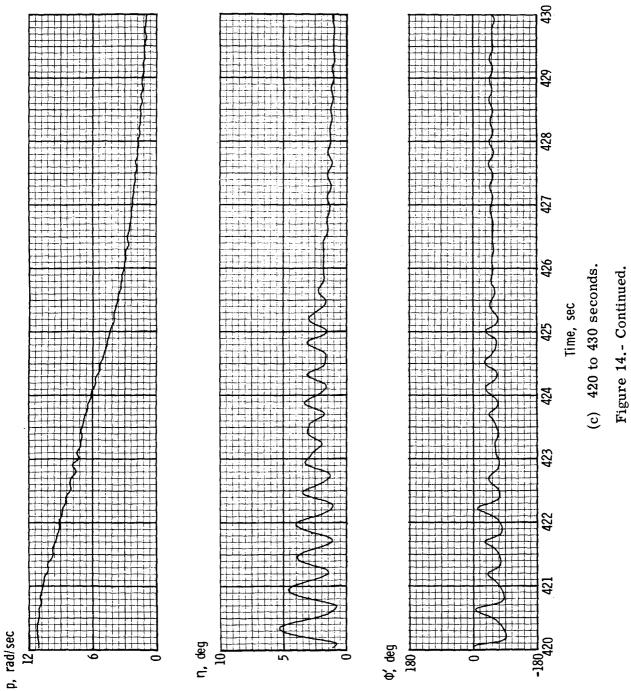




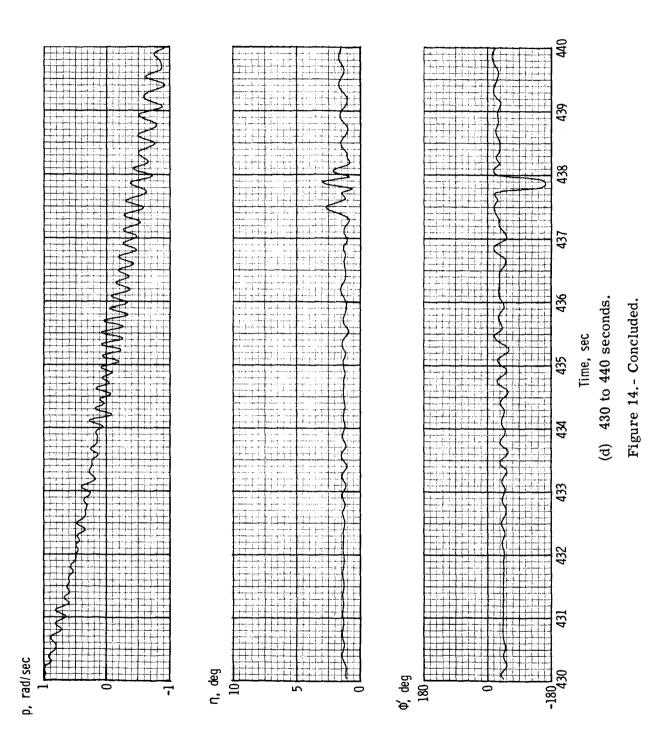


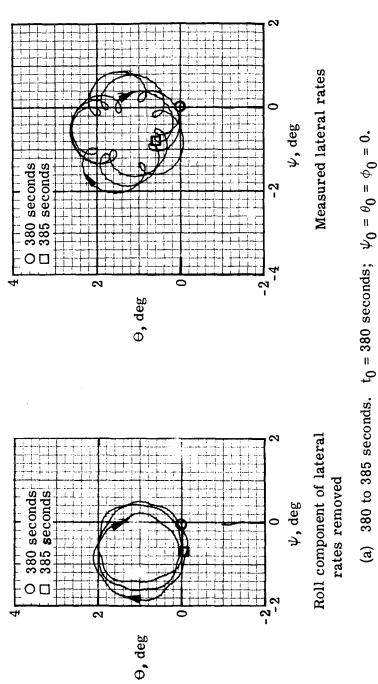






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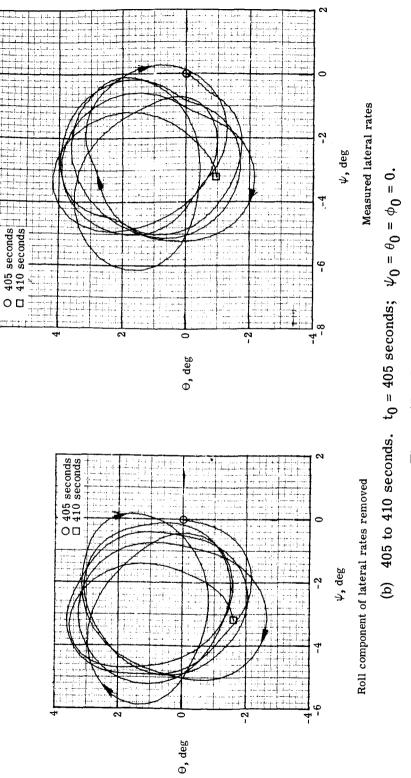
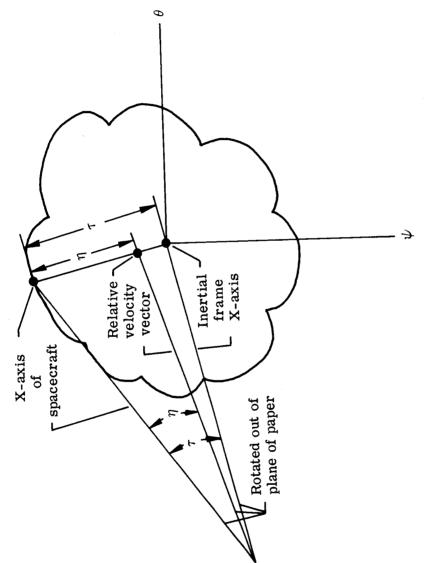


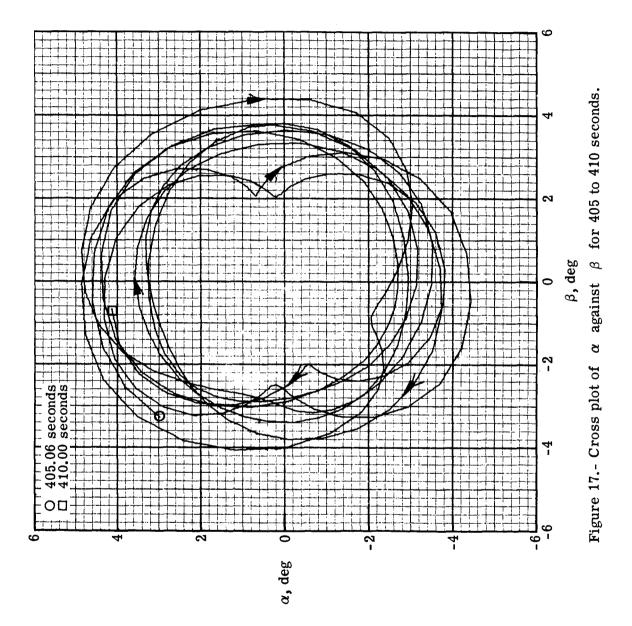
Figure 15.- Concluded.

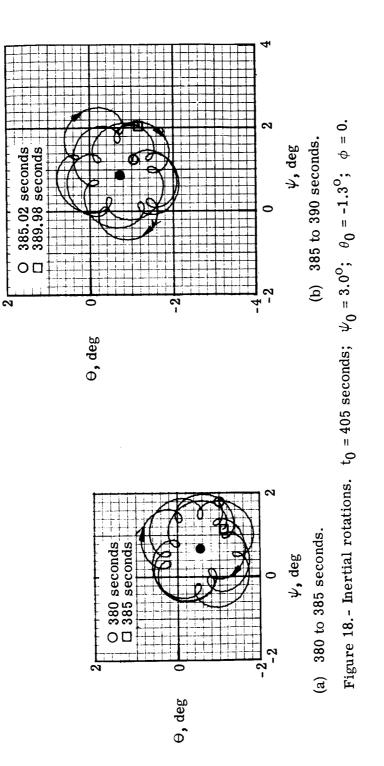
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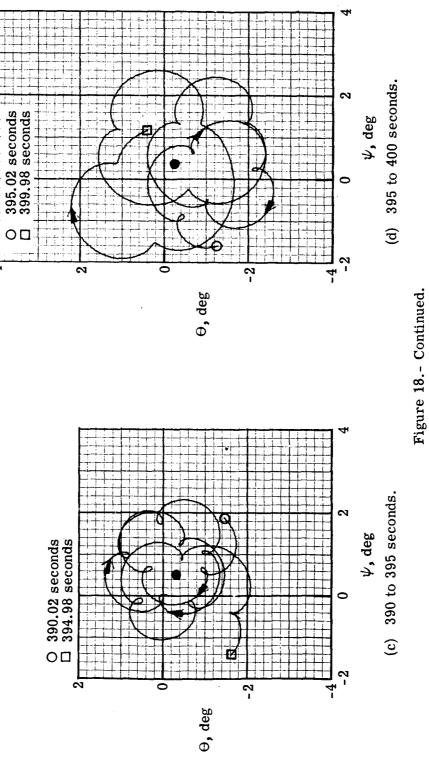


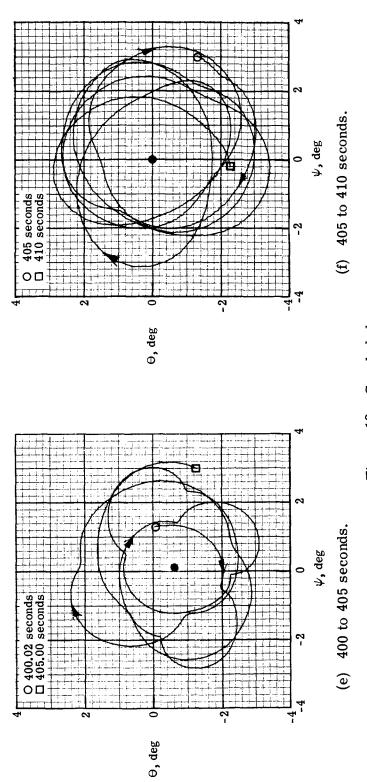
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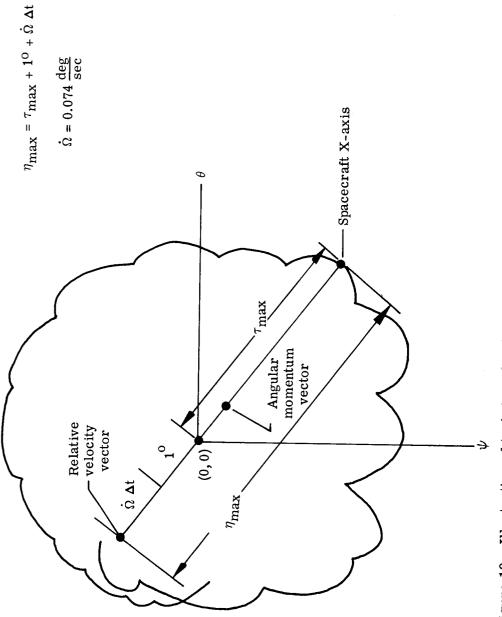














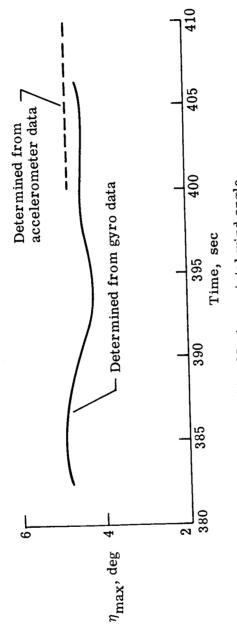
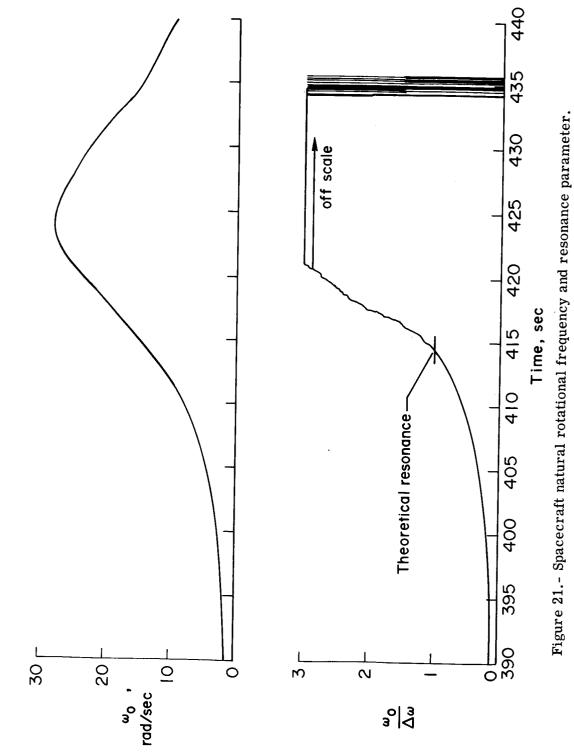


Figure 20.- Maximum total wind angle.



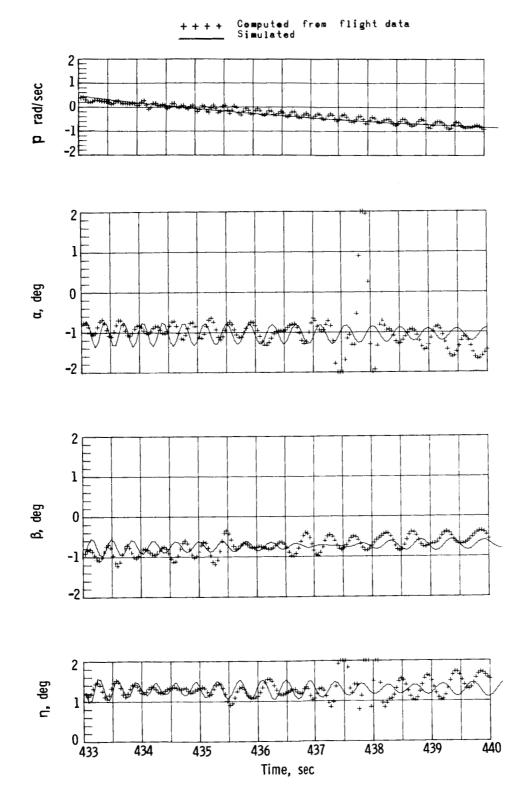


Figure 22.- Comparison between simulated and flight spacecraft motions.