Working Paper

A New Ridge Regression Causality Test in the Presence of Multicollinearity

by

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Abstract

This paper analyzes and compares the properties of the most commonly applied versions of the Granger causality (GC) test to a new ridge regression GC test (RRGC), in the presence of multicollinearity. The investigation has been carried out using Monte Carlo simulations. A large number of models have been investigated where the number of observations, strength of collinearity, and data generating processes have been varied. For each model we have performed 10000 replications and studied seven different versions of the test. The main conclusion from our study is that the traditional OLS version of the GC test over-rejects the true null hypothesis when there are relatively high (but empirically common levels of) multicollinearity, while it is established that the new RRGC test will remedy or substantially decrease this problem.

Keywords: Granger causality test, multicollinearity, ridge parameters, size and power.

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1. Introduction

The purpose of this paper is to evaluate the effect of multicollinearity on the most commonly applied tests for causality in the sense of Granger (1969). The dynamic nature of the Granger causality (GC) test implies that it, by pure definition, generally suffers from considerably high degrees of multicollinearity problems, primarily induced by its extensive lag structure. By means of Monte-Carlo simulations, it is demonstrated that multicollinearity causes over-rejections of the true null hypotheses for the traditional GC tests. As a remedy to this problem, a new ridge regression Granger causality (RRGC) test is proposed where ridge regression is used instead of ordinary least squares (OLS) to estimate the parameters in the dynamic regression model. In comparison to the traditional versions of the GC test, our newly proposed RRGC test exhibits superior size properties, which therefore may be considered as the main original contribution of this paper.

The concept of multicollinearity was first introduced by Frisch (1934) in order to denote a situation where the independent variables in the regression model are correlated. Despite the fact that high levels of multicollinearity is a very common problem when estimating dynamic models, no one (at least to the author's knowledge) has yet studied the effects of multicollinearity on the GC test. The main problem associated to multicollinearity is that it leads to instability and large variance of the OLS estimator. This may induce two different effects on the GC test which is also illustrated in the simulation section of this paper. Firstly, it might lead to a slower convergence rate of the tests based on asymptotic results since larger samples are required to obtain stable OLS estimates of the parameters. Secondly, it may cause over-rejections of the true null hypotheses in small and moderately sized samples regardless whether the tests are based on asymptotic distribution or not. Hence, if we apply the traditional GC tests in the presence of multicollinearity we need to obtain very large sample sizes, which often is not available in many areas of economics.

The method of ridge regression first introduced by Hoerl and Kennard, (1970a,b) is nowadays established as an effective and efficient remedial method to deal with the general problems caused by multicollinearity. The main advantage of the ridge regression method is to reduce the variance term of the slope parameters which is demonstrated in some recent papers (see Kibria, 2003; Khalaf and Shukur, 2005; Alkhamisi and Shukur, 2007 and Muniz and Kibria 2009). In view of the fact that the simulation results in this paper identified that multicollinearity causes severe problems for the traditional GC tests (for empirically relevant sample sizes) a new RRGC test is proposed. This method reduces the parameter instability and the new versions of the test exhibit superior statistical size properties in comparison to the commonly applied GC tests.

The paper is organized as follows: In section 2, we describe the GC test and define the generalized ridge regression estimator. Subsequently, in section 3, the Monte Carlo design is formalized, while in Section 4 we analyze the results obtained from the simulation study. Finally, in Section 5 the conclusions of the paper are summarized.

2. Methodology

This section describes the testing and estimation methodology.

2.1 Granger causality test

The central idea that is exploited by the GC test is the simple fact that events in the past can cause events to happen today while future events cannot, thus, we utilize the fundamental truth that cause must precedes effect. The GC test for two variables y_t and x_t can be defined as follows. x_t does not Granger cause y_t , if and only if, prediction of y_t based on the universe U of predictors is no better than prediction based on U–{ x_t }, i.e. on the universe with x_t omitted. According to Granger and Newbold (1986) one can test for Granger causality by evaluating a zero restriction in each of the single linear equations in the VAR-model. This basic method is a very common method of testing for Granger causality in empirical works (see e.g. Almasri and Shukur, (2003); and Ramsey and Lampart, 1998) and can be explained by considering the following linear regression model:

$$\mathbf{y} = \mathbf{X}\boldsymbol{\beta} + \mathbf{u}\,,\tag{1}$$

where **y** is a $T \times 1$ vector of observations, **X** is a $T \times 2p+1$ matrix of observations of the independent variables, **\beta** is a $2p+1 \times 1$ vector of coefficients, *p* is the number of the lagged variables in the VAR(p) model and **u** is a $T \times 1$ vector of residuals. The coefficient vector in expression (1) can be estimated using ordinary least squares (OLS):

$$\hat{\boldsymbol{\beta}} = \mathbf{X}'\mathbf{X}^{-1} \mathbf{X}'\mathbf{y} . \tag{2}$$

In order to test for Granger causality the following linear restrictions should be tested:

$$H_0: \mathbf{R}\boldsymbol{\beta} = \mathbf{r} \quad \text{vs.} \quad H_1: \mathbf{R}\boldsymbol{\beta} \neq \mathbf{r} \,. \tag{3}$$

where **R** is a fixed $q \times 2p+1$ matrix and **r** is a fixed $q \times 1$ vector of restrictions. To test the restrictions of expression (3) the following Wald (W), Likelihood Ratio (LR), Lagrange Multiplier (LM) and the F-test will be used:

$$W = \frac{T \ \mathbf{R}\hat{\boldsymbol{\beta}} - \mathbf{r}' \ \mathbf{R}\mathbf{X'}\mathbf{X}\mathbf{R'}^{-1} \ \mathbf{R}\hat{\boldsymbol{\beta}} - \mathbf{r}}{s_u}$$
(4)

$$LR = T\left(\log\left(\frac{W}{T} + 1\right)\right) \tag{5}$$

$$LM = \frac{T \ \mathbf{R}\hat{\boldsymbol{\beta}} \cdot \mathbf{r} \ \mathbf{R}\mathbf{X}'\mathbf{X}\mathbf{R'}^{-1} \ \mathbf{R}\hat{\boldsymbol{\beta}} \cdot \mathbf{r}}{s_r}$$
(6)

$$F = \frac{\Delta \mathbf{R}\hat{\boldsymbol{\beta}} - \mathbf{r} \mathbf{R} \mathbf{X}' \mathbf{X} \mathbf{R}'^{-1} \mathbf{R}\hat{\boldsymbol{\beta}} - \mathbf{r}}{qs_u}$$
(7)

where $s_u = \hat{\mathbf{u}}'_u \hat{\mathbf{u}}_u$ and $s_r = \hat{\mathbf{u}}'_r \hat{\mathbf{u}}_r$ are the matrices of cross-products of residuals from the *unrestricted* regression and *restricted* regression (when H_0 is imposed), respectively. The first three tests are all asymptotically $\chi^2 q$ distributed while the fourth test is distributed as an $F q, \Delta$, where $\Delta = T - 2p - 1$. Moreover, a small sample correction of the W, LR and LM (WC, LRC and LMC) tests is made to the first three tests where T is replaced by Δ .

2.2 Ridge regression

The effect of multicollinearity between the explanatory variables is that the matrix of crossproducts $\mathbf{X'X}$ is ill-conditioned which leads to instability and large variance of the OLS estimates. If this instability is not reflected by an increase in the covariance matrix then the traditional GC tests is biased. As a substitute and a remedy to the multicollinearity problems induced by the OLS estimator, Hoerl and Kennard (1970a,b) proposed the following ridge regression estimator.

$$\hat{\boldsymbol{\beta}} = \mathbf{X}'\mathbf{X} + k\mathbf{I}^{-1} \mathbf{X}'\mathbf{y} , \qquad (8)$$

where $(k \ge 0)$ is the so called ridge parameter. In order to estimate k, Hoerl and Kennard (1970a) suggested the following expression:

$$\hat{k}_{HK} = \frac{S^2}{\hat{\alpha}_{\max}^2},$$

where $S^2 = \mathbf{y} - \mathbf{X}\hat{\boldsymbol{\beta}} + \mathbf{y} - \mathbf{X}\hat{\boldsymbol{\beta}} + n - 2p - 1$ and $\hat{\alpha}_{max}^2$ is defined as the maximum element of $\gamma\hat{\boldsymbol{\beta}}$ where γ is the eigenvector of $\mathbf{X'X}$. However, in Alkhamisi and Shukur (2007) it is illustrated that there are many other superior ways of estimating *k*. The authors found that the following two ridge estimators work particularly well:

$$\hat{k}_{ARITHM} = \frac{1}{p} \sum_{i=1}^{p} \left(\frac{S^2}{\hat{\alpha}_i^2} + \frac{1}{t_i} \right) \text{ and } \hat{k}_{NAS} = \max\left(\frac{S^2}{\hat{\alpha}_i^2} + \frac{1}{t_i} \right),$$

where $\hat{\alpha}_{max}^2$ is defined as the *i*th element of $\gamma \hat{\beta}$. Other alternative potentially successful ridge regression estimators are proposed by Kibria and Muniz (2009):

$$\hat{k}_{KM4} = \left(\prod_{i=1}^{p} \frac{1}{\sqrt{\frac{s^2}{\hat{\alpha}_{\max}^2}}}\right)^{\frac{1}{p}}, \ \hat{k}_{KM5} = \left(\prod_{i=1}^{p} \sqrt{\frac{s^2}{\hat{\alpha}_{\max}^2}}\right)^{\frac{1}{p}} \text{ and } \hat{k}_{KM6} = median\left(\frac{1}{\sqrt{\frac{s^2}{\hat{\alpha}_{\max}^2}}}\right)^{\frac{1}{p}}$$

Now, the new RRGC test will be applied using the RR estimators instead of the OLS estimator of β .

3. The Monte-Carlo simulation

3.1 The design of the experiment for size calculations

The data used for the Monte Carlo simulation experiment are replicated according to the following data generating processes when the lag length equals two:

$$\begin{cases} y_t = 0.03 + 0.1y_{t-1} + 0.08y_{t-2} + \beta_1 x_{t-1} + \dots + \beta_p x_{t-p} + \varepsilon_{1t} \\ x_t = 0.02 + \lambda x_{t-1} + \varepsilon_{2t} \end{cases}$$

and the following when the lag length equals four:

$$\begin{cases} y_t = 0.03 + 0.1y_{t-1} + 0.08y_{t-2} + 0.06y_{t-3} + 0.04y_{t-4} + \beta_1 x_{t-1} + \dots + \beta_p x_{t-p} + \varepsilon_{1t} \\ x_t = 0.02 + \lambda x_{t-1} + \varepsilon_{2t} \end{cases}$$

The focus of this paper is to study the effect of the degree of multicollinearity between lags of the x variables of the GC test. As a first step, in order to evaluate whether the degree of multicollinearity has a direct impact on the statistical size of the GC test, and to test whether ridge regression is a remedy to this potential problem, we use the following DGPs:

DGP 1:
$$\lambda = 0$$
 DGP 2: $\lambda = 0.8$

DGP 3:
$$\lambda = 0.95$$
 DGP 4: $\lambda = 0.99$

It should be stressed that the parameter values are empirically very likely cases in real-world economics and they are encountered in many studies (e.g. Almasri and Shukur (2003) and Hacker et al. (2010)). Another factor that may have an impact on the GC test is the distribution of the error term. In previous research, this is illustrated by for instance Kibria (2003) and Alkhamisi and Shukur (2007) who demonstrated that increase in the variance of a normally distributed error term will enlarge the problem of multicollinearity. The sample size is another relevant factor that is expected to affect the performance of the GC test since the Wald, LR and LM tests are based on an asymptotic distribution that often leads to poor properties in empirically relevant sample sizes. Another important factor in this context is the lag-length specification. It can be expected that estimating more parameters leads to a higher probability of rejecting a true null hypothesis. To demonstrate the effects of increasing the lag lengths we vary the degrees of freedom (net observations after each regression) instead of the numbers of observations since it is well-known that it is the degrees of freedom and not the absolute sample size that matters on the performance of the tests. In Table 1, the fixed and varying factors that constitute the actual Monte Carlo experiment are summarized.

| Factor | Symbol | Design |
|------------------------------------|---------|-----------------|
| Number of replicates | Ν | 10 000 |
| Degrees of freedom | df | 15, 25, 50, 100 |
| Nominal size | π_0 | 5% |
| Lag length | p | 2, 4 |
| The distribution of the error term | ε | N 0,1 , N 0,10 |

Table 1. Values of factors in the experiment

The size of the Granger causality test is examined by observing the rejection frequency when x does not Granger cause y. Therefore, the β parameters of the linear regression models are set to zero when the statistical sizes of the tests are evaluated. In order to evaluate the empirical statistical size of the tests the following confidence interval is calculated:

$$\pi_0 \pm 2\sqrt{\frac{\pi_0 \ 1 - \pi_0}{N}} \,. \tag{9}$$

If, based on our simulation experiment, the actual statistical size is within the bounds of this interval the evaluated test is considered as unbiased (at a specified significance level). Throughout this paper we consistently defines biasedness at the 5% level of significance.

3.2 The design of the experiment to calculate the power

When the power is calculated the β parameters in the linear regression models should not equal zero since the time series x_t should actually Granger cause y_t . The number of replicates when calculating the power of the tests equals 1,000 and the chosen parameter values of β are defined in following Table 2:

Table 2: Values of parameter combinations for the power calculation

| | β_1 | β_2 | β_3 | β_4 |
|------------------------|-----------|-----------|-----------|-----------|
| p = 2 | | | | |
| 1. very weak causality | 0.1 | 0.05 | - | - |
| 2. weak causality | 0.2 | 0.1 | - | - |
| 3. strong causality | 0.3 | 0.15 | - | - |
| p = 4 | | | | |
| 1. very weak causality | 0.1 | 0.05 | 0.025 | 0.025 |
| 2. weak causality | 0.15 | 0.1 | 0.05 | 0.025 |
| 3. strong causality | 0.25 | 0.15 | 0.075 | 0.05 |

4. **Results**

In this section the results from the Monte Carlo experiment are presented. All the factors that are varied in the design of the Monte Carlo simulation are expected to have an impact on the performance of the tests. We will especially focus on discussing whether ridge regression can serve as a small-sample correction of the tests based on asymptotic results and to determine whether the new RRGC test is robust to multicollinearity.

The simulation study indicates that applying the RRGC test using the \hat{k}_{ARITHM} , \hat{k}_{NAS} and \hat{k}_{KMS} as ridge estimator leads to an immense underestimation of the nominal size. Since it is of no use to present several tables consisting of almost only zeros the result from the statistical size calculation from these estimators are excluded from this paper. Furthermore, none of the traditionally applied GC tests and most of the tests when using ridge regression performs well when the data are collinear. The results from these tests are therefore only presented when analyzing the statistical size of the tests. When we calculate the tests's statistical power, only the F-test when using \hat{k}_{KM6} will be presented since the other tests have extensively biased sizes. Finally there is no effect on the statistical size when the error term follows a standard normal distribution. However, full results are available from the authors upon request.

4.1 Analysis of the statistical size of the Granger causality test

This section presents the actual sizes of the different Granger causality tests for the different DGPs. The actual sizes of the tests are presented in tables 3-6. The confidence interval in equation (9) is doubled in magnitude in order to emphasize the pattern of well-performing tests more clearly. Therefore, if the actual size of a test exhibits a rejection frequency between 0.0413 and 0.0587 it is considered as unbiased, which is marked out as shaded cells in the following tables.

The multicollinearity effect

The effect of increasing the degree of multicollinearity in the linear regression model is that the actual size of the tests also increases. For example in Table 3 when using the OLS estimation method then the F-test is has unbiased size in the absence of multicollinearity (DGP 1). However, for the other DGPs the F-test tends to over-reject the null hypotheses. The other tests that are based on asymptotic distributions are often biased even for DGP 1 and this bias increases by the degree of multicollinearity. This increase in bias leads to a slower convergence rate towards the nominal size. For example, the LM test is unbiased for DGP 1 when the sample size equals 50 but when we include multicollinearity in the model the test is not unbiased even when the degrees of freedom increase to 100. Thus, when the data is collinear we need to have very large sample sizes in order to obtain unbiased test statistics if we want to use the OLS to estimate the model. This is true not only for the tests based on asymptotic distributions but also for the F-test. On the other hand, when ridge regression method is applied the effects of increasing the multicollinearity decreases, especially for \hat{k}_{KM4} and \hat{k}_{KM6} . For these estimators the bias of the tests based on asymptotic distributions actually decreases as the degree of multicollinearity increases. However, these tests are still severely biased and should, therefore, not be used. Instead, when the explanatory variables are highly correlated we recommend the F-test based on \hat{k}_{KM6} as ridge estimator to test for the Granger causality. For DGP 2, DGP3, and DGP 4 this test is almost always unbiased.

The lag-length effect

As previously mentioned, instead of considering the sample size, the tests' statistical sizes are evaluated with regards to the degrees of freedom for different models with various lag lengths. In this context, using OLS as estimation method, increasing the lag length does not cause any problems for DGP 1 for the F-test. However, the bias increases for all DGPs for the tests based on asymptotic distributions. This is also the case for the small-sample corrected of W, LR and LM tests. For the W test, the over-rejection increases while for the LR and LM tests the under-rejection of the nominal size increases. In addition to the above effects, there is also an interaction effect between increasing the lag length and the degree of multicollinearity. The problem caused by multicollinearity increases as the lag length increases for all estimation methods.

The degrees of freedom effect

When increasing the degrees of freedom, the actual size becomes substantially closer to the nominal size, which is especially true for the tests based on asymptotic distributions. However, even for DGP 1 when using small sample corrections of the W and LM tests the

actual size is always biased when we have access to less than 50 degrees of freedom. The LRC and LRE are then superior options. However, when x_t is purely random then it is better to use the F-test than the tests based on the asymptotic distribution. For all DGPs when the new RRGC test is used, the bias of the tests based on asymptotic distribution slightly decreases but it is still non-ignorable.

Table 3: OLS

| p= 2 | W | LR | LM | WC | LRC | LMC | F |
|--|---|---|--|--|---|---|---|
| DGP 1 | | | | | | | |
| 15 | 0.1481 | 0.1080 | 0.0681 | 0.0807 | 0.0473 | 0.0172 | 0.0464 |
| 25 | 0.1090 | 0.0874 | 0.0651 | 0.0718 | 0.0501 | 0.0297 | 0.0504 |
| 50 | 0.0771 | 0.0656 | 0.0556 | 0.0584 | 0.0491 | 0.0394 | 0.0480 |
| 100 | 0.0632 | 0.0595 | 0.0546 | 0.0560 | 0.0508 | 0.0458 | 0.0487 |
| DGP 2 | | | | | | | |
| 15 | 0.1858 | 0.1419 | 0.0952 | 0.1090 | 0.0691 | 0.0255 | 0.0677 |
| 25 | 0.1265 | 0.1027 | 0.0769 | 0.0840 | 0.0633 | 0.0399 | 0.0656 |
| 50 | 0.0874 | 0.0767 | 0.0663 | 0.0690 | 0.0586 | 0.0488 | 0.0654 |
| 100 | 0.0711 | 0.0656 | 0.0609 | 0.0626 | 0.0575 | 0.053 | 0.0640 |
| DGP 3 | | | | | | | |
| 15 | 0.1988 | 0.1524 | 0.0963 | 0.1134 | 0.0697 | 0.0274 | 0.0697 |
| 25 | 0.1385 | 0.1117 | 0.0848 | 0.0932 | 0.0706 | 0.0502 | 0.0706 |
| 50 | 0.0969 | 0.0861 | 0.0755 | 0.0789 | 0.0684 | 0.0555 | 0.0684 |
| 100 | 0.0743 | 0.0699 | 0.0637 | 0.0656 | 0.0602 | 0.0552 | 0.0602 |
| DGP 4 | | | | | | | |
| 15 | 0.1995 | 0.1538 | 0.1020 | 0.1160 | 0.0716 | 0.0281 | 0.0708 |
| 25 | 0.1365 | 0.1102 | 0.0831 | 0.0912 | 0.0679 | 0.0447 | 0.0694 |
| 50 | 0.0966 | 0.0831 | 0.0732 | 0.0764 | 0.0659 | 0.0548 | 0.0697 |
| 100 | 0.0726 | 0.0681 | 0.0633 | 0.0640 | 0.0598 | 0.0555 | 0.0613 |
| | | | | | | | |
| p=4 | W | LR | LM | WC | LRC | LMC | F |
| p=4 DGP 1 | W | LR | LM | WC | LRC | LMC | F |
| p=4 DGP 1 15 | W 0.3202 | LR 0.2168 | LM 0.1011 | WC 0.1088 | LRC 0.0355 | LMC 0.0002 | F 0.0487 |
| p=4 DGP 1 15 25 | W 0.3202 0.1977 | LR 0.2168 0.1366 | LM 0.1011 0.0783 | WC 0.1088 0.0833 | LRC 0.0355 0.0411 | LMC 0.0002 0.0111 | F 0.0487 0.0492 |
| p=4 DGP 1 15 25 50 | W 0.3202 0.1977 0.1046 | LR 0.2168 0.1366 0.0818 | LM 0.1011 0.0783 0.0596 | WC 0.1088 0.0833 0.0615 | LRC 0.0355 0.0411 0.0442 | LMC 0.0002 0.0111 0.028 | F 0.0487 0.0492 0.0471 |
| p=4 DGP 1 15 25 50 100 | W 0.3202 0.1977 0.1046 0.0767 | LR 0.2168 0.1366 0.0818 0.0667 | LM 0.1011 0.0783 0.0596 0.0577 | WC 0.1088 0.0833 0.0615 0.0583 | LRC 0.0355 0.0411 0.0442 0.0484 | LMC 0.0002 0.0111 0.028 0.0394 | F 0.0487 0.0492 0.0471 0.0505 |
| p=4 DGP 1 15 25 50 100 DGP 2 | W 0.3202 0.1977 0.1046 0.0767 | LR 0.2168 0.1366 0.0818 0.0667 | LM 0.1011 0.0783 0.0596 0.0577 | WC 0.1088 0.0833 0.0615 0.0583 | LRC 0.0355 0.0411 0.0442 0.0484 | LMC 0.0002 0.0111 0.028 0.0394 | F 0.0487 0.0492 0.0471 0.0505 |
| p=4 DGP 1 15 25 50 100 DGP 2 15 | W 0.3202 0.1977 0.1046 0.0767 0.3733 | LR 0.2168 0.1366 0.0818 0.0667 0.2681 | LM 0.1011 0.0783 0.0596 0.0577 0.1278 | WC 0.1088 0.0833 0.0615 0.0583 0.1404 | LRC 0.0355 0.0411 0.0442 0.0484 0.0507 | LMC 0.0002 0.0111 0.028 0.0394 0.0026 | F 0.0487 0.0492 0.0471 0.0505 0.0655 |
| p=4 DGP 1 15 25 50 100 DGP 2 15 25 | W 0.3202 0.1977 0.1046 0.0767 0.3733 0.2338 | LR 0.2168 0.1366 0.0818 0.0667 0.2681 0.1654 | LM 0.1011 0.0783 0.0596 0.0577 0.1278 0.0950 | WC 0.1088 0.0833 0.0615 0.0583 0.1404 0.1021 | LRC 0.0355 0.0411 0.0442 0.0484 0.0507 0.0536 | LMC 0.0002 0.0111 0.028 0.0394 0.0026 0.0158 | F 0.0487 0.0492 0.0471 0.0505 0.0655 0.0625 |
| p=4 DGP 1 15 25 50 100 DGP 2 15 25 50 | W 0.3202 0.1977 0.1046 0.0767 0.3733 0.2338 0.1293 | LR 0.2168 0.1366 0.0818 0.0667 0.2681 0.1654 0.1033 | LM 0.1011 0.0783 0.0596 0.0577 0.1278 0.0950 0.0765 | WC 0.1088 0.0833 0.0615 0.0583 0.1404 0.1021 0.0792 | LRC 0.0355 0.0411 0.0442 0.0484 0.0507 0.0536 0.0549 | LMC 0.0002 0.0111 0.028 0.0394 0.0026 0.0158 0.0346 | F 0.0487 0.0492 0.0471 0.0505 0.0655 0.0655 0.0625 0.0595 |
| p=4 DGP 1 15 25 50 100 DGP 2 15 25 50 100 | W 0.3202 0.1977 0.1046 0.0767 0.3733 0.2338 0.1293 0.0891 | LR 0.2168 0.1366 0.0818 0.0667 0.2681 0.1654 0.1033 0.0744 | LM 0.1011 0.0783 0.0596 0.0577 0.1278 0.0950 0.0765 0.0613 | WC 0.1088 0.0833 0.0615 0.0583 0.1404 0.1021 0.0792 0.0628 | LRC 0.0355 0.0411 0.0442 0.0484 0.0507 0.0536 0.0549 0.0532 | LMC 0.0002 0.0111 0.028 0.0394 0.0026 0.0158 0.0346 0.0442 | F 0.0487 0.0492 0.0471 0.0505 0.0655 0.0625 0.0595 0.0551 |
| p=4 DGP 1 15 25 50 100 DGP 2 15 25 50 100 DGP 3 | W 0.3202 0.1977 0.1046 0.0767 0.3733 0.2338 0.1293 0.0891 | LR 0.2168 0.1366 0.0818 0.0667 0.2681 0.1654 0.1033 0.0744 | LM 0.1011 0.0783 0.0596 0.0577 0.1278 0.0950 0.0765 0.0613 | WC 0.1088 0.0833 0.0615 0.0583 0.1404 0.1021 0.0792 0.0628 | LRC 0.0355 0.0411 0.0442 0.0484 0.0507 0.0536 0.0549 0.0532 | LMC 0.0002 0.0111 0.028 0.0394 0.0026 0.0158 0.0346 0.0442 | F 0.0487 0.0492 0.0471 0.0505 0.0655 0.0625 0.0595 0.0551 |
| p=4 DGP 1 15 25 50 100 DGP 2 15 25 50 100 DGP 3 15 | W 0.3202 0.1977 0.1046 0.0767 0.3733 0.2338 0.1293 0.0891 0.3992 | LR 0.2168 0.1366 0.0818 0.0667 0.2681 0.1654 0.1033 0.0744 0.2909 | LM 0.1011 0.0783 0.0596 0.0577 0.1278 0.0950 0.0765 0.0613 0.1467 | WC 0.1088 0.0833 0.0615 0.0583 0.1404 0.1021 0.0792 0.0628 0.1611 | LRC 0.0355 0.0411 0.0442 0.0484 0.0507 0.0536 0.0549 0.0532 0.0615 | LMC 0.0002 0.0111 0.028 0.0394 0.0026 0.0158 0.0346 0.0346 0.0442 0.0072 | F 0.0487 0.0492 0.0471 0.0505 0.0655 0.0625 0.0595 0.0551 0.0551 |
| p=4 DGP 1 15 25 50 100 DGP 2 15 25 50 100 DGP 2 15 25 50 100 DGP 3 15 25 | W 0.3202 0.1977 0.1046 0.0767 0.3733 0.2338 0.1293 0.0891 0.3992 0.2528 | LR 0.2168 0.1366 0.0818 0.0667 0.2681 0.1654 0.1033 0.0744 0.2909 0.1881 | LM 0.1011 0.0783 0.0596 0.0577 0.0577 0.1278 0.0950 0.0765 0.0613 0.1467 0.1149 | WC 0.1088 0.0833 0.0615 0.0583 0.1404 0.1021 0.0792 0.0628 0.1611 0.1220 | LRC 0.0355 0.0411 0.0442 0.0484 0.0507 0.0536 0.0549 0.0532 0.0615 0.0681 | LMC 0.0002 0.0111 0.028 0.0394 0.0026 0.0158 0.0346 0.0346 0.0442 0.0072 0.0072 0.0233 | F 0.0487 0.0492 0.0471 0.0505 0.0655 0.0625 0.0595 0.0551 0.0710 0.0779 |
| p=4 DGP 1 15 25 50 100 DGP 2 15 25 50 100 DGP 2 15 25 50 100 DGP 3 15 25 50 | W 0.3202 0.1977 0.1046 0.0767 0.3733 0.2338 0.1293 0.0891 0.3992 0.2528 0.1451 | LR 0.2168 0.1366 0.0818 0.0667 0.2681 0.1654 0.1033 0.0744 0.2909 0.1881 0.1174 | LM 0.1011 0.0783 0.0596 0.0577 0.0278 0.0950 0.0765 0.0613 0.1467 0.1149 0.0910 | WC 0.1088 0.0833 0.0615 0.0583 0.1404 0.1021 0.0792 0.0628 0.1611 0.1220 0.0921 | LRC 0.0355 0.0411 0.0442 0.0484 0.0507 0.0536 0.0532 0.0532 0.0615 0.0681 0.0679 | LMC 0.0002 0.0111 0.028 0.0394 0.0026 0.0158 0.0346 0.0346 0.0442 0.0072 0.0233 0.0459 | F 0.0487 0.0492 0.0471 0.0505 0.0655 0.0625 0.0595 0.0551 0.0551 0.0710 0.0779 0.0745 |
| p=4 DGP 1 15 25 50 100 DGP 2 15 25 50 100 DGP 2 15 25 50 100 DGP 3 15 25 50 100 DGP 3 15 25 50 100 | W 0.3202 0.1977 0.1046 0.0767 0.3733 0.2338 0.1293 0.0891 0.3992 0.2528 0.1451 0.0900 | LR 0.2168 0.1366 0.0818 0.0667 0.2681 0.1654 0.1033 0.0744 0.2909 0.1881 0.1174 0.0778 | LM 0.1011 0.0783 0.0596 0.0577 0.1278 0.0950 0.0765 0.0613 0.1467 0.1467 0.1149 0.0910 0.0667 | WC 0.1088 0.0833 0.0615 0.0583 0.1404 0.1021 0.0792 0.0628 0.1611 0.1220 0.0921 0.0673 | LRC 0.0355 0.0411 0.0442 0.0484 0.0507 0.0536 0.0549 0.0532 0.0615 0.0681 0.0679 0.0590 | LMC 0.0002 0.0111 0.028 0.0394 0.0026 0.0158 0.0346 0.0346 0.0442 0.0072 0.0233 0.0459 0.0477 | F 0.0487 0.0492 0.0471 0.0505 0.0655 0.0625 0.0595 0.0551 0.0710 0.0779 0.0745 0.0611 |
| p=4 DGP 1 15 25 50 100 DGP 2 15 25 50 100 DGP 2 15 25 50 100 DGP 3 15 25 50 100 DGP 3 15 25 50 100 DGP 4 | W 0.3202 0.1977 0.1046 0.0767 0.3733 0.2338 0.1293 0.0891 0.3992 0.2528 0.1451 0.0900 | LR 0.2168 0.1366 0.0818 0.0667 0.2681 0.1654 0.1033 0.0744 0.2909 0.1881 0.1174 0.0778 | LM 0.1011 0.0783 0.0596 0.0577 0.1278 0.0950 0.0765 0.0613 0.1467 0.1149 0.0910 0.0667 | WC 0.1088 0.0833 0.0615 0.0583 0.1404 0.1021 0.0792 0.0628 0.1611 0.1220 0.0921 0.0673 | LRC 0.0355 0.0411 0.0442 0.0484 0.0507 0.0536 0.0549 0.0532 0.0615 0.0681 0.0679 0.0590 | LMC 0.0002 0.0111 0.028 0.0394 0.0026 0.0158 0.0346 0.0442 0.0072 0.0233 0.0459 0.0477 | F 0.0487 0.0492 0.0471 0.0505 0.0655 0.0625 0.0595 0.0551 0.0710 0.0779 0.0745 0.0611 |
| p=4 DGP 1 15 25 50 100 DGP 2 15 25 50 100 DGP 2 15 25 50 100 DGP 3 15 25 50 100 DGP 3 15 25 50 100 DGP 4 15 | W 0.3202 0.1977 0.1046 0.0767 0.3733 0.2338 0.1293 0.0891 0.3992 0.2528 0.1451 0.0900 0.3935 | LR 0.2168 0.1366 0.0818 0.0667 0.2681 0.1654 0.1033 0.0744 0.2909 0.1881 0.1174 0.0778 0.2861 | LM 0.1011 0.0783 0.0596 0.0577 0.1278 0.0950 0.0765 0.0613 0.1467 0.1149 0.0910 0.0667 0.1398 | WC 0.1088 0.0833 0.0615 0.0583 0.1404 0.1021 0.0792 0.0628 0.1611 0.1220 0.0921 0.0673 0.1527 | LRC 0.0355 0.0411 0.0442 0.0484 0.0507 0.0536 0.0549 0.0532 0.0615 0.0681 0.0679 0.0590 | LMC 0.0002 0.0111 0.028 0.0394 0.0026 0.0158 0.0346 0.0442 0.0072 0.0233 0.0459 0.0477 0.0041 | F 0.0487 0.0492 0.0471 0.0505 0.0655 0.0655 0.0595 0.0551 0.0710 0.0779 0.0745 0.0611 |
| p=4 DGP 1 15 25 50 100 DGP 2 15 25 50 100 DGP 2 15 25 50 100 DGP 3 15 25 50 100 DGP 3 15 25 50 100 DGP 4 15 25 | W 0.3202 0.1977 0.1046 0.0767 0.3733 0.2338 0.1293 0.0891 0.3992 0.2528 0.1451 0.0900 0.3935 0.2527 | LR 0.2168 0.1366 0.0818 0.0667 0.2681 0.1654 0.1033 0.0744 0.2909 0.1881 0.1174 0.0778 0.2861 0.2861 0.1881 | LM 0.1011 0.0783 0.0596 0.0577 0.1278 0.0950 0.0765 0.0613 0.1467 0.1467 0.1149 0.0910 0.0667 0.1398 0.1175 | WC 0.1088 0.0833 0.0615 0.0583 0.1404 0.1021 0.0792 0.0628 0.1611 0.1220 0.0921 0.0673 0.1527 0.1245 | LRC 0.0355 0.0411 0.0442 0.0484 0.0507 0.0536 0.0549 0.0532 0.0615 0.0681 0.0679 0.0590 0.0521 0.0691 | LMC 0.0002 0.0111 0.028 0.0394 0.0026 0.0158 0.0346 0.0346 0.0346 0.0442 0.0072 0.0233 0.0459 0.0459 0.0477 0.0041 0.0094 | F 0.0487 0.0492 0.0471 0.0505 0.0655 0.0625 0.0595 0.0551 0.0710 0.0779 0.0745 0.0611 0.0708 0.0803 |
| $\begin{array}{c} p=4 \\ DGP 1 \\ 15 \\ 25 \\ 50 \\ 100 \\ DGP 2 \\ 15 \\ 25 \\ 50 \\ 100 \\ DGP 3 \\ 15 \\ 25 \\ 50 \\ 100 \\ DGP 3 \\ 15 \\ 25 \\ 50 \\ 100 \\ DGP 4 \\ 15 \\ 25 \\ 50 \\ 50 \\ \end{array}$ | W 0.3202 0.1977 0.1046 0.0767 0.3733 0.2338 0.1293 0.0891 0.3992 0.2528 0.1451 0.0900 0.3935 0.2527 0.1378 | LR 0.2168 0.1366 0.0818 0.0667 0.2681 0.1654 0.1033 0.0744 0.07744 0.2909 0.1881 0.1174 0.0778 0.2861 0.1881 0.1101 | LM 0.1011 0.0783 0.0596 0.0577 0.0278 0.0950 0.0765 0.0613 0.1467 0.1149 0.0910 0.0667 0.1398 0.1175 0.0812 | WC 0.1088 0.0833 0.0615 0.0583 0.1404 0.1021 0.0792 0.0628 0.1611 0.1220 0.0921 0.0673 0.1527 0.1245 0.0838 | LRC 0.0355 0.0411 0.0442 0.0484 0.0507 0.0536 0.0549 0.0532 0.0549 0.0532 0.0681 0.0679 0.0590 0.0590 0.0590 | LMC 0.0002 0.0111 0.028 0.0394 0.0026 0.0158 0.0346 0.0442 0.00442 0.0072 0.0233 0.0459 0.0459 0.0477 0.0041 0.0094 0.0396 | F 0.0487 0.0492 0.0471 0.0505 0.0555 0.0625 0.0551 0.0551 0.0710 0.0779 0.0745 0.0611 0.0708 0.0803 0.0701 |

| p= 2 | W | LR | LM | WC | LRC | LMC | F |
|-------|---------------|--------|--------|--------|--------|--------|--------|
| DGP 1 | | | | | | | |
| 15 | 0.0954 | 0.0697 | 0.0348 | 0.0513 | 0.0300 | 0.0083 | 0.0464 |
| 25 | 0.0587 | 0.0450 | 0.0270 | 0.0356 | 0.0252 | 0.0145 | 0.0454 |
| 50 | 0.0372 | 0.0317 | 0.0248 | 0.0281 | 0.0246 | 0.0177 | 0.0437 |
| 100 | 0.0263 | 0.0244 | 0.0216 | 0.0233 | 0.0213 | 0.0183 | 0.0437 |
| DGP 2 | | | | | | | |
| 15 | 0.1516 | 0.1138 | 0.0664 | 0.0861 | 0.0510 | 0.0170 | 0.0643 |
| 25 | 0.0969 | 0.0776 | 0.0545 | 0.0633 | 0.0473 | 0.0270 | 0.0651 |
| 50 | 0.0602 | 0.0517 | 0.0430 | 0.0464 | 0.0406 | 0.0318 | 0.0580 |
| 100 | 0.0415 | 0.0376 | 0.0333 | 0.0351 | 0.0326 | 0.0287 | 0.0326 |
| DGP 3 | | | | | | | |
| 15 | 0.1819 | 0.1397 | 0.0848 | 0.1036 | 0.0599 | 0.0201 | 0.0599 |
| 25 | 0.1151 | 0.0947 | 0.0695 | 0.0791 | 0.0573 | 0.0344 | 0.0573 |
| 50 | 0.0790 | 0.0704 | 0.0601 | 0.0647 | 0.0536 | 0.0438 | 0.0536 |
| 100 | 0.0629 | 0.0588 | 0.0535 | 0.0551 | 0.0506 | 0.046 | 0.0506 |
| DGP 4 | | | | | | | |
| 15 | 0.1838 | 0.1403 | 0.0896 | 0.1043 | 0.0660 | 0.0232 | 0.0744 |
| 25 | 0.124 | 0.0982 | 0.0728 | 0.0815 | 0.0608 | 0.0383 | 0.0709 |
| 50 | 0.0821 | 0.0712 | 0.0619 | 0.0648 | 0.0556 | 0.0477 | 0.0622 |
| 100 | 0.0671 | 0.0622 | 0.0576 | 0.0591 | 0.0543 | 0.0495 | 0.0607 |
| p=4 | W | LR | LM | WC | LRC | LMC | F |
| DGP 1 | | | | | | | |
| 15 | 0.2441 | 0.1657 | 0.0634 | 0.0862 | 0.0281 | 0.0000 | 0.0374 |
| 25 | 0.1247 | 0.0884 | 0.0406 | 0.0548 | 0.0258 | 0.0046 | 0.0313 |
| 50 | 0.0554 | 0.0426 | 0.0278 | 0.0329 | 0.0229 | 0.0119 | 0.0252 |
| 100 | 0.0326 | 0.0277 | 0.0195 | 0.0226 | 0.0184 | 0.0125 | 0.0190 |
| DGP 2 | | | | | | | |
| 15 | 0.2809 | 0.2032 | 0.0769 | 0.1013 | 0.0321 | 0.0000 | 0.0441 |
| 25 | 0.1892 | 0.1360 | 0.0743 | 0.0849 | 0.0420 | 0.0091 | 0.0510 |
| 50 | 0.0997 | 0.0786 | 0.0535 | 0.0581 | 0.0420 | 0.0249 | 0.0459 |
| 100 | 0.0595 | 0.0505 | 0.0412 | 0.0434 | 0.0366 | 0.0282 | 0.0380 |
| DGP 3 | | | | | | | |
| 15 | 0.3568 | 0.2528 | 0.1190 | 0.1336 | 0.0459 | 0.0002 | 0.0640 |
| 25 | 0.1982 | 0.1403 | 0.0816 | 0.0904 | 0.0469 | 0.0110 | 0.0548 |
| 50 | 0.1115 | 0.0873 | 0.0625 | 0.0671 | 0.0487 | 0.0312 | 0.0525 |
| 100 | 0.0722 | 0.0623 | 0.0521 | 0.0540 | 0.0454 | 0.0376 | 0.0472 |
| DGP 4 | | | | | | | |
| 15 | 0.3800 | 0.2748 | 0.1311 | 0.1474 | 0.0473 | 0.0002 | 0.0643 |
| 25 | | 0 1710 | 0 1040 | 0.1116 | 0.0588 | 0.0161 | 0.0686 |
| | 0.2421 | 0.1/13 | 0.1040 | 0.1110 | 0.0388 | 0.0101 | 0.0000 |
| 50 | 0.2421 0.1362 | 0.1713 | 0.1040 | 0.0852 | 0.0588 | 0.0387 | 0.0655 |

Table 4: Ridge parameter estimated using $\hat{k}_{\scriptscriptstyle HK}$

| p= 2 | W | LR | LM | WC | LRC | LMC | F |
|-------|--------|--------|--------|--------|--------|--------|--------|
| DGP 1 | | | | | | | |
| 15 | 0.1450 | 0.1050 | 0.0640 | 0.077 | 0.045 | 0.0120 | 0.0465 |
| 25 | 0.1061 | 0.0854 | 0.0624 | 0.0698 | 0.0486 | 0.0296 | 0.0500 |
| 50 | 0.0775 | 0.0665 | 0.0565 | 0.0601 | 0.0519 | 0.0410 | 0.0530 |
| 100 | 0.0651 | 0.0610 | 0.0561 | 0.0577 | 0.0528 | 0.0473 | 0.0501 |
| DGP 2 | | | | | | | |
| 15 | 0.1724 | 0.1285 | 0.0743 | 0.0944 | 0.0544 | 0.0139 | 0.0583 |
| 25 | 0.1239 | 0.0975 | 0.0706 | 0.0795 | 0.0585 | 0.0377 | 0.0569 |
| 50 | 0.0815 | 0.0713 | 0.0610 | 0.0641 | 0.0540 | 0.0450 | 0.0559 |
| 100 | 0.0693 | 0.0639 | 0.0587 | 0.0606 | 0.0557 | 0.0513 | 0.0575 |
| DGP 3 | | | | | | | |
| 15 | 0.1653 | 0.1255 | 0.0690 | 0.0919 | 0.0516 | 0.0125 | 0.0516 |
| 25 | 0.1248 | 0.0991 | 0.0735 | 0.0824 | 0.0630 | 0.0364 | 0.0630 |
| 50 | 0.0910 | 0.0787 | 0.0669 | 0.0704 | 0.0603 | 0.0494 | 0.0603 |
| 100 | 0.0700 | 0.0641 | 0.0596 | 0.0610 | 0.0558 | 0.0513 | 0.0558 |
| DGP 4 | | | | | | | |
| 15 | 0.1360 | 0.1004 | 0.0514 | 0.0717 | 0.0415 | 0.0084 | 0.0369 |
| 25 | 0.1169 | 0.0908 | 0.0646 | 0.0748 | 0.0526 | 0.0302 | 0.0561 |
| 50 | 0.0854 | 0.0743 | 0.0631 | 0.0675 | 0.0577 | 0.0468 | 0.0592 |
| 100 | 0.0655 | 0.0602 | 0.0550 | 0.0575 | 0.0519 | 0.0482 | 0.0576 |
| p=4 | W | LR | LM | WC | LRC | LMC | F |
| DGP 1 | | | | | | | |
| 15 | 0.3073 | 0.2112 | 0.0832 | 0.1019 | 0.0284 | 0.0000 | 0.0406 |
| 25 | 0.2039 | 0.1419 | 0.0760 | 0.0821 | 0.0414 | 0.0085 | 0.0491 |
| 50 | 0.1117 | 0.0870 | 0.0642 | 0.0664 | 0.0437 | 0.0275 | 0.0485 |
| 100 | 0.0786 | 0.0689 | 0.0584 | 0.0595 | 0.0494 | 0.0386 | 0.0518 |
| DGP 2 | | | | | | | |
| 15 | 0.3483 | 0.2440 | 0.0950 | 0.1219 | 0.0349 | 0.0000 | 0.0481 |
| 25 | 0.223 | 0.1591 | 0.0944 | 0.1010 | 0.0531 | 0.0120 | 0.0640 |
| 50 | 0.1213 | 0.0961 | 0.0696 | 0.0721 | 0.0504 | 0.0325 | 0.0557 |
| 100 | 0.0876 | 0.0770 | 0.0636 | 0.0654 | 0.0543 | 0.0444 | 0.0563 |
| DGP 3 | | | | | | | |
| 15 | 0.3498 | 0.2413 | 0.0883 | 0.1206 | 0.0335 | 0.0000 | 0.0483 |
| 25 | 0.2261 | 0.1595 | 0.0887 | 0.0968 | 0.0486 | 0.0108 | 0.0593 |
| 50 | 0.1226 | 0.0963 | 0.0717 | 0.0744 | 0.0516 | 0.0309 | 0.0547 |
| 100 | 0.0846 | 0.0744 | 0.0649 | 0.0663 | 0.0554 | 0.045 | 0.0574 |
| DGP 4 | | | | | | | |
| 15 | 0.3175 | 0.2118 | 0.0646 | 0.0980 | 0.0263 | 0.0000 | 0.0383 |
| 25 | 0.2256 | 0.1597 | 0.0869 | 0.0982 | 0.0490 | 0.0093 | 0.0575 |
| 50 | 0.1354 | 0.1061 | 0.078 | 0.0814 | 0.0561 | 0.0342 | 0.0617 |
| 100 | 0.0911 | 0.0779 | 0.0664 | 0.0678 | 0.0585 | 0.0478 | 0.0607 |

Table 5: Ridge parameter estimated using $\hat{k}_{{\scriptscriptstyle K\!M\!4}}$

| p= 2 | W | LR | LM | WC | LRC | LMC | F |
|---|--|--|---|---|--|--|--|
| DGP 1 | | | | | | | |
| 15 | 0.1405 | 0.1048 | 0.0636 | 0.0783 | 0.0441 | 0.0127 | 0.0420 |
| 25 | 0.1021 | 0.0800 | 0.0591 | 0.0671 | 0.0458 | 0.0264 | 0.0494 |
| 50 | 0.0734 | 0.0651 | 0.0543 | 0.0582 | 0.0473 | 0.0365 | 0.0487 |
| 100 | 0.0666 | 0.0622 | 0.0569 | 0.0590 | 0.0536 | 0.0487 | 0.0491 |
| DGP 2 | | | | | | | |
| 15 | 0.1791 | 0.1336 | 0.0783 | 0.0974 | 0.0554 | 0.0169 | 0.0584 |
| 25 | 0.1219 | 0.0978 | 0.0703 | 0.0794 | 0.0557 | 0.0342 | 0.0573 |
| 50 | 0.0879 | 0.0780 | 0.0680 | 0.0711 | 0.0599 | 0.0486 | 0.0568 |
| 100 | 0.0677 | 0.0624 | 0.0573 | 0.0592 | 0.0546 | 0.0499 | 0.0519 |
| DGP 3 | | | | | | | |
| 15 | 0.1596 | 0.1171 | 0.0622 | 0.0852 | 0.0482 | 0.0125 | 0.0482 |
| 25 | 0.1249 | 0.1017 | 0.0739 | 0.0848 | 0.0602 | 0.0368 | 0.0572 |
| 50 | 0.0868 | 0.0765 | 0.064 | 0.0683 | 0.0559 | 0.0462 | 0.0559 |
| 100 | 0.0720 | 0.0669 | 0.0621 | 0.0639 | 0.0594 | 0.0537 | 0.0594 |
| DGP 4 | | | | | | | |
| 15 | 0.1349 | 0.0916 | 0.0424 | 0.0644 | 0.0350 | 0.0056 | 0.0389 |
| 25 | 0.1133 | 0.0897 | 0.0619 | 0.0736 | 0.0525 | 0.0289 | 0.0548 |
| 50 | 0.0885 | 0.0777 | 0.0664 | 0.0697 | 0.0584 | 0.0467 | 0.0585 |
| 100 | 0.0742 | 0.0699 | 0.0655 | 0.0666 | 0.0621 | 0.0565 | 0.0567 |
| p=4 | W | IR | LM | WC | IRC | IMC | F |
| P ' | •• | | | | LIC | | 1 |
| DGP 1 | | | | | LICC | LIVIC | 1 |
| DGP 1 15 | 0.3061 | 0.2086 | 0.073 | 0.0955 | 0.0242 | 0.0000 | 0.0456 |
| DGP 1 15 25 | 0.3061 | 0.2086 0.1310 | 0.073 | 0.0955 | 0.0242 0.0408 | 0.0000 0.0088 | 0.0456 |
| DGP 1 15 25 50 | 0.3061 0.1909 0.1172 | 0.2086 0.1310 0.0904 | 0.073 0.0758 0.0635 | 0.0955 0.0819 0.0647 | 0.0242 0.0408 0.0437 | 0.0000 0.0088 0.0265 | 0.0456 0.0483 0.0477 |
| DGP 1 15 25 50 100 | 0.3061 0.1909 0.1172 0.0764 | 0.2086 0.1310 0.0904 0.0662 | 0.073 0.0758 0.0635 0.0551 | 0.0955 0.0819 0.0647 0.0565 | 0.0242 0.0408 0.0437 0.0461 | 0.0000 0.0088 0.0265 0.0392 | 0.0456 0.0483 0.0477 0.0478 |
| DGP 1 15 25 50 100 DGP 2 | 0.3061 0.1909 0.1172 0.0764 | 0.2086 0.1310 0.0904 0.0662 | 0.073 0.0758 0.0635 0.0551 | 0.0955 0.0819 0.0647 0.0565 | 0.0242 0.0408 0.0437 0.0461 | 0.0000 0.0088 0.0265 0.0392 | 0.0456 0.0483 0.0477 0.0478 |
| DGP 1 15 25 50 100 DGP 2 15 | 0.3061 0.1909 0.1172 0.0764 0.3416 | 0.2086 0.1310 0.0904 0.0662 0.2339 | 0.073 0.0758 0.0635 0.0551 0.0818 | 0.0955 0.0819 0.0647 0.0565 0.1121 | 0.0242 0.0408 0.0437 0.0461 0.0337 | 0.0000 0.0088 0.0265 0.0392 0.0001 | 0.0456 0.0483 0.0477 0.0478 0.0459 |
| DGP 1 15 25 50 100 DGP 2 15 25 | 0.3061 0.1909 0.1172 0.0764 0.3416 0.224 | 0.2086 0.1310 0.0904 0.0662 0.2339 0.1609 | 0.073 0.0758 0.0635 0.0551 0.0818 0.0900 | 0.0955 0.0819 0.0647 0.0565 0.1121 0.0977 | 0.0242 0.0408 0.0437 0.0461 0.0337 0.0481 | 0.0000 0.0088 0.0265 0.0392 0.0001 0.0122 | 0.0456 0.0483 0.0477 0.0478 0.0459 0.0570 |
| DGP 1 15 25 50 100 DGP 2 15 25 50 | 0.3061 0.1909 0.1172 0.0764 0.3416 0.224 0.1249 | 0.2086 0.1310 0.0904 0.0662 0.2339 0.1609 0.0991 | 0.073 0.0758 0.0635 0.0551 0.0818 0.0900 0.0716 | 0.0955 0.0819 0.0647 0.0565 0.1121 0.0977 0.0748 | 0.0242 0.0408 0.0437 0.0461 0.0337 0.0481 0.0525 | 0.0000 0.0088 0.0265 0.0392 0.0001 0.0122 0.0317 | 0.0456 0.0483 0.0477 0.0478 0.0478 0.0459 0.0570 0.0576 |
| DGP 1 15 25 50 100 DGP 2 15 25 50 100 | 0.3061 0.1909 0.1172 0.0764 0.3416 0.224 0.1249 0.0811 | 0.2086 0.1310 0.0904 0.0662 0.2339 0.1609 0.0991 0.0702 | 0.073 0.0758 0.0635 0.0551 0.0818 0.0900 0.0716 0.0604 | 0.0955 0.0819 0.0647 0.0565 0.1121 0.0977 0.0748 0.0613 | 0.0242 0.0408 0.0437 0.0461 0.0337 0.0481 0.0525 0.0518 | 0.0000 0.0088 0.0265 0.0392 0.0001 0.0122 0.0317 0.0420 | 0.0456 0.0483 0.0477 0.0478 0.0478 0.0459 0.0570 0.0576 0.0548 |
| DGP 1 15 25 50 100 DGP 2 15 25 50 100 100 DGP 3 | 0.3061 0.1909 0.1172 0.0764 0.3416 0.224 0.1249 0.0811 | 0.2086 0.1310 0.0904 0.0662 0.2339 0.1609 0.0991 0.0702 | 0.073 0.0758 0.0635 0.0551 0.0818 0.0900 0.0716 0.0604 | 0.0955 0.0819 0.0647 0.0565 0.1121 0.0977 0.0748 0.0613 | 0.0242 0.0408 0.0437 0.0461 0.0337 0.0481 0.0525 0.0518 | 0.0000 0.0088 0.0265 0.0392 0.0001 0.0122 0.0317 0.0420 | 0.0456 0.0483 0.0477 0.0478 0.0478 0.0478 0.0459 0.0570 0.0576 0.0548 |
| DGP 1 15 25 50 100 DGP 2 15 25 50 100 DGP 3 15 | 0.3061 0.1909 0.1172 0.0764 0.3416 0.224 0.1249 0.0811 0.338 | 0.2086 0.1310 0.0904 0.0662 0.2339 0.1609 0.0991 0.0702 0.2272 | 0.073 0.0758 0.0635 0.0551 0.0818 0.0900 0.0716 0.0604 0.0690 | 0.0955 0.0819 0.0647 0.0565 0.1121 0.0977 0.0748 0.0613 0.1081 | 0.0242 0.0408 0.0437 0.0461 0.0337 0.0481 0.0525 0.0518 0.0270 | 0.0000 0.0088 0.0265 0.0392 0.0001 0.0122 0.0317 0.0420 0.0000 | 0.0456 0.0483 0.0477 0.0478 0.0478 0.0478 0.0459 0.0570 0.0576 0.0548 0.00446 |
| DGP 1 15 25 50 100 DGP 2 15 25 50 100 DGP 3 15 25 25 | 0.3061 0.1909 0.1172 0.0764 0.3416 0.224 0.1249 0.0811 0.338 0.2182 | 0.2086 0.1310 0.0904 0.0662 0.2339 0.1609 0.0991 0.0702 0.2272 0.1509 | 0.073 0.0758 0.0635 0.0551 0.0818 0.0900 0.0716 0.0604 0.0604 0.0690 0.0815 | 0.0955 0.0819 0.0647 0.0565 0.1121 0.0977 0.0748 0.0613 0.1081 0.1081 | 0.0242 0.0408 0.0437 0.0461 0.0337 0.0481 0.0525 0.0518 0.0270 0.0422 | 0.0000 0.0088 0.0265 0.0392 0.0001 0.0122 0.0317 0.0420 0.0000 0.0000 0.0092 | 0.0456 0.0483 0.0477 0.0478 0.0478 0.0478 0.0459 0.0570 0.0576 0.0576 0.0548 0.0446 0.0512 |
| DGP 1 15 25 50 100 DGP 2 15 25 50 100 DGP 3 15 25 50 100 DGP 3 15 25 50 100 | 0.3061 0.1909 0.1172 0.0764 0.3416 0.224 0.1249 0.0811 0.338 0.2182 0.1179 | 0.2086 0.1310 0.0904 0.0662 0.2339 0.1609 0.0991 0.0702 0.2272 0.1509 0.0910 | 0.073 0.0758 0.0635 0.0551 0.0818 0.0900 0.0716 0.0604 0.0604 0.0815 0.0684 | 0.0955 0.0819 0.0647 0.0565 0.1121 0.0977 0.0748 0.0613 0.1081 0.0911 0.0708 | 0.0242 0.0408 0.0437 0.0461 0.0337 0.0461 0.0525 0.0518 0.0518 0.0270 0.0422 0.0501 | 0.0000 0.0088 0.0265 0.0392 0.0001 0.0122 0.0317 0.0420 0.0000 0.0092 0.0320 | 0.0456 0.0483 0.0477 0.0478 0.0478 0.0478 0.0459 0.0570 0.0576 0.0548 0.0548 0.0446 0.0512 0.0543 |
| DGP 1 15 25 50 100 DGP 2 15 25 50 100 DGP 3 15 25 50 100 DGP 3 15 25 50 100 DGP 3 15 25 50 100 DGP 3 15 25 50 100 DGP 3 15 25 50 100 DGP 3 15 15 100 100 100 100 100 100 | 0.3061 0.1909 0.1172 0.0764 0.3416 0.224 0.1249 0.0811 0.338 0.2182 0.1179 0.0889 | 0.2086 0.1310 0.0904 0.0662 0.2339 0.1609 0.0991 0.0702 0.2272 0.1509 0.0910 0.0760 | 0.073 0.0758 0.0635 0.0551 0.0818 0.0900 0.0716 0.0604 0.0604 0.0690 0.0815 0.0684 0.0651 | 0.0955 0.0819 0.0647 0.0565 0.1121 0.0977 0.0748 0.0613 0.1081 0.0911 0.0708 0.0663 | 0.0242 0.0408 0.0437 0.0461 0.0337 0.0481 0.0525 0.0518 0.0270 0.0422 0.0501 0.0551 | 0.0000 0.0088 0.0265 0.0392 0.0001 0.0122 0.0317 0.0420 0.0000 0.0092 0.0320 0.0447 | 0.0456 0.0483 0.0477 0.0478 0.0478 0.0478 0.0479 0.0570 0.0576 0.0548 0.0548 0.0543 0.0543 0.0574 |
| DGP 1 15 25 50 100 DGP 2 15 25 50 100 DGP 3 15 25 50 100 DGP 3 15 25 50 100 DGP 4 | 0.3061 0.1909 0.1172 0.0764 0.3416 0.224 0.1249 0.0811 0.338 0.2182 0.1179 0.0889 | 0.2086 0.1310 0.0904 0.0662 0.2339 0.1609 0.0991 0.0702 0.2272 0.1509 0.0910 0.0760 | 0.073 0.0758 0.0635 0.0551 0.0818 0.0900 0.0716 0.0604 0.0604 0.0690 0.0815 0.0684 0.0651 | 0.0955 0.0819 0.0647 0.0565 0.1121 0.0977 0.0748 0.0613 0.1081 0.0911 0.0708 0.0663 | 0.0242 0.0408 0.0437 0.0461 0.0337 0.0481 0.0525 0.0518 0.0270 0.0422 0.0501 0.0551 | 0.0000 0.0088 0.0265 0.0392 0.0001 0.0122 0.0317 0.0420 0.0000 0.0092 0.0320 0.0447 | 0.0456 0.0483 0.0477 0.0478 0.0478 0.0478 0.0478 0.0570 0.0570 0.0576 0.0548 0.0548 0.0512 0.0543 0.0574 |
| DGP 1 15 25 50 100 DGP 2 15 25 50 100 DGP 3 15 25 50 100 DGP 3 15 25 50 100 DGP 4 15 | 0.3061 0.1909 0.1172 0.0764 0.3416 0.224 0.1249 0.0811 0.338 0.2182 0.1179 0.0889 0.3018 | 0.2086 0.1310 0.0904 0.0662 0.2339 0.1609 0.0991 0.0702 0.2272 0.1509 0.0910 0.0760 0.0760 | 0.073 0.0758 0.0635 0.0551 0.0818 0.0900 0.0716 0.0604 0.0604 0.0815 0.0684 0.0651 0.0517 | 0.0955 0.0819 0.0647 0.0565 0.1121 0.0977 0.0748 0.0613 0.1081 0.0911 0.0708 0.0663 0.0908 | 0.0242 0.0408 0.0437 0.0461 0.0337 0.0461 0.0525 0.0518 0.0551 0.0551 0.0551 | 0.0000 0.0088 0.0265 0.0392 0.0001 0.0122 0.0317 0.0420 0.0000 0.0092 0.0320 0.0320 0.0447 0.0000 | 0.0456 0.0483 0.0477 0.0478 0.0478 0.0478 0.0478 0.0570 0.0570 0.0576 0.0548 0.0548 0.0512 0.0543 0.0574 0.0574 |
| DGP 1 15 25 50 100 DGP 2 15 25 50 100 DGP 3 15 25 50 100 DGP 3 15 25 50 100 DGP 4 15 25 50 100 | 0.3061 0.1909 0.1172 0.0764 0.3416 0.224 0.1249 0.0811 0.338 0.2182 0.1179 0.0889 0.3018 0.2352 | 0.2086 0.1310 0.0904 0.0662 0.2339 0.1609 0.0991 0.0702 0.2272 0.1509 0.0910 0.0910 0.0760 0.1964 0.1677 | 0.073 0.0758 0.0635 0.0551 0.0818 0.0900 0.0716 0.0604 0.0604 0.0690 0.0815 0.0684 0.0651 0.0517 0.0908 | 0.0955 0.0819 0.0647 0.0565 0.1121 0.0977 0.0748 0.0613 0.1081 0.0911 0.0708 0.0663 0.0908 0.1048 | 0.0242 0.0408 0.0437 0.0461 0.0337 0.0481 0.0525 0.0518 0.0270 0.0422 0.0501 0.0551 0.0220 0.0220 0.0518 | 0.0000 0.0088 0.0265 0.0392 0.0001 0.0122 0.0317 0.0420 0.0000 0.0092 0.0320 0.0447 0.0000 0.0000 0.0003 | 0.0456 0.0483 0.0477 0.0478 0.0478 0.0478 0.0570 0.0570 0.0576 0.0548 0.0548 0.0543 0.0543 0.0574 0.0329 0.0572 |
| DGP 1 15 25 50 100 DGP 2 15 25 50 100 DGP 3 15 25 50 100 DGP 3 15 25 50 100 DGP 4 15 25 50 100 | 0.3061 0.1909 0.1172 0.0764 0.3416 0.224 0.1249 0.0811 0.338 0.2182 0.1179 0.0889 0.3018 0.2352 0.1354 | 0.2086 0.1310 0.0904 0.0662 0.2339 0.1609 0.0991 0.0702 0.2272 0.1509 0.0910 0.0760 0.0760 0.1964 0.1677 0.1062 | 0.073 0.0758 0.0635 0.0551 0.0551 0.0818 0.0900 0.0716 0.0604 0.0604 0.0651 0.0684 0.0651 0.0684 0.0651 0.0908 0.0784 | 0.0955 0.0819 0.0647 0.0565 0.1121 0.0977 0.0748 0.0613 0.0013 0.1081 0.0911 0.0708 0.0663 0.0063 0.00908 0.1048 0.0814 | 0.0242 0.0408 0.0437 0.0461 0.0337 0.0461 0.0525 0.0518 0.0551 0.0551 0.0551 0.0220 0.0518 0.0220 | 0.0000 0.0088 0.0265 0.0392 0.0001 0.0122 0.0317 0.0420 0.0000 0.0092 0.0320 0.0447 0.0000 0.0093 0.0349 | 0.0456 0.0483 0.0477 0.0478 0.0478 0.0478 0.0478 0.0570 0.0570 0.0576 0.0548 0.0548 0.0512 0.0543 0.0574 0.0574 0.0329 0.0572 0.0587 |

Table 6: Ridge parameter estimated using $\hat{k}_{{\scriptscriptstyle K\!M\!6}}$

4.2 Analysis of the statistical power of the Granger causality test

The analysis of the power of the test is of central importance since a test will be of little use if it does not have enough power to reject a false null hypothesis. However, in the simulation part of this study it is detected that most applied tests in previous research suffer from serious size distortions for DGP 2 to DGP 4. Since it is meaningless to compare the power of biased test to power of unbiased tests, the power functions are only illustrated for tests that generally are unbiased in most of the cases. Thus, the power is only calculated when the parameters of the regression model is estimated using KM6 as ridge estimator together with the F test. In Figure 1 the power of the test when the lag length equals to two is showed and in Figure 2 we display the power when the lag length equals four. The most important factors for the power of the test are the degree of correlation, the sum of the causality parameters, the sample size and the lag length. All of those individual factors have positive impact on the power functions. Thus, the power becomes higher as any of these factors increases. The most remarkable positive effect has the degree of correlation. It is clear from the power functions that the new test is useful in the presence of multicolinearity.



Figure 1: Power of the F test using KM6 as ridge estimator when the lag length equals 2.



Figure 2: Power of the F test using KM6 as ridge estimator when the lag length equals 4.

5. Conclusions

This paper concludes that the traditional forms of the Granger causality test method overreject the true null hypothesis in the presence of multicollinearity. A new test named Ridge Regression Granger Causality (RRGC) test is suggested as a remedy to the problem. In order to compare the properties of all the Granger causality tests in this study a simulation experiment is conducted. The factors varied in the Monte Carlos simulation are the sample size, the lag length of the dynamic regression model and the degree of multicollinearity. For every applied DGP the performance of Wald (W), LR, LM, WC, LRC, LMC and the F-test are investigated when the regression model is estimated by OLS in comparison to ridge regression. The result of the analysis confirms that increasing the lag length or the degree of multicollinearity have a negative impact on the statistical size of the Granger causality test while increasing the sample size has a positive impact. The optimal method is to estimate the regression model by the use of KM6 as ridge estimator and by testing for Granger causality using the F-test. Thereafter, the power of the best test is calculated. The main factors that have an impact on the power of the test are the sum of the causality parameters, the sample size the lag length, and the degree of multicollinearity. A high value for these factors leads to higher power of the test. The main conclusion and essentially unique contribution of this paper is that multicollinearity causes over-rejections of the true null hypotheses for the traditional GC test and that the RRGC test can be used instead of traditional GC methods to gain control of the over-rejection of the null hypotheses in the presence of multicollinearity.

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