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Estimates for localised transverse electric modes in multi-structured crystal fibres

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Abstract

The paper presents analytical and numerical models describing localised transverse electric defect modes in a doubly periodic structure involving split ring inclusions. We provide an asymptotic estimate which can be implemented in the optimal design of low frequency stop bands in photonic crystal fibres.

Key words: Thin-bridges, split ring resonators, optical fibres

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1. Introduction

Split ring resonators (SRR) have recently attracted a great deal of attention since they are building blocks of so-called meta-materials exhibiting artificial magnetism [1]. Here, we propose to use them as the building blocks of locally resonant photonic crystal fibres. The idea is to replace each of the six air holes of the micro-structured fibre studied in [2] by a SRR. The dispersion diagrams for electromagnetic waves in such a structure possess low frequency stop bands. The boundaries of these stop bands can be evaluated analytically and hence the filtering properties can be controlled by changing the physical parameters of the system.

2. Formulation of the problem

We consider transverse electric waves propagating within a doubly periodic array of ‘defects’ represented by a ‘cloud’ of 6 voids $\Omega_1, \Omega_2, \dots, \Omega_6$ embedded in an hexagonal elementary cell Y (see figure 1(a)). In this case, the time harmonic transverse electric field has the form $\mathbf{E}(x, y, t) = (E_1(x, y), E_2(x, y), 0)e^{-i\omega t}$ so that its magnetic counterpart $\mathbf{H}(x, y, t) = (0, 0, H_3(x, y))e^{-i\omega t}$ is longitudinal. The propagation of these waves satisfies the Helmholtz equation taken in distributional sense

$$\left(\nabla \cdot \frac{1}{n^2(x, y)} \nabla \right) H_3(x, y) + \frac{\omega^2}{c^2} H_3(x, y) = 0, \quad (1)$$

where c is the speed of light in vacuum, ω the wave frequency and n the refractive index such that $\alpha \geq n \geq \beta > 0$, where α and β are positive arbitrary constants. We look for solutions H_3 of finite energy in Y which satisfy the Floquet-Bloch condition

$$H_3((x + p\mathbf{l}^{(1)}, y + q\mathbf{l}^{(2)})) = H_3(x, y)e^{i(k_1 p + k_2 q)}, \quad (2)$$

where $\mathbf{l}^{(1)} = d(1, 0)$, $\mathbf{l}^{(2)} = d/2(1, \sqrt{3})$ are the lattice vectors, d is the period of the structure, p and q are integers, and $\mathbf{k} = (k_1, k_2)$ represents the Bloch vector.

Equation (1) is then solved numerically by considering its weak formulation using test functions V taking values on nodes of a triangular mesh of the basic cell Y . The Finite element formulation was used in the numerical computations with Getdp [3] where special care was taken to enforce Floquet-Bloch conditions [4].

3. Helmholtz equation within thin-bridges

Here, the metallic inclusions $\Omega_1, \dots, \Omega_6$ are of the shape of the letter C and they are located and oriented in such a way as to preserve the six-fold symmetry (figure 1). Formally, using local coordinates associated with each inclusion

$$\Omega_j = \{a_j < \sqrt{x^2 + y^2} < b_j\} \setminus \overline{\Pi_\varepsilon^{(j)}}, j = 1, \dots, 6, \quad (3)$$

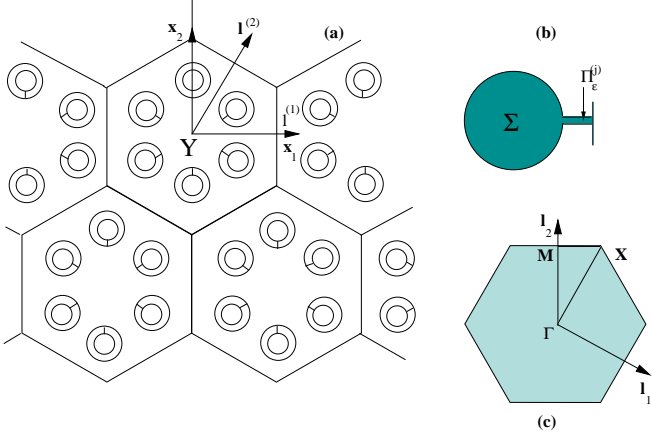


Fig. 1. (a) Physical space. A doubly periodic array of hexagonal macro-cells containing six split ring resonators located and oriented to preserve six-fold symmetry. b) Associated multi-structure consisting of a large body Σ connected to a thin bridge $\Pi_\varepsilon^{(j)}$ (c) Reciprocal space. Irreducible part of the first Brillouin zone $\Gamma M X$ where $\Gamma = (0, 0)$, $M = (0, 2\pi/(\sqrt{3}d))$ and $X = (2\pi/(3d), 2\pi/(\sqrt{3}d))$.

where a_j and b_j are given constants, and

$$\Pi_\varepsilon^{(j)} = \left\{ (x, y) : a_j < x < b_j, |y| < \varepsilon h_j/2 \right\}, \quad (4)$$

is a thin ligament between the ‘ends of the letter C’. Here εh_j is the thickness of the j -th bridge, with ε being a small positive non-dimensional parameter.

The function $H_3(x, y)$ satisfies the Helmholtz equation within the thin-ligament $\Pi_\varepsilon^{(j)}$ occupied by a material of constant refractive index n_j ,

$$\nabla^2 H_3(x, y) + n_j^2 \frac{\omega^2}{c^2} H_3(x, y) = 0, \quad (5)$$

together with homogeneous Neumann boundary conditions (infinite conducting walls)

$$\frac{\partial H_3}{\partial y} \Big|_{y=\pm \varepsilon h_j/2} = 0. \quad (6)$$

This system will be supplied with appropriate boundary conditions at the ends $x = a_j$ and $x = b_j$. From now on, we drop the index j for simplicity.

4. Thin-bridge analysis

Let us introduce the scaled variable $\xi = \frac{y}{\varepsilon}$. Hence, $\frac{\partial^2 v}{\partial y^2} = \frac{1}{\varepsilon^2} \frac{\partial^2 v}{\partial \xi^2}$, and the rescaled wave equation in $\Pi_1 = \left\{ (x, \xi) : a < x < b, |\xi| < h/2 \right\}$ becomes

$$\left(\frac{1}{\varepsilon^2} \frac{\partial^2}{\partial \xi^2} + \frac{\partial^2}{\partial x^2} + n^2 \frac{\omega^2}{c^2} \right) H_3 = 0. \quad (7)$$

The field H_3 is approximated in the form

$$H_3 \sim H_3^{(0)}(x, \xi) + \varepsilon^2 H_3^{(1)}(x, \xi). \quad (8)$$

To the leading order we obtain (see (6), (7) and (8))

$$\frac{\partial^2 H_3^{(0)}}{\partial \xi^2} = 0, \quad |\xi| < h/2, \quad \frac{\partial H_3^{(0)}}{\partial \xi} \Big|_{\xi=\pm h/2} = 0. \quad (9)$$

Hence, $H_3^{(0)} = H_3^{(0)}(x)$ (it is ξ -independent). The function $H_3^{(1)}$ satisfies the following model problem on the scaled cross-section of Π_1

$$\frac{\partial^2 H_3^{(1)}}{\partial \xi^2} = -\frac{\partial^2 H_3^{(0)}}{\partial x^2} - n^2 \frac{\omega^2}{c^2} H_3^{(0)}, \quad |\xi| < h/2, \quad \frac{\partial H_3^{(1)}}{\partial \xi} \Big|_{\xi=\pm h/2} = 0. \quad (10)$$

The solvability condition for the problem (10) gives us the equation for $H_3^{(0)}$, that is,

$$\frac{d^2 H_3^{(0)}}{dx^2} + n^2 \frac{\omega^2}{c^2} H_3^{(0)} = 0, \quad a < x < b. \quad (11)$$

Thus, to the leading order, we can approximate the field H_3 within the thin bridge Π_ε by the function $H_3^{(0)}(x)$ which satisfies the one-dimensional Helmholtz equation.

5. An asymptotic estimate of the frequency of the localised mode

We are interested in standing waves (flat curves on the dispersion diagram of Figure 2). For low frequencies, let C_1 denote the constant value of the field in the core $\Sigma = \{\sqrt{x^2 + y^2} < b\}$ of the multi-structure Ω , and C_2 denote the constant value of the field within the complementary area of the macro-cell $Y \setminus \Omega$ excluding the ligaments. Then, neglecting the small area of the ligament, we obtain

$$C_1 \mathcal{S}_\Sigma + C_2 \mathcal{S}_{Y \setminus \Omega} = O(\varepsilon), \quad (12)$$

where \mathcal{S}_Σ and $\mathcal{S}_{Y \setminus \Omega}$ denote the areas of Σ and $Y \setminus \Omega$.

Boundary layers occur at the end regions of the thin ligaments [6]. These boundary layers are characterized by exponential decay when $H_3^{(0)}$ satisfies:

$$\begin{aligned} H_3^{(0)}(a) &= C_1, \\ H_3^{(0)}(b) &= C_2 = -\frac{\mathcal{S}_\Sigma}{\mathcal{S}_{Y \setminus \Omega}} C_1. \end{aligned} \quad (13)$$

Now, integrating (5) over the multistructure Ω and applying the divergence theorem, we obtain that to order ε

$$\frac{dH_3^{(0)}}{dx} \Big|_{x=a} = -\frac{n^2 \mathcal{S}_\Sigma \omega^2}{c^2 \varepsilon h} C_1. \quad (14)$$

Combining (11), (13) and (14), in the low frequency limit we obtain

$$\omega^2 \sim \frac{\varepsilon h c^2}{(b-a) \mathcal{S}_\Sigma n^2} \left(1 + \frac{\mathcal{S}_\Sigma}{\mathcal{S}_{Y \setminus \Omega}} \right). \quad (15)$$

We note that this estimate is in agreement with the one derived in [5] for anti-plane shear waves when $\mathcal{S}_\Sigma/\mathcal{S}_{Y \setminus \Omega}$ vanishes.

6. Thin-bridge estimates versus finite elements results

Formula (15) is an accurate estimate for the frequency of TE modes trapped in split ring resonators. Here n is the refractive index of the dielectric material within the SRR, εh is the constant thickness of the thin bridge (split), \mathcal{S}_Σ is the area of the core of the ring, and $\mathcal{S}_{Y \setminus \Omega}$ is the area of the hexagonal cell excluding the six rings and their cores.

In our case, $\varepsilon h = 0.012$, $\mathcal{S}_\Sigma = \pi * 0.159^2$, $b - a = 0.1$ and $n = \sqrt{12}$, and $\mathcal{S}_{Y \setminus \Omega} = 3\sqrt{3}/2 - 6\pi 0.259^2 = 3.93$, so that $\frac{\mathcal{S}_\Sigma}{\mathcal{S}_{Y \setminus \Omega}} = 0.02$. Hence, we find $\omega_1 d/c = 0.3548$ whereas the finite element computation gives $\omega_1^* d/c = 0.35308$. This is associated with the lower flat band on the right dispersion diagram of Figure 2. We notice that this first localised eigenmode is axi-symmetric (constant) within each inclusion except for thin bridges. Its analytic expression in thin bridges is given by

$$H_3^{(0)}(x) = -\frac{C_2 \cos(\omega(b-a)/c) - 1}{\sin(\omega(b-a)/c)} \sin(\omega x/c) + C_2 \cos(\omega x/c). \quad (16)$$

7. Higher localised modes and possible applications

Finally, the upper flat curve (the seventh dispersion curve) in figure 2 corresponds to a dipole mode localised within each structured inclusion. In this case, the thin bridges play little part. Hence, if we denote the refractive index of the core of the inclusion by n , such a mode is simply the solution of the Helmholtz equation

$$\Delta H_3 + n^2 \frac{\omega^2}{c^2} H_3 = 0, \quad x_1^2 + x_2^2 < r_1^2. \quad (17)$$

In polar coordinates, the dipole solution of this problem is

$$H_3(r, \theta) = J_1\left(\frac{\omega n r}{c}\right) e^{i\theta}. \quad (18)$$

Further, the dipole mode we are looking for satisfies the Neumann condition $\partial H_3 / \partial r = 0$ on the inner circular boundary $r = r_1$ of the split ring. Hence, the associated frequency is given by the first root of the transcendental equation

$$\frac{\omega n}{c} J_1'\left(\frac{\omega n r_1}{c}\right) = 0, \quad (19)$$

where $r_1 = 0.159d$ and $n = \sqrt{12}$. This gives an estimate $\omega_2 d/c = 3.36$ for the normalised frequency of the first dipole mode of split rings (see Figure 2(b)) which fits reasonably well the numerical value $\omega_{FEM} = \omega_2^* d/c = 3.4540$ given by Finite Element Computations.

Dispersionless modes propagating along the crystal fiber at very low frequency (as it is the case for the localised mode associated with the lower flat band) may lead to sub-wavelength imaging in a way similar to that demonstrated in [7] for swiss-rolls at radio frequencies. Modes associated

with flat curves at higher frequencies suggest that they would be nearly leakage free in the case of multi-structured fibres of finite cross-section. Multi-structured crystal fibres hence have possible applications both in medical imaging (radio frequencies) and long-haul communications (from near infra-red to optical frequencies).

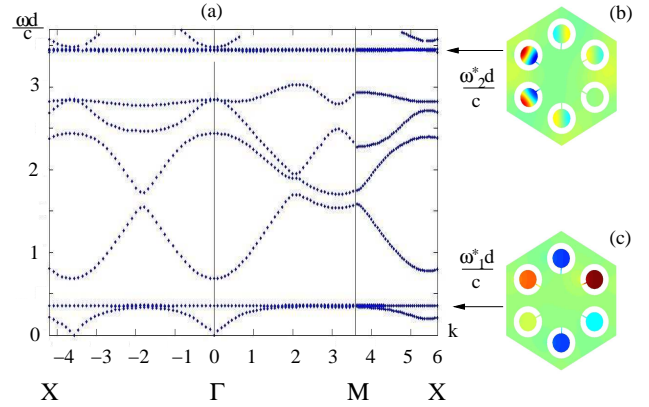


Fig. 2. Transverse incidence. (a) Dispersion diagram for six infinitely conducting inclusions shaped as split ring resonators of inner radius $0.159d$ and outer radius $0.259d$ (right) and filled with a dielectric material of relative permittivity 12. The center-to-center spacing of inclusions is $0.7d$. Inclusions are surrounded by a matrix of relative permittivity 1. The horizontal axis shows the magnitude of the Bloch vector describing the first Brillouin zone described in Figure 1(c). On the vertical axis, we represent the eigenfrequencies of propagating TE waves. (b) Eigenfield associated with eigenfrequency $\omega_1^* d/c = 0.35308$ (root of multiplicity six) which is constant in the center of each C-shaped inclusion. (c) Eigenfield associated with eigenfrequency $\omega_2^* d/c = 3.4540$ (multiple root). We note the dipole nature of modes confined in the center of each C-shaped inclusion.

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