

# OAM Beam Generation using All-fiber Fused Couplers

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**Abstract:** We demonstrate the orbital angular momentum (OAM) beam generation using an all-fiber fused coupler based on single mode fiber (SMF) and air-core fiber. The fabricated device is directly SMF compatible with ~80% power coupling efficiency.

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## 1. Introduction

Optical beams with orbital angular momentum (OAM), characterized by a helical phase front,  $\exp(il\phi)$  ( $l$  &  $\phi$  being topological charge and azimuthal angle, respectively), have gained much interest in recent years due to the potential for using OAM states as orthogonal signal channels for scaling the bandwidth of next-generation optical communication networks [1-3]. OAM generation has been widely studied in free space [1, 4, 5 and references therein], silicon chips [6, 7], and to a limited extent, in fiber [8, 9]. While a few of these devices offer scalability, i.e. ability to multiplex many OAM modes with low loss, none of them are directly fiber compatible. Hence, alternative all-fiber based techniques which offer the potential for direct integration with existing telecom/datacom infrastructures, and yet are mode-scalable, are highly desirable.

In this paper, we demonstrate generation of OAM beam through the well-known fused fiber coupler fabricated using single mode fiber (SMF) and OAM air-core fiber [10, 11], by using the mechanism of exciting specific higher order modes (HOM) [12, 13]. As fused fiber couplers as well as photonic lanterns [14] have been the widely utilized in Mode Division Multiplexing (MDM) transmission, the demonstrated all-fiber based fused coupler provides the first realistic pathway to multiplexing many OAM modes in fibers with low loss.

## 2. Fused fiber couplers and excitation of OAM beam

In general, modes in the air-core fibers propagate with different effective indices ( $n_{\text{eff}}$ ) than  $LP_{01}$  in SMF, due to the different fiber refractive index profiles. The  $n_{\text{eff}}$  or propagation constants of the selected modes must be matched in order to achieve coupling from  $LP_{01}$  in SMF to any HOM in the air-core fiber [13]. As HOMs are associated with lower  $n_{\text{eff}}$ , the diameter of the SMF is reduced, by pre-tapering, to phase match  $LP_{01}$  with that of a selected HOM in the air-core fiber.

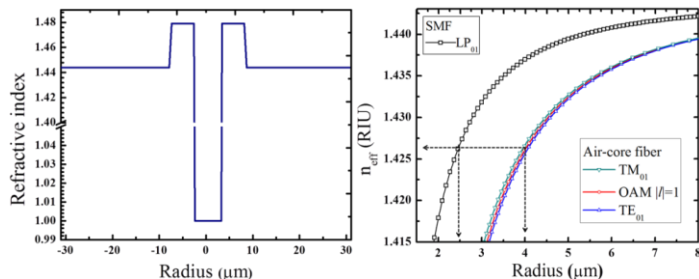


Figure 1: Simulation results: (a): Index profile of OAM air-core fiber, (b): Effective index ( $n_{\text{eff}}$ ) of different modes in SMF ( $LP_{01}$ ) and air-core fiber ( $TM_{01}$ , OAM  $|l|=1$ ,  $TE_{01}$ ) fiber as a function of radius of fiber; phase matching points are indicated.

The air-core fiber, shown in Fig. 1. (a), ensures stable propagation of excited OAM modes [10, 11] by lifting the modal degeneracy and suppressing the intermodal cross talk. The phase matching condition is studied using COMSOL Multiphysics<sup>®</sup> eigen mode solver to estimate the diameter ratio between SMF and OAM fiber. Fig 1. (b), shows  $n_{\text{eff}}$  for the  $LP_{01}$  mode in SMF and the OAM  $|l|=1$  mode in the air-core fiber are mapped as a function of fiber radius in order to calculate fiber diameter ratio to achieve phase matching [8]. When phase matching is achieved, the superposition of excited OAM  $|l|=1$  modes is tuned by controlling input polarization, with each circular polarization exciting one specific OAM mode in its 2-mode degenerate subspace.

## 3. Experimental details, results and discussion

Conventional telecom-grade SMF is pre-tapered to  $\sim 75.8\mu\text{m}$  (with less than 0.1dB loss) according to the diameter ratio calculated from simulation studies (Fig. 1. (b)). The pre-tapered SMF is longitudinally aligned with the un-

tapered air-core fiber without any twist, and fixed with a UV-curable adhesive glue. The coupler is fabricated using the modified flame brushing technique by fusing both the fibers at  $\sim 1400$  °C using a ceramic micro heater (NTT-AT, Japan) and by pulling them using a commercial fiber tapering rig. After a certain length of pulling, the fibers weakly fuse and the  $LP_{01}$  mode in the SMF couples into the OAM mode of the air-core fiber to which it is phase matched. The tapering is stopped when power measured out of the air-core fiber is maximized.

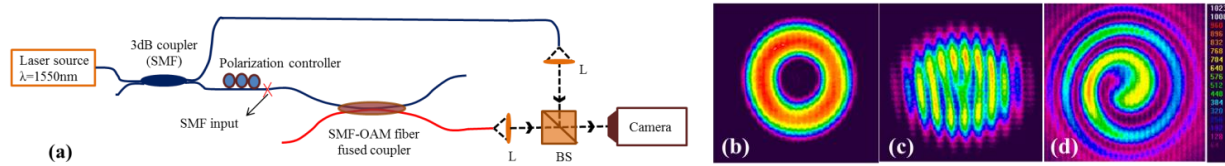


Figure 2: (a): Experimental setup to characterize the generated OAM beam—solid lines are propagation path of light through fiber, dashed lines are that of light through free space, L—collimating lens, BS—free space beam splitter. (b): Far field image of the generated OAM beam. (c) & (d): Fork and spiral interference patterns of OAM beam and Gaussian reference, respectively.

Fig. 2. (a) depicts the schematic for device characterization: light from a 1550-nm laser source (linewidth  $\sim 0.4$ nm) is split into two arms using a 3dB coupler. One arm is passed through a polarization controller and spliced to the fabricated OAM coupler, and the other arm is used to construct and SMF-based reference arm in the interference setup. The output beams from the reference SMF and air-core fiber (cleaved within  $\sim 30$ cm after the coupling region in the device) are collimated and then interfered using a free space beam splitter. The field patterns are imaged using a CCD camera (MicronViewer-7290A). Fig. 2. (b) shows a clear doughnut pattern out of the air-core fiber output when the reference arm is blocked. The absence of  $LP_{11}$  mode like patterns and a relatively uniform azimuthal intensity distribution qualitatively suggests that phase matched coupling to the OAM modes was achieved without substantial coupling to the neighboring  $HE_{11}$ ,  $TE_{01}$  or  $TM_{01}$  modes (see Fig. 1. (b) for mode designations). A polarization measurement performed using a polarizer and quarter wave plate combination reveals that this beam is uniformly circularly polarized, further suggesting that these beams are OAM eigenmodes of the air-core fiber. With the reference arm un-blocked but incident on the camera at a slight angle with respect to the beam from the air-core fiber, the input polarization is adjusted until the characteristic fork interference pattern is observed (Fig. 2. (c)). With the beam from the reference arm co-aligned with that from the air-core fiber, we observe the characteristic spiral interference between an OAM and an expanded Gaussian beam (Fig. 2. (d)). These observations are consistent with the fact that the beam exiting the air-core fiber is substantially a pure OAM mode. The coupling efficiency of the device is measured to be  $\sim 80\%$ , and further studies on quantitatively determining the purity of output OAM beams and enhancing the efficiency of the device are under progress.

In summary, we demonstrate the first, to the best of our knowledge, fused fiber coupler that enables generation of OAM beams in fibers that stably propagate them, using an SMF input. Since this is a side coupling technique, it could potentially be repeated along the length of the OAM fiber to simultaneously generate multiple OAM orders, thereby yielding a fiber-compatible, low loss, scalable (de)multiplexer of OAM beams, which are of immense interest to OAM-based capacity enhancement schemes.

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