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STATISTICAL ANALYSIS OF GENERAL AVIATION  
VG-VGH DATA

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Prepared under Contract No. NAS1-12389 by

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for

NATIONAL AERONAUTICS AND SPACE ADMINISTRATION

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## FOREWORD

This report, prepared by Technology Incorporated, Dayton, Ohio, documents the statistical analysis of general aviation VG-VGH data. All data contained herein were collected from general aviation aircraft operations over the past 10 years.

The NASA Langley Research Center was the procuring agency for this program under NASA Contract No. NAS1-12389. The Technical Representative for NASA was Mr. Joseph W. Jewel, Jr.

For Technology Incorporated, the principal personnel active in this program were as follows: Kenneth W. Payaays succeeded by Raymond L. Dickey, Project Engineer; Larry E. Clay, Senior Research Engineer; Martin S. Moran, Research Engineer; Thomas P. Severyn, Jr. Research Engineer; Ruth E. Meyers, Data Processing Specialist; James E. Kirchmer, Data Processing Specialist.

The contents of this report reflect the views of the authors who are responsible for the accuracy of the analysis presented herein. The contents do not necessarily reflect the official views or policies of the NASA Langley Research Center. This report does not constitute a standard, specification, or regulation.

## ABSTRACT

In support of a NASA program to represent the loads spectra of general aviation aircraft operating in the Continental United States, VG and VGH data collected since 1963 in eight operational categories [(1) twin-engine executive, (2) single-engine executive, (3) personal, (4) instructional, (5) commercial survey, (6) aerial application, (7) commuter, and (8) aerobatic] were processed and analyzed to determine or prepare the following: (a) adequacy of data sample and current operational categories, (b) parameter distributions required for valid data extrapolation, (c) envelopes of equal probability of exceeding the normal load factor ( $n_z$ ) versus airspeed for gust and maneuver loads, (d) probability of exceeding current design maneuver, gust, and landing impact  $n_z$  limits, (e) fatigue spectra for gust, maneuver, and landing impact  $n_z$  loads, and (f) relationship between design and operational airspeeds. Significant findings included the following: (1) the data distributions were mostly log-normal, the rest being normal; (2) the Instructional and Commercial Survey categories had the highest probability of exceeding the design  $n_z$  limit for maneuver and gust, respectively; (3) while the Aerial Application and Instructional categories required only 860 and 3393 landings, respectively, to experience landing impacts of  $1.67 \Delta n_z$ , the other categories required more than 19,000 landings to reach this level; (4) of the 24 aircraft types, 17 had airspeeds above the cruise velocity ( $V_C$ ), but none had airspeeds above the dive velocity ( $V_D$ ); the Personal category had the highest probability of exceeding  $V_C$ ; the Instructional and Commercial Survey categories had the highest  $V/V_C$  ratios (approximately 1.2); and the Twin-Engine Executive category had the highest  $V/V_D$  ratio (approximately 0.925); and (5) each of the eight operational categories had a distinct load spectrum which reflected the operational characteristics of the category definition, and the various aircraft types within each operational category generally had loads which conformed closely with the average spectrum.

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## 1. INTRODUCTION

### 1.1 Background of General Aviation VG/VGH Program

In 1963 NASA initiated a program to collect an operational data sample representative of the United States general aviation fleet. The following eight operational categories were defined to collectively represent general-aviation-aircraft usage: (1) twin-engine executive, (2) single-engine executive, (3) personal, (4) instructional, (5) commercial survey, (6) aerial application, (7) commuter, and (8) aerobatic. Reference 1 lists typical missions in these categories as follows:

#### Twin- and single-engine executive:

Charter flights - cargo and personnel.

Business flights - company and individual.

Instrument check flights - training for instrument card.

Instructional flights - check-out for larger aircraft.

#### Personal:

Flying club owned - aircraft flown by club with 3 to 21 members: used for pleasure, instruction, or business flights.

Individually owned - used for pleasure and business.

Company owned - airplane rented to individual for business or pleasure flying; also aircraft used as check-out for heavier airplane.

#### Instructional:

Training flights - all instrumented airplanes owned by flying schools; used as basic trainers for private license; also used by student after solo for cross-country flight.

#### Commercial survey:

Pipeline-patrol flights - patrols flown from 76 to 91 meters (250 to 300 feet) above terrain to check for leaks or breaks in the pipeline.

Forest-patrol flights - patrols flown 457 meters (1500 feet) above terrain for fire detection. When fire is spotted, descents are made to 61 to 91 meters (200 to 300 feet) to check condition of terrain around the fire.

Pathfinder flights - flies to fire perimeter and marks drop area. Descents are made to 15 to 46 meters (50 to 150 feet) above terrain to insure turbulence is not too severe for chemical bomber during dropping run. Chemical bomber drops are observed, and effects on fire are noted.

Fish-spotting flights - patrols flown 457 to 610 meters (1500 to 2000 feet) above water. Occasional descents are made to 91 to 152 meters (300 to 500 feet).

#### Aerobatic:

Noncompetitive flights - aircraft flown by amateurs. Occasional aerobatics are performed, usually as individual maneuvers.

Competitive flights - aircraft flown in airshows, in national and international aerobatic competition, and in practice sessions. Obligatory maneuvers, one immediately after another, are performed in a restricted cube of air.

#### Aerial application:

Crop dusting and/or spraying flights - aircraft flown at heights ranging from 0.9 to 5.5 meters (3 to 18 feet) above crops. Spreading runs are characterized by sharp pushover at start and hard pull-up at end of spreading runs.

#### Commuter:

Operational flights - normally scheduled passenger carrying operations.

Crew flights - crew training, or flights on which structural or mechanical tests are made on the aircraft.

These operational categories do not generally correspond to the Reference 2 aircraft categories (normal, utility, acrobatic) because, except for the aerobatic and aerial application operational categories, the operators select aircraft on the basis of performance and/or cost instead of design maneuver capability.

The analysis will examine about 12,000 hours of VGH and 70,000 hours of VG data. To obtain the data sample, three types of aircraft were generally selected as representative of each operational category. The type of operation, the number of basic types of aircraft, the number of aircraft, and the hours of data used in the analysis are listed in

Table I. The basic VG-VGH data were collected from aircraft selected nationwide to avoid a geographical bias. All instrumented aircraft were owned by individuals or companies who participated on a voluntary basis. The data collection objective for each instrumented aircraft was 1000 hours of in-flight data during each of the four calendar quarters.

TABLE I. SUMMARY OF RECORDED DATA

<u>Operational Category</u>	<u>Type of Data</u>	<u>No. of Aircraft Types</u>	<u>No. of Aircraft</u>	<u>Hours of Data</u>
Twin-engine executive	VG	3	18	14,722
	VGH	5	9	3,377
Single-engine executive	VG	3	15	8,430
	VGH	3	8	1,366
Personal	VG	3	15	5,456
	VGH	3	9	724
Instructional	VG	4	17	10,357
	VGH	5	6	2,843
Commercial survey	VG	2	14	26,089
	VGH	4	4	2,291
Aerial application	VG	3	7	1,857
	VGH	2	2	484
Commuter	VG	3	5	4,000
	VGH	2	2	1,510
Aerobatic	VG	3	5	382
	VGH	0	0	0

Two types of NASA recorders, the VGH and the VG recorder, were used to collect the data. The VGH recorder is an oscillograph which records a time history of indicated airspeed, pressure altitude, and c.g. normal acceleration at a rate of approximately one minute of elapsed time per 1.27 cm (0.5 inch) along a 70-mm-wide film. The VG recorder records an envelope of maximum c.g. normal accelerations and their corresponding airspeeds for the period of operation (a one-flight duration to several hundred hours) while the recording medium is installed. References 3 and 4 detail the VG and VGH recorders, respectively.

The VGH oscillograph data was reduced to digital samples of indicated airspeed and pressure altitude at one-minute intervals during the recorded flights and digital samples of c.g. normal acceleration, indicated airspeed, and pressure altitude at each acceleration peak and trough outside the prescribed thresholds ( $\pm 0.4g$  for general aviation aircraft and  $\pm 0.2g$  for airline aircraft). The VG data was reduced to the maximum and minimum

c.g. normal acceleration in each 10-knot indicated airspeed interval, the maximum indicated airspeed attained, and the number of flight hours during the period that each recording slide was installed.

Table II summarizes the pertinent data for the instrumented aircraft. With a breakdown by aircraft operational category, this table lists the type and number of installations, the amount of recorded data, and the pertinent aircraft configuration and operational characteristics.

TABLE II. CHARACTERISTICS OF INSTRUMENTED AIRCRAFT

VG hr: 14,722, VGH hr: 3,377

	Twin-engine executive type									
	1	2	3	4	5A	5B	5C	6	50	
V-G installations	0	0	2	8	4	3	1	1	1	
V-G hours	0	0	0	7191	3035	2730	145	486	1135	
VGH installations	4	1	2	1	1	0	0	0	0	
VGH hours	824	693	357	350	1153	0	0	0	0	
Maximum gross weight										
kN	117.7	55.6	40.0	21.4	21.5	32.7	22.2	30.2	23.1	
lb	26 455	12 500	9000	4800	4830	5100	4990	6800	5200	
Wing span:										
m	16.3	11.5	14.0	11.3	11.0	11.2	11.2	12.1	11.2	
ft	53.5	37.6	45.9	37.0	36.0	36.9	36.9	39.8	36.9	
Wing area:										
m <sup>2</sup>	41.0	21.5	26.0	19.2	16.3	16.3	16.3	18.6	16.3	
ft <sup>2</sup>	441	231.8	279.7	207	175	175	175	200	175	
Type propulsion	Turbojet	Turbojet	Turbo-prop	Piston	Piston	Piston	Piston	Piston	Piston	
V <sub>C</sub> at sea level, knots	368	350	208	172	182	182	182	200	182	
V <sub>NE</sub> at sea level, knots	437	358	234	216	215	223	219	236	219	
V <sub>D</sub> at sea level, knots	465	400	260	240	239	248	243	262	243	
Δn <sub>m</sub> at V <sub>C</sub>	1.50	3.40	2.70	2.80	2.80	2.80	2.80	2.60	2.80	
Δn <sub>m</sub> at V <sub>NE</sub>	2.00	2.76	2.68	2.52	2.52	2.52	2.52	2.44	2.52	
Δn <sub>m</sub> at V <sub>D</sub>	3.40	2.44	2.10	2.10	1.97	1.84	1.91	1.93	2.35	

<sup>a</sup>Maximum operating speed

VG hr: 8430, VGH hr: 1366

	Single-engine executive type												
	7A	7B	8A	8B	8C	8D	8E	8G	8F	9A	9B	9C	9D
V-G installations	2	1	0	2	1	2	1	0	1	1	2	0	2
V-G hours	1160	137	0	898	23	1392	277	0	1202	785	1170	0	1386
VGH installations	2	0	1	0	0	0	1	1	1	1	0	1	0
VGH hours	237	0	149	0	0	0	229	16	175	424	0	136	0
Maximum gross weight													
kN	12.9	12.9	11.8	12.3	12.3	13.1	13.9	14.7	15.1	11.3	11.8	11.8	12.5
lb	2900	2900	2650	2775	2775	2950	3125	3300	3400	2550	2800	2650	2800
Wing span:													
m	11.0	11.0	10.0	10.0	10.0	10.0	10.2	10.2	10.2	11.0	11.0	11.0	11.0
ft	36.0	36.0	32.8	32.8	32.8	32.8	33.5	33.5	33.5	36.0	36.0	36.0	36.2
Wing area:													
m <sup>2</sup>	16.5	16.5	16.5	16.5	16.5	16.5	16.8	16.8	16.8	16.2	16.2	16.2	16.2
ft <sup>2</sup>	175	178	177.6	177.6	177.6	177.6	181	181	181	174	174	174	174
Type propulsion	Piston	Piston	Piston	Piston	Piston	Piston	Piston	Piston	Piston	Piston	Piston	Piston	Piston
V <sub>C</sub> at sea level, knots	156	156	139	152	152	174	161	165	165	139	139	139	139
V <sub>NE</sub> at sea level, knots	197	197	175	175	182	195	195	195	195	160	167	162	167
V <sub>D</sub> at sea level, knots	219	219	217	217	201	217	217	217	217	177	186	180	186
Δn <sub>m</sub> at V <sub>C</sub>	2.80	2.80	3.40	3.40	3.40	3.40	3.40	3.40	3.40	2.80	2.80	2.80	2.80
Δn <sub>m</sub> at V <sub>NE</sub>	2.57	2.52	2.76	2.76	2.76	2.76	2.76	2.76	2.76	2.52	2.52	2.52	2.52
Δn <sub>m</sub> at V <sub>D</sub>	2.35	2.45	2.40	2.58	2.88	2.75	2.43	2.35	2.37	2.50	2.33	2.33	2.50

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## 1.2 Program Objective

The program objective was to provide the following:

- 1) A check on the adequacy of the sample size for statistical analysis.
- 2) The statistical distributions of the parameters required for extrapolation.
- 3) Envelopes of equal probability of exceeding  $n_z$  versus airspeed for gust and maneuver loads.
- 4) The probability of exceeding current design maneuver and gust limit loads for the aircraft categories, namely, normal, utility, and acrobatic.
- 5) A review of the adequacy of design categories to account for operational experiences.
- 6) Fatigue spectra for gust, maneuver, and landing impact loads.
- 7) The probability of exceeding the design landing gear load factor.
- 8) Airspeed practices in relation to design airspeeds.
- 9) Recommendations for future data collection and presentation.

## 2. RESULTS AND DISCUSSION

### 2.1 Recorded Data Sample Size

Table I lists the number of hours of VG and VGH data, the number of aircraft types, and the number of instrumented aircraft in each operational category.

The number of recorded VGH hours and VG records in each operation is a significant parameter in estimating the design probabilities. The minimum required sample size for the VG and VGH data was established by constructing a two-way contingency table and applying the chi-squared goodness-of-fit test. Accordingly, the minimum sample sizes for the VG and VGH data were found to be 125 records and 150 hours, respectively. Therefore, the sample size for the Aerobatic category in both the VG and VGH data was inadequate, and the sample sizes for the Aerial Application and Commuter categories in the VG data were inadequate. However, all the VGH



data for the Commuter category were recorded on only two instrumented aircraft which is not sufficiently representative of commuter-type aircraft.

In practice it is often assumed that an observed variate conforms to some particular distribution. It is then desirable to determine the size of data sample required to adequately describe the distribution of the parent population. One widely used technique is to test the independence of two randomly chosen data samples by the construction of a two-way contingency table. If the probability of occurrence of a particular value of the variate is independent of the random sample that it is taken from, then the random sample distribution is assumed to adequately describe the parent distribution.

Suppose that  $n$  individuals or items are classified according to two criteria A and B, that there are  $r$  classifications  $A_1, A_2, \dots, A_r$  in A and  $s$  classifications  $B_1, B_2, \dots, B_s$  in B, and that the number of individuals belonging to  $A_i$  and  $B_j$  is  $N_{ij}$ . We have then a  $r \times s$  contingency table with cell frequencies  $N_{ij}$  and  $\sum N_{ij} = n$ :

	$B_1$	$B_2$	$B_3$	...	$B_s$
$A_1$	$N_{11}$	$N_{12}$	$N_{13}$	...	$N_{1s}$
$A_2$	$N_{21}$	$N_{22}$	$N_{23}$	...	$N_{2s}$
$A_3$	$N_{31}$	$N_{32}$	$N_{33}$	...	$N_{3s}$
$A_r$	$N_{r1}$	$N_{r2}$	$N_{r3}$	...	$N_{rs}$

As a further notation we shall denote the row totals by  $N_i$  and the column totals by  $N_j$ ; that is,

$$N_i = \sum_j N_{ij} \quad \text{and} \quad N_j = \sum_i N_{ij}$$

Of course,

$$\sum_i N_i = \sum_j N_j = n$$

The  $n$  individuals will be regarded as a sample of size  $n$  from a multinomial population with probabilities  $p_{ij}$  ( $i=1, 2, \dots, r$ ;  $j=1, 2, \dots, s$ ). Let the null hypothesis,  $H_0$ , be that the A and B classifications are independent, i.e., that

the probability that an individual falls in  $B_j$  is not affected by the  $A$  class in which the individual belongs. When the null hypothesis is not true, there is said to be an interaction between the two classification criteria. Two statistical events  $A_i$  and  $B_j$  are said to be independent if

$$P\{A_i \cap B_j\} = P\{A_i\} P\{B_j\}$$

Thus the null hypothesis is

$$H_0 : p_{ij} = p_i p_j$$

where  $\sum p_i = 1$  ;  $\sum p_j = 1$

Now construct the statistic

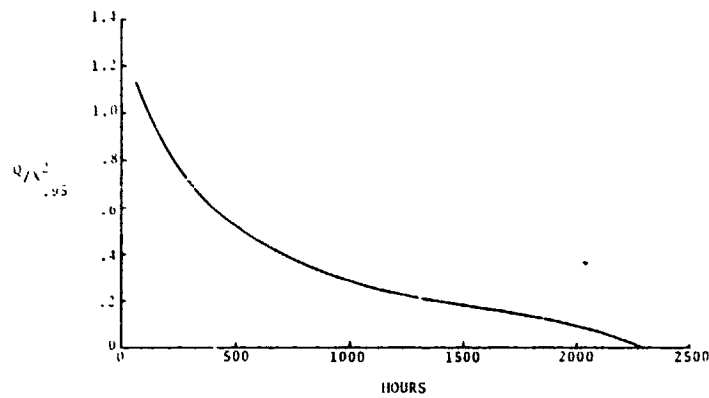
$$Q = \sum_{i,j} \frac{[N_{ij} - n(N_i/n)(N_j/n)]^2}{n(N_i/n)(N_j/n)}$$

where  $N_{ij} - n(N_i/n)(N_j/n)$  is the difference between the actual number of occurrences of a particular value of the variate  $N_{ij}$  and the predicted number if  $H_0$  is true. Of course,

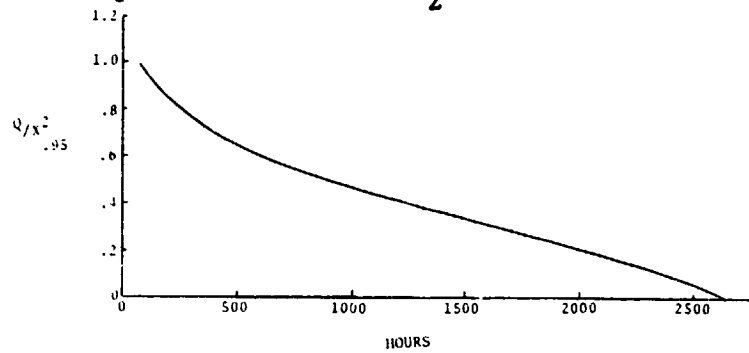
$$N_i/n = p_i ; N_j/n = p_j$$

It can then be shown that the statistic  $Q$  has approximately the chi-square distribution with  $(r-1)(s-1)$  degrees of freedom. The test criterion is to reject  $H_0$  for large  $Q$ . Thus,  $Q$  will tend to be small for  $H_0$  true and large for  $H_0$  false. The value of the chi-squared statistic  $Q$  is then compared with the critical value with  $(r-1)(s-1)$  degrees of freedom and the desired significance level.

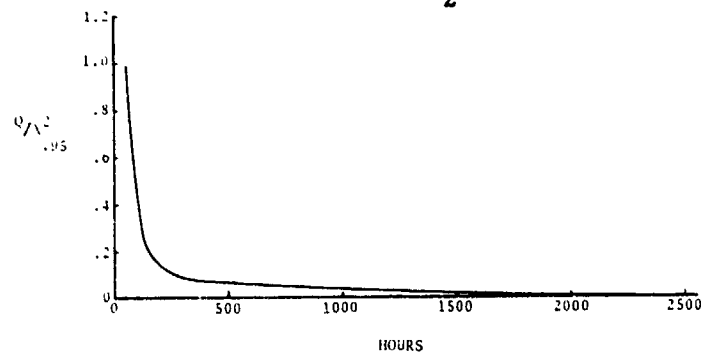
Contingency tables were constructed and the chi-squared goodness-of-fit test was applied in the VGH sample size investigation. Figures 1(a) through 1(d) present the results. The point at which the ratio of  $Q$  to  $\chi^2_{.95}$  exceeds 1.0 is the point at which the data sample distribution no longer adequately describes the parent distribution. Positive and negative maneuver and gust accelerations were investigated. The positive maneuver sample exhibited the largest amount of VGH hours required for an adequate sample size. The same test was applied to the VG data. The results are shown in Figure 2.



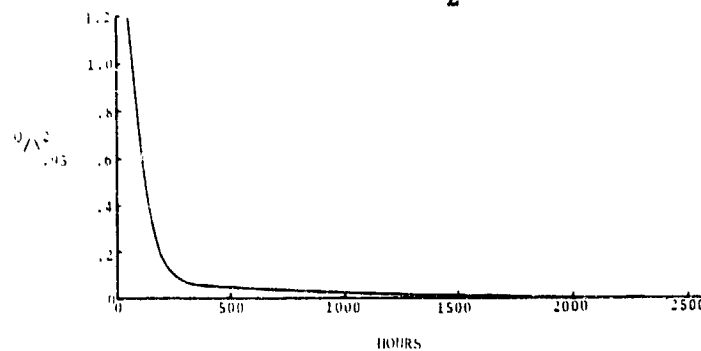
a. Composite Positive  $n_z$ 's in VGH Maneuvers



b. Composite Negative  $n_z$ 's in VGH Maneuvers



c. Composite Positive  $n_z$ 's in VGH Gusts



d. Composite Negative  $n_z$ 's in VGH Gusts

Figure 1. Plot of Hours vs. Sample Size Index for Composite VGH Positive and Negative Maneuver and Gust  $n_z$ 's

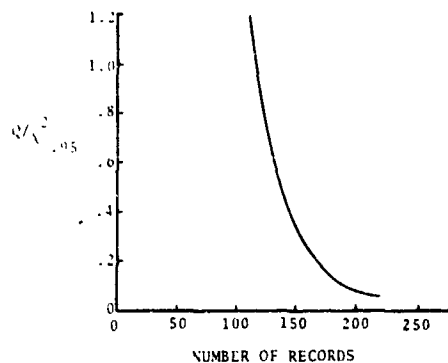


Figure 2. Plot of Records vs. Sample Size Index for Composite VG  $n_z$ 's

## 2.2 Observed Statistical Distributions

In extrapolating the load factor distributions to determine the probabilities of exceeding the design limits, it was necessary to fit a distributional form to the recorded data. Three standard distributions, normal, log-normal, and exponential (a special case of the Weibull distribution), were considered. A widely used procedure to establish the data distribution is the chi-square test. However, since this method requires a great deal of data, its application is limited. An alternative method is to plot the data on various types of probability paper (normal, log-normal, and Weibull). Then the plot which most closely approximates a straight line indicates the distribution type and consequently the corresponding paper type best suited to display the data. Figures 3 through 5 are samples of plots on each paper type. Since, as apparent, the plot on the log-normal paper most closely approximates a straight line and therefore best represents the data distribution, the data for each airspeed level in each of the operational categories were plotted on log-normal paper. Most of the recorded data conformed to the log-normal distribution, with the rest of the data resembling a normal distribution. None of the recorded data resembled an exponential distribution.

Except in a few flights where the instrumented aircraft within an operational category flew obviously different missions or where a single instrumented aircraft flew two distinct missions, there was no evidence to indicate that a load factor frequency distribution contained two or more sets of unrelated events. Flights where the instrumented aircraft within an operational category flew different missions were evident in the Commercial Survey and Aerial Application VGH data presented in Table IV (extreme values per flight). The distribution for aircraft type 23 in the Aerial Application category in Table IV also shows a dip at a  $\Delta n_z$  value of +0.7g. Those flights with maximum accelerations below a  $\Delta n_z$  of +0.8g were mostly cross-country flights and not the aircraft's primary crop-dusting mission which generally had maximum  $\Delta n_z$  values above +1.0g.

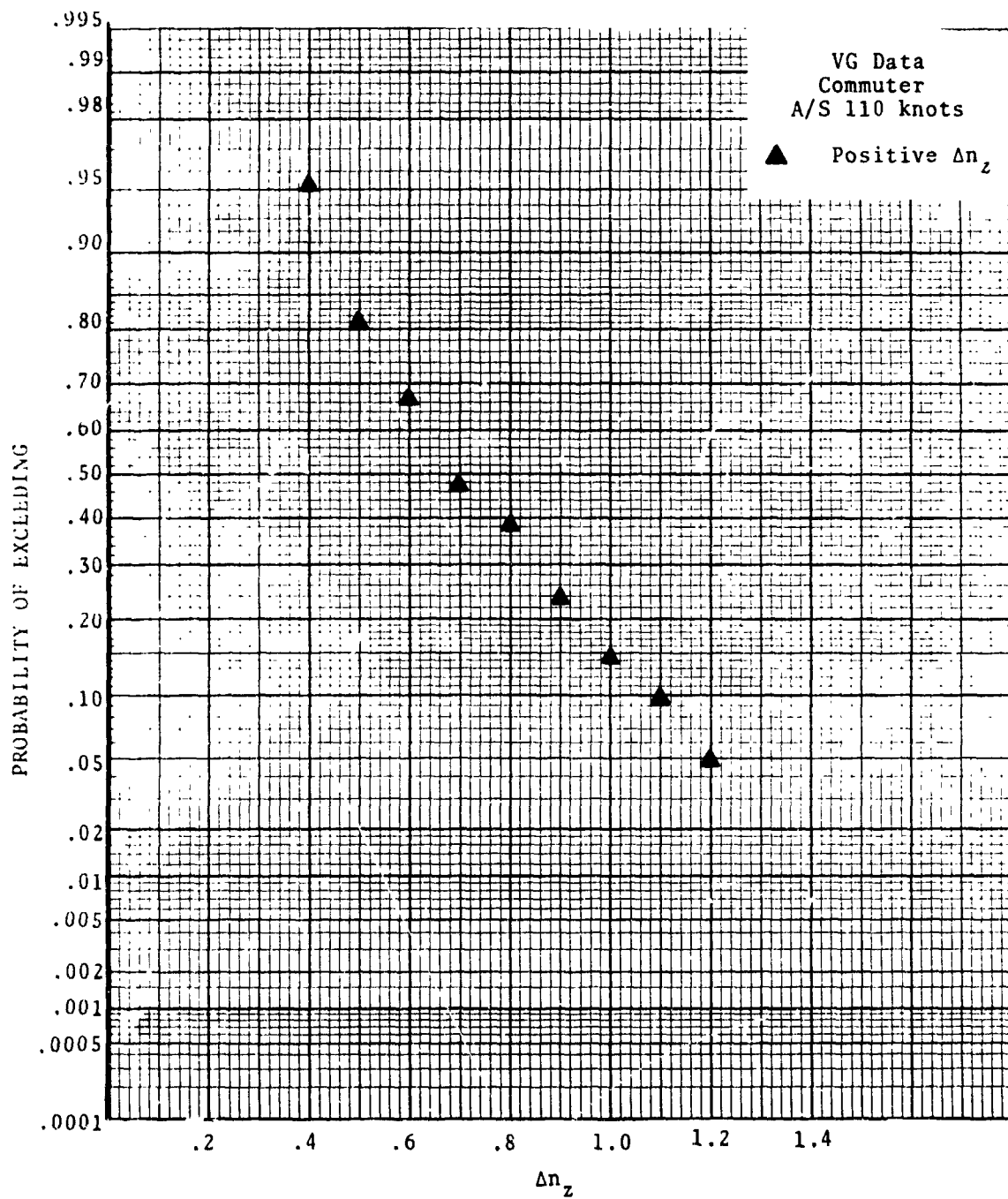


Figure 3. Sample of VG  $n_z$  Data Plotted as a Normal Distribution

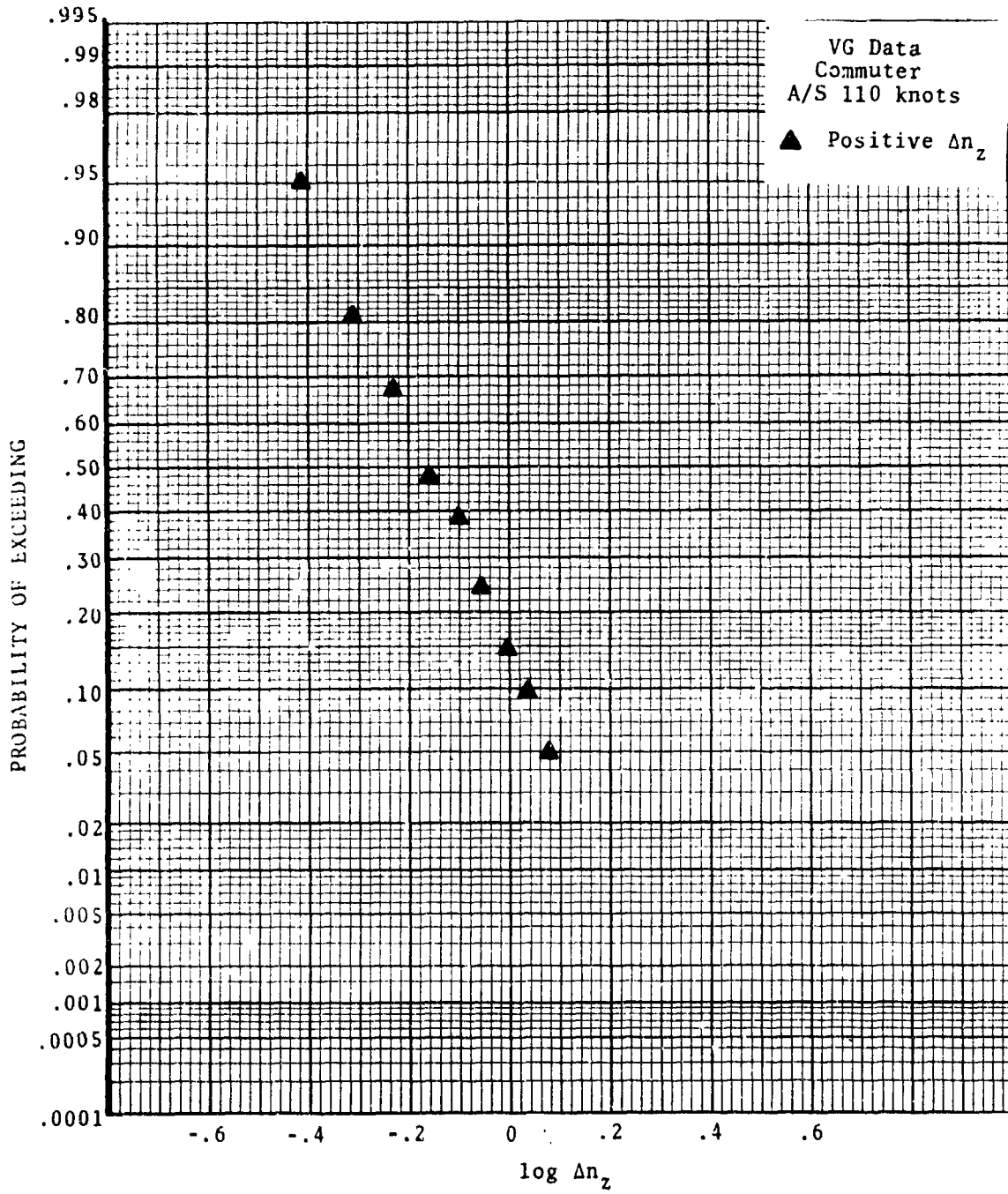


Figure 4. Sample of VG  $n_z$  Data Plotted as a Log-Normal Distribution

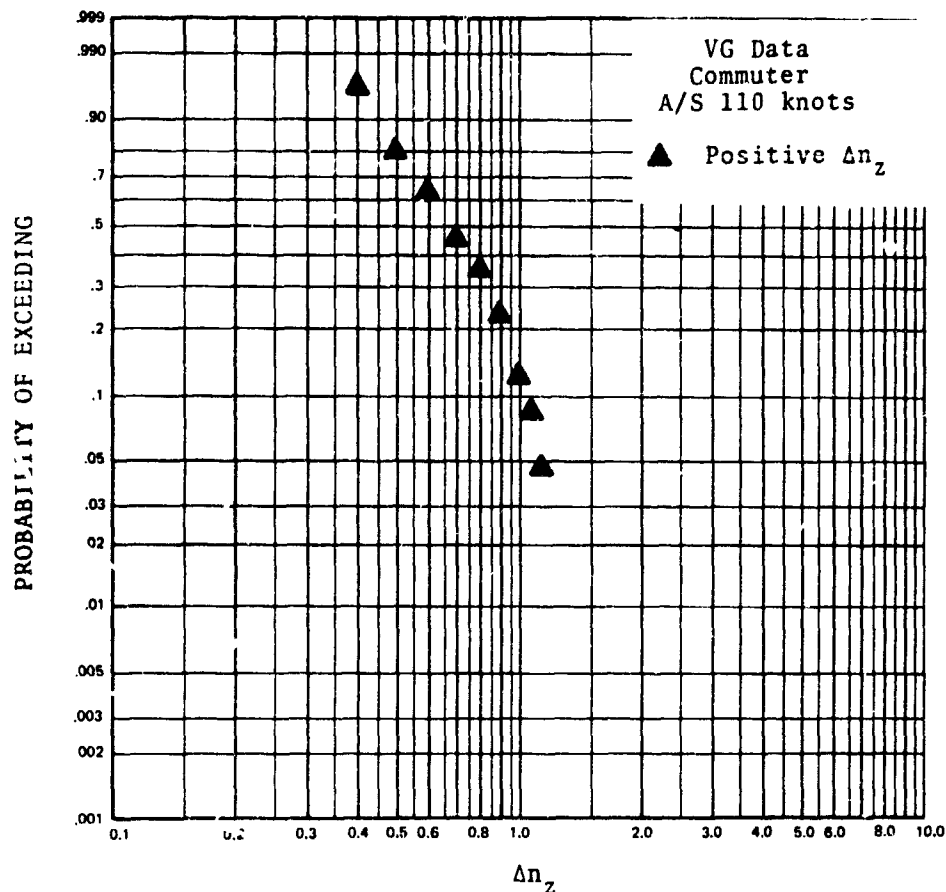


Figure 5. Sample of VG  $n_z$  Data Plotted as an Exponential Distribution

### 2.3 V-N Probability Distributions

Three V-N constant probability envelopes were constructed for each operational category from the VG data. The three envelopes represent 50%, 90%, and 95% probability levels and are based on an expected service life of 20,000 flight hours. This means that an aircraft flying 20,000 hours in a given operational category has a constant probability of not exceeding the  $\Delta n_z$ -airspeed combinations which define the envelope boundary. The three envelopes can also be interpreted as a 50%, 10%, or 5% probability that an aircraft will exceed the envelope boundary at least once during 20,000 flight hours. To construct the V-N envelopes for each operational category required first plotting the log of the  $\Delta n_z$  occurrences for each airspeed range on log-normal probability paper (see Figure 6). (In all tables and text discussions, the parameters are generally denoted by single values which represent the lower limits of the respective parameter ranges.) These "probability-of-exceeding- $\Delta n_z$ " curves yield a linear relationship between the log  $\Delta n_z$  values and the probability of a single  $\Delta n_z$  occurrence exceeding a  $\Delta n_z$  value. From these plots, and by considering each  $\Delta n_z$  occurrence as a

single statistical trial, it is possible to determine the probability of a single trial exceeding any  $\Delta n_z$  value. Dividing the total number of flight hours by the total number of  $\Delta n_z$  occurrences at a given airspeed in a particular operational category gives the expression for a statistical trial in terms of flight hours. With a single trial expressed in flight hours, the number of statistical trials occurring at each airspeed in 20,000 flight hours for a particular operational category can be calculated. It is assumed that the statistical trials ( $\Delta n_z$  occurrences expressed in flight hours) for the 20,000 flight hours satisfy the requirements for Bernoulli trials. That is, each trial has but two possible outcomes. Either the trial exceeds a particular  $\Delta n_z$  value or it does not. Second, each trial is independent of all other trials. Finally, the probability of exceeding a particular  $\Delta n_z$  value is constant from trial to trial. With the above assumption, the  $\Delta n_z$  values for the constant probability envelopes may be calculated as follows:

$$\{P(NE)\}^n = P_E$$

$$P(NE) = \{P_E\}^{1/n}$$

$$P(E) = 1 - P(NE)$$

where  $P(NE)$  = probability of not exceeding a particular  $\Delta n_z$  value in a single trial

$P(E)$  = probability of exceeding a particular  $\Delta n_z$  value in a single trial

$P_E$  = constant probability envelope value (0.5, 0.9, 0.95)

$n$  = number of trials at a given airspeed in 20,000 flight hours for a particular operational category

$\{P(NE)\}^n$  = probability of not exceeding a particular  $\Delta n_z$  value during  $n$  consecutive trials

Once  $P(E)$  is calculated at a given  $P_E$  value for a particular operational category and airspeed, the corresponding probability-of-exceeding- $n_z$  curve can be used to determine the  $\Delta n_z$  value. These  $\Delta n_z$  values are plotted versus airspeed for each operational category to form the three constant probability envelopes.

In the construction of these envelopes, the VG, rather than the VGH, data were used since the VG data provided the larger data sample.



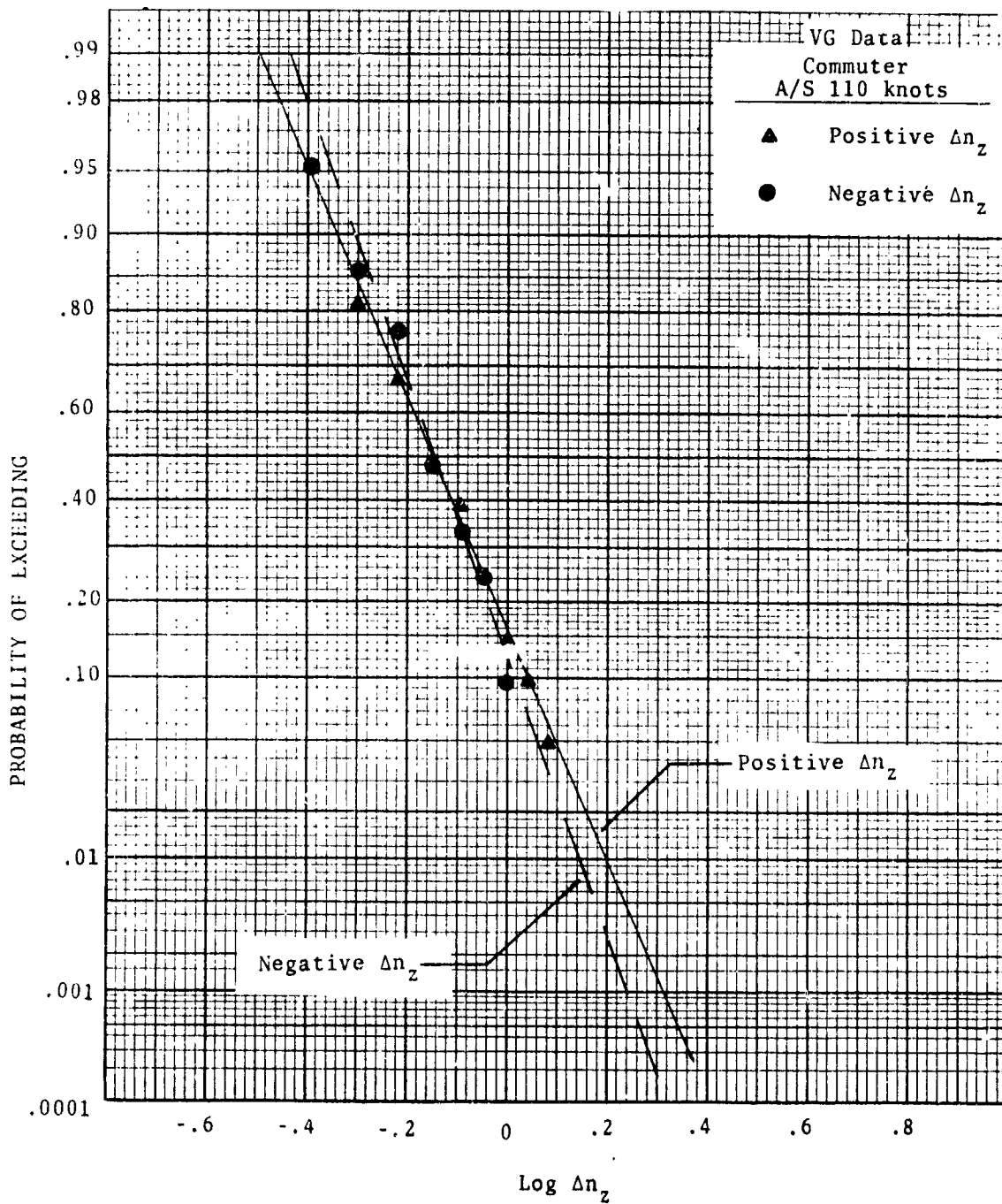


Figure 6. Probability-of-Exceeding- $\Delta n_z$  Curve at 110-Knot Airspeed for VG Data

Figures 7 through 13 show the constant probability envelopes for all the operational categories except Aerobatic which did not have enough  $\Delta n_z$  occurrences to construct valid probability-of-exceeding- $\Delta n_z$  curves for each airspeed.

Figure 7 shows the constant probability envelopes for the Twin-Engine Executive category. The envelope data compare favorably with the operational usage data presented in Table III. Figure 8 shows the constant probability envelopes for the Single-Engine Executive category. Again, the envelope data closely resemble those of the operational usage data presented in Table III.

Figure 9 shows the constant probability envelopes for the Personal category. The extreme values at 150 knots in each set of envelopes do not have corresponding values in the operational usage data presented in Table III. The probability-of-exceeding- $\Delta n_z$  curve for the 150-knot airspeed was constructed from only 20  $\Delta n_z$  occurrences and not all of the data points fall on any one of the three statistical distributions. However, since the probability-of-exceeding- $\Delta n_z$  curves for all other airspeeds in the Personal category were found to be log-normal distributions, the 150-knot distribution was also analyzed as log-normal. The tendency of the data points, as shown in Figure 14, to curve downward suggests that a linear extrapolation would yield higher than actual  $\Delta n_z$  values.

Figure 10 shows the constant probability envelopes for the Instructional category. The envelope data conform well with the operational data presented in Table III. Figure 11 shows the constant probability envelopes for the Commercial Survey category. The envelope data are the same as the operational data presented in Table III. The Commercial Survey and Aerial Application were the only two categories whose probability-of-exceeding- $\Delta n_z$  curves were constructed as normal, rather than log-normal, distributions. None of the categories had curves with an exponential distribution.

Figure 12 shows the constant probability envelopes for the Aerial Application category. The extreme values at 90 knots in the positive  $\Delta n_z$  envelopes do not have corresponding values in the operational usage data presented in Table III. The probability-of-exceeding- $\Delta n_z$  curve was analyzed as a log-normal distribution for the 90-knot airspeed and as a normal distribution for all other airspeeds. Any error in the linear extrapolation will of course be larger on a log scale than on a linear scale. An extreme  $\Delta n_z$  at low airspeed could also be due to a flap operation and a low-altitude approach.

Figure 13 shows the constant probability envelopes for the Commuter category. The extreme values at 190 knots in the negative  $\Delta n_z$  envelopes do not have corresponding values in the operational usage data presented in Table III. The probability-

of-exceeding- $\Delta n_z$  curves were constructed from only 17  $\Delta n_z$  occurrences. Again, any small error in the extrapolation would be compounded on the log scale.

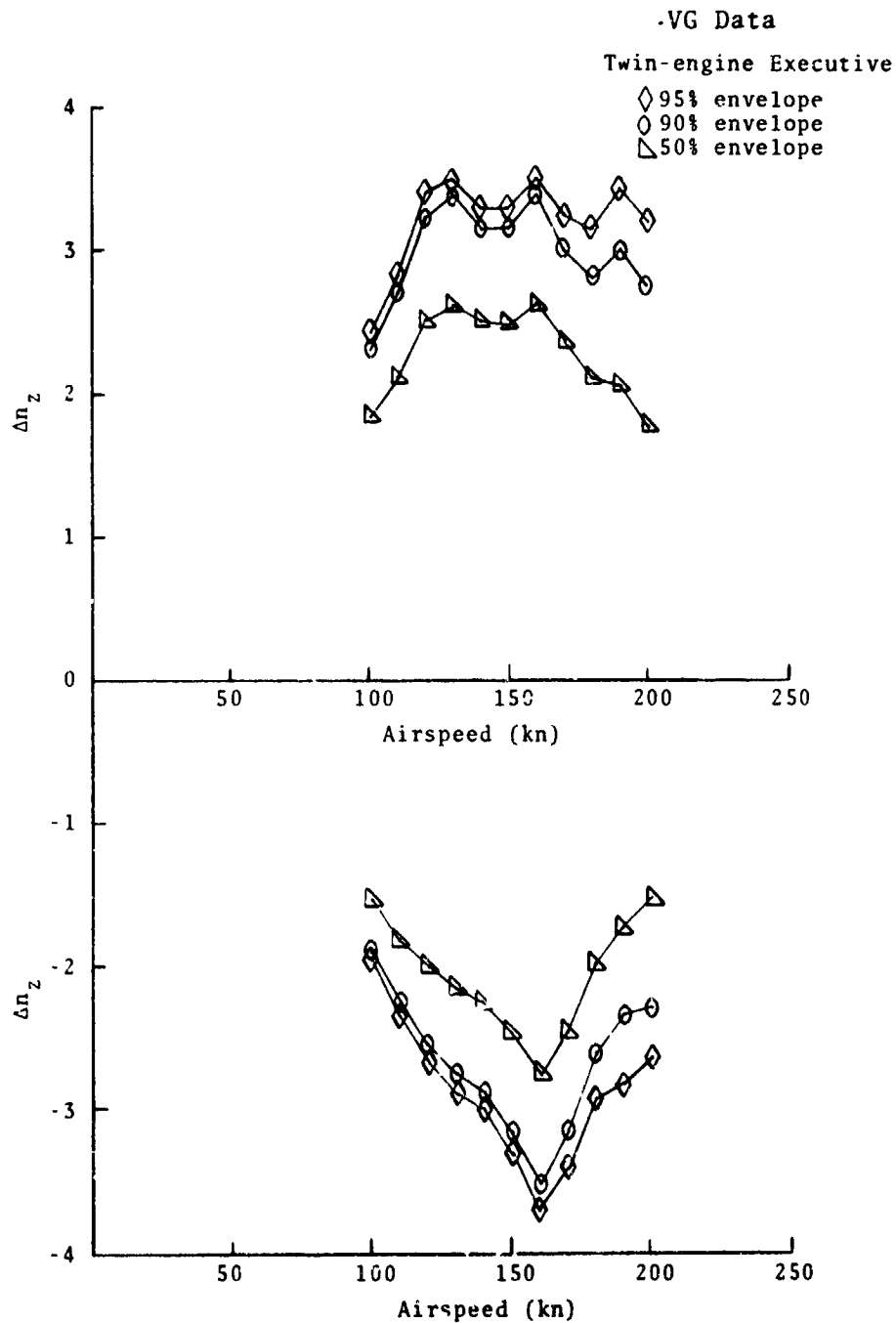


Figure 7. V-N Probability Distribution for Twin-Engine Executive Category Based on 20,000 Flight Hours of VG Data

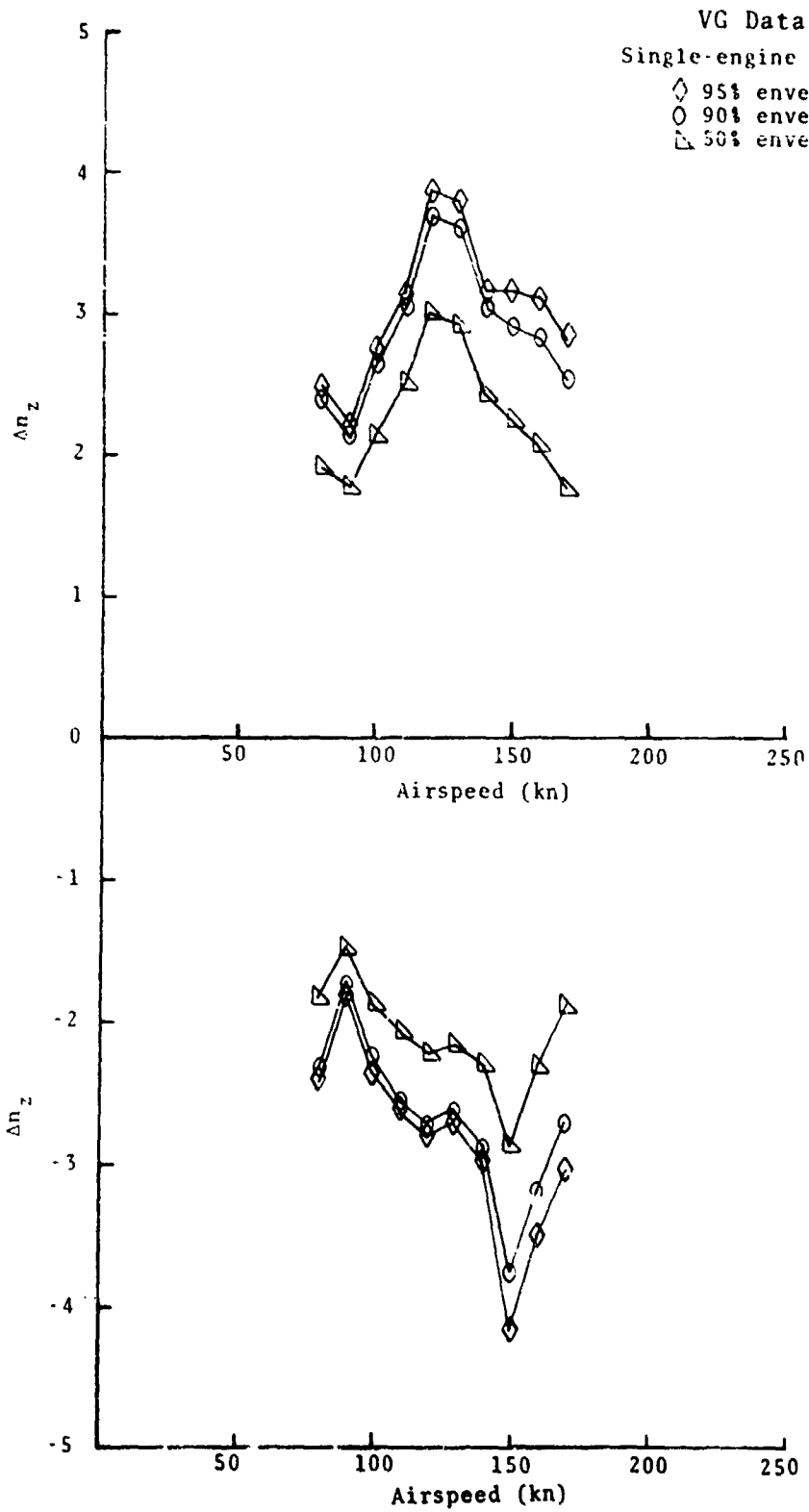


Figure 8. V-N Probability Distribution for Single-Engine Executive Category Based on 20,000 Flight Hours of VG Data

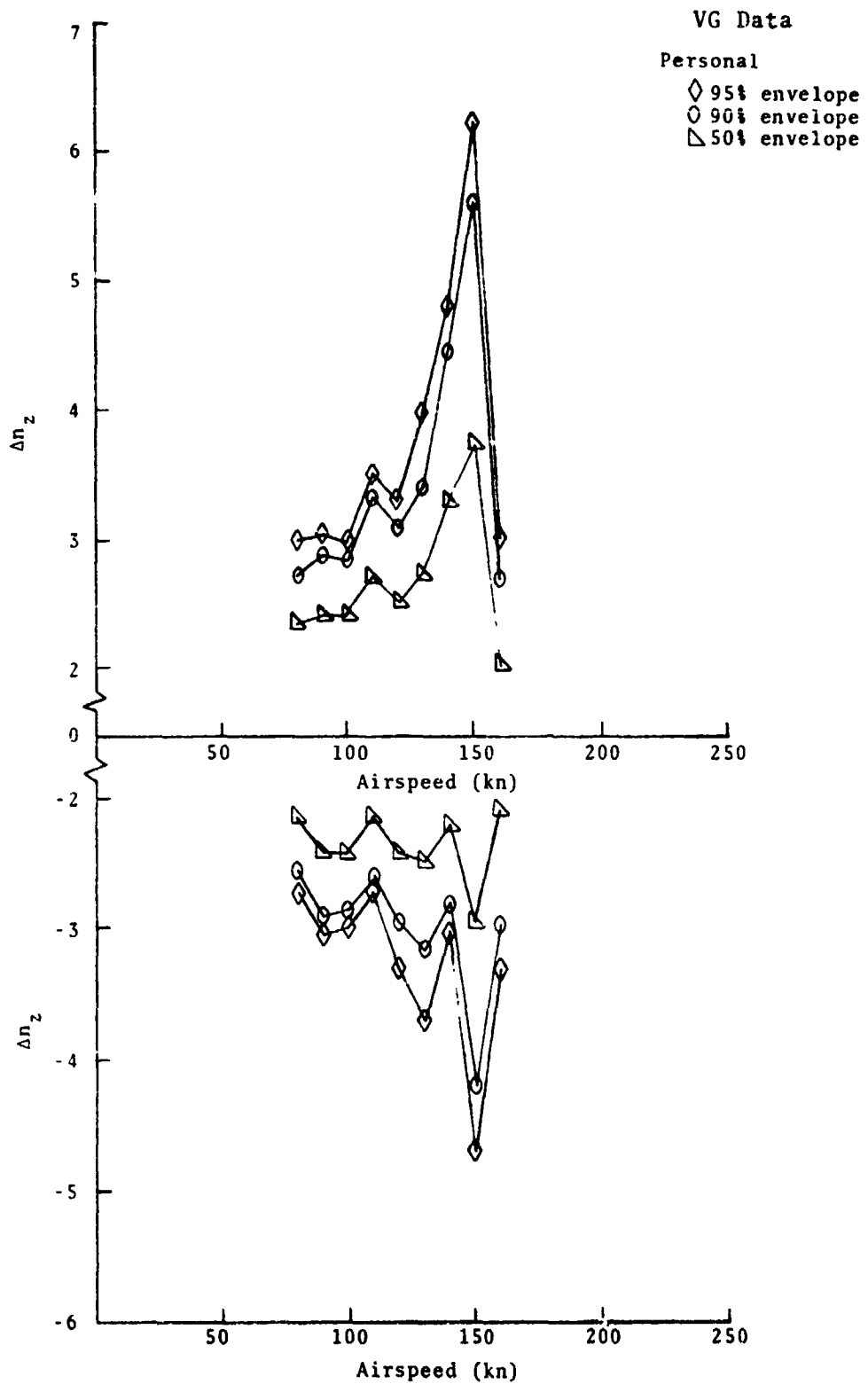


Figure 9. V-N Probability Distribution for Personal Category Based on 20,000 Flight Hours of VG Data

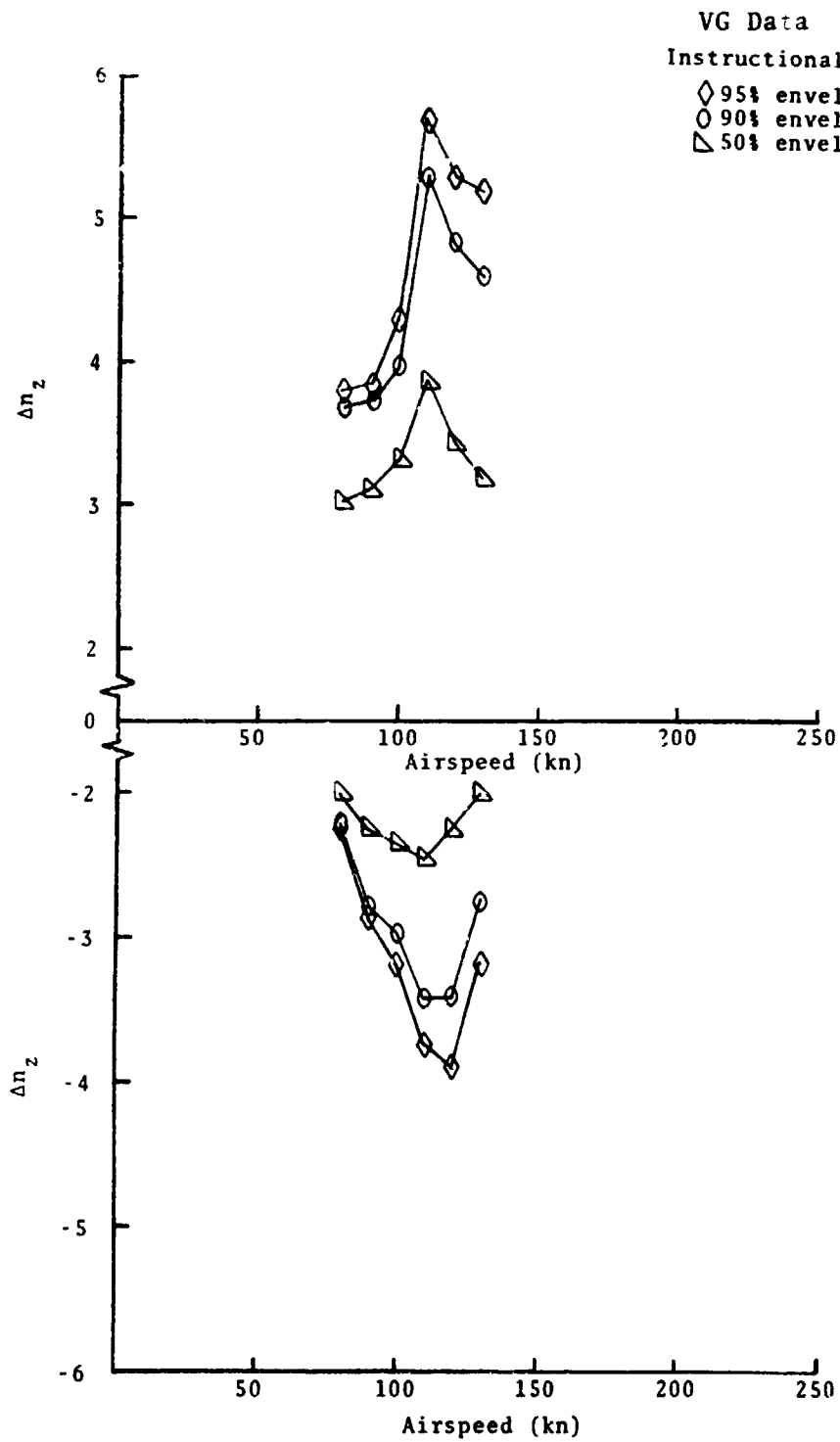


Figure 10. V-N Probability Distribution for Instructional Category Based on 20,000 Flight Hours of VG Data

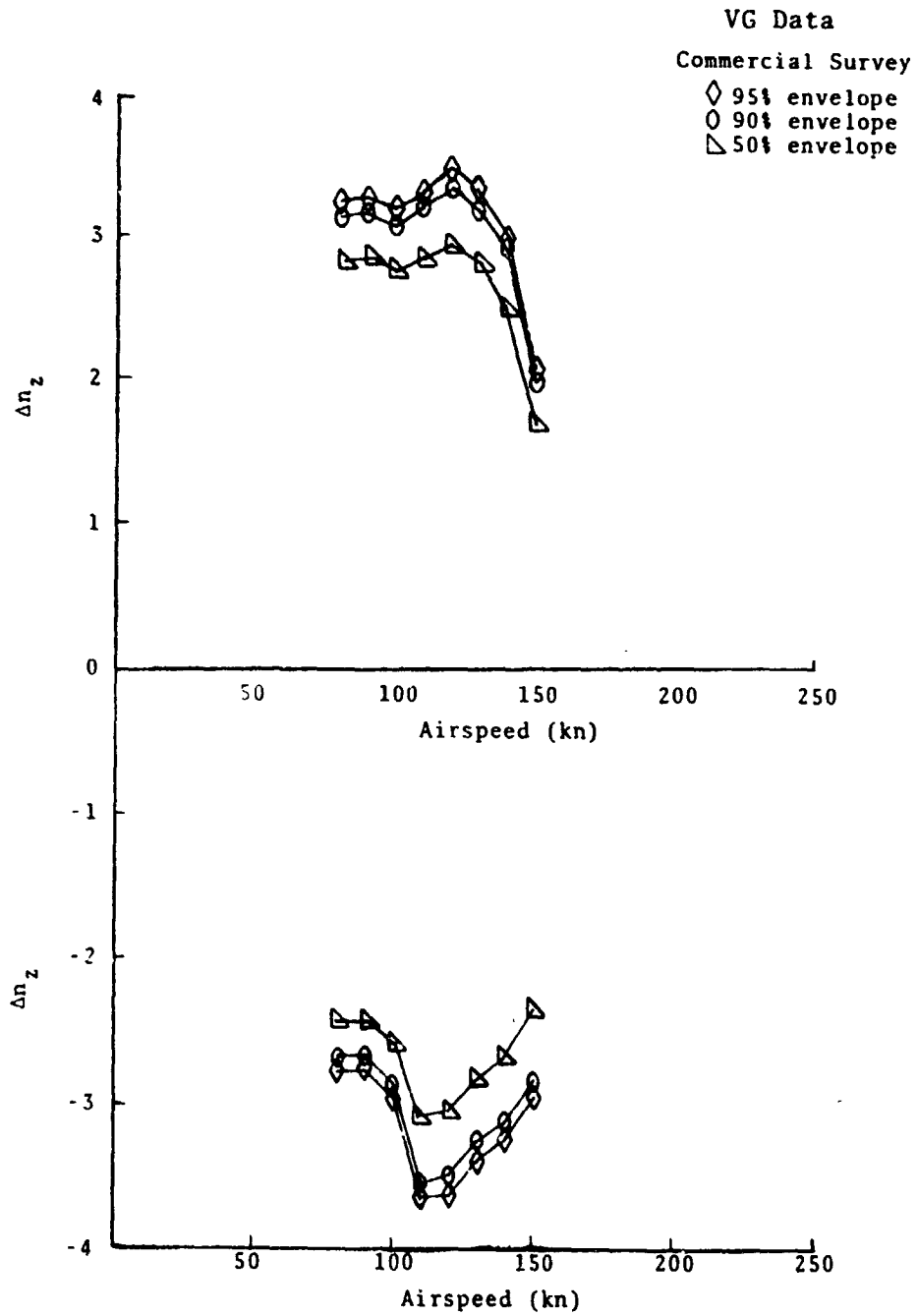


Figure 11. V-N Probability Distribution for Commercial Survey Category Based on 20,000 Flight Hours of VG Data

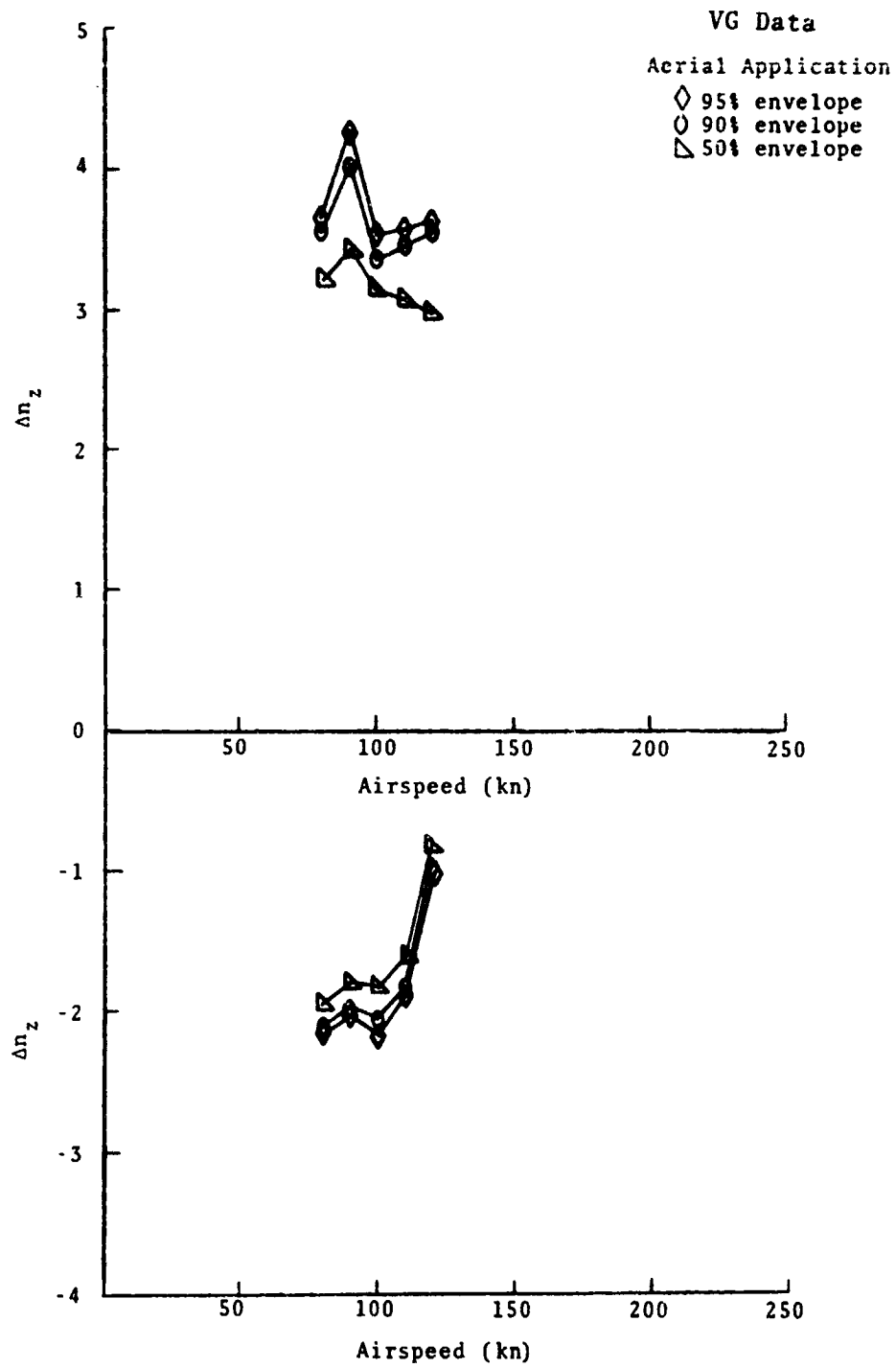


Figure 12. V-N Probability Distribution for Aerial Application Category Based on 20,000 Flight Hours of VG Data



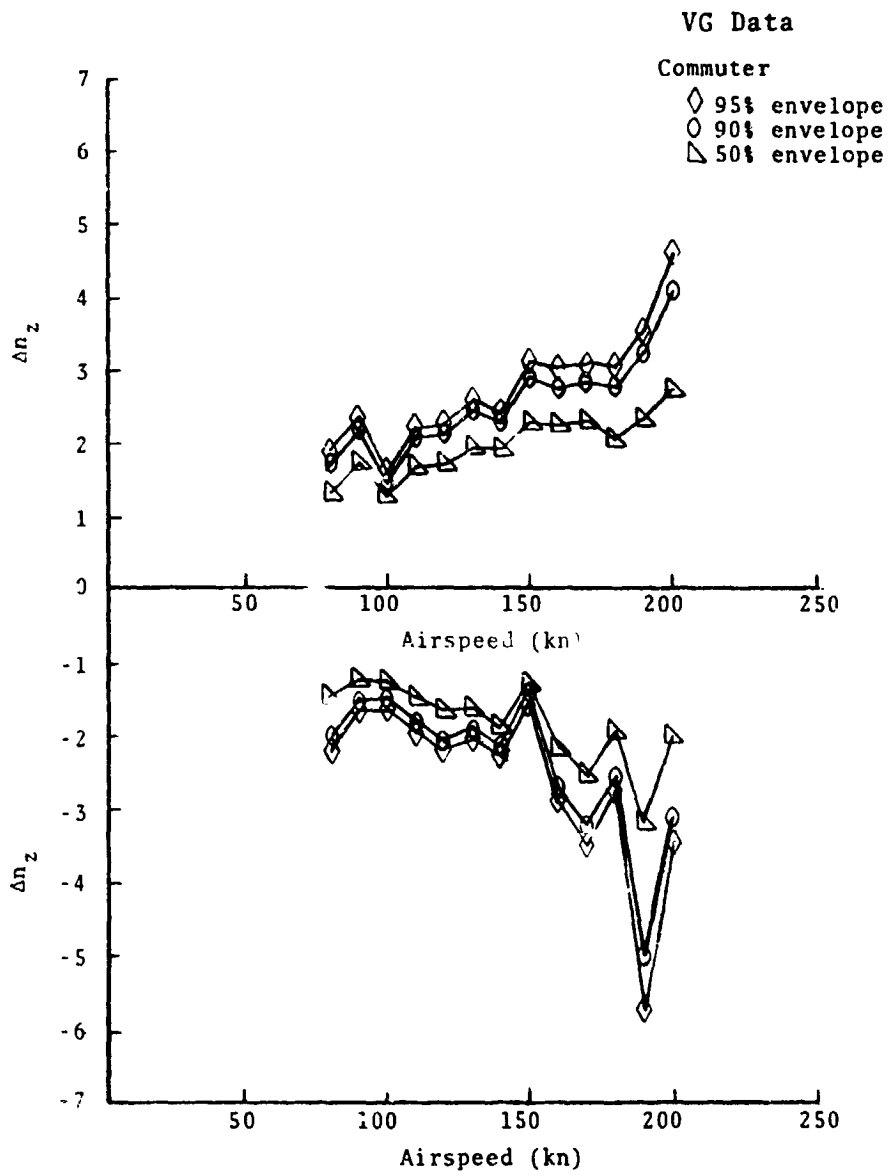


Figure 13. V-N Probability Distribution for Commuter Category Based on 20,000 Flight Hours of VG Data

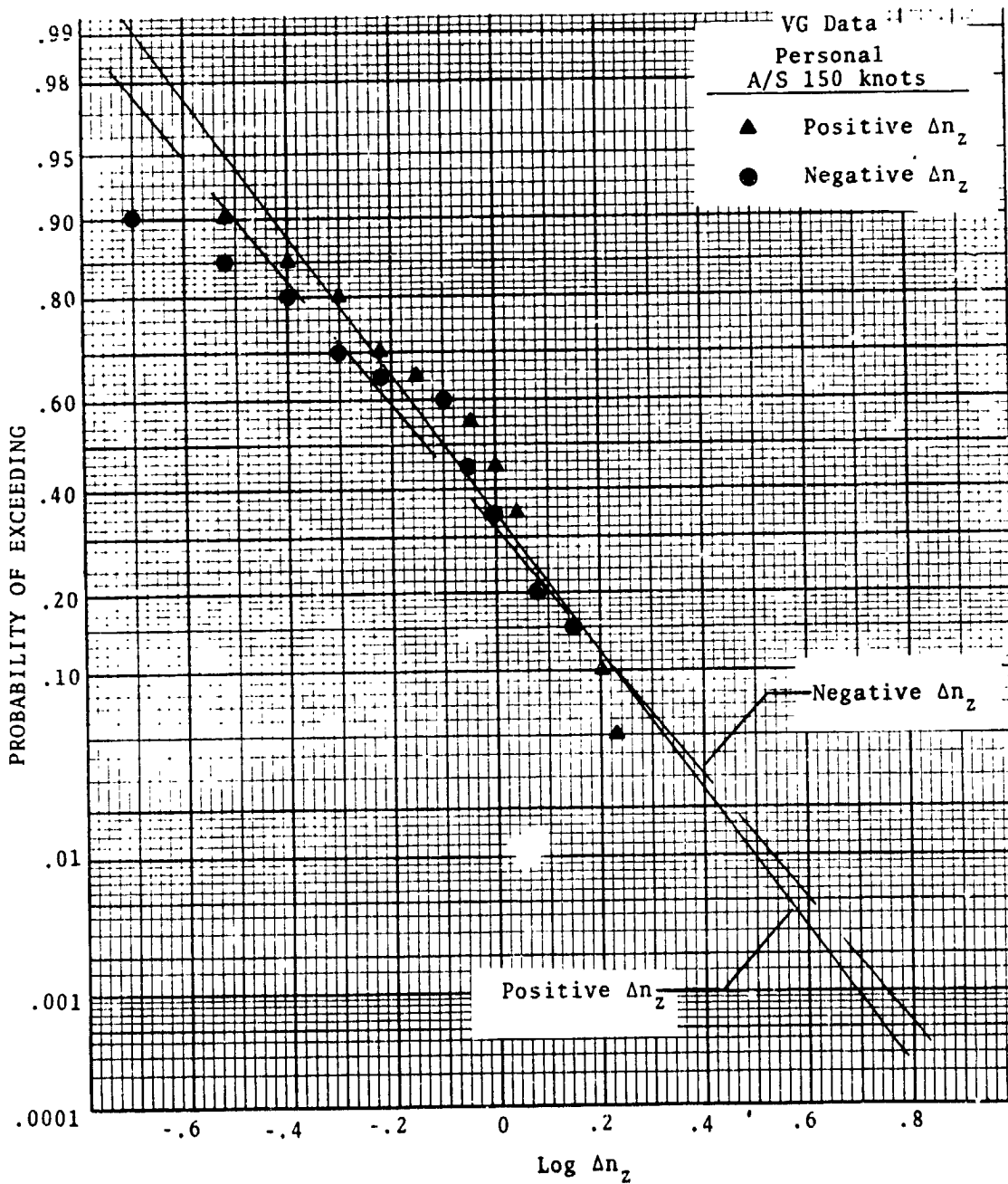


Figure 14. Probability-of-Exceeding- $\Delta n_z$  Curve at 150-Knot Airspeed for VG Data



















The data in the constant probability envelopes conform quite well with the operational usage data for all seven categories having sufficient  $\Delta n_z$  occurrences for each airspeed. In the 90% and 95% envelopes, the  $\Delta n_z$  values were usually considerably higher than the corresponding values in the operational data. This was expected since the  $\Delta n_z$  occurrences can be considered random events that would have a statistical distribution only within some range of  $\Delta n_z$ . The limits on this range are determined somewhat by the structural limitations of the aircraft and the effectiveness of the control system, but mostly by pilot actions. While the  $\Delta n_z$  occurrences may conform to a standard distribution within this range, the standard distribution will show a finite probability for a  $\Delta n_z$  occurrence beyond the limits of this range. Because of its larger data sample, the VG data was used to construct the constant probability envelopes. If VGH data had been used, the gust loads could have been separated from the maneuver loads. The gust loads could be treated as true random occurrences since they are an exponential function of altitude and are randomly generated by an external energy source. Maneuver loads would have to be treated as a conditional distribution which would be truncated at the limits of the  $\Delta n_z$  range.

## 2.4 Design Limit Probability Levels

### 2.4.1 Gust and Maneuver Design Limit Loads

The probability levels for current gust and maneuver design limit loads and ultimate (1.5 x design) limit loads were calculated from the VGH data presented in Table IV. The probability levels were based on 10,000 and 20,000 flight hours and were calculated for all operational categories except Aerobatic. Each probability level represents the probability of exceeding a particular limit load at least once in either 10,000 or 20,000 flight hours. Again it was necessary to first construct the probability-of-exceeding- $\Delta n_z$  curves for both gust and maneuver loads for each operational category. These curves show the probability of exceeding a given  $\Delta n_z$  in a single flight. Each flight was considered to be a statistical trial, and these trials were assumed to satisfy the requirements for Bernoulli trials. The number of trials (flights) in 10,000 and 20,000 hours was calculated for each operational category. The probability P(E) of exceeding a particular limit load at least once in either 10,000 or 20,000 flight hours was calculated as follows:

$$P_{NE} = 1 - P_E$$

$$P(NE) = P_{NE}^n$$

$$P(E) = 1 - P(NE)$$

where  $P_E$  = probability of exceeding a given  $\Delta n_z$  in a single trial (as read from probability-of-exceeding- $\Delta n_z$  curves)

$P_{NE}$  = probability of not exceeding a given  $\Delta n_z$  in a single trial

$P(NE)$  = probability of not exceeding a given  $\Delta n_z$  in  $n$  consecutive trials

$n$  = number of trials in either 10,000 or 20,000 flight hours

Tables V through VIII present the results of the above calculations. As indicated in these tables, the operational categories have the following trends: Instructional has the highest probability of exceeding the design and ultimate  $n_z$  limits during maneuver; Aerial Application has a high probability of exceeding the design  $n_z$  limits but a low probability of exceeding the ultimate  $n_z$  limits during maneuver; Commercial Survey has the highest probability of exceeding the design and ultimate  $n_z$  limits due to gust; and Aerial Application has almost a zero probability of exceeding the design  $n_z$  limits due to gusts.

#### 2.4.2 Maneuver Load-Gross Weight Relationships

Relationships between recorded maneuver loads and design gross weights were determined over the range of aircraft gross weights in the normal aircraft category. The three  $\Delta n_z$  values at each gross weight represent 50%, 90%, and 95% probability levels and are based on 20,000 flight hours. An aircraft flying 20,000 hours at a given gross weight has a 50%, 90%, or 95% probability of never exceeding the corresponding  $\Delta n_z$  value. The technique for computing these  $\Delta n_z$  values is the same as that discussed in Section 2.3, V-N Probability Distributions. Since the actual weight conditions corresponding to the recorded  $n_z$  values were not available, Figure 15 is a plot of  $\Delta n_z$  versus design gross weight for each of the three probability levels. Also shown in Figure 15 is a curve of the minimum design load factor as stated in FAR Part 23, Section 23.337 for the normal aircraft category. Table IX presents the design gross weights, number of recorded flight hours, number of recorded flights, and  $\Delta n_z$  values for each probability level.

TABLE IV. EXTREME VGH VALUES PER FLIGHT BY OPERATIONAL CATEGORY

VGH hr: 3377

POSITIVE MANUEVER  
OPERATION 991 -- TWIN ENGINE EXECUTIVE

A/C TYPE	$\Delta N_2$																	TOTAL		
	.4	.5	.6	.7	.8	.9	1.0	1.1	1.2	1.3	1.4	1.5	1.6	1.7	1.8	1.9	2.0		2.2	
4	53	17	11	6	3	1	1	2					1							95
7	290	139	66	39	23	15	3	5	4	1	1		2	1		2		1	592	
3	20	7	4	2	3	1		1	1				1	1			1		42	
5A	132	60	46	24	16	7	7	10	3	2	1		2						310	
1	36	26	9	13	7	6	2	3	2	4	1	1							110	
TOTAL	531	249	136	84	52	30	13	21	10	7	3	2	5	2		2	2	1	1149	

NEGATIVE MANUEVER  
OPERATION 991 -- TWIN ENGINE EXECUTIVE

A/C TYPE	$\Delta N_2$																	TOTAL
	.4	.5	.6	.7	.8	.9	1.0	1.1	1.2	1.3	1.4	1.5	1.6	1.7	1.8	1.9		
4	24	4	2															31
7	228	63	32	7	8													338
3	5	2	1															8
5A	73	28	10	4	3	1												119
1	32	6	2	1	1													42
TOTAL	362	103	47	12	13	1												538

VGH hr: 1366

POSITIVE MANUEVER  
OPERATION 992 -- SINGLE ENGINE EXECUTIVE

A/C TYPE	$\Delta N_2$																	TOTAL
	.4	.5	.6	.7	.8	.9	1.0	1.1	1.2	1.3	1.4	1.5	1.6	1.7	1.8	1.9		
7A	12	2	1	2														17
9A	54	28	14	14	7	7	1	2	2	3	5							137
8	86	41	26	19	3	11	3	5	1	1	2	1		2				201
TOTAL	152	71	41	35	10	18	4	7	3	4	7	1		2				355

NEGATIVE MANUEVER  
OPERATION 992 -- SINGLE ENGINE EXECUTIVE

A/C TYPE	$\Delta N_2$																	TOTAL	
	.4	.5	.6	.7	.8	.9	1.0	1.1	1.2	1.3	1.4	1.5	1.6	1.7	1.8	1.9	2.2		3.2
7A	4																		4
9A	48	13	14	17	11	8	5												116
8	42	15	9	1	1	1	1												70
TOTAL	94	28	23	18	12	9	6												190

TABLE IV. - Continued

VGH hr: 724

POSITIVE MANUEVER  
OPERATION 993 -- PERSONAL

A/C TYPE	$\Delta N7$																	TOTAL
	.4	.5	.6	.7	.8	.9	1.0	1.1	1.2	1.3	1.4	1.5	1.6	1.7	1.8	1.9	2.0	
12B	38	17	15	11	5	4	5	3		2	1		1				1	103
10A	21	8	4	5	4		1	1										44
11	26	7	4	2		3												43
TOTAL	85	32	23	18	5	7	6	4		2	1		1				1	190

NEGATIVE MANUEVER  
OPERATION 993 -- PERSONAL

A/C TYPE	$\Delta N2$																	TOTAL
	.4	.5	.6	.7	.8	.9	1.0	1.1	1.2	1.3	1.4	1.5	1.6	1.7	1.8	1.9		
12B	18	7	9	1	2	1		1		1							40	
10A	7	4	2	3	4												20	
11	7	1			1	1											10	
TOTAL	32	12	11	4	7	2		1		1							70	

VGH hr: 2843

POSITIVE MANUEVER  
OPERATION 994 -- INSTRUCTIONAL

A/C TYPE	$\Delta N2$																				TOTAL			
	.4	.5	.6	.7	.8	.9	1.0	1.1	1.2	1.3	1.4	1.5	1.6	1.7	1.8	1.9	2.0	2.1	2.3	2.4		3.1	3.2	
14	56	44	30	29	18	10	15	13	4	4	1	1	3	1		1	1	1						232
16	115	77	50	54	45	32	21	14	17	14	6	11	9	2	2	4	1	1						475
17	84	36	33	26	13	14	8	2	2	4	1		1					1	1					226
15	52	38	24	34	19	14	20	6	5	1		3	1	1		1		1	1	1	2	1	224	
13	183	121	80	58	46	43	35	23	20	17	10	9	5		3	2		1					657	
TOTAL	490	316	217	201	141	113	99	58	48	40	24	24	18	4	5	8	2	5	1	1	2	1	1809	

NEGATIVE MANUEVER  
OPERATION 994 -- INSTRUCTIONAL

A/C TYPE	$\Delta N2$																				TOTAL	
	.4	.5	.6	.7	.8	.9	1.0	1.1	1.2	1.3	1.4	1.5	1.6	1.7	1.8	1.9	2.0	2.1				
14	51	29	9	8		3																100
16	92	40	30	9	6	4	3					1										185
17	78	30	25	9	4	2	1															149
15	38	35	11	5	4	3	3															99
13	158	118	76	23	7	2	1		1													386
TOTAL	417	252	151	54	21	14	8		1		1											919

TABLE IV. - Continued

VGH hr: 2291

POSITIVE MANUFVER  
OPERATION 995 -- COMMERCIAL SURVEY

A/C TYPE	$\Delta N^2$															
	.4	.5	.6	.7	.8	.9	1.0	1.1	1.2	1.3	1.4	1.5	1.6	1.7	1.8	1.9
19	5	6	5	3		2	1		2		4		3	3	1	1
16A	17	14	9	18	22	33	46	77	77	57	24	13	10	8	9	1
9B	42	19	18	14	11	8	6	5	1	4					1	1
49	14	16	22	16	22	20	14	19	25	21	9	7	3	3		
TOTAL	78	55	54	51	55	63	67	101	105	82	37	20	16	14	11	3

POSITIVE MANUFVER  
OPERATION 995 -- COMMERCIAL SURVEY (CONTINUED)

A/C TYPE	$\Delta N^2$														TOTAL
	2.0	2.1	2.2	2.3	2.4	2.6	2.7	2.8	2.9	3.1	3.3	3.4	3.5	3.6	
19	6		3	2	2	5	2	3	3	2	1	2	1	1	69
16A		1													436
9B															130
49	1														212
TOTAL	7	1	3	2	2	5	2	3	3	2	1	2	1	1	847

NEGATIVE MANUFVER  
OPERATION 995 -- COMMERCIAL SURVEY

A/C TYPE	$\Delta N^2$															TOTAL	
	.4	.5	.6	.7	.8	.9	1.0	1.1	1.2	1.3	1.4	1.5	1.6	1.7	1.8		1.9
19	20	12	9	3		1	1										46
16A	26	10	1			1	2	1									41
9B	21	13	4		2					1							41
49	53	31	9	4	4	1											102
TOTAL	120	66	23	7	6	3	3	1		1							230

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TABLE IV. - Continued

VGH hr: 484

POSITIVE MANUEVER  
OPERATION 996 -- AERIAL APPLICATION

A/C TYPE	$\Delta N_7$																				TOTAL		
	.4	.5	.6	.7	.8	.9	1.0	1.1	1.2	1.3	1.4	1.5	1.6	1.7	1.8	1.9	2.0	2.1	2.2	2.3		2.4	2.5
24	71	127	126	119	86	67	49	39	14	12	2	3	3	2									720
23	16	15	13	6	18	18	47	75	101	164	167	190	178	144	111	65	41	20	10	6	3	1	1409
TOTAL	87	142	139	125	104	85	96	114	115	176	169	193	181	146	111	65	41	20	10	6	3	1	2129

NEGATIVE MANUEVER  
OPERATION 996 -- AERIAL APPLICATION

A/C TYPE	$\Delta N_7$																	TOTAL
	.4	.5	.6	.7	.8	.9	1.0	1.1	1.2	1.3	1.4	1.5	1.6	1.7	1.8	1.9		
24	174	98	45	14	6												337	
23	63	55	107	167	315	317	195	98	21	1	1	1	1	1	1	1	1341	
TOTAL	237	153	152	181	321	317	195	98	21	1	1	1	1	1	1	1	1678	

VGH hr: 1510

POSITIVE MANUEVER  
OPERATION 997 -- COMMUTER

A/C TYPE	$\Delta N_7$																	TOTAL
	.4	.5	.6	.7	.8	.9	1.0	1.1	1.2	1.3	1.4	1.5	1.6	1.7	1.8	1.9		
28	20	7	3	2	4												37	
26	102	21	11	9	2	4	1	1	1	1	3					156		
TOTAL	122	28	14	11	6	4	1	1	2	1	3					193		

NEGATIVE MANUEVER  
OPERATION 997 -- COMMUTER

A/C TYPE	$\Delta N_7$																TOTAL
	.4	.5	.6	.7	.8	.9	1.0	1.1	1.2	1.3	1.4	1.5	1.6	1.7	1.8		
28	7	1	2													10	
26	56	13	4	6	2	1									82		
TOTAL	63	14	6	6	2	1									92		



TABLE IV. - Continued

VGH hr: 3377

POSITIVE GUST  
OPERATION 991 -- TWIN ENGINE EXECUTIVE

A/C TYPE	$\Delta NZ$																	TOTAL	
	.4	.5	.6	.7	.8	.9	1.0	1.1	1.2	1.3	1.4	1.5	1.6	1.7	1.8	1.9	2.1		
4	60	34	23	9	14	4	4	1	2	1								1	153
2	178	98	36	24	13	4	1						1	1					356
3	83	41	16	4	4	2	2		2									154	
5A	234	165	82	43	21	10	3		2	1	1	2	1					565	
1	57	16	8	4	2		1											84	
TOTAL	612	354	165	84	54	20	11	1	6	2	1	2	2	1			1	1316	

NEGATIVE GUST  
OPERATION 991 -- TWIN ENGINE EXECUTIVE

A/C TYPE	$\Delta NZ$																	TOTAL
	.4	.5	.6	.7	.8	.9	1.0	1.1	1.2	1.3	1.4	1.5	1.6	1.7	1.8	1.9		
4	50	34	21	12	6	2	7		4				1					137
2	163	97	44	21	2	6	1											334
3	82	42	15	7	8	2			1									157
5A	243	155	63	41	17	8	5	4		1	1							538
1	54	16	7	2	1	1												81
TOTAL	592	344	150	83	34	19	13	4	5	1	1		1				1247	

VGH hr: 1366

POSITIVE GUST  
OPERATION 992 -- SINGLE ENGINE EXECUTIVE

A/C TYPE	$\Delta NZ$																	TOTAL
	.4	.5	.6	.7	.8	.9	1.0	1.1	1.2	1.3	1.4	1.5	1.6	1.7	1.8	1.9		
7A	39	53	34	24	13	7	3	2	1									176
9A	118	93	81	69	38	18	3	5	3	1	2	1					432	
8	78	73	81	72	57	34	24	13	8	5	3	1			1		450	
TOTAL	235	219	196	165	108	59	30	20	12	6	5	2			1		1058	

NEGATIVE GUST  
OPERATION 992 -- SINGLE ENGINE EXECUTIVE

A/C TYPE	$\Delta NZ$																			TOTAL
	.4	.5	.6	.7	.8	.9	1.0	1.1	1.2	1.3	1.4	1.5	1.6	1.7	1.8	1.9	2.2	2.4		
7A	45	43	31	27	12	3	4								1				166	
9A	116	105	80	42	37	12	7	4	2	2	3		1						411	
8	118	95	57	51	41	40	17	10	3	4							1	1	448	
TOTAL	279	243	178	120	90	55	28	14	5	6	3		1		1		1	1	1025	

TABLE IV. - Continued

VGH hr: 724

POSITIVE GUST  
OPERATION 993 -- PERSONAL

A/C TYPE	.4	.5	.6	.7	.8	.9	1.0	1.1	1.2	1.3	1.4	1.5	1.6	1.7	1.8	1.9	TOTAL
12B	92	52	21	10	1	2	1										179
10A	49	40	18	5	4			1			1						118
11	49	40	15	16	9	5											134
TOTAL	190	132	54	31	14	7	1	1			1						431

NEGATIVE GUST  
OPERATION 993 -- PERSONAL

A/C TYPE	.4	.5	.6	.7	.8	.9	1.0	1.1	1.2	1.3	1.4	1.5	1.6	1.7	1.8	1.9	TOTAL
12B	86	42	23	12	5	1				1							170
10A	42	33	17	6	1	1	1			1							102
11	62	25	18	7	4		1	1	1								119
TOTAL	190	100	58	25	10	2	2	1	1	2							391

VGH hr: 2843

POSITIVE GUST  
OPERATION 994 -- INSTRUCTIONAL

A/C TYPE	.4	.5	.6	.7	.8	.9	1.0	1.1	1.2	1.3	1.4	1.5	1.6	1.7	1.8	1.9	2.1	3.3	TOTAL	
14	184	88	26	13	2		1												314	
16A	150	145	82	38	20	10	1	2		2		1						1	1	453
17	77	58	18	9	2															164
15	113	67	35	14	6	2		1		1										239
13	584	252	58	23	8	7	2		1		1	1								937
TOTAL	1108	610	219	97	38	19	4	3	1	3	1	2						1	1	2107

NEGATIVE GUST  
OPERATION 994 -- INSTRUCTIONAL

A/C TYPE	.4	.5	.6	.7	.8	.9	1.0	1.1	1.2	1.3	1.4	1.5	1.6	1.7	1.8	1.9	TOTAL	
14	166	89	21	5	1	2	1										285	
16A	164	121	73	38	15	5	3	4		1	2						1	428
17	95	44	19	9		1		1										169
15	122	73	27	5	7	5									1			240
13	529	180	48	23	7	2				1								790
TOTAL	1076	507	188	80	30	15	4	5		2	2				1		1	1911

TABLE IV. - Concluded

VGH hr: 2291

POSITIVE GUST  
OPERATION 995 -- COMMERCIAL SURVEY

A/C TYPE	$\Delta N_Z$																	TOTAL
	.4	.5	.6	.7	.8	.9	1.0	1.1	1.2	1.3	1.4	1.5	1.6	1.7	1.8	1.9	2.2	
19	8	9	14	13	7	6	5	1		2	2							67
16A	13	49	84	120	86	90	31	16	3	5	2				1		1	501
9B	15	54	67	55	28	27	12	5	2	4	2		3	1				275
49	9	3	5															17
TOTAL	45	115	170	188	121	123	48	22	5	11	6		3	1	1		1	860

NEGATIVE GUST  
OPERATION 995 -- COMMERCIAL SURVEY

A/C TYPE	$\Delta N_Z$																	TOTAL
	.4	.5	.6	.7	.8	.9	1.0	1.1	1.2	1.3	1.4	1.5	1.6	1.7	1.8	1.9	2.1	
19	9	14	11	7	15	5	2	2	1	2	1			1				70
16A	15	47	49	66	100	71	54	33	23	22	7	5	3	1			1	497
9B	9	30	57	64	44	26	27	9	5	2	1		1					276
49	11		1	2														14
TOTAL	44	91	118	139	159	102	83	44	29	26	9	5	4	2			1	857

VGH hr: 484

POSITIVE GUST  
OPERATION 996 -- AERIAL APPLICATION

A/C TYPE	$\Delta N_Z$																	TOTAL
	.4	.5	.6	.7	.8	.9	1.0	1.1	1.2	1.3	1.4	1.5	1.6	1.7	1.8	1.9		
24	34	18	4	1														57
23	16	5	2															23
TOTAL	50	23	6	1														80

NEGATIVE GUST  
OPERATION 996 -- AERIAL APPLICATION

A/C TYPE	$\Delta N_Z$																	TOTAL
	.4	.5	.6	.7	.8	.9	1.0	1.1	1.2	1.3	1.4	1.5	1.6	1.7	1.8	1.9		
24	43	13	4	1														61
23	4	7					1											17
TOTAL	47	20	4	1			1											78

VGH hr: 1510

POSITIVE GUST  
OPERATION 997 -- COMMUTER

A/C TYPE	$\Delta N_Z$																	TOTAL
	.4	.5	.6	.7	.8	.9	1.0	1.1	1.2	1.3	1.4	1.5	1.6	1.7	1.8	1.9		
28	164	126	68	40	28	9	10	2	1	2								450
26	320	120	67	45	6	6		2	1		1		1					569
TOTAL	484	246	135	85	34	15	10	4	2	2	1		1					1019

NEGATIVE GUST  
OPERATION 997 -- COMMUTER

A/C TYPE	$\Delta N_Z$																	TOTAL
	.4	.5	.6	.7	.8	.9	1.0	1.1	1.2	1.3	1.4	1.5	1.6	1.7	1.8	1.9		
28	149	105	72	50	25	20	8	2	5	1	2		1					440
26	344	110	59	21	15	8	2	1	1									571
TOTAL	493	215	141	71	40	28	10	3	6	1	2		1					1011

TABLE V. PROBABILITY OF EXCEEDING MANEUVER DESIGN LOADS IN 10,000 FLIGHT HOURS OF EXTRAPOLATED VGH DATA

Operational Category	Aircraft Category	Design Limit		Design Ultimate	
		$n_z$	Probability	$n_z$	Probability
Twin-engine Executive	normal	+3.8	.487	+5.7	.017
		-1.52	.000	-2.28	.000
Single-engine Executive	normal	+3.8	.717	+5.7	.031
		-1.52	.515	-2.28	.047
Personal	normal	+3.8	.321	+5.7	.007
		-1.52	.046	-2.28	.004
Instructional	utility	+4.4	.877	+6.6	.052
		-1.76	.514	-2.64	.084
Commercial Survey	utility	+4.4	.000	+6.6	.000
		-1.76	.013	-2.64	.004
Aerial Application	normal	+3.8	.850	+5.7	.000
		-1.52	.000	-2.28	.000
Commuter	normal	+3.8	.372	+5.7	.020
		-1.52	.003	-2.28	.000

TABLE VI. PROBABILITY OF EXCEEDING MANEUVER DESIGN LOADS IN 20,000 FLIGHT HOURS OF EXTRAPOLATED VGH DATA

Operational Category	Aircraft Category	Design Limit		Design Ultimate	
		$n_z$	Probability	$n_z$	Probability
Twin-engine Executive	normal	+3.8	.737	+5.7	.033
		-1.52	.001	-2.28	.000
Single-engine Executive	normal	+3.8	.920	+5.7	.061
		-1.52	.531	-2.28	.092
Personal	normal	+3.8	.538	+5.7	.014
		-1.52	.089	-2.28	.007
Instructional	utility	+4.4	.985	+6.6	.101
		-1.76	.764	-2.64	.161
Commercial Survey	utility	+4.4	.000	+6.6	.000
		-1.76	.026	-2.64	.007
Aerial Application	normal	+3.8	.978	+5.7	.000
		-1.52	.000	-2.28	.000
Commuter	normal	+3.8	.606	+5.7	.040
		-1.52	.005	-2.28	.000

TABLE VII. PROBABILITY OF EXCEEDING GUST DESIGN LOADS IN 10,000 FLIGHT HOURS OF EXTRAPOLATED VGH DATA

Operational Category	Aircraft Category	Design Limit		Design Ultimate	
		$\Delta n_z$	Probability	$\Delta n_z$	Probability
Twin-engine Executive	normal	+2.4	.106	+3.6	.002
		-2.4	.065	-3.6	.001
Single-engine Executive	normal	+2.4	.271	+3.6	.001
		-2.4	.188	-3.6	.000
Personal	normal	+2.4	.002	+3.6	.000
		-2.4	.004	-3.6	.000
Instructional	utility	+2.5	.007	+3.75	.000
		-2.5	.009	-3.75	.000
Commercial Survey	utility	+2.5	.516	+3.75	.005
		-2.5	.729	-3.75	.014
Aerial Application	normal	+2.4	.000	+3.6	.000
		-2.4	.000	-3.6	.000
Commuter	normal	+2.4	.209	+3.6	.006
		-2.4	.390	-3.6	.009

TABLE VIII. PROBABILITY OF EXCEEDING GUST DESIGN LOADS IN 20,000 FLIGHT HOURS OF EXTRAPOLATED VGH DATA

Operational Category	Aircraft Category	Design Limit		Design Ultimate	
		$\Delta n_z$	Probability	$\Delta n_z$	Probability
Twin-engine Executive	normal	+2.4	.201	+3.6	.005
		-2.4	.126	-3.6	.001
Single-engine Executive	normal	+2.4	.468	+3.6	.001
		-2.4	.343	-3.6	.001
Personal	normal	+2.4	.005	+3.6	.000
		-2.4	.007	-3.6	.000
Instructional	utility	+2.5	.015	+3.75	.000
		-2.5	.018	-3.75	.000
Commercial Survey	utility	+2.5	.765	+3.75	.010
		-2.5	.926	-3.75	.029
Aerial Application	normal	+2.4	.000	+3.6	.000
		-2.4	.001	-3.6	.000
Commuter	normal	+2.4	.374	+3.6	.012
		-2.4	.628	-3.6	.017

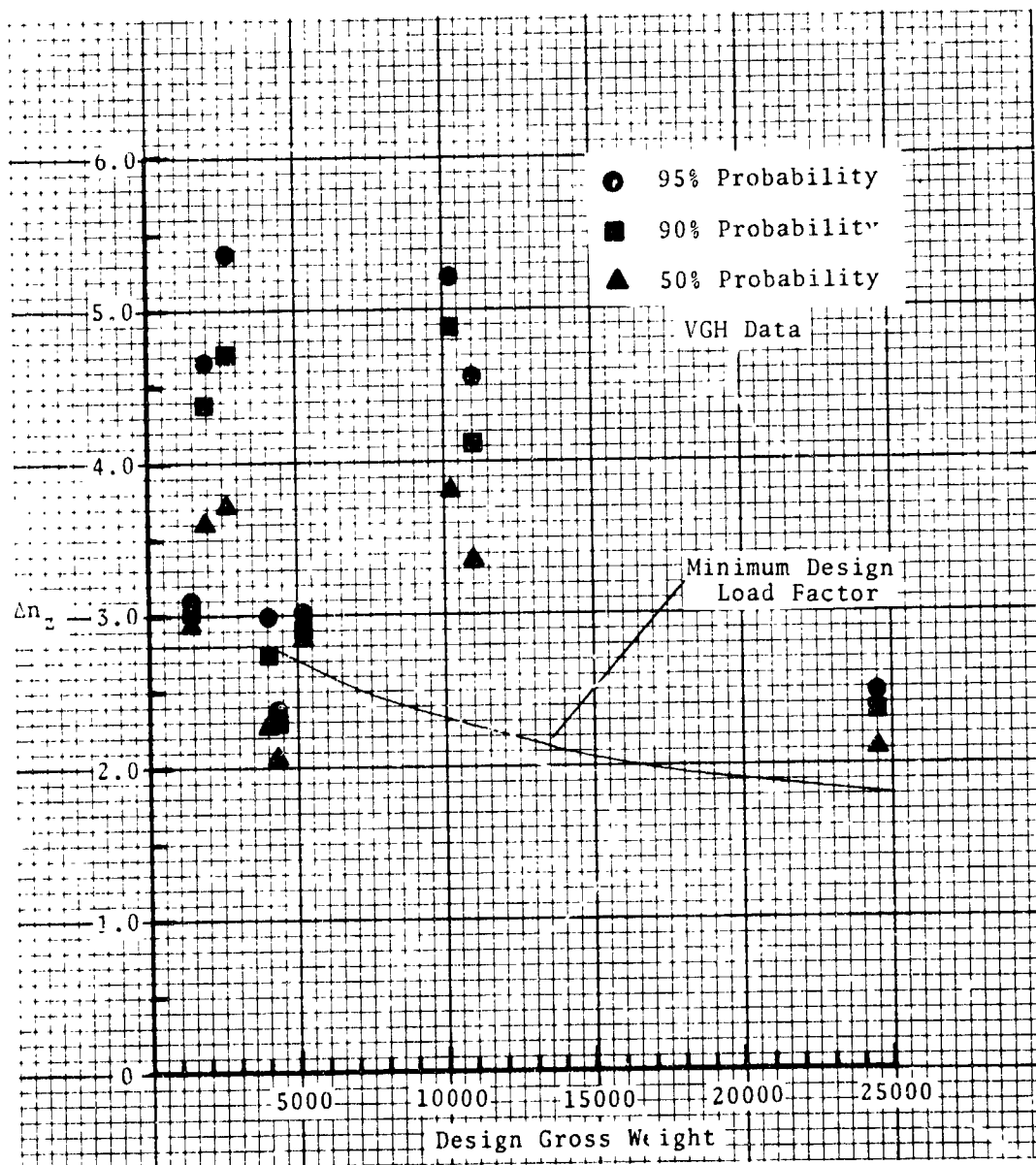


Figure 15. Maneuver  $\Delta n_z$  Versus Design Gross Weight for Three Probability Levels in VGH Data

TABLE IX. MANEUVER LOAD-DESIGN GROSS WEIGHT RELATIONSHIPS  
DURING 20,000 HOURS OF EXTRAPOLATED VGH DATA

Design Gross Weight (lb)	VGH Data		Probability of Never Exceeding $\Delta n_z$		
	Hours	Flights	95%	90%	50%
1,450	1007.1	3117	3.10	3.05	2.94
1,950	310.6	522	4.66	4.38	3.61
2,700	569.1	562	5.37	4.71	3.73
4,000	549.8	582	2.99	2.74	2.27
4,500	1152.8	1578	2.38	2.29	2.07
5,200	309.0	1417	3.03	2.99	2.86
10,250	914.7	3277	5.24	4.89	3.82
11,000	695.0	830	4.56	4.12	3.36
24,500	824.1	731	2.47	2.35	2.12

## 2.5 Review of Categories

As previously noted, the eight operational categories do not correspond to the FAA aircraft categories, normal, utility, and acrobatic. Although the eight operational categories more closely identify the operational load experiences of the various aircraft, the following analysis indicates the need for their further refinement.

Figures 16-a, 16-b, and 16-c show that both the magnitude and the frequency of the  $U_{de}$ 's for the Twin-Engine Executive category are greater in the 1829 to 6096 meters (6,000 to 20,000 ft) altitude range than in the 6,096 to 15,240 meters (20,000 to 50,000 ft) altitude range. Since aircraft flying in these two altitude ranges experience different gust and maneuver loads, the Twin-Engine Executive category should be separated into two categories, one for the higher flying turbojets and the other for the turboprop and piston aircraft.

The examination of the VG data by aircraft type shows that when aircraft in the Single-Engine Executive and Personal categories fly at common airspeeds, their  $\Delta n_z$ 's vary little. Although the single-engine executive aircraft can operate at higher airspeeds, the data analysis would not be affected by combining the two categories. Figure 10 shows that the constant probability envelopes for the Personal category are considerably higher than the FAR minimum maneuver load limits for aircraft in the normal aircraft category.

The examination of the VGH data for the Commercial Survey category shows that three of the four aircraft types in this category had very different maneuver load experiences. This suggests further breakdown of the Commercial Survey category by mission type.

## 2.6 Fatigue Spectra

From the distribution of repeated acceleration peaks recorded in the VGH data, fatigue spectra were derived for three types of load conditions: gust, maneuver, and landing impact. The gust accelerations were converted to derived gust velocity,  $U_{de}$ . The gust and maneuver  $n_z$  peak distributions are presented in Tables X and XI. The landing impact accelerations were normalized by dividing the load factor  $n_z$  by 2.67, the minimum design inertia load factor.

### 2.6.1 Derived Gust Velocity ( $U_{de}$ )

#### 2.6.1.1 $U_{de}$ Computations

A derived gust velocity  $U_{de}$  was computed for each gust acceleration peak in the VGH data by using the following equation:

$$n_z = 1 + \frac{K_g U_{de} V_e a}{498(W/S)}$$

where  $K_g$  = subsonic gust alleviation factor =  $\frac{0.88 \mu g}{5.3 + \mu g}$

$\mu g$  = airplane mass ratio =  $\frac{2(W/S)}{\rho \bar{c} ag}$

$U_{de}$  = derived gust velocity (fps)

$\rho$  = atmospheric density (slugs/ft<sup>3</sup>)

$W/S$  = wing loading (psf)

$\bar{c}$  = mean aerodynamic chord (ft)

$g$  = gravitational constant (ft/sec<sup>2</sup>)

$V_e$  = equivalent airspeed (knots)

$a$  = slope of normal force coefficient (1/rad)



TABLE X. MANEUVER LOADS IN VGH DATA BY OPERATIONAL CATEGORY

VGH hr: 3377

OPERATIONAL CATEGORY	n <sub>2</sub>																
	POSITIVE ACCELERATION																
	2.0	2.1	2.2	2.3	2.4	2.5	2.6	2.7	2.8	2.9	3.0	3.1	3.2	3.3	3.4	3.5	3.6
LF55	1																
80			1														
90			1														
100	1		1														
110	2		1														
120	7		2														
130	AD	18	1	1													
140	RR	16	1	1													
150	AD	17	1	1													
160	AD	17	1	1													
170	AD	12	1	1													
180	AD	16	1	1													
190	AD	21	1	1													
200	AD	24	1	1													
210	AD	15	1	1													
220	AD	26	1	1													
230	AD	24	1	1													
240	1	1	1	1													
250	1	1	1	1													
260	1	1	1	1													
270	1	1	1	1													
280	1	1	1	1													
290	1	1	1	1													
300	1	1	1	1													
310	1	1	1	1													
320	1	1	1	1													
330	1	1	1	1													
340	1	1	1	1													
350	1	1	1	1													
360	1	1	1	1													
370	1	1	1	1													
380	1	1	1	1													
390	1	1	1	1													
400	1	1	1	1													
TOTAL	198	185	181	89	122	166	88	50	29	24	13	9	5	2	6	2	2

OPERATIONAL CATEGORY	n <sub>2</sub>																
	POSITIVE ACCELERATION																
	3.0	3.1	3.2	3.3	3.4	3.5	TOTAL										
LF55							1										
80							7										
90							19										
100							45										
110							77										
120							104										
130							134										
140							205										
150							286										
160							287										
170							249										
180							217										
190							196										
200							187										
210							189										
220							185										
230							203										
240							205										
250							265										
260							316										
270							273										
280							211										
290							157										
300							132										
310							117										
320							122										
330							97										
340							97										
350							64										
360							53										
370							42										
380							16										
390							14										
400							8										
TOTAL							6788										

TABLE X. - Continued

OPERATION: TWIN ENGINE EXECUTIVE												TOTAL	
VFL (KIAS)	$\Delta n_z$											TOTAL	
	-0.2	-0.3	-0.4	-0.5	-0.6	-0.7	-0.8	-0.9	-1.0	-1.1	-1.2		-1.3
LESS													
50			4	4	3			1					7
60			4	4	7								15
70			21	6	3	1							29
80			7	6	2								17
90	1		1	3	3								23
100	3		24	2	3		1						33
110	3		37	10	2	2		1					51
120	7	1	17	7	1	2	2						37
130	9	2	14	7	1	1							34
140	37	4	16	5	3		3						64
150	16	8	24	2	3		1						74
160	52	3	21	3			3						84
170	50	7	32	2									91
180	46	7	19	3		1							72
190	34	8	22		1	2							71
200	41	9	30		5	1							86
210	23	8	33	2	4	2							72
220	39	5	33	8	3								88
230	41	11	36	4	1								93
240	56	11	39	23	6								137
250	65	9	30	18	3	2	1						137
260	90	7	47	11	7		1						123
270	44	13	36	8	2	1	2						106
280	26	8	30	12	1	1							77
290	15	8	34	4	1		1						65
300	20	4	29	1	2								56
310	15	13	20	4	5								57
320	7	5	13	5		1							44
330	11	4	6	2									23
340	3		7	2									12
350	3	1	5	1									10
360	2		4										6
370			1										1
ABOVE	1												1
TOTAL	757	157	774	165	64	17	18	1					1903

VGH hr: 1366

OPERATION: SINGLE ENGINE EXECUTIVE												TOTAL		
VFL (KIAS)	$\Delta n_z$											TOTAL		
	-0.2	-0.3	-0.4	-0.5	-0.6	-0.7	-0.8	-0.9	-1.0	-1.1	-1.2		-1.3	
LESS														
50													2	
60			1	1									31	
70	5	2	12	10	2								78	
80	28	10	28	8	2	2							176	
90	28	33	32	14	5	9							132	
100	17	9	45	23	13	10	3	5	3				170	
110	10	6	65	31	10	7	4	6	2	1	1	2	210	
120	49	45	97	58	23	13	4	10	1	3	1	5	410	
130	30	11	69	36	27	10	2	3	3	3			195	
140	4		48	20	13	7	6	2	1	2	2		102	
150		5	34	10	4	6	2	2					64	
160		1	9	4	2	7	1	1					22	
170				1									2	
180														
190														
200														
210														
220														
230														
240														
250														
260														
270														
280														
290														
300														
310														
320														
330														
340														
350														
360														
370														
ABOVE														
TOTAL	341	127	430	216	102	65	26	32	11	11	6	7	7	1384

TABLE X. - Continued

OPERATION	NEGATIVE ACCELERATION													
	-2.0	-2.1	-2.2	-2.3	-2.4	-2.5	-2.6	-2.7	-2.8	-2.9	-3.0	-3.1	-3.2	-3.3
100														
110														
120														
130														
140														
150														
160														
170														
180														
190														
200														
210														
220														
230														
240														
250														
260														
270														
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290														
300														
310														
320														
330														
340														
350														
360														
370														
380														
390														
400														
410														
420														
430														
440														
450														
460														
470														
480														
490														
500														
TOTAL														

OPERATION	NEGATIVE ACCELERATION													
	-2.0	-2.1	-2.2	-2.3	-2.4	-2.5	-2.6	-2.7	-2.8	-2.9	-3.0	-3.1	-3.2	-3.3
100														
110														
120														
130														
140														
150														
160														
170														
180														
190														
200														
210														
220														
230														
240														
250														
260														
270														
280														
290														
300														
310														
320														
330														
340														
350														
360														
370														
380														
390														
400														
410														
420														
430														
440														
450														
460														
470														
480														
490														
500														
TOTAL														

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TABLE X. - Continued

VGH hr: 2291

VEL. (KIAS)	OPERATION: COMMERCIAL SURVEY																	
	POSITIVE ACCELERATION																	
	2.0	2.1	2.2	2.3	2.4	2.5	2.6	2.7	2.8	2.9	3.0	3.1	3.2	3.3	3.4	3.5	3.6	
45																		
50																		
60																		
70																		
80																		
90																		
100																		
110																		
120																		
130																		
140																		
150																		
160																		
170																		
180																		
190																		
200																		
210																		
220																		
230																		
240																		
250																		
260																		
270																		
280																		
290																		
300																		
310																		
320																		
330																		
340																		
350																		
360																		
370																		
ABOVE																		
TOTAL	1661	1247	4754	2765	4528	4266	3703	2930	2007	1101	589	221	120	87	51	43	45	25

VEL. (KIAS)	OPERATION: COMMERCIAL SURVEY																	
	POSITIVE ACCELERATION																	
	2.0	2.1	2.2	2.3	2.4	2.5	2.6	2.7	2.8	2.9	3.0	3.1	3.2	3.3	3.4	3.5	3.6	
45																		
50																		
60																		
70																		
80																		
90																		
100																		
110																		
120																		
130																		
140																		
150																		
160																		
170																		
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190																		
200																		
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220																		
230																		
240																		
250																		
260																		
270																		
280																		
290																		
300																		
310																		
320																		
330																		
340																		
350																		
360																		
370																		
ABOVE																		
TOTAL	72	8	12	4	6	11	8	3	7	5		2		2	2	1	1	34316

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TABLE X. - Continued

OPERATION: AERIAL APPLICATION		$\Delta n_2$														TOTAL		
VFL (KIAS)	LESS	2.0	2.1	2.2	2.3	2.4	2.5	2.6	2.7	2.8	2.9	3.0	3.1	3.2	3.3		3.4	3.5
50																		33
60																		1377
70																		13778
80	1	2																24034
90	27	11	5	3	1													16409
100	18	11	6	4	1													1014
110			1		1													20
120																		
130																		
140																		
150	3																	1275
160																		1
170																		
180																		
190																		
200																		
210																		
220																		
230																		
240																		
250																		
260																		
270																		
280																		
290																		
300																		
310																		
320																		
330																		
340																		
350																		
360																		
370																		
380																		
390																		
400																		
TOTAL	49	24	15	7	3													57921

OPERATION: AERIAL APPLICATION		$\Delta n_2$																	TOTAL	
VFL (KIAS)	LESS	-2	-3	-4	-5	-6	-7	-8	-9	-10	-11	-12	-13	-14	-15	-16	-17	-18		-19
50																				1
60																				28
70																				280
80	1	4	1221	857	791	740	628	295	82	19	2								4641	
90		6	1968	1410	1298	1128	1093	679	334	97	10								8024	
100		3	512	400	304	243	231	173	128	65	19								2079	
110			20	19	12	9	8	9	6	1									92	
120																			1	
130																			1	
140																				
150																				
160																				
170																				
180																				
190																				
200																				
210																				
220																				
230																				
240																				
250																				
260																				
270																				
280																				
290																				
300																				
310																				
320																				
330																				
340																				
350																				
360																				
370																				
380																				
390																				
400																				
TOTAL	1	13	330	2821	2502	2208	2034	1198	558	182	31								15531	

TABLE X. - Concluded

VGH hr: 1510

OPERATION: COMPUTER	g <sub>n</sub>																TOTAL
	POSITIVE ACCELERATION																
VFL (KIAS) LFSS	.2	.3	.4	.5	.6	.7	.8	.9	1.0	1.1	1.2	1.3	1.4	1.5	1.6	1.7	
50																	1
60			1														1
70			5			1											7
80			9	1	1												11
90		2	17	6	1												27
100			32	3	2	2		1									40
110			14	4	2	2		1		1							24
120			15	4	3	2		1	1	1							31
130			35	8	3	4		1	1				2		1		54
140			32	12	5	4	2		2		1	1			1		60
150			24	1	3		1	2									31
160			10	1	1	1	1										14
170			7	5	1									1			14
180			2	1	1		5					1					10
190			4	4													9
200			1		1												2
210			1														1
220																	
230						1											1
240																	
250																	
260																	
270																	
280																	
290																	
300																	
310																	
320																	
330																	
340																	
350																	
360																	
370																	
APPROX TOTAL	2	213	50	25	18	9	5	2	4	1	2	2	1	3			337

OPERATION: COMPUTER	g <sub>n</sub>																TOTAL
	NEGATIVE ACCELERATION																
VFL (KIAS) LFSS	-.2	-.3	-.4	-.5	-.6	-.7	-.8	-.9	-1.0	-1.1	-1.2	-1.3	-1.4	-1.5	-1.6	-1.7	
50				1													1
60				1	1												2
70			1	1	1												3
80			7	2													9
90			24	2	3												29
100			22	4		1	1										30
110			7		1	1											12
120			4	2		2											9
130			7	3	2			1									13
140			8	2	1		2										13
150			2	3		1											6
160																	
170			1														1
180																	
190																	
200																	
210			1														1
220																	
230																	
240																	
250																	
260																	
270																	
280																	
290																	
300																	
310																	
320																	
330																	
340																	
350																	
360																	
370																	
APPROX TOTAL			21	3	9	3	1										37











TABLE XI. - Continued

VGH hr: 2291

OPERATION	COMMERCIAL SILEX															
	22	23	24	25	26	27	28	29	30	31	32	33	34	35	36	37
100																
110																
120																
130																
140																
150																
160																
170																
180																
190																
200																
210																
220																
230																
240																
250																
260																
270																
280																
290																
300																
310																
320																
330																
340																
350																
360																
370																
380																
390																
400																
TOTAL	350	400	22197	45 28	14953	4953	1177	342	91	89	11	14	6		3	1

OPERATION	COMMERCIAL SILEX															
	22	23	24	25	26	27	28	29	30	31	32	33	34	35	36	37
100																
110																
120																
130																
140																
150																
160																
170																
180																
190																
200																
210																
220																
230																
240																
250																
260																
270																
280																
290																
300																
310																
320																
330																
340																
350																
360																
370																
380																
390																
400																
TOTAL																



TABLE XI. - Continued

DEPTH	OPERATION COMMERCIAL SURVEY										NEGATIVE ACCELERATION									TOTAL
	-2.2	-2.3	-2.4	-2.5	-2.6	-2.7	-2.8	-2.9	-3.0	-3.1	-3.2	-3.3	-3.4	-3.5	-3.6	-3.7	-3.8	-3.9		
50			22	13	6	1	1	1												
60			45	39	17	9	1	1												
70	1	14	3520	2112	869	358	144	37	26	4	2	3	2							
80		171	4878	1794	7511	3428	1274	527	225	70	19	16	4	3	2					
90		71	23337	17556	9684	4253	1734	619	247	99	41	17	8	2	2	1				
100		5	5028	2263	984	406	185	75	31	6	6	1								
110		1	1502	877	313	147	58	20	11	6	1		2		1					
120	2		143	61	33	3	5	1		2										
130		1	225	92	25	6	3					1								
140	9	6	153	65	23	7	9	3		1										
150	71	13	55	22	10	6	2	2												
160	112	40	20	9	1	2	1													
170	76	18	12	7	1	3	1													
180	23	8	2	3																
190	26	10	2																	
200	14	7	4	2																
210	2	5		2																
220	3	1	1																	
230	1										2							2		
240		1																		
250																				
260																				
270																				
280																				
290																				
300																				
310																				
320																				
330																				
340																				
350																				
360																				
370																				
ABOVE																				
TOTAL	347	295	4026	2115	1954	654	3428	1294	548	186	75	39	16	5	5	2	2			

DEPTH	OPERATION COMMERCIAL SURVEY										NEGATIVE ACCELERATION						TOTAL	
	-2.0	-2.1	-2.2	-2.3	-2.4	-2.5	-2.6	-2.7	-2.8	-2.9	-3.0	-3.1	-3.2	-3.3	-3.4	-3.5		
50																		
60																		
70																		
80																		
90																		
100																		
110																		
120																		
130																		
140																		
150																		
160																		
170																		
180																		
190																		
200																		
210																		
220																		
230																		
240																		
250																		
260																		
270																		
280																		
290																		
300																		
310																		
320																		
330																		
340																		
350																		
360																		
370																		
ABOVE																		
TOTAL																		

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TABLE XI. - Continued

VGH hr: 484

12

OPERATIONS: AERIAL APPLICATION

VELOCITY (KIAS) LESS	POSITIVE ACCELERATION							TOTAL
	+2	+3	+4	+5	+6	+7	+8	
60								6
70			1					7
80			12		1			111
90			15		2			30
100			4		2			6
110			2					1
120								
130								
140								
150								
160								
170								
180								
190								
200								
210								
220								
230								
240								
250								
260								
270								
280								
290								
300								
310								
320								
330								
340								
350								
360								
370								
380								
390								
400								
TOTAL			23	17	7	1	1	29

12

OPERATIONS: AERIAL APPLICATION

VELOCITY (KIAS) LESS	NEGATIVE ACCELERATION							TOTAL
	-2	-3	-4	-5	-6	-7	-8	
60			1					6
70			4		10	1	1	62
80		1	7		13	2		95
90			11		4	1		16
100			2					1
110								
120								
130								
140								
150								
160								
170								
180								
190								
200								
210								
220								
230								
240								
250								
260								
270								
280								
290								
300								
310								
320								
330								
340								
350								
360								
370								
380								
390								
400								
TOTAL		1	16	17	4	1	1	172

### TABLE XI. - Concluded

VGH hr: 1510

OPERATION: COMPUTER       $g_{n_z}$

VEL. (KIAS) LESS	POSITIVE ACCELERATION														TOTAL				
	.2	.3	.4	.5	.6	.7	.8	.9	1.0	1.1	1.2	1.3	1.4	1.5		1.6	1.7		
50			1															1	
60			2		1													3	
70			5															2	
80			7		2													9	
90			14		2		1											17	
100			11		2			1										14	
110			30		12		3		3									49	
120			114		39		12		4			2					1	174	
130			247		58		22		11			1						363	
140		3	549		101		44		26			1						734	
150		2	348		96		43		18			2		1				534	
160		2	171		57		17		12			3		2				262	
170			220		86		36		15			4		3			1	369	
180			432		167		65		19		16	5		3			1	700	
190			591		223		67		16		6	2		1			1	900	
200			143		77		34		11		9	4		5			1	295	
210			37		19		7		3			2		1			1	68	
220																			
230																			
240																			3
250																			
260																			
270																			
280																			
290																			
300																			
310																			
320																			
330																			
340																			
350																			
360																			
370																			
ABOVE TOTAL	8	2769	962	336	139	51	25	15	6	3	3	2		1				4497	

OPERATION: COMPUTER       $g_{n_z}$

VEL. (KIAS) LESS	NEGATIVE ACCELERATION														TOTAL				
	-.2	-.3	-.4	-.5	-.6	-.7	-.8	-.9	-1.0	-1.1	-1.2	-1.3	-1.4	-1.5		-1.6	-1.7		
50																			2
60					2														1
70					1														8
80				4	1	2	1												8
90				21	6	3													30
100				41	13	4	3	2	2										65
110				55	14	8	2												80
120		3		247	49	30	7	1	1										336
130		2		532	112	49	14	10	4	2	1	1							727
140		2		377	109	35	11	5	3										542
150				155	61	18	8	1	1		1								244
160				221	91	34	12	8	5	1	2								374
170				348	182	67	29	12	9	3	1	2							649
180				556	244	105	36	15	5	5	1	2						1	969
190				132	80	31	20	4	7	1		2						2	277
200				22	6	2													31
210				5												1			2
220																			2
230																			2
240																			
250																			
260																			
270																			
280																			
290																			
300																			
310																			
320																			
330																			
340																			
350																			
360																			
370																			
ABOVE TOTAL	8	2769	973	393	143	58	36	13	6	6	1	2		1				4338	

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The values of  $V_e$  and  $\sigma$  were computed from the mid-values of the 10-knot indicated airspeed interval and the 2000-foot pressure altitude interval containing the recorded data at the gust acceleration peak. The aircraft weight was assumed to be constant for each instrumented aircraft and was set equal to a normal operating weight estimated by the operator.

In the analysis of derived gust data computed from recorded c.g. vertical accelerations, it is important to note that (1) the relation between  $\Delta z$  and  $U_{de}$  is inversely proportional to  $V_e$  so that the effects of inaccuracies in  $\Delta z$  measurements are magnified in  $U_{de}$  values at very low airspeeds, and (2) since the  $\Delta z$  measurements were not taken inside the digitizing thresholds ( $\pm 0.4g$  for most aircraft), the corresponding  $U_{de}$  values omitted were as large as 14 to 17 feet per second for the various operations so that the validity of the presented  $U_{de}$  spectrum is limited to the range outside approximately  $\pm 16$  feet per second. Table XII presents the calculated  $U_{de}$  peaks with a breakdown by operational category and airspeed range.

#### 2.6.1.2 $U_{de}$ Spectra

The cumulative frequencies of positive and negative  $U_{de}$  peaks per nautical mile are presented in Figure 16 for the seven operational categories represented by the VGH data. The low altitude spectra for 0 to 1829 meters (0 to 6000 ft) in Figure 16-a were most severe for the Commercial Survey category and least severe for the Aerial Application category. The middle altitude spectrum for 1829 to 6096 meters (6,000 to 20,000 ft) in Figure 16-b were relatively closely grouped with the Commercial Survey category having the most severe spectrum. As shown in Figure 16-c, only the Twin-Engine Executive category had a gust spectrum above 6096 meters (20,000 ft).

As described above, it is likely that the  $U_{de}$  spectra below 16 ft/sec (5 m/sec) are biased by the acceleration digitizing threshold at the lower airspeeds. For this reason, the  $U_{de}$  curves in the region of bias are shown as dashed lines.

#### 2.6.2 Gust Accelerations

The cumulative frequencies of positive and negative gust load factors per nautical mile are presented in Figure 17. The largest gust acceleration of 3.3 was recorded by an aircraft in the Instructional category and the highest frequency of gust acceleration peaks was recorded by an aircraft in the Commercial Survey category.

#### 2.6.3 Maneuver Normal Load Factors

The cumulative frequencies of positive and negative maneuver normal load factors per hour, per flight, and nautical mile are presented in Figures 18-a, 18-b, and 18-c, respectively.

TABLE XII. U<sub>d</sub>e PEAKS IN VGH DATA BY OPERATIONAL CATEGORY

VGH hr: 3377

a. Operation 991 - Twin Engine Executive

Positive U<sub>d</sub>e Peaks

TABLES BY OPERATION 991  
DERIVED GUST (POSITIVE) VS VELOCITY

VFL	DERIVED GUST														TOTAL	
	0	4	8	12	16	20	24	28	32	36	40	44	48	52		ABOVE
LFSS																
50																
60																
70																
80																
90																
100																
110																
120																
130																
140																
150																
160																
170																
180																
190																
200																
210																
220																
230																
240																
250																
260																
270																
280																
290																
300																
310																
320																
330																
340																
350																
360																
370																
ABOVE																
TOTAL	1810	7282	2748	614	130	27	14	3	3	3				1	12635	

Negative U<sub>d</sub>e Peaks

TABLES BY OPERATION 991  
DERIVED GUST (NEGATIVE) VS VELOCITY

VFL	DERIVED GUST														TOTAL	+-TOTAL
	0	-4	-8	-12	-16	-20	-24	-28	-32	-36	-40	-44	-48	-52		
LFSS																
50																
60																
70																
80																
90																
100																
110																
120																
130																
140																
150																
160																
170																
180																
190																
200																
210																
220																
230																
240																
250																
260																
270																
280																
290																
300																
310																
320																
330																
340																
350																
360																
370																
ABOVE																
TOTAL	1497	6259	2339	540	119	23	11	2	1					2	10793	23428

TABLE XII. - Continued

VGH hr: 1366

b. Operation 992 - Single Engine Executive

Positive U<sub>d</sub>e Peaks

TABLES BY OPERATION		992														
DERIVED GUST (POSITIVE) VS VELOCITY		DERIVED GUST														
VEL.	0	4	8	12	16	20	24	28	32	36	40	44	48	52	ABOVE	TOTAL
LFSS								2								8
50				1	3	1	2									7
60			1	7	1											9
70		5	9	36	10	2										62
80		43	171	69	10	5										248
90		83	482	110	7	3			1							666
100		148	678	79	8	1										914
110		1700	1579	199	21	1		1								3002
120	30	4233	2313	249	77	2	1	1								5856
130	11	2069	1848	161	29	1	2		1							4122
140	2	2192	1861	228	27	1										4315
150		1975	1647	224	37	5										3891
160		634	372	49	9											1064
170		17	10	4												31
180																
190																
200																
210																
220																
230		1														1
240																
250																
260																
270																
280																
290																
300																
310																
320																
330																
340																
350																
360																
370																
ABOVE																
TOTAL	43	11600	10921	1416	191	32	7	4	2							24216

Negative U<sub>d</sub>e Peaks

TABLES BY OPERATION		992															
DERIVED GUST (NEGATIVE) VS VELOCITY		DERIVED GUST															
VFL.	0	-4	-8	-12	-16	-20	-24	-28	-32	-36	-40	-44	-48	-52	ABOVE	TOTAL	+-TOTAL
LESS																1	9
50																	7
60				7	2												18
70		10	19	23	6	1									1	60	122
80		42	115	64	4	1										226	474
90		80	417	121	15	1										635	1321
100		240	913	128	15		1									1297	2211
110		1364	1737	170	19	4	1									3295	6297
120	25	1575	1119	103	10	3	1									2836	8692
130	13	1629	969	105	10	2		1								2729	6851
140		1631	1438	186	17	6					1					3279	7594
150		1587	1406	199	21	7			1							3216	7107
160		529	303	37	6											870	1934
170		27	11													38	69
180																	
190																	
200																	
210																	
220																	
230																	1
240																	
250																	
260																	
270																	
280																	
290																	
300																	
310																	
320																	
330																	
340																	
350																	
360																	
370																	
ABOVE																	
TOTAL	38	8714	8447	1138	126	20	3	2	1		1				1	18491	42707

TABLE XII. - Continued

VGH hr: 724  
 c. Operation 993 - Personal

Positive U<sub>d<sub>e</sub></sub> Peaks

TABLES BY OPERATION 993  
 DERIVED GUST (POSITIVE) VS VELOCITY

VEL.	DERIVED GUST														TOTAL	
	0	4	8	12	16	20	24	28	32	36	40	44	48	52		ABOVE
LESS																
50				2	4	6	1			1						14
60			12	11	6	1										11
70			70	50	3	2	1	2								33
80		4	295	81	5		1									125
90		135	523	90	4											386
100		97	374	13	2	1										752
110		93	190	23	1											487
120		291	268	20	2											307
130		243	97	10												581
140		34	8	1												350
150		5	1													43
160																6
170																
180																
190																
200																
210																
220																
230																
240																
250																
260																
270																
280																
290																
300																
310																
320																
330																
340																
350																
360																
370																
ABOVE																
TOTAL	902	1838	305	32	12	3	2		1							3095

Negative U<sub>d<sub>e</sub></sub> Peaks

TABLES BY OPERATION 993  
 DERIVED GUST (NEGATIVE) VS VELOCITY

VEL.	DERIVED GUST														TOTAL	+-TOTAL
	0	-4	-8	-12	-16	-20	-24	-28	-32	-36	-40	-44	-48	-52		
LESS																
50				3	7	5	2	-28	-32	-36	-40	-44	-48	-52		15
60			7	7	2											3
70			49	59	6											16
80		4	208	76	4											114
90		63	436	79	10	2										292
100		72	404	53	5											590
110		80	162	28	1											269
120		121	71	5	2	1										200
130		196	68	1												265
140		21	9													30
150		1														1
160																
170																
180																
190																
200																
210																
220																
230																
240																
250																
260																
270																
280																
290																
300																
310																
320																
330																
340																
350																
360																
370																
ABOVE																
TOTAL	558	1414	309	36	9	2		1								2329
																5424

TABLE XII. - Continued

VGH hr: 2843

d. Operation 994 - Instructional

Positive  $U_{de}$  Peaks

TABLES BY OPERATION 994  
DERIVED GUST (POSITIVE) VS VELOCITY

VFL.	DERIVED GUST														TOTAL	
	0	4	8	12	16	20	24	28	32	36	40	44	48	52		ABOVE
LESS																
50			46	81	35	9	9	1	1	1				1		86
60			778	274	37	11	2	1	1	1						183
70		6	2439	414	55	6	1									1103
80		967	2166	344	41	7	1	1								2921
90		417	617	112	15	3		2								3527
100		50	159	10			1									1166
110		21	9													220
120		2	2													30
130																4
140																
150																
160																
170																
180																
190																
200																
210																
220																
230																
240																
250																
260																
270																
280																
290																
300																
310																
320																
330																
340																
350																
360																
370																
ABOVE																
TOTAL	1463	6716	1253	226	45	19	8	6	1		2		1			9240

Negative  $U_{de}$  Peaks

TABLES BY OPERATION 994  
DERIVED GUST (NEGATIVE) VS VELOCITY

VFL.	DERIVED GUST														TOTAL	+-TOTAL
	0	-4	-8	-12	-16	-20	-24	-28	-32	-36	-40	-44	-48	-52		
LESS																
50			42	58	10	1	1									148
60			594	220	27	1	1									112
70		2	2150	377	38	5	2	1								843
80		694	2078	318	41	8	3	1		1						2575
90		332	721	107	19	4	1	1		1				1		3145
100		62	157	12	2									1		1189
110		6	18													233
120		2	1													26
130																3
140																
150		1														1
160																
170																
180																
190																
200																
210																
220																
230																
240																
250																
260																
270																
280																
290																
300																
310																
320																
330																
340																
350																
360																
370																
ABOVE																
TOTAL	1099	5761	1160	190	37	19	4	1	2					1	1	8275



TABLE XII. - Continued

VGH hr: 2291  
e. Operation 995 - Commercial Survey

Positive  $U_{de}$  Peaks

TABLES BY OPERATION 995  
DERIVED GUST (POSITIVE) VS VELOCITY

VFL	0	4	8	12	16	20	24	28	32	36	40	44	48	52	ABOVE	TOTAL
LF55				22	22	8	2	1								55
50			21	131	45	5	2	1								205
60			718	526	95	70	1									1360
70		1	6593	2202	340	62	8									9206
80	8749	49512	8344	461	18	5	1	1			1					67092
90	21715	30754	1423	86	15	2	2	1	2							54000
100	211	4813	282	45	10	2										5363
110	156	1375	226	59	8	3	3									2030
120	749	525	61	11	2											848
130	107	180	22	10	5	1										320
140	111	125	26	5	3	2										272
150	63	44	33	17	3	1	1									19
160	31	30	32	19	8	4	3	1								124
170	9	49	58	31	7	2	1	2	1		1					160
180	2	51	27	4	4	4	3	1								92
190		22	16	6	1											46
200		8	8	2												18
210		11	8	3												22
220		4	7	2												13
230		1	2													3
240																2
250																
260																
270																
280																
290																
300																
310																
320																
330																
340																
350																
360																
370																
ABOVE TOTAL	31599	94856	13458	1263	179	35	17	6	3	1						141417

Negative  $U_{de}$  Peaks

TABLES BY OPERATION 995  
DERIVED GUST (NEGATIVE) VS VELOCITY

VFL	0	-4	-8	-12	-16	-20	-24	-28	-32	-36	-40	-44	-48	52	ABOVE	TOTAL	+-TOTAL
LF55				14	14	12	1	1	1							43	98
50			6	78	32	9	1	1								127	332
60			429	354	82	12	2									879	2239
70	1	4	5044	1685	308	47	7	4								7100	16306
80	6478	39954	8084	1151	148	25	8	1								1 55850	122942
90	16868	33124	5956	627	84	9	3		4						6	56681	110681
100	1012	6935	912	109	26	1	1									8996	14359
110	852	2206	311	49	12	2	2			1						3435	5455
120	93	143	21	3												260	1108
130	153	188	11		1	1										354	674
140	144	101	22	6	2		1					5				281	553
150	53	40	59	15	7	6	1									181	363
160	22	40	78	30	13	9		2								194	322
170	4	46	32	16	8	1	2	1	1	1						112	272
180		16	8	4			3									32	125
190	2	21	9	6	2										1	39	85
200		13	2	5	3											23	41
210		3	5		2											9	31
220		3	1	3												7	20
230		1	2													7	10
240													2			1	3
250																	
260																	
270																	
280																	
290																	
300																	
310																	
320																	
330																	
340																	
350																	
360																	
370																	
ABOVE TOTAL	1	25685	88313	17644	2460	388	68	24	5	6	7	2			9	134612	276029

TABLE XII. - Continued

VGH hr: 484  
f. Operation 996 - Aerial Application

Positive  $U_{1e}$  Peaks

TABLES BY OPERATION 996  
DERIVED GUST (POSITIVE) VS VELOCITY

VEL.	0	4	8	12	16	20	24	DERIVED GUST					40	44	48	52	ABOVE	TOTAL
								28	32	36	40	44	48	52	ABOVE	TOTAL		
LESS																		
50																		6
60			3	2			1											67
70			47	14	5	1												111
80			99	11	1													30
90		4	14	12														9
100			4	4	1													1
110			1															
120																		
130																		
140																		
150																		
160																		
170																		
180																		
190																		
200																		
210																		
220																		
230																		
240																		
250																		
260																		
270																		
280																		
290																		
300																		
310																		
320																		
330																		
340																		
350																		
360																		
370																		
ABOVE		4	168	43	7	2												224
TOTAL																		

Negative  $U_{1e}$  Peaks

TABLES BY OPERATION 996  
DERIVED GUST (NEGATIVE) VS VELOCITY

VEL.	0	-4	-8	-12	-16	-20	-24	DERIVED GUST					-40	-44	-48	-52	ABOVE	TOTAL	**TOTL
								-28	-32	-36	-40	-44	-48	-52	ABOVE	TOTAL	**TOTL		
LESS																			
50																		6	12
60				2	3	1												59	126
70				42	6	9	1			1								95	206
80				83	11	1												16	46
90			1	9	5	1												3	12
100				1	2														1
110																			
120																			
130																			
140																			
150																			
160																			
170																			
180																			
190																			
200																			
210																			
220																			
230																			
240																			
250																			
260																			
270																			
280																			
290																			
300																			
310																			
320																			
330																			
340																			
350																			
360																			
370																			
ABOVE																			
TOTAL		1	137	27	12	1				1								179	403

TABLE XII. - Concluded

VGH hr: 1510  
g. Operation 997 - Commuter

Positive U<sub>d</sub>e Peaks

TABLES BY OPERATION 997  
DERIVED GUST (POSITIVE) VS VELOCITY

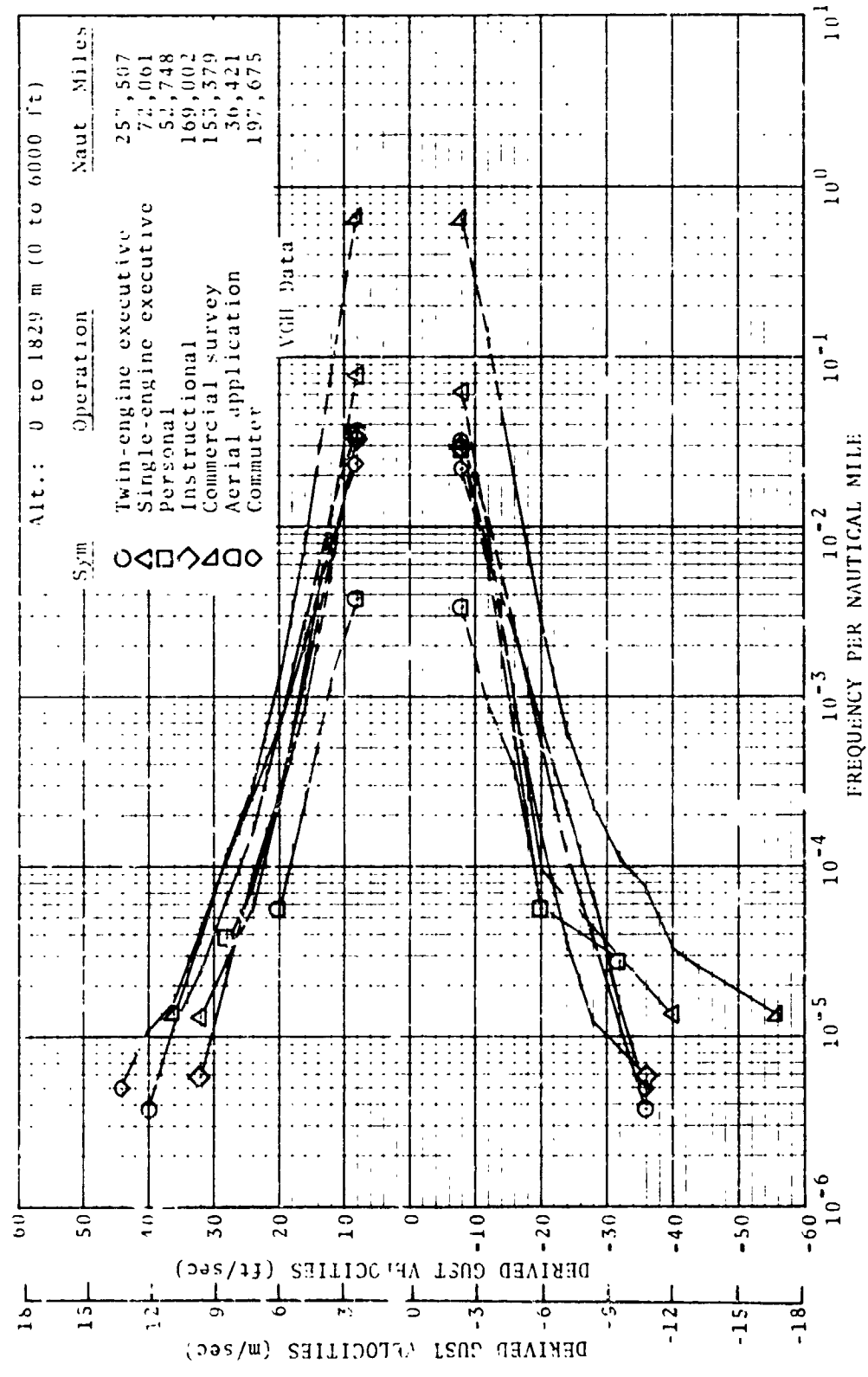
VEL.	DERIVED GUST														TOTAL	
	0	4	8	12	16	20	24	28	32	36	40	44	48	52		ABOVE
LFSS																
50									1							1
50							2	1								3
70							2									2
80					2	2	5									9
90				8	4	5	1	1								17
100				7	4	2	1									14
110				28	12	7	1					1				49
120			36	89	37	5	2	3	1				1			174
130			164	137	48	9	1	2	1	1						363
140			484	193	44	8	2	2	1							734
150			318	176	29	0	1	1								534
160			111	110	23	8	2									262
170			181	139	36	6	5	1	1							369
180			419	221	40	14	4	2								700
190			678	197	20	4	1									900
200			201	60	14	9	1	1								295
210			54	11	2	1										66
220																
230			3													3
240																
250																
260																
270																
280																
290																
300																
310																
320																
330																
340																
350																
360																
370																
ABOVE																
TOTAL			2649	1393	315	87	31	14	5	1	1	1				4497

Negative U<sub>d</sub>e Peaks

TABLES BY OPERATION 997  
DERIVED GUST (NEGATIVE) VS VELOCITY

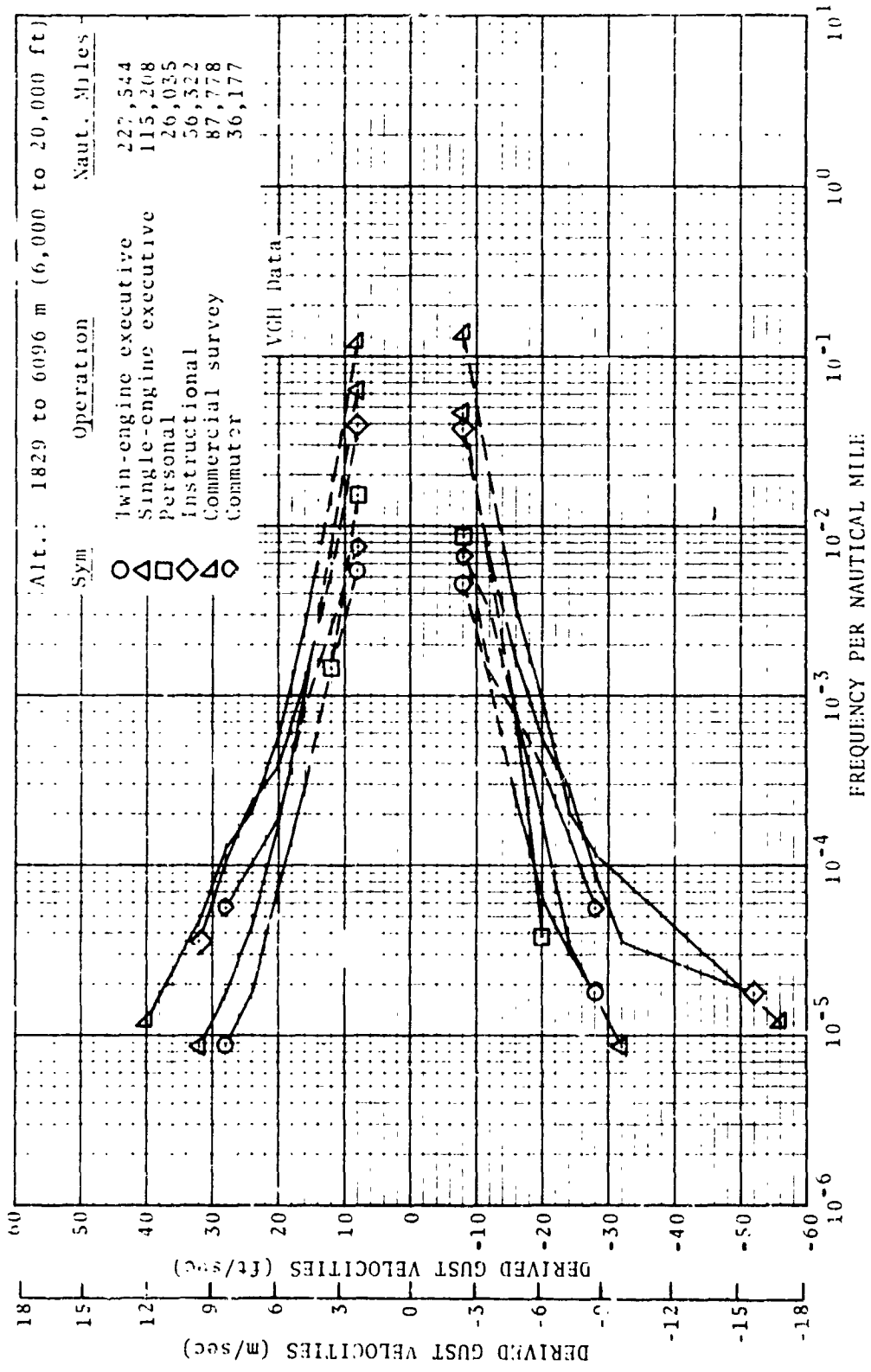
VEL.	DERIVED GUST														TOTAL	--TOTAL
	0	-4	-8	-12	-16	-20	-24	-28	-32	-36	-40	-44	-48	-52		
LFSS																
50																
60																
70									2							1
80							1									4
90					4	2	2									10
100				15	11	5										31
110				36	18	7	4									65
120			23	26	25	5	1									80
130			136	151	37	12										336
140			482	180	42	17	3	3								727
150			338	173	23	7	1									642
160			106	110	20	7		1								244
170			162	166	30	8	6	2								374
180			339	236	51	14	6	2								648
190			647	254	51	10	4		2	1						969
200			188	64	16	7	2									277
210			27	3			1									31
220			2													2
230			2													2
240																
250																
260																
270																
280																
290																
300																
310																
320																
330																
340																
350																
360																
370																
ABOVE																
TOTAL			2452	1413	328	102	30	8	4	1						4138

QUALITY OF THE ORIGINAL PAGE IS POOR



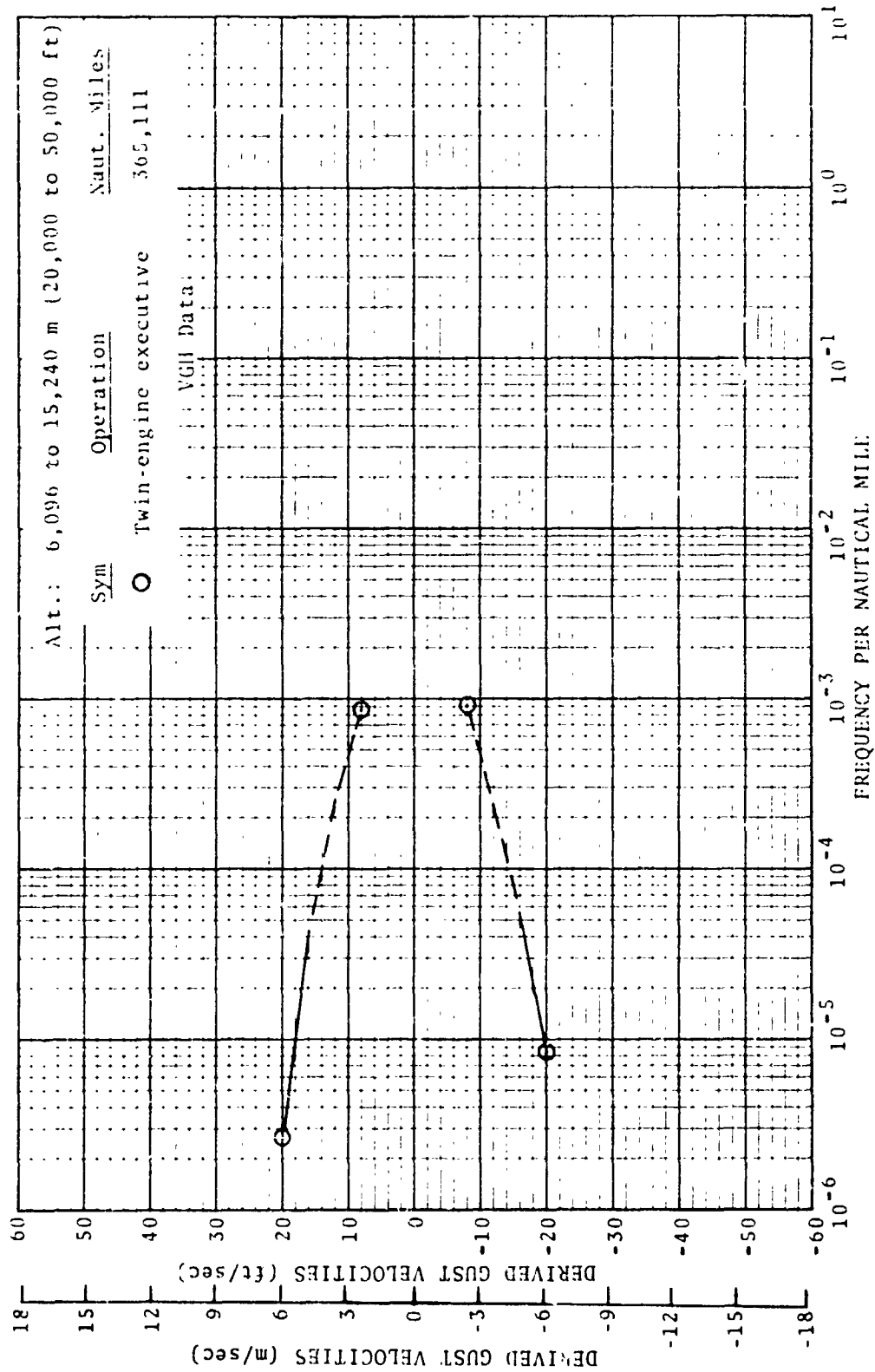
a. Altitude: 0 to 1829 m (0 to 6000 ft)

Figure 16. Use Cumulative Frequencies for Three Altitude Ranges in VGH Data



b. Altitude: 1829 to 6096 m (6,000 to 20,000 ft)

Figure 16. - Continued



c. Altitude: 6096 to 15,240 m (20,000 to 50,000 ft)

Figure 16. - Concluded

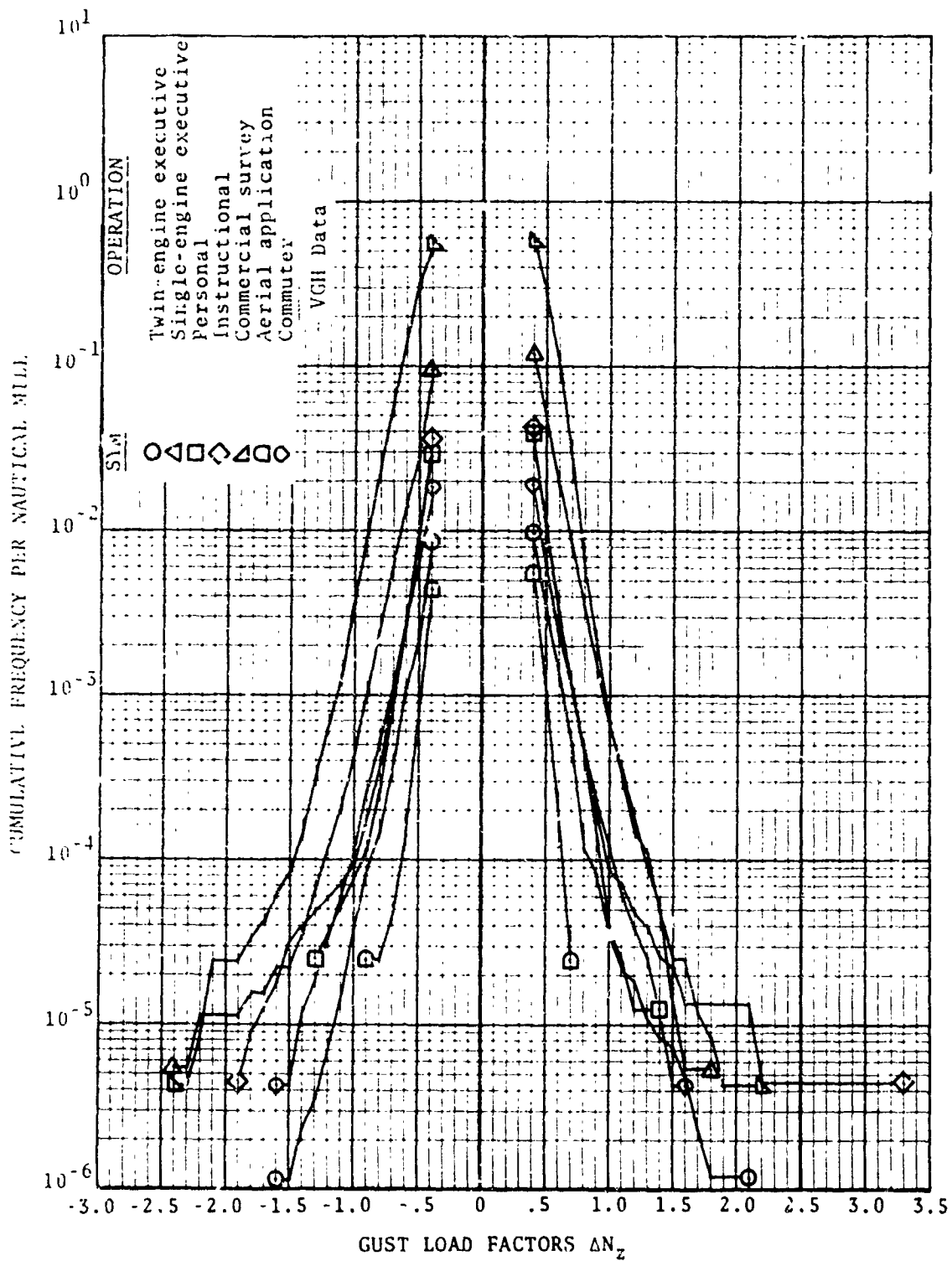
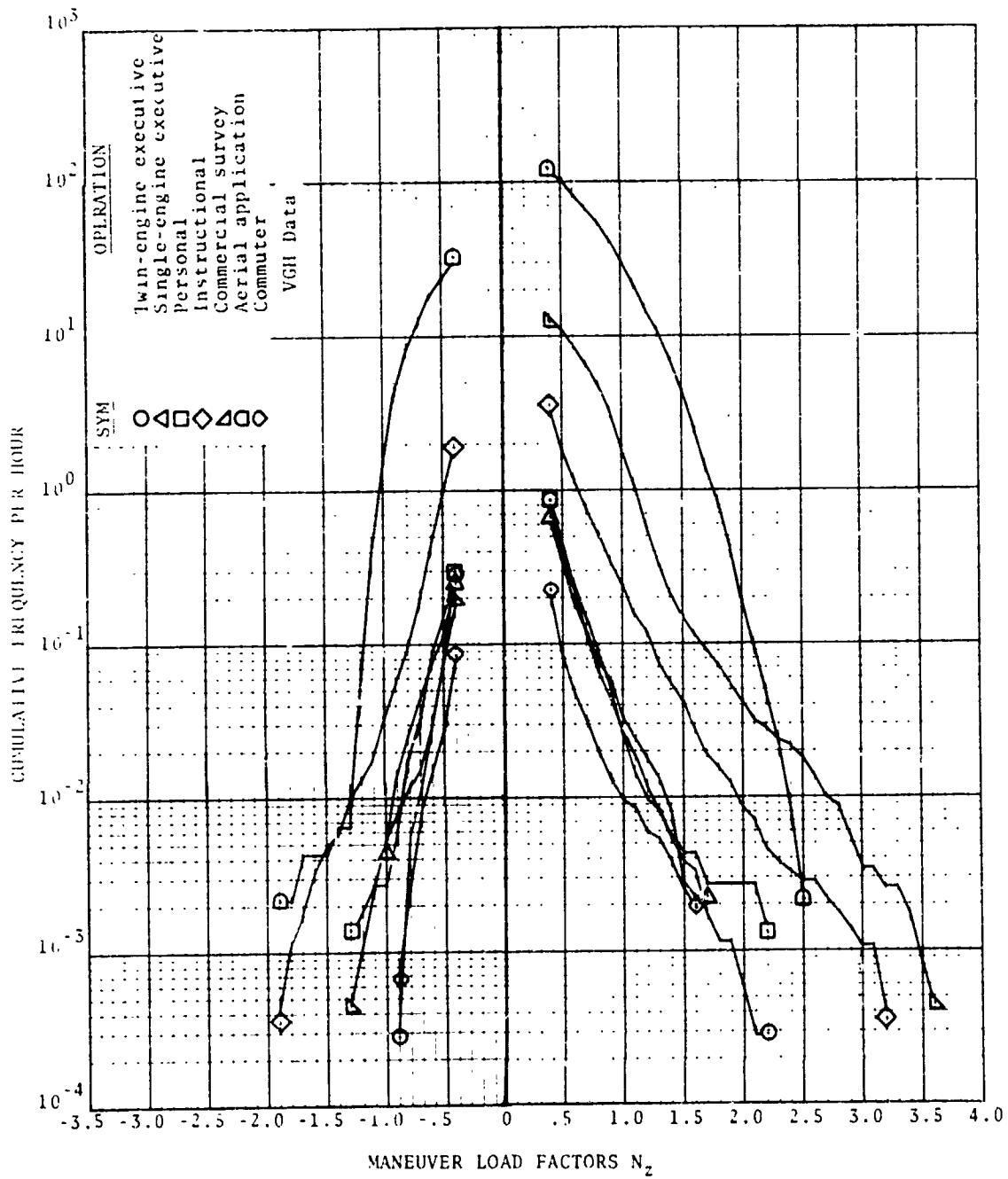


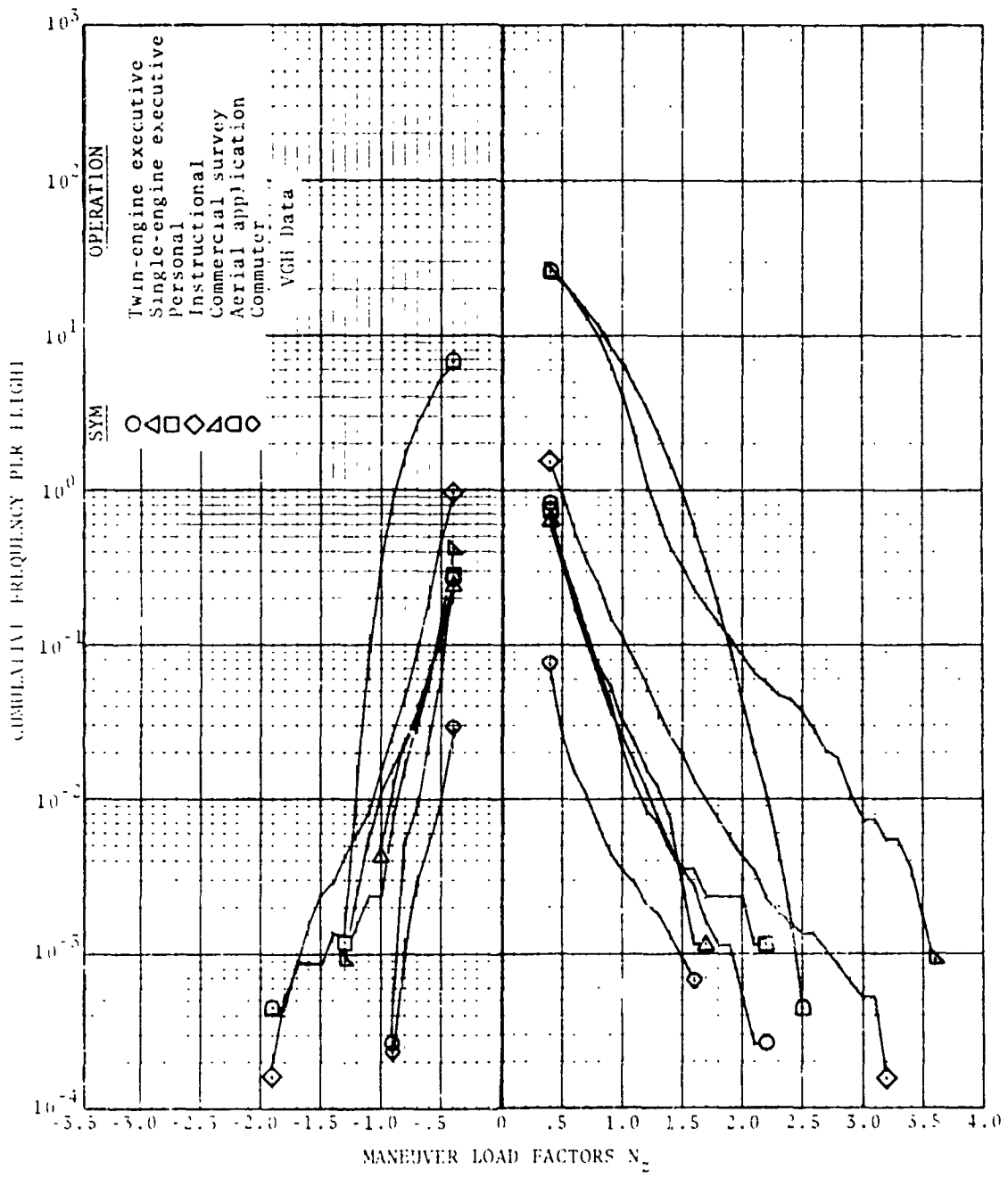
Figure 17. Gust Load Factor Cumulative Frequencies in VGH Data



a. Frequency per Hour

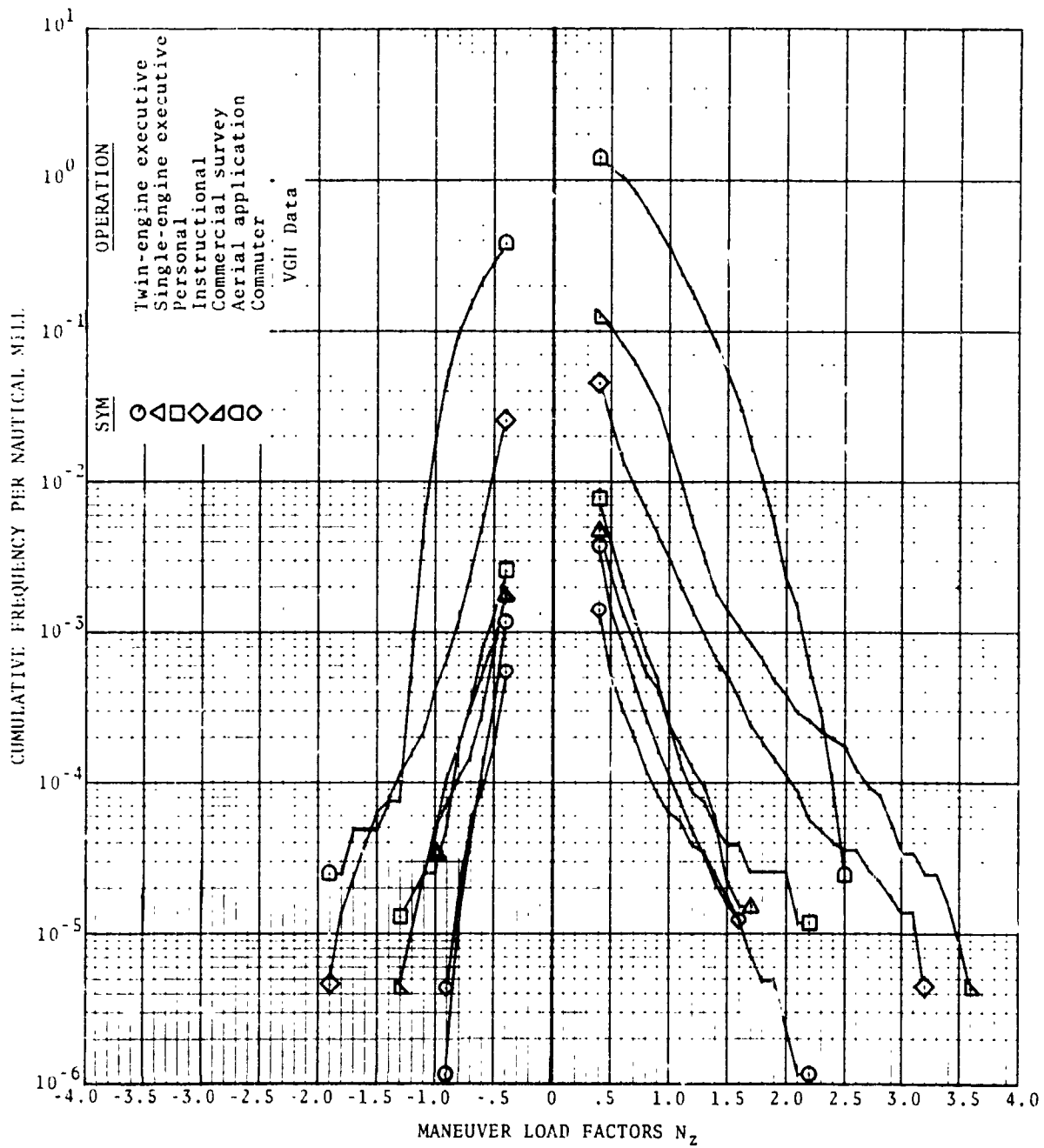
Figure 18. Maneuver Load Factor Cumulative Frequencies in VGH Data





b. Frequency per Flight

Figure 18. - Continued



c. Frequency per Nautical Mile

Figure 18. - Concluded

The Aerial Application category has the highest frequency of maneuver loads with 100 peaks per hour above  $0.5 n_z$ , one peak per hour above  $1.77 n_z$ , and one peak per hundred hours above  $2.38 n_z$ . The Commercial Survey and Instructional categories have the next highest frequencies at all levels up to  $2.5 n_z$  and the highest frequencies above  $2.5 n_z$ . The most extreme negative maneuver load of  $-1.9 n_z$  was recorded by an aircraft in the Instructional category.

#### 2.6.4 Landing Impact Acceleration Ratios

The cumulative frequencies of the positive impact acceleration ratio,  $n_z/2.67$ , per landing are presented in Figure 19. The 2.67 divisor is the minimum ground load design inertia load factor specified in Reference 2. The largest landing impact acceleration was recorded by an aircraft in the Instructional category but the highest frequencies at all  $n_z/2.67$  ratios below 0.95 were recorded by aircraft in the Aerial Application category.

#### 2.7 Landing Impact Probabilities

The  $\Delta n_{z_{max}}$  values in this section are the initial positive landing impact accelerations recorded during each landing impact. With the  $\Delta n_z$ 's grouped in 0.1g increments, the data represent the combined values from operational and checkout flights.

Since the recorded  $\Delta n_z$ 's are the initial positive values, they may not be the maximum values that occurred during landing impacts. Therefore, the small percentage of occurrences in the  $\Delta n_z$  range from 0.0g to 0.1g were excluded to make the frequency distribution for each operation more realistic. Further investigation showed that these exclusions would have had negligible effect on the analysis.

Table XIII summarizes the number of operational and checkout landings for the aircraft types in each operational category.

##### 2.7.1 Analysis

The extreme value theory discussed in Reference 5 was used in the analysis of the frequency distributions of landing impact data. The theory provides a limiting form of the maximum value distribution; this form is a simple analytic function. This section outlines the procedures used in deriving the frequency distributions and control curves, and presents the statistical data. Table XIV lists the symbols used in the following discussion.

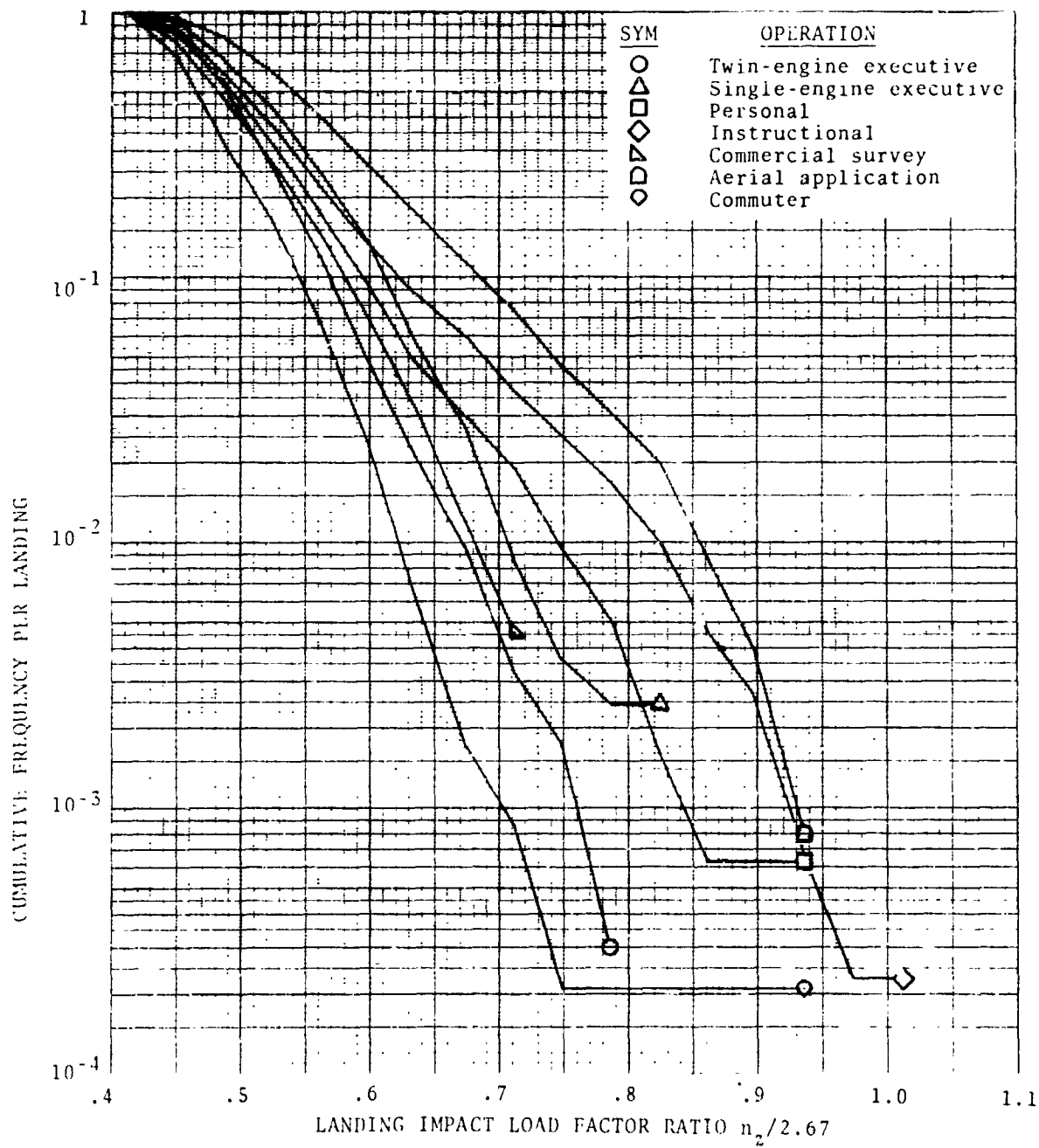


Figure 19. Landing Impact Acceleration Ratio Cumulative Frequencies

TABLE XIII. SUMMARY OF OPERATIONAL AND CHECKOUT LANDINGS BY OPERATIONAL CATEGORY AND AIRCRAFT TYPE

Operational Category/ Aircraft Type	Number of Landings		
	Operational Flights	Checkout Flights	Total
Twin Engine Executive Totals	2975	422	3397
Aircraft Type 1	749	164	913
Aircraft Type 2	595	63	658
Aircraft Type 3	167	31	198
Aircraft Type 4	504	23	527
Aircraft Type 5A	960	141	1101
Single Engine Executive Totals	784	36	820
Aircraft Type 7A	108	0	108
Aircraft Type 8E	260	10	270
Aircraft Type 9A	382	22	404
Aircraft Type 9C	34	4	38
Personal Totals	1642	0	1642
Aircraft Type 10A	260	0	260
Aircraft Type 11	256	0	256
Aircraft Type 12b	1126	0	1126
Instructional Totals	4422	0	4422
Aircraft Type 13	1904	0	1904
Aircraft Type 14	731	0	731
Aircraft Type 15	236	0	236
Aircraft Type 16A	1104	0	1104
Aircraft Type 17	447	0	447
Aerial Application Totals	1245	0	1245
Aircraft Type 23	921	0	921
Aircraft Type 24	324	0	324
Commercial Survey Totals	671	1	672
Aircraft Type 9B	293	1	294
Aircraft Type 16A	378	0	378
Commuter Totals	4977	15	4992
Aircraft Type 26	2621	10	2631
Aircraft Type 28	2356	5	2361
TOTALS	16716	474	17190

TABLE XIV. SYMBOLS USED IN LANDING IMPACT STUDY

$c$	statistical parameter of extreme value distribution
$u$	statistical parameter of extreme value distribution
$y$	reduced variable, defined by $y = c(x-u)$
$x$	random variable
$F^*(y)$	$1-W^*(y)$
$W^*(y)$	cumulative probability distribution of $y$ , defined as $e^{-e^{-y}}$
$n$	number of maximum values
$m$	number of value in order from smallest to largest
$f$	number of occurrences in a $\Delta n_{\max}$ band
$(\sigma\sqrt{n})_m$	reduced standard error of $m$ th of $n$ values
$V_{d_c}$	derived gust velocity
$T(x)$	return period, number of occurrences required to equal or exceed a value of $x$
$e$	Euler's number, equals 0.5772
$S_m$	standard deviation of $m$ th value, equals $\frac{(\sigma\sqrt{n})_m}{\alpha\sqrt{n}}$
$\bar{\quad}$	a bar over a symbol indicates the mean value of the variable

### 2.7.2 Equations and Procedures

The following paragraphs present the equations and procedures used in calculating the extreme value distributions.

After the raw data in  $\Delta n_{z_{\max}}$  bands of 0.1g were first summed from largest to smallest band, a relative cumulative frequency was calculated. This frequency is represented by the symbols (O) in Figures 20 through 27.

The mean values  $\bar{\Delta n}_{z_{\max}}$  and  $\bar{\Delta n}_{z_{\max}}^2$  were then calculated by

$$\bar{\Delta n}_{z_{\max}} = \frac{\sum \Delta n_{z_{\max}} \cdot f}{n} \quad \text{and} \quad \bar{\Delta n}_{z_{\max}}^2 = \frac{\sum \Delta n_{z_{\max}}^2 \cdot f}{n}$$

where the  $\bar{\Delta n}_{z_{\max}}$  values are the midpoints of the  $\Delta n_{z_{\max}}$  bands.

The reduced standard error was then calculated by

$$(\sigma\sqrt{n})_m = [\bar{\Delta n}_{z_{\max}}^2 - (\bar{\Delta n}_{z_{\max}})^2]^{1/2}$$

Next the statistical parameters of the extreme value distribution were computed by

$$\frac{1}{\alpha} = \frac{\sqrt{6}(\sigma\sqrt{n})_m}{\pi} \quad u = \bar{\Delta n}_{z_{\max}} - 1/\alpha(0.5772)$$

Then the reduced variable distribution was computed by

$$y = \alpha(\Delta n_{z_{\max}} - u)$$

From the foregoing computations, the cumulative probability and corresponding smallest value for the probability distributions were calculated by

$$W^*(y) = e^{-e^{-y}} \quad F^*(y) = 1 - W^*(y)$$

The smallest value for the probability distributions of the reduced variable were then plotted as solid lines in Figures 20 through 27. Table XV presents sample calculations for arbitrary data.

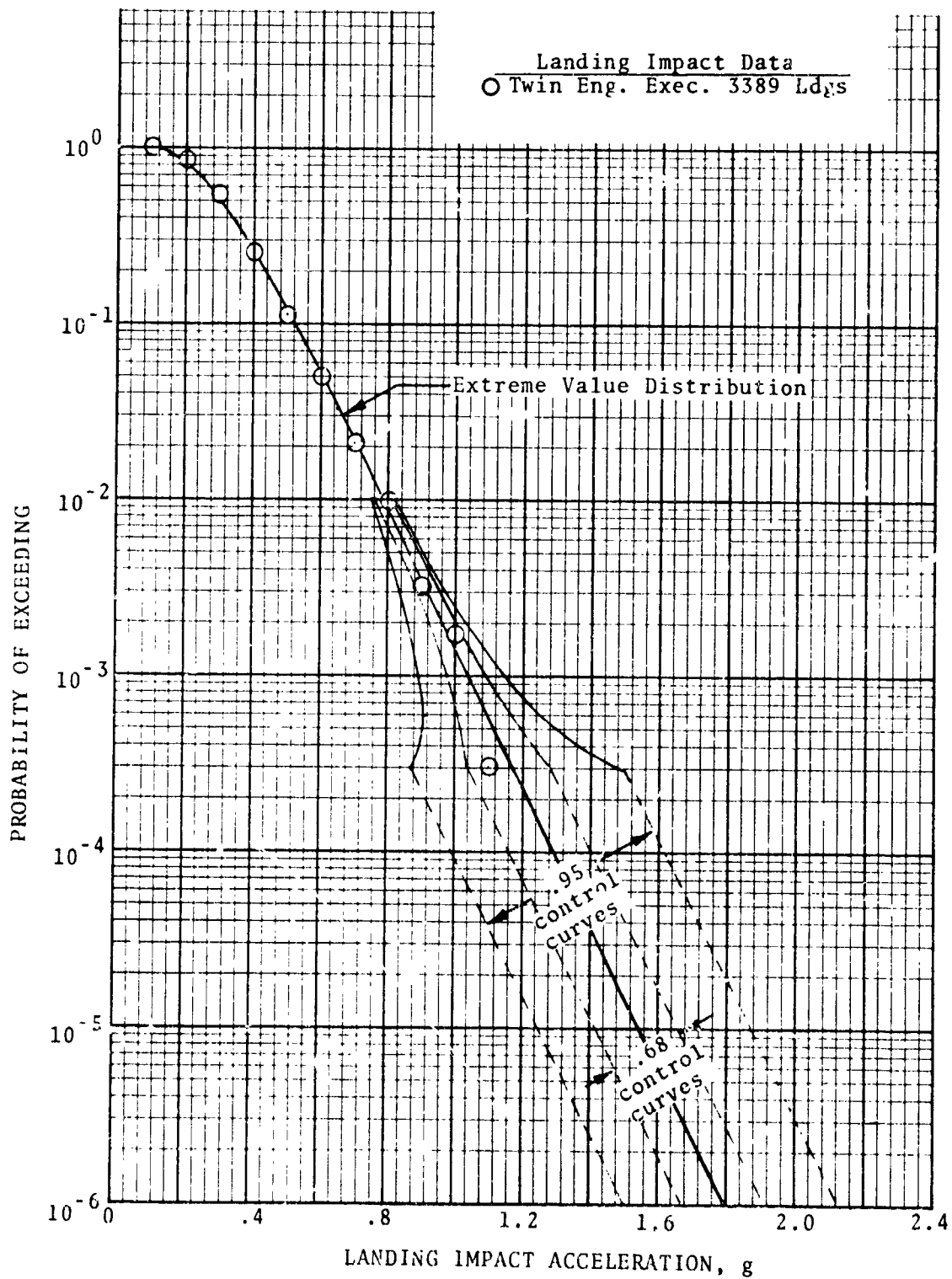


Figure 20. Landing Impact Data for Twin-Engine Executive Category



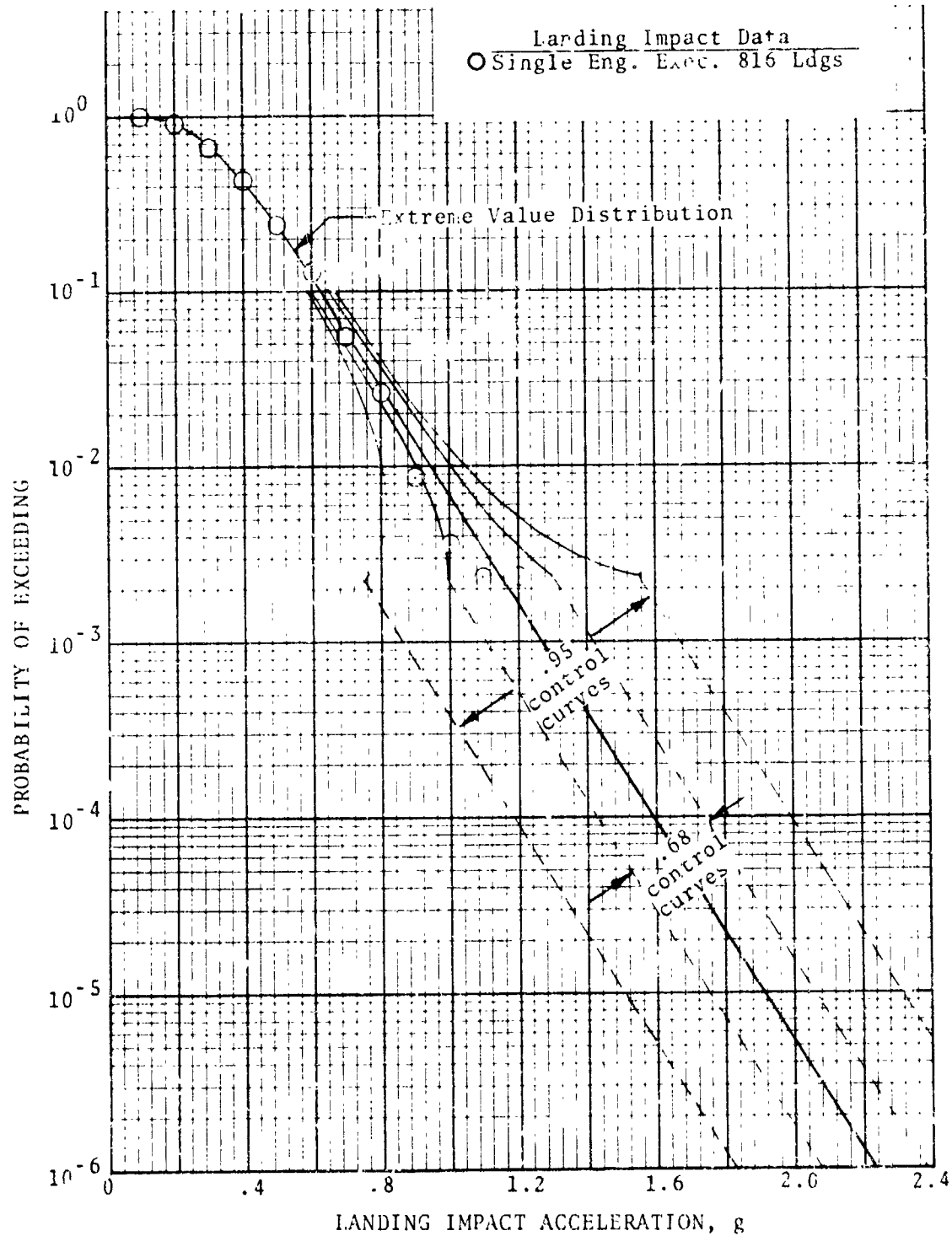


Figure 21. Landing Impact Data for Single-Engine Executive Category

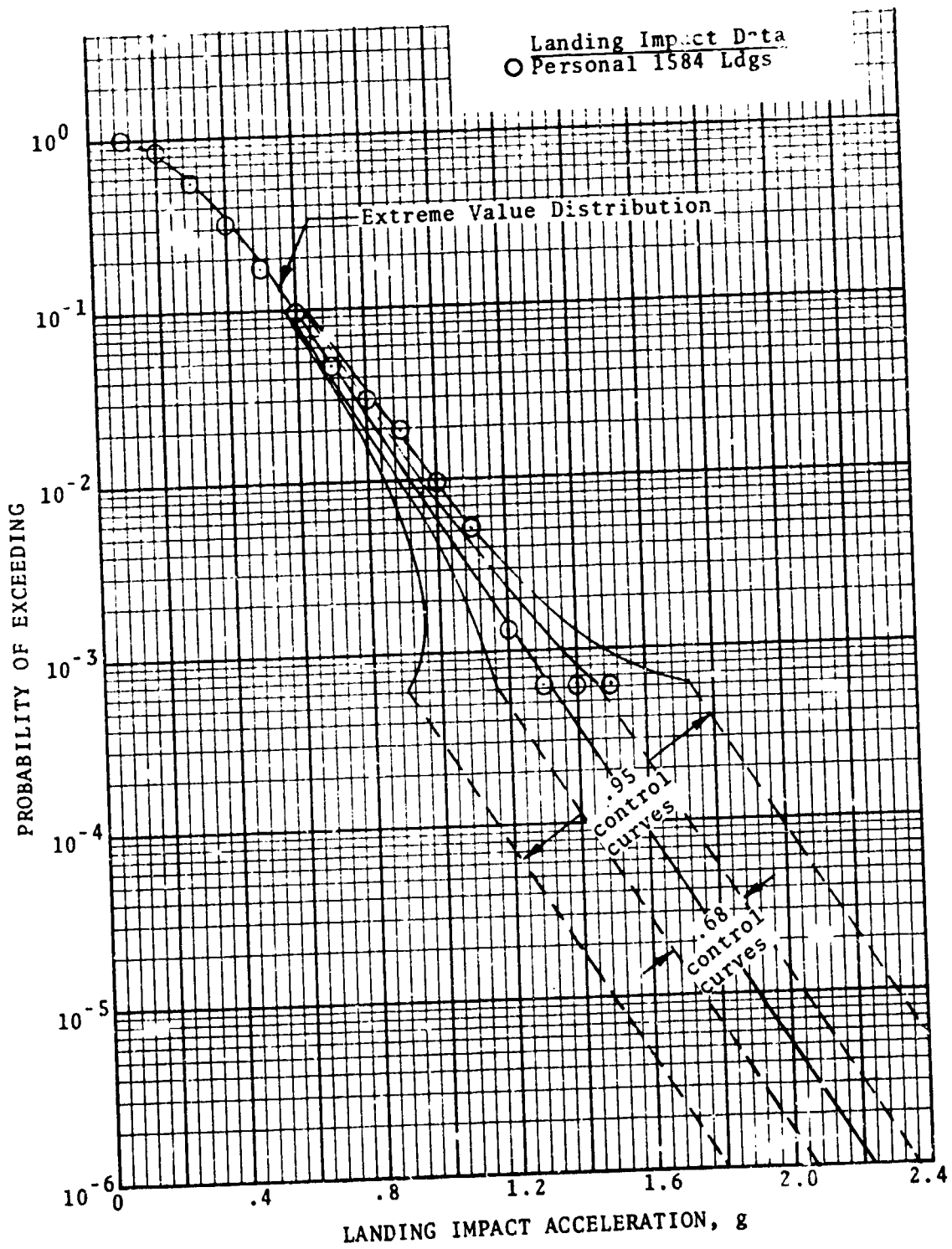


Figure 22. Landing Impact Data for Personal Category

C-2

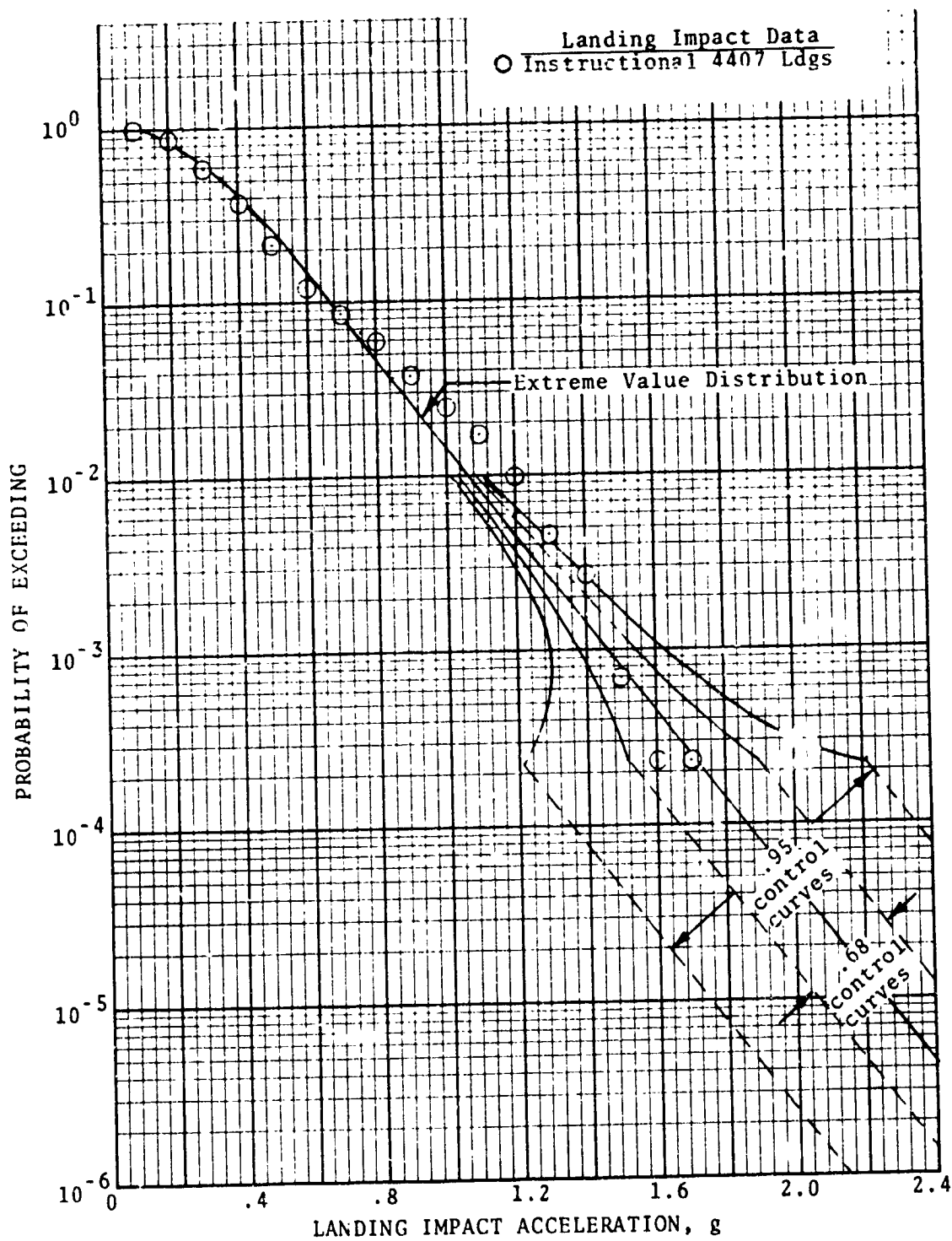


Figure 23. Landing Impact Data for Instructional Category

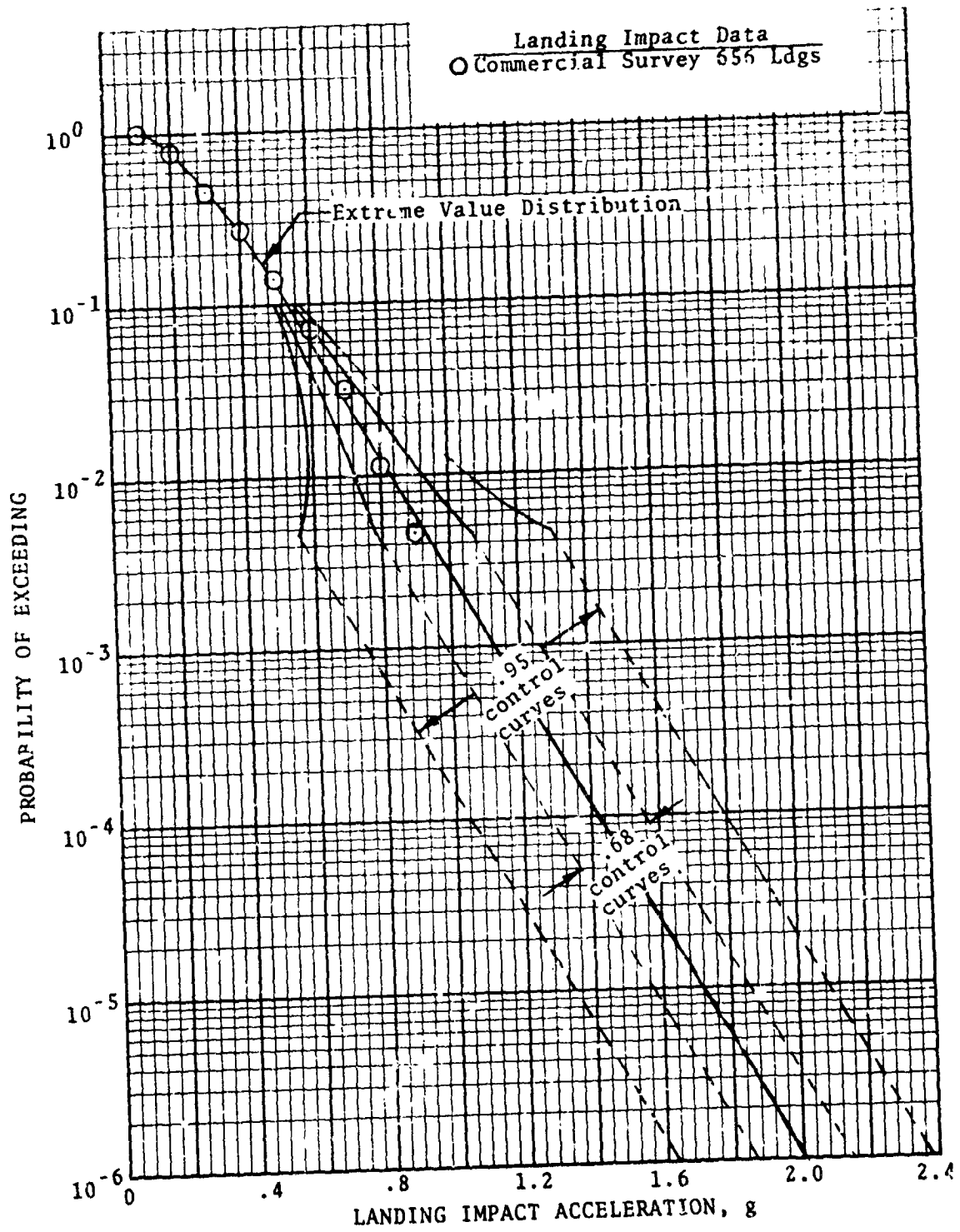


Figure 24. Landing Impact Data for Commercial Survey Category

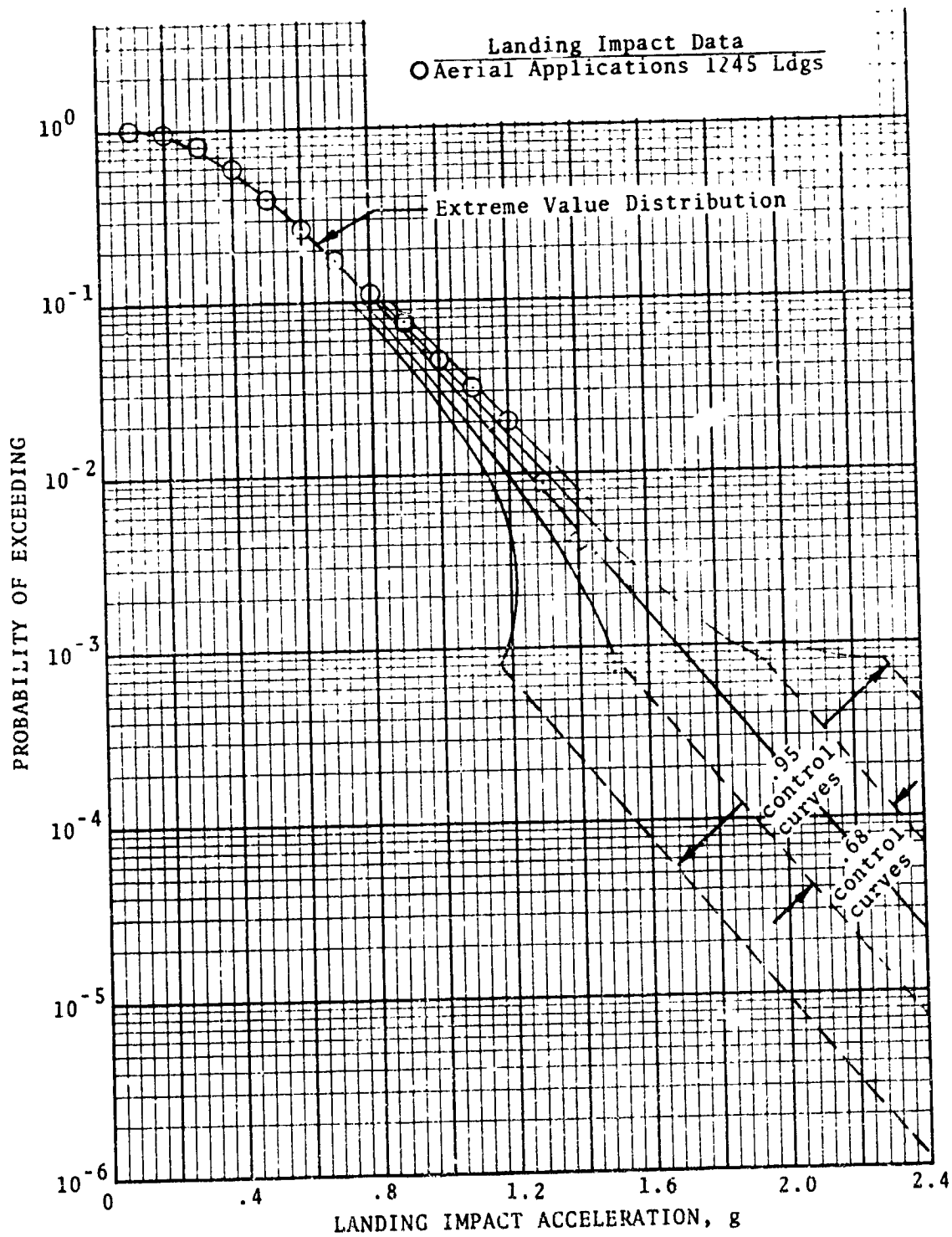


Figure 25. Landing Impact Data for Aerial Applications Category

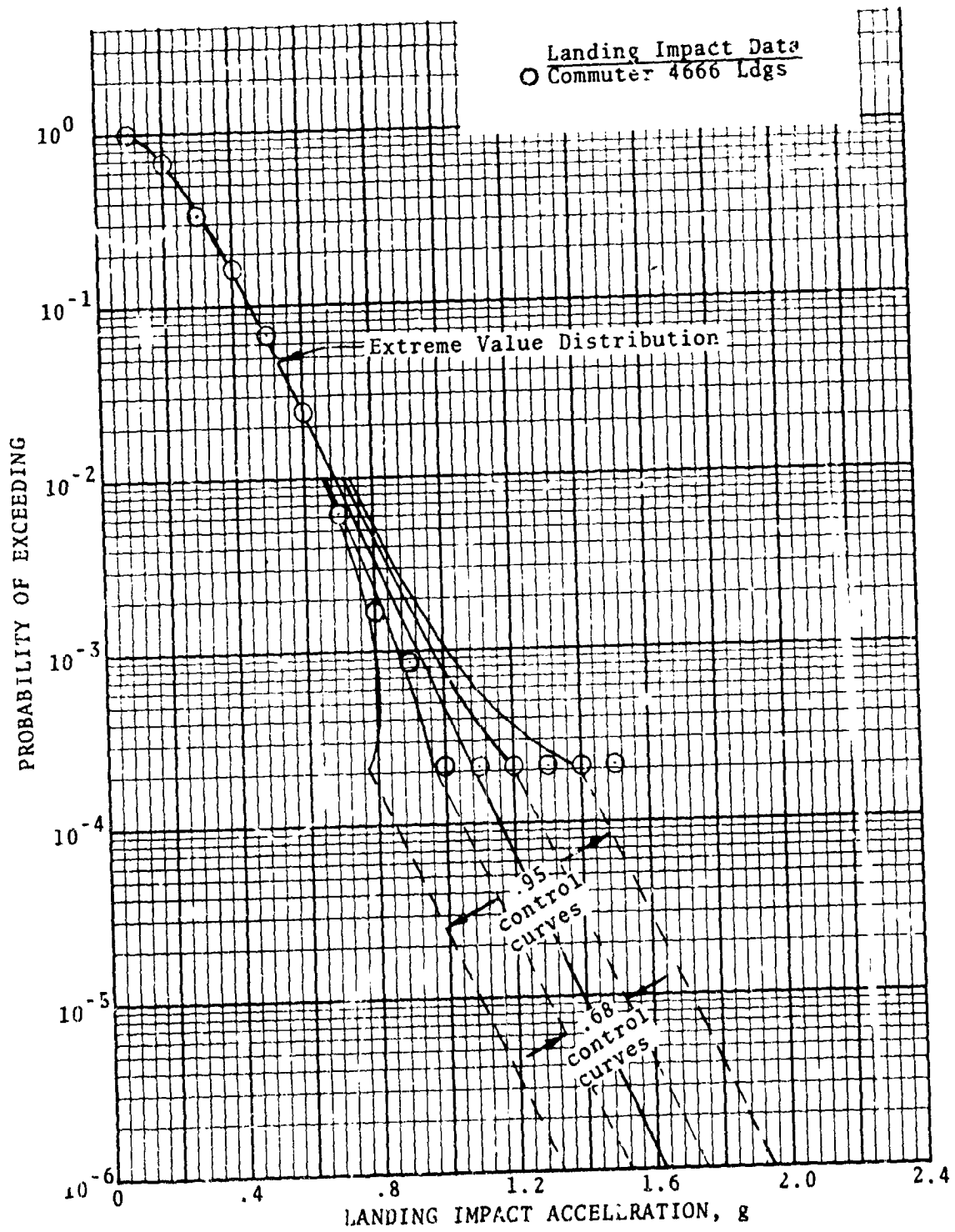


Figure 26. Landing Impact Data for Commuter Category

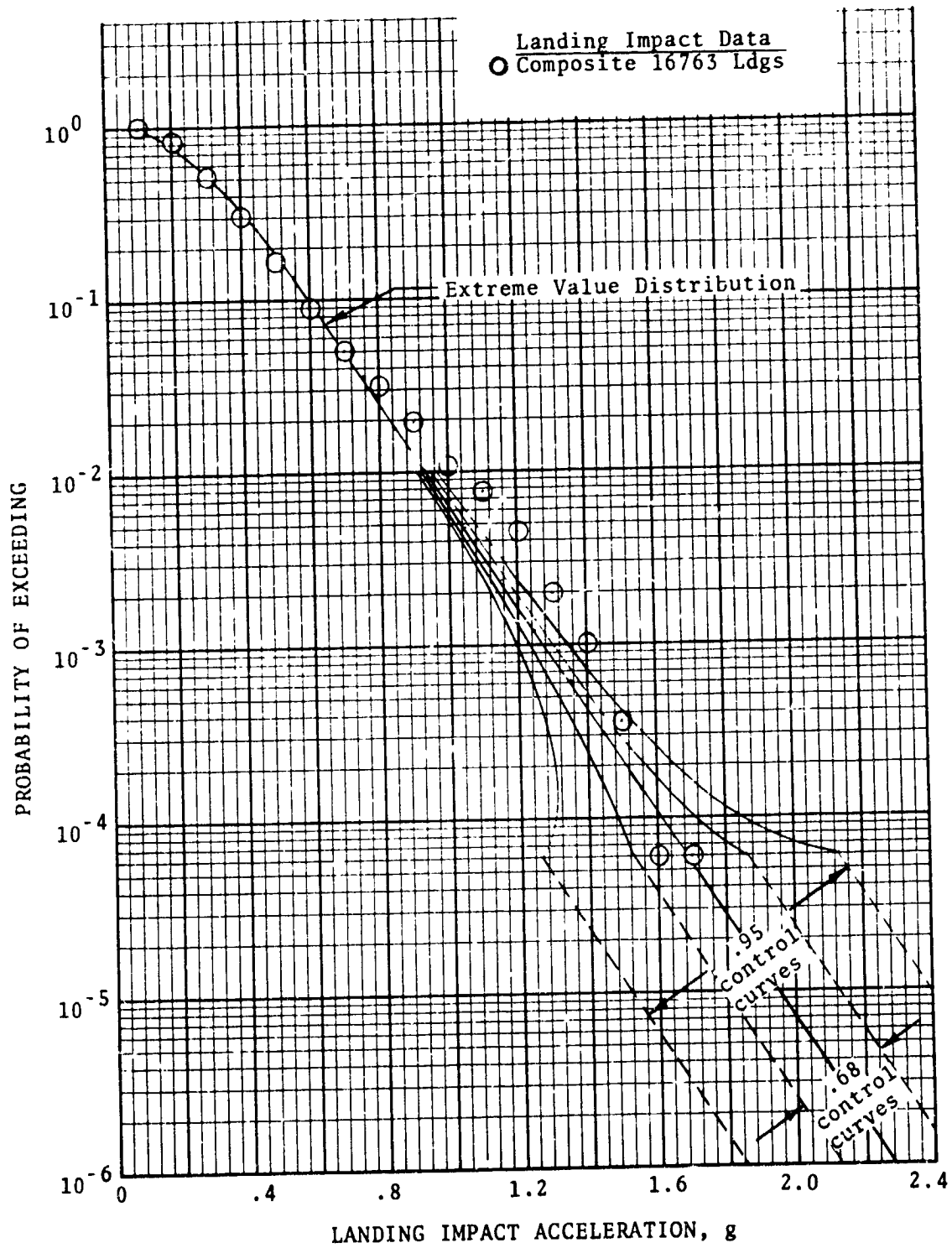


Figure 27. Landing Impact Data for Category Composite

TABLE XV. SAMPLE CALCULATIONS FOR EXTREME LANDING IMPACT PROBABILITY DISTRIBUTIONS

$\Delta n_{z_{\max}}$ Band	$\Delta n_{z_{\max}}$	f	$\epsilon f$	Pr(f)	$\Delta n_{z_{\max}} \cdot f$	$\Delta n_{z_{\max}}^2 \cdot f$	y	F*(y)
0.1-0.3	0.2	53	87	1.00	10.6	2.12	-0.350	0.758
0.3-0.5	0.4	24	34	0.391	9.6	3.84	1.486	0.203
0.5-0.7	0.6	10	10	0.115	6.0	3.60	3.321	0.035

$$\overline{\Delta n_{z_{\max}}} = 0.301 \quad \overline{\Delta n_{z_{\max}}^2} = 0.110$$

$$(\sigma\sqrt{n})_m = 0.139 \quad 1/\alpha = 0.109$$

$$u = 0.238$$

With a breakdown by operational category, Table XVI summarizes the maximum impact  $\Delta n_z$  for each landing in the entire data sample by listing the number of such occurrences in the respective  $\Delta n_z$  bands.

After the extreme value curves were developed, a method was needed to measure the reliability of the sample estimates. As indicated in Reference 5, the "control curve" method derived by E. J. Gumbel provides a simple and rapid method of indicating the reliability of extreme value distributions. With this method, the standard deviation for the different curves at various levels of probability is calculated by

$$S_m = \frac{(\sigma\sqrt{n})_m}{\alpha\sqrt{n}}$$

The extreme value curve plus or minus the standard deviation gives a 0.68 probability, and plus or minus two times the standard deviation gives a 0.95 probability, that a sample value lies within the interval.

For the ultimate value, the interval about the distribution for 0.68 probability was found to be

$$\pm S_m = \frac{1.14}{\alpha}$$

for 0.95 probability

$$\pm S_m = \frac{2.97}{\alpha}$$



The penultimate 0.68 and 0.95 probabilities were found to be

$$\pm S_{n-1} = \frac{0.754n}{\alpha(n-2)} \quad \text{and} \quad \pm S_{n-1} = \frac{1.73n}{\alpha(n-2)}$$

respectively.

The control intervals were extended along the extrapolated portion of the extreme value curve since the interval around the most probable largest value does not depend on the number of occurrences.

TABLE XVI. MAXIMUM LANDING IMPACT LOAD OCCURRENCES IN  $\Delta n_z$  BANDS BY OPERATIONAL CATEGORY

$\Delta n_{zmax}$ Band	Operational Category						
	Twin Engine Exec	Single Engine Exec	Person	Instr	Aerial Applic	Commer Survey	Comm mut
0.1-0.2	500	71	253	503	50	144	1516
0.2-0.3	1117	202	463	1304	187	206	1528
0.3-0.4	876	188	367	969	268	129	845
0.4-0.5	495	153	228	676	246	84	458
0.5-0.6	234	89	123	375	168	47	206
0.6-0.7	96	67	75	203	111	25	84
0.7-0.8	38	24	28	114	73	13	21
0.8-0.9	22	15	16	99	48	5	4
0.9-1.0	5	4	16	56	37	5	3
1.0-1.1	5	1	7	32	19		
1.1-1.2	1		6	32	13		
1.2-1.3		2	1	24	14		
1.3-1.4				10	6		
1.4-1.5				7	4		
1.5-1.6			1	2	1		1
1.6-1.7							
1.7-1.8				1			
TOTAL-n	3389	816	1584	4407	1245	656	4666

### 2.7.3 Design Load Factor

In smoothing the irregular probability curve of the recorded data, the extreme value theory provides a consistent and rational basis for extrapolation beyond the limits of the recorded data. Since the frequency distributions are of the exponential type, the number of occurrences required to reach or exceed a given  $\Delta n_z$  level can be computed by

$$\log_e T(\Delta n_z) = \alpha(x - u) \quad (\text{Reference 6})$$

or

$$T(\Delta n_z) = e^{\alpha(x - u)} = e^y$$

Using these equations and the data from Table XVI, the number of landings required to reach or exceed the minimum design impact load factor of 2.67g can be determined. Table XVII presents these totals for each operational category.

TABLE XVII. LANDINGS REQUIRED TO REACH OR EXCEED MINIMUM DESIGN LOAD FACTOR

<u>Operational Category</u>	<u>Ldgs to Reach or Exceed Min. Design Load Factor</u>
Twin Engine Executive	269,297
Single Engine Executive	19,295
Personal	19,554
Instructional	3,393
Aerial Application	860
Commercial Survey	81,321
Commuter	1,507,121
Composite	14,739

#### 2.7.4 Low-Range Occurrences

As mentioned previously, the occurrences in the 0.0- to 0.1- $\Delta n_z$  range were excluded in the extreme value calculations. The following discusses the effect of these exclusions on the frequency distributions derived.

Table XVIII lists the number of  $\Delta n_z$  occurrences omitted in the extreme value calculations and the corresponding percentage of the total landings for each operational category.

On the basis of the percentages in Table XVIII, the extreme value distributions for the Commuter category were recalculated with the  $\Delta n_{z\max}$  occurrences in the 0.0g to 0.1g range. Figure 28 depicts the curves derived with and without the low-range impacts. As apparent, the difference between the two extreme value curves is negligible. The control curves were not derived since they would reflect the same magnitude differences. The high acceleration values between 1.2g and 1.5g would not be present if more landing data was available.

TABLE XVIII. SUMMARY OF 0.1G TO 0.2G DATA

<u>Operational Category</u>	<u>No. of Occurrences</u>	<u>Percentage of Landings</u>
Twin Engine Executive	8	0.23
Single Engine Executive	4	0.49
Personal	58	3.53
Instructional	15	0.34
Aerial Applications	0	0.0
Commercial Survey	16	2.38
Commuter	326	6.53

## 2.8 Airspeed Practices

As calculated from VGH airspeed data, the probabilities of exceeding the design cruising speed ratio,  $V/V_C$ , and the design dive speed ratio,  $V/V_D$ , are presented in Figures 29 through 35 and Figures 36 through 42, respectively. In each figure, each symbol set represents a particular aircraft in the operation type, and the dashed line indicates the average probability for the ratios at incremental  $V/V_C$  and  $V/V_D$  levels.

Although 17 of the 24 aircraft types had airspeeds above  $V_C$ , none had airspeeds above  $V_D$ . The highest probability of a  $V_C$  exceedance is in the data for the Personal category. The highest  $V/V_C$  ratios, approximately 1.2, are in the data for the Instructional and Commercial Survey categories. The highest  $V/V_D$  ratio, approximately 0.925, is in the data for the Twin-Engine Executive category.

Based on the Unusual Events VG data, Figure 43 presents the probability of exceeding the  $V/V_D$  ratio on a log-normal scale. For each of seven of the operational categories, the curves are average probabilities at incremental  $V/V_D$  levels. The maximum  $V/V_D$  point in the curve for the Twin-Engine Executive category represents only one occurrence at that level. The high values in the curve for the Instructional category are based on seven airspeeds with  $V/V_D$  ratios at or above 1.0 as recorded on two different aircraft types.

For each of the seven operational categories, Figures 44 through 50 present histograms of the percentage of flight time spent in airspeed ranges for each aircraft type and the aircraft composite in a category.

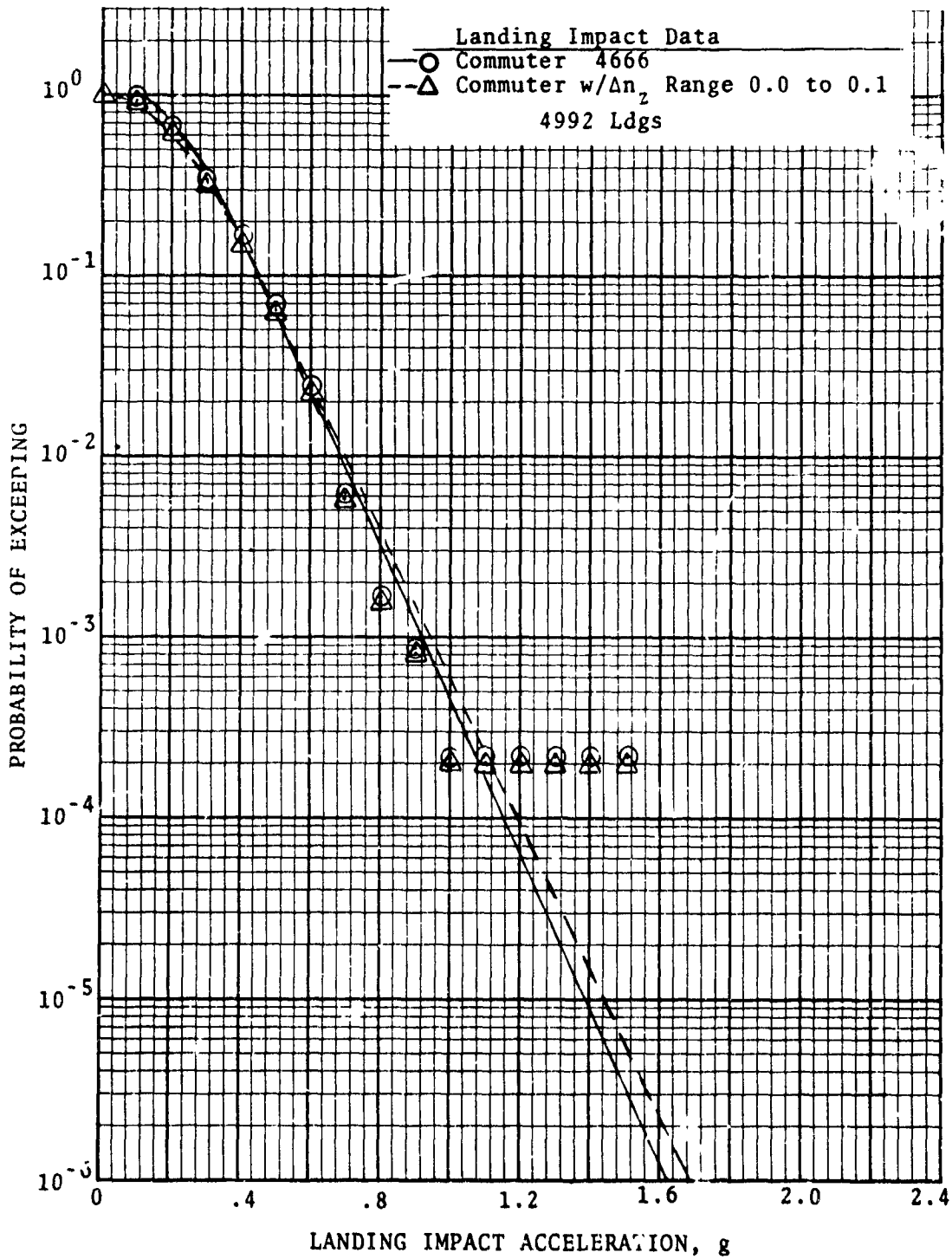


Figure 28. Landing Impact Data With and Without Low-Range Impacts for Commuter Category

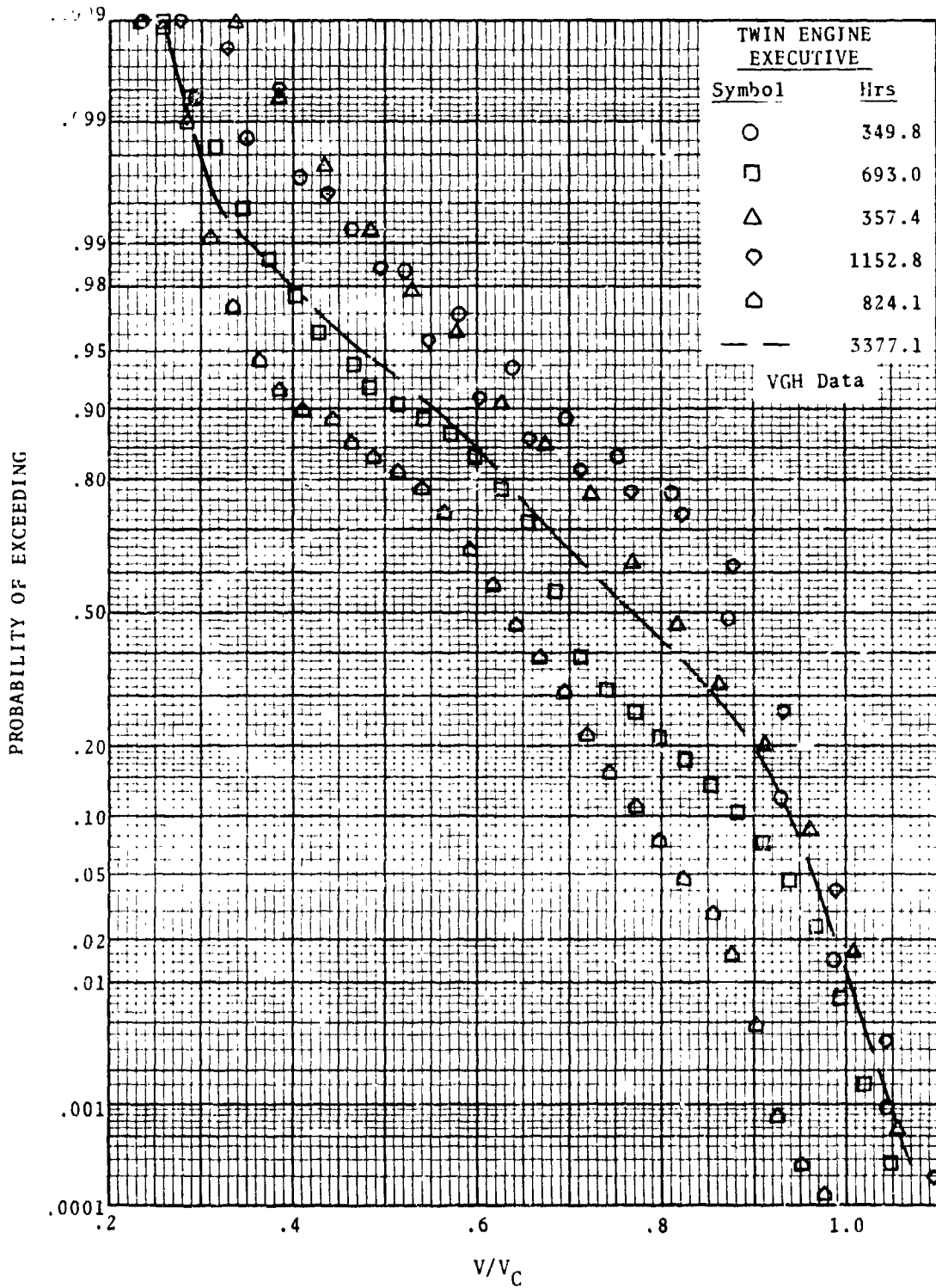


Figure 29. Probability of Exceedance Versus  $V/V_c$  for Twin-Engine Executive Category

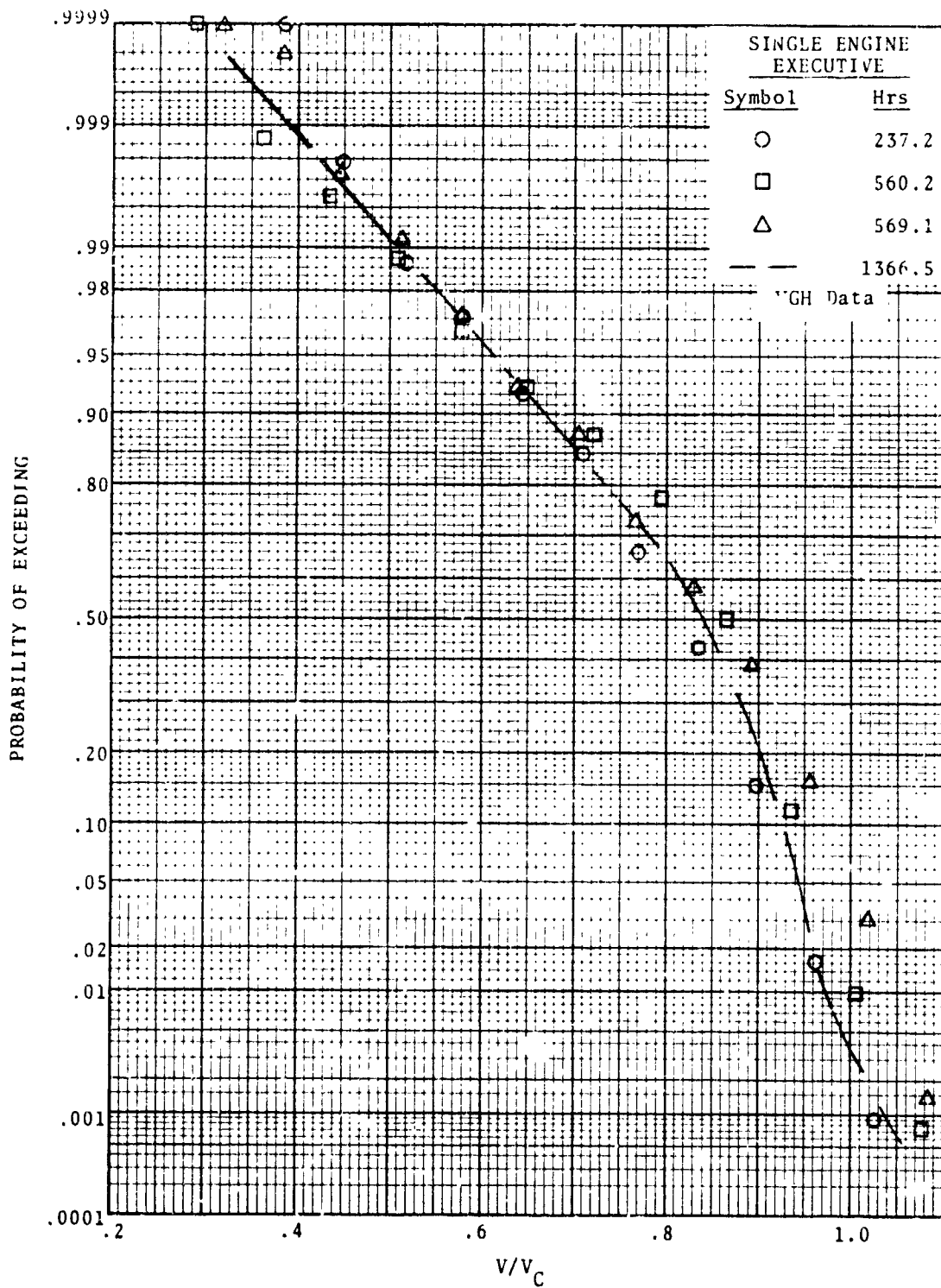


Figure 30. Probability of Exceedance Versus  $V/V_c$  for Single-Engine Executive Category

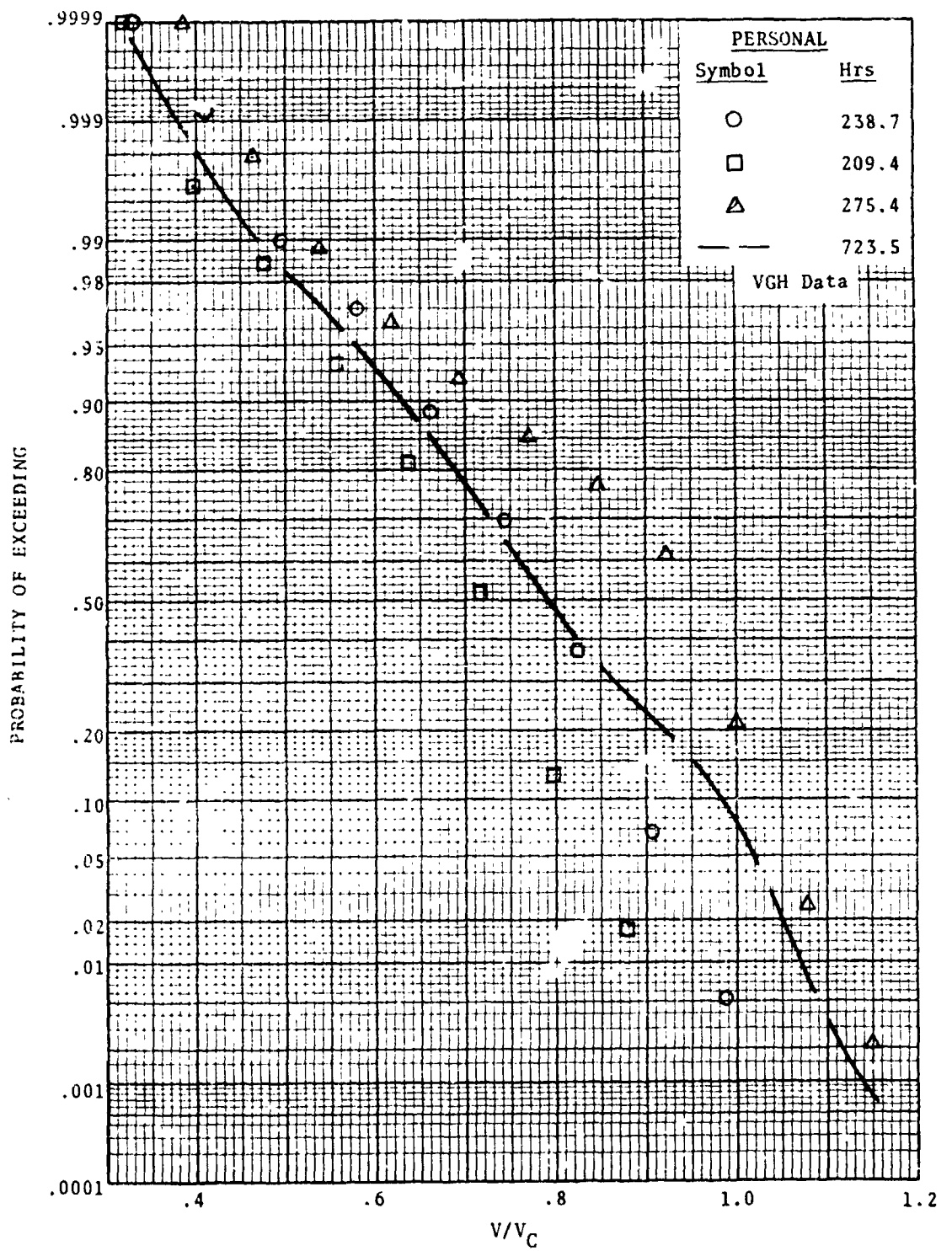


Figure 31. Probability of Exceedance Versus  $V/V_C$  for Personal Category

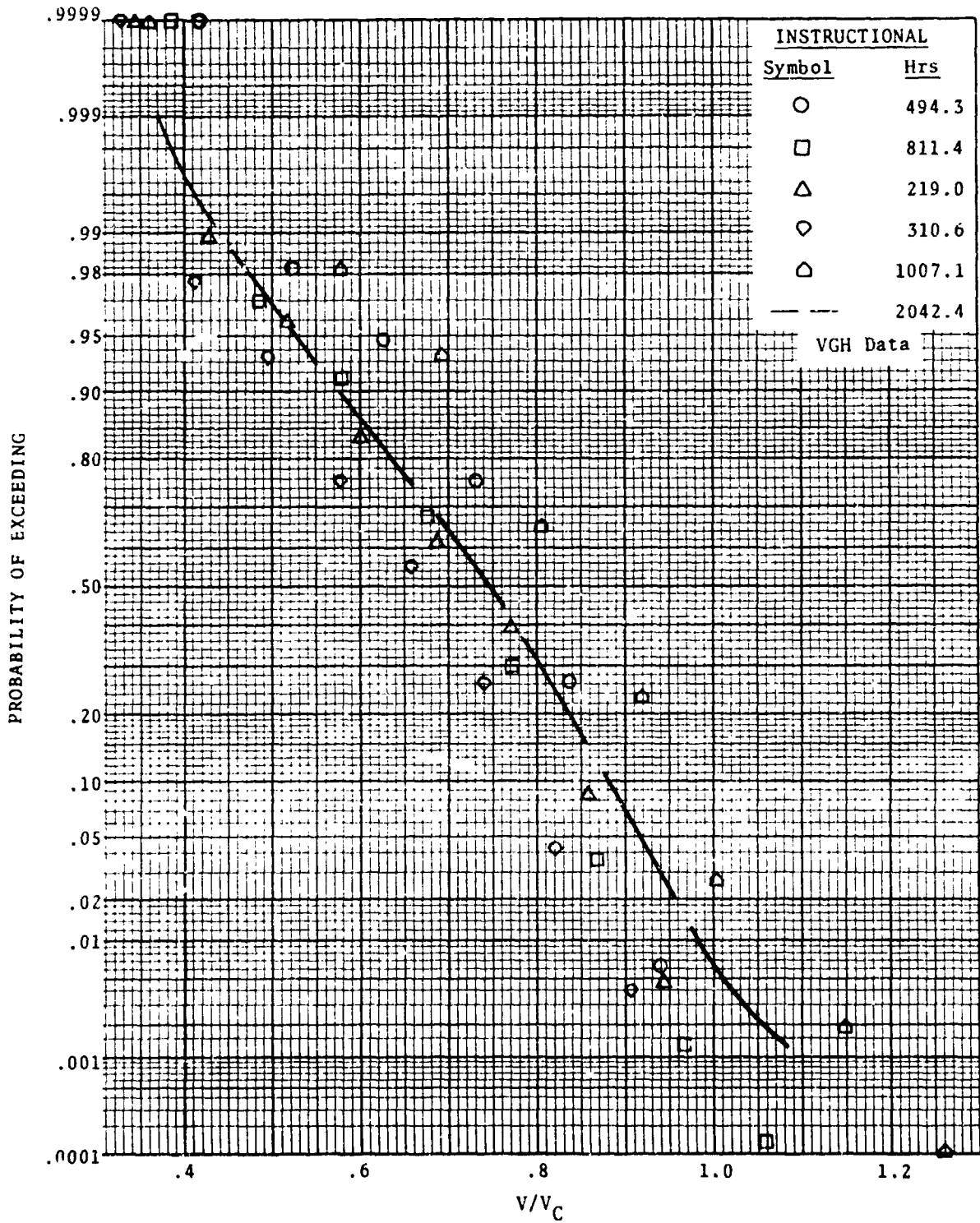


Figure 32. Probability of Exceedance Versus  $V/V_c$  for Instructional Category



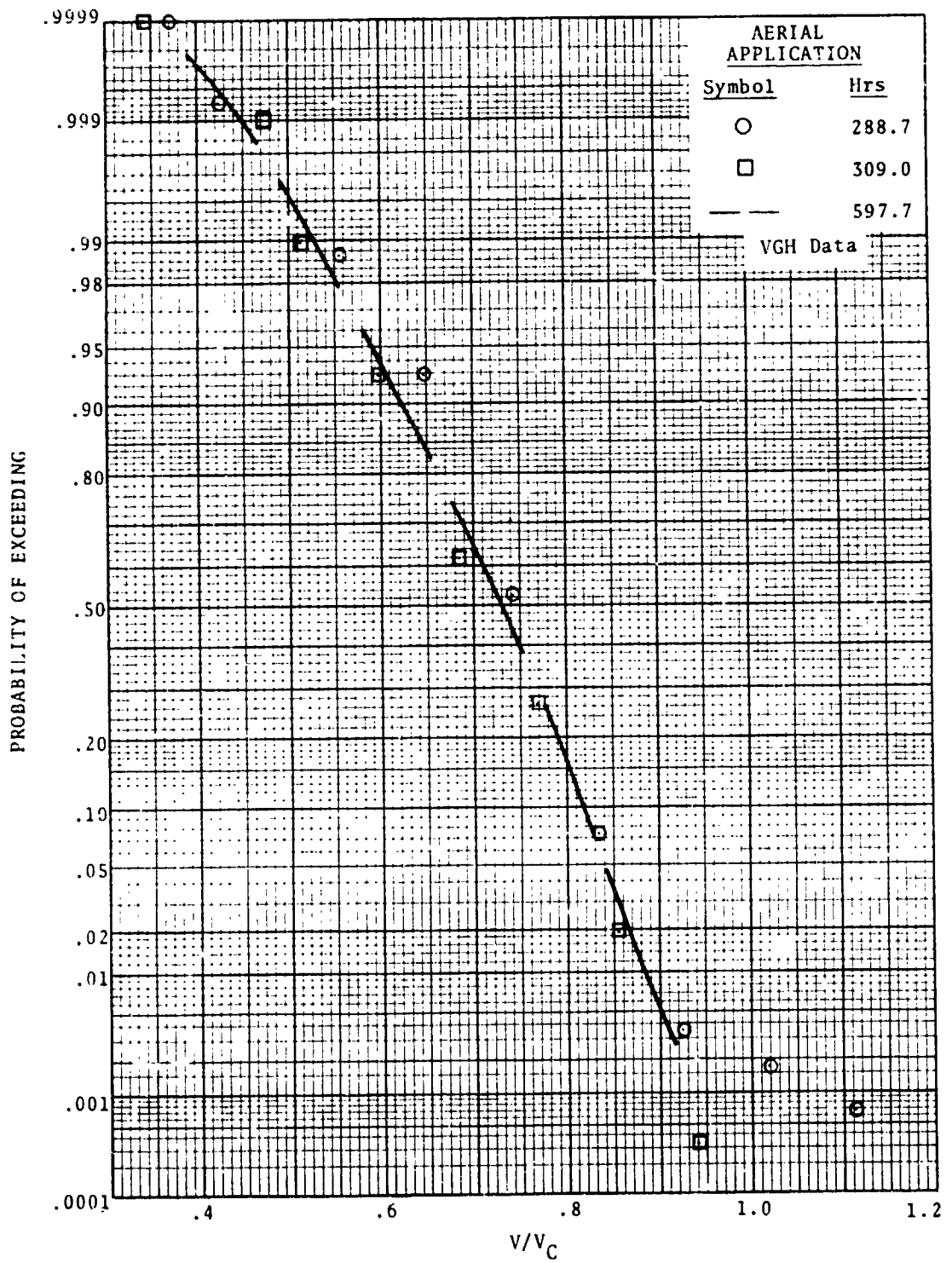


Figure 33. Probability of Exceedance Versus  $V/V_C$  for Aerial Application Category

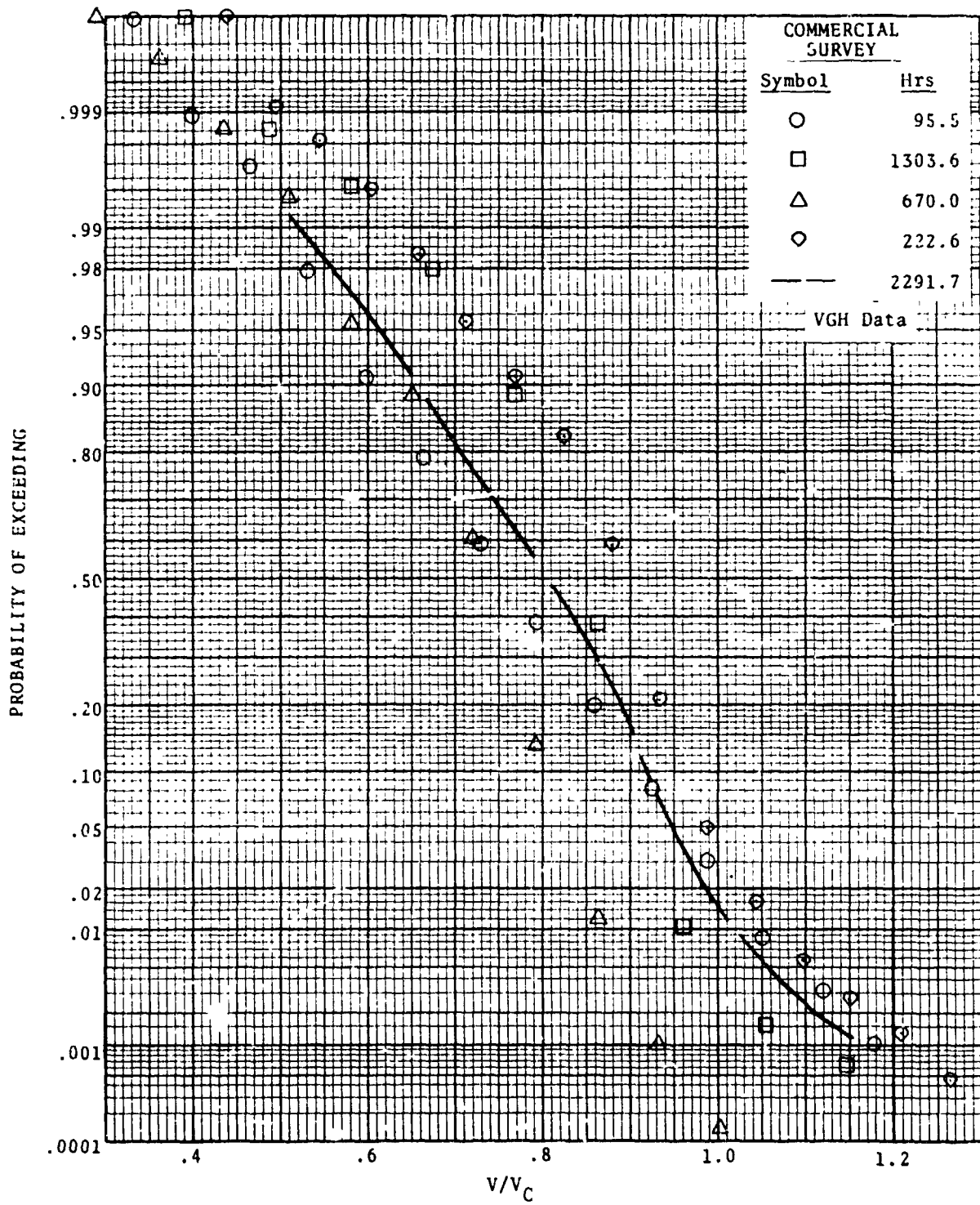


Figure 34. Probability of Exceedance Versus  $V/V_C$  for Commercial Survey Category

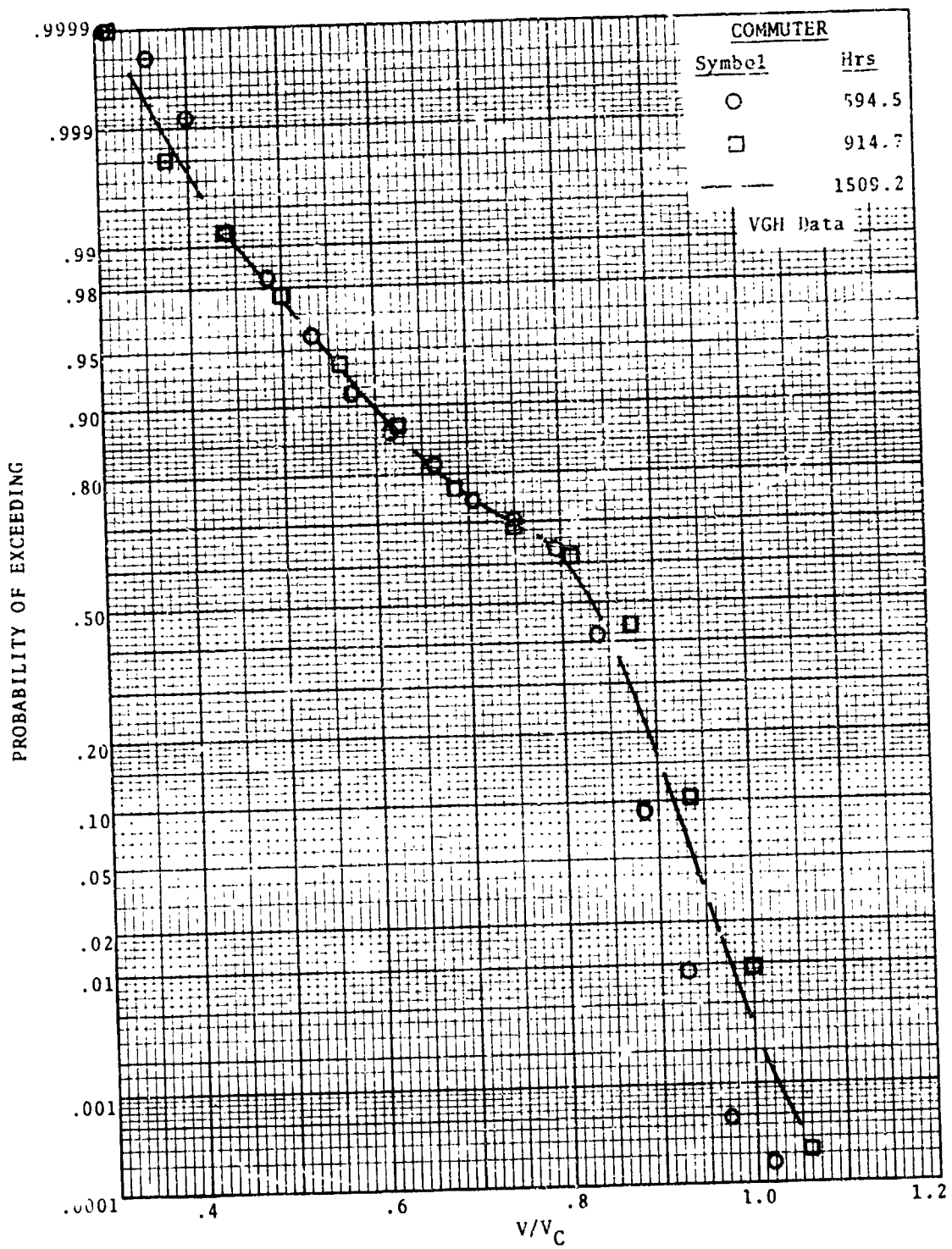


Figure 35. Probability of Exceedance Versus  $V/V_c$  for Commuter Category

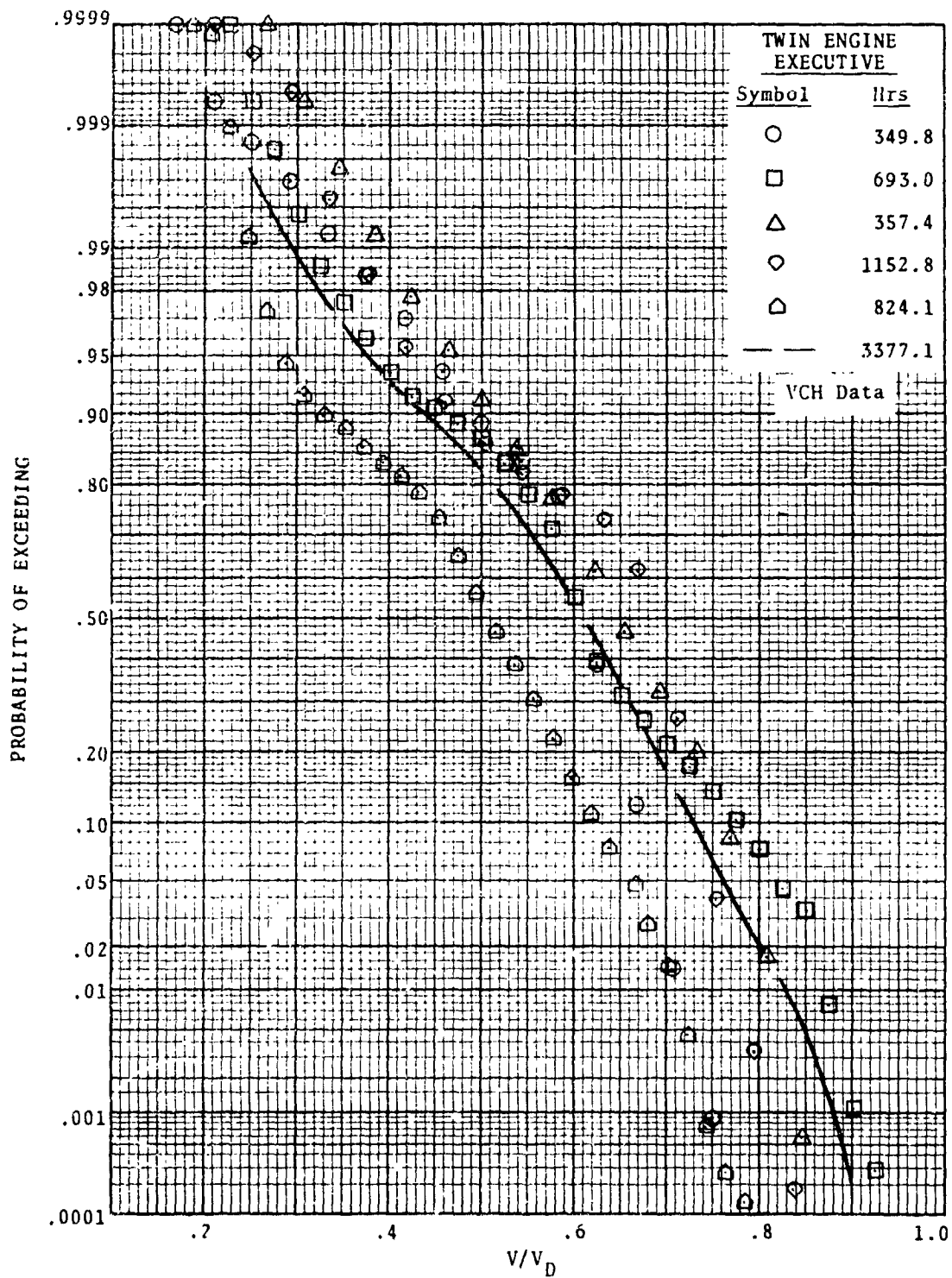


Figure 36. Probability of Exceedance Versus  $V/V_D$  for Twin-Engine Executive Category

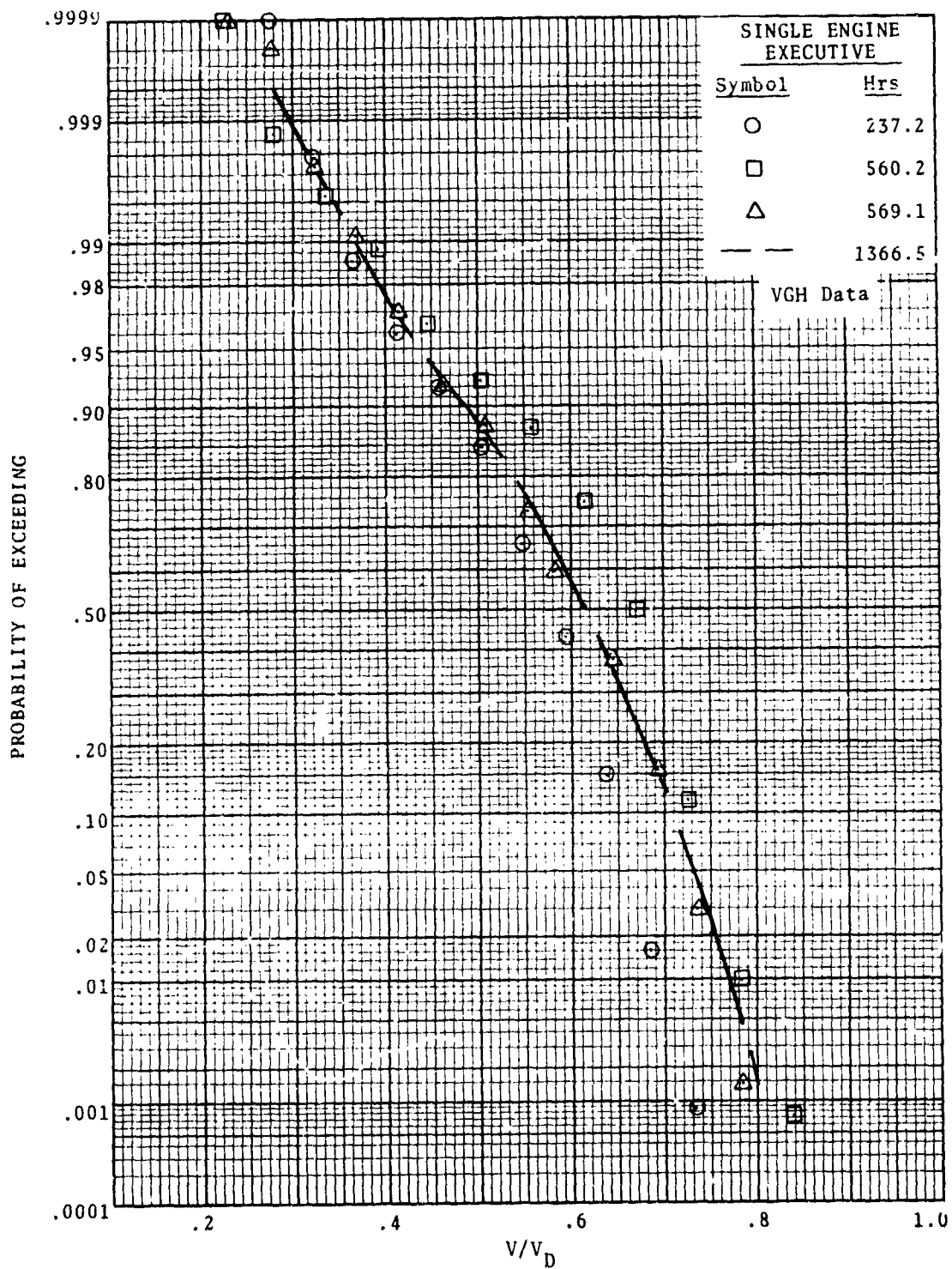


Figure 37. Probability of Exceedance Versus  $V/V_D$  for Single-Engine Executive Category

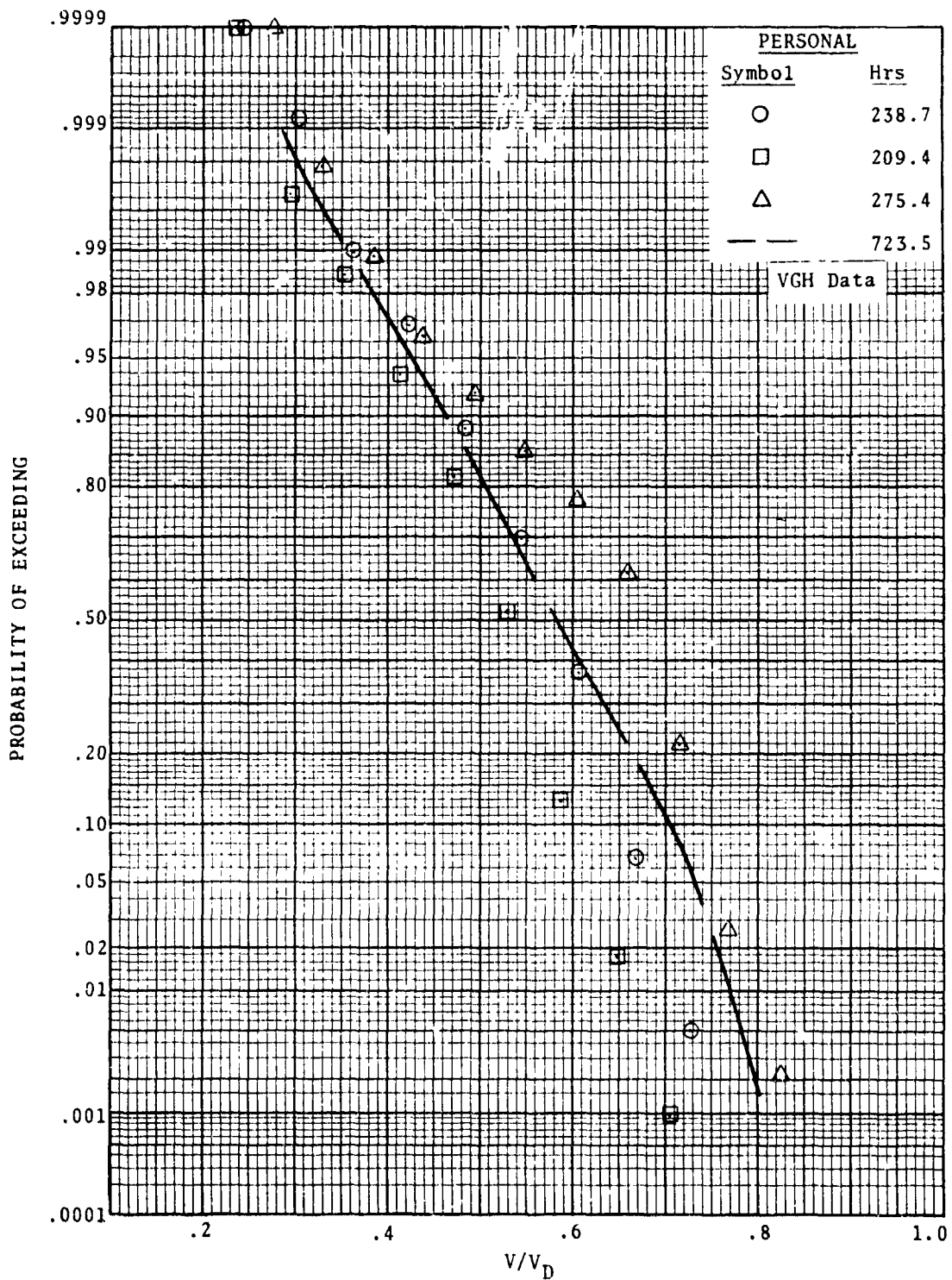


Figure 38. Probability of Exceedance Versus  $V/V_D$  for Personal Category

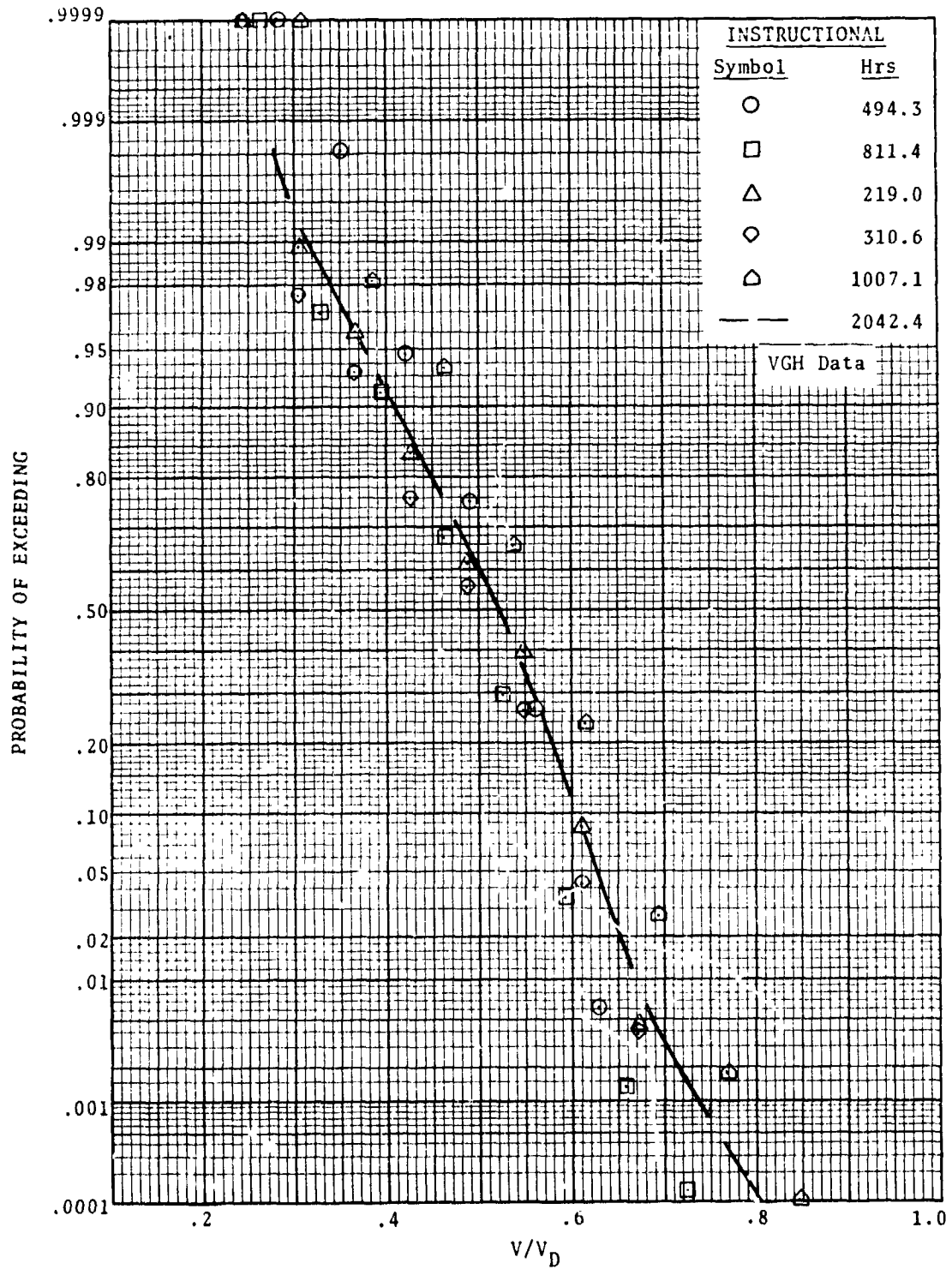


Figure 39. Probability of Exceedance Versus  $V/V_D$  for Instructional Category

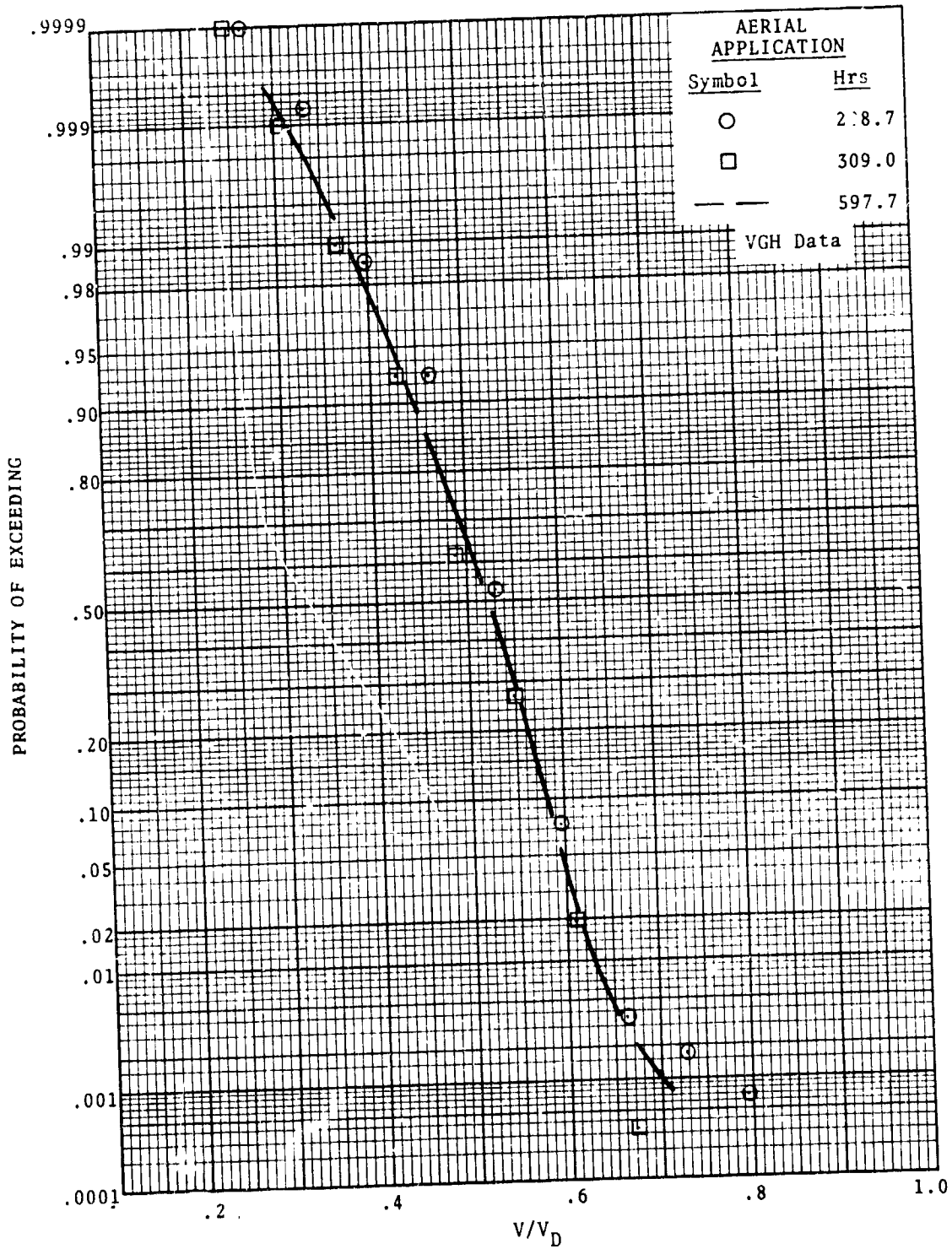


Figure 40. Probability of Exceedance Versus  $V/V_D$  for Aerial Application Category



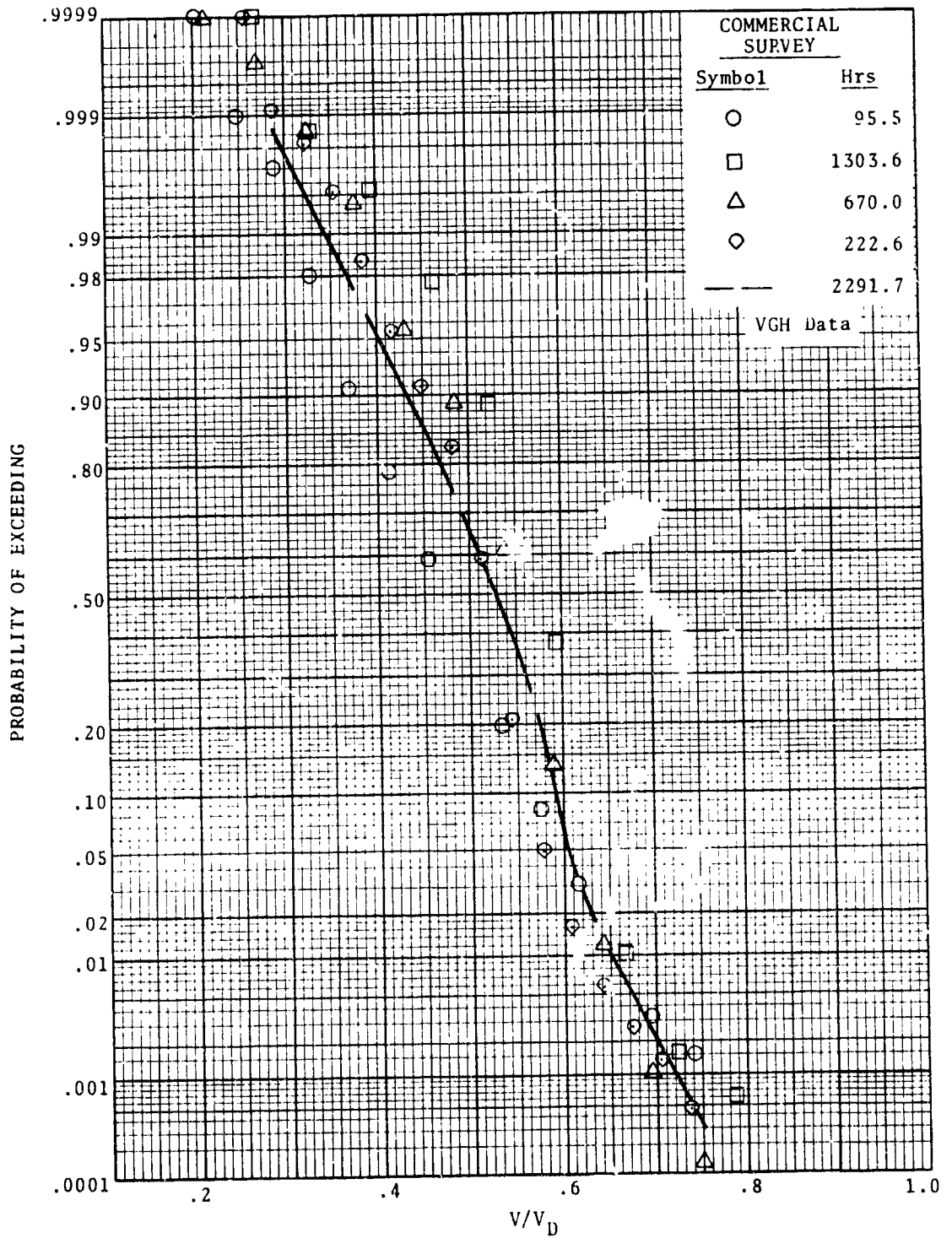


Figure 41. Probability of Exceedance Versus  $V/V_D$  for Commercial Survey Category

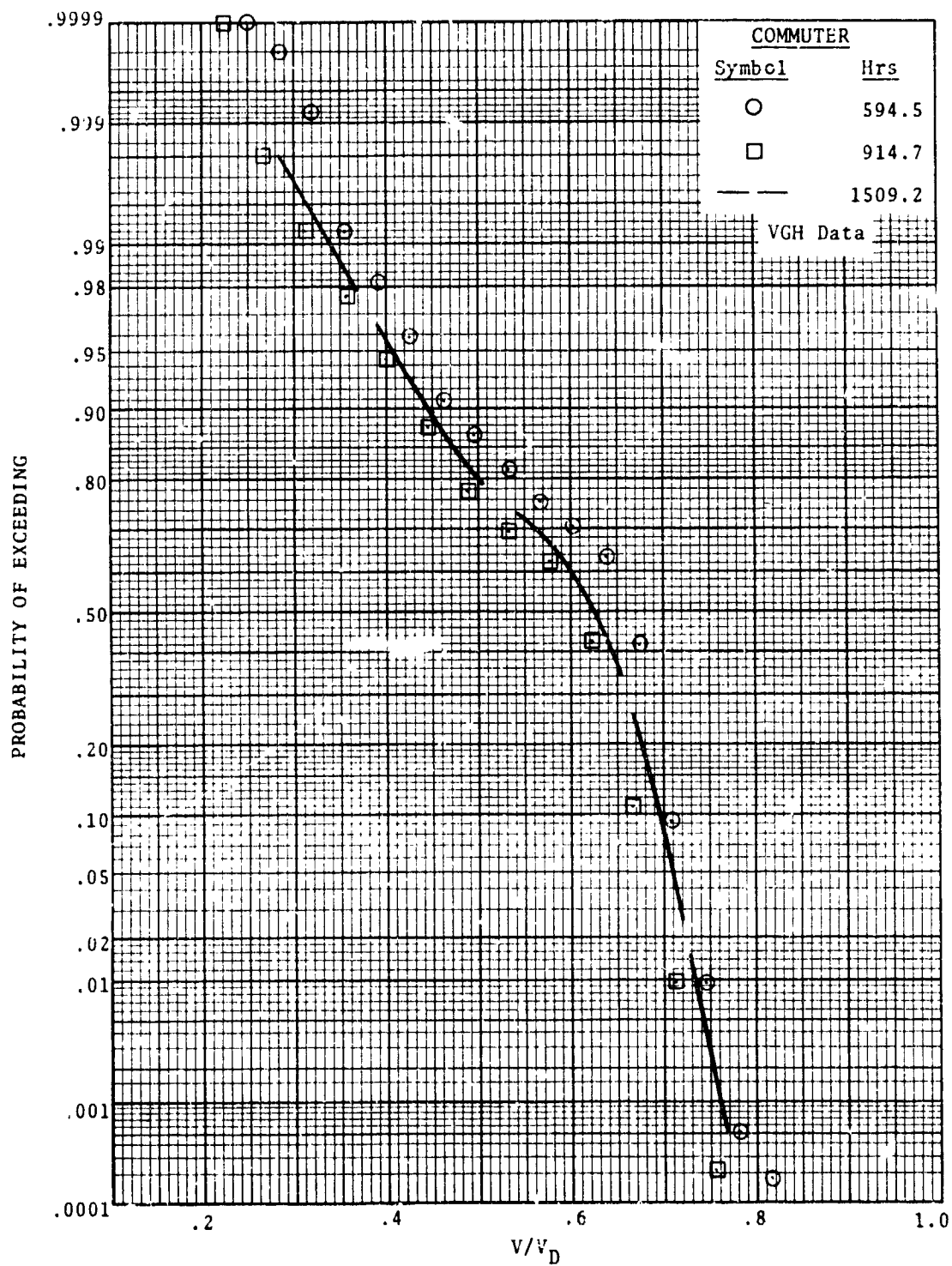


Figure 42. Probability of Exceedance Versus  $V/V_D$  for Commuter Category

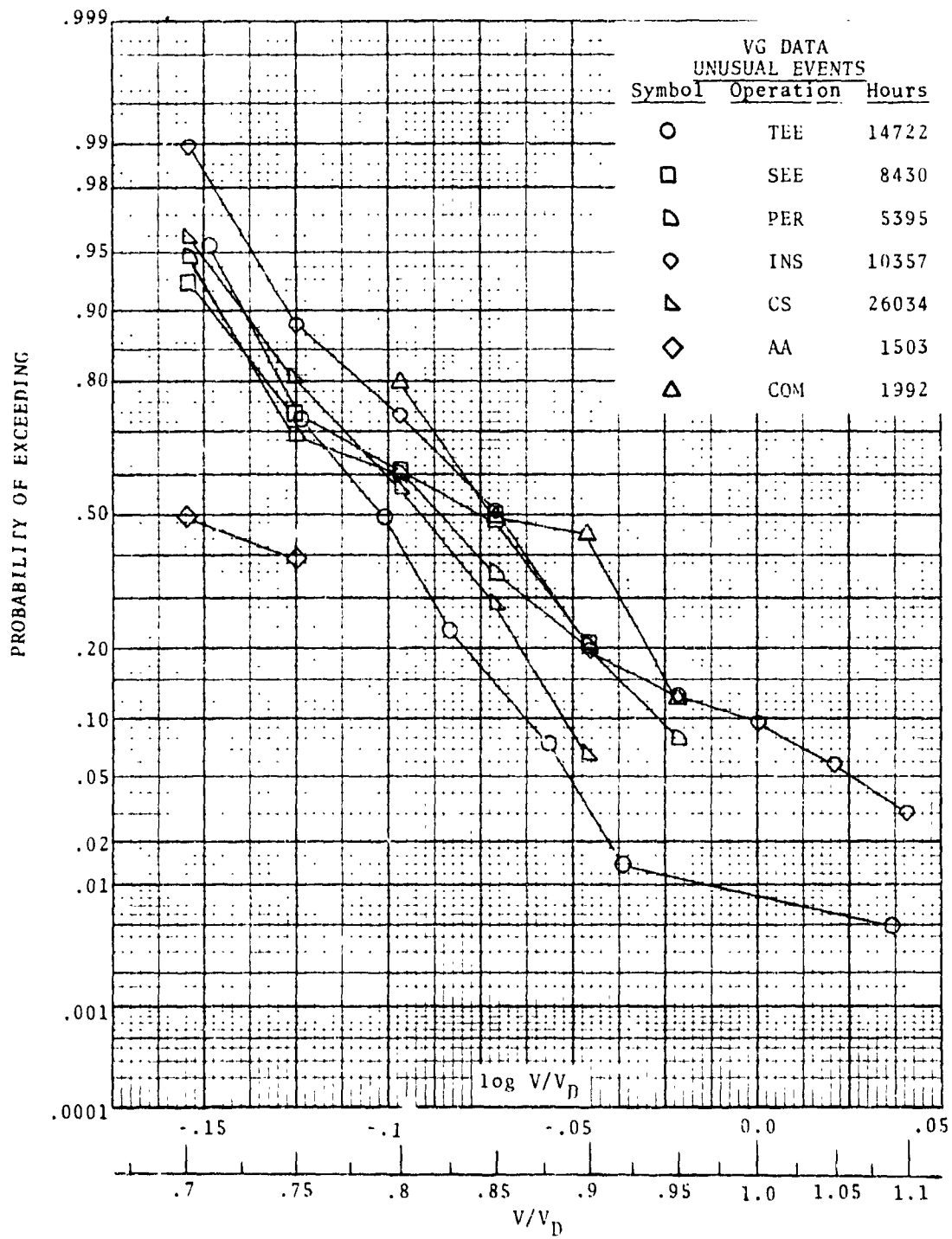


Figure 43. Probability of Exceedance Versus  $V/V_D$  for Unusual Events VG Data

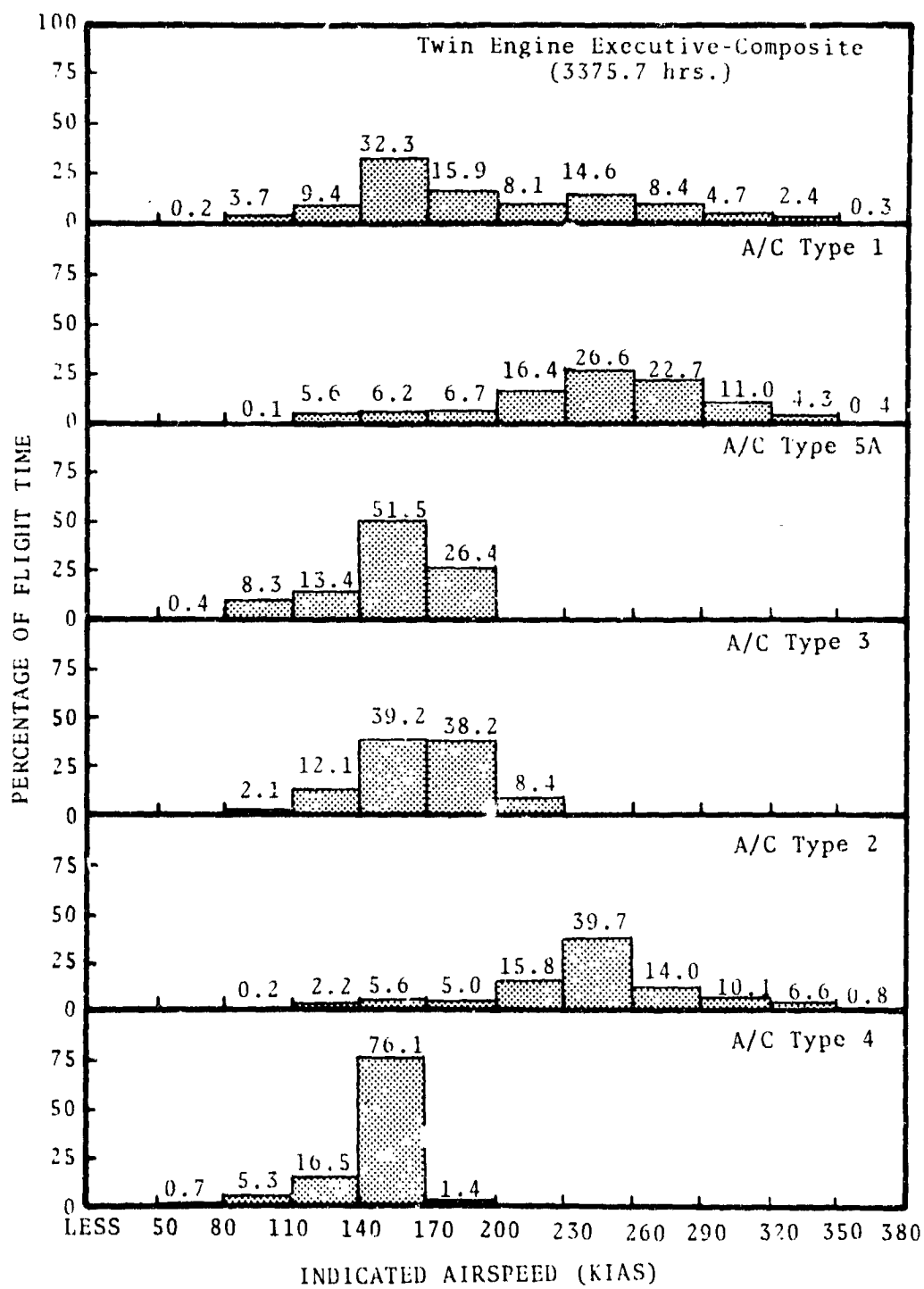


Figure 44. Percentage of Time in Airspeed Ranges for Twin-Engine Executive Category

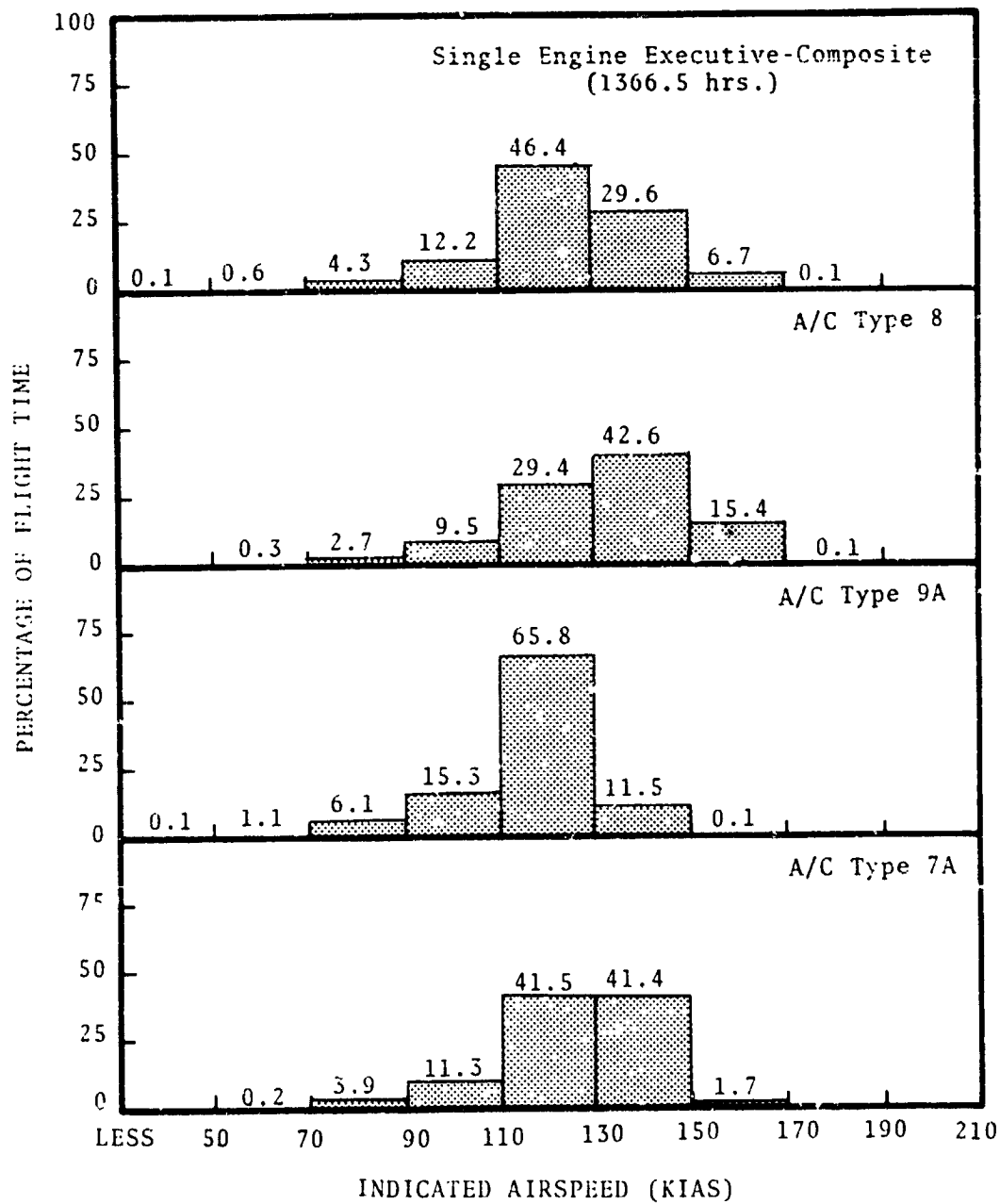


Figure 45. Percentage of Time in Airspeed Ranges for Single-Engine Executive Category

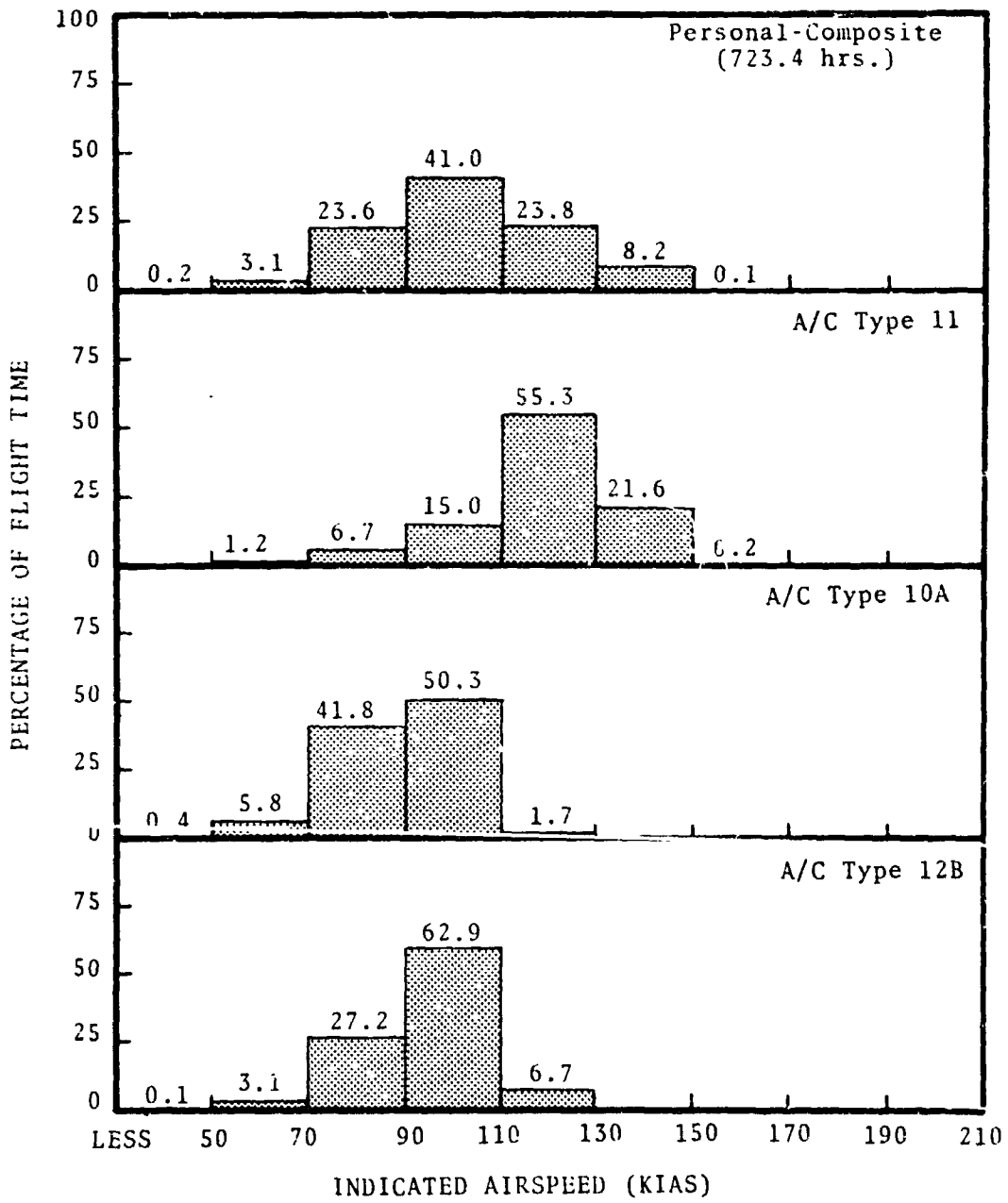


Figure 46. Percentage of Time in Airspeed Ranges for Personal Category

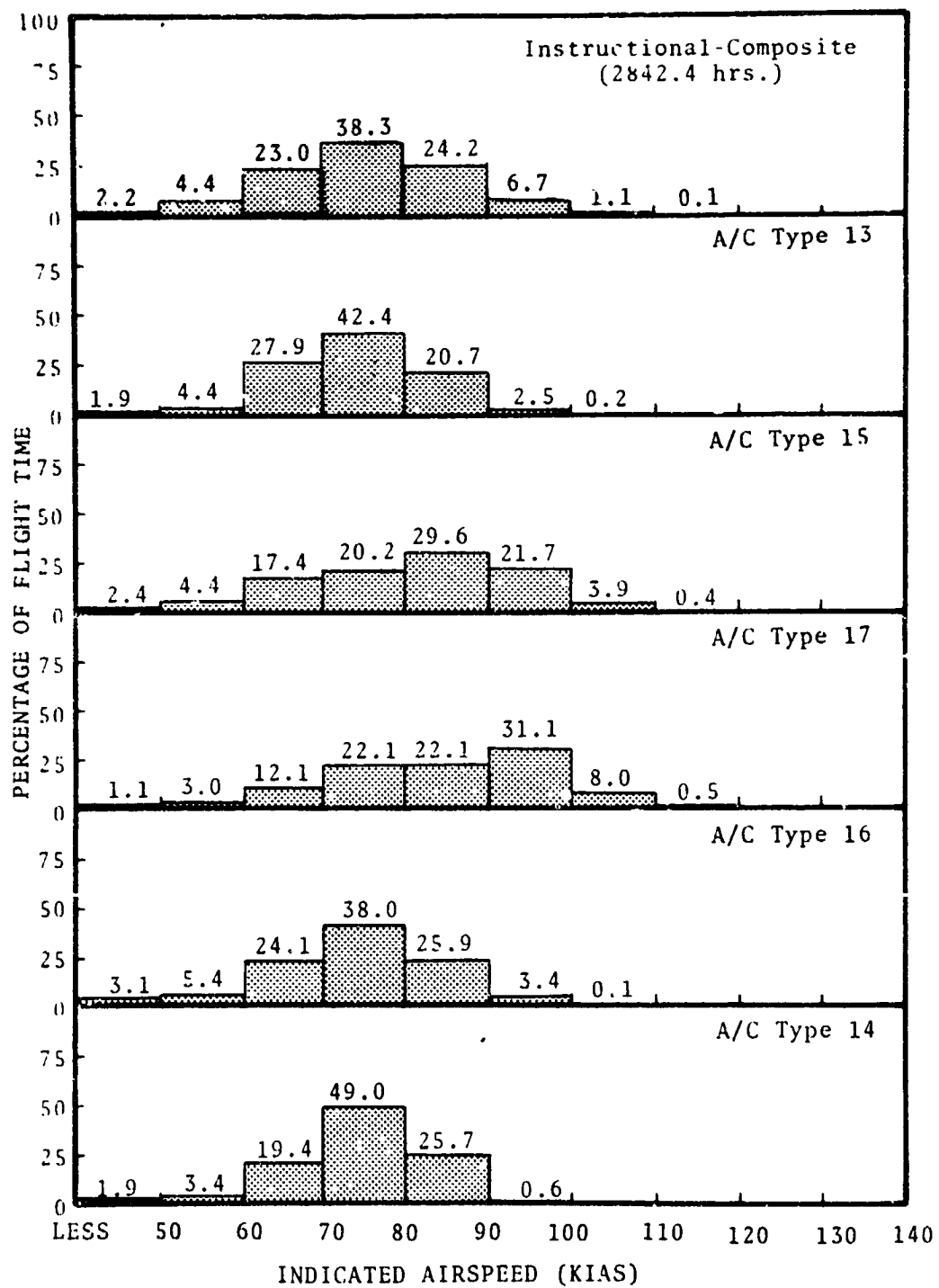


Figure 47. Percentage of Time in Airspeed Ranges for Instructional Category

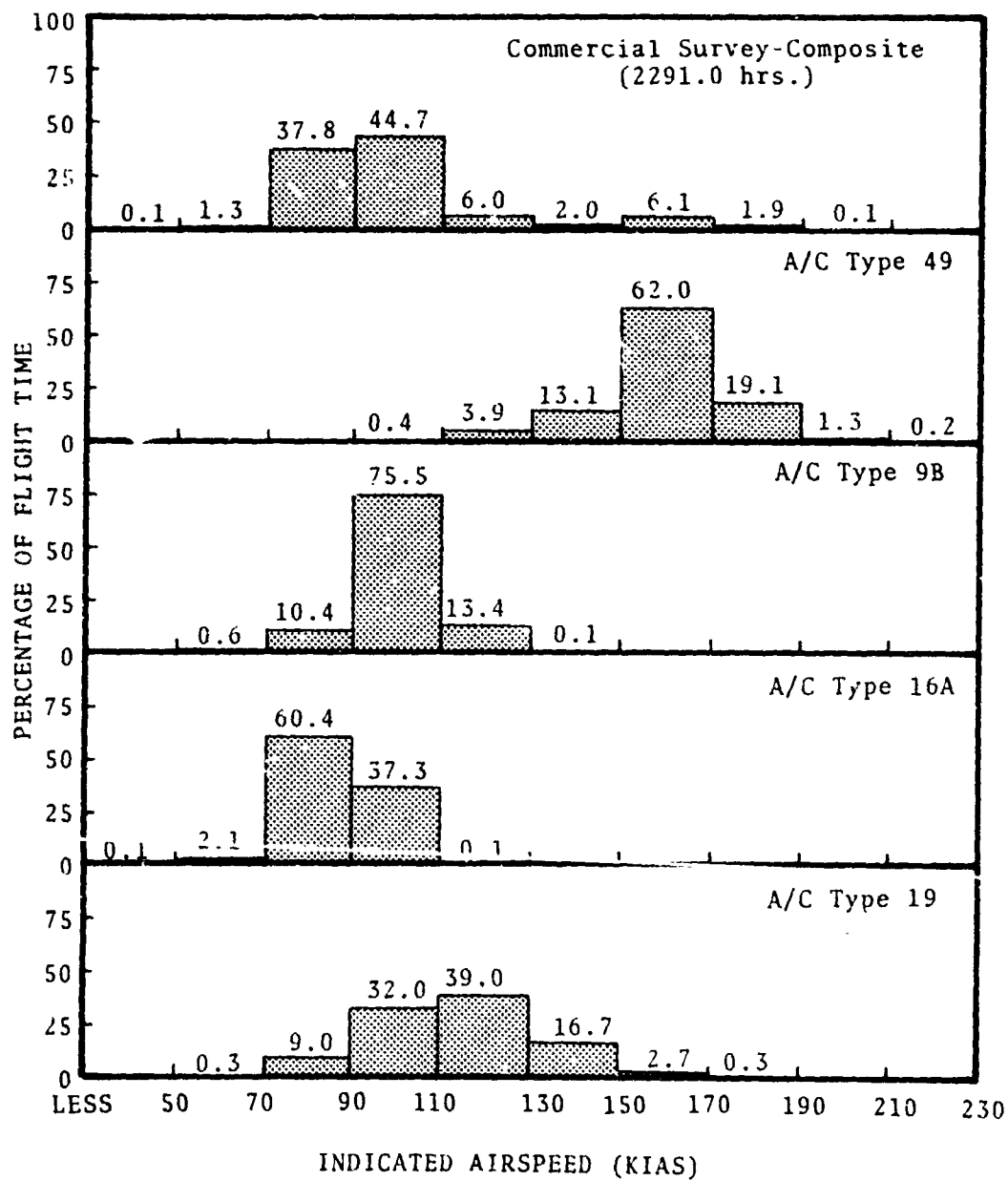


Figure 48. Percentage of Time in Airspeed Ranges for Commercial Survey Category



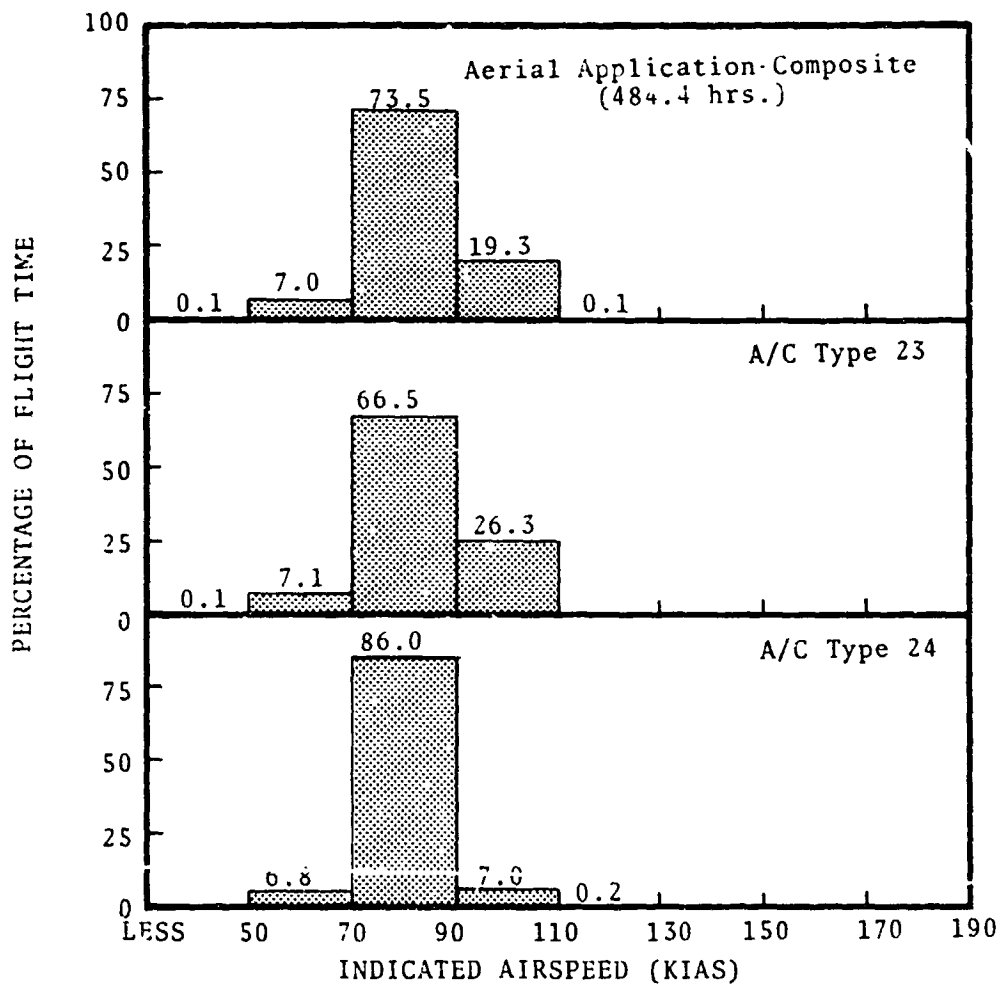


Figure 49. Percentage of Time in Airspeed Ranges for Aerial Application Category

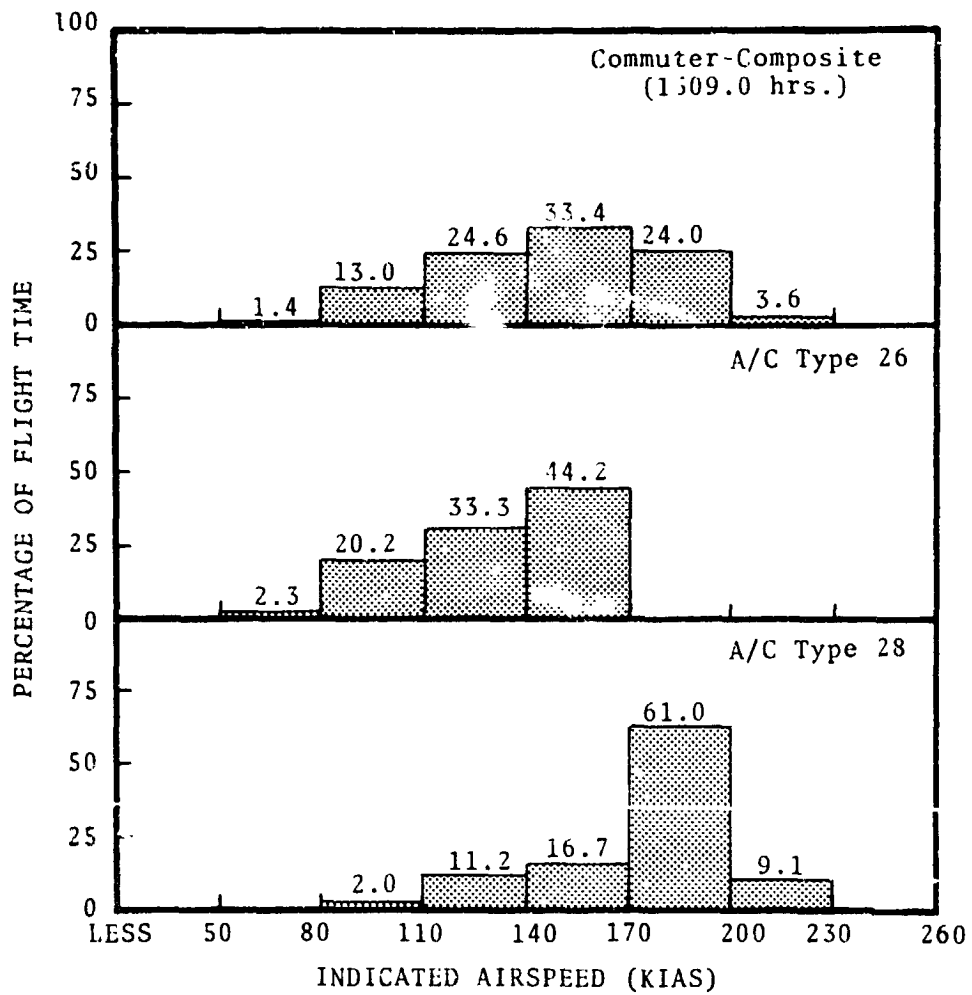


Figure 50. Percentage of Time in Airspeed Ranges for Commuter Category

### 3. CONCLUSIONS

On the basis of the number of recorded flight hours, the VGH data sample was adequate for all operational categories except the Aerobatic category. On the basis of the number of records, the VG data sample was inadequate for the Aerobatic, Aerial Application, and Commuter categories. The flight hours in the VG and VGH data could not be compared since the VG recorder registers only extreme values and the number and frequency of coincident peak values are unknown.

The observed data distributions were log-normal in most cases and approximately normal in the rest. The Commercial Survey category had two distinct data distributions, one en-route to and from the operational mission and the other during the mission performance.

The Instructional and Aerial Application categories had the highest probability of exceeding the design positive  $n_z$  limits for maneuver; the Instructional category had the highest probability of exceeding the design negative  $n_z$  limits for maneuver, and the Commercial Survey category had the highest probability of exceeding the design  $n_z$  limits for gust.

The Aerial Application and Instructional categories had the most severe landing impact data since they required 860 and 3393 landings, respectively, to attain  $1.67 \Delta n_z$  while the other categories required more than 19,000 landings to reach this level.

Of the 24 instrumented aircraft types, 17 had airspeeds above  $V_C$ , but none had airspeeds above  $V_D$ . The Personal category had the highest probability of exceeding  $V_C$ ; the Instructional and Commercial Survey categories had the highest  $V/V_C$  ratios, approximately 1.2; and the Twin-Engine Executive category had the highest  $V/V_D$  ratio, approximately 0.925.

Each of the eight operational categories had a distinct load spectrum which reflected the operational characteristics of the category definition, and the various aircraft types within each operational category generally had loads which conformed closely with the average spectrum. The data for the Twin-Engine Executive category could be analyzed better by separating the data for turbojets from the data for turboprop and piston aircraft. Because of the close similarity in the performance results, the Single-Engine and Personal categories could be combined to simplify the analysis.

#### 4. RECOMMENDATIONS

A statistical method to substantiate the adequacy of the sample size should be determined by periodic reduction and analysis of the data while it is being recorded. Comparison of each analysis to previous analyses should yield information concerning the adequacy of data already recorded.

The V-N data for the constant probability envelopes, such as those shown in Figures 7 through 13, should be refined to assess the design requirements for the high-air-speed, high-acceleration regime.

The landing impact spectra should also be investigated by using sink rates instead of load factors because of the complex dynamic transfer function inherent in the landing gear system.

## REFERENCES

1. Jewel, Joseph W., NASA Aircraft Safety and Operation, Problems Conference, May 4-6, 1971, NASA SP-270.
2. FEDERAL AVIATION REGULATIONS, TITLE 14, Part 23.
3. Taback, Israel, The NACA 0.1-Damped V-G Recorder, NACA TN 2194, 1950.
4. Richardson, Norman R., NACA VGH Recorder, NACA TN 2265, 1951.
5. Press, H., The Application of Statistical Theory of Extreme Values to Gust-Load Problems, NACA Report 991, 1949.
6. Gumbel, E.J., Applied Mathematics Series 33, National Bureau of Standards, Department of Commerce, 1954.
7. Pratt, K.G., and Walker, W.G., A Revised Gust-Load Formula and a Re-evaluation of V-G Data Taken on Civil Transport Airplanes from 1933 to 1950, NACA Report 1206, 1953.