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FOUR-D GLOBAL REFERENCE ATMOSPHERE USERS MANUAL AND PROGRAMMERS MANUAL Part II

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15. SUPPLEMENTARY NOTES This document was prepared based on the engineering design problems which have been identified or anticipated for the Space Shuttle program.					
16. ABSTRACT An empirical atmospheric model has been developed which generates values for pressure, density, temperature, and winds from surface levels to orbital altitudes. The output parameters consist of components for: (1) latitude, longitude, and altitude dependent monthly and annual means, (2) quasi-biennial oscillations, and (3) random perturbations to simulate partially the variability due to synoptic, diurnal, planetary wave, and gravity wave variations. Quasi-biennial and random variation perturbations are computed from parameters determined from various empirical studies and are added to the monthly mean values. This model has been developed as a computer program called PROFILE which can be used to generate altitude profiles of atmospheric parameters along any simulated trajectory through the atmosphere. The PROFILE program was developed for design applications in the Space Shuttle program. Other applications of the model are discussed, such as for global circulation and diffusion studies, and for generating profiles for comparison with other atmospheric measurement techniques, (e.g. satellite measured temperature profiles). The results are given in two parts, viz: TMX-64871 , Four-D Global Reference Atmosphere, Technical Description, Part I and TMX-64872 , Four-D Global Reference Atmosphere Model Users Manual and Programmers Manual, Part II. * Georgia Institute of Technology Atlanta, Georgia 30332					
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PREFACE

This preface covers a two-part publication. NASA TMX-64871 , Four-D Global Reference Atmosphere, Technical Description and NASA TMX-64872 , Four-D Global Reference Atmosphere Model, Users Manual and Programmers Manual, Part II, both with publication date of September 1974.

The motivation for the development of a global reference atmospheric model is from recognized needs for engineering design, mission planning, performance analysis, and possibly operational usage for the Space Shuttle program.

The concept of a global reference atmospheric model has its origin as an extension of the Range Reference Atmospheric Model which is a model of the gas properties over a particular geographic location. Particular range reference atmospheric models are the Patrick Reference Atmosphere (Annual) which is valid for Cape Kennedy, Florida, Vandenberg AFB Reference Atmosphere (Annual) and Edward AFB Reference Atmosphere (Annual). To represent the dispersions in the gas properties, pressure, temperature, and density there are also the Hot and Cold Reference Atmospheres for these three sites. Range Reference Atmospheres have been developed for a number of U. S. National Missile Test Ranges under the auspices of the Range Commanders Council/Meteorology Group (formerly the Inter-Range Instrumentation Group/Meteorological Working Group, IRIG/MWG).

The first development toward the present global reference atmosphere was a Four-Dimensional World-Wide Model valid for 0 - 25 km altitude. The four dimensions come from the three coordinates, latitude, longitude, and altitude, plus time, where time is with respect to monthly reference periods. The parameters modelled are gas properties and moisture. The monthly means and daily variation of these parameters are obtained for any latitude, longitude, altitude, and monthly reference period by a computer interpolation program. This four-dimensional world-wide model was developed for the design and performance analysis of earth viewing instrumentation used on earth orbiting satellites.

Man-made earth orbiting satellites created a need for and a means to develop atmospheric models at orbital altitudes. Models for these altitudes have a much different form than those at lower altitudes because of the strong solar influence which contributes to variation and the contrasting differences in the

basic measurements. Orbital altitude models express the gas properties as continuous variables with respect to time. The variables are given by a few simple, but complex equations, as a function of time with parameters for solar activity. The data for orbital models are derived from continuous sensors (satellites) which make many earth revolutions, over short periods up to many years covering all earth reference coordinates, whereas the data available for modelling at lower altitudes are derived from point measurements in time which are constrained to fixed earth coordinates of latitude and longitude, e. g., rawinsonde and meteorological rocketsonde measurements. Although difficult as it is to establish, a continuous atmospheric model from the earth's surface to and including orbital altitudes is required for a mission of the Space Shuttle. Layered models with respect to altitude and at discrete latitudes are not satisfactory for a Space Shuttle flight performance analysis. The Four-Dimensional Global Reference Atmosphere presented in this report is a first attempt to offer a means to represent the gas properties in a continuous manner over all altitudes for all earth coordinates (latitude and longitude) from the earth's surface up to orbital altitudes or from orbital altitudes down to the earth's surface.

The Four-D Global Reference Atmosphere Model (GRA) is in the form of a computer program which has several options for output data. The computer card input depends on the desired output option. The principal input parameters are height, latitude, longitude, solar activity parameters (geomagnetic index, F10.7 and 81 day mean 10.7 cm flux), date (month, day, and year or annual reference period) and Greenwich time. The computer used is the Univac 1103 with a core requirement of slightly under 32K words. All magnetic tapes are seven track. One program tape and one data tape are required for all altitudes above 30 km and from one to four data tapes for altitudes below 30 km altitude. Standard card punch is required if one of the optional card outputs is selected. The computer program is completely documented in a separate volume, entitled "Four-D Global Reference Atmosphere Model, Users Manual and Programmers Manual, Part II". Qualified requestors may receive the computer program, which includes the program magnetic tape and the required magnetic data tapes, and the documental manual by addressing their request to Chief, Aerospace Environment Division, ES41, Space Sciences Laboratory, NASA Marshall Space Flight Center, AL 35812.

A feature of the GRA is that representative wind fields may also be derived. This was done to assure consistency in the modelling process and for scientific interest in the general circulation pattern and for potential applications for long-term diffusion processes. With some innovations one can envision further adaptations and applications of the GRA for a general class of ascending and descending aerospace vehicles.

It is envisioned that as more familiarity with this Global Reference Atmosphere is gained, improvements and adaptations of various computer program options will be developed for specific problems. However, any near future revisions will not change the basic program.

The Four-D Global Reference Atmosphere Model should be used in its entirety where appropriate to include the monthly means and standard deviations of dispersions of the gas properties and the Monte Carlo generated profiles along the trajectory. For some analyses it may be sufficient to use only the means plus and minus 2.3263 standard deviations of the variables to obtain satisfactory engineering design or operational solutions. The means \pm 2.3263 standard deviations give the 1st and 99th percentile values of the variables which is the 98th interpercentile range of the variables. In other cases, such as maximum point aerodynamic heating, or for some particular feature of the guidance and control system a number of Monte Carlo generated atmospheric profiles may be required to obtain design and performance limits.

O. E. Smith and W. W. Vaughan
September 1974

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A. USERS MANUAL

1. GENERAL PROGRAM CHARACTERISTICS

As outlined in Figure 1.1 of the technical write-up of the PROFILE program, the simulation of monthly mean parameters is handled by three different models governing three sections of altitudes with transition regions in between to ensure a smooth resultant profile. The 0-25 km height range is modeled by the 4-D section of PROFILE, based on the NASA 4-D model (Spiegler and Fowler, 1972). The 30-90 km section is simulated by a modified Groves (1971) model. Above 115 km the atmosphere is simulated entirely by the Jacchia (1970) model. Between 25 and 30 km the model interpolates between 4-D and modified Groves values, and between 90 and 115 km the program fairs between the modified Groves values and the Jacchia results. In addition to the three methods of determining mean atmospheric parameters, based on height region, there are also two kinds of perturbations added to the mean parameters: random perturbations, and quasi-biennial oscillations.

The PROFILE program is designed to produce atmospheric parameter values either along a linear path (to be called a profile) with automatically stepped constant height, latitude, and longitude increments, or along any set of connected positions (to be called a trajectory) which must be input individually into the program.

There are three general types of input to the PROFILE program: (1) A set of three cards, called the initial data, which contain the values of the program options, the initial position, the profile increments, and other information required before the calculations are begun, (2) A data tape

(SCIDAT) containing parameter values for the Groves (1971) model, the stationary perturbations (deviations from the Groves model, to produce longitude varying monthly means), and random and quasi-biennial perturbation parameter values, and (3) The 4-D data tapes with one data file for each month, containing profiles of monthly mean pressure, density, temperature, and their variances from the surface to 25 km, for the entire globe. If it is desired to compute atmospheric parameters along a trajectory instead of a linear profile, then a fourth type of data - the trajectory times and positions - must be input.

In terms of program function, the major elements of the PROFILE program are the main segment (PROFIL), the subroutine SCIMOD, which is a driver for all of the atmospheric evaluation subroutines, and SETUP, a subroutine used to read the SCIDAT data tape, and load the necessary starting conditions for execution. Figure 1 shows a simplified schematic of the main segment and illustrates the function of the SETUP and SCIMOD subroutines.

Output of the PROFILE program consists of monthly mean pressure, density, temperature, wind, and wind shear, total (mean plus perturbation) values of pressure, density, temperature, winds, perturbation values, and magnitudes.

Complete discussion of the input, output, and program operation characteristics for the PROFILE program are given in the following sections of the users manual.

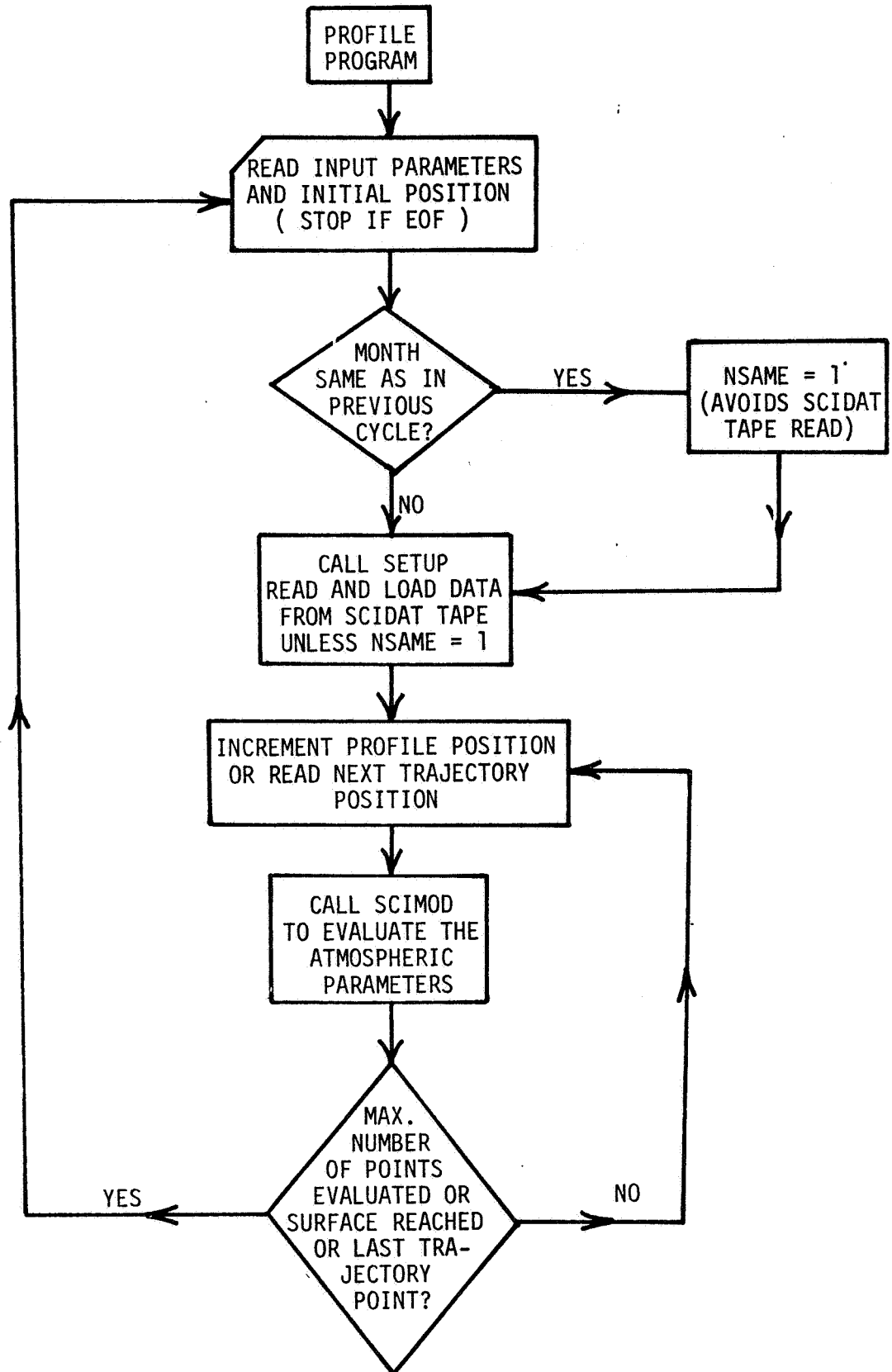


Figure 1: Simplified flow chart of the PROFILE program.

2. THE 4-D INPUT DATA TAPES (0-25 Km)

The description contained in this section was paraphrased from the 4-D program users manual (Fowler and Willard, 1972). For more information on the 4-D section of PROFILE, consult that document and Spiegler and Fowler (1972).

The world-wide meteorological data set developed for the 4-D model by Allied Research Associates is stored on three 7-track, 800 bpi binary tapes labelled WW1A-WW3A. Each tape contains four files of data where one file represents one month; WW1A contains months 1-4, WW2A contains months 5-8, and WW3A contains months 9-12. A 13th month containing the annual reference period has been added as a fourth tape.

Within each file are 3490 records representing the values at individual grid points. These points are grouped into three grids: 288 points on the northern hemisphere equatorial (EQN) grid; 1977 points on the northern hemisphere (National Meteorological Center) grid; and 1225 points on the southern hemisphere (SH) grid. On the NMC grid, the data was computed at NMC points and stored in the order given by the NMC grid table shown in the SCIDAT data tape listing in Appendix A. On the other two grids, the data was given at 5° latitude - longitude intersections westward from the Greenwich Meridian to 5° east. The EQN grid covers the latitudes from 0° to 15° north with points occurring in the following order: 1-4 = Lon. 0, Lat. 0, 5, 10, 15; 5-8 = Lon. 5W, Lat. 0, 5, 10, 15; ... 285-288 = Lon. 5° E, Lat. 0, 5, 10, 15. The SH grid contains all data from 5° south to the south pole as follows: 1 = South Pole, 2-18 = Lon. 0, Lat. -5 to -85; 19-35 =

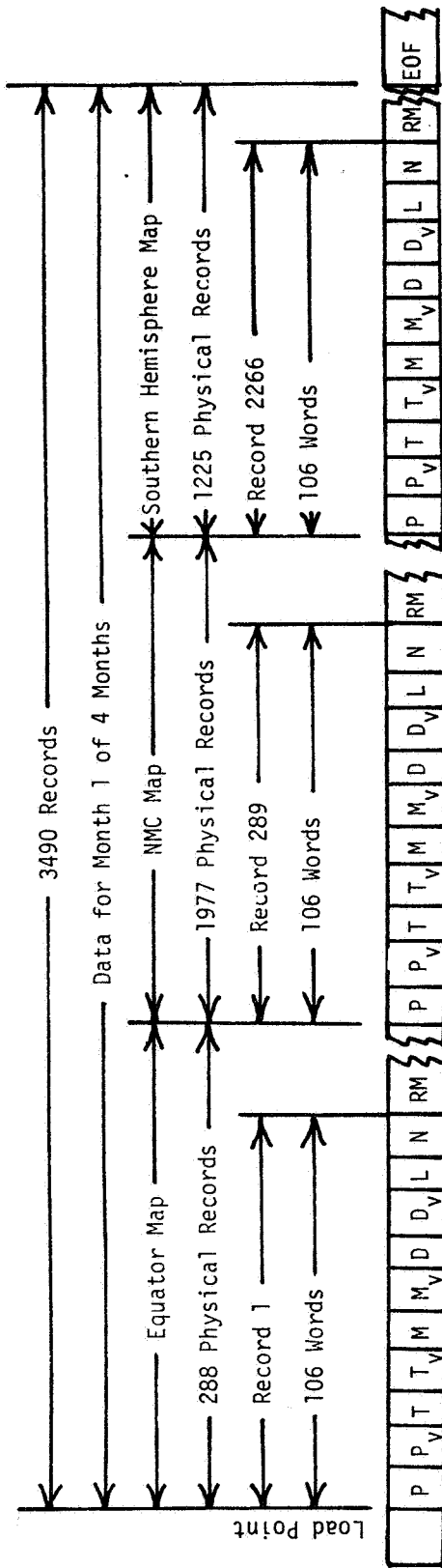
Lon. 5⁰W, Lat. -5 to -85; ... 1209 - 1225 = Lon. 5⁰E, Lat. -5 to -85.

It should be noted that the south pole is given only once, as the first point of the SH data set.

Each record consists of 106 36-bit words where the first 104 words contain the computed data for a point and the last two are identifiers. All data values are multiplied by 100 and converted to integer; they are then packed with two 18-bit values to a word. The data is arranged by level for each parameter; thus, the first 13 words contain the pressure means from the surface to 25 km and the next 13 words contain the pressure variances for the same levels. This pattern continues for the 26 levels of temperature means and variances, moisture means and variances, and density means and variances.

Word 105 contains the latitude and longitude of the point in question. These are integer values that have been multiplied by 10; each occupies 18 bits of the word. The latitude is always positive (since the southern hemisphere is identified by grid), and the longitude is always west.

The last word contains three 12 bit integer values. The left-most group of bits is the homogeneous moisture region in which the point lies, the center group is the point number, and the right-most group of bits is the month. It should be noted that the points are numbered within the grid that contains them, and not by their location on tape. Thus the point numbers run from 1-288, 1-1977, and 1-1225, not from 1-3490. Figure 2 shows the tape structure for one month.



This box represents 26 integer values of pressure in millibars $\times 10^2$. Each value is packed sequentially as an 18 bit byte, starting with the surface and ending with the 25 km value.

Variations are the square of the standard deviations.

RM denotes end of record mark.

EOF Denotes end of file mark.

- P - Pressure ($\text{mb} \times 10^2$)
- P_v - Pressure Variance ($\text{mb}^2 \times 10^2$)
- T - Temperature ($^\circ\text{K} \times 10^2$)
- T_v - Temperature Variance ($^\circ\text{K}^2 \times 10^2$)
- M - Moisture ($\text{g}/\text{m}^3 \times 10^2$)
- M_v - Moisture Variance ($\text{g}^2/\text{m}^6 \times 10^2$)
- D - Density ($\text{g}/\text{m}^3 \times 10^2$)
- D_v - Density Variance ($\text{g}^2/\text{m}^6 \times 10^2$)
- L - Word 105 Containing Latitude and Longitude
- N - Word 106 Containing Homogeneous Region Number, MSF Point Number, and Month Number

Figure 2. Record structure on the 4-D data tapes

3. The "SCIDAT" DATA TAPE

This section describes in detail the data contained on the SCIDAT data tape. A listing of this tape, and a one page synopsis of the data contained on it are given in Appendix A.

NMC Grid Data

This data set gives the 4-D northern hemisphere point number and the dual index for the corresponding NMC location. The NMC grid locations form an octagonal array, centered on the North Pole. The points are at square grid locations on the polar projection used for the NMC grid. A conversion between the latitude and longitude (treated as polar coordinates on the flat NMC grid plane) and the NMC grid indices (treated as Cartesian coordinates on the projection plane) is accomplished by a polar to Cartesian coordinate transformation, via equations programmed into the 4-D model. The NMC grid data on the SCIDAT tape merely establishes the equivalence between the sequential 4-D NMC point number and the two-dimensional x-y NMC grid point location. The NMC grid data constitute the first file on the SCIDAT tape. An end of file marker appears on the tape at the end of the NMC grid data.

Groves Data

The Groves (1971) data for monthly mean pressure, density, and temperature are tabulated at 10 degree latitude intervals from 0 to 90⁰ for each month. The yearly average Groves data is coded as month 13. The southern hemisphere data is the same as the northern hemisphere data displaced by 6 months. Annual mean (month 13) data is the same for both northern and southern hemispheres.

The format of the Groves data is the same as in Groves (1971) original report, except that a prefix code P, D, or T has been added at the front of each record. Each record contains the code, the month, the height in km and the 0, 10, 20, ... 90⁰ latitude values of the parameter expressed as a three digit integer, with an exponent common to all of the values on the record appearing at the end of the record. Thus a value of 276 with an exponent at the end of the record of -6, would be the same as $276 \times 10^{-6} = 2.76 \times 10^{-4}$. Pressure data are in units of nt/m², density values are in kg/m³, and temperatures are in ⁰K.

Stationary Perturbations

The stationary perturbations are latitude-longitude dependent relative perturbations to be applied to the Groves values, considered to be the longitudinal mean value. Data for each of 12 months and for the annual reference period (month 13) are given for the northern hemisphere latitudes. Southern hemisphere data are the same as the northern hemisphere values displaced by 16 months.

Each record contains the code S, the month, the height in km, the west longitude, in degrees, and then 15 values of stationary perturbations in per mill (%/10). The first five of the values are for pressure perturbations at latitudes 10, 30, 50, 70, and 90. The next five values are for density, and the last five values are for temperature. The monthly mean value y_m for parameter y at any latitude and longitude can be computed from the Groves value G_y at the latitude and the stationary perturbation s_y (in per mill) at the latitude and longitude by the relation

$$y_m = G_y (1 + s_y/1000) \quad (1)$$

Note that the stationary perturbation values at 90° latitude are always zero. However, there is a place for 90° values on the data tape, so that if a systematic departure from Groves values is desired at the poles, a set of stationary perturbation data reflecting this condition could be developed and put on the tape.

The Groves data and stationary perturbation data constitute the second file on the SCIDAT tape. An end of file marker appears at the end of the stationary perturbation data.

The Random Perturbation Data

Random perturbation magnitudes (standard deviations) are latitude dependent only. Each code R record has the code, the month (1-13) and the height in km, followed by 15 values of random perturbation magnitude, five for pressure (in per mill, at latitudes 10, 30, 50, 70, and 90), five for density, and five for temperature. These data give the relative standard deviations σ_p/p , σ_ρ/ρ , and σ_T/T , for use in the random perturbation model.

The code RW data are similar, except that only ten wind values appear in each record (after the code, month, and height): five for eastward wind magnitude (in m/s at latitudes 10, 30, 50, 70, and 90) and five for northward wind magnitude.

The code R and RW data constitute the third file on the SCIDAT tape. An end-of-file mark appears on the tape at the end of the code RW data.

The Quasi-Biennial Oscillation (QBO) Data

The QBO data consists of height and latitude dependent amplitudes and

phases for quasi-biennial variations in pressure (QP), density (QD), temperature (QT), and eastward and northward wind components (QU and QV, respectively). The amplitude of the QBO thermodynamic parameters are in per mill (%/10). The amplitudes of the QBO wind components are in decimeters per second (0.1 m/s). The phases of all of the QBO parameters are measured in days after January 0, 1966 for the occurrence of the first maximum value. Since the period of the QBO variations is taken to be 870 days, the phases could vary from 0 to 870.

Each QBO data record contains the code, the height in km, the amplitude and phase for 10° latitude, the amplitude and phase for 30° latitude, etc. out to the amplitude and phase for 90° latitude.

A final end of file mark appears at the end of the code QV data.

Appendix A gives a brief summary of the data on the SCIDAT tape and a complete listing of all the values appearing in the tape records.

4. THE INITIAL INPUT DATA

The initial input data consists of two free field (no set format with commas after each number) cards containing initial position data, program options, and other information required to begin computation, plus an optional third free field card to give initial random perturbation data if random perturbations are to be computed, plus an optional set of trajectory position data cards (followed by a backup card), if trajectory positions are to be read in rather than a linear profile generated automatically in the program. Appendix B gives a brief summary of the input characteristics, a summary of the data deck setup, and some sample input and output for the program. The following gives a more detailed description of each program input card.

Input Card Number 1

The first input card, read in by the main program segment PROFILE in free field format contains the following information. Designation R indicates real quantities, I denotes integer quantities.

1. Initial Height (R): The initial height in km for the beginning point of the profile or trajectory. This can be any non-negative real number. Atmospheric parameters are never evaluated at the first position, which is used only to establish the initial conditions. If the initial height is near the surface the program may not be able to compute atmospheric parameters at the first few heights. This happens when the surface at one or more adjacent 4-D grid points is higher than the surface at the initial position, so the interpolation between the 4-D grid positions can-

not be made. If the first height is below 30 km, care should be taken that subsequent positions do not go more than 15° of latitude or longitude away from the initial position while the height remains below 30 km. For normal ascent and re-entry trajectories this restriction will not pose any problem.

2. Initial Latitude (R): The latitude of the initial position in degrees, with southern latitudes negative. If the initial latitude, or any subsequent latitude is greater than 90° in absolute magnitude, then a transformation

$$\begin{aligned} \text{lat} &= (180^{\circ} - |\text{lat}|)(\text{lat}/|\text{lat}|) \\ \text{lon} &= \text{lon} + 180^{\circ} \end{aligned} \tag{2}$$

is made.

3. Initial West Longitude (R): The west longitude of the initial position in degrees. Each longitude can be put in as negative or converted to $0 - 360^{\circ}$ west longitude. If negative (east) longitudes are input they are converted to the $0-360^{\circ}$ scale before being used by the program. At any time during the run if a longitude gets outside the $0-360^{\circ}$ range it is put back into that range by adding or subtracting 360° , as necessary.

4. F10.7 (R): The solar 10.7 cm radio noise flux in units of 10^{-22} watts/m² (the normal units for this parameter) at the time for which the atmospheric values are to be computed. This factor is used only in the Jacchia section, so a value of zero can be used on input if the height never goes above 90 km. A value of 230 for both design steady state conditions and for maximum conditions may be used, or consult the Aerospace Environment Division (AED) of Marshall Space Flight Center (MSFC) for monthly predictions.

5. Mean F10.7 (R): The 81 day mean solar 10.7 cm radio flux. This parameter is used in the Jacchia section to compute the nighttime minimum global

exospheric temperature (equation (14) in Jacchia, 1970). Use zero if the height does not go above 90 km. A value of 230 may be used for both design steady state or maximum conditions, or consult the AED or MSFC for monthly predictions.

6. AP (R): The geomagnetic index a_p , used to compute a geomagnetic correlation to the exospheric temperature, in equation (22) of Jacchia, (1970). Use zero if the height does not go above 90 km. A design steady state value of 20.3 and a maximum condition value of 400 may be used for a_p , or consult the AED at MSFC for monthly predictions.

7-9. Date (I): The date, for the starting time of the trajectory or profile evaluation in month/day/two digit year form, as three integer input values. The day of the month and the year have no direct effect on the program calculations, except in the case of the quasi-biennial oscillation terms. For the annual reference period, use month 13. The quasi-biennial terms are automatically set to zero if month 13 is used. The month is used to establish which Groves data, stationary perturbation data, and random data to load from the SCIDAT data tape into the working arrays. The program will work more efficiently if multiple trajectories or profiles are evaluated during one run operation and the months are the same. (This avoids repeated look-up of the Groves, stationary perturbation, and random data from the SCIDAT tape).

10-12. Greenwich Time (I): The Greenwich mean time for the starting position in hours, minutes, and seconds, as three integer values. Only the Jacchia section is directly affected by the time of day, so unless the height goes above 90 km, the starting time would serve merely as a reference parameter for the particular run being done. Greenwich time corresponding to a local time of 0900 hours should be used for design steady state conditions, and for maximum conditions the local time should be taken as 1400 hours.

13. Latitude Increment (R): If a linear profile is to be generated automatically this is the latitude increment (in degrees) between successive profile positions. The new latitude would be the old latitude plus the latitude increment. For a profile with decreasing latitude (going southward) the increment must be negative. Use zero if separate trajectory position input is to be read in. If a vertical profile (i.e. changing only height) is to be evaluated, then use zero latitude increment.

14. West Longitude Increment (R): If a linear profile is to be generated automatically this is the west longitude increment (in degrees) between successive profile positions. The new longitude will be the old longitude plus the longitude increment. For a profile progressing eastward use a negative increment. Use zero if separate trajectory position input is to be read in. If a vertical profile is to be evaluated, then use zero increment.

15. Height Increment (R): The height decrease in km between successive positions, for an automatically generated linear profile. The profiles normally are generated downward (descending height). (New height = old height - height increment). If an upward generated profile is desired the height increment should be negative. Downward generated profiles will be evaluated until the height is incremented to a negative value or until the height becomes less than the surface height h_s which is the highest surface height of the four 4-D grid points being interpolated between (or until the maximum number of positions (item 16, 1st card) is exceeded). If the height is above sea level (i.e. > 0) but below the surface height h_s , then upward generated profiles will continue incrementing but will not output atmospheric parameter values until the height exceeds the surface height h_s .

16. Maximum Number of Positions (I): The maximum number of profile positions to be generated automatically. This does not include the initial

position, for which no atmospheric parameters are evaluated. Use zero if trajectory positions are to be read in.

17. Time Increment (I): The time displacement (seconds) between successive automatically generated profile positions. This would normally be set to zero, but could be used as a counter to be printed out in the time position with the output. For trajectories the time for each position is read in with the position data (see trajectory input section below). The hours, minutes, and seconds parameters (read in as items 10-12, 1st card) are updated according to the new time generated by the time increment. However, only the elapsed time in seconds is printed out on the present output.

18. Trajectory Option (I): This option tells the program whether a trajectory or a linear profile is to be evaluated. A value of 0 means a linear profile is to be generated automatically from the parameters read on the first card. A value greater than zero means that trajectory position data cards must be read in to determine the positions at which atmospheric parameters are to be evaluated.

19. Punch Option (I): This option tells the program whether or not to punch the atmospheric parameter output (see the output description section). Punched output is convenient to use as card input to plotter programs. A value of 0 means no punch output. A value greater than 0 means to punch the output.

With normal numbers of decimal places and no unnecessary blank spaces, the above 19 items should fit onto one card. However, if they occupy more

than the 80 columns allowed on one card, they may be spread out onto two cards if the following rule of UNIVAC 1108 free field input are observed on the first of the two cards: (1) Do not put a comma after the last number appearing on the first card. (2) If the last number on the first card is an integer, it should be right justified to column 80. For input on other computers, consult your operations manual for characteristics of free field input.

Input Card Number 2

The second input card is read in by the subroutine SETUP and contains various unit numbers to be used and options controlling the random and quasi-biennial calculations. The unit numbers are the parameters used in read statements in the FORTRAN program to control which file is being read from. The unit numbers are required in the input in order to give maximum flexibility in choice of I/O devices for the program. All input items on card number 2 are integers.

1. Groves Input Unit: This is the unit number of the SCIDAT tape file. If the SCIDAT tape has been assigned by the control statements -

```
@ ASG, T    SCIDAT, T, U1961 N
```

```
@ USE      3, SCIDAT
```

where U 1961 is the reel number for tape SCIDAT, then the Groves input unit number should be 3 on this input card. The Groves and Stationary perturbation data must be read from the SCIDAT tape. Later options on this card allow the NMC grid data, the random perturbation data, and the quasi-biennial data each to be read from other files.

2. Random Input Unit: This is the unit number for the random perturbation standard deviations. If this unit number is the same as the Groves input unit number, then the random perturbations are read from the SCIDAT data tape. Otherwise the random data is read from the file for whatever the unit number is set to. For card input, the unit number should be set to 5. The SCIDAT tape is read with NTRAN, but if alternate random data are read in from a different file, the file must be FORTRAN readable with format

1X, A1, I2, I4, 3(1X, 5I4)

for the random pressure, density, and temperature data (see Appendix A and Section 3 for which values must go in each record). For the random wind data the FORTRAN readable format for the alternate data is

1X, A2, I2, I4, 2(1X, 5I4)

Both random pressure, density, and temperature data and random wind data must be read in from the same file, either both from SCIDAT, or both from the alternate FORTRAN readable file.

3. QBO Input Unit: If the QBO data parameters are to be read in from the SCIDAT data tape, this unit number is set the same as the Groves input unit. If alternate QBO parameters are to be read in the QBO unit number can be any FORTRAN readable file. Use Unit 5 for card input. The format for all of the alternate QBO input is

1X, A2, I3, 5(I4, I5)

(See Appendix A and Section 3 for which data values must go into each record).

All of the QBO pressure, density, temperature, and wind data must be read from the same file, either all from SCIDAT or all from the alternate QBO input file.

4. 4-D Input Unit: This is the unit number for the 4-D data tape. Any available unit number can be used. If the 4-D tape WW1A, containing the January data, has been assigned by the control statements

```
@ ASG, T  WW1A, T, U 2400 N
```

```
@ USE    4, WW1A
```

then the 4-D input unit number is 4.

5. Random Option: This option tells the program whether or not to compute random perturbations. If the value is 1 random perturbations are computed. If the value is 2 then random perturbations are not computed. If any values other than 1 or 2 are input the run is terminated with a message "ERROR IN SETUP INPUT" and a dump of the parameters most recently read in.

6. QBO Option: This option tells the program whether or not to compute QBO perturbations. If the value is 1 QBO perturbations are computed. For 2 no QBO perturbations are computed, and for any other values the "ERROR IN SETUP INPUT" and dump of most recent parameters read in is given.

7. First Random Number: This number is required as a starting parameter for the random number generating subroutine RAND. Any odd positive integer can be used. Use a value of 1 for a standard design application run. Provided all other input is the same a given value for the starting random number will always produce the same random perturbation output.

Therefore, to get a set of different perturbations along a given single trajectory, a set of different starting random numbers should be used. Note, however, that if any other parameters are changed (different spacing along the trajectory, different starting position, etc.) then the same starting random number will produce a different set of random perturbations.

8. NMC Read Option: This option tells the program whether to read the NMC grid data from the SCIDAT data tape (value 0 for the option) or from an input card file (any non-zero value for the option).

9. 4-D Scratch Unit: In order to save array space the 4-D profiles required to interpolate to the $5^0 \times 5^0$ grid locations are read from the tapes to this scratch file rather than being put into arrays. The unit number for this scratch file can be any available unit. Normally the file is a temporary drum file, and, if so, does not have to be assigned (@ ASG) before execution of the program.

10. NMC Grid Point Scratch Unit: Also in order to save computer storage, the NMC grid point array read in from the SCIDAT tape (or from cards) is stored in a temporary scratch file (usually on drum). If the drum scratch file is used, it does not have to be assigned before execution of the program.

Input Card Number 3

This card is read by the SETUP subroutine and contains starting values for the random perturbation parameters at the initial position. If random perturbations are not to be computed (Random Option = 2), then this card should not be put in. All values on this free field format card are real.

For a normal design application the values on this card should all be zero, unless the run is to be a continuation of a previously run trajectory or profile segment, in which case the output random parameters of the last output position are input, and the last output position becomes the initial position of the new run.

1-3. Initial P, D, T: These are initial values of random relative pressure (p'/\bar{p}), density ($\rho'/\bar{\rho}$), and temperature (T'/\bar{T}) in percent. These are starting values for the initial position. Use zero for standard design applications.

4-6. Sigma P, D, T: These are initial values of relative standard deviations (in percent) for the random pressure (σ_p/\bar{p}), density ($\sigma_\rho/\bar{\rho}$), and temperature (σ_T/\bar{T}). Use zeros for standard design application runs. If zero values are input, the program looks up appropriate values for the initial height and latitude.

7-8. Initial U, V: Initial values of the random eastward and northward random wind components in m/s. Use zeros for standard design applications.

9-10. Sigma U, V: Initial values of the standard deviations (in m/s) for the eastward and northward random wind components. Use zeros for standard design application runs. If zero values are input, the program looks up the appropriate values for the initial height and latitude.

Trajectory Input

The free field trajectory position input and backup cards are put in only if a trajectory is to be evaluated, rather than a linear profile, generated automatically in the program from information on the first input

card. There is no limit to the number of trajectory positions which can be put in. The program continues evaluating the atmospheric parameters and looping back to read a new trajectory position until a position below the surface is reached (see Figure 1), or until the trajectory backup card is reached. Each free field trajectory card has the time (integer seconds), the height (kilometers), the latitude (degrees, southern latitude negative), and the west longitude (degrees, 0-360⁰ or east longitudes negative). Any east longitudes read in as negative values are converted to the 0-360⁰ system before being used by the program. The trajectory backup card has the same free field form as a regular trajectory card, except any negative value for height is used. The negative height terminates the loop which evaluates atmospheric parameters and reads a new trajectory card. If a trajectory height goes below the surface height h_s , then the remaining trajectory input cards are read and ignored. The surface height h_s is determined as the lowest height for which all four 4-D grid locations has non-zero data values required for interpolation to the trajectory position.

5. OUTPUT OF THE PROGRAM

The first few lines of print output are primarily a listing of the input parameters. Following a heading which describes each output value for the trajectory or profile evaluations, the position, time, monthly mean and total pressure, density, temperature, and winds are listed for each position. The thermal wind shear for the monthly mean winds, the percent deviation from the standard atmosphere (p , ρ , and T) and the perturbation data are also given for each position. The perturbation data consist of the stationary perturbations, the quasi-biennial values at the position and time, the quasi-biennial magnitudes, the random perturbation values, and the random perturbation standard deviations. Optional punch output for values at each position is also available to be used for card input to plotter programs, or for other purposes.

Heading Information

Primarily the heading information contains a listing of the input data values. However, there are some changes from the values input. If an east longitude is put in as a negative value, $-180^{\circ} < \text{lat} < 0^{\circ}$, then it is converted to a west longitude in the 0-360 range before the heading is listed. If zero values for the random pressure, density, temperature or wind standard deviations are input, then the program evaluates these from the data on the SCIDAT data tape, and lists the computed values on the heading. The Julian date is computed by the program from the input date and is also listed with the heading information. The Julian date is required by the

Jacchia and QBO sections of the program. If month 13 (annual reference period) is input, then the Julian date is set to zero. (The Jacchia section takes the exospheric temperature to be 1000° K and the QBO section is bypassed if month 13 is input).

Position and Time Output

Positions and times as generated by the automatic linear profile features or as input by the trajectory input cards are listed on the output. The time is given in seconds. Within the program, the input time in hours, minutes, and seconds are updated in that form also. However, only a continuously increasing time in seconds is printed out. If time in hours, minutes, and seconds were desired, these variables could easily be printed out by adding them to the output list. All output west longitudes are converted to the 0-360 range before being printed out. If a latitude greater than 90° in absolute magnitude is generated (or input) then a transformation

$$\begin{aligned} \text{lat} &= (180^{\circ} - |\text{lat}|)(\text{lat}/|\text{lat}|) \\ \text{lon} &= \text{lon} + 180^{\circ} \end{aligned} \tag{3}$$

is made.

Monthly Mean (and Thermal Wind Shear) Data

The monthly mean values of pressure, density, and temperatures, consist of either: (1) values from the 4-D data tapes if the height is below 25 km, (2) the sum of Groves plus stationary perturbation values if the height is between 30 and 90 km, (3) an interpolation between 4-D at 25 km and Groves plus stationary perturbations at 30 km if the height is between 25 and 30 km, (4) Jacchia model values if the height is above 115 km, and (5) faired val-

ues between Groves and Jacchia if the height is between 90 and 115 km.

The percent deviations from the U.S. 1962 Standard Atmosphere are evaluated by using standard atmosphere values computed by the subroutine STDATM. The percent deviations are evaluated by the relations $100(T - T_s)/T_s$, $100(\rho - \rho_s)/\rho_s$, and $100(p - p_s)/p_s$, where the subscript s refers to the standard atmosphere values. This subroutine accurately reproduces the tabulated U.S. Standard Atmosphere 1962 values to within an accuracy of better than 0.2% above 90 km. The STDATM values are based on a model of parabolic segments for the height variation of the molecular height above 90 km. The subroutine reproduces the tabular values even more accurately in the height region below 90 km, where the molecular weight is constant. Since the U.S. 1952 Standard Atmosphere is not defined above 700 km, the percent deviations printed out for heights above 700 km are zero.

The thermal wind shear values are values of $\partial u/\partial z$ and $\partial v/\partial z$ for the monthly mean geostrophic wind. The wind values, computed from the geostrophic wind equation, are determined by horizontal gradients of the monthly mean pressure. The thermal wind shear components, computed by the thermal wind equations, are determined by the horizontal gradients of the monthly mean temperature. Thus, a comparison of numerically differentiated geostrophic mean winds and the thermal wind shear serve as a check of the mean pressure and temperature fields (see Sections 7 and 10 of the technical discussion portion of this report).

The Total (Mean Plus Perturbation) Data

The parameter values listed under the heading of "Mean Plus Perturbations" are the monthly mean values, as defined above, plus the random pertur-

bations, plus (if the height is between 15 and 90 km) the quasi-biennial perturbations. These mean-plus-perturbation values represent values which would be typical "instantaneous" values of the pressure, density, temperature or winds. The percent deviations from the U.S. Standard atmosphere are computed in the same way as for the percent deviations of the monthly mean values from the standard atmosphere.

Perturbation Values

The data under the "Perturbation Values" heading are the various perturbation values, magnitudes, and amplitudes. The stationary perturbations (denoted SP on the printout) are defined only if the height is between 30 and 90 km. The monthly mean y_m of parameter y should be the Groves value G_y , evaluated from the SCIDAT data tape, modified by the given stationary perturbation value s_y , in percent by the relation

$$y_m = G_y (1 + s_y/100) \quad (4)$$

The data labeled "QBO" are the values of the QBO oscillation at the output time and position. The data labeled "MAG" gives the magnitude of the QBO oscillations at the output position and time. The QBO values should always be less than the magnitude values in absolute value. The data labeled "RAND" are the random perturbations evaluated at the output time and place. The data labeled "SIG" are the standard deviations of the random components at the output time and positions. According to the Gaussian distribution, on which the random perturbations are based, the perturbation values should be within the range $\pm \sigma$ 68% of the time and outside the range $\pm \sigma$ 32% of

the time. Similarly, the perturbation values should be within the range $\pm 2\sigma$ 95% of the time, and outside the range $\pm 2\sigma$ 5% of the time. The evaluation of the QBO and random perturbation output can be suppressed by the QBO and random options, if desired.

Punch Output

The punch output is available as an option, controlled by the input value of the punch option parameter. If punch output is desired, it comes out in the form of two cards for each position. The first, code "A", card contains the following information: (1) the time, in seconds, (2) the height in km, (3) the latitude in degrees, (4) the west longitude in degrees 0-360, (5-7) the mean monthly pressure, density, and temperature, (8-10) the percentage deviation of the mean monthly values of pressure, density, and temperature from the 1962 U.S. Standard Atmosphere, (11-12) the eastward and northward components of the monthly mean (geostrophic) wind, (13-14), the eastward and northward components of the mean wind shear. The format for the code "A" card is

I4, F5.1, 2F7.2, 2E8.3, F5.0, 3F5.1, 4F5.0, "A"

The second, code "B", card contains the following information: (1-4) the time, height, latitude, and longitude (same as on the code "A" card), (5-7) the total (monthly mean plus perturbation) values for pressure, density, and temperature, (8-10) the percent deviations of the total pressure, density, and temperature from the 1962 U.S. Standard Atmosphere, (11-12) the total (mean plus perturbation) values for the eastward and northward wind

components. The format for the code "B" card is

I4, F5.1, 2F7.2, 2E8.3, F5.0, 3F5.1, 2F5.0, 10X, "B".

6. PROGRAM DIAGNOSTICS

There are several possible reasons which can cause the printing of diagnostic messages and termination of the run during the SETUP phase. If, during the setup procedure, the NMC grid point number data table does not contain the required 1977 values, a message

Diagnostic 1: "N RECORDS WRITTEN BY GETNMC ON SCRATCH FILE M" is printed, and EXECUTION IS TERMINATED. This situation should only arise if the NMC grid point table is being read from cards, rather than the SCIDAT data tape. If during the reading of the SCIDAT data tape, any record is read which does not have the expected code character or characters (P, D, T, S, R, RW, QP, QD, QT, QU, or QV; see Appendix A), then the message results

Diagnostic 2: "ERROR IN SETUP INPUT" followed by a listing of the latest data values read in. This message is also produced if the random option and the quasi-biennial option do not have a value of either 1 or 2 (see Section 4). Any condition which results in this error message terminates the execution.

There are also general conditions which could result in diagnostic messages in the 4-D section: If during the reading of the 4-D data tape on the first access of the region below 30 Km, a parity error is encountered, a message

Diagnostic 3: "INPUT UNIT NO. M IN ERROR (-3) FOR RECORD NO N" is printed - execution continues. Such an error will only be of consequence if the particular record read is required for interpolation. If an end of file is read, a message is written

Diagnostic 4:

"* * * * * UNIT NØ. JT IN ERRØR IRC RECORDS READ

IREAD(IRN, 3) = XXXX MP = XX MØNTH = XX IP = XXXX IPT(I, J) = XXXX IRN = XX

M STATUS L"

Where

JT = Unit on which 4-D data tape is mounted

IRC = Total number of records read thus far from 4-D tape

IREAD(IRN, 3) = Sequential point number selected by SELEC4

MP = Month word in last record read

MØNTH = Run month

IP = Point number word in last record read

IPT(I, J) = Point number required for profile J to be interpolated
to Ith requested profile

IRN = Sequential point number required

M = Unit status (READ)

L = NTRAN status (-2 for end of file, -3 for parity, etc.)

and EXECUTIØN IS TERMINATED

If $IRC > IREAD(IRN, 3)$, the diagnostic message 4 is written - L should be 106, and IRC and IREAD values should indicate this condition. EXECUTIØN IS TERMINATED.

If $MP \neq MØNTH$, or $IP \neq IP(I, J)$ the diagnostic message 4 is printed, again with L = 106, and MP/MØNTH or IP/IP(I, J) indicating error. EXECUTIØN IS TERMINATED.

The writing of scratch file SCRCHI with data for subsequent unpacking and interpolation is also checked. If there is a write error, the diagnostic

4 is printed, with JT the scratch file unit number, M as WRITE and L as -3 or -4. EXECUTION IS TERMINATED.

These diagnostics can arise if a bad or wrong 4-D data tape is being accessed, or if there is a malfunction of the tape drive. In some cases a tape will, for example, indicate parity errors when being read from one tape drive, but not another.

If, during the course of evaluation of position in the 4-D height range, it is found that the position is outside the previously established 4-D grid, then a message results

Diagnostic 5: "POSITION OUTSIDE 4-D GRID"

The 4-D grid is either a polar grid between 75° N or S of the pole, or a non-polar 16 point grid at $5^{\circ} \times 5^{\circ}$ latitude spacing. If the position is less than 5° (total latitude and longitude) outside the 4-D grid (i.e. $|\text{latitude}| < 70^{\circ}$ for the polar grid, or $(\Delta\text{lat}^2 + \Delta\text{lon}^2)^{1/2} < 5^{\circ}$ for the non-polar grid), then the atmospheric parameters are evaluated by extrapolation or setting them equal to the nearest grid point. If the position is more than 5° outside the 4-D grid, then no evaluation is made and printed out, however execution does continue to cycle to subsequent positions, in hopes of finding valid positions for evaluation.

A diagnostic message

Diagnostic 6: "CORRELATION COEFFICIENT ERROR"

indicates that the correlation parameter $E^2 < 0$, as computed by equation (B10) from Appendix B of the technical description section of this report. If this occurs, E is set to zero and execution continues. The numbers listed

following diagnostic 6 are values of various correlation parameters. Consult a listing of subroutine PERTRB for their meaning.

B. PROGRAMMERS MANUAL

1. DESCRIPTION OF SUBROUTINES

The following is a brief description of each of the PROFILE program subroutines, in alphabetical order:

- CORR: Evaluates the correlation between density and temperature from a set of linear segments approximating the curve from NASA-TM X-64589. These values are used as default values if the correlation value computed directly from the variances on the 4-D data tape has a magnitude greater than 1.
- DXHLVL: Evaluates the horizontal and vertical correlation scales from equations plotted in Figure 8.3 of the technical description section of this report.
- FAIR: Fairs between the Groves and Jacchia values in the 90 to 115 km height range. (See equation 5.8, technical description section)
- GEN4D: Generates the polar ($|\text{latitude}| > 75^\circ$) or non-polar ($16 5^\circ \times 5^\circ$ points) grid of pressure, density, temperature and variance profiles. See Figure 3 for a flow chart of this subroutine.
- GETNMC: Reads the NMC grid point values from the SCIDAT data tape or from cards and loads them onto a scratch file. This subroutine is essentially unchanged from the subroutine of the same name in the original 4-D program.
- GRID4D: After array of 4-D grid lat-lons has been evaluated, this subroutine looks up the data from the 4-D data tapes and interpolates to determine profiles of pressure, density, temperature, and variance at the 4-D grid locations. Profiles to be interpolated to 4-D grid locations are loaded onto a scratch file from the tapes before the interpolation is done.
- GTERP: Uses linear latitude interpolation and linear temperature and

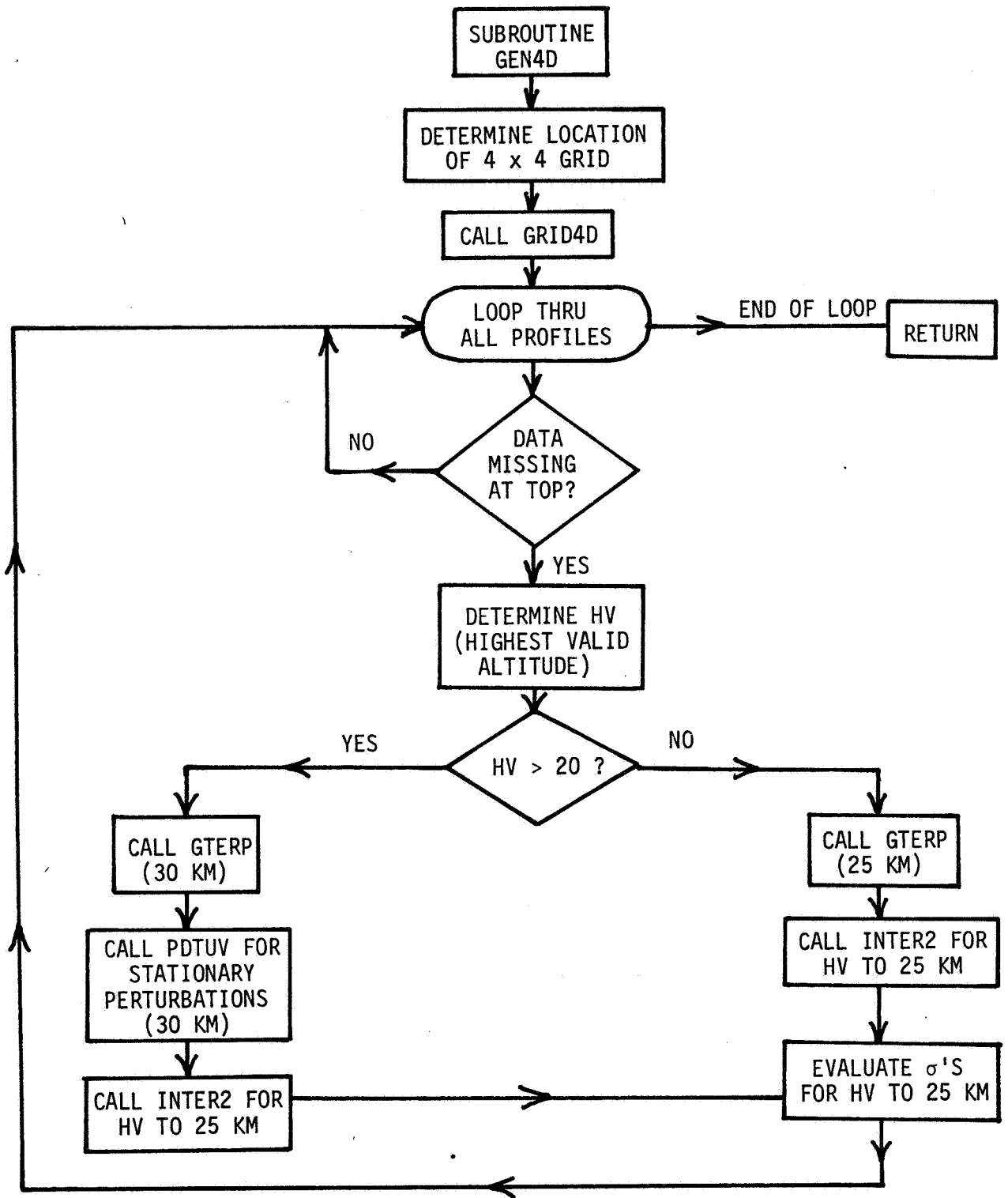


Figure 3: Simplified flow chart of the GEN4D subroutine.

linear logarithm of density interpolation on height to evaluate Groves data to a given latitude and height. See Section 5 of the technical description section.

INTERW: Two variable linear interpolation between known value U1 and V1 at Z1 and U2 and V2 at Z2 to determine U and V at Z, where Z is between Z1 and Z2.

INTERZ: Three variable interpolation, linear on temperature, and gas constant ($R = p/\rho T$), and linear on the logarithm of pressure, with pressure computed from perfect gas law and interpolated temperature and density, and gas constant. See Section 5 of the technical description section.

INTER2: Three variable interpolation, linear on all three variables.

INTER4: Interpolates between the pressure, density, and temperature profiles at the 4-D grid locations. This subroutine calls subroutine INTLL to do the latitude interpolation.

INTLL: One variable interpolation between values in an array of latitude and longitude locations by equation (5.6) of the technical description section.

INTRP4: The subroutine for the latitude-longitude interpolation of values from the 4-D data tapes into the 4-D grid array. This is a modification of the INTERP subroutine of the original 4-D program.

INTRUV: Evaluates the standard deviations of the random wind components at given height and latitude by calling INTERW subroutine.

JAC: Calculates the molecular weight, density, and temperature for the Jacchia model.

JACCH: Main subroutine of the Jacchia section, serves as a driver for JAC and the other Jacchia section subroutines. JACCHIA also evaluates the seasonal and latitudinal variations in the lower thermosphere.

- NORMAL:** Computes two independent random numbers selected from a Gaussian distribution with mean zero and unit standard deviation.
- PDTUV:** Interpolates the stationary perturbations on latitude and longitude at a given height. This subroutine is similar to INTLL.
- PERTRB:** Evaluates the pressure, density, temperature and wind component random perturbations by the correlated random perturbation model discussed in Section 8 of the technical description section of the report.
- PROFIL:** The main segment of the PROFILE program. The main segment serves as a driver for the SETUP and SCIMOD subroutines. See Figure 1 in the users manual section.
- QBOGEN:** Computes the QBO perturbation values and their amplitudes and phases. The amplitudes and phases of the QBO pressure, density, temperature, and wind perturbations are interpolated from the amplitude and phase data from the SCIDAT data tape, by calling the INTERZ and INTERW subroutines.
- RAND:** Produces a random number selected from a uniform distribution between 0 and 1. This is required as input to the subroutine NORMAL.
- RIG:** Computes the acceleration of gravity and the radius from the center of the Earth for a position at a given latitude and height.
- RTERP:** Computes the standard deviations of the random pressure, density, and temperature perturbations by calling subroutine INTERZ.
- RTRAN:** This subroutine contains several NTRAN read sections with multiple entry points coming from subroutine SETUP. The NTRAN read statements are for reading the SCIDAT data tape.
- SCIMOD:** The heart of the PROFILE program. This subroutine branches on height to evaluate the atmospheric parameters by the Jacchia,

the modified Groves, or the 4-D methods. The QBO and random perturbations are also evaluated and the output is printed (and optionally also punched) by the SCIMOD subroutine. See Figure 4 for a flow chart of the SCMOD subroutine and Figure 1, in the users manual section, for a flow chart showing how SCIMOD fits into the overall PROFILE program.

- SELEC4: Selects the 4-D data needed for interpolation. This subroutine is a modification of the INPUT subroutine of the original 4-D program.
- SETUP: This subroutine reads in the NMC grid points with the GETNMC subroutine and reads and loads the data from the required month on the SCIDAT data tapes into arrays. See Figure 5 for a flow chart of the SETUP subroutine, and Figure 1 for a flow chart showing how SETUP fits into the overall PROFILE program.
- SORT4: Sorts the 4-D locations for sequential tape reading from the 4-D data tapes. This subroutine is a modification of the SORT subroutine from the original 4-D program.
- STDATM: Evaluates the 1962 U.S. Standard Atmosphere values of pressure, density, and temperature, at any given height up to 700 km.
- TINF: This subroutine computes the exospheric temperature for the Jacchia model.
- TME: This subroutine calculates the variables necessary for input into the subroutine TINF in the Jacchia model.

If the PROFILE program is mapped without segmenting the program, it requires slightly less than 32 K core storage. In order to take up less core storage (e.g. to make room for further program additions), the program can be mapped in segmented form. An efficient segmentation of the program can be accomplished by subdividing the program into a primary segment, a setup segment, a Jacchia segment, and a 4-D segment. The primary segment should con-

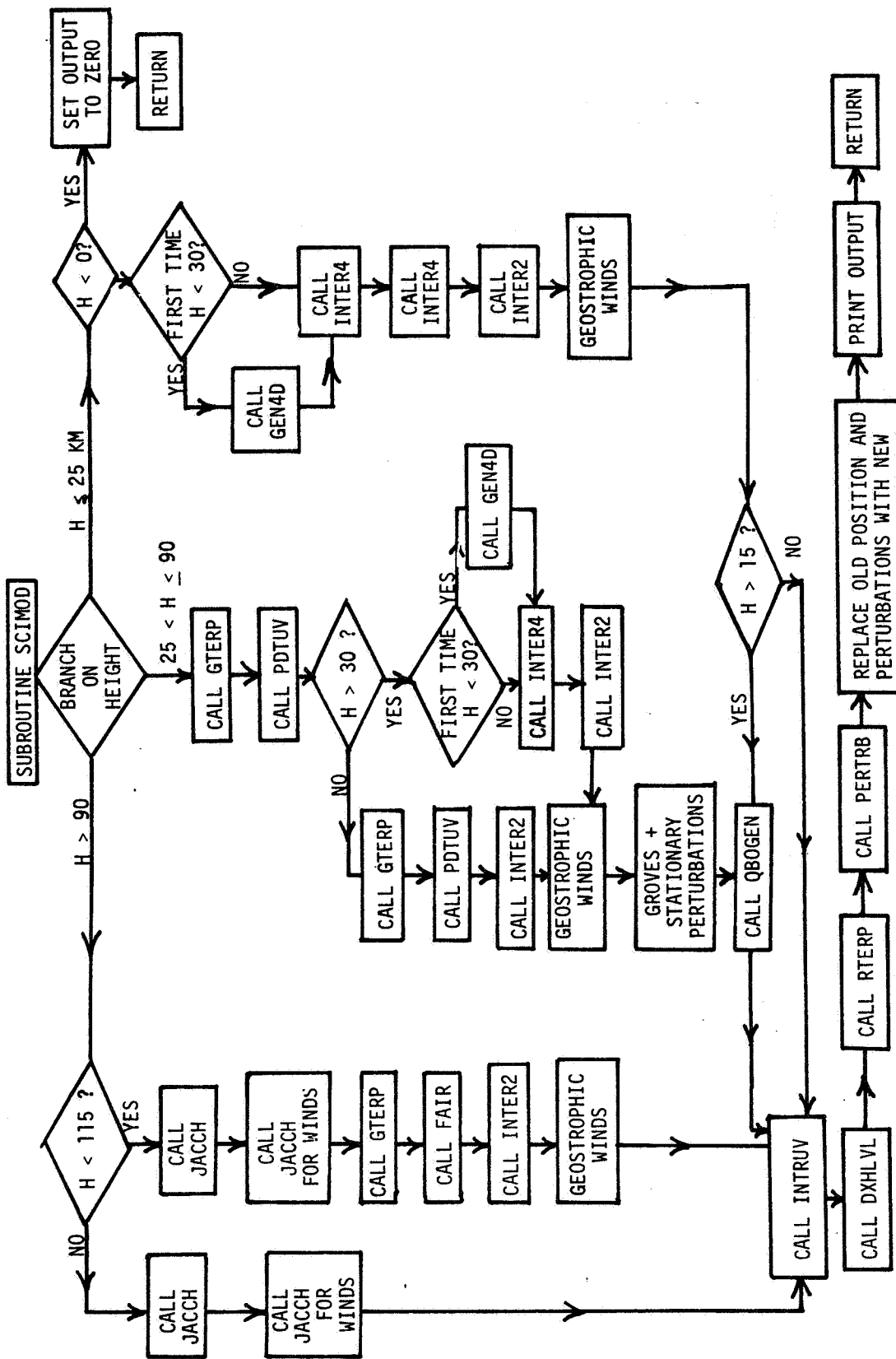


Figure 4: An abbreviated flow chart of the SCIMOD subroutine.

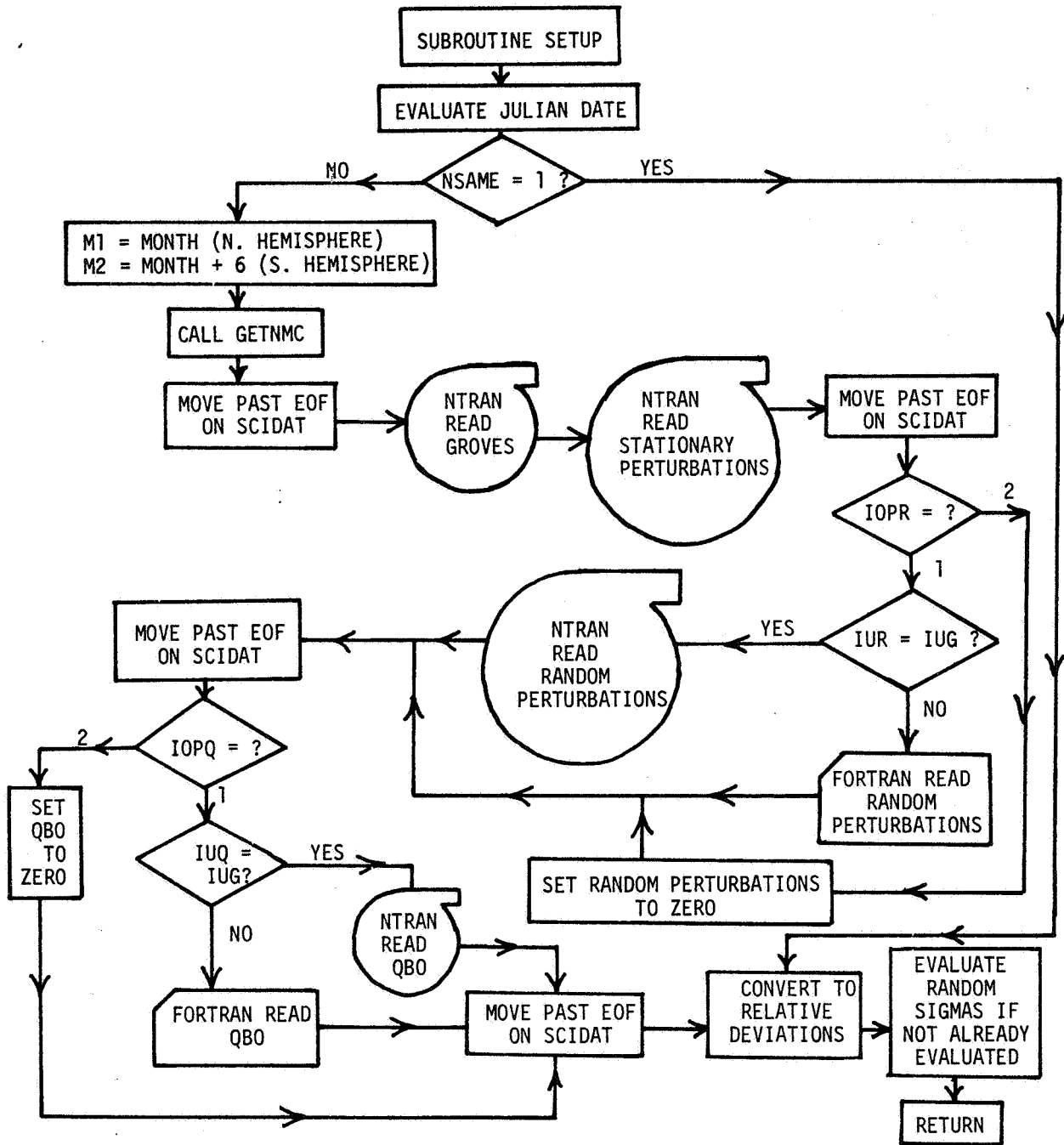


Figure 5: Abbreviated flow chart of the SETUP Subroutine.

tain CORR, DXHLVL, GTERP, INTERW, INTERZ, INTER2, INTRUV, NORMAL, PDTUV, PERTRB, PROFIL, QBOGEN, RAND, RIG, RTERP, SCIMOD, and STDATM. The setup segment should contain: GETNMC, RTRAN, and SETUP. The Jacchia segment should contain: FAIR, JAC, JACCH, TINF, and TME. The 4-D segment should contain: GEN4D, GRID4D, INTER4, INTLL, INTRP4, SELEC4, and SORT4. The following MAP statement for file PROFILE, to create absolute element ABS will accomplish the mapping of the program with these segments setup as described:

```

@MAP, IS      , PRØFILE. ABS
  IN PROFILE. CORR, . DXHLVL, . GTERP, . INTERW, . INTERZ
  IN PROFILE. INTER2, . INTRUV, . NORMAL, . PDTUV, . PERTRB
  IN PROFILE. PROFIL, . QBOGEN, . RAND, . RIG, . RTERP
  IN PROFILE. SCIMOD, . STDATM
  NOT TPF$
  SEG SETUP*
  IN PROFILE. GETNMC, . RTRAN, . SETUP
  NOT TPF$
  SEG JACCH*, SETUP
  IN PROFILE. FAIR, . JAC, . JACCH, . TINF, . TME
  NOT TPF$
  SEG SEG4D*, SETUP
  IN PROFILE. GEN4D, . GRID4D, . INTER4, . INTLL, . INTRP4
  IN PROFILE. SELEC4, . SORT4
  NOT TPF$
  END

```

This segmented map saves approximately 4 K in core storage, but does not significantly affect run time, since the segments being overlaid (the setup, Jacchia, and 4-D segments) only have to be loaded in once during any given trajectory or profile evaluation.

Some characteristics of some of the subroutines in each of these segments are described more fully in the following sections.

2. THE PRIMARY SECTION

This section consists of the main program segment PROFIL, the SCIMOD subroutine, the subroutines for evaluating Groves values, the stationary perturbations, the QBO and random perturbations, and general interpolation subroutines. With the exception of PROFIL and SCIMOD the parts of this section were adequately described in the previous section.

Many of the subroutines transfer their input and output via COMMON statements. This procedure saves much in core storage space. The discussion in this and subsequent sections describes the input and output of some of the subroutines, both by argument lists and via COMMON statements.

Main Segment PROFIL

This program serves as a driver for the SETUP and SCIMOD subroutines (see Figure 1 in the users manual section). It reads one card, the first input card, in free field format. This card contains:

1. The initial height	H1
2. The initial latitude (degrees)	PHI1
3. The initial west longitude (degrees)	THET1
4. The F10.7 solar flux	F10
5. The 81 day mean F10.7 solar flux	F10B
6. The a_p geomagnetic index	AP
7-9. The date month/date/2 digit year	MN/IDA/IYR
10-12. The Greenwich time hours: minutes: seconds	IMRO; MIN0; ISECO
13-15. The latitude, longitude, and height increments	DPHI, DTHET, DH
16. The maximum number of profile positions	NMAX
17. The time increment between profile positions	INCT
18. The trajectory option	IOPT
19. The punch option	IOPP

The trajectory input cards (if used) are also read by PROFIL, after control has returned from SETUP, which reads the second and third initial data input cards. See Section 4 of the users manual section and Appendix B for further description of the card input.

The COMMON "IOTEMP" transfers data from the card input in PROFIL to the other subroutines called by PROFIL (SETUP, SCIMOD, and RIG).

Subroutine SCIMOD

This program is the primary subroutine of the PROFILE program. It serves as a driver for all of the various sections of the atmospheric evaluation. See Figure 4 for a flow chart of this subroutine.

The input to SCIMOD, transferred by COMMON statements IOTEMP and PDTCOM, is:

1. Acceleration of gravity (m/sec ²)	G
2. Earth radius to height H (km)	RI
3. Height (km)	H
4. Latitude (Radians)	PHIR
5. Longitude (radians)	THETR
6. F10.7 solar flux	F10
7. Mean F10.7 solar flux	F10B
8. Geomagnetic index a_p	AP
9-11. Date	MN/IDA/IYR
12-14. Time	IHR: MIN: ISEC
15. Previous height (km)	H1
16. Previous latitude (radians)	PH1R
17. Previous longitude (radians)	TH1R
18-20. Previous random pressure, density, and temperature perturbations (%)	RP1, RD1, RT1
21-23. Previous random pressure, density, and temperature standard deviations (%)	SP1, SD1, ST1

24-25.	Previous random winds (m/s)	RU1, RV1
26-27.	Previous standard deviation of random winds (m/s)	SU1, SV1

The COMMON "PDTCOM" contains data transferred into SCIMOD from SETUP. The COMMON "IOTEMP" transfers data in from PROFIL. The COMMON "C4" transfers data out to the 4-D section of the program. The COMMON "COMPER" transfers data out to the random perturbation subroutines.

The present SCIDAT data tape has the random wind component standard deviation arrays (UR and VR) equal. In order to save space in core, these arrays were equivalenced in SCIMOD. If a subsequent SCIDAT tape is generated with different random wind standard deviation components, then the equivalence statement

```
EQUIVALENCE (UR (1, 1), VR (1, 1))
```

should be removed and the array VR (25, 10) added to the COMMON list "PDTCOM". Similar corrections are also required in subroutine SETUP.

The SCIMOD subroutine prints and (optionally) punches the output described in the users manual section and in Appendix B. It also transfers output to other subroutines via the above-mentioned COMMON lists. The SCIMOD subroutine updates the profile or trajectory positions by setting the current position equal to the previous position before exit. The previous position information then stays in the COMMON list until the next call to SCIMOD. The previous random perturbations are handled in similar fashion.

3. THE SETUP SECTION

The function of the setup section of the program is to load the initial data and the data from the SCIDAT tape. See Figure 1 for a flow chart illustrating how the SETUP subroutine fits into the overall program and Figure 4 for a flow chart of the SETUP subroutine.

The SETUP subroutine reads the second and third cards of input. The second card contains

1. Groves input unit	IUG
2. Random input unit	IUR
3. QBO input unit	IUQ
4. 4-D input unit	IU4
5. Random option	IOPR
6. QBO option	IOPQ
7. First random number	NR1
8. NMC read option	NMCOP
9. 4-D scratch unit	IOTEM1
10. NMC grid point scratch unit	IOTEM2

The third card (optional, read only if IOPR = 1) contains:

1-3. Initial random perturbations in pressure, density, and temperature (%)	RP1, RD1, RT1
4-6. Initial standard deviations for random pressure, density, and temperature (%)	SP1, SD1, ST1
7-8. Initial random wind perturbation (m/s)	RU1, RV1
9-10. Initial standard deviations for random winds (m/s)	SU1, SV1

The COMMON list "PDTCOM" transfers the arrays, loaded with the appropriate data from the SCIDAT data tape, to the other subroutines. This COMMON list contains the following arrays:

1-3. Groves pressure, density, and temperature	PG, DG, TG
--	------------

4-6. Stationary perturbations in pressure, density,	PSP, DSP, TSP
7-11. Amplitudes of QBO pressure, density, and temperature	PAQ, DAQ, TAQ, UAQ, VAQ
12-16. Phases of QBO pressure, density, and temperature, and winds	PDQ, DDQ, TDQ, UDQ, VDQ
17.21. Standard deviations for the random pressure, density, temperature and winds (UR = VR equivalence)	PR, DR, TR, UR, VR

The COMMON list "COTRAN" is used to transfer data to SETUP from the NTRAN read subroutine RTRAN, which has multiple entry points for various different types of data from the SCIDAT data tape.

4. THE JACCHIA SECTION

The subroutine JACCH calculates the pressure, density, and temperature at a point in space for heights above 90 km for a particular time.

The inputs to JACCHIA are:

1. height in km	H
2. latitude in radians	PHIR
3. West longitude in degrees (0 to 360 degrees)	THET
4. solar radio noise flux F10.7 (10^{-22} watts/m ²)	F10
5. 81 - day average solar flux F10.7	F10B
6. geomagnetic index a_p	AP
7. month	MN
8. day of month	IDA
9. year	IYR
10. hour of day in universal time	IHR
11. minute of hour in universal time	MIN
12. mean Julian day	XMJD

The outputs are:

1. pressure in units of nt/m ²	PH
2. density in units of kg/m ³	DH
3. temperature in Kelvin degrees	TH

The theory and methods used in JACCH for calculating the pressure, density, and temperature are given in Jacchia, (1970). A brief explanation will be given below.

The subroutine JACCH consists of four sections: the main routine and three imbedded subroutines. All sections have numerous comments to explain each part of the program.

Main Routine (JACCH)

The main routine acts as the calling routine and, also, calculates the seasonal - latitudinal variations in the lower thermosphere.

The seasonal - latitudinal density variations are given by equation (2.1) of the technical description section.

The equations for the molecular weight and the relative temperature were given as equations (2.2) and (2.3) of the technical description section.

After the density, temperature, and molecular weight are calculated, the pressure is calculated from the ideal gas law:

$$p = \frac{\rho RT}{M}$$

where ρ is the density, R is the universal gas constant, T is the temperature, and M is the molecular weight.

An option is included in the main routine whereby the yearly mean values of the density, pressure, and temperature may be calculated directly. If the value of the month input variable is thirteen, ($MN = 13$), the exosphere temperature is immediately set equal to 1000° K (which is the recommended design value for annual mean conditions) and the yearly mean density, pressure, and temperature values are calculated. Note that the 1962 U.S. Standard Atmosphere has an exospheric temperature of approximately 1500° K and is thus considerably different from the 1000° K results of the annual mean in the PROFILE program.

Subroutine TME

This subroutine calculates variables necessary for input into the subroutine TINF. The input variables are:

1. month (month = 13 denotes annual mean and bypasses this subroutine) MN
2. day of month IDA
3. year IYR

- | | |
|---|-------|
| 4. hour of day in universal time | IHR |
| 5. minute of day in universal time | MIN |
| 6. mean Julian day | XMJD |
| 7. latitude in radians | XLAT |
| 8. longitude in degrees (input: 0 to 360 degrees
turning westward; output: -180 to +180 degrees) | XLONG |

The output variables are:

- | | |
|---|-----|
| 1. solar declination angle in radians | SDA |
| 2. solar hour angle in radians | SHA |
| 3. day number from January 1 | DD |
| 4. day number divided by tropical year
(365.2422 days) | DY |

Subroutine TINF

This subroutine calculates the exospheric temperature. The input variables are:

- | | |
|---|------|
| 1. solar radio noise flux (10^{-22} watts/m ²) | F10 |
| 2. 81 - day average F10 | F10B |
| 3. geomagnetic latitude in radians | XLAT |
| 4. solar declination angle | SDA |
| 5. solar hour angle | SHA |
| 6. day number divided by tropical year | DY |
| 7. diurnal factor equal to 0.31 | R |

The output is the exospheric temperature, TE. Factors included in the calculation of the exospheric temperature are solar activity variations, diurnal variations, variations with the geomagnetic activity, and semi-annual variations.

Subroutine JAC

This subroutine calculates the molecular weight, density, and temperature without the seasonal - latitudinal variations. The input variables are:

1. height in km
2. exospheric temperature

Z
T

The output variables are:

1. temperature
2. molecular weight
3. density

TZ
EM
DENS

5. THE 4-D SECTION

GRID4D and subroutines SØRT4, INTRP4 and SELEC4 are basically the MAIN PROGRAM, SØRT, INTERP and INPUT as documented in the 4-D users reference manual and subsequent updates.

Some changes have been made.

Statement numbers have been ordered in GRID4D and SØRT4.

In GRID4D, NTRAN MØVE statements are used to select the appropriate file for a given month on the 4-D data tape mounted on UNIT IT.

If a parity error is encountered in reading IT, a message

"INPUT UNIT NO. IT IN ERRØR FØR RECORD NØ IRC"

is printed - execution continues. Such an error will only be of consequence if the particular record read in error is required for interpolation.

Grid point profiles for subsequent interpolation are tagged and filed on a dynamically assigned scratch UNIT SCRCH1 (IØTEM1 in calling program), instead of occupying core as in the 4-D model.

Any error in the handling of the 4-D data tape or UNIT SCRCH1 (IØTEM1 in calling program) by GRID4D which results in a transfer to

STATEMENT NO. 30

is fatal, and results in the printing of an error message and termination of execution (see user's manual).

Slight changes have been made to the logic of SØRT4 in the interests of efficiency.

SELEC4 is concerned only with the selection of the record numbers of the appropriate interpolation profiles.

GETNMC has been added to file the NMC grid point data, read either from cards of the SCIDAT data tape on UNIT IUG, on a dynamically assigned scratch file SCRCH2 (IØTEM2 in calling program), instead of occupying 1977 words of core as in the 4-D model. If other than 1977 records are filed, an error message

"N RECORDS WRITTEN BY GETNMC ON SCRATCH FILE M"

is printed and execution terminated.

INTRP4 uses a modified latitude - longitude interpolation scheme in the mixed NMC - equatorial, equatorial and southern hemisphere regions.

The dimensions of some variables have been altered in keeping with the maximum number of profiles to be used in interpolation (16 instead of 25 as in the 4-D model), and to provide the index word for each record on SCRCH1 (IN (107) instead of (106)).

All references to, and subroutines associated with, the determination of the coefficients of the best fit polynomials to the selected profiles, as performed in the original 4-D model, have been deleted. All vertical interpolations required are performed by SCIMØD.

APPENDIX A

LISTING OF THE DATA TAPE "SCIDAT" FOR THE PROFILE PROGRAM

The tape contains the following data, identified by code characters at the beginning of each record. Month 13 refers to annual mean values. For code P, D, T, S, R, and RW data, southern latitude are given by northern hemisphere data displaced six months. Annual mean data and the QBO parameters are the same for both southern and northern hemispheres. For a more complete discussion of the input data, see Section 2 of the Users Manual.

<u>Code</u>	<u>Data</u>	<u>Description</u>
None	NMC Grid Data	Same as NMC Grid Required by NASA version 4-D program. Data consists of sequential point number followed by the two corresponding NMC grid indices. There are five points per record on the tape.
P	Groves Pressure (nt/m^2)	Month, height, values at latitudes 0, 10, 20, ... 90 exponent. Same format as in Groves report.
D	Groves Density (kg/m^3)	
T	Groves Temperature ($^{\circ}\text{K}$)	
S	Stationary Perturbations in monthly means (per mill)	Month, height, longitude, Δp at north latitude, 10, 30, 50, 70, 90, Δp same, ΔT same.
R	Random pressure, density, and temperature perturbation magnitudes (per mill)	Month, height, Δp at north latitude 10, 30, 50, 70, 90, Δp same, ΔT same
RW	Random magnitudes wind perturbation (m/s)	Month, height, Δu at north latitude 10, 30, 50, 70, 90, Δv same

<u>Code</u>	<u>Data</u>	<u>Description</u>
QP	QBO pressure parameters - amplitude (per mill) and phase (days after Jan. 0, 1966 when 1st maximum occurs)	Height, amplitude and phase at 10 ⁰ latitude, amplitude and phase at 30 ⁰ , ... , amplitude and phase at 90 ⁰ .
QD	QBO density parameters (as in QP)	
QT	QBO temperature parameters	
QU	QBO eastward wind parameters - amplitude (0.1 m/s) and phase (days after Jan. 0, '66)	
QV	QBO northward wind parameters - (as in QU)	

The tape consists of four NTRAN readable files with an NTRAN end of file after each file. The first file contains the NMC grid data, the second contains the Groves and stationary perturbation data, the third contains the random perturbation data, and the fourth contains the QBO data. The number of words per NTRAN record is 15 for the NMC grid data. Each record contains NMC grid x-y coordinates for 5 points. The total number of NMC grid points is 1977. The NMC grid data file contains a total of 395 records, with the last record containing points 1976 and 1977 and zeros in the remaining words. There are 14 words per record for the Groves data (including the code word), 19 for the stationary perturbations, 18 for the code R data, 13 for the code RW data, and 12 for the quasi-biennial data. The Groves data contains 702 records, the stationary perturbation data contains 1248 records, the code R random data contains 260 records, the code RW random winds data contain 325 records, and the QBO data contain 80 records.

Following is a listing of the data contained on the SCIDAT tape.

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ORIGINAL PAGE IS POOR

NMC GRID DATA, ()*

1	15	1	2	16	1	3	17	1	4	18	1	5	19	1
6	20	1	7	21	1	8	22	1	9	23	1	10	24	1
11	25	1	12	26	1	13	27	1	14	28	1	15	29	1
16	30	1	17	31	1	18	32	1	19	33	1	20	14	2
21	15	2	22	16	2	23	17	2	24	18	2	25	19	2
26	20	2	27	21	2	26	22	2	29	23	2	30	24	2
31	25	2	32	26	2	33	27	2	34	28	2	35	29	2
36	30	2	37	31	2	38	32	2	39	33	2	40	34	2
41	13	3	42	14	3	43	15	3	44	16	3	45	17	3
46	18	3	47	19	3	48	20	3	49	21	3	50	22	3
51	23	3	52	24	3	53	25	3	54	26	3	55	27	3
56	28	3	57	29	3	58	30	3	59	31	3	60	32	3
61	33	3	62	34	3	63	35	3	64	12	4	65	13	4
66	14	4	67	15	4	68	16	4	69	17	4	70	18	4
71	19	4	72	20	4	73	21	4	74	22	4	75	23	4
76	24	4	77	25	4	78	26	4	79	27	4	80	28	4
81	29	4	82	30	4	83	31	4	84	32	4	85	33	4
86	34	4	87	35	4	88	36	4	89	11	5	90	12	5
91	13	5	92	14	5	93	15	5	94	16	5	95	17	5
96	18	5	97	19	5	98	20	5	99	21	5	100	22	5
101	23	5	102	24	5	103	25	5	104	26	5	105	27	5
106	28	5	107	29	5	108	30	5	109	31	5	110	32	5
111	33	5	112	34	5	113	35	5	114	36	5	115	37	5
116	10	6	117	11	6	118	12	6	119	13	6	120	14	6
121	15	6	122	16	6	123	17	6	124	18	6	125	19	6
126	20	6	127	21	6	128	22	6	129	23	6	130	24	6
131	25	6	132	26	6	133	27	6	134	28	6	135	29	6
136	30	6	137	31	6	138	32	6	139	33	6	140	34	6
141	35	6	142	36	6	143	37	6	144	38	6	145	9	7
146	10	7	147	11	7	148	12	7	149	13	7	150	14	7
151	15	7	152	16	7	153	17	7	154	18	7	155	19	7
156	20	7	157	21	7	158	22	7	159	23	7	160	24	7
161	25	7	162	26	7	163	27	7	164	28	7	165	29	7
166	30	7	167	31	7	168	32	7	169	33	7	170	34	7
171	35	7	172	36	7	173	37	7	174	38	7	175	39	7
176	8	8	177	9	8	178	10	8	179	11	8	180	12	8
181	13	8	182	14	8	183	15	8	184	16	8	185	17	8
186	18	8	187	19	8	188	20	8	189	21	8	190	22	8
191	23	8	192	24	8	193	25	8	194	26	8	195	27	8
196	28	8	197	29	8	198	30	8	199	31	8	200	32	8
201	33	8	202	34	8	203	35	8	204	36	8	205	37	8
206	38	8	207	39	8	208	40	8	209	7	9	210	8	9
211	9	9	212	10	9	213	11	9	214	12	9	215	13	9
216	14	9	217	15	9	218	16	9	219	17	9	220	18	9
221	19	9	222	20	9	223	21	9	224	22	9	225	23	9
226	24	9	227	25	9	228	26	9	229	27	9	230	28	9
231	29	9	232	30	9	233	31	9	234	32	9	235	33	9
236	34	9	237	35	9	238	36	9	239	37	9	240	38	9
241	39	9	242	40	9	243	41	9	244	6	10	245	7	10
246	8	10	247	9	10	248	10	10	249	11	10	250	12	10
251	13	10	252	14	10	253	15	10	254	16	10	255	17	10
256	18	10	257	19	10	258	20	10	259	21	10	260	22	10
261	23	10	262	24	10	263	25	10	264	26	10	265	27	10

266	28	10	267	29	10	268	30	10	269	31	10	270	32	10
271	33	10	272	34	10	273	35	10	274	36	10	275	37	10
276	38	10	277	39	10	278	40	10	279	41	10	280	42	10
281	5	11	282	6	11	283	7	11	284	8	11	285	9	11
286	10	11	287	11	11	288	12	11	289	13	11	290	14	11
291	15	11	292	16	11	293	17	11	294	18	11	295	19	11
296	20	11	297	21	11	298	22	11	299	23	11	300	24	11
301	25	11	302	26	11	303	27	11	304	28	11	305	29	11
306	30	11	307	31	11	308	32	11	309	33	11	310	34	11
311	35	11	312	36	11	313	37	11	314	38	11	315	39	11
316	40	11	317	41	11	318	42	11	319	43	11	320	4	12
321	5	12	322	6	12	323	7	12	324	8	12	325	9	12
326	10	12	327	11	12	328	12	12	329	13	12	330	14	12
331	15	12	332	16	12	333	17	12	334	18	12	335	19	12
336	20	12	337	21	12	338	22	12	339	23	12	340	24	12
341	25	12	342	26	12	343	27	12	344	28	12	345	29	12
346	30	12	347	31	12	348	32	12	349	33	12	350	34	12
351	35	12	352	36	12	353	37	12	354	38	12	355	39	12
356	40	12	357	41	12	358	42	12	359	43	12	360	44	12
361	3	13	362	4	13	363	5	13	364	6	13	365	7	13
366	8	13	367	9	13	368	10	13	369	11	13	370	12	13
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396	38	13	397	39	13	398	40	13	399	41	13	400	42	13
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461	13	15	462	14	15	463	15	15	464	16	15	465	17	15
466	18	15	467	19	15	468	20	15	469	21	15	470	22	15
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541	46	16	542	47	16	543	1	17	544	2	17	545	3	17
546	4	17	547	5	17	548	6	17	549	7	17	550	8	17

551	9	17	552	10	17	553	11	17	554	12	17	555	13	17
556	14	17	557	15	17	558	16	17	559	17	17	560	18	17
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566	24	17	567	25	17	568	26	17	569	27	17	570	28	17
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576	34	17	577	35	17	578	36	17	579	37	17	580	38	17
581	39	17	582	40	17	583	41	17	584	42	17	585	43	17
586	44	17	587	45	17	588	46	17	589	47	17	590	1	18
591	2	18	592	3	18	593	4	18	594	5	18	595	6	18
596	7	18	597	8	18	598	9	18	599	10	18	600	11	18
601	12	18	602	13	18	603	14	18	604	15	18	605	16	18
606	17	18	607	18	18	608	19	18	609	20	18	610	21	18
611	22	18	612	23	18	613	24	18	614	25	18	615	26	18
616	27	18	617	28	18	618	29	18	619	30	18	620	31	18
621	32	18	622	33	18	623	34	18	624	35	18	625	36	18
626	37	18	627	38	18	628	39	18	629	40	18	630	41	18
631	42	18	632	43	18	633	44	18	634	45	18	635	46	18
636	47	18	637	1	19	638	2	19	639	3	19	640	4	19
641	5	19	642	6	19	643	7	19	644	8	19	645	9	19
646	10	19	647	11	19	648	12	19	649	13	19	650	14	19
651	15	19	652	16	19	653	17	19	654	18	19	655	19	19
656	20	19	657	21	19	658	22	19	659	23	19	660	24	19
661	25	19	662	26	19	663	27	19	664	28	19	665	29	19
666	30	19	667	31	19	668	32	19	669	33	19	670	34	19
671	35	19	672	36	19	673	37	19	674	38	19	675	39	19
676	40	19	677	41	19	678	42	19	679	43	19	680	44	19
681	45	19	682	46	19	683	47	19	684	1	20	685	2	20
686	3	20	687	4	20	688	5	20	689	6	20	690	7	20
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1856	32	46	1857	33	46	1858	34	46	1859	35	46	1860	36	46
1861	37	46	1862	38	46	1863	11	47	1864	12	47	1865	13	47
1866	14	47	1867	15	47	1868	16	47	1869	17	47	1870	18	47
1871	19	47	1872	20	47	1873	21	47	1874	22	47	1875	23	47
1876	24	47	1877	25	47	1878	26	47	1879	27	47	1880	28	47
1881	29	47	1882	30	47	1883	31	47	1884	32	47	1885	33	47
1886	34	47	1887	35	47	1888	36	47	1889	37	47	1890	12	48
1891	13	48	1892	14	48	1893	15	48	1894	16	48	1895	17	48
1896	18	48	1897	19	48	1898	20	48	1899	21	48	1900	22	48
1901	23	48	1902	24	48	1903	25	48	1904	26	48	1905	27	48
1906	28	48	1907	29	48	1908	30	48	1909	31	48	1910	32	48
1911	33	48	1912	34	48	1913	35	48	1914	36	48	1915	13	49
1916	14	49	1917	15	49	1918	16	49	1919	17	49	1920	18	49
1921	19	49	1922	20	49	1923	21	49	1924	22	49	1925	23	49
1926	24	49	1927	25	49	1928	26	49	1929	27	49	1930	28	49
1931	29	49	1932	30	49	1933	31	49	1934	32	49	1935	33	49
1936	34	49	1937	35	49	1938	14	50	1939	15	50	1940	16	50
1941	17	50	1942	18	50	1943	19	50	1944	20	50	1945	21	50
1946	22	50	1947	23	50	1948	24	50	1949	25	50	1950	26	50
1951	27	50	1952	28	50	1953	29	50	1954	30	50	1955	31	50
1956	32	50	1957	33	50	1958	34	50	1959	15	51	1960	16	51
1961	17	51	1962	18	51	1963	19	51	1964	20	51	1965	21	51
1966	22	51	1967	23	51	1968	24	51	1969	25	51	1970	26	51
1971	27	51	1972	28	51	1973	29	51	1974	30	51	1975	31	51

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REPRODUCIBILITY OF THE
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1976 32 51 1977 33 51 0 0 0 0 0 0 0 0 0

----END OF FILE WRITTEN----

GROVES MODEL DATA (D,P,T)

P	1	25	250	247	244	239	237	241	244	240	238	237	1
P	1	30	118	117	114	112	111	112	111	105	101	100	1
P	1	35	582	576	562	546	529	527	509	472	450	442	0
P	1	40	259	295	286	275	261	254	237	216	203	199	0
P	1	45	157	155	152	146	136	127	116	103	95	93	0
P	1	50	842	832	816	778	720	659	587	515	472	457	-1
P	1	55	454	449	442	420	383	345	306	266	242	234	-1
P	1	60	241	237	232	217	198	177	155	134	121	117	-1
P	1	65	122	119	117	110	100	89	79	67	60	57	-1
P	1	70	577	561	549	519	481	435	382	317	278	265	-2
P	1	75	255	249	243	236	222	207	183	148	127	120	-2
P	1	80	110	108	105	102	100	95	84	67	57	53	-2
P	1	85	471	463	446	440	437	429	384	305	258	242	-3
P	1	90	197	194	187	184	190	191	174	138	116	109	-3
P	1	95	803	791	767	778	833	873	813	646	546	512	-4
P	1	100	350	345	338	345	379	401	376	301	256	241	-4
P	1	105	168	164	160	163	177	190	181	145	123	116	-4
P	1	110	898	889	856	843	899	939	887	701	589	552	-5
P	2	25	250	246	242	239	239	243	241	231	225	223	1
P	2	30	118	116	114	112	111	112	111	105	101	100	1
P	2	35	581	572	560	543	531	523	517	485	466	459	0
P	2	40	298	293	286	274	264	255	246	227	216	212	0
P	2	45	157	156	152	144	137	130	122	110	103	100	0
P	2	50	848	839	820	773	734	683	625	546	499	483	-1
P	2	55	458	455	443	413	390	359	325	279	251	242	-1
P	2	60	243	238	231	215	202	185	165	140	125	120	-1
P	2	65	122	119	114	106	100	92	83	69	61	58	-1
P	2	70	577	551	534	504	482	450	397	321	275	260	-2
P	2	75	256	245	240	229	223	211	188	147	122	114	-2
P	2	80	111	106	105	102	101	97	86	66	54	50	-2
P	2	85	469	448	451	439	440	434	393	295	236	217	-3
P	2	90	200	188	188	187	191	192	175	135	108	99	-3
P	2	95	855	802	797	784	814	843	792	600	485	446	-4
P	2	100	395	364	362	357	366	377	359	276	229	213	-4
P	2	105	199	182	178	171	174	179	174	135	112	104	-4
P	2	110	113	101	96	91	91	93	90	71	60	56	-4
P	3	25	251	246	244	240	240	243	238	225	217	215	1
P	3	30	118	117	115	113	112	112	110	105	102	101	1
P	3	35	582	575	566	552	533	529	521	501	489	485	0
P	3	40	299	297	290	279	267	262	255	242	234	232	0
P	3	45	159	158	154	146	139	135	130	121	116	114	0
P	3	50	860	859	833	781	741	718	675	616	581	569	-1
P	3	55	465	461	446	416	392	380	354	319	298	291	-1
P	3	60	244	241	231	214	203	196	181	162	151	147	-1
P	3	65	121	117	113	106	101	98	90	79	72	70	-1
P	3	70	569	547	528	503	487	475	434	372	335	322	-2
P	3	75	255	240	237	231	225	223	205	171	151	144	-2
P	3	80	110	105	105	103	102	102	94	76	65	62	-2
P	3	85	476	444	450	446	438	444	420	339	290	274	-3
P	3	90	206	191	191	188	187	191	182	146	124	117	-3
P	3	95	903	811	802	789	785	804	783	645	562	535	-4
P	3	100	419	374	362	354	354	365	355	298	264	252	-4

P	3	105	213	183	175	169	167	174	177	153	139	134	-4
P	3	110	122	104	96	89	88	94	98	86	79	76	-4
P	4	25	251	250	246	244	241	241	240	239	238	238	1
P	4	30	119	119	117	116	114	114	113	111	110	109	1
P	4	35	590	588	583	570	554	553	545	522	508	504	0
P	4	40	305	306	300	291	282	282	273	254	243	239	0
P	4	45	163	162	159	153	148	149	142	130	123	120	0
P	4	50	886	883	861	825	801	804	761	686	641	626	-1
P	4	55	478	473	462	439	427	430	407	363	337	328	-1
P	4	60	250	247	240	229	223	225	210	189	175	170	-1
P	4	65	123	121	119	114	111	112	106	93	85	83	-1
P	4	70	575	568	565	551	539	546	511	446	410	398	-2
P	4	75	253	250	257	253	250	253	240	209	190	184	-2
P	4	80	110	109	113	114	112	114	108	93	84	81	-2
P	4	85	479	471	494	493	478	475	458	392	352	339	-3
P	4	90	212	206	213	212	198	192	184	158	142	137	-3
P	4	95	920	880	900	873	813	769	754	658	600	581	-4
P	4	100	416	386	386	380	359	348	341	305	283	276	-4
P	4	105	202	182	178	172	165	167	176	164	157	154	-4
P	4	110	112	98	93	89	86	92	102	99	97	97	-4
P	5	25	251	254	250	249	247	246	249	254	257	258	1
P	5	30	120	120	120	118	117	117	118	120	121	122	1
P	5	35	595	598	595	584	576	577	581	586	589	590	0
P	5	40	309	311	307	299	298	300	299	292	288	286	0
P	5	45	164	165	163	159	158	160	159	155	153	152	0
P	5	50	889	896	882	859	861	880	869	832	810	802	-1
P	5	55	480	481	475	463	464	474	470	456	448	445	-1
P	5	60	253	254	248	242	244	250	248	239	234	232	-1
P	5	65	126	127	125	122	122	126	125	123	122	121	-1
P	5	70	582	597	600	587	591	607	608	596	589	586	-2
P	5	75	254	263	271	268	267	276	280	283	285	285	-2
P	5	80	111	115	118	115	115	118	121	121	121	121	-2
P	5	85	489	496	505	485	464	459	472	477	480	481	-3
P	5	90	213	214	215	199	181	169	170	170	170	170	-3
P	5	95	887	899	901	819	700	619	622	649	665	671	-4
P	5	100	379	379	382	351	308	276	280	292	299	302	-4
P	5	105	172	172	175	163	145	135	145	162	172	176	-4
P	5	110	91	88	89	84	78	79	89	100	107	109	-4
P	6	25	251	253	253	253	256	258	260	265	268	269	1
P	6	30	119	120	121	121	122	123	125	126	130	130	1
P	6	35	592	597	597	599	602	611	627	642	651	654	0
P	6	40	306	308	306	308	311	318	326	330	332	333	0
P	6	45	161	163	162	163	166	171	176	176	179	180	0
P	6	50	869	881	878	886	905	935	965	974	979	981	-1
P	6	55	468	474	474	477	487	508	528	537	542	544	-1
P	6	60	248	251	249	251	258	271	282	288	292	293	-1
P	6	65	125	127	126	125	128	137	144	150	154	155	-1
P	6	70	585	599	592	593	607	652	695	731	753	760	-2
P	6	75	255	265	264	262	265	286	313	335	348	353	-2
P	6	80	112	114	114	111	110	117	128	136	141	142	-2
P	6	85	486	487	479	456	423	423	453	483	501	507	-3
P	6	90	208	206	201	183	156	141	145	152	156	158	-3
P	6	95	853	852	833	737	577	480	489	526	548	556	-4
P	6	100	360	362	361	327	260	214	216	230	238	241	-4
P	6	105	162	164	167	156	127	108	112	124	131	134	-4
P	6	110	840	837	867	836	719	640	689	771	820	837	-5
P	7	25	250	252	256	259	263	265	269	274	277	278	1

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P	7	30	118	119	122	123	125	128	130	133	135	135	1
P	7	35	582	591	600	605	622	640	653	662	667	669	0
P	7	40	299	301	305	309	318	331	340	345	348	349	0
P	7	45	157	158	161	163	169	177	184	185	186	186	0
F	7	50	84	85	87	88	91	96	101	102	103	103	0
P	7	55	454	457	466	470	492	521	551	564	572	574	-1
P	7	60	241	242	245	246	257	275	295	307	314	317	-1
P	7	65	122	123	123	122	128	139	152	159	163	165	-1
P	7	70	577	578	573	562	595	654	730	779	808	818	-2
P	7	75	255	256	253	245	257	284	322	348	364	369	-2
P	7	80	110	110	109	104	104	111	126	137	144	146	-2
P	7	85	471	471	460	423	395	393	425	452	468	474	-3
P	7	90	197	198	191	170	145	131	131	135	137	138	-3
P	7	95	803	812	793	688	569	479	458	456	455	454	-4
P	7	100	350	357	354	317	262	218	198	191	187	185	-4
F	7	105	168	170	168	153	132	110	101	98	96	96	-4
P	7	110	898	903	895	835	725	626	576	559	549	545	-5
P	8	25	250	253	257	260	264	265	270	276	280	281	1
P	8	30	118	120	122	123	126	128	130	132	133	134	1
P	8	35	581	592	595	606	623	640	648	650	651	652	0
P	8	40	298	301	303	307	319	330	335	332	330	330	0
P	8	45	157	158	158	161	169	175	178	177	176	176	0
P	8	50	848	844	852	863	907	946	971	963	958	957	-1
P	8	55	458	457	454	462	485	509	526	525	524	524	-1
P	8	60	243	240	240	241	252	266	280	281	282	282	-1
P	8	65	122	123	121	120	124	132	141	145	147	148	-1
P	8	70	577	584	579	563	571	615	676	709	729	735	-2
P	8	75	256	268	261	251	250	268	295	316	329	333	-2
P	8	80	111	116	116	109	104	106	115	125	131	133	-2
P	8	85	469	506	501	459	408	390	397	430	450	456	-3
P	8	90	200	214	214	189	158	140	134	136	140	141	-3
P	8	95	855	931	902	796	660	567	504	489	480	477	-4
P	8	100	395	421	412	359	301	255	216	199	189	185	-4
P	8	105	199	213	199	171	145	122	102	91	84	82	-4
P	8	110	113	117	109	90	75	63	52	45	41	39	-4
P	9	25	251	253	254	257	259	260	260	262	263	264	1
P	9	30	118	120	121	122	124	124	124	124	124	124	1
P	9	35	582	589	596	597	607	613	610	599	592	590	0
P	9	40	299	301	303	302	307	313	310	301	296	294	0
P	9	45	159	159	160	158	162	165	163	157	153	152	0
P	9	50	860	858	858	845	865	883	875	840	819	812	-1
P	9	55	465	464	461	451	461	471	467	450	440	436	-1
P	9	60	244	245	242	234	235	241	243	237	233	232	-1
P	9	65	121	124	125	118	115	117	121	120	119	119	-1
P	9	70	569	600	606	560	528	537	573	582	587	589	-2
P	9	75	255	275	283	255	233	234	252	262	268	270	-2
P	9	80	110	122	126	112	98	96	103	110	114	116	-2
P	9	85	476	527	550	477	405	378	399	430	449	455	-3
P	9	90	206	230	236	200	166	150	153	164	171	173	-3
P	9	95	90	101	104	87	72	63	62	64	65	66	-3
P	9	100	419	480	487	404	328	280	265	261	259	258	-4
P	9	105	213	246	247	199	158	131	119	110	105	103	-4
P	9	110	122	141	138	107	82	66	56	48	43	42	-4
P	10	25	251	250	251	253	254	254	250	243	239	237	1
P	10	30	119	119	119	120	119	118	116	113	111	111	1
P	10	35	590	588	585	583	578	564	556	539	529	525	0
P	10	40	305	302	298	295	289	281	274	264	258	256	0

P 10	45	163	161	157	153	150	145	140	135	132	131	0
P 10	50	886	869	850	824	801	767	740	708	689	682	-1
P 10	55	478	468	457	439	426	403	389	374	365	362	-1
P 10	60	250	246	240	228	217	204	199	191	186	185	-1
P 10	65	123	123	122	113	106	99	99	95	93	92	-1
P 10	70	575	586	594	549	487	454	466	452	444	441	-2
P 10	75	253	265	274	248	217	202	213	207	203	202	-2
P 10	80	110	117	122	110	94	87	93	92	91	91	-2
P 10	85	479	515	533	471	402	371	398	400	401	402	-3
P 10	90	212	228	233	202	172	158	169	170	171	171	-3
P 10	95	92	09	102	88	75	69	74	74	74	74	-3
P 10	100	416	462	480	413	343	310	325	316	311	309	-4
P 10	105	202	230	242	207	172	151	150	139	132	130	-4
P 10	110	112	130	137	116	93	78	72	61	54	52	-4
P 11	25	251	250	248	247	246	245	244	239	236	235	1
P 11	30	120	119	118	116	115	113	111	109	108	107	1
P 11	35	595	589	578	562	546	529	518	511	507	505	0
P 11	40	309	303	294	283	270	255	247	244	242	242	0
P 11	45	164	161	155	148	139	129	123	122	121	121	0
P 11	50	889	869	838	792	736	666	633	632	631	631	-1
P 11	55	480	470	452	425	368	346	330	333	335	335	-1
P 11	60	253	248	239	221	200	177	168	169	170	170	-1
P 11	65	126	124	120	110	98	87	84	84	84	84	-1
P 11	70	582	576	571	525	464	413	404	396	391	390	-2
P 11	75	254	255	256	237	210	191	190	184	180	179	-2
P 11	80	111	112	113	104	93	86	87	84	82	82	-2
P 11	85	489	495	492	448	402	381	393	387	383	382	-3
P 11	90	213	216	212	192	175	169	178	170	175	174	-3
P 11	95	887	899	888	826	774	772	819	811	806	805	-4
P 11	100	379	395	405	384	365	364	386	372	364	361	-4
P 11	105	172	184	195	192	183	180	184	174	168	166	-4
P 11	110	91	100	109	106	99	93	91	81	75	73	-4
P 12	25	251	247	245	241	239	241	242	240	239	238	1
P 12	30	119	118	116	113	111	112	110	107	105	105	1
P 12	35	592	584	565	552	530	524	506	486	474	470	0
P 12	40	306	301	289	279	263	252	237	227	221	219	0
P 12	45	161	159	152	147	136	125	116	110	106	105	0
P 12	50	869	854	827	788	723	645	586	563	549	545	-1
P 12	55	468	460	442	422	382	336	303	294	289	287	-1
P 12	60	248	243	234	221	198	172	154	150	148	147	-1
P 12	65	125	122	117	111	99	86	78	75	73	73	-1
P 12	70	585	568	556	533	477	420	381	357	343	338	-2
P 12	75	255	250	245	239	220	199	183	167	157	154	-2
P 12	80	112	109	108	105	99	91	85	77	72	71	-2
P 12	85	486	477	459	449	433	411	388	353	332	325	-3
P 12	90	208	204	199	194	191	185	179	162	152	148	-3
P 12	95	853	833	807	822	849	867	841	764	718	702	-4
P 12	100	360	353	353	368	393	412	405	361	335	326	-4
P 12	105	162	161	161	173	188	201	195	172	158	154	-4
P 12	110	840	850	872	912	962	992	947	816	737	711	-5
P 13	25	251	250	249	248	249	250	251	249	248	248	1
P 13	30	119	119	118	118	117	118	118	116	115	115	1
P 13	35	588	588	583	576	570	570	567	555	550	549	0
P 13	40	303	302	298	292	288	286	282	273	271	271	0
P 13	45	161	160	157	154	151	149	145	139	138	138	0
P 13	50	865	861	848	824	808	792	769	734	730	729	-1
P 13	55	466	464	456	440	430	420	408	389	388	389	-1

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P	13	60	246	244	239	229	223	218	212	202	201	201	-1
P	13	65	123	122	120	115	111	109	106	102	100	99	-1
P	13	70	576	576	570	545	525	518	513	489	462	453	-2
P	13	75	256	258	258	247	237	236	236	224	202	195	-2
P	13	80	111	112	113	108	103	102	103	98	88	85	-2
P	13	85	482	486	488	460	433	425	428	405	375	365	-3
P	13	90	206	208	207	193	178	173	174	164	152	147	-3
P	13	95	877	882	877	814	752	724	723	678	626	608	-4
P	13	100	384	386	385	359	334	322	321	300	276	268	-4
P	13	105	182	182	181	169	158	153	154	143	132	128	-4
P	13	110	960	959	943	873	811	792	801	748	690	669	-5
U	1	25	400	393	392	381	377	382	395	403	408	409	-4
U	1	30	178	175	173	171	171	176	179	176	174	174	-4
U	1	35	820	815	805	800	791	812	813	772	747	739	-5
U	1	40	404	400	386	374	367	371	361	338	324	320	-5
U	1	45	207	203	196	189	180	177	168	153	144	141	-5
U	1	50	108	107	104	100	94	89	81	72	67	65	-5
U	1	55	585	581	575	554	511	467	420	367	335	325	-6
U	1	60	327	325	320	302	277	248	218	192	176	171	-6
U	1	65	182	179	174	164	146	131	115	100	91	88	-6
U	1	70	952	926	906	837	755	661	581	497	447	430	-7
U	1	75	444	431	421	403	365	330	289	241	212	203	-7
U	1	80	195	190	187	180	171	157	137	110	94	88	-7
U	1	85	850	832	809	791	760	722	634	503	424	398	-8
U	1	90	370	365	349	339	333	320	283	225	190	179	-8
U	1	95	148	146	139	138	141	143	131	103	86	81	-8
U	1	100	580	574	560	571	622	645	593	474	403	379	-9
U	1	105	242	236	234	244	271	294	278	224	192	181	-9
U	1	110	108	106	104	107	119	128	124	101	87	83	-9
U	2	25	400	393	386	379	382	391	387	377	371	369	-4
U	2	30	178	174	172	171	173	178	175	168	164	162	-4
U	2	35	823	813	799	791	790	799	804	765	742	734	-5
U	2	40	403	393	386	375	368	366	366	348	337	334	-5
U	2	45	205	201	195	187	181	176	173	162	155	153	-5
U	2	50	108	106	104	99	95	90	85	77	72	71	-5
U	2	55	591	592	580	545	521	483	446	390	356	345	-6
U	2	60	334	332	325	303	284	261	235	203	184	177	-6
U	2	65	182	181	174	161	149	136	122	105	95	91	-6
U	2	70	943	914	873	809	760	694	612	516	458	439	-7
U	2	75	444	425	408	382	364	338	300	243	209	197	-7
U	2	80	198	189	185	177	171	160	141	111	93	87	-7
U	2	85	845	812	817	785	766	738	654	494	398	366	-8
U	2	90	360	343	347	342	341	331	295	222	178	164	-8
U	2	95	147	140	139	137	142	145	133	99	79	72	-8
U	2	100	610	571	574	574	598	619	578	439	356	328	-9
U	2	105	264	246	249	247	257	266	254	195	160	148	-9
U	2	110	125	114	114	113	116	118	114	89	74	69	-9
U	3	25	399	387	388	380	381	390	381	354	338	332	-4
U	3	30	178	175	174	172	174	177	173	162	155	153	-4
U	3	35	827	811	805	802	787	795	785	755	737	731	-5
U	3	40	400	397	390	382	371	368	365	356	351	349	-5
U	3	45	204	202	198	191	183	180	177	170	166	164	-5
U	3	50	109	109	106	101	96	94	90	84	80	79	-5
U	3	55	605	604	591	555	524	509	479	439	415	407	-6
U	3	60	340	343	331	305	288	276	258	233	218	213	-6
U	3	65	185	182	174	161	150	145	134	121	113	111	-6
U	3	70	931	912	863	800	760	735	668	594	550	535	-7

U	3	75	440	417	400	384	368	358	325	282	256	248	-7
U	3	80	195	186	183	177	174	172	155	129	113	108	-7
U	3	85	841	793	803	796	778	776	724	589	508	481	-8
U	3	90	361	345	350	345	340	346	323	255	214	201	-8
U	3	95	153	140	142	139	138	141	136	108	91	86	-8
U	3	100	644	591	583	574	578	589	559	451	386	365	-9
U	3	105	279	249	247	248	247	251	241	200	175	167	-9
U	3	110	131	117	114	110	110	112	111	94	84	80	-9
U	4	25	398	394	386	383	379	378	375	376	377	377	-4
U	4	30	178	178	174	174	173	173	173	174	175	175	-4
U	4	35	829	823	822	814	796	793	802	793	788	786	-5
U	4	40	406	406	402	396	384	381	377	364	356	354	-5
U	4	45	208	208	205	198	192	192	187	175	168	165	-5
U	4	50	112	112	110	106	103	103	98	89	84	82	-5
U	4	55	623	622	610	582	563	565	541	485	451	440	-6
U	4	60	352	350	340	323	311	314	294	264	246	240	-6
U	4	65	189	186	179	168	164	165	155	139	129	126	-6
U	4	70	958	942	903	864	838	846	788	697	642	624	-7
U	4	75	440	435	435	416	409	412	389	341	312	303	-7
U	4	80	193	190	196	196	195	200	186	162	148	143	-7
U	4	85	826	821	864	872	871	889	853	730	656	632	-8
U	4	90	368	364	382	388	373	374	353	301	270	259	-8
U	4	95	159	157	163	159	147	139	135	115	103	99	-8
U	4	100	673	648	669	654	603	560	522	445	399	383	-9
U	4	105	282	265	269	265	253	234	223	192	173	167	-9
U	4	110	126	116	115	114	108	107	106	95	88	86	-9
U	5	25	396	400	391	389	384	381	385	396	406	408	-4
U	5	30	178	180	177	177	177	176	178	181	183	183	-4
U	5	35	829	832	835	830	816	811	823	857	877	884	-5
U	5	40	411	414	411	402	396	395	399	399	399	399	-5
U	5	45	212	212	209	204	202	201	201	200	199	199	-5
U	5	50	113	114	112	109	109	110	109	104	101	100	-5
U	5	55	621	628	624	608	605	616	606	580	574	570	-6
U	5	60	350	351	344	334	338	344	341	324	314	310	-6
U	5	65	193	191	184	180	179	184	183	176	175	174	-6
U	5	70	984	985	958	930	935	957	945	906	883	875	-7
U	5	75	444	458	465	457	456	469	466	467	468	468	-7
U	5	80	191	200	208	207	211	221	225	224	223	223	-7
U	5	85	838	872	897	894	903	941	978	990	997	1000	-8
U	5	90	384	383	390	375	366	365	372	365	361	359	-8
U	5	95	163	166	166	151	131	119	119	122	124	124	-8
U	5	100	663	670	665	602	510	439	424	422	421	420	-9
U	5	105	262	266	270	246	210	178	173	178	181	182	-9
U	5	110	111	112	115	107	94	85	85	86	90	90	-9
U	6	25	397	400	395	392	396	399	397	405	407	408	-4
U	6	30	177	178	180	181	182	183	183	187	189	190	-4
U	6	35	828	835	845	848	848	851	870	897	913	919	-5
U	6	40	411	413	412	414	413	416	426	436	442	444	-5
U	6	45	210	211	209	209	210	215	219	223	225	226	-5
U	6	50	111	112	111	112	114	117	119	120	121	121	-5
U	6	55	606	617	619	622	631	649	669	673	675	676	-6
U	6	60	339	341	343	347	356	368	379	380	381	381	-6
U	6	65	187	189	188	188	193	202	209	213	215	216	-6
U	6	70	98	99	97	97	100	106	110	115	115	115	-6
U	6	75	447	463	458	461	474	511	547	580	600	606	-7
U	6	80	193	202	204	204	211	232	257	275	286	289	-7
U	6	85	85	87	87	86	87	94	104	115	118	120	-7

D	6	90	384	380	372	355	335	333	350	365	374	377	-8
D	6	95	160	158	152	134	109	96	99	105	109	110	-8
D	6	100	636	633	616	535	412	330	328	345	355	359	-9
D	6	105	252	256	252	224	171	136	132	140	145	146	-9
D	6	110	106	109	113	104	83	67	66	69	71	71	-9
D	7	25	400	399	401	402	408	407	407	413	417	418	-4
D	7	30	178	179	182	185	186	187	190	194	196	197	-4
D	7	35	820	840	856	863	881	891	903	919	929	932	-5
D	7	40	404	410	415	419	428	437	444	452	457	458	-5
D	7	45	207	208	209	211	217	226	230	231	232	232	-5
L	7	50	108	109	111	112	116	121	125	125	125	125	-5
D	7	55	585	591	609	615	641	672	695	700	703	704	-6
L	7	60	327	328	338	343	357	374	393	400	404	406	-6
D	7	65	182	183	186	188	195	207	219	225	229	230	-6
D	7	70	95	95	95	95	100	108	117	122	125	126	-6
L	7	75	444	446	440	434	468	524	587	625	648	655	-7
D	7	80	195	196	195	191	203	231	265	291	307	312	-7
D	7	85	85	85	84	80	82	89	103	113	119	121	-7
D	7	90	370	370	358	329	302	297	314	332	343	346	-8
D	7	95	148	148	142	122	102	90	91	94	96	96	-8
L	7	100	580	591	581	500	399	333	310	305	302	301	-9
L	7	105	242	247	245	215	178	143	130	125	122	121	-9
D	7	110	108	112	113	103	86	70	62	58	56	55	-9
L	8	25	400	403	406	406	408	403	411	423	430	433	-4
L	8	30	178	179	184	185	188	188	192	196	198	199	-4
D	8	35	823	845	853	872	862	895	907	924	934	938	-5
D	8	40	403	410	417	420	429	440	445	445	445	445	-5
L	8	45	205	208	206	210	219	225	227	225	224	223	-5
D	8	50	108	108	110	111	117	120	122	120	119	118	-5
D	8	55	591	593	594	609	642	666	673	665	660	659	-6
L	8	60	334	326	330	336	353	370	379	373	369	368	-6
D	8	65	182	182	179	182	192	201	208	207	206	206	-6
L	8	70	94	93	93	92	96	102	110	112	113	114	-6
D	8	75	444	455	440	431	445	488	542	568	584	589	-7
L	8	80	198	203	202	194	197	216	244	261	271	275	-7
L	8	85	85	90	89	85	82	84	91	101	107	109	-7
L	8	90	360	384	390	351	305	287	293	321	338	343	-8
L	8	95	147	161	158	139	114	101	96	99	101	101	-8
L	8	100	610	658	659	583	479	408	360	349	342	340	-9
D	8	105	264	287	281	252	214	182	154	142	135	132	-9
D	8	110	125	133	129	112	96	81	68	62	58	57	-9
L	9	25	399	400	399	400	401	403	401	407	411	412	-4
D	9	30	178	180	181	185	185	186	186	188	189	190	-4
D	9	35	827	841	854	863	873	872	871	873	874	875	-5
D	9	40	400	406	412	415	418	424	422	416	412	411	-5
D	9	45	204	206	208	208	211	214	212	205	201	199	-5
D	9	50	109	109	110	109	112	114	113	108	105	104	-5
L	9	55	605	600	606	600	620	631	616	587	570	564	-6
L	9	60	340	336	328	326	340	347	339	323	313	310	-6
D	9	65	185	181	179	175	178	183	182	175	171	169	-6
D	9	70	931	945	939	895	880	903	932	922	916	914	-7
D	9	75	440	460	468	432	409	419	451	454	456	456	-7
D	9	80	195	212	217	196	180	184	200	209	214	216	-7
D	9	85	841	922	967	865	762	744	809	865	899	910	-8
D	9	90	361	403	417	361	302	282	300	329	346	352	-8
L	9	95	153	169	174	147	122	111	113	123	129	131	-8
L	9	100	644	721	741	633	526	464	459	479	491	495	-9

U	9	105	279	318	332	280	233	202	196	197	198	198	-9
U	9	110	131	151	154	127	104	88	83	80	78	78	-9
D	10	25	398	394	391	395	400	402	395	382	374	372	-4
U	10	30	178	178	179	181	162	184	180	175	172	171	-4
D	10	35	829	832	839	843	845	836	827	810	800	796	-5
D	10	40	406	405	404	408	402	393	390	378	371	368	-5
U	10	45	208	206	204	202	199	193	189	183	179	178	-5
D	10	50	112	110	108	106	104	101	97	93	91	90	-5
D	10	55	623	611	598	584	574	550	529	505	491	486	-6
U	10	60	352	341	329	321	313	297	282	271	264	262	-6
U	10	65	189	184	177	167	164	155	149	142	138	136	-6
U	10	70	958	945	928	873	808	754	745	719	703	698	-7
D	10	75	440	448	455	418	372	349	358	345	337	335	-7
U	10	80	193	202	211	192	167	155	164	157	153	151	-7
D	10	85	826	883	928	842	722	669	714	706	701	700	-8
U	10	90	368	396	409	361	303	277	298	302	304	305	-8
D	10	95	159	169	170	147	128	119	128	130	131	132	-8
L	10	100	673	719	731	631	534	502	546	553	557	559	-9
L	10	105	282	310	322	276	237	220	239	241	242	243	-9
U	10	110	126	142	150	132	110	100	104	101	99	99	-9
D	11	25	396	394	389	391	391	392	393	387	383	382	-4
U	11	30	178	177	177	178	178	179	178	173	170	169	-4
D	11	35	829	831	828	823	816	815	805	792	784	782	-5
U	11	40	411	416	399	389	382	372	367	361	357	356	-5
U	11	45	212	208	201	194	185	178	173	169	167	166	-5
D	11	50	113	111	107	102	96	90	85	84	83	83	-5
U	11	55	621	609	585	560	522	473	451	453	454	455	-6
D	11	60	350	343	329	309	286	253	239	241	242	243	-6
D	11	65	193	188	179	165	149	132	124	127	129	129	-6
D	11	70	984	960	926	846	749	654	625	627	628	629	-7
D	11	75	444	439	436	401	354	313	303	299	297	296	-7
U	11	80	191	192	197	183	160	144	144	137	133	131	-7
U	11	85	838	849	861	796	703	654	655	633	620	615	-8
D	11	90	384	390	386	345	304	283	294	288	284	283	-8
U	11	95	163	162	156	141	128	124	131	132	133	133	-8
U	11	100	663	668	651	593	555	559	606	602	600	599	-9
D	11	105	262	270	272	260	252	259	282	281	280	280	-9
D	11	110	111	116	125	123	119	121	129	125	123	122	-9
D	12	25	397	390	385	384	384	380	390	399	404	406	-4
U	12	30	177	175	177	172	172	177	178	176	175	174	-4
D	12	35	828	821	809	801	789	811	805	776	759	753	-5
U	12	40	411	415	392	381	369	372	362	348	340	337	-5
U	12	45	210	207	196	191	180	176	166	158	153	152	-5
U	12	50	111	109	105	101	95	87	80	76	74	73	-5
U	12	55	606	598	576	555	510	458	418	400	389	386	-6
D	12	60	339	332	321	305	279	242	218	214	212	211	-6
D	12	65	187	185	175	164	146	126	113	111	110	109	-6
D	12	70	980	951	918	859	749	642	575	555	543	539	-7
D	12	75	447	435	422	409	361	318	287	269	258	255	-7
U	12	80	193	189	189	184	169	150	138	125	117	115	-7
D	12	85	851	831	808	794	749	691	634	574	538	526	-8
D	12	90	384	378	366	347	327	302	286	260	244	239	-8
U	12	95	160	156	149	145	141	136	131	120	113	111	-8
D	12	100	636	617	605	609	627	633	619	563	529	518	-9
D	12	105	252	244	239	256	281	305	302	272	254	248	-9
U	12	110	106	103	106	114	126	137	137	124	116	114	-9
U	13	25	398	396	392	390	391	392	393	394	396	397	-4

REPRODUCIBILITY OF THE ORIGINAL PAGE IS POOR

D	13	30	178	178	178	178	179	180	181	180	179	178	-4
D	13	35	828	830	831	831	829	834	838	831	820	816	-5
D	13	40	406	406	403	399	395	396	396	389	387	386	-5
D	13	45	208	207	203	200	197	197	194	188	187	187	-5
D	13	50	110	110	108	106	104	100	100	96	94	94	-5
D	13	55	604	603	597	581	571	559	541	515	514	514	-6
D	13	60	339	336	331	320	314	305	294	281	283	284	-6
D	13	65	186	184	179	172	167	162	157	150	151	151	-6
D	13	70	956	946	921	878	846	824	803	768	776	779	-7
D	13	75	446	445	439	420	404	399	395	377	357	350	-7
D	13	80	195	197	198	191	185	184	185	175	150	142	-7
D	13	85	848	858	868	835	802	802	810	767	711	693	-8
D	13	90	373	377	378	356	333	326	329	311	288	281	-8
D	13	95	158	159	157	145	133	128	129	122	113	110	-8
D	13	100	649	652	648	600	551	528	523	491	453	440	-9
D	13	105	269	271	272	256	239	229	227	210	193	187	-9
D	13	110	118	119	120	114	107	103	103	96	89	86	-9
T	1	25	218	219	217	219	219	220	215	207	204	203	0
T	1	30	231	232	230	229	225	222	216	208	205	204	0
T	1	35	247	246	243	238	233	226	218	213	209	208	0
T	1	40	258	257	258	256	248	238	229	222	214	211	0
T	1	45	265	266	269	268	263	251	242	236	223	219	0
T	1	50	271	272	274	272	268	259	254	250	249	249	0
T	1	55	270	269	268	264	261	257	254	252	254	255	0
T	1	60	257	254	252	251	249	249	248	244	244	244	0
T	1	65	234	232	233	234	237	238	239	232	228	227	0
T	1	70	211	211	211	216	222	229	229	222	200	190	0
T	1	75	200	201	201	204	212	219	220	214	194	187	0
T	1	80	197	198	196	198	204	211	213	211	211	211	0
T	1	85	193	194	192	194	200	207	211	211	211	211	0
T	1	90	185	185	186	189	199	208	214	214	214	214	0
T	1	95	187	187	190	195	203	210	214	216	217	218	0
T	1	100	204	203	204	204	206	210	214	215	216	216	0
T	1	105	231	232	228	222	217	215	217	215	214	213	0
T	1	110	273	276	271	259	248	240	235	229	225	224	0
T	2	25	218	218	218	219	218	217	217	214	207	195	0
T	2	30	231	232	231	228	224	219	220	217	200	194	0
T	2	35	246	245	244	239	234	228	224	221	199	192	0
T	2	40	258	259	258	254	250	243	234	227	205	198	0
T	2	45	268	270	271	268	265	257	247	237	219	213	0
T	2	50	273	275	275	271	269	263	256	247	250	251	0
T	2	55	270	268	266	264	261	259	254	249	248	248	0
T	2	60	253	250	247	247	247	247	245	240	234	232	0
T	2	65	233	228	228	230	234	237	235	228	212	207	0
T	2	70	213	210	213	217	221	226	226	217	195	188	0
T	2	75	201	201	205	209	213	217	218	211	193	187	0
T	2	80	195	195	199	201	205	211	213	207	210	211	0
T	2	85	193	192	192	195	200	205	209	208	207	207	0
T	2	90	193	191	189	190	195	202	207	206	209	209	0
T	2	95	200	197	197	197	197	200	206	209	211	211	0
T	2	100	219	215	213	210	207	206	210	214	216	217	0
T	2	105	251	246	237	230	225	225	228	230	231	232	0
T	2	110	296	290	278	266	258	259	261	261	261	261	0
T	3	25	219	221	219	220	219	217	218	221	198	190	0
T	3	30	231	232	231	230	224	221	222	226	210	205	0
T	3	35	245	247	245	240	236	232	231	231	226	224	0
T	3	40	260	261	259	254	251	248	243	237	245	248	0

T	3	45	271	272	271	266	264	262	255	247	254	256	0
T	3	50	275	274	273	269	268	267	261	255	269	274	0
T	3	55	268	266	263	261	261	260	257	253	254	254	0
T	3	60	250	245	243	245	246	248	245	241	232	229	0
T	3	65	229	225	226	230	234	236	234	226	211	205	0
T	3	70	213	209	213	219	223	225	226	216	198	191	0
T	3	75	202	201	206	210	213	217	219	211	194	188	0
T	3	80	197	196	200	202	203	206	211	207	212	214	0
T	3	85	197	195	195	195	196	199	202	200	199	198	0
T	3	90	198	193	190	189	191	192	196	199	201	201	0
T	3	95	204	199	195	195	196	197	199	205	209	210	0
T	3	100	220	214	210	208	207	209	215	223	228	229	0
T	3	105	255	245	236	227	226	231	245	250	263	265	0
T	3	110	306	291	275	265	263	274	291	303	310	313	0
T	4	25	220	221	222	222	222	222	223	221	211	208	0
T	4	30	233	233	235	232	229	229	228	222	222	222	0
T	4	35	248	249	247	244	242	243	237	229	239	242	0
T	4	40	262	262	260	256	256	258	252	243	255	259	0
T	4	45	273	272	271	269	269	270	266	259	275	280	0
T	4	50	275	274	273	271	272	272	271	267	281	286	0
T	4	55	267	265	264	263	263	265	262	261	264	265	0
T	4	60	248	246	246	247	249	249	249	247	244	243	0
T	4	65	227	227	231	235	236	237	237	234	227	225	0
T	4	70	209	210	218	222	224	225	226	224	209	204	0
T	4	75	200	200	206	212	213	214	215	213	202	198	0
T	4	80	199	199	201	203	201	199	202	200	207	209	0
T	4	85	202	200	199	197	191	186	187	187	187	187	0
T	4	90	200	197	194	190	185	179	181	183	184	185	0
T	4	95	199	193	190	189	191	191	193	197	199	200	0
T	4	100	209	201	195	196	201	210	221	232	239	241	0
T	4	105	239	229	220	216	218	237	263	285	298	303	0
T	4	110	293	278	264	256	262	284	317	344	360	366	0
T	5	25	221	221	223	223	224	225	225	223	238	243	0
T	5	30	234	233	235	233	231	232	232	231	248	254	0
T	5	35	250	250	248	245	246	248	246	230	254	259	0
T	5	40	262	262	260	259	262	264	261	255	264	267	0
T	5	45	270	271	271	271	273	277	275	270	270	270	0
T	5	50	274	274	275	275	276	278	278	276	279	279	0
T	5	55	269	267	265	265	267	268	270	271	273	274	0
T	5	60	252	252	251	252	251	253	254	257	262	264	0
T	5	65	227	231	236	237	237	237	238	241	242	242	0
T	5	70	206	211	218	220	220	221	224	229	223	221	0
T	5	75	199	200	203	204	204	205	209	211	207	206	0
T	5	80	202	199	197	194	190	186	188	188	196	199	0
T	5	85	203	198	196	189	179	170	168	168	168	168	0
T	5	90	193	194	192	185	172	161	159	162	164	164	0
T	5	95	187	187	187	187	184	180	180	184	186	187	0
T	5	100	193	191	194	197	204	212	223	234	241	243	0
T	5	105	219	215	216	220	230	253	279	302	316	320	0
T	5	110	269	259	255	259	274	304	343	373	391	397	0
T	6	25	220	220	223	225	225	225	228	229	239	242	0
T	6	30	234	234	234	234	233	234	238	239	246	248	0
T	6	35	249	249	246	246	247	250	251	249	258	261	0
T	6	40	259	260	259	259	262	266	266	264	269	271	0
T	6	45	268	269	270	272	275	277	279	278	281	282	0
T	6	50	272	273	275	275	276	279	282	283	286	287	0
T	6	55	269	268	267	267	269	273	275	278	280	281	0

REPRODUCIBILITY OF THE
ORIGINAL PAGE IS POOR

T	6	60	255	256	253	252	252	256	259	264	267	268	0
T	6	65	232	234	233	232	232	236	240	245	247	248	0
T	6	70	208	211	213	213	212	214	220	225	220	218	0
T	6	75	199	199	201	198	195	195	199	201	204	205	0
T	6	80	201	196	194	190	181	175	173	173	185	189	0
T	6	85	199	195	192	184	170	156	151	149	148	147	0
T	6	90	189	189	188	179	162	147	144	145	146	146	0
T	6	95	184	186	189	189	182	173	171	173	174	175	0
T	6	100	191	193	198	206	213	219	222	226	228	229	0
T	6	105	215	214	221	232	247	265	282	295	303	305	0
T	6	110	261	253	253	264	285	313	343	366	380	384	0
T	7	25	218	220	222	224	224	227	230	231	239	242	0
T	7	30	231	233	233	232	235	238	239	238	248	251	0
T	7	35	247	245	244	244	246	250	252	251	259	262	0
T	7	40	258	256	256	257	259	264	267	266	269	270	0
T	7	45	265	265	268	268	271	274	278	279	283	284	0
T	7	50	271	271	273	272	274	276	281	285	293	296	0
T	7	55	270	269	267	266	267	270	276	281	283	284	0
T	7	60	257	257	253	250	251	256	262	267	267	267	0
T	7	65	234	234	230	226	229	234	241	246	244	243	0
T	7	70	211	211	209	207	207	211	217	222	214	211	0
T	7	75	200	200	200	197	191	189	191	194	196	197	0
T	7	80	197	196	195	189	178	168	165	164	182	188	0
T	7	85	193	194	191	183	167	153	144	140	138	137	0
T	7	90	185	196	186	179	167	153	145	141	139	138	0
T	7	95	187	189	193	195	192	184	174	166	164	163	0
T	7	100	204	204	206	214	222	221	216	212	210	209	0
T	7	105	231	229	229	237	246	255	258	260	261	262	0
T	7	110	273	265	260	265	276	293	306	314	319	320	0
T	8	25	218	219	221	223	225	229	229	227	239	243	0
T	8	30	231	233	230	232	234	238	237	234	247	251	0
T	8	35	246	244	243	242	246	249	249	245	259	264	0
T	8	40	258	255	253	254	259	261	262	260	270	273	0
T	8	45	268	265	267	267	269	271	274	274	285	289	0
T	8	50	273	272	271	271	271	274	277	279	289	292	0
T	8	55	270	268	266	264	263	266	272	275	276	276	0
T	8	60	253	257	254	250	248	250	257	263	260	259	0
T	8	65	233	236	235	230	225	229	237	245	240	238	0
T	8	70	213	218	217	212	208	210	215	221	212	209	0
T	8	75	201	205	207	203	196	191	190	194	197	198	0
T	8	80	195	199	201	196	183	172	165	167	192	200	0
T	8	85	193	196	196	188	174	161	151	148	146	146	0
T	8	90	193	194	191	187	180	170	159	150	145	143	0
T	8	95	200	199	197	197	199	194	181	170	163	161	0
T	8	100	219	216	211	208	212	211	203	193	187	185	0
T	8	105	251	247	236	226	225	224	220	213	209	207	0
T	8	110	296	291	276	263	256	254	250	241	236	234	0
T	9	25	219	220	222	224	225	225	226	224	229	231	0
T	9	30	231	232	233	231	233	234	233	229	237	240	0
T	9	35	245	244	243	241	242	245	244	239	248	251	0
T	9	40	260	258	256	254	256	257	256	252	260	263	0
T	9	45	271	269	268	265	267	268	268	260	272	274	0
T	9	50	275	273	272	270	270	271	271	272	278	280	0
T	9	55	268	269	265	262	259	260	264	267	263	262	0
T	9	60	250	254	257	250	241	242	250	250	245	241	0
T	9	65	229	238	242	234	224	223	232	240	229	225	0
T	9	70	213	221	225	218	209	207	214	220	204	199	0

T 9 75	202	208	211	206	198	194	195	201	191	188	0
T 9 80	197	200	202	198	190	182	180	184	211	220	0
T 9 85	197	199	198	192	185	177	172	173	174	174	0
T 9 90	198	199	197	193	191	185	177	173	171	170	0
T 9 95	204	207	206	205	203	196	188	179	174	172	0
T 9 100	220	225	222	216	211	204	195	184	177	175	0
T 9 105	255	257	248	236	226	216	202	187	178	175	0
T 9 110	306	307	294	278	261	244	223	198	183	178	0
T 10 25	220	221	223	223	221	220	220	221	213	210	0
T 10 30	233	233	232	230	228	224	225	225	216	213	0
T 10 35	248	246	243	241	238	235	234	232	225	223	0
T 10 40	262	260	257	252	251	249	245	244	237	235	0
T 10 45	273	271	269	265	263	261	259	257	253	252	0
T 10 50	275	274	273	271	269	265	265	265	261	260	0
T 10 55	267	267	266	262	258	255	256	258	250	247	0
T 10 60	248	251	254	247	241	240	246	246	231	226	0
T 10 65	227	233	240	236	224	222	231	233	214	208	0
T 10 70	209	216	223	219	210	210	218	219	198	191	0
T 10 75	200	206	210	207	203	202	207	209	200	197	0
T 10 80	199	202	202	200	197	196	198	203	223	230	0
T 10 85	202	203	200	195	194	193	194	197	199	199	0
T 10 90	200	200	198	195	197	198	197	196	195	195	0
T 10 95	199	200	206	205	202	201	199	195	190	192	0
T 10 100	209	217	222	221	217	209	210	193	183	179	0
T 10 105	239	247	250	249	241	228	209	192	182	178	0
T 10 110	293	301	299	290	276	256	227	199	182	177	0
T 11 25	221	221	222	220	219	210	216	215	201	196	0
T 11 30	234	234	232	220	220	220	210	220	207	200	0
T 11 35	250	247	243	238	233	226	224	225	215	212	0
T 11 40	262	260	257	253	246	209	205	205	224	220	0
T 11 45	270	270	269	266	261	252	248	251	209	205	0
T 11 50	274	274	273	271	266	258	250	260	250	250	0
T 11 55	269	269	269	264	259	255	255	256	255	255	0
T 11 60	252	252	253	249	244	240	245	244	206	200	0
T 11 65	227	229	234	233	229	230	235	231	226	224	0
T 11 70	206	209	215	216	216	220	225	220	210	207	0
T 11 75	199	202	205	206	206	212	218	215	196	190	0
T 11 80	202	203	201	199	201	207	211	214	222	225	0
T 11 85	203	203	199	196	199	203	209	213	215	216	0
T 11 90	193	192	191	194	200	207	211	212	213	210	0
T 11 95	187	191	196	202	208	214	215	212	210	210	0
T 11 100	193	200	210	219	222	220	215	209	205	204	0
T 11 105	219	227	239	245	241	231	217	206	199	197	0
T 11 110	269	282	286	284	272	253	231	212	201	197	0
T 12 25	220	221	222	219	217	221	216	210	206	205	0
T 12 30	234	234	229	229	224	221	216	211	208	207	0
T 12 35	249	248	243	240	234	225	219	218	215	214	0
T 12 40	259	259	257	255	248	236	228	227	220	218	0
T 12 45	268	267	270	268	263	248	242	243	234	231	0
T 12 50	272	272	273	271	266	257	254	258	255	254	0
T 12 55	269	268	267	265	261	255	253	256	258	259	0
T 12 60	255	255	254	252	248	247	247	245	247	248	0
T 12 65	232	230	233	236	235	238	240	233	238	240	0
T 12 70	208	208	211	216	222	228	201	224	206	200	0
T 12 75	199	200	202	204	212	218	222	217	198	192	0
T 12 80	201	201	198	198	204	211	214	214	219	221	0
T 12 85	199	200	198	197	201	207	213	214	215	215	0

T 12 90	189	188	189	194	203	213	217	217	217	217	0
T 12 95	184	184	187	196	207	219	222	219	217	217	0
T 12 100	191	193	197	204	212	220	221	217	215	214	0
T 12 105	215	220	225	225	222	219	215	211	209	208	0
T 12 110	261	270	271	263	250	238	227	216	209	207	0
T 13 25	219	220	221	222	221	222	222	220	218	217	0
T 13 30	232	233	232	231	229	228	227	225	224	224	0
T 13 35	247	247	244	241	240	238	236	233	234	234	0
T 13 40	260	259	257	255	254	252	248	244	244	244	0
T 13 45	269	269	269	268	267	264	261	258	257	257	0
T 13 50	273	273	273	272	270	268	267	267	270	271	0
T 13 55	269	268	266	264	262	262	262	263	263	263	0
T 13 60	252	252	251	249	247	248	251	251	247	246	0
T 13 65	230	231	233	233	231	233	237	236	230	228	0
T 13 70	210	212	215	216	216	219	223	222	207	203	0
T 13 75	200	202	205	205	205	206	209	208	198	194	0
T 13 80	198	199	199	197	195	194	194	194	206	210	0
T 13 85	198	197	196	192	188	185	184	184	184	184	0
T 13 90	193	192	191	189	187	185	184	183	183	183	0
T 13 95	193	193	194	196	197	197	195	194	193	193	0
T 13 100	206	206	207	209	211	213	214	213	212	212	0
T 13 105	235	234	232	230	230	233	236	236	239	239	0
T 13 110	283	280	273	268	265	268	271	271	271	271	0

STATIONARY PERTURBATIONS, (S)

S 1 30 10	-2	-11	-34	-43	0	3	-3	-13	-3	0	-2	-6	-16	-41	0
S 1 30 40	-2	-11	-43	-75	0	3	-8	-13	-23	0	-2	-1	-34	-51	0
S 1 30 70	-10	-11	-79	-75	0	-30	-14	-37	-43	0	19	3	-43	-36	0
S 1 30 100	-2	-20	-16	-32	0	-2	-14	15	-10	0	2	-10	-34	-17	0
S 1 30 130	-2	14	47	77	0	3	25	50	56	0	-2	-10	-7	21	0
S 1 30 160	-2	14	93	153	0	9	14	85	102	0	-11	-1	11	49	0
S 1 30 190	23	31	93	131	0	20	19	50	63	0	-2	12	43	63	0
S 1 30 220	6	14	47	66	0	9	14	-13	10	0	-6	3	61	59	0
S 1 30 250	-10	-3	-7	-21	0	-13	-14	-48	-36	0	-2	8	38	25	0
S 1 30 280	6	6	-34	-64	0	-2	3	-37	-56	0	6	-1	2	-8	0
S 1 30 310	-2	-11	-34	-64	0	-8	-14	-19	-36	0	6	3	-7	-27	0
S 1 30 340	-2	-11	-34	-53	0	9	-8	-19	-23	0	-6	-1	-16	-36	0
S 1 40 10	-17	2	-2	48	0	-16	-14	-8	69	0	1	16	5	-23	0
S 1 40 40	1	17	-2	33	0	2	-1	-3	31	0	1	20	0	-2	0
S 1 40 70	12	31	-21	-324	0	13	20	-38	-351	0	-3	12	17	41	0
S 1 40 100	15	-12	-75	-24	0	21	-19	-115	-51	0	-7	4	46	28	0
S 1 40 130	5	-45	-52	10	0	2	-48	-43	-32	0	5	4	-12	41	0
S 1 40 160	8	-5	37	62	0	5	-4	50	47	0	1	-4	-12	11	0
S 1 40 190	12	6	80	90	0	8	20	106	105	0	1	-15	-25	-10	0
S 1 40 220	15	2	37	62	0	16	20	56	69	0	-3	-19	-20	-10	0
S 1 40 250	8	-12	18	29	0	10	2	20	31	0	-3	-12	-12	-6	0
S 1 40 280	-17	13	-9	-10	0	-16	30	-3	6	0	1	-15	-4	-19	0
S 1 40 310	-17	6	-6	-5	0	-22	9	-6	22	0	5	-4	0	-27	0
S 1 40 340	-24	-2	-6	29	0	-24	-14	-24	54	0	1	12	17	-23	0
S 1 52 10	11	40	62	17	0	7	37	70	41	0	5	2	-8	-22	0
S 1 52 40	21	73	68	7	0	15	65	73	6	0	5	9	-5	2	0
S 1 52 70	31	72	64	4	0	26	63	51	-18	0	5	9	11	22	0
S 1 52 100	6	16	3	7	0	9	25	-5	-11	0	-3	-10	7	18	0
S 1 52 130	-10	-21	3	32	0	3	-8	8	9	0	-14	-13	-5	22	0
S 1 52 160	-14	-3	40	42	0	-14	-15	20	32	0	1	13	11	10	0
S 1 52 190	-5	-14	-10	32	0	1	-18	-14	11	0	-6	5	3	22	0
S 1 52 220	-7	-52	-38	17	0	-1	-47	-47	2	0	-6	-6	11	14	0

S 1 52	250	-14	-45	-36	-39	0	-11	-39	-44	-34	0	-3	-6	7	-6	0
S 1 52	280	-19	-40	-40	-51	0	-23	-39	-35	-30	0	5	-2	-5	-22	0
S 1 52	310	-7	-29	-49	-54	0	-11	-28	-32	-23	0	5	-2	-16	-30	0
S 1 52	340	5	2	-67	-16	0	-1	3	-54	15	0	5	2	-12	-30	0
S 1 60	10	17	43	53	-5	0	12	40	50	7	0	4	4	-2	-13	0
S 1 60	40	26	82	65	10	0	22	76	60	7	0	4	4	-2	0	0
S 1 60	70	36	77	77	25	0	32	76	60	13	0	4	4	6	8	0
S 1 60	100	3	8	11	25	0	6	12	5	13	0	0	-4	2	8	0
S 1 60	130	-21	-31	-1	48	0	-15	-23	0	44	0	-8	-8	-2	8	0
S 1 60	160	-16	8	47	48	0	-11	2	42	49	0	0	4	6	4	0
S 1 60	190	-11	-11	-7	48	0	-8	-12	-0	44	0	-4	0	2	8	0
S 1 60	220	-11	-56	-31	33	0	-8	-54	-33	23	0	-4	-4	2	8	0
S 1 60	250	-16	-51	-31	-43	0	-15	-47	-33	-45	0	0	-4	6	0	0
S 1 60	280	-16	-41	-43	-66	0	-18	-40	-42	-60	0	0	0	-2	-5	0
S 1 60	310	-2	-31	-61	-81	0	-4	-30	-54	-65	0	4	0	-10	-13	0
S 1 60	340	12	3	-79	-43	0	6	2	-71	-29	0	4	0	-6	-13	0
S 1 68	10	18	45	51	-13	0	13	47	53	-13	0	-1	1	-5	-3	0
S 1 68	40	29	83	60	6	0	32	87	65	3	0	-1	-3	-5	-3	0
S 1 68	70	39	83	79	29	0	42	87	70	33	0	-1	-3	-5	-3	0
S 1 68	100	2	4	12	25	0	4	7	16	33	0	-1	-3	-1	-3	0
S 1 68	130	-26	-36	-4	55	0	-24	-32	4	63	0	-1	1	-1	-7	0
S 1 68	160	-14	11	51	48	0	-15	7	53	48	0	-1	1	-1	-7	0
S 1 68	190	-14	-10	-4	51	0	-15	-12	-0	63	0	-1	1	-1	-7	0
S 1 68	220	-14	-57	-28	32	0	-15	-62	-33	33	0	-1	1	3	-3	0
S 1 68	250	-17	-52	-25	-39	0	-15	-52	-33	-43	0	-1	1	3	6	0
S 1 68	280	-14	-40	-45	-67	0	-15	-42	-45	-73	0	3	1	3	11	0
S 1 68	310	-2	-30	-67	-81	0	-6	-32	-60	-89	0	3	1	3	11	0
S 1 68	340	12	1	-78	-46	0	13	-2	-82	-58	0	3	1	8	6	0
S 1 76	10	18	40	39	-9	0	18	48	51	-17	0	-6	-7	-6	5	0
S 1 76	40	28	71	51	6	0	32	89	50	7	0	-6	-17	-11	1	0
S 1 76	70	37	71	69	21	0	41	89	82	32	0	-6	-17	-15	-8	0
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S 1 76	130	-24	-32	-3	43	0	-31	-39	-6	57	0	4	7	3	-12	0
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S 1 76	250	-15	-47	-21	-31	0	-17	-57	-25	-37	0	4	12	3	5	0
S 1 76	280	-10	-32	-39	-53	0	-14	-42	-40	-66	0	4	7	8	14	0
S 1 76	310	-1	-27	-57	-68	0	-2	-32	-71	-81	0	-1	7	12	14	0
S 1 76	340	13	-1	-69	-39	0	15	-1	-82	-52	0	-1	-2	17	10	0
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S 1 84	310	-1	-19	-43	-53	0	0	-24	-53	-59	0	0	6	10	5	0
S 1 84	340	10	-1	-54	-28	0	13	-1	-63	-33	0	0	1	10	5	0
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S 1 90	40	16	40	34	9	0	20	47	35	5	0	0	-5	0	2	0
S 1 90	70	21	40	45	16	0	26	47	45	16	0	-5	-5	0	2	0
S 1 90	100	1	3	6	16	0	0	2	6	12	0	0	0	0	2	0
S 1 90	130	-19	-19	1	28	0	-19	-22	0	28	0	0	0	0	2	0

REPRODUCIBILITY OF THE ORIGINAL PAGE IS POOR

S 1 90	160	-9	8	29	28	0	-8	8	20	28	0	0	0	0	2	0
S 1 90	190	-9	-3	1	28	0	-11	-4	0	28	0	0	0	0	2	0
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S 1 90	250	-9	-29	-16	-23	0	-11	-31	-13	-23	0	0	5	0	-3	0
S 1 90	280	-9	-19	-27	-42	0	-8	-22	-26	-39	0	0	5	0	-3	0
S 1 90	310	1	-13	-38	-49	0	0	-16	-30	-47	0	0	0	0	-3	0
S 1 90	340	11	-3	-49	-23	0	9	-1	-40	-23	0	0	0	0	-3	0
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S 2 30	40	7	-1	-45	-126	0	-3	1	-27	-64	0	7	1	-23	-58	0
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S 2 30	100	-10	-9	0	18	0	-9	1	13	14	0	3	-8	-10	10	0
S 2 30	130	-1	-1	45	131	0	-3	6	47	105	0	3	-3	-1	28	0
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S 2 30	190	-10	8	63	162	0	2	6	47	92	0	-6	1	17	60	0
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S 2 30	340	-1	-9	-45	-126	0	-3	-16	-22	-77	0	3	6	-19	-49	0
S 2 40	10	-16	1	-23	-173	0	-20	-16	-48	-145	0	5	19	24	-33	0
S 2 40	40	-2	11	-58	-164	0	-9	-6	-87	-138	0	5	19	28	-29	0
S 2 40	70	23	22	-86	-140	0	23	2	-104	-122	0	1	19	20	-20	0
S 2 40	100	16	11	-78	-77	0	12	5	-62	-60	0	5	8	-16	-16	0
S 2 40	130	12	-10	-19	38	0	7	13	17	48	0	5	-24	-37	-4	0
S 2 40	160	16	-3	53	158	0	12	13	84	149	0	1	-16	-28	13	0
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S 2 60	310	-43	-88	-50	-98	0	-38	-85	-51	-99	0	-3	-3	1	4	0
S 2 60	340	16	17	-19	-121	0	21	14	-21	-131	0	-3	1	1	8	0
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S 2 68	40	67	127	39	-115	0	66	132	37	-130	0	-1	-3	-4	20	0

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S 2 68	190	-8	-15	39	147	0	-7	-18	37-166	0	4	-3	-4	-28	0
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S 3 68	280	-77	-106	-109	-72	0	-77	-108	-127	-82	0	3	4	11	9	0
S 3 68	310	-63	-97	-86	-63	0	-68	-99	-91	-68	0	3	4	11	9	0
S 3 68	340	-12	-35	-43	-74	0	-15	-32	-44	-82	0	3	0	2	9	0
S 3 76	10	32	48	5	-49	0	37	60	2	-67	0	-7	-10	0	15	0
S 3 76	40	46	83	11	-13	0	56	98	14	-20	0	-7	-15	0	6	0
S 3 76	70	50	78	34	-6	0	58	95	43	-6	0	-7	-15	-9	2	0
S 3 76	100	41	48	40	44	0	50	60	47	55	0	-7	-10	-9	-11	0
S 3 76	130	32	29	40	80	0	39	36	51	102	0	-7	-5	-9	-25	0
S 3 76	160	27	19	64	95	0	31	22	80	125	0	-7	-5	-14	-29	0
S 3 76	190	0	9	64	66	0	-1	10	80	93	0	-2	-5	-14	-20	0
S 3 76	220	-32	-46	-1	-13	0	-39	-55	-5	-20	0	7	9	0	6	0

S 3 76	250	-59	-61	-54	-35	0	-71	-75	-68	-48	0	12	14	14	11	0
S 3 76	280	-68	-91	-96	-56	0	-82	-111	-112	-72	0	12	19	18	15	0
S 3 76	310	-55	-86	-72	-49	0	-66	-102	-86	-67	0	12	19	14	15	0
S 3 76	340	-14	-31	-36	-64	0	-14	-37	-46	-76	0	2	4	9	15	0
S 3 84	10	24	37	3	-37	0	26	47	8	-44	0	-8	-12	3	10	0
S 3 84	40	33	60	9	-10	0	45	79	8	-15	0	-8	-18	-2	5	0
S 3 84	70	36	58	28	0	0	45	79	32	0	0	-8	-18	-7	0	0
S 3 84	100	33	37	31	30	0	45	47	32	44	0	-8	-12	-7	-9	0
S 3 84	130	25	21	33	52	0	35	26	45	73	0	-8	-7	-7	-19	0
S 3 84	160	18	12	50	62	0	26	15	57	88	0	-8	-2	-12	-19	0
S 3 84	190	-2	6	50	49	0	-4	5	57	59	0	-3	-2	-12	-14	0
S 3 84	220	-26	-33	-1	-5	0	-32	-43	-2	-12	0	8	9	3	5	0
S 3 84	250	-42	-46	-44	-24	0	-56	-60	-52	-34	0	13	14	8	10	0
S 3 84	280	-50	-68	-73	-39	0	-64	-87	-87	-52	0	13	19	13	10	0
S 3 84	310	-41	-64	-58	-37	0	-53	-82	-68	-47	0	13	19	13	10	0
S 3 84	340	-8	-21	-27	-42	0	-14	-27	-30	-59	0	3	9	8	10	0
S 3 90	10	17	27	5	-30	0	22	34	4	-31	0	-2	-7	2	1	0
S 3 90	40	23	43	10	-4	0	31	55	7	-8	0	-7	-12	2	1	0
S 3 90	70	28	43	22	3	0	34	55	26	0	0	-7	-7	-3	1	0
S 3 90	100	23	27	27	22	0	31	34	26	27	0	-7	-7	-3	1	0
S 3 90	130	17	16	27	42	0	22	19	20	46	0	-2	-1	-3	-4	0
S 3 90	160	12	10	44	49	0	16	10	46	53	0	-2	-1	-3	-4	0
S 3 90	190	-3	5	44	42	0	-1	4	46	42	0	-2	-1	-3	-4	0
S 3 90	220	-19	-23	-1	-4	0	-24	-29	0	-4	0	3	4	2	1	0
S 3 90	250	-30	-34	-35	-17	0	-38	-41	-30	-23	0	8	9	2	1	0
S 3 90	280	-35	-51	-69	-37	0	-47	-62	-68	-34	0	8	9	2	1	0
S 3 90	310	-30	-45	-52	-30	0	-38	-56	-52	-31	0	8	9	2	1	0
S 3 90	340	-3	-17	-24	-37	0	-7	-20	-26	-38	0	3	4	2	1	0
S 4 30	10	-4	-8	-2	-4	0	-2	0	-1	15	0	-4	-9	-3	-17	0
S 4 30	40	-4	-8	-2	-4	0	-7	-5	-1	10	0	0	-5	-7	-13	0
S 4 30	70	4	1	-2	4	0	4	-5	5	4	0	0	8	-7	-4	0
S 4 30	100	4	1	-2	22	0	-7	-11	10	21	0	9	12	-12	-4	0
S 4 30	130	-4	-8	6	40	0	-7	-11	10	44	0	0	8	-12	-4	0
S 4 30	160	-12	1	15	40	0	-18	0	21	38	0	5	-1	-7	5	0
S 4 30	190	4	9	24	40	0	-2	0	32	21	0	9	4	-7	18	0
S 4 30	220	4	1	15	4	0	9	11	-6	-19	0	-4	-5	24	27	0
S 4 30	250	4	1	-2	-31	0	9	5	-23	-42	0	-4	-1	24	14	0
S 4 30	280	12	9	-19	-48	0	15	5	-34	-48	0	-4	-1	15	5	0
S 4 30	310	-4	1	-19	-40	0	4	5	-17	-42	0	-4	-5	2	-4	0
S 4 30	340	-4	1	-11	-22	0	4	5	5	-2	0	-4	-5	-12	-22	0
S 4 40	10	-1	-6	0	-35	0	-9	-17	-5	-27	0	7	11	5	-7	0
S 4 40	40	-5	5	-4	-39	0	-9	3	0	-36	0	3	3	-3	-7	0
S 4 40	70	12	18	-11	-35	0	17	23	-3	-30	0	-4	-5	-7	-7	0
S 4 40	100	15	18	-15	-15	0	22	28	0	-1	0	-4	-9	-15	-11	0
S 4 40	130	9	8	-4	18	0	12	16	5	20	0	-4	-9	-11	-3	0
S 4 40	160	9	8	11	38	0	6	16	16	34	0	0	-9	-3	1	0
S 4 40	190	-15	5	37	62	0	-14	16	40	54	0	0	-13	-3	9	0
S 4 40	220	-11	5	55	58	0	-6	11	50	46	0	-4	-5	-3	13	0
S 4 40	250	-11	-6	18	58	0	-11	-12	16	49	0	0	3	1	9	0
S 4 40	280	-11	-33	-26	-31	0	-14	-41	-40	-38	0	0	11	13	9	0
S 4 40	310	2	-19	-37	-39	0	-1	-29	-54	-38	0	3	11	16	1	0
S 4 40	340	9	-2	-23	-39	0	6	-14	-35	-33	0	3	11	13	-7	0
S 4 52	10	7	20	-1	-18	0	8	24	-8	-25	0	0	-5	6	9	0
S 4 52	40	10	28	3	-30	0	7	28	-4	-35	0	4	-1	6	5	0
S 4 52	70	19	19	-3	-32	0	15	16	-8	-43	0	4	2	6	9	0
S 4 52	100	15	11	-13	-28	0	11	4	-10	-35	0	4	6	6	5	0
S 4 52	130	3	-6	-23	-3	0	-4	-13	-28	-7	0	8	6	6	5	0

REPRODUCIBILITY OF THE ORIGINAL PAGE IS POOR

S 4 52	160	-1	6	6	29	0	-2	7	11	29	0	4	-1	-5	1	0
S 4 52	190	-5	6	30	52	0	-7	7	37	57	0	0	-1	-5	-6	0
S 4 52	220	-2	5	29	52	0	0	10	40	61	0	-3	-5	-12	-10	0
S 4 52	250	-5	-19	6	18	0	-2	-20	11	27	0	-3	2	-5	-10	0
S 4 52	280	-26	-33	-11	-18	0	-23	-38	-11	-14	0	-3	6	-1	-2	0
S 4 52	310	-13	-28	-13	-15	0	-7	-26	-11	-13	0	-7	-1	-1	1	0
S 4 52	340	-2	-8	-10	-7	0	3	1	0	-1	0	-7	-9	-1	-6	0
S 4 60	10	5	19	4	-16	0	8	19	0	-17	0	-3	-3	4	1	0
S 4 60	40	13	27	9	-27	0	11	28	4	-28	0	1	1	4	1	0
S 4 60	70	22	23	4	-21	0	20	19	0	-28	0	1	1	4	5	0
S 4 60	100	17	19	-6	-21	0	14	12	-10	-24	0	1	5	4	5	0
S 4 60	130	9	-3	-21	0	0	5	-4	-21	-1	0	5	5	0	1	0
S 4 60	160	0	6	4	28	0	-1	6	4	30	0	1	1	-4	1	0
S 4 60	190	-4	6	23	49	0	-4	6	28	49	0	1	1	-4	1	0
S 4 60	220	-4	1	18	44	0	-4	3	25	49	0	1	-3	-4	-3	0
S 4 60	250	-8	-20	4	11	0	-7	-16	4	14	0	-3	1	-4	-3	0
S 4 60	280	-29	-29	-11	-21	0	-28	-32	-10	-21	0	-3	1	0	-3	0
S 4 60	310	-17	-33	-16	-16	0	-13	-29	-14	-13	0	-3	-3	-4	-3	0
S 4 60	340	-4	-16	-11	-10	0	-4	-10	-10	-9	0	-3	-7	0	-3	0
S 4 68	10	3	16	9	-13	0	8	16	0	-21	0	-3	-3	4	1	0
S 4 68	40	13	30	11	-24	0	16	25	0	-32	0	1	2	4	1	0
S 4 68	70	23	23	5	-18	0	25	25	-1	-21	0	1	2	-1	5	0
S 4 68	100	19	21	-6	-18	0	16	16	-11	-21	0	1	2	4	5	0
S 4 68	130	11	3	-18	1	0	8	-1	-21	1	0	1	2	4	1	0
S 4 68	160	0	4	0	29	0	-1	8	-1	34	0	1	-3	-1	-4	0
S 4 68	190	-2	4	20	49	0	-1	8	20	55	0	1	-3	-5	-4	0
S 4 68	220	-4	-2	15	41	0	-1	-1	19	44	0	1	-3	-5	-4	0
S 4 68	250	-8	-18	0	8	0	-9	-18	-1	12	0	-3	2	-1	-4	0
S 4 68	280	-29	-27	-10	-24	0	-35	-26	-11	-21	0	1	2	-1	1	0
S 4 68	310	-19	-32	-17	-18	0	-18	-35	-11	-21	0	-3	2	-1	1	0
S 4 68	340	-7	-21	-9	-13	0	-9	-18	-11	-10	0	-3	-3	-1	1	0
S 4 76	10	5	14	10	-9	0	3	16	11	-13	0	1	-1	0	5	0
S 4 76	40	9	28	10	-16	0	13	32	15	-24	0	-4	-6	0	5	0
S 4 76	70	23	19	5	-9	0	26	24	5	-17	0	-4	-1	0	5	0
S 4 76	100	18	19	-5	-16	0	21	24	-4	-17	0	-4	-1	0	5	0
S 4 76	130	9	5	-16	3	0	13	3	-20	2	0	-4	-1	4	0	0
S 4 76	160	0	5	0	22	0	0	6	-1	33	0	1	-1	0	-9	0
S 4 76	190	0	5	16	34	0	0	6	21	52	0	1	-1	-5	-14	0
S 4 76	220	-5	-4	10	34	0	-5	-5	15	44	0	1	-1	-5	-14	0
S 4 76	250	-9	-17	0	3	0	-11	-20	-1	6	0	1	4	0	-4	0
S 4 76	280	-28	-22	-10	-22	0	-32	-28	-14	-28	0	6	4	4	10	0
S 4 76	310	-18	-31	-16	-16	0	-21	-33	-17	-21	0	6	4	4	5	0
S 4 76	340	-5	-22	-5	-9	0	-8	-23	-10	-17	0	1	4	0	5	0
S 4 84	10	2	8	6	-4	0	2	16	11	-2	0	-2	-2	-3	6	0
S 4 84	40	8	19	8	-9	0	11	26	11	-15	0	-2	-8	-3	6	0
S 4 84	70	15	16	4	-6	0	21	16	0	-15	0	-7	-2	2	6	0
S 4 84	100	13	16	-2	-6	0	21	16	0	-15	0	-2	-2	2	6	0
S 4 84	130	9	5	-10	1	0	11	6	-11	-2	0	-2	-2	2	1	0
S 4 84	160	0	3	0	10	0	2	6	0	24	0	-2	-2	2	-9	0
S 4 84	190	0	3	10	17	0	2	6	11	37	0	-2	-2	-3	-15	0
S 4 84	220	-4	-4	6	15	0	-8	-3	11	24	0	-2	-2	-3	-15	0
S 4 84	250	-6	-12	0	3	0	-8	-13	0	11	0	4	3	2	-4	0
S 4 84	280	-19	-15	-6	-9	0	-28	-23	-11	-15	0	9	9	2	6	0
S 4 84	310	-13	-21	-10	-6	0	-18	-32	-11	-15	0	4	9	2	6	0
S 4 84	340	-6	-17	-6	-4	0	-8	-23	-11	-15	0	4	3	2	6	0
S 4 90	10	0	7	8	2	0	0	9	6	-4	0	0	-5	-2	0	0
S 4 90	40	6	13	8	-5	0	6	18	0	-7	0	0	-5	-2	5	0

S 4 90	70	11	13	3	2	0	12	15	3	-4	0	-5	-5	-2	5	0
S 4 90	100	11	13	-3	2	0	12	15	-1	-4	0	-5	0	-2	5	0
S 4 90	130	6	2	-8	2	0	9	4	-10	0	0	0	0	3	0	0
S 4 90	160	0	2	-3	2	0	0	1	-1	7	0	0	0	-2	-6	0
S 4 90	190	0	2	8	2	0	0	1	0	15	0	0	0	-2	-11	0
S 4 90	220	0	-4	3	2	0	-2	-2	6	11	0	0	0	-2	-11	0
S 4 90	250	-6	-9	-3	2	0	-5	-11	-1	0	0	0	0	-2	0	0
S 4 90	280	-11	-9	-3	-5	0	-17	-14	-7	-7	0	6	6	3	5	0
S 4 90	310	-11	-15	-8	-5	0	-11	-19	-10	-4	0	0	6	3	5	0
S 4 90	340	-6	-15	-3	2	0	-5	-16	-4	-4	0	0	0	3	5	0
S 5 30	10	1	-5	-7	-1	0	0	-10	-4	16	0	-5	3	0	-14	0
S 5 30	40	1	-5	1	-1	0	-5	-5	1	11	0	0	3	0	-14	0
S 5 30	70	9	3	-7	-1	0	11	-5	-3	0	0	0	3	0	-5	0
S 5 30	100	1	3	-16	-9	0	-5	1	-3	-10	0	4	3	0	-1	0
S 5 30	130	-8	3	-7	-9	0	-5	1	-3	-5	0	0	3	0	-5	0
S 5 30	160	1	-5	-7	-9	0	-5	-15	-15	-10	0	8	7	4	4	0
S 5 30	190	9	-5	1	-1	0	0	-5	1	-10	0	8	3	0	8	0
S 5 30	220	-8	-5	9	7	0	-5	1	17	0	0	0	-6	-9	8	0
S 5 30	250	1	11	9	7	0	0	17	-4	-10	0	4	-10	13	16	0
S 5 30	280	9	11	17	7	0	6	17	12	0	0	0	-1	0	8	0
S 5 30	310	-8	3	9	7	0	0	6	12	6	0	-5	-6	-4	4	0
S 5 30	340	-8	-5	1	7	0	6	-5	7	11	0	-13	-1	-4	-9	0
S 5 40	10	13	3	-9	-7	0	11	1	-13	-13	0	2	1	4	7	0
S 5 40	40	-7	6	-12	-10	0	-11	8	-16	-13	0	2	-3	4	4	0
S 5 40	70	-7	-17	-2	-7	0	-8	-21	-3	-1	0	2	5	0	-4	0
S 5 40	100	0	-20	4	-3	0	-6	-26	-3	1	0	6	9	7	-4	0
S 5 40	130	-7	6	-6	-3	0	-8	1	-11	-4	0	2	5	4	0	0
S 5 40	160	-10	6	-9	-16	0	-13	8	-8	-13	0	2	-3	0	-4	0
S 5 40	190	-10	0	-22	-7	0	-11	5	-18	-1	0	-2	-3	-4	-4	0
S 5 40	220	-4	0	-12	6	0	-1	5	-8	8	0	-2	-3	-4	0	0
S 5 40	250	-7	3	34	22	0	-3	3	41	23	0	-2	1	-8	-4	0
S 5 40	280	10	6	24	16	0	13	8	29	15	0	-6	-3	-4	0	0
S 5 40	310	19	3	11	6	0	25	3	12	1	0	-6	1	0	4	0
S 5 40	340	10	3	1	3	0	11	5	-1	-1	0	-2	-3	4	7	0
S 5 52	10	0	-19	-1	8	0	2	-17	-2	6	0	-1	-2	2	3	0
S 5 52	40	2	-15	0	1	0	-2	-12	0	1	0	3	-2	2	-1	0
S 5 52	70	6	1	6	0	0	10	2	1	-2	0	-4	-2	5	-1	0
S 5 52	100	6	1	15	5	0	6	-5	0	4	0	-1	6	5	3	0
S 5 52	130	2	2	11	10	0	-5	0	6	9	0	7	2	5	3	0
S 5 52	160	2	10	-7	-14	0	3	11	-8	-10	0	-1	-2	-2	-4	0
S 5 52	190	-4	-1	-22	-11	0	-3	-4	-17	-7	0	-1	2	-5	-4	0
S 5 52	220	-4	-7	-18	-5	0	-3	-5	-15	-2	0	-1	-2	-5	-4	0
S 5 52	250	-4	-4	-4	-3	0	-3	-2	3	-3	0	-1	-2	-9	-1	0
S 5 52	280	-3	1	6	-3	0	-2	2	13	-3	0	-1	-2	-5	-1	0
S 5 52	310	-3	-3	11	-3	0	-2	0	0	-9	0	-1	-2	2	3	0
S 5 52	340	-1	35	5	15	0	-1	31	1	15	0	-1	6	5	3	0
S 5 60	10	0	-22	0	11	0	-1	-19	-2	9	0	-1	-1	0	0	0
S 5 60	40	4	-18	0	3	0	3	-16	1	0	0	3	-1	0	0	0
S 5 60	70	4	-1	12	-1	0	6	-1	7	0	0	-1	-1	4	0	0
S 5 60	100	8	7	20	7	0	6	3	16	6	0	-1	3	4	0	0
S 5 60	130	8	3	16	11	0	3	3	13	12	0	3	-1	4	0	0
S 5 60	160	0	7	-9	-16	0	3	9	-8	-15	0	-1	-1	0	0	0
S 5 60	190	-5	3	-29	-12	0	-4	-1	-23	-12	0	-1	3	-4	0	0
S 5 60	220	-5	-9	-21	-9	0	-4	-7	-20	-6	0	-1	-1	-4	0	0
S 5 60	250	-5	-5	-9	-5	0	-4	-4	-8	-3	0	-1	-1	-4	0	0
S 5 60	280	-5	-1	0	-5	0	-4	-1	4	-3	0	-1	-1	-4	0	0
S 5 60	310	-5	-5	12	-1	0	-4	-4	10	-3	0	-1	-1	0	4	0

REPRODUCIBILITY OF THE
ORIGINAL PAGE IS POOR

S 5 60	340	0	40	8	15	0	-1	36	7	15	0	-1	3	0	0	0
S 5 68	10	-2	-22	-2	10	0	-4	-18	-4	8	0	-1	0	-1	0	0
S 5 68	40	7	-18	0	2	0	4	-18	4	0	0	3	0	-1	0	0
S 5 68	70	2	-1	13	2	0	4	-2	12	0	0	-1	0	3	0	0
S 5 68	100	7	9	23	6	0	4	6	20	8	0	-1	0	3	0	0
S 5 68	130	11	6	17	10	0	13	6	12	8	0	3	0	3	0	0
S 5 68	160	1	7	-7	-18	0	4	6	-4	-16	0	-1	0	3	0	0
S 5 68	190	-6	4	-29	-14	0	-4	6	-20	-16	0	-1	0	-1	0	0
S 5 68	220	-6	-9	-21	-8	0	-4	-10	-20	-8	0	-1	0	-1	0	0
S 5 68	250	-6	-8	-13	-5	0	-4	-10	-12	0	0	-1	0	-1	0	0
S 5 68	280	-4	-1	-3	-5	0	-4	-2	-4	0	0	-1	0	-1	0	0
S 5 68	310	-4	-5	12	4	0	-4	-2	12	0	0	-1	0	-1	0	0
S 5 68	340	-2	39	8	16	0	-4	39	12	16	0	3	0	-1	0	0
S 5 76	10	-4	-22	-3	7	0	-2	-24	-2	12	0	0	3	2	-1	0
S 5 76	40	5	-18	2	2	0	9	-19	0	2	0	0	3	2	-1	0
S 5 76	70	1	0	15	2	0	3	-1	15	2	0	0	3	-3	-1	0
S 5 76	100	5	9	24	7	0	9	9	25	7	0	0	-3	-3	-1	0
S 5 76	130	14	5	15	7	0	14	6	12	12	0	0	-3	-3	-1	0
S 5 76	160	1	5	-7	-16	0	1	9	-7	-20	0	0	-3	2	4	0
S 5 76	190	-4	5	-29	-16	0	-7	4	-32	-15	0	0	-3	7	4	0
S 5 76	220	-4	-9	-20	-7	0	-7	-9	-22	-10	0	0	3	2	-1	0
S 5 76	250	-4	-9	-11	-2	0	-7	-9	-15	-6	0	0	3	2	-1	0
S 5 76	280	-4	0	-3	-2	0	-5	-1	-5	-6	0	0	3	2	-1	0
S 5 76	310	-4	-4	11	7	0	-5	-6	13	7	0	0	3	-3	-1	0
S 5 76	340	-4	37	6	11	0	-2	42	10	17	0	0	-8	-3	-1	0
S 5 84	10	-1	-14	-2	6	0	-6	-24	-5	13	0	-1	6	-2	-5	0
S 5 84	40	7	-12	0	2	0	4	-14	-5	3	0	-1	6	-2	2	0
S 5 84	70	1	0	10	2	0	4	-4	14	3	0	-1	0	-2	2	0
S 5 84	100	5	8	18	4	0	4	6	23	3	0	-1	0	-2	-5	0
S 5 84	130	10	6	14	4	0	14	6	14	13	0	-1	0	-2	-5	0
S 5 84	160	-1	4	-4	-12	0	4	6	-5	-16	0	-1	0	-2	2	0
S 5 84	190	-5	4	-22	-10	0	-6	6	-23	-16	0	4	0	5	2	0
S 5 84	220	-5	-6	-14	-5	0	-6	-4	-14	-6	0	4	0	5	2	0
S 5 84	250	-5	-6	-12	-3	0	-6	-4	-14	-6	0	4	0	5	2	0
S 5 84	280	-3	0	-4	-3	0	-6	-4	-5	-6	0	-1	0	-2	2	0
S 5 84	310	-3	-4	8	6	0	-6	-4	14	3	0	-1	0	-2	2	0
S 5 84	340	-1	24	6	9	0	4	35	5	13	0	-1	-12	-2	-5	0
S 5 90	10	-2	-9	-1	-1	0	-2	-12	-2	6	0	0	4	3	-5	0
S 5 90	40	4	-9	-1	-1	0	7	-12	0	3	0	0	4	3	-5	0
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S 5 90	100	4	4	12	-1	0	4	7	16	3	0	0	-1	-3	-5	0
S 5 90	130	9	4	12	-1	0	10	3	13	3	0	0	-1	-3	-5	0
S 5 90	160	-2	4	-1	-1	0	1	3	-3	-13	0	0	-1	3	9	0
S 5 90	190	-2	4	-14	-1	0	-5	3	-10	-9	0	0	-1	3	2	0
S 5 90	220	-2	-2	-8	-1	0	-5	-6	-12	-5	0	0	4	3	2	0
S 5 90	250	-2	-2	-8	-1	0	-5	-6	-10	-1	0	0	4	3	2	0
S 5 90	280	-2	-2	-8	-1	0	-2	0	-6	-1	0	0	-1	-3	2	0
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S 6 30	10	3	-7	-5	-4	0	11	-17	-2	4	0	-9	9	0	-6	0
S 6 30	40	3	-7	-5	-11	0	0	-7	-7	-6	0	0	4	4	-6	0
S 6 30	70	3	1	-5	-11	0	0	-1	-12	-16	0	4	0	9	2	0
S 6 30	100	3	1	-5	-11	0	-5	-1	-7	-16	0	4	0	0	2	0
S 6 30	130	-5	1	-13	-11	0	-11	-7	-17	-11	0	4	4	9	2	0
S 6 30	160	3	1	-5	-4	0	-5	-1	-12	-11	0	4	4	9	6	0
S 6 30	190	3	1	-5	4	0	0	-1	-7	-1	0	4	4	4	6	0
S 6 30	220	-5	1	3	11	0	0	9	0	9	0	0	-9	-4	2	0

S 6 30	250	3	1	18	11	0	0	15	20	9	0	0	-9	-13	2	0
S 6 30	280	3	17	10	11	0	5	15	0	9	0	0	0	-4	2	0
S 6 30	310	-5	-7	10	11	0	5	4	14	14	0	-9	-9	-9	-2	0
S 6 30	340	-5	-7	3	4	0	0	-7	3	14	0	-4	0	-4	-11	0
S 6 40	10	-1	-2	0	6	0	-8	-4	0	9	0	6	1	0	-2	0
S 6 40	40	2	-2	3	6	0	0	1	7	7	0	2	-3	-3	-2	0
S 6 40	70	-5	-2	0	0	0	-5	-4	0	2	0	2	1	0	-2	0
S 6 40	100	-1	-2	-6	0	0	-8	-4	-5	0	0	6	1	0	-2	0
S 6 40	130	-1	-2	-6	-3	0	2	1	-7	-2	0	-2	-3	0	-2	0
S 6 40	160	-1	-2	-6	-3	0	4	1	-7	-2	0	-6	-3	0	-2	0
S 6 40	190	-5	-5	-6	-44	0	-3	-4	-7	-47	0	-2	1	0	2	0
S 6 40	220	-1	-2	-3	0	0	-3	-1	-3	-2	0	2	1	0	2	0
S 6 40	250	2	5	3	9	0	4	4	4	7	0	-2	1	0	2	0
S 6 40	280	2	5	6	14	0	4	4	7	13	0	-2	1	0	2	0
S 6 40	310	5	5	10	11	0	7	4	0	11	0	-2	1	0	2	0
S 6 40	340	5	2	3	6	0	4	1	4	4	0	-2	1	0	2	0
S 6 52	10	-4	-3	-6	-2	0	-11	-10	-6	-2	0	5	9	1	3	0
S 6 52	40	-4	-8	-4	-6	0	0	-10	-6	-12	0	1	9	1	6	0
S 6 52	70	-5	-13	-6	-3	0	-11	-10	-6	-2	0	1	9	1	-1	0
S 6 52	100	-11	-4	-6	-7	0	-11	-10	-6	-2	0	1	-59	1	-1	0
S 6 52	130	-13	-16	-9	-9	0	-11	-10	-6	-12	0	-3	1	-2	-1	0
S 6 52	160	-13	-14	-11	-13	0	-11	-10	-6	-12	0	-3	-3	-6	-1	0
S 6 52	190	-11	-14	-13	-13	0	-11	-10	-6	-12	0	-3	1	-6	-1	0
S 6 52	220	-5	2	-7	-7	0	0	1	-6	-2	0	-3	1	-2	-1	0
S 6 52	250	4	17	8	11	0	11	23	4	8	0	-3	1	1	-1	0
S 6 52	280	21	24	21	21	0	23	23	15	18	0	1	9	5	-1	0
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S 6 52	340	18	7	12	10	0	11	1	15	8	0	1	9	1	-1	0
S 6 60	10	3	3	-4	-4	0	-3	0	-5	-1	0	5	5	1	-1	0
S 6 60	40	-6	-9	-4	0	0	-3	-6	-5	-4	0	-3	-3	1	3	0
S 6 60	70	3	-17	-4	-4	0	-6	-11	-5	-4	0	5	-7	1	-1	0
S 6 60	100	-10	11	-4	-10	0	-12	-17	-5	-7	0	1	33	1	-4	0
S 6 60	130	-14	-21	-11	-7	0	-12	-14	-10	-9	0	1	-7	-3	3	0
S 6 60	160	-14	-17	-15	-14	0	-12	-14	-13	-14	0	1	-3	-3	-1	0
S 6 60	190	-10	-17	-19	-14	0	-12	-14	-13	-14	0	1	-7	-3	-1	0
S 6 60	220	-10	3	-8	-10	0	-6	3	-8	-7	0	-3	1	1	-4	0
S 6 60	250	-1	11	11	13	0	3	17	0	11	0	-7	-7	1	3	0
S 6 60	280	16	23	26	24	0	22	26	22	21	0	-3	-3	5	3	0
S 6 60	310	20	19	26	17	0	22	23	22	19	0	-3	-7	5	-1	0
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S 6 68	10	13	5	-5	-3	0	5	7	-6	-1	0	5	2	1	1	0
S 6 68	40	-13	-7	-5	-3	0	-12	-9	-6	-1	0	-3	-3	1	1	0
S 6 68	70	13	-19	-5	-3	0	5	-17	-6	-1	0	5	-3	1	1	0
S 6 68	100	-13	42	-5	-14	0	-12	22	-6	-14	0	1	15	1	-4	0
S 6 68	130	-13	-32	-16	-3	0	-12	-25	-13	-8	0	1	-3	1	1	0
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S 6 68	250	-13	5	18	17	0	-4	7	0	12	0	-3	-3	1	1	0
S 6 68	280	13	17	29	27	0	14	22	30	26	0	-3	-3	1	1	0
S 6 68	310	27	5	29	17	0	23	15	30	19	0	-3	-3	1	1	0
S 6 68	340	27	17	7	7	0	31	15	0	12	0	1	2	-3	1	0
S 6 76	10	11	8	-6	-3	0	13	7	-6	-3	0	-2	-2	2	2	0
S 6 76	40	-12	-9	-2	5	0	-14	-12	-1	5	0	3	3	2	2	0
S 6 76	70	11	-23	-6	-7	0	10	-27	-6	-5	0	-2	3	2	2	0
S 6 76	100	-8	52	-6	-18	0	-11	55	-6	-19	0	3	-2	2	2	0
S 6 76	130	-12	-27	-10	-3	0	-14	-30	-12	-3	0	3	3	2	2	0

S 6 76	160	-12	-18	-18	-14	0	-14	-22	-19	-17	0	3	3	2	2	0
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S 6 76	250	-12	-1	14	16	0	-11	2	14	17	0	-2	-2	-3	-4	0
S 6 76	280	11	17	30	27	0	15	22	32	29	0	-2	-2	-3	-4	0
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S 6 76	340	29	12	2	12	0	32	17	3	13	0	-6	-2	-3	-4	0
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S 6 84	40	-11	-9	-1	6	0	-11	-7	-1	4	0	0	4	1	-2	0
S 6 84	70	9	-18	-4	-5	0	9	-26	-9	-4	0	0	4	1	-2	0
S 6 84	100	-7	53	-4	-16	0	-11	49	-9	-20	0	0	-1	1	-2	0
S 6 84	130	-9	-22	-10	1	0	-11	-26	-9	-4	0	6	4	1	5	0
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S 6 90	40	-7	-6	2	12	0	-10	-6	-1	8	0	0	4	2	3	0
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S 7 30	40	8	-8	-6	-9	0	9	-13	-7	-4	0	0	5	1	-8	0
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S 7 40	10	-1	-9	-4	2	0	-5	-10	-4	1	0	1	1	1	1	0
S 7 40	40	-1	-9	-1	0	0	-2	-10	-4	-1	0	1	1	1	1	0
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S 7 52	70	-14	-15	-12	-2	0	-5	-19	-10	-4	0	-5	-1	0	2	0
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S 7 68	40	-14	-20	-14	-9	0	-15	-13	-17	-6	0	-4	0	-2	-1	0
S 7 68	70	-28	-7	-14	1	0	-24	-5	-17	1	0	-4	4	-2	-1	0
S 7 68	100	-14	-7	-14	-9	0	-15	-13	-17	-6	0	4	4	-2	-1	0
S 7 68	130	-14	-20	-14	1	0	-15	-21	-0	1	0	4	0	2	-1	0
S 7 68	160	-1	-20	-14	1	0	-15	-21	-0	-6	0	4	0	2	-1	0
S 7 68	190	-1	-20	-3	1	0	-7	-21	-2	-6	0	4	-5	2	-1	0
S 7 68	220	-1	-7	19	1	0	2	-5	10	1	0	4	-5	2	-1	0
S 7 68	250	-1	18	8	1	0	2	19	12	7	0	-4	0	-2	-1	0
S 7 68	280	26	43	30	-28	0	28	35	26	-25	0	4	0	2	-1	0
S 7 68	310	12	18	19	30	0	11	27	10	26	0	-4	0	-2	4	0
S 7 68	340	52	30	8	11	0	54	27	12	13	0	-4	4	2	4	0
S 7 76	10	-11	-3	-21	2	0	-14	-4	-23	0	0	0	0	2	0	0
S 7 76	40	-20	-16	-17	-9	0	-25	-22	-10	-7	0	5	5	2	0	0
S 7 76	70	-29	-3	-17	2	0	-33	-4	-10	0	0	5	0	2	0	0
S 7 76	100	-7	-7	-17	-9	0	-8	-9	-10	-7	0	0	5	2	0	0
S 7 76	130	-7	-16	-9	2	0	-8	-19	-10	0	0	0	5	2	0	0
S 7 76	160	-2	-21	-9	-2	0	-3	-25	-10	-2	0	0	5	2	0	0
S 7 76	190	-2	-25	3	-2	0	-6	-30	3	-2	0	0	5	2	0	0
S 7 76	220	7	-12	18	-5	0	8	-9	20	-4	0	0	0	-3	0	0
S 7 76	250	-2	20	7	2	0	-3	22	7	2	0	0	-5	-3	0	0
S 7 76	280	29	33	30	-27	0	35	42	35	-28	0	-4	-5	-3	0	0
S 7 76	310	2	15	18	31	0	5	22	22	31	0	0	-5	-3	0	0
S 7 76	340	43	33	14	16	0	51	37	14	17	0	-9	-5	2	0	0
S 7 84	10	-10	-2	-17	-1	0	-10	-5	-22	1	0	3	1	3	-2	0
S 7 84	40	-17	-14	-13	-8	0	-19	-14	-13	-7	0	3	1	3	-2	0
S 7 84	70	-22	2	-13	1	0	-29	-5	-13	1	0	3	1	3	-2	0
S 7 84	100	-3	-2	-13	-7	0	-10	-5	-13	-7	0	3	1	3	-2	0
S 7 84	130	-3	-10	-6	1	0	-10	-14	-13	1	0	3	7	3	-2	0
S 7 84	160	1	-16	-6	-1	0	0	-24	-13	1	0	3	7	3	5	0
S 7 84	190	-1	-19	5	-1	0	0	-24	3	1	0	3	7	3	5	0
S 7 84	220	8	-10	14	-5	0	10	-5	20	-7	0	-2	1	-4	-2	0
S 7 84	250	-5	13	1	-3	0	0	14	3	1	0	-2	-5	-4	-2	0
S 7 84	280	24	23	25	-20	0	29	34	20	-30	0	-2	-10	-4	-5	0
S 7 84	310	-1	9	14	29	0	0	14	20	31	0	-2	-5	-4	-2	0

S 7 84	340	29	25	10	14	0	39	34	12	16	0	-13	-5	-4	-2	0
S 7 90	10	-10	1	-10	-6	0	-10	0	-15	-3	0	0	-1	3	-1	0
S 7 90	40	-15	-10	-10	-13	0	-16	-12	-12	-9	0	0	5	3	-1	0
S 7 90	70	-20	7	-10	2	0	-21	3	-12	1	0	0	5	3	-1	0
S 7 90	100	0	1	-10	-6	0	-2	-3	-12	-6	0	0	5	3	-1	0
S 7 90	130	0	-4	-4	2	0	-2	-9	-6	1	0	0	5	3	-1	0
S 7 90	160	5	-10	-4	2	0	0	-15	-6	1	0	0	5	3	6	0
S 7 90	190	0	-16	9	2	0	-2	-18	5	1	0	0	5	3	6	0
S 7 90	220	10	-10	9	-6	0	9	-9	14	-6	0	0	-1	-4	-1	0
S 7 90	250	-5	7	-4	-6	0	-5	12	0	-3	0	0	-7	-4	-8	0
S 7 90	280	20	13	15	-13	0	22	21	27	-18	0	0	-7	-4	6	0
S 7 90	310	-5	1	9	25	0	0	9	11	29	0	0	-7	-4	-1	0
S 7 90	340	20	19	9	17	0	27	24	11	13	0	-5	-7	-4	-1	0
S 8 30	10	0	1	1	-3	0	5	-2	-3	14	0	-4	1	0	-15	0
S 8 30	40	0	1	-7	-11	0	0	-2	-3	-17	0	0	1	0	7	0
S 8 30	70	0	-7	-7	-11	0	5	-2	-8	-11	0	0	1	0	-2	0
S 8 30	100	0	1	-7	-11	0	0	3	-3	-6	0	0	-4	-4	-6	0
S 8 30	130	0	-7	-7	-11	0	-6	-7	-8	-6	0	5	5	0	-2	0
S 8 30	160	0	-7	-7	-3	0	0	-7	-8	-1	0	0	1	0	-2	0
S 8 30	190	0	1	1	4	0	0	-2	2	4	0	5	1	0	2	0
S 8 30	220	0	-7	8	12	0	-6	-7	7	9	0	0	1	0	2	0
S 8 30	250	-8	8	8	12	0	-6	8	7	-1	0	0	-4	4	11	0
S 8 30	280	16	16	8	12	0	16	13	7	4	0	0	1	0	7	0
S 8 30	310	-8	8	8	4	0	-6	13	12	9	0	-4	-4	-4	-2	0
S 8 30	340	0	-7	1	4	0	0	-7	-3	4	0	-4	1	4	-2	0
S 8 40	10	-1	-3	3	-1	0	-4	-1	3	-4	0	1	-1	-1	1	0
S 8 40	40	-11	-6	0	-4	0	-11	-5	3	-4	0	1	-1	-1	1	0
S 8 40	70	-11	-6	0	-1	0	-11	-5	-4	-2	0	1	-1	3	1	0
S 8 40	100	-4	-6	0	-1	0	-6	-8	3	3	0	1	3	-1	-3	0
S 8 40	130	-4	-3	0	1	0	-8	-3	1	3	0	1	-1	-1	-3	0
S 8 40	160	-4	-6	0	-1	0	-6	-5	5	1	0	1	-1	-5	-3	0
S 8 40	190	-4	-6	0	1	0	-6	-5	-1	3	0	1	-1	-1	-3	0
S 8 40	220	5	-3	0	-1	0	8	-1	-4	-2	0	-3	-1	3	1	0
S 8 40	250	9	9	6	4	0	13	6	10	3	0	-3	3	-1	1	0
S 8 40	280	9	15	-30	1	0	13	15	-30	-2	0	-3	-1	3	5	0
S 8 40	310	12	18	12	4	0	13	17	10	3	0	-3	-1	3	1	0
S 8 40	340	5	0	6	-1	0	4	-3	3	-2	0	1	3	3	1	0
S 8 52	10	-2	-3	-6	-5	0	3	-5	-2	-2	0	-2	-1	1	1	0
S 8 52	40	6	2	-7	-2	0	3	6	-12	-2	0	-2	-1	1	-3	0
S 8 52	70	-2	3	-2	-3	0	3	-5	-2	-2	0	-2	3	1	-3	0
S 8 52	100	-5	2	-6	-5	0	-8	-5	-12	-2	0	6	7	5	1	0
S 8 52	130	-6	3	-3	-3	0	-8	6	-2	-2	0	6	-1	-3	1	0
S 8 52	160	-2	-7	-5	-6	0	-8	-5	-2	-2	0	2	-1	-3	1	0
S 8 52	190	0	-10	-9	-3	0	3	-5	-2	-2	0	-2	-5	-3	1	0
S 8 52	220	1	-5	-2	-2	0	3	-5	-2	-2	0	-2	-5	-3	1	0
S 8 52	250	3	8	5	3	0	3	6	0	-2	0	2	-1	-3	1	0
S 8 52	280	3	12	17	9	0	3	17	10	7	0	-2	-1	1	1	0
S 8 52	310	1	0	16	9	0	3	-5	0	7	0	-2	3	5	1	0
S 8 52	340	1	-5	2	9	0	3	-5	-2	7	0	-2	3	1	1	0
S 8 60	10	-5	1	-9	-8	0	-1	-2	-5	-4	0	-4	1	-6	-2	0
S 8 60	40	8	-3	-2	-2	0	5	1	-7	-4	0	4	-3	6	2	0
S 8 60	70	-5	13	-2	-5	0	-1	4	-2	-4	0	-4	9	-2	-2	0
S 8 60	100	0	9	-2	-8	0	-4	4	-5	-4	0	0	5	6	-2	0
S 8 60	130	-5	1	-5	-5	0	-4	4	-5	-4	0	0	-3	-2	-2	0
S 8 60	160	4	-7	-5	-8	0	-1	-8	-5	-6	0	8	-3	-2	-5	0
S 8 60	190	-5	-16	-16	-5	0	-1	-11	-10	-4	0	-4	-3	-6	-2	0
S 8 60	220	0	-7	-2	-2	0	2	-8	-2	-1	0	0	1	2	-2	0

S 8 60	250	4	9	2	8	0	2	7	3	4	0	0	1	-2	6	0
S 8 60	280	4	5	13	12	0	2	13	17	9	0	0	-3	-2	2	0
S 8 60	310	0	5	21	12	0	2	1	17	9	0	0	5	6	2	0
S 8 60	340	0	-7	6	12	0	2	-5	3	9	0	0	-3	2	2	0
S 8 68	10	-10	6	-17	-6	0	-7	3	-15	-9	0	-1	1	-4	-3	0
S 8 68	40	17	-6	6	-6	0	10	-5	0	-3	0	3	-4	4	2	0
S 8 68	70	-10	19	-6	-6	0	-7	11	0	-3	0	-1	5	0	2	0
S 8 68	100	3	6	6	-6	0	1	11	0	-9	0	3	1	4	-3	0
S 8 68	130	-10	-6	-6	-6	0	-7	3	-7	-3	0	-1	-4	0	-3	0
S 8 68	160	3	-6	-6	-16	0	10	-14	-7	-9	0	3	1	0	-3	0
S 8 68	190	-10	-19	-17	-6	0	-7	-14	-15	-3	0	-1	1	-4	-3	0
S 8 68	220	3	-6	-6	-6	0	1	-5	0	-3	0	-1	1	0	2	0
S 8 68	250	3	6	-6	14	0	1	11	0	10	0	-1	1	0	2	0
S 8 68	280	3	6	17	14	0	1	3	15	10	0	-1	-4	-4	2	0
S 8 68	310	3	6	28	14	0	1	3	22	10	0	-1	1	4	2	0
S 8 68	340	3	-6	6	14	0	1	-5	7	10	0	-1	1	0	2	0
S 8 76	10	-10	2	-14	-10	0	-11	3	-17	-11	0	3	-2	1	0	0
S 8 76	40	13	-7	6	1	0	14	-10	4	1	0	-2	3	1	0	0
S 8 76	70	-10	20	-2	-3	0	-11	21	-3	-5	0	3	-2	1	0	0
S 8 76	100	0	11	6	-10	0	0	14	6	-11	0	-2	-2	1	0	0
S 8 76	130	-5	-2	-6	-7	0	-5	-5	-5	-7	0	3	-2	1	0	0
S 8 76	160	13	-11	-10	-14	0	14	-12	-10	-15	0	-2	3	1	0	0
S 8 76	190	-5	-16	-22	-7	0	-5	-20	-23	-7	0	3	3	1	0	0
S 8 76	220	0	-2	-2	-3	0	0	-5	-1	-3	0	-2	3	1	0	0
S 8 76	250	0	11	-2	16	0	0	11	-3	15	0	-2	-2	1	0	0
S 8 76	280	4	-2	10	12	0	3	1	13	13	0	-2	-2	-4	0	0
S 8 76	310	0	7	26	12	0	0	11	31	13	0	-2	-2	-4	0	0
S 8 76	340	0	-11	10	12	0	0	-10	10	13	0	-2	3	1	0	0
S 8 84	10	-8	4	-13	-10	0	-12	3	-17	-7	0	0	-2	1	0	0
S 8 84	40	11	-8	6	2	0	17	-6	1	1	0	0	-2	1	0	0
S 8 84	70	-8	15	-2	-2	0	-12	13	1	1	0	0	-2	1	0	0
S 8 84	100	1	9	7	-10	0	-2	13	0	-7	0	0	-2	1	0	0
S 8 84	130	-3	-4	-4	-4	0	-2	-6	-8	-7	0	0	-2	1	0	0
S 8 84	160	11	-8	-7	-14	0	17	-6	-8	-15	0	0	4	1	0	0
S 8 84	190	-5	-12	-19	-4	0	-2	-16	-25	-7	0	0	4	1	0	0
S 8 84	220	-1	-2	0	0	0	-2	-6	1	1	0	0	4	1	0	0
S 8 84	250	1	8	-4	15	0	-2	13	1	17	0	0	-2	1	0	0
S 8 84	280	4	-4	4	9	0	7	-6	0	9	0	0	-2	-5	0	0
S 8 84	310	-1	8	22	9	0	-2	13	27	9	0	0	-2	-5	0	0
S 8 84	340	-1	-6	9	9	0	-2	-6	0	9	0	0	4	1	0	0
S 8 90	10	-6	2	-10	-9	0	-8	2	-13	-8	0	0	1	2	2	0
S 8 90	40	9	-9	9	5	0	11	-7	6	2	0	0	1	2	2	0
S 8 90	70	-6	14	-4	-2	0	-8	14	-1	-2	0	0	1	2	2	0
S 8 90	100	-1	8	9	-9	0	0	8	0	-8	0	0	1	2	2	0
S 8 90	130	-1	-3	-4	-2	0	-3	-4	-4	-5	0	5	1	2	2	0
S 8 90	160	9	-3	-4	-9	0	11	-7	-7	-11	0	0	1	2	2	0
S 8 90	190	-6	-9	-16	-2	0	-5	-10	-10	-5	0	0	1	2	2	0
S 8 90	220	-1	2	3	-2	0	0	-1	-1	-2	0	0	1	2	2	0
S 8 90	250	-1	2	-4	13	0	0	5	-4	14	0	0	-5	-5	2	0
S 8 90	280	4	-9	-4	5	0	3	-4	3	8	0	0	-5	-5	-5	0
S 8 90	310	-1	8	15	5	0	0	8	21	8	0	0	1	-5	-5	0
S 8 90	340	-1	-3	9	5	0	0	-7	0	8	0	0	1	2	-5	0
S 9 30	10	5	-3	-7	6	0	7	-7	-8	13	0	-3	1	-3	-6	0
S 9 30	40	-3	-3	1	-11	0	-4	-7	2	-3	0	1	5	-3	-6	0
S 9 30	70	-3	-3	-7	-19	0	-9	-2	-3	-8	0	5	1	-3	-6	0
S 9 30	100	-3	-11	-7	-11	0	-4	-12	-8	-8	0	1	1	-3	-6	0
S 9 30	130	-3	-3	-7	-3	0	-4	-2	2	3	0	1	1	-11	-6	0

REPRODUCIBILITY OF THE
ORIGINAL IS POOR

S 9 30	160	-3	-3	-7	-3	0	-4	-2	2	-3	0	1	-3	-7	-1	0
S 9 30	190	-3	5	1	6	0	-4	9	7	-8	0	1	-3	-3	12	0
S 9 30	220	-3	5	9	14	0	2	4	13	8	0	-3	-3	-3	3	0
S 9 30	250	-3	5	9	14	0	-9	9	-3	3	0	5	-3	15	7	0
S 9 30	280	14	13	9	6	0	18	19	-3	-3	0	-3	-3	11	12	0
S 9 30	310	-3	5	9	6	0	2	4	-3	-3	0	-3	1	11	3	0
S 9 30	340	5	-3	1	-3	0	7	-12	2	8	0	-3	5	-3	-6	0
S 9 40	10	-2	-6	3	9	0	-3	-10	0	13	0	0	6	3	-4	0
S 9 40	40	-6	1	9	12	0	-6	2	0	16	0	0	2	-1	-4	0
S 9 40	70	-2	7	12	12	0	-3	9	4	11	0	0	-2	7	0	0
S 9 40	100	-2	1	6	9	0	-3	2	-3	3	0	0	2	7	4	0
S 9 40	130	-6	-2	-7	2	0	-6	-1	-7	-4	0	0	-2	3	4	0
S 9 40	160	-6	-6	-7	-8	0	-3	-3	-7	-9	0	-4	-2	-1	4	0
S 9 40	190	-6	-6	-10	-14	0	-8	-1	-3	-11	0	0	-6	-9	0	0
S 9 40	220	-2	-6	-1	-14	0	-6	-3	0	-13	0	0	-2	-9	0	0
S 9 40	250	11	1	-1	-11	0	11	-5	2	-11	0	0	6	-1	0	0
S 9 40	280	14	10	-1	-4	0	16	9	2	-1	0	0	-2	-1	-4	0
S 9 40	310	7	7	-1	2	0	9	6	2	1	0	0	2	-1	0	0
S 9 40	340	1	-2	-4	6	0	2	-5	-7	6	0	0	2	3	0	0
S 9 52	10	4	7	1	5	0	2	2	1	0	0	2	4	-1	5	0
S 9 52	40	18	22	18	16	0	23	20	11	11	0	-5	0	7	5	0
S 9 52	70	12	15	30	17	0	13	18	31	12	0	-2	-3	-1	5	0
S 9 52	100	0	6	22	17	0	1	8	29	20	0	-2	-3	-4	-3	0
S 9 52	130	-7	0	12	5	0	-6	15	14	7	0	-2	-15	-4	-3	0
S 9 52	160	-9	-11	1	2	0	-7	-10	1	0	0	-2	0	-1	1	0
S 9 52	190	-3	-8	-2	-3	0	-6	-12	-10	-4	0	2	4	7	1	0
S 9 52	220	-6	-12	-12	-14	0	-8	-16	-10	-13	0	2	4	7	1	0
S 9 52	250	1	-5	-24	-21	0	7	-5	-22	-11	0	-5	0	-1	-10	0
S 9 52	280	-1	-5	-17	-15	0	0	-5	-12	-7	0	-2	0	-4	-7	0
S 9 52	310	-6	-3	-12	-7	0	-11	-8	-8	-9	0	6	4	-4	1	0
S 9 52	340	-3	-5	-17	-1	0	-9	-8	-17	-5	0	6	4	-1	5	0
S 9 60	10	8	12	1	9	0	5	7	2	5	0	3	3	0	3	0
S 9 60	40	12	24	21	22	0	17	22	20	17	0	-1	3	4	3	0
S 9 60	70	12	12	30	22	0	11	13	20	17	0	-1	-1	0	3	0
S 9 60	100	0	4	17	13	0	-1	4	20	17	0	-1	-1	-4	-1	0
S 9 60	130	-9	-13	9	5	0	-7	-4	11	5	0	-1	-9	0	-1	0
S 9 60	160	-13	-13	1	5	0	-10	-10	2	2	0	-1	-1	0	3	0
S 9 60	190	0	-4	5	-4	0	-4	-7	-1	-1	0	3	3	4	-1	0
S 9 60	220	-5	-9	-8	-13	0	-7	-10	-10	-14	0	-1	3	4	-1	0
S 9 60	250	-5	-4	-24	-30	0	-1	-4	-25	-23	0	-5	-1	0	-5	0
S 9 60	280	-5	-4	-20	-21	0	-1	-4	-19	-17	0	-1	-1	-4	-5	0
S 9 60	310	0	0	-16	-8	0	-4	-1	-13	-8	0	3	3	0	-1	0
S 9 60	340	4	-4	-16	0	0	-1	-4	-16	-1	0	3	3	0	3	0
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S 9 68	40	11	25	26	23	0	16	27	26	22	0	-4	-1	3	0	0
S 9 68	70	11	9	27	25	0	7	10	26	22	0	0	-1	-1	0	0
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S 9 68	130	-10	-22	11	2	0	-10	-14	10	5	0	0	-6	-1	0	0
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S 9 68	190	1	-2	9	-2	0	-1	-6	10	-4	0	0	3	3	0	0
S 9 68	220	-3	-8	-3	-14	0	-1	-6	-7	-12	0	0	3	3	0	0
S 9 68	250	-6	-5	-28	-35	0	-1	-6	-31	-38	0	0	-1	-1	0	0
S 9 68	280	-3	-5	-24	-26	0	-1	-6	-23	-29	0	0	-1	-1	0	0
S 9 68	310	1	4	-18	-6	0	-1	2	-15	-4	0	0	3	-1	0	0
S 9 68	340	5	-1	-16	4	0	-1	2	-15	5	0	0	3	3	0	0
S 9 76	10	8	14	2	11	0	8	15	2	14	0	-1	0	0	-3	0
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S 9 76	130	-11	-23	11	0	0	-10	-26	17	2	0	4	5	0	-3	0
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S11 40	250	-3	-5	18	-11	0	-3	-2	24	-4	0	-1	-4	-4	-8	0
S11 40	280	-3	-22	-13	-71	0	-1	-12	-2	-56	0	-1	-12	-8	-12	0
S11 40	310	-3	-29	-83	-89	0	-3	-20	-75	-69	0	-1	-8	-8	-20	0
S11 40	340	-3	-19	-79	-80	0	-1	-20	-75	-66	0	-1	0	-4	-16	0
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S11 60	130	17	-11	45	89	0	18	-12	42	88	0	-1	0	7	2	0

REPRODUCIBILITY OF THE
ORIGINAL PAGE IS POOR

S11 60	160	13	27	103	131	0	18	25	91	127	0	-5	0	11	6	0
S11 60	190	13	3	97	124	0	12	5	82	122	0	-1	0	11	2	0
S11 60	220	-17	-30	51	159	0	-12	-29	42	151	0	-1	0	11	6	0
S11 60	250	-30	-53	-24	-23	0	-34	-53	-27	-29	0	3	0	2	2	0
S11 60	280	-39	-72	-76	-80	0	-40	-67	-67	-83	0	-1	-8	-6	2	0
S11 60	310	-34	-58	-70	-101	0	-31	-56	-63	-102	0	-1	0	-6	-2	0
S11 60	340	-4	-16	-70	-108	0	0	-16	-67	-102	0	-1	0	-6	-2	0
S11 68	10	19	54	-35	-92	0	20	59	-36	-101	0	0	-4	-1	11	0
S11 68	40	30	58	-24	-69	0	28	59	-24	-73	0	0	-4	-1	6	0
S11 68	70	30	67	-21	-36	0	28	69	-24	-44	0	0	0	-1	2	0
S11 68	100	10	32	8	10	0	11	31	11	13	0	0	0	-1	-3	0
S11 68	130	14	-8	50	86	0	20	-6	58	99	0	-4	0	-1	-12	0
S11 68	160	9	25	105	123	0	11	31	105	141	0	-4	0	-6	-16	0
S11 68	190	13	3	102	121	0	11	3	105	141	0	0	0	-6	-16	0
S11 68	220	-16	-30	59	152	0	-14	-34	58	170	0	0	0	-1	-16	0
S11 68	250	-28	-50	-23	-23	0	-31	-53	-24	-30	0	5	4	3	2	0
S11 68	280	-37	-77	-75	-74	0	-40	-81	-83	-87	0	0	0	7	11	0
S11 68	310	-36	-58	-73	-98	0	-40	-62	-71	-115	0	0	4	3	15	0
S11 68	340	-6	-16	-73	-100	0	-6	-16	-71	-115	0	0	0	7	15	0
S11 76	10	19	44	-28	-70	0	20	57	-30	-91	0	-2	-9	7	21	0
S11 76	40	28	49	-22	-55	0	34	63	-28	-73	0	-7	-14	7	17	0
S11 76	70	28	59	-16	-26	0	34	72	-24	-39	0	-7	-14	3	8	0
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S11 76	130	10	-6	44	68	0	13	-8	51	88	0	-2	0	-11	-18	0
S11 76	160	5	19	92	98	0	7	27	114	131	0	-2	-4	-20	-27	0
S11 76	190	10	4	86	98	0	13	4	111	126	0	-2	0	-20	-27	0
S11 76	220	-13	-26	50	119	0	-17	-32	66	159	0	2	5	-16	-36	0
S11 76	250	-22	-42	-22	-19	0	-30	-52	-24	-25	0	7	10	3	4	0
S11 76	280	-31	-67	-64	-62	0	-40	-85	-80	-77	0	7	15	16	17	0
S11 76	310	-31	-47	-64	-77	0	-38	-61	-76	-101	0	7	10	16	21	0
S11 76	340	-8	-16	-64	-84	0	-6	-17	-76	-106	0	2	5	16	21	0
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S11 84	250	-16	-28	-14	-8	0	-22	-36	-18	-20	0	8	9	5	3	0
S11 84	280	-21	-46	-46	-43	0	-31	-68	-56	-50	0	8	20	14	12	0
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S11 90	250	-11	-15	-7	-4	0	-14	-26	-13	-6	0	4	6	1	1	0
S11 90	280	-11	-32	-36	-37	0	-19	-41	-39	-37	0	4	12	6	1	0
S11 90	310	-16	-21	-36	-51	0	-19	-29	-30	-52	0	4	12	6	1	0
S11 90	340	-5	-3	-36	-51	0	-5	-7	-39	-52	0	-1	1	6	1	0
S12 30	10	4	-4	-50	-41	0	5	-5	-25	-23	0	-2	0	-26	-18	0
S12 30	40	4	-13	-41	-30	0	5	-10	-13	-16	0	-2	0	-26	-13	0

S12 30	70	-4	-4	-41	-30	0	-6	-5	-10	-16	0	2	0	-22	-13	0
S12 30	100	-4	-21	-23	2	0	-1	-16	-2	16	0	-2	-9	-22	-13	0
S12 30	130	4	-4	14	44	0	5	6	44	55	0	-2	-9	-26	-13	0
S12 30	160	-4	4	59	87	0	-1	6	61	80	0	-2	0	-8	6	0
S12 30	190	-4	21	95	119	0	-1	23	67	80	0	2	-4	24	39	0
S12 30	220	4	4	77	44	0	-1	-5	15	10	0	2	9	55	30	0
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S12 30	280	4	13	-32	-62	0	-1	6	-36	-68	0	2	9	10	11	0
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S12 40	40	7	34	7	-2	0	13	17	-15	-2	0	-4	16	22	-2	0
S12 40	70	18	38	11	17	0	20	15	-15	27	0	-4	24	26	-6	0
S12 40	100	11	16	15	32	0	13	-1	-3	46	0	-4	16	14	-15	0
S12 40	130	7	5	15	72	0	10	-9	28	91	0	-4	12	-11	-20	0
S12 40	160	4	2	52	101	0	7	-1	81	107	0	-4	4	-28	-6	0
S12 40	190	1	-2	73	86	0	5	15	90	72	0	-4	-16	-15	12	0
S12 40	220	-10	-16	-1	2	0	-10	9	16	-14	0	4	-24	-19	16	0
S12 40	250	-13	-34	-46	-57	0	-26	-33	-37	-62	0	11	-4	-7	7	0
S12 40	280	-13	-38	-63	-96	0	-21	-27	-57	-97	0	7	-8	-7	-2	0
S12 40	310	-6	-16	-59	-91	0	-3	4	-60	-94	0	0	-20	1	3	0
S12 40	340	1	-2	-9	-52	0	0	7	-17	-59	0	0	-8	10	12	0
S12 52	10	11	38	75	-14	0	9	35	73	-1	0	2	2	2	-15	0
S12 52	40	12	48	52	-9	0	10	45	51	7	0	2	2	2	-15	0
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S12 52	130	17	53	15	57	0	19	41	10	43	0	-2	10	6	13	0
S12 52	160	12	12	24	95	0	14	10	10	68	0	-2	2	6	25	0
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S12 52	250	-26	-101	-106	-66	0	-23	-91	-98	-60	0	-2	-9	-9	-7	0
S12 52	280	-35	-13	-97	-74	0	-32	-11	-98	-73	0	-2	-2	-2	1	0
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S12 60	10	12	41	79	-22	0	12	37	78	-24	0	0	2	2	-1	0
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S12 60	70	21	60	73	3	0	19	54	74	4	0	4	6	-2	-1	0
S12 60	100	16	70	54	11	0	12	68	52	21	0	0	2	2	-6	0
S12 60	130	16	65	17	67	0	15	54	17	66	0	0	6	2	3	0
S12 60	160	12	17	30	116	0	12	13	26	105	0	0	2	2	7	0
S12 60	190	3	-25	5	100	0	3	-21	4	93	0	0	-2	2	7	0
S12 60	220	-10	-82	-81	3	0	-7	-75	-74	-1	0	0	-6	-2	3	0
S12 60	250	-28	-111	-112	-70	0	-26	-102	-108	-68	0	0	-6	-2	-1	0
S12 60	280	-37	-16	-94	-78	0	-35	-14	-100	-74	0	-4	-2	2	-1	0
S12 60	310	-19	-68	-50	-62	0	-16	-61	-48	-63	0	0	-6	-2	3	0
S12 60	340	-1	-2	24	-46	0	-1	0	26	-40	0	0	-2	-2	-6	0
S12 68	10	13	41	74	-24	0	9	46	83	-31	0	0	-1	-9	4	0
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S12 68	130	14	69	21	65	0	18	65	20	67	0	0	-1	0	-9	0
S12 68	160	10	15	27	112	0	9	17	33	133	0	0	-1	-4	-18	0
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S12 68	220	-10	-83	-78	5	0	-9	-87	-81	1	0	0	3	9	-1	0
S12 68	250	-28	-112	-108	-67	0	-27	-116	-119	-81	0	0	3	13	12	0
S12 68	280	-40	-16	-89	-69	0	-44	-21	-106	-81	0	0	-1	9	12	0
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S12 68	340	0	-4	25	-44	0	0	-2	33	-48	0	0	-1	-4	8	0
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S12 76	190	7	-24	3	82	0	7	-29	7	93	0	-2	6	0	-15	0
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S12 76	250	-25	-99	-91	-51	0	-31	-122	-111	-63	0	3	25	18	7	0
S12 76	280	-34	-14	-78	-59	0	-42	-17	-91	-68	0	8	1	14	7	0
S12 76	310	-16	-59	-41	-51	0	-17	-74	-48	-58	0	3	15	9	7	0
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S12 84	130	8	45	16	46	0	15	60	17	42	0	-1	-15	-4	0	0
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S12 84	190	5	-16	5	67	0	5	-26	4	74	0	-1	6	1	-4	0
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S12 84	280	-26	-10	-62	-52	0	-33	-13	-69	-54	-5	4	6	10	0	0
S12 84	310	-10	-42	-29	-42	0	-15	-58	-35	-37	0	4	16	6	0	0
S12 84	340	-1	-3	16	-32	0	-5	-5	17	-37	0	-1	0	-4	0	0
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S12 90	250	-15	-50	-70	-52	0	-17	-64	-69	-45	0	0	14	-4	-7	0
S12 90	280	-20	-6	-58	-59	0	-26	-9	-56	-49	0	5	4	-4	-7	0
S12 90	310	-9	-28	-24	-46	0	-9	-39	-26	-40	0	0	9	1	-7	0
S12 90	340	1	0	16	-32	0	-1	-3	14	-28	0	0	-1	1	-2	0
S13 30	10	2	-4	-15	-23	0	4	-5	-7	-2	0	-2	1	-8	-20	0
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S13 30	130	-1	0	10	37	0	-2	0	13	33	0	2	1	-1	5	0
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S13 30	250	0	3	5	-4	0	0	7	-12	-13	0	0	-1	18	11	0
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S13 30	340	0	-4	-13	-25	0	4	-4	-3	-7	0	-2	0	-9	-18	0
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S13 40	160	2	1	21	48	0	3	5	28	43	0	-1	-3	-6	4	0
S13 40	190	-2	2	34	54	0	-1	8	41	51	0	0	-6	-5	4	0
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S13 40	250	0	-5	5	11	0	3	-4	7	8	0	-2	-1	-1	3	0
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S13 40	310	0	-5	-23	-34	0	0	-5	-27	-31	0	0	0	4	-2	0
S13 40	340	-2	-2	-11	-30	0	-4	-7	-10	-25	0	2	5	8	-4	0
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S13 52	190	-1	-3	16	45	0	0	0	16	45	0	0	-1	0	1	0
S13 52	220	-9	-22	-4	30	0	-7	-19	-2	34	0	-1	-3	-2	-2	0
S13 52	250	-17	-31	-23	-8	0	-14	-29	-10	-4	0	-1	-1	-3	-4	0
S13 52	280	-20	-30	-35	-32	0	-19	-29	-33	-29	0	0	0	-2	-2	0
S13 52	310	-11	-27	-24	-37	0	-10	-26	-22	-35	0	0	0	0	-1	0
S13 52	340	6	-1	-14	-29	0	6	-2	-14	-27	0	0	1	0	-1	0
S13 60	10	13	27	13	-22	0	12	25	14	-22	0	0	2	0	0	0
S13 60	40	18	37	19	-15	0	17	35	18	-16	0	1	2	1	1	0
S13 60	70	16	37	23	-6	0	15	34	20	-8	0	1	3	1	2	0
S13 60	100	9	24	12	7	0	7	20	10	7	0	1	5	1	1	0
S13 60	130	4	2	8	33	0	3	3	7	32	0	1	0	1	1	0
S13 60	160	2	5	25	50	0	2	5	24	50	0	1	0	0	0	0
S13 60	190	-1	-5	15	45	0	-1	-3	15	46	0	0	-1	0	0	0
S13 60	220	-11	-26	-7	28	0	-9	-23	-4	29	0	0	-1	0	-1	0
S13 60	250	-19	-34	-25	-10	0	-17	-31	-24	-9	0	-2	-1	-1	0	0
S13 60	280	-21	-32	-37	-33	0	-20	-30	-36	-33	0	0	0	0	0	0
S13 60	310	-12	-28	-25	-39	0	-11	-27	-24	-38	0	0	-1	0	0	0
S13 60	340	6	-1	-15	-31	0	6	-1	-14	-30	0	0	0	0	0	0
S13 68	10	13	28	13	-20	0	13	29	14	-24	0	0	0	-1	3	0
S13 68	40	19	37	19	-14	0	19	39	20	-17	0	0	0	0	2	0
S13 68	70	17	39	22	-4	0	17	41	22	-6	0	0	0	0	1	0
S13 68	100	9	28	12	6	0	9	26	13	7	0	0	1	0	-1	0
S13 68	130	4	1	8	33	0	5	2	8	38	0	0	0	0	-4	0
S13 68	160	3	5	23	45	0	3	5	26	53	0	0	0	-2	-6	0
S13 68	190	-2	-6	14	42	0	-2	-6	16	49	0	1	0	-1	-6	0
S13 68	220	-12	-27	-6	24	0	-11	-28	-5	29	0	0	0	1	-3	0
S13 68	250	-21	-35	-26	-11	0	-20	-36	-28	-13	0	0	2	2	1	0
S13 68	280	-21	-32	-36	-32	0	-22	-34	-41	-37	0	1	1	3	5	0
S13 68	310	-11	-30	-24	-35	0	-14	-30	-26	-40	0	0	2	2	6	0
S13 68	340	7	-1	-14	-28	0	6	0	-13	-33	0	0	0	2	6	0
S13 76	10	12	24	11	-16	0	14	30	13	-20	0	-1	-4	-1	4	0
S13 76	40	16	33	16	-9	0	19	39	20	-12	0	-2	-6	-2	3	0
S13 76	70	16	34	20	-3	0	18	42	23	-3	0	-2	-6	-3	0	0
S13 76	100	9	26	10	5	0	11	31	12	6	0	-1	-3	-1	0	0
S13 76	130	5	1	7	26	0	6	1	9	34	0	0	0	0	-6	0
S13 76	160	3	3	19	35	0	4	4	24	46	0	0	0	-3	-9	0
S13 76	190	-1	-6	11	33	0	-2	-8	15	42	0	0	1	-2	-7	0
S13 76	220	-10	-24	-5	19	0	-13	-29	-6	23	0	2	5	1	-4	0
S13 76	250	-20	-31	-22	-7	0	-24	-37	-27	-12	0	3	7	5	2	0
S13 76	280	-18	-28	-31	-26	0	-21	-34	-38	-33	0	4	6	7	7	0
S13 76	310	-12	-26	-20	-27	0	-14	-31	-24	-35	0	2	6	5	8	0
S13 76	340	6	-1	-11	-22	0	7	-1	-15	-28	0	0	0	3	6	0
S13 84	10	9	18	8	-14	0	10	24	9	-13	0	-1	-5	-1	0	0
S13 84	40	12	23	12	-8	0	16	30	16	-10	0	-2	-7	-2	1	0
S13 84	70	11	25	14	-3	0	14	31	18	-1	0	-2	-7	-3	0	0
S13 84	100	7	21	8	3	0	8	25	10	4	0	-1	-4	-1	-1	0
S13 84	130	4	1	5	20	0	5	1	7	23	0	0	0	0	-3	0

REPRODUCIBILITY OF THE
ORIGINAL PAGE IS POOR

S13 84	160	3	2	14	26	0	4	3	16	33	0	0	0	-3	-3	0
S13 84	190	-1	-4	8	25	0	-2	-7	9	30	0	0	2	-1	-3	0
S13 84	220	-8	-17	-3	14	0	-10	-22	-4	17	0	2	6	2	-2	0
S13 84	250	-15	-22	-17	-4	0	-18	-27	-21	-8	0	4	7	5	3	0
S13 84	280	-12	-21	-23	-18	0	-17	-27	-28	-24	0	4	7	5	5	0
S13 84	310	-9	-19	-14	-18	0	-12	-24	-16	-22	0	2	6	4	5	0
S13 84	340	4	0	-8	-16	0	5	0	-11	-21	0	0	0	3	3	0
S13 90	10	7	13	8	-15	0	8	17	7	-13	0	0	-3	0	-1	0
S13 90	40	9	15	11	-9	0	11	21	11	-7	0	-1	-3	0	-1	0
S13 90	70	8	18	11	-3	0	10	23	13	-2	0	-2	-3	0	0	0
S13 90	100	5	16	6	2	0	6	19	7	3	0	0	-1	0	0	0
S13 90	130	3	1	5	18	0	3	0	5	18	0	0	0	0	1	0
S13 90	160	1	2	12	25	0	2	1	12	23	0	0	0	0	2	0
S13 90	190	-1	-2	8	24	0	-1	-4	7	22	0	0	1	0	1	0
S13 90	220	-4	-12	-2	13	0	-7	-15	-3	11	0	1	3	1	1	0
S13 90	250	-11	-16	-14	-2	0	-14	-20	-15	-4	0	2	3	0	1	0
S13 90	280	-8	-16	-22	-16	0	-12	-19	-21	-15	0	3	3	0	1	0
S13 90	310	-7	-13	-12	-16	0	-7	-16	-12	-15	0	1	3	0	0	0
S13 90	340	4	0	-7	-15	0	4	0	-7	-14	0	0	0	1	-1	0

---END OF FILE WRITTEN---

RANDOM PERTURBATIONS, (R)

K 1 25	33	46	45	72	82	21	34	34	47	51	26	31	31	56	65
K 1 30	29	45	44	76	87	23	42	42	64	71	27	35	34	67	78
K 1 35	22	32	32	64	74	24	41	41	81	94	28	37	37	73	85
K 1 40	16	27	27	56	65	26	47	47	96	113	28	39	39	76	89
K 1 45	16	32	32	69	81	28	56	56	115	135	28	39	39	74	85
R 1 50	17	40	41	90	107	29	66	66	136	159	28	40	40	65	74
R 1 55	17	47	47	108	128	31	74	74	151	170	26	39	39	58	65
K 1 60	18	54	65	115	132	32	81	81	158	184	29	38	20	58	70
K 1 65	25	61	61	119	138	34	85	85	162	187	35	43	43	73	83
K 1 70	32	63	63	126	148	35	87	87	164	189	44	57	57	69	74
K 1 75	34	58	58	109	128	37	86	86	157	180	51	73	73	85	89
K 1 80	41	70	70	107	122	39	88	88	146	166	56	86	85	102	108
K 1 85	48	68	67	98	110	41	84	85	141	160	69	96	96	115	121
K 1 90	74	69	69	95	108	43	80	80	141	161	100	102	103	118	123
K 1 100	144	144	144	144	144	154	154	154	154	154	75	75	75	75	75
K 1 120	196	196	196	196	196	79	79	79	79	79	211	211	211	211	211
K 1 140	136	136	136	136	136	72	72	72	72	72	146	146	146	146	146
K 1 160	101	101	101	101	101	65	65	65	65	65	105	105	105	105	105
K 1 180	80	80	80	80	80	58	58	58	58	58	81	81	81	81	81
K 1 200	69	69	69	69	69	52	52	52	52	52	69	69	69	69	69
K 2 25	33	46	46	73	82	21	34	34	47	51	26	31	31	57	65
K 2 30	29	45	44	76	86	23	42	42	64	71	27	35	34	66	76
R 2 35	22	32	32	63	74	24	41	41	81	94	28	37	37	73	85
K 2 40	16	27	27	56	65	26	47	47	96	113	28	38	38	76	88
R 2 45	16	32	32	68	80	27	56	56	115	134	28	39	39	73	85
K 2 50	17	40	40	83	98	29	66	66	129	149	28	40	40	66	74
K 2 55	17	47	48	98	114	31	74	74	140	162	26	39	38	58	65
K 2 60	18	54	54	103	120	32	81	81	146	168	30	38	38	59	65
K 2 65	26	61	61	108	124	34	85	85	149	171	36	43	44	72	82
K 2 70	32	63	63	116	135	35	87	87	153	175	44	57	57	69	73
K 2 75	34	58	58	106	124	37	86	86	153	176	51	73	72	87	91
K 2 80	41	70	70	108	122	39	88	88	146	166	55	86	85	103	109
K 2 85	48	67	68	98	110	41	85	84	141	160	69	96	97	114	120
K 2 90	74	68	68	95	108	43	80	80	141	161	100	102	101	118	124

R 2	100	144	144	144	144	144	154	154	154	154	154	75	75	75	75	75
R 2	120	196	196	196	196	196	79	79	79	79	79	211	211	211	211	211
R 2	140	136	136	136	136	136	72	72	72	72	72	146	146	146	146	146
R 2	160	101	101	101	101	101	65	65	65	65	65	105	105	105	105	105
R 2	180	80	80	80	80	80	58	58	58	58	58	81	81	81	81	81
R 2	200	69	69	69	69	69	52	52	52	52	52	69	69	69	69	69
R 3	25	34	45	45	58	63	21	41	41	46	47	27	19	19	37	43
R 3	30	29	37	37	59	67	23	38	38	58	65	27	22	22	41	47
R 3	35	21	30	30	51	58	24	39	39	68	78	28	24	24	45	52
R 3	40	16	27	27	48	56	26	44	44	79	90	28	26	27	47	54
R 3	45	16	30	31	55	63	27	50	50	88	101	27	31	30	49	55
R 3	50	17	35	35	64	74	29	57	57	96	109	28	34	34	46	50
R 3	55	17	42	43	75	86	31	65	65	103	116	26	33	32	38	40
R 3	60	19	50	49	83	94	32	72	72	110	123	31	30	30	37	39
R 3	65	25	59	59	94	106	34	76	76	116	129	35	29	29	35	37
R 3	70	32	61	61	99	111	36	79	79	121	134	44	35	35	37	38
R 3	75	34	53	53	95	110	37	79	79	123	138	51	53	54	45	42
R 3	80	40	59	59	94	108	39	78	78	124	139	55	68	68	61	58
R 3	85	48	62	62	84	95	41	78	78	123	137	69	88	87	92	94
R 3	90	74	72	71	90	98	43	79	79	122	136	100	107	107	129	137
R 3	100	144	144	144	144	144	154	154	154	154	154	75	75	75	75	75
R 3	120	196	196	196	196	196	79	79	79	79	79	211	211	211	211	211
R 3	140	136	136	136	136	136	72	72	72	72	72	146	146	146	146	146
R 3	160	101	101	101	101	101	65	65	65	65	65	105	105	105	105	105
R 3	180	80	80	80	80	80	58	58	58	58	58	81	81	81	81	81
R 3	200	69	69	69	69	69	52	52	52	52	52	69	69	69	69	69
R 4	25	34	45	45	57	62	21	41	41	44	45	27	19	19	37	43
R 4	30	29	37	37	56	63	23	38	38	53	59	27	22	21	42	48
R 4	35	21	30	30	46	51	24	39	39	61	68	27	23	24	44	51
R 4	40	16	27	27	42	46	26	44	44	70	79	28	26	26	47	54
R 4	45	16	30	30	47	53	28	50	50	79	89	27	31	31	49	55
R 4	50	17	35	35	55	61	29	57	57	86	95	28	33	33	45	49
R 4	55	18	42	43	63	70	31	65	65	91	99	27	33	32	38	40
R 4	60	18	50	50	67	73	32	71	72	93	101	30	29	30	36	37
R 4	65	25	58	58	77	84	34	76	76	100	107	35	29	30	36	38
R 4	70	32	61	61	86	95	36	79	79	108	117	44	36	35	37	38
R 4	75	34	53	53	87	100	37	79	79	115	127	52	54	53	44	41
R 4	80	41	59	59	89	101	39	78	78	118	131	55	68	69	60	58
R 4	85	48	62	62	81	91	41	77	78	118	132	68	88	89	92	93
R 4	90	74	71	72	89	96	43	79	79	118	131	101	107	107	138	137
R 4	100	144	144	144	144	144	154	154	154	154	154	75	75	75	75	75
R 4	120	196	196	196	196	196	79	79	79	79	79	211	211	211	211	211
R 4	140	136	136	136	136	136	72	72	72	72	72	146	146	146	146	146
R 4	160	101	101	101	101	101	65	65	65	65	65	105	105	105	105	105
R 4	180	80	80	80	80	80	58	58	58	58	58	81	81	81	81	81
R 4	200	69	69	69	69	69	52	52	52	52	52	69	69	69	69	69
R 5	25	38	45	45	55	59	27	41	41	40	40	27	19	19	37	44
R 5	30	33	37	37	52	57	29	38	38	48	51	27	22	22	41	47
R 5	35	24	30	30	40	44	31	39	39	52	57	27	23	24	43	50
R 5	40	19	27	27	34	37	32	44	44	59	65	28	26	26	47	54
R 5	45	19	30	30	39	43	34	50	50	68	75	28	31	30	49	55
R 5	50	20	35	35	44	47	35	57	58	73	79	28	34	34	46	50
R 5	55	21	43	42	50	52	37	65	65	76	80	26	32	33	38	40
R 5	60	22	50	50	53	55	38	72	72	79	82	30	30	30	36	38
R 5	65	28	58	58	65	67	40	76	76	86	89	35	30	30	35	36
R 5	70	34	60	60	75	79	42	79	79	95	101	44	36	36	37	38
R 5	75	35	53	53	77	86	44	79	79	104	113	52	54	54	45	42

R 5	80	41	59	59	84	94	45	78	78	112	123	55	68	69	61	58
R 5	85	47	62	62	78	86	47	78	78	113	125	69	87	88	93	95
R 5	90	71	72	71	88	94	49	79	79	113	125	100	107	107	129	136
R 5	100	144	144	144	144	144	154	154	154	154	154	75	75	75	75	75
R 5	120	196	196	196	196	196	79	79	79	79	79	211	211	211	211	211
R 5	140	136	136	136	136	136	72	72	72	72	72	146	146	146	146	146
R 5	160	101	101	101	101	101	65	65	65	65	65	105	105	105	105	105
K 5	180	80	80	80	80	80	58	58	58	58	58	81	81	81	81	81
R 5	200	69	69	69	69	69	52	52	52	52	52	69	69	69	69	69
K 6	25	37	41	41	44	45	27	33	33	37	39	26	24	24	24	24
K 6	30	33	35	35	42	44	29	33	33	42	45	27	25	25	26	26
K 6	35	24	27	26	36	39	31	35	35	48	52	27	27	26	27	27
R 6	40	19	23	23	33	37	32	39	39	52	56	28	26	27	28	29
R 6	45	19	29	29	36	38	34	48	48	55	58	28	28	28	28	29
K 6	50	20	34	33	35	36	35	54	54	55	55	28	30	31	29	28
K 6	55	21	34	34	35	36	37	56	56	54	54	26	35	35	28	25
K 6	60	22	33	33	36	38	39	57	57	57	56	29	40	41	29	25
K 6	65	28	43	43	48	51	40	63	63	67	68	35	50	50	33	28
R 6	70	34	53	53	59	64	42	70	70	79	82	44	63	63	40	33
K 6	75	35	53	53	63	71	44	75	75	91	97	52	73	73	50	43
K 6	80	41	60	60	75	84	45	72	72	102	112	55	76	77	64	59
R 6	85	47	61	61	74	83	47	73	73	108	120	69	87	87	78	75
R 6	90	72	63	62	74	80	49	79	79	109	119	100	92	91	93	93
K 6	100	144	144	144	144	144	154	154	154	154	154	75	75	75	75	75
R 6	120	196	196	196	196	196	79	79	79	79	79	211	211	211	211	211
R 6	140	136	136	136	136	136	72	72	72	72	72	146	146	146	146	146
R 6	160	101	101	101	101	101	65	65	65	65	65	105	105	105	105	105
R 6	180	80	80	80	80	80	58	58	58	58	58	81	81	81	81	81
K 6	200	69	69	69	69	69	52	52	52	52	52	69	69	69	69	69
R 7	25	37	41	41	44	45	27	33	33	37	39	26	25	24	24	24
K 7	30	33	35	35	42	44	29	33	33	42	45	27	26	25	26	26
K 7	35	24	27	26	36	39	31	35	35	48	52	28	27	26	27	27
K 7	40	19	23	23	33	37	32	39	39	52	56	28	27	27	28	28
R 7	45	19	29	29	35	37	34	48	48	55	58	28	28	28	29	30
K 7	50	20	34	34	35	36	35	54	54	55	55	28	30	30	29	28
K 7	55	21	34	34	35	35	37	56	56	54	54	26	35	35	29	27
K 7	60	22	33	33	36	38	39	57	57	57	56	30	40	41	30	26
K 7	65	28	43	43	48	51	40	63	63	67	68	35	51	51	33	27
K 7	70	34	53	52	59	64	42	70	70	79	81	44	63	62	40	32
R 7	75	35	53	53	64	71	44	75	75	91	97	52	74	73	50	42
K 7	80	41	60	60	75	84	45	72	72	102	112	55	77	77	63	58
K 7	85	48	61	61	74	83	47	73	72	108	120	69	88	88	77	73
K 7	90	72	63	62	74	79	49	79	79	109	119	101	92	92	92	92
R 7	100	144	144	144	144	144	154	154	154	154	154	75	75	75	75	75
R 7	120	196	196	196	196	196	79	79	79	79	79	211	211	211	211	211
R 7	140	136	136	136	136	136	72	72	72	72	72	146	146	146	146	146
K 7	160	101	101	101	101	101	65	65	65	65	65	105	105	105	105	105
R 7	180	80	80	80	80	80	58	58	58	58	58	81	81	81	81	81
K 7	200	69	69	69	69	69	52	52	52	52	52	69	69	69	69	69
K 8	25	37	44	44	47	48	27	37	37	41	42	26	25	24	24	24
R 8	30	33	37	36	47	50	29	36	36	48	52	27	26	25	26	27
K 8	35	24	28	28	40	44	31	37	37	52	57	28	27	27	27	27
K 8	40	19	25	25	40	45	32	42	42	59	65	28	27	27	29	29
K 8	45	19	30	30	47	53	34	49	49	68	75	28	28	28	29	29
K 8	50	20	35	35	52	58	35	55	55	74	80	28	30	31	29	29
K 8	55	21	38	37	56	62	37	60	60	76	82	26	34	35	28	26
K 8	60	22	38	38	57	65	38	64	64	79	84	30	40	40	29	26

R 8 65	28	47	47	65	74	40	70	70	86	91	34	51	51	33	27
R 8 70	34	55	55	74	83	42	75	75	96	103	44	62	62	40	32
R 8 75	35	54	54	75	87	44	77	77	104	113	53	74	74	50	42
R 8 80	41	61	61	83	95	45	75	75	112	124	55	77	77	63	59
R 8 85	48	61	61	78	89	47	75	75	113	126	70	88	87	76	72
R 8 90	71	63	63	76	83	49	79	79	113	125	100	93	93	92	92
R 8 100	144	144	144	144	144	154	154	150	150	150	75	75	75	75	75
R 8 120	196	196	196	196	196	79	79	79	79	79	211	211	211	211	211
R 8 140	136	136	136	136	136	72	72	72	72	72	146	146	146	146	146
R 8 160	101	101	101	101	101	65	65	65	65	65	105	105	105	105	105
R 8 180	80	80	80	80	80	58	58	58	58	58	81	81	81	81	81
R 8 200	69	69	69	69	69	52	52	52	52	52	69	69	69	69	69
R 9 25	33	45	45	57	61	21	41	41	44	45	26	20	20	36	42
R 9 30	29	37	37	56	63	23	38	38	54	59	27	22	22	41	48
R 9 35	22	30	30	46	52	24	39	39	61	66	28	23	23	46	54
R 9 40	16	27	27	41	46	26	44	44	70	79	28	28	27	50	57
R 9 45	16	30	30	47	52	27	50	50	79	89	28	31	31	51	58
R 9 50	17	35	35	55	62	29	57	57	86	95	28	33	33	45	49
R 9 55	17	41	41	65	73	31	65	65	91	99	26	35	36	38	34
R 9 60	18	49	49	68	75	32	72	72	93	101	29	32	31	34	34
R 9 65	25	60	60	79	86	34	76	76	100	107	35	26	27	32	34
R 9 70	32	59	59	86	95	36	79	79	108	117	44	40	40	38	37
R 9 75	35	54	54	88	99	37	79	79	115	127	52	47	45	43	42
R 9 80	40	61	61	89	102	39	78	78	118	131	55	72	74	60	55
R 9 85	48	59	59	81	91	41	78	78	118	132	69	81	82	86	88
R 9 90	73	65	65	83	90	43	79	79	118	131	99	96	96	112	117
R 9 100	144	144	144	144	144	154	154	154	154	154	75	75	75	75	75
R 9 120	196	196	196	196	196	79	79	79	79	79	211	211	211	211	211
R 9 140	136	136	136	136	136	72	72	72	72	72	146	146	146	146	146
R 9 160	101	101	101	101	101	65	65	65	65	65	105	105	105	105	105
R 9 180	80	80	80	80	80	58	58	58	58	58	81	81	81	81	81
R 9 200	69	69	69	69	69	52	52	52	52	52	69	69	69	69	69
R 10 25	34	45	45	58	62	21	41	41	46	47	27	20	20	36	41
R 10 30	29	37	37	60	68	23	38	38	58	65	27	21	22	42	49
R 10 35	22	30	30	51	58	24	39	39	68	76	28	23	22	46	53
R 10 40	16	27	27	48	55	26	44	44	79	90	28	28	27	50	57
R 10 45	16	30	30	54	62	27	50	50	88	101	28	31	30	51	58
R 10 50	17	35	35	65	74	29	57	57	96	109	28	33	33	45	49
R 10 55	17	41	41	77	90	31	65	65	103	116	26	35	35	35	35
R 10 60	18	48	49	85	97	32	71	71	110	123	30	32	31	34	35
R 10 65	25	60	60	95	106	34	76	76	116	129	35	26	27	33	35
R 10 70	32	59	59	98	112	35	79	79	121	134	44	40	41	38	37
R 10 75	35	54	54	96	110	37	79	79	123	138	52	47	46	43	42
R 10 80	41	61	61	94	109	39	78	78	124	139	56	73	73	60	55
R 10 85	49	59	59	84	95	41	78	78	123	137	69	81	81	86	88
R 10 90	74	65	64	84	93	43	79	79	122	136	100	97	96	112	118
R 10 100	144	144	144	144	144	154	154	154	154	154	75	75	75	75	75
R 10 120	196	196	196	196	196	79	79	79	79	79	211	211	211	211	211
R 10 140	136	136	136	136	136	72	72	72	72	72	146	146	146	146	146
R 10 160	101	101	101	101	101	65	65	65	65	65	105	105	105	105	105
R 10 180	80	80	80	80	80	58	58	58	58	58	81	81	81	81	81
R 10 200	69	69	69	69	69	52	52	52	52	52	69	69	69	69	69
R 11 25	34	39	39	58	65	21	34	34	46	51	27	20	20	36	41
R 11 30	29	40	40	62	70	23	42	42	62	69	27	21	22	41	47
R 11 35	21	31	31	56	64	24	41	41	75	86	28	23	23	47	55
R 11 40	16	29	29	55	64	26	47	47	88	101	28	28	29	50	57
R 11 45	16	35	35	64	74	28	56	56	100	114	28	31	31	52	58

R11	50	17	43	43	76	87	29	66	66	109	123	28	33	33	45	49
R11	55	17	49	49	89	103	31	74	74	116	130	26	35	35	35	35
R11	60	18	57	57	94	107	32	81	81	121	134	30	32	32	34	35
R11	65	25	68	68	102	113	34	85	85	123	136	36	26	27	32	34
R11	70	32	66	66	106	120	35	87	87	129	143	44	41	40	38	37
R11	75	36	60	60	102	117	37	86	86	130	145	53	47	46	43	42
R11	80	41	66	66	98	111	39	88	88	128	142	55	73	73	61	56
R11	85	49	61	61	88	99	41	84	84	128	142	69	81	81	86	87
R11	90	75	64	65	88	98	43	80	80	129	146	101	95	97	112	117
R11	100	144	144	144	144	144	154	154	154	154	154	75	75	75	75	75
R11	120	196	196	196	196	196	79	79	79	79	79	211	211	211	211	211
R11	140	136	136	136	136	136	72	72	72	72	72	146	146	146	146	146
R11	160	101	101	101	101	101	65	65	65	65	65	105	105	105	105	105
R11	180	80	80	80	80	80	58	58	58	58	58	81	81	81	61	81
R11	200	69	69	69	69	69	52	52	52	52	52	69	69	69	69	69
R12	25	34	46	45	72	81	21	34	34	47	51	27	31	31	56	64
R12	30	29	45	44	75	86	23	42	42	64	71	27	35	34	66	76
R12	35	21	32	32	63	74	24	41	41	81	94	27	37	37	73	84
R12	40	16	27	27	56	65	26	47	47	96	113	28	38	39	76	88
R12	45	16	32	32	64	74	28	56	56	109	127	28	39	39	73	85
R12	50	17	41	40	76	88	29	66	66	120	138	28	40	40	66	74
R12	55	17	47	47	88	101	31	74	74	129	148	26	39	39	58	65
R12	60	18	54	54	93	107	32	81	81	135	153	29	38	38	57	64
R12	65	25	61	61	98	111	34	85	85	138	156	35	44	43	73	82
R12	70	32	63	63	108	123	36	87	87	143	162	44	57	57	70	74
R12	75	34	58	58	98	113	37	86	86	144	163	52	73	74	86	90
R12	80	41	70	70	103	115	39	88	88	139	157	56	86	85	103	109
R12	85	48	68	67	94	105	41	85	84	136	150	68	97	96	114	120
R12	90	75	68	69	92	103	43	80	80	135	154	101	102	102	119	124
R12	100	144	144	144	144	144	154	154	154	154	154	75	75	75	75	75
R12	120	196	196	196	196	196	79	79	79	79	79	211	211	211	211	211
R12	140	136	136	136	136	136	72	72	72	72	72	146	146	146	146	146
R12	160	101	101	101	101	101	65	65	65	65	65	105	105	105	105	105
R12	180	80	80	80	80	80	58	58	58	58	58	81	81	81	81	81
R12	200	69	69	69	69	69	52	52	52	52	52	69	69	69	69	69
R13	25	36	53	57	87	105	25	43	44	63	81	26	25	29	51	103
R13	30	32	52	64	107	130	27	49	46	78	97	27	27	40	62	110
R13	35	26	49	82	130	154	29	50	57	97	120	28	30	50	71	117
R13	40	23	51	107	166	191	31	60	80	127	149	29	31	51	79	121
R13	45	24	54	131	205	237	33	67	108	166	192	29	33	49	78	116
R13	50	27	60	150	239	275	36	74	134	210	239	28	34	44	66	81
R13	55	26	64	165	266	307	39	80	155	240	275	26	35	42	57	63
R13	60	28	71	178	293	339	42	86	175	268	303	33	36	39	55	73
R13	65	35	78	185	314	372	40	95	193	299	340	38	40	45	53	80
R13	70	44	79	178	331	401	45	99	206	334	385	47	53	61	50	70
R13	75	52	72	154	319	404	50	99	203	362	431	53	66	82	69	66
R13	80	59	76	124	270	362	56	94	189	369	457	56	79	111	117	96
R13	85	70	76	99	173	268	60	90	149	315	411	71	91	138	170	177
R13	90	96	86	147	128	196	65	90	128	199	287	103	103	153	186	195
R13	100	178	162	252	238	246	172	169	261	246	270	91	83	79	103	127
R13	120	196	196	196	196	196	79	79	79	79	79	211	211	211	211	211
R13	140	136	136	136	136	136	72	72	72	72	72	146	146	146	146	146
R13	160	101	101	101	101	101	65	65	65	65	65	105	105	105	105	105
R13	180	80	80	80	80	80	58	58	58	58	58	81	81	81	81	81
R13	200	69	69	69	69	69	52	52	52	52	52	69	69	69	69	69

RANDOM WINDS (RW)

Rw 1	0	3	7	5	5	39	3	7	5	5	39
Kw 1	5	2	16	9	3	33	2	16	9	3	33
Kw 1	10	10	35	14	3	17	10	35	14	3	17
Rw 1	15	11	33	14	9	6	11	33	14	9	6
Kw 1	20	2	16	11	14	17	2	16	11	14	17
Rw 1	25	8	8	12	21	33	8	8	12	21	33
Rw 1	30	8	18	17	23	35	8	18	17	23	35
Kw 1	35	11	23	19	40	69	11	23	19	40	69
Rw 1	40	12	28	27	32	51	12	28	27	32	51
Rw 1	45	16	28	36	41	72	16	28	36	41	72
Kw 1	50	25	32	44	14	5	25	32	44	14	5
Kw 1	55	17	30	54	18	3	17	30	54	18	3
Kw 1	60	19	34	38	18	6	19	34	38	18	6
Kw 1	65	9	24	27	21	7	9	24	27	21	7
Rw 1	70	16	19	19	16	20	16	19	19	16	20
Rw 1	75	23	22	16	35	29	23	22	16	35	29
Kw 1	80	20	12	22	67	82	20	12	22	67	82
Rw 1	85	31	22	21	50	54	31	22	21	50	54
Rw 1	90	37	2	21	52	54	37	2	21	52	54
Rw 1	100	21	5	24	53	53	21	5	24	53	53
Kw 1	120	72	24	52	52	52	72	24	52	52	52
Kw 1	140	69	69	69	69	69	69	69	69	69	69
Rw 1	160	87	87	87	87	87	87	87	87	87	87
Rw 1	180	87	87	87	87	87	87	87	87	87	87
Kw 1	200	87	87	87	87	87	87	87	87	87	87
Rw 2	0	3	8	3	3	9	3	8	3	3	9
Rw 2	5	2	18	5	2	8	2	18	5	2	8
Rw 2	10	9	39	8	2	4	9	39	8	2	4
Rw 2	15	10	37	8	6	1	10	37	8	6	1
Kw 2	20	2	18	6	9	4	2	18	6	9	4
Rw 2	25	7	9	7	13	8	7	9	7	13	8
Kw 2	30	7	15	9	17	12	7	15	9	17	12
Rw 2	35	10	21	17	13	6	10	21	17	13	6
Rw 2	40	15	24	30	6	9	15	24	30	6	9
Rw 2	45	13	26	39	8	4	13	26	39	8	4
Rw 2	50	24	29	53	13	16	24	29	53	13	16
Rw 2	55	18	25	42	6	17	18	25	42	8	17
Rw 2	60	16	33	32	21	5	16	33	32	21	5
Rw 2	65	16	31	22	19	8	16	31	22	19	8
Rw 2	70	20	33	5	9	19	20	33	5	9	19
Kw 2	75	27	40	5	35	30	27	40	5	35	30
Kw 2	80	22	24	9	60	90	22	24	9	60	90
Rw 2	85	30	21	7	40	58	30	21	7	40	58
Rw 2	90	4	31	2	47	56	4	31	2	47	56
Rw 2	100	12	44	9	53	53	12	44	9	53	53
Rw 2	120	50	3	52	52	52	50	3	52	52	52
Rw 2	140	69	69	69	69	69	69	69	69	69	69
Rw 2	160	87	87	87	87	87	87	87	87	87	87
Rw 2	180	87	87	87	87	87	87	87	87	87	87
Rw 2	200	87	87	87	87	87	87	87	87	87	87
Rw 3	0	2	7	3	3	9	2	7	3	3	9
Rw 3	5	2	16	6	2	8	2	16	6	2	8
Rw 3	10	8	35	9	2	4	8	35	9	2	4
Rw 3	15	8	33	9	5	1	8	33	9	5	1
Rw 3	20	2	16	7	8	4	2	16	7	8	4
Rw 3	25	6	8	8	12	8	6	8	8	12	8
Rw 3	30	7	11	12	10	5	7	11	12	10	5

REPRODUCIBILITY OF THE
ORIGINAL PAGE IS POOR

Rw 3	35	10	18	14	13	10	10	18	14	13	10
Rw 3	40	11	14	21	10	2	11	14	21	10	2
Rw 3	45	12	23	27	19	11	12	23	27	19	11
Rw 3	50	15	22	34	26	26	15	22	34	26	26
Rw 3	55	14	19	30	25	26	14	19	30	25	26
Rw 3	60	15	25	24	21	37	15	25	24	21	37
Rw 3	65	23	30	47	14	7	23	30	47	14	7
Rw 3	70	24	15	40	10	20	24	15	40	10	20
Rw 3	75	30	20	25	35	29	30	20	25	35	29
Rw 3	80	23	47	11	32	82	23	47	11	32	82
Rw 3	85	28	15	7	48	54	28	15	7	48	54
Rw 3	90	39	20	4	51	54	39	20	4	51	54
Rw 3	100	27	21	29	53	53	27	21	29	53	53
Rw 3	120	31	40	52	52	52	31	40	52	52	52
Rw 3	140	69	69	69	69	69	69	69	69	69	69
Rw 3	160	87	87	87	87	87	87	87	87	87	87
Rw 3	180	87	87	87	87	87	87	87	87	87	87
Rw 3	200	87	87	87	87	87	87	87	87	87	87
Rw 4	0	2	4	11	9	5	2	4	11	9	5
Rw 4	5	1	8	17	8	4	1	8	17	8	4
Rw 4	10	4	17	26	8	3	4	17	26	8	3
Rw 4	15	4	15	19	7	2	4	15	19	7	2
Rw 4	20	3	9	7	5	3	3	9	7	5	3
Rw 4	25	5	7	9	9	5	5	7	9	9	5
Rw 4	30	9	10	14	14	13	9	10	14	14	13
Rw 4	35	10	12	11	13	8	10	12	11	13	8
Rw 4	40	11	15	11	12	5	11	15	11	12	5
Rw 4	45	12	13	15	5	5	12	13	15	5	5
Rw 4	50	15	14	14	13	2	15	14	14	13	2
Rw 4	55	14	11	18	10	13	14	11	18	10	13
Rw 4	60	17	18	16	14	15	17	18	16	14	15
Rw 4	65	18	19	4	8	6	18	19	4	8	6
Rw 4	70	4	27	7	11	22	4	27	7	11	22
Rw 4	75	27	19	5	34	28	27	19	5	34	28
Rw 4	80	14	22	13	4	75	14	22	13	4	75
Rw 4	85	38	26	7	55	51	38	26	7	55	51
Rw 4	90	20	24	6	54	53	20	24	6	54	53
Rw 4	100	58	25	4	53	53	58	25	4	53	53
Rw 4	120	22	71	52	52	52	22	71	52	52	52
Rw 4	140	69	69	69	69	69	69	69	69	69	69
Rw 4	160	87	87	87	87	87	87	87	87	87	87
Rw 4	180	87	87	87	87	87	87	87	87	87	87
Rw 4	200	87	87	87	87	87	87	87	87	87	87
Rw 5	0	1	1	12	13	6	1	1	12	13	6
Rw 5	5	1	1	18	13	6	1	1	18	13	6
Rw 5	10	1	3	27	13	6	1	3	27	13	6
Rw 5	15	1	1	18	6	6	1	1	18	8	6
Rw 5	20	4	3	3	3	6	4	3	3	3	6
Rw 5	25	5	5	6	8	12	5	5	6	8	12
Rw 5	30	9	6	9	8	11	9	6	9	8	11
Rw 5	35	9	6	11	6	13	9	6	11	6	13
Rw 5	40	9	15	11	4	16	9	15	11	4	16
Rw 5	45	8	13	12	9	10	8	13	12	9	10
Rw 5	50	11	18	16	20	15	11	18	16	20	15
Rw 5	55	14	13	20	21	6	14	13	20	21	6
Rw 5	60	9	13	6	11	15	9	13	6	11	15
Rw 5	65	12	11	10	9	5	12	11	10	9	5

RW 5 70	7	22	6	20	23	7	22	6	20	23
RW 5 75	21	38	10	10	27	21	38	10	10	27
KW 5 80	11	15	2	24	67	11	15	2	24	67
RW 5 85	42	10	4	29	47	42	10	4	29	47
KW 5 90	24	8	7	41	51	24	8	7	41	51
RW 5 100	41	36	1	53	53	41	36	1	53	53
RW 5 120	16	20	52	52	52	16	20	52	52	52
RW 5 140	69	69	69	69	69	69	69	69	69	69
RW 5 160	87	87	87	87	87	87	87	87	87	87
RW 5 180	87	87	87	87	87	87	87	87	87	87
RW 5 200	87	87	87	87	87	87	87	87	87	87
RW 6 0	1	1	4	5	2	1	1	4	5	2
RW 6 5	1	1	6	5	2	1	1	6	5	2
RW 6 10	1	2	9	5	2	1	2	9	5	2
KW 6 15	1	1	6	3	2	1	1	6	3	2
KW 6 20	6	2	1	1	2	6	2	1	1	2
KW 6 25	7	4	2	3	4	7	4	2	3	4
RW 6 30	8	5	3	4	5	8	5	3	4	5
RW 6 35	9	5	3	5	6	9	5	3	5	6
KW 6 40	6	5	2	6	9	6	5	2	6	9
RW 6 45	7	6	3	8	12	7	6	3	8	12
KW 6 50	11	8	5	9	18	11	8	5	9	18
RW 6 55	16	8	2	9	16	16	8	2	9	16
RW 6 60	12	10	5	11	15	12	10	5	11	15
KW 6 65	9	11	10	9	4	9	11	10	9	4
RW 6 70	11	10	16	20	24	11	10	16	20	24
RW 6 75	14	26	9	14	26	14	26	9	14	26
RW 6 80	7	32	13	19	59	7	32	13	19	59
RW 6 85	47	28	1	10	43	47	28	1	10	43
RW 6 90	28	23	17	34	49	28	23	17	34	49
RW 6 100	24	28	15	53	53	24	28	15	53	53
RW 6 120	9	44	52	52	52	9	44	52	52	52
RW 6 140	69	69	69	69	69	69	69	69	69	69
RW 6 160	87	87	87	87	87	87	87	87	87	87
KW 6 180	87	87	87	87	87	87	87	87	87	87
KW 6 200	87	87	87	87	87	87	87	87	87	87
RW 7 0	1	1	4	5	1	1	1	4	5	1
KW 7 5	1	1	6	5	1	1	1	6	5	1
RW 7 10	1	2	9	5	1	1	2	9	5	1
RW 7 15	1	1	6	3	1	1	1	6	3	1
KW 7 20	4	2	1	1	1	4	2	1	1	1
KW 7 25	5	4	2	3	2	5	4	2	3	2
RW 7 30	5	5	3	4	4	5	5	3	4	4
KW 7 35	6	6	2	3	3	6	6	2	3	3
RW 7 40	11	7	3	3	4	11	7	3	3	4
RW 7 45	8	7	6	6	9	8	7	6	6	9
RW 7 50	12	7	21	5	6	12	7	21	5	6
RW 7 55	17	9	39	10	14	17	9	39	10	14
RW 7 60	20	13	7	8	21	20	13	7	8	21
RW 7 65	5	21	20	8	3	5	21	20	8	3
RW 7 70	14	22	14	20	25	14	22	14	20	25
RW 7 75	8	33	14	16	25	8	33	14	16	25
RW 7 80	4	3	22	14	52	4	3	22	14	52
RW 7 85	51	25	20	2	40	51	25	20	2	40
RW 7 90	32	13	30	27	47	32	13	30	27	47
RW 7 100	32	13	31	53	53	32	13	31	53	53
RW 7 120	41	67	52	52	52	41	67	52	52	52

Rw 7 140	69	69	69	69	69	69	69	69	69	69
Rw 7 160	87	87	87	87	87	87	87	87	87	87
Rw 7 180	87	87	87	87	87	87	87	87	87	87
Rw 7 200	87	87	87	87	87	87	87	87	87	87
Rw 8 0	2	1	4	3	5	2	1	4	3	5
Rw 8 5	2	1	6	3	5	2	1	6	3	5
Rw 8 10	2	2	9	3	5	2	2	9	3	5
Rw 8 15	2	1	6	2	5	2	1	6	2	5
Rw 8 20	6	2	1	1	5	6	2	1	1	5
Rw 8 25	8	3	2	2	9	8	3	2	2	9
Rw 8 30	11	4	3	2	3	11	4	3	2	3
Rw 8 35	8	5	4	2	6	8	5	4	2	6
Rw 8 40	13	5	4	4	19	13	5	4	4	19
Rw 8 45	10	8	3	2	7	10	8	3	2	7
Rw 8 50	16	8	10	6	6	16	8	10	6	6
Rw 8 55	16	10	8	6	5	16	10	8	6	5
Rw 8 60	22	16	6	12	12	22	16	6	12	12
Rw 8 65	27	25	15	6	2	27	25	15	8	2
Rw 8 70	14	16	12	20	26	14	16	12	20	26
Rw 8 75	13	40	18	22	24	13	40	18	22	24
Rw 8 80	4	24	31	33	44	4	24	31	33	44
Rw 8 85	40	21	38	30	36	40	21	38	30	36
Rw 8 90	20	8	43	41	45	20	8	43	41	45
Rw 8 100	100	19	47	53	53	100	19	47	53	53
Rw 8 120	90	24	52	52	52	90	24	52	52	52
Rw 8 140	69	69	69	69	69	69	69	69	69	69
Rw 8 160	87	87	87	87	87	87	87	87	87	87
Rw 8 180	87	87	87	87	87	87	87	87	87	87
Rw 8 200	87	87	87	87	87	87	87	87	87	87
Rw 9 0	1	1	6	5	2	1	1	6	5	2
Rw 9 5	1	1	9	5	2	1	1	9	5	2
Rw 9 10	1	2	14	5	2	1	2	14	5	2
Rw 9 15	1	1	9	3	2	1	1	9	3	2
Rw 9 20	5	2	2	1	2	5	2	2	1	2
Rw 9 25	6	3	3	3	3	6	3	3	3	3
Rw 9 30	8	5	4	4	3	8	5	4	4	3
Rw 9 35	13	6	3	4	3	13	6	3	4	3
Rw 9 40	7	6	3	5	5	7	6	3	5	5
Rw 9 45	9	7	11	5	5	9	7	11	5	5
Rw 9 50	15	9	16	6	7	15	9	16	6	7
Rw 9 55	13	10	17	8	5	13	10	17	8	5
Rw 9 60	13	14	4	13	18	13	14	4	13	18
Rw 9 65	5	13	7	14	3	5	13	7	14	3
Rw 9 70	13	16	25	24	25	13	16	25	24	25
Rw 9 75	17	15	11	26	25	17	15	11	26	25
Rw 9 80	3	19	50	49	52	3	19	50	49	52
Rw 9 85	28	20	39	44	40	28	20	39	44	40
Rw 9 90	22	18	40	48	47	22	18	40	48	47
Rw 9 100	71	28	45	53	53	71	28	45	53	53
Rw 9 120	64	51	52	52	52	64	51	52	52	52
Rw 9 140	69	69	69	69	69	69	69	69	69	69
Rw 9 160	87	87	87	87	87	87	87	87	87	87
Rw 9 180	87	87	87	87	87	87	87	87	87	87
Rw 9 200	87	87	87	87	87	87	87	87	87	87
Rw10 0	2	2	5	6	10	2	2	5	6	10
Rw10 5	2	4	8	6	4	2	4	8	6	4
Rw10 10	5	8	12	6	3	5	8	12	6	3

Rw10	15	5	7	9	5	2	5	7	9	5	2
Kw10	20	4	4	3	3	3	4	4	3	3	3
Kw10	25	6	3	4	6	5	6	3	4	6	5
Rw10	30	7	4	8	7	3	7	4	8	7	3
Rw10	35	10	4	7	11	16	10	4	7	11	16
Rw10	40	12	6	10	11	16	12	6	10	11	16
Kw10	45	11	7	11	28	57	11	7	11	28	57
Rw10	50	21	12	14	27	8	21	12	14	27	8
Rw10	55	17	14	7	28	7	17	14	7	28	7
Rw10	60	18	19	5	26	3	18	19	5	26	3
Rw10	65	28	18	14	19	4	28	18	14	19	4
Rw10	70	13	16	19	27	24	13	16	19	27	24
Rw10	75	22	14	36	29	26	22	14	36	29	26
Kw10	80	3	10	69	64	59	3	10	69	64	59
Rw10	85	17	54	39	57	43	17	54	39	57	43
Rw10	90	24	10	37	55	49	24	10	37	55	49
Rw10	100	41	26	43	53	53	41	26	43	53	53
Rw10	120	37	60	52	52	52	37	60	52	52	52
Kw10	140	69	69	69	69	69	69	69	69	69	69
Rw10	160	87	87	87	87	87	87	87	87	87	87
Rw10	180	87	87	87	87	87	87	87	87	87	87
Kw10	200	87	87	87	87	87	87	87	87	87	87
Rw11	0	2	5	3	2	14	2	5	3	2	14
Kw11	5	2	12	5	1	12	2	12	5	1	12
Kw11	10	8	26	8	1	6	8	26	8	1	6
Kw11	15	8	25	8	4	2	8	25	8	4	2
Kw11	20	2	12	6	6	6	2	12	6	6	6
Rw11	25	6	6	7	9	12	6	6	7	9	12
Rw11	30	7	8	10	13	17	7	8	10	13	17
Kw11	35	10	11	12	14	17	10	11	12	14	17
Rw11	40	12	17	12	15	34	12	17	12	15	34
Kw11	45	11	13	21	34	53	11	13	21	34	53
Rw11	50	21	13	14	31	26	21	13	14	31	26
Rw11	55	17	16	11	29	6	17	16	11	29	6
Rw11	60	18	17	9	30	18	18	17	9	30	18
Kw11	65	19	23	23	25	5	19	23	23	25	5
Rw11	70	24	31	26	31	23	24	31	26	31	23
Rw11	75	29	25	32	33	27	29	25	32	33	27
Rw11	80	16	39	52	80	67	16	39	52	80	67
Rw11	85	22	23	39	71	47	22	23	39	71	47
Rw11	90	28	24	34	62	51	28	24	34	62	51
Rw11	100	36	33	41	53	53	36	33	41	53	53
Rw11	120	34	36	52	52	52	34	36	52	52	52
Rw11	140	69	69	69	69	69	69	69	69	69	69
Rw11	160	87	87	87	87	87	87	87	87	87	87
Rw11	180	87	87	87	87	87	87	87	87	87	87
Rw11	200	87	87	87	87	87	87	87	87	87	87
Rw12	0	3	7	8	4	28	3	7	8	4	28
Rw12	5	2	16	14	2	24	2	16	14	2	24
Rw12	10	10	35	21	2	12	10	35	21	2	12
Rw12	15	11	33	21	7	4	11	33	21	7	4
Rw12	20	12	16	17	11	12	12	16	17	11	12
Rw12	25	8	8	18	17	24	8	8	18	17	24
Rw12	30	12	17	13	20	25	12	17	13	20	25
Rw12	35	12	18	17	23	32	12	18	17	23	32
Rw12	40	16	18	20	32	59	16	18	20	32	59
Rw12	45	15	29	35	9	48	15	29	35	9	48

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Rw12	50	17	26	30	28	32	17	26	30	28	32
Rw12	55	15	25	37	28	28	15	25	37	28	28
Rw12	60	15	24	26	28	37	15	24	26	28	37
Rw12	65	26	26	31	23	6	26	26	31	23	6
Rw12	70	10	28	32	24	22	10	28	32	24	22
Rw12	75	36	11	27	34	28	36	11	27	34	28
Rw12	80	28	28	35	73	75	28	28	35	73	75
Rw12	85	26	22	39	61	51	26	22	39	61	51
Rw12	90	33	27	30	57	53	33	27	30	57	53
Rw12	100	30	55	39	53	53	30	55	39	53	53
Rw12	120	31	45	52	52	52	31	45	52	52	52
Rw12	140	69	69	69	69	69	69	69	69	69	69
Rw12	160	87	87	87	87	87	87	87	87	87	87
Rw12	180	87	87	87	87	87	87	87	87	87	87
Rw12	200	87	87	87	87	87	87	87	87	87	87
Rw13	0	2	4	6	5	11	2	4	6	5	11
Rw13	5	2	8	9	5	9	2	8	9	5	9
Rw13	10	5	17	14	5	5	5	17	14	5	5
Rw13	15	5	16	11	5	3	5	16	11	15	3
Rw13	20	4	9	5	5	5	4	9	5	5	5
Rw13	25	6	6	7	9	10	6	6	7	9	10
Rw13	30	8	9	9	11	11	8	9	9	11	11
Rw13	35	10	11	10	12	16	10	11	10	12	16
Rw13	40	12	13	13	12	19	12	13	13	12	19
Rw13	45	11	15	18	17	24	11	15	18	17	24
Rw13	50	17	17	23	17	14	17	17	23	17	14
Rw13	55	16	16	24	17	12	16	16	24	17	12
Rw13	60	16	20	15	18	17	16	20	15	18	17
Rw13	65	16	21	19	15	5	16	21	19	15	5
Rw13	70	14	21	18	19	23	14	21	18	19	23
Rw13	75	22	25	17	27	27	22	25	17	27	27
Rw13	80	13	23	27	43	67	13	23	27	43	67
Rw13	85	33	24	22	41	47	33	24	22	41	47
Rw13	90	26	17	23	47	51	26	17	23	47	51
Rw13	100	41	28	27	53	53	41	28	27	53	53
Rw13	120	41	40	52	52	52	41	40	52	52	52
Rw13	140	69	69	69	69	69	69	69	69	69	69
Rw13	160	87	87	87	87	87	87	87	87	87	87
Rw13	180	87	87	87	87	87	87	87	87	87	87
Rw13	200	87	87	87	87	87	87	87	87	87	87

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QUASI-BIENNIAL OSCILLATIONS, (QP, QD, QT)

QP 15	2	110	1	440	2	415	2	380	2	375
QP 20	5	260	3	490	3	435	3	375	3	360
QP 25	6	394	4	523	5	470	6	420	6	405
QP 30	6	580	4	642	11	500	16	340	18	280
QP 35	8	701	6	613	19	480	29	330	33	300
QP 40	9	745	10	653	29	490	46	310	51	245
QP 45	9	819	7	767	30	605	50	310	55	220
QP 50	8	837	6	66	29	620	46	305	51	200
QP 55	7	808	11	127	27	650	44	265	49	175
QP 60	7	737	23	143	26	660	33	280	35	190
QP 65	6	680	25	205	25	690	25	265	25	170
QP 70	5	610	23	255	21	710	16	250	13	160
QP 75	4	550	15	300	14	730	10	240	8	150

QP 80	2	485	8	350	7	755	6	230	5	140
QP 85	1	420	3	400	3	780	2	220	1	130
QP 90	0	360	0	450	0	805	0	210	0	120
QU 15	3	711	1	465	1	610	1	785	1	850
QU 20	5	130	4	530	2	575	2	620	2	640
QU 25	8	277	5	587	4	545	3	495	2	475
QU 30	12	400	2	658	8	500	10	335	10	290
QU 35	8	596	4	489	14	425	20	350	22	325
QU 40	9	714	7	605	21	470	32	315	35	280
QU 45	11	767	11	700	31	525	46	335	51	280
QU 50	11	808	5	822	29	640	52	290	58	210
QU 55	8	847	6	64	33	620	54	270	61	205
QU 60	13	792	18	77	40	630	52	270	56	205
QU 65	10	741	13	122	32	645	44	260	47	190
QU 70	7	690	9	140	25	660	34	260	38	190
QU 75	4	650	6	152	16	660	22	260	23	190
QU 80	2	600	3	162	8	660	11	260	12	190
QU 85	1	555	1	170	3	660	4	260	4	190
QU 90	0	510	0	170	0	660	0	260	0	190
QT 15	2	467	1	750	3	351	4	120	4	0
QT 20	4	568	2	100	5	880	7	180	8	75
QT 25	6	604	2	285	8	750	11	225	12	150
QT 30	12	770	2	630	10	510	13	280	14	240
QT 35	6	868	5	704	15	525	19	300	20	270
QT 40	2	43	4	731	16	548	23	300	25	260
QT 45	9	70	6	192	8	700	10	250	11	210
QT 50	3	287	4	222	3	600	1	860	0	770
QT 55	3	566	6	213	6	540	7	700	7	630
QT 60	6	403	10	254	10	450	11	450	11	350
QT 65	5	518	8	270	9	440	10	370	10	270
QT 70	3	633	6	285	6	400	7	190	7	90
QT 75	3	685	4	297	4	365	5	150	5	30
QT 80	2	800	3	310	3	340	3	70	3	840
QT 85	1	13	1	322	1	300	2	830	2	740
QT 90	0	97	0	332	0	270	0	730	0	640

QUASI-BIENNIAL OSCILLATIONS-WINDS, (QU, QV)

QU 15	70	180	1	45	8	165	20	280	30	305
QU 20	130	280	3	140	20	195	45	260	60	280
QU 25	163	382	4	192	35	230	62	265	75	285
QU 30	161	506	45	265	58	250	69	235	73	225
QU 35	125	761	64	350	55	295	51	245	50	220
QU 40	120	778	48	435	40	320	32	230	30	195
QU 45	117	820	9	533	18	320	28	135	30	70
QU 50	99	836	60	740	30	485	19	240	12	170
QU 55	66	235	62	720	50	485	38	275	30	210
QU 60	54	314	86	682	75	460	60	265	51	200
QU 65	42	420	75	720	65	490	50	270	40	200
QU 70	30	520	65	720	50	520	35	280	30	205
QU 75	23	620	50	720	35	550	25	285	20	210
QU 80	16	720	36	720	20	580	13	295	10	215
QU 85	9	820	20	720	10	615	5	305	5	220
QU 90	0	50	0	720	0	650	0	315	0	230
QV 15	2	450	1	718	5	791	7	835	7	15
QV 20	4	520	2	620	10	710	15	760	15	830
QV 25	6	602	3	510	15	600	22	675	24	700
QV 30	8	562	6	288	15	475	22	650	24	720

QV 35	5	587	16	382	22	485	27	585	29	630
QV 40	8	687	17	292	23	440	28	575	30	640
QV 45	1	96	11	209	19	325	25	430	27	475
QV 50	9	105	12	593	22	240	32	370	37	405
QV 55	19	431	4	651	9	165	14	285	17	320
QV 60	40	660	58	625	35	30	14	140	7	190
QV 65	30	769	45	480	29	0	12	150	5	135
QV 70	22	7	28	376	22	790	9	90	3	80
QV 75	14	285	17	279	15	710	6	20	2	25
QV 80	8	393	9	181	8	630	4	815	1	790
QV 85	3	586	3	84	4	550	2	750	1	635
QV 90	0	770	0	717	0	470	0	685	0	580

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APPENDIX B
SAMPLE INPUT AND OUTPUT FOR THE PROFILE PROGRAM

Input to PROFILE is as follows:

(All input data cards are in free field format.)

CARD 1	INITIAL HEIGHT	-	Height of starting position, km
	INITIAL LATITUDE	-	Latitude of starting position (degrees, southern latitudes negative)
	INITIAL WEST LONGITUDE	-	West longitude of starting position (degrees, 0 to 360 degrees, or east longitudes negative)
	F10.7	-	Solar 10.7 cm radio noise flux (10^{-22} watts/m ²) at time of calculations. Use zero if height does not go over 90 km. Use 230 for design applications or consult Aerospace Environment Division (AED) of Marshall Space Flight Center (MSFC) for monthly predictions.
	MEAN F10.7	-	81 day mean solar 10.7 cm flux. Use zero if height does not go over 90 km. Use 230 for design applications or consult AED, MSFC for monthly predictions.
	AP	-	Geomagnetic index a_p . Use zero if height does not go over 90 km. Use 20.3 for design steady state conditions, or 400 for maximum conditions, or consult AED, MSFC.
	DATE	-	Date for starting time of calculations (month, date, two digit year). Use month 13 for annual reference period.
	GREENWICH TIME	-	Time for starting position (hours, minutes, seconds). Use time corresponding to local time = 0900 for design steady state, or 1400 for maximum conditions.
	LAT INCREMENT	-	Latitude displacement (degrees) between successive positions (new lat = old lat + lat increment). Use zero if trajectory positions are to be read in.
	WEST LON INCREMENT	-	West longitude displacement (degrees) between successive positions (new lon = old lon + lon increment). Use zero if trajectory positions are to be read in.
	HEIGHT INCREMENT	-	Height decrease (km) between successive positions (new height = old height - height increment). Normal profiles are generated downward. If an upward generated profile is desired set height increment negative.
	MAXIMUM NUMBER OF POSITIONS	-	Number of positions to be computed, <u>not</u> including initial position. Use zero if trajectory positions are to be read in.

CARD 1 CONT'D	TIME INCREMENT	-	Time displacement (seconds) between successive positions for automatically generated profiles (new time = old time + time increment)
	TRAJECTORY OPTION	-	0 for linear profile generated automatically internal to the program, greater than 0 for a trajectory with each position to be read in.
	PUNCH OPTION	-	0 for no punch output of atmospheric parameter values, non-zero to get punch output.
CARD 2	GROVES INPUT UNIT	-	Unit number for tape containing Groves and stationary perturbations (SCIDAT tape in Appendix A). Use any available unit number.
	RANDOM INPUT UNIT	-	Unit number of file from which random perturbation data are to be read. If same as Groves input unit, these are read from SCIDAT tape. If card input, use 5.
	QBO INPUT UNIT	-	Unit number of file from which QBO parameters are to be read. If same as Groves input unit, these are read from SCIDAT tape. If card input, use 5.
	4-D INPUT UNIT	-	Unit number for 4-D input data tape. Use any available unit number.
	RANDOM OPTION	-	1 means compute random perturbation output, 2 means do not compute random perturbation output.
	QBO OPTION	-	1 means compute QBO output, 2 means do not compute QBO output.
	FIRST RANDOM NUMBER	-	Initial number for random number generator used to compute random perturbations (can be any odd positive integer). Use 1 for standard design applications.
	NMC READ OPTION	-	0 means read NMC grid data from SCIDAT tape, otherwise these data are read from cards.
	4-D, P, D, T, SCRATCH UNIT	-	Unit number for scratch file for 4-D grid profiles required in computations. Use any available unit number. This normally is a temporary drum file.
	NMC GRID POINTS SCRATCH UNIT	-	Unit number for scratch file to store NMC grid point data. Use any available unit number. This normally is a temporary drum file.
CARD 3 (OPTIONAL)*	INITIAL P, D, T	-	Initial values of random relative pressure, density, and temperature perturbations, percent. Use zeros for standard design applications.
	SIGMA P, D, T	-	Initial values of relative standard deviation (percent) for random pressure, density, and temperature. Use zeros for standard design applications.
	INITIAL U, V	-	Initial values of random wind components, m/s. Use zeros for standard design applications.
	SIGMA U, V	-	Initial values of standard deviation for random winds, m/s. Use zeros for standard design applications.

* - Include card 3 only if random option = 1.

TRAJECTORY INPUT	-	Use only if linear profile is not to be generated automatically. Each record has time (seconds), height (km), latitude (degrees), and west longitude (degrees).
TRAJECTORY BACK- UP CARD	-	Only if trajectory input is used. Same form as a trajectory position but with any negative height value.

The trajectory input cards are optional, in free field format. If included, use as many cards as necessary.

A sample output listing is shown beginning on page 112. The input for this sample run would be:

```

CARD 1:  121.92, 57.97, 350.80, 136., 155., 9., 1, 1, 73, 0, 0, 0, .0, .0,
        .0, 58, 0, 58, 0,
CARD 2:  3, 3, 3, 4, 1, 1, 8941, 0, 12, 13,
CARD 3:  .0, .0, .0, .0, .0, .0, .0, .0, .0, .0,
TRAJECTORY INPUT:  0, 121.92, 57.97, 350.80,
                  30, 118.82, 59.80, 352.80,
                  50, 116.73, 61.00, 354.50,
                  :
                  :
                  :
                  1850, 5.11, 34.61, 120.43
                  1882, 3.53, 34.64, 120.47
                  9999, -9.9, 99.99, 99.99, (trajectory backup card)

```

Input for the sample output listing beginning on page 120 is as follows:

```

CARD 1:  92.9, 28.45, 80.53, .0, .0, .0, 1, 1, 73, 0, 0, 0, .0, .0, 2., 46,
        0, 0, 0,
CARD 2:  3, 3, 3, 4, 1, 1, 8941, 0, 12, 13,
CARD 3:  -12.7, -7.2, -5.6, 10.21, 10.43, 9.91, -18.0, -16.0, 19.96, 19.96,

```

A SUMMARY OF THE ORGANIZATION OF AN
INPUT DATA DECK IS AS FOLLOWS

Initial Data

Card 1, See Section 4 or earlier in this Appendix

Card 2, See Section 4 or earlier in this Appendix

Card 3, Optional, included only if random option = 1

NMC Grid Data

Optional. Include as card input only if this is not to be read from the SCIDAT data tape.

Random Perturbation Data

Optional. Include as card input only if the random input unit is 5 and these data are not to be read from the SCIDAT data tape or some other input file. Do not include if random option = 2.

QBO Parameters

Optional. Include as card input only if the QBO input unit is 5 and these data are not to be read from the SCIDAT data tape or some other file. Do not include if QBO option = 2.

Trajectory Position Data and Backup Card

Optional. Include if trajectory, rather than linear profile generated by the program, is to be evaluated.

More Data of the Same Kind (Starting with Initial Data, Card 1)

If additional trajectories or profiles are to be evaluated, the data may be input one set immediately after the other. The program is actually more efficient for such multiple runs if the month remains the same. This is because as long as the month remains the same the SCIDAT data tape read can be avoided for each subsequent data set.

OUTPUT OF PROFILE IS AS FOLLOWS

- JULIAN DATE - Computed from input date, set equal to zero for month 13 (annual average)
- HEIGHT, LAT, LON, TIME - Position and time where atmospheric parameters are evaluated
- UNPERTURBED PRESSURE DENSITY, TEMPERATURE AND GEOSTROPHIC WIND (monthly mean values) - Computed from Jacchia, 4-D, or Groves - plus - stationary perturbations, depending on height.
- TOTAL PRESSURE, DENSITY, TEMPERATURE, AND WIND - Monthly means plus random perturbations and QBO perturbations
- THERMAL WIND SHEAR - From thermal wind equations using finite differences of Jacchia, 4-D, or Groves - plus - stationary perturbations, depending on height.
- PERTURBATION VALUES - Stationary perturbations, QBO perturbations and amplitudes, and random perturbations and magnitudes. Perturbations are those which were added to monthly means to produce total results output.

Following is a listing of sample output from the PROFILE program. Initial lines of output are merely listings of the input data for easy reference. These listings are provided to indicate formats and kinds of input and output data. For a listing of the input cards for these sample outputs, see page 109.

SAMPLE PROFILE PROGRAM OUTPUT
JANUARY MISSION 3 RE-ENTRY AND RETURN TRAJECTORY

INITIAL HEIGHT = 121.92 KM
 F10.7 = 136.00
 DATE = 1/ 1/73
 LAT INCREMENT = .00 DEG
 MAXIMUM NUMBER OF POSITIONS = 58
 TRAJECTORY OPTION = 58

INITIAL LAT = 57.97 DEG
 MEAN F10.7 = 155.00
 GREENWICH TIME = 0: 0: 0
 WEST LON INCREMENT = .00 DEG
 TIME INCREMENT = 0 SEC
 PUNCH OPTION = 0

INITIAL WEST LON = 350.80 DEG
 AP = 9.00
 HEIGHT INCREMENT = .00 KM

INITIAL P,D,T = .00 % .00 % .00 %
 INITIAL U,V = .00 M/S .00 M/S

SIGMA P,D,T = 19.02 % 7.83 % 20.48 %
 SIGMA U,V = 53.63 M/S 53.03 M/S

INITIAL P,D,T = 19.02 % 7.83 % 20.48 %
 INITIAL U,V = 53.63 M/S 53.03 M/S

** PERCENT DEVIATIONS FROM 1962 US STANDARD ATMOSPHERE APPEAR BELOW PRESSURE, DENSITY, AND TEMPERATURE VALUES **

HEIGHT (KM)	LAT (DEG)	WEST LON (DEG)	UNPERTURBED (MONTHLY MEAN)			MEAN PLUS PERTURBATIONS			THERMAL			PERTURBATION VALUES		
			PRES. (INT/ M**2)	DENS. (KG/ M**3)	TEMP (DEG WIND (M/S) F-W N-S)	PRES. (NT/ M**2)	DENS. (KG/ M**3)	TEMP (DEG WIND (M/S) E-W N-S)	WIND SHEAR (M/S/KM)	P	D	T	U	V
118.82 30	59.80	352.80	.303-02 7.7%	.307-07 9.2%	-10. -1. .326-02 15.0%	.318-07 13.0%	330. -2.5%	-46. 14. 1. -0.	.0 .0 .0 .0 .0 .0	.0 .0 .0 .0 .0 .0	.0 .0 .0 .0 .0 .0	.0 .0 .0 .0 .0 .0	SP GBO 0. MAG	
116.73 50	61.00	354.50	.373-02 8.1%	.405-07 10.6%	-10. -1. .371-02 7.7%	.380-07 3.9%	315. -1.6%	-37. 29. 0. -0.	.0 .0 .0 .0 .0 .0	.0 .0 .0 .0 .0 .0	.0 .0 .0 .0 .0 .0	.0 .0 .0 .0 .0 .0	SP GBO 0. MAG	
114.62 70	62.19	355.80	.471-02 9.7%	.547-07 12.3%	-9. -1. .523-02 21.0%	.616-07 26.4%	276. -8.1%	-4. 33. 0. -0.	.0 .0 .0 .0 .0 .0	.0 .0 .0 .0 .0 .0	.0 .0 .0 .0 .0 .0	.0 .0 .0 .0 .0 .0	SP GBO 0. MAG	
112.47 90	63.36	357.46	.616-02 12.8%	.760-07 14.1%	-3. -1. .670-02 22.8%	.784-07 17.8%	280. -1.1%	-3. 21. 0. -0.	.0 .0 .0 .0 .0 .0	.0 .0 .0 .0 .0 .0	.0 .0 .0 .0 .0 .0	.0 .0 .0 .0 .0 .0	SP GBO 0. MAG	
109.19 120	65.09	.23	.934-02 14.5%	.126-06 14.0%	9. -1. .109-01 33.6%	.147-06 33.0%	244. -3.5%	-9. -6. 0. -0.	.0 .0 .0 .0 .0 .0	.0 .0 .0 .0 .0 .0	.0 .0 .0 .0 .0 .0	.0 .0 .0 .0 .0 .0	SP GBO 0. MAG	

106.99 140	66.21	2.27	.127-01 10.5%	.181-06 16.9%	233. -4.0%	21.	-0.	.147-01 15.1%	.198-06 26.0%	249. 2.3%	14.	-15.	-0.	-0.	.0 16.7 16.8	.0 16.7 12.0	.0 13.7 49.	0. 0. -5.	0. MAG RAND	SIG
104.77 160	67.30	4.49	.172-01 16.3%	.257-06 17.1%	223. -4.1%	29.	-0.	.186-01 26.1%	.268-06 21.9%	233. .0%	76.	-36.	-0.	-0.	.0 0. 16.1 16.2	.0 0. 9.5 12.8	.0 0. 6.6 12.3	0. 0. -8. 49.	0. MAG RAND	SIG
102.53 180	68.37	6.92	.234-01 14.7%	.160-06 12.9%	219. -1.5%	50.	-0.	.236-01 15.2%	.353-06 10.7%	224. .9%	6.	24.	-0.	-0.	.0 0. 8.4 15.6	.0 0. 4.1 13.0	.0 0. 4.3 10.7	0. 0. 47. 50.	0. MAG RAND	SIG
101.38 190	68.89	8.21	.274-01 12.8%	.427-06 9.7%	217. -.0%	55.	-0.	.267-01 9.0%	.414-06 6.4%	217. .4%	-15.	40.	-0.	-0.	.0 0. 5 15.1	.0 0. 1.9 14.5	.0 0. 2.4 9.2	0. 0. -44. 51.	0. MAG RAND	SIG
99.10 210	69.90	10.99	.372-01 7.4%	.591-06 1.7%	214. 3.3%	71.	-0.	.388-01 11.8%	.594-06 2.2%	222. 7.0%	7.	49.	-0.	-0.	.0 0. -2.6 14.8	.0 0. -3.0 14.9	.0 0. 4 8.4	0. 0. -71. 51.	0. MAG RAND	SIG
96.80 230	70.86	14.03	.510-01 1.3%	.813-06 -6.8%	215. 7.0%	53.	-0.	.535-01 6.1%	.846-06 -3.0%	217. 7.9%	-3.	7.	-0.	-0.	.0 0. 4.1 14.0	.0 0. 5 15.3	.0 0. 3.6 7.9	0. 0. -65. 53.	0. MAG RAND	SIG
94.51 250	71.77	17.37	.697-01 -5.7%	.112-05 -15.8%	215. 10.9%	59.	-0.	.701-01 -5.1%	.110-05 -17.1%	220. 13.3%	-20.	-31.	-0.	-0.	.0 0. 4.9 12.8	.0 0. 4.1 15.0	.0 0. 8 8.9	0. 0. -56. 53.	0. MAG RAND	SIG
92.19 270	72.63	21.02	.903-01 -13.0%	.156-05 -24.4%	215. 14.6%	67.	-0.	.953-01 -13.0%	.159-05 -22.6%	207. 10.7%	-12.	-52.	-0.	-0.	.0 0. 6 11.8	.0 0. 1.8 14.8	.0 0. 2.2 9.9	0. 0. -78. 53.	0. MAG RAND	SIG
															.0 0. 0.	.0 0. 0.	.0 0. 0.	0. MAG RAND	SIG	

89.88	73.41	25.02	.133+00	.217-05	214.	67.	-5.	.151+00	.256-05	205.	-24.	-21.	0.	.0	.0	0.	MAG
290			-20.7%	-72.9%	18.0%			-10.1%	-21.1%	13.2%				-1.1	2.4	-3.5	-78.
														10.7	14.0	10.9	52.
																	SIG
87.58	74.11	20.38	.190+00	.311-05	213.	71.	-4.	.102+00	.315-05	213.	b.	-5.	0.	.2	.1	.2	SP
310			-25.9%	-77.1%	17.6%			-25.0%	-36.3%	17.7%				-0.0	-0.0	0.	0.
														.0	.0	0.	0.
														13.1	17.7	4.6	-90.
														9.7	14.4	11.9	52.
																	SIG
84.19	74.99	30.59	.321+00	.526-05	211.	68.	-4.	.340+00	.546-05	215.	25.	23.	0.	.4	.2	.0	SP
340			-32.9%	-42.9%	16.9%			-20.1%	-40.8%	19.3%				-1.1	-1.3	.2	0.
														.2	.5	.2	0.
														5.7	3.8	1.9	0.
														10.3	14.7	11.4	27.
																	SIG
80.97	75.03	44.52	.500+00	.971-05	211.	67.	-4.	.593+00	.923-05	222.	125.	49.	-0.	.0	.0	0.	SP
370			-30.9%	-47.9%	16.8%			-31.6%	-44.0%	23.0%				-1.1	-1.5	0.	0.
														.5	1.0	0.	0.
														12.1	6.5	5.6	53.
														10.9	15.1	10.6	67.
																	SIG
77.30	70.04	55.87	.947+00	.157-04	206.	67.	-5.	.907+00	.149-04	205.	114.	-23.	3.	.9	1.3	0.	SP
410			-43.7%	-48.9%	7.5%			-46.1%	-51.3%	7.2%				-2.2	-1.9	0.	0.
														.8	1.7	0.	0.
														-4.1	-3.9	0.	0.
														11.3	15.8	9.4	18.
																	SIG
75.32	75.99	04.54	.131+01	.217-04	202.	63.	-6.	.113+01	.167-04	220.	123.	-10.	5.	1.3	1.9	0.	SP
440			-44.7%	-47.6%	1.4%			-52.3%	-59.7%	10.4%				-3.3	-1.1	0.	0.
														.9	2.2	0.	0.
														-13.4	-22.1	8.7	4.
														11.4	16.3	8.7	36.
																	SIG
74.00	75.64	72.92	.162+01	.206-04	203.	64.	0.	.166+01	.248-04	222.	82.	-15.	b.	1.6	2.3	0.	SP
470			-44.9%	-40.9%	-4%			-43.4%	-50.6%	8.6%				-4.4	-1.3	0.	0.
														1.1	2.9	0.	0.
														3.2	5.7	8.9	1.
														11.8	16.5	8.3	16.
																	RAND
																	SIG
71.26	72.69	95.73	.258+01	.413-04	214.	59.	1.	.249+01	.359-04	232.	64.	-4.	6.	2.1	2.7	0.	SP
570			-43.2%	-44.0%	-5%			-45.2%	-51.3%	8.0%				-7.7	-1.8	0.	0.
														1.4	3.1	0.	0.
																	MAG
																	SIG

REPRODUCIBILITY OF THE ORIGINAL PAGE IS POOR

70.04 030	70.03	105.13	.324+01 -40.9%	.512-04 -41.2%	221. .7%	57.	-11.	.322+01 -41.3%	.482-04 -44.7%	230. 4.7%	55.	-16.	b.	u.	2.9 -1.8 1.6 .5 12.6	3.7 -3.3 3.4 -3.5 16.4	-4 -1 .7 4.1 6.9	7. 21.	-6. 21.	RAND SIG
68.38 700	60.51	112.97	.445+01 -30.8%	.605-04 -30.9%	227. .3%	76.	-8.	.506+01 -28.2%	.703-04 -35.2%	247. 9.3%	55.	-3.	z.	u.	3.2 -1.8 2.0 15.7 11.3	4.0 -3.3 3.5 6.2 15.0	-4 -6 .8 9.6 6.7	4. 4. 4. 17. 18.	-4. -0. 1. 6. 18.	SP 0B0 MAG RAND SIG
66.28 750	03.83	117.07	.634+01 -33.6%	.047-04 -33.3%	233. -.4%	70.	-5.	.653+01 -31.4%	.933-04 -34.3%	238. 1.7%	37.	7.	z.	u.	2.9 -2.3 2.3 5.4 10.3	3.4 -3.8 3.8 2.3 13.9	-2 -9 .9 3.0 6.4	2. 5. 28. 21.	2. 5. 12. 21.	SP 0B0 MAG RAND SIG
63.47 810	60.55	120.76	.986+01 -30.3%	.142-03 -23.2%	242. -1.5%	65.	-2.	.102+02 -28.1%	.141-03 -29.9%	246. .2%	81.	24.	z.	u.	2.4 -2.2 2.6 5.5 9.2	2.5 -3.7 4.1 2.8 12.4	.1 -1.0 1.0 2.7 5.3	1. 6. 6. 22. 25.	1. 2. 25. 25.	SP 0B0 MAG RAND SIG
62.49 830	59.45	121.74	.114+02 -29.4%	.103-03 -27.8%	244. -2.1%	62.	-2.	.122+02 -24.5%	.173-03 -23.3%	239. -3.9%	77.	14.	-0.	u.	2.1 -2.0 2.7 9.2 8.9	2.1 -3.5 4.2 10.1 11.9	.1 -9 1.0 -9 4.8	6. 6. 21. 26.	6. 2. 14. 26.	SP 0B0 MAG RAND SIG
60.43 870	57.25	123.39	.154+02 -27.2%	.217-03 -25.1%	248. -2.7%	61.	-0.	.155+02 -26.8%	.212-03 -26.9%	250. -2.1%	88.	19.	-0.	u.	1.7 -1.5 2.8 2.1 8.3	1.5 -2.9 4.4 .5 10.9	.2 -9 1.0 1.6 3.6	2. 7. 34. 30.	2. 3. 17. 30.	SP 0B0 MAG RAND SIG
57.23 930	54.02	125.11	.246+02 -23.5%	.339-03 -21.0%	253. -3.2%	61.	0.	.265+02 -17.5%	.376-03 -12.3%	241. -7.6%	95.	25.	0.	u.	.9 -1.5 2.9 8.3 0.6	.8 -1.3 4.0 12.7 9.3	.1 -4 .8 -4.1 3.6	5. 6. 40. 41.	1. 2. 24. 41.	SP 0B0 MAG RAND SIG
54.17 1030	48.98	126.30	.309+02 -18.1%	.527-03 -14.9%	257. -3.8%	58.	2.	.412+02 -13.1%	.576-03 -6.9%	246. -7.8%	58.	-5.	1.	u.	.1 .3 2.6 5.5	.4 .0 3.1 9.4	-.3 -.3 .6 -3.9	3. 5. 3.	3. -6.	SP 0B0 MAG RAND

51.52	45.83	126.17	.561+02	.753-03	200.	56.	2.	.57P+02	.018-03	250.	03.	-24.	z.	u.	4.6	7.3	3.9	51.	51.	SIG
1100			-15.1% -11.4%	-3.9%				-12.5% -3.7%	-7.7%						-4	.1	-5			SP
															-1.4	.4	-3	-2.	-1.	0B0
															2.4	2.3	.4	4.	2.	MAG
															4.5	8.2	-3.8	10.	-25.	RAND
															4.3	6.8	4.0	44.	44.	SIG
47.80	42.11	124.96	.911+02	.121-02	203.	55.	2.	.943+02	.135-02	247.	74.	-26.	3.	1.	-2.8	-2.5	-3			SP
1200			-13.1% -10.4%	-2.9%				-10.1% -.3%	-8.6%						-1.1	.9	-4	-2.	-2.	0B0
															2.0	2.1	.5	3.	2.	MAG
															4.7	10.2	-5.5	21.	-26.	RAND
															3.7	6.2	4.0	36.	36.	SIG
45.84	40.66	124.04	.117+03	.155-02	263.	55.	2.	.123+03	.167-02	255.	91.	-22.	4.	1.	-3.8	-3.8	-0			SP
1250			-12.7% -11.5%	-1.3%				-8.2% -4.8%	-4.5%						.4	.4	-6	-2.	-1.	0B0
															1.9	2.1	.6	2.	2.	MAG
															4.8	7.5	-2.6	38.	-23.	RAND
															3.3	5.8	3.9	33.	33.	SIG
44.21	39.70	123.21	.144+03	.192-02	261.	60.	2.	.141+03	.195-02	249.	66.	-2.	z.	1.	-4.6	-4.9	.2			SP
1290			-12.6% -12.5%	-.2%				-14.4% -11.2%	-5.1%						.9	.0	-6	-2.	-1.	0B0
															1.8	2.0	.7	2.	2.	MAG
															2.8	1.5	-4.3	8.	-3.	RAND
															3.1	5.5	3.9	31.	31.	SIG
41.98	38.22	121.65	.196+03	.267-02	256.	52.	4.	.192+03	.267-02	248.	71.	-18.	2.	1.	-3.8	-4.1	.2			SP
1370			-11.1% -11.1%	-.1%				-13.0% -11.2%	-3.0%						.4	-2	-3	-3.	-2.	0B0
															1.7	1.5	.8	3.	2.	MAG
															-2.5	.2	-2.7	22.	-20.	RAND
															2.9	5.1	3.9	29.	29.	SIG
38.74	37.52	121.20	.304+03	.430-02	247.	41.	1.	.310+03	.439-02	246.	82.	12.	3.	1.	-3.7	-4.0	.2			SP
1410			-10.8% -10.7%	-.1%				-8.9% -8.7%	-.2%						-2	-5	.3	-5.	-2.	0B0
															1.6	1.1	.9	5.	2.	MAG
															2.3	2.7	-4	46.	13.	RAND
															2.8	4.5	3.8	26.	26.	SIG
37.34	37.03	121.02	.374+03	.538-02	242.	44.	-1.	.392+03	.563-02	242.	64.	10.	3.	1.	-2.9	-2.9	.0			SP
1440			-9.5% -9.1%	-.4%				-5.1% -5.0%	-.2%						-2	-0	.3	-5.	-2.	0B0
															1.3	1.0	.8	5.	2.	MAG
															5.0	5.2	-1	36.	12.	RAND
															3.0	4.4	3.8	24.	24.	SIG
35.26	36.58	120.97	.507+03	.752-02	235.	24.	-4.	.529+03	.777-02	237.	12.	3.	2.	u.	-1.7	-1.5	-.3			SP
1470			-8.4% -7.5%	-1.0%				-4.4% -4.4%	-.1%						-2	-6	.3	-6.	-2.	0B0
															1.1	.8	.8	6.	2.	MAG
															4.6	4.0	.6	-6.	9.	RAND
															3.2	4.1	3.7	22.	22.	SIG

33.58 1010	36.07 121.03	.654+03 -7.2%	.065-02 -6.8%	231. -0.0%	14. -6.651+03 -7.6%	.996-02 -5.7%	227. -2.3%	5. -22.	z. 0.	-.8 -1.1 -.9 -3.3 3.6	-0.3 -0.4 0.0 1.5 4.1	-0.6 -0.2 0.7 -1.9 3.6	-5. -2. 6. -3. 21.	SP GRO MAG RAND SIG
31.08 1040	35.75 121.99	.926+03 -0.2%	.147-01 -5.8%	226. -0.6%	2. -10. 0.980+03 -3.0%	.147-01 -5.8%	232. 1.9%	b. -15.	z. -0.	.5 -0.0 -0.7 2.5 4.2	1.4 -0.1 0.4 0.1 4.2	-1.0 0.0 0.5 2.4 3.5	-4. -1. 5. 10. 19.	SP GRO MAG RAND SIG
29.02 1060	35.57 121.92	.131+04 -5.6%	.204-01 -4.6%	225. -1.3%	-2. -10. 0.127+04 -8.4%	.195-01 -8.7%	226. 0.1%	8. -9.	z. -0.	.0 -0.1 0.4 -2.9 4.5	0.0 0.0 0.4 1.5 4.0	0.0 -1.1 0.4 1.5 3.4	-2. 4. 12. 16.	SP GRO MAG RAND SIG
27.39 1080	35.42 121.83	.108+04 -5.2%	.205-01 -3.8%	220. -1.6%	-1. -8. 0.160+04 -9.0%	.251-01 -8.9%	221. -1.1%	2. 1.	1. -0.	.0 -0.2 0.5 -4.6 4.5	0.0 -0.0 0.4 0.7 3.8	0.0 -0.3 0.4 -0.0 3.3	-1. 3. 10. 13. 16.	SP GRO MAG RAND SIG
26.13 1000	35.30 121.73	.204+04 -5.1%	.125-01 -3.2%	218. -1.9%	-0. -6. 0.202+04 -5.7%	.307-01 -8.7%	229. 2.7%	-2. -3.	1. -0.	.0 -0.2 0.5 -5.5 4.6	0.0 -0.1 0.4 5.1 3.0	0.0 -0.3 0.4 5.1 3.2	-1. 2. 4. 11.	SP GRO MAG RAND SIG
23.69 1040	35.08 121.58	.298+04 -4.4%	.403-01 -2.0%	215. -2.4%	2. -4. 0.304+04 -2.6%	.470-01 -4.0%	224. 1.9%	7. -0.	-0. -0.	.0 -0.3 0.4 2.1 1.4	0.0 -0.3 0.3 4.7 1.4	0.0 -0.0 1.0 5.0 11.0	-0. 0. 10. 11.	SP GRO MAG RAND SIG
21.30 1070	34.95 121.52	.437+04 -3.2%	.717-01 -0.7%	212. -2.5%	4. -4. 0.444+04 -1.7%	.716-01 -0.8%	216. -1.1%	-11. -1.	-1. -0.	.0 -0.2 0.3 1.7 1.2	0.0 -0.1 0.3 0.0 1.4	0.0 -0.3 0.3 1.8 1.4	-0. 0. 0. 3. 13.	SP GRO MAG RAND SIG
19.71 1090	34.88 121.47	.506+04 -2.1%	.025-01 0.5%	211. -2.6%	10. -3. 0.570+04 -1.5%	.939-01 0.9%	211. -2.5%	19. -2.	-0. -0.	.0 -0.2 0.3 0.8 1.2	0.0 -0.2 0.3 0.3 1.0	0.0 -0.0 1.0 27. 16.	SP GRO MAG RAND SIG	

17.56 1708	34.83	120.44	.803+04 -.9%	.134+00 2.5%	209. -3.4%	14.	-4.	.806+04 -.6%	.134+00 3.0%	209. -3.6%	-6.	24.	-3.	0.	.0 -.2 .2 .5 1.6	.0 -.1 .2 -.0 1.9	.0 -.2 0. -20. 1.9	21. 21. 28. 21. 21.	SP GBO MAG RAND SIG
15.67 1722	34.79	120.41	.110+05 .7%	.182+00 4.0%	210. -3.1%	22.	-4.	.112+05 2.7%	.185+00 5.5%	211. -2.6%	1.	66.	-2.	-0.	.0 -.1 .1 1.0 2.6	.0 -.1 .2 .5 2.4	.0 0. 0. -21. 2.0	27. 27. 69. 27. 27.	SP GBO MAG RAND SIG
13.59 1736	34.76	120.39	.154+05 1.7%	.252+00 3.8%	212. -2.0%	25.	-4.	.153+05 1.1%	.251+00 3.1%	213. -1.8%	-19.	61.	-0.	-0.	.0 .0 .0 -.4 2.8	.0 .0 .0 -.2 2.4	.0 0. 0. -44. 2.0	29. 29. 64. 29. 29.	SP GBO MAG RAND SIG
11.32 1752	34.73	120.38	.221+05 2.4%	.754+00 2.0%	218. .4%	22.	-2.	.218+05 1.1%	.350+00 1.0%	217. .2%	-37.	72.	2.	-0.	.0 .0 .0 -1.3 2.5	.0 .0 .0 -2 2.1	.0 0. 0. -59. 1.9	30. 30. 74. 30. 30.	SP GBO MAG RAND SIG
9.52 1768	34.70	120.36	.291+05 2.2%	.446+00 1.8%	227. .4%	20.	-3.	.291+05 2.2%	.446+00 1.8%	227. .4%	-53.	28.	2.	0.	.0 .0 .0 -0.0 2.1	.0 .0 .0 -0 1.8	.0 0. 0. -72. 1.8	29. 29. 50. 29. 29.	SP GBO MAG RAND SIG
8.46 1780	34.68	120.35	.340+05 2.0%	.505+00 1.4%	235. .6%	18.	-3.	.344+05 3.1%	.512+00 2.8%	234. .5%	-50.	30.	3.	-0.	.0 .0 .0 1.3 1.9	.0 .0 .0 -0 1.8	.0 0. 0. -68. 1.8	25. 25. 33. 25. 25.	SP GBO MAG RAND SIG
7.54 1796	34.65	120.35	.388+05 1.9%	.560+00 1.0%	241. .9%	16.	-2.	.394+05 3.5%	.562+00 1.3%	244. 2.2%	-44.	20.	3.	-0.	.0 .0 .0 1.6 1.7	.0 .0 .0 1.3 1.7	.0 0. 0. -61. 1.7	22. 22. 22. 22. 22.	SP GBO MAG RAND SIG
7.07 1806	34.63	120.35	.415+05 1.9%	.590+00 .7%	245. 1.1%	15.	-2.	.426+05 4.6%	.594+00 1.5%	250. 3.1%	-42.	4.	3.	-0.	.0 .0 .0 2.7 1.6	.0 .0 .0 2.0 1.7	.0 0. 0. -57. 1.7	21. 21. 6. 21. 21.	SP GBO MAG RAND SIG
5.11	34.61	120.43	.540+05	.727+00	259.	10.	-1.	.557+05	.733+00	265.	-12.	5.	3.	-0.					

1050	1.5v	-0.1%	1.6%	4.6%	.7%	4.0%	.0	.0	.0	0.	SP		
3.53	34.64	120.47	.692+05	.857+00	269.	6.	-1.	.669+05	.872+00	267.	0.	3.	-1.
1882	1.0%	-0.5%	1.5%	2.1%	1.3%	0.7%	.0	.0	.0	.0	0.	0.	0.
							0.	0.	0.	0.	0.	0.	0.
							3.1	.8	2.3	-22.	7.	RAND	
							1.2	1.7	1.7	15.	15.	SIG	
							.0	.0	.0	.0	0.	0.	0.
							.0	.0	.0	.0	0.	0.	0.
							1.0	1.8	-0.7	-16.	2.	RAND	
							.9	1.7	1.7	12.	12.	SIG	

REPRODUCIBILITY OF THE ORIGINAL PAGE IS POOR

SAMPLE PROFILE PROGRAM OUTPUT
VERTICAL PROFILE FOR JANUARY AT CAPE KENNEDY

INITIAL HEIGHT = 92.00 KM INITIAL LAT = 28.45 DEG INITIAL WEST LON = 80.53 DEG
 F10.7 = .00 MEAN F10.7 = .00 AP = .00
 DATE = 1/ 1/73 GREENWICH TIME = 0: 0: 0 HEIGHT INCREMENT = 2.00 KM
 LAT INCREMENT = .00 DEG WEST LON INCREMENT = .00 DEG
 MAXIMUM NUMBER OF POSITIONS = 46 PUNCH OPTION = 0
 TRAJECTORY OPTION = 0
 GROVES INPUT UNIT = 3 RANDOM INPUT UNIT = 3 G90 INPUT UNIT = 3
 4-D INPUT UNIT = 4 RANDOM OPTION = 1 G90 OPTION = 1
 FIRST RANDOM NUMBER = 8941
 NMC READ OPTION = 0 4-D P,D,T DATA SCRATCH UNIT = 12
 NMC GRID POINTS SCRATCH UNIT = 13 JULIAN DATE = 2441684.0
 INITIAL P,D,T = -12.70 % -7.20 % -5.60 % SIGMA P,D,T = 10.21 % 10.43 % 9.91 %
 INITIAL U,V = -18.00 M/S -16.00 M/S -19.96 M/S SIGMA U,V = 19.96 M/S 19.96 M/S

** PERCENT DEVIATIONS FROM 1962 US STANDARD ATMOSPHERE APPEAR BELOW PRESSURE, DENSITY, AND TEMPERATURE VALUES **

HEIGHT (KM)	LAT (DEG)	WEST LON (DEG)	UNPERTURBED (MONTHLY MEAN)						MEAN PLUS PERTURBATIONS						THERMAL WIND SHEAR (M/S/KM)						PERTURBATION VALUES					
			PRES. (M**2)	DENS. (KG/M**3)	TEMP (DEG KEL- VIN)	GEOSTROPH. WIND (M/S)	PRES. (NT/ M**2)	DENS. (KG/ M**3)	TEMP (DEG KEL- VIN)	TOTAL WIND (M/S)	E-W	N-S	E-W	N-S	E-W	N-S	P	D	T	U	V					
90.00 0	28.45	80.53	184+00 12.2%	.341-05 7.4%	189. 4.4%	11. 0.	0. .180+00	.335-05 5.8%	187. 3.3%	5. -2.	-2. 0.	0. 0.	0. 0.	0. 0.	0. 0.	0. 0.	0. 0.	0. 0.	0. 0.	SP GRO MAG						
88.00 0	28.45	80.53	264+00 13.3%	.494-05 7.8%	190. 5.0%	6. 11.	.257+00 8.1%	.449-05 -2.0%	198. 9.9%	-6. 11.	-2. -0.	0. 0.	0. 0.	0. 0.	0. 0.	0. 0.	0. 0.	0. 0.	0. 0.	SP GRO MAG						
86.00 0	28.45	80.53	382+00 11.4%	.695-05 5.1%	191. 5.9%	4. 12.	.397+00 15.8%	.743-05 12.3%	186. 3.0%	-1. 17.	-1. -1.	0. 0.	0. 0.	0. 0.	0. 0.	0. 0.	0. 0.	0. 0.	0. 0.	SP GRO MAG						
84.00 0	28.45	80.53	540+00 8.4%	.975-05 1.9%	193. 6.7%	8. 14.	.547+00 10.4%	.974-05 1.8%	196. 8.6%	3. 16.	-1. -1.	0. 0.	0. 0.	0. 0.	0. 0.	0. 0.	0. 0.	0. 0.	0. 0.	SP GRO MAG						
82.00 0	28.45	80.53	758+00 5.8%	.136-04 -1.6%	194. 7.5%	13. 15.	.802+00 11.9%	.145-04 5.1%	193. 6.8%	7. 15.	-1. -1.	0. 0.	0. 0.	0. 0.	0. 0.	0. 0.	0. 0.	0. 0.	0. 0.	SP GRO MAG						

80.00	28.45	80.53	.107+01	.190-04	196.	13.	16.	.112+01	.195-04	201.	12.	13.	-1.	-1.	-0	-2	2.	-0.	GR0
0			2.8%	-5.0%	8.3%			7.9%	-2.6%	11.4%					.6	.2	3.	1.	MAG
															6.4	6.8	-8.	0.	RAND
															6.7	8.3	8.8	17.	SIG
78.00	28.45	80.53	.149+01	.263-04	198.	14.	17.	.151+01	.262-04	201.	31.	6.	-1.	-1.	4.0	4.9	-1.0		SP
0			.5%	-4.3%	5.0%			1.2%	-4.6%	6.7%					-7	-1	-3	3.	GR0
															.8	3	3.	1.	MAG
															5.8	2.6	3.2	-3.	RAND
															6.8	8.4	8.4	13.	SIG
76.00	28.45	80.53	.210+01	.365-04	200.	13.	18.	.204+01	.353-04	203.	-2.	27.	-1.	-1.	4.3	5.2	-1.1		SP
0			-.4%	-2.4%	2.0%			-2.9%	-5.6%	3.4%					-1.0	-1	-3	3.	GR0
															1.0	.4	3	4.	MAG
															1.7	-2	2.0	14.	RAND
															6.3	8.3	7.9	16.	SIG
74.00	28.45	80.53	.291+01	.497-04	204.	21.	19.	.279+01	.479-04	204.	-8.	37.	-2.	-0.	4.6	5.6	-1.1		SP
0			-.9%	-1.0%	-.0%			-5.0%	-4.4%	.1%					-1.2	-1	-3	3.	GR0
															1.3	.5	4	5.	MAG
															-1.4	-3.2	1.8	-18.	RAND
															5.8	8.3	7.4	20.	SIG
72.00	28.45	80.53	.400+01	.667-04	209.	30.	21.	.402+01	.658-04	215.	7.	39.	-2.	-0.	4.7	5.6	-9		SP
0			-1.1%	.1%	-1.3%			-.8%	-1.1%	1.3%					-1.4	-1	-4	4.	GR0
															1.6	.6	4	5.	MAG
															-2.8	-3.4	.5	-32.	RAND
															5.7	8.2	6.8	21.	SIG
70.00	28.45	80.53	.551+01	.896-04	214.	32.	22.	.551+01	.904-04	215.	14.	23.	-3.	-0.	4.9	5.6	-7		SP
0			-.3%	2.3%	-2.5%			-.2%	3.3%	-2.3%					-1.5	-1	-4	4.	GR0
															1.9	.8	5	6.	MAG
															1.9	-1.2	3.1	-27.	RAND
															5.9	8.3	6.2	20.	SIG
68.00	28.45	80.53	.746+01	.117-03	222.	39.	24.	.732+01	.115-03	224.	11.	10.	-2.	0.	5.1	5.6	-5		SP
0			.2%	2.7%	-2.4%			-1.7%	.8%	-1.6%					-1.6	-1	-5	4.	GR0
															2.2	.9	6	6.	MAG
															1.7	1.0	.7	-22.	RAND
															6.1	8.3	5.6	19.	SIG
66.00	28.45	80.53	.101+02	.153-03	230.	40.	24.	.988+01	.154-03	226.	10.	0.	-1.	0.	5.3	5.7	-3		SP
0			1.2%	3.9%	-2.4%			-.6%	4.4%	-4.1%					-1.5	-1	-5	4.	GR0
															2.2	1.0	.7	7.	MAG
															-4	-1.7	1.4	-32.	RAND
															6.0	8.2	5.1	20.	SIG
															5.2	5.5	-2	5.	GR0
															-1.3	-1	-6		SP

64.00	28.45	80.53	.134+02	.197-03	237.	43.	23.	.143+02	.215-03	233.	3.	14.	-0.	0.	5.2	5.4	-1.1	0	4.	SP
0			1.8%	4.6%	-2.5%			8.7%	14.1%	-4.2%					-1.1	0	-0.6	4.	4.	GR0
															2.3	1.4	0.8	7.	5.	MAG
															7.9	9.0	-1.1	-45.	-7.	RAND
															5.7	8.0	4.1	25.	25.	SIG
62.00	28.45	80.53	.176+02	.251-03	244.	47.	23.	.176+02	.253-03	243.	14.	22.	0.	0.	5.1	5.3	0	0	0.	SP
0			1.9%	5.0%	-2.7%			1.8%	5.8%	-3.2%					-2.7	0.2	-0.6	4.	4.	GR0
															2.2	1.6	0.9	8.	5.	MAG
															0.6	0.5	0.1	-37.	-0.	RAND
															5.4	7.9	3.9	29.	29.	SIG
60.00	28.45	80.53	.230+02	.320-03	251.	47.	23.	.234+02	.327-03	251.	17.	38.	1.	0.	5.1	5.1	0.1	0	0.	SP
0			2.6%	4.7%	-1.7%			4.4%	6.9%	-1.8%					-0.4	0.4	-0.6	3.	3.	GR0
															2.2	1.8	1.0	8.	6.	MAG
															2.1	1.6	0.5	-33.	14.	RAND
															5.1	7.7	3.7	33.	33.	SIG
58.00	28.45	80.53	.300+02	.407-03	257.	42.	23.	.311+02	.421-03	259.	59.	46.	1.	0.	5.0	5.0	0.2	0	0.	SP
0			2.9%	4.3%	-1.1%			6.9%	7.6%	-3%					-2	0.3	-0.5	3.	1.	GR0
															1.7	1.3	0.8	8.	4.	MAG
															4.2	2.9	1.3	13.	22.	RAND
															4.9	7.5	3.8	31.	31.	SIG
56.00	28.45	80.53	.390+02	.518-03	262.	37.	22.	.385+02	.515-03	261.	60.	18.	2.	1.	5.0	4.9	0.2	0	0.	SP
0			3.6%	4.1%	-0.5%			2.3%	3.5%	-1.1%					-1.1	0.2	-0.4	3.	0.	GR0
															1.3	0.8	0.7	7.	2.	MAG
															-1.1	-0.9	-0.2	20.	-4.	RAND
															4.6	7.2	3.8	30.	30.	SIG
54.00	28.45	80.53	.503+02	.657-03	267.	35.	21.	.479+02	.599-03	276.	82.	23.	2.	1.	5.0	4.8	0.2	0	0.	SP
0			3.7%	4.1%	-0.3%			-1.2%	-5.1%	5.1%					-0	-0.4	-0.3	4.	0.	GR0
															1.0	0.6	0.5	6.	1.	MAG
															-4.7	-8.5	3.8	43.	1.	RAND
															4.3	6.9	3.8	29.	29.	SIG
52.00	28.45	80.53	.643+02	.832-03	270.	34.	20.	.658+02	.820-03	278.	51.	7.	1.	1.	5.0	4.7	0.2	0	0.	SP
0			3.4%	3.9%	-0.3%			5.7%	2.4%	2.8%					0.1	-0.2	-0.2	5.	-0.	GR0
															0.8	0.6	0.5	6.	1.	MAG
															2.1	-1.2	3.3	12.	-13.	RAND
															4.1	6.6	3.9	30.	30.	SIG
50.00	28.45	80.53	.816+02	.104-02	273.	35.	19.	.822+02	.102-02	283.	50.	8.	1.	1.	4.1	3.7	0.4	0	0.	SP
0			2.3%	1.6%	1.0%			3.0%	-1.1%	4.6%					0.2	0.5	-0.2	6.	-0.	GR0
															0.6	0.5	0.4	6.	1.	MAG

REPRODUCIBILITY OF THE ORIGINAL PAGE IS POOR

46.00	28.45	80.53	.104+03	.133-02	272.	37.	18.	.104+03	.133-02	277.	41.	5.	0.	1.	3.3	2.7	.5	5	SP
0			1.8%	1.2%	.5%			1.8%	.9%	2.2%					-7	.7	-2	2.	-1. GBO
															.7	.8	.5	4.	1. MAG
															.7	-1.1	1.8	2.	-11. RAND
															3.5	5.9	3.9	30.	30. SIG
46.00	28.45	80.53	.133+03	.170-02	271.	37.	16.	.141+03	.175-02	282.	16.	19.	-0.	0.	2.4	1.7	.7	7	SP
0			1.1%	-.7%	1.4%			7.3%	1.9%	5.5%					.2	.8	-1	0.	-1. GBO
															.7	1.0	.6	3.	1. MAG
															5.9	1.8	4.1	-21.	4. RAND
															3.2	5.6	3.8	28.	28. SIG
44.00	28.45	80.53	.169+03	.219-02	268.	39.	15.	.174+03	.222-02	270.	7.	26.	-0.	0.	1.6	.7	.8	8	SP
0			-.1%	-2.9%	2.5%			2.5%	-1.5%	3.2%					.7	.6	-.4	-1.	-0. GBO
															.8	1.0	.6	2.	1. MAG
															1.8	.8	1.1	-32.	11. RAND
															3.0	5.2	3.8	27.	27. SIG
42.00	28.45	80.53	.219+03	.290-02	263.	36.	15.	.226+03	.294-02	266.	48.	38.	0.	0.	2.1	1.4	.7	7	SP
0			-.2%	-3.1%	2.8%			2.9%	-1.8%	3.9%					.6	.3	-.4	-3.	-1. GBO
															.9	.9	.5	4.	1. MAG
															2.5	1.0	1.5	14.	23. RAND
															2.8	4.9	3.8	27.	27. SIG
40.00	28.45	80.53	.281+03	.379-02	258.	36.	14.	.289+03	.396-02	253.	44.	19.	0.	0.	1.6	.7	.8	8	SP
0			-2.1%	-5.3%	3.2%			.4%	-1.0%	1.0%					.4	.1	.2	-5.	-1. GBO
															1.0	.7	.4	5.	2. MAG
															2.1	4.5	-2.4	13.	7. RAND
															2.6	4.5	3.8	27.	27. SIG
38.00	28.45	80.53	.368+03	.510-02	251.	33.	12.	.375+03	.514-02	254.	48.	19.	1.	0.	1.0	.3	.6	6	SP
0			-2.5%	-5.0%	2.5%			-.6%	-4.3%	3.7%					.3	-1.1	.3	-6.	-2. GBO
															.8	.6	.4	6.	2. MAG
															1.8	.9	.9	21.	9. RAND
															2.8	4.3	3.7	25.	25. SIG
36.00	28.45	80.53	.480+03	.687-02	243.	29.	9.	.492+03	.720-02	237.	43.	19.	2.	0.	.4	-.2	.5	5	SP
0			-3.6%	-5.3%	1.7%			-1.3%	-.8%	-.7%					.1	-.3	.3	-7.	-2. GBO
															.7	.5	.5	7.	2. MAG
															2.3	5.1	-2.8	21.	11. RAND
															3.0	4.1	3.7	23.	23. SIG
34.00	28.45	80.53	.632+03	.927-02	238.	25.	7.	.653+03	.976-02	233.	25.	6.	2.	1.	-.2	-.6	.3	3	SP
0			-4.8%	-6.3%	1.6%			-1.6%	-1.3%	-.3%					.1	-.2	.3	-7.	-1. GBO
															.6	.4	.5	7.	1. MAG
															3.2	5.5	-2.3	6.	0. RAND

32.00	28.45	80.53	.837+03	.125-01	233.	21.	5.	.869+03	.132-01	230.	23.	-4.	2.	1.	3.4	4.0	3.6	21.	21.	SIG
0			-5.9%	-7.7%	2.1%			-2.3%	-2.8%	.5%						-1.0	.1			SP
																-.0	.2	-5.	-1.	GRO
																.5	.4	6.	1.	MAG
																3.7	5.4	-1.7	7.	RAND
																3.9	4.0	3.5	19.	SIG
30.00	28.45	80.53	.111+04	.169-01	229.	18.	2.	.117+04	.181-01	226.	25.	-9.	1.	1.	-1.4	-1.4	-0.			SP
0			-7.5%	-8.3%	1.1%			-2.0%	-1.5%	-.4%					.1	.1	.1	-4.	-1.	GRO
															.4	.3	.3	5.	1.	MAG
															5.7	7.3	-1.6	11.	-11.	RAND
															4.4	4.1	3.4	17.	17.	SIG
26.00	28.45	80.53	.152+04	.235-01	225.	16.	1.	.162+04	.248-01	228.	30.	-8.	1.	0.	.0	.0	.0			SP
0			-6.2%	-6.2%	.1%			.2%	-1.2%	1.6%					-.0	.0	-.2	-2.	-0.	GRO
															.4	.4	.3	4.	0.	MAG
															6.9	5.2	1.6	16.	-9.	RAND
															4.4	3.8	3.3	14.	14.	SIG
26.00	28.45	80.53	.207+04	.328-01	220.	14.	1.	.205+04	.330-01	216.	14.	1.	1.	0.	.0	.0	.0			SP
0			-5.2%	-4.3%	-.9%			-6.5%	-3.6%	-3.1%					-.2	-.1	-.2	-1.	-0.	GRO
															.4	.5	.2	2.	0.	MAG
															-1.2	.8	-1.9	2.	0.	RAND
															4.5	3.4	3.1	10.	10.	SIG
24.00	28.45	80.53	.284+04	.457-01	216.	11.	0.	.280+04	.458-01	213.	17.	-5.	1.	0.	.0	.0	.0			SP
0			-4.6%	-2.6%	-1.9%			-5.8%	-2.3%	-3.5%					-.3	-.2	-.2	-0.	-0.	GRO
															.4	.5	.2	2.	0.	MAG
															-1.0	.4	-1.5	6.	-6.	RAND
															.7	.9	.8	9.	9.	SIG
22.00	28.45	80.53	.391+04	.643-01	212.	8.	0.	.390+04	.646-01	210.	27.	5.	-0.	-0.	.0	.0	.0			SP
0			-3.5%	-3.3%	-3.2%			-3.6%	.2%	-3.8%					-.3	-.2	-.1	-0.	-0.	GRO
															.4	.5	.2	1.	0.	MAG
															.1	.7	-.6	20.	5.	RAND
															.6	.9	.9	12.	12.	SIG
20.00	28.45	80.53	.545+04	.914-01	207.	16.	3.	.548+04	.924-01	207.	34.	9.	-2.	-0.	.0	.0	.0			SP
0			-1.5%	2.8%	-4.2%			-.8%	3.9%	-4.6%					-.3	-.3	.0	0.	0.	GRO
															.3	.4	.2	1.	0.	MAG
															.9	1.3	-.4	18.	6.	RAND
															.7	1.0	1.0	15.	15.	SIG
18.00	28.45	80.53	.759+04	.129+00	205.	19.	4.	.766+04	.130+00	205.	8.	11.	-3.	-0.	.0	.0	.0			SP
0			.3%	6.0%	-5.4%			1.2%	6.9%	-5.5%					-.2	-.2	-.2	0.	0.	GRO
															.2	.3	.2	1.	0.	MAG
															1.1	1.1	1.0	-11.	7.	RAND
															1.0	1.1	1.1	21.	21.	SIG

16.00	28.45	80.53	.107+05	.183+00	204.	30.	3.	.106+05	.183+00	203.	21.	-22.	-4.	-0.	.0	.0	.0	.0	.0	SP
0			3.5%	9.4%	-5.8%			2.7%	9.8%	-6.5%					-0.1	-0.1	0	0	0	GRO
															-1	.2	1	1	0	MAG
															-0.6	.2	-7	-9	-25	RAND
															1.7	1.4	1.2	28.	28.	SIG
14.00	26.45	80.53	.149+05	.246+00	210.	37.	4.	.150+05	.246+00	212.	50.	-6.	-1.	-0.	.0	.0	.0	.0	.0	SP
0			5.0%	8.1%	-2.9%			5.5%	7.9%	-2.2%					0	0	0	0	0	GRO
															0	0	0	0	0	MAG
															.5	-2	7	13	-11	RAND
															1.8	1.5	1.2	32.	32.	SIG
12.00	28.45	80.53	.205+05	.328+00	217.	35.	3.	.202+05	.323+00	218.	56.	4.	2.	0.	.0	.0	.0	.0	.0	SP
0			5.5%	5.2%	.3%			4.2%	3.4%	.7%					0	0	0	0	0	GRO
															0	0	0	0	0	MAG
															-1.2	-1.7	.5	21.	1.	RAND
															1.7	1.4	1.2	32.	32.	SIG
10.00	28.45	80.53	.278+05	.421+00	230.	32.	3.	.273+05	.412+00	231.	25.	28.	4.	0.	.0	.0	.0	.0	.0	SP
0			4.8%	1.8%	3.0%			3.2%	-.3%	3.4%					0	0	0	0	0	GRO
															0	0	0	0	0	MAG
															-1.6	-2.0	.4	-7.	25.	RAND
															1.4	1.2	1.2	33.	33.	SIG
8.00	28.45	80.53	.370+05	.529+00	244.	26.	3.	.373+05	.519+00	250.	20.	8.	4.	0.	.0	.0	.0	.0	.0	SP
0			3.9%	.6%	3.3%			4.6%	-1.4%	6.0%					0	0	0	0	0	GRO
															0	0	0	0	0	MAG
															.7	-1.9	2.6	-6.	5.	RAND
															1.2	1.1	1.1	26.	26.	SIG
6.00	28.45	80.53	.486+05	.654+00	259.	20.	3.	.495+05	.651+00	265.	27.	19.	4.	0.	.0	.0	.0	.0	.0	SP
0			2.9%	-.9%	3.8%			4.9%	-1.4%	6.3%					0	0	0	0	0	GRO
															0	0	0	0	0	MAG
															1.9	-5	2.4	7.	16.	RAND
															1.0	1.0	1.0	19.	19.	SIG
4.00	28.45	80.53	.628+05	.808+00	271.	12.	3.	.636+05	.814+00	272.	-4.	5.	4.	0.	.0	.0	.0	.0	.0	SP
0			1.9%	-1.4%	3.3%			3.2%	-.6%	3.9%					0	0	0	0	0	GRO
															0	0	0	0	0	MAG
															1.3	.7	.5	-16.	2.	RAND
															.7	.9	.9	13.	13.	SIG
2.00	28.45	80.53	.804+05	.996+00	281.	6.	2.	.805+05	.101+01	279.	-12.	17.	3.	1.	.0	.0	.0	.0	.0	SP
0			1.1%	-1.1%	2.2%			1.3%	-.1%	1.4%					0	0	0	0	0	GRO
															0	0	0	0	0	MAG
															.2	.9	-7	-18.	15.	RAND
															.6	1.1	1.1	10.	10.	SIG

APPENDIX C - PROFILE PROGRAM LISTING

Following is a listing of the PROFILE program. The subroutines are in order alphabetically. Numbers on the left hand side of the listing are relative addresses and consecutive record numbers. Sequence numbers containing a three character subroutine code and a five digit number appear on the right of the printout. Information on the storage requirements, and a listing of the identifiers used appear at the beginning of each subroutine.

REPRODUCIBILITY OF THE ORIGINAL PAGE IS POOR

GH06,P ***** CORR *****
 @FOR,S PROFAS,CORR,CORR
 FOR S11E-02/04/74--18:52:00 (0,)

FUNCTION CORR ENTRY POINT 000122

STORAGE USED: CODE(1) 000126; DATA(0) 000027; BLANK COMMON(2) 000000

EXTERNAL REFERENCES (BLOCK, NAME)

0003 NERR35

STORAGE ASSIGNMENT (BLOCK, TYPE, RELATIVE LOCATION, NAME)

0001	000037	10L	0001	000110	100L	0001	000046	17L	0001	000055	24L	0001	000066	36L
0001	000076	62L	0001	000103	90L	0000	R	000000	CORR	0000	000022	INP\$		

00101	1*	FUNCTION CORR(H)												
00101	2*	C.....LINEAR APPROXIMATIONS TO CORRELATION BETWEEN DENSITY AND												COR00100
00101	3*	TEMPERATURE FROM NASA-TM X-64589, USED IF CORRELATION COMPUTED												COR00200
00101	4*	FROM P,D,T AND T SIGMAS HAS ABSOLUTE VALUE GT 1.												COR00300
00103	5*	IF (H,LT,10.) GO TO 10												COR00400
00107	6*	IF (H,LT,17.) GO TO 17												COR00500
00107	7*	IF (H,LT,24.) GO TO 24												COR00600
00111	8*	IF (H,LT,38.) GO TO 38												COR00700
00113	9*	IF (H,LT,62.) GO TO 62												COR00800
00115	10*	IF (H,LT,90.) GO TO 90												COR00900
00117	11*	GO TO 100												COR01000
00117	12*	C.....-0.95 AT SURFACE TO -0.46 AT 10 KM												COR01100
00120	13*	10 CORR = -0.95+0.049*H												COR01200
00121	14*	RETURN												COR01300
00121	15*	C.....-0.46 AT 10 KM TO -0.81 AT 17 KM												COR01400
00122	16*	17 CORR = -0.46-0.05*(H-10.)												COR01500
00123	17*	RETURN												COR01600
00123	18*	C.....-0.81 AT 17 KM TO -0.02 AT 24 KM												COR01700
00124	19*	24 CORR = -0.81 + 0.1129*(H-17.)												COR01800
														COR01900

```

***** CORR *****
00125 20* RETURN
00126 21* C.....-0.02 AT 24 KM TO -0.82 AT 38 KM
00127 22* 38 CORR = -0.02 -0.0571*(H-24.)
00128 23* RETURN
00129 24* C.....-0.82 BETWEEN 38 AND 62 KM
00130 25* 62 CORR = -0.82
00131 26* RETURN
00132 27* C.....-0.70 BETWEEN 62 AND 90 KM
00133 28* 90 CORR = -0.7
00134 29* RETURN
00135 30* C.....-0.75 ABOVE 90 KM
00136 31* 100 CORR = -0.75
00137 32* RETURN
00138 33* END

```

END OF COMPILATION: NO DIAGNOSTICS.

```

@HDG,P ***** DXHLVL *****
@FOR,S PROFAS,DXHLVL,DXHLVL
FOR S11E-02/04/74-18:52:02 (0,)

```

SUBROUTINE DXHLVL ENTRY POINT 000052

STORAGE USED: CODE(1) 000056; DATA(0) 000021; BLANK COMMON(2) 000000

COMMON BLOCKS:

0003 IOTEMP 000050

EXTERNAL REFERENCES (BLOCK, NAME)

```

0004 COS
0005 SORT
0006 NERR3$

```

STORAGE ASSIGNMENT (BLOCK, TYPE, RELATIVE LOCATION, NAME)

```

0000 R 000000 AH 0003 000040 AP 0000 R 000002 AV 0000 R 000001 BH 0000 R 000003 BV
0003 R 000033 CH 0003 R 000034 CLAT 0003 R 000035 CLON 0003 000004 DX 0003 R 000004 DD
0003 000047 DZ 0003 000036 F10 0003 000037 F10B 0003 000031 G 0003 R 000045 HL
0003 000024 IDA 0003 000041 IHR 0000 000010 IOTEM1 0003 000001 IOTEM2
0003 000002 IUG 0003 000025 IYR 0003 000042 MIN 0003 000023 MN 0003 000003 NMCOP
0003 000045 NMORE 0003 000010 NSAME 0003 000026 PH 0003 000007 PHI 0003 000006 PHI1
0003 R 000027 PLAT 0003 R 000030 PLON 0003 R 000032 R 0003 000012 RDI 0003 000011 RPI
0003 000013 RT1 0003 000017 RU1 0003 000020 RV1 0003 000015 SD1 0003 000014 SPI
0003 000016 ST1 0003 000021 SU1 0003 000022 SV1 0003 R 000046 VL 0003 000005 XMJD

```

```

00101 1* SUBROUTINE DXHLVL DXH00100
00102 2* COMMON/IOTEMP/IOTEM1,IOTEM2,IUG,NMCOP,DD,XMJD,PHI1,PHI,NSAME, DXH00200
00103 3* $ RPI,RDI,RT1,SPI,SD1,ST1,RT1,RVI,SU1,SV1,MN,IDA,IYR,PH,PLAT, DXH00300

```


***** DXHLVL *****

```

00103 4* * PLON,G,R,CH,CLAT,CLON,F10,F10B,AP,IHR,MIN,NMORE,DX,HL,VL,DZ DXH00400
00104 5* DX = R*SQRT((CLAT-PLAT)**2 + (CLON-PLON)**2) DXH00500
00104 6* C.....DX IS HORIZONTAL DISTANCE BETWEEN POSITIONS PLAT,PLON AND CLAT,CLODXH00600
00105 7* AH = 900. DXH00700
00106 8* SH = 6. DXH00800
00107 9* AV=5. DXH00900
00110 10* SV=0.05 DXH01000
00111 11* HL = AH + BH*CH @ HORIZONTAL WAVELENGTH, KM DXH01100
00112 12* VL = AV + BV*CH @ VERTICAL WAVELENGTH, KM DXH01200
00113 13* RETURN DXH01300
00114 14* END DXH01400

```

END OF COMPILATION: NO DIAGNOSTICS.

```

@HDG,P ***** FAIR *****
@FOR,S PROFAS,FAIR,FAIR
FOR S1E-02/04/74-18:52:04 (0.)

```

SUBROUTINE FAIR ENTRY POINT 000110

STORAGE USED: CODE(1) 000160; DATA(0) 000040; BLANK COMMON(2) 000000

EXTERNAL REFERENCES (BLOCK, NAME)

```

0003 ALOG
0004 EXP
0005 NERR3$

```

STORAGE ASSIGNMENT (BLOCK, TYPE, RELATIVE LOCATION, NAME)

```

0000 R 000000 CZ 0000 R 000007 CZI 0000 I 000006 I 0000 000012 INJP$ 0000 R 000010 SZI

```

```

00101 1* SUBROUTINE FAIR (PG, DG, TG, PJ, DJ, TJ, IH, P, D, T, DPXG, FAI00100
00101 2* $ DPYG, DPXJ, DPYJ, DPX, DPY, DTXG, DTYG, DTXJ, DTYJ, DTX, CTY) FAI00200
00101 3* C.....FAIRS BETWEEN GROVES AND JACCHIA VALUES 90 LE HEIGHT LE 115 KM FAI00300
00103 4* DIMENSION CZ(6) FAI00400
00103 5* FAIRING VALUES FAI00500
00104 6* DATA CZ /1.0,0.9045085,0.6545085,0.3454915,0.0954915,0.0/ FAI00600
00106 7* I = (IH - 85)/5 @.....HEIGHT INDEX FAI00700
00107 8* CZI = CZ(I) @.....GROVES FAIRING COEFFICIENT FAI00800
00110 9* SZI = 1.0 - CZI @.....JACCHIA FAIRING COEFFICIENT FAI00900
00111 10* T = TG*CZI + TJ*SZI @.....FAIRED TEMPERATURE FAI01000
00112 11* P = EXP(ALOG(PG)*CZI + ALOG(PJ)*SZI) @.....FAIRED PRESSURE FAI01100
00113 12* D = EXP(ALOG(DG)*CZI + ALOG(DJ)*SZI) @.....FAIRED DENSITY FAI01200
00114 13* DPX = DPXJ FAI01300
00115 14* DPY=DPYG*CZI+DPYJ*SZI @.....DP/DY FOR GEOSTROPHIC WINDS FAI01400
00116 15* DTX = DTXJ FAI01500
00117 16* DTY = DTYG * CZI + DTYJ * SZI @.....DT/DY FOR THERMAL WINDS FAI01600
00120 17* RETURN FAI01700
00121 18* END FAI01800

```

***** FAIR *****
 END OF COMPILATION: NO DIAGNOSTICS.
 @HDG,P ***** GEN4D *****
 @FOR,S PROFAS.GEN4DIGEN4D
 FOR S11E-02/04/74-18:52:06 (0*)

SUBROUTINE GEN4D ENTRY POINT 001134

STORAGE USED: CODE(1) 001150; DATA(0) 000106; BLANK COMMON(2) 000000

COMMON BLOCKS:

0003 C4 004743
 0004 IOTEMP 000054
 0005 PDTCOM 007505

EXTERNAL REFERENCES (BLOCK, NAME)

0006 GRID4D
 0007 GTERP
 0010 INTER2
 0011 PDTUV
 0012 ATAN
 0013 FERR2S
 0014 SORT
 0015 NERR3S

STORAGE ASSIGNMENT (BLOCK, TYPE, RELATIVE LOCATION, NAME)

0001	000216	I10L	0001	000225	I20L	0001	000234	I30L	0001	000243	I40L	0001	000247	I50L
0001	000253	I60L	0001	000314	I70G	0001	000257	I70L	0001	000334	I74G	0001	000266	I80L
0001	000274	I90L	0001	000022	I20L	0001	000354	I200L	0001	000364	I255G	0001	000414	I216G
0001	000415	I221G	0001	000446	I232G	0001	000467	I240G	0001	000571	I261G	0001	000050	I30L
0001	000751	I306G	0001	001035	I325G	0001	000405	I400L	0001	000507	I440L	0001	000637	I445L
0001	000650	I480L	0001	001017	I485L	0001	000405	I400L	0004	000040	AP	0004	000050	B
0000	R 000011	CHECK	0004	R 000007	CLAT	0003	R 004742	CLON	0003	R 000701	D	0004	R 000004	DD
0005	R 003705	DSP	0000	R 000031	DH	0000	R 000033	DP	0000	R 000022	DPX	0000	R 000023	DPY
0000	R 000001	DY	0000	R 000034	DT	0000	R 000020	D2	0000	R 000025	DTY	0004	R 000044	DX
0004	R 000036	F10	0004	R 000047	DZ	0000	R 000020	D2	0004	R 000051	EPS	0000	R 000000	F
0000	R 000027	H	0004	000037	F10B	0004	000031	G	0003	R 000000	GLAT	0004	R 000020	GLON
0000	I 000026	IHP	0004	000045	HL	0004	000026	H1	0000	I 000006	I	0004	000024	IDA
0005	000002	IOPR	0004	000041	IHR	0000	I 000012	IHV	0000	000060	INJPS	0004	000052	IOPP
0004	000025	IYR	0000	I 000007	I12	0004	000001	IOTEM1	0004	000002	IUG	0005	000000	IU4
0000	I 000005	LONO	0004	I 000053	LOOK	0004	I 000010	J	0000	I 000003	K	0000	I 000004	LATO
0003	I 000040	NG	0004	I 000003	NACOP	0004	000043	NMORE	0004	000025	MN	0005	000001	MONTH
0005	R 000003	PG	0000	R 000030	PH	0004	000034	PHIR	0004	000027	PH1R	0003	R 000041	P
0003	R 004741	PLON	0005	R 002005	PSP	0004	R 000017	P2	0004	000012	RD1	0004	R 000006	PLAT
0004	R 000011	RPI	0004	000013	RT1	0004	R 002401	SP	0004	000020	RV1	0003	R 000032	RI
0000	R 000015	SDR	0004	000015	SD1	0003	R 002401	SP	0000	R 000014	SPR	0004	R 000004	SD
0003	R 004101	ST	0000	R 000016	STR	0004	000016	ST1	0004	000021	SU1	0004	000022	SV1
0003	R 001541	T	0005	R 000531	TG	0000	R 000032	TH	0000	R 000002	THETA	0004	000035	THETR
0004	000030	THET1R	0005	R 005605	TSP	0000	R 000021	T2	0000	R 000046	VL	0004	000005	XNJD
0004	000033	Z	0000	R 000013	Z1									

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```

***** GEN4D *****
00101 1* SUBROUTINE GEN4D
00102 2* GENERATES NG = 9 OR 16 4D PROFILES P,D,T AND SIGMAS SP,SD,ST AT
00103 3* GRID OF LATITUDES AND LONGITUDES GLAT,GLON, CURRENT LATITUDE,
00104 4* LONGITUDE=CLAT,CLON, PREVIOUS LATITUDE, LONGITUDE=PLAT,PLON,
00105 5* COMMON/C4/GLAT(16),GLON(16),NG,P(16,26),D(16,26),T(16,26),
00106 6* SP(16,26),SD(16,26),ST(16,26),PLON,CLON
00107 7* COMMON/IOTEMP/IOTEM1,IOTEM2,IUG,NMCO,DD,XMJD,PLAT,CLAT,
00108 8* $ NAME,RPL,PDI,RT1,SP1,SD1,ST1,RU1,RV1,SU1,SV1,
00109 9* $ MN,IDA,IYR,H1,PH1R,TH1R,G,RI,Z,PHIR,THETR,F10,F10B,AP,
00110 10* $ IHR,MIN,NMOR,DX,HL,VL,DZ,R,EPS,IOPP,LOOK
00111 11* COMMON/PDTCOM/IU4,MONTH,IOPR,PG(18,19),TG(18,19),DG(18,19),
00112 12* PSP(8,10,12),DSP(8,10,12),TSP(8,10,12)
00113 13* C.....GENERATES NG=9 OR 16 4D PROFILES P,D,T AND SIGMAS SP,SD,ST AT
00114 14* GRID OF LATITUDES AND LONGITUDES GLAT,GLON, CURRENT LATITUDE
00115 15* LONGITUDE = CLAT, CLON, PREVIOUS LATITUDE, LONGITUDE = PLAT,
00116 16* PLON
00117 17* LOOK=0
00118 18* F = 0.017453293
00119 19* NG = 16
00120 20* DX = PLON - CLON
00121 21* C..... LONGITUDE DISPLACEMENT FROM PREVIOUS TO CURRENT POSITION
00122 22* DY = CLAT - PLAT
00123 23* C..... LATITUDE DISPLACEMENT FROM PREVIOUS TO CURRENT POSITION
00124 24* IF (CY) 20,10,20
00125 25* 10 THETA = 180. + SIGN(90.,DX)
00126 26* GO TO 30
00127 27* 20 THETA = ATAN(DX/DY)/F
00128 28* IF (DY.GT.0.) THETA = THETA + 180.
00129 29* IF (THETA.LT.0.) THETA = THETA + 360.
00130 30* C..... THETA = AZIMUTH ANGLE OF TRAJECTORY, USED TO ORIENT LAT-LON GRID
00131 31* 30 K = INT((THETA + 67.5)/45.)
00132 32* IF (K.GT.8)K=8 @ INDEX USED IN COMPUTED GO TO FOR I10 THRU 180
00133 33* IF (CLAT.GT.75.0.AND.K.GE.3.AND.K.LE.7)GO TO 200@NORTH POLAR GRID
00134 34* IF (CLAT.LT.-75.0.AND.(K.GE.7.OR.K.LE.3))GO TO 200@SOUTH POL GRID
00135 35* C..... INITIAL ESTIMATE OF REFERENCE LATITUDE (LOWER LEFT GRID POINT)
00136 36* LATO = 5*INT(CLAT/5.)
00137 37* IF (CLAT.LT.0.) LATO = LATO - 5
00138 38* C..... INITIAL ESTIMATE OF REFERENCE LONGITUDE (LOWER LEFT GRID POINT)
00139 39* LONO=5*INT(CLON/5.)
00140 40* C..... ADJUSTS LATO,LONO ACCORDING TO DIRECTION OF TRAJECTORY AZIMUTH
00141 41* 110 LATO = LATO-10
00142 42* LONO = LONO + 10
00143 43* GO TO 190
00144 44* 120 LATO = LATO-10
00145 45* LONO = LONO+15
00146 46* GO TO 190
00147 47* 130 LATO = LATO-5
00148 48* LONO = LONO+15
00149 49* GO TO 190
00150 50* 140 LONO = LONO+15
00151 51* GO TO 190
00152 52* 150 LONO = LONO+10
00153 53* GO TO 190
00154 54* 160 LONO = LONO+5
00155 55* GO TO 190
00156 56* LONO = LONO+5
00157 56* GO TO 190

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***** GENHD *****
00160 57* 170 LATO = LATO-5
00161 58* LONO = LONO+5
00162 59* GO TO 190
00163 60* 180 LATO = LATO-10
00164 61* LONO = LONO+5
00165 62* 190 IF (LONO.GT.360) LONO = LONO - 360
00167 63* DO 195 I=1,4
00172 64* I12 = I+12
00173 65* DO 195 J=I,I12,4
00176 66* GLAT(J) = LATO + 1.25*(J-I)
00176 67* C.....LATITUDE, LONGITUDE GRID AT 5 DEGREE INTERVALS
00177 68* 195 GLON(J) = LONO - 5. * (I - 1)
00202 69* GO TO 400
00203 70* 200 NG = 9 C.....POLAR GRID
00204 71* DC 210 J=1,8
00207 72* C.....POLAR GRID LATITUDES 1-8 = +75 (N) OR -75 (N)
00207 73* GLAT(J) = SIGN(75.,GLAT)
00210 74* C.....POLAR GRID LONGITUDES 1-8 AT 45 DEG INTERVALS
00210 75* 210 GLON(J) = 45.*(J-1)
00212 76* C.....POLAR GRID LATITUDE 9 = POLE +93 OR -90
00212 77* GLAT(9) = SIGN(90.,GLAT)
00213 78* C.....POLAR GRID LONGITUDE 9 = 0
00213 79* GLON(9) = 0.
00213 80* C.....GENERATES 16 PROFILES (OR 9 PROFILES FOR POLAR GRID)
00214 81* 400 CALL GRID4D
00215 82* DO 410 I=1,NG
00220 83* DO 410 J=1,26
00220 84* C.....CONVERTS RELATIVE VARIANCES TO RELATIVE STANDARD
00220 85* C DEVIATIONS (SIGMAS)
00223 86* SP(I,J) = SORT(SPI,I,J)
00224 87* SD(I,J) = SORT(SDI,I,J)
00225 88* ST(I,J) = SORT(ST(I,J))
00226 89* 410 CONTINUE
00231 90* DO 500 I=1,NG
00234 91* CHECK=SP(I,26)*D(I,26)*T(I,26)*SP(I,26)*SD(I,26)*ST(I,26)
00235 92* IF (CHECK.GT.0.) GO TO 500 C.....CHECK FOR ZERO DATA AT HEIGHT 25GE08800
00237 93* DO 420 J=25,1,-1
00242 94* CHECK = PI(I,J) * D(I,J) * T(I,J) * SP(I,J) * SD(I,J) * ST(I,J)
00243 95* IHV = J C.....FINDS INDEX IHV OF HIGHEST HEIGHT WITH NON-ZERO DATA
00244 96* IF (CHECK.GT.0.) GO TO 440
00246 97* 420 CONTINUE
00250 98* 440 Z1 = IHV -1. C.....HEIGHT = HEIGHT INDEX - 1
00251 99* SPR=SP(I,IHV) C.....SPR,SDR,STR=SIGMAS AT HEIGHT Z1
00252 100* SDR=SD(I,IHV)
00253 101* STR=ST(I,IHV)
00253 102* C.....IF HEIGHT Z1 GEQ 20 KM, USE GROVES AT 30 KM FOR INTERPOLATION,
00253 103* C OTHERWISE USE GROVES AT 25 KM
00254 104* IF (IHV.GE.21) GO TO 480.
00254 105* C.....EVALUATES GROVES AT 25 KM FOR INTERPOLATION AND
00254 106* C FILL IN OF ZERO DATA
00256 107* CALL GTERP(25,GLAT(I),P2,D2,T2,P6,D6,T6,DPX,DPY,DTX,DTY)
00257 108* IHP = IHV + 1
00260 109* DO 450 K=IHP,26
00260 110* C.....AVOIDS INTERPOLATION OF P,D,T IF ONLY SIGMAS ARE ZERO
00263 111* IF ((P(I,K)*D(I,K)*T(I,K)).GT.0.) GO TO 445
00265 112* H=K-1
00265 113* C.....INTERPOLATES BETWEEN 4D AT HEIGHT Z1 AND GROVES AT 25 TO FILL

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REPRODUCIBILITY OF THE ORIGINAL PAGE IS POOR

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***** GEN40 *****
00265 114* IN MISSING DATA
00266 115* CALL INTER2(P(I,IHV),D(I,IHV),T(I,IHV),Z1,P2,U2,T2,25.,PH,DH,TH,H)
00267 116* P(I,K)=PH
00270 117* D(I,K)=DH
00271 118* T(I,K)=TH
00272 119* 445 SP(I,K) = SPR
00273 120* SD(I,K)=SDR
00274 121* C.....SETS MISSING SIGMAS EQUAL TO SIGMAS AT HEIGHT Z1
00275 122* 450 ST(I,K)=STR
00276 123* GO TO 500
00277 124* C.....EVALUATES GROVES AT 30 KM FOR INTERPOLATION AND FILL IN OF
00278 125* ZERO DATA
00279 126* 480 CALL GTERP(30,GLAT(I),P2,U2,T2,P6,DG,TG,DPX,DPY,DTX,DTY)
00300 127* CALL PDTUV(PSP,DSP,TSP,GLAT(I),GLON(I),30,DP,DD,DT,DPX,DPY,DTX,DTY)
00301 128* $ ) .....COMPUTE STATIONARY PERTURBATIONS AT 30 KM
00302 129* C.....ADD STATIONARY PERTURBATIONS TO GROVES MODEL
00303 130* P2 = P2*(1. + DP)
00304 131* T2 = T2*(1. + DT)
00305 132* IHP = IHV + 1
00306 133* DO 490 K=IHP,26
00307 134* C.....AVOIDS INTERPOLATING P,D,T IF ONLY SIGMAS ARE ZERO
00308 135* IF ((P(I,K)*D(I,K)+T(I,K)).GT.0.) GO TO 485
00309 136* H=K-1
00310 137* C.....INTERPOLATES BETWEEN 4D AT HEIGHT Z1 AND GROVES AT 30 KM TO
00311 138* FILL IN MISSING DATA
00312 139* CALL INTER2(P(I,IHV),D(I,IHV),T(I,IHV),Z1,P2,U2,T2,30.,PH,DH,TH,H)
00313 140* P(I,K)=PH
00314 141* D(I,K)=DH
00315 142* T(I,K)=TH
00316 143* 485 SP(I,K) = SPR
00317 144* SD(I,K)=SDR
00320 145* 490 ST(I,K)=STR
00321 146* IHP = IHV - 1
00322 147* DO 495 K=1,IHP
00323 148* C.....SETS MISSING SIGMAS TO SIGMAS AT HEIGHT Z1
00324 149* IF (SP(I,K).LE.0.0.AND.P(I,K).GT.0.) SP(I,K) = SPR
00325 150* IF (SD(I,K).LE.0.0.AND.D(I,K).GT.0.) SD(I,K) = SDR
00326 151* IF (ST(I,K).LE.0.0.AND.T(I,K).GT.0.) ST(I,K) = STR
00327 152* 500 CONTINUE
00328 153* RETURN
00329 154* END
00341 155*

```

END OF COMPILATION: NO DIAGNOSTICS.

GHUG,P ***** GETNMC *****
 GFOR,S PROFAS,GETNMC,GETNMC
 FOR S1E-02/04/74-18:52:12 (0,)

SUBROUTINE GETNMC ENTRY POINT 000133

STORAGE USED: CODE(1) 000137; DATA(0) 000057; BLANK_COMMON(2) 000000

COMMON BLOCKS:

***** GETNMC *****

0003 IOTEMP 000004

EXTERNAL REFERENCES (BLOCK, NAME)

0004 NTRAN
 0005 FRODUS
 0006 NIO1\$
 0007 NIO2\$
 0010 NWDUS
 0011 P\$TOP\$
 0012 NERR3\$

STORAGE ASSIGNMENT (BLOCK, TYPE, RELATIVE LOCATION, NAME)

0001 000003 1L 0000 000024 100F 0001 000031 120G 0001 000023 2L
 0000 000025 200F 0001 000035 3L 0001 000075 5L 0001 000111 6L 0000 I 000021 I
 0000 I 000023 1J 0000 000051 100P\$ 0000 I 000000 1P 0003 I 000002 1UG 0000 I 000020 L
 0000 I 000022 M C003 I 000003 NMCOP 0000 I 000017 NREC 0003 I 000000 SCRCH1 0003 I 000001 SCRCH2

```

00101 1*
00101 2*
00101 3*
00101 4*
00101 5*
00103 6*
00103 7*
00104 8*
00104 9*
00105 10*
00105 11*
00106 12*
00107 13*
00107 14*
00111 15*
00112 16*
00113 17*
00115 18*
00116 19*
00124 20*
00125 21*
00130 22*
00131 23*
00133 24*
00134 25*
00135 26*
00136 27*
00137 28*
00141 29*
00143 30*
00144 31*
00146 32*
00147 33*

SUBROUTINE GETNMC
READS 'SETUP' DATA TAPE, OR NMC GRID DATA CARDS,
AND WRITES SCRATCH FILE FOR USE BY SELE4.
DIMENSION IP(15)
COMMON /IOTEMP/ SCRCH1,SCRCH2,IUG,NMCOP
INTEGER SCRCH2
NREC=0
IF(NMCOP.NE.0) GO TO 2
1 CALL NTRAN(IUG,2,15,IP,L)
CALL NTRAN(IUG,22)
IF(L.NE.15) GO TO 6
GO TO 3
2 READ(5,100) (IP(I),I=1,15)
100 FORMAT(15I5)
3 DO 4 I=1,15,3
N=IP(I)
IF(M.LT.1) GO TO 5
IJ=IP(I+1)*100+IP(I+2)
CALL NTRAN (SCRCH2,I,IJ,L)
CALL NTRAN (SCRCH2,22)
NREC=NREC+1
4 CONTINUE
IF(NMCOP.NE.0) GO TO 2
GO TO 1
5 IF(NREC.NE.1977) GO TO 6
CALL NTRAN(IUG,8,1) @ MOVES PAST FIRST EOF ON INIT IUG
RETURN
    
```

```

***** GETNMC *****
00150 34* 6 WRITE(6,200) NREC,SCRCH2
00154 35* 200 FORMAT(1H1/1X,16,' RECORDS WRITTEN BY GETNMC IN SCRATCH FILE',I3)
00155 36* STOP
00156 37* END
    
```

```

GET03400
GET03500
GET03600
GET03700
    
```

```

END OF COMPILATION: NO DIAGNOSTICS.
RDG,P ***** GRID4D *****
RFOR,S PROFAS,GRID4D,GRID4D
FOR S11E-02/04/74-18:52:30 (0, )
    
```

SUBROUTINE GRID4D ENTRY POINT 000641

STORAGE USED: CODE(1) 000662; DATA(0) 000334; BLANK COMMON(2) 000000

COMMON BLOCKS:

```

0003 C4 004741
0004 PDTCOM 000002
0005 TOTEMP 000002
0006 POINT 000200
0007 ORDER 000423
0010 INT 002037
    
```

EXTERNAL REFERENCES (BLOCK, NAME)

```

0011 NTRAN
0012 SELEC4
0013 INTRP4
0014 NWDUS
0015 NIC2$
0016 NIC1$
0017 NSTOPS
0020 NERR3$
    
```

STORAGE ASSIGNMENT (BLOCK, TYPE, RELATIVE LOCATION, NAME)

```

0001 000204 1726 0001 000057 21L 0001 000261 217G 0001 000063 22L 0001 000267 222G
0001 000270 2256 0000 000203 23F 0001 000301 234G 0001 000136 24L 0001 000154 25L
0001 000350 253G 0001 000207 27L 0001 000424 271G 0001 000251 28L 0001 000320 30L
0001 000433 301G 0001 000454 315G 0001 000415 32L 0001 000437 35L 0001 000447 36L
0001 000452 37L 0001 000561 39L 0000 000217 40F 0010 R 000000 D 0000 R 000202 DIVIDE
0010 R 002027 DLA 0010 R 002033 DLO 0006 R 000140 DXY 0010 R 002025 DYX 0000 I 000176 INDEX
0000 I 000170 I 0010 I 002020 IG 0000 I 000175 II 0000 I 000000 IN 0000 I 000176 INDEX
0000 I 000302 INJPS 0000 I 000172 IP 0006 I 000000 IPT 0007 I 000000 IPTN 0000 I 000163 IRC
0007 I 000120 IREAD 0000 I 000164 IRN 0004 I 000000 IT 0000 I 000171 J 0000 I 000165 JT
0000 I 000200 J1 0000 I 000177 J2 0000 I 000174 K 0000 I 000167 L 0000 I 000201 LALO
0003 R 000000 LAT 0006 I 000120 LL 0003 R 000020 LON 0000 I 000166 M 0004 I 000001 MONTH
0000 I 000173 MP 0000 I 000162 N 0003 I 000040 NP 0000 R 000156 ONE 0003 R 000041 P
0003 R 000701 R 0000 I 000153 READ 0005 I 000000 SCRCH1 0005 I 000001 SCRCH2 0003 R 002401 SP
0003 R 003241 SR 0003 R 004101 ST 0003 R 001541 T 0000 R 000157 TEN 0000 R 000161 THOU
0000 I 000154 WRITE 0000 R 000155 ZERO
    
```

***** GRID4D *****

```

00101 1* SUBROUTINE GRID4D
00102 2* REAL LAT, LON
00103 3* COMMON/4/LAT(16), LON(16), NP, P(16,26), R(16,26), T(16,26), SP(16,26)
00104 4* $ SR(16,26), ST(16,26)
00105 5* COMMON /PDTCOM/ IT, MONTH
00106 6* C
00107 7* C SUBROUTINE TO SELECT PRESSURE, TEMPERATURE, AND DENSITY PROFILES
00108 8* C TOGETHER WITH THE NORMALIZED VARIANCES IN EACH, AT UP TO 16 GRID
00109 9* C AT LAT/LONS SELECTED BY CALLING PROGRAM.
00110 10* C
00111 11* C USES NASA HUNTSVILLE W5FC 4-D DATA TAPES
00112 12* C
00113 13* C DIMENSION IH(107)
00114 14* C
00115 15* C COMMON /IOTEMP/ SCRCH1, SCRCH2
00116 16* C COMMON /POINT/ IPT(16,5), ILL(16), DXY(16,2)
00117 17* C COMMON /ORDER/ IPTN(16,5), IREAD(65,3)
00118 18* C COMMON /INT/ D(208,5), IG(5), DYX(2), DLA(4), DLO(4)
00119 19* C
00120 20* C INTEGER SCRCH1, READ, WRITE
00121 21* C
00122 22* C INITIALIZE
00123 23* C
00124 24* C ZERO=0.0
00125 25* C ONE=1.0
00126 26* C TEN=10.0
00127 27* C HUNDRE=100.0
00128 28* C THOU=1000.0
00129 29* C READ=6H READ
00130 30* C WRITE=6H WRITE
00131 31* C
00132 32* C NEMONTH=1-((2*MONTH)/9)*4
00133 33* C CALL NTRAN (IT,10)
00134 34* C CALL NTRAN (IT,22)
00135 35* C CALL NTRAN(IT,8/N)
00136 36* C CALL NTRAN (IT,22)
00137 37* C
00138 38* C APPROPRIATE 4-D INPUT TAPE NOW POSITIONED - FILE NEEDED PROFILES
00139 39* C
00140 40* C
00141 41* C 20 CALL SELEC4
00142 42* C
00143 43* C
00144 44* C IRC=0
00145 45* C IRN=1
00146 46* C IF(IREAD(IRN,3).EQ.0) GO TO 39
00147 47* C 21 JT=IT
00148 48* C M=READ
00149 49* C 22 CALL NTRAN (IT,2,106,IN/L)
00150 50* C CALL NTRAN (IT,22)
00151 51* C IRC=IRC+1
00152 52* C IF(IRC.EQ.-2) GO TO 39
00153 53* C IF(LT.0) WRITE(6,23) IT,L,IRC
00154 54* C 23 FORMAT(' INPUT UNIT NO.,',I3, ' IN ERROR (' ,I2,') FOR RECORD NO.,',I5GR105400
00155 55* C 1)
00156 56* C IF(IRC.LT.IREAD(IRN,3)) GO TO 22

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REPRODUCIBILITY OF THE ORIGINAL PAGE IS POOR

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***** GRID4D *****
00155 57* IF(IRC.GT.IREAD(IRN,3)) GO TO 39
00157 58* I=IREAD(IRN,1)
00160 59* J=IREAD(IRN,2)
00161 60* IF(IRN.EQ.1) GO TO 25
00163 61* IF(IREAD(IRN,3).EQ.IREAD(IRN-1,3)) GO TO 27
00165 62* IP=FLO(12,12,IN(106))
00166 63* 4P=FLO(24,12,IN(106))
00167 64* IF((IP.NE.MONTH).OR.(IP.NE.IPT(I,J))) GO TO 39
00171 65* DO 26 K=106,1,-1
00174 66* IN(K+1)=IN(K)
00175 67* CONTINUE
00177 68* 27 FLD(0,18,IN(1))=I
00200 69* FLD(18,18,IN(1))=J
00201 70* JT=SCRCHI
00202 71* WRITE
00203 72* CALL NTRAN (SCRCHI,1,107,IN,L)
00204 73* CALL NTRAN (SCRCHI,22)
00205 74* IRN=IRN+1
00206 75* IF(L.NE.107) GO TO 39
00210 76* IF(IREAD(IRN,3).EQ.IRC) GO TO 24
00212 77* IF(IREAD(IRN,3).EQ.0) GO TO 28
00214 78* GO TO 21
00214 79*
00214 80* C INTERPOLATE TO GIVEN LAT/LON FROM GRID DATA
00214 81* C
00215 82*
00216 83* 28 *READ
00221 84* DO 29 I=1,208
00224 85* DO 29 J=1,5
00227 86* D(I,J)=0.0
00230 87* CONTINUE
00233 88* DO 32 J=1,4
00236 89* IF(IPT(II,J).EQ.0) GO TO 32
00240 90* FLD(0,18,INDEX)=I
00241 91* FLD(18,18,INDEX)=J
00242 92* CALL NTRAN(SCRCHI,10)
00243 93* CALL NTRAN(SCRCHI,22)
00244 94* CALL NTRAN(SCRCHI,2,107,IN,L)
00245 95* CALL NTRAN(SCRCHI,22)
00246 96* IF(L.EQ.-2) GO TO 39
00250 97* IF(IN(1).NE.INDEX) GO TO 30
00252 98* DO 31 I=2,105
00255 99* J2=2*I-2
00256 100* J1=J2-1
00257 101* D(J1,J)=FLD(0,18,IN(I))/HUNDR
00260 102* D(J2,J)=FLD(18,18,IN(I))/HUNDR
00261 103* CONTINUE
00263 104* DLA(J)=FLD(0,18,IN(106))/TEN
00264 105* DLO(J)=FLD(18,18,IN(106))/TEN
00265 106* CONTINUE
00265 107*
00265 108* C IF NECESSARY, INTERPOLATE
00265 109* C
00266 110* LALO=LL(I)
00270 111* DO 33 I=1,5
00273 112* IG(I)=IPT(II,I)
00274 113* CONTINUE

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```

***** GRID40 *****
00276 114* IF (IG(2),NE,0) GO TO 35
00300 115* DO 34 I=1,208
00303 116* D(I,5)=D(I,1)
00304 117* 34 CONTINUE
00306 118* GO TO 37
00307 119* 35 IF (IG(5),NE,2) GO TO 36
00311 120* JYX(1)=DX(I,1)
00312 121* JYX(2)=DX(I,2)
00312 122* C
00313 123* 36 CALL INTRP4 (LALO)
00313 124* C
00314 125* 37 DO 38 I=1,26
00317 126* P(I,I)=D(I,5)*HUNDR
00320 127* R(I,I)=D(I+156,5)/THOU
00321 128* T(I,I)=D(I+52,5)
00322 129* DIVIDE=ONE
00323 130* IF (P(I,I),GT,ZERO) DIVIDE=(P(I,I)/HUNDR)**2
00325 131* SP(I,I)=D(I+26,5)/DIVIDE
00326 132* DIVIDE=ONE
00327 133* IF (R(I,I),GT,ZERO) DIVIDE=(THOU*R(I,I))**2
00331 134* SR(I,I)=D(I+182,5)/DIVIDE
00332 135* DIVIDE=ONE
00333 136* IF (T(I,I),GT,ZERO) DIVIDE=T(I,I)**2
00335 137* ST(I,I)=D(I+78,5)/DIVIDE
00336 138* 38 CONTINUE
00341 139* CALL NTRAN(SCRCH1,10)
00342 140* CALL NTRAN(SCRCH1,22)
00343 141* RETURN
00344 142* 39 WRITE(6,40) JT,IRC,I,READ(IRN,3),MP,MONTH,IP,I,J,IPT(I,J),IRN,M,L
00362 143* 40 FORMAT(,' ***** UNIT NO.,',I3,' IN ERROR,',I7,' RECORDS READ',/
00362 144* 1, I, READ(IRN,3) =',I5,' MP =',I3,' MONTH =',I3,
00362 145* 2, IP =',I5,' IPT(',I2,',',I1,',) =',I5,' IRN =',I3/A6,' STATUS',I5)
00363 146* STOP
00364 147* END

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END OF COMPILATION: NO DIAGNOSTICS.
 @HDS,P ***** GTERP *****
 @FOR,S PROFAS.GTERP,GTERP
 FOR S11E-02/04/74-18:52:36 (3.)

SUBROUTINE GTERP ENTRY POINT 000227

STORAGE USED: CODE(1) 000263; DATA(0) 000040; BLANK COMMON(2) 000000

EXTERNAL REFERENCES (BLOCK, NAME)

0003 NERR3\$

STORAGE ASSIGNMENT (BLOCK, TYPE, RELATIVE LOCATION, NAME)

0001	000067	20L	0001	000161	30L	0000	R	000003	CHK	0000	R	000006	DL	0000	I	000000	I	
0000	000017	INJPs	0000	I	000001	J	0000	I	000002	JP	0000	R	000004	PHIF	0000	R	000011	R

***** GTERP *****

0000 R 000007 R1 0000 R 000010 R2 0000 R 000005 TL

```

00101 1* SUBROUTINE GTERP(IH,PHI,P,D,T,P6,DG,T6,DPX,DPY,DTX,DTY)
00102 2* INTERPOLATES GROVES DATA TO HEIGHT IH AND LATITUDE PHI
00103 3* DIMENSION PG(18,19),TG(18,19),DG(18,19)
00104 4* I = (IH - 20)/5  @.....HEIGHT INDEX
00105 5* J = INT((PHI + 100.)/10.) @.....LOWER LATITUDE INDEX
00106 6* JP = J + 1 @.....UPPER LATITUDE INDEX
00107 7* C.....CHECK FOR DENSITY OR TEMPERATURE LEO 0
00108 8* CHK = DG(I,J) * TG(I,J) * DG(I,JP) * TG(I,JP)
00109 9* IF (CHK) 10,10,20
00110 10 P = PG(I,J)
00111 11 D = DG(I,J)
00112 12 T = TG(I,J)
00113 13 GO TO 30
00114 14 C.....LATITUDE DEVIATION FROM GROVES ARRAY POSITION
00115 15 20 PHIF = (PHI + 100. - 10.*J)/10.
00116 16 TLE = TG(I,J) + (TG(I,JP) - TG(I,J))*PHIF
00117 17 DLE = DG(I,J) + (DG(I,JP) - DG(I,J))*PHIF @LATITUDE INTERPOLATION
00118 18 R1 = PG(I,J)/(DG(I,J)*TG(I,J))
00119 19 R2 = PG(I,JP)/(DG(I,JP)*TG(I,JP))
00120 20 R = R1 + (R2 - R1)*PHIF @.....INTERPOLATED GAS CONSTANT
00121 21 P = DL*R*TL @.....PRESSURE COMPUTED FROM INTERPOLATED GAS CONSTANT
00122 22 J = DL
00123 23 T = TL
00124 24 30 DPX = 0.
00125 25 DTY = 0.
00126 26 DPY = (P6(I,JP) - P6(I,J)) * 0.5 @.....DP/DY FOR GEOSTROPHIC WINDS
00127 27 DTY = (TG(I,JP) - TG(I,J)) * 0.5 @.....DT/DY FOR THERMAL WINDS
00128 28 RETURN
00129 29 END

```

END OF COMPILATION: NO DIAGNOSTICS.

INTERW *****
#FOR,S PROFAS.INTERW/INTERW
FOR S11E-02/04/74-18:52:39 (0.)

SUBROUTINE INTERW ENTRY POINT 000041

STORAGE USED: CODE(1) 000072; DATA(0) 000012; BLANK COMMON(2) 000000

EXTERNAL REFERENCES (BLOCK, NAME)

0003 NERR3s

STORAGE ASSIGNMENT (BLOCK, TYPE, RELATIVE LOCATION, NAME)

0001 000012 20L 0000 R 000000 A 0000 000001 INJPS

***** INTERW *****

```

00101 1* SUBROUTINE INTERW(U1,V1,Z1,U2,V2,Z2,U,V,Z)
00103 2* IF ( Z1 - Z2 ) 20,10,20
00106 3* 10 U = U1
00107 4* V = V1 @.....SETS U,V = U1,V1 IF Z1=Z2
00110 5* RETURN
00111 6* 20 A = (Z-Z1)/(Z2-Z1)
00112 7* U = U1 + (U2-U1) * A
00113 8* V = V1 + (V2-V1) * A
00113 9* C.....LINEAR INTERPOLATION BETWEEN U1,V1 AT HEIGHT Z1 AND U2,V2 AT
00113 10* C HEIGHT Z2. OUTPUT IS U,V AT HEIGHT Z
00114 11* RETURN
00115 12* END

```

END OF COMPILATION: NO DIAGNOSTICS.

QHDG,P ***** INTERZ *****
 @FOR,S PROFAS,INTERZ,INTERZ
 FOR S11E-02/04/74-18:52:41 (9,)

SUBROUTINE INTERZ ENTRY POINT 000050

STORAGE USED: CODE(1) 000110; DATA(0) 000014; BLANK COMMON(2) 000000

EXTERNAL REFERENCES (BLOCK, NAME)

0003 NERR35

STORAGE ASSIGNMENT (BLOCK, TYPE, RELATIVE LOCATION, NAME)

0001 000014 20L 0000 R 000000 A 0000 000001 INJPS

```

00101 1* SUBROUTINE INTERZ(P1,D1,T1,Z1,P2,D2,T2,Z2,P,D,T,Z)
00103 2* 5 IF ( Z1 - Z2 ) 20,10,20
00106 3* 10 P = P1
00107 4* D = D1
00110 5* T = T1 @.....SETS P,D,T = P1,D1,T1, IF Z1=Z2
00111 6* RETURN
00112 7* 20 A = (Z - Z1) / (Z2 - Z1)
00113 8* T = T1 + (T2 - T1) * A
00114 9* D = D1 + (D2 - D1) * A
00115 10* P = P1 + (P2 - P1) * A
00115 11* C.....LINEAR INTERPOLATION BETWEEN P1,D1,T1 AT HEIGHT Z1 AND P2,D2,T2
00115 12* C AT HEIGHT Z2 TO OUTPUT VALUES OF P,D,T AT HEIGHT Z
00116 13* RETURN
00117 14* END

```

END OF COMPILATION: NO DIAGNOSTICS.

QHDG,P ***** INTER2 *****

***** I,ITER2 *****
 QFOR,S PROFAS,INTER2,ITER2
 FOR S,IE-02/04/74-18:52:43 (0,)

SUBROUTINE INTER2 ENTRY POINT 000135

STORAGE USED: CODE(1) 000202; DATA(0) 000031; BLANK COMMON(2) 000000

EXTERNAL REFERENCES (BLOCK, NAME)

- 0003 ALOG
- 0004 EXP
- 0005 FERR35

STORAGE ASSIGNMENT (BLOCK, TYPE, RELATIVE LOCATION, NAME)

0001	000012	10L	0001	000023	20L	0001	000121	30L	0000 R	000001	A	0000 R	000000	CHK
0000	R	000002	DZ	0000	000007	INJPS	0000	R	000006	R	0000 R	000004	R1	0000 R
0000	R	000003	TZ											0000 R

```

00101 1* SUBROUTINE INTER2(P1,D1,T1,Z1,P2,D2,T2,Z2,P,D,T,Z)
00102 2* C.....INTERPOLATES BETWEEN P1,D1,T1 AT HEIGHT Z1 AND P2,D2,T2 AT
00103 3* C.....HEIGHT Z2 TO OUTPUT VALUES OF P,D,T AT HEIGHT Z
00104 4* C.....CHECKS FOR T1,D1,T2,D2 PRODUCT = 0, FOR GAS CONSTANT INTERPOLATION
00105 5* CHK=T1*D1*T2*D2
00106 6* IF (CHK) 10,10,S
00107 7* 5 IF (Z1 - Z2) 20,10,20
00108 8* 10 P = P1
00109 9* D = D1
00110 10* T = T1 Q.....SETS P,D,T = P1,D1,T1 IF Z1=Z2
00111 11* RETURN
00112 12* 20 IF(P1*D1*T1*P2*D2*T2,LE,0.)GO TO 30
00113 13* A=ALOG(D2/D1)/(Z2-Z1)
00114 14* DZ= D1*EXP(A*(Z - Z1)) Q.....LINEAR INTERPOLATION ON LOG D
00115 15* A=(Z-Z1)/(Z2-Z1) Q.....LINEAR INTERPOLATION ON T
00116 16* TZE T1 + A*(T2-T1)
00117 17* R1=P1/(D1*T1)
00118 18* R2=P2/(D2*T2)
00119 19* R=(R2-R1)*A+R1 Q.....LINEAR INTERPOLATION ON GAS CONSTANT R
00120 20* P = DZ * R * TZ Q.....PRESSURE FROM PERFECT GAS LAW
00121 21* D = DZ
00122 22* T = TZ
00123 23* RETURN
00124 24* 30 P=0.
00125 25* D=0.
00126 26* T=0.
00127 27* RETURN
00128 28* END
  
```

END OF COMPILATION: NO DIAGNOSTICS.

REPRODUCIBILITY OF THE ORIGINAL PAGE IS POOR

***** INTER2 *****

GH0G,P ***** INTER4 *****
 GFOR,S PROFAS,INTER4,INTER4
 FOR S1E-02/04/74-18:52:45 (0,)

SUBROUTINE INTER4 ENTRY POINT 001066

STORAGE USED: CODE(1) 001237; DATA(0) 000106; BLANK COMMON(2) 000000

EXTERNAL REFERENCES (BLOCK, NAME)

0003 INTLL
 0004 NNDUS
 0005 NIO2S
 0006 SGR1
 0007 NERR3S

STORAGE ASSIGNMENT (BLOCK, TYPE, RELATIVE LOCATION, NAME)

0001	000354	100L	0001	000101	110S	0001	000426	110L	0001	000154	20L	0001	000467	200L
0001	000475	2076	0001	000526	210L	0001	000633	220L	0001	000240	25L	0000	000016	30F
0001	000646	300L	0001	000341	40L	0000	R	000007	CHECK	0000	R	0000	R	000005
0000	R	000011	DMIN	0000	R	0000	I	000001	I	0000	I	0000	I	000002
0000	I	000004	IC	0000	I	000005	ID	0000	I	000000	IH	0000	I	000002
0000	I	000012	J	0000	R	000010	XLON			0000	I	0000	I	000014
										0000	I	0000	I	000036
										0000	I	0000	I	000036

00101	1*	SUBROUTINE INTER4 (GLAT, GLON, CLAT, CLON, IZ, NG, P, D, T,	IN400100
00101	2*	\$ P4, D4, T4, DPX, DPY, DTX, DTY)	IN400200
00101	3*	C.....INTERPOLATES BETWEEN 4D ARRAYS P(I,IH),D(I,IH),T(I,IH) AT GRID	IN400300
00101	4*	C LOCATIONS LATITUDE GLAT(I) LONGITUDE GLON(I),	IN400400
00101	5*	C CLAT,CLON = CURRENT LATITUDE, LONGITUDE	IN400500
00101	6*	C IZ = HEIGHT	IN400600
00101	7*	C OUTPUT = P4,D4,T4, AND DERIVATIVES DPX,DPY,DTX,DTY	IN400700
00103	8*	DIMENSION GLAT(16),GLON(16),P(16,26),D(16,26),T(16,26)	IN400800
00104	9*	IH=IZ+1 @.....HEIGHT INDEX = HEIGHT + 1	IN400900
00105	10*	IF (NG.GT.9) GO TO 100	IN401000
00107	11*	DO 10 I=10,16 @.....NG = 9 MEANS POLAR GRID	IN401100
00112	12*	P(I,IH) = P(9,IH)	IN401200
00113	13*	D(I,IH) = D(9,IH)	IN401300
00114	14*	T(I,IH) = T(9,IH)	IN401400
00115	15*	GLAT(I) = GLAT(9)	IN401500
00116	16*	10 GLON(I) = GLON(I-8) @.....I=10-16 ALL AT 90 DEG	IN401600
00120	17*	IB = INT(CLON/45) + 1 @.....LOWER RIGHT INTERPOLATION INDEX	IN401700
00121	18*	IA = IB+1 @.....LOWER LEFT INTERPOLATION INDEX	IN401800
00122	19*	IF (IA.GT.8) IA = IA-8	IN401900
00124	20*	IF (ABS(CLAT).LT.75.) GO TO 20 @.....POSITION OUTSIDE POLAR GRID	IN402000
00126	21*	IC = IA+8 @.....UPPER LEFT INTERPOLATION INDEX	IN402100
00127	22*	ID = IB+8 @.....UPPER RIGHT INTERPOLATION INDEX	IN402200
00130	23*	GO TO 300	IN402300
00131	24*	20 IF (ABS(CLAT).LT.70.) GO TO 40	IN402350
00131	25*	C.....DIFFERENTIAL LONGITUDE FROM REF LON (IA)	IN402400

***** INTER4 *****

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00133 26*      DLON = (CLON - GLON(IA))/(GLON(IB) - GLON(IA))
00134 27*      C.....INTERPOLATION BETWEEN LATITUDE 75 POINTS FOR POSITION
00135 28*      CHECK=P(IA,IH)*D(IA,IH)*T(IA,IH)*P(IB,IH)*D(IB,IH)*T(IB,IH)
00140 29*      IF(CHECK) 25,23,25
00141 30*      23  P4=0.
00142 31*      T4=0.
00143 32*      WRITE(6,30)
00144 33*      RETURN
00145 34*      25  P4 = P(IA,IH) + (P(IB,IH) - P(IA,IH))*DLON
00146 35*      P4 = D(IA,IH) + (D(IB,IH) - D(IA,IH))*DLON
00147 36*      T4 = T(IA,IH) + (T(IB,IH) - T(IA,IH))*DLON
00150 37*      C.....DP/DX FOR GEOSTROPHIC WIND EQUATIONS
00151 38*      DPXP(IB,IH)-P(IA,IH)
00152 39*      OPY=P(IA+8,IH)-P(IA,IH)
00153 40*      C.....DP/DY FOR GEOSTROPHIC WIND EQUATIONS
00154 41*      DPY = D(Y) + (P(IB+8,IH) - P(IA,IH) - D(Y))*DLON
00155 42*      C.....DT/DX FOR THERMAL WIND EQUATIONS
00156 43*      DTX = T(IB,IH) - T(IA,IH)
00157 44*      DTY = T(IA+8,IH) - T(IA,IH)
00158 45*      C.....DT/DY FOR THERMAL WIND EQUATIONS
00159 46*      DTY = D(Y) + (T(IB+8,IH) - T(IA,IH) - D(Y))*DLON
00160 47*      C.....INDICATES ERROR BECAUSE OF POSITION OUTSIDE POLAR GRID
00161 48*      C.....INDICATES ERROR BECAUSE OF POSITION OUTSIDE POLAR GRID
00162 49*      30  FORMAT (' POSITION OUTSIDE 4-D GRID')
00163 50*      RETURN
00164 51*      40  WRITE(6,30)
00165 52*      P4=0.
00166 53*      T4=0.
00167 54*      C.....
00168 55*      RETURN
00169 56*      100 XLON = CLON
00170 57*      IF (CLON.GT.345) XLON = CLON - 360.
00171 58*      C.....CHECKS FOR POSITION WITHIN 16 POINT GRID 110=GOOD. 200=POSITION
00172 59*      C.....CHECKS FOR POSITION WITHIN 16 POINT GRID 110=GOOD. 200=POSITION
00173 60*      C.....CHECKS FOR POSITION WITHIN 16 POINT GRID 110=GOOD. 200=POSITION
00174 61*      C.....CHECKS FOR POSITION WITHIN 16 POINT GRID 110=GOOD. 200=POSITION
00175 62*      C.....CHECKS FOR POSITION WITHIN 16 POINT GRID 110=GOOD. 200=POSITION
00176 63*      IF (CLAT.GE.GLAT(1) .AND. CLAT.LT.GLAT(16) .AND. XLON.LE.GLON(1)
00177 64*      5 .AND. XLON.GT.GLON(16)) GO TO 110
00178 65*      GO TO 200
00179 66*      110 IA = 1 + INT((GLON(1) - XLON) / 5)
00180 67*      C.....IA = LOWER LEFT (REFERENCE) INTERPOLATION INDEX
00181 68*      IA = IA + 4 * INT((CLAT - GLAT(1)) / 5)
00182 69*      IB = IA + 1 @.....LOWER RIGHT INTERPOLATION INDEX
00183 70*      IC = IA + 4 @.....UPPER LEFT INTERPOLATION INDEX
00184 71*      ID = IA + 5 @.....UPPER RIGHT INTERPOLATION INDEX
00185 72*      GO TO 300
00186 73*      200 DMIN = 360
00187 74*      DO 210 J=1,16
00188 75*      DR = SQRT((CLAT-GLAT(J))**2 + (CLON-GLON(J))**2)
00189 76*      IF (DR.GT.DMIN) GO TO 210
00190 77*      IA = J
00191 78*      OMIN = DR
00192 79*      C.....210 LOOP FINDS CLOSEST 16 POINT GRID POSITION TO POSITION OUTSIDE
00193 80*      C.....210 LOOP FINDS CLOSEST 16 POINT GRID POSITION TO POSITION OUTSIDE
00194 81*      C.....210 LOOP FINDS CLOSEST 16 POINT GRID POSITION TO POSITION OUTSIDE
00195 82*      210 CONTINUE
00196 83*      IF(DMIN.GT.5.) GO TO 220
00197 84*      C.....TAKES INTERPOLATED VALUES TO BE CLOSEST GRID POINT
00198 85*      P4 = P(IA,IH)
00199 86*      P4 = P(IA,IH)
00200 87*      P4 = P(IA,IH)
00201 88*      P4 = P(IA,IH)
00202 89*      P4 = P(IA,IH)
00203 90*      P4 = P(IA,IH)
00204 91*      P4 = P(IA,IH)
00205 92*      P4 = P(IA,IH)
00206 93*      P4 = P(IA,IH)
00207 94*      P4 = P(IA,IH)
00208 95*      P4 = P(IA,IH)
00209 96*      P4 = P(IA,IH)
00210 97*      P4 = P(IA,IH)
00211 98*      P4 = P(IA,IH)
00212 99*      P4 = P(IA,IH)
00213 100*      P4 = P(IA,IH)
00214 101*      P4 = P(IA,IH)
00215 102*      P4 = P(IA,IH)
00216 103*      P4 = P(IA,IH)
00217 104*      P4 = P(IA,IH)
00218 105*      P4 = P(IA,IH)
00219 106*      P4 = P(IA,IH)
00220 107*      P4 = P(IA,IH)
00221 108*      P4 = P(IA,IH)
00222 109*      P4 = P(IA,IH)

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***** INTER4 *****
00223 83*
00224 84*
00225 85*
00226 86*
00230 87*
00232 88*
00233 89*
00234 90*
00235 91*
00235 92*
00236 93*
00240 94*
00241 95*
00243 96*
00244 97*
00245 98*
00246 99*
00246 100*
00247 101*
00250 102*
00251 103*
00251 104*
00252 105*
00252 106*
00253 107*
00254 108*
00254 109*
00255 110*
00256 111*
00256 112*
00257 113*
00260 114*
00260 115*
00261 116*
00262 117*
00262 118*
00263 119*
00264 120*
00265 121*

D4 = D(IA,IH)
T4 = T(IA,IH)
I1=IA
IF (I1.GE.9) I1=I1-4
IF (MOD(I1,4).EQ.0) I1=I1-1
DPX=P(I1+1,IH)-P(I1,IH) Q.....DP/DX FOR GEOSTROPHIC WIND EQUATIONS IN 47400
DPY=P(I1+4,IH)-P(I1,IH) Q.....DP/DY FOR GEOSTROPHIC WIND EQUATIONS IN 47500
DTX = T(I1+1,IH) - T(I1,IH) Q.....DT/DX FOR THERMAL WIND EQUATIONS IN 47600
DTY = T(I1+4,IH) - T(I1,IH) Q.....DT/DY FOR THERMAL WIND EQUATIONS IN 47700
C.....INDICATES ERROR BECAUSE OF POSITION OUTSIDE 16 POINT GRID
WRITE (6,30)
RETURN
220 WRITE(6,30)
P4=0.
T4=0.
RETURN
C.....INTERPOLZTION FOR POSITION INSIDE 16 POINT GRID OR POLAR GRID
300 CALL INTLL(P,IA,IB,IC,ID,IP4,GLAT,GLON,CLAT,CLON,IH)
CALL INTLL(D,IA,IB,IC,ID,D4,GLAT,GLON,CLAT,CLON,IH)
CALL INTLL(T,IA,IB,IC,ID,T4,GLAT,GLON,CLAT,CLON,IH)
C.....RELATIVE LONGITUDE DISPLACEMENT FROM REFERENCE POSITION (IA)
DLOH = (CLON - GLON(IA))/(GLON(IB) - GLON(IA))
C.....RELATIVE LATITUDE DISPLACEMENT FROM REFERENCE POSITION(IA)
DLAT = (CLAT - GLAT(IA))/(GLAT(IC) - GLAT(IA))
DPX=P(IB,IH)-P(IA,IH)
C.....DP/DX FOR GEOSTROPHIC WIND EQUATIONS
DPX = DPX + (P(ID,IH) - P(IC,IH) - DPX)*DLAT
DTX = T(IB,IH) - T(IA,IH)
C.....DT/DX FOR THERMAL WIND EQUATIONS
DTX = DTX + (T(ID,IH) - T(IC,IH) - DTX)*DLAT
DPY = P(IC,IH) - P(IA,IH)
C.....DP/DY FOR GEOSTROPHIC WIND EQUATIONS
DPY = DPY + (P(ID,IH) - P(IB,IH) - DPY)*DLON
DTY = T(IC,IH) - T(IA,IH)
C.....DT/DY FOR THERMAL WIND EQUATIONS
DTY = DTY + (T(ID,IH) - T(IB,IH) - DTY)*DLON
RETURN
END
IN406900
IN407000
IN407100
IN407200
IN407300
IN407400
IN407500
IN407600
IN407700
IN407800
IN407900
IN408000
IN408010
IN408020
IN408040
IN408060
IN408080
IN408100
IN408200
IN408300
IN408400
IN408500
IN408600
IN408700
IN408800
IN408900
IN409000
IN409100
IN409200
IN409300
IN409400
IN409500
IN409600
IN409700
IN409800
IN409900
IN410000
IN410100
IN410200

```

END OF COMPILATION: NO DIAGNOSTICS.
 GHGG,P ***** INTLL *****
 QFOR,S PROFAS,INTLL,INTLL
 FOR S11E-02/04/74-18:52:51 (0,)

SUBROUTINE INTLL ENTRY POINT 000132

STORAGE USED: CODE(1) 000154; DATA(0) 000251; BLANK COMMON(2) 000000

EXTERNAL REFERENCES (BLOCK, NAME)

0003 NERR35

***** INTLL *****

STORAGE ASSIGNMENT (BLOCK, TYPE, RELATIVE LOCATION, NAME)

0001 000053 20L 0000 000002 IN-IP\$ 0000 R 000000 X 0000 R 000001 Y

```

00101 1* SUBROUTINE INTLL(F,IA,IB,IC,ID,FLL,GLAT,GLON,CLAT,CLON,IH)
00101 2* INTERPOLATES FUNCTION (ARRAY) F FROM VALUES OF GLAT AND GLON AT
00101 3* INDEX VALUES IA, IB, IC, ID TO OUTPUT VALUE FLL AT HEIGHT IH
00101 4* AND POSITION CLAT, CLON
00101 5* DIMENSION F(16,26),GLAT(16),GLON(16)
00101 6* .....NORMALIZES LONGITUDE DISPLACEMENT
00101 7* IF(F(IA,IH)*F(IB,IH)*F(IC,IH)*F(ID,IH)) 20,10,20
00101 8* FLL=0.
00101 9* RETURN
00101 10* 20 X=(CLON-GLON(IB))/(GLON(IA)-GLON(IB))
00101 11* .....NORMALIZES LATITUDE DISPLACEMENT
00101 12* Y=(CLAT-GLAT(IA))/(GLAT(IC)-GLAT(IA))
00101 13* C.....TWO DIMENSIONAL INTERPOLATION
00101 14* FLL=F(IA,IH)*X*(F(ID,IH)-F(IB,IH))*Y*(F(IA,IH)-F(IB,IH))*X
00101 15* 1 +F(IC,IH)-F(IA,IH)-F(ID,IH)+F(IB,IH))*X*Y
00101 16* RETURN
00101 17* END
INL00100
INL00200
INL00300
INL00400
INL00500
INL00600
INL00630
INL00660
INL00690
INL00700
INL00800
INL00900
INL01000
INL01100
INL01200
INL01300
INL01400

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END OF COMPILATION: NO DIAGNOSTICS.

GHDP,P ***** INTRP4 *****
BFOR,S PROFAS,INTRP4,INTRP4
FOR S1E-02/04/74-18:52:53 (0,)

SUBROUTINE INTRP4 ENTRY POINT 000775

STORAGE USED: CODE(1) 001005; DATA(0) 000112; BLANK COMMON(2) 000000

COMMON BLOCKS:

0003 INT 002037

EXTERNAL REFERENCES (BLOCK, NAME)

0004 ATAN
0005 COS
0006 SORT
0007 SIN
0010 NERR3\$

STORAGE ASSIGNMENT (BLOCK, TYPE, RELATIVE LOCATION, NAME)

0001	000045	1236	0001	000054	1266	0001	000067	1346	0001	000134	1476	0001	000200	1646
0001	000207	1676	0001	000222	1756	0001	000035	20L	0001	000300	2206	0001	000320	2306
0001	000352	2456	0001	000116	25L	0001	000462	2756	0001	000123	30L	0001	000647	3256
0001	000656	3306	0001	000671	3366	0001	000252	38L	0001	000257	50L	0001	000266	55L

***** INTRP4 *****

```

0001 000307 60L 0001 000350 63L 0001 000466 66L 0001 000522 69L
0001 000611 71L 0000 R 000051 A 0000 R 000046 B 0000 R 000047 C
0000 R 000050 DD 0000 R 000020 DEGRAD 0003 R 002027 DLA 0000 R 000047 C
0003 R 002025 DXY 0000 R 000042 E 0000 R 000044 ER 0000 I 000034 ITH 0000 R 002033 DLO
0003 I 002020 IG 0000 C00070 INJPS 0000 I 000034 ITH 0000 I 000027 J 0000 R 000045 E4
0000 I 000026 L 0000 I 000021 LALO 0000 I 000022 L1 0000 I 000023 L2 0000 R 000030 K
0000 R 000036 TH3 0000 R 000032 X 0000 R 000010 XC 0000 R 000024 XL 0000 R 000000 XLL
0000 R 000033 Y 0000 R 000014 YC 0000 R 000025 YL 0000 R 000004 YLL 0000 R 000041 Z
0000 R 000040 ZA 0000 R 000043 Z4
    
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00101 SUBROUTINE INTRP4 (LALON)
00101 C
00101 C SUBROUTINE TO INTERPOLATE VALUES
00101 C
00101 C DIMENSION XLL(4),YLL(4),XC(4),YC(4)
00101 C
00101 C COMMON/INT/D(208,5),IG(5),DXY(2),DLA(4),DLO(4)
00101 C
00101 DEGRAD=3.14159/180.
00101 LALO=IABS(LALON)
00101 L1=LALO/10000
00101 L2=LALO-L1*10000
00101 XL=L1/10.
00101 YL=L2/10.
00101 IF (IG(5)-2) 30,20,10
00101 IF (IG(5)-3) 30,30,50
00101 C
00101 C INTERPOLATE FROM NMC GRID
00101 C
00101 C 20 CONTINUE
00101 DO 25 L=1,26
00101 DO 22 J=1,4
00101 22 IF (D(L,J).LT.0.01) GO TO 25
00101 DO 24 K=1,8
00101 I=(K-1)*26+L
00101 D(I,5)=(1.-DXY(2))*((1.-DXY(1))*D(I,1)+DXY(1)*D(I,2))
00101 1 +DXY(2)*((1.-DXY(1))*D(I,3)+DXY(1)*D(I,4))
00101 C
00101 25 CONTINUE
00101 RETURN
00101 C
00101 C INTERPOLATE FROM EQUATION FOR SOUTHERN HEMISPHERE GRID
00101 C
00101 C 30 CONTINUE
00101 DO 32 J=1,2
00101 XLL(J)=DLA(J)
00101 YLL(J)=DLO(J)
00101 IF ((YL.GE.355.) .AND. (YLL(J).LT.0.01)) YLL(J)=360.
00101 C
00101 32 CONTINUE
00101 X=(YLL(1)-YL)/5.
00101 Y=(XLL(1)-X)/5.
00101 IF (IG(5).EQ.3) Y=-Y
00101 DO 38 L=1,26
00101 DO 36 J=1,4
    
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REPRODUCIBILITY OF THE ORIGINAL PAGE IS POOR

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***** INTRP4 *****
00171 45* 36 IF (D(L,J).LT.0.01) GO TO 3R
00174 46* DO 37 K=1,8
00177 47* I=(K-1)*26+L
00200 48* D(I,5)=D(I,1)+X*(D(I,2)-D(I,1))+Y*(D(I,3)-D(I,1))+X*Y*
00201 49* 1 D(I,4)-D(I,3)-D(I,2)+D(I,1)
00203 50* 37 CONTINUE
00205 51* 38 CONTINUE
00205 52* RETURN
00205 53*
00205 54* C
00205 55* C INTERPOLATE FROM ACROSS GRIDS
00206 56*
00207 57* 50 CONTINUE
00211 58* IF (IG(5).NE.1133) GO TO 55
00212 59* IG(5)=3
00213 60* GO TO 30
00214 61* 55 CONTINUE
00216 62* IF (IG(5).NE.333) GO TO 60
00217 63* DLO(1)=(DLO(2)+DLO(3))/2.
00222 64* DO 52 I=1,208
00224 65* DLA(4)=DLA(3)
00225 66* DLO(4)=DLO(3)
00226 67* 60 CONTINUE
00227 68* DO 62 I=1,4
00232 69* XLL(I)=DLA(I)
00233 70* YLL(I)=DLO(I)
00234 71* IF ((YL.GT.350.).AND.(YLL(I).LT.0.01)) YLL(I)=360.
00236 72* 62 CONTINUE
00240 73* ITH=0
00241 74* Y=YLL(1)-YL
00242 75* Y=XL-XLL(1)
00243 76* 63 CONTINUE
00244 77* DO 65 I=2,4
00247 78* XC(I)=YLL(1)-YLL(I)
00250 79* YC(I)=XLL(1)-XLL(I)
00252 80* TH2=3.14159/4
00253 81* TH3=3.14159/4
00254 82* IF (ABS(XC(2)).GT.0.01) TH2=ATAN(YC(2)/XC(2))
00256 83* IF (ABS(YC(3)).GT.0.01) TH3=ATAN(XC(3)/YC(3))
00260 84* IF (XC(2).LT.0.) TH2=3.14159+TH2
00262 85* IF (XC(3).LT.0.) TH3=3.14159+TH3
00264 86* DNN=COS(TH2+TH3)
00265 87* IF (ABS(DNN).GT.0.001) GO TO 66
00267 88* ITH=ITH+1
00270 89* IF (ITH.EQ.2) GO TO 66
00272 90* XLL(3)=XLL(4)
00273 91* YLL(3)=YLL(4)
00274 92* DO 61 I=1,208
00277 93* 61 D(I,3)=D(I,4)
00301 94* GO TO 63
00302 95* 66 CONTINUE
00303 96* ZA=SQRT(XC(2)**2+YC(2)**2)
00304 97* IF (ITH.LT.2) GO TO 69
00306 98* Z=SQRT(X**2+Y**2)
00307 99* E=0.
00310 100* Z4=0.
00311 101* GO TO 71

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```

***** INTRP4 *****
00312 102* 69 CONTINUE
00313 103* EB=SQR(XC(3)**2+YC(3)**2)
00314 104* Z4=(XC(4)*COS(TH3)-YC(4)*SIN(TH3))/DNN
00315 105* E4=(YC(4)*COS(TH2)-XC(4)*SIN(TH2))/DNN
00316 106* Z=(X*COS(TH3)-Y*SIN(TH3))/DNN
00317 107* E=(Y*COS(TH2)-X*SIN(TH2))/DNN
00320 108* B=0.
00321 109* C=0.
00322 110* DD=0.
C
00323 111* 71 CONTINUE
00324 112* DO 70 L=1,26
00325 113* DO 68 J=1,4
00327 114* 68 IF (D(L,J).LT.0.01) GO TO 70
00332 115* DO 67 K=1,8
00335 116* I=(K-1)*26+L
00340 117* A=D(I,1)
00341 118* IF (ZA.GT.0.01) B=(D(I,2)-D(I,1))/ZA
00342 119* IF (EB.GT.0.01) C=(D(I,3)-D(I,1))/EB
00344 120* IF ((ABS(Z4).GT.0.01).AND.(ABS(E4).GT.0.01))
00346 121* 1 DD=(D(I,4)-A-B*Z4-C*E4)/(Z4*E4)
00348 122* D(I,5)=A+B*Z4+C*E4+DD*Z4
00350 123* 67 CONTINUE
00351 124* 70 CONTINUE
00353 125* RETURN
00355 126* END
00356 127*

```

END OF COMPILATION: NO DIAGNOSTICS.
 GHDG,P ***** INTRUV *****
 DEOR,S PROFAS,INTRUV,INTRUV
 FOR S11E-02/04/74-18:52:58 (0,)

SUBROUTINE INTRUV ENTRY POINT 000334

STORAGE USED: CODE(1) 000361; DATA(0) 000037; BLANK COMMON(2) 000000

EXTERNAL REFERENCES (BLOCK, NAME)

0003 INTERW
 0004 NERR\$

STORAGE ASSIGNMENT	(BLOCK, TYPE, RELATIVE LOCATION, NAME)
0001 000150 10L	0001 000157 20L
0000 000021 INJ\$	0000 I 000001 IP
0000 R 000005 PHI2	0000 R 000010 U1
0000 R 000006 Z1	0000 R 000007 Z2
	0001 000174 30L
	0000 I 000002 J
	0000 R 000012 U2
	0001 000,03 40L
	0000 I 000,03 JP
	0000 R 000011 V1
	0000 I 000000 I
	0000 R 000004 PHI1
	0000 R 000013 V2

00101 1* SUBROUTINE INTRUV(UR,VR,H,PHI,SUF,SVH) INV00100

```

***** INTRUV *****
00101 2*-
00101 3* C.....FINDS RANDOM WIND STANDARD DEVIATION AT HEIGHT H (KM), LATITUDE
00103 4* C PHI (DEGREES), FROM UR AND VR ARRAYS
00103 5* C DIMENSION UR(25,10),VR(25,10)
00104 6* C.....I - LOWER HEIGHT INDEX
00106 7* IF (H.LI.95.) I = 1 + INT(H) / 5
00110 8* IF (H.GE.95.) I=19+(INT(H)-90)/20
00112 9* IF (I.GT.25) I = 25
00113 10* IP=I+1 @.....UPPER HEIGHT INDEX
00115 11* J=INT((PHI+110.)/20 @.....LOWER LATITUDE INDEX
00116 12* JPE=J+1 @.....UPPER LATITUDE INDEX
00117 13* IF (JP.GT.10) JP=10
00117 14* C.....PHI1 - LOWER LATITUDE FOR UR AND VR ARRAY VALUES
00121 15* C.....PHI2 - UPPER LATITUDE FOR UR AND VR ARRAY VALUES
00121 16* PHI1=-110.+20.*J
00122 17* PHI2=-110.+20.*JP
00123 18* IF (I.GT.19) GO TO 10
00125 19* Z1=5.*(I-1) @.....LOWER HEIGHT FOR UR AND VR ARRAY VALUES
00126 20* GO TO 20
00127 21* Z1=20.*(I-15)
00130 22* IF (IP.GT.10) GO TO 30
00132 23* Z2=5.*(IP-1) @.....UPPER HEIGHT FOR UR AND VR ARRAY VALUES
00133 24* GO TO 40
00134 25* Z0 Z2 = 20. * (IP - 15)
00135 26* 40 CALL INTERW(UR(I,J),VR(I,J),PHI1,UR(I,JP),VR(I,JP),PHI2,U1,V1,
00135 27* $PHI) @.....INTERPOLATE ON LATITUDE AT LOWER HEIGHT
00136 28* CALL INTERW(UR(IP,J),VR(IP,J),PHI1,UR(IP,JP),VR(IP,JP),PHI2,U2,V2,
00136 29* $PHI) @.....INTERPOLATE ON LATITUDE AT UPPER HEIGHT
00137 30* CALL INTERW(U1,V1,Z1,U2,V2,Z2,$UH,$VH,$H) @.....INTERPOLATE ON HEIGHT
00140 31* RETURN
00141 32* END

```

END OF COMPILATION: NO DIAGNOSTICS.

RHDG,P ***** JAC *****
 GFOR,S PROFAS,JAC,JAC
 FOR S11E=02/04/74-18:53:02 (0,)

SUBROUTINE JAC ENTRY POINT 002062

STORAGE USED: CODE(1) 002131; DATA(0) 000227; BLANK COMMON(2) 000000

COMMON BLOCKS:

0003 IOTEMP 000050
 0004 COMJAC 000010

EXTERNAL REFERENCES (BLOCK, NAME)

0005 EXP
 0006 ALOG10
 0007 XPRR
 0010 ATAN
 0011 NERR3\$

***** JAC *****

STORAGE ASSIGNMENT (BLOCK, TYPE, RELATIVE LOCATION, NAME)

0001	000360	1666	0001	001156	2760	0001	001310	3236	0001	001336	3326	0001	000623	40L				
0001	001676	4166	0001	001413	48L	0001	001042	5L	0001	001117	51L	0001	001221	52L				
0001	000672	55L	0001	000753	60L	0001	001535	60L	0001	001602	62L	0001	002026	64L				
0001	000151	70L	0001	000334	74L	0001	000500	75L	0001	000511	76L	0001	001132	81L				
0001	001251	83L	0001	001300	84L	0001	001405	90L	0001	001752	91L	0001	001770	95L				
0000	R	000057	A	0000	R	000100	AH	0000	R	000101	AHE	0000	R	000000	ALPHA			
0000	R	000077	AN	0000	R	000102	AO	0000	R	000103	AP	0000	R	000040	AV			
0000	R	000111	AL	0000	R	000047	A2	0000	R	000073	CUR	0000	R	000056	D			
0000	R	000004	DD	0000	R	000067	DEL	0000	R	000014	DI	0000	R	000031	DIT			
0000	R	000075	DL	0003	R	000044	DX	0004	R	000004	DZ	0000	R	000113	DI			
0000	R	000006	EI	0004	R	000007	EM	0000	R	000051	EPS	0000	R	000112	FAI			
0000	R	000061	FD	0000	R	000114	FD1	0000	R	000045	FK	0000	R	000116	FX1			
0003	000036	F10	0003	I	000070	I	0003	000031	G	0003	000031	H	0003	000045	HL			
0003	000026	H1	0000	I	000001	IOTEM2	0003	000022	IUG	0003	000025	IYR	0000	I	000050	M		
0003	000000	IOTEM1	0003	000023	MIN	0000	I	000063	N	0000	I	000062	NPT	0003	000003	NMCOP		
0003	000042	MIN	0003	000010	NSAME	0000	R	000076	PAR	0003	000007	PHI	0003	000034	PHIR			
0003	000043	NMORE	0003	000027	PHIR	0000	R	000064	PREV	0000	R	000043	GA	0000	R	000044	GHE	
0003	000006	PHI1	0003	000042	GC2	0000	R	000037	GO	0000	R	000074	R	0000	R	000012	RD1	
0000	R	000041	QN	0003	R	000011	RP1	0003	CJ0013	RT1	0003	000017	RU1	0003	000020	RV1		
0003	000032	RI	0004	000002	SDA	0003	000015	SD1	0003	000016	ST1	0004	000003	SHA	0000	R	000065	SONE
0000	R	000117	S	0000	R	000066	ST#0	0003	000030	THETIR	0003	000021	SU1	0000	R	000022	SV1	
0003	000014	SP1	-0003	000035	THETR	0000	R	000053	T4	0003	000046	TX	0000	R	000106	T23		
0004	R	000006	T	0000	R	000054	T3	0003	000005	XMJD	0003	000046	VL	0000	R	000071	X	
0000	R	000052	T1	0004	R	000001	XLONG	0003	000105	Z3	0000	R	000115	X1				
0004	000000	XLAT	0000	R	000055	Z2												
0000	R	000107	ZM3															

00101	1*	SUBROUTINE	JAC(Z1Z2,DENS)	JAC00100
00103	2*	COMMON/IOTEMP/IOTEM1	IOTEM2,IUG,NMCOP,DD,XMJD,PHI1,PHI,	JAC00200
00103	3*	NSAME,RP1,	ROI, RT1, SPI, SDI, STI, RUI, RV1, SU1, SV1,	JAC00300
00103	4*	S MN, IDA, IYR, HI,	PHIR,THETR,6,RI,H,PHIR,THETR,F10,F10B,AP,	JAC00400
00103	5*	IMR,MIN,NMORE,DX,HL,	VL,LDZ	JAC00500
00104	6*	COMMON/COMJAC/XLAT,XLONG,	SDA,SHA,DY,Y,T,EM	JAC00600
00105	7*	DIMENSION ALPHA(6),EI(6),	DI(6), B(7),DIT(6)	JAC00700
00106	8*	GG = 100.		JAC00800
00107	9*	DATA ALPHA/0.0,0.0,0.0,	0.0,0.0,-0.38,0.0/	JAC00900
00111	10*	DATA EI/28.0134,31.9988,	15.9994,39.948,4.0026,1.00797/	JAC01000
00113	11*	DATA B/28.15204,-0.085586,	1.284E-04,-1.0056E-05,-1.021E-05,	JAC01100
00113	12*	11.5044E-06,9.9826E-08/		JAC01200
00115	13*	AV=6.02257E23		JAC01300
00116	14*	GN= .78110		JAC01400
00117	15*	Q02=-.20955		JAC01500
00120	16*	GA= .009343		JAC01600
00121	17*	GHE = 1.289E-5		JAC01700
00122	18*	FK=8.31432		JAC01800
00122	19*	TEMPERATURE AT Z = 125	KM, EO. 9	JAC01900
00122	20*			JAC02000
00122	21*			JAC02100
00122	22*			JAC02200
00123	23*	TX=44.3807+0.2385*T	-392.8792*EXP(--0.021357*T)	JAC02300
00124	24*	A2=2.*(T-TX)/3.14159265		JAC02400
00124	25*			JAC02500

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00125 *****
00126 26*
00127 27*
00128 28*
00129 29*
00130 30*
00131 31*
00132 32*
00133 33*
00134 34*
00135 35*
00136 36*
00137 37*
00138 38*
00139 39*
00140 40*
00141 41*
00142 42*
00143 43*
00144 44*
00145 45*
00146 46*
00147 47*
00148 48*
00149 49*
00150 50*
00151 51*
00152 52*
00153 53*
00154 54*
00155 55*
00156 56*
00157 57*
00158 58*
00159 59*
00160 60*
00161 61*
00162 62*
00163 63*
00164 64*
00165 65*
00166 66*
00167 67*
00168 68*
00169 69*
00170 70*
00171 71*
00172 72*
00173 73*
00174 74*
00175 75*
00176 76*
00177 77*
00178 78*
00179 79*
00180 80*
00181 81*
00182 82*

)IT(6)=0.
4=10
EPS=.0001
C TEMPERATURE FOR 90<Z<125, EQ. 10
C
C T1=1.9*(TX-183.)/35.
T4=3.*(TX-183.-2.*T1*35./3.)/(35.**4)
T3=-T1/(3.**35.**2)+4.*T4*35./3.
T2=TX+T1*(Z-125.)/3+T3*(Z-125.)*3+T4*(Z-125.)*4
IF (Z-105.) 43,43,40
C MEAN MOLECULAR WEIGHT FOR 90<Z<105, EQ. 1
C
C 43 Z2 = Z - 00
EM=B(1)+B(2)*Z2+B(3)*Z2**2+R(4)*Z2**3+B(5)*Z2**4+B(6)*Z2**5
1+R(7)*Z2**6
)EZ
C CONTINUE
70
C INTEGRATION OF EQ. 5 FOR DENSITY BETWEEN 90<Z<105
C
C A=9J.
FA=B(1)+B(2)*(A-00)+B(3)*(A-00)**2+B(4)*(A-00)**3+B(5)*(A-00)**4
1+B(6)*(A-00)**5 +B(7)*(A-00)**6
FA=FA*9.80665/((1.+A/6.356766E+3)**2)
FA=FA/(TX+T1*(A-125.)/3+T3*(A-125.)*3 +T4*(A-125.)*4)
FD=B(1)+B(2)*(D-00)+R(3)*(D-00)**2+R(4)*(D-00)**3+B(5)*(D-00)**4
1+B(6)*(D-00)**5 +B(7)*(D-00)**6
DFD=9.80665/((1.+D/6.356766E+3)**2)
DF=FU/(TX+T1*(D-125.)/3+T3*(D-125.)*3 +T4*(D-125.)*4)
SR04, SIMPSONS RULE QUADRATURE - G.F.KUNCIR
DEFINITIONS -
A = LOWER LIMIT OF INTEGRATION
D = UPPER LIMIT OF INTEGRATION
FUNC = INTEGRAND FUNCTION SUBPROGRAM
EPS = RELATIVE ERROR OF CONVERGENCE CRITERION
M = MAXIMUM NUMBER OF INTEGRATIONS
R = RESULT OF INTEGRATION
N = NUMBER OF INTEGRATIONS9RIQRID TO FIND R
NINT = 1
NE0
PREV=0.
SOME=(D-A)*(FA+FD)/2.
IF (N=N1)
NINT = 2 * NINT
IF (N=N) 72,72,75
STWO=0.
DEL=(D-A)/FLOAT(NINT)
DO 73 I=1,NINT,2
X=A+DEL*FLOAT(I)
FX=B(1)+B(2)*(X-00)+B(3)*(X-00)**2+R(4)*(X-00)**3+B(5)*(X-00)**4
1+R(6)*(X-00)**5 +B(7)*(X-00)**6
FX=FX*9.80665/((1.+X/6.356766E+3)**2)
FX=FX/(TX+T1*(X-125.)/3+T3*(X-125.)*3 +T4*(X-125.)*4)
STWO=STWO+FX
73

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REPRODUCIBILITY OF THE ORIGINAL PAGE IS POOR

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***** JAC *****
00176 83* CUR=SOME+*,DEL*STW0
00177 84* IF (EPS*ABS(CUR)-ARS*(CUR-PREV)) 74,75,75
00202 85* PREV=CUR
00203 86* SOME=(SOME+CUR)/4.
00204 87* SO TO 71
00205 88* RECUR/3
00206 89* IF (Z-105.) 44,76,44
00211 90* IF (C-105.) 76,55,76
00211 91*
00211 92* C DENSITY FOR 90<Z<105
00211 93* C
00214 94* C
00215 95* DENS=3.46E-9*183.*EM*EXP(-R/FK)/(TZ*28.878)
00216 96* DL=ALOG10(DENS)
00217 97* PAR=AV*DENS/EM
00220 98* AN=ALOG10(QH*EM*PAR/28.96)
00221 99* AA=ALOG10(OA*EM*PAR/28.96)
00222 100* AHE=:LOG10(QHE*EM*PAR/28.96)
00223 101* AOE=:LOG10(2.*PAR*(1.-EM/28.96))
00224 102* A02=:ALOG10(PAR*(EM*(1.+002)/28.96-1.))
00225 103* AHE=0.
00225 104* RETURN
00225 105* C TEMPERATURE AND MEAN MOLECULAR WEIGHT AT Z=105 KM
00225 106* C
00226 107* 40 Z3=105.
00227 108* TZ3=TX+T1*(Z3-125.)+TZ*(Z3-125)**3+T4*(Z3-125)**4
00230 109* ZH3=B(1)+B(2)* 5.+B(3)* 25.+B(4)* 125.+B(5)* 5.**4.+B(6)* 5.**5.
00230 110* 1+B(7)* 5.**6.
00231 111* D=105.
00232 112* GO TO 70
00232 113* C DENSITY AT Z=105 KM
00232 114* C
00232 115* C
00233 116* DENI=3.46E-9*183.*ZM3*EXP(-R/FK)/(TZ3*28.878)
00234 117* PAR=AV*DENI/ZM3
00235 118* DI(1)=QN*ZM3*PAR/28.96
00236 119* DI(2)=PAR*(ZM3*(1.+002)/28.96-1.)
00237 120* DI(3)=2.*PAR*(1.-ZM3/28.96)
00240 121* DI(4)=QA*ZM3*PAR/28.96
00241 122* DI(5)=QHE*ZM3*PAR/28.96
00242 123* IF (Z-125.) 56,56,90
00245 124* CONTINUE
00245 125* C
00245 126* C INTEGRATION OF EQ. 6 FOR DENSITY ABOVE 105 KM
00246 127* C
00246 128* A1=105.
00247 129* FAI=9.80665/((1.+A1/6.356766E+3)**2)
00250 130* FAI=FAI/(TX+T1*(A1-125.)+TZ*(A1-125.))**3+T4*(A1-125.))**4)
00251 131* D1=Z
00252 132* FDI=9.80665/((1.+D1/6.356766E+3)**2)
00253 133* IF (D1-125.) 45,45,50
00256 134* FDI=FDI/(TX+T1*(D1-125.)+TZ*(D1-125.))**3+T4*(D1-125.))**4)
00257 135* GO TO 51
00260 136* FDI=FDI/(TX+A2*ATAN(T1*(D1-125.)*(1.+4.5E-6*(D1-125.))**2.5)/A2)
00261 137* TZ=TX+A2*ATAN(T1*(Z-125.)*(1.+4.5E-6*(Z-125.))**2.5)/A2)
00262 138* N=0
00263 139* NINT = 1

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REPRODUCIBILITY OF THE ORIGINAL PAGE IS POOR

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***** JAC *****
00264 140*
00265 141*
00266 142*
00267 143*
00272 144*
00273 145*
00274 146*
00275 147*
00300 148*
00301 149*
00302 150*
00305 151*
00306 152*
00307 153*
00310 154*
00312 155*
00313 156*
00316 157*
00317 158*
00320 159*
00321 160*
00321 161*
00321 162*
00321 163*
00322 164*
00325 165*
00326 166*
00330 167*
00331 168*
00334 169*
00335 170*
00335 171*
00335 172*
00335 173*
00337 174*
00337 175*
00337 176*
00337 177*
00340 178*
00341 179*
00342 180*
00343 181*
00344 182*
00345 183*
00346 184*
00351 185*
00352 186*
00353 187*
00354 188*
00355 189*
00356 190*
00357 191*
00360 192*
00361 193*
00361 194*
00361 195*
00361 196*

PREV=0
SONE=(D1-A1)*(FA1+FC1)/2.
NEN+1
IF (N-M) 82,82,85
NINT = 2 * NINT
STWO=0.
DEL=(D1-A1)/FLOAT(NINT)
DO 83 I=1,NINT,2
X1=A1+DEL*FLOAT(I)
FX1=9.80665/(1.+X1/6.356766F+3)*2)
IF(X1-125.) 46,45,52
46 FX1=FX1/(TX+TI*(X1-125.))+T3*(X1-125.):**3+T4*(X1-125.):**4)
30 TO 83
FX1=FX1/(TX+A2*ATAN(T1*(X1-125.))*(1.+4.5E-6*(X1-125.):**2.5)/A2))
STWO=STWO+FX1
CUR=SONE+4.*DEL*STWO
IF (EPS*ABS(CUR)-ABS(CUR-PREV)) 84,85,85
PREV=CUR
SONE=(SONE+CUR)/4.
GO TO 81
RECUR/3.
DENSITY ABOVE 105 KM
DO 41 I=1,5
DIT(I)=DI(I)*(TZ3/TZ)**(1.+ALPHA(I))*EXP(-EI(I)*R/FK)
41 CONTINUE
DENS=0
DENS=DENS+EI(I)*DIT(I)/AV
CONTINUE
MEAN MOLECULAR WEIGHT FOR Z>105 KM
EM=DENS*AV/(DIT(1)+DIT(2)+DIT(3)+DIT(4)+DIT(5)+DIT(6))
LOG DENSITY
DL=ALOG10(DENS)
AN=ALOG10(DIT(1))
AO2=ALOG10(DIT(2))
AO=ALOG10(DIT(3))
AA=ALOG10(DIT(4))
AHE=ALOG10(DIT(5))
IF(Z-500.) 47,48,48
47 DIT(6)=10.**(-6)
48 AH=ALOG10(DIT(6))
AN=AMAX1(-0., AN)
AO2=AMAX1(-0., AO2)
AO=AMAX1(-0., AO)
AA=AMAX1(-0., AA)
AHE=AMAX1(-0., AHE)
AH=AMAX1(-0., AH)
RETURN
C TEMPERATURE AND DENSITY AT Z=500 KM
C
C

```

```

***** JAC *****
00362 197* 90 S=IX+42*ATAN(T1*375.*(1.+4.5E-6*375.**2.5)/A2)
00363 198* JI(P)=10.**((73.13-30.4*ALOG10(S)+5.5*ALOG10(S))*ALOG10(S))
00364 199* A1=500.
00365 200* IF(Z=500.) 49,60,60
C
00365 201* C INTEGRATION OF EQ. 6 FOR DENSITY FOR Z>125 KM
C
00365 202* C
00365 203*
00370 204* 49 A1=Z
00371 205* 60 FA1=9.80665/((1.+A1/6.356766E+3)**2)
00372 206* FAI=FA1/(TX+A2*ATAN(T1*(A1-125.))*(1.+4.5E-6*(A1-125.))**2.5)/A2)
00373 207* JI=Z
00374 208* IF(Z=500.) 61,62,62
00377 209* 61 JI=500.
00400 210* 62 FDI=9.80665/((1.+J1/6.356766E+3)**2)
00401 211* FDI=FD1/(TX+A2*ATAN(T1*(D1-125.))*(1.+4.5E-6*(D1-125.))**2.5)/A2)
00402 212* H=0
00403 213* NINT = 1
00404 214* PREV=0
00405 215* SONE=(D1-A1)*(FA1+FD1)/2.
00406 216* NEN+1
00407 217* IF (N-M) 92,92,95
00412 218* NINT = 2 * NINT
00413 219* STWO=0.
00414 220* DEL=(D1-A1)/FLOAT(NINT)
00415 221* DO 93 I=1,NINT,2
00420 222* XI=A1+DEL*FLOAT(I)
00421 223* FXI=9.80665/((1.+XI/6.356766E+3)**2)
00422 224* FXI=FXI/(TX+A2*ATAN(T1*(XI-125.))*(1.+4.5E-6*(XI-125.))**2.5)/A2)
00423 225* STWO=STWO+FXI
00425 226* CUR=SONE+4.*DEL*STWO
00426 227* IF (EPS*ABS(CUR)-ABS(CUR-PREV)) 94,95,95
00431 228* 94 PREV=CUR
00432 229* SONE=(SONE+CUR)/4.
00433 230* GO TO 91
00434 231* RECUR/5.
C
00434 232* C TEMPERATURE AT Z>500 KM
C
00434 233* C
00434 234*
00435 235* TZ=TX+A2*ATAN(T1*(Z-125.))*(1.+4.5E-6*(Z-125.))**2.5)/A2)
00436 236* IF(Z=500.) 63,64,64
00441 237* 63 R=-R
C
00441 238* C DENSITY OF HYDROGEN FOR Z>500 KM
C
00441 239* C
00441 240*
00442 241* 64 DIT(6)=DI(6)*(S/TZ)*EXP(-EI(6)*R/FK)
00443 242* GO TO 56
00444 243* END

```

END OF COMPILATION: NO DIAGNOSTICS.
 @HDG,P ***** JACCH *****
 @FOR,S PROFAS,JACCH,JACCH
 FOR 511E-02/04/74-18:53:09 (0)

SUBROUTINE JACCH ENTRY POINT 000244

***** JACCH *****
 STORAGE USED: CODE(1) 000302; DATA(0) 000052; BLANK COMMON(2) 000000

COMMON BLOCKS:

0003 COMJAC 000010
 0004 IOTEMP 000050

EXTERNAL REFERENCES (BLOCK, NAME)

0005 TIME
 0006 TINF
 0007 JAC
 0010 SIN
 0011 EXP
 0012 SGRT
 0013 PERR35

STORAGE ASSIGNMENT (BLOCK, TYPE, RELATIVE LOCATION, NAME)

0001	000131	150L	0001	000160	250L	0001	000224	300L	0001	00017	SOL	000021	75L				
0001	000063	80L	0001	000074	90L	0004	000040	AP	0004	00034	CLAT	000035	CLON				
0000	R	000002	C1	0000	R	000003	C2	0004	R	00006	DEM	000005	DLRHO				
0000	R	000010	DIH	0004	000044	DX	0003	000004	DY	0004	00047	EM					
0004	000026	H1	0004	000037	F10B	0004	000031	G	0004	00033	H	000045	HL				
0004	000042	MIN	0004	000024	ICA	0004	000041	IHR	0000	00042	INJPS	000000	IOTEM1				
0004	000006	PHI1	0004	000002	IUG	0004	I	000025	IYR	0000	I	000023	M				
0004	000011	RP1	0004	000003	NMCOP	0004	000043	NMORE	0004	00010	NSAME	000007	PHI				
0004	000015	SD1	0004	000027	PHIR	0004	R	000005	R	0004	00012	RI	000032	SDA			
0004	000022	SV1	0004	000013	RT1	0004	000017	RU1	0004	00020	RV1	000002	SDA				
0003	R	000001	XLONG	0003	000003	SHA	0004	000014	SPI	0004	00016	ST1	000021	SUI			
				0003	R	000006	T	0004	000030	THET1R	0004	00046	VL	0003	R	000000	XLAT
				0004		000005	XMJJD	0000	R	000000	YDA	0000	R	000004	Z90		

00101	1*	SUBROUTINE JACCH(Z,PHIR,THET,PH,PH,TH)	JAH00100
00103	2*	COMMON/COMJAC/XLAT,XLONG,SDA,SHA,DY,R,T,EM	JAH00200
00104	3*	COMMON/IOTEMP/IOTEM1,IOTEM2,IUG,NMCOP,DD,XMJD,PHI1,PHI,	JAH00300
00104	4*	NSAME,RP1, RD1, RT1, SPI, SD1, ST1, RUI, RV1, SUI, SV1, JAH00400	
00104	5*	\$ M , IDA, IYR, H1, PHIR,THET1R,G,RI,H,CLAT,CLON ,F10,F10B,AP,	JAH00500
00104	6*	THR,MIN,NMORE,DX,HL,VL,DZ	JAH00600
00104	7*		JAH00700
00104	8*	JACCH CALCULATES THE PRESSURE, DENSITY, AND TEMPERATURE AT A	JAH00800
00104	9*	POINT IN SPACE ABOVE 90 KM FOR A PARTICULAR TIME	JAH00900
00104	10*	INPUT	JAH01000
00104	11*	Z = HEIGHT IN KM	JAH01100
00104	12*	PHIR = LATITUDE IN RADIANS	JAH01200
00104	13*	THET = LONGITUDE IN DEGREES	JAH01300
00104	14*	F10 = SOLAR RADIO NOISE FLUX (XE - 22 WATTS/M**2)	JAH01400
00104	15*	F10B = 81-DAY AVERAGE F10	JAH01500
00104	16*	AP = GEOMAGNETIC INDEX	JAH01600
00104	17*	M = MONTH (FOR YEARLY MEAN VARIABLES M IS SET TO 13)	JAH01700
00104	18*	IDA = DAY OF MONTH	JAH01800
00104	19*		JAH01900

```

*****
JAUCH *****
00104 20* C IYR = YEAR
00104 21* C IHR = HOUR OF DAY (UNIVERSAL TIME)
00104 22* C MIN = MINUTE (UNIVERSAL TIME)
00104 23* C XNJD = MEAN JULIAN DAY (SET EQUAL TO ZERO FOR ANNUAL MEAN)
00104 24* C JD = DAY NUMBER WITH RESPECT TO JAN 0 OF YEAR IYR
00104 25* C OUTPUT
00104 26* C PH = PRESSURE IN UNITS OF NT/M**2
00104 27* C DH = DENSITY IN UNITS OF KG/M**3
00104 28* C TH = TEMPERATURE IN KELVIN DEGREES
00104 29* C JD = DAY NUMBER WITH RESPECT TO JAN 1 OF YEAR IYR
00104 30* C
00104 31* C REPLACEMENT OF SUBROUTINE VARIABLES TO INSURE NO CHANGES IN THEM
00104 32* C
00104 33* C
00104 34* C
00105 35* C
00106 36* C
00107 37* C
00110 38* C
00110 39* C
00110 40* C
00111 41* C
00112 42* C
00112 43* C
00112 44* C
00113 45* C
00114 46* C
00115 47* C
00115 48* C
00115 49* C
00115 50* C
00115 51* C
00116 52* C
00117 53* C
00121 54* C
00122 55* C
00123 56* C
00125 57* C
00126 58* C
00131 59* C
00132 60* C
00133 61* C
00133 62* C
00133 63* C
00133 64* C
00134 65* C
00135 66* C
00136 67* C
00136 68* C
00136 69* C
00136 70* C
00137 71* C
00142 72* C
00143 73* C
00144 74* C
00147 75* C
00150 76* C

75 CALL JAC(Z,TH,DH)
IF (M.EQ.13) GO TO 300
YDA = 365.0
J1 = MOD(IYR,4)
IF (J1.EQ.0) YDA = 366.0
C1 = SIN(1360. / YDA) * 0.0174532925 * (DD + 100.0)
IF (PHIR) 80,70,80
70 C2 = 0.0
80 C2 = (SIN(PHIR) ** 2) * (PHIR / ABS(PHIR))

C DENSITY WITH SEASONAL VARIATIONS
90 Z90 = Z - 90.0
DLR40 = 0.02 * Z90 * EXP(-0.045 * Z90) * C1 * C2
DH = DH * EXP(DLR40)

C MOLECULAR WEIGHT WITH SEASONAL VARIATION
IF (Z - 120.0) 100,100,150
100 EM = EM + 0.006 * Z90 * C1
30 TO 250
150 IF (Z - 230.0) 200,250,250
200 DEM = EXP(-0.02424 * Z90) * (0.0316 * Z90 - 0.0002257 * Z90 * Z90) * Z90 * C1 * 0.5
EM = EM + DEM * C1 * 0.5

```

***** JALCH *****

```

00150 77* C
00150 78* C
00150 79* C
00151 80* TEMPERATURE WITH SEASONAL VARIATIONS
00154 81* 250 IF (Z-260.0) 270,300,300
00155 82* 270 Z110 = Z - 110.0
00155 83* DTH = -2.291753 * Z110 + U.02154336 * Z110*Z110 - 4.1766671E-05 *
00156 84* $ (Z110 ** 3)
00157 85* DTH = EXP(-0.290655 * SQRT(ABS(Z110))) * DTH
00157 86* TH = TH + (DTH * C1 * C2 * TH) / 100.0
00157 87* C
00157 88* C DENSITY IN METRIC UNITS AND PRESSURE CALCULATED
00160 89* 300 DH = DH * 1000.0
00161 90* PH = ((DH * 8.31432 * TH) / EV) * 1000.0
00162 91* RETURN
00163 92* END
    
```

END OF COMPILATION: NO DIAGNOSTICS.

RDG/P ***** NORMAL *****
 @FOR,S PROFAS,NORMAL,NORMAL
 FOR S1E-02/04/74-18:53:12 (0,)

SUBROUTINE NORMAL ENTRY POINT 000062

STORAGE USED: CODE(1) 000070; DATA(0) 000016; BLANK COMMON(2) 000000

EXTERNAL REFERENCES (BLOCK, NAME)

```

0003 RAND
0004 ALOG
0005 SQRT
0006 NERR3$
    
```

STORAGE ASSIGNMENT (BLOCK, TYPE, RELATIVE LOCATION, NAME)

```

0001 000000 50L 0000 000011 INJPS 0000 R 000000 L
0000 R 000001 X 0000 R 000003 XX 0000 R 000002 Y 0003 R 000000 RAND 0000 R 000005 S
    
```

```

00101 1* SUBROUTINE NORMAL (D1,D2)
00101 2* C.....PRODUCES 2 RANDOM NUMBERS, D1, D2, PICKED FROM A NORMAL DIST.
00101 3* C
00103 4* REAL L
00104 5* 50 X = RAND(0)
00105 6* Y = 2*RAND(0) - 1
00106 7* XX = X**2
00107 8* YY = Y**2
00110 9* S = XX + YY
00111 10* IF (S-1) 51,51,50
00114 11* 51 L = SQRT(-2*ALOG(RAND(0)))/S
    
```

```

NOR00100
NOR00200
NOR00300
NOR00400
NOR00500
NOR00600
NOR00700
NOR00800
NOR00900
NOR01000
NOR01100
    
```

NOR01200
NOR01300
NOR01400
NOR01500

***** NORMAL *****

00115 12* D1 = (XX-YY)*L
00116 13* C2 = 2*XY*AL
00117 14* RETURN
00120 15* END

END OF COMPILATION: NO DIAGNOSTICS.
@HDS,P ***** PDTUV *****
@FOR,S PROFAS,PDTUV,PDTUV
FOR S11E-02/04/74-18:53:16 (C1)

SUBROUTINE PDTUV ENTRY POINT 000375

STORAGE USED: CODE(1) 000450; DATA(0) 000062; BLANK COMMON(2) 000000

EXTERNAL REFERENCES (BLOCK, NAME)

0003 NERR3\$

STORAGE ASSIGNMENT (BLOCK, TYPE, RELATIVE LOCATION, NAME)

0001 000031 10L 0001 000037 20L 0001 000041 30L 0000 R 000007 DLAT
0000 I 000005 I 0000 000022 INJPs 0000 I 000006 IP 0000 I 000002 J 0000 R 000003 DLON
0000 I 000000 K 0000 R 000001 XLON 0000 I 000004 JP

00101 1* SUBROUTINE PDTUV (PSP, DSP, TSP, CLAT, CLON, IH, PS, OS, TS,
00101 2* \$ DRY, DRY, DTX, DTY)
00101 3* C.....INTERPOLATES STATIONARY PERTURBATIONS ON LATITUDE AND LONGITUDE
00101 4* C AT HEIGHT IH
00103 5* DIMENSION PSP(8,10,12),DSP(8,10,12),TSP(8,10,12)
00104 6* IF (IH,LT,52) GO TO 10
00106 7* IF (IH,GT,84) GO TO 20
00110 8* K = ((I+4)/8) - 40.....HEIGHT INDEX
00111 9* 30 TO 30
00112 10* 10 K = (IH-20)/10
00113 11* 30 TO 30
00114 12* 20 K = 8
00115 13* 30 XLON = CLON
00116 14* IF (CLON,LT,10.) XLON = 360. + CLON
00120 15* J = INT((XLON + 20.)/30.) @.....LOWER LONGITUDE INDEX
00120 16* C.....DLON = RELATIVE LONGITUDE DEVIATION FROM CORNER REFERENCE LOCATION
00121 17* DLON = (XLON - 30.*J + 20.)/30.
00122 18* JP = J+10.....UPPER LONGITUDE INDEX
00123 19* IF (JP,GT,12) JP=1
00125 20* I = INT((CLAT + 110.)/20.) @.....LOWER LATITUDE INDEX
00126 21* IP = I+1 @.....UPPER LATITUDE INDEX
00127 22* IF (IP,GT,10) IP=10
00127 23* C.....DLAT = RELATIVE LATITUDE DEVIATION FROM CORNER REFERENCE LOCATION
00131 24* DLAT = (CLAT-20.*I + 110.)/20.
00132 25* PSP=PSP(K,I,J)+(PSP(K,IP,J)-PSP(K,I,J))*DLAT+(PSP(K,I,JP)-PSP(K,I,JP)*DLON

***** PJTUV *****

```

00132 26* 1)*DLON*(PSP(K,IP,JP)-PSP(K,I,JP)-PSP(K,IP,JP)+PSP(K,I,J))*DLAT* PDI02600
00132 27* 2)DLON 3).....PRESSURE LAT-LON INTERPOLATION PDI02700
00133 28* )SDSP(K,I,J)+(DSP(K,IP,JP)-DSP(K,I,J))*DLAT*(DSP(K,I,JP)-DSP(K,I,J))*DLAT* I,J)PDI02800
00133 29* 1)*DLON*(DSP(K,IP,JP)-DSP(K,I,JP)-DSP(K,IP,JP)+DSP(K,I,J))*DLAT* PDI02900
00133 30* 2)DLON 3).....DENSITY LAT-LON INTERPOLATION PDI03000
00134 31* TS=TSP(K,I,J)+(TSP(K,IP,JP)-TSP(K,I,JP))*DLAT+(TSP(K,I,JP)-TSP(K,I,J))*DLAT* I,J)PDI03100
00134 32* 1)*DLON*(TSP(K,IP,JP)-TSP(K,I,JP)-TSP(K,IP,JP)+TSP(K,I,J))*DLAT* PDI03200
00134 33* 2)DLON 3).....TEMPERATURE LAT-LON INTERPOLATION PDI03300
00134 34* C).....DPX = DP/DX FOR GEOSTROPHIC WINDS PDI03400
00135 35* DPX = (PSP(K,I,J) - PSP(K,I,JP)) / 6. PDI03500
00136 36* DPX = DPX + ((PSP(K,IP,JP) - PSP(K,IP,JP)) / 6. - DPX) * DLAT PDI03600
00136 37* C).....DPY = DP/DY FOR GEOSTROPHIC WINDS PDI03700
00137 38* DPY = (PSP(K,IP,JP) - PSP(K,I,J)) / 4. PDI03800
00140 39* DPY = DPY + ((PSP(K,IP,JP) - PSP(K,I,JP)) / 4. - DPY) * DLON PDI03900
00141 40* C).....DTX = DT/DX FOR THERMAL WINDS PDI04000
00141 41* DTX = (TSP(K,I,J) - TSP(K,I,JP)) / 6. PDI04100
00142 42* DTX = DTX + ((TSP(K,IP,JP) - TSP(K,IP,JP)) / 6. - DTX) * DLAT PDI04200
00143 43* C).....DTY = DT/DY FOR THERMAL WINDS PDI04300
00144 44* DTY = (TSP(K,IP,JP) - TSP(K,I,J)) / 4. PDI04400
00144 45* DTY = DTY + ((TSP(K,IP,JP) - TSP(K,I,JP)) / 4. - DTY) * DLON PDI04500
00145 46* RETURN PDI04600
00146 47* END PDI04700

```

END OF COMPILATION: NO DIAGNOSTICS.

GHGS/P ***** PERTRB *****
 #FOR/S PROFAS,PERTRB,PERTRB
 FOR S1E-02/04/74-18:53:20 (0,)

SUBROUTINE PERTRB ENTRY POINT 000355

STORAGE USED: CODE(1) 000360; DATA(0) 000041; BLANK COMMON(2) 000000

COMMON BLOCKS:

0003 IOTEMP 000050
 0004 COMPER 000012

EXTERNAL REFERENCES (BLOCK, NAME)

0005 NORMAL
 0006 CORR
 0007 SORT
 0010 EXP
 0011 NWDUS
 0012 NIC2\$
 0013 NERR3\$

STORAGE ASSIGNMENT (BLOCK, TYPE, RELATIVE LOCATION, NAME)

0001	000205	10L	0001	000275	12L	0001	000074	5L	0000	000017	900F	0000	R	000005	AD			
0003	000040	AP	0000	R	000014	AT	0000	R	000006	BD	0000	R	000015	BT	0006	R	000000	CORR
0000	R	000016	CT	0003	000004	DO	0003	R	000044	DX	0003	R	000047	DZ	0003	R	000012	D1

***** PERTRB *****

```

0004 R 000004 Q2
0003 R 000033 H
0000 000032 INJPS
0003 000042 MIN
0003 000007 PHI
0004 R 000003 P2
0000 R 000010 RT2
0003 R 000014 SP1
0004 R 000010 SU
0003 000030 THETR
0003 R 000046 VL
0000 R 000001 ZT
0000 R 000002 EX
0003 R 000045 HL
0003 000000 IOTEM1
0003 000023 MN
0003 000034 PHIR
0000 R 000013 R
0000 R 000011 RX1
0004 R 000000 SP2
0003 R 000021 SU1
0003 R 000013 T1
0003 R 000020 V1
0003 R 000036 F10
0003 R 000026 H1
0000 000001 IOTEMP
0003 000003 NMCOP
0003 000006 PHI1
0000 R 000003 RD
0000 R 000012 RX2
0000 R 000004 SRD
0004 R 000011 SV
0003 R 000005 T2
0004 R 000007 V2
0003 000037 F10R
0003 000024 INA
0000 000002 IUG
0003 000043 NMORE
0003 000027 PHIR
0000 R 000032 RI
0004 R 000015 SD1
0004 R 000016 ST1
0003 R 000022 SV1
0004 R 000017 U1
0000 R 000005 XNJD
0003 000031 G
0003 000041 IHR
0003 000025 IYR
0003 000010 NSAME
0003 000011 P1
0000 R 000007 RT1
0004 R 000001 SD2
0004 R 000002 ST2
0003 000035 THETR
0004 R 000006 U2
0000 R 000000 ZD
    
```

```

00101 SUBROUTINE PERTRR
00102 C.....COMPUTES PERTURBATIONS P2,D2,T2,U2,V2 AT NEW POSITION FROM
00103 C VALUES PI,DI,T1,UI,V1 AT PREVIOUS POSITION, SIGMAS SP1,SD1,
00104 C ST1,SU1,SV1 AT PREVIOUS POSITION, SIGMAS SP2,SD2,ST2,SU2,SV2
00105 C AT NEW POSITION. DX AND DZ ARE HORIZONTAL AND VERTICAL
00106 C DISPLACEMENTS BETWEEN OLD AND NEW POSITIONS. HL AND VL ARE
00107 C HORIZONTAL AND VERTICAL SCALES, H1 AND H2 ARE PREVIOUS AND
00108 C CURRENT HEIGHT.
00109 C COMMON/IOTEMP/IOTEM1,IOTEM2,IUG,NMCOP,DD,XNJD,PHI1,PHI,
00110 C *NSAME,PI,DI,T1,SPI,SD1,ST1,UI,V1,SU1,SV1,
00111 C *MN,IDA,IYR,H1,PHIR,THETR,G,RI,H,PHIR,THETR,F10,F10B,AP,
00112 C IHR,MIN,NMORE,DX,HL,VL,DZ
00113 C COMMON/COMPET/SP2,SD2,ST2,P2,D2,T2,U2,V2,SU,SV
00114 C CALL NORMAL(ZD,ZT)@.....GENERATES GAUSSIAN RANDOM NUMBERS
00115 C EX=SQRT((DX/HL)**2+(DZ/VL)**2)
00116 C RD=1./EXP(1X)*@.....DENSITY CORRELATION BETWEEN OLD AND NEW POS.
00117 C SRD=SQRT(1.-RD)
00118 C IF (SD1*ST1*SD2*ST2.GT.0.) GO TO 5
00119 C.....DEFAULT VALUES AVOID DIVISION BY ZERO
00120 C IF (SD1.LE.0.) SD1 = .01
00121 C IF (ST1.LE.0.) ST1 = .01
00122 C IF (SD2.LE.0.) SD2 = .01
00123 C IF (ST2.LE.0.) ST2 = .01
00124 C 5 AD=RD*SD2/SD1
00125 C HD=SD2*SRD
00126 C D2=AD*DI+BD*ZD @.....NEW DENSITY PERTURBATION
00127 C.....CORRELATION BETWEEN DENSITY AND TEMPERATURE AT OLD POSITION
00128 C RT1=(SP1*SP1-SD1*SD1-ST1*ST1)/(2.*ST1*SD1)
00129 C.....CORRELATION BETWEEN DENSITY AND TEMPERATURE AT NEW POSITION
00130 C RT2=(SP2*SP2-SD2*SD2-ST2*ST2)/(2.*ST2*SD2)
00131 C IF (ABS(RT1).LE.1.AND.ABS(RT2).LE.1) GO TO 10
00132 C RX1 = CORR(H1) @.....DEFAULT CORRELATIONS COMPUTED BY CORR
00133 C RX2 = CORR(H)
00134 C IF (ABS(RT1).GT.1.) RT1=RX1
00135 C IF (ABS(RT2).GT.1.) RT2=RX2
00136 C 10 RERD=RT1
00137 C AT=(ST2/ST1)*((RD-R*RT2)/(1.-R*R))
00138 C RT=(ST2/SD2)*((RT2-R*RD)/(1.-R*R))
00139 C CT=ST2*ST2-AT*AT*ST1*ST1-2.*AT*BT*R*SD2*ST1-BT*BT*SD2*SD2
00140 C IF (CT.GE.0.) GO TO 12
00141 C WRITE(6,900) AT,BT,SD2,ST1,ST2,R,CT
00142
00101 PER00100
00102 PER00200
00103 PER00300
00104 PER00400
00105 PER00500
00106 PER00600
00107 PER00700
00108 PER00800
00109 PER00900
00110 PER01000
00111 PER01100
00112 PER01200
00113 PER01300
00114 PER01400
00115 PER01500
00116 PER01600
00117 PER01700
00118 PER02100
00119 PER02200
00120 PER02300
00121 PER02400
00122 PER02500
00123 PER02600
00124 PER02630
00125 PER02660
00126 PER02690
00127 PER02700
00128 PER02800
00129 PER02900
00130 PER03000
00131 PER03100
00132 PER03200
00133 PER03300
00134 PER03400
00135 PER03500
00136 PER03600
00137 PER03700
00138 PER03800
00139 PER03900
00140 PER04000
00141 PER04100
    
```



```

***** PERTRB *****
00157          900 FORMAT(' CORRELATION COEFFICIENT ERROR',( ))
00160          CT=0.
00161          12 CT=SQRT(CT)
00162          T2 = AT*TI+BT*D2+CT*ZT 3.....NEW TEMPERATURE PERTURBATION
00163          P2=D2*TI2          3.....NEW PRESSURE PERTURBATION
00163          C.....GENERATES 2 NEW GAUSSIAN RANDOM NUMBERS
00164          CALL NORMAL(ZO,ZT)
00165          AT=RD*SU/SU1
00166          3I=SU*SRD
00166          C.....NEW EASTWARD VELOCITY PERTURBATION
00167          U2=AT*UI+BT*ZD
00170          AT=RD*SV/SV1
00171          3I=SV*SRD
00171          C.....NEW NORTHWARD VELOCITY PERTURBATION
00172          V2=AT*VI+BT*ZT
00173          RETURN
00174          END
PER04200
PER04300
PER04400
PER04500
PER04600
PER04700
PER04800
PER04900
PER05000
PER05100
PER05200
PER05300
PER05400
PER05500
PER05600
PER05700
PER05800

```

END OF COMPILATION: NO DIAGNOSTICS.

QHDG,P ***** PROFIL *****
 QFOR,S PROFAS,PROFIL,PROFIL
 FOR S1E-02/04/74-18:53:41 (9,)

MAIN PROGRAM

STORAGE USED: CODE(1) 000551; DATA(0) 000175; BLANK COMMON(2) 000000

COMMON FLOCKS:

0003 IOTEMP 000055

EXTERNAL REFERENCES (BLOCK, NAME)

0004 SETUP
 0005 RIG
 0006 SCIMOD
 0007 NINTRS
 0010 NRDU\$
 0011 NI02\$
 0012 RNDU\$
 0013 NSTOP\$

STORAGE ASSIGNMENT (BLOCK, TYPE, RELATIVE LOCATION, NAME)

0000	000023	10F	0001	000245	18L	0001	000260	19L	0001	00027	20L	0001	000367	21L
0001	000415	22L	0001	000450	23L	0001	000475	25L	0001	000011	5L	0001	000043	6L
0001	000125	7L	0001	000545	90L	0000	000024	9010F	0000	R	000021	A	0003	R
0003	R	000050	B	0003	000004	DD	0000	R	0000	R	000011	DPHI	0000	R
0000	R	000012	DTHET	0000	R	000017	DTHETR	0003	000044	DX	0003	000047	DZ	0003
0000	R	000001	FAC	0003	R	000036	F10	0003	R	000037	F10B	0003	R	000033
0003	I	000045	HL	0003	R	000026	H1	0003	I	000024	IDA	0003	I	000041
0000	I	000006	IHR0	0000	I	000015	INCT	0003	I	000052	IOPP	0003	I	000000
0003	000001	IOTEM2	0000	I	000022	ISEC	0000	I	000010	ISECO	0003	I	000025	IYR
0003	I	000053	LOOK	0003	I	000042	MIN	0000	I	000007	MINO	0003	I	000002
														MONTH

0000 I 000014 NMAX
 0003 R 000007 PHI
 0003 000012 RDI
 0003 000020 RV1
 0003 000022 SV1
 0003 000046 VL

0003 I 000043 NMORE
 0003 R 000006 PH1R
 0003 000011 RP1
 0003 000014 SP1
 0003 R 000035 THETR
 0000 R 000005 XWJD

0003 I 000010 NSAME
 0003 R 000027 PH1R
 0003 000013 RT1
 0003 000016 ST1
 0003 R 000005 THET1R

0000 I 000020 NT
 0000 R 000000 PI
 0003 000017 RUI
 0003 000021 SUI
 0003 R 000030 THET1R

```

00100 C.....FIRST DATA CARD READS INITIAL HEIGHT (KM), INITIAL LATITUDE (DEG) PRO00100
00100 C INITIAL LONGITUDE (DEG), F10.7, MEAN F10.7, AP, MONTH, DAY, PRO00200
00100 C YEAR (TOTAL YEAR - 1900), GREENWICH HOUR, MINUTES, SECONDS, PRO00300
00100 C LATITUDE INCREMENT (DEG), LONGITUDE INCREMENT (DEG), PRO00400
00100 C HEIGHT DECREASE (KM), MAXIMUM NUMBER OF POSITIONS (EXCLUDING PRO00500
00100 C INITIAL POSITION) TO BE COMPUTED, TIME INCREMENT BETWEEN PRO00600
00100 C POSITIONS, TRAJECTORY OPTION, PUNCH OPTION. PRO00700
00100 C COMMON/IOTEMP/IOTEM1,IOTEM2,IUG,NMCOP,DD,XMJD,PHI1,PHI, PRO00800
00100 C NSAME,RP1, RDI, RT1, SP1, ST1, RUI, RV1, SUI, SV1, PRO00900
00100 C * MN, IDA, IYR, HI, PHIR,THETR,G,RI,H,PHIR,THETR,F10,F10B,AP, PRO01000
00100 C * IHR,MIN,NMORE,DX,HL,VL,DZ,IB,EPS,IOPP,LOOK,IET PRO01050
00100 C * PI=3.1415927 PRO01100
00100 C * FAC=0.017453293 PRO01150
00100 C * LOOK=0 PRO01180
00100 C * MONTH = 0 PRO01200
00100 C * IOPT=0 PRO01220
00100 C * IF(IOPT,EG,0,OR.(IOPT.GT.0,AND,H.LT.0.)) GO TO 6 PRO01240
00100 C READ(5,10)IET,H,PHI,THET PRO01260
00100 C GO TO 5 PRO01280
00100 C * MN = MONTH PRO01300
00100 C * NSAME = 0 PRO01400
00100 C * READ(5,10,END=99) H1,PHI1,THET1,F10,F10B,AP,MN,IDA ,IYR,IHRO,MINO,PRO01500
00100 C * ISECO,DPHI,DTHET,DH,NMAX,INCT,IOPT,IOPP PRO01520
00100 C * IF(ABS(PHI).LT.90.160 TO 7 PRO01540
00100 C * PHI1=SIGN(180,-ABS(PHI1),PHI1) PRO01560
00100 C * THET1=THET1+180. PRO01580
00100 C * IF(THET1.GT.360.)THET1=THET1-360. PRO01600
00100 C * *WRITE(6,9010) H1,PHI1,THET1,F10,F10B,AP,MN,IDA ,IYR,IHRO,MINO, PRO01620
00100 C * ISECO,DPHI,DTHET,DH,NMAX,INCT,IOPT,IOPP PRO01700
00100 C * *FORMAT( ) PRO01800
00100 C * 15 IF (MN.EQ.MONTH) NSAME = 1 @.....SETS NSAME TO AVOID SETUP PRO01900
00100 C * MONTH = MN @.....LOOKUP ON MULTIPLE PASSES PRO02000
00100 C * PHI1=PHI1*FAC @.....LATITUDE TO RADIANS PRO02100
00100 C * THETR=THET1*FAC @.....LONGITUDE TO RADIANS PRO02400
00100 C * DPHIR=DPHI*FAC @.....LONGITUDE INCREMENT TO RADIANS PRO02500
00100 C * DTHET=DTHET*FAC @.....LONGITUDE INCREMENT TO RADIANS PRO02600
00100 C * CALL SETUP @.....LONGITUDE INCREMENT TO RADIANS PRO02700
00100 C * NT = 1 @.....READS DATA TAPE TO INITIALIZE ARRAYS PRO02800
00100 C * IF(IOPT.EQ.0) GO TO 18 PRO02900
00100 C * READ(5,10)IET,H,PHI,THET PRO02910
00100 C * IF(THET.LT.0.)THET=THET+360. PRO02920
00100 C * PHIR=PHI*FAC PRO02930
00100 C * THETR=THET*FAC PRO02940
00100 C * GO TO 19 PRO02950
00100 C * 18 H = H1 - DH PRO02960
00100 C.....DISPLACES POSITION BEFORE EVALUATION OF ATMOSPHERIC PARAMETERS PRO03000
00234 PRO03100
    
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REPRODUCIBILITY OF THE ORIGINAL PAGE IS POOR

DATE 020474

PROFIL *****

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00235 48* IET = INCT
00236 49* PHIR=PI*IR+DPHIR
00237 50* THETR=THETR+DTHETR
00240 51* R = 6378.160 @.....EQUATORIAL EARTH RADIUS
00241 52* R = 6356.7747 @.....POLAR EARTH RADIUS
00242 53* EPS=(1-(B*R)/(A*A)).@.....EARTH ECCENTRICITY
00242 54* C.....COMPUTES RADIUS TO HEIGHT H, AND GRAVITY AT HEIGHT AND
00242 55* C LATITUDE PHIR
00243 56* CALL RIG
00244 57* ISEC=ISECO+IET
00245 58* ISEC=MOD(ISEC,60)
00246 59* MIN = MINO + IET/60
00247 60* MIN = IHRO + MIN / 60
00250 61* MIN = MOD(MIN,60)
00250 62* C.....COMPUTES P,D,T,U,V AT FIRST POSITION AFTER INITILL POSITION
00251 63* IF(H1.LE.30.) LOOK=1
00254 64* CALL SCIMOD
00254 65* 20 NT = NT + 1
00255 66* IF (10PT.EQ.0) GO TO 22
00257 67* READ(5,10)IET,H,PHI,THETR
00265 68* IF(H.LT.0)GO TO 5
00267 69* IF(ABS(PHI).LT.90.)GO TO 21
00271 70* PHI=SIGN(180,-ABS(PHI),PHI)
00272 71* THETR=THETR+180.
00273 72* IF(THET.LT.0.)THETR=THETR+360.
00275 73* IF(THET.GE.360.)THETR=THETR-360.
00277 74* PHIR=PHI*FAC
00300 75* THETR=THETR*FAC
00301 76* GO TO 25
00302 77* H = H1 - DH @.....INCREMENTS HEIGHT
00303 78* IF (H.LT.0.0) GO TO 5
00305 79* PHIR=PHIR+DPHIR @.....INCREMENTS LATITUDE
00306 80* THETR=THETR+DTHETR @.....INCREMENTS LONGITUDE
00306 81* C.....READS NEW INPUT IF ABS(LAT) GTR 90 DEG
00307 82* IF (ABS(PHIR).LT.PI/2) GO TO 23
00311 83* PHIR=SIGN(PI-ABS(PHIR),PHIR)
00312 84* THETR=THETR+PI
00313 85* IF (THETR.GE.2.*PI) THETR = THETR - 2. * PI
00315 86* IF (THETR.LT.0.) THETR = THETR + 2. * PI
00317 87* IET=IET+INCT @.....INCREMENTS TIME
00320 88* MIN=MINO+IET/60
00321 89* ISEC=ISECO+IET
00322 90* ISEC=MOD(ISEC,60)
00323 91* IHR=IHR0+MIN/60
00324 92* MIN=MOD(MIN,60)
00325 93* CALL RIG @.....COMPUTE RADIUS AND GRAVITY AT NEW POSITION
00326 94* CALL SCIMOD @.....COMPUTE P,D,T,U,V AT NEW POSITION
00326 95* C.....READS NEW INPUT IF NMORE = 0 OR MAX POINTS COMPUTED
00327 96* IF(NMORE.EQ.0.OR.(10PT.EQ.0.AND.NT.GE.NMAX)) GO TO 5
00331 97* GO TO 20 @.....CYCLES TO NEW POSITION
00332 98* 90 STOP
00332 98* 9010 FORVAT(2H1,'INITIAL HEIGHT =',F7.2,' KM',T43,'INITIAL LAT =',
00333 99* 'F6.2,' DEG',T83,'INITIAL WEST LON =',F6.2,' DEG',/, ' F10.7 =',FPR006600
00333 100* 38.2,
00333 101* 2T43,' MEAN F10.7 =',F7.2,T83,'AP =',F8.2,/, ' DATE =',I2,/,I2,PRO066700
00333 102* 3/,I2,T43,'GREENWICH TIME =',I2,/,I2,/,I2,/, ' LAT INCREMENT PRO06750
00333 103* 4 =',F6.2,' DEG',T43,'WEST LON INCREMENT =',F6.2,' DEG',T83,'HEI',PRO06800
00333 104*

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***** PROFIL *****

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00333 105* S'GHT I:CR',
00333 106* S'EMENT = ,F7,2, K',/, ' MAXIMUM NUMBER OF POSITIONS = ,I4,I4,3,PRO06850
00333 107* O'TIME INCREMENT = ,I4, SEC',/2X, TRAJECTORY OPTION=',I4, PRO06800
00333 108* 7I43, PUNCH OPTION=',I2/) PRO07000
00333 109* END PRO07100
PRO07200

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END OF COMPILATION: NO DIAGNOSTICS.

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QHDP ***** QBOGEN *****
QFOR,S PROFAS,QBOGEN,QBOGEN
FOR S1E-02/04/74-18:53:51 (0, )

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SUBROUTINE QBOGEN ENTRY POINT 000620

STORAGE USED: CODE(1) 000631; DATA(0) 000074; BLANK COMMON(2) 000000

COMMON BLOCKS:

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0003 IOTEMP 000050
0004 PDCOM 012701

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EXTERNAL REFERENCES (BLOCK, NAME)

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0005 INTERZ
0006 INTERW
0007 COS
0010 NERR35

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STORAGE ASSIGNMENT (BLOCK, TYPE, RELATIVE LOCATION, NAME)

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0001 000014 IOL 0003 000040 AP 0004 R 012675 DA 0004 R 000014 DAI
0002 000020 DA2 0003 R 000004 DD 0004 R 010205 DDQ 0004 R 000023 DAI
0003 000025 DG 0004 R 012670 DC 0004 010755 DR 0004 R 000023 DDI 0004 R 000026 DD2
0004 000047 DZ 0003 000036 F10 0003 000037 F10B 0003 000031 G 0003 R 000044 DX 0003 R 000033 H
0005 000010 HI 0003 000045 HL 0000 000016 HP 0003 000026 HI 0003 000024 IDA 0003 000024 IDA
0006 000000 IH 0003 000041 IHR 0000 000054 INJP$ 0004 000002 IOPR 0003 000000 IOTEM1 0003 000000 IOTEM1
0007 000001 IOTEM2 0000 I 000001 IP 0003 000002 IUG 0004 000000 IU4 0003 000025 IYR 0003 000025 IYR
0008 000003 JLCOP 0000 I 000004 JP 0003 000042 MIN 0003 000023 MN 0004 000001 MONTH 0004 000001 MONTH
0009 000013 PA1 0000 R 000017 PA2 0003 000010 NSAME 0004 R 012674 PA 0004 R 007505 PAG 0004 R 007505 PAG
0010 000025 PD2 0004 000003 PG 0000 R 000030 PD 0004 R 010065 PDQ 0004 R 000022 PDI 0004 R 000011 PHIJ
0011 000012 PHIP 0003 000034 PHIR 0003 000006 PH1 0003 000027 PH1R 0004 R 012667 PG 0004 R 000011 PHIJ
0012 010445 PR 0004 002005 PSP 0003 000012 RD1 0003 000032 RI 0003 000011 RPI 0003 000011 RPI
0013 000013 RT1 0003 000017 RJ1 0003 000020 RV1 0003 000015 SD1 0003 000014 SPI 0003 000014 SPI
0014 000016 ST1 0003 000021 SU1 0003 000021 SV1 0004 R 010325 TDG 0004 R 007745 TAG 0004 R 007745 TAG
0015 000015 TAI 0000 R 000021 TA2 0000 R 000031 TD 0004 R 010325 TDG 0004 R 000024 TDI 0004 R 000024 TDI
0016 000027 TD2 0004 000531 T6 0003 000035 THEIR 0003 000030 THEIR 0000 R 000006 TMJD 0000 R 000006 TMJD
0017 000007 TP 0004 R 012671 T8 0004 R 011265 TR 0004 000042 TSP 0004 R 012677 UA 0004 R 012677 UA
0018 011575 UAQ 0000 R 000034 UA1 0000 R 000034 UA2 0000 R 000042 UD 0004 R 012035 UDG 0004 R 012035 UDG
0019 000036 UD1 0000 R 000040 UD2 0004 R 012672 UQ 0004 R 01275 UR 0004 R 012700 VA 0004 R 012700 VA
0020 011715 VAG 0000 R 000033 VA1 0000 R 000035 VA2 0000 R 000043 VQ 0004 R 012155 VQG 0004 R 012155 VQG
0021 000037 VDI 0000 R 000041 VD2 0000 R 000046 VL 0003 000043 VQ 0003 R 000005 XMJD 0003 R 000005 XMJD
0022 000005 XMJDO 0000 R 000005 XMJDO

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00101 1* SUBROUTINE QBOGEN
00101 2* C.....COMPUTES QBO VALUES P,Q,R,S,T,U,V,W AT HEIGHT H, LATITUDE PHI
00101 3* C OH JULIAN DAY XMJD FROM ARRAYS OF AMPLITUDES PAQ,DAG,TAQ,
00101 4* C UAG,VAQ AND PHASES PQQ,DQD,TQQ,UQQ,VQQ
00103 5* C COM=OH/IOTEVP/IOTEM1,IOTEM2,IUG,NMCCP,DD,XMJD,PHI1,PHI,
00103 6* C *SAME,SP1, RDI, RT1, SPI, SDI, ST1, RUI, RVI, SUI, SV1,
00103 7* C $ MN, IDA, IYR, HI, PHIR,THETR1,G,RI,H,PHIR,THETR1,F10,F10R,AP,
00103 8* C IHR,MIN,NMOR,OX,HL,VL,DZ
00103 9* C COM=CN/PDTCOM/IU4,MONTH,IOPR,PG(18,19),TG(18,19)
00104 10* C ,PSP(8,11,12)
00104 11* C ,DSP(8,10,12),TSP(8,10,12),PAQ(16,5),DAQ(16,5),TAQ(16,5),
00104 12* C ,PDQ(16,5),DDQ(16,5),TDD(16,5),PR(20,10),DR(20,10),TR(20,10),
00104 13* C ,UAG(16,5),VAQ(16,5),UDQ(16,5),VDQ(16,5),UR(25,10),PR,DG,TG,UQ,VQ
00104 14* C ,PA,DA,TA,UA,VA
00105 15* C IF (XMJD.GT.0) GO TO 10
00107 16* C PG=0.
00110 17* C QG=3.
00111 18* C TG=0.
00112 19* C UG=0.
00113 20* C VQ=0.
00114 21* C RETURN
00115 22* C 10 I=INT((H-10.)/5.) @.....LOWER HEIGHT INDEX
00116 23* C IF (TH.LT.1) I=I+1 @.....UPPER HEIGHT INDEX
00120 24* C IF (IP.GT.16) IP = 16
00121 25* C PHA = ABS(PHI)
00123 26* C JL = INT( ( PHA + 10. ) / 20. ) @.....LOWER LATITUDE INDEX
00124 27* C JP = JL+1 @.....UPPER LATITUDE INDEX
00125 28* C IF (JL.LE.0) JL=1
00126 29* C IF (JP.GT.5) JP=5
00130 30* C XMJD=2439126. @.....JULIAN DAY FOR JAN 0, 1966
00132 31* C TMJD=XMJD-XMJD0 @.....TIME RELATIVE TO JAN 0, 1966
00133 32* C TP = 6.2831853/870. @.....2PI/PERIOD, PERIOD = 870 DAYS
00134 33* C *I = 10. + 5.*IH @.....LOWER HEIGHT
00135 34* C *JL = 10. @.....LOWER LATITUDE
00136 35* C *JP=20.*JP-10. @.....UPPER HEIGHT
00137 36* C INTERPOLATES QBO P,D,T AMPLITUDE ON LATITUDE AT UPPER HEIGHT
00137 37* C CALL INTERZ(PAQ(IH,JL),DAQ(IH,JL),TAG(IH,JL),PHIJ,PAQ(IH,JP),
00140 38* C 1DAQ(IH,JP),TAG(IH,JP),PHIP,PA1,DA1,TA1,PHA)
00140 39* C *P=10.+5.*IP @.....UPPER HEIGHT
00141 40* C INTERPOLATES QBO P,D,T AMPLITUDE ON LATITUDE AT LOWER HEIGHT
00141 41* C CALL INTERZ(PAQ(IP,JL),DAQ(IP,JL),TAG(IP,JL),PHIJ,PAQ(IP,JP),
00142 42* C 2DAQ(IP,JP),TAG(IP,JP),PHIP,PA2,DA2,TA2,PHA)
00142 43* C INTERPOLATES QBO P,D,T AMPLITUDE ON HEIGHT AT LATITUDE PHI
00143 44* C CALL INTERZ(PA1,DA1,TA1,HI,PA2,DA2,TA2,HP,PA,DA,TA,H)
00143 45* C INTERPOLATES QBO P,D,T PHASE ON LATITUDE AT LOWER HEIGHT
00143 46* C CALL INTERZ(PDQ(IH,JL),DDQ(IH,JL),TDD(IH,JL),PHIJ,PDQ(IH,JP),
00144 47* C 3DDQ(IH,JP),TDD(IH,JP),PHIP,PD1,DD1,TD1,PHA)
00144 48* C INTERPOLATES QBO P,D,T PHASE ON LATITUDE AT UPPER HEIGHT
00144 49* C CALL INTERZ(PDQ(IP,JL),DDQ(IP,JL),TDD(IP,JL),PHIJ,PDQ(IP,JP),
00145 50* C 4DDQ(IP,JP),TDD(IP,JP),PHIP,PD2,DD2,TD2,PHA)
00145 51* C INTERPOLATES QBO P,D,T PHASE ON HEIGHT AT LATITUDE PHI
00145 52* C CALL INTERZ(PD1,DD1,TD1,HI,PD2,DD2,TD2,HP,PD,DD,TD,H)
00146 53* C INTERPOLATES QBO WIND AMPLITUDE ON LATITUDE AT LOWER HEIGHT
00146 54* C CALL INTERW(UAQ(IH,JL),VAQ(IH,JL),PHIJ,UAQ(IH,JP),VAQ(IH,JP),
00147 55* C 5PHIP,UA1,VA1,PHA)
00147 56*

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00147 57* ***** 030GEN *****
00150 58* C.....INTERPOLATES QBO WIND AMPLITUDES ON LATITUDE AT UPPER HEIGHT
00150 59* CALL INTERW(UAQ(IP,JL),VAG(IP,JL),PHIU,UAQ(IP,JP),VAG(IP,JP),
00150 60* 6PHIP,UA2,VA2,PHA)
00151 61* C.....INTERPOLATES QBO WIND AMPLITUDES ON HEIGHT AT LATITUDE PHI
00151 62* CALL INTERW(UAI,VAI,HI,UA2,VA2,HP,UA,VA,H)
00152 63* C.....INTERPOLATES QBO WIND PHASE ON LATITUDE AT LOWER HEIGHT
00152 64* CALL INTERW(UDQ(IH,JL),VDQ(IH,JL),PHIU,UDQ(IH,JP),VDQ(IH,JP),
00152 65* 7PHIP,U21,VD1,PHA)
00153 66* C.....INTERPOLATES QBO WIND PHASE ON LATITUDE AT UPPER HEIGHT
00153 67* CALL INTERW(U2Q(IP,JL),VDQ(IP,JL),PHIU,UDQ(IP,JP),VDQ(IP,JP),
00153 68* 8PHIP,UD2,VD2,PHA)
00154 69* C.....INTERPOLATES QBO WIND PHASE ON HEIGHT AT LATITUDE PHI
00154 70* CALL INTERW(UDI,VD1,HI,UD2,VD2,HP,UD,VD,H)
00155 71* C.....EVALUATES QBO VALUES FROM INTERPOLATED AMPLITUDES AND PHASES
00156 72* PG=PA*COS(TP*(TMJD-PD))
00157 73* TG=TA*COS(TP*(TMJD-PD))
00160 74* UG=UA*COS(TP*(TMJD-UD))
00161 75* VG=VA*COS(TP*(TMJD-VD))
00162 76* RETURN
00163 77* END

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END OF COMPILATION: NO DIAGNOSTICS.

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QHDG,P ***** RAND *****
QFOR,S PROFAS,RAND,RAND
FOR S11E-02/04/74-18:53:58 (0,)

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FUNCTION RAND ENTRY POINT 000035

STORAGE USED: CODE(1) 000C371 DATA(0) 000011; BLANK COMMON(2) 000000

EXTERNAL REFERENCES (BLOCK, NAME)

0003 HERR35

STORAGE ASSIGNMENT (BLOCK, TYPE, RELATIVE LOCATION, NAME)

0000 000005 INJPS 0000 R 000000 RAND 0000 R 000001 X

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00101 1* FUNCTION RAND(X0)
00101 2* C.....PRODUCES A RANDOM NUMBER FROM A UNIFORM DIST. FROM 0 TO +1
00103 3* INTEGER X0
00104 4* IF (X0.NE.0) X = X0/262144.
00106 5* X = X*509
00107 6* X = X - INT(X)
00110 7* RAND = X
00111 8* RETURN
00112 9* END

```

***** RAID *****

END OF COMPILATION: NO DIAGNOSTICS.

QHDG,P ***** RIG *****

QFOR,S PROFAS,RIG,RIG

FOR S11E-02/04/74-18:54:01 (0,)

SUBROUTINE RIG ENTRY POINT 000072

STORAGE USED: CODE(1) 000075; DATA(0) 000024; BLANK COMMON(2) 000000

COMMON BLOCKS:

0003 IOTEMP 000052

EXTERNAL REFERENCES (BLOCK, NAME)

0004 COS
0005 SQR
0006 NERR3s

STORAGE ASSIGNMENT (BLOCK, TYPE, RELATIVE LOCATION, NAME)

0003	000040	AP	0003	R	000050	B	0000	R	000000	CPHI2	0000	R	000001	C2PHI	
0003	000004	DD	0003	000044	DX	0003	000047	DZ	0003	R	000051	EPS	0003	000036	F10
0003	000037	F10B	0003	R	000031	G	0003	R	000033	H	0003	000045	HL	000026	H1
0003	000024	IDA	0003	000041	IHR	0000	000015	INJPS	0003	000000	IOTEM1	0003	000001	IOTEM2	
0003	000002	IUG	0003	000025	IYR	0003	000042	MIN	0003	000023	MN	0003	000003	NMCOP	
0003	000043	NMORE	0003	000010	NSAME	0003	000007	PHI	0003	R	000034	PHIR	0003	000006	PHI1
0003	000027	PHI1R	0003	000012	RD1	0000	R	000003	RE	0003	R	000032	RI	000011	RP1
0003	000013	RT1	0003	000017	RU1	0003	000020	RV1	0003	R	000015	SD1	0003	000014	SPI
0003	000016	ST1	0003	000021	SU1	0003	000022	SV1	0003	000035	T4ETR	0003	000030	THE1R	
0003	000046	VL	0003	000005	XMJD										

00101	1*	SUBROUTINE RIG	0000	R	000001	C2PHI	0000	R	000001	C2PHI	0000	R	000001	C2PHI
00103	2*	COMMON/IOTEMP/IOTEM1,IOTEM2,IUG,NMCOP,DD,XMJD,PHI1,PHI,												
00103	3*	MSAME,RP1, RD1, RT1, SPI, SD1, ST1, RV1, SU1, SV1, RI, F10B, AP,												
00103	4*	\$ MN, IDA, IYR, H1, PHIR,THE1R,G,RI,H,PHIR,THE1R,F10,F10B,AP,												
00103	5*	IHR,MIN,NMORE,DX,HL,VL,DZ,B,EPS												
00103	6*	C.....GRAVITY G AT H, LATITUDE PHIR (RADIAN)												
00103	7*	C.....RADIUS RI FROM CENTER OF EARTH TO HEIGHT H												
00103	8*	C.....R = POLAR EARTH RADIUS, EPS = ECCENTRICITY												
00104	9*	CPHI2 = COS(PHIR) ** 2												
00105	10*	RI = B / SQRT(1. - EPS * CPHI2) @.....EARTH RADIUS												
00106	11*	C2PHI = 2. * CPHI2 - 1. @.....COS(2*PHIR)												
00107	12*	C4PHI = 8. * CPHI2 * (CPHI2 - 1.) + 1. @.....COS(4*PHIR)												
00110	13*	C.....G AT SURFACE												
00110	14*	G = 9.80616 * (1. - 0.0026373 * C2PHI + 0.0000059 * C2PHI * C2PHI)												
00110	15*	C.....EFFECTIVE RADIUS												
00111	16*	RE = 2. * G / (3.085462E-3 + C2PHI * 2.27E-6 - C4PHI * 2.E-9)												
00112	17*	G = G / (1. + (H / RE)) ** 2 @.....G AT HEIGHT H												
00113	18*	RI = RI + H @.....RADIUS AT HEIGHT H												

REPRODUCIBILITY OF THE ORIGINAL PAGE IS POOR

RIG01900

***** RIG *****

00114 19* END

END OF COMPILATION: NO DIAGNOSTICS.
 @HDG,P ***** RTERP *****
 @FOR,S PROFAS,RTERP,RTERP
 FOR S11E-02/04/74-18:54:08 (C.)

SUBROUTINE RTERP ENTRY POINT 000353

STORAGE USED: CODE(1) 000404; DATA(0) 000047; BLANK COMMON(2) 000000

EXTERNAL REFERENCES (BLOCK, NAME)

0003 INTERZ
 0004 NERR3S

STORAGE ASSIGNMENT (BLOCK, TYPE, RELATIVE LOCATION, NAME)

0001	000121	10L	0001	000139	20L	0001	000144	30L	0001	000153	40L	0000	R	000011	D1				
0000	R	000014	D2	0000	I	000000	I	0000	000026	INJP\$	0000	I	000001	IP	0000	I	000002	J	
0000	I	000003	JP	0000	R	000006	PHI1	0000	R	000007	PHI2	0000	R	000010	P1	0000	R	000013	P2
0000	R	000012	T1	0000	R	000015	T2	0000	R	000004	Z1	0000	R	000005	Z2				

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00101 1* SUBROUTINE RTERP(H,PHI,PR,DR,TR,P,D,I)
00101 2* C.....COMPUTES RANDOM PERTURBATION STANDARD DEVIATIONS P,D,T AT
00101 3* C HEIGHT H (KM), LATITUDE PHI(DEGREES) FROM SIGMA ARRAYS
00101 4* C PR,DR,AND TR
00103 5* C.....I = LOWER HEIGHT INDEX
00103 6* IF (H.LT.95.) I = INT((H-20.)/5.)
00104 7* IF (H.GE.95.) I = 14 + INT((H-80.)/20.)
00106 8* IP = I+1
00110 9* IF (IP.GT.20) IP = 20
00111 10* J = INT((PHI + 110.)/20.) @.....LOWER LATITUDE INDEX
00113 11* JP = J+1
00114 12* IF (JP.GT.10) JP=10
00115 13* IF (I.GT.14) GO TO 10
00117 14* Z1=5.*I+20. @.....LOWER HEIGHT FOR PR,TR,DR ARRAYS
00121 15* GO TO 20
00122 16* Z1=20.*(I-10)
00123 17* Z2=5.*IP+20. @.....UPPER HEIGHT FOR PR,DR,TR ARRAYS
00124 18* GO TO 40
00126 19* Z2=20.*(IP-10)
00127 20* GO TO 40
00130 21* PHI=-110.+20.*J
00131 22* PHI2=-110.+20.*JP
00132 23* C.....INTERPOLATE ON LATITUDE AT LOWER HEIGHT
00132 24* CALL INTERZ(PR(I,J),DR(I,J),TR(I,J),PHI1,PR(I,JP),DR(I,JP),
00133 25* TR(I,JP),PHI2,P1,D1,T1,PHI)
00133 26*

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RTP02700
 RTP02800
 RTP02900
 RTP03000
 RTP03100
 RTP03200
 RTP03300

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***** RTERP *****
00133 27* C.....INTERPOLATE ON LATITUDE AT UPPER HEIGHT
00134 28* CALL INTERZ(PR(IP,J),DR(IP,J),TR(IP,J),PHI1,PR(IP,JP),DR(IP,JP),
00134 29* TR(IP,JP),PHI2,P2,D2,I2,PHI)
00134 30* C.....INTERPOLATION ON HEIGHT USING LATITUDE INTERPOLATED VALUES
00135 31* CALL INTERZ(P1,D1,I1,Z1,P2,Z2,I2,Z2,P,D,T,H)
00136 32* RETURN
00137 33* END
    
```

END OF COMPILATION: NO DIAGNOSTICS.

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@HDG,P ***** RTRAN *****
@FOR,S PROFAS,RTRAN,RTRAN
FOR S11E-02/04/74-18:54:16 (07)
    
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```

SUBROUTINE RTRAN ENTRY POINT 000115
RTRAN1 ENTRY POINT 000122
RTRAN2 ENTRY POINT 000125
    
```

STORAGE USED: CODE(1) 000130; DATA(0) 000017; BLANK COMMON(2) 000000

COMMON BLOCKS:

```

0003 IOTEMP 000003
0004 COTRAN 000041
    
```

EXTERNAL REFERENCES (BLOCK, NAME)

```

0005 NTRAN
0006 NERR3$
    
```

STORAGE ASSIGNMENT (BLOCK, TYPE, RELATIVE LOCATION, NAME)

```

0001 000043 I20G 0001 000072 I33G 0000 I 000001 I 0000 000007 INJPS 0003 000000 IOTEM1
0003 000001 IOTEM2 0003 I 000002 IUG 0004 I 000023 I1 0004 I 000024 I2 0004 I 000025 I3
0004 I 000026 I4 0004 I 000040 I5 0000 I 000000 L 0004 I 000000 NDATA
    
```

```

00101 1* SUBROUTINE RTRAN(N)
00103 2* COMMON/IOTEMP/IOTEM1,IOTEM2,IUG
00104 3* COMMON/COTRAN/NDATA(19),I1,I2,I3,I4,I10,I15
00104 4* C.....ENTRY POINT FOR NTRAN READ OF STATIONARY PERTURBATION DATA, AND
00104 5* C RANDOM PERTURBATION DATA IN SETUP
00105 6* CALL NTRAN(IUG,2,N,NDATA,L)
00106 7* CALL NTRAN(IUG,22)
00107 8* RETURN
00110 9* ENTRY RTRAN1
00111 10* C.....ENTRY POINT FOR NTRAN READ OF GROVES DATA IN SETUP
00111 11* CALL NTRAN(IUG,2,19,NDATA,L)
00112 12* CALL NTRAN(IUG,2,22)
00113 13* I1=NDATA(1)
00114 14* I2=NDATA(2)
RTR00100
RTR00200
RTR00300
RTR00400
RTR00500
RTR00600
RTR00700
RTR00800
RTR00900
RTR01000
RTR01100
RTR01200
RTR01300
RTR01400
    
```

00115 15* I3=NDATA(3)
 00116 16* I5=NDATA(14)
 00117 17* DO 1 I=1,10
 00122 18* 1 I4(I)=NDATA(I+3)
 00124 19* RETURN
 00125 20* ENTRY RTRAN2
 00125 21* C.....ENTRY POINT FOR NTRAN READ OF QRO PARAMETERS IN SETUP
 00126 22* CALL NTRAN(IUG,2,12,NDATA,L)
 00127 23* CALL NTRAN(IUG,22)
 00130 24* I1=NDATA(1)
 00131 25* I3=NDATA(2)
 00132 26* DO 2 I=1,10
 00135 27* 2 I4(I)=NDATA(2+I)
 00137 28* RETURN
 00140 29* END

RTR01500
 RTR01600
 RTR01700
 RTR01800
 RTR01900
 RTR02000
 RTR02100
 RTR02200
 RTR02300
 RTR02400
 RTR02500
 RTR02600
 RTR02700
 RTR02800
 RTR02900

END OF COMPILATION: NO DIAGNOSTICS.

PHDG,P ***** SCIMOD *****
 QFOR,S PROFAS,SCIMOD,SCIMOD
 FOR S1E-02/04/74-18:54:20 (0.)

SUBROUTINE SCIMOD ENTRY POINT 002712

STORAGE USED: CODE(1) 002720; DATA(0) 000347; BLANK COMMON(2) 000000

COMMON BLOCKS:

0003 IOTEMP 000055
 0004 FDTCOM 012701
 0005 C4 004743
 0006 COMPER 000012

EXTERNAL REFERENCES (BLOCK, NAME)

0007 JACCH
 0010 GTERP
 0011 FAIR
 0012 INTER2
 0013 INTERW
 0014 PDTUV
 0015 INTERZ
 0016 QBOKEN
 0017 GENHD
 0020 INTER4
 0021 INTRUV
 0022 RTERP
 0023 DXHLVL
 0024 PERTRB
 0025 STDATM
 0026 SIN
 0027 COS
 0030 ALOG
 0031 IWDJ5

REPRODUCIBILITY OF THE ORIGINAL PAGE IS POOR

***** SCIMOD *****
 0032 NI02\$
 0033 NWDC\$
 0034 WERH3\$

STORAGE ASSIGNMENT (BLOCK, TYPE, RELATIVE LOCATION, NAME)

Block	Type	Relative Location	Name
0001	R	000104 10L	000725 220L
0001	R	000727 230L	001500 500L
0001	R	001513 505L	001633 540L
0001	R	001715 550L	002154 800L
0001	R	002211 810L	002422 870L
0001	R	002450 880L	000040 AP
0003	R	000050 B	000004 DD
0004	R	010205 DQ	000032 DGH
0000	R	000215 DGH	000220 DHP
0000	R	000043 DJA	000022 DPX
0000	R	000107 DPXA	000100 DPXGR
0000	R	000053 DPXJA	000131 DPXSR
0000	R	000163 DPX4	000110 DPYA
0000	R	000117 DPY3	000054 DPYJA
0000	R	000063 DPYJB	000164 DPY4
0000	R	000202 DPY4A	000175 DR
0006	R	000094 DRH	000002 DSH
0004	R	003705 DSP	000154 DTXG
0000	R	000073 DTXGA	000156 DTXS
0000	R	000146 DTXSA	000174 DTX4A
0000	R	000026 DTY	000074 DTXGA
0000	R	000103 DTYGB	000147 DTXSA
0000	R	000134 DTYSB	000027 DIH
0000	R	000030 DVH	000114 D2
0000	R	000161 D4	000005 FCORX
0000	R	000004 FCORY	000000 GLAT
0005	R	000020 GLON	000136 HGA
0000	R	000123 H6B	000026 H1
0003	I	000024 IDA	000155 IHGA
0000	I	000422 INGB	000331 INJPF
0003	I	000052 IOPP	000023 IUG
0004	I	000000 IU4	000023 MN
0004	I	000001 MONTH	000010 NSAME
0000	R	000176 PA	000003 PG
0000	R	000066 PGA	000006 PH
0000	R	000016 PHE	000006 PH1
0003	R	000027 PH1R	000057 PJR
0000	R	000050 PJE	000045 PR
0006	R	000003 PRH	000001 PSH
0004	R	002005 PSP	000041 P4D
0003	R	000012 RD1	000017 RU1
0003	R	000020 RV1	000324 SD4
0006	R	000000 SPH	000002 STH
0003	R	000016 ST1	000071 TB
0006	R	000011 SVH	000021 SUI
0004	R	010325 TDQ	000171 TG
0000	R	000216 T6HP	000033 TGH
0003	R	000035 THETR	000012 THETE
0000	R	000044 TJA	000022 THP
0004	R	012676 TGA	000143 TSA
0001	R	000611 200L	000707 210L
0001	R	001037 250L	001272 300L
0001	R	001565 515L	001624 520L
0001	R	001757 575L	002007 600L
0001	R	002332 825L	002356 830L
0000	R	000284 950F	00074 960F
0000	R	007625 DAG	000170 DB
0000	R	000067 DGA	000076 DGB
0000	R	000017 DHE	00014 DHN
0000	R	00001 DJE	000046 DJN
0000	R	000150 DPXG	000071 DPXGA
0000	R	000152 DPXS	000144 DPXSA
0000	R	000172 DPX4A	000021 DPY
0000	R	000072 DPYGA	000101 DPYGB
0000	R	000145 DPYSA	000132 DPYSR
0004	R	02670 DG	012 75 DGA
0000	R	000142 DSA	000127 DSB
0000	R	000111 DTXA	000120 DTXB
0000	R	000055 DTXJA	000064 DTXJR
0000	R	000155 DTX4	000 03 DTX4A
0000	R	000121 DTY5	000155 DTYG
0000	R	000065 DTYJB	000157 DTY5
0000	R	000204 DTY4A	000175 DTY4B
0003	R	000047 DZ	000105 D1
0003	R	000051 EPS	000000 FAC
0003	R	000037 F10B	000031 G
0000	R	000040 HA	000041 HB
0000	R	000140 HSA	000125 HSB
0000	I	000036 IHA	000037 IHB
0000	I	000137 IHSA	000124 IHSB
0003	I	000007 IOTEM1	000001 IOTEM2
0003	I	000003 LOOK	000042 MIN
0003	I	000003 NMCOP	000043 NMORE
0000	R	000157 PB	010065 PDG
0000	R	000031 PGB	000 14 PGBP
0000	R	000011 PHIN	000034 PH1R
0000	R	000217 PHP	000042 PJA
0004	R	012667 P0	000 12 74 P0A
0000	R	000141 PSA	000126 PSB
0000	R	000113 P2	000160 P4
0003	R	000011 RP1	000013 RT1
0003	R	000015 SD1	000507 SD2
0000	R	000206 SP2	000240 SP4
0005	R	004101 ST4	000010 SUH
0000	R	000200 TA	007745 TAG
0000	R	000070 TGA	000077 TGB
0000	R	000010 THE	000474 THET
0003	R	000030 THE1P	000015 THN
0000	R	000052 TJE	000047 TJN
0006	R	000005 TRH	000211 TS

***** SCINOD *****

```

0000 R 000130 TSB
0000 R 000115 T2
0004 R 012035 UQ
0006 R 000006 URH
0000 R 000024 VH
0003 000005 XMJD
0000 R 000003 TSH
0000 R 000162 T4
0000 R 000034 UGH
0004 R 012700 VA
0003 000046 VL
0004 R 005605 TSP
0005 R 001541 T4D
0000 R 000023 UH
0004 R 011715 VAG
0004 R 012673 VQ
0000 R 000'05 T7
0004 R 012677 UA
0004 R 012672 UG
0000 R 000035 VGH
0006 R 000007 VRH
    
```

```

00101 1* SUBROUTINE SCINOD
00101 2* COMPUTES VALUES P,D,T,U,V AND SHEAR DUH,DVH FROM INPUT AND
00101 3* ARRAYS IN COMMON PDTCOM. INPUT TO SCINOD IS:
00101 4* G = GRAVITY AT POSITION
00101 5* PHIR = LATITUDE (RADIAN)
00101 6* F10 = F10.7 SOLAR FLUX
00101 7* AP = SOLAR-GEOMAGNETIC A SUB P INDEX
00101 8* MN/IDA/YR = DATA (YR = FULL YEAR-1900)
00101 9* IHR:MIN = TIME
00101 10* PHIR = PREVIOUS LATITUDE
00101 11* RP1,RD1,RT1 = PREVIOUS RANDOM PERTURBATIONS
00101 12* SP1,SD1,ST1 = PREVIOUS RANDOM STANDARD DEVIATIONS (SIGMAS)
00101 13* RU1,RV1 = PREVIOUS RANDOM WINDS
00101 14* SU1,SV1 = PREVIOUS RANDOM WIND SIGMAS
00103 15* COMMON/IOTEMP/IOTEM1,IOTEM2,IUG,NMCOP,DD,XMJD,PHI1,PHI,
00103 16* $ MN, IDA, IYR, H1, PHIR,THEIR,G,RI,H,PHIR,THEIR,F10,F10B,AP,
00103 17* . IHR,MIN,NMOR,DX,HL,VL,DZ,B,EP,IOPP,LOOK,IET
00103 18* . COMMON/PDTCOM/IU4,MONTH,IOPR,PG(18,19),TG(18,19)
00104 19* . PSP(8,10,12)
00104 20* . DSF(8,10,12),TSP(8,10,12),PAQ(16,5),DAQ(16,5),TAG(16,5),
00104 21* . PDQ(16,5),DDQ(16,5),TDQ(16,5),PR(20,10),DR(20,10),TR(20,10),
00104 22* . JAG(16,5),VAG(16,5),UDQ(16,5),VDQ(16,5),UR(25,10),PRQ,DG,TQ,UQ,VQ
00104 23* . ,PGA,DGA,TGA,UAVA
00104 24* . COMMON /C4/ GLON(16),NG,P4D(16,26),D4D(16,26),T4D(16,26),
00105 25* . SP4(16,26),SD4(16,26),ST4(16,26),THET1,THET
00105 26* DIMENSION VR(25,10)
00106 27* COMMON/COMP/SPH,SDH,STH,PRH,DRH,TRH,URH,VRH,SUH,SVH
00107 28* C.....THE PRESENT SCIDAT TAPE HAS UR=VR. IF THESE ARE MADE DIFFERENT,
00107 29* C REMOVE THIS EQUIVALENCE AND PLACE VR(25,10) INTO COMMON PDTCOM
00107 30* C EQUIVALENCE (UR(1,1),VR(1,1))
00110 31* FAC = 57.2957795 G.....FACTOR FOR RADIAN TO DEGREE
00111 32* PG=0.
00112 33* DG=0.
00113 34* TQ=0.
00114 35* PRH=0.
00115 36* DRH=0.
00116 37* TRH=0.
00117 38* URH=0.
00120 39* VRH=0.
00121 40* UQ=0.
00122 41* VQ=0.
00123 42* PQA=0.
00124 43* DQA=0.
00125 44* TQA=0.
00126 45* UA=0.
00127 46* VA=0.
00130 47*
    
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***** SCINOD *****
00131 48* PSH=0.
00132 49* PSH=0.
00133 50* TSH=0.
00134 51* MONTH=MN
00135 52* PHI = PHIR*FAC @.....RANGE OF ALTITUDE, DEG
00136 53* THE1 = THE1*FAC @.....PRESENT LONGITUDE, DEG
00137 54* PHI1 = PHIR*FAC @.....PRESENT LONGITUDE, DEG
00140 55* THE11 = THE1R*FAC @.....PRESENT LONGITUDE, DEG
00140 56* C.....FCORY = NORTH COMPONENT CORR IS FACTOR TIMES DISTANCE FOR
00140 57* C 5 DEGREES OF LATITUDE
00141 58* FCORY=(100.*RI*SIN(PHIR))/FAC*FAC
00142 59* IF (ABS(FCORY).LE.0.0) FCORX=0.01
00142 60* C.....FCORX = EAST COMPONENT, CORRECTED TIMES DISTANCE FOR
00142 61* C 5 DEGREES OF LONGITUDE
00144 62* FCORX=FCORY*COS(PHIR)
00144 63* C.....IN JACCHIA OR MIXED GROVES-JACCHIA HEIGHT RANGE
00145 64* 8 IF (H.LE.90.0) GO TO 10
00145 65* C.....IN 4-D DATA HEIGHT RANGE
00147 66* IF (H.LE.25.0) GO TO 500
00151 67* 30 TO 200 @.....IN GROVES OR MIXED GROVES-4D HEIGHT RANGE
00151 68* C.....IN MIXED JACCHIA-GROVES RANGE NEED TO FAIR DATA
00152 69* 10 IF (H.LT.115.) GO TO 20
00152 70* C.....FOLLOWING IS THE PURE JACCHIA HEIGHT RANGE SECTION
00152 71* C.....JACCHIA VALUES AT CURRENT POSITION
00154 72* CALL JACCH(H,PHIR,THE1,PH,OH,TH)
00155 73* PHIR = PHIR + 5. / FAI
00156 74* THE1 = THE1 - 5.
00156 75* C.....JACCHIA VALUES AT CURRENT POSITION WITH DEGREES LAT, FOR DP/DY AND
00157 76* C DT/DY
00157 77* CALL JACCH(H,PHIN,THE1,PH,N,PHN,THN)
00157 78* C.....JACCHIA VALUES AT CURRENT POSITION-5 DEGREES LON, FOR DP/DX AND
00157 79* C DT/DX
00160 80* CALL JACCH(H,PHIR,THE1,PHE,DHE,THE)
00161 81* DPY=PHN-PH @.....DP/DY FOR GEOSTROPHIC WIND
00162 82* DPX=PHE-PH @.....DP/DX FOR GEOSTROPHIC WIND
00163 83* UH=-DPY/(FCORY*DH) @.....EASTWARD GEOSTROPHIC WIND COMPONENT
00164 84* VH=-DPX/(FCORX*DH) @.....NORTHWARD GEOSTROPHIC WIND COMPONENT
00165 85* DTX = THE - TH @.....DT/DY FOR THERMAL WIND SHEAR
00166 86* DTY = THN - TH @.....DT/DY FOR THERMAL WIND SHEAR
00166 87* C.....DUH = THERMAL WIND SHEAR EASTWARD COMPONENT
00167 88* DUH = -(G * DTY) / (FCORY * TH)
00167 89* C.....DVH = THERMAL WIND SHEAR NORTHWARD COMPONENT
00170 90* DVH = (G * DTX) / (FCORX * TH)
00171 91* @.....CHANGE NOTATION FOR OUTPUT
00172 92* PGH=PH
00173 93* DGH=DH
00174 94* TGH=TH
00175 95* UGH=UH
00176 96* VGH=VH
00177 97* GO TO 800 @.....GO TO RANDOM PERTURBATIONS SECTION
00177 98* C.....FOLLOWING IS THE MIXED JACCHIA-GROVES HEIGHT RANGE SECTION
00200 99* IHA = 5*(INT(H)/75) @.....LOWER HEIGHT INDEX
00201 100* IHB = IHA + 5 @.....UPPER HEIGHT INDEX
00201 101* HA = IHA*1. @.....LOWER HEIGHT FOR INTERPOLATION
00202 102* HB = IHB*1. @.....UPPER HEIGHT FOR INTERPOLATION
00203 103* C.....JACCHIA VALUES AT LOWER HEIGHT, CURRENT LAT-LON
00204 104* CALL JACCH(HA,PHIR,THE1,PLA,PUA,TJA)
PHIN = PHIR + 5. / FAI

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SCI04160
SCI04170
SCI04180
SCI04190
SCI04200
SCI04300
SCI04400
SCI04500
SCI04600
SCI04700
SCI04800
SCI04900
SCI04950
SCI05000
SCI05100
SCI05200
SCI05300
SCI05400
SCI05500
SCI05600
SCI05700
SCI05800
SCI05900
SCI06000
SCI06100
SCI06200
SCI06300
SCI06400
SCI06500
SCI06600
SCI06700
SCI06800
SCI06900
SCI07000
SCI07100
SCI07200
SCI07300
SCI07400
SCI07500
SCI07600
SCI07700
SCI07800
SCI07900
SCI08000
SCI08100
SCI08200
SCI08300
SCI08400
SCI08500
SCI08600
SCI08700
SCI08900
SCI09000
SCI09100
SCI09200
SCI09300
SCI09400

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***** SCINOD *****
00205 105* THETE = THET - 5.
00205 106* JACCHIA VALUES AT LOWER HEIGHT, CURRENT LAT-LON+5 DEGREES
00205 107* LAT, FOR DP/DY AND DT/DY
00206 108* CALL JACCH(HA,PHIN,THET,PJN,DJN,TJN)
00206 109* JACCHIA VALUES AT LOWER HEIGHT, CURRENT LAT-LON-5 DEGREES
00206 110* LON, FOR DP/DX, AND DT/DX
00207 111* CALL JACCH(HA,PHIR,THETE,PJE,DJE,TJE)
00210 112* JACCHIA DP/DY AT LOWER HEIGHT
00211 113* JACCHIA DP/DY AT LOWER HEIGHT
00212 114* JACCHIA DT/DX AT LOWER HEIGHT
00213 115* JACCHIA DT/DY AT LOWER HEIGHT
00213 116* JACCHIA DT/DY AT LOWER HEIGHT
00214 117* JACCHIA VALUES AT UPPER HEIGHT, CURRENT LAT-LON
00215 118* CALL JACCH(HB,PHIR,THET,PJB,DJB,TJB)
00216 119* PHIN = PHIR + 5. / FAC
00216 120* THETE=THETE-5
00217 121* JACCHIA VALUES AT UPPER HEIGHT, CURRENT LAT/LON+5 DEGREES
00217 122* LAT, FOR DP/DY AND DT/DY
00217 123* CALL JACCH(HR,PHIR,THET,PJN,DJN,TJN)
00217 124* JACCHIA VALUES AT UPPER HEIGHT, CURRENT LAT-LON-5 DEGREES
00217 125* LON, FOR DP/DX AND DT/DX
00220 126* CALL JACCH(HB,PHIR,THETE,PJE,DJE,TJE)
00221 127* DPXJB = PJE - PJB @.....JACCHIA DP/DX FOR GEOSTROPHIC WINDS
00222 128* DPYJB = PJN - PJB @.....JACCHIA DP/DY FOR GEOSTROPHIC WINDS
00223 129* DTXJR = TJE - TJB @.....JACCHIA DT/DX FOR THERMAL WIND SHEAR
00224 130* DTYJR = TJN - TJB @.....JACCHIA DT/DY FOR THERMAL WIND SHEAR
00225 131* GROVES AT LOWER HEIGHT, TO RE FAIRED WITH JACCHIA
00225 132* CALL GTERP(IHA,PHI,PGA,DGA,TGA,PGA,DTGA,DTYGA,DTXGA,DTYGA)
00226 133* GROVES AT UPPER HEIGHT, TO RE FAIRED WITH JACCHIA
00226 134* CALL GTERP(IHB,PHI,PGA,DGB,TGB,PGA,DTGB,DTYGB,DTXGB,DTYGB)
00227 135* FAIRED RESULTS AT LOWER HEIGHT
00227 136* CALL FAIR(PGA,DGA,TGA,PJA,DJA,TJA,IHA,PI,DI,T1,DPXGA,DPYGA,
00227 137* DPXJA,DPYJA,DPXA,DPYA,DTXGA,DTYGA,DTXJA,DTYJA,DTXA,DTYA)
00230 138* FAIRED RESULTS AT UPPER HEIGHT
00230 139* CALL FAIR(PGB,DGB,TGB,PJR,DJR,TJR,IHR,P2,D2,T2,DPXGR,DPYGR,
00230 140* DPXJR,DPYJR,DPXR,DPYR,DTXGR,DTYGR,DTXJR,DTYJR,DTXR,DTYR)
00231 141* HEIGHT INTERPOLATION ON FAIRED P,D,T
00231 142* CALL INTER2(P1,DI,T1,Ha,P2,D2,T2,HB,PH,DH,TH,H)
00232 143* HEIGHT INTERPOLATION ON FAIRED DP/DX,DP/DY
00232 144* CALL INTERW(DPXA,DPYA,HA,DPXB,DPYB,HB,DPX,DPY,H)
00233 145* HEIGHT INTERPOLATION ON FAIRED DT/DX,DT/DY
00233 146* CALL INTERW(DTXA,DTYA,HA,DTXR,DTYB,HB,DTX,DTY,H)
00233 147* EASTWARD COMPONENT OF GEOSTROPHIC WIND
00234 148* UH = -DPY / (FCORY * DH)
00235 149* NORTHWARD COMPONENT OF GEOSTROPHIC WIND
00235 150* VH = DPX / (FCORX * DH)
00236 151* EASTWARD COMPONENT OF THERMAL WIND SHEAR
00236 152* DUH = -(G * DTY) / (FCORY * TH)
00236 153* NORTHWARD COMPONENT OF THERMAL WIND SHEAR
00237 154* DVH = (G * DTX) / (FCORX * TH)
00240 155* PGR=PH
00241 156* DGR=DH
00242 157* TGR=TH
00243 158* UGR=UH
00244 159* VGR=VH
00245 160* GO TO 800
00246 161* *****GO TO RANDOM PERTURBATIONS SECTION
*****THE FOLLOWING SECTION IS FOR GROVES OR MIXED GROVES 4D HEIGHTS
200 IHB3 = 5*(INT(H)/5) + 5 @.....UPPER HEIGHT INDEX

```

```

SCI09500
SCI09600
SCI09700
SCI09800
SCI09900
SCI10000
SCI10100
SCI10200
SCI10300
SCI10400
SCI10500
SCI10600
SCI10700
SCI10800
SCI10900
SCI11000
SCI11100
SCI11200
SCI11300
SCI11400
SCI11500
SCI11600
SCI11700
SCI11800
SCI11900
SCI12000
SCI12100
SCI12200
SCI12300
SCI12400
SCI12500
SCI12600
SCI12700
SCI12800
SCI12900
SCI13000
SCI13100
SCI13200
SCI13300
SCI13400
SCI13500
SCI13600
SCI13700
SCI13800
SCI13900
SCI14000
SCI14100
SCI14200
SCI14300
SCI14400
SCI14500
SCI14600
SCI14700
SCI14800
SCI14900
SCI15000
SCI15100

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***** SCINOD *****
00247 162* HGB = IHGB*1. @.....UPPER HEIGHT
00247 163* C.....GROVES AT UPPER HEIGHT
00250 164* CALL GTERP(IHGB,PHI,@G@,DGA,TGA,HGA,PGB,DGR,TGR,HGB,PGB,DGH,TGH,H)
00250 165* C.....STATIONARY PERTURBATION HEIGHT = 40
00251 166* IF (H.LT.40.0) GO TO 210
00251 167* C.....UPPER STATIONARY PERTURBATION HEIGHT = 90
00253 168* IF (H.GT.84.0) GO TO 220
00253 169* C.....UPPER STATIONARY PERTURBATION HEIGHT = 52,60,68,76,OR 84
00255 170* IHGB = 8*((INT(H) + 4)/8) + 4
00255 171* C.....UPPER STATIONARY PERTURBATION HEIGHT = 52
00256 172* IF (IHGB.LT.52.0) IHGB = 52
00260 173* GO TO 230
00261 174* 210 IHGB = 10*(INT(H)/10) + 10
00262 175* GO TO 230
00263 176* 220 IHGB = 90
00264 177* 230 HSB = IHGB*1. @.....UPPER STATIONARY PERTURBATION HEIGHT
00264 178* C.....STATIONARY PERTURBATIONS AT UPPER HEIGHT
00265 179* CALL PDTUV(PSP,DSP,TSP,PHI,THET,IHSR,PSB,DSB,ISA,DPXSB,DPYSA,
00265 180* $ DTXSA,DTYSA)
00266 181* IF (H.LT.30.0) GO TO 300 @.....MIXED GROVES 40 SECTION
00270 182* IHGA = IHGB - 5 @.....LOWER HEIGHT INDEX
00271 183* HGA = IHGA*1. @.....LOWER HEIGHT INDEX
00271 184* C.....GROVES AT LOWER HEIGHT
00272 185* CALL GTERP(IHGA,PHI,PGA,DGA,TGA,HGA,PGB,DGR,TGR,HGB,PGB,DGH,TGH,H)
00272 186* C.....LOWER STATIONARY PERTURBATION HEIGHT = 30
00273 187* IF (H.LT.40.0) GO TO 240
00273 188* C.....LOWER STATIONARY PERTURBATION HEIGHT = 52,60,68,76, OR 84
00275 189* IHSA = 8*((INT(H) + 4)/8) - 4
00275 190* C.....LOWER STATIONARY PERTURBATIONS HEIGHT = 40
00276 191* IF (IHSA.LT.40.0) IHSA = 40
00300 192* GO TO 250
00301 193* 240 IHSA = 30
00302 194* 250 ISA = IHSA*1. @.....LOWER STATIONARY PERTURBATION HEIGHT
00302 195* C.....STATIONARY PERTURBATIONS AT LOWER HEIGHT
00303 196* CALL PDTUV(PSP,DSP,TSP,PHI,THET,IHSA,PSA,DSA,ISA,DPXSA,DPYSA,
00303 197* $ DTXSA,DTYSA)
00303 198* C.....GROVES VALUES HEIGHT INTERPOLATIONS
00304 199* CALL INTER2(PGA,DGA,TGA,HGA,PGB,DGR,TGR,HGB,PGB,DGH,TGH,H)
00304 200* C.....STATIONARY PERTURBATION HEIGHT INTERPOLATION
00305 201* CALL INTER(PSA,DSA,ISA,HSA,PSB,DSB,ISR,HSB,PSH,DSH,TSB,H)
00306 202* CALL OROGEN @.....QUASI-BIENNIAL VALUES
00306 203* C.....UNPERTURBED (MONTHLY MEAN) VALUES FOR OUTPUT
00307 204* TGH = TGH * (1. + T54)
00310 205* PGH = PGH * (1. + P54)
00311 206* DGH = DGH * (1. + D54)
00311 207* C.....UNPERTURBED VALUES PLUS 0.0 PERTURBATIONS
00312 208* PH = (1. + PQ) * PGH
00313 209* DH = DGH * (1. + DQ)
00314 210* TH = (1. + TQ) * TGH
00314 211* C.....HEIGHT INTERPOLATION OF GROVES DP/DX AND DP/DY
00315 212* CALL INTER(DPXGA,DPYGA,PGA,DGA,DPXGB,DPYGB,HGB,DGX,DGY,H)
00315 213* C.....HEIGHT INTERPOLATION OF STATIONARY PERTURBATION DP/DX AND DP/DY
00316 214* CALL INTER(DPXSA,DPYSA,HSA,PSA,DPXSB,DPYSB,HSB,DPXS,DPYS,H)
00316 215* C.....HEIGHT INTERPOLATION OF GROVES DT/DX AND DT/DY
00317 216* CALL INTER(DTXGA,DTYGA,HGA,DTXGB,DTYGB,HGB,DTXG,DTYG,H)
00317 217* C.....HEIGHT INTERPOLATION OF STATIONARY PERTURBATION DT/DX AND DT/DY
00320 218* CALL INTERW(DTXSA,DTYSA,HSA,DTXSB,DTYSB,HSB,DTXS,DTYS,H)

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SCIMQD

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00321 DTX = DTG + DTXS * TGHQ.....TOTAL DT/DX
00322 DTY = DTYG + DTYS * TGHQ.....TOTAL DT/DY
00323 C.....THERMAL WIND SHEAR, EASTWARD COMPONENT
00324 DUH = -(G * DTY) / (FCORX * TH)
00325 C.....THERMAL WIND SHEAR, NORTHWARD COMPONENT
00326 DVH = (G * DTX) / (FCORX * TH)
00327 DPX = DPXG + DPXS * PGH Q.....TOTAL DP/DX
00328 DPY = DPG + DPYS * PGH Q.....TOTAL DP/DY
00329 C.....EASTWARD COMPONENT GEOSTROPHIC WIND
00330 UGH=-DPY/(FCORX*CH)
00331 C.....NORTHWARD COMPONENT GEOSTROPHIC WIND
00332 VGH=DPX/(FCORX*DH)
00333 UH=UGH+UG Q.....GEOSTROPHIC WIND PLUS Q80 WIND PERTURBATIONS
00334 VH=VGH+VG
00335 GO TO 800 Q.....GO TO RANDOM PERTURBATIONS SECTION
00336 C.....THE FOLLOWING IS THE MIXED GROVES 4D SECTION
00337 C.....GENERATE GRID OF 4D PROFILES IF PREVIOUS HEIGHT GE 30
00338 300 IF (H1.GE.30..OR..LOOK.EQ.1) CALL GEN4D
00339 C.....LAT-LON INTERPOLATION OF 4D DATA AT 25 KM
00340 CALL INTER4(GLAT,GLON,PHI,THET,25,NG,P4D,D4D,T4D,P4A,D4A,T4A,
00341 $ DPX4,DPY4,DTX4,DTY4)
00342 PB = PGB*(1. + PSB) Q.....GROVES PLUS STATIONARY PERTURBATION:
00343 DR = DGB*(1. + DSB) Q P,D,T
00344 TB = TGB*(1. + TSB)
00345 DPX3 = DPXGB + DPXSR * PB Q.....GROVES PLUS STATIONARY
00346 DPY3 = DPG3B + DPG3SR * PB Q PERTURBATIONS: DP/DX,DP/DY,
00347 DTX3 = DTXGB + DTXSB * TB Q DT/DX,DT/DY
00348 DTY3 = DTYGB + DTYSR * TB
00349 C.....HEIGHT INTERPOLATION BETWEEN 4D AT 25 AND GROVES AT UPPER HEIGHT
00350 C DP/OX AND DT/DY
00351 CALL INTERW(DPX4,DPY4,DTX4,DTY4,25,DPX3,DPY3,HSB,DPX,DPY,H)
00352 C.....HEIGHT INTERPOLATION BETWEEN 4D AT 25 AND GROVES AT UPPER HEIGHT
00353 C P,D,T
00354 CALL INTER2(P4A,D4A,T4A,25,,PB,DB,TB,HGB,PGH,DGH,TGH,H)
00355 C.....HEIGHT INTERPOLATION BETWEEN 4D AT 25 AND GROVES AT UPPER HEIGHT
00356 C DT/OX AND DT/DY
00357 CALL INTERW(DTX4,DTY4,25,DTX3,DTY3,HSB,DTX,DTY,H)
00358 PHEPGH*(1.+PQ) Q.....ADD Q80 PERTURBATIONS TO P,D,T
00359 QHEDGH*(1.+DQ)
00360 THETGH*(1.+TQ)
00361 UGH=-DPY/(FCORX*DH) Q.....GEOSTROPHIC WIND COMPONENTS
00362 VGH=DPX/(FCORX*DH)
00363 C.....THERMAL WIND SHEAR COMPONENTS
00364 DUH = -(G * DTY) / (FCORX * TH)
00365 DVH = (G * DTX) / (FCORX * TH)
00366 UH=UGH+UG Q.....ADD Q80 WIND PERTURBATIONS TO WIND
00367 VH=VGH+VG
00368 GO TO 800 Q.....GO TO RANDOM PERTURBATIONS SECTION
00369 500 IF (H.GE.0.0) GO TO 510
00370 IF (H.LT.-0.005) GO TO 505
00371 H = 0. Q.....IF -5 METER LE H LT 0 , H IS SET TO 0
00372 505 NMORE = 0 Q.....NO MORE COMPUTATIONS TO BE MADE IF HEIGHT LT -5 M
00373 RETURN
00374 C.....GENERATE GRID OF 4D PROFILES IF PREVIOUS HEIGHT GE 30
00375 510 IF (H1.GE.30..OR..LOOK.EQ.1) CALL GEN4D

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REPRODUCIBILITY OF THE ORIGINAL PAGE IS POOR

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***** SCIN30 *****
00376 276* IHA = INT(H) @.....LOWER HEIGHT INDEX
00377 277* IA = IHA*1. @.....L...R HEIGHT INDEX
00400 278* IHB = IHA + 1 @.....UPPER HEIGHT INDEX
00401 279* IF (IHA.GT.25) IHB = 25
00403 280* IB = IHB*1. @.....UPPER HEIGHT
C.....LAT-LON INTERPOLATION OF 4D VALUES AT UPPER HEIGHT
00403 281* 515 CALL INTER4(GLAT,GLON,PHI,THET,IHA,NG,P4D,D4D,T4D,
00404 282* $ DPX4B,DPY4B,DTX4B,DTY4B)
00405 283* IF (IHA.EQ.0.AND.PB*DB*TB.LE.0.) GO TO 520
00407 284* GO TO 540
00410 285* 520 IHB=IHB+1
00410 286* C.....LOOP TO FIND LOWEST VALID HEIGHT
00411 287* HB=HR+1.
00412 288* GO TO 515
00413 289* 540 IF (IHA.GT.0) CALL INTER4(GLAT,GLON,PHI,THET,IHA,NG,P4D,D4D,T4D,
00413 290* IPA,DA,TA,DPX4A,DPY4A,DTX4A,DTY4A)
00415 291* IF (IHA.EQ.0.OR.(PA*DA*TA.LE.0.AND.IHA.LT.10.AND.PB*DB*TB.GT.0.))
00415 292* 130 TO 550
00415 293* GO TO 550
00417 294* 550 CALL INTER4(GLAT,GLON,PHI,THET,0,NG,P4D,D4D,T4D,
00420 295* ,PA,DA,TA,DPX4A,DPY4A,DTX4A,DTY4A)
00420 296*
00421 297* 560 TZ=(TA-TB)/ALOG(TA/TB)
00424 298* GO TO 575
00425 299*
00426 300* 570 TZ=TA
C...COMPUTES HEIGHT OF SURFACE
00426 301* 575 IA=HB+0.28705*TZ*ALOG(PB/PA)/G
00430 302* IF (H.GT.HA) GO TO 600
00430 303* PH=0.
00432 304* DHE=0.
00433 305* THE=0.
00434 306* DHEC=0.
00435 307* DGM=0.
00436 308* TGH=0.
00437 309* GO TO 800
00440 310* C.....LAT-LON INTERPOLATION OF 4D VALUES AT LOWER HEIGHT
00440 311* C.....HEIGHT INTERPOLATION OF P,D,T
00441 312* 600 CALL INTER2(PA,DA,TA,HA,PB,DP,IB,PGH,DGH,TGH,H)
00442 313* PH=PGH
00442 314* DHE=DGH
00443 315* THE=TGH
00444 316* C.....HEIGHT INTERPOLATION OF DP/DX AND DP/DY
00444 317* CALL INTER(DPX4A,DPY4A,HA,DPX4B,DPY4B,HB,DPX,DPY,H)
00445 318* C.....HEIGHT INTERPOLATION OF DT/DX AND DT/DY
00445 319* CALL INTER(DTX4A,DTY4A,HA,DTX4B,DTY4B,HB,DTX,DTY,H)
00446 320* PH = PGH
00447 321* DH = DGH
00450 322* TH = TGH
00451 323* IF (PH*DH*TH.LE.0.) GO TO 800
00452 324* UGHE=DPY/(FCORY*DH)
00454 325* UGHE=DPX/(FCORY*DH)
00455 326* UH = UGH @.....GEOSTROPHIC WIND COMPONENTS
00456 327* VH = UGH @.....CHANGE OF NOTATION FOR OUTPUT
00457 328* C.....THERMAL WIND SHEAR COMPONENTS
00460 329* DUH = -(G * DTY) / (FCORY * TH)
00461 330* DVH = (G * DTX) / (FCORY * TH)
00462 331* IF (H,LT.15.) GO TO 800 @.....@80=0 IF H LT 15
00462 332*

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SC126600
 SC126700
 SC126800
 SC126900
 SC127000
 SC127400
 SC127500
 SC127600
 SC127603
 SC127606
 SC127609
 SC127612
 SC127615
 SC127618
 SC127622
 SC127624
 SC127627
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 SC127633
 SC127636
 SC127639
 SC127642
 SC127645
 SC127648
 SC127651
 SC127654
 SC127657
 SC127660
 SC127663
 SC127666
 SC127669
 SC127672
 SC127675
 SC127678
 SC127681
 SC127684
 SC1278YX
 SC127800
 SC127830
 SC127860
 SC127890
 SC127900
 SC12A000
 SC12A100
 SC12A200
 SC128300
 SC128400
 SC128500
 SC128550
 SC128600
 SC128700
 SC12A800
 SC12A900
 SC129000
 SC129100
 SC129200
 SC129300

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***** SCIMOD *****
00464 333* CALL BPOGEN 9.....COMPUTES QUASI-BIENNIAL PERTURBATIONS
00465 334* PHEFGH*(1.+PO) 9.....ADDS QRO PERTURBATIONS TO P,D,T
00466 335* THEFGH*(1.+PO)
00467 336* THEFGH*(1.+PO)
00470 337* THEUGH+UQ 9.....ADDS QBO WIND PERTURBATIONS TO U,V
00471 338* VHEVGH+VQ
00471 339* C.....THE FOLLOWING IS THE RANDOM PERTURBATIONS SECTION
00471 340* C.....NO RANDOM PERTURBATIONS IF IOPR GT 1
00472 341* 800 IF (IOPR,GT,1) GO TO 830
00472 342* C.....INTERPOLATES RANDOM WIND MAGNITUDES TO HEIGHT H, LATITUDE PHI
00474 343* CALL INTRUV(UH,VR,H,PHI,SUH,SVH)
00474 344* C.....IF H LE .25 USE 4D DATA RANDOM P,D,T SIGMAS
00475 345* IF (H,LE,.25) GO TO 810
00475 346* C.....INTERPOLATE PR,DR,TR ARRAYS TO GET P,D,T SIGMAS AT HEIGHT H,
00477 347* C LATITUDE PHI
00477 348* CALL RTERP(H,PHI,PR,DR,TR,SPH,SDH,STH)
00500 349* GO TO 820
00500 350* C.....LAT-LON INTERPOLATION ON P,D,T SIGMAS AT LOWER HEIGHT
00501 351* 810 CALL INTER4(GLAT,GLON,PHI,THET,HA,NG,SP4,SD4,ST4,SP1,SD1,ST1,
00501 352* $ DPX,DY,DIX,DIV)
00501 353* C.....LAT-LON INTERPOLATION ON P,D,T SIGMAS AT UPPER HEIGHT
00502 354* CALL INTER4(GLAT,GLON,PHI,THET,HA,NG,SP4,SD4,ST4,SP2,SD2,ST2,
00502 355* $ DPX,DY,DIX,DIV)
00502 356* C.....HEIGHT INTERPOLATION OF SIGMAS
00502 357* CALL INTERZ(SPI,SDI,STI,HA,SP2,SD2,ST2,HB,SPH,SDH,STH,H)
00503 358* IF (PH+DH+TH,LE,0.) GO TO 825
00504 359* C.....HEIGHT DISPLACEMENT BETWEEN PREVIOUS AND CURRENT POSITION
00504 360* 820 JZ = H1 - H
00506 361* C.....COMPUTES HORIZONTAL DISPLACEMENT DX BETWEEN PREVIOUS AND CURRENT
00506 362* C POSITION, HORIZONTAL SCALE HL, AND VERTICAL SCALE VL
00507 363* CALL DXHLVL
00507 364* C.....COMPUTES PERTURBATION VALUES PRH,DRH,TRH,URH AND VRH
00510 365* CALL PERTRB
00511 366* PH = PH*(1. + PRH) 9.....ADDS RANDOM PERTURBATIONS TO PH,DH,TH
00512 367* JH = DH*(1. + DRH)
00513 368* TH = TH*(1. + TRH)
00514 369* UH=UH+URH 9.....ADDS RANDOM WINDS TO UH,VH
00515 370* VH=VH+VRH
00515 371* C.....SETS PREVIOUS RANDOM PERTURBATION IN P,D,T TO CURRENT
00515 372* C PERTURBATIONS, FOR NEXT CYCLE
00516 373* 825 RP1 = PRH
00517 374* RD1 = DRH
00520 375* RT1 = TRH
00520 376* C.....SETS PREVIOUS MAGNITUDES FO CURRENT VALUES, FOR NEXT CYCLE
00521 377* SP1=SPH
00522 378* SD1 = SDH
00523 379* ST1=STH
00523 380* C.....SETS PREVIOUS WIND PERTURBATION VALUES TO CURRENT VALUES,
00523 381* C FOR NEXT CYCLE
00524 382* RU1=URH
00525 383* RV1=VRH
00525 384* C.....SETS PREVIOUS WIND PERTURBATION MAGNITUDES TO CURRENT VALUES,
00525 385* C FOR NEXT CYCLE
00526 386* SU1=SUH
00527 387* SV1=SVH
00527 388* C.....SETS PREVIOUS HEIGHT TO CURRENT HEIGHT, FOR NEXT CYCLE
00530 389* 830 H1 = H

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***** SCIMOD *****
390* 00530
391* 00531
392* 00531
393* 00532
394* 00533
395* 00533
396* 00534
397* 00536
398* 00537
399* 00541
400* 00542
401* 00543
402* 00544
403* 00545
404* 00546
405* 00547
406* 00550
407* 00551
408* 00552
409* 00553
410* 00554
411* 00555
412* 00556
413* 00557
414* 00560
415* 00561
416* 00562
417* 00563
418* 00564
419* 00565
420* 00566
421* 00567
422* 00570
423* 00571
424* 00572
425* 00573
426* 00574
427* 00575
428* 00576
429* 00577
430* 00577
431* 00577
432* 00656
433* 00656
434* 00656
435* 00656
436* 00657
437* 00661
438* 00661
439* 00701
440* 00702
441* 00720
442* 00721
443* 00722
444* 00723

C.....SETS PREVIOUS LATITUDE TO CURRENT LATITUDE, FOR NEXT CYCLE
PHI=PHI-R
C.....SETS PREVIOUS LONGITUDE TO CURRENT LONGITUDE, FOR NEXT CYCLE
THEIR=THEIR
C.....NO MORE DATA IF P, Q, OR T LEG 0
IF (PH*DH*TH,LE,0.) RETURN
CALL STDATM(H,TS,PS,DS)
IF ((PS*DS*TS).GT,0.) GO TO 870
DGRP=0.
TGRP=0.
PHP=0.
JHP=0.
THP=0.
GO TO 880
870 PGRP=100.*(PGH-PS)/PS
DGRP=100.*(DGH-DS)/DS
TGRP=100.*(TGH-TS)/TS
PHP=100.*(PH-PS)/PS
JHP=100.*(JH-DS)/DS
THP=100.*(TH-TS)/TS
C.....CONVERTS QBO P,Q,T TO PERCENT
Q=100.*Q
D=100.*D
T=100.*T
PRM=100.*PRH
DRH=100.*DRH
TRH=100.*TRH
DUH = DUH * 1000.
DVH = DVH * 1000.
PQA=PQA*100.
DQA=DQA*100.
TQA=TQA*100.
SPH=SPH*100.
SDH=SDH*100.
STH=STH*100.
PSH=PSH*100.
DSH=DSSH*100.
TSH=TSH*100.
WRITE(6,900)
$ DUH,DVH,IET,PGH,DGH,TGH,UGH,VGH,PH,PHI,TH,PHI,
$ VG,PQA,DQA,TQA,VA,PRH,DRH,TRH,URH,VRH,SPH,SDH,STH,SUH,SVH
900 FORMAT(1X,3F7.2,2(2F8.3,3F6.0),2F5.0/
$ 18,1X,2(2(F7.1,X),F6.1,X),11X,
$ F5.1,10X,SP,100X,3F5.1,2F5.0, QB0/100X,3F5.1,2F5.0, MAG/
$ 10X,3F5.1,2F5.0, RAND/100X,3F5.1,2F5.0, SIG/)
IF (JOPP.EQ,0) RETURN
PUNCH 950,IET,HIPHI,THEI,PGH,DGH,TGH,PGHP,DGHP,TGHP,UGH,VGH,
$ DUH,DVH
950 FORMAT(14,F5.1,2F7.2,2E8.3,F5.0,3F5.1,4F5.0,'A')
PUNCH 960,IET,HIPHI,THEI,PH,PHI,TH,PHI,PHP,PHI,THP,URH,VRH
960 FORMAT(14,F5.1,2F7.2,2E8.3,F5.0,3F5.1,2F5.0,10X,'B')
THEI=THEI*FAC
RETURN
END

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- SCI35400
- SCI35500
- SCI35600
- SCI35700
- SCI35800
- SCI35900
- SCI35910
- SCI35920
- SCI35930
- SCI35940
- SCI35950
- SCI35960
- SCI35970
- SCI35980
- SCI35990
- SCI35999
- SCI36010
- SCI36020
- SCI36030
- SCI36040
- SCI36050
- SCI36060
- SCI36100
- SCI36200
- SCI36300
- SCI36400
- SCI36500
- SCI36600
- SCI36700
- SCI36800
- SCI36810
- SCI36820
- SCI36830
- SCI36840
- SCI36850
- SCI36860
- SCI36870
- SCI36880
- SCI36890
- SCI36900
- SCI36930
- SCI36960
- SCI36990
- SCI37010
- SCI37040
- SCI37070
- SCI37100
- SCI37130
- SCI37160
- SCI37190
- SCI37300
- SCI37400

***** SCIMOD *****
 END OF COMPILATION; NO DIAGNOSTICS.
 @HDG,P ***** SELE4 *****
 @FOR,S PROFAS,SELE4,SELE4
 FOR S11E-02/04/74-18;54:51 (0,)

SUBROUTINE SELE4 ENTRY POINT 001625

STORAGE USED: CODE(1) 001644; DATA(0) 000262; RLINK COMMON(2) 000000

COMMON BLOCKS:

0003 C4 000041
 0004 IOTEMP 000002
 0005 POINT 000200
 0006 ORDER 000423

EXTERNAL REFERENCES (BLOCK, NAME)

0007 NTRAN
 0010 SORT4
 0011 COS
 0012 SIN
 0013 NERR3\$

STORAGE ASSIGNMENT (BLOCK, TYPE, RELATIVE LOCATION, NAME)

0001	001561	100L	0001	000013	1226	0001	000014	1256	0001	000025	1336	0001	000425	2206	
0001	000443	225G	0001	000521	2446	0001	000541	2476	0001	000073	30L	0001	000712	3076	
0001	000233	31L	0001	000732	3126	0001	000260	32L	0001	000360	34L	0001	000402	35L	
0001	000460	40L	0001	001305	4226	0001	001323	4276	0001	000573	45L	0001	001525	4756	
0001	000631	50L	0001	001543	5026	0001	000671	51L	0001	001566	5166	0001	000774	52L	
0001	001567	521G	0001	001040	54L	0001	001055	55L	0001	001070	70L	0001	001211	72L	
0001	001240	75L	0001	001246	74L	0001	001261	75L	0001	001267	76L	0001	001340	80L	
0001	001424	82L	0001	001443	84L	0001	001470	86L	0001	001507	88L	0001	001553	89L	
0000	R	000160	DEGRAD	0000	R	000173	DX	0005	R	000174	DY	0000	R	000166	EL
0000	I	000161	I	0000	I	000000	IC	0000	I	000163	II	0000	I	000004	IL
0000	000232	INJPS	0000	I	000175	IP	0000	I	000176	IPG	0005	I	000000	IPTN	
0006	000120	IREAD	0000	I	000162	J	0000	I	000006	JL	0000	I	000201	KI	
0000	I	000205	K2	0000	I	000200	L	0000	I	000164	LA	0000	I	000073	L1MU
0005	I	000120	LL	0000	I	000165	LO	0000	I	000202	L1	0000	I	000040	NP
0000	R	000167	PHI	0000	R	000156	PI	0000	R	000157	PI4	0003	I	000000	SCRCHI
0004	I	000001	SCRCH2	0003	R	000000	XL	0000	R	000171	XX	0000	R	000172	YY

00101 1*
 00103 2*
 00103 3*
 00103 4*
 00103 5*
 00104 6*
 00105 7*

SUBROUTINE SELE4
 COMMON/C4/XL(16),YL(16),NP

SUBROUTINE TO SELECT POINTS FOR INTERPOLATION
 COMMON /IOTEMP/ SCRCHI,SCRCH2
 COMMON /POINT/ IPT(16,5),LL(16),DXY(16,2)

SEL00100
 SEL00200
 SEL00300
 SEL00400
 SEL00500
 SEL00600
 SEL00700

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*****
SELEC+ *****
00106 8*
00106 9*
00107 10*
00110 11*
00110 12*
00110 13*
00112 14*
00112 15*
00114 16*
00114 17*
00116 18*
00116 19*
00116 20*
00117 21*
00120 22*
00121 23*
00121 24*
00124 25*
00127 26*
00127 27*
00127 28*
00127 29*
00132 30*
00132 31*
00135 32*
00136 33*
00137 34*
00140 35*
00140 36*
00142 37*
00145 38*
00145 39*
00145 40*
00145 41*
00150 42*
00151 43*
00152 44*
00153 45*
00154 46*
00155 47*
00156 48*
00157 49*
00160 50*
00161 51*
00162 52*
00163 53*
00164 54*
00166 55*
00170 56*
00172 57*
00173 58*
00175 59*
00176 60*
00177 61*
00200 62*
00202 63*
00202 64*

*****
COMMON /ORDER/ IPTN(16,5),IPEAD(65,3)
DIMENSION IC(4),IL(2),JL(2),LJML(51),LIMU(51)
DATA LJML/15,14,13,12,11,10,9,8,7,6,5,4,3,2,23*1,2,3,4,5,6,7,8,9,
110,11,12,13,14,15/
DATA LIMU/33,34,35,36,37,38,39,40,41,42,43,44,45,46,23*47,46,45,
144,43,42,41,40,39,38,37,36,35,34,33/
DATA PI/3.14159/
INTEGER SCRCH2
C INITIALIZE
C
C PI4=PI/4,
DEGRAD=PI/180,
DO 1 I=1,16
DO 1 J=1,5
1 IPT(I,J)=0
C MAJOR LOOP FOR POINTS
DO 100 II=1,NP
LA=ABS(XL(II))*10.+5
LO=YL(II)*10.+5
LL(II)=LA*1000+LO
IF (XL(II).LT.0.) LL(II)=-LL(II)
C
15 IF (XL(II)-15,1) 15,30,30
IF (XL(II) 50,40,40)
C NMC GRID
30 IPT(II,5)=2
EL=(350-YL(II))*DEGRAD
PHI=XL(II)*DEGRAD
R=31.204359052*(SIN(PI4-PHI/2.)/COS(PI4-PHI/2.))
XX=ER*COS(EL)+24.
YY=ER*SIN(EL)+26.
I=XX
J=YY
DX=XX-I
DY=YY-J
DXY(II,1)=DX
DXY(II,2)=DY
IF (XL(II).GT.17,18) GO TO 31
IF ((J.LT.1).OR.(J.GT.51)) GO TO 70
IF ((I.LT.LJML(J)).OR.(I.GT.LIMU(J))) GO TO 70
31 IC(1)=I*1000+J
IF ((ABS(DX).GT.,1).OR.(ABS(DY).GT.,1)) GO TO 32
IP=1
GO TO 35
32 CONTINUE
IF (XL(II).GT.17,18) GO TO 34
IF ((I.GT.LIMU(J)-1)).AND.((J.GE.15).AND.(J.LE.37))
1 .OR.(J.GT.50)) GO TO 70

```

```

*****
SELEC+ *****
00204 65*
00206 66*
00210 67*
00211 68*
00212 69*
00213 70*
00214 71*
00215 72*
00216 73*
00217 74*
00222 75*
00223 76*
00224 77*
00227 78*
00233 79*
00233 80*
00233 81*
00233 82*
00234 83*
00235 84*
00236 85*
00237 86*
00240 87*
00241 88*
00242 89*
00243 90*
00246 91*
00251 92*
00251 93*
00253 94*
00255 95*
00256 96*
00257 97*
00262 98*
00264 99*
00265 100*
00266 101*
00267 102*
00270 103*
00270 104*
00270 105*
00270 106*
00271 107*
00272 108*
00273 109*
00274 110*
00276 111*
00277 112*
00301 113*
00302 114*
00303 115*
00304 116*
00305 117*
00306 118*
00311 119*
00314 120*
00314 121*

IF ((I+1).GT.LIMU(J+1)).OR.(I.LT.LIML(J+1)) GO TO 80
IF ((I.EQ.LIMU(J)).OR.(I.EQ.LIML(J))) GO TO 80
34 IP=4
IC(2)=(I+1)*1000+J
IC(3)=I*1000+J+1
IC(4)=(I+1)*1000+J+1
35 CONTINUE
CALL NTRAN (SCRCH2,IJ)
CALL NTRAN (SCRCH2,22)
DO 38 IPG=1,1977
CALL NTRAN (SCRCH2,2,I,J,L)
CALL NTRAN (SCRCH2,22)
DO 38 K=1,IP
38 IF(IC(K).EQ.IJ) IPT(II,K)=IPG
GO TO 100

C
C EQUATORIAL GRID
C
40 IPT(II,5)=1
L1=XL(II)
L2=YL(II)
IL(1)=L1/5
IL(2)=IL(1)+1
JL(1)=(L2/5)+1
JL(2)=JL(1)-1
DO 45 K1=1,2
DO 45 K2=1,2
45 IF ((ABS(XL(II))-IL(K1)*5).GT.0.1).OR.(ABS(YL(II))-JL(K2)*5).GT.0.1)
1 ) GO TO 45
IF (JL(K2).EQ.72) JL(K2)=0
IPT(II,1)=JL(K2)*4+IL(K1)+1
GO TO 100
45 CONTINUE
IF (JL(1).EQ.72) JL(1)=0
IPT(II,1)=JL(1)*4+IL(1)+1
IPT(II,2)=JL(2)*4+IL(1)+1
IPT(II,3)=JL(1)*4+IL(2)+1
IPT(II,4)=JL(2)*4+IL(2)+1
GO TO 100

C
C SOUTHERN HEMISPHERE
C
50 IPT(II,5)=3
L1=XL(II)
L2=YL(II)
IF (/RS(XL(II)).LT.85.0) GO TO 51
IPT(II,1)=1
IF (ABS(XL(II)+90.).LT.0.11) GO TO 100
51 CONTINUE
IL(1)=(L1/5)-1
JL(1)=(L2/5)+1
IL(2)=IL(1)+1
JL(2)=JL(1)-1
DO 52 K1=1,2
DO 52 K2=1,2
52 IF ((ABS(XL(II))-IL(K1)*5).GT.0.1).OR.(ABS(YL(II))-JL(K2)*5).GT.0.1)
1 ) GO TO 52
SEL06500
SEL06600
SEL06700
SEL06800
SEL06900
SEL07000
SEL07100
SEL07200
SEL07300
SEL07400
SEL07500
SEL07600
SEL07700
SEL07800
SEL07900
SEL08000
SEL08100
SEL08200
SEL08300
SEL08400
SEL08500
SEL08600
SEL08700
SEL08800
SEL08900
SEL09000
SEL09100
SEL09200
SEL09300
SEL09400
SEL09500
SEL09600
SEL09700
SEL09800
SEL09900
SEL10000
SEL10100
SEL10200
SEL10300
SEL10400
SEL10500
SEL10600
SEL10700
SEL10800
SEL10900
SEL11000
SEL11100
SEL11200
SEL11300
SEL11400
SEL11500
SEL11600
SEL11700
SEL11800
SEL11900
SEL12000
SEL12100

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REPRODUCIBILITY OF THE ORIGINAL PAGE IS POOR

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00316 122*  IF (JL(K2),EQ,72) JL(K2)=1
00320 123*  IPT(II,1)=JL(K2)*17-IL(K1)+1
00321 124*  IF (IL(K1),NE,0) GO TO 100
00323 125*  IPT(II,1)=JL(K2)*+1
00324 126*  IPT(II,5)=1
00325 127*  GO TO 100
00326 128*  52 CONTINUE
00331 129*  IF (JL(1),EQ,72) JL(1)=0
00333 130*  IF (IPT(II,1),EQ,1) GO TO 54
00335 131*  IPT(II,1)=JL(1)*17-IL(1)+1
00336 132*  IPT(II,2)=JL(2)*17-IL(1)+1
00337 133*  IF (IL(2)) 55,53,55
00342 134*  IPT(II,3)=JL(1)*+1
00343 135*  IPT(II,4)=JL(2)*+1
00344 136*  IPT(II,5)=1133
00345 137*  GO TO 100
00346 138*  54 IPT(II,2)=JL(1)*17-IL(2)+1
00347 139*  IPT(II,3)=JL(2)*17-IL(2)+1
00350 140*  IPT(II,5)=333
00351 141*  GO TO 100
00352 142*  55 CONTINUE
00353 143*  IPT(II,3)=JL(1)*17-IL(2)+1
00354 144*  IPT(II,4)=JL(2)*17-IL(2)+1
00355 145*  GO TO 100
00355 146*  C
00355 147*  C
00355 148*  C
00356 149*  70 CONTINUE
00356 150*  TWO NMC, TWO EQUATORIAL
00357 151*  IPT(II,5)=2211
00360 152*  L=YL(II)
00361 153*  IPT(II,1)=((L/5)+2)*4
00362 154*  IPT(II,2)=IPT(II,1)*4
00363 155*  IF (L.GE.355) IPT(II,1)=4
00363 156*  C
00365 157*  IF (J.LT.1) J=1
00365 158*  IF (J.GT.51) J=51
00371 159*  IF (I.LT.LIML(J)) I=LIML(J)
00373 160*  IF (I.GT.LIMU(J)) I=LIMU(J)
00375 161*  IC(1)=I*1000+J
00376 162*  IF ((J.LT.15).OR.(J.GT.37)) GO TO 72
00400 163*  IC(2)=I*1000+J+1
00401 164*  GO TO 76
00402 165*  72 IF ((J.NE.1).AND.(J.NE.51)) GO TO 74
00404 166*  IF (I.EQ.LIMU(J)) GO TO 73
00406 167*  IC(2)=(I+1)*1000+J
00407 168*  GO TO 76
00410 169*  73 IC(2)=(I-1)*1000+J
00411 170*  GO TO 76
00412 171*  74 IF (I.EQ.LIML(J)) GO TO 75
00414 172*  IC(2)=LIMU(J+1)*1000+J+1
00415 173*  GO TO 76
00416 174*  75 IC(2)=LIML(J+1)*1000+J+1
00416 175*  C
00417 176*  76 CALL NTRAN (SCRCH2,10)
00420 177*  CALL NTRAN (SCRCH2,2)
00421 178*  GO TO 77 IPG=1,1977

```

```

SEL12200
SEL12300
SEL12400
SEL12500
SEL12600
SEL12700
SEL12800
SEL12900
SEL13000
SEL13100
SEL13200
SEL13300
SEL13400
SEL13500
SEL13600
SEL13700
SEL13800
SEL13900
SEL14000
SEL14100
SEL14200
SEL14300
SEL14400
SEL14500
SEL14600
SEL14700
SEL14800
SEL14900
SEL15000
SEL15100
SEL15200
SEL15300
SEL15400
SEL15500
SEL15600
SEL15700
SEL15800
SEL15900
SEL16000
SEL16100
SEL16200
SEL16300
SEL16400
SEL16500
SEL16600
SEL16700
SEL16800
SEL16900
SEL17000
SEL17100
SEL17200
SEL17300
SEL17400
SEL17500
SEL17600
SEL17700
SEL17800

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*****
00424 179*
00425 180*
00426 181*
00431 182*
00435 183*
00435 184*
00436 185*
00436 186*
00437 187*
00440 188*
00441 189*
00442 190*
00443 191*
00445 192*
00447 193*
00451 194*
00452 195*
00453 196*
00454 197*
00455 198*
00456 199*
00457 200*
00460 201*
00461 202*
00463 203*
00464 204*
00465 205*
00466 206*
00467 207*
00470 208*
00471 209*
00471 210*
00472 211*
00473 212*
00474 213*
00477 214*
00500 215*
00501 216*
00504 217*
00506 218*
00510 219*
00510 220*
00513 221*
00515 222*
00520 223*
00523 224*
00526 225*
00527 226*
00530 227*

*****
CALL NTRAN (SCRCH2,2,1,I,J,L)
CALL NTRAN (SCRCH2,23)
DO 77 K=1,2
77 IF (IC(K).EQ.IJ) IPT(II,K+2)=IPG
30 TO 100
C
80 CONTINUE
C
THREE NMC, ONE EQUATORIAL
IPT(II,5)=2212
IC(2) = 0
L=YL(II)
IPT(II,2)=((L/5)+1)*4
IF (L.GE.355) IPT(II,2)=4
IF (I.EQ.LIML(J)) GO TO 84
IF (J.GT.37) GO TO 82
IC(1)=I*1000+J
IC(3)=I*1000+J+1
IC(4)=(I+1)*1000+J+1
90 TO 88
82 IC(1)=(I+1)*1000+J
IC(3)=I*1000+J
IC(4)=I*1000+J+1
30 TO 86
84 IF (J.GT.37) GO TO 86
IC(1)=(I-1)*1000+J+1
IC(3)=I*1000+J+1
IC(4)=I*1000+J
90 TO 88
86 IC(1)=(I+1)*1000+J+1
IC(3)=(I+1)*1000+J
IC(4)=I*1000+J
C
88 CALL NTRAN (SCRCH2,10)
CALL NTRAN (SCRCH2,22)
DO 89 IPG=1,1977
CALL NTRAN (SCRCH2,2,1,I,J,L)
CALL NTRAN (SCRCH2,22)
DO 89 K=1,4
IF (IC(K).EQ.0) GO TO 89
IF (IC(K).EQ.IJ) IPT(II,K)=IPG
89 CONTINUE
C
100 CONTINUE
DO 150 I=1,16
DO 150 J=1,5
150 IPTN(I,J)=IPT(I,J)
CALL SORT4(NP)
RETURN
END
SEL17900
SEL18000
SEL18100
SEL18200
SEL18300
SEL18400
SEL18500
SEL18600
SEL18700
SEL18800
SEL18900
SEL19000
SEL19100
SEL19200
SEL19300
SEL19400
SEL19500
SEL19600
SEL19700
SEL19800
SEL19900
SEL20000
SEL20100
SEL20200
SEL20300
SEL20400
SEL20500
SEL20600
SEL20700
SEL20800
SEL20900
SEL21000
SEL21100
SEL21200
SEL21300
SEL21400
SEL21500
SEL21600
SEL21700
SEL21800
SEL21900
SEL22000
SEL22100
SEL22200
SEL22300
SEL22400
SEL22500
SEL22600
SEL22700

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END OF COMPILATION: NO DIAGNOSTICS.
 QHDG,P ***** SETUP *****
 @FOR,S PROFAS.SETUP,SETUP
 FOR S11E-02/04/74-18:55:02 (0,)

SUBROUTINE SETUP ENTRY POINT 002274

STORAGE USED: CODE(1) 002306; DATA(0) 000527; BLANK COMMON(2) 000000

COMMON BLOCKS:

0003 COTRAN 000041
 0004 TOTEMP 000030
 0005 PDTCOM 012667

EXTERNAL REFERENCES (BLOCK, NAME)

0006 RAND
 0007 GETNMC
 0010 RTRANI
 0011 RTRAN
 0012 ITRAN
 0013 RTRAN2
 0014 RTERP
 0015 INTRUV
 0016 ARDUS
 0017 NIO2\$
 0020 IARDUS
 0021 XPRI
 0022 NERR2\$
 0023 NIO3\$
 0024 NIO1\$
 0025 NISTOP\$
 0026 NERR3\$

STORAGE ASSIGNMENT (BLOCK, TYPE, RELATIVE LOCATION, NAME)

0001	000330	100L	0001	001707	10016	0001	001747	10206	0001	001764	10276	0001	002024	10466	
0001	002042	1056G	0001	002043	1061G	0001	00231	12L	0001	00245	13L	0001	000354	130L	
0001	000357	140L	0001	000361	150L	0001	00056	2L	0000	00070	20F	0001	000415	200L	
0001	000247	216G	0001	000441	230L	0001	000310	236G	0001	00044	240L	0001	000334	2466	
0001	000446	250L	0001	000375	266G	0001	000421	276G	0001	000267	30L	0001	000502	300L	
0001	000542	308L	0000	000057	310F	0001	000462	316G	0001	000606	320L	0001	000514	3306	
0001	000611	330L	0001	000517	333G	0001	000613	340L	0001	000544	345G	0001	000562	3566	
0001	000711	360L	0001	000763	368L	0001	001003	370L	0001	001034	375L	0000	000064	380F	
0001	001056	385L	0001	001073	390L	0001	000272	40L	0001	001076	400L	0001	000656	4056	
0001	001100	410L	0001	000723	421G	0001	000726	424G	0001	000735	427G	0001	001165	430L	
0001	001226	440L	0001	001005	445G	0001	001254	460L	0001	001302	462L	0000	000074	465F	
0001	001322	467L	0001	001047	470G	0001	001337	470L	0001	001342	475L	0001	000344	480L	
0001	001420	490L	0000	000056	5F	0001	000274	50L	0001	001456	500L	0001	001476	510L	
0001	001133	516G	0000	000100	520F	0001	001520	525L	0001	001522	527L	0001	001177	5326	
0001	001202	535G	0001	001575	535L	0001	001577	537L	0001	001652	545L	0001	001654	547L	
0001	001230	550G	0001	001231	553G	0001	001727	555L	0001	001731	557L	0001	001243	5636	
0001	002004	565L	0001	001244	565G	0001	002006	567L	0001	00156	576G	0001	002040	600L	
0001	001315	620G	0001	002062	624G	0001	002072	621L	0001	002123	623L	0001	002140	626L	
0000	000121	630F	0001	001377	644G	0001	001432	657G	0001	001435	662G	0001	002211	666L	
0001	001500	676G	0001	000212	7L	0000	000104	700F	0001	001540	716G	0001	001555	7256	
0001	001615	744G	0001	001632	75.3	0001	001672	772G	0000	00062	9000F	0000	000355	9001F	
0005	R	007625	DAQ	0004	R	000004	DD	0005	R	001257	DG	0005	R	010755	DR

***** SETUP *****

```

0005 R 003705 USP
0000 I 000033 IDA
0000 I 000055 IHR
0004 I 000001 IOTEM2
0000 I 000035 IUG
0000 I 000046 J
0000 I 000053 L
0000 I 000041 M1
0004 I 000010 NSAME
0004 R 000006 PHI1
0006 R 000000 RAND
0004 R 000020 RV1
0004 R 000022 SV1
0005 R 011265 TR
0005 R 011715 VAQ
0000 I 000026 H1
0000 I 000017 IDAY
0000 I 000024 IDD
0000 I 000036 IOPQ
0000 I 000052 ISH
0000 I 000000 IP
0000 I 000034 IUR
0000 I 000050 J10
0000 I 000051 LON
0000 I 000042 M2
0005 R 007505 PA3
0004 000027 PHIIR
0004 R 000012 RD1
0004 R 000015 SD1
0005 R 007745 TAQ
0005 R 005605 TSP
0005 R 012155 VDQ
0004 R 000026 H1
0004 I 000024 IDD
0000 I 000036 IOPQ
0000 I 000052 ISH
0000 I 000000 IP
0000 I 000034 IUR
0000 I 000050 J20
0003 I 000024 MI
0003 I 000000 NDATA
0005 R 010065 PDQ
0005 R 010495 PR
0004 R 000011 RP1
0004 R 000014 SP1
0005 R 010325 TDQ
0005 R 011575 UAG
0005 R 012155 VR
0000 I 000043 I
0003 I 000023 IC
0004 I 000040 IEX
0005 I 000002 IOPR
0000 I 000012 IT
0003 I 000026 IX
0000 I 000047 K
0004 I 000023 MN
0004 I 000003 NMCOP
0005 R 000003 PG
0005 R 002005 PSP
0004 R 000011 RT1
0004 R 000016 ST1
0000 R 000045 TENX
0005 R 012035 UDQ
0004 R 000005 XMDJ

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```

00101 1*
00103 2*
00104 3*
00105 4*
00105 5*
00105 6*
00106 7*
00106 8*
00106 9*
00106 10*
00106 11*
00107 12*
00110 13*
00111 14*
00113 15*
00114 16*
00116 17*
00117 18*
00120 19*
00122 20*
00122 21*
00122 22*
00122 23*
00122 24*
00122 25*
00122 26*
00122 27*
00122 28*
00122 29*
00122 30*
00122 31*
00122 32*
00122 33*
00122 34*
00122 35*
00122 36*
00122 37*
00122 38*

SUBROUTINE SETUP
COMMON/COTRAN/NDATA(19),IC,M1,IH,IX(10),IEX
DIMENSION IP(5),ID(5),IT(5),IDAY(12)
COMMON/IOTEMP/IOTEM1,IOTEM2,IUG,NMCOP,RD,XMDJ,PHI1,PHI,
* NSAME,RP1, RD1, RT1, RV1, SU1, SV1,
$ MN, IDD, IYR, H1, PHIIR
COMMON/POTCOM/IU4*MONTH,IOPR,PG(18,19),TG(18,19),DG(18,19)
*,PSP(8,10,12)
1,DSP(8,10,12),TSP(8,10,12),PAQ(16,5),DAQ(16,5),TAQ(16,5),PDQ(16,5)
2,DDG(16,5),TDQ(16,5),PR(20,10),DR(20,10),TR(20,10),UAG(16,5)
3,VAQ(16,5),VUQ(16,5),VDQ(16,5),UR(25,10)
DIMENSION VR(25,10)
EQUIVALENCE (VR(1,1),VR(1,1))
DATA IDAY/0,31,59,90,120,151,181,212,243,273,304,334/
XMDJ = 0.
IF (MN,GT,12) GO TO 2
IDA = IDAY(MN) + IDD
DD = IDA
IF (MOD(IYR,4),EQ,0.AND,MN,GT,2) IDA = IDA + 1
XMDJ = 2439856. + 365. * (IYR - 68.) + IDA + INT((IYR - 65.)
$/ 4.)
C.....SECOND DATA CARD READS, FREE FIELD, THE FOLLOWING DATA:
C IUG = UNIT NUMBER FOR GROVES DATA TAPE
C IUR = UNIT NUMBER FOR RANDOM SIGMA DATA
C (IF IUR=IUG UNIT IUG WILL BE READ)
C IUG = UNIT NUMBER FOR GBO DATA
C (IF IUG=IUG DATA ON TAPE ON UNIT IUG WILL BE READ)
C IU4 = UNIT FOR 4-D INPUT P,D,T 0-25KM DATA
C IOPR = RANDOM OUTPUT
C.....IOPR=1 RANDOM OUTPUT IOPR=2 NO RANDOM OUTPUT
C IOPQ = GBO OUTPUT
C.....IOPQ=1 GBO OUTPUT IOPQ=2 NO GBO OUTPUT
C NR1 = STARTING RANDOM NUMBER
C NMCOP = NMC GRID DATA READ OPTION
C.....NMCOP=0 READS NMC GRID DATA FROM UNIT IUG, OTHERWISE READS FORM
C CARDS
C.....IOTEM=UNIT FOR 4-D P, D, T DATA (SCRATCH FILE, DOES NOT NEED TO
C BE ASSIGNED)
SET00100
SET00200
SET00300
SET00400
SET00500
SET00600
SET00700
SET00800
SET00900
SET01000
SET01100
SET01200
SET01300
SET01400
SET01500
SET01600
SET01700
SET01800
SET01900
SET02000
SET02100
SET02200
SET02300
SET02400
SET02500
SET02600
SET02700
SET02800
SET02900
SET03000
SET03100
SET03200
SET03300
SET03400
SET03500
SET03600
SET03700
SET03800

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REPRODUCIBILITY OF THE ORIGINAL PAGE IS POOR

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***** SETUP *****
00122 39* C.....IOTEN2=UNIT FOR NMC GRID POINTS (SCRATCH FILE, DOES NOT NEED TO
00123 40* RE ASSIGNED)
00124 41* READ(5,5) IUG,IUR,IU3,IU4,IOPR,IOPQ,NR1,NMCOPI,IOTEM1,IOTEM2
00125 42* WRITE(6,9000) IUG,IUR,IU3,IU4,IOPR,IOPQ,NR1,NMCOPI,IOTEM1,IOTEM2
00126 43* 5 *XJUD
00127 44* 5 FOR'IAT(I)
00128 45* IF (IOPR.LT.1.OR.IOPR.GT.2) GO TO 666
00129 46* IF (IOPQ.LT.1.OR.IOPQ.GT.2) GO TO 666
00130 47* 10NTHEMN
00131 48* IF (IOPR.EQ.2) GO TO 7
00132 49* R=RAND(NR1)
00133 50* C.....THIRD DATA CARD READS FREE FIELD; THE FOLLOWING DATA:
00134 51* RPI = INITIAL RANDOM PRESSURE PERTURBAIONS, PERCENT
00135 52* RDI = INITIAL RANDOM DENSITY PERTURBATION, PERCENT
00136 53* RII = INITIAL RANDOM TEMPERATURE PERTURBATION, PERCENT
00137 54* SDI = INITIAL STANDARD DEVIATION FOR RANDOM DENSITY
00138 55* PERTURBATION, PERCENT
00139 56* RUI = INITIAL EASTWARD WIND PERTURBATION, M/S
00140 57* RVI = INITIAL NORTHWARD WIND PERTURBATION, M/S
00141 58* SVI = INITIAL STANDARD DEVIATION FOR RANDOM EASTWARD WIND, M/S
00142 59* SVI = INITIAL STANDARD DEVIATION FOR RANDOM NORTHWARD WIND, M/S
00143 60* READ(5,5) RPI,RDI,RTI,SP1,SD1,ST1,RUI,RVI,SUI,SVI
00144 61* 7 IF (NSAME.EQ.1) GO TO 621 0 AVOIDS TAPE SEARCH IF CURRENT MONTH
00145 62* IS SAME AS PREVIOUS MONTH
00146 63* CALL GETNMC
00147 64* C.....LOADS NMC GRID DATA FROM INPUT UNIT TO SCRATCHFILE UNIT IOTEM2
00148 65* IF (MONTH.LT.13) GO TO 12
00149 66* 12=13
00150 67* 13=13
00151 68* C.....MONTH=13 IS ANNUAL AVERAGE CASE
00152 69* GO TO 13
00153 70* 12=MONTH + 6
00154 71* 13=MONTH
00155 72* C.....SOUTHERN HEMISPHERE DATA IS 6 MONTHS DISPLACED FOR GROVES,
00156 73* STATIONARY PERTURBATIONS, AND RANDOM PERTURBATIONS
00157 74* IF (M2.GT.12) M2=M2 - 12
00158 75* 13 00 100 I=1,254
00159 76* 15 CALL RTRANI
00160 77* C.....READS GROVES PRESSURE DATA
00161 78* IF (IC.NE.P) GO TO 666
00162 79* IF (MI.EQ.M1) GO TO 30
00163 80* IF (MI.EQ.M2) GO TO 40
00164 81* GO TO 100
00165 82* 30 KS=1
00166 83* GO TO 50
00167 84* 40 KS=-1
00168 85* 50 I=(IH-20)/75
00169 86* TENX=10.**IEX
00170 87* DO 60 J=1,10
00171 88* K=10+KS*(J-1)
00172 89* 60 P5(IH,K) = IX(J)*TENX
00173 90* C.....CONVERSION TO REAL AND STORAGE IN ARRAY COMPLETE
00174 91* 100 CONTINUE
00175 92* DO 200 I=1,234
00176 93* 115 CALL RTRANI
00177 94* C.....READS GROVES DENSITY DATA
00178 95* IF (IC.NE.D) GO TO 566
00179 96*
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***** SETUP *****
00253 96* IF (MI.EG.M1) GO TO 130
00255 97* IF (MI.EG.M2) GO TO 140
00257 98* GO TC 200
00260 99*
00261 100* GO TO 150
00262 101*
00263 102* 140 KS=-1
00264 103* 150 I=(IH-20)/5
00265 104* TENX=10.**IEX
00270 105* DO 160 J=1,10
00271 106* K=10+KS*(J-1)
00272 107* 160 D(I,H,K) = IX(J)*TENX
00273 108* C.....CONVERSION TO REAL AND STORAGE IN ARRAY COMPLETE
00275 109* 200 CONTINUE
00300 110* DO 300 I=1,234
00301 111* 215 CALL RTRANI
00303 112* C.....READS GROVES TEMPERATURE DATA
00304 113* IF (IC.NE.'T') GO TO 666
00305 114* IF (MI.EG.M1) GO TO 230
00310 115* IF (MI.EG.M2) GO TO 240
00311 116* GO TO 300
00312 117* 230 KS=-1
00313 118* GO TO 250
00314 119* 240 KS=-1
00315 120* 250 I=(IH-20)/5
00316 121* TENX=10.**IEX
00317 122* DO 260 J=1,10
00318 123* K=10+KS*(J-1)
00319 124* 260 T(I,H,K) = IX(J)*TENX
00320 125* C.....CONVERSION TO REAL AND STORAGE IN ARRAY COMPLETE
00321 126* 300 CONTINUE
00322 127* IF (MONTH.LT.13) GO TO 308
00323 128* C.....ANNUAL MEAN CASE - BOTH HEMISPHERES EQUAL
00324 129* DO 304 I=1,18
00325 130* DO 304 J=1,9
00326 131* J20=20-J
00327 132* P(I,J)=PG(I,J20)
00328 133* D(I,J)=DG(I,J20)
00329 134* T(I,J)=TG(I,J20)
00330 135* 304 CONTINUE
00331 136* 308 DO 360 I=1,1248
00332 137* 310 FORMAT (1X,A1,I2,I3,I5,2(5I4,4X),5I4)
00333 138* CALL RTRAN(19)
00334 139* C.....READS STATIONARY PERTURBATIONS DATA (TO BE STORED IN PSP, DSP, AND SET13900)
00335 140* TSP ARRAYS)
00336 141* IC=JDATA(1)
00337 142* IH=JDATA(2)
00338 143* IJ=JDATA(3)
00339 144* LON=JDATA(4)
00340 145* DO 311 K=1,5
00341 146* IP(K)=NDATA(4+K)
00342 147* ID(K)=NDATA(9+K)
00343 148* IT(K)=NDATA(14+K)
00344 149* 311 IF (IC.NE.'S') GO TO 666
00345 150* IF (MI.EG.M1) GO TO 320
00346 151* IF (MI.EG.M2) GO TO 330
00347 152* GO TO 360
00348 153* 320 KS=-1
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C-3

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***** SETUP *****
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30 TO 340
330 KS=-1
340 ISH=2+(IH-44)/8
L=(LON+20)/20
IF(IH,LT,52) ISH = (IH-20)/10
IF (IH,GT,84) ISH=8
DO 350 J=1,5
K=5+KS*(J+(KS-1)/2)
PSP(ISH,K,L) = IP(J)/1000.
PSP(ISH,K,L) = IP(J)/1000.
350 TSP(ISH,K,L) = IT(J)/1000.
C.....CONVERSION TO REAL AND STORAGE IN ARRAYS COMPLETE
360 CONTINUE
IF (MONTH,LT,13) GO TO 368
C.....ANNUAL MEAN CASE - BOTH HEMISPHERES EQUAL
DO 364 I=1,8
DO 364 K=1,12
DO 364 J=1,5
J10=11-J
PSP(I,J,K)=PSP(I,J10,K)
PSP(I,J,K)=CSP(I,J10,K)
TSP(I,J,K)=TSP(I,J10,K)
364 CONTINUE
366 CALL NTRAN(IUG,8,1) G.....MOVES PAST 2ND EOF ON UNIT IUG
DO TO (370,449),IOPP
C.....IOPR=1 READS RANDOM SIGMAS, IOPR=2 ZEROS RANDOM SIGMAS
370 DO 430 I=1,260
IF (IUR,EQ,IUG) GO TO 375
READ (IUR,390) IC,MI,IH,IP,ID,IT
C.....USES FORTRAN READ ON UNIT IUR IF IUR NFO IUG
380 FORMAT (1X,A1,I2,I4,3(1X,5I4))
DO TO 385
375 CALL RTRAN(18)
C.....USES NTRAN READ ON UNIT IUG IF IUR = IUG
IC=NDATA(1)
IH=NDATA(2)
I=NDATA(3)
DO 381 K=1,5
IP(K)=NDATA(3+K)
ID(K)=NDATA(8+K)
381 IT(K)=NDATA(13+K)
DO 385
20 FORMAT (1X,A1,I3,I4,I3,I1,I5)
IF (MI,EQ,M1) GO TO 390 G.....M1 = NORTHERN HEMISPHERE MONTH
IF (MI,EQ,M2) GO TO 400 G.....M2 = SOUTHERN HEMISPHERE MONTH
C.....I2 = M1 + 6 UNLESS M1 = M2 = 13
DO 420 J=1,5
390 KS=1
GO TO 410
400 KS=-1
410 IF (IH,LT,95) IHR=(IH-20)/5
IF (IH,GE,95) IHR = 14 + (IH - 80) / 20 G.....IHR = HEIGHT INDEX
K = 5 + KS * (J + (KS - 1) / 2)
C.....K = LATITUDE INDEX I=5 = LAT -90 TO -10, 6-10 = LAT +10 TO +90
PR(IHR,K) = IP(J)/1000.

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SETUP

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00522      JR(IHR,K) = ID(J)/1000.
00523      TR(IHR,K) = IT(J)/1000.
00525      420 CONTINUE
00527      IF (MONTH,LT,13) GO TO 460
00531      C.....ANNUAL MEAN CASE - BOTH HEMISPHERES EQUAL
00534      DO 435 I=1,20
00537      DO 435 J=1,5
00540      J10=11-J
00541      PR(I,J)=PR(I,J10)
00542      TR(I,J)=TR(I,J10)
00543      435 CONTINUE
00546      GO TO 460
00552      440 DO 450 I=1,20
00555      DO 450 J=1,10
00556      PR(I,J) = 0.
00557      PR(I,J) = 0.
00557      C.....RANDOM SIGMAS ARE ZEROED IF IOPR=2
00562      DO 455 I=1,25
00565      DO 455 J=1,10
00570      UR(I,J)=0.
00571      455 VR(I,J) = 0.
00574      DO 460 I=1,325
00575      IF (IUR,EG,IUG) GO TO 462
00600      READ(IUR,465) IC,MI,IH,IP,ID
00602      C.....READS RANDOM WIND STANDARD DEVIATIONS WITH FORTRAN READ FROM
00602      UNIT IUR IF IUR NEG IUG
00611      465 FORMAT(IX,A2,I2,I4,2(1X,5I4))
00612      GO TO 467
00613      462 CALL RTRAN(13)
00614      C.....USES NTRAN READ FROM UNIT IUG IF IUR = IUG
00615      IC=DATA(1)
00616      IH=DATA(2)
00617      MI=DATA(3)
00622      IP(K)=DATA(3+K)
00623      ID(K)=DATA(8+K)
00625      461 ID(K)=DATA(8+K)
00627      IF (IC,NE,IRW,1) GO TO 666
00631      IF (MI,EG,M2) GO TO 475
00633      GO TO 490
00634      470 KS=1
00635      GO TO 480
00636      475 KS=-1
00637      480 IF (IH,LT,95) IHR=1+IH/5
00641      IF (IH,GE,95) IHR=19+(IH-80)/20
00643      Q.....NORTHERN HEMISPHERE MONTH
00644      Q.....SOUTHERN HEMISPHERE MONTH
00646      DO 485 J=1,5
00647      K=5+KS*(J+(KS-1)/2)
00650      UR(IHR,K)=IP(J)*1.
00650      485 VR(IHR,K)=ID(J)*1.
00652      490 CONTINUE
00654      IF (MONTH,LT,13) GO TO 500
00654      C.....ANNUAL MEAN CASE - BOTH HEMISPHERES EQUAL
00656      DO 495 I=1,25
00661      DO 495 J=1,5
00661      495 VR(I,J)=0.

```

REPRODUCIBILITY OF THE ORIGINAL PAGE IS POOR

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*****
***** SETUP *****
00664 267* J10=11-J
00665 268* UR(I,J)=UR(I,J10)
00666 269* VR(I,J)=VR(I,J10)
00667 270* 495 CONTINUE
00672 271* 500 CALL NTRAN(IUG,8,1) 3.....READS PAST 3RD EOF ON UNIT IUG
00673 272* CALL NTRAN(IUG,22)
00674 273* 30 TO (510,600),IOPQ
00675 274* C.....IOPQ=1 READS QBO PARAMETERS, IOPQ=2 ZEROS THESE PARAMETERS
00700 275* 510 DO 530 I=1,16
00701 276* IF (IUG.EQ.IUG) GO TO 525
00702 277* READ(IUG,520) IC,IH,IX
00703 278* C.....READS WITH FORTRAN FROM UNIT IUG IF IUG NEQ IUG
00707 279* 520 FORMAT (IX,A2,I3,I5(I4,I5))
00710 280* 30 TO 527
00711 281* 525 CALL RTRAN2
00712 282* C.....READS WITH NTRAN FROM UNIT IUG IF IUG = IUG
00714 283* 527 IF (IC.NE.'QP') GO TO 666
00715 284* IH = (IH-10)/5
00716 285* DO 530 J=1,5
00717 286* C.....CONVERT FROM INTEGER PER MIL - QBO PRESSURE AMPLITUDE
00720 287* PAQ(IH,J) = IX(2*J-1)/1000.
00721 288* C.....QBO PRESSURE PHASE (DAYS PAST JAN 0, 1966)
00724 289* 530 PDQ(IH,J) = IX(2*J)*1.
00727 290* DO 540 I=1,16
00731 291* IF (IUG.EQ.IUG) GO TO 535
00736 292* READ (IUG,520) IC,IH,IX
00740 293* 30 TO 537
00742 294* 535 CALL RTRAN2
00743 295* 537 IF (IC.NE.'QD') GO TO 666
00746 296* IH=(IH-10)/5
00747 297* DO 540 J=1,5
00752 298* C.....CONVERT FROM INTEGER PER MIL - QBO DENSITY AMPLITUDE
00755 299* DAQ(IH,J) = IX(2*J-1)/1000.
00764 300* C.....QBO DENSITY PHASE (DAYS PAST JAN 0, 1966)
00765 301* 540 DDQ(IH,J)=IX(2*J)*1.
00770 302* DO 550 I=1,16
00771 303* IF (IUG.EQ.IUG) GO TO 545
00774 304* READ (IUG,520) IC,IH,IX
00775 305* 30 TO 547
00777 306* 545 CALL RTRAN2
00778 307* 547 IF (IC.NE.'QT') GO TO 666
00780 308* IH = (IH-10)/5
00781 309* DO 550 J=1,5
00784 310* C.....CONVERTS FROM INTEGER PER MIL - QBO TEMPERATURE AMPLITUDE
00785 311* TAQ(IH,J) = IX(2*J-1)/1000.
00787 312* C.....QBO TEMPERATURE PHASE
00790 313* 550 TDQ(IH,J) = IX(2*J)*1.
00795 314* DO 560 I=1,16
00800 315* IF (IUG.EQ.IUG) GO TO 555
00803 316* C.....READS WITH FORTRAN IF IUG NEQ IUG
00807 317* READ(IUG,520) IC,IH,IX
00810 318* 30 TO 557
00811 319* 555 CALL RTRAN2
00813 320* C.....READS WITH NTRAN IF IUG = IUG
00814 321* 557 IF (IC.NE.'QU') GO TO 666
00816 322* IH=(IH-10)/5
00817 323* DO 560 J=1,5

```

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SET26700
SET26800
SET26900
SET27000
SET27100
SET27200
SET27300
SET27400
SET27500
SET27600
SET27700
SET27800
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SET28000
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SET30000
SET30100
SET30200
SET30300
SET30400
SET30500
SET30600
SET30700
SET30800
SET30900
SET31000
SET31100
SET31200
SET31300
SET31400
SET31500
SET31600
SET31700
SET31800
SET31900
SET32000
SET32100
SET32200
SET32300

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SETUP

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01017 324* C.....EASTWARD WIND Q80 AMP*AMPLITUDE - CONVERTED TO M/S
01022 325*   VAG(IH,J) = IX(2 * J - 1) / 10.
01022 326* C.....EASTWARD WIND Q80 PHASE (DAYS PAST JAN 0, 1966)
01023 327*   S60 UDG(IH,J)=IX(2*J)*1.
01026 328*   DO 570 I=1,16
01031 329*     IF (IUG,EG,IUG) GO TO 565
01033 330*     READ(IUG,520) IC,IH,IX
01040 331*     GO TO 567
01041 332*   S65 CALL RTRAN2
01042 333*   S67 IF (IC,NE,'OV') GO TO 666
01044 334*     IH=(IH-10)/5
01045 335*     DO 570 J=1,5
01045 336* C.....NORTHWARD WIND Q80 AMPLITUDE - CONVERTED TO M/S
01050 337*   VAG(IH,J) = IX(2 * J - 1) / 10.
01050 338* C.....NORTHWARD WIND Q80 PHASE (DAYS PAST JAN 0,1966)
01051 339*   S70 VDG(IH,J)=IX(2*J)*1.
01054 340*     GO TO 620
01055 341*   S60 DO 610 I=1,16
01060 342*     DO 610 J=1,5
01063 343*     VAG(I,J) = 0.
01064 344*     DAG(I,J) = 0.
01065 345*     TAG(I,J) = 0.
01066 346*     PDG(I,J) = 0.
01067 347*     DDG(I,J) = 0.
01070 348*     TDG(I,J) = 0.
01071 349*     UAG(I,J)=0.
01072 350*     VAG(I,J)=0.
01073 351*     WAG(I,J)=0.
01074 352*     YDQ(I,J)=0.
01075 353*   S610 CONTINUE
01075 354* C.....ZEROS Q80 PARAMETERS IF IOPQ = 2
01100 355*   S620 CALL NTRAN(IUG,10) Q.....REWINDS TAPE UNIT IUG
01101 356*   S621 IF (SPI*SDI*STI.GT.0.) GO TO 623
01102 357*     CALL RTRP(HI,PHI,PR,DR,TR,SPI,SDI,STI)
01105 358*     SPI = SPI * 100.
01106 359*     SDI = SDI * 100.
01107 360*     STI = STI * 100.
01110 361*   S623 IF (SUI*SVI.GT.0.) GO TO 626
01112 362*     CALL INTRUV(UR,VR,HI,PHI,SUI,SVI)
01113 363*     S626 WRITE(6,9001) RPI,RD1,RTI,SPI,SDI,STI,RU1,RV1,SUI,SVI
01127 364*     RPI=RP1/100.
01130 365*     RD1=RD1/100.
01131 366*     RTI=RTI/100.
01132 367*     SPI=SPI/100.
01133 368*     SDI=SDI/100.
01134 369*     STI=STI/100.
01135 370*     WRITE(6,630)
01137 371*     RETURN
01137 372*   S666 WRITE(6,700) IUG,IUR,IUG,IOPQ,IOPQ,NR1,NMCOP,IOTEM1,IOTEM2,
01140 373*     S670 MONTH,IC,MI,IH,IX,FX,IP,ID,IT,SDI
01140 374*   S700 FORWAT(' ERROR IN SETUP INPUT',/,'IX,5I3,I10,4I3,A2,I3,I4,/,1I4,
01165 375*     $/,15I4,/,F10,1)
01166 376*   S701 STOP
01167 377*   S630 FORWAT(27X,'UNPERTURBED (MONTHLY MEAN)',9X,'MEAN PLUS PERTURBATION',37R00
01167 378*     1S,'8X,'THERMAL',/,'24X,2(32(',-),2X),3X,'WIND',7X,'PERTURBATION VAL',37R00
01167 379*     2UES',/, ' HEIGHT LAT WEST PRES. DENS. TEMP GEOSTROPH. SEI38000
01167 380*

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***** SETUP *****

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01167 3 PRES. DENS. TEMP TOTAL SHEAR,/,3X,.(KM),,11X,.(LON), SET38050
01167 4+X,.(NT/ (KG/ (NT/ (KG/ (DEG WIND (MSET38100
01167 5/S) (M/S/KM) ,.28(.-),/, TIME (DEG) (DEG) ,.2( M**2) MSET38200
01167 6**3) KEL- ,.10(.-),,2X,.(.-),, P D T U V,/,/, SET38300
01167 7(SEC),.33X,.(VIN) E-W N-S E-W N-S (*),SET38400
01167 8 (X) (X) M/S M/S,/, SET38500
01167 9000 FORMAT(, GROVES INPUT UNIT = ,I2,T43,RANDOM INPUT UNIT = ,I2, SET38600
01170 1T83,.(Q80 INPUT UNIT = ,I2,/, 4-D INPUT UNIT = ,I2,T43,RANDOM SET38700
01170 2OPTION = ,I2,T83,.(Q80 OPTION = ,I2,/, FIRST RANDOM NUMBER = , SET38800
01170 215, NMC READ OPTION = ,I2,T43,.(4-D P,D,T DATA SCRATCH UNIT = , SET39000
01170 3/, NMC GRID POINTS SCRATCH UNIT = ,I2,T43,.(JULIAN DATE = , SET39100
01170 5F9.1,/, SET39200
01171 9001 FORMAT(, INITIAL P,D,T = ,3(F6.2), ( ),T60,.(SIGMA P,D,T = , SET39300
01171 13(F6.2), ( ),/, INITIAL U,V = ,2(F7.2), M/S ( ),T60,.(SIGMA SET39400
01171 2U,V = ,2(F7.2), M/S ( ),/, ** PERCENT DEVIATIONS FROM 1962 US SET39450
01171 3STANDARD ATMOSPHERE APPEAR BELOW PRESSURE, DENSITY, AND TEMPERATURE,SET39500
01171 4E VALUES **/,/,/, SET39550
01172 END SET39600

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END OF COMPILATION: NO DIAGNOSTICS.

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@HDS/P ***** SORT4 *****
@FOR,S PROFAS,SORT4,SORT4
FOR S11E-02/04/74-18:55:17 (0, )

```

SUBROUTINE SORT4 ENTRY POINT 000354

STORAGE USED: CODE(1) 000370; DATA(0) 000035; BLANK COMMON(2) 000000

COMMON BLOCKS:

0003 ORDER 000423

EXTERNAL REFERENCES (BLOCK, NAME)

0004 NERR35

STORAGE ASSIGNMENT (BLOCK, TYPE, RELATIVE LOCATION, NAME)

0001	000204	10L	0001	000005	1056	0001	000225	11L	0001	000006	1109	0001	000016	1166	
0001	000265	12L	0001	000326	13L	0001	000333	14L	0001	000065	1426	0001	000104	1536	
0001	000051	2L	0001	000207	2076	0001	000216	2126	0001	000234	2226	0001	000237	2256	
0001	000075	3L	0001	000100	4L	0001	000114	5L	0001	000117	6L	0001	000136	7L	
0001	000155	8L	0001	000202	9L	0000	I	000000	I	0000	I	0000	000011	INJPS	
0003	I	000000	IPT	0000	I	000002	IR	0003	I	000120	IREAD	0000	I	000007	JJ
0000	I	000003	K	0000	I	000004	L	0000	I	000005	.P	0000	I	000007	JJ

SUBROUTINE SORT4(INP)

SOR0100
SOR00200

00101 1* C
00101 2*

```

***** SJRT4 *****
00101 C
00101 C
00101 C
00101 C
00103 C
00104 C
00107 C
00112 C
00115 C
00120 C
00122 C
00124 C
00126 C
00130 C
00132 C
00134 C
00136 C
00140 C
00141 C
00144 C
00146 C
00147 C
00151 C
00152 C
00155 C
00157 C
00160 C
00162 C
00163 C
00165 C
00167 C
00170 C
00172 C
00174 C
00175 C
00177 C
00201 C
00203 C
00203 C
00203 C
00205 C
00206 C
00211 C
00214 C
00215 C
00217 C
00220 C
00221 C
00224 C
00227 C
00231 C
00233 C
00235 C
00236 C
00237 C

SORTS POINTS FOR SEQUENTIAL TAPE READING
ASSIGNS POINT NUMBERS BY ORDER ON TAPE, NOT BY GRID
COMMON /ORDER/ IPT (16,5),IRFAD(65,3)

DO 1 I=1,65
DO 1 J=1,3
1 IREAD(I,J)=0
DO 2 I=1,MP
IF(IPT(I,5).LT.1) GO TO 10
IF(IPT(I,5).EQ.1) GO TO 9
IF(IPT(I,5).EQ.2) GO TO 2
IF(IPT(I,5).EQ.3) GO TO 4
IF(IPT(I,5).EQ.113)GO TO 6
IF(IPT(I,5).EQ.221) GO TO 7
IF(IPT(I,5).EQ.2212)GO TO 8
IF (IPT(I,5).EQ.335) GO TO 4
GO TO 10
2 DO 3 J=1,4
IF(IPT(I,J).LT.1) GO TO 3
IPT(I,J)=IPT(I,J)+288
3 CONTINUE
GO TO 9
4 DO 5 J=1,4
IF(IPT(I,J).LT.1) GO TO 5
IPT(I,J)=IPT(I,J)+265
5 CONTINUE
GO TO 9
6 IF(IPT(I,1).GT.0)IPT(I,1)=IPT(I,1)+2265
IF(IPT(I,2).GT.0)IPT(I,2)=IPT(I,2)+2265
GO TO 9
7 IF(IPT(I,3).GT.0)IPT(I,3)=IPT(I,3)+288
IF(IPT(I,4).GT.0)IPT(I,4)=IPT(I,4)+288
GO TO 9
8 IF(IPT(I,1).GT.0)IPT(I,1)=IPT(I,1)+288
IF(IPT(I,3).GT.0)IPT(I,3)=IPT(I,3)+288
IF(IPT(I,4).GT.0)IPT(I,4)=IPT(I,4)+288
9 CONTINUE

C
C
C
10 IR=0
DO 13 K=1,MP
DO 13 L=1,4
MP=IPT(K,L)
IF(MP.LT.1) GO TO 13
11 I=K
J=L
JJ=L
DO 12 I=1,MP
DO 12 J=1,4
IF (IPT(I,J).LT.1) GO TO 12
IF(IPT(I,J).GT.3490) GO TO 12
I=I
J=J
MP=IPT(I,J)
59*
00237 C

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SAR00300
SAR00400
SAR00500
SAR00600
SAR00700
SAR00800
SAR00900
SAR01000
SAR01100
SAR01200
SAR01300
SAR01400
SAR01500
SAR01600
SAR01700
SAR01800
SAR01900
SAR02000
SAR02100
SAR02200
SAR02300
SAR02400
SAR02500
SAR02600
SAR02700
SAR02800
SAR02900
SAR03000
SAR03100
SAR03200
SAR03300
SAR03400
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SAR03600
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SAR04400
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SAR05200
SAR05300
SAR05400
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SAR05600
SAR05700
SAR05800
SAR05900

***** SORT4 *****

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00240 60* 12 CONTINUE
00243 61* IF(IPT(II, JJ), GT, 349) GO TO 14
00245 62* IR=IR+1
00246 63* IREAD(IR, 1)=II
00247 64* IREAD(IR, 2)=JJ
00250 65* IREAD(IR, 3)=IPT(II, JJ)
00251 66* IPT(II, JJ)=IPT(II, JJ)+9000
00252 67* VP=IPT(K, L)
00253 68* IF(MP, GT, 3490) GO TO 13
00255 69* 30 TO 11
00256 70* 13 CONTINUE
00261 71* 14 RETURN
00262 72* END

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END OF COMPILATION: NO DIAGNOSTICS.
RHDG,P ***** STDATM *****
RFOR,S PROFAS, STDATM, STDATM
FOR SIE-02/04/74-18:55:31 (2)

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SUBROUTINE STDATM ENTRY POINT 000452

STORAGE USED: CODE(1) 000502; DATA(0) 000327; BLANK COMMON(2) 000000

EXTERNAL REFERENCES (BLOCK, NAME)

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0003 EXP
0004 XPRR
0005 NERR3$

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STORAGE ASSIGNMENT (BLOCK, TYPE, RELATIVE LOCATION, NAME)

```

0001 000167 12L 0001 000214 13L 0001 000030 131G 0001 000225 162G 0001 000427 25L
0001 000051 5L 0001 000223 6L 0001 000254 8L 0000 R 000266 A
0000 R 000261 AO 0000 R 000263 A1 0000 R 000262 A2 0000 R 000267 B 0000 R 000256 G
0000 R 000257 GM 0000 R 000242 G0 0000 R 000255 HM 0000 R 000254 HT 0000 I 000240 I
0000 000305 INJPS 0000 R 000170 PS 0000 R 000241 RC 0000 R 000244 RS 0000 R 000244 RS
0000 R 000265 S 0000 R 000264 TK 0000 R 000270 TM 0000 R 000050 TMS 0000 R 000253 WM 0000 R 000245 ZM
0000 R 000243 WMO 0000 R 000120 WMS 0000 R 000247 ZL 0000 R 000251 ZLM 0000 R 000252 ZUM
0000 R 000260 ZMID 0000 R 000030 ZS 0000 R 000250 ZU

```

```

00101 1* SUBROUTINE STDATM(Z, T, P, D)
00103 2* DIMENSION ZS(40), TMS(40), WMS(40), PS(40)
00104 3* DATA(ZS(I), TMS(I), WMS(I), PS(I)), I=1, 18)/
00104 4* 10, 288, 15, 28, 9644, 1, 0, 13, 25E+3,
00104 5* 111, 019, 216, 65, 28, 96, 4, 2, 25, 320E+2,
00104 6* 120, 363, 216, 65, 28, 9644, 5, 7487E-1,
00104 7* 132, 162, 228, 65, 28, 9644, 8, 68014,
00104 8* 147, 35, 270, 65, 28, 9644, 1, 10905,
00104 9* 152, 429, 270, 65, 28, 9644, 5, 90005E-1,

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REPRODUCIBILITY OF THE ORIGINAL PAGE IS POOR

***** STUATM *****

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00104 10* 161.591,252.65,28.964,1.82099E-1,
00104 11* 179.944,180.65,28.964,1.0377E-2,
00104 12* 190.180,65,28.964,1.6438E-3,
00104 13* 195.0, 28.94, 0.,
00104 14* 1100.,210.55,28.88,3.0075E-4,
00104 15* 1105., 0., 28.75, 0.,
00104 16* 1110.,260.65,28.56,7.3544E-5,
00104 17* 1115., 0., 28.32, 0.,
00104 18* 1120.,360.65,29.07,2.5217E-5,
00104 19* 1135., 0., 27.37, 0.,
00104 20* 1150.,980.65,26.92,5.0617E-6,
00104 21* 1155., 0., 26.79, 0.,
00111 22* DATA(ZS(I),TMS(I),WMS(I),PS(I),I=19,35)/
00111 23* 1160.,1110.65,26.66,3.6943E-6,
00111 24* 1165., 0.,26.52, 0.,
00111 25* 1170.,1210.65,26.45,2.7926E-6,
00111 26* 1180., 0., 26.13, 0.,
00111 27* 1190.,1350.65,25.85,1.6852E-6,
00111 28* 1210., 0., 25.27, 0.,
00111 29* 1230.,1550.65,24.69,6.9604E-7,
00111 30* 1265., 0., 23.67, 0.,
00111 31* 1300.,1830.65,22.66,1.8838E-7,
00111 32* 1350., 0., 21.24, 0.,
00111 33* 1400.,2160.65,19.94,4.0304E-9,
00111 34* 1450., 0., 18.82, 0.,
00111 35* 1500.,2420.65,17.94,1.0957E-8,
00111 36* 1550., 0., 17.29, 0.,
00111 37* 1600.,2590.65,16.84,3.4502E-9,
00111 38* 1650., 0., 16.50, 0.,
00111 39* 1700.,2700.65,16.17,1.1918E-9/
00116 40* IF(Z.LT.0.) GO TO 81
00120 41* 30=6356.36
00121 42* 30=9.8066
00122 43* WMO=28.9644
00123 44* 35=8314.32
00124 45* ZM=Z*1000.
00125 46* ROME=6356360.
00126 47* IF(Z.GT.90.) GO TO 6
00130 48* DO 3 I=1,8
00133 49* IF(ZS(I).LE.Z.AND.Z.LT.ZS(I+1)) GO TO 5
00137 51* 3 CONTINUE
00140 52* 5 ZL=INT(ZS(I))*1.
00141 53* ZU=INT(ZS(I+1))*1.
00142 54* ZLM=ZL*1000.
00143 55* ZUM=ZU*1000.
00144 56* IF(I.EQ.8) ZU=88.743
00146 57* W=M*MO
00147 58* HT=(RO*Z)/(RO+Z)
00150 59* HM=HT*1000.
00151 60* G=(TMS(I+1)-TMS(I))/(ZU-ZL)
00152 61* IF(G.LT.0. OR .G.GT.0.) GO TO 12
00154 62* P=PS(I)*EXP(-(GO*WMO*(HM-ZLM)))/(RS*TMS(I))*100.
00155 63* GO TO 13
00156 64* 12 P=PS(I)*((TMS(I)/(TMS(I)+G*(H1-ZL)))*((GO*WMO)/(RS*GM)))*100.
00157 65* 13 T=TMS(I)+G*(HT-ZL)
00160 66* GO TO 25

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***** SDATA *****
00161 67* 6 DO 7 I=9,33*2
00164 68* IF(ZS(I).LE.Z.AND.7.LT.ZS(I+2)) GO TO 8
00166 69* 7 CONTINUE
00170 70* 81 TED.
00171 71* PED.
00172 72* DED.
00173 73* RETURN
00174 74* 8 ZL=ZS(I)
00175 75* ZU=ZS(I+2)
00176 76* ZLM=ZL*1000.
00177 77* ZUM=ZU*1000.
00200 78* ZMID=ZS(I+1)
00201 79* AO=X*S(I)
00202 80* A2=-2.*(P.**MS(I+1)-MMS(I+2)-AO)/(ZU-ZL)**2.)
00203 81* A1=(MMS(I+2)-AO-A2*(ZU-ZL)**2.)/(ZU-ZL)
00204 82* A=AO+A1*(Z-ZL)+A2*(Z-ZL)**2.)
00205 83* S=(TMS(I+2)-TMS(I))/(ZS(I+2)-ZS(I))
00206 84* G=M*G*.001
00207 85* TK=ZLM-(TMS(I)/GM)
00210 86* SE=(F*O*G*ROM*ROM)/(RS*GM)
00211 87* A=((ROM+ZM)*(ZLM-TK)/(ZM-TK)*(ROM+ZLM))
00212 88* BE(S/((TK+ROM)**2.))
00213 89* P=PS(I)*((ROM+ZM)*(ZLM-TK)/(ZM-TK)*(PCV+ZLM))**S/((TK+ROM)
00214 90* 1**2.))**EXP((-S*(ZLM-ZM))/((TK+ROM)*(ZM+ZM))*(ZLM+ROM))**100.
00215 91* T=TW*(I)+G*(Z-ZS(I))
00216 92* T=(W*/MHO)*TM
00217 93* 25 DE(LW*P)/(RS*T)
00218 94* 26 RETURN
00220 95* END

```

END OF COMPILATION: NO DIAGNOSTICS.
 @HDG,P ***** TIME *****
 @FOR,S PROFAS,TIME,TINF
 FOR S11E-02/04/74-18:55:51 (0,)

SUBROUTINE TINF ENTRY POINT 000340

STORAGE USED: CODE(1) 000347; DATA(0) 000127; BLANK COMMON(2) 000000

COMMON BLOCKS:

0003 IOTEMP 000050
 0004 COMJAC 000010

EXTERNAL REFERENCES (BLOCK, NAME)

0005 SIN
 0006 XPRR
 0007 COS
 0010 EXP
 0011 RERR35

***** TINF *****

STORAGE ASSIGNMENT (BLOCK, TYPE, RELATIVE LOCATION, NAME)

0001	000136	210L	0001	000156	250L	0000	R	000040	A1	0000	R	000041	A2		
0000	R	000042	A3	0000	R	000043	B1	0000	R	000044	B2	0000	R	000004	CON
0000	R	000000	C1	0000	R	000001	C2	0000	R	000002	C3	0003	R	000044	DX
0004	R	000004	D1	0000	R	000012	D1	0000	R	000013	D2	0000	R	000014	D3
0000	R	000015	D4	0004	R	000016	D5	0004	R	000017	E1	0000	R	000017	E1
0000	R	000030	E10	0000	R	000031	E11	0000	R	000032	E12	0000	R	000021	E3
0000	R	000022	E4	0000	R	000023	E5	0000	R	000024	E6	0000	R	000026	ER
0000	R	000027	E9	0003	R	000036	F10	0003	R	000037	F10B	0000	R	000006	GAMMA
0003	R	000040	G1	0000	R	000052	G1	0000	R	000053	G2	0000	R	000033	H
0003	R	000045	HL	0003	R	000026	H1	0003	R	000024	IDA	0003	R	000110	INJPS
0003	R	000000	IOTEM1	0003	R	000001	IOTEM2	0003	R	000002	IUG	0003	R	000042	MTN
0003	R	000023	MN	0003	R	000003	NMCOP	0003	R	000043	NMORE	0003	R	000007	P
0003	R	000007	PHI	0003	R	000034	PHIR	0003	R	000006	PHI1	0003	R	000003	PI
0004	R	000005	R	0003	R	000012	RD1	0003	R	000032	RI	0003	R	000013	RT1
0003	R	000017	RU1	0003	R	000020	RV1	0004	R	000002	SDA	0003	R	000003	SHA
0000	R	000051	TAU1	0000	R	000016	ST1	0003	R	000021	SU1	0003	R	000036	TAU
0003	R	000035	THETR	0000	R	000033	TC	0004	R	000006	TE	0000	R	000035	THETA
0000	R	000045	TV	0003	R	000046	VL	0000	R	000046	TL	0000	R	000054	TS
0003	R	000005	XMJD	0000	R	000011	XMN	0004	R	000000	XLAT	0004	R	000010	XM

00101	1*	SUBROUTINE TINF	TINF0100
00103	2*	COMMON/IOTEMP/IOTEM1,IOTEM2,IUG,NMCOP,DD,XMJD,PHI1,PHI,	TINF0200
00103	3*	NSAME,RP1, RD1, RT1, SPl, SPl, SPl, SPl, SPl, SPl, SPl, SPl, SPl, SPl,	TINF0300
00103	4*	S, MN, IDA, IYR, HI, PHIR, THETR, S, RI, H, PHIR, THETR, F10, F10B, GI,	TINF0400
00103	5*	. IHR, MIN, NMORE, DX, HL, VL, DZ	TINF0500
00104	6*	COMMON/COMJAC/XLAT, XLONG, SDA, SHA, DY, R, TE, EM	TINF0600
00104	7*	SUBROUTINE TINF CALCULATES THE EXOSPHERIC TEMPERATURE ACCORDING TO	TINF0700
00104	8*	SAO NO. 313, 1973.	TINF0800
00104	9*		TINF0900
00104	10*		TINF1000
00104	11*		TINF1100
00104	12*		TINF1200
00104	13*	F10 = SOLAR RADIO NOISE FLUX (XE-22 WATTS/M**2)	TINF1300
00104	14*	F10B = 81-DAY AVERAGE F10	TINF1400
00104	15*	GI = GEOMAGNETIC ACTIVITY INDEX, AP	TINF1500
00104	16*	LAT = GEOGRAPHIC LATITUDE AT PERIGEE (IN RAD)	TINF1600
00104	17*	SDA = SOLAR DECLINATION ANGLE	TINF1700
00104	18*	SHA = SOLAR HOUR ANGLE	TINF1800
00104	19*	DY = D/Y (DIURNAL/TROPICAL YEAR) + 1	TINF1900
00104	20*	R = 0.31 (DIURNAL FACTOR)	TINF2000
00104	21*	CONSTANTS -- C=SOLAR ACTIVITY VARIATION, BETA, ETC. = DIURNAL VARIATION	TINF2100
00104	22*	D=GEOMAGNETIC VARIATION, E=SEMIANNUAL VARIATION.	TINF2200
00104	23*		TINF2300
00105	24*	C1 = 383.0	TINF2400
00106	25*	C2 = 3.32	TINF2500
00107	26*	C3 = 1.80	TINF2600
00107	27*		TINF2700
00110	28*	PI = 3.14159265	TINF2800
00111	29*	CON = 0.01745329252	TINF2900
00112	30*	BETA = -37.0*CON	TINF3000
00113	31*	GAMMA = 43.0*CON	TINF3100

REPRODUCIBILITY OF THE ORIGINAL PAGE IS POOR

DATE 020474

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***** T.I.F *****
00114 32*
00115 35*
00116 34*
00117 35*
00118 36*
00119 37*
00120 38*
00121 39*
00122 40*
00123 41*
00124 42*
00125 43*
00126 44*
00127 45*
00130 46*
00131 47*
00132 48*
00133 49*
00134 50*
00135 51*
00136 52*
00137 53*
00138 54*
00139 55*
00140 56*
00141 57*
00142 58*
00143 59*
00144 60*
00145 61*
00150 62*
00151 63*
00152 64*
00153 65*
00154 66*
00155 67*
00156 68*
00157 69*
00158 70*
00159 71*
00160 72*
00161 73*
00162 74*
00163 75*
00164 76*
00165 77*
00166 78*
00167 79*
00168 80*
00169 81*
00170 82*
00171 83*
00172 84*
00173 85*
00174 86*
00175 87*
00176 88*

P = 6.0*CON
XN = 2.5
XNN = 3.0

C
D1 = 28.0
D2 = 0.03
D3 = 1.0
D4 = 100.0
D5 = -0.08

C
E1 = 2.41
E2 = 0.349
E3 = 0.206
E4 = 360.*CON
E5 = 226.5*CON
E6 = 720.*CON
E7 = 247.6*CON
E8 = 0.1145
E9 = 0.5
E10 = E4
E11 = 342.3*CON
E12 = 2.16

C SOLAR ACTIVITY VARIATION:
C TC = C1 + C2*F10B + C3*(F10 - F10B)
C
C DIURNAL VARIATION
C
ETA = 0.5*ABS(XLAT - SDA)
THETA = 0.5*ABS(XLAT + SDA)
TAU = SHA + BETA + P*SIN(SHA + GAMMA)
TPI = 2*PI
210 IF(TAU+PI) 210,230,250
220 TAU=TAU+TPI
90 TC 210
230 IF(TAU-PI) 250,250,240
240 TAU=TAU-TPI
90 TO 230
250 CONTINUE
A1 = SIN(THETA)**XM
A2 = COS(ETA)**XM
A3 = COS(TAU/2.0)**YH
D1 = 1.0 + P*A1
D2 = (A2-A1)/B1
TV = R1*(1. + R*B2*A3)
TL = TC*TV

C GEO-MAGNETIC VARIATION
C
T6 = D3*GI + D4*(1-EXP(.35*GI))

C SEMI-ANNUAL VARIATION
C
G3 = 0.5*(1.0 + SIN(E10.0Y +E11) )
G3 = G3**E12
00174 88*

```

TIN09900
 TIN09000
 TIN09100
 TIN09200
 TIN09300
 TIN09400
 TIN09500
 TIN09600
 TIN09700
 TIN09800

***** TIME *****
 00175 89*
 00176 90*
 00177 91*
 00200 92*
 00200 93*
 00200 94*
 00200 95*
 00201 96*
 00202 97*
 00203 98*

TAU1 = DY + E8*(G3 - E9)
 G1 = E2 + E3*(SIN(E4*TAU1 + E5))
 G2 = SIN(E6*TAU1 + E7)
 TS = E1 + F103*G1*G2
 C EXOSPHERIC TEMPERATURE
 TE = TL + TG + TS
 RETURN
 END

END OF COMPILATION: NO DIAGNOSTICS.

SHDG,P ***** THE *****
 GFOR,S PROFAS,TIME,TIME
 FOR S1E-02/04/74-18:55:54 (0,)

SUBROUTINE TME ENTRY POINT 000335

STORAGE USED: CODE(1) 000344; DATA(0) 000101; BLANK COMMON(2) 000000

COMMON BLOCKS:

0003 COMJAC 000013
 0004 IOTEMP 000050

EXTERNAL REFERENCES (BLOCK, NAME)

0005 SIN
 0006 ASIN
 0007 TAN
 0010 NERR35

STORAGE ASSIGNMENT (BLOCK, TYPE, RELATIVE LOCATION, NAME)

0001	000253	110L	0001	000263	120L	0001	000266	130L	0001	000272	140L	0001	000301	210L																	
0001	000311	230L	0001	000321	250L	0004	000040	AP	0004	000007	A1	0000	000010	A2																	
0000	R	000011	A3	0000	R	000012	A4	0000	R	000022	B2	0000	000023	B3																	
0000	R	000027	B4	0004	R	000004	DX	0004	000044	DX	0004	000047	DZ	0004	000031	G															
0003	000007	EM	0000	R	000002	FMJD	0004	000036	F10	0004	000037	F10B	0004	000026	H1	0004	000000	IOTEM1													
0000	R	000005	GMT	0000	R	000013	GP	0004	000033	H	0004	000045	HL	0004	000023	MN	0004	000007	PHI												
0004	000024	IDA	0000	I	000016	IFACT	0004	I	000041	IHR	0004	I	000042	MIN	0004	000032	PI2	0004	000007	PHI											
0004	000001	IOTEM2	0004	000002	IUG	0004	I	000025	IYR	0004	I	000010	NSAME	0004	000007	PHI	0004	000032	PI2	0004	000007	PHI									
0000	I	000014	N	0004	000003	NWCOP	0004	000043	NMORE	0004	000031	PI	0000	R	000032	PI2	0004	000012	RD1	0004	000020	RV1									
0004	000034	PHIR	0004	000006	PH11	0004	000027	PH1R	0000	R	000020	RAP	0000	R	000030	RAS	0004	000017	RU1	0004	000016	ST1									
0000	R	000033	PI32	0003	000005	R	0004	000013	RT1	0004	000013	RT1	0004	000014	SPI	0004	000003	SHA	0004	000035	THETR	0004	000003	XHR							
0004	000032	RI	0004	000011	RP1	0004	000015	SD1	0003	000006	T	0004	000046	VL	0000	R	000017	XFACT	0000	R	000004	XMIN	0000	R	000024	Y1					
0004	000021	SU1	0004	000022	SV1	0004	000026	TP1	0000	R	000000	XLAT	0003	R	000001	XLONG	0000	R	000000	YEAR	0000	R	000000	YR	0000	R	000001	YR			
0004	000030	THETR1R	0000	R	000002	SDA	0004	000002	SDA	0004	000022	SV1	0003	000006	T	0004	000046	VL	0000	R	000000	XLAT	0003	R	000001	XLONG	0000	R	000000	YEAR	
0000	R	000006	XJ	0003	000000	XJ	0000	R	000000	XLAT	0003	R	000001	XLONG	0000	R	000000	YEAR	0000	R	000000	YR	0000	R	000000	YR	0000	R	000001	YR	
0004	R	000005	XMJD	0000	R	000015	YN	0000	R	000000	YEAR	0000	R	000000	YEAR	0000	R	000000	YEAR	0000	R	000000	YR	0000	R	000000	YR	0000	R	000001	YR

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***** TIME *****

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00101 1* SUBROUTINE TME
00102 2* COMMON/CONJAC/XLAT,XLONG,SPA,SHA,DY,R,T,EM
00103 3* COMMON/IOTEMP/IOTE,ITEMP,IUG,NMCCP,DD,XM,IO,PHI,PHI,
00104 4* *SAME/R... ,I, RTI, SPI, SPl, RUI, RV1, SV1,
00104 5* S MIN, IDA, IYR, HI, PHIR,THET1,,G,KI,H,PHIR,THETR,F10,F10E,AP,
00104 6* IHR,MIN,MMORE,DX,HL,VL,DZ
00104 7*
00104 8*
00104 9* C LIST
00104 10* C INPUT
00104 11* C MM=MONTH, IDA=DAY, IY=HR, HR = HOUR, MIN = MINUTE
00104 12* C XLAT = LATITUDE (INPUT-GEOCENTRIC LATITUDE.)
00104 13* C XLONG = LONGITUDE (INPUT-GEOCENTRIC LONGITUDE. OUTPUT -180 TO + 180)
00104 14* C SDA = SOLAR DECLINATION ANGLE (IN RAD)
00104 15* C SHA = SOLAR HOUR ANGLE (IN RAD)
00104 16* C UD = DAY NUMBER FROM 1JAN.
00104 17* C DY = DD/TROPICAL YEAR
00104 18* C
00104 19* C
00104 20* C SET CONSTANTS
00104 21* C YEAR = 365.2422
00105 22* C YR=IYR
00106 23* C DY = DD/YEAR
00107 24* C 30 FMJD = XMJD - 2455619.
00110 25* C
00110 26* C COMPUTE GREENWICH MEAN TIME IN MINUTES GMT
00110 27* C
00110 28* C
00111 29* C XHR = IHR
00112 30* C XMIN = MIN
00113 31* C GMT = 60*XHR + XMIN
00113 32* C
00113 33* C COMPUTE GREENWICH MEAN POSITION - GP (IN DEG)
00113 34* C
00114 35* C XJ = (XMJD - 2415020.0)/(36525.0)
00115 36* C A1=99.6909833
00116 37* C A2 = 36000.76854
00117 38* C A3 = 0.00038706
00117 39* C A4 = 0.25068447
00120 40* C GP = A1 + A2*XJ + A3*XJ*XJ + A4*GMT
00121 41* C N = GP/360.
00122 42* C XN = N
00123 43* C GP = GP - XN*360.
00124 44* C
00124 45* C COMPUTE RIGHT ASCENSION; POINT - RAP (IN DEG)
00124 46* C
00124 47* C
00124 48* C
00124 49* C
00125 50* C IFACT = XLOI/G/180.
00126 51* C XFACT = IFACT
00127 52* C XLONG = 360. * XFACT - XLONG
00130 53* C RAP = GP + XLONG
00131 54* C IJ = RAP/360.
00132 55* C XN = N
00133 56* C RAP = RAP - XN*360.

```

```

***** THE *****
00133 57* C
00133 58* C COMPUTE CELESTIAL LONGITUDE - XLS (IN RAD) - -PI/2 TO +PI/2
00133 59* C
00134 60* B1 = 0.017203
00135 61* S2 = 0.0335
00136 62* R3 = 1.410
00137 63* Y1 = B1*FMJN
00140 64* XLS = Y1 + R2*SIN(Y1) - B3
00141 65* TPI = 6.28318
00142 66* N = XLS/TPI
00143 67* XN = N
00144 68* XLS = XLS - XN*TPI
00144 69* C COMPUTE SOLAR DECLINATION ANGLE - SDA (IN RAD)
00144 70* C
00144 71* B4 = (TPI/360.)*23.45
00145 72* SDA = ASIN(SIN(XLS)*SIN(B4))
00146 73* C
00146 74* C COMPUTE RIGHT ASCENSION OF SUN - RAS (IN RAD) - -PI/2 TO +PI/2
00146 75* C
00146 76* RAS = ASIN(TAN(SDA)/TAN(B4))
00147 77* C
00147 78* C PUT RAS IN SAME QUADRANT AS XLS
00147 79* C
00147 80* C
00150 81* PI = 3.14159265
00151 82* PI2 = PI/2.
00152 83* PI32 = 3.*PI2
00153 84* RAS = ABS(RAS)
00154 85* TEMP = ABS(XLS)
00155 86* IF(TEMP = PI2) 130,130,100
00150 87* 100 IF(TEMP = PI) 105,105,110
00153 88* 105 RAS = PI - RAS
00164 89* GO TO 130
00165 90* 110 IF(TEMP = PI32) 115,115,120
00170 91* 115 RAS = PI + RAS
00171 92* GO TO 130
00172 93* 120 RAS = TPI - RAS
00173 94* 130 IF (RAS) 135,140,140
00176 95* 135 RAS = -RAS
00177 96* 140 CONTINUE
00177 97* C
00177 98* C COMPUTE SOLAR HOUR ANGLE - SHA (IN DEG) - -
00177 99* C
00200 100* SHA = RAP*(PI/180.) - RAS
00201 101* IF(SHA) 210,230,230
00204 102* 210 IF(SHA+PI) 220,250,250
00207 103* 220 SHA=SHA+TPI
00210 104* 90 TO 210
00211 105* 230 IF(SHA-PI) 250,250,240
00214 106* 240 SHA=SHA-TPI
00215 107* 90 TO 230
00216 108* 250 CONTINUE
00217 109* C
00217 110* RETURN
00220 111* END

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TME05703
TME05800
TME05900
TME06000
TME06100
TME06200
TME06300
TME06400
TME06500
TME06600
TME06700
TME06800
TME06900
TME07000
TME07100
TME07200
TME07300
TME07400
TME07500
TME07600
TME07700
TME07800
TME07900
TME08000
TME08100
TME08200
TME08300
TME08400
TME08500
TME08600
TME08700
TME08800
TME08900
TME09000
TME09100
TME09200
TME09300
TME09400
TME09500
TME09600
TME09700
TME09800
TME09900
TME10000
TME10100
TME10200
TME10300
TME10400
TME10500
TME10600
TME10700
TME10800
TME10900
TME11000
TME11100

APPENDIX D - SUMMARY OF PROGRAM CHARACTERISTICS
(Program Operating Environment)

1. Hardware

- a. Computer - Univac 1108
- b. Core Requirements - slightly under 32 K words
- c. Magnetic Tapes - All tapes are 7 tracks. Tapes required are:
1 program tape, 1 "SCIDAT" data tape (see pages 7-10 and 51-106), from 1 to 4 4-D data tapes, depending on the number of months to be used under control of one run card (see pages 4-6).
- d. Card Punch - Standard card punch required if optional card output is selected (see page 108).
- e. Plotter - None required
- f. Drum or Disk - 2 temporary drum files are required. No permanent drum or disk files are created by a program run. Optional punch output could easily be converted to come out on permanent drum or disk file instead.
- g. Other Hardware - None

2. Software

- a. Operating System - EXEC 8
- b. Language - FORTRAN IV (UNIVAC FORTRAN V)
- c. Type of Run - Batch
- d. Library Subroutines - None
- e. Program Overlays - (Optional) see page 39

3. Program Specifications

- a. Common - See pages 40-44
- b. Program Segments - See pages 39-50
- c. Program Subroutines - See pages 32-36
- d. Listing - See pages 126-202
- e. Flow Charts - See pages 3, 33, 37, and 38
- f. Sample Input - See pages 107-110, and 11-21
- g. Sample Output - See pages 111-125, and 22-27
- h. Diagnostic Messages - See pages 28-31

REFERENCES

- Fowler, Mary G., and J. H. Willard, (1972): "Users Manual for Four-Dimensional Models", Contract No. NAS 8-28720, June, 1972 Environmental Research and Technology.
- Groves, G. V., (1971); "Atmospheric Structure and Its Variations in the Region From 25 to 120 Km", AD-737-794, AFCRL-71-0410, July.
- Jacchia, L. G., (1970); "New Static Models of the Thermosphere and Exosphere with Empirical Temperature Profiles", Smithsonian Astrophysical Observatory, Special Report 313.
- Spiegler, D. B., and Mary G. Fowler, (1972); "Four-Dimensional World-Wide Atmospheric Models (Surface to 25 Km Altitude)", NASA CR-2082.

APPROVAL

FOUR-D GLOBAL REFERENCE ATMOSPHERE
USERS MANUAL AND PROGRAMMERS MANUAL
PART II

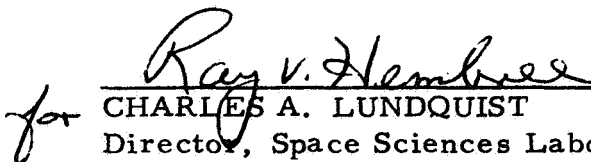
By C. G. Justus, Arthur Woodrum, R. G. Roper
and O. E. Smith

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This document has also been reviewed and approved for technical accuracy.



W. W. VAUGHAN
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for CHARLES A. LUNDQUIST
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