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2 **Reliability of Measurement of Skin Ultrasonic Properties *in Vivo*:**

3 **A Potential Technique for Assessing Irradiated Skin**

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1 **Abstract**

2 **Background/aims:** Quantitative and objective technique to assess radiation-induced
3 tissue fibrosis is important for clinicians to estimate the efficiency of radiotherapeutic
4 schemes. It has been widely reported that ultrasonic properties are sensitive to
5 changes of acoustic scatterers in biological tissues. Therefore, measurement of
6 ultrasonic properties may serve as a potential assessment technique for irradiated
7 skins. The aim of the present study is to investigate the reliability of such
8 measurement so as to evaluate its potentials for future clinical applications.

9 **Methods:** Ultrasonic parameters including attenuation slope (β), integrated
10 attenuation (IA) and integrated backscatter (IBS) were measured for the frequency
11 range of 10 to 25 MHz from echographic signals of the forearm and neck dermis of 20
12 normal subjects *in vivo*. The intra- and inter-rater reliability of measurement was
13 assessed in 10 normal subjects using intra-class correlation coefficients (ICC) and
14 Bland-Altman test.

15 **Results:** The intra- and inter-rater measurement was demonstrated to be reliable as
16 indicated by high ICC values generally larger than 0.80. In addition, the ultrasonic
17 parameters could successfully differentiate the skins in the neck and forearm regions.

18 **Conclusion:** The measurement provided reliable information on the ultrasonic
19 properties of the skins and could be potentially applied to comparative clinical trials
20 to assess the late effects of radiotherapy on skins.

21

22 **Keywords:** radiotherapy – skin – fibrosis – high frequency ultrasound – ultrasonic
23 tissue characterization – ultrasonic properties – reliability.

1 **Introduction**

2 Fibrosis is a common late side effect of radiotherapy. Assessment and
3 quantification of the severity of tissue fibrosis are important in determining the curing
4 ratio of different radiotherapeutic regimes or assessing the efficiency of various anti-
5 fibrotic medicines (1). Although some standard protocols such as the LENT/SOMA
6 scoring system have been established to assess the degrees of late radiation toxicities
7 (1), clinical practice is still mainly limited to hand palpation. Quantitative and
8 objective methods have not been intensively investigated for this purpose.

9 Being noninvasive and inexpensive, high-frequency (larger than 10 MHz)
10 ultrasound has been successfully introduced in dermatology to detect the delicate skin
11 structures and lesions in the last two decades (2-4). Applications of ultrasound
12 reported in dermatology generally include two kinds of measurement, i.e., skin
13 thickness and echogenicity. Skin thickness can be directly measured from the
14 ultrasound images, while a common way to calculate the echogenicity is based on
15 counting the number of pixels with a certain range of intensity values in images (5).
16 This method has been used for the study of skin reactions induced by therapeutic or
17 accidental radiation and high frequency ultrasonic imaging is recommended as a
18 reliable tool to assess the irradiated effects on the skin (6, 7).

19 On the other hand, it has been widely reported that ultrasonic propagation
20 properties are sensitive to the structural, compositional and pathological changes of
21 acoustic scatterers in biological tissues (8). The propagation parameters are extracted
22 from the radiofrequency (RF) signals, thus capable of providing new information on
23 tissue conditions, such as frequency-dependent attenuation, in addition to the
24 envelope signals used in the conventional ultrasonic imaging. Previous studies had
25 showed that it was potential to monitor the skin changes induced by healing process

1 or patch-test (9, 10). We have successfully used an ultrasound indentation technique
2 to measure the mechanical properties of neck tissues with radiotherapy-induced
3 fibrosis (11-13). During the study, we noted that the ultrasound signals scattered from
4 the skin and subcutaneous tissues were different for subjects with different degrees of
5 tissue fibrosis. In this study, we aimed to test the reliability of the high frequency
6 ultrasound measurement for the skin assessment so as to prepare for the future clinical
7 applications of this technique.

8 There had been some reports on the reliability of measurement of skin ultrasonic
9 parameters in literature. For example, Guittet et al. (14) reported a coefficient of
10 variation of 12% for the attenuation slope of skin; Fournier et al. (15) reported a
11 standardized coefficient of variation of less than 20% for the backscatter spectral
12 parameters of skin. However, it is difficult to transfer the measurement precision from
13 one system to another due to the use of different devices and detection techniques.
14 Accordingly, we investigated the reliability of measurement of ultrasonic parameters
15 including attenuation slope, integrated attenuation and integrated backscatter in the
16 skin *in vivo* using a 20 MHz ultrasonic imaging system. Intra-class correlation
17 coefficients (ICC) and Bland-Altman test were used to estimate the reliability with
18 respect to the intra- and inter-rater operations.

19

20 **Methods**

21 **Data acquisition system**

22 The system used for data collection was a 20 MHz ultrasonic imaging system
23 developed for skin applications (Ultrasons Technologies, Tours, France). A handheld
24 cylindrical probe, inside which there was a focused mono-element transducer, was

1 used to collect echographic RF signals. Using the reflection signals from a planar steel
2 plate immersed in a water tank, the measured central frequency of the transducer was
3 15 MHz with a -3 dB bandwidth of 10~25 MHz. A rigid removable cover with a flat
4 membrane of 15 μm in thickness was tightly attached to the end of the probe to allow
5 the ultrasound propagating through and to form the chamber for the acoustic coupling
6 medium. The ultrasonic beam focused at approximately 2 mm beyond the membrane.
7 Water was used to fill the cavity formed by the cover and the transducer. The
8 transducer was translated linearly in the probe during operation. The contact area
9 between the cover and the skin was small with a dimension of $11 \times 19 \text{ mm}^2$ and the
10 effective width of image was 6 mm in the lateral direction. Each collected image
11 provided a set of 256 RF signal lines, with 1024 data points in each line sampled at
12 100 MHz. The lateral resolution of the transducer was approximately 0.2 mm,
13 therefore producing totally 28 independent lines per image, which were used for
14 spatial averaging. In the studied region of interest (from 0.3 to 1.3 mm beneath the
15 skin surface), we found that the average Pearson correlation for two adjacent lines
16 was 0.24 ± 0.04 in the forearms of 5 normal subjects, indicating good independence
17 for the signals.

18 **Extraction of ultrasonic parameters**

19 In this study, the skin was assumed to be composed of epidermis and dermis with
20 a total thickness larger than 1.3 mm and the speed of sound was assumed to be 1.58
21 mm/ μs throughout the whole skin layer (16). The ultrasonic propagation parameters
22 were extracted from the spatially averaged RF signals using a multi-narrowband
23 algorithm (17). The reference signals from a planar steel plate were collected in order
24 to correct the system-dependent effects. The detailed procedure was described as
25 follow.

1 Attenuation slope (β) and integrated attenuation (IA). A Hamming-window with a
2 length of 50 points (0.40 mm) was used to gate the original temporal signal from the
3 point 40 (0.32 mm) after the skin entry echo to the point 165 (1.30 mm) with 50%
4 overlapping between two consecutive windows. This region was defined as the region
5 of interest (ROI) as shown in Fig 1.a and 1.b. The skin entry echo was detected
6 automatically in a custom-designed program based on the sudden change of the signal
7 energy. According to the window selection principle, totally six short signals were
8 obtained from each scanned line. Fast Fourier transform (FFT) was used to obtain the
9 power spectra of the short signals after they were zero-padded to 512 points. The
10 power spectra from the 28 independent lines were then averaged before they were
11 divided by those of the corresponding reference signals to correct the system-
12 dependent effects. The spectra of reference signals were obtained by applying the
13 same window to the signals completely reflected from the steel plate in water at the
14 same distance as the selected short signals. The signal lines which had saturated in the
15 ROIs were excluded in the averaging procedure in order to avoid the contamination of
16 spectra induced by the saturation. After correction, the six power spectra were
17 logarithmically transformed (Fig 1.c) and regressed by the propagation distances of
18 ROIs. Based on a commonly used hypothesis that the skin backscatter was
19 homogeneous in all selected skin depths (18), the attenuation coefficients $\alpha(f)$ (unit:
20 dB/mm) in 10~25 MHz were obtained (Fig 1.d). It was assumed that $\alpha(f)$ was
21 linearly dependent on frequency, i.e.:

$$22 \quad \alpha(f) = \beta \cdot f + \alpha_0 \quad (1)$$

23 where β (unit: dB/mm/MHz) is the attenuation slope and α_0 (unit: dB/mm) is the
24 intercept at zero frequency. β was then calculated from the regression of $\alpha(f_i)$ to

1 frequency f_i obtained from the experiment. The integrated attenuation (IA, unit:
2 dB/mm) was defined as:

$$3 \quad \text{IA} \equiv \frac{1}{f_h - f_l} \int_{f_l}^{f_h} \alpha(f) df \quad (2)$$

4 where $f_l = 10$ MHz and $f_h = 25$ MHz, are the lower and upper bounds of the -3 dB
5 bandwidth of the transducer.

6 Integrated backscatter (IBS). The signal in the ROI from the point 40 to 165 (0.32
7 to 1.30 mm) after the skin entry was used for the calculation of the backscatter
8 coefficient. The temporal signals were gated using a Hamming-window (125 points)
9 and zero-padded to 512 points before FFT transformation to power spectra. The
10 power spectra of the independent lines of each image were averaged and divided by
11 those of the reference signals using the same Hamming-window. The system-
12 corrected spectra were then logarithmically transformed to obtain the backscatter
13 spectra $B(f)$. The integrated backscatter (IBS, unit: dB) was then defined similarly to
14 that of IA:

$$15 \quad \text{IBS} \equiv \frac{1}{f_h - f_l} \int_{f_l}^{f_h} B(f) df \quad (3)$$

16 where f_h and f_l are the range of the -3 dB bandwidth as in Eq. (2). It should be
17 noted that IBS was not corrected by attenuation of the skin-film-water interface and
18 the partial skin on top of the selected region. This parameter represented an average
19 level of backscatter of the selected skin.

20 **Tests of reliability and experiments on normal subjects**

21 The *in-vivo* study was conducted for 20 normal subjects (age: 27 ± 3 yrs) under
22 room temperature at approximately 25°C. In order to test the intra-rater reliability of

1 this measurement, tests on 10 normal subjects were conducted by the first operator
2 twice with a time lapse of one week. To test the inter-rater reliability, the
3 measurement was also conducted by a second operator during the first data collection
4 by the first operator. The two operators were both working in the ultrasound field and
5 knew well the principles and details of the measurement. The selected testing sites
6 were located on the palmar side (3 cm away from the radiocarpal joint and along the
7 media nerve) and the dorsal side (in the middle portion of the forearm and 2 cm
8 proximal to the ulnar styloid) of the distal forearm and also on both sides (5 cm below
9 the mastoid bone) of the neck. We were interested in neck sites because we would
10 recruit patients who had skin fibrosis in the neck due to radiotherapeutic radiation in
11 future studies. The forearm testing sites served as the comparative parts of the neck
12 sites in the same subject. The study was approved by the Research Ethics Committee
13 of the investigators' affiliated institutions and written informed consent was obtained
14 from each subject at recruitment.

15 The subjects were asked to be seated when the forearm sites were tested, and to lie
16 on their sides when the neck sites were tested, both in a relaxing state. The probe was
17 applied to the skin surface using a very small pressure in order to avoid changing the
18 ultrasonic properties inconsistently by the probe pressure (15). Water was used as
19 coupling medium between the probe and skin. Three repeated tests were conducted at
20 each testing site and the averaged results of the three tests were used to represent the
21 ultrasonic properties at that site.

22 **Data analysis methods**

23 The intraclass correlation coefficient (ICC) and the Bland-Altman test (19) were
24 used to estimate the reliability of the ultrasound measurement. ICC represents the
25 proportional contribution of variance of interest with respect to total variance

1 (variance of interest + measurement error). In our study, intra-rater and intra-rater
2 reliability was respectively assessed by ICC(1,3) and ICC(3,3), the detailed meaning
3 of which was described in (19). Bland-Altman test is used to analyze the individual
4 difference of two repeated measurements. The reliability coefficient, as defined to be
5 two standard deviations of the individual difference by assuming the mean difference
6 to be zero, stands for the range of individual difference observed for 95% pairs of
7 measurements (19). ICC and Bland-Altman test were widely used to quantify the
8 reliability of measurement for continuous data.

9 The ultrasonic parameters in normal subjects were compared using the paired *t*-
10 test between two sites in the forearm, in the neck, and between the forearm and neck
11 regions. The parameters of two testing sites in the forearm or neck were pooled to be
12 mean values of the forearm or neck if no significant difference was found in the two
13 regions. All the statistical analyses were conducted by using the statistical software
14 SPSS (SPSS Inc., Chicago, IL, USA). A comparison with $P < 0.05$ was used to
15 indicate a significant difference.

16

17 **Results**

18 Table 1 shows the results of ICC and their 95% confidence intervals for the intra-
19 and inter-rater measurement. All ICCs were larger than 0.80, which indicated a high
20 reliability. Table 2 shows the results of Bland-Altman test for the individual
21 difference of intra- and inter-rater operations. 95% CIs of the individual difference of
22 ultrasonic properties included zero value, indicating the intra- and inter-rater
23 measurement was unbiased.

24 Fig 2 shows the typical images obtained from the forearm and neck regions of a
25 normal subject. It was consistently observed from these images that the neck skin in

1 the dermal region was darker in comparison with the forearm skin. Fig 3 shows a
2 summary of the ultrasonic properties measured from the 20 normal subjects. For all
3 the parameters, no significant difference was demonstrated between two sites of the
4 forearm ($P > 0.05$) and between two sides of the neck ($P > 0.05$). Therefore, data of
5 the two sites within each region were pooled for the subsequent data analyses. For the
6 attenuation coefficients, a linear relationship versus frequency with a regressed
7 correlation coefficient larger than 0.90 could be generally obtained (Fig 1.d), showing
8 that a linear relationship was good enough to describe the frequency-dependent
9 characteristics. In the neck and forearm regions of the normal subjects, β was 0.328
10 ± 0.037 and 0.375 ± 0.037 dB/mm/MHz ($P < 0.001$), IA was 2.17 ± 1.90 and $0.58 \pm$
11 1.34 dB/mm ($P = 0.001$), and IBS was -33.55 ± 3.12 and -31.42 ± 2.44 dB ($P <$
12 0.001), respectively. The finding of a smaller IBS in the neck region was consistent
13 with the observation of the dermal echogenicity in the images.

14

15 **Discussion**

16 A hand-held 20 MHz ultrasound probe was introduced in the current study to
17 measure the ultrasonic propagation properties of skin *in vivo*. The reliability of intra-
18 and inter-rater measurement was investigated in order to assess its potential use in
19 clinical trials. Tests for 20 normal subjects were conducted and results were reported.

20 The results showed that all ICCs for the intra- and inter-rater tests were larger than
21 0.80, indicating that the measurement was highly reliable (20). It means that the
22 influence of day-to-day and rater-to-rater variations were limited in the given test
23 conditions. However, it should be noted that in order to maintain such high test
24 reliability, basic training on the test operations for a rater was necessary before the
25 rater could conducted the corresponding research. The key factors in operating the

1 probe included gentle contact pressure, accurate probe orientation and good coupling
2 between the probe and skin. If these conditions could be guaranteed, the measurement
3 could be highly reliable and this ultrasound method was potential to be applied in
4 clinical trials to assess the skin effects induced by radiotherapy.

5 The acoustic properties of the skins in the forearm and neck were demonstrated to
6 be significantly different by the ultrasonic measurement. The difference was regarded
7 as a reflection of the anatomic distinction of the skins in these two regions. Raju et al.
8 (18) reported a larger β in the dermis of fingertip in comparison with that of two
9 locations in the forearm. They attributed the difference to the potential variations of
10 skin tension and collagen structure between the fingertip and forearm skins. A
11 significantly smaller value of *IBS* was found in the neck than forearm region in the
12 current study. Relevant study about skin echogenicity by Pellacani and Seidenari (21)
13 demonstrated that the facial skin was much less reflective than the forearm skin. Thus
14 the current findings were not contradictive to their results if the neck skin was
15 assumed to be more similar to the facial skin in terms of ultrasonic scattering. Further
16 investigations are required to explain the exact reason for the differences between the
17 two regions.

18

19 **Conclusion**

20 The reliability of the current measurement of the ultrasonic properties was high
21 with ICCs larger than 0.80. The ultrasonic parameters could discriminate the skins in
22 the forearm and neck regions in the normal subjects. Considering that the operation of
23 the current method was reliable, easy, and non-invasive, we expected that it would be
24 potentially useful for the comparative clinical trials to assess the late effects of
25 radiotherapy to the skin and future research towards this direction is being conducted.

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6

7

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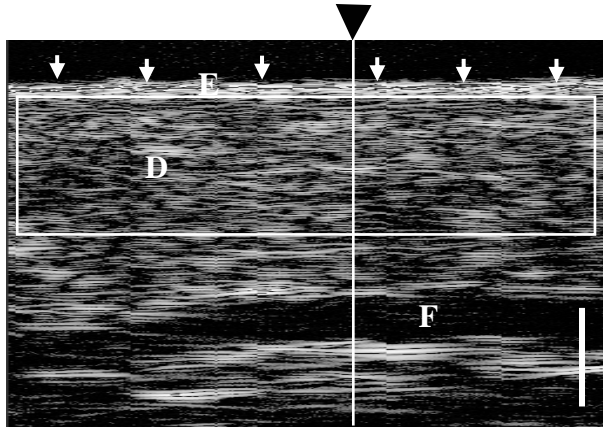
1 **Figure captions:**

2 Fig. 1. The processing of the RF signals for the extraction of the attenuation
3 coefficients. (a) One typical RF image of the normal skin. The black arrow
4 and the vertical line indicate where the RF signal in (b) locates. The white
5 arrows indicate there is a spatial averaging of the power spectra along the
6 lateral direction for calculating the ultrasonic properties. The white rectangle
7 indicates the region of interest where the ultrasonic properties are calculated.
8 The white bar in the lower right indicates a scale of 1 mm. **E** – skin entry
9 and epidermis, **D** – dermis, **F** – subcutaneous fat. (b) One typical RF signal
10 from the site where the black arrow and the vertical line indicate in (a). The
11 dotted windows show where the power spectrum for each small region of
12 interest is obtained. (c) The power spectra from the 6 small regions of
13 interest which have been corrected for the system-dependent effects. At each
14 frequency point as indicated by the dotted line, a regression of the power
15 spectra with the axial distance is performed and then the attenuation
16 coefficients are obtained. (d) The frequency-dependent attenuation
17 coefficients of the dermis. The typical attenuation coefficient at 20 MHz is
18 calculated where the dotted line in (c) indicates.

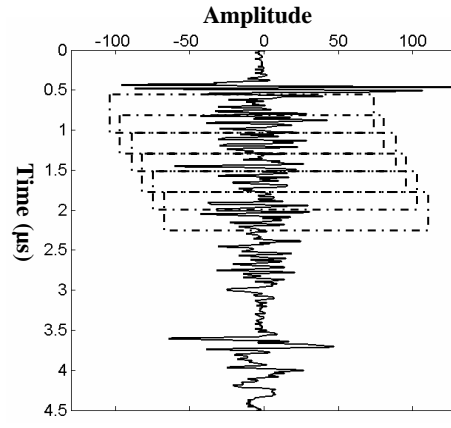
19 Fig. 2. Typical RF images of the skin observed in (a) forearm and (b) neck regions
20 of a normal subject. The white bar in the lower right indicates a scale of 1
21 mm.

22 Fig. 3. Ultrasonic properties of the skin in the forearm and the neck regions of the
23 normal subjects: (a) the attenuation slope β ; (b) the integrated attenuation IA;
24 (c) the integrated backscatter IBS.

1

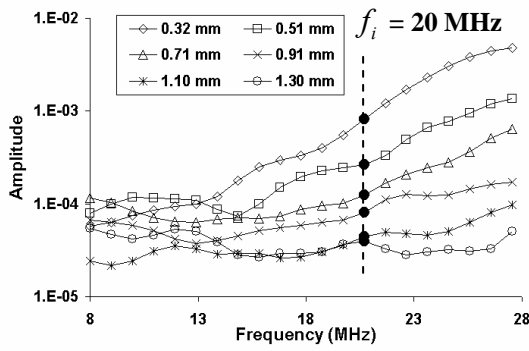


(a)

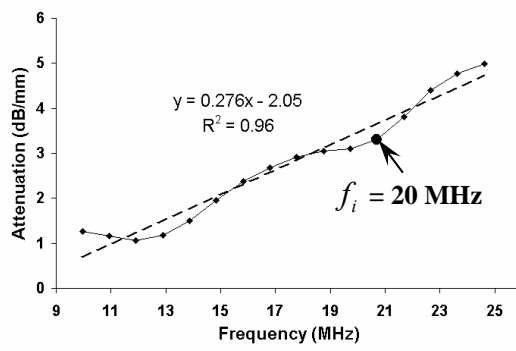


(b)

2



(c)



(d)

3

4 Fig. 1.

1

2

3

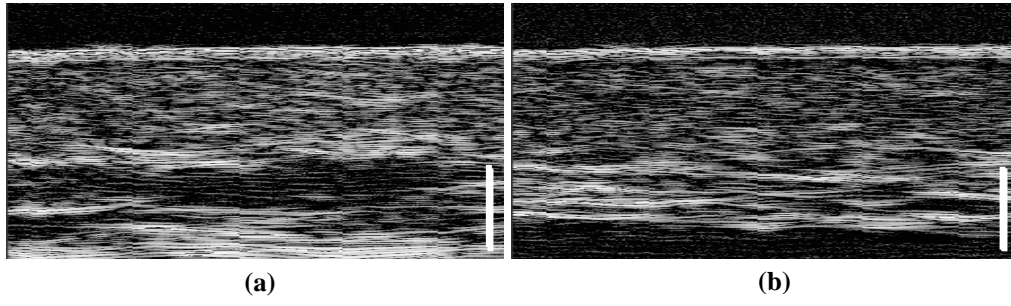
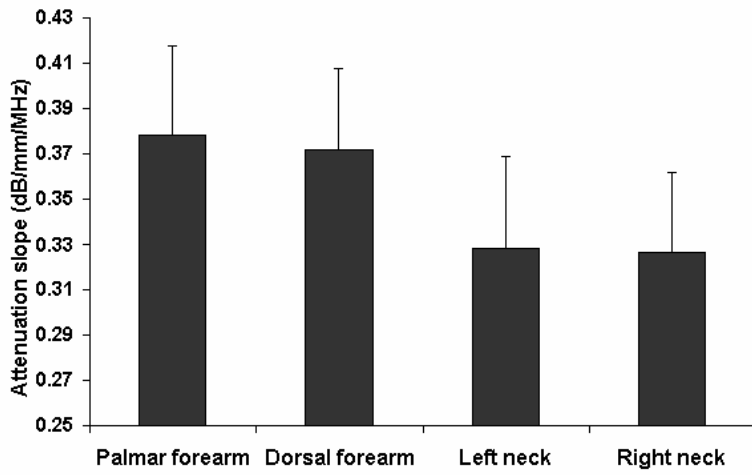
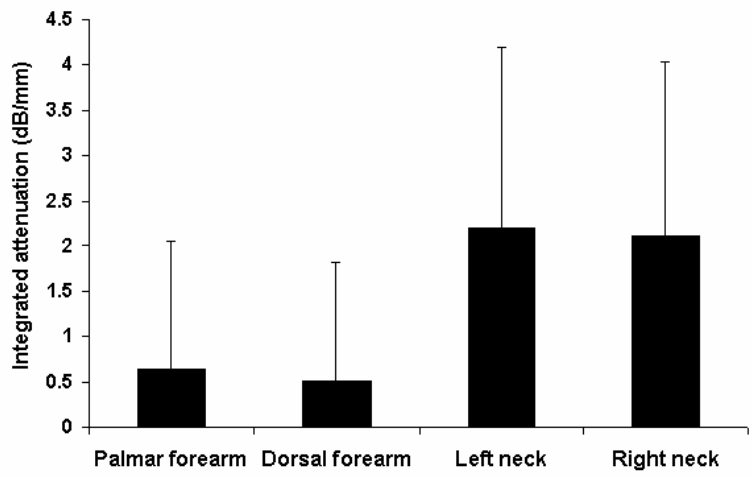


Fig. 2.



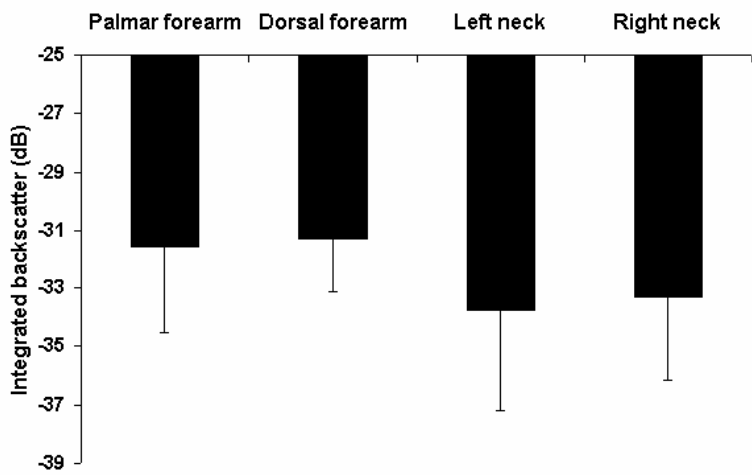
1

2 Fig. 3. (a)



3

4 Fig. 3. (b)



5

6 Fig. 3. (c)

1 TABLE 1. Intra- and inter-rater reliability of the ultrasonic (US) measurement

| <i>US parameters</i> | <i>Intra-rater measurement</i> | | <i>Inter-rater measurement</i> | |
|----------------------|--------------------------------|---------------|--------------------------------|---------------|
| | <i>ICC(1,3)</i> | <i>95% CI</i> | <i>ICC(3,3)</i> | <i>95% CI</i> |
| β (dB/mm/MHz) | 0.87 | 0.75 - 0.93 | 0.83 | 0.67 - 0.91 |
| IA (dB/mm) | 0.86 | 0.73 - 0.92 | 0.91 | 0.83 - 0.95 |
| IBS (dB) | 0.88 | 0.77 - 0.93 | 0.97 | 0.94 - 0.98 |

2 **CI: confidence interval.**

1 TABLE 2. (a) Bland-Altman test of the intra-rater measurement

2

| <i>US parameters</i> | \bar{d} | $SD_{\bar{d}}$ | 95% limits of agreement | $SE_{\bar{d}}$ | 95% CI of \bar{d} | Reliability coefficient |
|----------------------|-----------|----------------|--------------------------------|----------------|---------------------------------------|--------------------------------|
| β (dB/mm/MHz) | -0.001 | 0.031 | -0.063 \rightarrow 0.060 | 0.005 | -0.011 \rightarrow 0.009 | 0.063 |
| IA (dB/mm) | 0.09 | 0.95 | -1.77 \rightarrow 1.95 | 0.15 | -0.21 \rightarrow 0.39 | 1.91 |
| IBS (dB) | -0.15 | 1.64 | -3.37 \rightarrow 3.07 | 0.26 | -0.68 \rightarrow 0.38 | 3.30 |

3

4 (b) Bland-Altman test of the inter-rater measurement

5

| <i>US parameters</i> | \bar{d} | $SD_{\bar{d}}$ | 95% limits of agreement | $SE_{\bar{d}}$ | 95% CI of \bar{d} | Reliability Coefficient |
|----------------------|-----------|----------------|--------------------------------|----------------|---------------------------------------|--------------------------------|
| β (dB/mm/MHz) | 0.004 | 0.035 | -0.065 \rightarrow 0.073 | 0.006 | -0.007 \rightarrow 0.015 | 0.071 |
| IA (dB/mm) | -0.11 | 0.91 | -1.89 \rightarrow 1.68 | 0.14 | -0.40 \rightarrow 0.18 | 1.84 |
| IBS (dB) | 0.15 | 1.02 | -1.84 \rightarrow 2.15 | 0.16 | -0.17 \rightarrow 0.48 | 2.06 |

6

Totally $n = 40$ measurements were used for computation of each test. \bar{d} is the mean difference of the second measurement to the first measurement for the intra-rater operation, or the measurement of the second rater to that of the first rater for the inter-rater operation; $SD_{\bar{d}}$ is the SD of the mean difference calculated from the original data; $SE_{\bar{d}}$ is the standard error of the difference, calculated as $SE_{\bar{d}} = SD_{\bar{d}} / \sqrt{n}$; 95% CI of \bar{d} is the 95% CI for the mean difference, being defined as $\bar{d} \pm t_{n-1} \cdot SE_{\bar{d}}$, where t is the critical value of t -distribution at $p = 0.05$.

10

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Reliability coefficient is calculated to be $2\sqrt{\sum_{i=1}^n d_i^2 / n}$, where d_i is the individual difference for test i among a total of n measurements.

13