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# Several New Ultra-wideband Antenna Systems for Radio Telescopes and Industry Sensor Imaging Process

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**Abstract** – This paper presents an overview of several ultra-wideband (UWB) antenna systems recently developed at Chalmers for applications in future UWB radio telescopes and industry sensor imaging process.

## 1 INTRODUCTION

Due to its quite unique properties, ultra-wideband (UWB) technology finds many applications in different areas, such as UWB sensor network for precise ranging and geolocation, UWB radar and imaging systems with superior penetration and high resolution, and super sensitive UWB radio astronomy.

In the paper, we present an overview of several new UWB antenna systems developed at Antenna Group at Chalmers University of Technology, including the circular Eleven feed reflector antenna system [1] for future UWB radio telescopes, such as the square kilometer array (SKA) and very long baseline interferometer (VLBI2010), a UWB indoor radar system [2], and a UWB antenna sensor imaging system for industry product processing [3].

## 2 The circular Eleven feed for reflector antennas for radio telescopes

Figure 1 shows the modeling and prototype of the new developed circular Eleven feed. It is known that only  $n=1$  component (referred to as BOR<sub>1</sub> component) in the Fourier series of the far-field function of a feed contributes to the directivity of the reflector antenna, while all other  $n \neq 1$  components cause sidelobes. Therefore, a high BOR<sub>1</sub> efficiency (the power in BOR<sub>1</sub> component relative to the total radiated power) is critical for achieving a high aperture efficiency and low sidelobes in feed design.

One way for a feed to achieve a high BOR<sub>1</sub> efficiency is to make its geometry more rotationally symmetrical. Figure 2 shows the aperture efficiency and its sub-efficiencies of the circular Eleven feed when it illuminates a reflector with a subtended angle of  $2 \times 60^\circ$ , based on the simulated and the measured

radiation function. Very good agreement between the simulation and the measurement is observed. The aperture efficiency is higher than 60% over 1–10 GHz and 50% up to 14 GHz, which is a significant improvement, especially below 2.2 GHz and above 13 GHz, compared to the previous 2–13GHz Eleven feed consisting of straight folded dipoles in [4]. The simulated and measured reflection coefficient is shown in Figure 3.

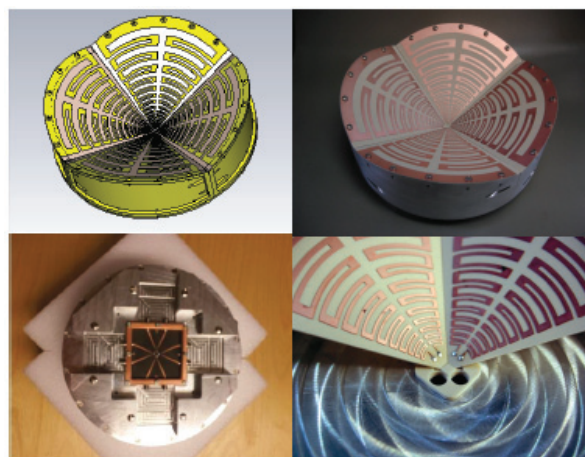


Figure 1: The circular Eleven antenna with dual linear polarization, with the diameter and the height of 210 mm and 65 mm, respectively: (left-up) simulation model; (right-up) proto-type; (left-down) center puck on rear side; (right-down) detailed center puck on front side.

We have investigated the effect of the cryostat used in our VLBI2010 project on the radiation performance by CST simulation. The simulation model and the calculated aperture efficiency are shown in Figure 4. Compared to the aperture efficiency without the cryostat in Figure 2, we can see that the cryostat helps to improve the spillover efficiency at the low frequencies, and has no effect on the performance at high frequencies.

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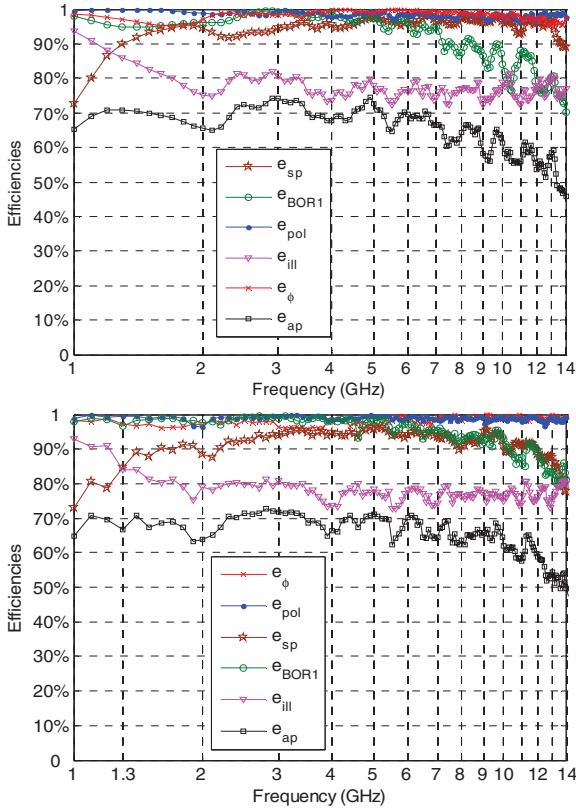


Figure 2: Calculated aperture efficiency and its sub-efficiencies when the circular feed illuminates a paraboloid with a subtended angle of  $2 \times 60^\circ$ , based on (up) simulated and (down) measured radiation function.

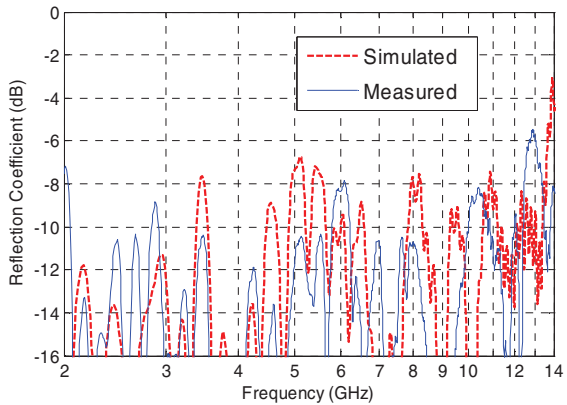


Figure 3: Simulated and measured reflection coefficient of the circular Eleven feed.

### 3 A Compact UWB Indoor Radar System

UWB radar systems exhibit several distinct advantages over the narrowband counterparts: 1) higher ranging resolution with higher penetration ability through lossy materials simultaneously; 2) enhanced target recognition; 3) better penetration ability to passive interference (i.e., rain, fog, clutter); 4) very low cost.

A new compact and low-cost UWB radar system for ranging and tracking of moving objects in indoor and

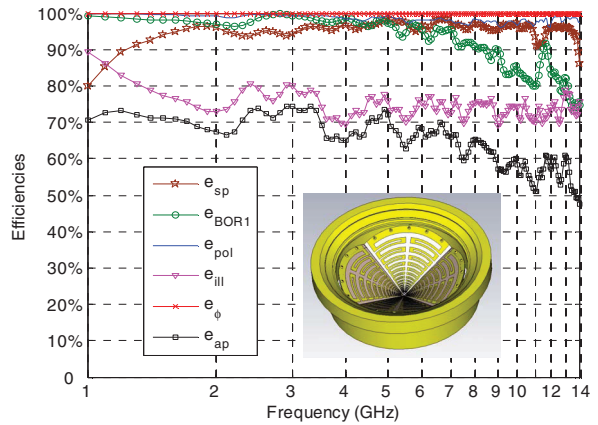


Figure 4: Calculated aperture efficiency and its sub-efficiencies when the circular feed located inside the cryostat illuminates a paraboloid with a subtended angle of  $2 \times 60^\circ$ , based on simulated radiation function.

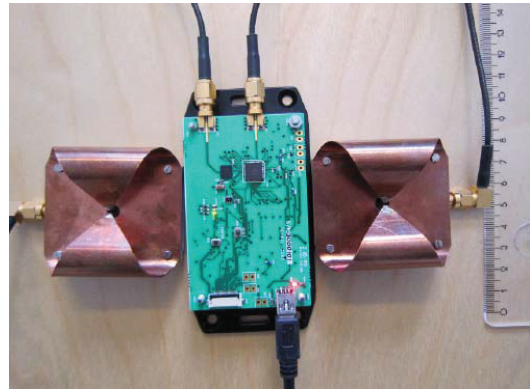


Figure 5: The compact UWB radar system for indoor and through-wall ranging and tracking.

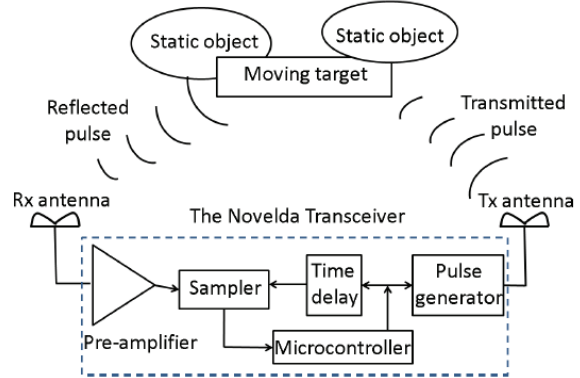


Figure 6: Operating principle of the compact UWB radar system

through-wall environments has been developed, see Figure 5. The UWB radar consists of a commercially available Novelda R2A UWB CMOS chip transceiver operating over 2–8 GHz and the recently developed UWB 2–15-GHz self-grounded Bow-Tie antennas [5]. Pulses are transmitted via one antenna (Tx antenna),

reflected by targets, and then received by the second antenna (Rx antenna), as depicted in Figure 6.

The measured time-domain response of the UWB radar system is shown in Figure 7, when the two antennas are separated by a distance of 250 mm in the face-to-face configuration in an anechoic chamber. From the figure, two time-response measures, the width of the pulse full-width at half-maximum (FWHM)  $\tau_{FWHM}$  and the duration of the ringing  $\tau_{r=0.22}$ , can be obtained as  $\tau_{FWHM} = 134\text{ps}$  and  $\tau_{r=0.22} = 260\text{ps}$ , which states a fast time pulse response of the radar system. Please refer to [6] for the definitions of  $\tau_{FWHM}$  and  $\tau_{r=0.22}$ .

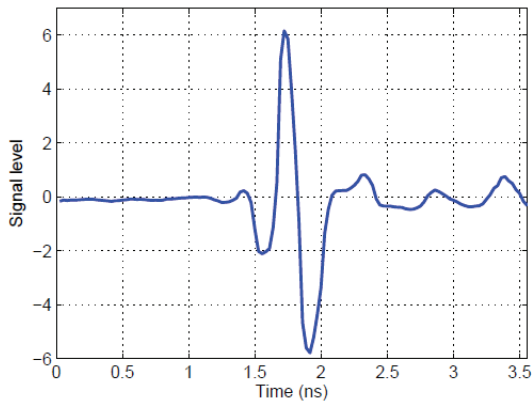


Figure 7: Measured time-domain impulse response of the UWB radar system when the two antennas are separated by 250 mm in face-to-face configuration.

Algorithm	Without clutter map removal	With clutter map removal
<i>Pulse signature matching</i>	75.4 (mm)	48.1 (mm)
<i>Pulse-spectrum signature matching</i>	7.2 (mm)	2.6 (mm)
<i>Pulse-spectrum signature matching + subsample delay estimation</i>	5.0 (mm)	1.4 (mm)

Table 1: Comparison of the ranging techniques in terms of RMSE between the real and estimated positions.

A robust and accurate algorithm for ranging and tracking, the pulse-spectrum signature matching plus subsample delay estimation, have been developed [2]. The ranging function of the radar system is evaluated by the measurements of a metal ball with a diameter of 20 mm moving in an indoor environment. Table 1 shows the ranging accuracy for this case by different algorithms. It can be seen that the ranging accuracy achieves to 1–2 mm. Figure 8 illustrates the tracking performance of the radar system, where the red dot in Matlab program screen follows the movement of the target very well.

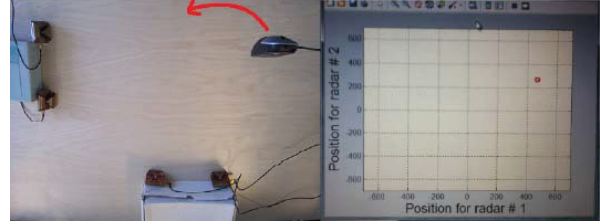


Figure 8: An orthogonal measurement setup for two dimensional tracking (left), and the graphical user interface implemented in Matlab (right), where the red dot indicates the location of the target.

### 3 Imaging of Near-Field Object Using UWB SAR Algorithm

UWB technology and its use in imaging and sensing have drawn significant interest in the last two decades. Extensive studies have contributed to utilizing UWB transient scattering for automated target recognition and imaging purposes [7], [8], where a UWB synthetic aperture radar (SAR) imaging algorithm was presented and applied for subsurface object imaging. One limitation of the algorithm is that an artefact in the imaging procedure causes ambiguity. Here, a simple modified procedure is proposed to reduce such artefact. The feasibility of the proposed algorithm is presented and verified using experimental data.

The UWB imaging system for objects in near-field region is shown in Figure 9. It consists of a self-grounded Bow-Tie antenna located in front of the object, a vertically placed rectangular metal plate. To obtain multiple views, the metal plate is placed in 68 equal-spaced positions along a straight line of 1088 mm long, and the monostatic responses at each of these 68 positions are measured using a network vector analyzer (VNA) from 0.5 GHz to 13 GHz. The above setup is equivalent to the case that a single antenna moves along a straight line in front of the static object, and transmits and receives the monostatic responses at these 68 positions, as shown in Figure 10. Therefore, the SAR algorithm can be employed to have an imaging of the object.

The image is reconstructed by the simple SAR, shown in Figure 11(up). The vertically-placed metal plate is observed but it comes with a “smile” shape around it. This smiling is an undesirable artefact introduced from the algorithm. To remove this artefact, we use the same antenna moving in the other side of the object, say behind the object. The same measurement and image reconstruction procedures are repeated. The resultant image is shown in Figure 11 (down). It is observed that the “smile” is changed to a “crying” in the image. By a correlation of these two images - each pixel intensities of the two images are multiplied by each other, the “smile” and the “crying” are canceled while the object image remains. The resultant image is shown in Figure 12



and it is clear that the artefact has been significantly suppressed.

### 3 Conclusions

An overview of several UWB antenna systems is presented to show the applications of new developed UWB systems in different areas.

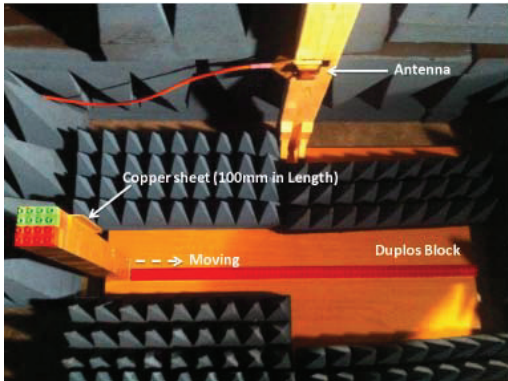


Figure 9: The test UWB imaging system

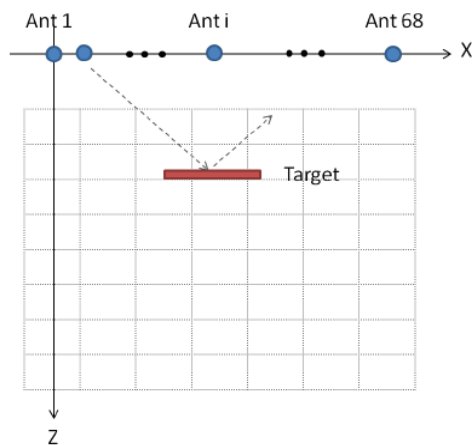


Figure 10: The geometry of the SAR configuration

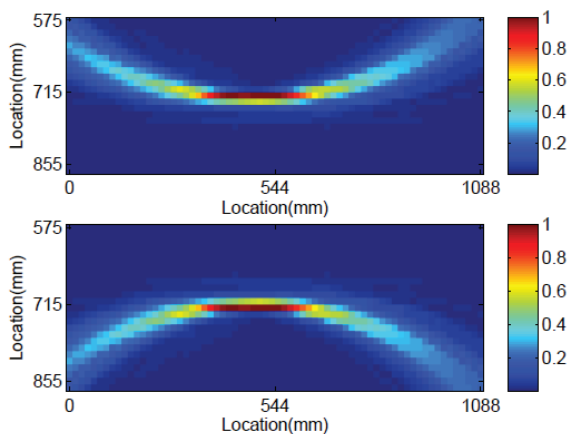


Figure 11: Image reconstruction results based on: (a) front antenna (up); (b) back antenna (down).

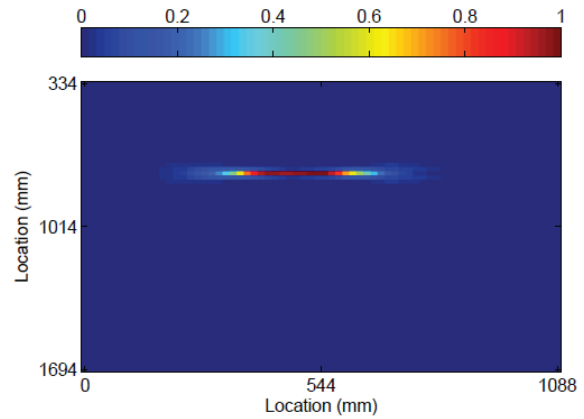


Figure 12: The resultant image after modified algorithm.

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