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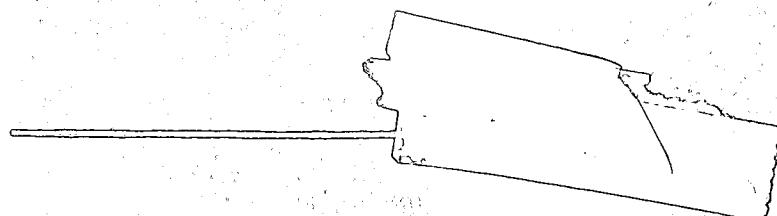
NTIS HC \$4.75

(NASA-CR-130142) MAGNETIC CONTROL
ASSEMBLY QUALIFICATION MODEL Final
Report (Ithaco, Inc.) 52 p HC \$4.75

N73-15479

CSCL 14B

G3/14 Unclas
52583



ITHACA, N.Y.

Report #90569
File #10-2724
October 25, 1972

N73-15479

FINAL REPORT

MAGNETIC CONTROL ASSEMBLY

QUALIFICATION MODEL

NASA GSFC CONTRACT No. NAS 5-21867

I

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REPRODUCED BY
NATIONAL TECHNICAL
INFORMATION SERVICE
U.S. DEPARTMENT OF COMMERCE
SPRINGFIELD, VA. 22161

FINAL REPORT
MAGNETIC CONTROL ASSEMBLY
QUALIFICATION MODEL
NASA GSFC CONTRACT NO. NAS 5-21867

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II

TABLE OF CONTENTS

1.0 INTRODUCTION

 1.1 Scope

 1.2 Description of System

2.0 PHYSICAL CHARACTERISTICS

 2.1 Power

 2.2 Weight

 2.3 Size

 2.4 Torque

3.0 APPLICABLE DOCUMENTS

 3.1 ITHACO Reports

 3.2 ITHACO Drawings

4.0 CHRONOLOGICAL EVENTS

 4.1 Planned Test Sequence

 4.2 Chronological Summary

5.0 PROBLEM REPORT SUMMARY

6.0 LOG BOOK SUMMARY

7.0 MALFUNCTION REPORT SUMMARY

8.0 VIBRATION AND THERMAL VACUUM TESTS

 8.1 Vibration

 8.2 Thermal Vacuum

9.0 RELIABILITY AND QUALITY ASSURANCE SUMMARY

10.0 FABRICATION SUMMARY

11.0 SUBCONTRACTORS

12.0 CONFIGURED ARTICLE LIST

III

Table of Content cont.

13.0 DATA SUMMARY

14.0 PHOTOS

15.0 DRAWINGS

IV

FINAL REPORT

MAGNETIC CONTROL ASSEMBLY (MCA)

NASA, GSFC Contract NAS 5-21867

Report #90569

1.0 INTRODUCTION

1.1 Scope

This report summarizes the work accomplished under the NASA Contract NAS 5-21867 which resulted in building and qualifying the Magnetic Control Assembly (MCA) according to NASA Environmental Test Specification S-320-EN-1. This assembly consists of:

1. Control Logic Assembly (CLA)
2. Magnetometer probe

The MCA was designed as an add-on unit for certain existing components of the Nimbus or ERTS attitude control system. The acceptance electrical and environmental tests verified that the MCA is electrically, mechanically, and functionally compatible with the existing Nimbus or ERTS attitude control systems.

All major drawings and photographs are included in this report; procedures for manufacturing and inspections are outlined. A chronological list of events and fabrication summary is provided for the MCA.

1.2 Description of System

1.2.1 Description of Operation

The MCA system consists of three orthogonal electro-magnets (X, Y, and Z axes) capable of generating ± 5000 pole-cm in each axis; a magnetometer probe capable of sensing external magnetic fields in the X, Y, and Z axes; and the control electronics. Inputs to the MCA are provided by the Control Logic Box and consist of the following:

1. Pitch error
2. Yaw error
3. Roll reaction wheels differential speed
(It could accept Roll error also with slight modifications)

4. Pitch reaction wheel speed

5. Yaw reaction wheel speed

The magnetometer probe of the MCA measures the external magnetic fields of the satellite with respect to the X, Y, and Z axes of the satellite. Using these inputs the MCA computes the required drive signals and energizes the three orthogonal electro-magnets to generate the proper magnetic moments to decrease the satellite's position and rate errors as well as to continuously unload the reaction wheels.

1.2.2 Fine Control Mode

The ERTS orbits the earth at an altitude of 564 miles and each orbit takes 103.2 minutes. At this altitude, we can assume that the external magnetic B field is uniform and changing slowly. The maximum B field strength is about 0.4 gauss at this altitude.

Refer to Fig. 1. Assume that we have a magnetic field (B) pointing along the positive Y axis. A magnetic dipole will tend to align itself with the B field. The magnet (dipole moment M) in Fig. 1 points toward the minus Z axis. Since it wants to align itself with the B field, there exists a torque on the magnet along the X axis as shown in Fig. 1. In normal operation of the MCA in a satellite, a satellite position error in the X axis will require the Y axis electro-magnet acting on the Z axis magnetic field and Z axis electro-magnet acting on the Y axis magnetic field to correct it. The MCA computes the required strength (magnetic moment) of the electro-magnets using the measured strength of the external B field relative to the spacecraft and the position error and/or reaction wheel speeds of the satellite.

The MCA's vital function is to control the speeds of the reaction wheels in a satellite to reduce pneumatic gating in the normal operation mode. To correct the reaction wheel speeds in one axis, the MCA will energize the electro-magnet in the second axis in accordance with the magnetic B field in the third axis. For detailed

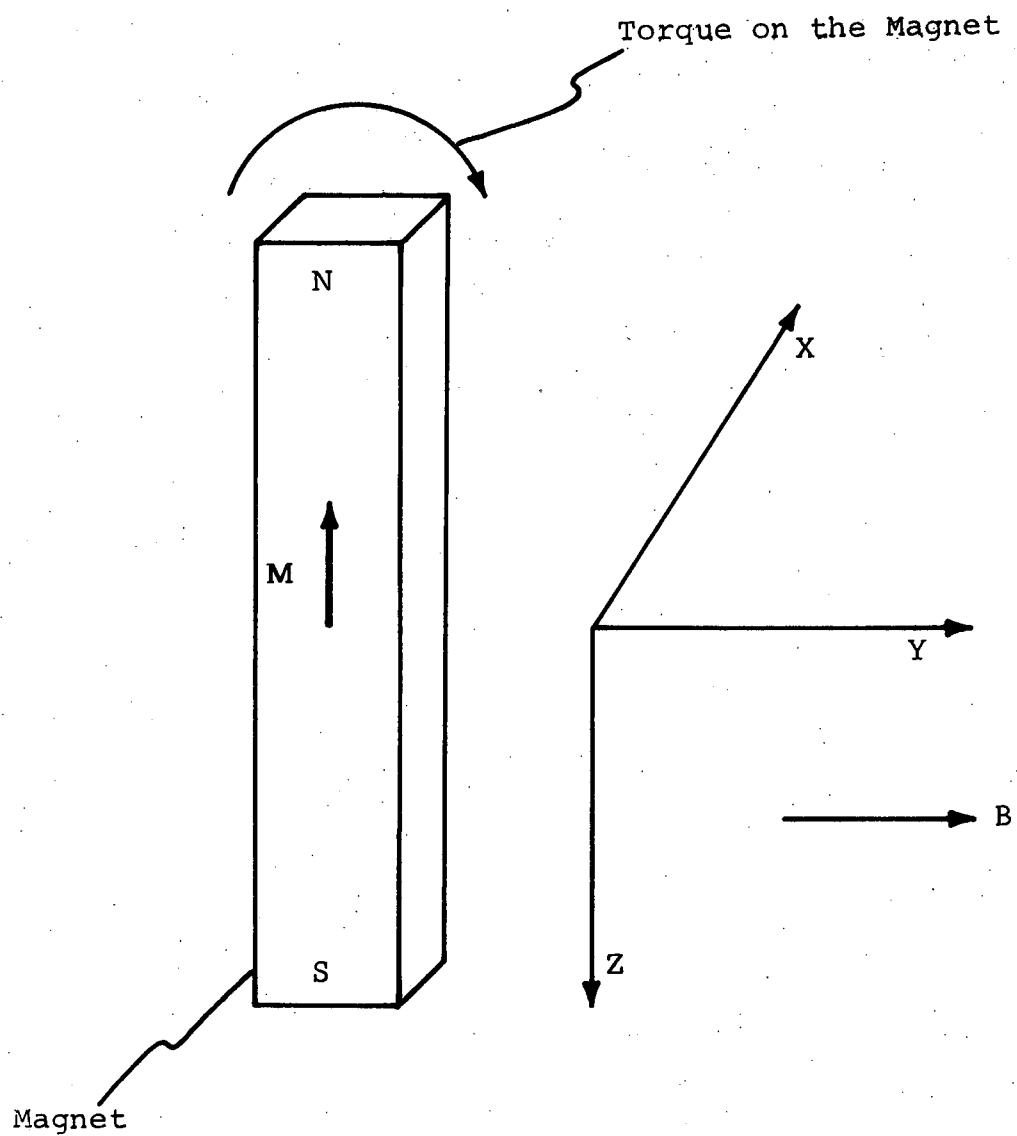


Figure 1

equations and simulations, see MCA's "Design Study Report" by A.C. Stickler, ITHACO, Inc. Report #90559.

1.2.3 Acquisition Mode

The MCA can be used for earth acquisition when the satellite is tumbling after separation from its booster. The acquisition principle is based upon the fact that in normal operation, when the satellite is stable, the external magnetic B field with respect to the satellite is almost constant at the speed the ERTS satellite is orbiting the earth (564 miles orbit height and 103.2 minutes per orbit.)

The derivative of the external magnetic B field, \dot{B} is therefore close to zero. When the satellite is tumbling, the external B fields with respect to the satellite will be changing and their derivative \dot{B} will no longer be zero. In the acquisition mode, the MCA will differentiate the B field input from its magnetometer probe and energize its magnets to create a torque to oppose the vehicle's rotation. Each electromagnet (X, Y, and Z) acts on the \dot{B} of its own axis according to:

$$M_X = -K_1 \dot{B}_X$$

$$M_Y = -K_2 \dot{B}_Y$$

$$M_Z = -K_3 \dot{B}_Z$$

where M is the magnetic dipole moment of the electro-magnets, and K_1 , K_2 , K_3 are constants.

Example: Let us work in the rotation of a single plane. See Fig. 2

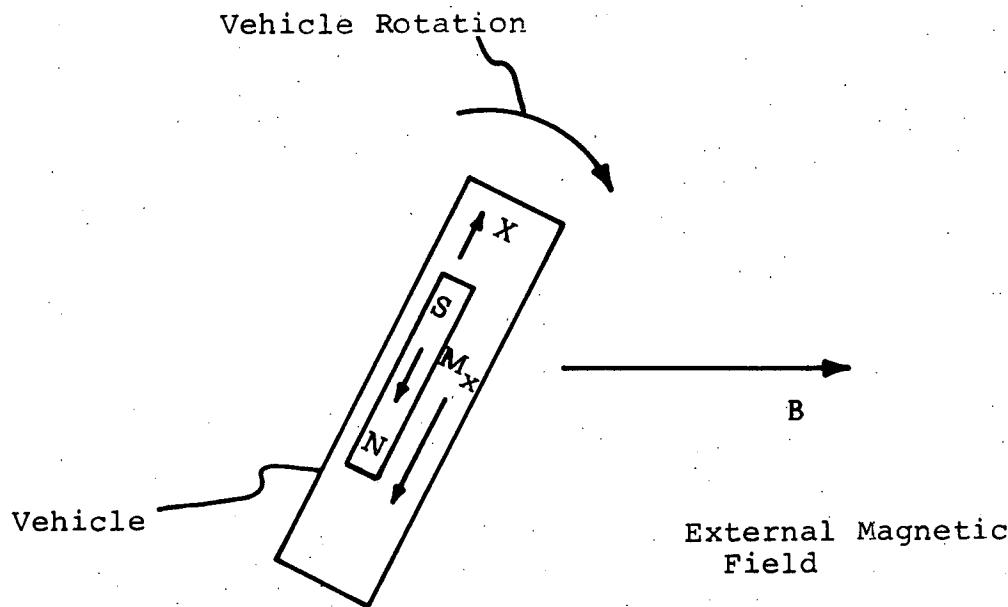


Figure 2

The vehical is tumbling in the direction shown, and there exists an external B field in the direction shown. \dot{B}_X in that direction of rotation is increasing and therefore is positive. Thus according to the equation:

$$M_X = -K_1 \dot{B}_X$$

the X axis electro-magnet will be energized to point in the negative X axis direction as shown in Figure 2. This will create a torque opposite to the direction of the vehicle rotation. This torque will continue until the direction of the vehicle's X, Y, and Z axes with respect to the direction of the external B field (earth's magnetic field) is constant. The acquisition circuit can be commanded off to prevent interference during normal operation.

1.2.4 Operation with Failed Pitch Wheel

If the pitch wheel control fails with the wheel speed at zero, or any constant speed, the space-craft attitude shall remain within one degree on all axes.

1.2.5 Example of Torque Generated

The Maximum magnetic field in the ERTS orbit is 0.4 gauss and the maximum magnetic moment of each electro-magnet is 5000 p-cm ($.37 \times 10^{-3}$ ft-lb/gauss).

The mass moment of inertia of the ERTS satellite is as follows:

$$I_{\text{roll}} = 367 \text{ slug ft}^2$$

$$I_{\text{pitch}} = 349 \text{ slug ft}^2$$

$$I_{\text{yaw}} = 154 \text{ slug ft}^2$$

The equations involved are:

$$\omega = \alpha t \quad \text{eq. 1}$$

Angular velocity = angular acceleration times time

$$\Gamma = \bar{M} \times \bar{B} \quad \text{eq. 2}$$

Torque = magnetic moment across the magnetic flux density

and

$$\Gamma = I\alpha \quad \text{eq. 3}$$

Torque = mass moment of inertia times angular acceleration

Let us say the satellite is tumbling around its yaw axis and the average useable external B field the MCA magnets can act on is .2 gauss and the average magnetic moment generated by the MCA is 500 p-cm or $.37 \times 10^{-3}$ ft-lb/gauss.

How fast can the MCA despin the ERTS satellite that is spinning around its yaw axis at the rate of one revolution per orbit?

$$\Gamma = M \times B = .37 \times 10^{-3} \times .20 \quad \text{eq. 2}$$

$$\Gamma = I\alpha = 154 \cdot \alpha \quad \text{eq. 3}$$

$$\alpha = \frac{M \times B}{I} = .4805 \times 10^{-6} \text{ rad/sec}^2 = \\ .0765 \times 10^{-6} \text{ rev/sec}^2$$

$$\omega = \alpha t \quad \text{eq. 1}$$

for one revolution per orbit

$$\omega = \frac{1}{6192} \text{ rev/sec} \quad (\text{one orbit takes } 6192 \text{ sec})$$

$$\omega = \alpha t \rightarrow \frac{1}{6192} = .0765 \times 10^{-6} \times t$$

$$\text{or } t = 2.11 \times 10^3 \text{ sec} \approx 35 \text{ min.}$$

It will take the MCA approximately 35 minutes or about one third of an orbit to despin the ERTS satellite from an initial velocity of one revolution per orbit in its yaw axis. (This, of course, is a rough calculation, disregarding roll-yaw coupling, reaction wheels, efficiency factors, etc.) For detailed calculation, see ITHACO, Inc., MCA Design Study Report #90559 by A.C. Stickler.

2.0 PHYSICAL CHARACTERISTICS

2.1 Power

The MCA receives its power from a -24.5 volt power supply. Its average current consumption is 100 ma (2.45 watts). Its maximum power will not exceed 5 watts.

2.2 Weight

The total weight of the MCA and the probe is 7.66 pounds with the probe and its connecting wires taking up one pound out of the 7.66 pounds.

2.3 Size

The size of the magnetometer probe is 4.7" X 2.8" X 2.8". See ITHACO Drawing #C31512 in this report.

The size of the Control Logic Assembly of the MCA is roughly 7" X 7" X 7.625." See ITHACO Drawing D41114 in this report.

2.4 Available Moment

The maximum available magnetic moment is 5000 p-cm in each axis.

3.0 APPLICABLE DOCUMENTS

3.1 Publications

- a) ITHACO Report No. 90474, "Progress on MCA and present Status," July 24, 1972, A.C. Stickler.

A report on the development of the MCA's control laws, implementation details, and recommendations for further work.

- b) ITHACO Report No. 90496, "Status of Magnetic Compensation Assembly (MCA)," August 22, 1972, A.C. Stickler.

This report details the final form of the MCA control laws, details simulated system performance, and summarizes some of the more significant MCA characteristics.

- c) ITHACO Report No. 90506, "MCA Signal Polarities and Mounting Information," Sept. 1, 1972, A.C. Stickler.

This report covers proper mounting orientation and coordinates.

- d) ITHACO Report No. 90529, "Telemetry for Magnetic Compensation Assembly (MCA)," Sept. 15, 1972, A.C. Stickler to G. Branchflower.

This report requests the allocation of certain telemetry channels for the MCA.

- e) ITHACO Report No. 90539, "Disturbance Torques and Parameters for ERTS/MCA Study," Sept. 26, 1972, A.C. Stickler.

This report details a new disturbance torque model to be used for ERTS/MCA simulation work.

- f) ITHACO Report No. 90559, "Simulated ERTS Performance with the MCA," October 6, 1972, A.C. Stickler.

This report indicates probable ERTS performance with the MCA on board. The simulated performance reported here is based on an updated disturbance torque model (5) and supercedes performance predictions made in (2). A performance prediction considering the unexplained 44 μ ft-lbf yaw torque apparently experienced by ERTS A is also included.

- g) Memo titled "Backup Magnetic Control System for Nimbus/ERTS," R.Z. Fowler & A.C. Stickler to Seymour Kant, Feb. 15, 1972.

This memo proposes and details the original concept of the MCA. It describes the proposed system, its modes of operation, major characteristics and control laws.

- h) ITHACO Report No. 90420, "Performance of Nimbus/ERTS MCA," April 25, 1972, A.C. Stickler.

This report contains preliminary performance predictions.

- i) ITHACO Report No. 90429, "Control Laws for Proposed MCA for Nimbus," May 5, 1972, A.C. Stickler.

This is a developmental report on MCA control laws.

- j) ITHACO Report No. 90505, "MCA and Schonstedt's Magnetometer Mounting Orientations," August 30, 1972, R. Shen.
- k) ITHACO Report No. 90506, "MCA Signal Polarities and Mounting Information," Sept. 1, 1972, A.C. Stickler.
- l) ITHACO Report No. 90526, "Thermal Vacuum Test Plan for the Qualification Model MCA (MCA Pr1)," Sept. 18, 1972, R. Shen.
- m) ITHACO Report No. 90548, "Qualification Test Report MCA (Includes Vibration Test Plan and Vibration Levels)," October 5, 1972, R. Fleming.

3.2 Drawings

DRAWING TITLE	DRAWING NO.
Miscellaneous Drawings	
a. Major Assy	D41105-G1
b. Parts List for	D44105-G1 (A)
c. Outline	D41114 (A)
d. Block Diag.	F50030 (B)
e. Pin Assign Diag	D41094 (B)
f. Drawing Tree	B22039
g. Wire Diag. Harn	C31546
h. Assy Harn & P.L.	C31545-G1
i. Sensor Unit Outline	C31512-P1
j. Flow Plan	D41123
Pitch/Roll Module	
a. Elem Diag	C31514 (E)
b. PWB Assy	D41101-G1 (C)
c. Parts List for	D41101-G1 (C)
d. PWB Detail	D41101-P1 (B)
e. Module Assy	D41086-G1 (A)
f. Parts List for	D41086-G1 (A)
g. PWB Control	C88195-G1 (A)
h. Frame	D41085-P1 & P2 (A)
Control Module	
a. Elem Diag	F50027 (A)
b. PWB Assy	D41098-G2
c. Parts List for	D41098-G2
d. PWB Detail	D41098-P1
e. Module Assy	C31532-G2
f. Parts List for	C31532-G2
g. PWB Control	D88188
h. Frame	D41107-P1
Power Supply Module	
a. Elem Diag	D41115 (A)
b. PWB Assy	D41097-G2 (A)
c. Parts List for	D41097-G2 (A)
d. PWB Detail	D41097-P1 (A)
e. Module Assy	C31531-G2
f. Parts List for	C31531-G2
g. PWB Control	C88189 (A)
h. Frame	D41108-P1 (A)

Yaw Module

a. Elem Diag	F50026 (B)
b. PWB Assy	D41096-G1 (A)
c. Parts List for	D41096-G1 (A)
d. PWB Detail	D41096-P1
e. Module Assy	D41093-G1 (A)
f. Parts List for	D41093-G1 (A)
g. PWB Control	C88190
h. Frame	D41092-P1
i. Plate	C31511-P1
j. Cover	C31508-P1
k. Connector Assy	B22032-G1
l. Parts List for	B22032-G1
m. PWB Detail	B22032-P1

**Spec Control, Selected &
Altered Items**

a. Transformer (S.C.)	C88118-P2 (A)
b. Transistor (S.I.)	A86089-P1 & P2 (A)
c. Screwlock (A.I.)	A86088-P1

**Miscellaneous Mechanical
Details**

a. Base Plate	C31509-P1
b. Label, Module	A11183-P1
c. Shield	B21957-P1
d. Cover, Silkscreen	C31547-P1
e. Cover	C31458-P1
f. Cover, Basic	C31479-P1 (B)
g. Label	A11270-P1
h. Spacer	A11149-P13
i. Dust Cover	A11218-P1, P5 & P6
j. Dust Cover, Basic	B21989-P1 & P2
k. Frame, Basic	D41017-P1 (B)

Magnet & Magnetometer Module

a. Magnet Assy & P.L.	C31520-G1
b. Lamination	A11231-P1
c. Mounting Block	B21993-P1 (A)
d. Control Mgt Mtr Module	SKC00352 (A)
e. Frame	D41065-P1

4.0 CHRONOLOGICAL EVENTS

4.1 Planned Test Sequence

The Qualification Model MCA testing included in-process, acceptance, and environmental acceptance tests in accordance with GSFC Environmental Test Specification S-320-EN-1. The planned chronological sequence was as follows:

Card Tests: ITHACO, In Process Test Procedure (ITPS)
at room temperature

System Trim test: ITHACO, In Process Test Procedure
(ITPS) at room temperature

Acceptance test: System test at room temperature

Vibration test

Thermal Vacuum Test: -5°C and 50°C temperature cycles.
Acceptance tests were performed
during the temperature plateaus

All acceptance test data was compiled in a separate "Data Summary" section in this report. Tolerances for each result were specified. Any result not within the specified tolerance in the data summary was then discussed in ITHACO Problem Reports. Failures were reported on GSFC Malfunction Report forms.

4.2 Chronological Summary

Date	Event
8-25-72	Card fabrication completed
8-30-72	Card tests finished
9-1-72	Intercard harness fabrication completed
9-9-72	Finished pre-system test trim
9-14-72	Successfully completed system test, ATPS 1105. The roll and yaw electro-magnet leads were switched around for proper polarity.
9-25-72	Final assembly of MCA
9-27-72	Successfully completed vibration test ATPS 1106 at GSFC (ITHACO Report No. 90548, Qual Test for MCA)

10-6-72 Successfully completed Qual level Thermal Vacuum test ATPS 1107 (ITHACO Report No. 90526, Thermal Vac Test Plan).

10-10-72 MCA was taken apart for inspection after Environmental test. All parts were satisfactory.

5.0 PROBLEM REPORT SUMMARY

Report Number	Problem
11-101	The ± 10 volt voltage regulation capacitors C10 and C15 on the A4 card were slightly stressed during a power turn on with no load attached to the ± 10 volts. These are 22 μ f ± 15 volt capacitors (rated 20 volt peak voltage). When power was turned on with no load, they were stressed at 16.5 volts for a duration of about two minutes. The recommendation was use as is for this Qual Model. The C10 and C15 on the Elem Diagram of this report has been up-dated to 20V capacitors to be used on future flight cards.
11-102	A resistor R30 of the Yaw card was changed to give proper Telemetry gain voltage.
11-103	Due to a slight electrical offset, the MCA will unload the Yaw wheel speed to around +20 to 62RPM (depending on temperature) rather than to zero RPM. This does not present any problem.
11-104 and 11-105	The Q1 dual FETs of the Yaw card used a variable resistors are more sensitive to temperature than others. Thus at -5°C the Roll Magnet moment vs Pitch Wheel speed gain is increased by 21.8% (spec $\pm 20\%$). Similarly at $+50^{\circ}\text{C}$, the Roll magnet moment vs Yaw wheel speed gain is decreased by 25% (spec $\pm 20\%$). A gain change of this order at extreme temperatures will not affect the MCA performance appreciably.

6.0 LOG BOOK SUMMARY

The Running Time of the MCA System as of 10-7-72 is 249 hours and 53 minutes.

The connector mate/demate history as of 10-12-72 is as shown below:

Card	Connector	Mated	Demated
A1	J1	8	8
A1	J1	5	5
A2	J1	7	7
A2	J2	3	3
A3	J2	1	1
A3	J3	6	6
A3	J4	5	5
A4	J1	6	6
A4	J2	5	5
A4	J3	6	6
A4	J4	7	7
A5	J1	8	8

7.0 MALFUNCTION REPORT (MR) SUMMARY MCA

MR No.	Card	Name	Description
D07183	15034	Power Supply	A short circuit was detected on a 2N2907A transistor from base to collector (the case). This was caused by a solder bridge formed during soldering of the device. This was an isolated occurrence. Recent redesign of the Power Supply board to provide stress relief by means of off pad soldering will eliminate any future occurrence on subsequent units.

8.0 VIBRATION AND THERMAL VACUUM TESTS

8.1 Vibration

The vibration levels for the MCA Control Logic Assembly and the Magnetometer Probe are shown in the tables on the following two pages. The vibration specifications are according to NASA's environmental test specification S-320-EN-1 (November, 1971). The MCA went through the vibration test successfully. (See ITHACO Report No. 90548 for details.)

MCA Control Logic Assembly
Vibration levels according to S-320-EN1, Nov. 1971

SINUSOIDAL

Frequency	Amplitude - "g" O-to-Peak	
	Thrust Axis	Transverse Axes
5-40	8.0*	6.0*
40-200	10.0	18.0
200-2000	5.0	5.0

*Vibration limited to 1/2" double amplitude.

Sweep Rate: 1 octave/minute.

RANDOM

Direction	Frequency Range (cps)	Power Spectral Density (g^2/cps)	g-RMS
Thrust Axis	20-2000	0.09	13.4
Transverse Axes	20-2000	0.09	13.4

The duration of the test shall be 4 minutes in each direction -- 12 minutes total.

Magnetometer Probe
Vibration levels according to S-320-EN1, Nov. 1971

SINUSOIDAL

Frequency Range (cps)	Amplitude - "g" O-to-Peak	
	Thrust Axis	Transverse Axes
5-100	15.0*	15.0*
100-200	10.0	10.0
200-2000	5.0	5.0

*Vibration limited to 1/2" double amplitude.

Sweep Rate: 1 octave/minute.

RANDOM

Direction	Frequency Range (cps)	Power Spectral Density (g ² /cps)	g-RMS
Thrust Axis	20-2000	0.09	13.4
Transverse Axes	20-2000	0.09	13.4

The duration of the test shall be 4 minutes in
each direction -- 12 minutes total.

8.2 Thermal Vacuum

The MCA CLA went through the Thermal Vacuum Test cycle successfully and the temperature cycle profile is according to the NASA specification⁵ S-320-EN-1. (See Figure 3) The vacuum level was 10 mm Hg or less.

The magnetometer probe was cycled between -20°C and 80°C at atmospheric pressure as shown in Figure 3. The acceptance system test (ATPS 1105) for the MCA was run twice, once during the high temperature plateau and once during the low temperature plateau. (See Figure 3)

At the places where "*"s are marked in Figure 3, the magnetometer probe received a fixed on off magnetic field to test the effect of temperature on the probe.

9.0 RELIABILITY AND QUALITY ASSURANCE (R&QA) SUMMARY

9.1 R&QA Plan

The MCA qualification unit, PR1, fabrication was controlled by procedures outline in the ITHACO Quality Control Manual ITHACO Report No. 90399 dated March 1972. The QC Manual meets the requirements of MIL-Q-9858A.

The primary functions served by Quality Assurance were incoming test and inspection, in process inspection, monitoring of acceptance and environmental testing, and data review and approval. Quality assurance also served on MRB actions and coordinated malfunction reporting.

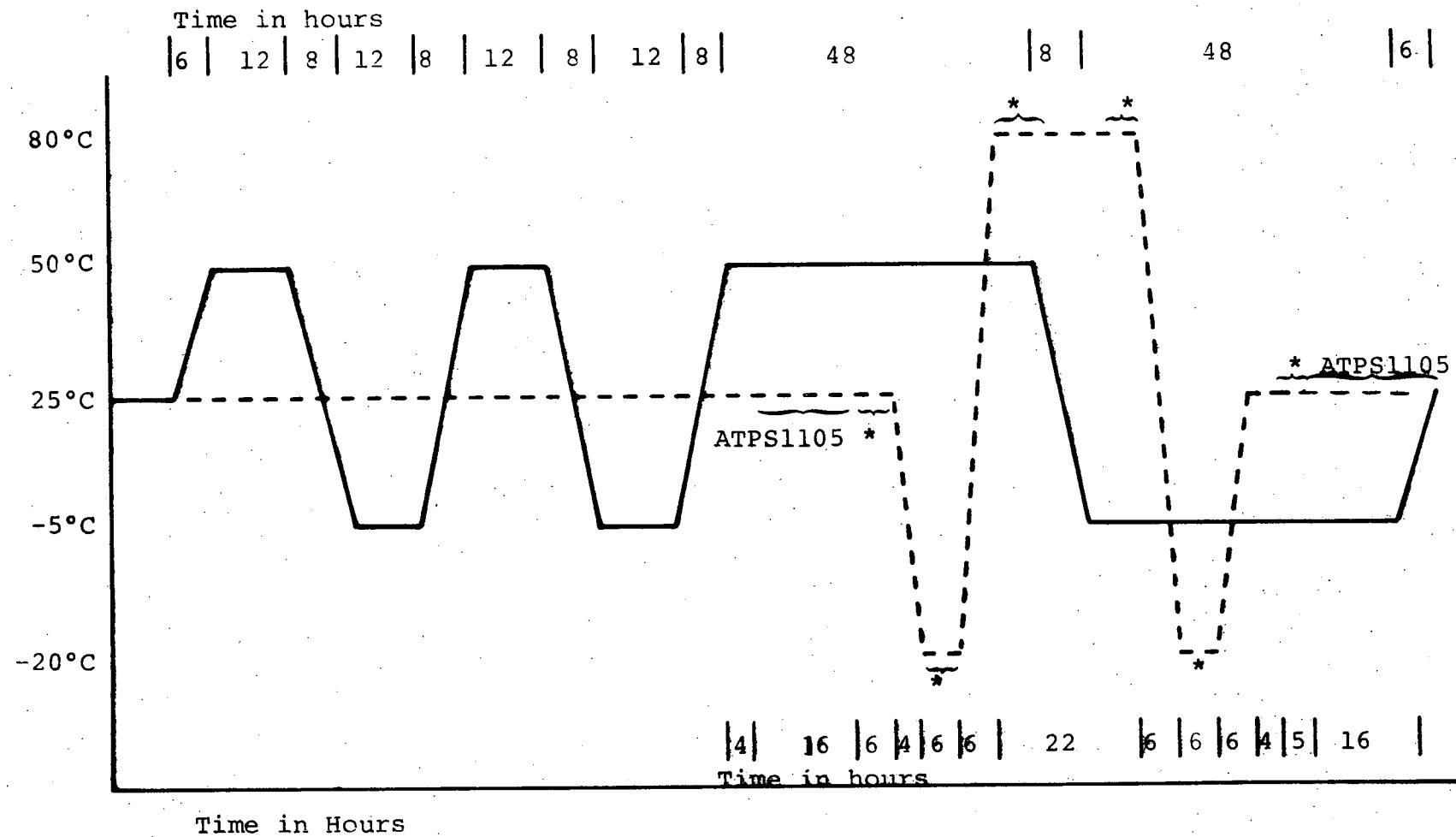
9.2 Implementation

Control of materials and workmanship was performed in accordance with ITHACO Incoming Test and Inspection Procedures (ITPS 11 series), Manufacturing Operation Procedure, Space Systems (MOPS 30 series), and R&QA Procedures for Space Systems (RQPS 15 series) as per Flow Plan D41123.

The Triaxial Magnetometer C31512P1 S/N 15062 (Schonstedt Model SAM-63B-7) electronics module and probe was supplied by Schonstedt Instrument Company, Reston, Va. Control was by means of procurement document ITHACO Report No. 90362 and incoming inspection at ITHACO.

One Malfunction in the MCA CLA, a shorted JANTX 2N2907A in the Power Supply, was reported. Failure analysis revealed a solder bridge apparently formed during

- - - - MAGNETOMETER PROBE (Not in Vacuum)
 _____ MCA CLA (In Thermo Vac)



Time in Hours

MCA & MAGNETOMETERS TEMPERATURE TEST
PROFILE

*See Para 8.2

Fig. 3

installation of the device. Redesign of the printed wiring board to provide stress relief by means of off pad soldering will preclude recurrence.

9.3 Qualification

The MCA Qualification unit, MCA PR1, was subjected to Qualification Vibration levels as described in ITHACO Report #90548. The unit was also subjected to Qualification Thermal Vacuum as indicated in paragraph 8.2. A thorough visual examination performed subsequent to Qualification testing confirmed that no degradation had occurred.

Additional Environmental History on the Triaxial Magnetometer was supplied by Schonstedt in a letter from C. Upton to V. Selby dated Sept. 28, 1972.

10.0 FABRICATION SUMMARY

All P.C. boards were fabricated by ITHACO, Inc. All frames were made by Lansing Research Co. except for the Al frame which was machined by Kolar's Machine shop. Covers were manufactured by Lansing Precision Tool Co.

During P.C. board assembly, MOPS 30.3 was revised to implement off pad soldering techniques. Two of the P.C. boards, Yaw card and A5 Pitch/Roll card, were fabricated to use off pad soldering but time did not permit a new layout of A3 Control card and A4 Power Supply card. These latter P.C. boards were assembled using off pad soldering on a standard board. This was done by cutting off transistor I.C. solder pads and bending the leads onto the runs and soldering. All feed through and component leads used as feed throughs were soldered off pad on the wire side, the same as transistor leads.

Frames and covers were iridited and painted at ITHACO and the frames were silk screened by Thompson Co. Cover markings were applied with press on lettering at ITHACO.

Harness fabrication was to MOPS 30.38 using 24 gauge wire Raychem specification #44 and Cannon Burgundy type connectors.

Magnet fabrication was per MOPS 30.40. The magnet material is Alloy 48, .014" thick, ground to size at Kolar's Machine shop, and heat treated to MOPS 30.25B at Owego Heat Treat, Inc. Fifteen layers of #30 Heavy Formvar magnet wires were used around each magnet.

11.0 SUBCONTRACTORS

Schonstedt Instrument Co.
1775 Wiehle Avenue
Reston, Va. 22070

Magnetometer Probe and A2 card

Thompson Co.
85 Eldrege St.
Binghamton, N.Y. 13900

Silk Screening

Owego Heat Treat, Inc.
Marshland Rd.
Appalachian, N.Y. 13732

Heat treating magnet laminations

Kolar's Machine Shop
407 Cliff Street
Ithaca, N.Y. 14850

Grinding laminations

Lansing Research Co.
705 Willow Avenue
Ithaca, N.Y. 14850

Machining Frames

Lansing Precision Tool Co.
1191 Warren Road
Ithaca, N.Y. 14850

Machining Covers

12.0 CONFIGURED ARTICLE LIST

(See next page)

CONFIGURED ARTICLE LIST



ITHACO INC
735 W. CLINTON ST.,
ITHACA, N.Y. 14850

PROGRAM MCA

COMPONENT MCA Qual

DATE 10-6-72

INDENTURED ITEM NO.		NAME	PART NO.	SERIAL NO.	MRB	ECP	REMARKS
1	2	3	4				
1		Major Assy	D41105-G1	PR1			
1		A1 Yaw Mod.	D41093-G1	15033			
2		A2 Mag. Mod.	SKC00352	4493			
3		A3 Cont. Mod.	C31532-G1	15035			
4		A4 Pwr. Sup.	C31531-G1	15034			
5		A5 Pitch/Roll	D41086-G1	15037			
6		Harness Assy	C3154-G1				
7		Cover	C31547-P1				
8		Base Plate	C31509-P1				
9		Shield	B21957-P1				
10		Spacer	A11149-P13				
11		Magnetometer Probe	C31512	15062			
12		Magnets Yaw	C31520	15030			
12		Magnets Roll	C31520	15028			
12		Magnets Pitch	C31520	15029			

13.0 DATA SUMMARY

See following pages:

T R E N D C H A R T

FUNCTION	TEST CONDITIONS	SPEC	INPUT	OUTPUT	XY PLOT NO.	ROOM	50°C	-5°C
Power	Current from -24V supply with inputs grounded	100 ±20ma				100ma	100ma	100ma
+10V		+10.0 ±5V			10.238	10.120V	10.243V	
-10V		-10.0 ±5V			-10.285	-10.178V	-10.271V	
Temp TLM	MCA CLA	Room =-1± .2V 50°C =-.39±.08 -5°C=-3.36±.7V	A4J2-9 A4J2-9 A4J2-9		-1.037V -.349V -2.997V			

PROCEDURE NO. ATPS 1105 S/N MCA DATE 10-18-72 PAGE 1



COMPONENT MCA PERFORMED BY RS APPROVED BY RS

T R E N D C H A R T

FUNCTION	TEST CONDITIONS	SPEC	INPUT	OUTPUT	XY PLOT NO.	ROOM	50°C	-5°C
Power on TLM		-7.8 ±1V		A4J2-14		7.807	-7.870V	-7.855V
Power off TLM		0 ±5mV		A4J2-14	+1mV	+1mV	+1mV	+1mV
Acquisition On TLM		-6.0 ±1V		A4J2-10	-6.481V	-6.436V	-6.470V	
Acquisition Off TLM		0 ±5mV		A4J2-10	+1mV	0mV	-1mV	
Roll Magnet	+Moment saturation 575 p-cm/V	+5000±1000p-cm		A1J1-12	6.5.2	-7.647 +4397p- cm	-7.827V +501 p- cm	-7.422V +4267p- cm
	-Moment saturation 575 p-cm/V	-5000±1000p-cm		A1J1-12	6.5.2	+8.526V -4902p- cm	+8.602V -4946p- cm	+8.431V -4848p- cm
Yaw Magnet	+Moment saturation 615 p-cm/V	+5000±1000p-cm		A1J1-4	6.5.15	-7.588V +4667p- cm	-7.744V +4763p- cm	-7.463V +4590p- cm
	-Moment saturation 615 p-cm/V	-5000±1000p-cm		A1J1-4	6.1.15	+8.499V -5227p- cm	+8.569 -5270p- cm	+8.430V -5184p- cm
Pitch Magnet	+Moment saturation 607 p-cm/V	+5000±1000p-cm		A1J1-10	6.5.22	-7.727V +4690p- cm	-7.898V +4794p- cm	-7.587 +4605p- cm
	-Moment saturation 607 p-cm/V	-5000±1000p-cm		A1J1-10	6.5.22	+8.561V -5197p- cm	+8.652V -5252p- cm	+8.469V -5141p- cm

PROCEDURE NO. ATPS1105 S/N MCA PR1 DATE 10-18-72 PAGE 2

COMPONENT MCA PERFORMED BY RS APPROVED BY AS

T R E N D C H A R T

FUNCTION	TEST CONDITIONS	SPEC	INPUT	OUTPUT	XY Plot No.	ROOM	+50°C	-5°C
Offsets								
$M\psi$ TLM for $M\psi = 0$		$-3.7 \pm .7V$	A1J1-4	A1J1-3	6.5.17	-3.70V	-3.70V	-3.63V
$M\phi$ TLM for $M\phi = 0$		$-3.7 \pm .7V$	A1J1-12	A1J1-11	6.5.3	-3.70V	-3.86V	-3.67V
$M\theta$ TLM for $M\theta = 0$		$-3.7 \pm .7V$	A1J1-10	A1J1-9	6.5.10	-3.70V	-3.73V	-3.7V

-16-

PROCEDURE NO. ATPS 1105 S/N MCA DATE 10-18-72 PAGE 3



ITH-200

COMPONENT MCA PERFORMED BY RS APPROVED BY RS

T R E N D C H A R T

FUNCTION	TEST CONDITIONS	SPEC	INPUT	OUTPUT	XY PLOT	ROOM	50°C	-5°C
Offsets	Inputs not mentioned are at null							
Mψ Yaw Moment	+Bθ = +.1 gauss	± .68v	AlJ1-4	6.5.36	.00volt	-.40v	.00v	
	-Bθ = -.1 gauss	± .68v		6.5.35	.00v	-.65v	-.05v	
	+Bφ = +.25 gauss	± 1.7v		6.5.21	-.1v	+1.5v	-.05v	
	-Bφ = -.1 gauss	± .68v		6.5.19	+.05v	-.30v	.00v	
	+Bφ = +.1 gauss	± .68v		6.5.20	-.05v	+.80v	-.05v	
	Roll diff tach +75RPM	± .85v		6.5.34	.00v	-.55v	.00v	
	Pitch θ = .75°	± .85v		6.5.15	.00v	-.20v	.00v	
	Pitch wheel tach +75RPM	± .85v		6.5.16	.00v	+.07v	.00v	
All Inputs at null		± 300mv		"	Offset Test	-18mv	-47mv	-20mv

PROCEDURE NO. ATPS 1105 S/N MCA PRI DATE 10-10-72 PAGE 4



COMPONENT MCA PERFORMED BY RS APPROVED BY RS

T R E N D C H A R T

FUNCTION	TEST CONDITIONS	SPEC		OUTPUT	XY PLOT	ROOM	50°C	-5°C
Offsets	Inputs not mentioned are at null							
M _Φ Roll Moment	+Bθ = +.1 gauss	±.68v	AIJ1-12	6.5.33	-.45v	-.20v	-.40v	
	-Bθ = -.1 gauss	±.68v		" 6.5.32	+.45v	-.90v*	+.05v	
	+Bψ = +.25 gauss +.1 gauss	±1.7v ±.68v		" 6.5.5 " 6.5.6	.10 v .12 v	-.60v -.2v	.00v .00v	
	-Bψ = -.1 gauss	±.68v		" 6.5.7	.05v	+.43v	.00v	
	Pitchθ = .75°	±.85v		" 6.5.1	.00v	+.10v	.00v	
	Yaw wheel tach 75 RPM	±.85v		" 6.5.31	.00v	+.20v	.00v	
	Yaw Rate - .75X10 ⁻³ deg/sec	±.85v		" 6.5.30	.00v	+.40v	+.05v	
	All Inputs at null	±300mv		" Offset Test	+8mv	-4mv	+8mv	

* PR II-103 C

PROCEDURE NO. ATPS 1105 S/N MCA PRI DATE 10-10-72 PAGE 5
 COMPONENT MCA PERFORMED BY RS APPROVED BY RS

TREND CHART

FUNCTION	TEST CONDITIONS	SPEC	OUTPUT	XY PLOT	ROOM	50 °C	-5 °C
Offsets	Inputs not mentioned are at null		1				
M0 Pitch Moment	+Bψ = -.25 gauss	$\pm 1.7\text{v}$	AIJ1-9	6.5.11	-.15v	+.15v	+.70v
	+.25 gauss	$\pm 1.7\text{v}$	"	6.5.12	+.30v	+.10v	+.00v
	-Bψ =						
	-Bφ = +.1 gauss	$\pm .68\text{v}$	"	6.5.26	+.45v	+.11v*	+.20v
	+.25gauss	$\pm 1.7\text{v}$	"	6.5.27	+1.1v	+2.2v*	+.50v
	-Bφ = -.25gauss	$\pm 1.7\text{v}$	"	6.5.24	-1.0v	-1.0v	-.9v
	-Bφ = -.1 gauss	$\pm .68\text{v}$	"	6.5.25	-.40v	-.40v	-.5v
	Yaw wheel tach +75RPM	$\pm .85\text{v}$	"	6.5.23	.0v	+.40v	-.05v
	-75RPM	$\pm .85\text{v}$	"	6.5.22	.0v	+.60v	-.08v
	Yaw Rate $-.75 \times 10^{-3}$ deg/sec	$\pm .85\text{v}$	"	6.5.22	.00v	-.15v	-.10v
	Roll wheels diff tach						
	+75RPM	$\pm .85\text{v}$	"	6.5.8	.00v	+.05v	+.50v
	-75RPM	$\pm .85\text{v}$	"	6.5.9	.00v	+.20v	+.60v
	All Inputs at Null	$\pm 300\text{mv}$	"	Offset Test	-25mv	+216mv	-102mv

* PR11-103 Rev B

PROCEDURE NO. ATPS 1105 S/N MCA PRI DATE 10-10-72 PAGE 6



COMPONENT MCA PERFORMED BY RS APPROVED BY RS

TEST CONDITIONS

FUNCTION	TEST CONDITIONS	SPEC	INPUT	OUTPUT	DATA SHEET	ROOM	50°C	-5°C
<u>Gain</u>								
M _θ vs B _ψ	0.75° pitch	-5.12 ± 1.0 v/v	10v/gauss	A1J1-12	XY-1	-5.18 v/v	-4.35 v/v	-5.55 v/v
M _θ TLM vs M _θ	75 RPM pitch tach	+2.33 ± .6 v/v 0.286 ± .02 v/v	A1J1-12	A1J1-11	XY-2 XY-3	+2.80 v/v +0.284 v/v	+2.35 v/v +.284 v/v	+2.61 v/v +.283 v/v
M _θ vs θ	B _ψ = -0.25 gauss	171 ± 30 v/v	A3J3-8	A1J1-12	XY-4	+200 v/v	+161 v/v	+192 v/v
M _θ vs δωθ	B _ψ = + 0.25 gauss	67.7 ± 13 v/v	A3J3-4	A1J1-12	XY-5	+75 v/v	+63.5 v/v	+79 v/v
	B _ψ = + 0.1 gauss	27.1 ± 5 v/v			XY-6	+28.5 v/v	+25.0 v/v	+33.0 v/v*
	B _ψ = - 0.1 gauss	-27.1 ± 5 v/v			XY-7	-30.8 v/v	-27.2 v/v	-28.6 v/v
M _θ vs B _ψ	75RPM diff tach	+1.2 ± .3 v/v	10v/gauss	A1J1-10	XY-8	+1.18 v/v	+1.41 v/v	+1.11 v/v
	-75 RPM diff tach	-1.2 ± .3 v/v			XY-9	-1.30 v/v	-1.0 v/v	-1.42 v/v
M _θ TLM vs M _θ		0.286 ± .02 v/v	A1J1-10	A1J1-9	XY-10	.281 v/v	.282 v/v	.280 v/v
M _θ vs δωφ	B _ψ = -0.25 gauss	-16.5 ± 3.3 v/v	A3J3-1	A1J1-10	XY-11	-17.1 v/v	-16.1 v/v	-17.4 v/v
	B _ψ = 0.25 gauss	16.5 ± 3.3 v/v			XY-12	+17.2 v/v	+16.4 v/v	+16.4 v/v
Yaw Acquisition	B > 0, 2000 p-cm Y=3.42v	0°C 25°C 45°C	0.272 ± .04 v 0.235 ± .04 v 0.204 ± .04 v	1mgauss/sec-volt	A1J1-4	+.24 v	.308 v	
	saturation	0°C 25°C 45°C	0.311 ± .05 v 0.273 ± .04 v 0.242 ± .04 v			+.268 v	+.192 v	+.335 v

PROCEDURE NO. ATPS 1105 S/N MCA PR1 DATE 10-10-72 PAGE 7



COMPONENT MCA PERFORMED BY RS APPROVED BY RS

*PR11-104

T R E N D C H A R T

FUNCTION	TEST CONDITIONS	SPEC	INPUT	OUTPUT	DATA SHEET	ROOM	50°C	-5°C
Yaw Acquisition	$B < 0$, 2000 p-cm $Y=3.42v$	$0^\circ C$ $25^\circ C$ $45^\circ C$	$-0.272 \pm .04v$ $-0.235 \pm .04v$ $-0.204 \pm .04v$		XY-14	.253 v	.310 v	
	saturation	$0^\circ C$ $25^\circ C$ $45^\circ C$	$-0.311 \pm .05v$ $-0.273 \pm .04v$ $-0.242 \pm .04v$.279 v	.330 v	
$M\psi$ vs $B\phi$	$\theta = 0.75^\circ$	$+5.12 \pm 1.0v/v$	10 v/ gauss	AlJ1-4	XY-15	$+5.10 \frac{v}{v}$	$+4.4 \frac{v}{v}$	$+5.56 \frac{v}{v}$
	75 RPM pitch tach	$-2.33 \pm .6v/v$			XY-16	$-2.62 \frac{v}{v}$	$-2.25 \frac{v}{v}$	$-2.8 \frac{v}{v}$
$M\psi$ TLM vs $M\psi$		$0.286 \pm .02v/v$	AlJ1-4	AlJ1-3	XY-17	$.280 \frac{v}{v}$	$.280 \frac{v}{v}$	$.285 \frac{v}{v}$
$M\psi$ vs θ	$B\phi = -0.25$ gauss	-171 ± 30 v/v	A3J3-8	AlJ1-4	XY-18	$-191.3 \frac{v}{v}$	$-160 \frac{v}{v}$	$-186 \frac{v}{v}$
$M\psi$ vs $\delta\omega\theta$	$B\phi = -0.1$ gauss	$+27.1 \pm 5$ v/v	A3J3-4	AlJ1-4	XY-19	$+28.9 \frac{v}{v}$	$+30 \frac{v}{v}$	$+29.2 \frac{v}{v}$
	$B\phi = 0.1$ gauss	-27.1 ± 5 v/v			XY-20	$-29.0 \frac{v}{v}$	$-26 \frac{v}{v}$	$-28.6 \frac{v}{v}$
	$B\phi = 0.25$ gauss	-67.7 ± 13 v/v			XY-21	$-74.4 \frac{v}{v}$	$-70 \frac{v}{v}$	$-75 \frac{v}{v}$
$M\theta$ vs $B\phi$	$-0.00075^\circ/\text{sec}$ yaw rate	$+4.26 \pm .9v/v$	10v/ gauss	AlJ1-10	XY-22	$+4.57 \frac{v}{v}$	$+5.0 \frac{v}{v}$	$+4.3 \frac{v}{v}$
	75 RPM yaw tach	$-1.17 \pm .3v/v$			XY-23	$-.766 \frac{v}{v}$ $+1.58 \frac{v}{v}$	$-.472 \frac{v}{v}$ $+1.82 \frac{v}{v}$	$.90 \frac{v}{v}$ $1.5 \frac{v}{v}$
$M\theta$ vs Yaw Rate	$B\phi = -0.25$ gauss	-112 ± 22 v/v	A3J3-9	AlJ1-10	XY-24	$-116 \frac{v}{v}$	$-115 \frac{v}{v}$	$115 \frac{v}{v}$
$M\theta$ vs Yaw Tach	$B\phi = -0.1$ gauss	$+7.07 \pm 1.4$ v/v	A3J3-5	AlJ1-10	XY-25	$+6.92 \frac{v}{v}$	$+7.3 \frac{v}{v}$	$+6.8 \frac{v}{v}$
	$B\phi = +0.1$ gauss	-7.07 ± 1.4 v/v			XY-26	$-7.42 \frac{v}{v}$	$-7.2 \frac{v}{v}$	$-6.9 \frac{v}{v}$
	$B\phi = +0.25$ gauss	-17.7 ± 3.5 v/v			XY-27	$-18.2 \frac{v}{v}$	$-17.8 \frac{v}{v}$	$-17.9 \frac{v}{v}$

PROCEDURE NO. ATPS 1105 S/N MCA PR1 DATE 10-10-72

PAGE 8

COMPONENT MCA

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**PR11-103

FUNCTION	TEST CONDITIONS	SPEC	INPUT	OUTPUT	DATA SHEET	ROOM	50°C	-5°C
Roll Acquisition	$B > 0$, 2000 p-cm $Y = 3.42v$ saturation	0°C 25°C 45°C	$1.129 \pm .17\text{v}$ $0.953 \pm .14\text{v}$ $0.812 \pm .12\text{v}$	1mgauss sec volt	AlJ1-12	XY-28	+.950v	+1.27v
		0°C 25°C 45°C	$1.305 \pm .20\text{v}$ $1.129 \pm .17\text{v}$ $0.988 \pm .15\text{v}$				+1.09v	+1.39v
	$B < 0$, 2000 p-cm $Y = 3.42v$ saturation	0°C 25°C 45°C	$-1.129 \pm .17\text{v}$ $-0.953 \pm .14\text{v}$ $-0.812 \pm .12\text{v}$		XY-29		.98v	-1.26v
		0°C 25°C 45°C	$-1.305 \pm .20\text{v}$ $-1.129 \pm .17\text{v}$ $-0.988 \pm .15\text{v}$				-1.10v	-1.37v
M_y vs $B\theta$	$-0.00075^{\circ}/\text{sec}$ Yaw rate 75 RPM Yaw tach	$-4.26 \pm .9\text{v/v}$ $+1.17 \pm .3\text{v/v}$	10v/gauss	AlJ1-12	XY-30 XY-31	$-4.59 \frac{\text{v}}{\text{v}}$ $+.736 \frac{\text{v}}{\text{v}}$	$-4.7 \frac{\text{v}}{\text{v}}$ $+.45 \frac{\text{v}}{\text{v}}$	$4.7 \frac{\text{v}}{\text{v}}$ $+.88 \frac{\text{v}}{\text{v}}$
M_y vs Yaw Rate	$B\theta = -0.1$ gauss	$+44.9 \pm 9\text{v/v}$	A3J3-9	AlJ1-12	XY-32	$+46.2 \frac{\text{v}}{\text{v}}$	$+44.8 \frac{\text{v}}{\text{v}}$	$43.5 \frac{\text{v}}{\text{v}}$
M_y vs yaw tach	$B\theta = +0.1$ gauss	$+7.07 \pm 1.4\text{v/v}$	A3J3-5	AlJ1-12	XY-33	$+6.3 \frac{\text{v}}{\text{v}}$	$+5.3 \frac{\text{v}}{\text{v}}$	$+7.8 \frac{\text{v}}{\text{v}}$
M_y vs $B\theta$	75RPM Diff Tach	$-1.20 \pm .3 \text{ v/v}$	10v/gauss	AlJ1-4	XY-34	$-1.23 \frac{\text{v}}{\text{v}}$	$-.97 \frac{\text{v}}{\text{v}}$	$-1.25 \frac{\text{v}}{\text{v}}$
M_y vs Diff Tach	$B\theta = -0.1$ gauss	$6.58 \pm 1.3 \text{ v/v}$	A3J3-1	AlJ1-4	XY-35	$6.78 \frac{\text{v}}{\text{v}}$	$+6.0 \frac{\text{v}}{\text{v}}$	$+6.4 \frac{\text{v}}{\text{v}}$
	$B\theta = 0.1$ gauss	$-6.58 \pm 1.3 \text{ v/v}$			XY-36	$-6.24 \frac{\text{v}}{\text{v}}$	$-5.4 \frac{\text{v}}{\text{v}}$	$-6.5 \frac{\text{v}}{\text{v}}$
Pitch Acquisition	$B > 0$, 2000 p/m $Y = 3.42v$	0°C 25°C 45°C	$1.082 \pm .16\text{v}$ $0.931 \pm .14\text{v}$ $0.810 \pm .12\text{v}$	1mgauss sec-volt	AlJ1-10	XY-37	$+.937$ $+.71$	+1.17v

PROCEDURE NO. ATPS 1105

S/N MCA PRI

DATE 10-10-72

PAGE 9



COMPONENT

MCA

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RS

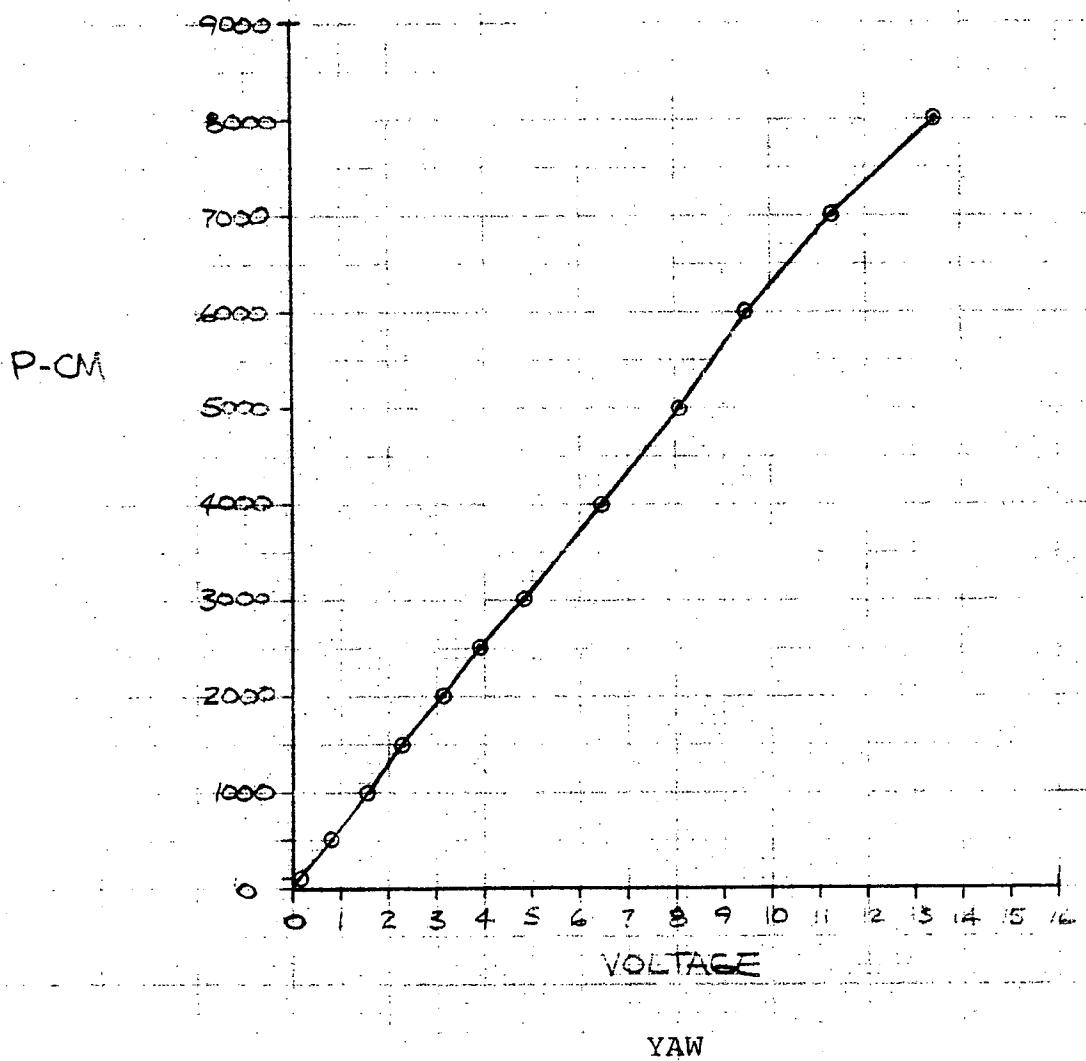
TEST REPORT

FUNCTION	TEST CONDITIONS	SPEC	DATA SHEET	ROOM	50°C	-5°C
Pitch Acquisition	saturation 0°C 25°C 45°C B. < 0, 2000 p/m Y = -3.42v	1.233± .18v 1.082± .16v 0.961± .14v -1.082± .16v -0.931± .14v -0.810± .12V -1.233± .18v -1.082± .16v -0.961± .14v	XY-37 XY-38	+1.055v -.94v -1.040v	+1.26v +.85v -1.18v -.73v -1.28v -.85v	

-34-

PROCEDURE NO. ATPS1105 S/N MCA DATE 10-10-72 PAGE 10

COMPONENT MCA PERFORMED BY RS APPROVED BY RS



ITPS 1108, Para 6.1
ITHACO, Inc. Qual Model
MCA Electromagnets

Dipole moment vs voltage
post conformal coating

Axis YAW

S/N 15030

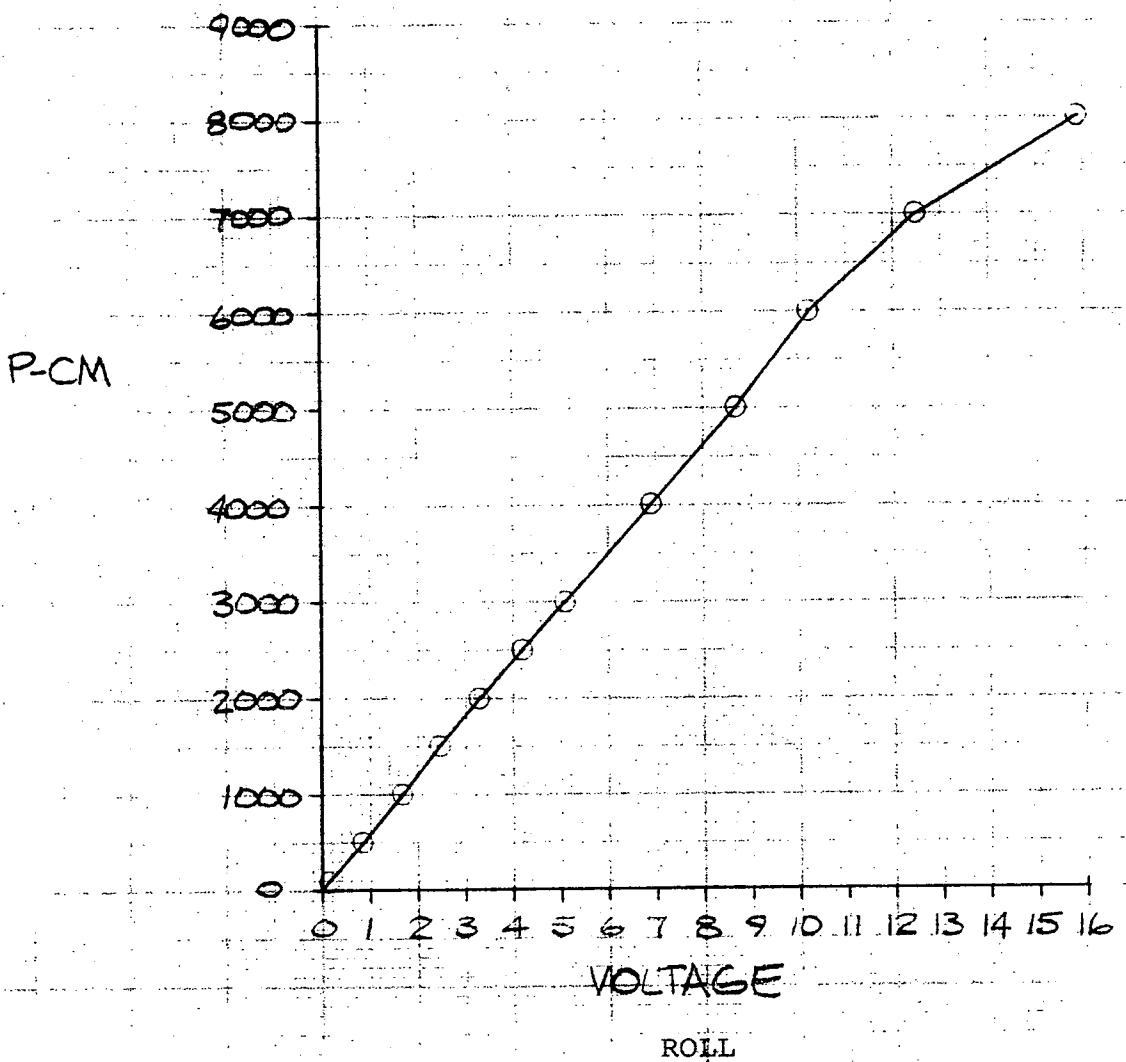
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Temp: 22°C

Performed by: K. Kabelac

615 P-CM/V

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11



ITPS 1108, Para 6.1
ATHACO, Inc. Qual Model
MCA Electromagnets

Dipole moment vs voltage
Post conformal coating

Axis PITCH

S/N 15029

Date: 7-24-72

Temp: 22°C

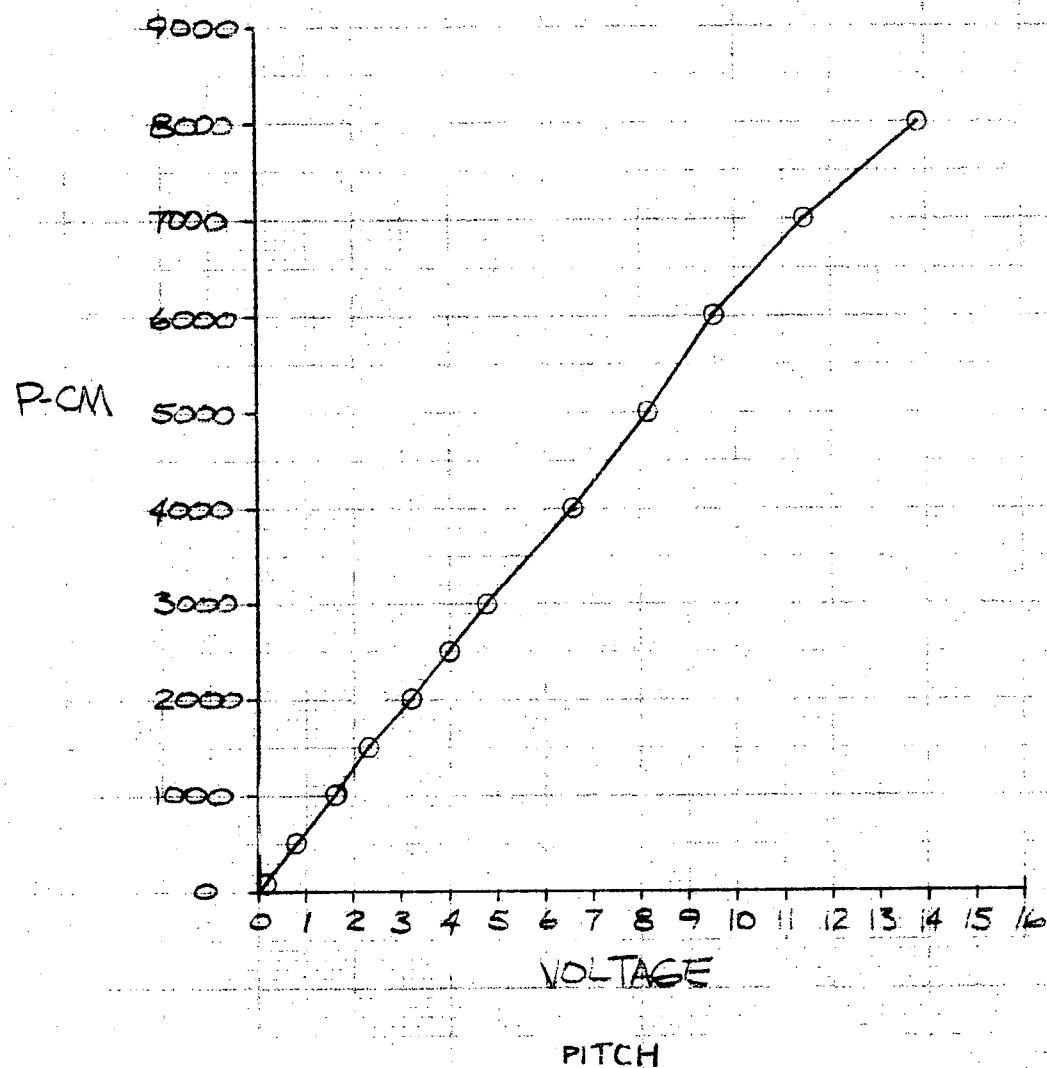
Performed by: K. Kabelac

RS

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607 P-cm/V



-38-

14.0 PHOTOS

See following pages:

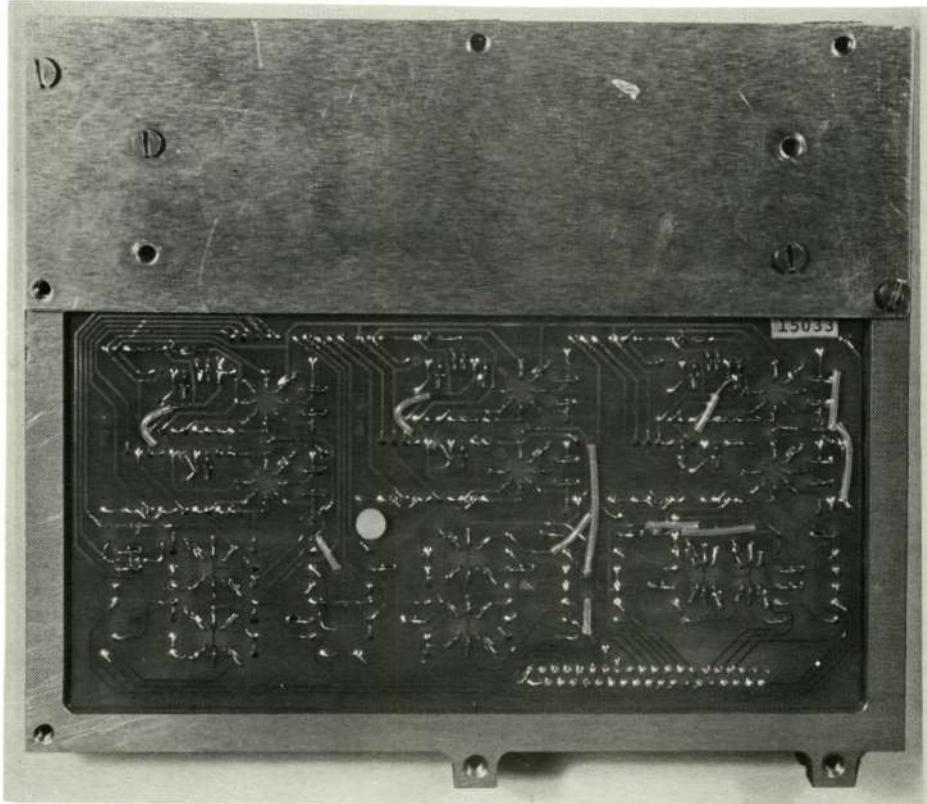
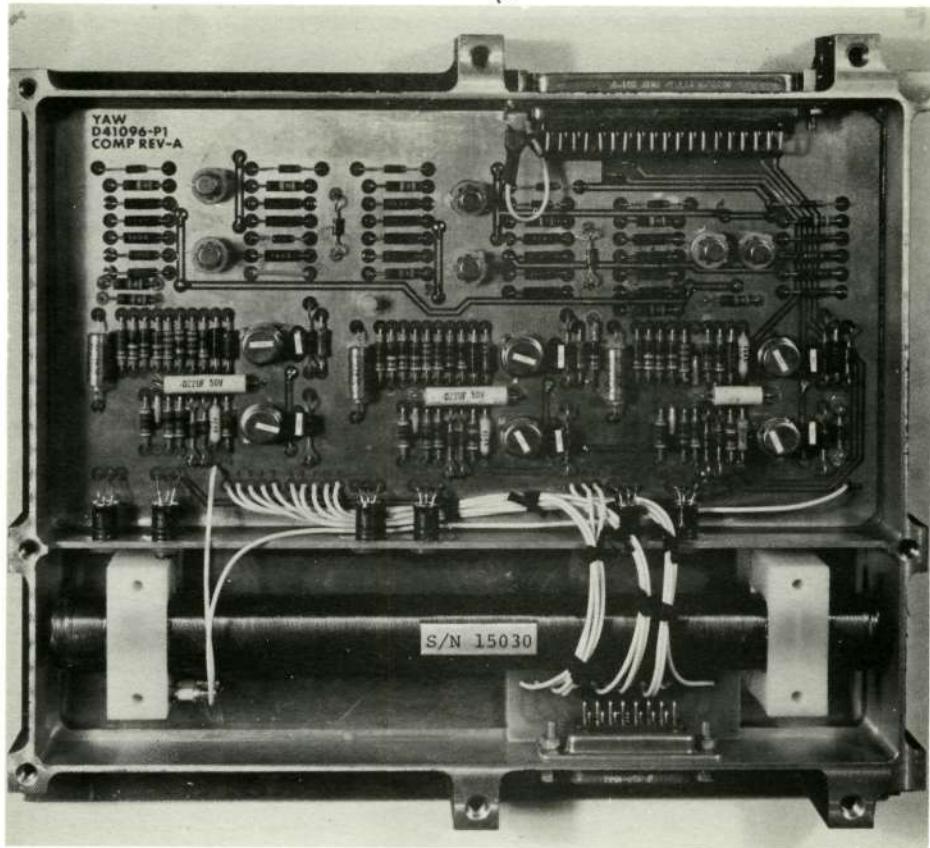


Control Logic Assembly of MCA PRL

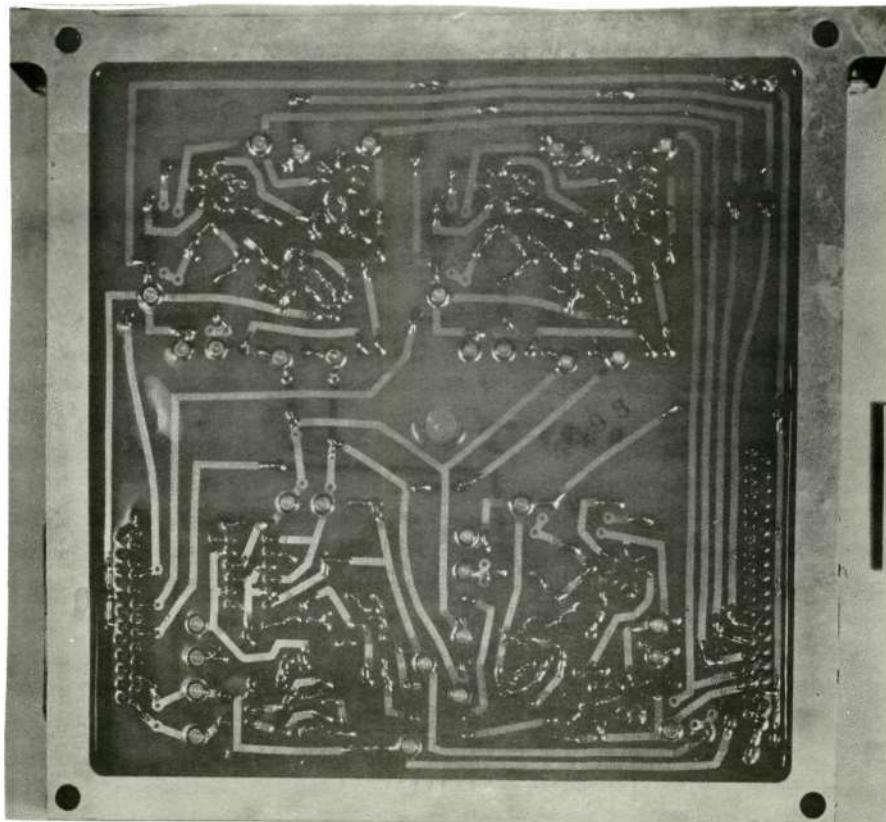
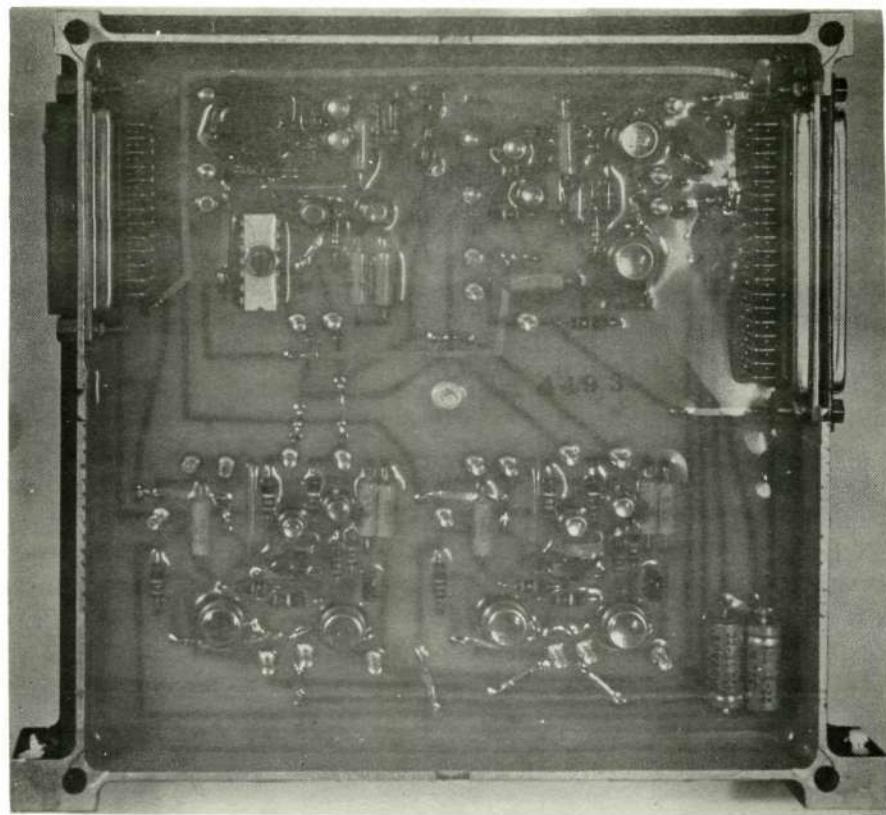


Magnetometer of MCA PR1 S/N 15062

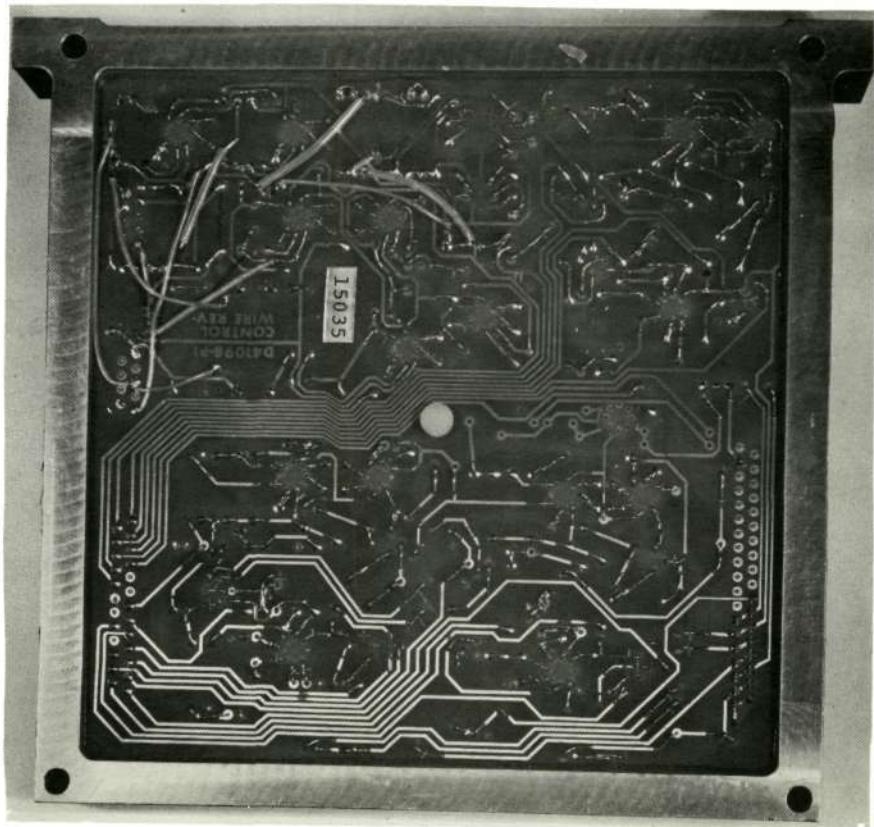
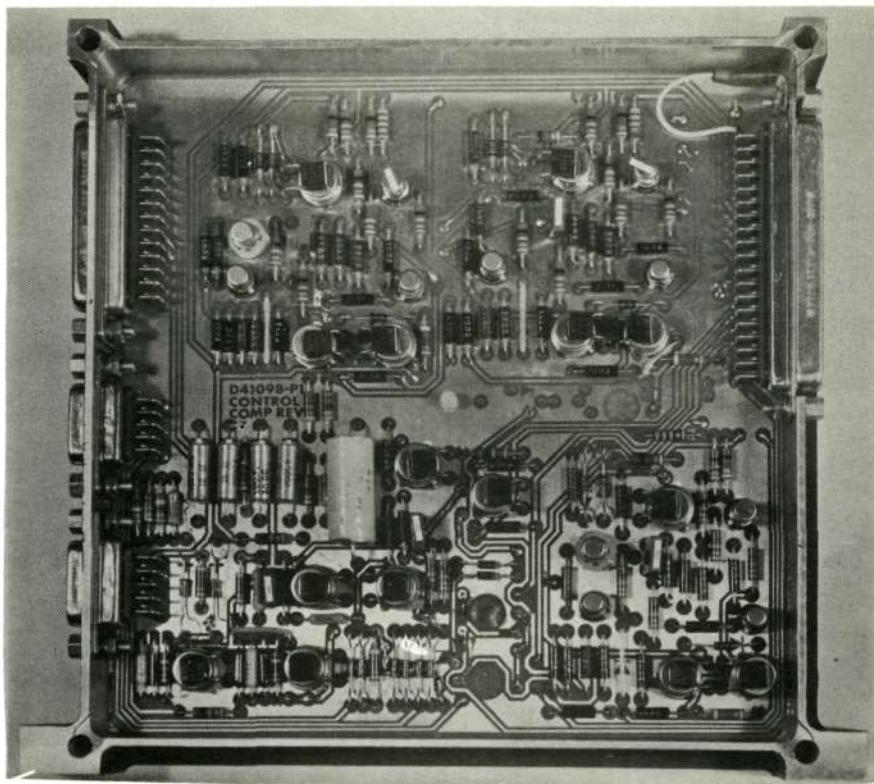
-41-



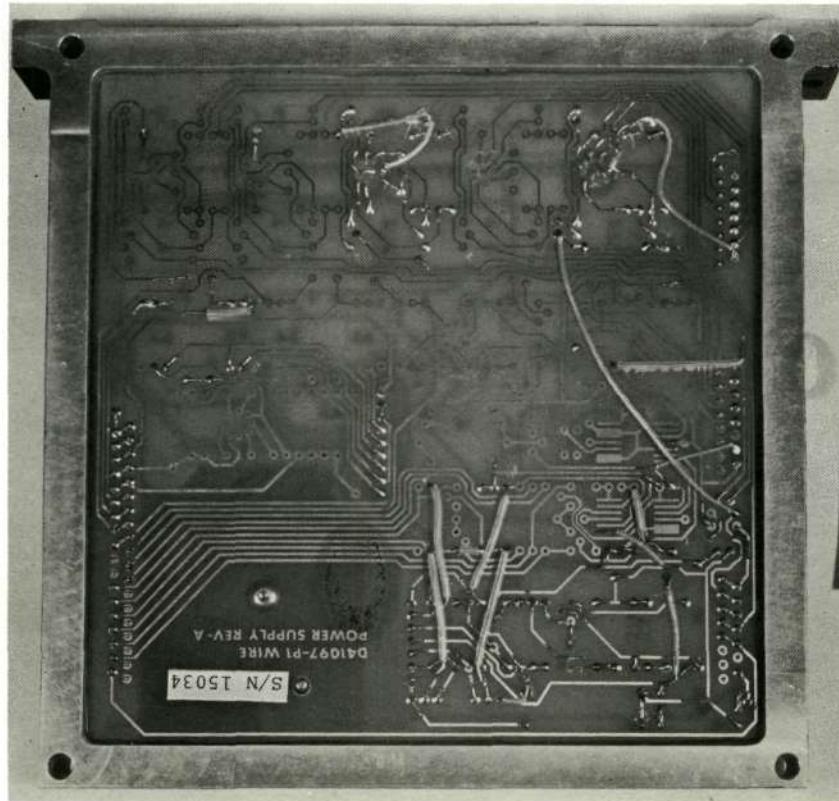
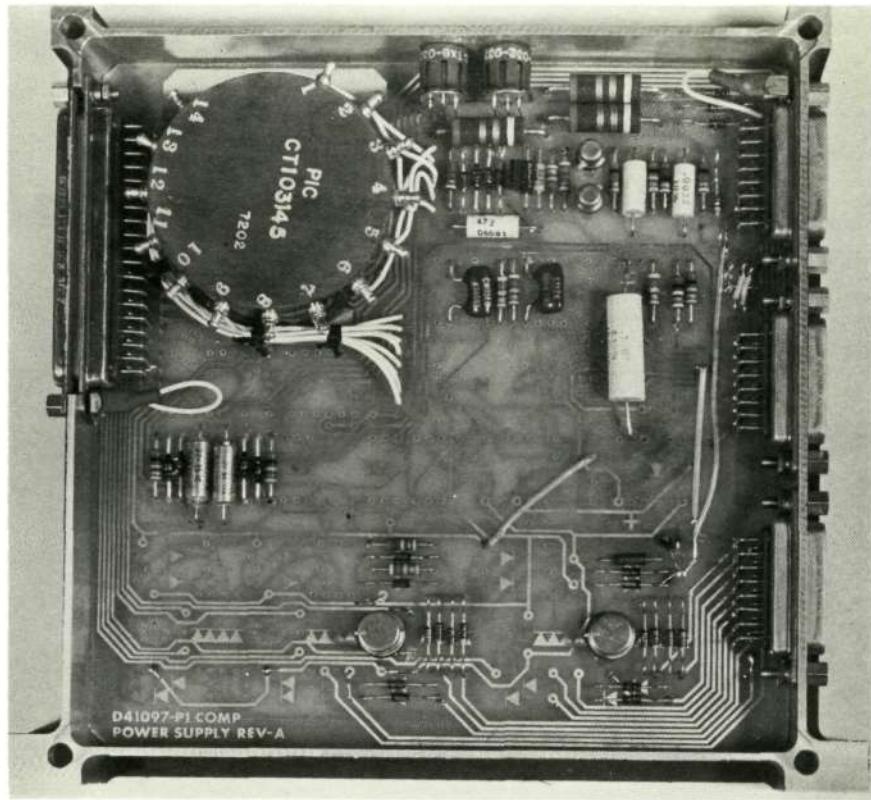
Yaw Card of MCA PRI S/N 15033



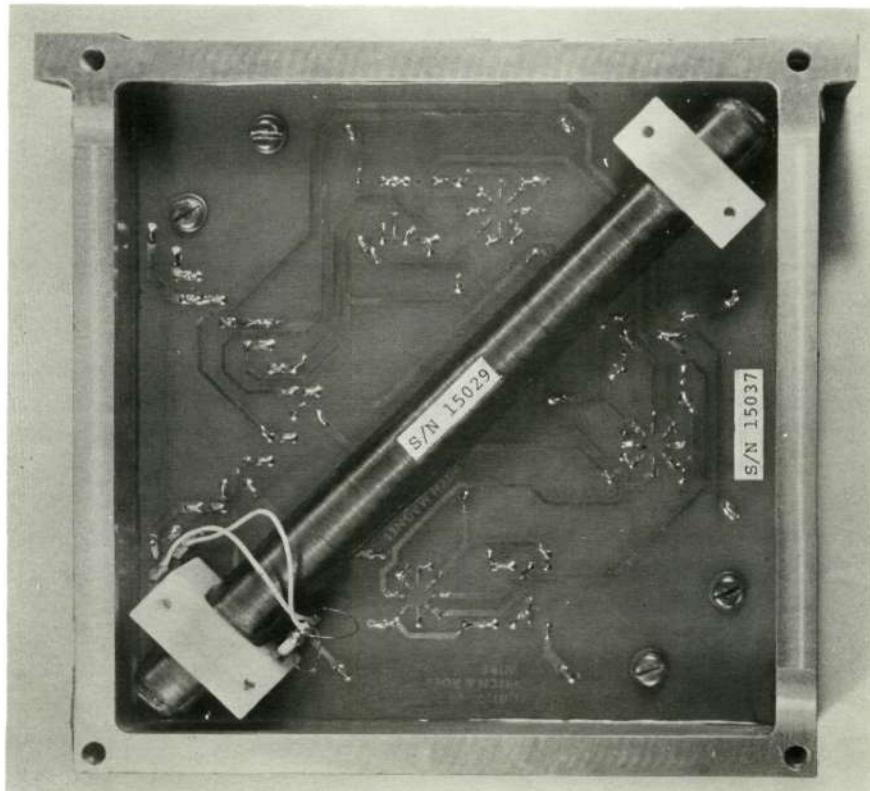
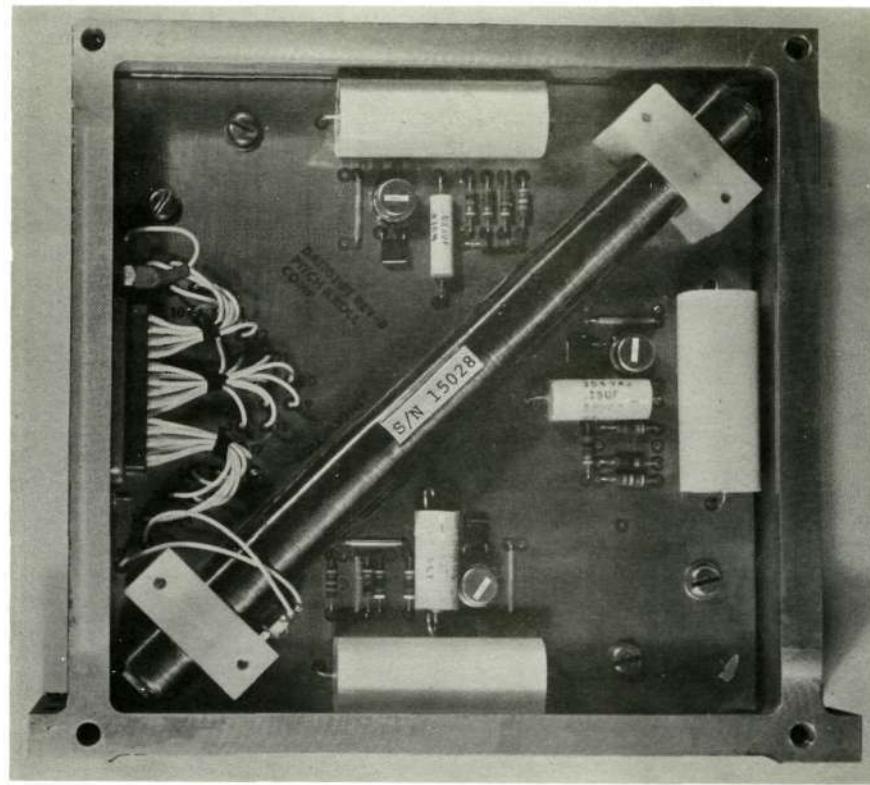
Magnetometer Electronics of MCA PR1 S/N 4493



Control Card of MCA PR1 S/N 15035



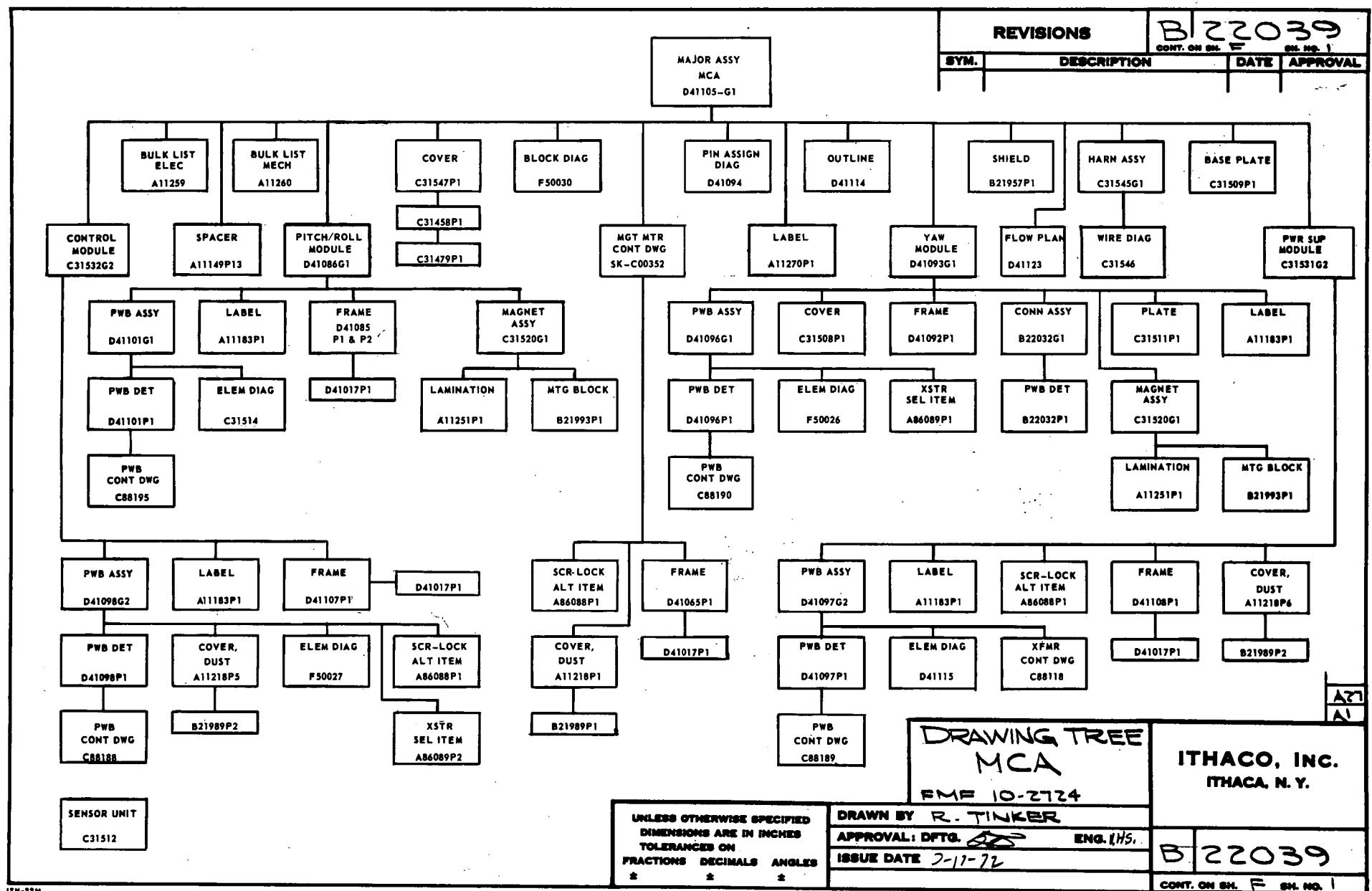
Power Supply Card of MCA PR1 S/N 15034

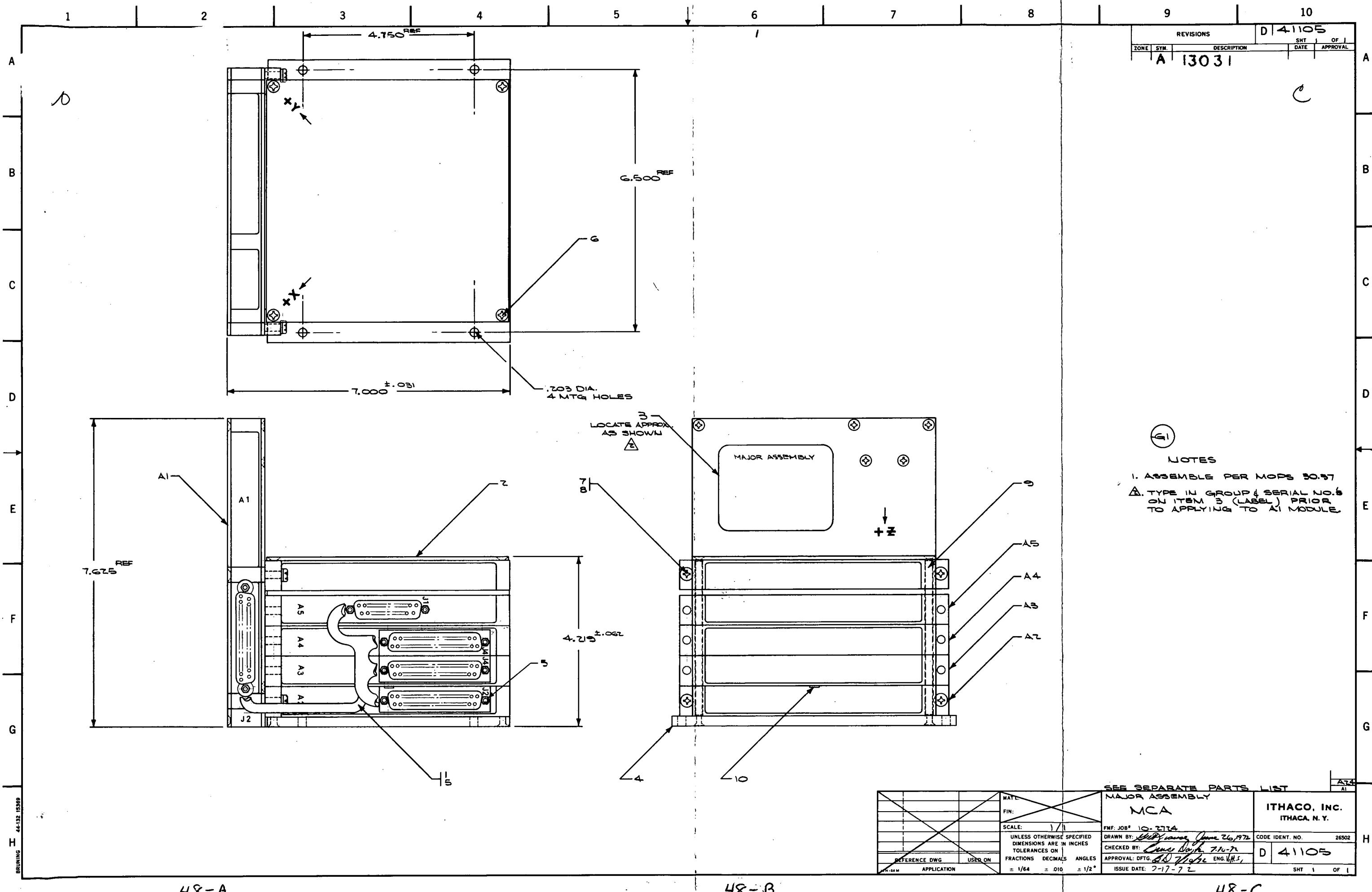


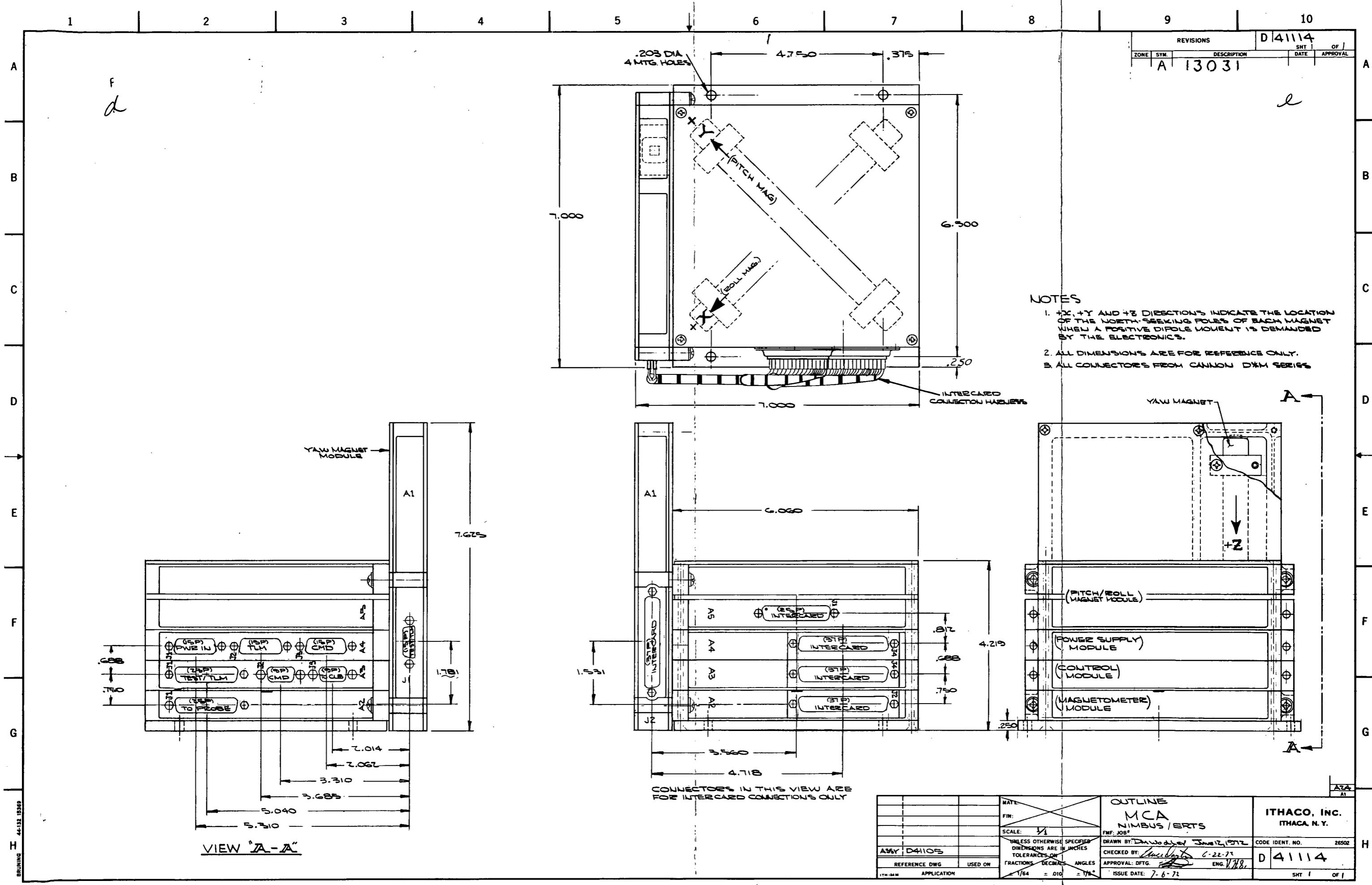
Pitch and Roll Card of MCA PR1 S/N 15037

15.0 DRAWINGS

See following pages:

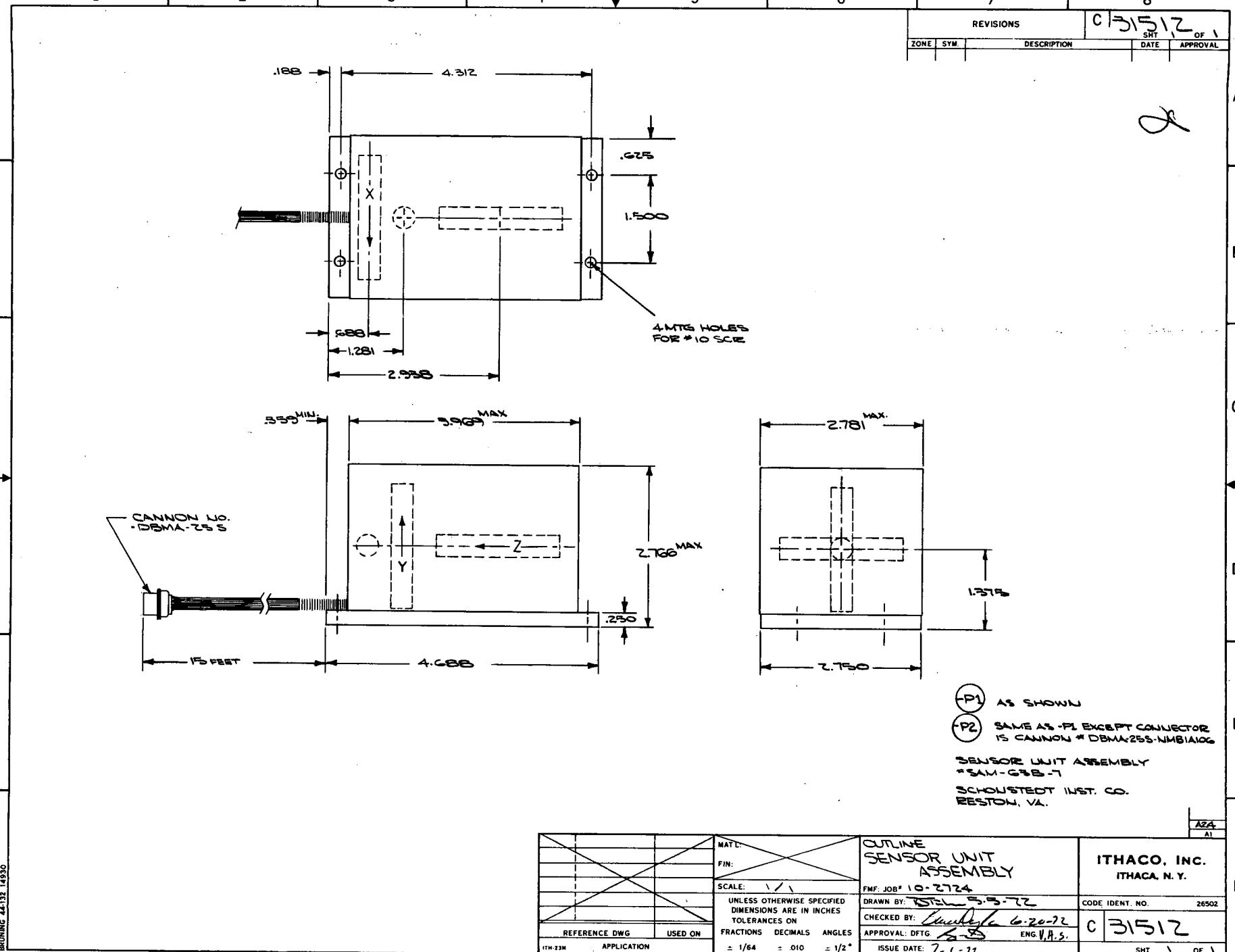






1 2 3 4 5 6 7 8

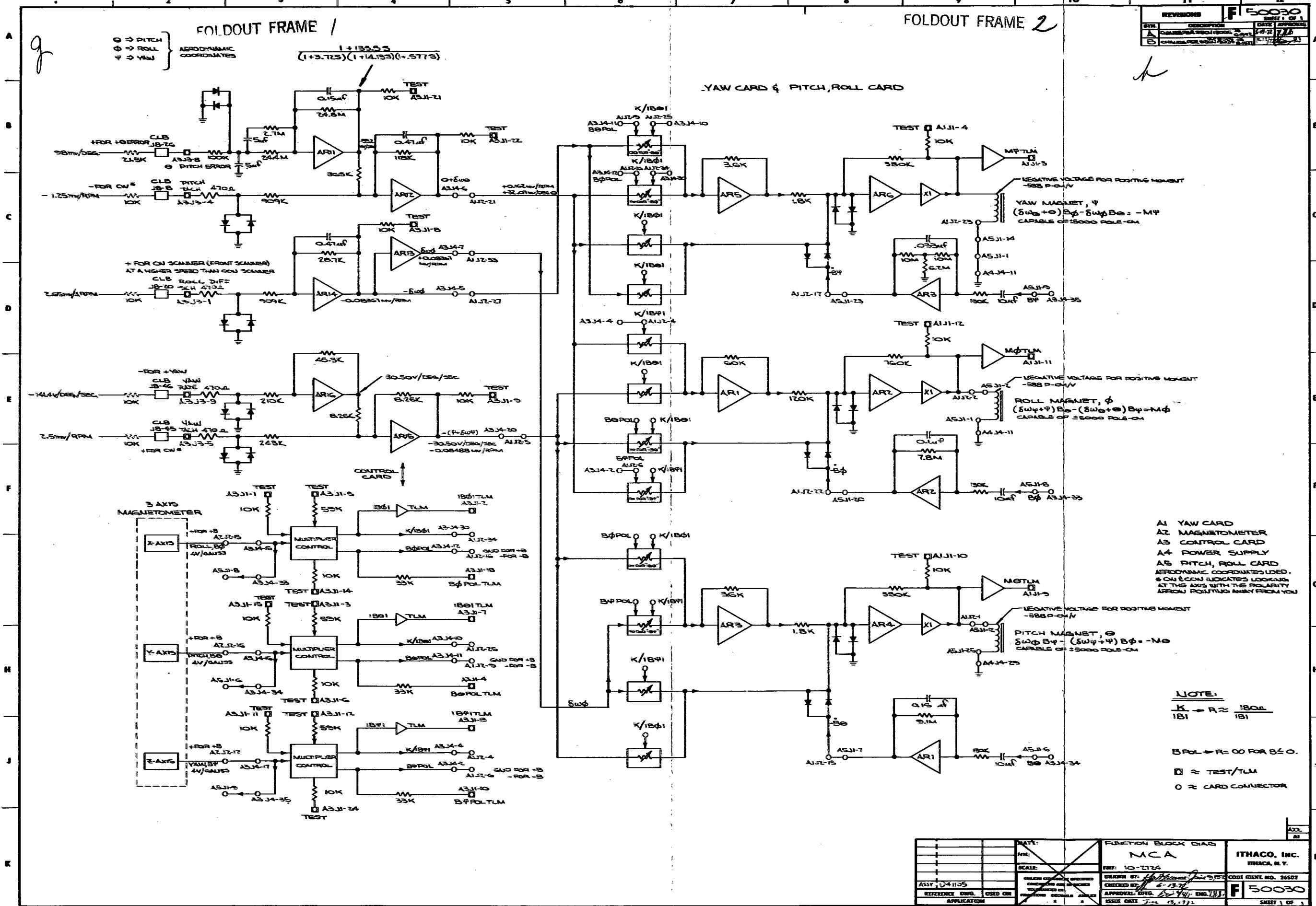
REVISIONS		C 31512	
ZONE	SYM.	DESCRIPTION	DATE



-51-A

51-B

51-C



52-A

52-B

52-C

FOLDOUT FRAME 1

EXTERNALMAGNETOMETER
ELECTRONICS
TO MAGNETOMETER

PROBE

(25P)
AZJ1

1	
14	TEST
2	
15	TEST
3	
16	TEST
4	BΦ POLARITY TLM
17	
5	TEST
18	BΦ POLARITY TLM
6	TEST
19	
7	BΦ TLM
20	
8	TEST
21	TEST
9	
22	TEST
10	BΦ POLARITY TLM
23	
11	TEST
24	TEST
12	TEST
25	
13	BΦ TLM

CONTROL
CARDTEST/TLM
(25P)
ABJ1

1	TEST
14	TEST
2	BΦ TLM
15	TEST
3	
16	TEST
4	BΦ POLARITY TLM
17	
5	TEST
18	BΦ POLARITY TLM
6	TEST
19	
7	BΦ TLM
20	
8	TEST
21	TEST
9	
22	TEST
10	BΦ POLARITY TLM
23	
11	TEST
24	TEST
12	TEST
25	
13	BΦ TLM

POWER
SUPPLYPWR
(15P)
AAJ1

8	
15	MΦ TLM
7	
14	
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4	
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YAW
CARDTEST/TLM
(15P)
A1J1

1	TEST
14	MΦ TLM
2	TEST
15	TEST
3	
16	
4	BΦ POLARITY TLM
17	
5	TEST
18	BΦ POLARITY TLM
6	TEST
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7	BΦ TLM
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YAW
CARD(37P)
A1J2

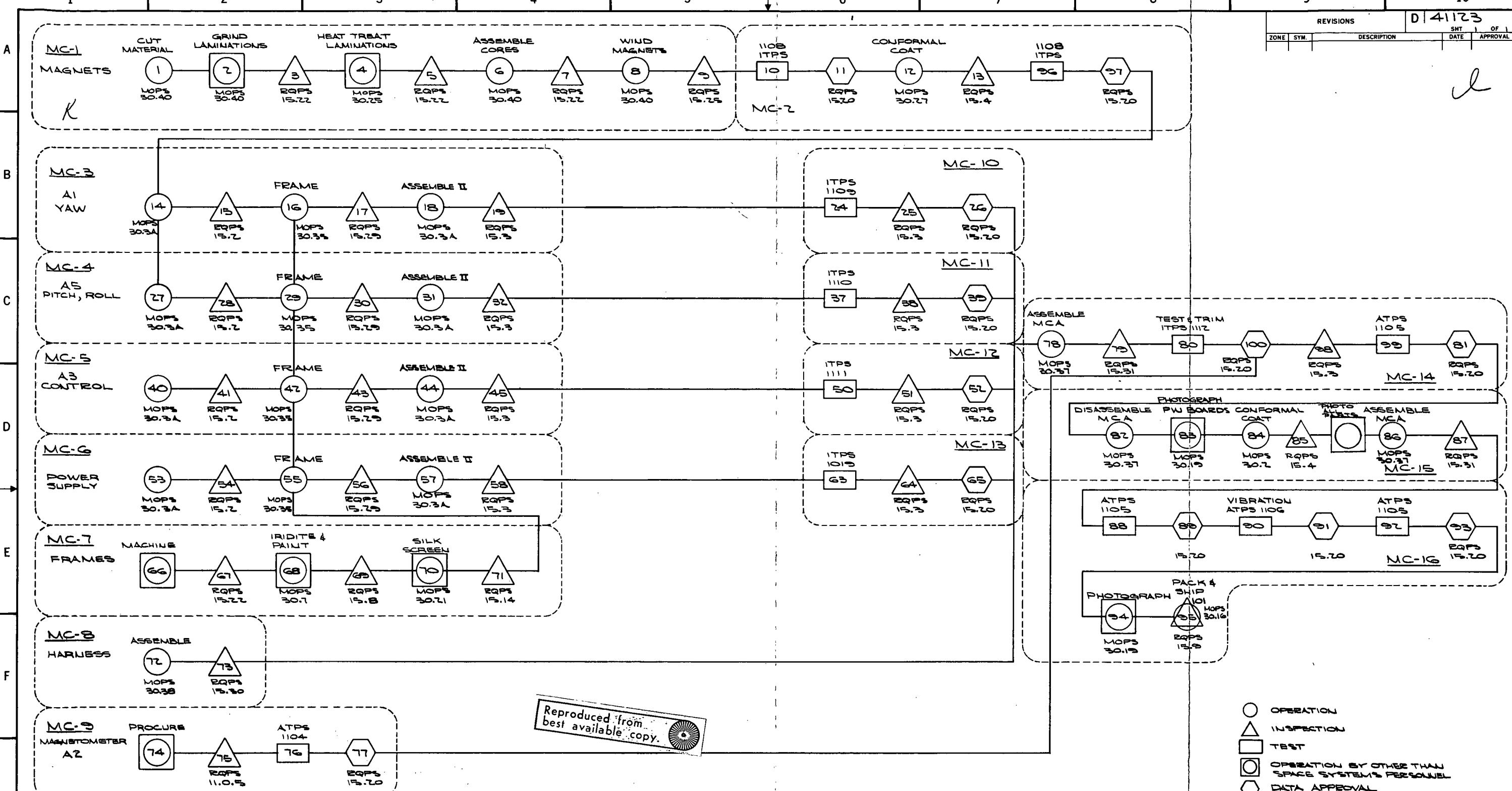
1	TEST
14	MΦ TLM
2	TEST
15	TEST
3	
16	
4	BΦ POLARITY TLM
17	
5	TEST
18	BΦ POLARITY TLM
6	TEST
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7	BΦ TLM
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8	TEST
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FOLDOUT FRAME 1

54-A

54-B

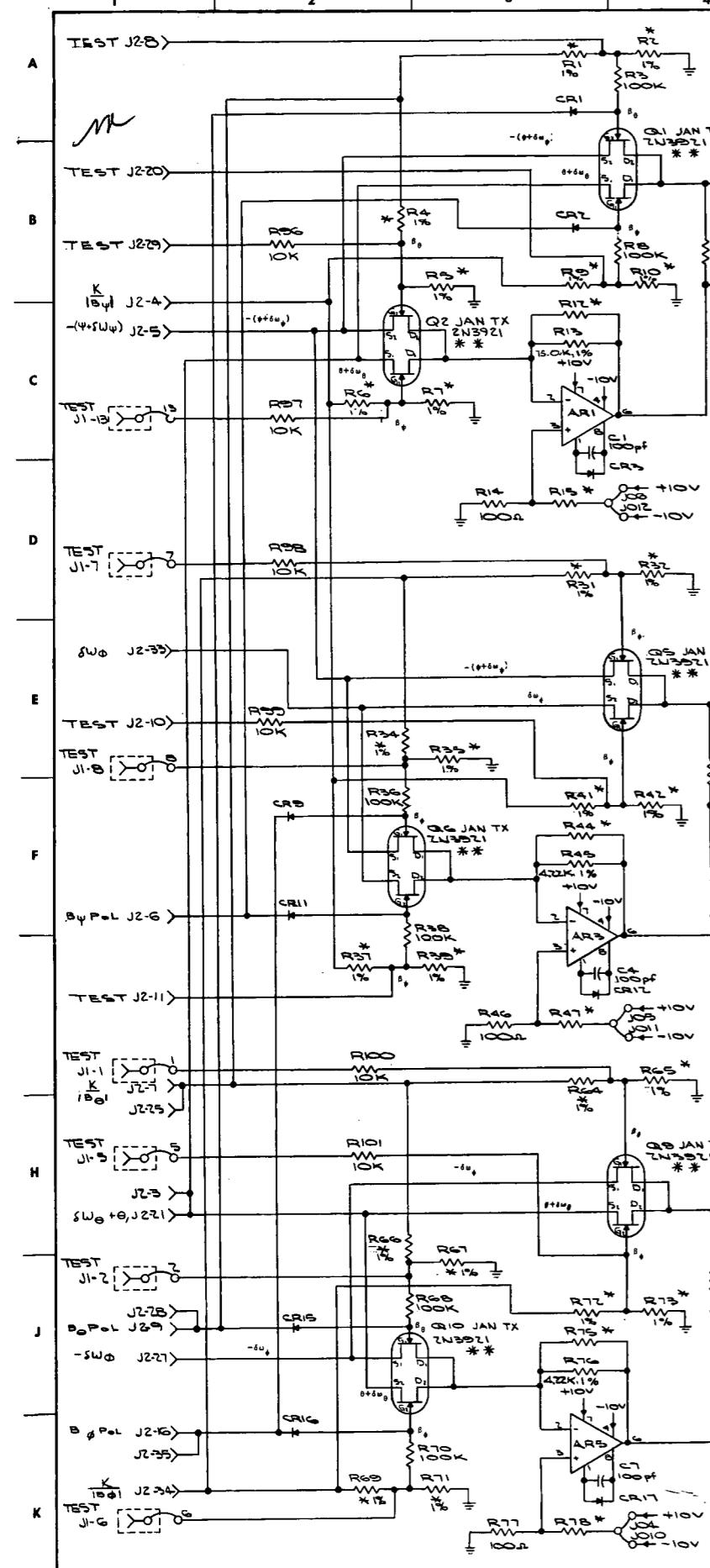
54C FOLDOUT FRAME 2

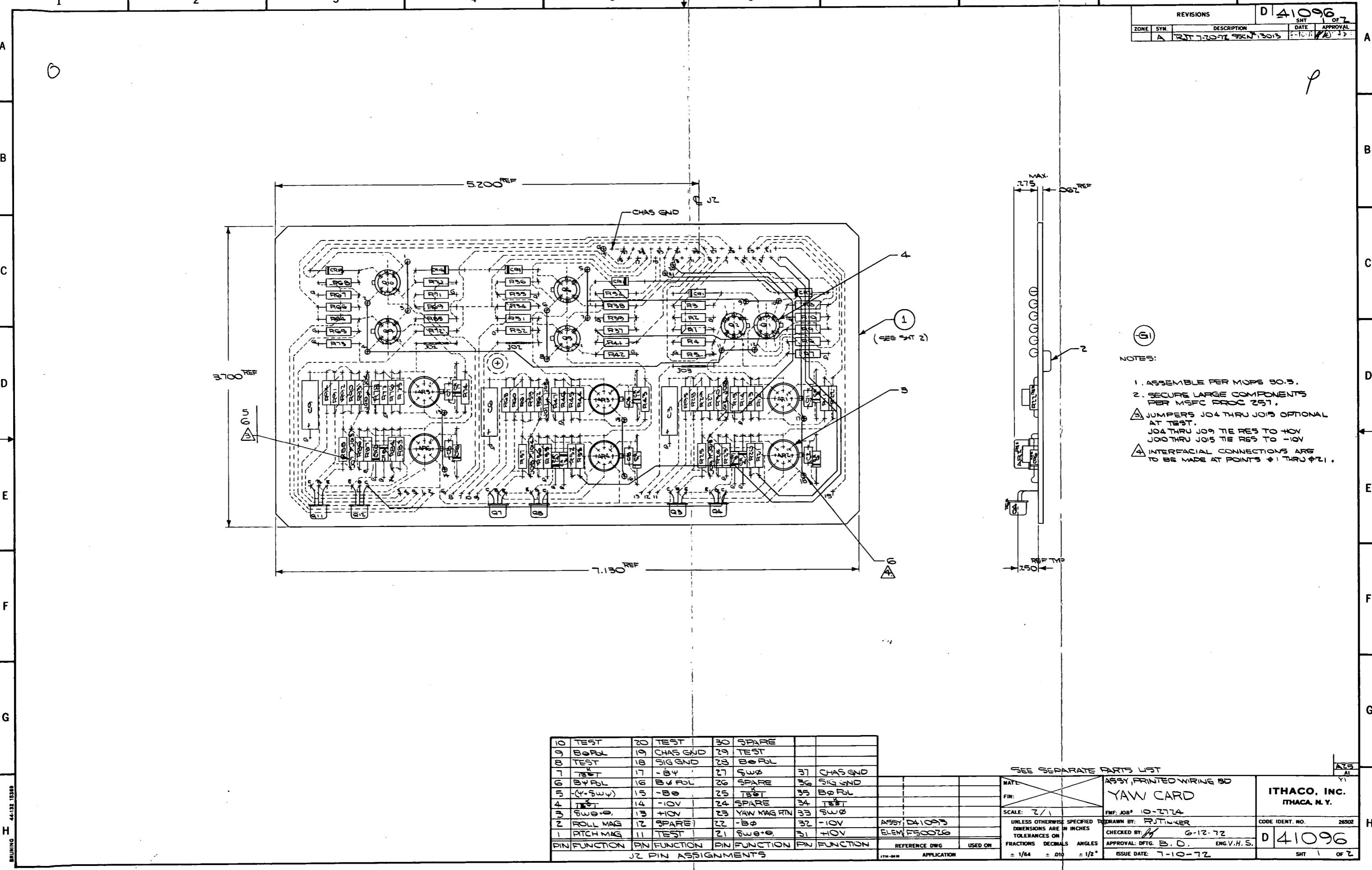


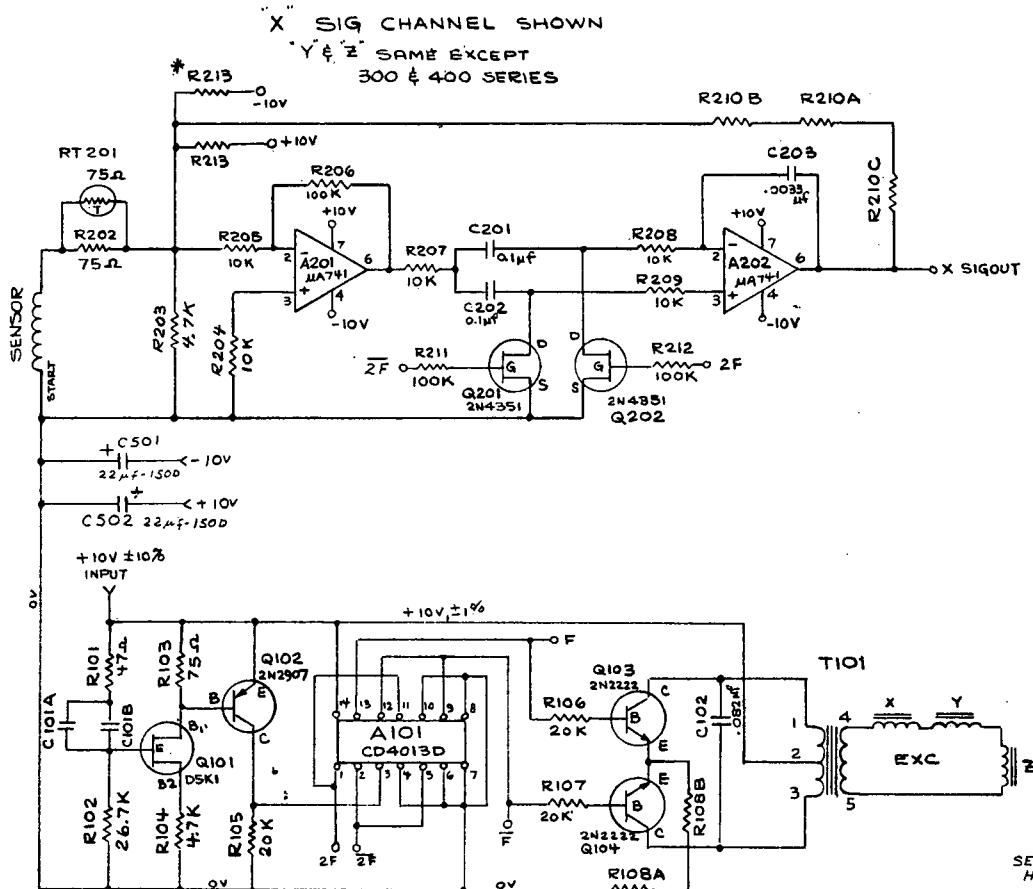
		MATL:	MANUFACTURING & INSPECTION			ITHACO, INC.	
		FIN:	FLOW PLAN			ITHACA, N.Y.	
SCALE:		SPECIFIED					
FMF: JOB# 10-7724		UNLESS OTHERWISE					
DRAWN BY: <i>John J. Hayes</i> June 12, 1972		DIMENSIONS ARE IN INCHES					
CHECKED BY: <i>John J. Hayes</i>		TOLERANCES ON					
APPROVAL: DFTG <i>John J. Hayes</i>		FRACTIONS	DECIMALS	ANGLES			
ENG. RS		± 1/64	± .010	± 1/2°			
ISSUE DATE: Sept 28, 1972							
SHT 1 OF 1							

FOLDOUT FRAME 1

55-A





NOTES:

* ALTERNATE POSITION

A101	CD4013D	ICCD4013D
T101	205309	
Q101	D5K1 (G.E.)	
Q102	2N2907	TC2N2907
Q103	2N2222	TC2N2222
Q104	2N2222	TC2N2222
C101A	TEST	
C101B	TEST	
C102	.082μF	CDAP--- } ~ 910μF CDAP--- } TOTAL CL06BX823K
R101	47Ω	RAAC047
R102	26.7 K	RDLB2672
R103	75 Ω	RAAC075
R104	4.7 K	RDLB4701
R105	20 K	RAAC2002
R106	20 K	RAAC2002
R107	20 K	RAAC2002
R108A	TEST	RDLB--- } ~ 100Ω RDLB--- } TOTAL
R108B	TEST	
C501	22μF-1500-35v	
C502	22μF-1500-35v	CTAT226
A201	A301 A401	μA741
A202	A302 A402	μA741
Q201	Q301 Q401	2N4351
Q202	Q302 Q402	2N4351
C201	Q401	CCEL104
C202	Q402	CCEL104
C203	Q403	CL05BX332M
IN SENSOR HEAD	{ RT201 RT301 RT401	75 Ω T2V18E5
	{ R202 R302 R402	75 Ω RDLB75.0
	{ R203 R303 R403	RDLB4701
	{ R204 R304 R404	4.7 K RAAC1002
	{ R205 R305 R405	10 K RAAC1002
	{ R206 R306 R406	100 K RAAC1003
	{ R207 R307 R407	10 K RAAC1002
	{ R208 R308 R408	10 K RAAC1002
	{ R209 R309 R409	10 K RAAC1002
	{ R210A R310A R410A	TEST RDLB---
	{ R210B R310B R410B	TEST RDLB---
	{ R210C R310C R410C	TEST RDLB---
	{ R211 R311 R411	100 K RAAC1003
	{ R212 R312 R412	100 K RAAC1003

UNLESS OTHERWISE SPECIFIED	APPROVED
DIMENSIONS ARE IN INCHES	18
REMOVE BURRS AND SHARP EDGES	
TOLERANCES ON FRACTIONS ±	
DECIMALS ±	
ANGLES ±	
DO NOT SCALE THIS DRAWING	
SLD-1555 SAM-63B-7	
NEXT ASSY	USED ON
APPLICATION	

UNLESS OTHERWISE SPECIFIED
DIMENSIONS ARE IN INCHES
REMOVE BURRS AND SHARP EDGES
TOLERANCES ON FRACTIONS ±
DECIMALS ±
ANGLES ±
DO NOT SCALE THIS DRAWING

MATERIAL: ELECTRICAL: 1/4W 5%
MECHANICAL: CHECKED
FINISH: DRAWN: FEB 4-72

SPECIFICATIONS OF LATEST ISSUE APPLY

CIR DIAGRAM
SAM-63B-7

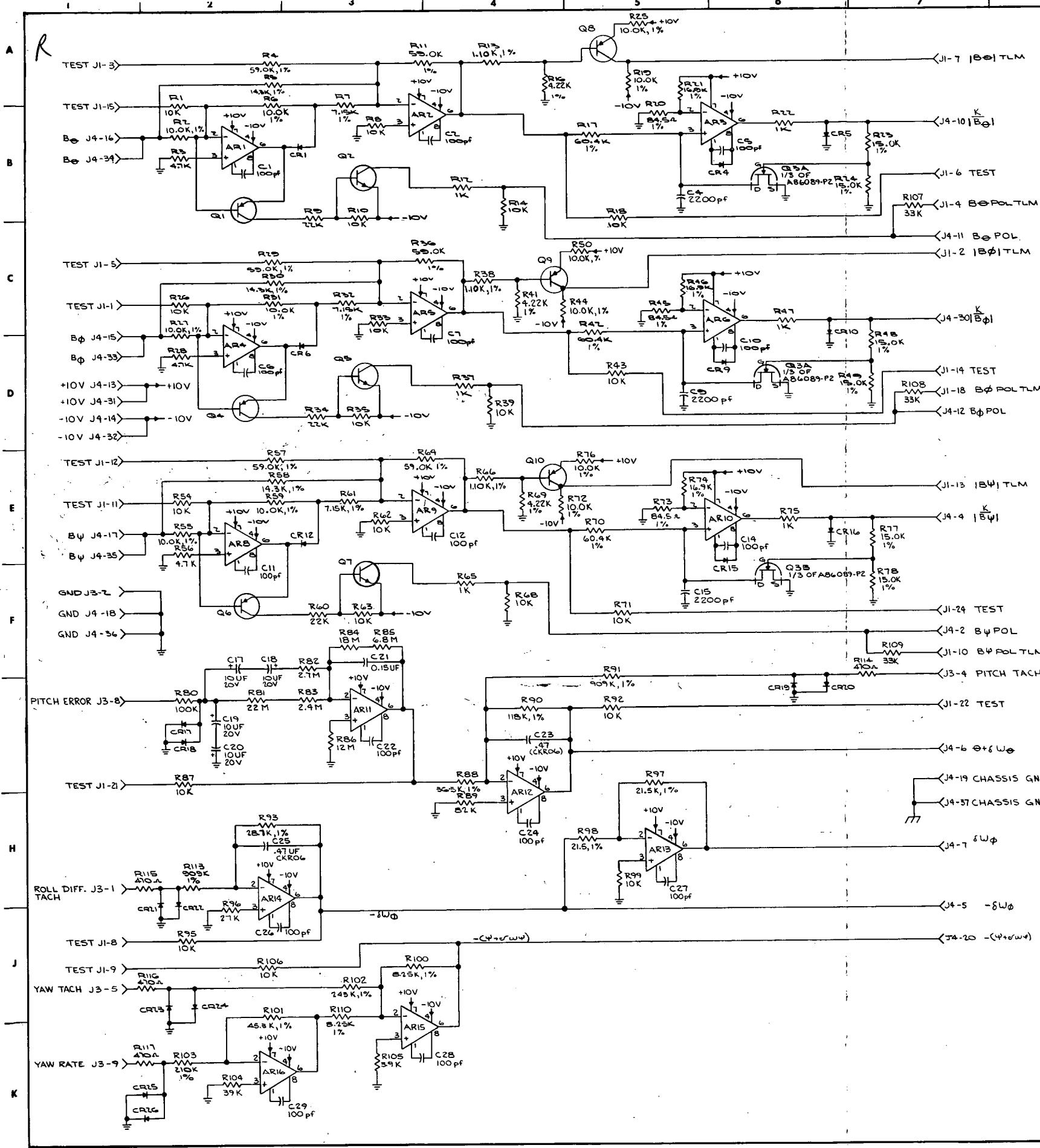
SCHONSTEDT
INSTRUMENT CO.
Reston, Virginia

SL CO. DRAWING NUMBER
301016

58-A FOLDOUT FRAME 1

58-B

58-C FOLDOUT FRAME 2

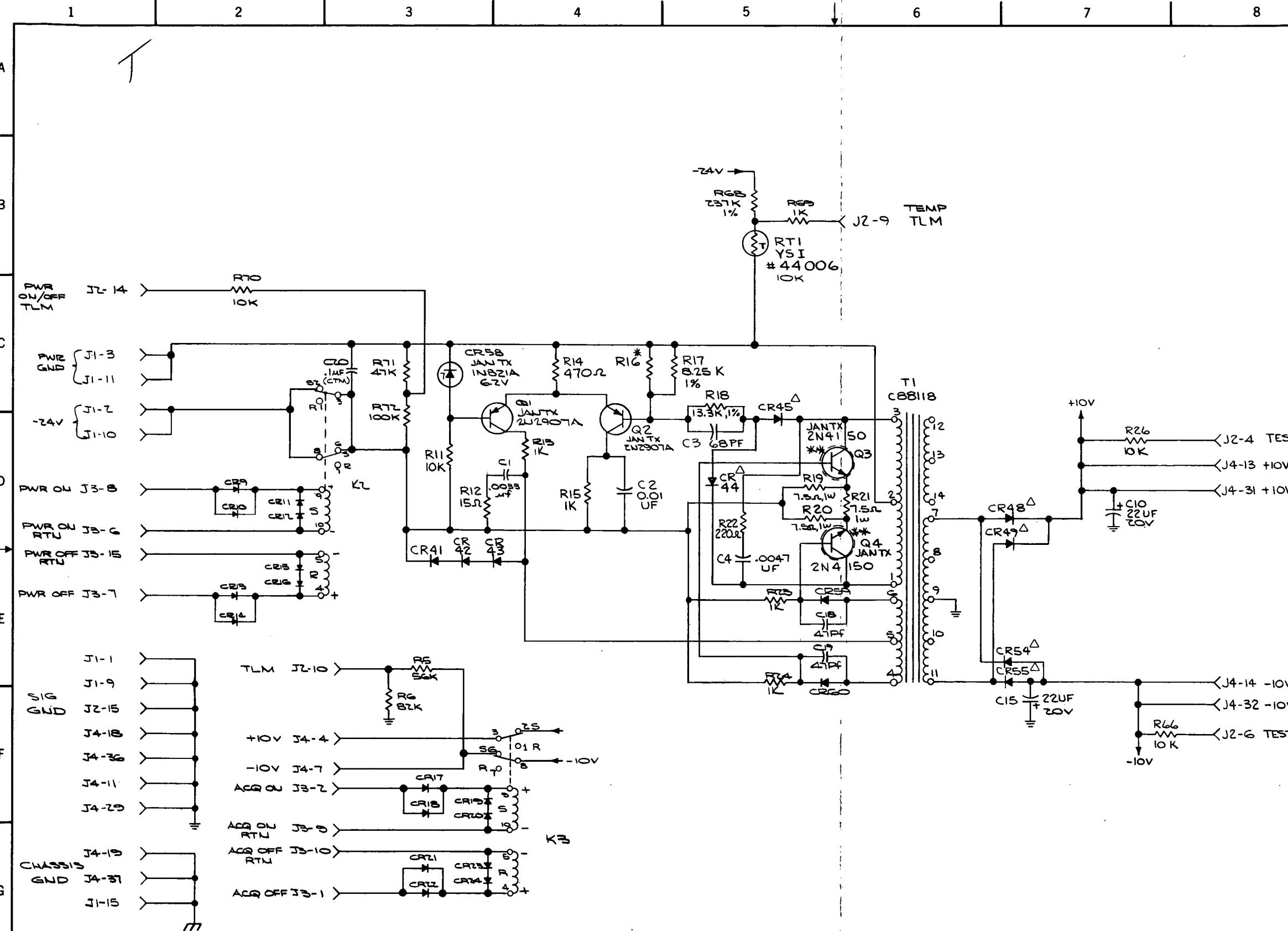


FOLDOUT FRAME / 59-A

59.

FOLDOUT FRAME

259-c



NOTES :

- UNLESS OTHERWISE SPECIFIED

 1. RESISTORS : ARE 1/4W, 5%, STYLE RCR07
1% UNITS ARE 1/10W, STYLE RNR55H
1W UNITS ARE 5% STYLE RCR32
* INDICATES TRIM RESISTOR, VALUE TO BE SELECTED AT TEST.
 2. CAPACITORS : POLARIZED UNITS ARE ELECTROLYTIC,
SPRAGUE TYPE 350D
: UNITS WITH VALUES IN PF ARE CERAMIC,
STYLE CKR05.
: OTHERS ARE MYLAR, GE TYPE 63P.
 3. DIODES : ARE JAN TX 1N4148
: △ INDICATES UNIRODE UTX-220
 4. CONNECTOR : J1, J2 & J3 ARE CANNON DMM-15PPNMBK56
: J4 IS CANNON DCM-37PPNMBK56
 5. ** INDICATES HEATSINK TO FRAME.

		ATL:	ELEM DIAS POWER SUPPLY				
		FIN:					
		SCALE:					
		UNLESS OTHERWISE SPECIFIED DIMENSIONS ARE IN INCHES TOLERANCES ON			DRAWN BY: L. AYERS		
PUB ASBY	D41115-1	MCA	FRACTIONS	DECIMALS	ANGLES	CODE IDENT. NO.	26502
REFERENCE DWG		USED ON				CHECKED BY: S.G. 9/72	
ITM-24M		APPLICATION	$\pm 1/64$ ± 0.010 $\pm 1/2^\circ$			APPROVAL: DFTG 6/9/72 ENG. V.H.S.	D 41115
						ISSUE DATE: June 9 1972	SHT 1 OF 1

FOLDOUT FRAME

60-A

60 -

FOLDOUT FRAME

60-c

1 **2** **3** **4** **5**

6 7 8 9 10

REVISIONS	D	41098	SHT 1 OF 2
SYM.	DESCRIPTION	DATE	APPROVAL

1

1

1

A rectangular stamp with a decorative border containing the text "Reproduced from best available copy." and a circular logo.

PIN	FUNCTION																
J1	PIN ASSIGNMENTS	J2	PIN ASSIGNMENTS	J3	PIN ASSIGNMENTS	J4	PIN ASSIGNMENTS	J5	PIN ASSIGNMENTS	J6	PIN ASSIGNMENTS	J7	PIN ASSIGNMENTS	J8	PIN ASSIGNMENTS	J9	PIN ASSIGNMENTS
10	BY POL TLM	20	SPARE	9	SPARE	9	YAW RATE	10	K1/B61	20	-4V+6WY	20	K1/B61	10	CHAS GND	20	SPARE
9	TEST	19	SPARE	8	SPARE	8	PITCH ERR	9	SPARE	19	CHAS GND	29	SPARE	9	CHAS GND	19	SPARE
8	B6 POL TLM	18	SPARE	7	SPARE	7	SPARE	8	SPARE	18	SIG GND	28	SPARE	8	SIG GND	18	SPARE
7	B6 TLM	17	SPARE	6	SPARE	6	SPARE	7	6W	17	3V	27	SPARE	7	CHAS GND	17	SPARE
6	TEST	16	SPARE	5	SPARE	5	YAW TACH	6	6W	16	B6	26	SPARE	6	6W	16	SPARE
5	TEST	15	TEST	25	MODE III TLM	6	TEST	5	YAW TACH	5	-6W	15	B6	25	3V	15	SPARE
4	B6 POL TLM	14	TEST	24	TEST	4	SPARE	4	PITCH TACH	4	K1/B41	14	-10V	24	3V	14	B6
3	TEST	13	BY4 TLM	23	TEST	3	SPARE	3	SPARE	3	SPARE	13	+10V	23	SPARE	13	B6
2	B6 TLM	12	TEST	22	TEST	2	SPARE	2	6G GND	2	BY POL	12	B6 POL	22	SPARE	2	-10V
1	TEST	11	TEST	21	TEST	1	SPARE	1	ROLL/PIT TACH	1	DISCRIM.	11	B6 POL	21	SPARE	11	+10V

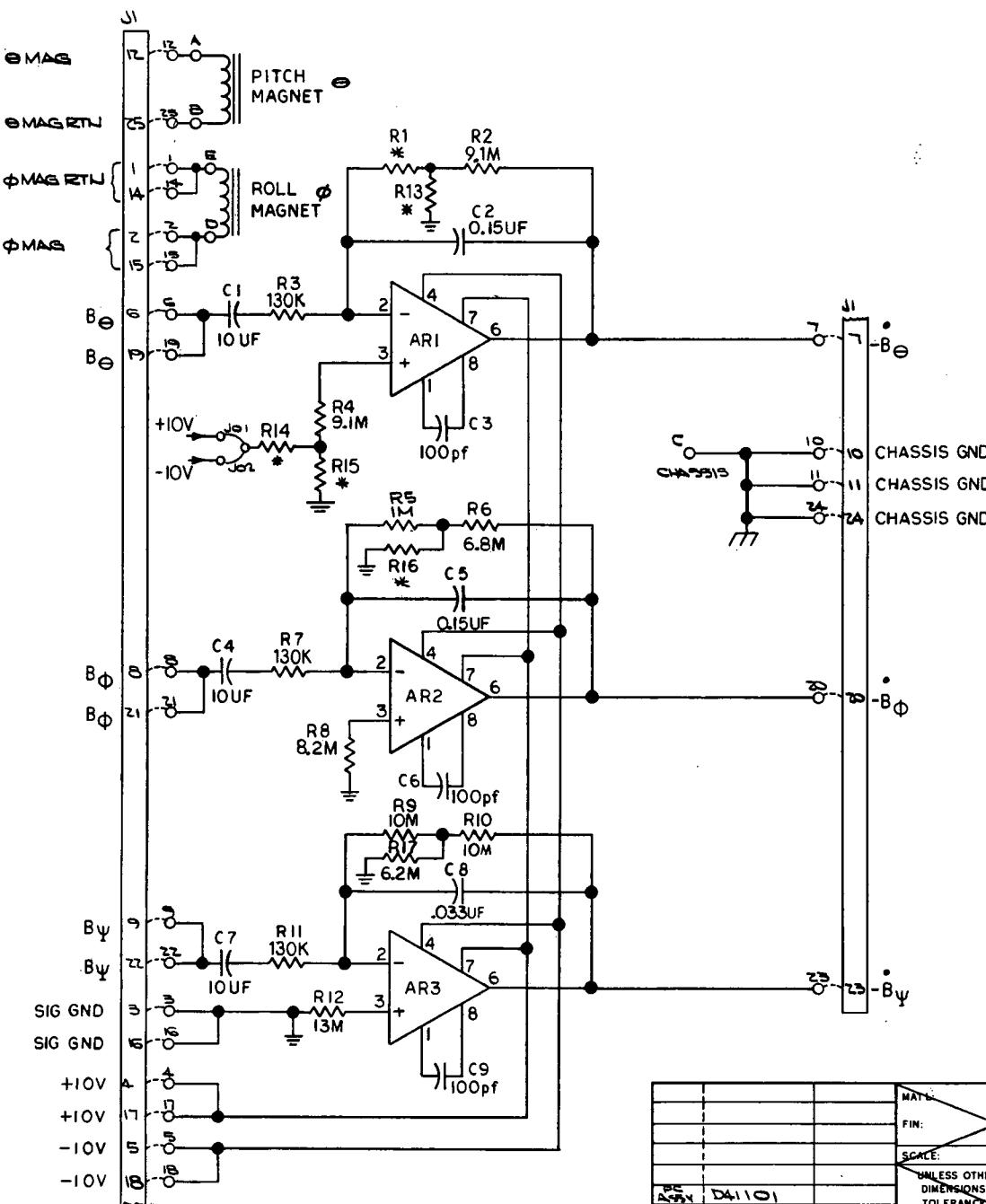
SEE SEPARATE PARTS LIST(S)

		MATERIAL FIN:	ASSY, PRINTED WIRING BD - CONTROL CARD			ITHACO, INC. ITHACA, N.Y.
		SCALE: 2/1	FMF: JOB# 10-7174			C-1
UNLESS OTHERWISE SPECIFIED DIMENSIONS ARE IN INCHES TOLERANCES ON			DRAWN BY: J. GOSART S-12-72	CODE IDENT. NO. 26502		
REFERENCE DWG USED ON			CHECKED BY: 6-14-72	APPROVAL: DFTG. S-13	ENG. Y-13	D 41098
1TH-24M	APPLICATION	FRACTIONS DECIMALS ANGLES	1/64 .010 ± 1/2"	ISSUE DATE: 2-7-72	SHT 1 OF 7	

1 2 3 4 5 6 7 8

REVISIONS		C 31514	SHT OF
ZONE	SYM.	DESCRIPTION	DATE APPROVAL
A	A	CHANGE PER SECN 1/2004 7-1-72	6/19/72
B	B	CHANGE PER SECN 1/2004 7-1-72	6/19/72
C	C	CHANGE PER SECN 1/2004 7-1-72	7-21-72
D	D	CHANGE PER SECN 1/2004 7-1-72	6/19/72
E	E	REV PER SECN 1/2004 7-1-72	6/19/72

X

**NOTES**

UNLESS OTHERWISE SPECIFIED:

1. RESISTOR ARE 1/4W, 5%, STYLE RCR07
* INDICATES TRIM RESISTOR, VALUE TO BE SELECTED AT TEST
 2. CAPACITORS:
VALUES IN μ F ARE CERAMIC, STYLE CKR05, OTHERS ARE MYLAR, GE TYPE 63F; C1, C4, C7 ARE ELECTROCUBE NO. 625BIB106J, POLYCARBONATE, $\pm 5\%$.
 3. OP AMP: ARE NATIONAL SEMICONDUCTOR LM108AH/883
 4. CAPACITORS:
VALUES IN μ F ARE CERAMIC, STYLE CKR05, OTHERS ARE MYLAR, GE TYPE 63F; C1, C4, C7 ARE ELECTROCUBE NO. 625BIB106J, POLYCARBONATE, $\pm 5\%$.
5. J0* INDICATES JUMPERS

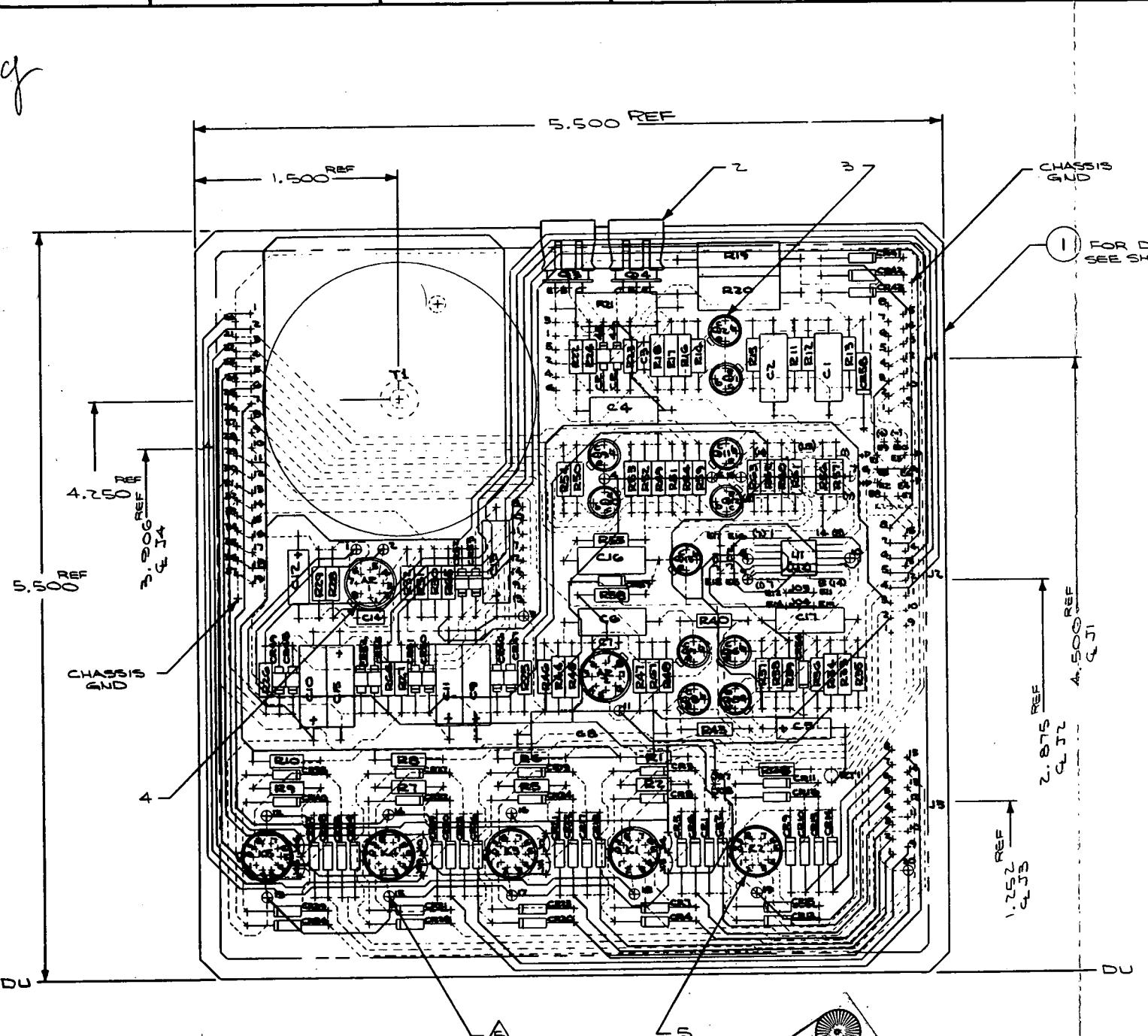
MATERIAL:	ELEM DIAGRAM	
FIN:	PITCH, ROLL - CARD	
SCALE:	FMF. JOB# 10-2724	
UNLESS OTHERWISE SPECIFIED DIMENSIONS ARE IN INCHES TOLERANCES ON FRACTIONS DECIMALS ANGLES		
REF. DWG: D41101	DRAWN BY: S. Clegg	5/8/72
REFERENCE DWG	USED ON	CODE IDENT. NO. 26502
CHECKED BY: B.C. 5-12-72		
APPROVAL: DFTG. ENG. 100% /		
ISSUE DATE: May 23, 1972		
SHT OF		C 31514

62-A FOLDOUT FRAME 1

62-B

FOLDOUT FRAME 2

62-C



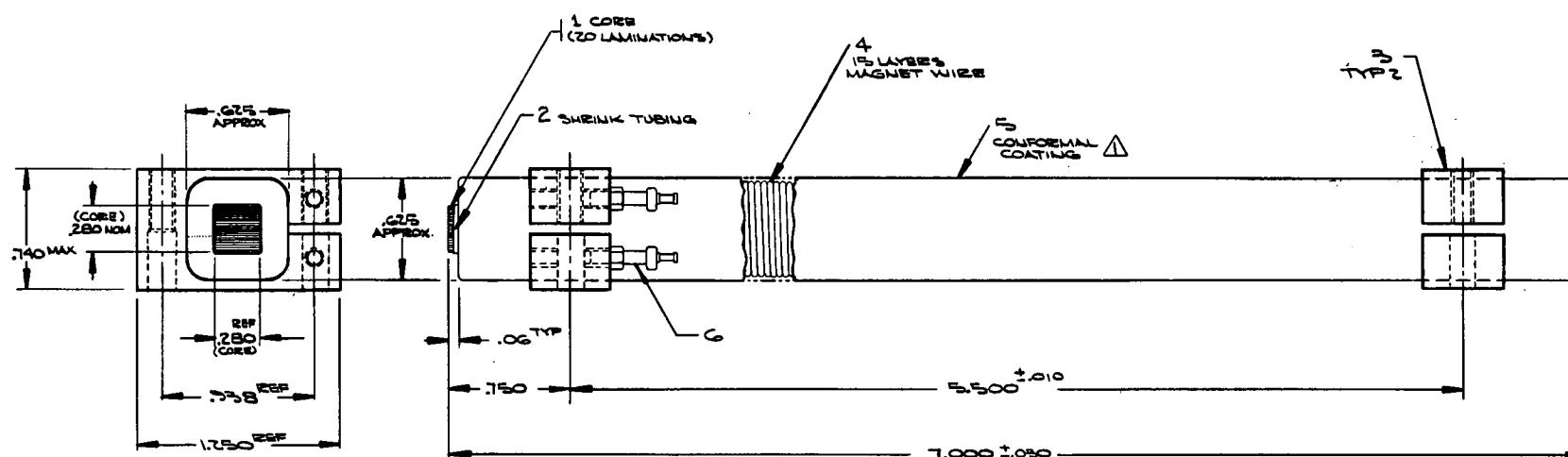
1 | 2 | 3 | 4 | 5 | 6 | 7 | 8

REVISIONS			C 131520
ZONE	SYM.	DESCRIPTION	SHT 1 OF 1
3C	A	REV PZB SEE N 13020 10-17-2000 R/S	DATE APPROVAL

三

A

-63-



NOTES:

- ASSEMBLE & CONFORMAL COAT PER MOPS 30.40**
2. ASSEMBLE ITEM 3 (MOUNTING BLOCKS) USING
FIXTURE J805B

G	Z	CAMBICON #2156-1	TERMINAL, INS.			
S	AZ	HYSOL PC-2Z	CONFORMAL COATING			
4	AZ	#50 HEAVY FORMBARE	MAGNET WIRE			
3	Z	B21993-PI	MOUNTING BLOCK			
2	AZ	RAYCHAM	SHRINK TUBING	KYNAR		
1	ZO	A11231-PI	LAMINATE			
ITEM NO.	QTY REQD.	CODE IDENT.	PART NO. OR IDENTIFYING NO.	DESCRIPTION	MATERIAL	SPECIFICATION

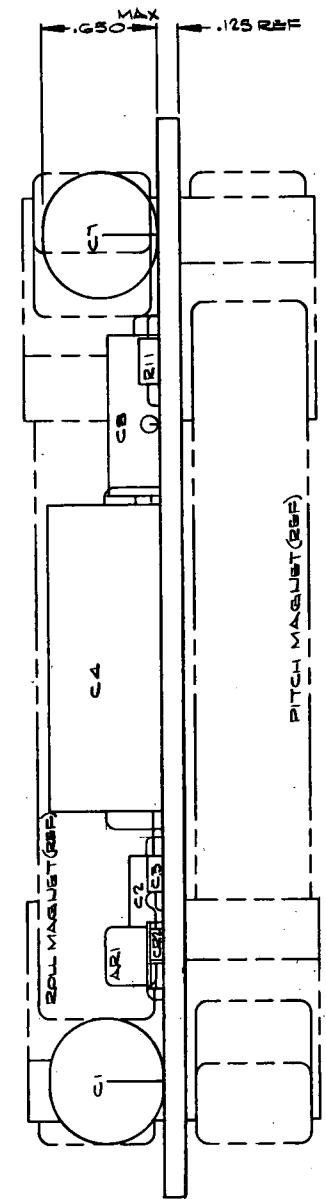
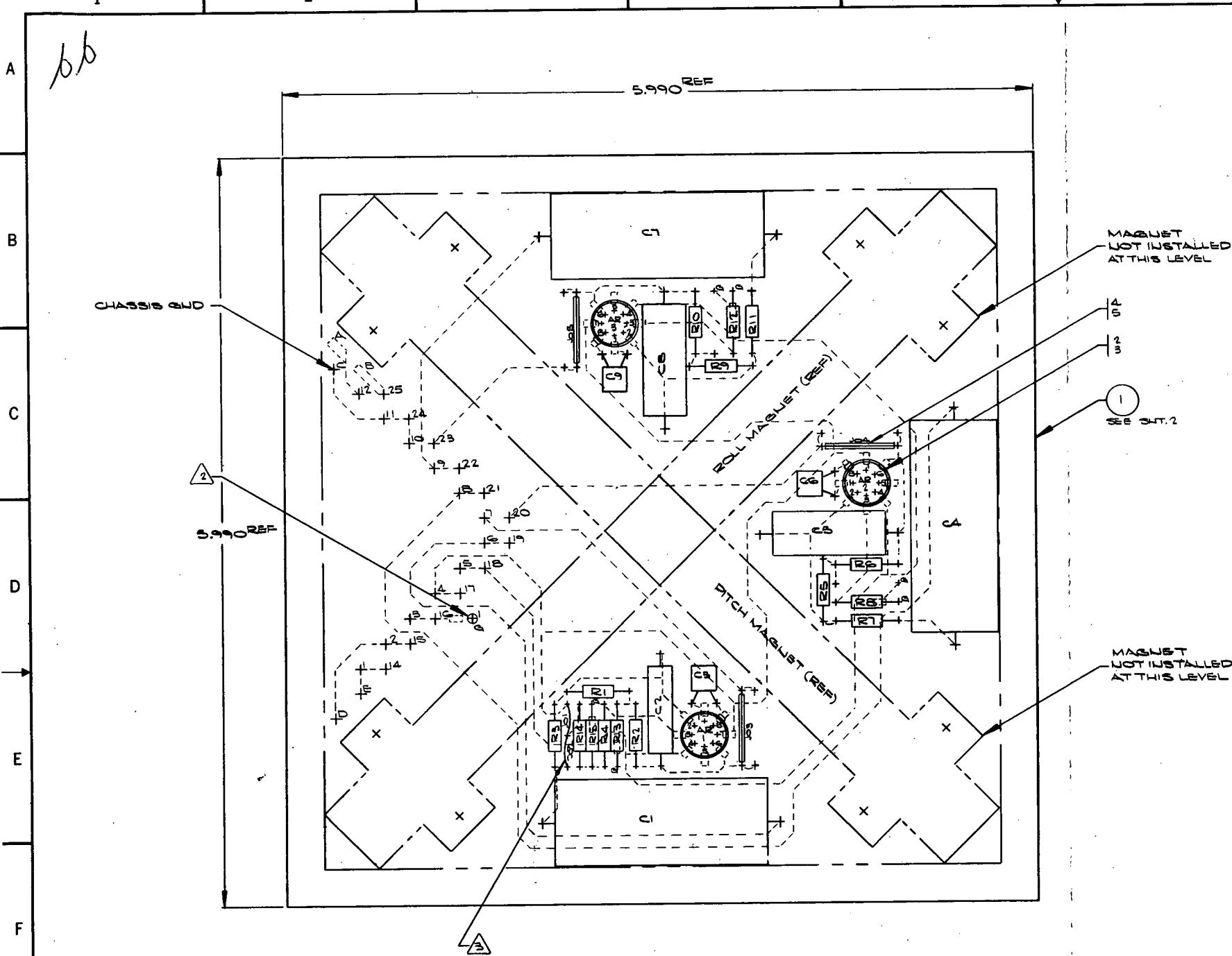
10

Q1		PARTS LIST				A1	
		MATERIAL FIN:	SEE NOTES AND PARTS LIST	ASSY		ITHACO, INC. ITHACA, N.Y.	
				7" MAGNET			
		SCALE: 2/1		FMF. JOB# 10-2724		CODE IDENT. NO. 26502	
ASSY	D41086	PLATE WIRE MAGNET	UNLESS OTHERWISE SPECIFIED	DRAWN BY: <i>John W. Dugay</i> JUN 15 1972			
ASSY	D41093	VANE MAGNET	DIMENSIONS ARE IN INCHES	CHECKED BY: <i>John W. Dugay</i> JUN 15 1972			
			TOLERANCES ON	APPROVAL DTG: <i>John W. Dugay</i> JUN 15 1972			
REFERENCE DWG		USED ON	FRACTIONS DECIMALS ANGLES	ENG. V.H.B.		C 31520	
APPLICATION				ISSUE DATE June 15, 1972		SHT 1	OF 1

64-A FOLDOUT FRAME /

64-B

FOLDOUT FRAME 2 64-C



REVISIONS			
D 4110			
ZONE	SYM.	DESCRIPTION	SHT OF 2
A	REV 4 RED. 55011300G 340G-65TL	DATE 7-6-72	VH3
B	REV PER 550113015 340H-65TL	DATE 7-21-72	VH3
C	REV PER 550113000 340H-65TL	DATE 9-4-72	VH3

CC

(G1) INACTIVE FOR NEW DESIGN
AFTER SEPT. 11, 1972 USE D41101-G1

NOTES:

1. ASSEMBLE PER MOPS 50.3
2. AT POINT 1 MAKE INTERFACIAL CONNECTION PER FIGURE 6 OF MOPS 50.5
3. FOR +10V TO R14 INSTALL J01 ONLY
FOR -10V TO R14 INSTALL J02 ONLY

9	B4	18	-10V	
8	B6	17	+10V	
7	-B6	16	SIG GND	25
6	B6	15	ΦMAS	24
5	-10V	14	ΦMAS RTN	23
4	+10V	13	SPARE	22
3	SIG GND	12	Φ MAS	21
2	ΦMAS	11	CHAS GND	20
1	ΦMAS RTN	10	CHAS GND	19
PIN FUNCTION				
J1 PIN ASSIGNMENTS				

SEE SEPARATE PARTS LIST

44-132 15369	A75
	P/R-1
	FIN:
	SCALE: 2/1
	FMP. JOB# 1027724
ASSY: D41086	DRAWN BY: J. GOSART G-22-72
ELEM: CB1514	CHECKED BY: _____
REFERENCE DWG. NO. ITH-24M	APPROVAL: DTG. J. LONG ENG. V.H.B.
USED ON APPLICATION	CODE IDENT. NO. 26502
FRACTIONS DECIMALS ANGLES	D 41101
± 1/64 = .016 = 1/2°	ISSUE DATE: JUNE 5, 1972
SHT 1 OF 2	