

**AJAE Appendix:**

**Grading, Minimum Quality Standards, and the Labeling of Genetically Modified Products**

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### Proof of Proposition 5 – Comparative Statics Results

With a uniform distribution of types  $H(\beta) = \beta$ , and thus in the uncovered market when both GM and non-GM products are produced, market demands are, respectively,  $D_g = \hat{\beta}$  and  $D_n = \tilde{\beta} - \hat{\beta}$ , so that total demand is  $D_T \equiv D_n + D_g = \tilde{\beta}$ . Upon recalling the arbitrage relations of competitive equilibrium, that is,

$$p_n^0 = p_g^0 + \delta$$

$$p_g^1 = p_g^0 + \eta$$

$$(p_n^1 - p_g^1)F(R) = \delta + \sigma$$

we have

$$\tilde{\beta}(R) \equiv \frac{u - p_g^0 - \eta - \frac{\delta + \sigma}{F(R)}}{a\bar{s}(R)}$$

$$\hat{\beta}(R) = \frac{\delta + \sigma}{aF(R)[1 - \bar{s}(R)]}.$$

In what follows we simplify notation and omit the functional dependence on  $R$  by writing  $F(R) = F$ ,

$f(R) = f$  and  $\bar{s}(R) = \bar{s}$ . Also, we define  $k \equiv \delta + \sigma$ ,  $A \equiv u - p_g^0 - \eta$ , and  $P \equiv p_g^0$ , so that

$$\hat{\beta} = \frac{k}{Fa(1 - \bar{s})}$$

$$\tilde{\beta} = \frac{AF - k}{Fa\bar{s}}.$$

Aggregate consumer surplus here is  $CS = \frac{1}{2}a \left[ \tilde{\beta}^2 \bar{s} + \hat{\beta}^2 (1 - \bar{s}) \right]$ . Substituting and simplifying obtains

$$CS = \frac{1}{2a} \left[ \frac{\left( A - \frac{k}{F} \right)^2}{\bar{s}} + \frac{\left( \frac{k}{F} \right)^2}{(1 - \bar{s})} \right].$$

Hence, the welfare function is

$$W = \Pi(P) + \frac{1}{2a} \left[ \frac{\left(A - \frac{k}{F}\right)^2}{\bar{s}} + \frac{\left(\frac{k}{F}\right)^2}{(1-\bar{s})} \right]$$

where  $\Pi(P)$  is producer surplus. The optimality conditions for welfare maximization (yielding the optimal standard purity  $R^*$  and the competitive farm-level equilibrium price  $P^*$ ) are

$$(1) \quad W_P = \Pi'(P) - \frac{1}{a} \frac{\left(A - \frac{k}{F}\right)}{\bar{s}} = 0$$

$$(2) \quad W_R = \frac{1}{2a} \left[ \frac{2\left(A - \frac{k}{F}\right) \frac{k}{F^2} f}{\bar{s}} - \frac{\left(A - \frac{k}{F}\right)^2}{\bar{s}^2} \frac{f}{F} (R - \bar{s}) - \frac{2\left(\frac{k}{F}\right)^2 \frac{f}{F}}{(1-\bar{s})} + \frac{\left(\frac{k}{F}\right)^2}{(1-\bar{s})^2} \frac{f}{F} (R - \bar{s}) \right] = 0.$$

Upon substitution and simplification we obtain

$$(3) \quad W_R = \left(\frac{af}{2F}\right) (\tilde{\beta} - \hat{\beta}) \left[ \hat{\beta}((1-\bar{s}) + (1-R)) - \tilde{\beta}(R - \bar{s}) \right] = 0 \rightarrow \left[ \hat{\beta}((1-\bar{s}) + (1-R)) - \tilde{\beta}(R - \bar{s}) \right] = 0.$$

Consider now the comparative statics effect of the parameter  $k \equiv \sigma + \delta$ . Differentiating the optimality conditions in (1) and (2) and expressing the results in matrix form yields

$$\begin{bmatrix} W_{RR} & W_{RP} \\ W_{PR} & W_{PP} \end{bmatrix} \begin{bmatrix} R_k \\ P_k \end{bmatrix} = \begin{bmatrix} -W_{Rk} \\ -W_{Pk} \end{bmatrix}.$$

Solving by Cramer's rule obtains

$$R_k = \frac{1}{\Delta} \begin{vmatrix} -W_{Rk} & W_{RP} \\ -W_{Pk} & W_{PP} \end{vmatrix} = \frac{-W_{Rk}W_{PP} + W_{Pk}W_{RP}}{\Delta}$$

$$P_k = \frac{1}{\Delta} \begin{vmatrix} W_{RR} & -W_{Rk} \\ W_{PR} & -W_{Pk} \end{vmatrix} = \frac{-W_{RR}W_{Pk} + W_{PR}W_{Rk}}{\Delta}$$

where  $\Delta = \begin{vmatrix} W_{RR} & W_{RP} \\ W_{PR} & W_{PP} \end{vmatrix} < 0$ ,  $W_{RR} < 0$  and  $W_{PP} > 0$  by the second-order conditions of the welfare

optimization problem (saddle point).

We now compute the partial effects that enter these comparative statics expressions.

Differentiating the optimality conditions in (1) and (2) yields

$$W_{PR} = -\frac{1}{a} \frac{k}{F^2} \frac{f}{\bar{s}} + \frac{1}{a} \left( A - \frac{k}{F} \right) \frac{f}{\bar{s}^2} (R - \bar{s})$$

which can be simplified to

$$W_{PR} = \frac{f}{F\bar{s}} \left[ -\hat{\beta}(1 - \bar{s}) + \tilde{\beta}(R - \bar{s}) \right].$$

Evaluating this partial effect at the optimality conditions, such that (3) holds, we obtain

$$W_{PR} = \frac{f}{F\bar{s}} \hat{\beta}(1 - R) > 0.$$

Next, differentiating (1) we find

$$W_{Pk} = \frac{1}{aF\bar{s}} > 0.$$

And differentiating (2) we obtain

$$W_{Rk} = \frac{1}{a} \left[ -\frac{kf}{F^3\bar{s}} + \left( A - \frac{k}{F} \right) \frac{1}{(F\bar{s})^2} (f\bar{s} + f(R - \bar{s})) - \frac{k}{F^3} \frac{f}{(1 - \bar{s})} + \frac{k}{F^2} \frac{1}{(1 - \bar{s})^2} \frac{f}{F} (R - \bar{s}) \right]$$

which simplifies to

$$W_{Rk} = \frac{f}{F^2} \frac{1}{\bar{s}(1 - \bar{s})} \left[ \tilde{\beta}R(1 - \bar{s}) - \hat{\beta} \left( (1 - \bar{s})^2 + \bar{s}(1 - R) \right) \right].$$

Evaluating this partial effect at the optimality conditions, such that (3) holds, we obtain

$$W_{kR} = \frac{f}{F^2} \frac{1}{\bar{s}(1 - \bar{s})} \hat{\beta} \left[ \frac{(1 - R) \left[ R(1 - \bar{s}) - \bar{s}(R - \bar{s}) \right] + \bar{s}(1 - \bar{s})^2}{(R - \bar{s})} \right].$$

Thus, a sufficient condition for  $W_{kR} > 0$  is  $R(1 - \bar{s}) \geq \bar{s}(R - \bar{s})$ , which does hold because  $R \geq \bar{s}$  and  $R \leq 1$ . Hence, we conclude that  $W_{kR} > 0$ .

The foregoing partial effects allow us to sign the comparative statics effect on farm price:

$$P_k = \frac{W_{RR}W_{Pk} - W_{PR}W_{Rk}}{-\Delta} < 0.$$

But  $sign(R_k) = sign(W_{Rk}W_{PP} - W_{Pk}W_{RP})$ . Note that

$$W_{PP} = \Pi''(p_g^0) + \frac{1}{a\bar{s}}.$$

Because  $\Pi''(p_g^0) = S'(p_g^0) > 0$  (the profit function is convex) and  $W_{Rk} > 0$ , to conclude that  $R_k > 0$  it

suffices to show that  $Z \equiv W_{Rk} \frac{1}{a\bar{s}} - W_{Pk}W_{RP} \geq 0$ . From earlier derivations,

$$Z \equiv \frac{f}{F^2} \frac{1}{\bar{s}(1-\bar{s})} \hat{\beta} \left[ \frac{(1-R)[R(1-\bar{s}) - \bar{s}(R-\bar{s})] + \bar{s}(1-\bar{s})^2}{(R-\bar{s})} \right] \frac{1}{a\bar{s}} - \frac{1}{aF\bar{s}} \frac{f}{F\bar{s}} \hat{\beta}(1-R)$$

which can be simplified to yield

$$Z = \frac{1}{a} \frac{f}{F^2} \frac{1}{\bar{s}^2(1-\bar{s})} \hat{\beta} \left[ \frac{\bar{s}(1-R)^2 + \bar{s}(1-\bar{s})^2}{(R-\bar{s})} \right] > 0$$

and so we can conclude that  $R_k > 0$ . Recalling that  $k \equiv \delta + \sigma$ , we have therefore established parts (i) and

(ii) of Proposition 4.

The comparative statics analysis for the parameter  $k$  is readily adapted to the comparative statics of the ‘‘GM aversion’’ parameter  $a$ . Specifically,

$$R_a = \frac{W_{Ra}W_{PP} - W_{Pa}W_{RP}}{-\Delta}$$

$$P_a = \frac{W_{RR}W_{Pa} - W_{PR}W_{Ra}}{-\Delta}.$$

The partial effects of interest here are

$$W_{Pa} = \frac{1}{a^2 F \bar{s}} (AF - k) = \frac{1}{a} \tilde{\beta} > 0$$

$$W_{Ra} = -\frac{1}{a} W_R = 0$$

and so we find

$$P_a = \frac{W_{RR}W_{Pa}}{-\Delta} < 0$$

$$R_a = \frac{-W_{Pa}W_{RP}}{-\Delta} < 0$$

which establishes part (iii) of Proposition 4.

Finally, concerning the parameters  $u$  and  $\eta$ , we note that they enter the problem only through the term  $A \equiv u - p_g^0 - \eta$ . For the comparative statics of this term we have

$$R_A = \frac{W_{RA}W_{PP} - W_{PA}W_{RP}}{-\Delta}$$

$$P_A = \frac{W_{RR}W_{PA} - W_{PR}W_{RA}}{-\Delta}.$$

The partial effects of interest here are

$$W_{PA} = -\frac{1}{a\bar{s}} < 0$$

and  $W_{RA} < 0$  because  $W_{RA} = -W_{PR}$  and we showed earlier that  $W_{PR} > 0$ . Thus we can immediately

conclude that  $P_A > 0$ . The sign of  $R_A$  is the sign of  $Z \equiv (W_{RA}W_{PP} - W_{PA}W_{RP})$ . By using  $W_{RA} = -W_{PR}$

we find  $Z \equiv W_{RA}(W_{PP} + W_{PA})$ , and by noting that  $W_{PP} = \Pi''(p_g^0) - W_{PA}$  we get  $Z \equiv W_{RA}\Pi''(p_g^0) < 0$ , and

so we conclude that  $R_A < 0$ . Recalling again that  $A \equiv u - p_g^0 - \eta$ , this concludes the comparative statics

of parameters  $u$  and  $\eta$  (part (iv) of Proposition 5). ■