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# A revised parameterization for gaseous dry deposition in air-quality models

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## Abstract

A parameterization scheme for calculating gaseous dry deposition velocities in air-quality models is revised based on recent study results on non-stomatal uptake of O<sub>3</sub> and SO<sub>2</sub> over 5 different vegetation types. Non-stomatal resistance, which includes in-canopy aerodynamic resistance, soil resistance and cuticle resistance, for SO<sub>2</sub> and O<sub>3</sub> is parameterized as a function of friction velocity, relative humidity, leaf area index, and canopy wetness. Non-stomatal resistance for all other species is scaled to those of SO<sub>2</sub> and O<sub>3</sub> based on their chemical and physical characteristics. Stomatal resistance is calculated using a leaf-stomatal-resistance model for all gaseous species of interest. The improvements in the present model compared to its earlier version include a newly developed non-stomatal resistance formulation, a realistic treatment of cuticle and ground resistance in winter and the handling of seasonally-dependent input parameters. Model evaluation shows that the revised parameterization can provide more realistic deposition velocities for both O<sub>3</sub> and SO<sub>2</sub>, especially for wet canopies. Example model output shows that the parameterization provides reasonable estimates of dry deposition velocities for different gaseous species, land types and diurnal and seasonal variations. Maximum deposition velocities from model output are close to reported measurement values for different land types. The current parameterization can be easily adopted into different air-quality models that require inclusion of dry deposition processes.

## 1. Introduction

Dry deposition is an important process that requires treatment in regional air-quality models. Wesely (1989) developed a parameterization scheme for estimating gaseous dry deposition velocities, which has been widely used in a number of models (RADM, Chang et al., 1987; STEM, Carmichael et al., 1991; URM, Harley et al., 1993; CMAQ, Byun and Ching, 1999). Similar dry deposition models have been developed for air-

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quality models by Padro et al. (1991), Scire (1991), Pleim and Xiu (1995) and Zhang et al. (2002a). Dry deposition models have also been used in estimating total acid deposition. For this purpose, some single layer (usually called big-leaf) and multi-layer dry deposition models have also been developed (Erisman et al., 1994; Meyers et al., 1998; Brook et al., 1999a; Smith et al., 2000). A review of available dry deposition models was recently reported by Wesely and Hicks (2000).

Most existing dry deposition models utilize the multiple resistance analogy approach when parameterizing the deposition velocity to vegetation and other surfaces. In this approach, the canopy resistance is usually separated into stomatal and non-stomatal portions. While the overall deposition flux is the major concern of most air-quality models, it can be important to separate the stomatal uptake of pollutants from the overall deposition for some applications (e.g. O<sub>3</sub> dose to agricultural crops). Separating stomatal and non-stomatal uptake also allows us to model the diurnal variations of dry deposition more accurately, especially since stomatal uptake only occurs during the daytime for most canopy species, during which time it dominates over non-stomatal uptake. There are many different approaches for stomatal resistance calculations ranging from simple parameterizations as functions of solar radiation and/or time of day (Wesely, 1989; Padro et al., 1991), one- or two-big-leaf approaches (Jarvis, 1976; Hicks et al., 1987; Zhang et al., 2002a), to a multi-layer leaf-resistance model (Baldocchi et al., 1987). For non-stomatal resistance, a constant is usually chosen for a particular season or land type, thereby excluding the effects of meteorology. However, many recent measurements have shown that non-stomatal resistance is also affected by meteorological conditions, e.g. friction velocity ( $u_*$ ), relative humidity (RH) and canopy wetness, in addition to biological factors, e.g. canopy type, leaf area index (LAI) and growing period. For example, measurements over several different canopies (forests, maize) in France (Lamaud et al., 2002; Laville et al., 2002; Lopez et al., 2002) all show that the non-stomatal uptake of O<sub>3</sub> (e.g. the nighttime deposition) is controlled by the friction velocity. Zhang et al. (2002b) analyzed O<sub>3</sub> deposition flux data from measurements taken over five different canopies (mixed forest, deciduous forest, corn, soybean and pasture)

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in the eastern USA (Finkelstein et al., 2000; Meyers et al., 1998) and found that the non-stomatal resistance is affected by  $u^*$ , RH, LAI, canopy wetness and possibly other factors that were not measured. Based on the data from these five sites, Zhang et al. (2002b) proposed a set of parameterizations for the non-stomatal resistance of  $O_3$ . Zhang et al. (2003) further evaluated this set of parameterization, with adjustments to some parameters, using  $SO_2$  flux data measured at the same five canopies and obtained very good agreement between model results and measurements.

Zhang et al. (2002a) developed a parameterization scheme (a big-leaf model), similar to the approach used in Wesely (1989), for calculating dry deposition velocities for 30 gaseous species that are usually considered in air-quality models. Only seasonally adjusted values are used for non-stomatal resistance and meteorological effects are not considered. The purpose of the present study is to revise the parameterization scheme developed by Zhang et al. (2002a) by adopting the newly developed non-stomatal resistance parameterization presented in Zhang et al. (2002b, 2003). Other improvements include more realistic treatment of cuticle and ground resistance in winter and the handling of seasonally-dependent input parameters. The land use categories (LUC) used in Zhang et al. (2002a) are based, with some modifications, on BATS (Biosphere Atmosphere Transfer Scheme, Dickinson, 1986), a widely-used scheme in North America. In the present study, the surface scheme of GEM (Global Environmental Multi-scale model, Coté et al., 1997), Canada's operational weather forecast model, is used. This is because GEM is, or will be, used as the meteorological driver for many Canadian air-quality models, e.g. AURAMS (Moran et al., 1998) and CHRONOS (Pudykiewicz et al., 1997). Furthermore, this LUC scheme is based on BATS with an extra 6 LUCs. Choosing this 26-category scheme will also benefit air-quality models developed elsewhere.

The next section describes in detail the model equations. Two important input parameters (LAI and roughness length  $z_0$ ) are given in Sect. 3. Comparison of model results with single site measurements of  $O_3$  and  $SO_2$  dry deposition velocity and example model output are given in Sect. 4.

## 2. Model description

The scheme for the revised model is shown in Fig. 1. The primary resistances to pollutant uptake are the aerodynamic resistance ( $R_a$ ), the quasi-laminar sublayer resistance ( $R_b$ ) above the canopy, and the overall canopy resistance ( $R_c$ ).  $R_c$  can be separated into two parallel paths; one is stomatal resistance ( $R_{st}$ ) with its associated mesophyll resistance ( $R_m$ ), and the other is non-stomatal resistance ( $R_{ns}$ ).  $R_{ns}$  can be further decomposed into resistance to soil uptake, which includes in-canopy aerodynamic resistance ( $R_{ac}$ ) and the subsequent soil resistance ( $R_g$ ), as well as resistance to cuticle uptake ( $R_{cut}$ ). Note that  $R_{cut}$  here is slightly different from that defined in traditional big-leaf models in that it also considers the aerodynamic and quasi-laminar resistances to individual leaves. This is done by parameterizing  $R_{cut}$  as a function of friction velocity, similar to the concept of overall cuticle uptake considered in a multi-layer model framework (e.g. Baldocchi, 1988).

Based on the above discussion, the dry deposition velocity,  $V_d$ , is defined as:

$$V_d = \frac{1}{R_a + R_b + R_c}, \quad (1)$$

where expressions for  $R_a$  and  $R_b$  can be computed as in many earlier dry deposition studies (e.g. Padro, 1996). The uncertainties in  $R_a$  and  $R_b$  from the different models are small. In the present study, only  $R_c$  is discussed.  $R_c$  is parameterized as:

$$\frac{1}{R_c} = \frac{1 - W_{st}}{R_{st} + R_m} + \frac{1}{R_{ns}} \quad (2)$$

$$\frac{1}{R_{ns}} = \frac{1}{R_{ac} + R_g} + \frac{1}{R_{cut}}, \quad (3)$$

where  $W_{st}$  is the fraction of stomatal blocking under wet conditions.  $R_{st}$  is calculated using a sunlit/shade (two-big-leaf) stomatal resistance approach.  $R_m$  is treated as dependent only on the chemical species and the values for some common species

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considered in air-quality models can be found in Zhang et al. (2002a). Note that Eqs. (2) and (3) are for surfaces with canopies. For surfaces without canopies (e.g. water, ice, desert),  $R_{st}$ ,  $R_m$ ,  $R_{ac}$  and  $R_{cut}$  are not applicable. For the convenience of using the same equations for all LUCs, we define  $R_g$  as resistances to any surfaces (soil, ice, snow, water), (more discussion below). Thus, for surfaces without canopy, a value of 0 is given to  $R_{ac}$  and a very large value (i.e.  $10^{25} \text{ s m}^{-1}$ ) should be used for  $R_{st}$ ,  $R_m$  and  $R_{cut}$ .

$R_{ac}$  is not species-dependent while  $R_g$  and  $R_{cut}$  are.  $R_g$  and  $R_{cut}$  are calculated for  $\text{SO}_2$  and  $\text{O}_3$  and then scaled for other gaseous species based on the equation:

$$\frac{1}{R_x(i)} = \frac{\alpha(i)}{R_x(\text{SO}_2)} + \frac{\beta(i)}{R_x(\text{O}_3)}, \quad (4)$$

where  $R_x$  represents non-stomatal resistance components (i.e.  $R_{cut}$  and  $R_g$ ) and  $i$  represents the particular gaseous species. Parameters  $\alpha$  and  $\beta$  are two scaling factors and are functions of the chemical species. Scaling parameters for a total of 30 species has been presented in Table 1 of Zhang et al. (2002a). The details of each term in Eqs. (2)–(4) are discussed below.

$W_{st}$ : Zhang et al. (2002b), using  $\text{O}_3$  flux data from five sites in eastern North America, found that  $W_{st}$  is not important under most wet conditions because of weak solar radiation (SR), which leads to large  $R_{st}$ . However, there are some exceptions such as morning dew and sunshine immediately after rain when the stomata can be blocked but solar radiation is strong. Under these conditions,  $W_{st}$  should be considered. Thus, the following equation is suggested for wet canopies (for dry canopies,  $W_{st}$  always equals to 0):

$$W_{st} = \begin{cases} 0, & SR \leq 200 \text{ W m}^{-2} \\ (SR - 200)/800, & 200 < SR \leq 600 \text{ W m}^{-2} \\ 0.5, & SR > 600 \text{ W m}^{-2} \end{cases} \quad (5)$$

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$W_{st}$  is given a value other than 0 only when solar radiation is relatively strong ( $>200 \text{ W m}^{-2}$ ) and the canopy is wet. If rain or dew occurs, the canopy is treated as wet. Occurrence of dew can be defined based on particular meteorological conditions, e.g. RH,  $u^*$  and cloud cover (Janssen and Romer, 1991) as adopted in Brook et al. (1999a).

$R_{st}$ : A sunlit/shade (two-big-leaf) stomatal resistance sub-model described in Zhang et al. (2002a) is used for calculating  $R_{st}$  for all gaseous species.  $R_{st}$  is calculated as:

$$R_{st} = 1 / [G_s(PAR)f(T)f(D)f(\Psi)(D_i/D_v)], \quad (6)$$

where  $G_s(PAR)$  is the unstressed leaf stomatal conductance, a function of photosynthetically active radiation ( $PAR$ ). Calculation of  $G_s(PAR)$  is described in Zhang et al. (2002a) and is not repeated here. The dimensionless functions  $f(T)$ ,  $f(D)$  and  $f(\Psi)$  represent the conductance-reducing effects of air temperature  $T$ , water-vapour-pressure deficit  $D$ , and water stress (leaf water potential)  $\Psi$ , respectively, on leaf stomatal conductance (Brook et al., 1999a). The equations for these functions are:

$$f(T) = \frac{T - T_{\min}}{T_{\text{opt}} - T_{\min}} \left[ \frac{T_{\max} - T}{T_{\max} - T_{\text{opt}}} \right]^{b_t} \quad (6a)$$

with

$$b_t = \frac{T_{\max} - T_{\text{opt}}}{T_{\max} - T_{\min}} \quad (6b)$$

$$f(D) = 1 - b_{\text{vpd}}D \quad (6c)$$

with

$$D = e^*(T) - e \quad (6d)$$

and

$$f(\Psi) = (\Psi - \Psi_{c2}) / (\Psi_{c1} - \Psi_{c2}) \quad (6e)$$



with

$$\Psi = -0.72 - 0.0013SR. \quad (6f)$$

$T_{\min}$  and  $T_{\max}$  are minimum and maximum temperatures ( $^{\circ}\text{C}$ ) that indicate the temperatures below and above which complete stomatal closure occurs.  $T_{\text{opt}}$  is an optimum temperature that indicates the temperature of maximum stomatal opening.  $b_{\text{vpd}}$  is a water-vapour-pressure-deficit constant ( $\text{kPa}^{-1}$ ),  $D$  is the vapour pressure deficit ( $\text{kPa}$ ),  $e^*(T)$  is the saturation water vapour pressure ( $\text{kPa}$ ) at air temperature  $T$  ( $^{\circ}\text{C}$ ), and  $e$  is the ambient water vapour pressure ( $\text{kPa}$ ).  $\Psi_{\text{c1}}$  and  $\Psi_{\text{c2}}$  ( $\text{MPa}$ ) are parameters that specify leaf-water-potential dependency. When  $\Psi > \Psi_{\text{c1}}$  (i.e. no leaf water potential stress),  $f(\Psi) = 1.0$ . Values for all parameters required for calculating  $R_{st}$  are taken from Brook et al. (1999a), Dorman and Sellers (1989), Dickinson et al. (1986), and NOAA (1992) library data, and are listed in Table 1. These parameters are  $r_{\text{smin}}$  (minimum stomatal resistance),  $b_{rs}$  (empirical constant in stomatal resistance),  $T_{\min}$ ,  $T_{\max}$ ,  $T_{\text{opt}}$ ,  $b_{\text{vpd}}$ ,  $\Psi_{\text{c1}}$  and  $\Psi_{\text{c2}}$ .

During nighttime when there is no solar radiation, the leaf stomata are assumed to be completely closed.  $R_{st}$  estimated from Eq. (2) then has an infinite value. Recent research suggests that the stomata of some canopy species may still be partially open even at night (Gunthardt-Goerg et al., 1997; Musselman and Minnick, 2000; Wiser and Havranek, 1993, 1995). However, this behaviour is difficult to quantify given present knowledge. In this study we treat the stomata as fully closed at night.

$R_{ac}$ : In-canopy aerodynamic resistance should be the same for all gaseous species. The equation developed in Zhang et al. (2002b) is used:

$$R_{ac} = \frac{R_{ac0} LAI^{1/4}}{u_*^2}, \quad (7)$$

where  $LAI$  is the leaf area index,  $u_*$  is the friction velocity, and  $R_{ac0}$  is the reference value for in-canopy aerodynamic resistance.  $R_{ac0}$  is expected to vary with different canopies and suggested values are given in Table 1 for all LUC. For some LUC, a range

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of  $R_{ac0}$  values are given to reflect the change of canopy structure at different times in the growing season. The minimum values,  $R_{ac0}(\min)$ , correspond to leafless periods for deciduous forests and earlier growing periods for agricultural lands. The maximum values,  $R_{ac0}(\max)$ , correspond to the full-leaf period for forests and the maturity period for agricultural lands. Here a simple equation is suggested for extracting  $R_{ac0}$  values for any day of the year based on minimum and maximum  $LAI$  values since this information is available in most air-quality models:

$$R_{ac0}(t) = R_{ac0}(\min) = \frac{LAI(t) - LAI(\min)}{LAI(\max) - LAI(\min)} [R_{ac0}(\max) - R_{ac0}(\min)], \quad (7a)$$

where  $R_{ac0}(t)$  corresponds to the  $R_{ac0}$  value at any day of the year.  $LAI(\min)$  and  $LAI(\max)$  represents minimum and maximum  $LAI$  values, respectively, during the year.

$R_g$ : Surface resistance is considered separately for different surface types (water, ice, snow, soil). The following equation is used according to Erisman et al. (1994):

$$R_g = \begin{cases} R_{\text{water}} \\ R_{\text{ice}} \\ R_{\text{snow}} \\ R_{\text{soil}} \end{cases}, \quad (8)$$

where  $R_{\text{water}}$ ,  $R_{\text{ice}}$ ,  $R_{\text{snow}}$  and  $R_{\text{soil}}$  represent resistance to water, ice, snow, and soil surfaces, respectively.  $R_{\text{snow}}$  and  $R_{\text{ice}}$  are assumed to have the same values. For  $O_3$ ,  $R_{\text{water}}$ ,  $R_{\text{snow}}$  and  $R_{\text{ice}}$  are given a value of  $2000 \text{ s m}^{-1}$ . For  $SO_2$ ,  $R_{\text{water}}$  is given a value of  $20 \text{ s m}^{-1}$ , while  $R_{\text{snow}}$  and  $R_{\text{ice}}$  are taken as a function of temperature with a lower limit of  $100 \text{ s m}^{-1}$  and an upper limit of  $500 \text{ s m}^{-1}$  (Erisman et al., 1994) as follows:

$$R_{\text{snow}}, R_{\text{ice}}(SO_2) = 70(2 - T). \quad (8a)$$

Information on  $R_{\text{soil}}$  is limited for both  $O_3$  and  $SO_2$ , as discussed in Zhang et al. (2002b). Based on previous studies, a value of  $200 \text{ s m}^{-1}$  is given for  $O_3$  for all vegetated surfaces (LUC 4-19, 25 and 26) and  $500 \text{ s m}^{-1}$  for non-vegetated surfaces or

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surfaces with wet ground (LUC 20-24).  $R_{\text{soil}}$  is more complicated for  $\text{SO}_2$  due to its sensitivity to wetness. Thus, soil resistance to  $\text{SO}_2$  may be smaller when dew or rain occurs. The following approach is suggested for  $R_{\text{soil}}$  for  $\text{SO}_2$ :

$$R_{\text{soil}} = \begin{cases} R_{\text{gd}} \\ R_{\text{grain}} \\ R_{\text{gdew}} \end{cases}, \quad (8b)$$

5 where  $R_{\text{gd}}$  represents the soil resistance over land surfaces with no dew or rain has occurred,  $R_{\text{grain}}$  and  $R_{\text{gdew}}$  are the resistances to soil when rain or dew occur. Values of 50 and  $100 \text{ s m}^{-1}$  are assigned to  $R_{\text{grain}}$  and  $R_{\text{gdew}}$ , respectively. Suggested  $R_{\text{gd}}$  values for all LUCs are presented in Table 1. For canopies with relatively high soil moisture content (e.g. tropical forest),  $R_{\text{gd}}$  is given a smaller value compared to vegetation types  
10 with dry soils (e.g. desert).

A more rigorous approach for  $R_{\text{soil}}$  is to separate soil into dry and wet portions (Zhang et al., 2002a). However, the information on the wet fraction of soil is usually not available. Although a sophisticated method for extracting this fraction is available (Sellers et al., 1996), this method requires more detailed information than is typically available  
15 in air-quality models.

$R_{\text{cut}}$ : Canopy cuticle resistance is calculated for dry and wet conditions separately according to Zhang et al. (2002b):

$$R_{\text{cutd}} = \frac{R_{\text{cutd0}}}{e^{3\text{RH}LAI^{1/4}u_*}} \quad (9a)$$

$$R_{\text{cutw}} = \frac{R_{\text{cutw0}}}{LAI^{1/2}u_*}, \quad (9b)$$

20 where RH is relative humidity (as a fraction).  $R_{\text{cutd0}}$  and  $R_{\text{cutw0}}$  are reference values for dry and wet cuticle resistance, respectively. When rain or dew occurs, the canopy is treated as wet. Values of  $R_{\text{cutd0}}$  and  $R_{\text{cutw0}}$  for  $\text{O}_3$  and values of  $R_{\text{cutd0}}$  for  $\text{SO}_2$  for

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each LUC are presented in Table 1.  $R_{\text{cutw}0}$  for  $\text{SO}_2$  is treated differently under dew and rain conditions. For all vegetated surfaces values of  $50 \text{ s m}^{-1}$  and  $100 \text{ s m}^{-1}$  are given for  $R_{\text{cutw}0}$  for rain and dew conditions, respectively. Equations (9a) and (9b) were developed based on the 5-site flux data set for which  $u^*$  values seldom exceeded  $1.5 \text{ m s}^{-1}$  for the two forest locations and  $0.8 \text{ m s}^{-1}$  for the other three sites (crops). It is expected that these equations give reasonable values for most conditions, but they may give unrealistically small values for  $\text{SO}_2$  when  $u^*$  is extremely large (e.g.  $u^* > 2 \text{ m s}^{-1}$ ). Thus, a lower limit of  $100 \text{ s m}^{-1}$  is suggested for dry canopies and  $20 \text{ s m}^{-1}$  for wet canopies for  $\text{SO}_2$ .

In winter when temperatures are below  $-1^\circ \text{C}$ ,  $R_{\text{gd}}$  and  $R_{\text{cutd}}$  are increased by as much as double their original value according to the equation:

$$R_{\text{gd}}(T < -1^\circ \text{C}) = R_{\text{gd}} e^{0.2(-1-T)} \quad (10a)$$

$$R_{\text{cutd}}(T < -1^\circ \text{C}) = R_{\text{cutd}} e^{0.2(-1-T)}. \quad (10b)$$

For snow on the ground and leaves, both  $R_g$  and  $R_{\text{cut}}$  are adjusted by including a snow cover fraction ( $f_{\text{snow}}$ ):

$$\frac{1}{R_g} = \frac{1 - 2f_{\text{snow}}}{R_g} + \frac{2f_{\text{snow}}}{R_{\text{snow}}} \quad (10c)$$

$$\frac{1}{R_{\text{cut}}} = \frac{1 - f_{\text{snow}}}{R_{\text{cut}}} + \frac{f_{\text{snow}}}{R_{\text{snow}}}. \quad (10d)$$

Since snow on ground persists longer than on leaves for high canopies, the snow fraction for the ground ( $R_g$ ) is taken as 2 times that of leaves ( $R_{\text{cut}}$ ). Note that both  $f_{\text{snow}}$  and  $2f_{\text{snow}}$  have a range of values between 0.0-1.0. Since the snow fraction is usually not available from meteorological models, a simple equation is suggested to estimate

$f_{\text{snow}}$  from snow depth (SD in cm):

$$f_{\text{snow}} = \frac{sd}{sd_{\text{max}}}, \quad (10e)$$

where  $sd_{\text{max}}$  is a parameter at or above which value the snow fraction for canopy leaves is assumed to be 1. Suggested  $sd_{\text{max}}$  values are also listed in Table 1 (Note that the actual  $sd_{\text{max}}$  for underlying soil surfaces is only half of the values presented in Table 1 as can be seen from the comparison of Eqs. 10c and 10d).

### 3. Other parameters

$LAI$  is an extremely important parameter for calculating canopy resistances.  $LAI$  values used in GEM are adopted here. Monthly  $LAI$  values at the beginning of each month are presented in Fig. 2.  $LAI$  values on any day are interpolated using the day number of the month. Note that several LUC that have constant  $LAI$  values are not shown in Fig. 2. They are set to 5.0 (LUC 4), 6.0 (LUC 5, 8), 4.0 (LUC 9, 23), 3.0 (LUC 10, 12) and 0.0 (LUC 1-3, 22, 24).  $LAI$  values for LUC 21 (urban) are set to a constant value of 1 in GEM. Since  $LAI$  values for urban locations in different regions can have quite different seasonal variations, here we choose to give  $LAI$  a value of 0.1 in the winter season, gradually increasing to 1 in the late spring. We keep it as 1 until early fall, and then reduce it gradually to 0.1 again at the end of fall (figure not shown).

Roughness length ( $z_0$ ) is needed for calculating friction velocity, which subsequently affects aerodynamic resistance and non-stomatal resistance.  $z_0$  from GEM cannot be used directly since it is treated together with topography. Suggested  $z_0$  values for each LUC are presented in Table 1. For water surfaces (LUC 1 and 3),  $z_0$  is calculated as a function of wind speed. For some surfaces a constant  $z_0$  value is suggested, while for others a range of  $z_0$  values is given. For those surfaces that have variable  $z_0$  values, an equation similar to Eq. (7a) is used to obtain  $z_0$  for any time period based on  $LAI$

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values:

$$z_o(t) = z_o(\min) + \frac{LAI(t) - LAI(\min)}{LAI(\max) - LAI(\min)} [z_o(\max) - z_o(\min)]. \quad (11)$$

Note that for higher canopies and canopies with large  $LAI$ ,  $z_o$  is given a larger value.

#### 4. Model evaluation and example output

5 The non-stomatal resistance parameterization has been evaluated in Zhang et al. (2002b, 2003) using  $O_3$  and  $SO_2$  flux data from 5 sites. Here measurements of  $O_3$  and  $SO_2$  dry deposition data at one site (deciduous forest in Pennsylvania, USA) are used to show the performance of the revised model. This site is chosen because it has a large data set for  $O_3$  and  $SO_2$  under both dry and wet canopy conditions (Finkelstein et al., 2000). The other 4 sites have very few  $SO_2$  measurements over wet canopies. Figure 3 shows the observed mean diurnal cycle of half-hourly  $V_d$  along with the modelled estimates. The suitability of the current model can be seen from the very good agreement of  $O_3$  deposition over wet canopies (Fig. 3b) and  $SO_2$  deposition over both dry and wet canopies (Figs. 3c and 3d). As discussed in Zhang et al. (2002b), earlier models could not predict the diurnal cycle of  $O_3$  and  $SO_2$   $V_d$  over wet canopies since meteorological conditions are not explicitly considered. Although the non-stomatal resistance parameterization was developed based on  $O_3$  flux data, it also gives very good results for  $SO_2$  over dry and wet canopies with adjustments of species-dependent parameters (Table 1), and the results for  $SO_2$  from the current model compare better to the data than do earlier models (Finkelstein et al., 2000; Zhang et al., 2002a). It is noted that there is an underestimation of  $O_3$   $V_d$  during mid-morning hours when maximum  $V_d$  appeared. This problem also exists in other models since most models predict maximum  $V_d$  around noon. Since the daytime  $O_3$   $V_d$  is mainly controlled by stomatal uptake, adopting the new non-stomatal resistance parameterization will not solve the problem shown in Fig. 3a. It is worth pointing out that the phenomenon of mid-morning

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maximum  $V_d$  has only been observed over several forest canopies and not over crops (Finkelstein et al., 2000). More research is needed on this phenomenon before model improvements can be made.

Based upon the model structure described above we expect model results to be sensitive to several of the input parameters, namely  $LAI$ ,  $z_0$ ,  $u^*$ , SR, T and RH. These parameters can vary widely due to meteorological variations (i.e., hourly to daily) and seasonal variation, as well as geographic variations. Due to this large variation, it is difficult to provide typical  $V_d$  values from the model. We therefore ran the model for a wide but realistic range of input values for these parameters, and estimated the typical range of  $V_d$  values that can be expected. Here we present the results for each LUC under dry canopy conditions assuming a reference height for the  $V_d$  calculation of 20 m. The range of  $u^*$  values used depended upon LUC with the two roughest surfaces, evergreen broadleaf forests (LUC 5 and 8), being assumed values within the range of  $0.1\text{--}1.5\text{ m s}^{-1}$ ; forests and urban areas, a range of  $0.1\text{--}1.2\text{ m s}^{-1}$ ; and the remaining surfaces, a range of  $0.1\text{--}0.8\text{ m s}^{-1}$ . Surface temperature was allowed to vary between  $-10$  and  $30^\circ\text{C}$ , solar radiation from  $0$  to  $800\text{ W m}^{-2}$  and relative humidity from  $50\text{--}90\%$ . All possible contributions of  $u^*$ , T, SR and RH were input separately into the model (using small increments for all variables:  $0.1$  for  $u^*$ ,  $1^\circ\text{C}$  for T,  $50\text{ W m}^{-2}$  for SR and  $5\%$  for RH) to calculate the range of  $V_d$  values possible for each LUC. In addition, calculations were done for the first day of every month so that the seasonal variation in  $LAI$  was accounted for. Since, realistically, some of the test conditions would be highly unlikely (e.g. high temperatures and large solar radiation over tundra), the allowed ranges were adjusted so that  $50^\circ\text{C}$  is the minimum temperature for tropical forests and  $20^\circ\text{C}$  and  $500\text{ W m}^{-2}$  are the maximum values for tundra. Although information (i.e. scaling parameters) on a total of 30 species is available in Zhang et al. (2002a), we show results for only 9 species in Table 2. Overall, we expect that the maximum  $V_d$  values extracted from these model test runs will be representative of the real-world typical maximum  $V_d$  for most land types under dry conditions.

The model test results in Table 2 indicate that maximum  $V_d$  values occur when  $LAI$

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is large, the temperature is close to an optimum value (Topt in Table 1),  $u^*$  is large, RH is high and solar radiation is relatively strong (not necessarily maximum SR for some canopies due to the water stress, see Eq. 6). The maximum  $V_d$  values for forest canopies and agricultural lands range around 1.1–1.7 cm s<sup>-1</sup> for SO<sub>2</sub>, 1.0–1.4 cm s<sup>-1</sup> for O<sub>3</sub>, and 3.5–5.1 cm s<sup>-1</sup> for HNO<sub>3</sub>. NO<sub>2</sub>  $V_d$  follows the pattern of O<sub>3</sub>  $V_d$  but with slightly smaller values ( $\alpha = 0$ ,  $\beta = 0.8$ ). H<sub>2</sub>O<sub>2</sub>  $V_d$  is higher than both SO<sub>2</sub> and O<sub>3</sub> during both day and night ( $\alpha = 1$ ,  $\beta = 1$ ). HNO<sub>3</sub> has the highest  $V_d$  among all the chemical species considered here due to its high solubility and reactivity ( $\alpha = 10$ ,  $\beta = 10$ ). The  $V_d$  of PAN mimics the pattern of O<sub>3</sub> ( $\alpha = 0$ ,  $\beta = 0.6$ ) but is always smaller while the  $V_d$  of HCHO follows the pattern of SO<sub>2</sub> ( $\alpha = 0.8$ ,  $\beta = 0.2$ ). NH<sub>3</sub> is similar to SO<sub>2</sub> ( $\alpha = 1$ ,  $\beta = 0$ ), but slightly higher during the day due to its higher molecular diffusivity. The  $V_d$  of ROOH is similar to  $V_d$  of O<sub>3</sub> ( $\alpha = 0.1$ ,  $\beta = 0.8$ ). Zhang et al. (2002a) reviewed and discussed all published measurements for all species of interest. Most flux measurements of SO<sub>2</sub>, O<sub>3</sub>, NO<sub>2</sub>, NH<sub>3</sub> and HNO<sub>3</sub> support the results generated from the present model. The very limited set of measurements for PAN, HCHO, H<sub>2</sub>O<sub>2</sub> and ROOH also agree well with model results. There are no data for many of the species presented in Zhang et al. (2002a) and thus the present model provides a tool to estimate their deposition rates.

To attempt to provide an indication of the typical  $V_d$  values (instead of maximum range as shown in Table 2) and to demonstrate the effect of day vs. night, wet vs. dry and snow, we ran the model again and used typical values for the input parameters. Figure 4 shows the  $u^*$  values used for different LUCs for several typical conditions. Note that  $u^*$  for dry and wet summer days was given the same set of values. Typically LUC 5 (evergreen broadleaf trees) and 8 (tropical broadleaf trees) can expect to have the largest  $u^*$  values reflecting their large roughness; conversely, smooth surfaces (ice, water, tundra) have the smallest  $u^*$  values. The other dominant meteorological variables used for the tests are: 20° C (T), 75% (RH) and 600 Wm<sup>-2</sup> (SR) for dry summer day; 20° C (T) and 200 Wm<sup>-2</sup> (SR) for rain summer day; 10° C (T) and 75% (RH) for dry summer night; and -2° C (T) and 20 cm (SD) for snow condition (note that for ice



surfaces, the temperature is given a value of  $-2^{\circ}\text{C}$  for all the tests).

For  $\text{SO}_2$  and  $\text{O}_3$ ,  $V_d$  is found to typically be around  $0.6\text{--}1.0\text{ cm s}^{-1}$  for a summer day for most vegetated surfaces with dry canopy conditions. As expected,  $V_d$  is larger over canopies with larger  $LAI$  and smaller  $r_{\text{smmin}}$ . Stomatal resistance is the dominant term during dry daytime conditions. When canopies are wet due to rain,  $\text{SO}_2$   $V_d$  increases substantially for vegetated surfaces while  $\text{O}_3$   $V_d$  increases only slightly. During nighttime over dry canopies,  $\text{SO}_2$   $V_d$  is around  $0.2\text{--}0.4\text{ cm s}^{-1}$ , and  $\text{O}_3$   $V_d$  is  $0.1\text{--}0.3\text{ cm s}^{-1}$ .  $V_d$  of  $\text{SO}_2$  is larger than that of  $\text{O}_3$  due to the smaller cuticle and soil resistances assigned to  $\text{SO}_2$ . Note that during nighttime over wet canopies caused by rain (figure not presented),  $V_d$  of  $\text{O}_3$  is slightly larger compared to dry nighttime conditions, while  $V_d$  of  $\text{SO}_2$  can be substantially larger. When canopies are wetted by dew, both  $\text{SO}_2$  and  $\text{O}_3$  have slightly larger  $V_d$  values compared to dry nighttime conditions. In winter when there is snow,  $\text{SO}_2$   $V_d$  is around  $0.4\text{ cm s}^{-1}$ . However, it can be close to  $1\text{ cm s}^{-1}$  over snow surfaces if the temperature is higher than  $1^{\circ}\text{C}$  (see Eq. 8a).  $\text{O}_3$   $V_d$  is less than  $0.1\text{ cm s}^{-1}$  if the surfaces are fully covered by snow, but can be higher than  $0.2$  if the surfaces are partially covered by snow (e.g. forest canopies).

It is well known that surface resistance for  $\text{HNO}_3$  is very small. Thus, aerodynamic resistance usually dominates the rate of  $\text{HNO}_3$  dry deposition. Figure 5 shows that for summer daytime dry canopy conditions,  $V_d$  of  $\text{HNO}_3$  is higher than  $1.5\text{ cm s}^{-1}$  for canopies with small roughness lengths and as high as  $3\text{ cm s}^{-1}$  for forest canopies with larger roughness lengths. Under wet conditions,  $V_d$  values are even larger. During nighttime,  $\text{HNO}_3$   $V_d$  is still close to  $1.0\text{ cm s}^{-1}$  for canopies with small  $z_0$  values and even higher for canopies with large  $z_0$ . As discussed earlier, and also shown in Fig. 5,  $V_d$  of  $\text{HCHO}$  follows the pattern of  $\text{SO}_2$  and  $V_d$  of  $\text{PAN}$  mimics the pattern of  $\text{O}_3$ . Overall, the typical  $V_d$  values shown in Fig. 5 are consistent with the published measurements reviewed by Sehmel (1984), Brook et al. (1999b), Wesely and Hicks (2000) and Zhang et al (2002a).

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## 5. Conclusions

A parameterization for estimating dry deposition velocities in air-quality models is revised by including a newly developed non-stomatal resistance formulation, a realistic treatment of cuticle and ground resistance in winter (low temperature, snow surfaces) and the handling of seasonally-dependent input parameters (i.e.  $LAI$ ,  $z_0$ , resistance components). Evaluation using measurement data demonstrates that this model predicts more accurate deposition velocities compared to other existing models, especially for wet canopies. Model produced maximum deposition velocities and values for typical meteorological conditions are realistic compared to published measurements.

There are few measurements of  $V_d$  for species other than  $SO_2$ ,  $O_3$ ,  $NO_2$ ,  $HNO_3$ ,  $NH_3$ . So, although the approach presented here and in Zhang et al. (2002a) are expected to be reasonably realistic, the estimated values are unvalidated due to the lack of data. Further developments will rely on the availability of more detailed measurements in the future. Furthermore, it is recommended that future field campaigns include direct flux measurements of different gases so the scaling method can be validated, and at several levels inside canopies, e.g. at the canopy floor so that soil resistance can be estimated. Separate measurements of stomatal and non-stomatal uptake is also important for evaluating the model and for estimating  $O_3$  damage to crops.

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**Table 1.** Land use categories and all related parameters (na = not applicable; f(u) means a function of wind speed)

LUC	R <sub>aod</sub>	R <sub>cond0</sub> O <sub>3</sub>	R <sub>condw</sub> O <sub>3</sub>	R <sub>cond0</sub> SO <sub>2</sub>	R <sub>gd</sub> SO <sub>2</sub>	f <sub>amin</sub> (s m <sup>-1</sup> )	b <sub>s</sub> (Wm <sup>-2</sup> )	T <sub>min</sub> (°C)	T <sub>max</sub> (°C)	T <sub>opt</sub> (°C)	b <sub>hyd</sub> (kPa <sup>-1</sup> )	ψ <sub>c1</sub> (MPa)	ψ <sub>c2</sub> (MPa)	z <sub>0</sub> (m)	Sdmax (cm)	
1	water	0	na	na	na	20	na	na	na	na	na	na	na	f(u)	na	
2	ice	0	na	na	na	Eq.8a	na	na	na	na	na	na	na	0.01	1	
3	inland lake	0	na	na	na	20	na	na	na	na	na	na	na	f(u)	na	
4	evergreen needleleaf trees	100	4000	200	2000	200	250	44	-5	40	15	0.31	-2	-2.5	0.9	200
5	evergreen broadleaf trees	250	6000	400	2500	100	150	40	0	45	30	0.27	-1	-5.0	2.0	400
6	deciduous needleleaf trees	60-100	4000	200	2000	200	250	44	-5	40	15	0.31	-2	-2.5	0.4-0.9	200
7	deciduous broadleaf trees	100-250	6000	400	2500	200	150	43	0	45	27	0.36	-1.9	-2.5	0.4-1.0	200
8	tropical broadleaf trees	300	6000	400	2500	100	150	40	0	45	30	0.27	-1	-5.0	2.5	400
9	drought deciduous trees	100	8000	400	6000	300	250	44	0	45	25	0.31	-1	-4.0	0.6	200
10	evergreen broadleaf shrubs	60	6000	400	2000	200	150	40	0	45	30	0.27	-2	-4.0	0.2	50
11	deciduous shrubs	20-60	5000	300	2000	200	150	44	-5	40	15	0.27	-2	-4.0	0.05-0.2	50
12	thorn shrubs	40	5000	300	2000	200	250	44	0	45	25	0.27	-2	-3.5	0.2	50
13	short grass and forbs	20	4000	200	1000	200	150	50	5	40	30	0	-1.5	-2.5	0.04	5
14	long grass	10-40	4000	200	1000	200	100	20	5	45	25	0	-1.5	-2.5	0.02-0.1	20
15	crops	10-40	4000	200	1500	200	120	40	5	45	27	0	-1.5	-2.5	0.02-0.1	10
16	rice	10-40	4000	200	1500	50	120	40	5	45	27	0	-1.5	-2.5	0.02-0.1	10
17	sugar	10-40	4000	200	2000	200	120	50	5	45	25	0	-1.5	-2.5	0.02-0.1	10
18	maize	10-50	5000	300	2000	200	250	65	5	45	25	0	-1.5	-2.5	0.02-0.1	10
19	cotton	10-40	5000	300	2000	200	125	65	10	45	30	0	-1.5	-2.5	0.02-0.2	10
20	irrigated crops	20	4000	200	2000	50	150	40	5	45	25	0	-1.5	-2.5	0.05	10
21	urban	40	6000	400	4000	300	200	42	0	45	22	0.31	-1.5	-3	1.0	50
22	tundra	0	8000	400	2000	300	150	25	-5	40	20	0.24	0	-1.5	0.03	2
23	swamp	20	5000	300	1500	50	150	40	0	45	20	0.27	-1.5	-2.5	0.1	10
24	Desert	0	na	na	na	700	na	na	na	na	na	na	na	na	0.04	2
25	mixed wood forests	100	4000	200	2500	200	150	44	-3	42	21	0.34	-2	-2.5	0.6-0.9	200
26	Transitional forest	100	4000	200	2500	200	150	43	0	45	25	0.31	-2	-3	0.6-0.9	200

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## Revised parameterization for gaseous dry deposition

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**Table 2.** Range of deposition velocities (in  $\text{cm s}^{-1}$ ) for 9 chemical species over all land types under dry canopy conditions

LUC	SO <sub>2</sub>	O <sub>3</sub>	NO <sub>2</sub>	H <sub>2</sub> O <sub>2</sub>	HNO <sub>3</sub>	PAN	HCHO	NH <sub>3</sub>	ROOH	
1	water	0.118 - 2.07	0.036 - 0.05	0.030 - 0.04	0.119 - 2.13	0.119 - 2.61	0.024 - 0.03	0.119 - 1.93	0.121 - 2.18	0.099 - 0.47
2	ice	0.129 - 0.80	0.038 - 0.05	0.032 - 0.04	0.132 - 0.85	0.146 - 2.91	0.025 - 0.03	0.128 - 0.68	0.133 - 0.82	0.073 - 0.14
3	inland lake	0.118 - 2.07	0.036 - 0.05	0.030 - 0.04	0.119 - 2.13	0.119 - 2.61	0.024 - 0.03	0.119 - 1.93	0.121 - 2.18	0.099 - 0.47
4	evergreen needleleaf trees	0.025 - 1.51	0.017 - 1.19	0.015 - 1.09	0.033 - 2.09	0.114 - 5.07	0.013 - 0.80	0.024 - 1.60	0.026 - 1.83	0.017 - 1.18
5	evergreen broadleaf trees	0.020 - 1.67	0.010 - 1.23	0.009 - 1.15	0.026 - 2.17	0.106 - 5.33	0.007 - 0.83	0.018 - 1.78	0.020 - 2.07	0.011 - 1.24
6	deciduous needleleaf trees	0.025 - 1.51	0.017 - 1.19	0.015 - 1.09	0.031 - 2.09	0.081 - 5.07	0.013 - 0.80	0.024 - 1.60	0.025 - 1.83	0.017 - 1.18
7	deciduous broadleaf trees	0.018 - 1.44	0.010 - 1.16	0.009 - 1.10	0.022 - 1.89	0.068 - 5.07	0.007 - 0.79	0.017 - 1.59	0.018 - 1.88	0.010 - 1.16
8	tropical broadleaf trees	0.079 - 1.64	0.039 - 1.21	0.033 - 1.13	0.107 - 2.13	0.166 - 5.33	0.027 - 0.82	0.072 - 1.75	0.080 - 2.04	0.041 - 1.22
9	drought deciduous trees	0.013 - 0.92	0.012 - 0.83	0.011 - 0.75	0.018 - 1.23	0.074 - 3.97	0.010 - 0.56	0.013 - 0.90	0.014 - 1.00	0.012 - 0.79
10	evergreen broadleaf shrub	0.027 - 1.15	0.017 - 0.94	0.016 - 0.90	0.032 - 1.48	0.102 - 3.49	0.015 - 0.65	0.025 - 1.26	0.028 - 1.47	0.018 - 0.94
11	deciduous shrubs	0.027 - 1.18	0.018 - 1.01	0.017 - 0.96	0.033 - 1.54	0.094 - 3.53	0.015 - 0.70	0.026 - 1.31	0.028 - 1.53	0.019 - 1.01
12	thorn shrubs	0.031 - 1.04	0.023 - 0.83	0.021 - 0.76	0.037 - 1.39	0.105 - 3.56	0.019 - 0.56	0.030 - 1.10	0.031 - 1.25	0.023 - 0.82
13	short grass and forbs	0.049 - 1.18	0.038 - 0.80	0.036 - 0.72	0.055 - 1.54	0.114 - 3.20	0.033 - 0.54	0.048 - 1.19	0.050 - 1.35	0.038 - 0.80
14	long grass	0.041 - 1.58	0.025 - 1.26	0.023 - 1.21	0.047 - 1.96	0.112 - 3.43	0.021 - 0.88	0.039 - 1.72	0.042 - 2.00	0.026 - 1.27
15	crops	0.035 - 1.49	0.024 - 1.28	0.022 - 1.23	0.042 - 1.90	0.104 - 3.43	0.020 - 0.90	0.034 - 1.66	0.036 - 1.92	0.024 - 1.28
16	rice	0.037 - 1.74	0.024 - 1.36	0.022 - 1.31	0.044 - 2.08	0.104 - 3.43	0.019 - 0.96	0.035 - 1.90	0.037 - 2.18	0.024 - 1.40
17	sugar	0.031 - 1.37	0.024 - 1.26	0.022 - 1.21	0.039 - 1.80	0.099 - 3.43	0.020 - 0.89	0.030 - 1.56	0.032 - 1.80	0.024 - 1.25
18	maize	0.029 - 1.03	0.020 - 0.81	0.018 - 0.75	0.035 - 1.36	0.097 - 3.41	0.017 - 0.56	0.027 - 1.08	0.029 - 1.24	0.020 - 0.80
19	cotton	0.031 - 1.31	0.022 - 1.14	0.021 - 1.08	0.038 - 1.71	0.098 - 3.63	0.019 - 0.79	0.030 - 1.46	0.032 - 1.70	0.022 - 1.13
20	irrigated crops	0.045 - 1.39	0.033 - 0.64	0.030 - 0.58	0.049 - 1.61	0.100 - 3.22	0.027 - 0.42	0.044 - 1.38	0.046 - 1.56	0.036 - 0.74
21	urban	0.025 - 0.76	0.022 - 0.58	0.021 - 0.51	0.030 - 1.13	0.069 - 4.44	0.019 - 0.37	0.025 - 0.79	0.026 - 0.89	0.022 - 0.57
22	tundra	0.051 - 0.97	0.039 - 0.53	0.036 - 0.48	0.057 - 1.12	0.103 - 3.07	0.031 - 0.35	0.050 - 0.92	0.052 - 1.04	0.039 - 0.55
23	swamp	0.045 - 1.70	0.029 - 0.96	0.027 - 0.91	0.050 - 1.97	0.114 - 3.43	0.024 - 0.65	0.043 - 1.76	0.046 - 2.02	0.032 - 1.06
24	Desert	0.049 - 0.75	0.061 - 0.19	0.053 - 0.16	0.082 - 0.87	0.142 - 2.27	0.043 - 0.12	0.052 - 0.66	0.050 - 0.77	0.056 - 0.24
25	mixed wood forests	0.021 - 1.56	0.016 - 1.42	0.015 - 1.33	0.028 - 2.19	0.103 - 5.07	0.013 - 0.96	0.020 - 1.75	0.021 - 2.03	0.016 - 1.39
26	Transitional forest	0.021 - 1.55	0.016 - 1.41	0.015 - 1.32	0.028 - 2.19	0.103 - 5.07	0.013 - 0.95	0.020 - 1.74	0.021 - 2.02	0.016 - 1.38

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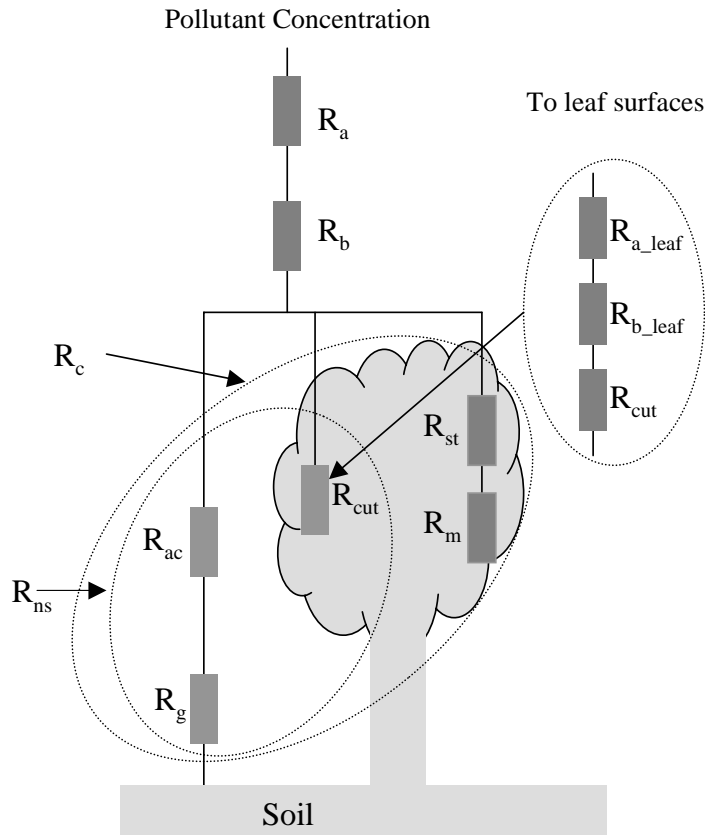


Fig. 1. Scheme of resistance analogy.

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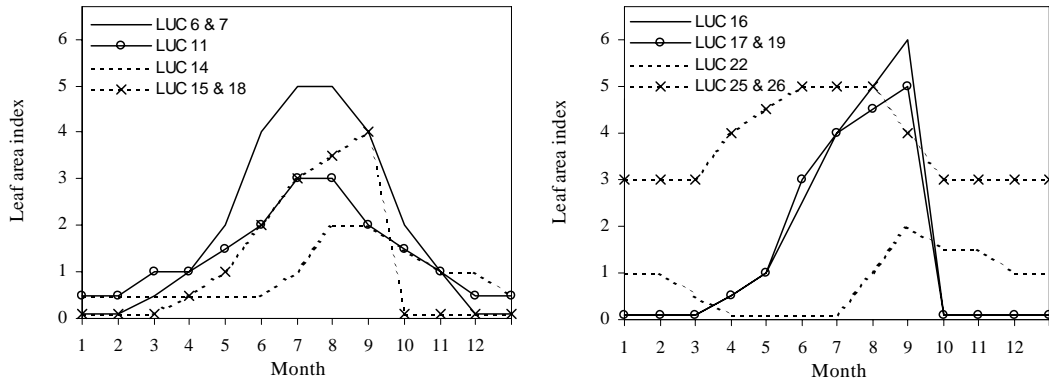


Fig. 2. Leaf area index in the Northern Hemisphere.

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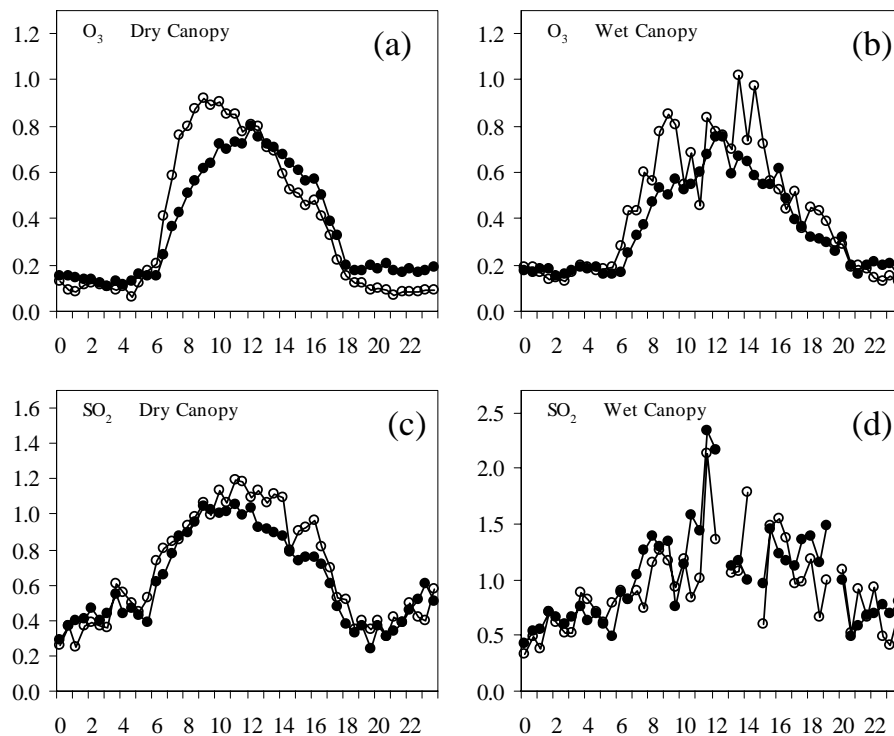
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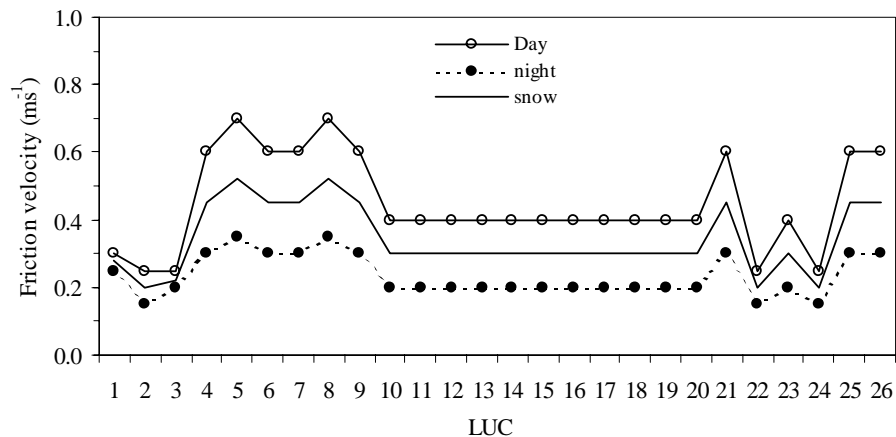
**Fig. 3.** Average diurnal cycle of modelled (filled points) and observed (open points) deposition velocities.

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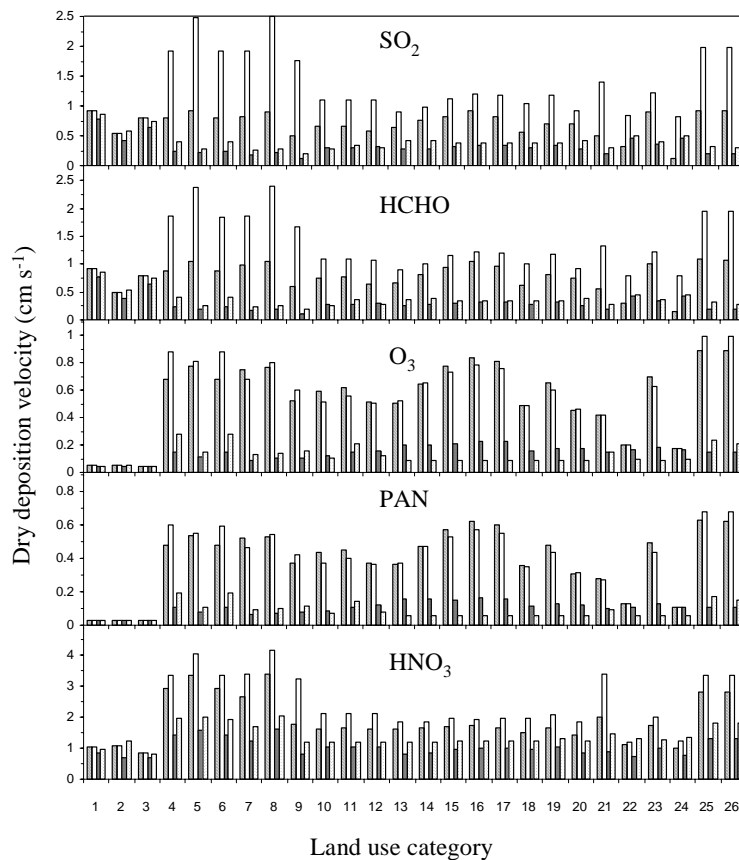
**Fig. 4.** Friction velocity values used for producing Fig. 5.

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**Fig. 5.** Dry deposition velocity for chemical species  $\text{SO}_2$ ,  $\text{HCHO}$ ,  $\text{O}_3$ ,  $\text{PAN}$  and  $\text{HNO}_3$  under 4 typical conditions: dry summer day, rain summer day, dry summer night and winter with snow (shown, respectively as 4 columns from left to right).

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