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## Joint tests for zero restrictions on nonnegative regression coefficients

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### SUMMARY

Three tests for zero restrictions on regression coefficients that are known to be nonnegative are considered: the classical  $F$  test, the likelihood ratio test, and a one-sided  $t$  test in a particular direction. Critical values for the likelihood ratio test are given for the cases of two and three restrictions, and the power function is calculated for the case of two restrictions. The analysis is conducted in terms of a characterization of the class of all similar tests for the problem, of which each of the above tests is a member. The likelihood ratio test emerges as the preferred test.

*Some key words:* Likelihood ratio test; One-sided alternative; Regression; Similar regions.

### 1. INTRODUCTION

There are numerous applications of the linear model in which the signs of at least some of the regression coefficients are known a priori. Without loss of generality we can assume that the coefficients of interest are known to be nonnegative. This paper is concerned with the problem of testing the joint null hypothesis that  $k \geq 2$  such coefficients are zero, against the alternative that they are nonnegative, in the context of the classical normal linear model. Writing the model as

$$y = X\beta + Z\gamma + u, \quad u \sim N(0, \sigma^2 I_n), \quad (1)$$

with  $X$  an  $n \times p$  matrix,  $Z$  an  $n \times k$  matrix, and  $W = (X, Z)$  of full column rank  $(p + k)$ , the problem of interest is that of testing  $H_0: \gamma = 0$  against the one-sided alternative  $H_a^+: \gamma > 0$ , where  $\gamma > 0$  means that  $\gamma_i \geq 0$  for each  $i = 1, \dots, k$ , with strict inequality for at least one  $i$ . Both the case of more general constraints on  $\eta' = (\beta', \gamma')$ , for example  $H_0: R\eta = r$  against  $R\eta \geq r$ ,  $R$  and  $r$  both known, and the case  $u \sim N(0, \sigma^2 \Omega)$ ,  $\Omega$  known, are easily transformed into this form.

A number of authors, notably Bartholomew (1959a, b; 1961), Chacko (1963), Kudô (1963), Nüesch (1966), Perlman (1969), Oosterhoff (1969) and Shorack (1967), have considered closely related multivariate one-sided testing problems. Oosterhoff (1969, § 3.1) gives results for the case  $\beta = 0$ , while Gourieroux, Holly & Monfort (1982) and Yancey, Judge & Bock (1981) have recently considered the same problem under the simplifying assumptions that the covariance matrix is completely known, in the former paper, or that the regressors are orthonormal, in the latter. Kudô (1963, § 5) claims to have characterized the likelihood ratio test for the case where  $\sigma^2$  in (1) is unknown, but we shall see later that Kudô's advice is incorrect.

In the present paper we assume that  $\sigma^2$  is unknown, and impose no special restrictions on  $X$  and  $Z$ . The paper is primarily concerned with the likelihood ratio test but we also

consider for comparison the traditional  $F$  test, which takes no account of the signs of the coefficients under the alternative, and a one-sided  $t$  test in a particular direction from the null. All three tests are similar tests for  $H_0$ , and we start with a characterization of the class of similar tests. The critical region for any similar test of  $H_0$  must be defined in terms of a statistic that measures the direction of any departure from  $H_0$ , and a statistic that measures the extent of any such departure. This immediately suggests ways of improving the  $F$  test, which is based purely on the latter statistic, when the alternative hypothesis is restricted to  $H_a^+$ , and also provides a very simple way of describing the critical region for the likelihood ratio test.

## 2. SIMILAR REGIONS

For testing  $H_0: \gamma = 0$  in (1) the parameters  $\beta$  and  $\sigma^2$  are nuisance parameters, but under  $H_0$  the statistics  $\hat{\beta}_0 = (X'X)^{-1}X'y$  and  $s_0^2 = y'M_x y$ , where  $M_x = I - X(X'X)^{-1}X'$ , are jointly sufficient for  $(\beta, \sigma^2)$  and the distribution of  $(\hat{\beta}_0, s_0^2)$  is complete. Hence, every size  $\alpha$  critical region  $\omega$  for testing  $H_0$  consists of a fraction  $\alpha$  of the surface content of the manifold in  $y$ -space defined by  $(\hat{\beta}_0, s_0^2) = \text{const}$ ; see Cox & Hinkley (1974, pp. 134-6). If attention is confined to similar regions the relevant density for the problem becomes the conditional density of  $y$  given  $\hat{\beta}_0$  and  $s_0^2$ , or the density of  $y$  on the manifold defined by  $(\hat{\beta}_0, s_0^2) = \text{const}$ .

We show in the Appendix that the manifold defined by  $(\hat{\beta}_0, s_0^2) = \text{const}$  has three components: the surface of the unit  $m$ -sphere,  $S_m: v'v = 1$ , where  $m = n - k - p$ , the surface of the unit  $k$ -sphere,  $S_k: h'h = 1$ , and the line segment  $0 \leq b \leq 1$ , where  $b$  is related to the usual  $F$  statistic for testing  $H_0$  by  $b = (kF/m)/(1 + kF/m)$ , and  $v$  and  $h$  are defined in the Appendix. Hence every similar region for testing  $H_0$  must consist of some fraction of the surface  $v'v = 1$ , some fraction of the surface  $h'h = 1$ , and some fraction of the line segment  $0 \leq b \leq 1$ .

The statistic  $v$  is independent of  $h$ ,  $b$  and  $s_0^2$ , and is uniformly distributed on  $S_m$ , whether or not  $H_0$  is true. It follows from this that the most powerful critical regions must include the entire surface  $v'v = 1$ , so that attention may be confined to critical regions defined in terms of  $h$  and  $b$  alone.

Under  $H_0$ ,  $h$ ,  $b$  and  $s_0^2$  are mutually independent,  $h$  is uniformly distributed on  $S_k$ ,  $b$  has the beta distribution  $B(\frac{1}{2}k, \frac{1}{2}m)$ , and  $s_0^2/\sigma^2 \sim \chi^2(m+k)$ . Hence, as expected, the conditional distribution of  $y$  given  $\hat{\beta}_0$  and  $s_0^2$  is free of nuisance parameters when  $H_0$  is true. Under the general alternative  $H_a: \gamma \neq 0$  the conditional density of  $h$  and  $b$  given  $s_0^2$  is

$$p(h, b | s_0^2) = K_1 b^{k-1} (1-b)^{m-1} \exp(s_0 b^{\frac{1}{2}} h' \bar{\gamma} / \sigma^2), \quad (2)$$

where  $\bar{\gamma} = T\gamma$ , with  $T$  as defined in the Appendix, and

$$K_1 = \Gamma(\frac{1}{2}k) [2\pi^{\frac{1}{2}k} B(\frac{1}{2}k, \frac{1}{2}m) \Sigma(\frac{1}{4}\lambda s_0^2 / \sigma^2)^j \{j!(\frac{1}{2}m + \frac{1}{2}k)_j\}^{-1}]^{-1},$$

with  $(a)_j = a(a+1) \dots (a+j-1)$  and  $\lambda = \bar{\gamma}'\bar{\gamma} / \sigma^2$ . The statistic  $h$  may be interpreted as a measure of the direction of any departure from  $H_0$ , while  $b$ , or  $F$ , is a measure of the extent of any such departure.

## 3. THE $F$ TEST AND DIRECTED $t$ TESTS

Applying the Neyman-Pearson Lemma to the density (2) shows that the best similar region for testing  $H_0$  against the specific alternative  $\gamma = \gamma^* > 0$  consists of large values

of  $b^{\frac{1}{2}} \cos \theta^*$ , where  $\theta^*$  is the angle between  $h$  and the unit vector  $\mu^* = \bar{\gamma}^*/(\bar{\gamma}^{*\prime} \bar{\gamma}^*)^{\frac{1}{2}}$ . This has the following well-known consequences:

- (i) if  $k = 1$  the one-sided  $t$  test that rejects  $H_0$  for large positive values of  $b^{\frac{1}{2}}h$  is uniformly most powerful similar;
- (ii) if  $k > 1$  there is no uniformly most powerful similar test for  $H_0$ , whether or not the alternative is restricted to  $H_a^+$ ;
- (iii) if  $k > 1$  and, under  $H_a$ ,  $\gamma = \delta\gamma^*$ , with  $\gamma^* > 0$  known and  $\delta \geq 0$ , the best similar region consists of large positive values of  $b^{\frac{1}{2}} \cos \theta^*$ .

This is equivalent to a one-sided  $t$  test of  $\delta = 0$  against  $\delta > 0$  in the equation  $y = X\beta + \delta Z\gamma^* + u$ , because the  $t$  statistic for this problem is

$$(m+k-1)^{\frac{1}{2}} b^{\frac{1}{2}} \cos \theta^* / (1 - b \cos^2 \theta^*)^{\frac{1}{2}}. \quad (3)$$

For testing  $H_0$  against  $H_a^+$ , (iii) above suggests that the following strategy may yield a reasonable test: choose a particular vector  $\gamma^*$  in the region  $\gamma > 0$ , and simply use a one-sided  $t$ -test for  $\delta = 0$  against  $\delta > 0$  in the equation  $y = X\beta + \delta Z\gamma^* + u$ . The resulting test is evidently locally most powerful similar in directions close to that of  $\gamma^*$ , and might be expected to have reasonable power over the whole region  $\gamma > 0$ . We discuss this approach in more detail in § 5 below.

Let  $\mu = \bar{\gamma}/(\bar{\gamma}'\bar{\gamma})^{\frac{1}{2}}$  be the point on  $S_k$  determined by the true vector  $\bar{\gamma}$ ;  $\mu$  indicates the direction in which the true vector  $\bar{\gamma}$  lies, and  $\mu$  and  $\lambda$  are the population analogues of  $h$  and  $F$ . From (2), the conditional power, given  $s_0^2$ , of a critical region  $\omega$  is given by

$$P_{\omega}(s_0^2) = \int_{\omega} K_1 b^{\frac{1}{2}k-1} (1-b)^{\frac{1}{2}m-1} \exp\{(\lambda b s_0^2)^{\frac{1}{2}} h'\mu\} db(dh), \quad (4)$$

where  $(dh)$  denotes the invariant measure on the surface of the unit  $k$ -sphere (James, 1954). Using (4) it is easy to show that the power of the test depends only upon  $\lambda$  if and only if  $\omega$  includes the entire surface of the  $S_k$ :  $h'h = 1$ , a result due to Wolfowitz (1949). It is well known that the traditional  $F$  test has precisely this property. In fact, on integrating (4) over  $h'h = 1$ , and then integrating out  $s_0^2$ , it follows that the  $F$  test is uniformly most powerful among similar tests whose power depends only upon  $\lambda$  (Hsu, 1941).

Now notice that  $h'\mu = \cos \bar{\theta}$ , where  $\bar{\theta}$  is the angle between  $h$  and  $\mu$ . For any fixed  $\mu$ , that is, for  $\bar{\gamma}$  in any fixed direction,  $\cos \bar{\theta}$  ranges over the entire interval  $-1 \leq \cos \bar{\theta} \leq 1$  as  $h$  ranges over  $S_k$ , so that the power of the  $F$  test is in fact diminished by the inclusion in the critical region of that part of  $S_k$  for which  $\cos \bar{\theta}$  is negative. Of course, if the direction  $\mu$  of  $\bar{\gamma}$  is arbitrary, this observation is nugatory, but for the problem of testing  $H_0$  against  $H_a^+$  it suggests that a test which excludes that part of the  $S_k$ :  $h'h = 1$  for which  $\cos \bar{\theta}$  must be negative from the critical region is likely to improve upon the  $F$  test. We shall now show that the likelihood ratio test does exactly that, and does indeed improve upon the  $F$  test.

#### 4. THE LIKELIHOOD RATIO TEST

##### 4.1. Critical regions

After maximizing the likelihood with respect to the nuisance parameters  $\beta$  and  $\sigma^2$  we find the profile likelihood to be proportional to

$$L = \{s_0^2 + l^2 - 2ls \cos \bar{\theta}\}^{-\frac{1}{2}n}, \quad (5)$$

where  $l = (\bar{\gamma}'\bar{\gamma})^{\frac{1}{2}}$  denotes the length of  $\bar{\gamma}$  and the other notation is as in § 3 and the Appendix. Now, the region  $\gamma > 0$  for  $\bar{\gamma}$  corresponds to a subset of the surface of the unit sphere  $S_k: \mu'\mu = 1$ , say  $S_a$ . Provided the 'direction'  $\mu = 0$  is admitted as a possibility, the problem of maximizing (5) with respect to  $\gamma$ , subject to  $\gamma > 0$ , is equivalent to that of maximizing (5) first with respect to the direction,  $\mu$ , of  $\bar{\gamma}$ , subject to  $\mu \in S_a$ , then with respect to its length,  $l$ . But, if  $h \in S_a$  it is clear at once that (5) is maximized by choosing  $\mu = h$ , so that  $\cos \bar{\theta} = 1$ , and  $l = s$ , giving a maximum of  $\{s_0^2(1-b)\}^{-\frac{1}{2}n}$ .

Let  $\bar{S}_a$  denote the subset of the  $S_k: h'h = 1$  for which  $\cos \bar{\theta} = h'\mu$  must be negative when  $\mu \in S_a$ . That is,  $\bar{S}_a$  is the set of points  $h$  on  $S_k$  that make an angle greater than  $\frac{1}{2}\pi$  with every point  $\mu \in S_a$ . Clearly, if  $h \in \bar{S}_a$ , (5) is maximized by setting  $\mu = 0$ , and hence  $l = 0$ , giving a maximum of  $(s_0^2)^{-\frac{1}{2}n}$ .

If  $h$  is in neither  $S_a$  nor  $\bar{S}_a$ , so that  $\mu$  cannot be chosen to give  $\bar{\theta} = 0$ , but can be chosen so that  $\bar{\theta} \leq \frac{1}{2}\pi$ , then (5) is clearly maximized by choosing  $\mu$  on the edge of  $S_a$  so as to minimize the angle between  $\mu$  and the given point  $h$ . We denote such a choice for  $\mu$  by  $\tilde{\mu}_h$ , and it is clear that (5) is then maximized by setting  $l = sh'\tilde{\mu}_h$ , giving a maximum of  $[s_0^2\{1 - b(h'\tilde{\mu}_h)^2\}]^{-\frac{1}{2}n}$ .

Since the maximized value of the likelihood under  $H_0$  is proportional to  $\{s_0^2\}^{-\frac{1}{2}n}$ , the critical region for the likelihood ratio test has the following form:

$$\omega_{LR}: \begin{cases} b > c & (h \in S_a), \\ b(h'\tilde{\mu}_h)^2 > c & (h \in (S_k - S_a - \bar{S}_a)), \end{cases} \quad (6)$$

where  $c$  is a suitably chosen critical value.

Notice that, because  $\omega_{LR}$  is defined in terms of  $b$  and  $h$ , the likelihood ratio test is a member of the class of similar tests for  $H_0$  against  $H_a^+$ . Also, since points  $h \in \bar{S}_a$  are not included in the critical region,  $\omega_{LR}$  excludes precisely those points  $h$  on  $S_k$  for which  $\cos \bar{\theta}$  must be negative when  $\mu \in S_a$ .

The results above define the maximum likelihood estimates for  $\gamma$ ,  $\beta$  and  $\sigma^2$ , subject to  $\gamma > 0$ . The details are easily deduced from the results that follow for the cases  $k = 2, 3$  and are omitted.

#### 4.2. The case $k = 2$

Let  $Z = (z_1, z_2)$ , and write

$$Z'M_x Z = \begin{bmatrix} \sigma_1^2 & \sigma_1\sigma_2\rho \\ \sigma_1\sigma_2\rho & \sigma_2^2 \end{bmatrix}, \quad T = \begin{bmatrix} \sigma_1 & \sigma_2\rho \\ 0 & \sigma_2(1-\rho^2)^{\frac{1}{2}} \end{bmatrix},$$

where  $\sigma_i^2 = z_i'M_x z_i$  ( $i = 1, 2$ ) and  $\rho = (z_1'M_x z_2)/(\sigma_1\sigma_2)$ . The region  $\gamma > 0$  corresponds to the region  $\{\bar{\gamma}_1 \geq \rho\bar{\gamma}_2/(1-\rho^2)^{\frac{1}{2}}, \bar{\gamma}_2 \geq 0\}$ , where  $\bar{\gamma}' = (\bar{\gamma}_1, \bar{\gamma}_2)$ . Writing  $\mu' = (\mu_1, \mu_2)$ , the region  $S_a$  for  $\mu$  is an arc on the positive semicircle for  $\mu_2$  that subtends an angle  $a = \cos^{-1} \rho$ , measured clockwise from the vertical axis; see Fig. 1.

The region  $(S_2 - S_a - \bar{S}_a)$  has two components,  $S'_a$  and  $S''_a$  in Fig. 1. For  $h \in S'_a$ ,  $\tilde{\mu}_h = (1, 0)$ , while, for  $h \in S''_a$ ,  $\tilde{\mu}_h = (\rho, (1-\rho^2)^{\frac{1}{2}})$ . In terms of the elements of  $\hat{\gamma}' = (\hat{\gamma}_1, \hat{\gamma}_2)$  the regions  $S_a, S'_a, S''_a$  are

$$S_a: \hat{\gamma}_1 \geq 0, \quad \hat{\gamma}_2 \geq 0; \quad S'_a: \sigma_1\hat{\gamma}_1 + \sigma_2\rho\hat{\gamma}_2 \geq 0, \quad \hat{\gamma}_2 \leq 0; \\ S''_a: \sigma_1\rho\hat{\gamma}_1 + \sigma_2\hat{\gamma}_2 \geq 0, \quad \hat{\gamma}_1 \leq 0.$$

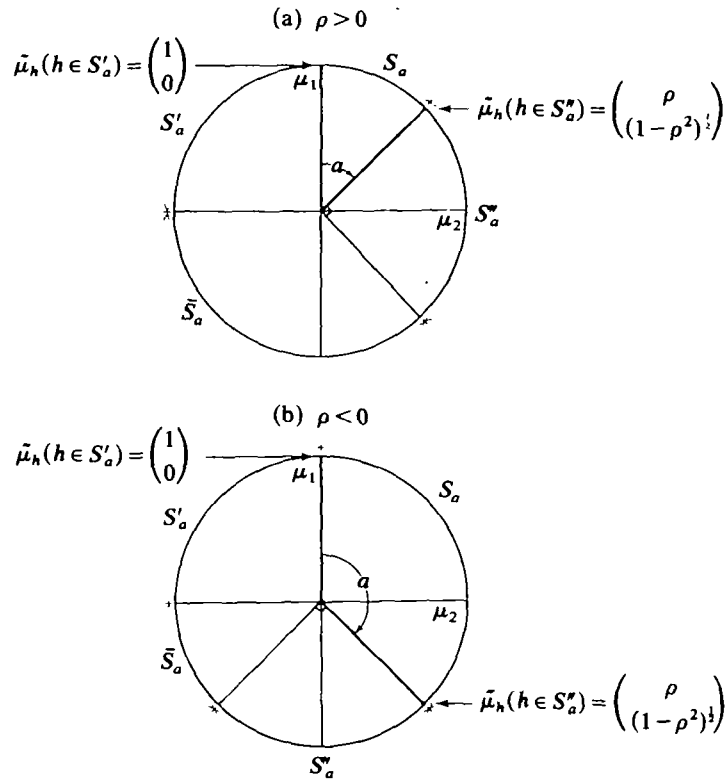


Fig. 1. Regions  $S_a$ ,  $S'_a$ ,  $S''_a$  and  $\bar{S}_a$  when  $\rho > 0$  and  $\rho < 0$ .

Using (3) and the fact that  $b = (kF/m)(1 + kF/m)^{-1}$ , the critical region (6) has the form

$$\omega_{LR}: \begin{cases} F > f & (\hat{\gamma} \in S_a), \\ t_1^2 > 2(m+1)f/m & (\hat{\gamma} \in S'_a), \\ t_2^2 > 2(m+1)f/m & (\hat{\gamma} \in S''_a), \end{cases}$$

where  $t_i$  is the  $t$  statistic for the coefficient of  $z_i$  in the regression of  $y$  on  $X$  and  $z_i$  alone, and the critical value  $c$  in (6) is related to  $f$  by  $c = (2f/m)(1 + 2f/m)^{-1}$ .

It is important that the boundary of  $S_a$  corresponds to points where, in the original parameter space, one or other of the elements of  $\gamma$  is zero, and the likelihood ratio test explicitly takes this into account in the denominators of  $t_1^2$  and  $t_2^2$ . The tests of Kudô (1963, § 5) and Yancey, Judge & Bock (1981) do not incorporate this adjustment and hence are not the likelihood ratio test.

The critical value  $c$ , and hence  $f$ , is determined by the equation

$$\alpha = \int_{\omega_{LR}} \frac{(1-b)^{1/2 m-1}}{2\pi B(1, \frac{1}{2}m)} db(dh),$$

where  $\alpha$  is the chosen level of significance. From the results above we see that this integral has three components, with regions of integration

$$\{b > c; h \in S_a\}, \quad \{b(h'\tilde{\mu}_1)^2 > c; h \in S'_a\}, \quad \{b(h'\tilde{\mu}_2)^2 > c; h \in S''_a\},$$

respectively, where  $\tilde{\mu}'_1 = (1, 0)$  and  $\tilde{\mu}'_2 = (\rho, (1 - \rho^2)^{1/2})$ .

Now, the invariant differential form ( $dh$ ) on, in this case,  $S_2$ , may be decomposed (James, 1954, pp. 57-8) into ( $dh$ ) =  $d\theta$ , where  $\theta$  is the angle, measured in a clockwise direction, between any conveniently chosen fixed point on  $S_2$  and  $h$ . For the first of the above regions we measure  $\theta$  from the vertical axis and we have at once

$$\int_{b>c} \int_0^a \frac{(1-b)^{\frac{1}{2}m-1}}{2\pi B(1, \frac{1}{2}m)} db d\theta = \frac{a}{2\pi} \int_{b>c} \frac{(1-b)^{\frac{1}{2}m-1}}{B(1, \frac{1}{2}m)} db$$

$$= \frac{a}{2\pi} \text{pr} \{F(2, m) > f\},$$

where  $f = \frac{1}{2}mc/(1-c)$ .

For the third region we measure  $\theta$  from the point  $\tilde{\mu}_2$  and we have, on putting  $b_1 = b \cos^2 \theta$ ,  $b_2 = b \sin^2 \theta$ ,

$$\int_{b_1>c} \int_0^{1-b_1} \frac{b_1^{-\frac{1}{2}} b_2^{-\frac{1}{2}} (1-b_1-b_2)^{\frac{1}{2}m-1}}{4\pi B(1, \frac{1}{2}m)} db_2 db_1 = \frac{1}{4} \int_{b_1>c} \frac{b_1^{-\frac{1}{2}} (1-b_1)^{\frac{1}{2}m-1}}{B(\frac{1}{2}, \frac{1}{2}m + \frac{1}{2})} db_1$$

$$= \frac{1}{4} \text{pr} \{F(1, m+1) > f_1\},$$

where  $f_1 = (m+1)c/(1-c) = 2(m+1)f/m$ . It is easy to check that the contribution of the second region is identical to that of the third, so that the critical value  $f$  is the solution to the equation

$$\alpha = \frac{\cos^{-1} \rho}{2\pi} \text{pr} \{F(2, m) > f\} + \frac{1}{2} \text{pr} \{F(1, m+1) > 2(m+1)f/m\}. \tag{7}$$

Note that (7) admits a solution for  $f$  only if  $\alpha < \frac{1}{2}\{1 + (\cos^{-1} \rho)/\pi\}$ . This, of course, is unlikely to present any difficulty in practice; it is a consequence of the fact that  $\omega_{LR}$  explicitly excludes part of the  $S_2$ :  $h'h = 1$ . Table 1 gives selected critical values,  $f$ , calculated from (7) for various values of  $\rho$  and  $m$ , and for  $\alpha = 0.05$  and  $\alpha = 0.01$ .

The last two lines in Table 1 give the comparable critical values for the  $F$  test, and it is striking that these can be much larger than those for the likelihood ratio test. Thus, in the case where it turns out that  $\hat{\gamma}_1 \geq 0$ ,  $\hat{\gamma}_2 \geq 0$ , and it is known that  $\gamma_1, \gamma_2 \geq 0$ , the acceptance region for the  $F$  test can be much too large. We shall see shortly that this is reflected in a comparison of the power of the two tests.

### 4.3. The case $k = 3$

Let  $Z = (z_1, z_2, z_3)$ , and write

$$Z' M_x Z = \begin{bmatrix} \sigma_1^2 & \sigma_1 \sigma_2 \rho_{12} & \sigma_1 \sigma_3 \rho_{13} \\ \sigma_1 \sigma_2 \rho_{12} & \sigma_2^2 & \sigma_2 \sigma_3 \rho_{23} \\ \sigma_1 \sigma_3 \rho_{13} & \sigma_2 \sigma_3 \rho_{23} & \sigma_3^2 \end{bmatrix},$$

where  $\sigma_i^2 = z_i' M_x z_i$  ( $i = 1, 2, 3$ ) and  $\rho_{ij} = z_i' M_x z_j / (\sigma_i \sigma_j)$  ( $i, j = 1, 2, 3$ ). The matrix  $T$  is given by

$$T = \begin{bmatrix} \sigma_1 & \sigma_2 \rho_{12} & \sigma_3 \rho_{13} \\ 0 & \sigma_2 (1 - \rho_{12}^2)^{\frac{1}{2}} & \sigma_3 \rho_{23.1} (1 - \rho_{13}^2)^{\frac{1}{2}} \\ 0 & 0 & \sigma_3 (1 - \rho_{13}^2)^{\frac{1}{2}} (1 - \rho_{23.1}^2)^{\frac{1}{2}} \end{bmatrix},$$

and  $\rho_{ij.k} = (\rho_{ij} - \rho_{ik} \rho_{jk}) / \{(1 - \rho_{ik}^2)(1 - \rho_{jk}^2)\}^{\frac{1}{2}}$ .

Table 1. 5% and 1% critical values for the likelihood ratio test:  $k = 2$ 

$\rho$		$m = 10$	$m = 15$	$m = 20$	$m = 30$	$m = 50$
0.9	5%	1.83	1.76	1.72	1.69	1.66
	1%	4.03	3.68	3.51	3.36	3.24
0.7	5%	2.08	1.98	1.93	1.89	1.85
	1%	4.46	4.02	3.82	3.63	3.48
0.5	5%	2.25	2.13	2.07	2.02	1.97
	1%	4.73	4.23	4.01	3.80	3.64
0.3	5%	2.39	2.25	2.18	2.12	2.07
	1%	4.95	4.40	4.16	3.93	3.76
0.1	5%	2.51	2.35	2.28	2.21	2.16
	1%	5.14	4.55	4.29	4.04	3.86
0.0	5%	2.56	2.40	2.33	2.25	2.20
	1%	5.23	4.62	4.35	4.10	3.91
-0.1	5%	2.62	2.45	2.37	2.29	2.24
	1%	5.31	4.69	4.41	4.15	3.95
-0.3	5%	2.73	2.54	2.46	2.37	2.31
	1%	5.48	4.81	4.52	4.25	4.04
-0.5	5%	2.84	2.64	2.55	2.46	2.39
	1%	5.65	4.94	4.63	4.35	4.13
-0.7	5%	2.96	2.74	2.64	2.54	2.47
	1%	5.83	5.08	4.75	4.45	4.23
-0.9	5%	3.11	2.87	2.76	2.66	2.57
	1%	6.06	5.26	4.91	4.58	4.35
$F$		4.10	3.68	3.49	3.32	3.18
		7.56	6.36	5.85	5.39	5.06

Linear interpolation between successive  $\rho$  values for fixed  $m$  is extremely accurate.

The region  $\gamma > 0$  corresponds to the region  $\{\bar{\gamma} - c_1\bar{\gamma}_2 - c_2\bar{\gamma}_3 \geq 0; \bar{\gamma}_2 - c_3\bar{\gamma}_3 \geq 0; \bar{\gamma}_3 \geq 0\}$  with  $c_1 = \rho_{12}/(1 - \rho_{12}^2)^{1/2}$ ,  $c_2 = \rho_{13.2}/(1 - R_{1.23}^2)^{1/2}$  and  $c_3 = \rho_{23.1}/(1 - \rho_{23.1}^2)^{1/2}$ , where  $1 - R_{1.23}^2 = (1 - \rho_{12}^2)(1 - \rho_{13.2}^2) = (1 - \rho_{12}^2)(1 - \rho_{13}^2)(1 - \rho_{23.1}^2)/(1 - \rho_{23}^2)$ .

The regions  $S_a$  for  $\mu$  is the region  $ABC$  in Fig. 2 which is drawn for the case  $\rho_{12} > 0$ ,  $\rho_{23.1} > 0$ ,  $\rho_{13.2} > 0$ . The region  $\bar{S}_a$  may be described as follows: draw three 'equators'  $EA$ ,  $EB$  and  $EC$  with  $A$ ,  $B$  and  $C$  respectively as 'north poles'. The southernmost unbroken line that can be drawn while remaining on one of these 'equators' is the northern boundary of  $\bar{S}_a$ .

The points  $A$ ,  $B$  and  $C$  are

$$A = \{1, 0, 0\}, \quad B = \{\rho_{13}, \rho_{23.1}(1 - \rho_{13}^2)^{1/2}, (1 - \rho_{13}^2)^{1/2}(1 - \rho_{23.1}^2)^{1/2}\}, \\ C = \{\rho_{12}, (1 - \rho_{12}^2)^{1/2}, 0\}.$$

The coordinates of  $A'$ ,  $B'$  and  $C'$  are easily deduced from the obvious orthogonality relations with  $A$ ,  $B$  and  $C$ . The line  $BB'$ , for example, represents the locus of the points of tangency between latitudes drawn with  $B$  as 'north pole' and latitudes drawn with  $B'$  as 'north pole', so that points in  $BB'C'$  are closest, in terms of angular distance, to  $B$ , while points in  $AB'B$  are closest to points on the edge  $AB$  of  $S_a$ . Thus, for  $h \in BB'C'$ ,  $\tilde{\mu}_h$  is at  $B$ , while, for  $h \in AB'B$ ,  $\tilde{\mu}_h$  is a point on the edge  $AB$  of  $S_a$ . Similar remarks hold for the other four regions depicted in Fig. 2.



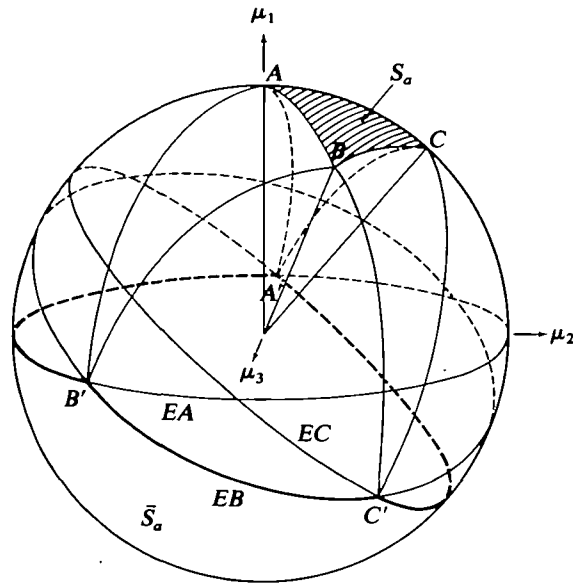


Fig. 2. Regions  $S_a$  and  $\bar{S}_a$  when  $\rho_{12} > 0, \rho_{13} > 0, \rho_{23} > 0$ .

The six components of  $(S_3 - S_a - \bar{S}_a)$  can be expressed in terms of the elements of  $\hat{\gamma}' = (\hat{\gamma}_1, \hat{\gamma}_2, \hat{\gamma}_3)$  by using the definition of  $h$  in terms of  $\hat{\gamma}$ . The results are summarized in Table 2, which also gives the appropriate test statistic and critical value for each section of  $(S_3 - S_a - \bar{S}_a)$ .

Table 2. Critical region for the likelihood ratio test:  $k = 3$

Region	Test statistic	Critical value
I $\hat{\gamma}_1 \geq 0, \hat{\gamma}_2 \geq 0, \hat{\gamma}_3 \geq 0$	$F$	$f$
II $\sigma_i(1 - \rho_{ij}^2)^{1/2} \hat{\gamma}_i + \sigma_k \rho_{ikj}(1 - \rho_{jk}^2)^{1/2} \hat{\gamma}_k \geq 0,$ $\sigma_j(1 - \rho_{ij}^2)^{1/2} \hat{\gamma}_j + \sigma_k \rho_{jk i}(1 - \rho_{ik}^2)^{1/2} \hat{\gamma}_k \geq 0,$ $\hat{\gamma}_k \leq 0$	$F_{ij}$	$\frac{3}{2}(m+1)f/m$
III $\sigma_i \hat{\gamma}_i + \sigma_j \rho_{ij} \hat{\gamma}_j + \sigma_k \rho_{ik} \hat{\gamma}_k \geq 0,$ $\sigma_j \rho_{jk i}(1 - \rho_{ij}^2)^{1/2} \hat{\gamma}_j + \sigma_k(1 - \rho_{ik}^2)^{1/2} \hat{\gamma}_k \leq 0,$ $\sigma_j(1 - \rho_{ij}^2)^{1/2} \hat{\gamma}_j + \sigma_k \rho_{jk i}(1 - \rho_{ik}^2)^{1/2} \hat{\gamma}_k \leq 0$	$t_i^2$	$3(m+2)f/m$
II: $(i, j) = (1, 2), (1, 3), (2, 3); k = 3, 2, 1.$		
III: $i = 1, 2, 3; (j, k) = (2, 3), (1, 3), (1, 2).$		

In Table 2,  $F_{ij}$  is the  $F$  statistic that would be used to test the joint significance of  $z_i$  and  $z_j$  in the regression of  $y$  on  $X, z_i$  and  $z_j$ , with  $z_k$  excluded, and  $t_i$  is the  $t$  statistic for the coefficient of  $z_i$  in the regression of  $y$  on  $X$  and  $z_i$  alone. The critical value  $c$  in (6) is related to  $f$  in Table 2 by  $c = (3f/m)(1+3f/m)^{-1}$ . As before, the use of  $F_{ij}$  and  $t_i$  explicitly acknowledges that, on the boundary of  $S_a$ , one or more elements of  $\gamma$  are zero.

The integral that defines the critical value,  $c$ , for the test decomposes in this case into seven components, and the invariant measure  $(dh)$  on  $S_3$  decomposes as  $(dh) = \sin \theta_1 d\theta_1 d\theta_2$ , where  $\theta_1$  is the angle between  $h$  and a fixed point  $\mu_0$ , say, on  $S_3$ , and  $\theta_2$  is the angle between the unit vector lying along the orthogonal projection of  $h$  onto the  $S_2$  orthogonal to  $\mu_0$  and a point  $\bar{\mu}_0$ , say, in that  $S_2$ . By judiciously choosing the points  $\mu_0$  and  $\bar{\mu}_0$ , the components of the integral can be calculated in exactly the same manner

as was used in § 4.2 above for the case  $k=2$ . Thus we find that the critical value  $f$  in Table 2 is defined by

$$\begin{aligned} \alpha = & \frac{1}{4\pi} [\{\cos^{-1} \rho_{12,3} + \cos^{-1} \rho_{13,2} + \cos^{-1} \rho_{23,1} - \pi\} \text{pr} \{F(3, m) > f\} \\ & + \{\cos^{-1} \rho_{12} + \cos^{-1} \rho_{13} + \cos^{-1} \rho_{23}\} \text{pr} \{F(2, m+1) > \frac{3}{2}(m+1)f/m\} \\ & + \{\cos^{-1} (-\rho_{12,3}) + \cos^{-1} (-\rho_{13,2}) + \cos^{-1} (-\rho_{23,1})\} \\ & \times \text{pr} \{F(1, m+2) > 3(m+2)f/m\}]. \end{aligned} \quad (8)$$

As in the case  $k=2$ , equation (8) admits a solution for  $f$  only if  $\alpha < \frac{1}{2}\{1 + (\cos^{-1} \rho_{12} + \cos^{-1} \rho_{13} + \cos^{-1} \rho_{23})/(2\pi)\}$ , but this constraint is unlikely to be of practical importance. Table 3 gives a small selection of critical values,  $f$ , calculated from (8).

Table 3. Some 5% critical values for the likelihood ratio test:  $k=3$

$\rho_{12}$	$\rho_{13}$	$\rho_{23}$	$m=10$	$m=15$	$m=20$	$m=30$	$m=50$
0.9	0.9	0.9	1.23	1.21	1.21	1.20	1.19
0.9	0.6	0.3	1.50	1.46	1.44	1.42	1.41
0.9	0.1	-0.1	1.71	1.65	1.63	1.60	1.57
0.6	-0.5	-0.3	2.14	2.02	1.97	1.91	1.87
-0.1	-0.5	-0.3	2.52	2.35	2.26	2.18	2.12
-0.3	-0.5	-0.5	2.80	2.57	2.55	2.44	2.36
-0.9	-0.5	0.1	3.00	2.74	2.62	2.50	2.41
0.0	0.0	0.0	2.15	2.03	1.98	1.92	1.88
		$F$	3.71	3.29	3.10	2.92	2.79

Again, it is striking that the likelihood ratio critical values can be much smaller than those of the traditional  $F$  test, the differences being greatest when  $\rho_{12}$ ,  $\rho_{13}$  and  $\rho_{23}$  are all large and positive.

#### 4.4. Power function: $k=2$

As in the case of the size of the test, the conditional power function, given  $s_0^2$ ,

$$P_{LR}(s_0^2) = \int_{\omega_{LR}} K_1(1-b)^{1/2m-1} \exp\{(\lambda b s_0^2)^{1/2} h' \mu / \sigma\} db(dh),$$

decomposes into three components, with regions of integration

$$\{b > c; h \in S_a\}, \quad \{b(h' \tilde{\mu}_1)^2 > c; h \in S'_a\}, \quad \{b(h' \tilde{\mu}_2)^2 > c; h \in S''_a\}.$$

Consider first the last of these regions. Setting  $(dh) = d\theta$ , as before,  $\theta$  with the angle, measured in a clockwise direction, between  $\tilde{\mu}_2$  and  $h$ , the contribution to the conditional power from this region is simply

$$\iint_R K_1(1-b)^{1/2m-1} \exp\{(\lambda b s_0^2)^{1/2} \cos(\theta + a - \theta_0) / \sigma\} db d\theta,$$

where  $R = \{b \cos^2 \theta > c; 0 \leq \theta \leq \frac{1}{2}\pi\}$ ,  $\theta_0$  is the angle between the vertical axis and  $\mu$ , and  $a = \cos^{-1} \rho$ . Transforming to  $b_1 = b \cos^2 \theta$ ,  $b_2 = b \sin^2 \theta$  and evaluating the integral gives, after averaging with respect to the density of  $s_0^2$ , the contribution of this region to

the unconditional power of the test. It is easy to see that the contribution of the second region is identical to that of the third except that  $(a - \theta_0)$  is replaced by  $\theta_0$  itself. Hence we find that the contribution from these two regions is

$$\frac{1}{2}e^{-\lambda/2} \sum_{i,j=0}^{\infty} \frac{(\frac{1}{2}\lambda)^{\frac{1}{2}i+\frac{1}{2}j}(-1)^j}{\Gamma(\frac{1}{2}i+1)\Gamma(\frac{1}{2}j+1)} K_{ij}(\theta_0) I_{1-c}(\frac{1}{2}m+\frac{1}{2}j+\frac{1}{2}, \frac{1}{2}i+\frac{1}{2}), \tag{9}$$

where

$$K_{ij}(\theta_0) = \frac{1}{2}\{\cos^i(a - \theta_0) \sin^j(a - \theta_0) + \cos^i \theta_0 \sin^j \theta_0\} \tag{10}$$

and  $I_u(a, b)$  denotes the incomplete beta integral with parameters  $a$  and  $b$  and upper limit  $u$ .

Turning next to the first region, we again put  $(dh) = d\theta$  but in this case measure  $\theta$  from the vertical axis, i.e. from  $\tilde{\mu}_1$ , so that  $h'\mu = \cos(\theta - \theta_0)$  and  $0 \leq \theta \leq a$ . Provided both  $\theta_0$  and  $a - \theta_0$  are less than  $\frac{1}{2}\pi$  the calculation is straightforward and gives, after averaging with respect to the density of  $s_0^2$ , the unconditional power deriving from the region  $\{b > c; h \in S_a\}$  to be

$$\frac{1}{2}e^{-\lambda} \sum_{j=0}^{\infty} \frac{(\frac{1}{2}\lambda)^{\frac{1}{2}j}}{\Gamma(\frac{1}{2}j+1)} J_j(\theta_0) I_{1-c}(\frac{1}{2}m, \frac{1}{2}j+1) \tag{11}$$

where

$$J_j(\theta_0) = \frac{1}{2}\{I_{\sin^2 \theta_0}(\frac{1}{2}, \frac{1}{2}j+\frac{1}{2}) + I_{\sin^2(a-\theta_0)}(\frac{1}{2}, \frac{1}{2}j+\frac{1}{2})\}. \tag{12}$$

Since both  $\theta_0$  and  $(a - \theta_0)$  must be less than  $\frac{1}{2}\pi$  when  $\rho > 0$ , expressions (11) and (12) are valid when  $\rho > 0$ . When  $\rho < 0$  either  $\theta_0$  or  $(a - \theta_0)$  can exceed  $\frac{1}{2}\pi$ , and in that case  $J_j(\theta_0)$  in (11) is replaced, for even values of  $j$ , by

$$J_j^*(\theta_0) = \begin{cases} \frac{1}{2}\{I_{\sin^2 \theta_0}(\frac{1}{2}, \frac{1}{2}j+\frac{1}{2}) + 2 - I_{\sin^2(a-\theta_0)}(\frac{1}{2}, \frac{1}{2}j+\frac{1}{2})\} & (a - \theta_0 > \frac{1}{2}\pi), \\ \frac{1}{2}\{I_{\sin^2(a-\theta_0)}(\frac{1}{2}, \frac{1}{2}j+\frac{1}{2}) + 2 - I_{\sin^2 \theta_0}(\frac{1}{2}, \frac{1}{2}j+\frac{1}{2})\} & (\theta_0 > \frac{1}{2}\pi). \end{cases} \tag{13}$$

The total power of the test is given by the sum of expressions (9) and (11), and is evidently a function of  $\lambda$ ,  $m$  and  $\theta_0$ , with  $\theta_0$  reflecting the direction in which the true vector  $\tilde{\gamma}$  lies. From (10), (12) and (13) it follows that the power function is symmetric with respect to  $\theta_0$  about the point  $\theta_0 = \frac{1}{2}a$ , is maximized with respect to  $\theta_0$  when  $\theta_0 = \frac{1}{2}a$ , and is minimized with respect to  $\theta_0$  when  $\theta_0 = a$ . Some power calculations based on (9)-(13) are in Table 4. Comparison with the last two lines of Table 5 shows that the likelihood ratio test is superior to the  $F$  test over the whole range for  $\rho$ , and that the improvement in power in the likelihood ratio test is substantial when  $\rho$  is large and positive.

The power function for the case  $k = 3$  can be obtained by an obvious generalization of the argument above. We omit details and merely note that, since the source of the improvement in power is the same in  $k \geq 3$  dimensions as it is in the case  $k = 2$ , there are good grounds for expecting that the above conclusions will remain valid in general.

### 5. DIRECTED $t$ TESTS

We consider next the test suggested in § 3, a one-sided  $t$  test based on a preselected vector,  $\gamma^*$  say, in the feasible region under  $H_a^+$ . From (3), this test rejects  $H_0$  when  $b^{\frac{1}{2}}h'\mu^* = b^{\frac{1}{2}}\cos \theta^*$  is large and positive. Hence, the critical region for the test is  $\omega^* = \{b^{\frac{1}{2}}\cos \theta^* > c, h \in S^*\}$ , where  $S^*$  is the set of points on the  $S_k: h'h = 1$  which make an angle less than  $\frac{1}{2}\pi$  with  $\mu^*$ . Notice that, since  $\mu^* \in S_a$ ,  $S^*$  excludes all of  $\bar{S}_a$ , and also

Table 4. Power of the likelihood ratio test:  $k = 2, \alpha = 0.05, \lambda = 2, 8$

$\rho$	$a$	$\lambda$	$\theta_0$	$m = 10$	$m = 15$	$m = 20$	$m = 30$	$m = 50$
0.9	0.4510	2	$a$	0.358	0.369	0.375	0.381	0.386
		2	$\frac{1}{2}a$	0.370	0.380	0.386	0.391	0.396
		8	$a$	0.820	0.836	0.844	0.852	0.859
		8	$\frac{1}{2}a$	0.834	0.848	0.856	0.863	0.868
0.5	1.0472	2	$a$	0.311	0.323	0.329	0.336	0.342
		2	$\frac{1}{2}a$	0.347	0.358	0.364	0.370	0.375
		8	$a$	0.766	0.790	0.802	0.813	0.822
		8	$\frac{1}{2}a$	0.803	0.822	0.831	0.840	0.847
0.0	1.5708	2	$a$	0.271	0.284	0.291	0.299	0.305
		2	$\frac{1}{2}a$	0.320	0.331	0.338	0.344	0.349
		8	$a$	0.722	0.752	0.767	0.781	0.792
		8	$\frac{1}{2}a$	0.768	0.791	0.803	0.814	0.823
-0.5	2.0944	2	$a$	0.239	0.253	0.261	0.269	0.275
		2	$\frac{1}{2}a$	0.292	0.304	0.310	0.317	0.323
		8	$a$	0.684	0.719	0.736	0.752	0.766
		8	$\frac{1}{2}a$	0.733	0.761	0.775	0.789	0.799
-0.9	2.6906	2	$a$	0.212	0.226	0.233	0.241	0.248
		2	$\frac{1}{2}a$	0.263	0.276	0.282	0.290	0.296
		8	$a$	0.646	0.685	0.705	0.724	0.739
		8	$\frac{1}{2}a$	0.698	0.730	0.746	0.762	0.776

Table 5. Minimum power of the optimal directed  $t$  test:  $k = 2, \alpha = 0.05$

$\rho$	$\lambda$	$m = 10$	$m = 15$	$m = 20$	$m = 30$	$m = 50$
0.9	2	0.360	0.371	0.376	0.382	0.387
	8	0.817	0.834	0.843	0.850	0.857
0.5	2	0.298	0.310	0.316	0.322	0.328
	8	0.692	0.724	0.741	0.757	0.770
0.3	2	0.266	0.278	0.285	0.291	0.297
	8	0.614	0.654	0.675	0.695	0.712
0.1	2	0.235	0.247	0.253	0.260	0.266
	8	0.527	0.573	0.598	0.622	0.643
-0.2	2	0.187	0.199	0.205	0.211	0.217
	8	0.385	0.435	0.463	0.492	0.517
-0.5	2	0.140	0.149	0.155	0.160	0.165
	8	0.240	0.284	0.311	0.339	0.365
-0.9	2	0.070	0.076	0.080	0.083	0.086
	8	0.065	0.084	0.097	0.112	0.127
$\theta_0^* = 0$	2	0.375	0.386	0.391	0.396	0.401
	8	0.842	0.856	0.862	0.869	0.874
Power of $F$ :	2	0.178	0.192	0.200	0.207	0.216
	8	0.575	0.623	0.647	0.670	0.694

excludes part of  $(S_k - S_a - \bar{S}_a)$ . Integrating (2) over  $\omega^*$ , and then averaging with respect to the density of  $s_0^2$ , gives the power function

$$P_i^* = \frac{1}{2} e^{-\lambda} \sum_{i,j=0}^{\infty} \frac{(\frac{1}{2}\lambda)^{j+i} \cos^i \theta_0^* \sin^{2j} \theta_0^*}{j! \Gamma(\frac{1}{2}i + 1)} I_{1-c^2}(j + \frac{1}{2}m + \frac{1}{2}k - \frac{1}{2}, \frac{1}{2}i + \frac{1}{2}), \quad (14)$$

where  $\theta_0^*$  is the angle between  $\bar{\gamma}$  and  $\bar{\gamma}^*$ , and  $1 - c^2 = \{1 + t_c^2 / (m + k - 1)\}^{-1}$ , with  $t_c^2$  determined by  $\text{pr}\{F(1, m + k - 1) > t_c^2\} = 2\alpha$ .

The power function (14) is evidently a function of  $\lambda, m, k$  and  $\theta_0^*$ , the angle between the true vector  $\bar{\gamma}$  and the preselected vector  $\bar{\gamma}^*$ . The power is a maximum at  $\theta_0^* = 0$  and is a decreasing function of  $\theta_0^*$ , but it is, of course, impossible to choose  $\gamma^*$  so as to ensure that  $\theta_0^*$  is small even when it is known that  $\gamma > 0$ . Nevertheless, there is an optimal choice for  $\gamma^*$  when  $\gamma$  is restricted to the region  $\gamma > 0$  under  $H_a$  in the following sense. The test based on the vector  $\gamma^*$  for which the maximum value of  $\theta_0^*$  over all  $\mu \in S_a$  is smallest will maximize the minimum possible power of the test.

In the case  $k = 2$  the vector  $\mu^*$  corresponding to  $\gamma^*$  should obviously bisect the angle  $a$ , see Fig. 1, which yields the vector  $\gamma^{*'} = (\sigma_2, \sigma_1)$  as the optimal choice for  $\gamma^*$  in the above sense. For  $k \geq 3$  the problem of finding the optimal  $\gamma^*$  is more complicated. When  $k = 3$ , if the point  $\mu_a$ , say, that makes the same angle with each of the extremities of  $S_a$  is within  $S_a$ , then  $\mu^* = \mu_a$  and  $\gamma^* = (Z'M_x Z)^{-1}d$ , where  $d' = (\sigma_1, \sigma_2, \sigma_3)$ . However, the point  $\mu_a$  may not lie within  $S_a$ , and in that case  $\mu^*$  should be taken as the point on the longest edge of  $S_a$  that bisects the angle between its endpoints.

Table 5 gives some power calculations based on (14) for  $k = 2, \alpha = 0.05$ , various values for  $\lambda$  and  $m$  and, in the body of the table,  $\theta_0^* = \frac{1}{2}a$ . Values in the main body of Table 5 represent the minimum power of the directed  $t$  test for which this minimum power is largest. Table 5 gives also the power of the directed  $t$  test when  $\theta_0^* = 0$ , and the power of the  $F$  test. The entries for  $\theta_0^* = 0$  give the maximum possible power for any test of  $H_0$  because the  $t$  test in the correct direction is uniformly most powerful similar.

The minimum power of the best directed  $t$  test exceeds that of  $F$  for  $\rho \geq -0.2$  when  $\lambda = 2$ , for  $\rho \geq 0.1$  when  $\lambda = 5$ , and for  $\rho \geq 0.3$  when  $\lambda = 8$ . Thus, when  $\rho$  is reasonably large this test is better than the  $F$  test for  $k = 2$ . Tables 4 and 5 reveal that the likelihood ratio test dominates the directed  $t$  test, in terms of minimum power, for almost all values of  $\rho$ . Both tests are excellent when  $\rho$  is large, but the power of the directed  $t$  test falls off much more sharply than that of the likelihood ratio test as  $\rho$  declines. Hence, at least for the case  $k = 2$ , the likelihood ratio test is superior.

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APPENDIX

*The manifold defined by  $(\hat{\beta}_0, s_0^2)$  constant*

Let  $m = n - k - p$ , and let  $C$  be an  $n \times m$  matrix such that  $CC' = I_n - W(W'W)^{-1}W'$  and  $C'C = I_m$ . Put  $w = C'y, \hat{\beta}_0 = (X'X)^{-1}X'y$  and  $\hat{\gamma} = (Z'M_x Z)^{-1}Z'M_x y$ . The vectors  $w, \hat{\beta}_0$  and  $\hat{\gamma}$  are mutually independent,  $w \sim N(0, \sigma^2 I_m), \hat{\beta}_0 \sim N(\beta + (X'X)^{-1}X'Z\gamma, \sigma^2(X'X)^{-1})$  and  $\hat{\gamma} \sim N(\gamma, \sigma^2(Z'M_x Z)^{-1})$ . Let  $T$  be a  $k \times k$  upper triangular matrix such that  $T'T = Z'M_x Z$ , and put  $\tilde{\gamma} = T\hat{\gamma}, \bar{\gamma} = T\gamma$ , so that  $\tilde{\gamma} \sim N(\bar{\gamma}, \sigma^2 I_k)$ . Note that  $s_0^2 = w'w + \tilde{\gamma}'\tilde{\gamma}$ .

Now make the transformations  $w \rightarrow vr, \tilde{\gamma} \rightarrow hs$ , with  $v = w/(w'w)^{1/2}, h = \tilde{\gamma}/(\tilde{\gamma}'\tilde{\gamma})^{1/2}, r^2 = w'w$  and  $s^2 = \tilde{\gamma}'\tilde{\gamma} = \hat{\gamma}'Z'M_x Z\hat{\gamma}$ . By construction,  $v'v = 1$  and  $h'h = 1$ , and the volume elements  $dw$  and  $d\tilde{\gamma}$  are transformed as

$$dw = \frac{1}{2}(r^2)^{1/2 m - 1} dr^2(dv), \quad d\tilde{\gamma} = \frac{1}{2}(s^2)^{1/2 k - 1} ds^2(dh),$$

where  $(dv)$  and  $(dh)$  denote the invariant differential forms on the surfaces of the unit  $m$ -sphere and the unit  $k$ -sphere respectively (James, 1954). Because  $w \sim N(0, \sigma^2 I_m)$ ,  $v$  and  $r^2$  are independent,  $v$  is uniformly distributed on the  $m$ -sphere  $S_m: v'v = 1$ , and  $r^2/\sigma^2 \sim \chi^2(m)$ . Note that at this point we have resolved  $p(y)$  into  $p(\hat{\beta}_0) \times p(v) \times p(r^2) \times p(h, s^2)$ .

Now make the transformations  $(r^2, s^2) \rightarrow (s_0^2, b)$ , with  $s_0^2 = r^2 + s^2$  and  $b = s^2/(r^2 + s^2)$ , and note that  $b = (kF/m)(1 + kF/m)^{-1}$ , where  $F = ms^2/kr^2$  is the usual  $F$  statistic for testing  $H_0$ . We then have the resolution of  $p(y)$  into  $p(\hat{\beta}_0) \times p(s_0^2) \times p(v) \times p(h, b | s_0^2)$ , with  $p(h, b | s_0^2)$  given by (2) in the text, and it is straightforward to check that  $s_0^2/\sigma^2 \sim \chi^2(m+k, \lambda)$ , with  $\lambda = \bar{\gamma}'\bar{\gamma}/\sigma^2 = \gamma'Z'M_x Z\gamma/\sigma^2$ . The manifold defined by  $(\hat{\beta}_0, s_0^2) = \text{const}$  thus has three components: the surface of the unit  $m$ -sphere  $S_m: v'v = 1$ , the surface of the unit  $k$ -sphere  $S_k: h'h = 1$ , and the line segment  $0 \leq b \leq 1$ .

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