

MONTE CARLO VALUATION OF NATURAL GAS INVESTMENTS

by

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Abstract

This paper deals with the valuation of energy assets related to natural gas. In particular, we evaluate a baseload Natural Gas Combined Cycle (NGCC) power plant and an ancillary installation, namely a Liquefied Natural Gas (LNG) facility, in a realistic setting; specifically, these investments enjoy a long useful life but require some non-negligible time to build. Then we focus on the valuation of several investment options again in a realistic setting. These include the option to invest in the power plant when there is uncertainty concerning the initial outlay, or the option's time to maturity, or the cost of CO_2 emission permits, or when there is a chance to double the plant size in the future.

Our model comprises three sources of risk. We consider uncertain gas prices with regard to both the current level and the long-run equilibrium level; the current electricity price is also uncertain. They all are assumed to show mean reversion.

The two-factor model for natural gas price is calibrated using data from NYMEX NG futures contracts. Also, we calibrate the one-factor model for electricity price using data from the Spanish wholesale electricity market, respectively. Then we use the estimated parameter values alongside actual physical parameters from a case study to value natural gas plants.

Finally, the calibrated parameters are also used in a Monte Carlo simulation framework to evaluate several American-type options to invest in these energy assets. We accomplish this by following the least squares MC approach.

Keywords: Real options, power plants, stochastic revenues and costs, CO_2 allowances, LNG.

JEL codes: C6, E2, D8, G3.

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1 Introduction

Energy resource prices in general are now at or near record levels. This situation may be explained both from the demand side and the supply side. With regard to the former, strong economic growth in America, on the one hand, and in China and India, on the other, has placed world reserves under substantial strain. At the same time, new discoveries and investment by the industry have not kept pace. In sum, energy markets are currently very tight, and energy security concerns sound ever louder. As a consequence, consumers can arguably expect any external shock to translate into greater volatility of oil and gas prices.

On the other hand, regulatory uncertainties cannot be neglected. A decade ago the United States decided to break up the vertically integrated electricity industry (generation, transmission, and distribution). The rationale for this was basically to accomplish higher levels of competition and efficiency at every stage. This process has brought a number of deals concerning the buying and selling of assets. Meanwhile, the European Union has been pushing ever harder for the creation of a single market in traditionally fragmented industries, among them energy. As a consequence, several takeovers and mergers have taken place at the national level and even cross-border mergers are being proposed.

In the case of energy investments, this uncertain environment is coupled with irreversibility considerations, or a chance to defer investment, or to manage it in a flexible way. Under these circumstances, valuation techniques based on the methods for pricing options (such as Contingent Claims Analysis or Dynamic Programming) are superior to traditional approaches based on discounted cash flows.¹ In addition, power utilities (at least in the European Union) now face a new carbon market which, regardless of whether it is seen as a threat or an opportunity, no doubt will influence decision making.

¹See Dixit and Pindyck [14], Sick [31], and Trigeorgis [32].

The aim of this paper is to use the real options methodology to evaluate energy investments related to natural gas, which is gaining market share to the detriment of crude oil, let alone standard coal. Brekke and Schieldrop [6] consider a power plant which can burn either natural gas or oil. Specifically, they focus on the choice between flexible and inflexible technologies when fuel prices are assumed to follow standard geometric Brownian motions. Valuation of power plants has also been studied by Deng et al. [13]. They point out that, due to the non-storable nature of electricity, the traditional storage-based, no-arbitrage methods of valuing commodity derivatives are unavailable. In addition, electricity prices can (and do) show strong mean reversion over short time horizons. They develop a method to value electricity derivatives, and ultimately electricity assets, by exploting the fact that, even though electricity is not a financial asset, derivatives contracts on electricity price are financial assets and can be replicated. Näsäkkälä and Fleten [22] extend this model in several directions. They assume that there are two technologies for a gas-fired power plant. A base load plant produces electricity with constant capacity, irrespective of the difference between the price of the output electricity and that of the input gas (the so-called "spark spread"); thus the plant produces even if it is unprofitable. In contrast, a peak load plant can be ramped up and down according to price changes without delay; hence the plant produces only when the spark spread exceeds emission costs. This grater flexibility, though, arises at the expense of higher operational costs. They also account for the possibility of upgrading a base load plant to a peak load plant. Following Schwartz and Smith [29], they use a two-factor model for the spark spread, where the shortterm deviations are modeled as a mean-reverting process and the equilibrium price evolves according to a Brownian motion. Finally, Deng [12] focuses on the jumps and spikes in power prices. He models the electricity spot price as a one-factor process which shows mean reversion, jumps and seasonality. By explicitly modeling price spikes, he examines the sensitivity of the value of investments (and options to invest) to the characteristics of price jumps such as their frequency and the average jump size.

In this paper, we evaluate a base load Natural Gas Combined Cycle (NGCC) power plant and an ancillary installation, namely a Liquefied Natural Gas (LNG) facility, in a realistic setting; specifically, these investments enjoy a long useful life but require some non-negligible time to build.² Then we focus on the valuation of several investment options again in a realistic setting. These include the option to invest in the power plant when there is uncertainty concerning the initial outlay, or the option's time to maturity, or the cost of CO_2 emission permits, or when there is a chance to double the plant size in the future.³

Our model comprises three sources of risk. We consider uncertain gas prices with regard to both the current level and the long-run equilibrium level; the current electricity price is also stochastic. They all are assumed to show mean reversion. Specifically, they are assumed to follow an Inhomogeneous Geometric

²Majd and Pindyck [21] analyze this subject, which is typically neglected. See also Bar-Ilan and Strange [3] and Alvarez and Keppo [1].

³See Trigeorgis [32] for an intuitive exposition of this and related options.

Brownian Motion (IGBM). This is a relatively general stochastic process in that it reduces to standard Geometric Brownian Motion, or even accounts for jumps in the state variable, depending on its parameter values.

The two-factor model for natural gas price is calibrated using data from NYMEX NG futures contracts. The specific procedure is based on Cortazar and Schwarz [11]. Also, we calibrate the one-factor model for electricity price with data from the Spanish wholesale electricity market. Then we use the estimated parameter values alongside actual physical parameters from our case study to value natural gas plants.

Finally, the calibrated parameters are also used in a Monte Carlo simulation framework to evaluate several American-type options to invest in these energy assets.⁴ We accomplish this by following the Least Squares Monte Carlo (LSM) approach as developed by Longstaff and Schwarz [19].

The paper is organized as follows. Section 2 briefly describes the technology for producing electricity in a gas-fired power plant. Then we introduce that for storing natural gas; it has the potential to connect previously fragmented markets by unlocking the intimate relation between consumers and local providers. Section 3 shows the mean-reverting stochastic process for input and output prices. For valuation purposes, the risk-neutral version of the model is then derived. Also, since we adopt Monte Carlo simulation below as a numerical technique, the model must be adapted to a discrete-time context. Section 4 aims to get the parameter values of the stochastic processes. To this end, the model for the gas price and that for electricity are separately calibrated using actual data. Section 5 describes our case study; it includes physical parameter values of the NGCC plant and the LNG plant. In Section 6 we derive the value of each plant in operation. Then Section 7 evaluates several options to invest in a NGCC power plant. A section with final remarks concludes.

2 Basic description

2.1 The NGCC technology

It is based on the employment of two turbines, one of natural gas and another one of steam. The exhaust gases from the first one are used to generate the steam that is used in the second turbine which produces approximately one-third of the total power output. Thus it consists of a Gas-Air (Brayton) cycle and a Water-Steam (Rankine) cycle. This system allows for a higher net efficiency than coal-fired power plants,⁵ close to 55%; future trends aim at reaching net efficiencies of 60% in NGCC plants of 500 Mw.⁶

The advantages of a NGCC power plant are:⁷

⁴See, among others, Cortazar and Schwartz [10].

 $^{^5}$ The net efficiency refers to the percentage of the heating value of the fuel that is transformed into electric energy.

⁶See Watson [33].

⁷Our reference is ELCOGAS [15]: "Integrated gasification combined cycle technology: IGCC" and its actual application at the power plant in Puertollano (Spain).

- a) Lower emissions of CO_2 , estimated about 350 g/Kwh, which allow an easier fulfillment of the Kyoto protocol;
 - b) Higher net efficiency, between 50% and 60%;
 - c) Low cost of the investment, about 422.5 €/Kw installed;
- d) Less consumption of water and space requirements, which allow to build in a shorter period of time and closer to consumer sites. A NGCC power plant can be built in 30 months 8 employing $100 \ m^2/MW$.
 - e) Useful life of 25 years.
 - f) Lower operation costs, with typical values of 0.35 cents €/KWh.
- g) Depending on the design of the gas turbine, some facilities can use other combustibles as Diesel oil and fuel.

In addition, a NGCC power plant can be designed as a baseload plant or as a peaking plant; in the latter case, it only operates when electricity prices are high enough, what usually happens during periods of strong growth in demand.

The advantages of the NGCC Power Plants make it easier to obtain permissions of construction by new electricity producers.

On the other hand, the disadvantages of a NGCC Power Plant are:

- a) The higher cost of the natural gas fired in relation to coal's;
- b) The insecurity concerning gas supplies, since reserves are more unevenly distributed over the world;
- c) The strong rise in the demand for natural gas, which can cause a consolidation of prices at higher than historical levels.

Nonetheless, the spreading of Liquefied Natural Gas (LNG) plants entails an improvement in ensuring fuel supplies and a stronger link among formerly geographically fragmented natural gas markets.

2.2 The LNG technology

A Liquefied Natural Gas (LNG) plant stores liquefied gas in cryogenic tanks after being downloaded from the vessels in which it is transported at a temperature of -160°C. Then it is regasified and pumped into the gas pipelines so as to make it avaliable for the consuming units, for instance a NGCC power plant. The liquefied gas comes from liquefying plants located at the producing countries. Thus a power utility in a developed country may purchase and import gas from distant producers at affordable prices; this may be sensible not only on economic grounds, but on diversification and reliability concerns as well.

A LNG plant can be modelled as a spread option between using domestic gas or buying foreign gas, at any time choosing the cheapest possibility while increasing supply reliability. A restrictive requirement for the construction of one of these facilities is the need of a coastal site with a sufficiently deep port to harbour LNG freight vessels.

To the extent that these plants allow for access to new natural gas markets, their construction enables these markets to get interlinked, depending on the

⁸ In some cases the time of construction has dropped to a year. See Watson [33].

arbitrage opportunities once transport costs between different sites have duly been accounted for.

3 The stochastic model for input and output prices

The stochastic behaviour of energy prices shows both a short-term and a long-term dynamics. The short run behaviour displays mean reversion, seasonality, stochastic volatility and, in some instances, discrete jumps; long run behaviour, though, is determined by equilibrium price's dynamics. Since one aim of the paper is to value an asset (a base load NGCC plant) with 25 years of useful life, short-term features bar mean reversion have been deemed less relevant. ¹⁰

3.1 A three-factor model

The following model is adopted:

$$dG_t = k_q(L_t - G_t)dt + \sigma_q G_t dW_t^G, \tag{1}$$

$$dL_t = \mu(L_q - L_t)dt + \xi L_t dW_t^L, \tag{2}$$

$$dE_t = k_e (L_e - E_t) dt + \sigma_e E_t dW_t^E, \tag{3}$$

where:

 G_t : the price of natural gas at time t.

 L_t : the natural gas equilibrium price level, which behaves according to equation (2).

 k_g : the speed of reversion of natural gas price towards its "normal" level. It can be computed as $k_g = \log 2/t_{1/2}$, where $t_{1/2}$ is the expected half-life, that is, the time for the gap between G_t and L_t to halve.

 σ_q : the instantaneous volatility of fuel price.

 μ : the speed of reversion of L_t towards its longer-term equilibrium value $L_q.$

 ξ : the instantaneos volatility of natural gas equilibrium price.

 E_t : the price of electricity at time t.

 k_e : the speed of reversion of electricity price towards its "normal" level in the long run L_e .

⁹Schwartz and Smith [29] discuss these twin dynamics in a model which allows for mean reversion in the short term and uncertainty in the equilibrium price to which prices revert. See also Pilipovic [24] and Baker, Mayfield and Parsons [2].

 $^{^{10}}$ Seasonality would be much more important in a valuation model for the short run. It could be included by means of a function f(t) in the expression for the current price G_t . In this case, the formulae in this paper would correspond to the deseasonalised series. Concerning price jumps, in case there are, they would only be important to the extent that they have an impact on average prices; thus they should be taken into account when computing the parameters of the stochastic model adopted.

 σ_e : the instantaneous volatility of electricity price.

 dW_t^G , dW_t^L and dW_t^E : increments to a standard Wiener process. They are assumed to be normally distributed with mean zero and variance dt. It is further assumed that $\rho_{W^GW^L} = \rho_{W^LW^E} = 0$ and $\rho_{W^GW^E} = \rho$.¹¹

This model has some convenient implications:

- a) There is no chance for G_t or E_t to take on negative values.
- b) It allows the existence of an equilibrium level for both natural gas and electricity output. In the former's case, the equlibrium price is not constant.
 - c) Expected values of long-run equilibrium prices remain finite, L_q and L_e . ¹²
- d) The stochastic process for natural gas price is similar to Pilipovic [24] model; yet they differ in that equation (2) above is of the IGBM type, as opposed to the standard GBM in Pilipovic. 13 This kind of models seems preferable if the equilibrium price in the longer term is jointly determined by production cost and demand level.
 - e) The model allows for price jumps depending on parameter values.
- f) It also allows, as a particular case, that equations (1) and (2) adopt a GBM format, again depending on the values of the parameters.
- g) Consistent with futures markets, volatilities do not grow without bound as $t \to \infty$; instead, they approach a finite value if reversion speed is high enough in relation to volatility.

The expected value of natural gas price is:

$$E(G_t) = L_g - \frac{k_g(L_0 - L_g)}{\mu - k_g} e^{-\mu t} + \left[G_0 - L_g + \frac{k_g(L_0 - L_g)}{\mu - k_g} \right] e^{-k_g t}.$$
 (4)

See equation (54) in the Appendix.¹⁴

On the other hand, the expected value of electricity price is:

$$E(E_t) = L_e + (E_0 - L_e)e^{-k_e t}. (5)$$

3.2 The risk-neutral model

The model in a risk-neutral world would be:

$$d\hat{G}_t = [k_g(\hat{L}_t - \hat{G}_t) - \lambda_g \sigma_g \hat{G}_t] dt + \sigma_g \hat{G}_t dW_t^G,$$
(6)

$$d\hat{L}_t = \left[\mu(L_g - \hat{L}_t) - \lambda_l \xi \hat{L}_t\right] dt + \xi \hat{L}_t dW_t^L, \tag{7}$$

$$d\hat{E}_t = [k_e(L_e - \hat{E}_t) - \lambda_e \sigma_e \hat{E}_t]dt + \sigma_e \hat{E}_t dW_t^E,$$
(8)

The similarly to Pilipovic model [24] for $\rho_{WGWL} = 0$.

12 In this model $E(L_t) = L_g + (L_0 - L_g)e^{-\mu t}$, which implies $E(L_\infty) = L_g$.

13 In Pilipovic's model there is no equilibrium price in the long run; in our notation, $L_g = 0$.

¹⁴ For $L_g = 0$ and $\mu = -\varphi$ equation (2) reduces to: $dL_t = \varphi L_t dt + \xi L_t dW_t^L$. In this case, the expected value becomes: $E(G_t) = \frac{k_g L_0}{\varphi + k_g} e^{\varphi t} + \left[G_0 - \frac{k_g L_0}{\varphi + k_g} \right] e^{-k_g t}$.

where:

 λ_g : is the market price of risk stemming from current natural gas price (assumed to be constant).

 λ_l : is the market price of equilibrium gas price risk.

 λ_e : is the market price of current electricity price risk.

In this risk-neutral setting, the expected value of natural gas price, as shown by equation (55) in the Appendix, is:

$$E(\hat{G}_{t}) = \frac{\mu k_{g} L_{g}}{(\mu + \lambda_{l} \xi)(k_{g} + \lambda_{g} \sigma_{g})} \left(1 - e^{-(k_{g} + \lambda_{g} \sigma_{g})t}\right) +$$

$$+ \left[\frac{\mu k_{g} L_{g}}{(\mu + \lambda_{l} \xi)(\mu + \lambda_{l} \xi - k_{g} - \lambda_{g} \sigma_{g})} - \frac{k_{g} L_{0}}{(\mu + \lambda_{l} \xi - k_{g} - \lambda_{g} \sigma_{g})}\right] \cdot$$

$$\cdot \left(e^{-(\mu + \lambda_{l} \xi)t} - e^{-(k_{g} + \lambda_{g} \sigma_{g})t}\right) + G_{0}e^{-(k_{g} + \lambda_{g} \sigma_{g})t}.$$

$$(9)$$

This value $E(\hat{G}_t)$ equals the estimated futures price of natural gas \hat{F}_t for maturity t.

For an arbitrarily long maturity, the estimate for the futures price would be:

$$\hat{F}_{\infty} = \frac{\mu k_g L_g}{(\mu + \lambda_l \xi)(k_g + \lambda_g \sigma_g)}.$$
 (10)

Now the expression for the forward risk premium would be the difference between the values in equations (4) and (9):

$$RP_{g_t} = E(G_t) - E(\hat{G}_t). \tag{11}$$

In principle, this difference could be either positive or negative.¹⁵

The risk-neutral version for the electricity price is:

$$E(\hat{E}_t) = E_0 e^{-(k_e + \lambda_e \sigma_e)t} + \frac{k_e L_e}{(k_e + \lambda_e \sigma_e)} \left(1 - e^{-(k_g + \lambda_e \sigma_e)t} \right). \tag{12}$$

3.3 The discrete-time version

In our Monte Carlo simulations below, we shall use the following discretization of equations (6), (7) and (8):

$$\Delta \hat{G}_t = [k_g \hat{L}_t - \hat{G}_t (k_g + \lambda_g \sigma_g)] \Delta t + \hat{G}_t \sigma_g \sqrt{\Delta t} \epsilon_t^G, \tag{13}$$

$$\Delta \hat{L}_t = [\mu L_g - \hat{L}_t(\mu + \lambda_l \xi)] \Delta t + \hat{L}_t \xi \sqrt{\Delta t} \epsilon_t^L, \tag{14}$$

$$\Delta \hat{E}_t = k_e (L_e - \hat{E}_t) \Delta t + \sigma_e \hat{E}_t \sqrt{\Delta t} \epsilon_t^E, \tag{15}$$

If $L_g = 0$ and $\mu = -\varphi$ equation (9) reduces to: $E(\hat{G}_t) = G_0 e^{-(k_g + \lambda_g \sigma_g)t} + \frac{k_g L_0}{(\varphi - \lambda_t \xi + k_g + \lambda_g \sigma_g)} (e^{(\varphi - \lambda_t \xi)t} - e^{-(k_g + \lambda_g \sigma_g)t}).$

where ϵ_t^G , ϵ_t^L and ϵ_t^E are standard Normal variates and Δt is measured in yearly terms. Whereas ϵ_t^G and ϵ_t^L are assumed to be independent, and also ϵ_t^L and ϵ_t^E , so $\rho_{G,L} = \rho_{L,E} = 0.0$, the correlation coefficient between electricity and natural gas prices $\rho_{G,E}$ may be different from zero. Note that since there is no Spanish futures electricity market from which to infer a risk premium, we assume $\lambda_e = 0$.

4 Parameters of the stochastic processes

4.1 Model calibration for natural gas price

Our data set consists of all NYMEX NG futures prices from January 5th 2004 to April 29th 2005, a total of 330 days; contract maturities range from one month up to six years. These series have been deseasonalised for later use in all our computations. Figure 1 shows futures prices on a typical day and also the deseasonalised series on that day. The seasonal component displays a strong regularity. The seasonal component displays a strong regularity.

Figure 2 shows deseasonalised prices for futures contracts with one month and five years to maturity. As in some related papers, it can be noted that volatility decreases as the time horizon increases.¹⁸ On the other hand, the positive drift observed in futures prices along trading sessions seems to suggest a structural change in the market, e.g. in the form of a higher equilibrium price level.

Now we describe the calibration procedure. It is based on the approach developed by Cortazar and Schwartz [11], who propose a method which minimizes a sum of square errors. These errors are the difference between actual futures prices and those computed at each time as a function of global parameters and state variables for each day. The choice of this method has to do with the non-linearity of equation (9) and the unequal number of futures contracts in which the market has not operated.

We have seven general parameters in the model: $k_g, \lambda_g, \lambda_l, \sigma_g, \xi, \mu$ and L_g . Nonetheless, given the optimization procedure chosen, mere observation of expression (9) leads to the conclusion that only the following combinations may be estimated:¹⁹

$$V_1 \equiv k_a + \lambda_a \sigma_a,\tag{16}$$

¹⁶As already mentioned, it is assumed that seasonality has a rather limited impact on investment valuations when long time horizons (e.g. 25 years) are involved; at the moment of discounting, most of seasonal variations would cancel each other. Deseasonalisation has been accomplished by using the Arima-X12 procedure.

 $^{^{17}{\}rm NYMEX}$ NG futures contracts refer to 10,000 million BTU. Prices, though, are quoted for 1 million BTU; this figure amounts to 1,055 GJ.

¹⁸See, among others, Schwartz [28], Baker, Mayfield and Parsons [2], Cortazar and Schwartz [11]. This behaviour is not consistent with a GBM model.

 $^{^{19}}$ The particular values of the seven original parameters of the model should also take into account the behaviour of the original time series.

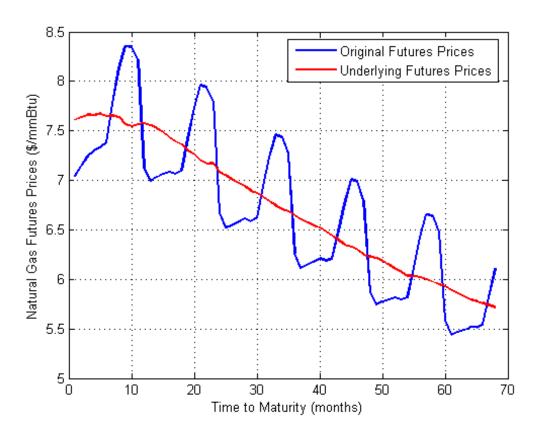


Figure 1: Nymex NG futures prices on 2005/04/19 and deseasonalised series.

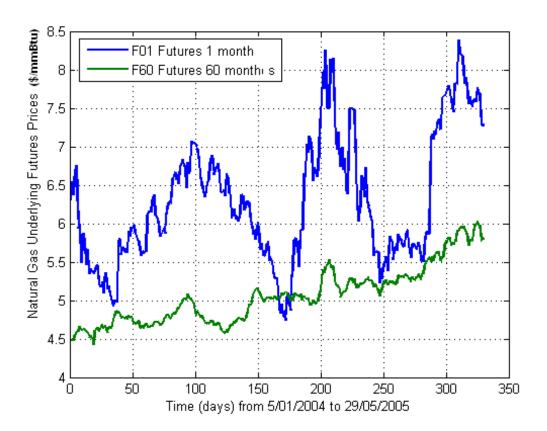


Figure 2: Nymex deseasonalised futures prices with one month (F01) and five years (F60) to expiry.

$$V_2 \equiv \mu + \lambda_l \xi,\tag{17}$$

$$V_3 \equiv \mu k_a L_a. \tag{18}$$

On the other hand, L_0 is a state variable for each trading day i, but only the product $k_q L_0$ on each day can be estimated by the procedure adopted, i.e.:

$$U_i \equiv k_q L_{0_i}. \tag{19}$$

If we have price quotes in N days (dated t_i , with i = 1, 2, ..., N), and on each day there are M_i different contracts, with no reason why there must be the same number of price quotes every day, the function to be minimised is:

$$\sum_{i=1}^{N} \sum_{j=1}^{M_i} (\hat{F}_{ij}(V_1, V_2, V_3, U_i, T_j - t_i, F_{i1}) - F_{ij})^2, \tag{20}$$

where F_{ij} denotes the futures quote on day i with maturity in (month) j, and \hat{F}_{ij} stands for the contract price when this is estimated by means of expression (9) as a function of the parameters used (V_1, V_2, V_3) , the state variables U_i for each day i, and time $T_j - t_i$ which is the difference (in years) between the futures contract maturity T_j and the date of the first futures contract on day i (assumed to be that for one month; this is F_{i1} futures contract, which is used as the spot price).

The estimation procedure involves two steps which are repeated until the sum of square errors converges:

a) A set of initial parameter values $\Omega = \{V_1, V_2, V_3\}$ is chosen. Then it is possible to estimate the state variables on each day in a single step:

$$\{U_{1}, U_{2,\dots,U_{N}}\} \in \underset{U_{1}, U_{2},\dots,U_{N}}{\operatorname{argmin}} \sum_{i=1}^{N} \sum_{j=1}^{M_{i}} \left(\hat{F}_{ij}(V_{1}, V_{2}, V_{3}, U_{i}, T_{j} - t_{i}, F_{i1}; \Omega) - F_{ij}\right)^{2}.$$

$$(21)$$

b) The next step consists in estimating the values of the model parameters:

$$\{V_1, V_2, V_3\} \in \underset{V_1, V_2, V_3}{\operatorname{argmin}} \sum_{i=1}^{N} \sum_{j=1}^{M_i} \left(\hat{F}_{ij}(V_1, V_2, V_3, U_i, T_j - t_i, F_{i1}; \Omega) - F_{ij} \right)^2. \quad (22)$$

Table 1 shows the results obtained using the whole sample, the last one hundred days, and the last fifty days.

 $^{^{20}\}mathrm{In}$ our case, initially the whole sample of 330 days would be used up.

Concept	Panel I	Panel II	Panel III
N^o Days	330	100	50
N ^o Observations	23,571	6,989	3,436
Sum of Square Errors	405.47	32.02	15.82
Sum of Square Errors / Days	1.2287	0.3202	0.3164
V_1	0.2122	0.1393	0.1283
V_2	2.5338	6.0412	6.1852
V_3	2.1346	2.9469	2.5870
\hat{F}_{∞}	3.9704	3.5025	3.2604

Table 1: Risk Neutral parameter composites.

Figure 3 shows actual market data on 2005/04/19 as compared with the results of the models estimated with observations from 330 and 100 days. As will be shown below, in our case study the time to build natural gas plants is assumed to range from 30 to 36 months. Interestingly, for contract maturities of 30 months or more, the series of market futures prices and model (100 days) futures prices seem to agree most.

Figure 4 shows, also for 2005/04/19, the comparison between actual futures prices and those predicted in the long run. Note the trend in the longer term, where $\hat{F}_{\infty} = 3.5025$. In sum, actual futures quotes from natural gas contracts seem rather consistent with the model adopted.²¹

In order to estimate the remaining parameters, which are necessary for Monte Carlo simulations, the series obtained for the values of G_t and $U_t \equiv k_g L_{0_t}$ will be used up, according to the following discretization:

$$\frac{G_{t+\Delta t} - G_t}{G_t} = \frac{k_g(L_t - G_t)\Delta t}{G_t} + \sigma_g \epsilon_t^G, \tag{23}$$

where ϵ_t^G is an $iid \sim N(0,1)$ variate. This allows to compute k_g by a process of square errors minimization or by OLS. Once k_g has been obtained, σ_g is computed from the residuals' standard deviation. With this value it is possible to get the series L_{0_i} .

Similarly, once we know the value of $V_3/k_g \equiv \mu L_g$ we can use

$$\frac{L_{t+\Delta t} - L_t}{L_t} = \frac{\mu(L_g - L_t)\Delta t}{L_t} + \xi \epsilon_t^L, \tag{24}$$

where ϵ_t^L is an $iid \sim N(0,1)$ variate. Then, following similar procedures, the values of μ y ξ are isolated, which allows to deduce L_g . Last, it is easy to deduce the value of the risk premia λ_g and λ_l from the definitions of V_1 and V_2 .

Table 2 summarizes the results:

²¹It is necessary to stress the lower liquidity of futures contracts as the time to maturity increases, and the fact that there are no quotes for terms longer than six years.

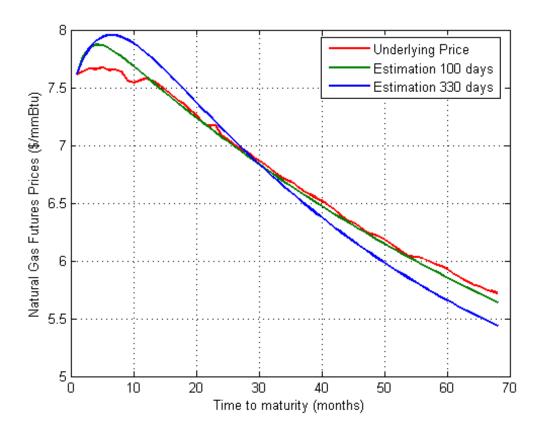


Figure 3: Actual (deseasonalised) futures prices on 2005/04/19 against theoretical values from estimated models.

Parameter	Value
k_g	0.3818
σ_g	43.44%
μ	4.1492
ξ	43.66%
λ_g	-0.5583
λ_l	4.3330
L_g	1.8603

Table 2: Actual parameters.

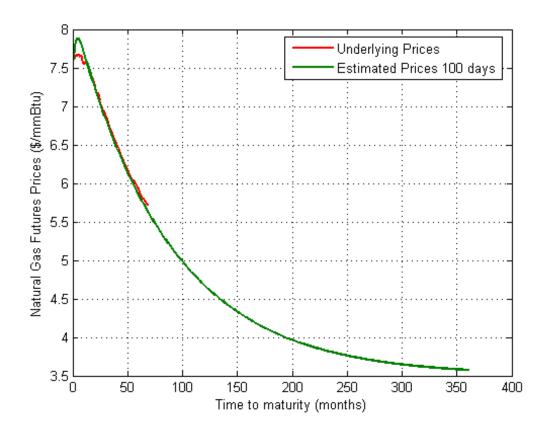


Figure 4: Actual (deseasonalised) futures prices on 2005/04/19 and those predicted in the long run.

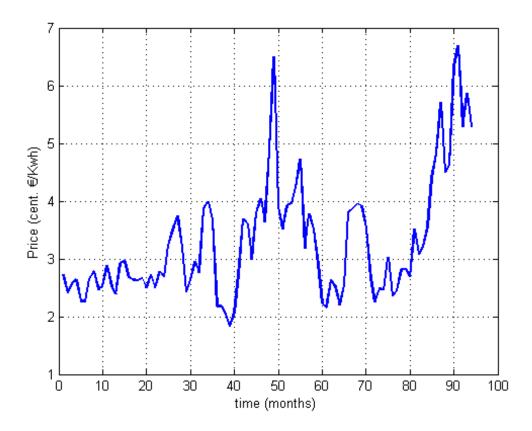


Figure 5: Monthly average electricity prices from Spanish OMEL market (January 1998 - October 2005).

4.2 Model calibration for electricity price

The data set comprises 95 monthly average electricity prices from the Spanish wholesale spot market (OMEL).²² The time span goes from January 1998 to October 2005, as shown in Figure 5.

Table 3 displays some basic statistics from the mean price series.

The following model is estimated:

$$dE_t = k_e(L_e - E_t)dt + \sigma_e E_t dW_t^E, \qquad (25)$$

 $^{^{22}\}mathrm{Since}$ the aim of the paper concerns (long-lived) base load plants, monthly average prices have been chosen.

Average	3.2879
Median	2.9195
Minimum	1.8250
Maximum	6.6910
Standard deviation	1.0451
Coeff. Variation	0.31787
Skewness	1.3264
Excess Kurtosis	1.4949

Table 3: Actual statistics from OMEL market.

which corresponds to an autorregresive model of order 1, or AR(1). In fact, the partial autocorrelation function shown in Figure 6 is consistent with an AR(1) model.

After discretization and rearranging this equation becomes:

$$\frac{E_{t+1} - E_t}{E_t} = k_e L_e \Delta t \frac{1}{E_t} - k_e \Delta t + \sigma_e \epsilon_t^E.$$
 (26)

Expressed as $Y_t = \beta_1 + \beta_2 X_{2t} + u_t$, we get the following OLS estimates for $\hat{\beta}_1$ and $\hat{\beta}_2$:

Coefficient	Estimate	Standard dev.	t-statistic	p-value
\hat{eta}_1	-0.116136	0.0632336	-1.8366	0.0695
\hat{eta}_2	0.403814	0.186756	2.1623	0.0332

$$\hat{\beta}_1 = -0.116136 = \frac{-k_e}{12},\tag{27}$$

$$\hat{\beta}_2 = 0.403814 = \frac{k_e L_e}{12} = -\hat{\beta}_1 L_e. \tag{28}$$

The standard deviation of the residuals is 0.142427. Hence $\sigma_e = 0.142427 \times \sqrt{12} = 0.4934 = 49.34\%$. It follows that:

Parameter	Value
k_e	1.3936
L_e	3.4771
σ_e	0.4934

In our computations below we will assume $\lambda_e = 0$ and also $\rho = 0.55$.

5 Case study

5.1 The NGCC plant

The representative values are shown in Table 4.

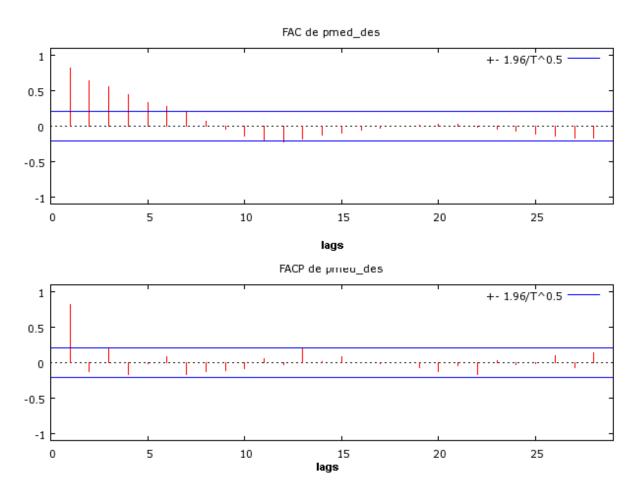


Figure 6: Partial autocorrelation function from (deseasonalised) average electricity price series.

Concept	Value
Output Mw (P_{NGCC})	500
Production Factor (% Capacity) (FP)	80%
Net Efficiency (%) (RDTO)	55%
Investment Cost (€/kw) (i)	422,5
Useful Life (years)	25
Time to Build (months)	30
Necessary Surface (m^2/Mw)	100
Annual Maintenance (weeks)	3.5
Time to Start (minutes)	15-60
O & M (cts.€/kwh) (CVAR)	0.32
Refrigeration Water (m^3/hMw)	7

Table 4: Basic NGCC parameters. Source: ELCOGAS.

Concept	Value
Heat Rate GJ/Kwh	0.006545
Total Investment (million €)	211.25
Annual production (million Kwh)	3,504
Fuel Energy (GJ/year)	22,935,273
CO ₂ Emissions (tonne/year) (EM)	1,226,400

Table 5: Resulting NGCC parameters.

The Production Factor is the percentage of the total capacity used on average over the year. Using these data, the heat rate, the plant's consumption of energy, and the total production of electricity can be computed:

Heat Rate: HR = 3600/RDTO/1000000, in GJ/Kwh.²³

Investment Cost I = 1000 * i * P, in Euros.²⁴

Total annual production: A = 1000P * 365 * 24 * FP, in Kwh.

Fuel energy needs: B = 1000P * 365 * 24 * FP * HR, in GJ/year.

Yearly CO_2 emissions: EM = 350 * A/1000000, in tonnes per year.

Now with these formulae we estimate the parameters in Table 5.

We may think of a firm that is at its outset. It has no prior emission allowances, so as much carbon permits as tonnes emitted will have to be purchased at a price. Initially a fixed permit price will be assumed; then a stochastic price process typical of financial assets will be adopted.

Similarly, the firm has no prior contractual links to any gas supplier. Thus the gas consumed by the power plant may in principle be either taken from the local pipeline or brought from abroad and then processed at the LNG plant.²⁵

 $^{^{23}\}mathrm{One}\ \mathrm{Kwh}$ amounts to 3.600 KJ, and one GJ (Gigajoules) is 1 million KJ (Kilojoules).

 $^{^{24}\}mathrm{Since}$ power is measured in Mw.

²⁵Obviously firms currently in operation may be subject to contracts that bind them to local suppliers. As these contracts approach their expiration, though, they may ponder the chance to adopt the LNG technology.

Concept	Value
Output (P_{LNG}) (Nm^3/h)	200,000
Investment Cost (million \in) (I_{LNG})	318
Useful Life (years)	30
Time to Build (months)	36
Necessary Surface	$150,000 \ m^2$
Unit Variable Cost ($\$$ /million Btu) ($CVAR_{LNG}$)	0.30
Fixed Cost (million \in /year) ($CFIX_{LNG}$)	11.8

Table 6: Basic LNG parameters. Source: Basque Government EVE; Bahia Bizkaia.

5.2 The LNG Plant

We consider a LNG plant with total capacity of 200,000 Nm^3/h which is equivalent to 1,752 million Nm^3 per year.²⁶

Under the assumption of 9,500 Kcal for each Nm^3 ,²⁷ this amount is equivalent to:²⁸

$$1,752,000,000 * 9500 * 0.000004186 = 69,671,784 GJ.$$
 (29)

This quantity amounts to 5,805,982 GJ for each month in which the plant operates.

The representative values used are shown in Table 6.

Total investment cost is 318 million €. Fixed costs per month amount to 982,938 €.

6 Valuation of natural gas investments

6.1 The operating NGCC plant

First we compute the value of an immediate investment in a NGCC power plant, which is designed to operate 80% of the time. Revenues come from the electricity produced; they are assumed to be stochastic. Costs include:

- a) The initial outlay, which for the time being is assumed constant.
- b) Variable costs, among them those due to the consumption of fuel (in our case natural gas), assumed stochastic.
- c) Costs related to the emission of CO_2 (tonnes); initially we assume they are deterministic

The present value of revenues, for a finite number of periods (taking into account that there will be no production of electricity until the construction

 $^{^{26}\,}Nm^3$ refers to cubic metres measured at normal conditions of 0 oC temperature and 1 atm pressure.

 $^{^{27}}$ We adopt an average of typical calorific values: 10,000 Kcal for natural gas with upper calorific power and 9,000 Kcal for that of lower calorific power.

²⁸One kilocalorie amounts to 0.000004186 GJ.

phase is completed and, therefore, it will only be in operation from time τ_1 to τ_2) is (see expression (62) in the Appendix):

$$PVR = A \left[\frac{L_e}{r} \left(e^{-r\tau_1} - e^{-r\tau_2} \right) + \frac{E_0 - L_e}{k_e + r} \left(e^{-(k_e + r)\tau_1} - e^{-(k_e + r)\tau_2} \right) \right], \quad (30)$$

where:

A = annual production: 3,504 million Kwh.

 E_0 = current wholesale electricity price: 0.05286542 \in /kwh.(as of April-05, deseasonalised).

 $L_e = \text{long term equilibrium price: } 0.034771 \in /kwh.$

 k_e = speed of reversion for electricity price: 1.3936.

 $\tau_1 = \text{time to build: } 2.5 \text{ years.}$

 $\tau_2 - \tau_1 = \text{useful life of the plant: 25 years.}$

r = riskless interest rate: 5%.

With these values, we get PVR = 1,535.51 million \in .

Variable costs (other than the gas fired and the emission allowances) are computed as follows:

$$PVC_{var} = A.C_{var}.\frac{e^{-r\tau_1} - e^{-r\tau_2}}{r},$$
 (31)

where C_{var} denotes unit variable costs: $0.0032 \in /kwh$. Using these data, we get $PVC_{var} = 141.20$ million \in .

The cost of CO_2 emissions is assumed to be C=10 \in /tonne. This figure times EM=1,226,400 tonnes emitted per year, and applying a formula similar to (31) allow us to compute a present value of carbon costs PVC=154.44 million euros.²⁹

As for the present value of natural gas, this is computed using the estimates from model II, taking as a base date the last day of the series (2005/04/29): $G_0 = 7.2822$ \$/million Btu and $k_gL_0 = 4.2007$. The value of a unit of natural gas consumed from year 2.5 to year 27.5 is determined by formula (58) in the Appendix: 58.4867 \$/million Btu fired per year. This figure amounts to 55.4376 \$/GJ, which translates into $42.7859 \in$ /GJ for an exchange rate of 1.2957 \$/ \in . Given that 22.935.273 GJ/year are needed, the present value of total energy costs is PVG = 981.31 million \in .

In sum, the present value of an operating NGCC plant is a function of G_0 , L_0 and E_0 ceteris paribus:

$$V(G_0, L_0, E_0) = PVR - PVC_{var} - PVG - PVC = 258.56 \text{ million } \in.$$
 (32)

This value includes the positive influence from the expected fall in natural gas price over the construction period of 30 months.

²⁹It is assumed that initially the plant has no emission permit, unlike incumbent plants under their National Allocation Plans.

Since the initial disbursement amounts to I = 211.25 million \in , if the alternatives were to invest at that precise moment or not to invest, we would invest and get a net result of $V(G_0, L_0, E_0) - I = 47.31$ million \in .

6.2 The operating LNG plant

The above results are now used to value an operating LNG plant. We consider an initial situation in which the spread between domestic and foreign gas prices is 0.70\$/mmBtu, and that this difference reflects exactly transport costs of the natural gas to the consuming NGCC plant.³⁰ Therefore, initially it is indifferent whether to use the LNG plant or not from the point of view of the fuel input; yet it would not be used because of variable costs. In other words, initially the import price plus transport costs just equal the domestic price (= 7.2822 \$/mmBtu). From then on, both resources evolve on their own. Specifically, we run 30,000 simulation runs for each gas price.

First we assume a correlation coefficient of 75% between domestic and foreign gas prices. Also, the decision to fire one kind of gas or the other is taken on a monthly basis.

The risk-neutral model is:

$$d\hat{S}_t^d = \left[k(\hat{L}_t^d - \hat{S}_t^d) - \lambda_q \sigma \hat{S}_t^d\right] dt + \sigma \hat{S}_t^d dW_t^{dG},\tag{33}$$

$$d\hat{L}_{t}^{d} = \left[\mu(LE^{d} - \hat{L}_{t}^{d}) - \lambda_{l}\xi\hat{L}_{t}^{d}\right]dt + \xi\hat{L}_{t}^{d}dW_{t}^{dL},$$
(34)

$$d\hat{S}_t^f = [k(\hat{L}_t^f - \hat{S}_t^f) - \lambda_g \sigma \hat{S}_t^f]dt + \sigma \hat{S}_t^f dW_t^{fG}, \tag{35}$$

$$d\hat{L}_t^f = [\mu(LE^f - \hat{L}_t^f) - \lambda_l \xi \hat{L}_t^f]dt + \xi \hat{L}_t^f dW_t^{fL}, \tag{36}$$

$$\rho_{W^{dG}W^{fG}} = 0.75,\tag{37}$$

with the remaining correlation coefficients assumed to equal 0.

Each month, the LNG provides a net cash flow:

$$CF = e^{-\frac{r}{24}} \left[\max \left(\left(\frac{B}{12} (\hat{S}_t^d - \hat{S}_t^f - 0.2195), 0 \right) - 982,938 \right]$$
(38)

where B = 69,671,784 GJ is the amount of energy processed at the plant in a year if it operates every month. We are assuming that the cash flow is obtained at the middle point of each monthly period; thus it must be discounted over half a month

A variable cost of 0.30 \$/mmBtu is assumed; this is equivalent to 0.2195 €/GJ.³¹ Variable costs are only incurred if the LNG plant operates in that

³⁰In other words, initially the import price plus transport costs just equal the domestic price. From then on, each gas reasource evolves on its own.

³¹ Again, we use the equivalence 1 mmBtu = 1,055 GJ and an exchange rate $1.2957\$/\in$.

period. 982,938 is 1/12 of yearly fixed costs. Under the assumption of a useful life of 30 years, there are 360 monthly periods in which to compute the cash flows. Discounted at the risk-free interest rate r = 0.05, these will give us the present value of the plant; for this to be profitable, the value must be higher than the building costs which are disbursed 36 months before starting operation.

The LNG plant's average gross and net present values (in million euros) as a function of the correlation coefficient appears in Table 7.

$ ho_{W^{dG}W^{fG}}$	GPV	NPV
0.65	948.54	630.54
0.70	867.02	549.02
0.75	776.80	458.80
0.80	675.24	357.24
0.85	557.98	239.98

Table 7: Gross and net present values of a LNG plant as a function of the correlation coefficient between domestic and foreign gas prices.

As could be expected, when the correlation between domestic and foreign natural gas prices decreases the LNG plant becomes more valuable.

7 Options on a base load NGCC plant

7.1 Value of a finite-lived option to double plant size

Let us consider a firm which now can build a plant of size X and decide to build another one of equal size in the next five years.³² In order to value this opportunity we run 30,000 Monte Carlo simulations for each one of the 500 regularly distributed dates from year 0 to year 5. Any simulation run fits the discretized equations (13), (14) and (15). Depending on the specific values of the correlation coefficients, the Monte Carlo simulation technique may require the generation of two or more correlated Normal variates. In our case, we assume $\rho_{G,L} = \rho_{L,E} = 0.0$, but $\rho_{G,E} = 0.55$; also, we adopt $\Delta t = 0.01$.

The series obtained for \hat{G}_t , \hat{L}_t and \hat{E}_t allow to compute at any time the value V_t of an investment at that time, taking into account the evolution of electricity and gas prices, as well as the behaviour of the equilibrium gas price in the short term (\hat{L}_t) . Apart from the initial outlay (which is disbursed at the time of the investment), all other costs and revenues are due starting 2.5 years later.³³

Given the values of V_t at any moment and in each path, the Least Squares MonteCarlo (LSM) approach is used.³⁴ At the last moment, the value of the

 $^{^{32}}$ As before, in case the firm decides to invest, building the new plant takes time, namely 2.5 years.

³³Previously we have checked the convergence of the average price for a long term, say $\hat{G}_{27,5}$, towards the expected futures price for that specific date; this can be computed analytically and happens to be $3.5983 \in /\text{GJ}$.

³⁴See Longstaff and Schwartz [19] for a description of this method.

investment in each path is:

$$\max(V(G_T, L_T, E_T) - I, 0).$$
 (39)

At earlier moments, the method is based on the computation of a series of parameters that allow to construct a linear combination of basic functions. This combination allows to estimate at each step the continuation value. The specification adopted consists of a second-order expected continuation value function with 10 regressors (since there are 3 sources of risk), namely:³⁵

$$E_i^Q[e^{-r\Delta t}V_{i+1}(\hat{G}_{i+1},\hat{L}_{i+1},\hat{E}_{i+1})] \approx a_1 + a_2\hat{G}_i + a_3\hat{G}_i^2 + a_4\hat{L}_i + a_5\hat{L}_i^2 + a_6\hat{E}_i + a_7\hat{E}_i^2 + a_8\hat{G}_i\hat{L}_i + a_9\hat{G}_i\hat{E}_i + a_{10}\hat{L}_i\hat{E}_i.$$
(40)

At any time, considering the paths that are in-the-money and by ordinary least squares, we can get the value of the 10 coefficients.³⁶

The valuation results are shown in Figure 7; as can be noted, the value of this option increases with the maturity of the option.

The most significant values are displayed in Table 8.

Maturity (years)	Option Value (million €)	Project Total Value
0.00	47.31	94,62
1.00	111.37	158.68
2.00	144.26	191.57
3.00	167.15	214.46
4.00	183.46	230.77
5.00	195.48	242.79

Table 8: Value of the option to decide doubling the plant size.

With 5 years to decide doubling the plant size, the value of the option increases to 195.48 million \in ; it benefits from the expected decline in gas prices and from a lower present value of the initial disbursement. Project's total value, i.e. the net value of the initial investment in an operating plant plus the option to double plant size, results from adding 47.31 million \in to the above series. With 5 years ahead, project's total value is 242.79 million \in , some 150 million \in above the value of building two lower-sized plants at the initial moment.

³⁵Cortazar, Gravet and Urzua [9] propose using powers of expected spot prices instead of functional forms of the state variables. The rationale for this is that, in many cases, optimal exercise depends on expected spot prices and volatilities. They successfully implement their method in an extended version of Brennan and Schwarz [7] model.

 $^{^{36}}$ The optimal exercise frontier would be given by a surface formed with those values of \hat{G}_i , \hat{L}_i and \hat{E}_i that satisfy the following condition: $V_i(\hat{G}_i,\hat{L}_i,\hat{E}_i) = a_1 + a_2\hat{G}_i + a_3\hat{G}_i^2 + a_4\hat{L}_i + a_5\hat{L}_i^2 + a_6\hat{E}_i + a_7\hat{E}_i^2 + a_8\hat{G}_i\hat{L}_i + a_9\hat{G}_i\hat{E}_i + a_{10}\hat{L}_i\hat{E}$, that is, the values for which the present value of investing at that time i equals the continuation value.

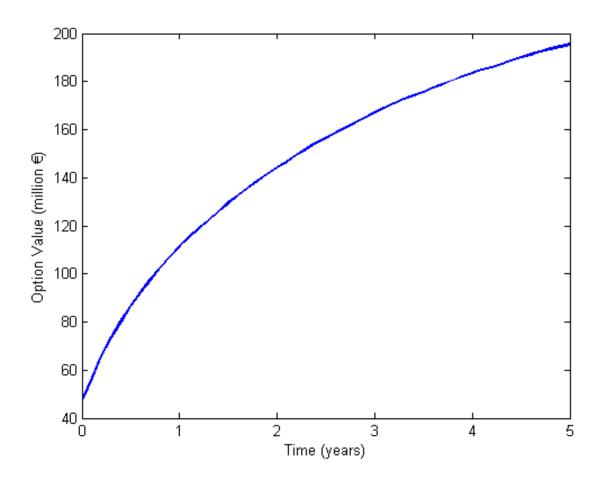


Figure 7: Value of the option to invest as a function of the option's maturity.

If it is compared with a project to invest in a double-sized plant, with a 10% saving in building costs and a higher efficiency of 57%, the project's value amounts to 205.72 million €; this is more than the value of investing initially in two smaller plants, but less than the value of a modular project, when the option to invest has a maturity of 3 or more years.

7.2 Value of the option to invest when the initial investment cost I is stochastic

Consider now a stochastic initial investment I according to the following equation:

$$dI_t = \alpha_I I_t dt + \sigma_I I_t dW_t^I, \tag{41}$$

with the traditional meaning for each variable and $\rho_{W^IW^G} = \rho_{W^IW^L} = \rho_{W^IW^E} = 0$.

The risk-adjusted version would be:

$$d\hat{I}_t = (\alpha_I - \lambda_I \sigma_I)\hat{I}_t dt + \sigma_I \hat{I}_t dW_t^I. \tag{42}$$

After discretization:

$$\Delta \hat{I}_t = (\alpha_I - \lambda_I \sigma_I) \hat{I}_t \Delta t + \sigma_I \hat{I}_t \sqrt{\Delta t} \epsilon_t^I, \tag{43}$$

where $\epsilon_t^I \sim N(0,1)$.

We analyse the case in which $\alpha_I - \lambda_I \sigma_I = 0$, $\Delta t = 0.01$ and $\sigma_I = 0.30.^{37}$ For each of the 30,000 paths of \hat{G}_t , \hat{E}_t and \hat{L}_t we get a path for \hat{I}_t . This will allow to estimate, at each moment, the value of an immediate investment and hence what paths are in-the-money at that precise time. For the option with 5 years to maturity we compute a value of 204.38 million \in , a figure which is slightly above the 195.48 million \in estimated above. Table 9 shows the value of the option to invest as a function of initial investment's volatility.

7.3 Value of the option to invest when the cost of CO_2 emissions is stochastic

Now consider that, in addition to the initial outlay, also the cost of CO_2 emissions is stochastic and follows the process:

$$dC_t = \alpha_C C_t dt + \sigma_C C_t dW_t^C \tag{44}$$

with the usual meaning for each variable and $\rho_{W^CW^G}=\rho_{W^CW^L}=\rho_{W^CW^E}=\rho_{W^CW^I}=0.$

 $^{^{37}}$ With this volatility, one year from now the initial investment will range between -30% and +30% times the current amount with a probability of 68.27% (approximately 2/3).

 $^{^{38}}$ Obviously at every time the average of the 30,000 simulations must be 211.25 million \in

Volatility (σ_I)	Option Value (million €)
0.00	195.48
0.10	195.59
0.20	198.26
0.30	204.38
0.40	214.53
0.50	226.73
0.60	239.87
0.70	253.23
0.80	266.02
0.90	278.17
1.00	289.45

Table 9: Vaue of the option to invest in 5 years with stochastic building costs.

The risk-neutral version would be:

$$d\hat{C}_t = (\alpha_C - \lambda_C \sigma_C)\hat{C}_t dt + \sigma_C \hat{C}_t dW_t^C. \tag{45}$$

After discretization:

$$\Delta \hat{C}_t = (\alpha_C - \lambda_C \sigma_C) \hat{C}_t \Delta t + \sigma_C \hat{C}_t \sqrt{\Delta t} \epsilon_t^C. \tag{46}$$

where $\epsilon_t^C \sim N(0, 1)$.

Next we compute the value of the option to invest up to five years ahead for different values of emission permits' volatility and two possible values for $(\alpha_C - \lambda_C \sigma_C)$, namely 0 and r.

Given an initial level C_0 , the expected value at time t under the risk-neutral probability measure is:

$$E(\hat{C}_t) = C_0 e^{(\alpha_C - \lambda_C \sigma_C)t}. (47)$$

The value of an annuity between time τ_1 and time τ_2 is determined by:

$$V_{\tau_1,\tau_2}^c = \int_{\tau_1}^{\tau_2} E(\hat{C}_t) e^{-rt} dt \tag{48}$$

which gives:

$$V_{\tau_1,\tau_2}^c = \frac{C_0}{\alpha_C - \lambda_C \sigma_C - r} \left[e^{(\alpha_C - \lambda_C \sigma_C - r)\tau_2} - e^{(\alpha_C - \lambda_C \sigma_C - r)\tau_1} \right]. \tag{49}$$

The total cost comes from multiplying this amount times 1,226,400 tonnes of CO_2 per year. Consider two situations:

a) When $(\alpha_C - \lambda_C \sigma_C) = 0$ we have:

$$V_{\tau_1,\tau_2}^c = \frac{C_0}{-r} [e^{-r\tau_2} - e^{-r\tau_1}]. \tag{50}$$

With $C_0 = 10$ \in /tonne, $\tau_1 = 2.5$ and $\tau_2 = 27.5$ this amounts to a cost of 125.93 \in /tonne, which corresponds to a present value of total emission cost of 154.44 million, the same figure as in the base case.

b) When $(\alpha_C - \lambda_C \sigma_C) = r = 0.05$ we have an annuity value

$$V_{\tau_1,\tau_2}^c = C_0[\tau_2 - \tau_1]. (51)$$

With $C_0 = 10$ \in /tonne, $\tau_1 = 2.5$ and $\tau_2 = 27.5$ this gives a cost of 250.00 \in /tonne, which corresponds to a present value of total emission cost of 306.60 million \in .

Now the difference in both cases is that these values are not fixed. Instead, they depend on the initial value C_0 at each moment and which is obtained by Monte Carlo simulations. The value of the option to invest (in million euros) is shown in Table 10.

Maturity (years)	Option Value (0%)	Option Value (5%)
0.00	47.31	0.00
0.50	87.41	16.50
1.00	113.08	34.31
1.50	131.58	47.94
2.00	146.72	58.73
2.50	159.09	68.14
3.00	169.78	76.59
3.50	178.69	83.28
4.00	186.76	89.51
4.50	193.85	94.91
5.00	199.56	99.76

Table 10: Vaue of the option to invest in 5 years with stochastic CO2 emission costs.

When the expected growth rate of emission costs is 0%, the option values obtained are a bit higher than in the base case, whereas they are significantly lower with an expected growth rate of 5%.

7.4 Value of the option to invest when its maturity is stochastic

Here we consider the case in which the option to invest has a stochastic time to maturity. This means that there is a probability λ that it will disappear in a given year; thus the probability to disappear during a period dt is λdt . We assume that the opportunity to invest vanishes anyway at the end of the fifth year. Also, as soon as the option expires, the value of the project becomes 0.

Random samples from a Poisson distribution with parameter λ are drawn to get the moment at which the right to invest ceases; given the value of the project at each simulation run the LSM approach is used; these values will be 0

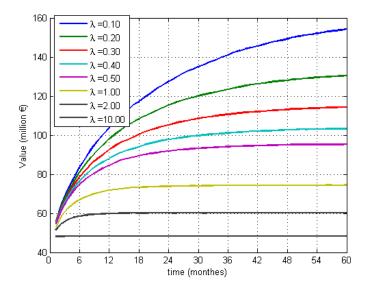


Figure 8: Value of the option to invest as a function of its maturity under several expiration probabilities.

whenever the option to invest has disappeared. In other words, the continuation value takes into account the chance that while waiting for one more period the option to invest may vanish.

Figure 8 shows the value of the option to invest as a function of the probability λ and the option's maturity.

For low probabilities λ , the values of the option are slightly lower than in the base case. For very high values of λ , the value approaches 47.31 million \in , which happens to be the option's value when the only decision is whether to invest at the initial moment or not.

8 Concluding remarks

This paper evaluates investments in natural gas plants. Our first example is a plant which burns gas to produce electricity by means of a combined cycle; the second one is a plant for storing gas depending on the price gap between domestic and foreign gas resources (or as a move towards greater diversification due to energy security concerns). The fact that these plants take time to build is explicitly modelled. Also, the recent operation of the EU Emmission Trading Scheme has brought a new commodity, carbon, that will have an impact on energy investments, at least for European utilities.

We assume that both natural gas and electricity prices follow mean-reverting

stochastic processes, namely an Inhomogenous Geometric Brownian Motion. We calibrate a model for each price using actual market data. The first set consists of NYMEX Natural Gas futures contracts; the second one refers to the Spanish wholesale electricity market. Once we have described the basic features of our case study, the above operating plants are valued under the assumption of a finite useful life. Finally, Least Squares Monte Carlo Simulation is used to value several American-type options to invest in a natural gas power plant.

A Valuation of annuities for an IGBM process

A.1 Annuity of natural gas

In this model composed of equations (1) and (2), the expected values must satisfy the following differential equations:

$$E(dG_t) = k_g[E(L_t) - E(G_t)]dt,$$
(52)

$$E(dL_t) = \mu [L_q - E(L_t)]dt. \tag{53}$$

From the second equation it is possible to get: $E(L_t) = L_g + (L_0 - L_g)e^{-\mu t}$, and substituting in the first one results:

$$E(dG_t) = k_q [L_q + (L_0 - L_q)e^{-\mu t} - E(G_t)]dt.$$

Using a factor of integration $e^{k_g t}$ and rearranging:

$$e^{k_g t} E(dG_t) + k_g e^{k_g t} E(G_t) dt = \left[k_g L_g e^{k_g t} + k_g (L_0 - L_g) e^{-(\mu - k_g) t} \right] dt,$$

$$e^{k_g t} E(G_t) = L_g e^{k_g t} - \frac{k_g (L_0 - L_g)}{\mu - k_g} e^{-(\mu - k_g)t} + c.$$

For t = 0 then $E(G_t) = G_0$.

$$c = G_0 - L_g + \frac{k_g(L_0 - L_g)}{\mu - k_g}.$$

Solving for the expected value:

$$E(G_t) = L_g - \frac{k_g(L_0 - L_g)}{\mu - k_g} e^{-\mu t} + \left[G_0 - L_g + \frac{k_g(L_0 - L_g)}{\mu - k_g} \right] e^{-k_g t}$$
 (54)

For the particular case in which equation (2) reduces to a GBM type, the solution of Pilipovic [24] results.

Nonetheless, the last equation does not allow to compute the value of an annuity. It is necessary to use the risk-neutral version of the model composed by equations (6) and (7). Following the same steps we obtain:

$$E(\hat{G}_t) = \frac{\mu k_g L_g}{(\mu + \lambda_l \xi)(k_g + \lambda_g \sigma_g)} (1 - e^{-(k_g + \lambda_g \sigma_g)t}) + G_0 e^{-(k_g + \lambda_g \sigma_g)t} +$$

$$+ \left[\frac{\mu k_g L_g}{(\mu + \lambda_l \xi)(\mu + \lambda_l \xi - k_g - \lambda_g \sigma_g)} - \frac{k_g L_0}{(\mu + \lambda_l \xi - k_g - \lambda_g \sigma_g)} \right] \cdot (55)$$

$$\cdot \left(e^{-(\mu + \lambda_l \xi)t} - e^{-(k_g + \lambda_g \sigma_g)t} \right)$$

$$(56)$$

When $\lambda_q = \lambda_l = 0$, we have equation (54).

The value of an annuity between time τ_1 and time τ_2 is determined by the following equation:

$$V_{\tau_1,\tau_2} = \int_{\tau_1}^{\tau_2} E(\hat{G}_t) e^{-rt} dt$$
 (57)

The resulting value for the annuity is:

$$V_{\tau_1,\tau_2} = \frac{\mu k_g L_g}{r(\mu + \lambda_l \xi)(k_g + \lambda_g \sigma_g)} (e^{-r\tau_1} - e^{-r\tau_2}) +$$

$$+\frac{\mu k_g L_g}{(\mu+\lambda_l \xi)(k_g+\lambda_g \sigma_g)(k_g+\lambda_g \sigma_g+r)} (e^{-(k_g+\lambda_g \sigma_g+r)\tau_2} - e^{-(k_g+\lambda_g \sigma_g+r)\tau_1}) +$$

$$+\frac{k_g L_0}{(\mu + \lambda_l \xi - k_g - \lambda_g \sigma_g)(\mu + r + \lambda_l \xi)} \left(e^{-(\mu + \lambda_l \xi + r)\tau_2} - e^{-(\mu + \lambda_l \xi + r)\tau_1}\right) +$$

$$+\frac{k_g L_0}{(\mu + \lambda_l \xi - k_g - \lambda_g \sigma_g)(k_g + r + \lambda_g \sigma)} \left(e^{-(k_g + \lambda_g \sigma_g + r)\tau_1} - e^{-(k_g + \lambda_g \sigma_g + r)\tau_2}\right) +$$

$$+\frac{\mu k_g L_g}{(\mu + \lambda_l \xi)(\mu + \lambda_l \xi - k_g - \lambda_g \sigma_g)(\mu + r + \lambda_l \xi)} (e^{-(\mu + \lambda_l \xi + r)\tau_1} - e^{-(\mu + \lambda_l \xi + r)\tau_2}) +$$

$$+\frac{\mu k_g L_g}{(\mu+\lambda_l \xi)(\mu+\lambda_l \xi-k_g-\lambda_g \sigma_g)(k_g+r+\lambda_g \sigma_g)} (e^{-(k_g+\lambda_g \sigma_g+r)\tau_2}-e^{-(k_g+\lambda_g \sigma_g+r)\tau_1})$$

$$+\frac{G_0}{k_g+r+\lambda_g\sigma_g}\left(e^{-(k_g+\lambda_g\sigma_g+r)\tau_1}-e^{-(k_g+\lambda_g\sigma_g+r)\tau_2}\right). \tag{58}$$

When equation (2) is of the GBM form with $L_g = 0$ and $\mu = -\varphi$, the value of the annuity is:

$$V_{\tau_1,\tau_2} = \frac{k_g L_0}{(\varphi - \lambda_l \xi + k_g + \lambda_g \sigma_g)(\varphi - r - \lambda_l \xi)} (e^{(\varphi - \lambda_l \xi - r)\tau_2} - e^{(\varphi - \lambda_l \xi - r)\tau_1}) +$$

$$+\frac{k_g L_0}{(\varphi - \lambda_l \xi + k_g + \lambda_g \sigma_g)(k_g + r + \lambda_g \sigma_g)} (e^{-(k_g + \lambda_g \sigma_g + r)\tau_2} - e^{-(k_g + \lambda_g \sigma_g + r)\tau_1}) +$$

$$+\frac{G_0}{k_g+r+\lambda_g\sigma_g}\left(e^{-(k_g+\lambda_g\sigma_g+r)\tau_1}-e^{-(k_g+\lambda_g\sigma_g+r)\tau_2}\right). \tag{59}$$

If, in addition, $\varphi = 0$ and $\xi = 0$, we get the value of an annuity between $\tau_1 y$ which follows an IGBM process:

$$V_{\tau_{1},\tau_{2}} = \frac{k_{g}L_{0}}{r(k_{g} + \lambda_{g}\sigma_{g})} (e^{-r\tau_{1}} - e^{-r\tau_{2}}) - \frac{k_{g}L_{0}}{(k_{g} + \lambda_{g}\sigma_{g})(k_{g} + r + \lambda_{g}\sigma_{g})} \cdot$$

$$\cdot \left(e^{-(k_g + \lambda_g \sigma_g + r)\tau_1} - e^{-(k_g + \lambda_g \sigma_g + r)\tau_2} + \frac{G_0}{k_g + r + \lambda_g \sigma_g} \left(e^{-(k_g + \lambda_g \sigma_g + r)\tau_1} - e^{-(k_g + \lambda_g \sigma_g + r)\tau_2}\right). \tag{60}$$

Finally if also $\tau_1 = 0$ then:

$$V_{0,\tau_{2}} = \frac{k_{g}L_{0}}{r(k_{g} + \lambda_{g}\sigma_{g})} (1 - e^{-r\tau_{2}}) - \frac{k_{g}L_{0}}{(k_{g} + \lambda_{g}\sigma_{g})(k_{g} + r + \lambda_{g}\sigma_{g})} \cdot (1 - e^{-(k_{g} + \lambda_{g}\sigma_{g} + r)\tau_{2}}) + \frac{G_{0}}{k_{g} + r + \lambda_{g}\sigma_{g}} (1 - e^{-(k_{g} + \lambda_{g}\sigma_{g} + r)\tau_{2}}).$$
(61)

A.2 Annuity of electricity

In this case, fiven the parameters adopted, it is easy to show that the value of the annuity is:

$$V_{\tau_1,\tau_2} = \frac{L_e}{r} \left(e^{-r\tau_1} - e^{-r\tau_2} \right) + \left(\frac{E_0}{k_e + r} - \frac{L_e}{k_e + r} \right) \left(e^{-(k_e + r)\tau_1} - e^{-(k_e + r)\tau_2} \right). \tag{62}$$

The first term in the right-hand side accounts for the equilibrium price, whereas the second one adds the spread between current price and the equilibrium price.

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