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Technical Note

NASA CR-14155

Film Type SO-168 Radiation Study

Prepared Under

NAS 9-11500

Written by

W. Norman Pierce

January 1972



Photographic Technology Division

National Aeronautics and Space Administration

Manned Spacecraft Center

Houston, Texas

(NASA-CR-141554) FILM TYPE SO-168 RADIATION STUDY (Technicolor Graphic Services, Inc.) 21 p HC \$3.25 CSCL 14E

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N75-15942

Unclas _G3/35_09094 Film Type SO-168 Radiation Study

This Report has been reviewed and is approved.

John R. Brinkmann, Chief Photographic Technology Division

Eugen J. Elmond

Eugene G. Edmonds Technical Manager's Representative

15. So

Noel T. Lamar Technical Monitor

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SECTION I SUMMARY

Under Task Order HT 32 investigations were preformed to determine optimum exposure and processing procedures necessary to partially offset the effect of radiation to which film type SO-168 will be exposed during the Skylab Mission. This task became necessary when it was determined that original predictions of 2 to 3 RADS of radiation to which the film will be exposed were too low, and that levels as high as 3.5 to 4.0 RADS may be incurred, thus reducing image quality below an acceptable level.

Test results provided information that lead to the conclusion that forced processing of type SO-168 film tended to reduce the density range to an unusable level, and that processing to a lower ASA value would provide greater image quality for the user.

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SECTION II

PROCEDURES

In order to establish a procedure for offsetting the degrading effects of radiation to which the type SO-168 film would be exposed, several techniques, such as under-development, under-exposure, or some combination of these two techniques, were considered. Verification of the usefulness of this approach was attempted by means of the initial investigation. The experimental design for the initial investigation is outlined in Table 1. In addition to comparing data acquired at various radiation levels, a comparison was made between film radiated prior to and after exposure.

Indicated exposures were made on the Photographic Technology Division's I-B Sensitometer, Model DM-70-3, using step tablet #772-150. The film was radiated to the stated levels by the Manned Spacecraft Center's High Range Calibration Facility, and processed in ME-4 chemistry on the Houston Fearless Hi-Speed Processor located in the Motion Picture Laboratory. Resultant data is shown by the chart in Table 2.

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Because inappropriate control strips were used during the processing phase of the initial investigation, it was decided

TEST #1

| | Nor | mal Expos | ure | 1 Stop Under Exposure | | | |
|-----------|---------|-----------|---------|-----------------------|----------|----------|--|
| Process | ASA 500 | ASA 320 | ASA 250 | ASA 500 | ASA 320 | ASA 250 | |
| Radiation | | | | | † | | |
| 3.50 | Strip 1 | Strip 4 | Strip 7 | Strip 10 | Strip 13 | Strip 16 | |
| 3.75 | Strip 2 | Strip 5 | Strip 8 | Strip 11 | Strip 14 | Strip 17 | |
| 4.00 | Strip 3 | Strip 6 | Strip 9 | Strip 12 | Strip 15 | Strip 18 | |

Test #1. Film to be exposed to CO₆₀ radiation prior to exposure of step wedges.

TEST #2

| | Nor | mal Exposu | re | 1 Stop Under Exposure | | | |
|----------------------|----------------------------------|----------------------------------|----------------------------------|-------------------------------------|-------------------------------------|-------------------------------------|--|
| Process | ASA 500 | ASA 320 | ASA 250 | ASA 500 | ASA 320 | ASA 250 | |
| Radiation | | | | | · · | | |
| 3.50 3.75 4.00 | Strip 1A Strip 2A Strip 3A | Strip 4A Strip 5A Strip 6A | Strip 7A Strip 8A Strip 9A | Strip 10A Strip 11A Strip 12A | Strip 13A Strip 14A Strip 15A | Strip 16A Strip 17A Strip 18A | |

Test #2. Test film to be exposed to CO_{60} radiation after the exposure of step tablets.

Normal Exposure:

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Process:

I-B Sensitometer 2850^{°K} 1/100 second 5500 filter

ME-4 chemistry Temperature - 98°F TN-72-2 6/20 J

Table 2. Results of Initial Investigation

| <u>Sample Number</u> Test 1 - Test 2 | | | Process ASA | Radiation | Dmaz | Dmax | | Dmin | | Maximum Density | |
|---|------|----------|----------------|-----------|------------------------|------|---------------------------------------|----------|-------|-----------------|--|
| | | Exposure | | Level | <u>Test 1 - Test 2</u> | | <u>Test 1 - Test 2</u> | | Range | | |
| | | | - " | | | | · · · · · · · · · · · · · · · · · · · |) | | | |
| 1 1 | lA | 1/100 | 500 | 3.50 | 0.55 | 0.52 | 0.10 | 0.10 | 0.45 | 0,42 | |
| 2 | 2A | 1/100 | 500 | 3.75 | 0.50 | 0.48 | 0.10 | 0.10 | 0.40 | 0.38 | |
| 3 | - 3A | 1/100 | 500 | 4.00 | 0.46 | 0.47 | 0.10 | 0.10 | 0,30 | 0.37 | |
| 4 | 4A | 1/100 | 320 | 3.50 | 0.65 | 0.64 | 0.10 | 0.10 | 0.55 | 0.54 | |
| 5 | 5A | 1/100 | 320 | 3.75 | | 0.56 | · | 0.10 | | 0.46 | |
| 6 | 6A | 1/100 | 320 | 4.00 | 0.54 | 0.55 | 0.10 | 0.10 | 0.44 | 0.45 | |
| 7 | 7A | 1/100 | 250 | 3.50 | 1.30 | 1.28 | 0.15 | 0.15 | 1.15 | 1.13 | |
| 8 | A8 | 1/100 | 250 | 3.75 | 1.24 | 1.18 | 0.16 | 0.15 | 1.08 | 1.03 | |
| 9 | 9A | 1/100 | 250 | 4,00 | 1.20 | 1.14 | 0.16 | 0.15 | 1.04 | 0.99 | |
| 10 | 10A | 1/200 | 500 | 3.50 | 0.54 | 0.52 | 0.12 | 0.12 | 0.42 | 0.40 | |
| 1 11 | 114 | 1/200 | 500 | 3.75 | 0.49 | 0.48 | 0.11 | 0.11 | 0.38 | 0.37 | |
| 12 | 124 | 1/200 | 500 | 4.00 | 0.47 | 0.46 | 0.11 | 0.11 | 0.36 | 0.35 | |
| 13 | 13A | 1/200 | 320 | 3.50 | 0.64 | 0.62 | 0.12 | 0.12 | 0.52 | 0.50 | |
| 14 | | 1/200 | 320 | 3.75 | 0.62 | 0.60 | 0.11 | 0.12 | 0.51 | 0.48 | |
| 15 | 15A | 1/200 | 320 | 4.00 | 0.60 | 0.60 | 0.11 | 0.11 | 0.49 | 0.49 | |
| 16 | 16A | 1/200 | 250 | 3,50 | 1.30 | 1.34 | 0.20 | 0.22 | 1.10 | 1.12 | |
| 17 | 174 | 1/200 | 250 | 3.75 | 1.24 | 1.20 | | 0.21 | · · | 0.99 | |
| 1 18 | 184 | 1/200 | 250 | 4.00 | 1.23 | 1.20 | 0.22 | 0.22 | 1.03 | 0.98 | |

to run a secondary investigation. Although conclusions could be made from the initial investigation, data of an absolute nature was deemed more desirable.

The secondary investigation consisted of using a single exposure time (normal exposure), a single radiation level (4.0 RADS), and three processing conditions to produce ASA values of 500, 320, and 125. Three irradiated strips were processed at each ASA level along with appropriate control strips for a total of twelve strips. The results are shown in Table 3; in addition, the densities and visual curves are included in the appendix of this report.

Quantitative evaluation of the data from the secondary investigation was accomplished as follows. Using the given constraints of camera speed (maximum available 1/60 second), maximum lens aperature (f/2), and illumination level inside the capsule (20 foot candles), a value of maximum intensity falling on the film plane was calculated using the following formula*:

$$I' = \frac{.8}{.4 (f/2)} I$$

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* This formula is for an approximate value only, but it is considered to be sufficiently accurate for the purposes of this investigation.

| | | | | • | · · · · · | | |
|-----------|--------------------|----------------|------------------|------------------|-------------------------|----------------------------|--|
| Exposure | Radiation Level | Process ASA | Averaged Dmax | Averaged Dmin | Averaged Dens. Range | Calculated* Dens. Range | |
| 1/100 sec | 4.0 | 125 | 1.22 | 0.15 | 1.07 | 0.64 | |
| 1/100 sec | 4.0 | 320 | 0.83 | 0.13 | 0.70 | 0.40 | |
| 1/100 sec | 4.0 | 500 | 0.62 | 0.12 | 0.50 | 0,30 | |

Table 3. Results of Secondary Investigation

* These results are based on the calculations to determine an approximate value for the maximum exposure level to be received on the film and an assumed scene brightness range of 20:1.

where

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I' = intensity falling on film plane
f/ = lens aperature
I = illumination intensity

The result was that the log E point of 2.255 on the relative log E scale was determined as the maximum exposure level capable of being received on the film under these conditions. Actual exposure values will undoubtedly be less than this value since it is primarily reflected light that is being recorded. An arbitrary scene brightness range of 20:1 was selected in order that a maximum density range for each processing condition could be calculated. The resultant calculated density range is also shown in Table 3.

SECTION III RECOMMENDATIONS AND CONCLUSIONS

The results of the initial investigation indicated that forced processing of type SO-168 film to ASA 500 tended to reduce the density range to an unusable level when the film receives between 3.5 and 4.0 RADS of radiation. The data goes on to indicate a 50% drop in Dmax and 60% drop in usable density range when the film is forced processed as compared to when it is processed to ASA 250. Under the same conditions, the maximum density range dropped over The initial investigation also indicated there is 60%. no appreciable difference between the film being irradiated prior to or after exposure. The results of the secondary investigation verified those achieved during the initial investigation. All this leads to the basic conclusion that processing type SO-168 film to a lower ASA value will give more usable results. Usability in this particular instance means that which will produce results with the greatest amount of information rather than that which is of subjectively better quality. It also must be considered that the end use of this film is as an original printing master to produce third and second generation copies for the intended investigators.

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Because of the 50^d increase in density range achieved, processing to lower ASA values must be considered significant and the most feasible approach to reducing the effects of the radiation levels to which this film will likely be exposed.

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APPENDIX



Table 4. List of Calculations

$$f/ = f/2$$

$$I = 20 \text{ foot candles} = 215.280 \text{ meter candles}$$

$$t = 1/60 \text{ second}$$

$$I' = \frac{.8}{.4 \text{ f}^2} I$$

$$I = .72 \text{ meter candle seconds}$$

$$\log I = 9.233^{-10} = \text{maximum intensity falling on film plane}$$

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