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SPACE SHUTTLE LAUNCH VEHICLE PERFORMANCE TRAJECTORY, EXCHANGE RATIOS, AND DISPERSION ANALYSIS

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TABLE OF CONTENTS

	Page
SUMMARY	1
INTRODUCTION	1
SECTION I	
NOMINAL LAUNCH VEHICLE PARAMETERS AND BASELINE TRAJECTORY	3
SECTION II	
EXCHANGE RATIOS	53
SECTION III	
DESIGN ENVIRONMENT AND FLIGHT PERFORMANCE RESERVES	75
CONCLUSION	93
RECOMMENDATION	93
REFERENCES	94

DEFINITION OF ABBREVIATIONS

AOA	Abort-Once-Around
A _Z	Azimuth
ET	External Tank
FPR	Flight Performance Reserve Propellants
fps	feet per second
g	gravity
in ²	square inches
I _{sp}	Specific Impulse
lb	pounds
MECO	Orbital Main Engine Cutoff
n. mi.	Nautical Miles
OMS	Orbital Maneuvering System
P ₁	Payload
RCS	Reaction Control System
RI/SD	Rockwell International/Space Division
RSS	Root Sum Squared
RTLS	Return To Launch Site
s	seconds
SRB	Solid Rocket Booster
SSLV	Space Shuttle Launch Vehicle
SSME(s)	Space Shuttle Main Engine(s)
WTR	Western Test Range
Δ	change from baseline
3-DOF	Three Degree Of Freedom
°	degrees of temperature
γ	flight path angle
V _R	Earth Relative Velocity
WT	Weight
W̄	Weight Flow Rate

TECHNICAL MEMORANDUM X- 64918

SPACE SHUTTLE LAUNCH VEHICLE PERFORMANCE TRAJECTORY, EXCHANGE
RATIOS, AND DISPERSION ANALYSIS

SUMMARY

A baseline Space Shuttle Trajectory for Mission 3A launched from WTR has been generated. Design constraints of maximum dynamic pressure, longitudinal acceleration, and delivered payload were satisfied. Payload exchange ratios for use in rapid tradeoff studies were generated and presented. A detailed dispersion analysis simulating vehicle parameters at their $\pm 3\sigma$ values was performed to define design envelopes of dynamic pressure, SRB staging point, aerodynamic stagnation point heating, and flight performance reserves. Optimum fuel bias quantity was calculated.

INTRODUCTION

The Space Shuttle Program has reached a phase where all major system elements have been contracted. Each contractor has evaluated the requirements and replied with a definition of operation of his particular element.

These data have been assembled to define a launch vehicle that will perform the mission requirements. A detailed evaluation and study of these data have been performed. This report contains the baseline vehicle definition, Mission 3A baseline performance trajectory, payload exchange ratios, dispersion analysis with design environment envelopes, and a definition of flight performance reserve propellants.

SECTION I

NOMINAL LAUNCH VEHICLE PARAMETERS AND BASELINE TRAJECTORY

A. Discussion

The Space Shuttle Launch Vehicle (SSLV) has been sized under Level I groundrules (Reference 1) for a flight labeled Mission 3A. This has been ascertained through various studies as the most payload critical mission defined in Reference 1. This mission is a single revolution payload delivery flight launched from Western Test Range (WTR) into a 50 X 100 n. mi. orbit inclined at 104° with respect to the equatorial plane. The requirement of 'orbiter intact abort' sizes the propulsion system for an Abort-Once-Around (AOA) flight caused by Space Shuttle Main Engine (SSME) failure. The current abort requirement provides safe landing in the vicinity of the launch site following a SSME failure.

The Shuttle powered flight is divided into three phases, each of which requires a different response to an abort situation. The first phase is from liftoff through Solid Rocket Booster (SRB) burn-out and staging, and into the orbiter/ET flight. During this phase, if a failure causing an abort occurs, the SSLV executes a powered turn around maneuver, initiated after SRB staging, and flies back to the launch site. The latest time that this maneuver can be executed, and thus the terminal time of this first phase, is designated the last Return To Launch Site (RTLS), first AOA interface. Beyond this time the downrange energy is too great to be cancelled, and a second phase of flight is in effect. If a SSME failure occurs in this phase the SSLV is targeted to the AOA Main Engine Cutoff (MECO) conditions stated in Table I.1. Following MECO the Orbital Maneuvering System (OMS) is fired to place the orbiter on a conic from which safe entry and landing may occur. A third and final phase occurs when the powered flight nears the nominal targeting conditions of Table I.1. If a SSME failure occurs during this phase, the remaining orbiter engines are burned to the Nominal targeting conditions and a post MECO OMS burn is used to place the orbiter into the required 50 X 100 n. mi. orbit. The MECO target conditions are such that the ET is on an earth impacting conic required for safe ET disposal.

B. Description of Launch Vehicle

The SSLV has been sized by the prime contractor, Rockwell International/Space Division (RI/SD), and the component weight and mass data used for this study are contained in Reference 2 and displayed in Table I.2. A management requirement of 7000 pounds payload growth margin at the time when this sizing exercise was performed was implemented. A sketch of the launch vehicle is displayed in Figure I.1. The aerodynamic

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data was obtained from Reference 3. The forebody axial force coefficient vs Mach Number and base force vs altitude curves are displayed in Figures I.2 and I.3 respectively. The Solid Rocket Booster vacuum thrust and weight flow rate profiles produced by Thiokol Chemical Corporation and designated as TC-207-1, are displayed in Figure I.4. Values of vacuum thrust and specific impulse for the SSME, OMS, and aft firing RCS engines are presented in Table I.3.

The ascent trajectory for Mission 3A was simulated using the following groundrules:

1. Launch from WTR, latitude = 35° , West Longitude = 120.5°
2. Payload weight = 32,000 lbs. (exclusive of 7000 lb payload growth margin)
3. Orbit inclination = 104° .
4. 1971 Vandenberg Reference Atmosphere simulated (Reference 4).
5. Maximum dynamic pressure on nominal trajectory \leq 650 psf.
6. Vehicle erected on launch pad with tail fin pointing due south, $A_2 = 180^{\circ}$). Roll program ($^{\circ}/\text{Sec}$) began at 6 seconds flight until azimuth = 198.55° as required for coplanar flight.
7. Booster open loop pitch attitude profile selected to maximize payload while limiting loads in region of maximum dynamic pressure.
8. Optimum guidance initiated at SRB staging and is in effect until MECO.
9. Thrust vector control supplied by SRB's from liftoff to beginning of thrust decay at which time orbiter engines assume control until cutoff.
10. Orbiter main engine throttle set at 109% from liftoff to AOA MECO or 100% from RTLS to Nominal MECO except for throttling as required to maintain longitudinal acceleration limit of 3g's.
11. Last RTLS time equals earliest AOA time ($V_R = 8932 \text{ fps}$)
12. Trajectory shaped for earliest AOA (Table I.1 for targeting) with orbiter engine #1 failure. Nominal trajectory simulation started at RTLS/AOA point and targeted to nominal MECO target (Table I.1).

13. OMS propellant loading of 250 fps ΔV in excess of 50 X 100 n. mi. reference orbit and RCS loading of 100 fps on orbit translational ΔV respectively (Reference 1) are assumed.

14. OMS and aft firing RCS engines burned in parallel with orbiter main engines during AOA burn after engine failure. The duration is limited such that sufficient propellants are available to perform the post MECO maneuvers.

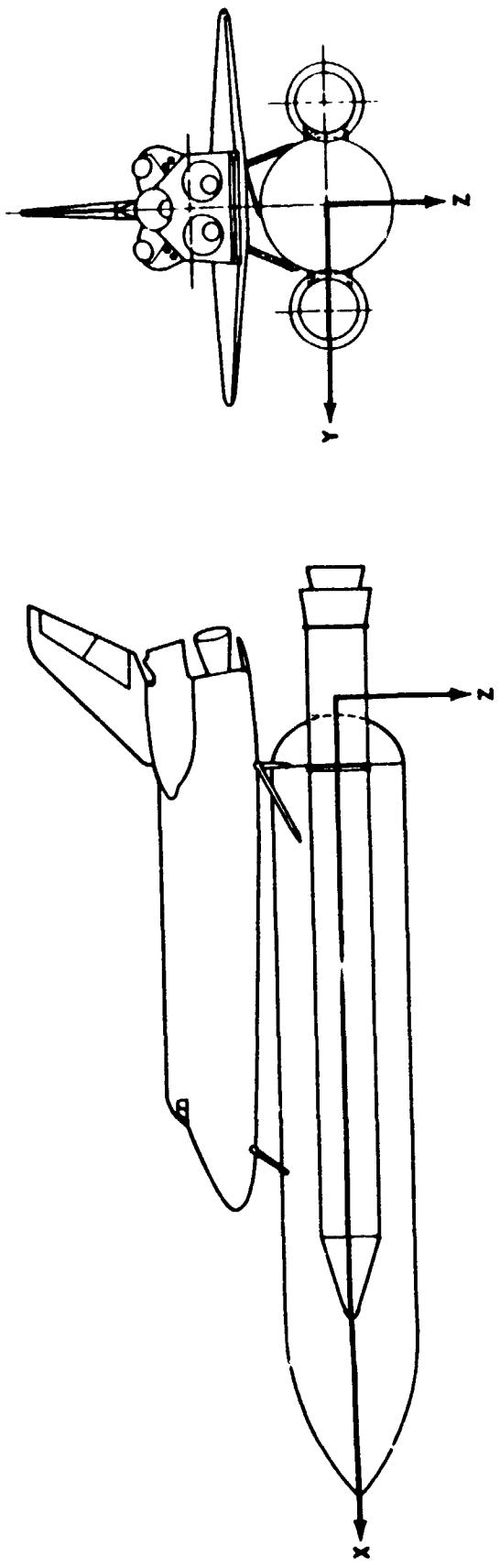
C. Trajectory Results

A sequence of events and resulting trajectory weight statement for both AOA and Nominal MECO conditions are contained in Table I.4.

Plots of dynamic pressure versus time and longitudinal acceleration versus time are displayed in Figures I.5, and I.6, respectively. A plot of stagnation point heating (Referenced to a one foot sphere) is displayed in Figure I.7.

Table I.5 is a definition of symbols of the trajectory tables. The detailed printout of the trajectory simulation from liftoff to AOA MECO is presented in Tables I.6 through I.13. Printout of the trajectory simulation from the RTLS/AOA point to Nominal MECO is presented in Tables I.14 through I.21.

FIGURE 1-1 SHUTTLE LAUNCH VEHICLE AND BODY COORDINATE SYSTEM



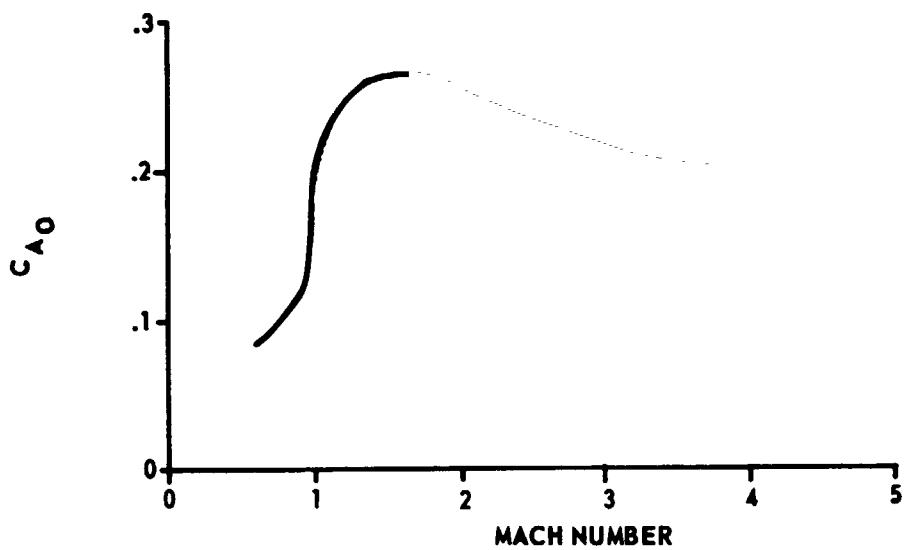


FIGURE 1.2 FOREBODY AXIAL FORCE COEFFICIENT (C_{A0}) VERSUS MACH NUMBER

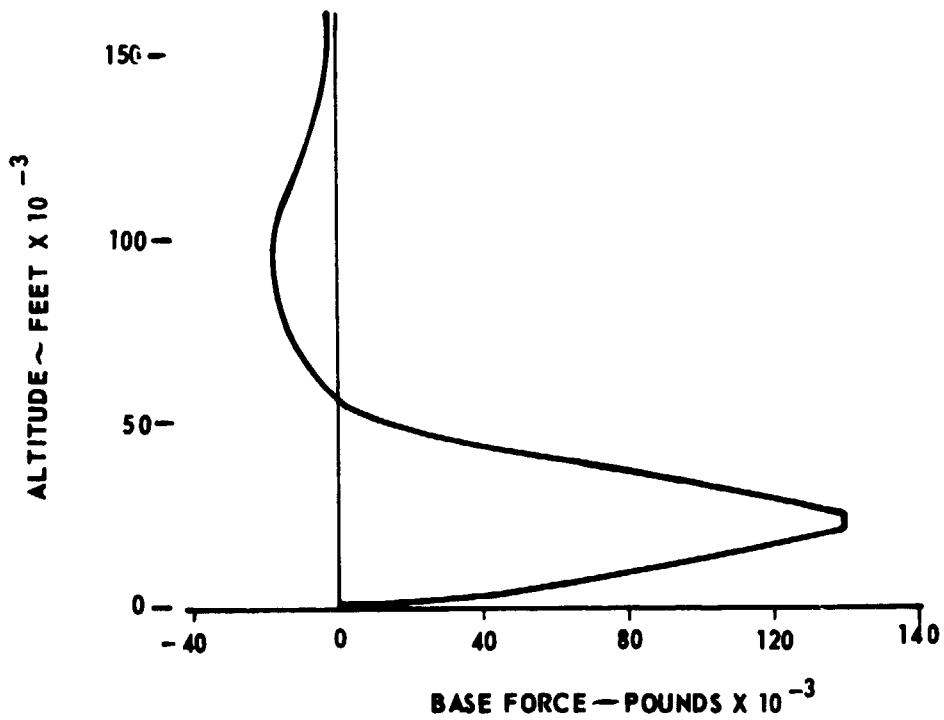


FIGURE 1.3 ALTITUDE VERSUS POWER ON BASE FORCE

FIGURE 1.4 SRB VACUUM THRUST AND PROPELLANT WEIGHT FLOWRATE VERSUS TIME

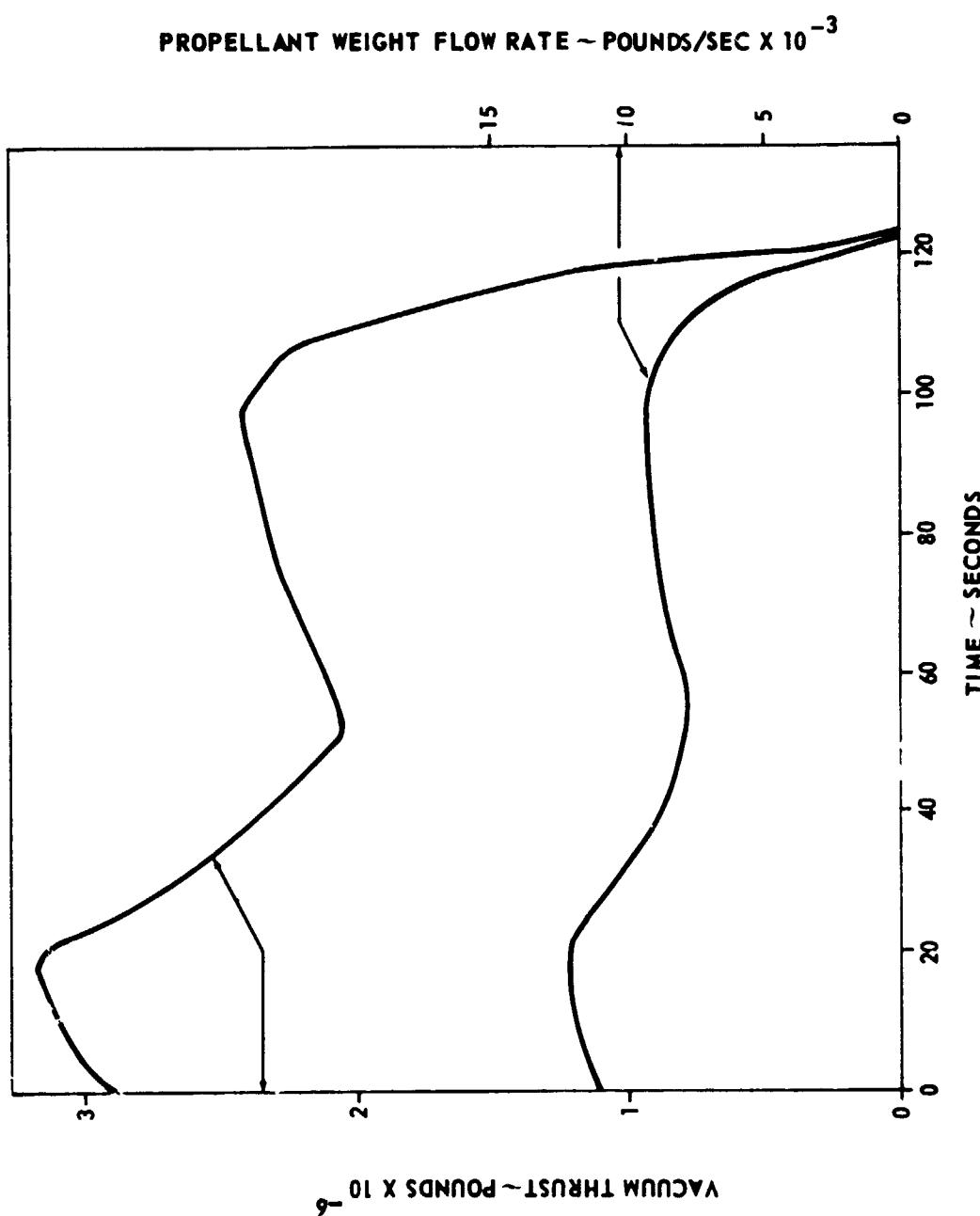


TABLE I.1
MECO TARGETS - MISSION 3A

AOA Trajectory

Altitude	= 55 n. mi. *
Inertial Velocity	= 25,317 fps
Inertial Flight Path Angle	= .75°
Inclination	= 104°

Nominal Trajectory

Altitude	= 60 n. mi. *
Inertial Velocity	= 25,383 fps
Inertial Flight Path Angle	= .5°

* above equatorial radius

TABLE I.2

SHUTTLE COMPONENT WEIGHT AND CENTER OF GRAVITY DATA - MISSION 3A

		32000 lb
Payload		2636
Personnel		156000
Inert Wet Orbiter		3915
Usable RCS Propellant		12978
External Tank (WET)		75000
External Tank Propellant		1555338
Capacity Incl FPR and Fuel Bias		350380
SRB Inert Staging Weight		2202400
SRB Propellants Incl Inerts		4390647
Gross Liftoff Weight at T/W = 1.5		
 Center of Gravity		
Weight lb		XCG* (in)
		ZCG* (in)
S	4400000	-448.0
T	4368500	-449.2
A	3615100	-454.1
G	2957400	-415.8
E	1911000	-279.4
	1791600	-266.3
1		
S	1428000	-122.0
T	973400	-244.5
A	601700	-412.9
G	301300	-756.9
E		
2	YCG* = 0	

* See Figure I.1

TABLE I.3
ORBITER LIQUID ENGINE PROPULSION PARAMETERS

I Space Shuttle Main Engine (3)

Vacuum Thrust at 100% Power Level = 470000 lb
Vacuum Isp at 100% Power Level = 455.2 s
 at 109% Power Level = 455.3 s
Exit Area = 6471 in²/Engine

Throttle range of 109% to 50% Nominal Power Level

II Orbital Maneuvering System (2)

Vacuum Thrust = 6000 lb
Vacuum Isp = 313.2 s

III Reaction Control System (4) (aft firing)

Vacuum Thrust = 875 lb
Vacuum Isp = 289 s

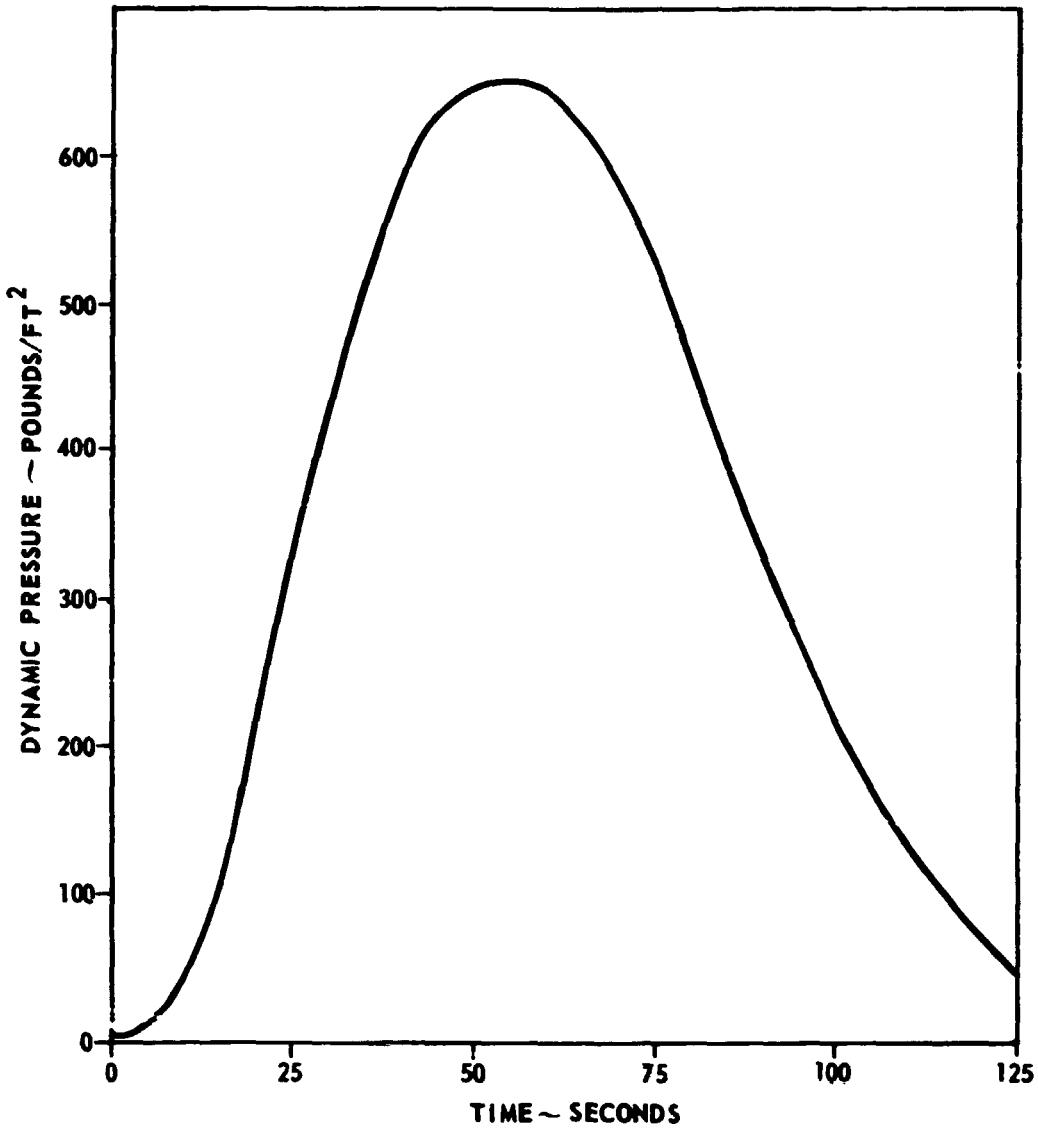


FIGURE 1.5 DYNAMIC PRESSURE VERSUS TIME

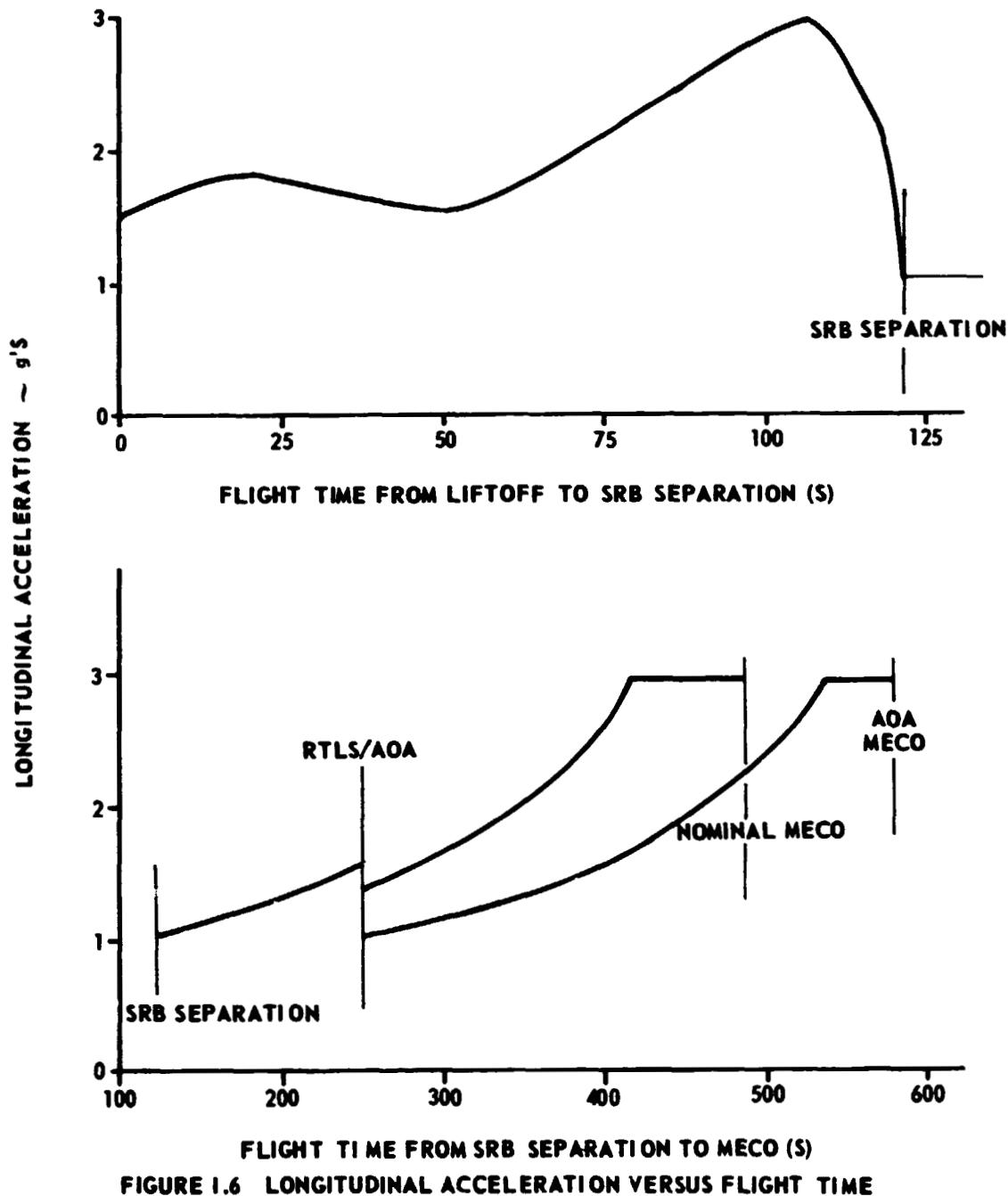


FIGURE I.6 LONGITUDINAL ACCELERATION VERSUS FLIGHT TIME

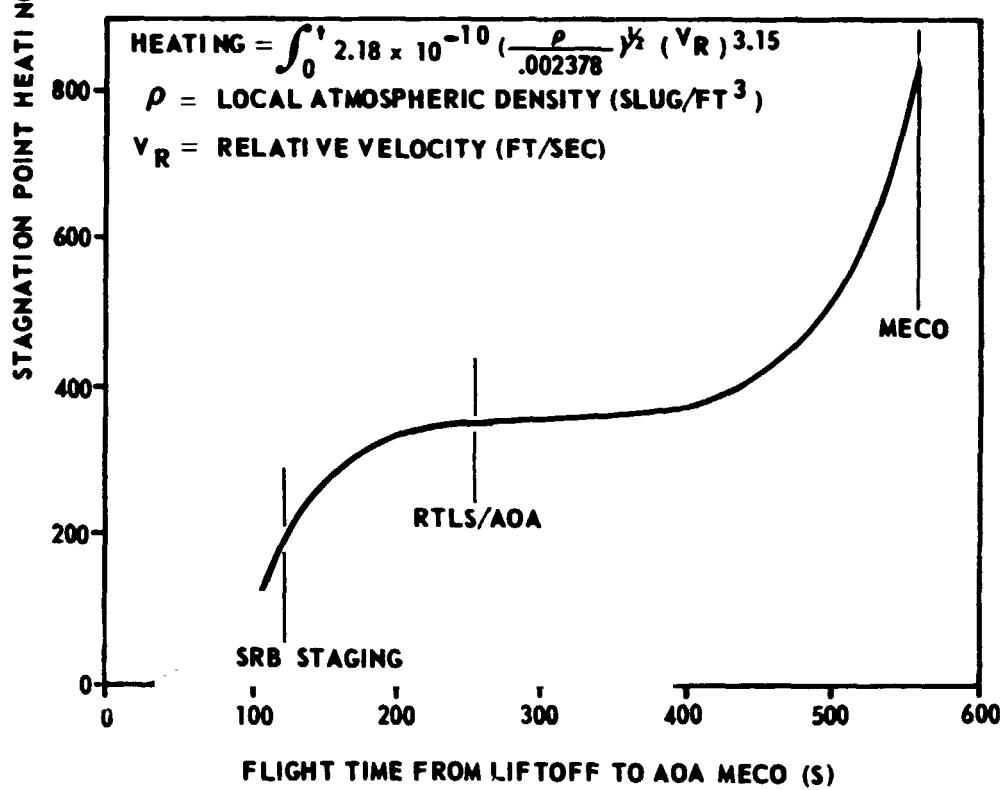
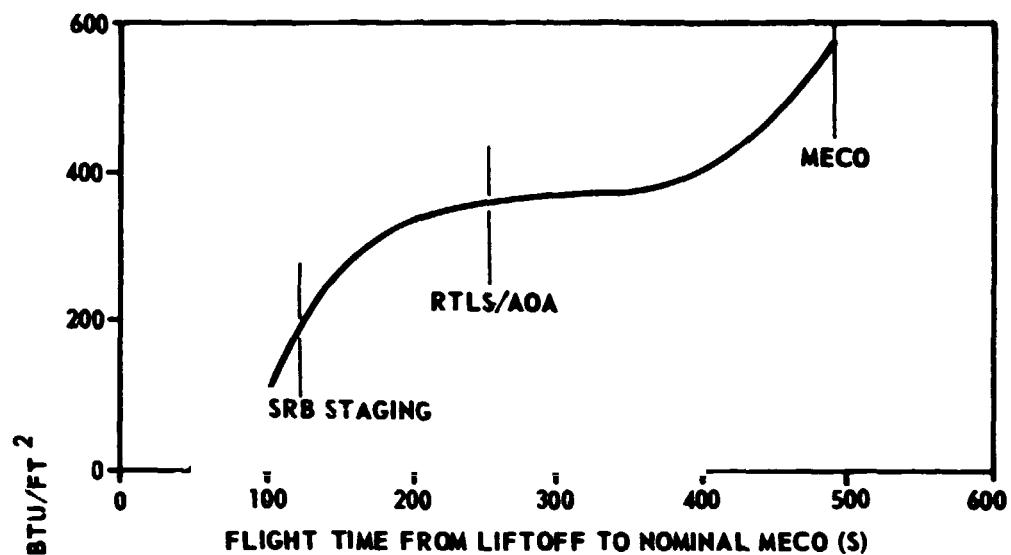


FIGURE 1.7 STAGNATION POINT HEATING VERSUS FLIGHT TIME

TABLE I.4
TIMED SEQUENCE OF EVENTS WITH CORRESPONDING WEIGHT HISTORY

AOA Trajectory

<u>TIME (s)</u>	<u>EVENT</u>	<u>VEHICLE WT</u>
0	Liftoff	4390647 lb
6	Initiate Tilt and Roll Attitude Program	4233432
7.86	Terminate Roll Maneuver	4183779
45.94	Mach Number = 1	3251833
54.49	Max Dynamic Pressure = 650 psf	3082478
107.50	Max SRB Longitudinal Acceleration	
	Orbiter Engines Assume Thrust Vector Control	1979738
121.42	SRB Staging	1778393
	Initiate Closed Loop Guidance	1428013
253.04	Common RTLS/AOA Point	
	Engine #1 Failed/Ignite OMS & RCS	983719
286.81	RCS Cutoff	905960
342.12	OMS Cutoff	779372
536.68	Max Longitudinal Acceleration - Throttle	341533
558.71	AOA MECO	295395
	ET Propellants Consumed for AOA Trajectory	1538597

Nominal Mission

253.04	Common RTLS/AOA Point	983719
418.89	Max Longitudinal Acceleration - Throttle	470000
485.23	Nominal Mission MECO	303576
	ET Propellants consumed for Nominal Trajectory	1534298

DEFINITIONS AND SYMBOLS FOR TRAJECTORY TABLES

TABLE NO. I.5

<u>SYMBOL</u>	<u>UNITS</u>	<u>DEFINITION</u>
TIME	SECONDS	INSTANTANEOUS TIME FROM LIFTOFF
R	FEET	INSTANTANEOUS RADIUS FROM CENTER OF EARTH
VI	FT/SEC	INERTIAL VELOCITY
GAMMA I	DEGREES	INERTIAL FLIGHT PATH ANGLE
LAT-GD	DEGREES	GEODETIC LATITUDE
LONG	DEGREES	RELATIVE LONGITUDE
AZI	DEGREES	INERTIAL AZIMUTH (ANGULAR MEASUREMENT OF VI IN LOCAL HORIZONTAL PLANE)
ALT	FEET	INSTANTANEOUS ALTITUDE ABOVE REFERENCE ELLIPSOID
INC	DEGREES	INSTANTANEOUS INCLINATION
NODE	DEGREES	ANGULAR MEASUREMENT OF THE DESCENDING NODE FROM THE LAUNCH MERIDIAN
GAMMAR	DEGREES	RELATIVE FLIGHT PATH ANGLE
AZR	DEGREES	RELATIVE AZIMUTH ANGLE
MACH		MACH NUMBER

DEFINITIONS AND SYMBOLS FOR TRAJECTORY TABLES (Continued)

TABLE NO. I.5

<u>SYMBOL</u>	<u>UNITS</u>	<u>DEFINITION</u>
Q	LB/FT**2	DYNAMIC PRESSURE
ALPHA	DEGREES	ANGLE OF ATTACK MEASURED IN VEHICLE PITCH PLANE
BETA	DEGREES	SIDESLIP ANGLE (LATERAL ANGLE OF ATTACK)
QALPHA	LB*DEG/FT**2	PRODUCT OF Q AND ALPHA
QBETA	LB*DEG/FT**2	PRODUCT OF Q AND BETA
THRUST	POUNDS	INSTANTANEOUS THRUST
WEIGHT	POUNDS	INSTANTANEOUS WEIGHT
AXIAL FORCE	POUNDS	AERODYNAMIC AXIAL FORCE
NORMAL FORCE	POUNDS	AERODYNAMIC NORMAL FORCE
SIDE FORCE	POUNDS	AERODYNAMIC SIDE FORCE
LONG ACC	G'S	LONGITUDINAL ACCELERATION
NORMAL ACC	G'S	NORMAL ACCELERATION
CHIR	DEGREES	INERTIAL ROLL ATTITUDE ANGLE
CHIP	DEGREES	INERTIAL PITCH ATTITUDE ANGLE
CHIY	DEGREES	INERTIAL YAW ATTITUDE ANGLE
DELRC	DEGREES	ROLL THRUST GIMBAL COMMAND

DEFINITION AND SYMBOLS FOR TRAJECTORY TABLES (Continued)

TABLE NO. I.5

<u>SYMBOL</u>	<u>UNITS</u>	<u>DEFINITION</u>
DELPC	DEGREES	PITCH THRUST GIMBAL COMMAND
DELYC	DEGREES	YAW THRUST GIMBAL COMMAND
RANGE	NAUT MILES	RELATIVE SURFACE RANGE FROM INSTANTANEOUS LAUNCH POINT TO THE SUBVEHICLE POINT
RANGE ANGLE	DEGREES	RELATIVE RANGE ANGLE
IIP LAT	DEGREES	INSTANTANEOUS IMPACT POINT LATITUDE
IIP LONG	DEGREES	INSTANTANEOUS IMPACT POINT LONGITUDE
VCH	FT/SEC	CHARACTERISTIC VELOCITY
VIDEAL	FT/SEC	IDEAL VELOCITY
X	FEET	SHUTTLE COORDINATE SYSTEM NO 8 X POSITION
Y	FEET	SHUTTLE COORDINATE SYSTEM NO 8 Y POSITION
Z	FEET	SHUTTLE COORDINATE SYSTEM NO 8 Z POSITION
XDOT	FT/SEC	SHUTTLE COORDINATE SYSTEM NO 8 X VELOCITY
YDOT	FT/SEC	SHUTTLE COORDINATE SYSTEM NO 8 Y VELOCITY
ZDOT	FT/SEC	SHUTTLE COORDINATE SYSTEM NO 8 Z VELOCITY
XACC	FT/SEC**2	SHUTTLE COORDINATE SYSTEM NO 8 X ACCELERATION

DEFINITION AND SYMBOLS FOR TRAJECTORY TABLES (Continued)

TABLE NO. I.5

<u>SYMBOL</u>	<u>UNITS</u>	<u>DEFINITION</u>
YACC	FT/SEC**2	SHUTTLE COORDINATE SYSTEM NO 8 Y ACCELERATION
ZACC	FT/SEC**2	SHUTTLE COORDINATE SYSTEM NO 8 Z ACCELERATION
HEAT	BTU/FT**2	STAGNATION POINT HEATING INDICATOR
HEAT RATE	BTU/FT**2/S	STAGNATION POINT HEATING RATE

SA-1/EL-24

MISSION=3A/MCR=500/LIFTOFF TO AOA MECO/

CASE 1

TIME SEC	R FT	V FT/SEC	VI	LAT-60 DEG	LONG DEG	GAMMA DEG
LIFT-OFF 0.000	20902727.0	1251.343	-0.000	35.000	-120.500	90.000
4.000	20902661.0	1253.215	3.159	35.000	-120.500	90.008
BEGIN ROLL 6.000	20903038.0	1255.882	4.912	35.000	-120.500	90.016
BEGIN TILT 6.000	20903038.0	1255.882	4.912	35.000	-120.500	90.016
END ROLL 7.655	20903272.0	1259.414	6.613	35.000	-120.500	90.051
8.000	20903293.0	1259.718	6.749	35.000	-120.500	90.056
12.000	20904057.0	1270.326	10.668	35.000	-120.500	90.180
16.000	20905185.7	1286.184	14.896	35.000	-120.500	91.101
17.200	20905710.0	1293.794	16.553	35.000	-120.500	91.491
17.500	20905710.0	1293.794	16.553	35.000	-120.500	91.491
20.000	20906712.5	1308.618	19.355	34.999	-120.500	92.298
24.000	20908650.7	1335.816	23.564	34.999	-120.501	93.938
28.000	20910974.2	1365.709	27.307	34.998	-120.501	95.946
32.000	20913651.5	1397.128	30.570	34.996	-120.502	98.266
36.000	20916651.0	1430.358	33.449	34.994	-120.503	100.995
40.000	20919952.7	1466.005	36.000	34.991	-120.504	104.107
44.000	20923536.5	1503.280	38.163	34.987	-120.505	107.599
45.935	20925362.2	1521.281	39.038	34.985	-120.506	109.386
48.000	20927371.7	1540.652	39.864	34.983	-120.507	111.342
52.000	20931427.5	1579.211	41.169	34.978	-120.510	115.123
54.491	20934056.0	1605.870	41.836	34.974	-120.511	118.051
55.500	20935143.7	1617.521	42.077	34.973	-120.512	119.213
55.500	20935143.7	1617.521	42.077	34.973	-120.512	119.213
55.891	20935548.0	1622.194	42.166	34.972	-120.512	119.672
56.000	20935687.2	1623.514	42.191	34.972	-120.512	119.801
60.000	20940154.0	1678.293	42.968	34.965	-120.515	124.810
64.000	20944844.0	1746.919	43.046	34.956	-120.519	130.257
64.000	20944844.0	1746.919	43.046	34.956	-120.522	134.771
67.160	20948718.0	1812.687	43.426	34.949	-120.523	135.991
68.000	2094974.5	1832.070	43.431	34.947	-120.525	138.911
70.000	20952335.2	1881.644	43.576	34.941	-120.525	141.031
70.000	20952335.2	1881.644	43.576	34.941	-120.525	141.031
72.000	20954963.0	1936.202	43.426	34.935	-120.528	147.560
76.000	20960427.2	2060.980	42.849	34.922	-120.533	

MAXIMUM
10 KMS.

14 KMS.

ORIGINAL PAGE IS
OF POOR QUALITY

SA+1/EL=24

MISSION-3A/MCR=500/LIFTOFF TO AOA MECD/

CASE 1

TABLE NO. I.6

TIME SEC	H	V	VI	GAMMA	LONG		LAT-60		AZI	
					FT	FT/SEC	DEG	DEG	DEG	DEG
80.000	20966180.0	2206.960	41.947	34.907	-120.539	-152.966				
84.000	20972232.7	2375.206	40.793	34.890	-120.547	-157.933				
86.000	20978598.2	2566.637	39.464	34.871	-120.555	-162.410				
92.000	20985287.5	2781.835	38.029	34.849	-120.564	-166.389				
96.000	20992312.2	3021.392	36.543	34.824	-120.575	-169.896				
97.500	20995035.2	3117.606	35.983	34.814	-120.579	-171.097				
97.500	20995035.2	3117.606	35.983	34.814	-120.579	-171.097				
100.000	20999682.7	3283.805	35.059	34.796	-120.586	-172.951				
104.000	21007400.2	3561.379	33.627	34.766	-120.599	-175.549				
107.500	21014432.7	3814.931	32.430	34.736	-120.612	-177.505				
107.500	21014432.7	3814.931	32.430	34.736	-120.612	-177.505				
108.000	21015458.0	3851.583	32.262	34.732	-120.614	-177.762				
112.000	21023826.0	4129.702	30.959	34.695	-120.629	-179.545				
116.000	21032423.7	4376.907	29.729	34.654	-120.646	-179.074				
120.000	21041151.2	4562.665	28.595	34.612	-120.664	-178.113				
121.000	21044244.7	4591.878	28.228	34.596	-120.671	-177.918				
121.420	21044244.7	4591.878	28.228	34.596	-120.671	-177.918				
121.420	21044244.7	4591.878	28.228	34.596	-120.671	-177.918				
124.000	21049815.7	4637.672	27.576	34.567	-120.683	-177.658				
140.000	21082933.7	4956.180	23.718	34.379	-120.763	-176.030				
156.000	21113642.5	5328.153	20.275	34.172	-120.850	-174.602				
172.000	21142061.5	5748.886	17.279	33.946	-120.946	-173.356				
186.000	21168337.0	6216.208	14.712	33.698	-121.050	-172.266				
204.000	21192636.5	6729.157	12.537	33.428	-121.164	-171.308				
220.000	21215146.2	7287.760	10.716	33.134	-121.287	-170.444				
236.000	21236074.2	7892.982	9.210	32.815	-121.420	-169.716				
252.000	21255651.5	8547.037	7.976	32.470	-121.563	-169.052				
253.041	21256883.2	8591.555	7.900	32.446	-121.573	-169.011				
268.000	21273135.0	9021.916	6.312	32.100	-121.716	-168.642				
284.000	21287430.0	9514.586	4.801	31.710	-121.876	-168.277				
286.811	21289621.0	9604.541	4.556	31.639	4.556	168.216				
286.811	21289621.0	9604.541	4.556	31.639	4.556	168.216				

ORIGINAL PAGE IS
OF POOR QUALITY

INTERMEDIATE

SA-1/EL-24

MISSION-3A/MCR-500/LIFTOFF TO AOA MECON/

CASE 1

TABLE NO. I.6

TIME SEC	R FT	V1 FT/SEC	GAMMAI DEG	LONG DEG	AZI DEG
300.000	21298664.5	10038.053	3.480	31.298	-167.044
316.000	21306984.2	10596.517	2.338	30.863	-167.221
332.000	21312557.7	11189.003	1.364	30.404	-167.405
342.121	21314748.5	11582.430	0.829	30.101	-167.526
342.121	21314748.5	11582.430	0.629	30.101	-167.526
348.000	21315567.7	11815.074	0.540	29.921	-167.598
364.000	21316186.0	12474.155	0.146	29.410	-166.830
380.000	21314628.7	13173.206	0.697	28.871	-123.011
396.000	21311148.0	13915.249	0.120	28.303	-123.232
412.000	21306028.0	14704.013	-0.421	27.703	-123.463
428.000	21299591.0	15544.075	-0.608	27.069	-123.705
444.000	21292202.7	16441.045	-0.684	26.398	-123.957
460.000	21284263.5	17401.016	-1.652	25.689	-124.221
476.000	21276318.0	18434.950	-1.517	24.938	-124.497
492.000	21268867.2	19551.152	-1.279	24.142	-124.786
508.000	21262589.0	20764.002	-0.939	23.298	-125.069
524.000	21258259.7	22091.020	-0.496	22.399	-125.407
536.683	21256920.2	23239.047	-0.071	21.646	-125.671
540.000	21256806.5	23551.814	0.050	21.443	-125.741
556.000	21259177.0	25060.9C8	0.447	20.424	-126.092
556.712	21260010.2	25316.696	0.751	20.245	-126.153
558.712	21260010.2	25316.696	0.751	20.245	-126.153
558.712	21260010.2	25316.696	0.751	20.245	-126.153

BEGIN GLIMIT

INJECTION

SA-1/LL-24

MISSION-3A/MCR-5JU/LIFTOFF TO AOA MECON/

CASE 1

TABLE NO. I.7

	TIME SEC	ALT FT	INC DEG	VR FT/SEC	NODE DEG	AZR DEG
LIFT-OFF	0.000	0.00	34.819	90.300	-2.179	98.001
BLINN ROLL	4.000	134.10	34.819	90.303	83.853	-166.980
BLINN TILT	6.000	310.45	34.819	89.998	107.533	-164.873
END ROLL	7.655	544.41	34.819	89.944	145.036	-162.867
	8.000	565.53	34.819	89.936	148.041	-162.319
	12.000	1329.15	34.821	89.385	235.330	67.850
	16.000	2457.75	34.834	88.139	331.610	85.599
	17.500	2981.87	34.847	87.462	370.244	84.675
	17.500	2981.87	34.847	87.462	370.204	84.675
	20.000	3984.16	34.885	86.062	436.885	83.077
	24.000	5921.49	35.012	83.226	541.450	80.503
	26.000	8243.71	35.258	79.777	640.593	77.972
	32.000	10919.02	35.667	75.817	734.022	75.477
	36.000	13916.07	36.298	71.354	824.566	72.969
	40.000	17214.53	37.223	66.403	914.614	70.413
	44.000	20744.13	38.496	61.118	1003.204	67.805
MACH ONE	45.935	22617.66	39.236	58.532	1044.529	66.537
	48.000	24624.56	40.109	55.799	1087.831	65.200
	52.000	28674.28	42.075	50.542	1170.991	62.293
W MAXIMUM	54.491	31298.74	43.552	47.177	1225.945	60.892
	55.500	32384.49	44.211	45.799	1249.258	60.189
	55.500	32384.49	44.211	45.799	1249.258	60.189
10 KMS.	55.891	32806.33	44.476	45.264	1258.485	59.915
	56.000	32927.06	44.550	45.115	1261.076	59.839
	60.000	37385.92	47.598	39.605	1363.976	56.999
	64.000	42066.23	51.182	34.212	1482.534	54.157
14 KMS.	67.160	45931.87	54.326	30.150	1588.292	51.945
	68.000	46985.64	55.196	29.109	1618.332	51.365
	70.000	49539.97	57.320	26.703	1693.214	49.998
	70.000	49539.97	57.320	26.703	1693.214	49.998
	72.000	52160.95	59.487	24.410	1777.133	48.655
	76.000	57610.41	63.846	20.196	1946	46.058
						-160.745

MISSION-3A/MCR-500/LIFTOFF TO AOA MECON

CASE 1

TABLE NO. I.7

TIME SEC	ALT FT	INC DEG	VR FT/SEC	AZR DEG	
				NODE DEG	GAMMAR DEG
80.000	63345.92	68.065	16.503	2138.841	43.604
84.000	69379.17	72.011	13.302	2350.213	41.321
86.000	75722.46	75.612	10.541	2581.351	39.196
92.000	92386.44	78.840	8.162	2832.778	37.228
96.000	89382.82	81.701	6.111	3105.192	35.405
97.500	92094.43	82.684	5.416	3212.886	34.759
97.500	92094.43	82.684	5.416	3212.886	34.759
100.000	96721.63	84.203	4.350	3397.074	33.729
104.000	10444.12	86.337	2.865	3700.471	32.207
107.500	11142.75	87.945	1.753	3973.994	30.985
107.500	11142.75	87.945	1.753	3973.994	30.985
108.000	112422.88	88.157	1.607	4013.310	30.816
112.000	120748.61	89.625	.596	4310.355	29.529
116.000	129300.11	90.763	-.186	4572.880	28.337
120.000	137979.14	91.556	-.730	4770.049	27.245
121.420	141054.72	91.701	-.830	4801.724	26.892
121.420	141054.72	91.701	-.830	4801.724	26.692
BEGIN MIINH	141054.72	91.701	-.830	4801.724	26.892
124.000	146592.97	91.933	-.989	4851.620	26.264
140.000	179496.65	93.283	-1.912	5194.179	22.569
156.000	209970.26	94.474	-2.723	5587.408	19.296
172.000	238132.53	95.520	-3.432	6026.631	16.460
186.000	264128.41	96.442	-4.054	6509.987	14.034
204.000	288124.23	97.260	-4.603	7036.869	11.981
220.000	310305.12	97.990	-5.089	7607.644	10.261
236.000	330837.79	98.646	-5.523	8223.568	8.836
252.000	350072.31	99.238	-5.911	8867.112	7.069
253.041	351278.02	99.275	-5.935	8932.215	7.597
INTERMEDIATE	351278.02	99.275	-5.935	8932.215	7.597
268.000	367147.62	99.622	-6.160	9369.018	6.078
284.000	381015.49	99.972	-6.384	9867.071	4.629
286.811	383129.57	100.031	-6.422	9958.845	4.394
286.811	383129.57	100.031	-6.422	9958.845	4.394

ORIGINAL PAGE IS
OF POOR QUALITY

MISSION-3A/MCR-500/LIFTOFF TO AOA MEKO/
SA+I/EL-24

TIME SEC	ALT FT	INC DEG	NODE DEG	VR FT/SEC
300.000	391602.25	100.300	-6.592	10397.678
316.000	399653.49	100.610	-6.785	10960.338
332.000	404736.53	100.902	-6.964	11557.363
342.121	406405.58	101.079	-7.071	11953.457
342.121	406605.58	101.079	-7.071	11953.457
346.000	407233.65	101.178	-7.130	12187.571
364.000	407314.50	101.437	-7.284	12850.437
380.000	405200.97	101.683	-7.427	13552.993
396.000	401137.86	101.918	-7.560	14298.303
412.000	395411.37	102.141	-7.684	15090.131
426.000	386343.02	102.354	-7.800	15933.061
444.000	380298.62	102.558	-7.907	16832.787
460.000	371697.92	102.753	-8.007	17796.162
476.000	363025.24	102.940	-8.100	18831.785
492.000	354842.02	103.120	-8.187	19950.373
508.000	347606.28	103.293	-8.267	21165.518
524.000	342694.54	103.461	-8.342	22494.746
536.683	340617.56	103.590	-8.397	23644.471
540.000	340434.86	103.623	-8.410	23957.472
556.000	341977.67	103.769	-8.470	25468.727
558.712	342669.11	103.793	-8.479	25724.828
558.712	342669.11	103.793	-8.479	25724.828
INJECTION				0.739

CASE I	TABLE NO. I.7
GAMMAR	AZN DEG
	3.360
	2.261
	1.320
	.803
	.803
	.524
	.142
	.677
	.611
	.385
	.189
	.275
	.668
	.778
	.611
	.464
	.611
	.562
	.254
	.921
	.487
	.611
	.669
	.049
	.637
	.620
	.620
	.620
	.620

SA+1/EL=24

MISSION-3A/M.R.=500/LIFTOFF TO AOA MECS/

CASE 1

TABLE NO. I.8

TIME SEC	MACH	Q	L8/FT ⁰⁰²	ALPHA DEG	BETA DEG	L8*DEG/FT ⁰⁰²	L8*DEG/FT ⁰⁰²	GALPHA DEG	GBETA DEG
LIFT-OFF	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
4.000	0.062	5.690	2.0509	-0.019	1.4.276	-0.110			
6.000	0.096	13.706	2.0469	-0.028	3.0.844	-0.384			
6.000	0.096	13.706	2.0469	-0.028	3.0.844	-0.384			
6.000	0.110	24.716	2.0903	-0.094	7.0.746	2.0.334			
8.000	0.133	25.730	2.0932	-0.091	7.5.441	2.0.345			
12.000	0.211	63.209	3.0245	-0.027	20.5.137	1.0.720			
16.000	0.297	120.554	3.0183	-0.010	38.3.764	-0.0218			
17.500	0.332	147.544	3.0142	-0.02	46.3.556	-1.0.044			
17.500	0.332	147.544	3.0142	-0.024	46.3.556	-1.0.044			
20.000	0.392	198.592	3.0064	-0.035	6.0.6.389	-7.0.031			
24.000	0.488	286.203	2.0854	-0.054	8.16.780	-15.0.591			
26.000	0.561	372.056	2.0611	-0.070	9.71.407	-26.0.071			
32.000	0.671	449.432	2.0382	-0.083	1.070.402	-37.0.481			
36.000	0.762	516.606	2.0195	-0.095	1.134.015	-48.0.896			
40.000	0.856	573.342	2.0046	-0.104	1.172.864	-59.0.496			
44.000	0.953	615.051	1.9890	-0.112	1.163.975	-69.0.189			
MACH JNL	45.935	1.000	629.726	1.0.792	-0.116	1.128.270	-73.0.059		
45.000	1.051	640.021	1.0.727	-0.120	1.105.591	-76.0.563			
52.000	1.154	648.515	1.0.709	-0.126	1.108.444	-81.0.474			
54.491	1.224	649.711	1.0.743	-0.129	1.132.165	-83.0.915			
55.000	1.254	649.383	1.0.764	-0.131	1.145.0.347	-84.0.779			
55.000	1.254	649.383	1.0.764	-0.131	1.145.0.347	-84.0.779			
55.000	1.266	649.071	1.0.773	-0.131	1.150.789	-85.0.086			
6.000	1.269	648.960	1.0.776	-0.131	1.152.0.391	-85.0.168			
6.000	1.298	639.765	1.0.857	-0.136	1.187.958	-87.0.322			
6.000	1.356	617.292	1.0.846	-0.142	1.139.255	-87.0.486			
6.000	1.656	394.334	1.0.846	-0.146	1.096.974	-86.0.735			
6.000	1.669	567.735	1.0.847	-0.147	1.085.509	-86.0.437			
7.000	1.773	571.235	1.0.853	-0.150	1.058.647	-85.0.560			
7.000	1.773	571.235	1.0.853	-0.150	1.058.647	-85.0.560			
7.000	1.662	553.314	1.0.858	-0.152	1.028.483	-84.0.425			
7.000	2.044	507.450	1.0.829	-0.158	931.694	-80.0.564			

MISSION-3A/MCR=500/LIFTOFF TO AOA MECH/

CASE 1

TIME SEC	MACH	4 L8/RT ⁰⁰²	ALPHA DEG	BETA DEG	GAMMA DEG	L8-DEG/FT ⁰⁰²	L8-DEG/FT ⁰⁰²	TABLE NO. I.8
00.000	2.0233	458.534	1.0742	-0.164	0.666.629	798.610	-0.75.202	
64.000	2.0433	407.533	1.0636	-0.170	0.640.761	781	-0.69.274	
68.000	2.0451	356.210	1.0518	-0.176	0.62.724			
92.000	2.0890	310.041	1.0404	-0.182	0.535.413		-0.56.511	
96.000	3.0149	266.620	1.0316	-0.186	0.560.600		-0.50.219	
97.500	3.0248	250.424	1.0251	-0.191	0.513.328		-0.47.758	
97.500	3.0246	250.424	1.0251	-0.191	0.513.328		-0.47.758	
100.000	3.0411	224.231	1.0104	-0.196	0.427.650		-0.43.635	
104.000	3.0474	164.964	0.945	-0.201	0.156.359		-0.37.208	
107.500	3.0910	154.197	0.725	-0.207	1.11.754		-0.31.945	
107.500	3.0910	154.197	0.725	-0.207	1.11.754		-0.31.945	
108.000	3.0944	147.078	0.722	-0.208	1.08.274		-0.31.208	
112.000	4.0184	118.531	0.793	-0.217	0.94.029		-0.26.673	
116.000	4.0378	90.993	0.848	-0.227	0.77.127		-0.20.446	
120.000	4.0499	68.471	0.696	-0.248	0.47.647		-0.16.496	
121.420	4.0506	60.795	0.687	-0.248	0.29.603		-0.15.061	
121.420	4.0506	60.795	0.687	-0.248	0.29.603		-0.15.061	
124.000	4.0504	60.795	0.687	-0.248	0.29.603		-0.15.061	
140.000	4.0836	45.119	0.48.783	-0.317	0.64.237		-0.12.707	
156.000	5.0490	16.089	0.16.089	-0.325	-0.5.227		-0.04.418	
172.000	6.204	6.051	0.06.051	-0.322	-1.14.053		-0.2.163	
		2.0227	0.06.068	-0.471	-0.9.059		-0.1.048	
		7.0239	0.789	-0.5.974	-0.562.8		-0.04.16	
		7.0940	0.262	-0.6.544	-0.567.9		-0.04.220	
		8.0294	0.081	-0.7.056	-0.42.4		-0.04.647	
		8.0538	0.031	-0.7.792	-0.46.4		-0.05.887	
		2.0220	0.014	-0.7.321	-0.70.0		-0.05.021	
		2.0220	0.013	-0.7.099	-0.70.2		-0.05.010	
		2.0200	0.007	-0.7.099	-0.70.2		-0.05.009	
		2.0200	0.007	-0.6.942	-0.74.8		-0.05.005	
		2.0200	0.004	-0.7.268	-0.79.3		-0.05.030	
		2.0200	0.004	-0.7.385	-0.80.1		-0.05.028	
		2.0200	0.004	-0.7.396	-0.80.1		-0.05.028	
		2.0200	0.004	-0.7.396	-0.80.1		-0.05.028	
		2.0200	0.004	-0.7.396	-0.80.1		-0.05.028	

INTERMEDIATE

SA+1 / EL=24
 MISSION=JA/MCR=500/LIFTOFF TO AOA MECH/

CASE 1

TIME SEC	MACH	θ	$L_B/F_T \cdot 10^2$	ALPHA DEG	Ω	Q	$L_B \cdot DEG/F_T \cdot 10^2$	$\Omega\alpha\lambda\mu$	BETA DEG	$L_B \cdot DEG/F_T \cdot 10^2$	$\Omega\beta\epsilon\tau$
300.000	9.419	.003	-7.774	-8.110	-0.834	-0.110	-0.024	-0.020	-0.002	-0.003	-0.003
316.000	8.396	.002	-8.002	-8.309	-0.904	-0.104	-0.016	-0.016	-0.002	-0.002	-0.002
332.000	8.499	.002	-8.002	-8.368	-0.924	-0.108	-0.018	-0.018	-0.002	-0.002	-0.002
342.121	8.471	.002	-8.002	-8.368	-0.924	-0.108	-0.018	-0.018	-0.002	-0.002	-0.002
342.121	8.471	.002	-8.002	-8.368	-0.924	-0.108	-0.018	-0.018	-0.002	-0.002	-0.002
348.000	8.003	.002	-8.002	-8.395	-0.934	-0.119	-0.019	-0.019	-0.002	-0.002	-0.002
364.000	9.276	.002	-8.002	-8.353	-0.961	-0.021	-0.021	-0.021	-0.002	-0.002	-0.002
380.000	9.932	.003	-8.003	-8.217	-0.985	-0.025	-0.025	-0.025	-0.003	-0.003	-0.003
396.000	10.020	.004	-7.985	-1.006	-0.031	-0.004	-0.004	-0.004	-0.004	-0.004	-0.004
412.000	11.944	.005	-7.066	-1.024	-0.042	-0.006	-0.006	-0.006	-0.006	-0.006	-0.006
428.000	13.132	.006	-7.279	-1.036	-0.059	-0.016	-0.016	-0.016	-0.006	-0.006	-0.006
444.000	14.354	.012	-6.834	-1.050	-0.084	-0.021	-0.021	-0.021	-0.013	-0.013	-0.013
460.000	15.799	.020	-6.033	-1.059	-0.126	-0.031	-0.031	-0.031	-0.021	-0.021	-0.021
476.000	17.557	.033	-5.0776	-1.065	-0.192	-0.035	-0.035	-0.035	-0.021	-0.021	-0.021
492.000	19.196	.054	-5.0166	-1.068	-0.289	-0.060	-0.060	-0.060	-0.040	-0.040	-0.040
508.000	20.759	.087	-4.491	-1.068	-0.390	-0.093	-0.093	-0.093	-0.073	-0.073	-0.073
524.000	22.410	.124	-3.747	-1.064	-0.445	-0.132	-0.132	-0.132	-0.111	-0.111	-0.111
534.683	23.717	.152	-3.098	-1.058	-0.471	-0.161	-0.161	-0.161	-0.141	-0.141	-0.141
540.000	24.046	.157	-2.922	-1.057	-0.490	-0.164	-0.164	-0.164	-0.144	-0.144	-0.144
556.000	25.432	.165	-2.044	-1.050	-0.537	-0.173	-0.173	-0.173	-0.153	-0.153	-0.153
558.712	25.630	.163	-1.694	-1.049	-0.506	-0.171	-0.171	-0.171	-0.151	-0.151	-0.151
558.712	25.630	.163	-1.694	-1.049	-0.506	-0.171	-0.171	-0.171	-0.151	-0.151	-0.151
BEGIN GLIMIT											
INJECTION											
IMPROVEMENT											

SAW-1 / EL=24

MISSION=3A/MCR=500/LIFTOFF TO AOA MECH/

CASE 1

TIME SEC	THRUST LBS	WEIGHT LBS	AXIAL FORCE LBS		NORMAL FORCE LBS		SIDE FORCE LBS	
			LIFT-OFF	BEGIN ROLL	BEGIN TILT	END TOLL	LONG ACC G/S	NORMAL ACC G/S
0.000	4617381.3	4390646.9	0	0	0	0	1.5004	0.0744
4.000	4786809.5	4286742.5	2462.1	534.1	11.8	1.5764	0.0744	
6.000	6854633.7	4223431.8	5014.5	1205.5	41.6	1.6111	0.0745	
6.000	6854633.7	4223431.8	5014.5	1205.5	41.5	1.6111	0.0745	
7.055	6901844.7	4183779.3	10342.6	3775.9	-251.8	1.6404	0.0741	
8.000	6905595.6	4179898.1	10756.1	4043.0	-253.0	1.6427	0.0741	
12.000	7013792.6	4072454.5	25868.3	12892.7	-185.6	1.7068	0.0724	
14.000	7130945.4	3963207.2	48622.8	23471.7	131.4	1.7797	0.0703	
17.500	7177182.2	3922099.0	59268.5	27810.5	328.4	1.8074	0.0693	
17.500	7177182.2	3922097.0	59268.5	27810.5	328.4	1.8074	0.0693	
20.000	7138259.6	3853285.7	79503.1	35108.2	758.4	1.8243	0.0681	
24.000	6795422.6	3747914.6	116235.5	41426.5	148.7	1.7742	0.0670	
28.000	6464642.4	3646803.3	149901.6	39061.1	260.7	1.7233	0.0723	
32.000	6157651.9	3551652.4	194277.0	52429.2	4124.9	1.6705	0.0763	
34.000	5998622.1	3462608.4	246870.4	61235.6	555.6	1.6521	0.0753	
40.000	5839113.0	3373584.3	290150.4	11444.0	4971.8	1.6353	0.0755	
44.000	5678188.7	3291030.1	401816.6	109904.5	6380.2	1.5434	0.0757	
MACH ONE	45.915	5599470.5	3251632.7	4649540.6	68400.4	9047.4	1.5674	0.0791
48.000	5514613.2	3209985.9	507897.5	65064.8	9748.7	1.6495	0.0886	
52.000	5422795.3	3130429.0	552542.2	132482.2	10557.5	1.5450	0.0825	
54.491	5441683.1	3082478.0	551068.6	1422681.9	10743.8	1.5756	0.0742	
55.500	5448831.9	3063074.9	548009.3	168810.3	10819.4	1.5889	0.0710	
55.500	5448831.9	3063074.9	548009.3	168810.3	10819.4	1.5889	0.0710	
55.891	5461593.6	3055409.7	546503.1	170574.6	10844.8	1.5975	0.0727	
56.000	5465144.1	3053276.1	546061.2	171039.4	10851.4	1.6000	0.0724	
60.000	5593125.7	2974685.1	520835.6	176760.7	10947.1	1.6902	0.0712	
64.000	5715858.4	2896494.1	496911.6	160832.8	10786.5	1.7893	0.0751	
67.160	5809197.8	2833214.7	459499.6	146102.4	10549.4	1.8761	0.0764	
66.000	5833486.5	2816119.1	447631.8	141938.5	10533.6	1.9004	0.0793	
70.000	5690436.9	2775147.0	420761.7	131306.9	10317.4	1.9586	0.0815	
70.000	5690436.9	2775147.0	420761.7	131306.9	10317.4	1.9586	0.0815	
72.000	5946183.9	2734175.0	341994.7	119683.0	10101.7	2.0182	0.0834	
76.000	4030705.7	2651132.4	341992.9	93022.2	9473.7	2.1328	0.0906	

ORIGINAL PAGE IS
OF POOR QUALITY

SA+1/EL=24

MISSION-3A/MCH-500/LIFTOFF TO AGA MECON

CASE 1

TABLE NO. 1.9

TIME SEC	THRUST LBS	WEIGHT LBS	NORMAL FORCE			LONG FORCE			SIDE FORCE		
			LBS	LBS	LBS	G'S	G'S	G'S	ACC	ACC	ACC
00.000	6096873.0	2567430.5	290693.0	62584.0	6668.0	2.2481	2.3494	2.4981	0.0996	0.1085	0.1161
01.000	6159572.9	2482914.7	242150.1	34519.0	7811.6	2.0404	1.0805	1.1611	0.0996	0.1032	0.1222
02.000	6219609.8	2396984.6	201065.0	10804.4	6900.5	2.4964	2.0707	2.6292	0.1222	0.1245	0.1245
03.000	6277248.6	2310888.5	166617.2	-7878.3	6045.9	2.6292	2.0769	2.7697	0.1269	0.1269	0.1269
04.000	6331832.2	2224349.9	135935.2	-18415.6	5235.8	2.7697	2.0769	2.8237	0.1269	0.1269	0.1269
05.000	6348483.4	2191547.5	125141.5	-21583.2	4936.2	2.8237	2.0823	2.8237	0.1269	0.1269	0.1269
06.000	6348483.4	2191547.5	125141.5	-21583.2	4936.2	2.8237	2.0823	2.8237	0.1269	0.1269	0.1269
07.000	6260194.4	2137497.3	109434.0	-26043.5	4449.9	2.8611	2.0861	2.8611	0.1237	0.1237	0.1237
08.000	6118112.3	2052435.2	87336.0	-29477.5	3716.5	2.9212	2.0921	2.9212	0.1407	0.1407	0.1407
09.000	5957623.7	1979737.6	71243.4	-27379.7	3137.0	2.9555	2.1370	2.9555	0.1451	0.1451	0.1451
10.000	5957623.7	1979737.6	71243.4	-27379.7	3137.0	2.9555	2.1370	2.9555	0.1451	0.1451	0.1451
11.000	5865353.5	1969741.1	69249.8	-26751.9	3057.4	2.9320	2.1354	2.9320	0.1417	0.1417	0.1417
12.000	5125607.4	1895649.4	55043.2	-20763.5	2471.6	2.6619	2.1354	2.6619	0.1554	0.1554	0.1554
13.000	4386915.1	1832543.8	43501.4	-15630.1	1962.3	2.3545	2.1354	2.3545	0.1709	0.1709	0.1709
14.000	2509132.5	1786299.2	33094.0	-12780.5	1551.3	2.3613	2.1354	2.3613	0.2125	0.2125	0.2125
15.000	1735336.3	1776393.4	29284.5	-12653.9	1417.4	2.3932	2.1354	2.3932	0.2300	0.2300	0.2300
16.000	1536324.2	1428013.4	27858.9	+322.2	1340.1	1.0262	1.0262	1.0262	0.2445	0.2445	0.2445
17.000	1536324.2	1428013.4	27858.9	+322.2	1340.1	1.0262	1.0262	1.0262	0.2445	0.2445	0.2445
18.000	1536439.4	1419304.4	22083.7	-1004.0	1107.1	1.0387	1.0387	1.0387	0.2464	0.2464	0.2464
19.000	1536767.3	1365295.3	5346.7	-2260.1	956.8	1.0924	1.0924	1.0924	0.2558	0.2558	0.2558
20.000	1536861.4	1311286.2	249.4	-1621.7	203.9	1.1419	1.1419	1.1419	0.2643	0.2643	0.2643
21.000	1536869.2	1257277.1	-1474.6	+836.5	87.3	1.1926	1.1926	1.1926	0.2732	0.2732	0.2732
22.000	1536871.1	1203268.0	-2136.5	+365.0	34.7	1.2474	1.2474	1.2474	0.2828	0.2828	0.2828
23.000	1536899.2	1149258.9	-2384.0	+133.1	12.1	1.3068	1.3068	1.3068	0.2934	0.2934	0.2934
24.000	1536899.8	1095249.8	-2456.1	-46.2	4.2	1.3720	1.3720	1.3720	0.3048	0.3048	0.3048
25.000	1536899.9	1041240.7	-2475.4	-18.4	1.7	1.4439	1.4439	1.4439	0.3173	0.3173	0.3173
26.000	1536900.0	987231.6	-2484.6	-7.7	.8	1.5237	1.5237	1.5237	0.3308	0.3308	0.3308
27.000	1536900.0	983719.0	-2485.2	-7.1	.6	1.5292	1.5292	1.5292	0.3318	0.3318	0.3318
28.000	1040100.0	983658.0	1.4	-7.1	.6	1.0332	1.0332	1.0332	0.2245	0.2245	0.2245
29.000	1040100.0	949239.3	9.7	-3.4	4.4	1.0711	1.0711	1.0711	0.2309	0.2309	0.2309
30.000	1040100.0	912426.9	7.2	-2.2	.3	1.1146	1.1146	1.1146	0.2381	0.2381	0.2381
31.000	1040100.0	905959.6	6.9	-2.1	.3	1.1226	1.1226	1.1226	0.2394	0.2394	0.2394
32.000	1036600.0	905959.6	6.9	-2.1	.3	1.1190	1.1190	1.1190	0.2386	0.2386	0.2386

INTERMEDIATE

SUPPLY MISSION
BEGIN MISSION

SA-1/ELO-24

MISSION-JA/MCR-500/LIFTOFF TO AOA MECCO/

CASE 1

TIME SEC	THRUST LBS	WEIGHT LBS	AXIAL FORCE LBS	SIDE FORCE LBS		NORMAL FORCE LBS	LONG ACC G/S	NORMAL ACC G/S
				G'S	G'S			
300.000	1034400.0	875773.3	6.1	-0.7	0.2	1.1580	0.2449	
314.000	1034400.0	839154.2	5.5	-0.4	0.2	1.2091	0.2531	
332.000	1034400.0	802535.1	5.9	-0.3	0.2	1.2649	0.2619	
342.121	1034400.0	779372.2	5.5	-0.3	0.2	1.3028	0.2678	
342.121	1024400.0	779372.2	5.5	-0.3	0.2	1.2877	0.2647	
348.000	1024400.0	766141.3	5.7	-0.3	0.2	1.3102	0.2681	
364.000	1024400.0	730135.2	6.4	-0.4	0.2	1.3755	0.2780	
380.000	1024400.0	694129.1	7.7	-0.7	0.2	1.4474	0.2868	
396.000	1024400.0	658123.0	9.7	-2.1	0.3	1.5277	0.3095	
412.000	1024400.0	622117.0	13.0	-2.9	0.5	1.6164	0.3132	
428.000	1024400.0	586110.9	16.1	-4.2	0.7	1.7177	0.3269	
444.000	1024400.0	550104.6	26.3	-6.0	1.1	1.8309	0.3415	
460.000	1024400.0	514098.8	37.3	-7.3	1.8	1.9405	0.3574	
476.000	1024400.0	478082.7	56.2	-14.4	3.0	2.1096	0.3750	
492.000	1024400.0	442064.6	64.9	-22.7	5.0	2.2823	0.3950	
508.000	1024400.0	406080.6	121.4	-32.0	7.7	2.4877	0.4185	
524.000	1024400.0	370074.5	149.5	-40.4	11.0	2.7319	0.4470	
534.483	1024400.0	341533.3	198.1	-43.5	13.4	2.9616	0.4749	
540.000	1002449.9	324150.0	205.6	-43.3	13.9	2.9619	0.4727	
556.000	902141.1	300720.4	224.7	-36.1	14.4	2.9622	0.4639	
558.712	886185.7	295395.2	224.8	-34.0	14.2	2.9624	0.4627	
558.712	886185.7	295395.1	0.0	0.0	0.0	2.9626	0.4627	
558.712	0.0	295395.1	0.0	0.0	0.0	0.0000	0.0000	
BEGIN GLIMIT								
INJECTION								

SA-1/EL-24

MISSION-3A/MCR-500/LIFTOFF TO AOA MELO/

CASE 1

TABLE NO. I.10

	TIME SEC	CNTR DEG	CHIP DEG	CHI Y DEG	DELRC DEG	DELYC DEG
LIFT-OFF	0.000	-161.471	-2.690	-9.02	0.00	0.000
	4.000	-161.492	-2.686	-9.00	0.00	0.000
BEGIN ROLL	6.000	-161.492	-2.684	-8.99	0.00	0.000
BEGIN TILT	6.000	-161.492	-2.684	-8.99	0.00	0.000
END ROLL	7.655	-160.000	-3.522	-0.00	0.00	0.000
	8.000	-160.000	-3.522	-0.00	0.00	0.000
	12.000	-160.000	-5.553	-0.00	0.00	0.000
	16.000	-160.000	-7.737	-0.00	0.00	0.000
	17.500	-160.000	-8.617	-0.00	0.00	0.000
	17.500	-160.000	-8.617	-0.00	0.00	0.000
	20.000	-160.000	-10.135	-0.00	0.00	0.000
	24.000	-160.000	-12.495	-0.00	0.00	0.000
	28.000	-160.000	-14.760	-0.00	0.00	0.000
	32.000	-160.000	-17.043	-0.00	0.00	0.000
	36.000	-160.000	-19.362	-0.00	0.00	0.000
	40.000	-160.000	-21.768	-0.00	0.00	0.000
	44.000	-160.000	-24.220	-0.00	0.00	0.000
	45.935	-160.000	-25.389	-0.00	0.00	0.000
	48.000	-160.000	-26.662	-0.00	0.00	0.000
	52.000	-160.000	-29.252	-0.00	0.00	0.000
MACH MAXIMUM	54.4491	-160.000	-30.987	-0.00	0.00	0.000
	55.500	-160.000	-31.712	-0.00	0.00	0.000
	55.891	-160.000	-31.995	-0.00	0.00	0.000
	56.000	-160.000	-32.074	-0.00	0.00	0.000
	60.000	-160.000	-34.999	-0.00	0.00	0.000
	64.000	-160.000	-37.834	-0.00	0.00	0.000
	67.160	-160.000	-40.050	-0.00	0.00	0.000
	68.000	-160.000	-40.633	-0.00	0.00	0.000
	70.000	-160.000	-42.010	-0.00	0.00	0.000
	72.000	-160.000	-43.362	-0.00	0.00	0.000
	76.000	-160.000	-45.938	-0.00	0.00	0.000
10 KMS.						
14 KMS.						

SA+1/EL-24

MISSION-3A/MCR-500/LIFTOFF TO AOA MECO/

CASE 1

TIME SEC	CHIR DEG	CHIP DEG	CHIV DEG	TABLE NO. I.10		
				DELPC DEG	DELYC DEG	DELRC DEG
80.000	180.000	-48.312	0.000	0.007	0.016	0.000
84.000	180.000	-50.508	0.000	0.202	0.014	0.000
88.000	180.000	-52.531	0.000	0.391	0.012	0.000
92.000	180.000	-54.404	0.000	0.568	0.011	0.000
96.000	180.000	-56.159	0.000	0.693	0.010	0.000
97.500	180.000	-56.751	0.000	0.728	0.009	0.000
97.500	180.000	-56.751	0.000	0.728	0.009	0.000
100.000	180.000	-57.649	0.000	0.757	0.009	0.000
104.000	180.000	-58.941	0.000	0.789	0.008	0.000
107.500	180.000	-60.069	0.000	0.813	0.007	0.000
107.500	180.000	-60.069	0.000	0.813	0.007	0.000
108.000	180.000	-60.239	0.000	0.843	0.007	0.000
112.000	180.000	-61.632	0.000	0.901	0.026	0.000
116.000	180.000	-62.917	0.000	0.931	0.022	0.000
120.000	180.000	-63.897	0.000	0.946	0.022	0.000
121.420	180.000	-64.056	0.000	0.954	0.015	0.000
121.420	180.000	-65.105	0.000	0.954	0.014	0.000
121.420	180.000	-65.105	0.000	0.954	0.014	0.000
124.000	180.000	-65.541	0.000	0.968	0.016	0.000
140.000	180.000	-67.774	0.000	1.014	0.014	0.000
156.000	180.000	-69.250	0.000	1.052	0.014	0.000
172.000	180.000	-70.561	0.000	1.073	0.017	0.000
188.000	180.000	-71.825	0.000	1.117	0.014	0.000
204.000	180.000	-73.075	0.000	1.151	0.014	0.000
220.000	180.000	-74.325	0.000	1.187	0.014	0.000
236.000	180.000	-75.580	0.000	1.203	0.014	0.000
252.000	180.000	-77.554	0.000	1.227	0.014	0.000
253.041	180.000	-77.882	0.000	1.226	0.014	0.000
INTERMEDIATE	180.000	-77.882	0.000	1.226	0.014	0.000
268.000	180.000	-80.207	0.000	1.241	0.014	0.000
284.000	180.000	-81.402	0.000	1.205	0.014	0.000
286.811	180.000	-81.613	0.000	1.203	0.014	0.000
286.811	180.000	-81.613	0.000	1.203	0.014	0.000

ORIGINAL PAGE IS
OF POOR QUALITY

SA+1/EL=24
 MISSION=3A/MCR=500/LIFTOFF TO AOA MECO/

CASE 1

TABLE NO. I.10

TIME SEC.	CHIR DEG	CHIP DEG	CHIY DEG	DELRC DEG	DELYC DEG
300.000	180.000	-82.402	0.000	0.000	-11.942
316.000	180.000	-83.805	0.000	0.000	-11.823
332.000	180.000	-85.011	0.000	0.000	-11.697
342.121	180.000	-85.777	0.000	0.000	-11.614
348.000	180.000	-86.223	0.000	0.000	-11.566
364.000	180.000	-87.439	0.000	0.000	-11.426
380.000	180.000	-88.660	0.000	0.000	-11.282
396.000	180.000	-89.884	0.000	0.000	-11.127
412.000	180.000	-91.110	0.000	0.000	-10.963
428.000	180.000	-92.329	0.000	0.000	-10.777
444.000	180.000	-93.536	0.000	0.000	-10.564
460.000	180.000	-94.734	0.000	0.000	-10.329
476.000	180.000	-95.927	0.000	0.000	-10.076
492.000	180.000	-97.124	0.000	0.000	-9.811
508.000	180.000	-98.333	0.000	0.000	-9.545
524.000	180.000	-99.565	0.000	0.000	-9.290
BEGIN GLIMIT	536.683	180.000	0.000	0.000	-9.106
540.000	180.000	-100.570	0.000	0.000	-9.063
556.000	180.000	-100.836	0.000	0.000	-8.892
558.712	180.000	-102.174	0.000	0.000	-8.870
INJECTION	558.712	180.000	-102.405	0.000	-8.870
	558.712	180.000	-102.405	0.000	0.000

SA+I/EL-24

MISSION-3A/MCR=500/LIFTOFF TO AOA MECO/

CASE I

TABLE NO. I.11

	TIME SEC	RANGE NM	LIP LONG ANGLE DEG	VCH FT/SEC	VIDEAL FT/SEC
LIFT-OFF	0.000	0.0	0.0	0.000	0.000
BEGIN ROLL	4.000	12.000	34.0 8	-120.5	197.656
BEGIN TILT	6.000	16.000	34.0 8	-120.5	300.479
END ROLL	7.455	17.500	34.0 8	-120.5	300.479
	8.000	20.000	34.0 8	-120.5	397.718
	12.000	24.000	34.0 8	-120.5	405.395
	16.000	28.000	34.0 8	-120.5	621.780
	17.500	32.000	34.0 8	-120.5	847.594
	17.500	36.000	34.0 8	-120.5	943.621
	20.000	40.000	34.0 8	-120.5	934.890
	24.000	44.000	34.0 8	-120.5	934.890
	28.000	45.935	34.0 8	-120.5	1039.840
	32.000	46.000	34.0 8	-120.5	1082.891
	36.000	52.000	34.0 8	-120.5	1317.944
	40.000	54.491	34.0 8	-120.5	1547.966
	44.000	55.500	34.0 8	-120.5	1772.995
MACH ONE	45.935	55.500	34.0 7	-120.5	1957.254
	48.000	55.691	34.0 7	-120.5	1994.718
	52.000	56.000	34.0 7	-120.5	2216.813
	54.491	56.500	34.0 7	-120.5	2438.478
	55.500	56.500	34.0 7	-120.5	2674.957
	55.500	56.500	34.0 7	-120.5	2708.757
0 MAXIMUM	48.000	55.691	34.0 7	-120.5	2659.223
	52.000	56.000	34.0 7	-120.5	2879.524
	54.491	56.500	34.0 7	-120.5	3019.149
	55.500	56.500	34.0 7	-120.5	3076.501
	55.500	56.500	34.0 7	-120.5	3240.371
10 KMS.	55.691	56.000	34.0 7	-120.5	3348.197
	56.000	56.000	34.0 7	-120.5	3371.517
	56.500	56.500	34.0 7	-120.5	3411.961
	56.500	56.500	34.0 7	-120.5	3288.317
	56.500	56.500	34.0 7	-120.5	3348.197
	56.500	56.500	34.0 7	-120.5	3076.501
	56.500	56.500	34.0 7	-120.5	3098.860
	56.500	56.500	34.0 7	-120.5	3105.103
	56.500	56.500	34.0 7	-120.5	3378.025
	56.500	56.500	34.0 7	-120.5	3622.289
	56.500	56.500	34.0 7	-120.5	3587.378
	56.500	56.500	34.0 7	-120.5	3676.763
	56.500	56.500	34.0 7	-120.5	3791.116
	56.500	56.500	34.0 7	-120.5	3846.598
	56.500	56.500	34.0 7	-120.5	3981.001
	56.500	56.500	34.0 7	-120.5	4279.928
	56.500	56.500	34.0 7	-120.5	4118.705
	56.500	56.500	34.0 7	-120.5	4420.268
	56.500	56.500	34.0 7	-120.5	4404.002
	56.500	56.500	34.0 7	-120.5	4710.235

SA+1/EL-24

MISSION-3A/MCR=500/LIFTOFF TO AOA MECH/

CASE 1

TABLE NO. I.11

TIME SEC	RANGE NM	ANGLE DEG	LIP		VIDEAL	
			LAT DEG	LAT DEG	FT/SEC	FT/SEC
80.000	5.9	.3	34.3	-120.7	5012.109	
84.000	7.0	.3	34.2	-120.8	5012.089	5326.604
86.000	8.2	.3	34.0	-120.8	5337.960	5654.757
92.000	9.6	.3	33.9	-120.9	5678.083	5997.678
96.000	11.2	.3	33.7	-121.0	6034.302	6356.496
97.500	11.6	.3	33.6	-121.0	6172.219	6475.349
97.500	11.6	.3	33.6	-121.0	6172.219	6495.349
100.000	12.9	.3	33.5	-121.1	6405.396	6720.045
104.000	14.9	.4	33.3	-121.1	6783.057	7110.054
107.500	16.7	.4	33.1	-121.2	7119.955	7448.948
107.500	16.7	.4	33.1	-121.2	7119.955	7448.948
108.000	17.0	.4	33.1	-121.2	7167.987	7497.147
112.000	19.4	.4	32.8	-121.3	7532.920	7863.453
116.000	21.9	.4	32.4	-121.4	7840.278	8192.269
120.000	24.6	.5	32.1	-121.5	8119.774	8453.301
121.420	25.6	.5	32.0	-121.5	8173.438	8507.330
121.420	25.6	.5	32.0	-121.5	8173.438	8507.330
121.423	25.6	.5	32.0	-121.5	8173.438	8507.330
124.000	27.4	.5	32.0	-121.5	8263.020	8596.942
140.000	39.4	.7	31.9	-121.7	8831.243	9165.261
156.000	52.5	.9	31.5	-121.7	9422.474	9756.522
172.000	66.9	1.1	31.0	-122.1	10038.598	10372.654
188.000	82.6	1.3	30.4	-122.3	10681.785	11015.894
204.000	99.6	1.6	29.8	-122.6	11354.514	11688.576
220.000	118.4	1.9	29.2	-122.6	12059.636	12393.696
236.000	138.7	2.2	28.5	-123.1	12800.420	13134.481
252.000	160.6	2.5	27.7	-123.4	13580.671	13914.731
253.041	162.1	2.5	27.7	-123.4	13432.885	13946.945
INTERMEDIATE	253.041	162.1	2.5	27.7	13632.885	13946.945
268.000	184.1	2.9	27.2	-123.6	14150.923	14484.983
284.000	206.8	3.3	26.6	-123.8	14726.210	15060.270
286.911	213.3	3.4	26.5	-123.9	14829.658	15163.716
286.911	213.3	3.4	26.5	-123.9	14829.658	15163.716

SA+I/EL=24

MISSION-3A/MCR-500/LIFTOFF TO AGA MECON/

CASE I

TABLE NO. I.11

TIME SEC	RANGE NM	LIP		VIDEAL	
		ANGLE DEG	LONG DEG	VCH FT/SEC	FT/SEC
300.000	235.0	3.7	26.0	-124.1	15323.480
316.000	262.5	4.1	25.4	-124.3	1545.904
332.000	291.6	4.6	24.7	-124.5	16596.104
342.121	310.8	4.9	24.3	-124.7	17022.882
342.121	310.8	4.9	24.3	-124.7	17356.942
348.000	322.2	5.1	24.0	-124.9	17022.862
364.000	354.6	5.6	23.3	-125.1	17273.701
380.000	388.7	6.2	22.5	-125.3	17978.051
396.000	424.6	6.7	21.7	-125.6	18312.911
412.000	462.6	7.4	20.8	-126.0	19053.728
428.000	502.6	8.0	19.8	-126.3	19499.955
444.000	545.0	8.7	18.6	-126.7	19834.015
460.000	589.7	9.4	17.3	-127.1	20650.215
476.000	637.1	10.2	15.6	-127.6	21197.511
492.000	687.2	11.0	13.8	-128.3	22126.258
508.000	740.4	11.9	11.1	-129.2	22460.316
524.000	797.0	12.8	6.9	-130.5	23117.891
536.693	844.3	13.6	9	-132.3	24515.616
540.000	857.1	13.8	6	-133.1	25328.544
556.000	921.1	14.6	-35.8	-145.0	26573.0.7
558.712	932.4	15.0	-59.0	-160.4	27933.133
558.712	932.4	15.0	-59.0	-160.4	28267.193
558.712	932.4	15.0	-59.0	-160.4	29108.837
BEGIN GLIMIT					29442.898
INJECTION					29763.078

ORIGINAL PAGE IS
OF POOR QUALITY

SAI/EL-24

MISSION-3A/MCN-500/LIFTOFF TO AOA MELO/

CASE 1

TABLE NO. I.12

	TIME SEC	X FT	Y FT	Z FT	XDOT FT/SEC	YDOT FT/SEC	ZDOT FT/SEC
LIFT-OFF	0.000	20902623.5	-209462.5	62469.2	+000	-1186.331	-398.092
BEGIN ROLL	4.000	20902757.7	-25708.0	60877.4	68.757	-1186.374	-397.916
BEGIN TILT	6.000	20902933.2	-28080.0	60081.8	107.082	-1186.415	-397.737
END ROLL	6.000	20902933.2	-28080.8	60081.8	107.082	-1186.415	-397.737
	7.000	20903166.2	-30281.7	59344.5	144.440	-1186.471	-396.925
	8.000	20903187.2	-30453.7	59287.0	147.433	-1186.466	-396.801
	12.000	20903947.7	-35199.3	57712.1	234.243	-1186.319	-389.238
	16.000	20905072.2	-39944.2	56185.1	329.369	-1186.149	-372.608
	17.000	20905594.5	-41723.4	55632.7	367.209	-1186.060	-363.693
	17.500	20905594.5	-41723.4	55632.7	367.209	-1186.080	-363.693
	20.000	20906593.5	-44688.5	54745.5	432.071	-1185.963	-345.379
	24.000	20908524.2	-49431.9	53434.6	532.018	-1185.773	-308.713
	26.000	20910839.0	-54174.7	52285.7	624.124	-1185.587	-264.601
	32.000	20913505.7	-58916.6	51326.3	707.759	-1185.413	-214.101
	36.000	20916443.0	-63658.0	50582.1	785.194	-1185.258	-156.760
	40.000	20919781.2	-68398.7	50082.5	858.042	-1185.123	-91.752
	44.000	20923349.5	-73139.0	49857.8	924.782	-1185.011	-19.519
MACH ONE	45.935	20925167.0	-75431.5	49855.6	953.862	-1184.965	17.329
	48.000	20927167.5	-77878.9	49932.8	982.773	-1184.926	57.667
	52.000	20931204.2	-82618.4	50325.9	1034.558	-1184.874	140.255
✓ MAXIMUM	54.491	20933820.0	-85569.7	50745.5	1065.807	-1184.844	197.529
	55.500	20934902.0	-86765.4	50957.2	1078.509	-1184.831	222.185
	55.500	20934902.0	-86765.4	50957.2	1078.509	-1184.831	222.185
✓ KM50	55.591	20935324.7	-87228.9	51046.0	1083.461	-1184.826	231.975
	56.000	20935442.7	-87357.8	51071.4	1084.844	-1184.825	234.9726
	60.000	20939887.0	-92097.0	52223.4	1137.854	-1184.764	343.932
	64.000	20944551.2	-9468.9	53844.0	1195.081	-1184.678	449.090
	67.160	20948403.5	-1001.1	554498.7	1243.454	-1184.587	580.308
	68.000	20949453.5	-1011.4	55999.0	1256.785	-1184.559	611.386
	70.000	20951999.2	-1036.1	57299.0	1289.300	-1184.485	689.408
	70.000	20951999.2	-1036.1	57299.0	1289.300	-1184.485	689.408
	72.000	20954611.0	-1021.2	58759.8	1322.816	-1184.401	772.159
	76.000	20960040.7	-111044.6	62271.8	1392.539	-1184.199	951.916

SA+1/EL-24

MISSION-SA/MCR=500/LIFTOFF TO AOA MEKO/

CASE 1

TIME SEC	X FT	Y FT	Z FT	XDOT FT/SEC	YDOT FT/SEC	ZDOT FT/SEC
80.000	20965755.0	-115785.9	66399.5	1465.066	-1163.949	1150.010
81.000	20971765.0	-120521.1	71426.6	1540.368	-1183.649	1366.693
86.000	20978081.0	-125255.0	77358.7	1618.408	-1183.294	1602.559
92.000	20984715.0	-129487.4	84273.4	1699.041	-1182.881	1858.133
96.000	20991677.2	-134718.0	92251.0	1792.097	-1182.408	2134.210
97.500	20994374.2	-136491.4	95533.0	1813.893	-1182.216	2243.128
97.500	20994374.2	-136491.4	95533.0	1813.893	-1182.216	2243.128
100.000	20998975.2	-139446.5	101373.4	1866.769	-1181.677	2429.345
104.000	21006608.7	-144172.9	111700.9	1949.668	-1181.287	2736.198
107.500	21013556.7	-148306.4	121760.2	2020.140	-1180.724	3013.075
117.500	21013556.7	-148306.4	121760.2	2020.140	-1180.724	3013.075
118.000	21014569.2	-148896.8	123276.7	2029.766	-1180.639	3053.004
112.000	21022824.5	-153617.9	136107.8	2094.151	-1179.924	3158.096
116.000	21031292.2	-158336.1	150102.4	2135.820	-1179.157	3633.693
120.000	21039872.0	-163051.1	165111.8	2144.511	-1176.339	3851.039
121.420	21042908.5	-164724.1	170611.9	2131.257	-1178.038	3892.983
121.420	21042908.5	-164724.1	170611.9	2131.257	-1178.038	3892.983
SEPARATION BEGIN MINH	21042908.5	-164724.1	170611.9	2131.257	-1178.038	3892.983
121.420	21042908.5	-164724.1	170611.9	2131.257	-1178.038	3892.983
140.000	21048371.2	-167762.7	180744.4	2103.605	-1177.476	3961.868
156.000	21360653.2	-186572.4	247679.6	1931.538	-1173.630	4410.836
172.000	21110187.7	-205316.1	322056.1	1760.644	-1169.254	4891.032
188.000	2113707.7	-22396.0	404344.7	1592.353	-1164.405	5369.839
236.000	21218058.2	-297784.3	922300.6	947.876	-1140.660	7752.392
252.000	21161158.5	-242574.7	495006.1	1426.986	-1159.179	5938.133
268.000	21231982.7	-315979.5	951735.0	792.316	-1133.678	8434.365
253.041	21232801.7	-317159.0	960535.7	781.630	-1133.215	8480.548
253.041	21232801.7	-317159.0	960535.7	781.630	-1133.215	8480.548
INTERMEDIATE	21242525.0	-334059.8	1090782.4	516.774	-1126.287	8936.406
284.000	21248496.0	-352010.5	1237810.3	229.071	-1118.490	9445.038
286.011	21249068.5	-355160.2	1264487.6	176.199	-1117.078	9537.693
286.011	21249068.5	-355160.2	1264487.6	176.199	-1117.078	9537.693

MISSION=3A/MCR=300/LIFTOFF TO AGA MECO/
SAE/EL-24

CASE I

TABLE NO. T-12

TIME SEC	X FT	Y FT	Z FT	XDOT FT/SEC	YDOT FT/SEC	ZDOT FT/SEC
300.000	21249833.6	-369849.3	13931630.6	-62.619	-110.286	977.070
316.000	21246470.2	-387545.5	1567209.4	-358.632	-1101.676	10532.993
332.000	2123834.7	-405100.6	1730363.7	-659.282	-1092.662	1116.990
342.121	21230607.2	-416127.4	1844796.0	-652.380	-1066.751	1149.778
342.121	21230607.2	-416127.4	1844796.0	-852.380	-1086.751	1149.778
348.000	21225340.7	-422508.5	1913064.9	-744.461	-1083.243	11725.548
349.000	212207345.0	-439742.4	2108723.5	-1291.449	-1073.420	1231.422
350.000	21194287.2	-456885.8	2308823.6	-1604.439	-1063.143	1301.836
356.000	21155976.2	-473782.4	2522942.7	-1935.994	-1062.563	13739.657
412.000	21122261.7	-490535.7	2748714.7	-2277.623	-1041.531	1449.156
420.000	21083030.7	-507109.3	2984843.4	-2430.835	-1020.077	1520.930
444.000	21038023.7	-52494.7	3238116.0	-2997.415	-1018.263	1613.400
446.000	2098750.7	-53494.1	3503427.8	-3379.470	-1006.035	1700.741
474.000	20929784.7	-56556.7	3783786.7	-3779.547	-993.406	1801.980
492.000	20845972.7	-571476.4	4080266.9	-4200.748	-980.394	1909.380
509.000	20795227.7	-587058.0	4394492.2	-4644.926	-966.994	2021.4220
524.000	2071711.7	-602420.3	4727788.9	-5123.019	-953.225	21467.431
540.000	20649409.2	-61443.6	5006847.0	-5523.747	-942.054	22552.858
556.000	2051098.0	-61755.7	5082149.2	-5593.280	-943.045	23489.407
558.000	205457.7	-6246.4	515402.8	-5666.413	-952.125	24247.711
558.712	2051946.8	-63497.2	5228220.2	-5623.922	-922.125	24507.161
559.712	2051946.8	-63497.2	5228220.2	-5623.922	-922.125	24507.161
560.712	2051946.8	-63497.2	5228220.2	-5623.922	-922.125	24507.161

BEGIN GLOWIT

INJECTION

SA=1/EL=24

MISSION=3A/MCR=100/LIFTOFF TO AOA MECH/

CASE 1

TABLE NO. 1.13

TIME SEC	X ACC FT/SEC ²	Y ACC FT/SEC ²	Z ACC FT/SEC ²	HEAT RATE		
				BTU/FT ² SEC ⁻²	BTU/FT ² SEC ⁻²	BTU/FT ² SEC ⁻²
4.000	18.568	-0.017	-0.013	0.0	0.0	0.0
4.000	16.122	4.000	-0.013	0.0	0.0	0.0
BEGIN ROLL	19.473	0.026	0.112	0.0	0.0	0.0
BEGIN TILT	19.473	-0.026	0.112	0.0	0.0	0.0
END ROLL	20.407	0.028	0.017	0.0	0.0	0.0
7.855	20.480	-0.031	-0.004	0.0	0.0	0.0
8.000	22.733	0.099	2.957	0.0	0.0	0.0
12.000	24.833	-0.049	-0.428	0.0	0.0	0.0
16.000	25.420	0.042	0.470	0.0	0.0	0.0
17.500	25.420	-0.062	-0.470	0.0	0.0	0.0
17.500	20.400	0.074	0.132	0.2	0.4	0.4
20.000	25.492	-0.074	-0.146	0.0	0.0	0.0
24.000	24.012	0.073	0.146	0.0	0.0	0.0
28.000	22.012	-0.053	-0.035	0.0	0.0	0.0
32.000	19.912	0.014	0.024	0.0	0.0	0.0
34.000	18.794	0.063	0.275	2.4	3.4	3.4
40.000	17.598	0.010	0.226	0.0	0.0	0.0
44.000	15.600	0.021	0.070	0.2	0.2	0.2
45.935	14.509	-0.021	-0.295	0.0	0.0	0.0
48.000	13.692	0.014	0.197	0.5	0.5	0.5
52.000	12.537	0.017	0.444	0.0	0.0	0.0
54.491	12.565	0.025	0.222	0.0	0.0	0.0
55.500	12.405	0.030	0.041	0.0	0.0	0.0
55.500	12.405	-0.030	-0.041	0.0	0.0	0.0
55.691	12.713	0.012	0.216	0.0	0.0	0.0
56.000	12.743	0.013	0.323	0.0	0.0	0.0
60.000	13.758	0.018	0.280	0.0	0.0	0.0
64.000	14.842	0.024	0.366	0.0	0.0	0.0
67.140	15.752	0.024	0.871	0.2	0.2	0.2
68.000	15.908	0.044	0.941	0.2	0.2	0.2
70.000	16.512	0.095	1.048	0.4	0.4	0.4
70.000	16.512	-0.095	-1.048	0.0	0.0	0.0
72.000	17.004	0.047	0.575	0.2	0.2	0.2
76.000	17.008	-0.054	-0.575	0.0	0.0	0.0

MACH ONE
at MAXIMUM
10 KMS.

14 KMS.

SA-1/EL-24
MISSION-3A/MCR-600/LIFTOFF TO AOA MECO/

CASE I

TABLE NO.I.13

TIME SEC	XACC FT/SEC ^{0.2}	YACC FT/SEC ^{0.2}	ZACC FT/SEC ^{0.2}	HEAT RATE BTU/FT ^{0.2}	HEAT RATE BTU/FT ^{0.2}
60.000	18.4789	0.0687	51.08238	42.7	2.0
64.000	19.1711	0.0814	56.5452	51.1	2.3
68.000	19.0393	0.0960	61.04048	40.8	2.6
72.000	20.4693	0.1107	66.04146	71.8	2.7
76.000	21.0746	0.1254	71.04681	84.4	3.1
77.500	21.3440	0.1310	73.04038	89.4	3.5
97.500	21.3440	0.1310	73.04038	89.4	3.5
100.000	20.9720	0.1402	76.03562	98.4	3.7
104.000	20.4712	0.1547	78.05623	112.9	4.0
107.500	19.6165	0.1669	79.04022	128.5	4.3
107.500	19.5957	0.1702	80.02274	126.5	4.3
108.000	18.9102	0.1719	79.04060	130.6	4.3
112.000	13.2429	0.1853	72.08220	148.3	4.6
116.000	7.5596	0.1983	64.07558	166.3	4.5
120.000	-6.3852	0.2102	36.0172	183.8	4.2
121.420	-12.0385	0.2144	23.04574	189.7	4.1
121.420	-10.7232	0.2141	26.04841	189.7	4.1
121.420	-10.7232	0.2141	26.04841	189.7	4.1
124.000	-10.7162	0.2214	26.09112	199.7	3.7
140.000	-10.7514	0.2579	29.01003	247.9	2.6
156.000	-10.6051	0.2886	30.09063	281.5	1.8
172.000	-10.4276	0.3172	37.07056	305.4	1.3
188.000	-10.2430	0.3446	60.016	322.7	0.9
204.000	-10.0627	0.3713	50.0404	334.4	0.6
220.000	-7.8935	0.3976	38.08566	342.2	0.4
236.000	-9.7397	0.4235	41.02841	347.7	0.3
252.000	-10.1704	0.4492	44.02252	351.8	0.2
253.041	-10.3609	0.4508	44.04982	352.0	0.2
253.041	-17.0840	0.4508	29.06204	352.0	0.2
264.000	-17.6683	0.4747	31.01424	355.0	0.2
284.000	-18.0812	0.5001	32.0530	357.7	0.2
286.611	-18.1191	0.5045	32.08116	358.1	0.2
286.611	-18.1625	0.5045	32.06951	358.1	0.2

INTERMEDIATE

SA-1/EL-24
MISSION-JA/MCR-500/LIPTOFF TO ADA MEKO/

CASE 1
TABLE NO. I-13

TIME SEC	X ACC		Y ACC		Z ACC		HEAT RATE BTU/FT ² SEC ⁻²
	FT/SEC ²	FT/SEC ^{0.2}	FT/SEC ²	FT/SEC ^{0.2}	FT/SEC ²	FT/SEC ^{0.2}	
300.000	-18.3591	-0.5254	32.9434	-0.3601	362.5	-0.2	
316.000	-18.6377	-0.5508	35.9584	-0.3625	362.5	-0.2	
332.000	-18.9444	-0.5760	37.3304	-0.3650	365.0	-0.2	
342.121	-19.1984	-0.5920	38.5253	-0.3667	366.7	-0.2	
342.121	-19.3336	-0.5920	38.0467	-0.3667	366.7	-0.2	
348.000	-19.4914	-0.613	38.7521	-0.3677	367.7	-0.2	
344.000	-19.9251	-0.6264	40.7801	-0.3709	370.9	-0.2	
380.000	-20.4357	-0.6518	43.0246	-0.3747	374.7	-0.3	
396.000	-21.0224	-0.6770	45.4953	-0.3795	379.5	-0.3	
412.000	-21.6947	-0.7021	48.2420	-0.3857	385.7	-0.5	
428.000	-22.4731	-0.7271	51.3146	-0.3942	394.2	-0.6	
444.000	-23.3707	-0.7521	54.7854	-0.4059	405.9	-0.9	
460.000	-24.4124	-0.7768	58.7327	-0.4223	422.3	-1.2	
476.000	-25.6291	-0.8013	63.2664	-0.4462	446.2	-1.8	
492.000	-27.0411	-0.8254	68.5394	-0.4812	481.2	-2.4	
508.000	-28.7638	-0.8490	74.7450	-0.5216	521.6	-3.7	
524.000	-30.6126	-0.8720	82.1619	-0.5614	561.4	-5.1	
524.000	-32.7560	-0.897	89.1594	-0.6733	673.3	-6.2	
540.000	-33.6312	-0.942	99.0328	-0.6945	694.5	-6.5	
556.000	-35.4419	-0.959	108.3447	-0.8084	808.4	-7.4	
556.712	-36.0407	-0.9495	108.2426	-0.8295	829.5	-7.7	
556.712	-36.0407	-0.9195	108.2425	-0.8295	829.5	-7.7	
556.712	-30.0973	-0.9219	-0.0724	-0.8295	829.5	-7.7	

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INJECTION

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SA-1/EL-24

MISSION-3A/MCR-SLC/AOA/RTLS POINT TO NOR MEKO

CASE 1

TABLE NO. 1.14

	TIME	R	V1	CAMPAI	LAT-CD	LONG	AZI
	SEC	FT	FT/SEC	DEG	DEG	DEG	DEG
IGNITION	253.041	21250882.7	8591.555	7.000	32.446	-121.573	-169.011
SECTION MINH	253.041	21256382.7	8591.555	7.200	32.446	-121.573	-169.011
269.000	21273375.7	9273.717	5.002	32.072	-121.728	-168.448	
285.000	21237306.7	10012.652	4.195	31.656	-121.934	-167.348	
301.000	21297427.7	10868.851	2.780	31.227	-122.072	-167.507	
317.000	21304169.0	11665.734	1.638	30.755	-122.262	-167.116	
333.000	21309097.5	12588.139	*733	70.245	-122.466	-166.770	
349.000	21303434.7	13532.563	*243	29.696	-122.693	-166.463	
365.000	21308457.5	14657.557	*455	29.104	-122.914	-166.191	
381.000	21305915.2	15924.223	*759	29.465	-123.161	-165.951	
397.000	21302651.7	17097.089	*694	27.770	-123.424	-165.739	
413.000	21297620.0	18495.318	*962	27.072	-123.734	-165.553	
418.898	21296L01.5	19C46.275	*211	26.743	-123.812	-165.490	
429.200	21293403.5	20011.215	*589	26.277	-124.073	-165.395	
445.000	21290116.5	21539.185	*478	25.358	-124.321	-165.279	
461.000	21289365.7	23067.906	*117	24.425	-124.658	-165.197	
477.000	21288861.7	24596.624	*272	23.429	-125.011	-165.145	
485.231	21290246.0	25382.783	*000	22.391	-125.200	-165.127	
485.231	21290246.0	25382.783	*000	22.391	-125.200	-165.127	
485.231	21293346.0	25382.703	*000	22.391	-125.200	-165.127	

SA+I/EL-24

MISSION-ZA/MCR-5CD/ADA/RTLS POINT TO NOM MECO

CASE 1

TABLE NO. I.15

TIME SEC	ALT FT	INC DEG	VR FT/SEC	GAMMAR		
				NCE DEG	AZR DEG	
IGNITION BEGIN MINH	253.041	351277.61	99.275	-5.935	0.32.215	7.597
	253.041	351277.61	39.275	-5.935	9.32.215	-160.656
	269.000	367857.30	99.789	-6.208	5.623.028	5.668
	285.300	380844.43	100.255	-6.567	10.359.414	-160.702
	301.000	390249.45	100.679	-6.835	11.172.082	-160.753
	317.000	396720.63	101.067	-7.277	12.034.647	-160.823
	333.000	400106.65	101.422	-7.295	12.962.103	-160.894
	349.000	400364.12	101.752	-7.492	13.961.074	-160.974
	365.000	399309.50	102.057	-7.672	15.040.194	-161.060
	381.000	396070.62	102.391	-7.936	16.210.660	-161.154
	397.000	391568.07	102.607	-7.985	17.407.053	-161.255
	413.000	396335.77	102.358	-8.122	18.198.788	-161.364
	418.888	384443.30	102.947	-8.269	19.940.714	-161.480
	429.000	381353.27	103.091	-8.245	20.407.556	-161.524
	445.000	377216.90	103.292	-8.547	21.938.231	-161.602
	461.000	374538.79	103.467	-8.433	23.469.750	-161.729
	477.000	374195.25	103.621	-8.555	25.000.223	-161.855
	485.231	375106.30	103.692	-8.538	25.787.411	-161.984
	485.231	375106.30	103.692	-8.538	25.787.411	-162.051
INJECTION	485.231	375106.30	103.692	-8.538	25.787.411	-162.051

INJECTION

SA+T/EL-24

MISSION-3A/MCR-500/ACA/RTLS POINT TC NOM MEKO

CAST 1

TABLE NO. I.16

	MACH	LB/FT•°2	0	ALPHA DEG	BETA DEG	GAL/HA LB•DEG/FT•°2	GBETA LB•DEG/FT•°2
IGNITION SEC	8.687	.013	4.455	-7.02	.059	-0.009	
IGNITION MINA	253.041	.013	4.455	-7.02	.059	-0.009	
253.041	8.687	.013	4.455	-7.02	.059	-0.009	
269.000	8.734	.007	3.262	-7.74	.023	-0.005	
285.000	8.823	.005	2.336	-7.51	.011	-0.003	
301.000	9.115	.004	1.048	-7.84	.006	-0.003	
317.000	9.435	.003	1.168	-9.03	.004	-0.003	
333.000	9.892	.002	.871	-9.18	.003	-0.003	
349.000	10.593	.004	.734	-9.30	.003	-0.003	
365.000	11.547	.005	.739	-8.78	.003	-0.004	
381.000	12.770	.006	.869	-3.44	.005	-0.005	
397.000	14.182	.009	1.110	-9.46	.010	-0.007	
413.000	15.710	.012	1.450	-9.45	.018	-0.010	
BEGIN CLIMIT	418.888	.014	1.598	-1.44	.022	-0.012	
429.000	17.329	.017	1.864	-3.42	.022	-0.015	
445.000	18.951	.024	2.297	-8.12	.054	-0.020	
461.000	20.522	.030	2.744	-3.43	.084	-0.026	
477.000	21.902	.035	3.200	-8.47	.113	-0.035	
485.231	22.492	.036	3.447	-8.99	.124	-0.030	
485.231	22.497	.036	3.447	-8.99	.124	-0.030	
485.231	22.492	.035	3.447	-8.99	.124	-0.030	

INJECTION

SA+I/IL-24

MISSION-24/MCR-3LC/ACA/RTLS PCINT TC NCM MECO

CASE 1

TIME SEC	THRUST LBS	WEIGHT LBS	AXIAL FORCE LBS	NORMAL FORCE LBS	SIDE FORCE LBS	LONG ACC G'S	NORMAL ACC G'S
IGNITION	1410000.0	992719.0	-2495.2	2.3	.8	1.3980	.3272
BEGIN MINH	1410000.0	983719.0	-2405.4	2.3	.8	1.3980	.3272
269.000	1410000.0	934234.1	-2459.8	.3	.4	1.4725	.3424
285.000	1410000.0	884723.4	-2491.6	.2	.2	1.5555	.3593
301.000	1410000.0	835162.9	-2492.4	.1	.2	1.6364	.3779
317.000	1410000.0	785622.2	-2452.5	.0	.2	1.7521	.3988
333.000	1410000.0	756041.5	-2431.2	.0	.2	1.8719	.4223
349.000	1410000.0	686480.9	-2490.6	-.2	.2	2.0C79	.4490
365.000	1410000.0	636920.3	-2488.4	-.0	.3	2.1651	.4795
381.000	1410000.0	587359.6	-2484.6	-.0	.4	2.3489	.5150
397.000	1410000.0	537799.0	-2479.2	.1	.0	2.5567	.5565
412.000	1410000.0	488238.4	-2471.6	.4	.0	2.8287	.6061
418.999	1410000.0	470000.0	-2468.2	.5	1.0	2.9790	.6269
429.000	1319132.5	439710.8	-2461.4	.9	1.2	2.9404	.6221
445.500	1137163.9	395721.2	-2448.3	1.8	1.7	2.3425	.6148
461.000	1068383.9	356128.0	-2475.1	3.2	2.1	2.9446	.6079
477.000	961493.7	320494.6	-2423.3	4.7	2.5	2.9487	.5012
485.231	910723.9	302576.3	-2420.6	5.4	2.5	2.9476	.5979
485.231	1410000.0	303576.3	-2420.5	5.4	2.5	2.9478	.5979
485.231	1410000.0	303576.3	-2420.6	5.4	2.5	2.9534	.6257

INJECTION

SA+I/IL-24

MISSION-TA/MCR-500/ADA/RTLS POINT TO NOM MECO

CASE 1

TABLE NO. I.1a

	TIME SEC	CHIR DEG	CHYY DEG	DELPC DEG
IGNITION BEGIN MINH	253.041	180.000	-89.436	.000
BEGIN MINH	253.041	190.000	-89.436	.000
269.000	180.000	-90.550	.000	-13.115
285.000	180.000	-91.661	.000	-13.028
301.000	180.000	-92.767	.000	-12.938
317.000	180.000	-93.869	.000	-12.938
333.000	180.000	-94.967	.000	-12.755
349.000	180.000	-96.101	.000	-12.626
365.000	180.000	-97.151	.000	-12.510
381.000	180.000	-98.236	.000	-12.387
397.000	190.000	-99.316	.000	-12.256
413.000	180.000	-100.391	.000	-12.115
418.888	180.000	-100.785	.000	-12.061
429.000	180.000	-101.462	.000	-11.988
445.000	180.000	-102.542	.000	-11.826
461.000	180.000	-103.634	.000	-11.685
477.000	180.000	-104.737	.000	-11.561
485.231	190.000	-105.308	.000	-11.477
485.231	180.000	-105.308	.000	-11.497
485.231	190.000	-105.308	.000	-11.477

SA-1/EL-24

MISSION-3A/MCR-500/AOA/RTLS POINT TO NOME MECD

CASE 1

TABLE NO.1.19

	RANGE NM	TIP LAT DEG	TIP LONG DEG	VCH FT/SEC	VTEAL FT/SEC
TIME SEC	253.041	162.1	2.5	-123.4	.000
IGNITION BEGIN MIN	253.041	162.1	2.5	-123.4	.000
	269.000	185.9	2.9	-123.7	755.123
	285.000	211.6	3.3	-123.9	1553.388
	301.000	239.4	3.8	-124.2	2397.683
	317.000	269.4	4.2	-124.5	3293.645
	333.000	301.6	4.9	-124.8	4248.010
	349.000	336.4	5.7	-125.2	5268.927
	365.000	373.3	5.9	-125.6	6366.380
	381.000	414.7	6.6	-126.0	7552.778
	397.000	457.7	7.3	-126.6	9843.823
	413.000	504.7	8.0	-127.2	10259.776
BEGIN LIMIT	418.389	522.9	8.3	-127.5	10917.349
	429.000	555.5	8.9	-128.1	11793.377
	445.000	610.2	9.8	-129.4	13337.729
	461.000	669.0	10.7	-131.4	14882.080
	477.000	731.7	11.7	-136.9	16426.431
INJECTION	485.231	765.5	12.3	-164.8	17220.872
	485.231	765.5	12.3	-164.8	17220.873
	485.231	765.5	12.3	-164.8	17220.873

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SA+I/EL-24

MISSION-3A/MCR-5CD/AOA/RTLS POINT TC NOM MECO

CASE 1

TABLE NO. I.20

	TIME SEC	X FT	Y FT	Z FT	XDOT FT/SEC	YDOT FT/SEC	ZDOT FT/SEC
IGNITION	253.041	212323C1.5	-217159.0	960535.7	-1133.210	8480.549	
BEGIN MIMH	253.041	212328D1.5	317159.0	960535.7	-1133.210	3490.549	
	269.000	21242694.7	337185.8	111521.5	457.247	-1125.815	2192.764
	285.000	21247569.2	-353136.8	1254607.8	125.039	-1117.398	9349.242
	301.000	21246688.7	-370959.3	1420135.7	-212.324	-1109.757	10749.634
	317.000	21240331.2	-398646.8	1599865.5	-559.937	-1101.113	11600.193
	333.000	21229755.2	-406192.9	1791645.1	-914.978	-1092.073	12507.262
	349.000	21211136.0	-423591.0	1039435.0	-1232.012	-1092.620	13478.521
	365.000	21187661.7	-440834.8	2223345.7	-1662.112	-1072.761	14523.448
	381.000	21157327.1	-457217.2	2454647.8	-2057.466	-1062.435	15653.381
	397.000	21121726.5	-474832.2	2724855.0	-2470.926	-1051.824	16884.867
	413.000	21079741.7	-431573.4	3055593.6	-2006.123	-1043.750	18235.900
	418.838	21061442.1	-497689.1	3114526.5	-3072.662	-1036.575	18768.188
	429.000	21029587.2	-509134.1	3309026.0	-3369.302	-1022.274	19638.823
	445.000	2L970785.7	-524508.0	2625594.8	-362.205	-1017.402	21165.651
	461.000	20904826.1	-540693.9	3936277.8	-4398.013	-1005.141	22624.396
	477.000	20830400.2	-516670.5	4259876.9	-4945.542	-992.497	24073.857
	485.231	20783270.3	-564812.1	4551075.2	-5244.511	-935.345	24315.476
	485.231	20783270.3	-564812.1	4551075.2	-5244.611	-985.845	24815.476
	485.231	20783270.3	-564812.1	4551075.2	-5244.611	-135.845	24915.476

MISSION-?A/MCR-5LO/ADA/RTLS POINT TC NOM MECO

CASE 1

TABLE NO. I.21

	TIME SEC	XACC FT/SEC*2	YACC FT/SEC*2	ZACC FT/SEC*2	HEAT BTU/FT*2-S	HEAT RATE
IGNITION	253.341	-20.1556	.4508	43.5276	.0	.0
BEGIN MINH	253.041	-20.1556	.4508	43.5276	.0	.0
269.000	-20.5045	.4763	45.9297	3.3	.2	
285.000	-20.9130	.5017	48.5709	6.3	.2	
301.000	-21.3981	.5272	51.5226	9.3	.2	
317.000	-21.9395	.5526	54.8536	12.6	.2	
333.000	-22.5815	.5781	58.6592	15.3	.3	
349.000	-23.3296	.6035	62.8562	20.8	.3	
365.000	-24.2065	.6283	67.8421	26.6	.4	
381.000	-25.2427	.6543	73.6175	34.2	.6	
397.000	-26.4776	.6796	80.4557	44.8	.8	
413.000	-27.9720	.7047	88.6292	59.7	1.1	
418.389	-28.6030	.7139	32.1586	66.6	1.2	
429.000	-29.8638	.7296	51.9032	80.6	1.5	
BEGIN CLIMB	445.300	-31.8675	.7547	91.4357	109.5	2.1
461.600	-33.8562	.7794	90.8539	148.3	2.7	
477.000	-35.8316	.8021	90.2761	197.4	3.4	
485.231	-36.8387	.8141	89.9297	226.5	3.7	
INJECTION	485.231	-36.8387	.8141	89.9297	226.5	3.7
	485.231	-40.3567	.8141	142.777	226.5	3.7

SECTION II

EXCHANGE RATIOS

A. Discussion

After a baseline launch vehicle system is defined, there are design variations that occur during detailed development phases. These variations may be advantageous or disadvantageous. The effects of these variations on delivered performance must be continuously analyzed. This can be done by performing a trajectory simulation with the changes evaluated. A more cost effective method is the use of exchange ratios, sometimes called payload partials whose primary purpose is to provide a quick and economical assessment of design variations on the payload delivery capability in the region near the baseline. Exchange ratios are used by multiplying a change of a baseline parameter by its corresponding exchange ratio to define the performance change at MECO. Combining these data with similar cost analyses data, trade studies may be performed to define the minimum cost impact required to recover performance capability lost due to design changes. A secondary use is to increase the baseline capability using the same methodology. The final test of any proposed change is the trajectory simulation containing all the proposed changes. This will define the new baseline payload capability and then the exchange ratios may be used during the next design cycle.

As stated in Section I the 3A Mission is the design reference (payload critical) mission. The exchange ratios contained herein are generated to describe the effects of a 'planned change' in the baseline system as compared to the random occurrence of unknown variations about the baseline as discussed in Section III. Exchange ratios are generated by changing each system parameter individually and simulating a maximum payload trajectory through the RTLS/AOA point of $V_R = 8932$ fps to the AOA and Nominal MECO conditions specified on Table I.1. This is done by optimizing the tilt over maneuver and closed loop guidance while limiting ET propellant consumption to maximum loaded value.

A change in the weight at AOA MECO provides a similar change in the gross payload (cargo bay plus consumables) weight. The case of Nominal MECO is not the same. At this point the change in MECO weight represents a change in gross payload from the AOA condition and a change in the ET propellant residuals. The residual increase or decrease is dependent upon whether the Nominal MECO exchange ratio is greater or less than at AOA MECO.

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Historically, exchange ratios have been assumed and used as linear values. This is generally valid in small regions about the baseline; but for some cases, the design parameters of max q and accelerations are violated and must be constrained. The method for constraining max q in this analysis is reducing the initial tilt-over (lofting) prior to max q which causes the vehicle to exit the dense atmosphere quicker. This results in a non-optimum trajectory and a resulting payload improvement less for a given system change than the non-constrained results. Detailed SSME throttling prior to max q was not investigated.

A rule of thumb for use of exchange ratios is that the unconstrained ratios are used when payload is degraded or when recovering payload lost due to design refinements and the constrained curves are used when trying to increase the baseline performance.

B. Description of Results

A summary of linearized exchange ratios for both AOA MECO and Nominal MECO is shown in Table II.1. The exchange ratios for each deviation are shown in terms of Δ gross payload per unit parameter change at AOA MECO. At Nominal MECO the exchange ratio is labeled as Δ MECO weight per unit change and includes the change in AOA gross payload and ET residuals.

Figures II.1 through II.17 display Δ weight for both AOA and Nominal MECO conditions for unconstrained trajectory results. Figures II.1, 6, 7, 8, 9, 10, 12 and 17 include the effects at AOA MECO when the trajectory must be reshaped to meet the dynamic pressure design constraint. These constrained curves emphasize that the exchange ratios must be used correctly in order to obtain valid results.

A method of recovering the performance losses due to meeting the constraints is by reoptimizing the trajectory portion past the time of max q to SRB staging. The system parameter chosen for this illustration is SSME thrust variation. Figure II.17 shows weight losses for a 30000 pound increase of vacuum thrust per engine of about 1000 pounds for the constrained q case as compared to 6400 pounds gain for the unconstrained q case. By optimizing the flight path profile after max q has been passed, a net gain of 3100 pounds weight can be attained as shown on Figure II.18. This example stresses that linear exchange ratios are valid only when used for small deviations about the baseline. In order to increase the baseline performance, it is more realistic to perform detailed analysis than to use the exchange ratios where design constraints are violated.

MISSION 3A

TABLE II.1 EXCHANGE RATIOS*

PARAMETER VARIED	@ AOA MECO Δ PAYLOAD Δ PARAMETER	@ NOMINAL MECO Δ MECO WEIGHT ** Δ PARAMETER
FOREBODY DRAG (C_{A_0})	- 84 lb/%	- 94 lb/%
BASE DRAG	- 20 lb/%	- 28 lb/%
SRB SEPARATION DELAY	-185 lb/s	-200 lb/s
SRB VACUUM ISP (CONSTANT THRUST)	300 lb/s	330 lb/s
SRB VACUUM ISP (CONSTANT W)	810 lb/s	880 lb/s
SRM VACUUM THRUST (CONSTANT ISP)	664 lb/%	720 lb/%
SRM VACUUM THRUST (CONSTANT W)	2,120 lb/%	2,300 lb/%
SRB INERT WEIGHT	-.093 lb/lb	-.1 lb/lb
SRB PROPELLANT CAPACITY	.024 lb/lb	.025 lb/lb
SRB PROPELLANT TEMPERATURE	90 lb/deg F	100 lb/deg F
LAST RTLS - RELATIVE VELOCITY	3.3 lb/fps	1.2 lb/fps
ET PROPELLANT CAPACITY (NO ET INERT WT CHANGE)	.061 lb/lb	-
ET PROPELLANT CAPACITY (ET INERT WT CHANGE)	.015 lb/lb	-
SSME VACUUM ISP (CONSTANT THRUST)	1,090 lb/s	865 lb/s
SSME VACUUM ISP (CONSTANT W)	1,360 lb/s	1,100 lb/s
SSME VACUUM THRUST (CONSTANT W)	.4 lb/lb	.43 lb/lb
SSME VACUUM THRUST (CONSTANT ISP)	.08 lb/lb	.07 lb/lb

* LINEARITY ASSUMED OVER SMALL VARIATIONS

** REPRESENTS Δ PAYLOAD + Δ ET PROPELLANT RESERVE AT MECO

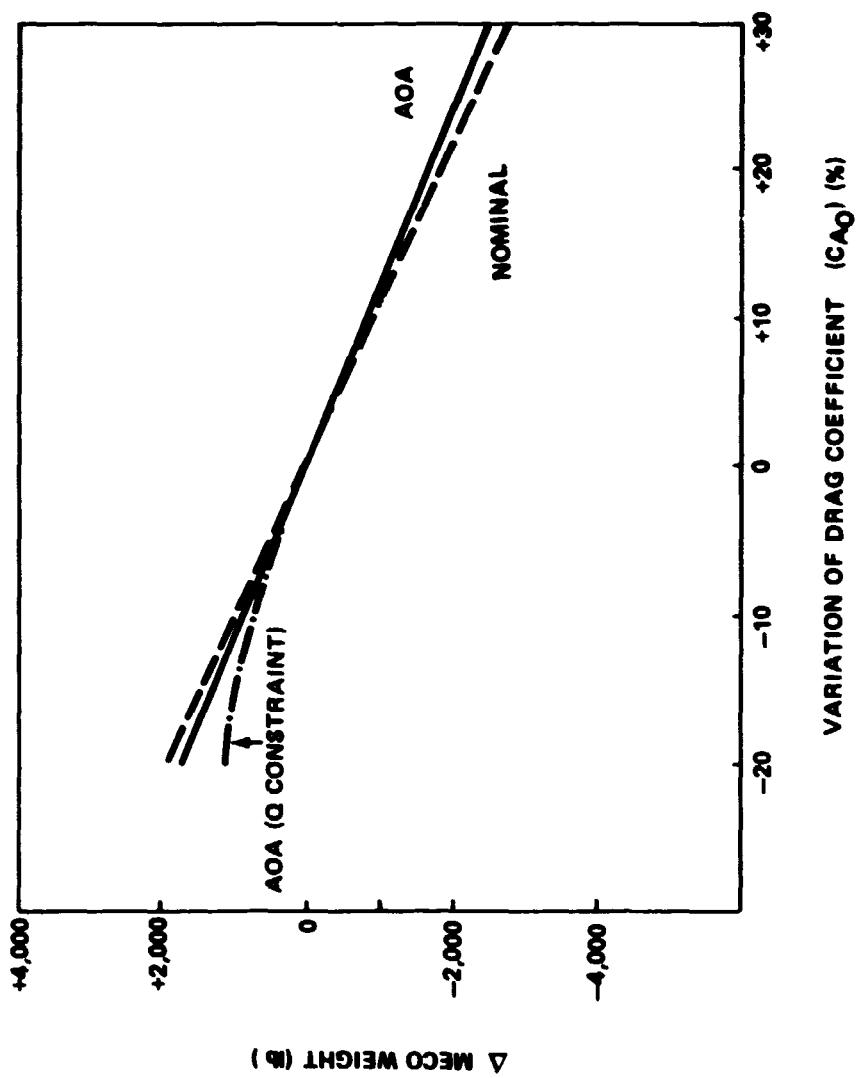


FIGURE II. 1 MECO WEIGHT VARIATION WITH VARIATION OF FOREBODY AXIAL FORCE COEFFICIENT CA_0

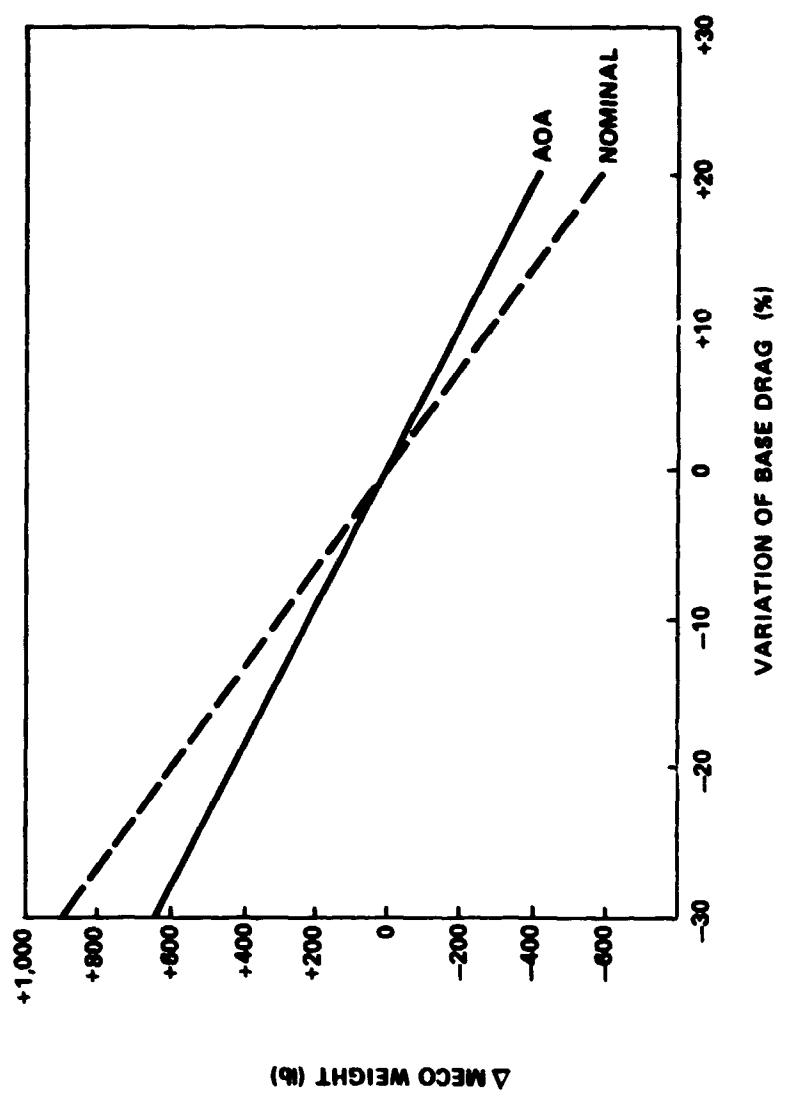


FIGURE II. 2 MECO WEIGHT VARIATION WITH VARIATION OF THE BASE DRAG

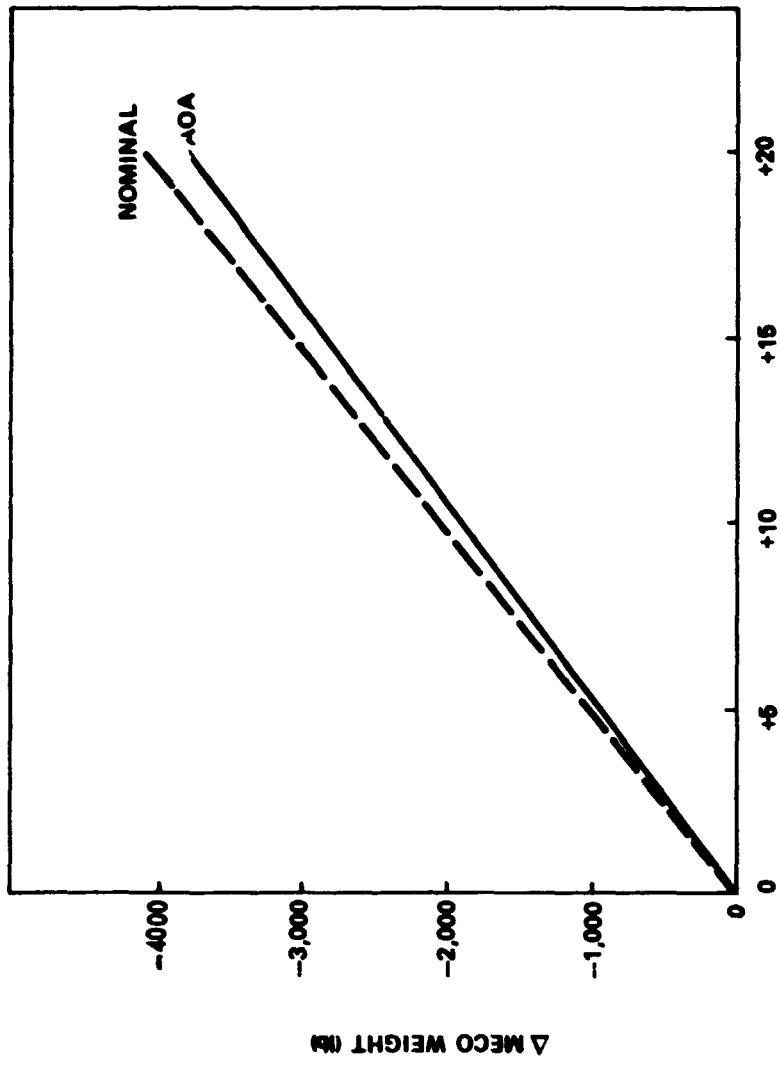


FIGURE II. 3 MECO WEIGHT VARIATION WITH VARIATION OF SRB SEPARATION DELAY TIME WITH NO THRUST

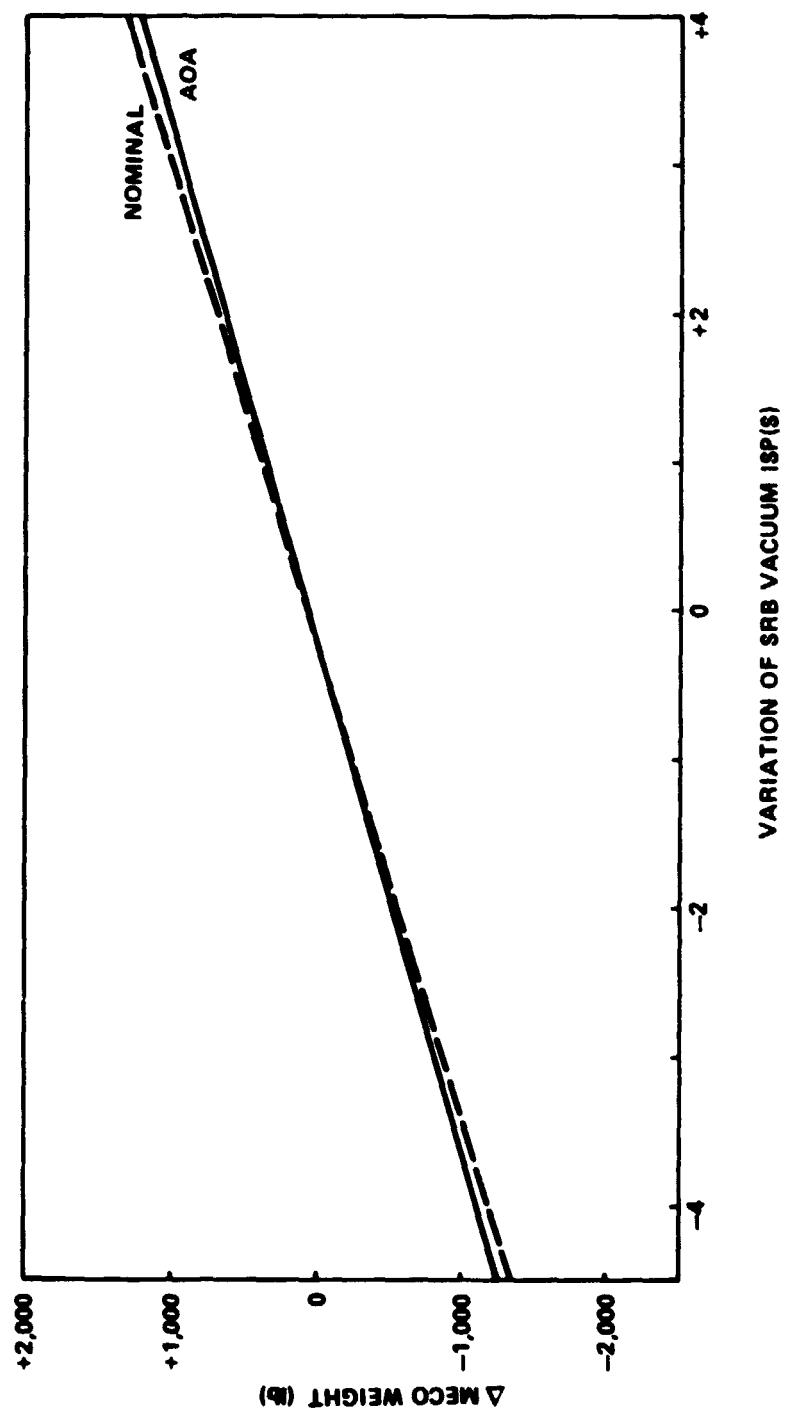


FIGURE 11. 4 MECO WEIGHT VARIATION WITH VARIATION OF SRB VACUUM ISP WITH CONSTANT SRB VACUUM THRUST TRACE

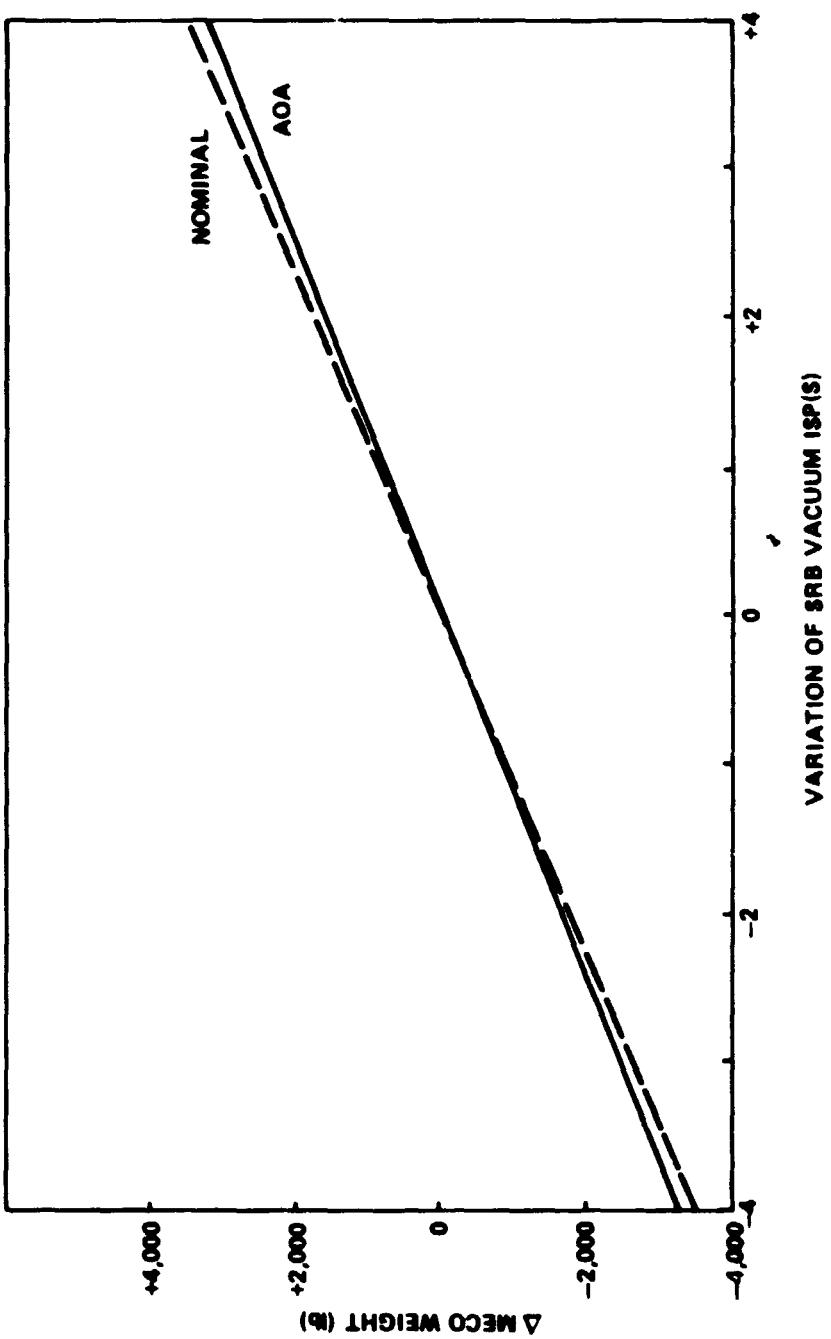


FIGURE II. 5 MECO WEIGHT VARIATION WITH VARIATION OF SRB VACUUM ISP
WITH CONSTANT SRB PROPELLANT LOADING

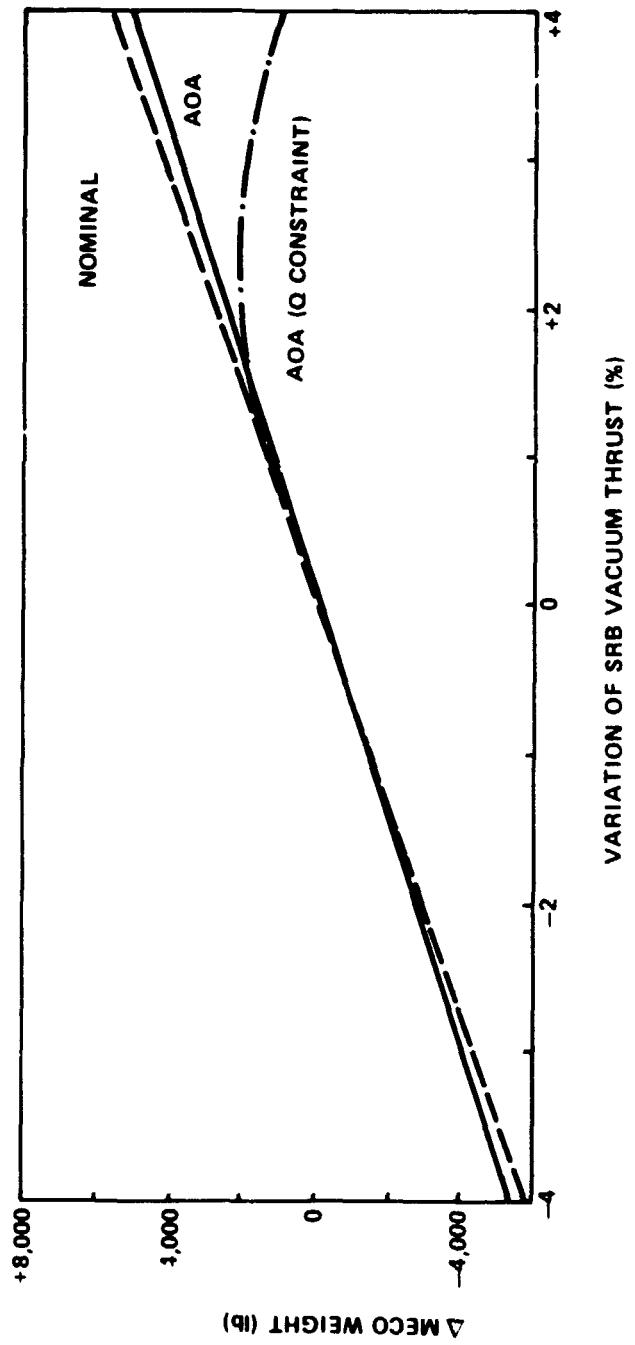


FIGURE I. 6 MECO WEIGHT VARIATION WITH VARIATION OF SRB VACUUM THRUST WITH CONSTANT VACUUM ISP

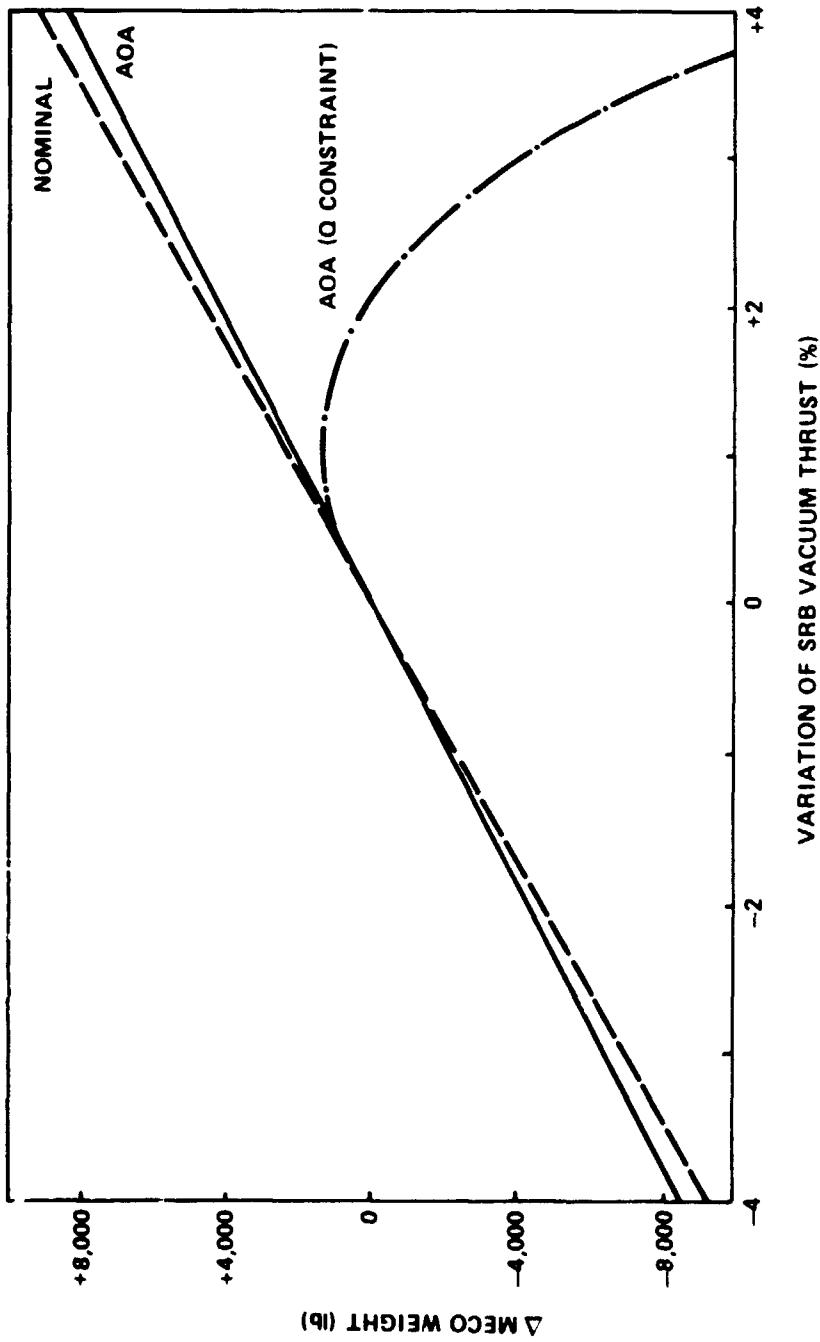


FIGURE II. 7 MECO WEIGHT VARIATION WITH VARIATION OF SRB VACUUM THRUST WITH CONSTANT SRB PROPELLANT LOADING

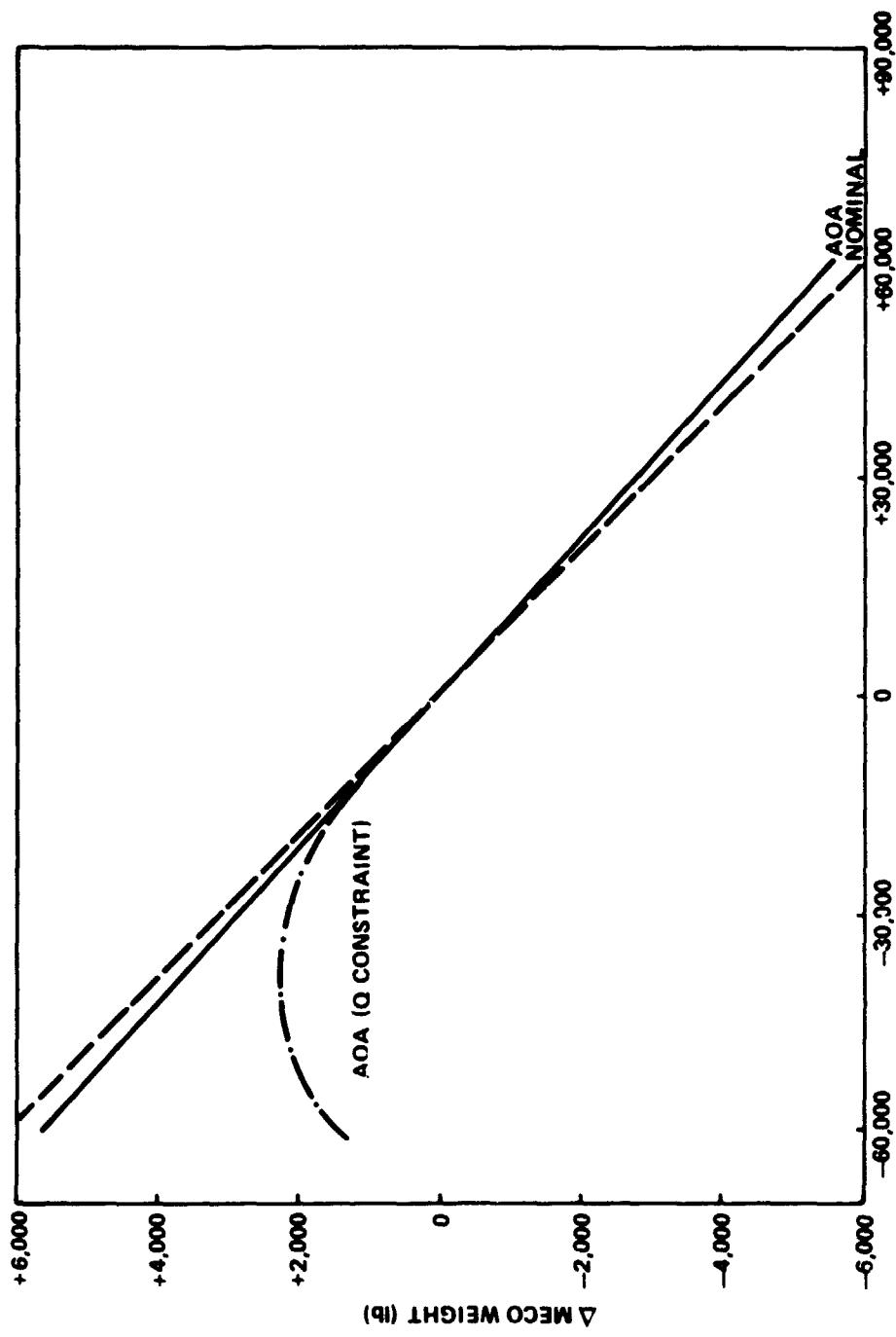


FIGURE II. 8 MECO WEIGHT VARIATION WITH VARIATION OF TOTAL SRB INERT WEIGHT
VARIATION OF TOTAL SRB INERT WEIGHT (lb)

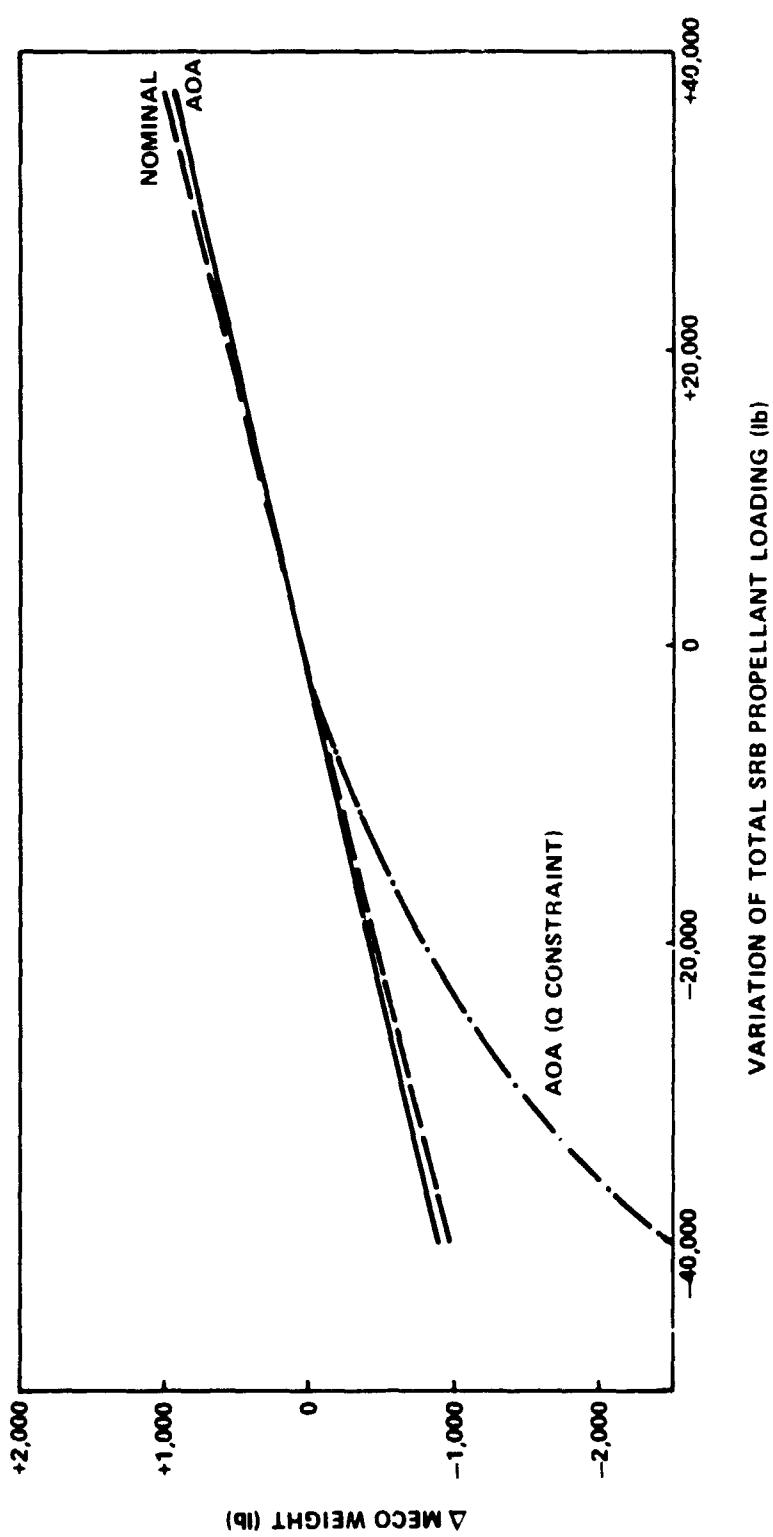


FIGURE II. 9 MECO WEIGHT VARIATION WITH VARIATION OF SRB TOTAL PROPELLANT LOADING

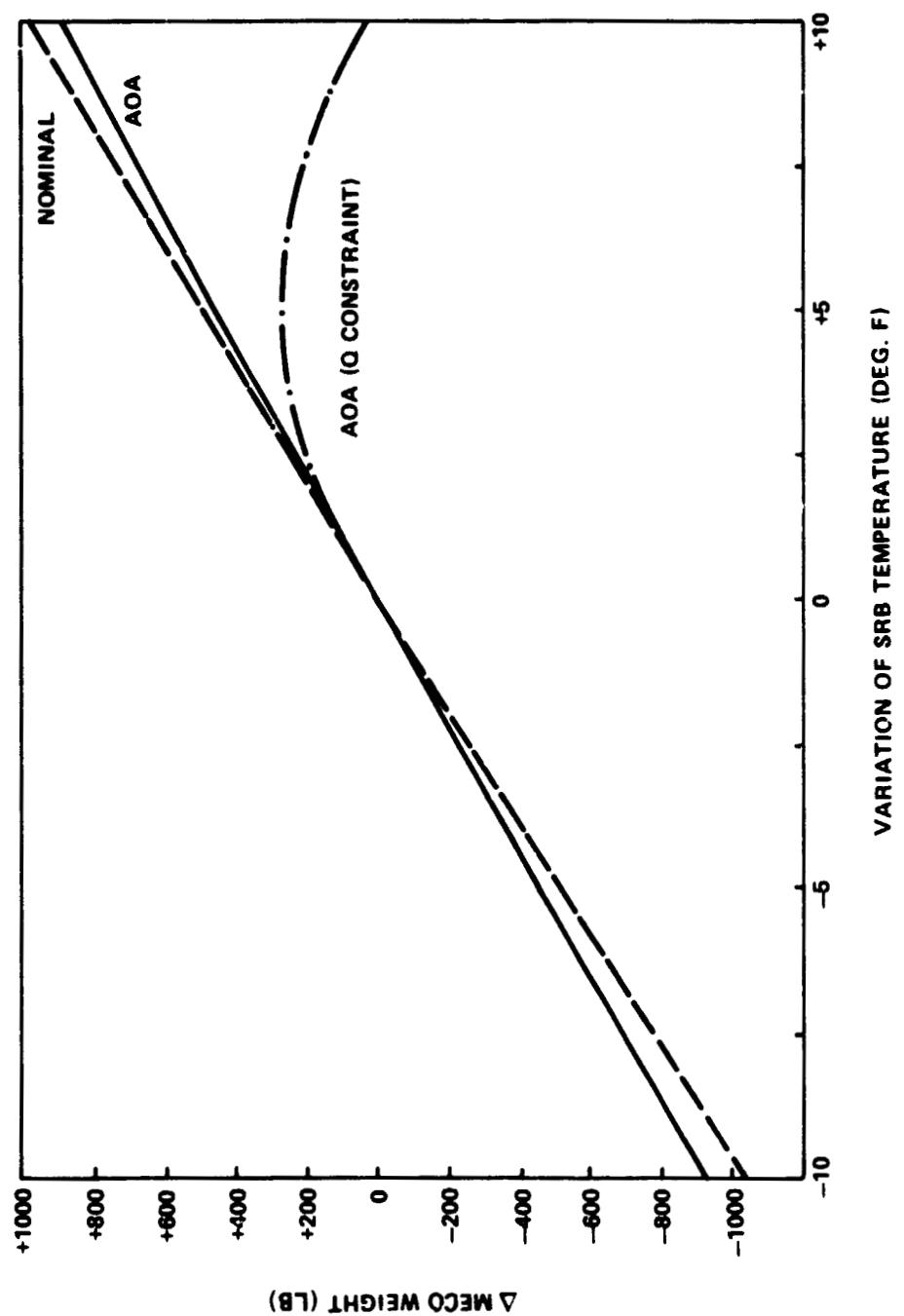


FIGURE II. 10 MECO WEIGHT VARIATION WITH VARIATION OF SRB PROPELLANT TEMPERATURE

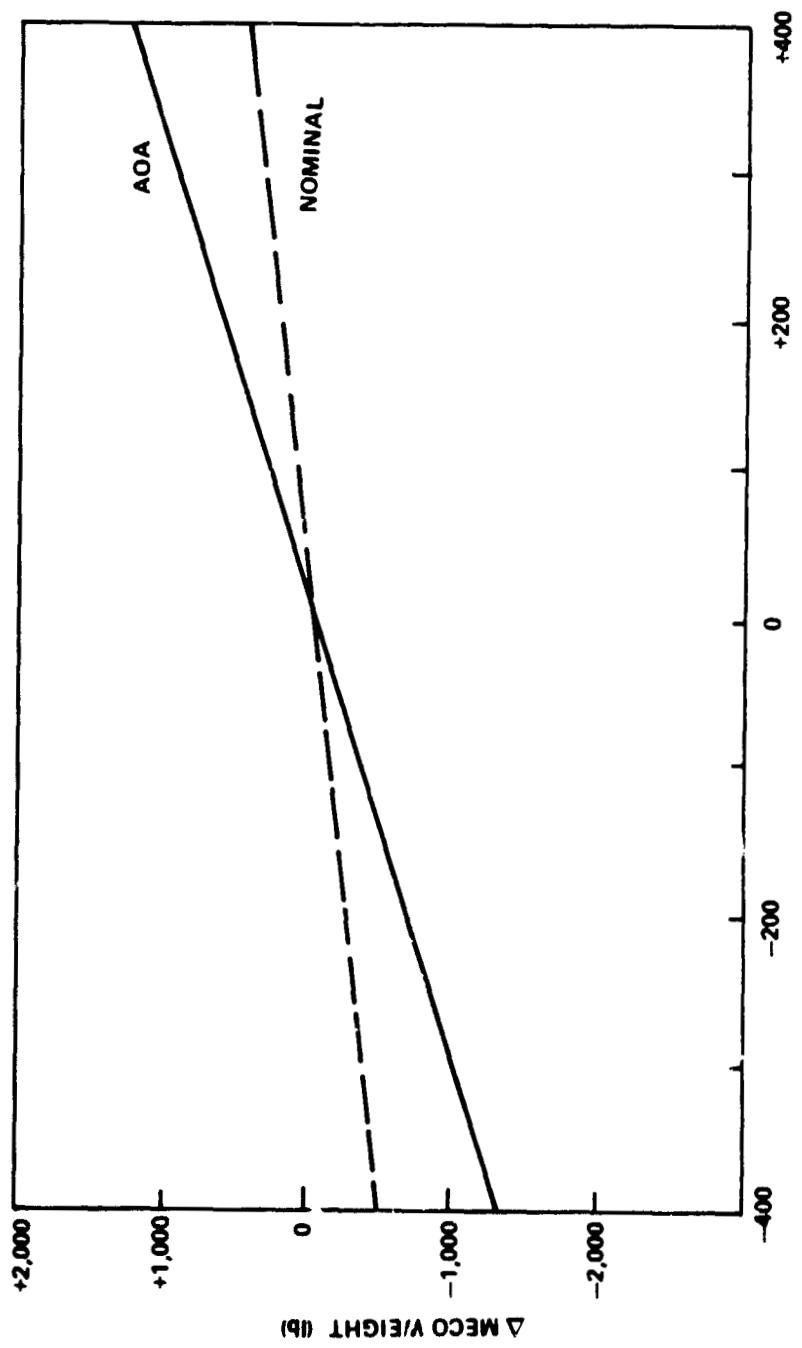


FIGURE II. 11 MECO WEIGHT VARIATION WITH VARIATION OF RELATIVE VELOCITY AT LAST RTLS POINT

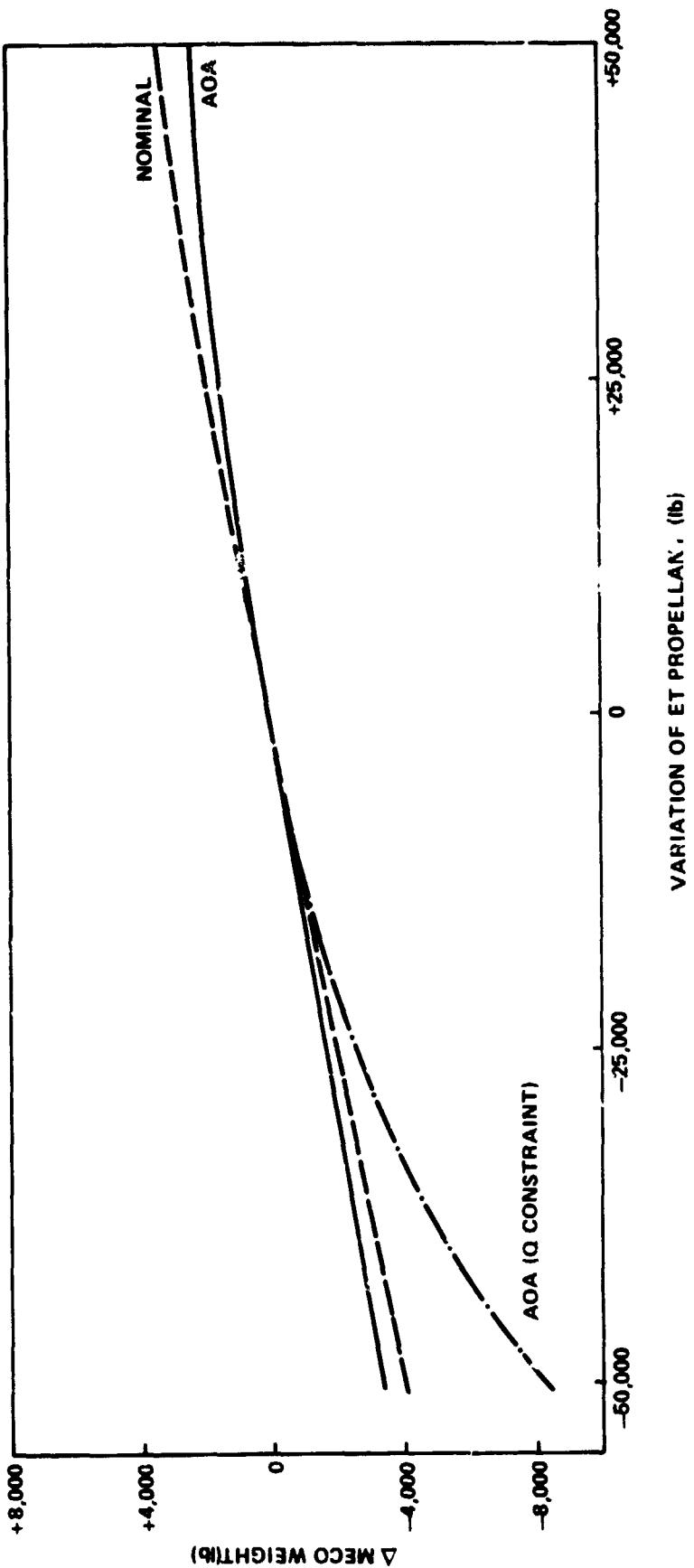


FIGURE II. 12 MECO WEIGHT VARIATION WITH VARIATION OF ET PROPELLANT AND
CONSTANT ET INERT WEIGHT

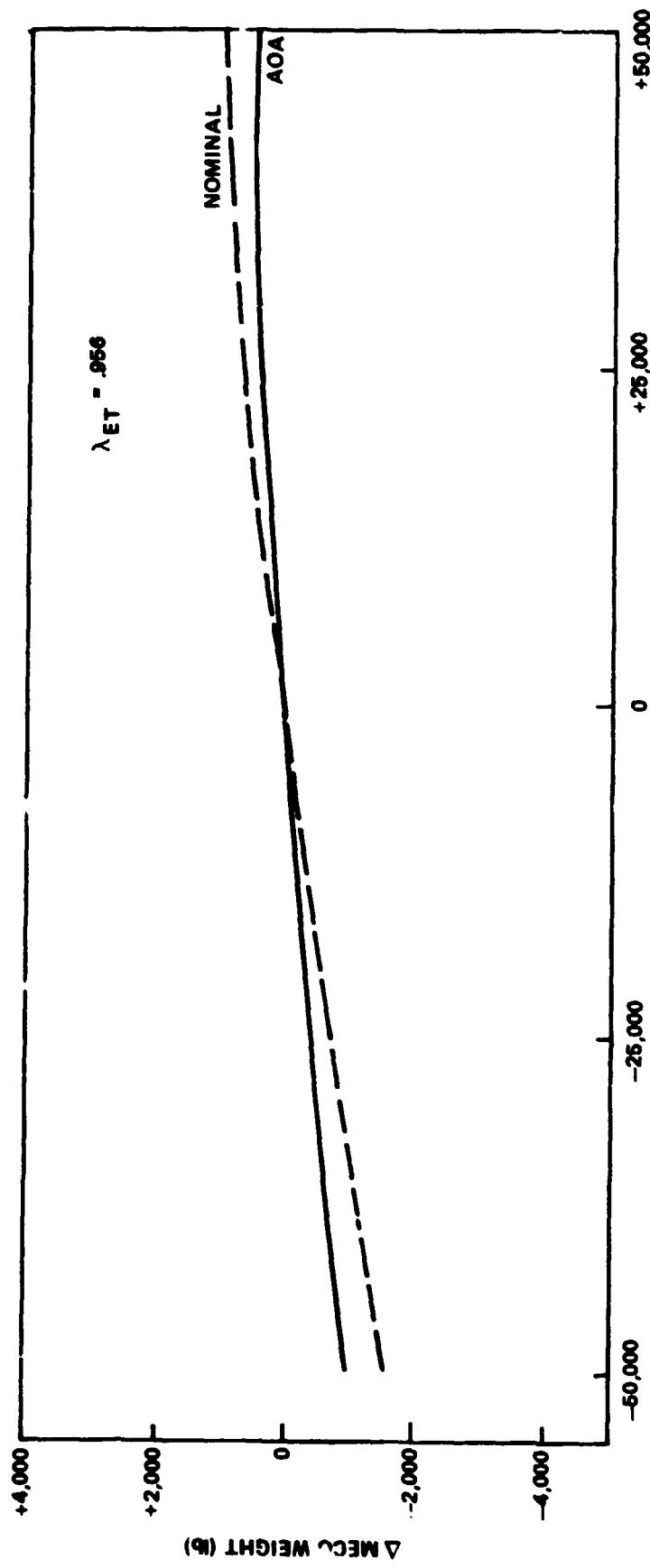


FIGURE II.13 MECO WEIGHT VARIATION WITH VARIATION OF ET PROPELLANT AND ET INERT WEIGHT WITH CONSTANT ET MASS FRACTION

VARIATION OF ET PROPELLANT (lb)

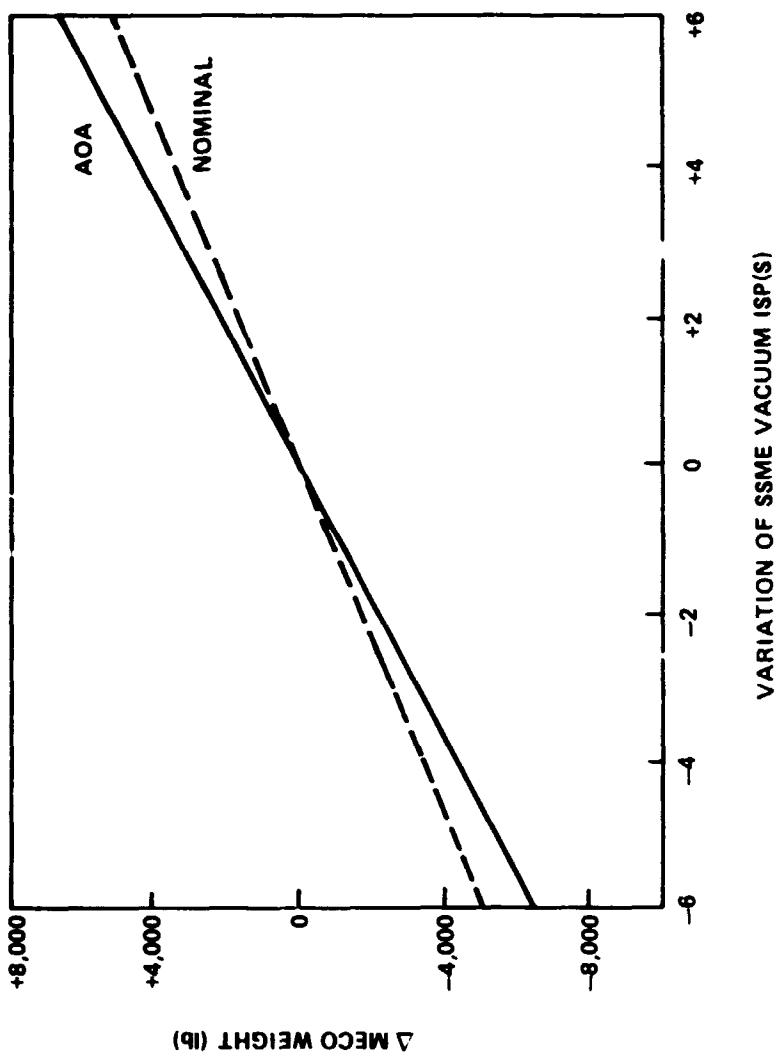


FIGURE II. 14 MECC WEIGHT VARIATION WITH VARIATION OF SSME VACUUM ISP
WITH CONSTANT SSME VACUUM THRUST

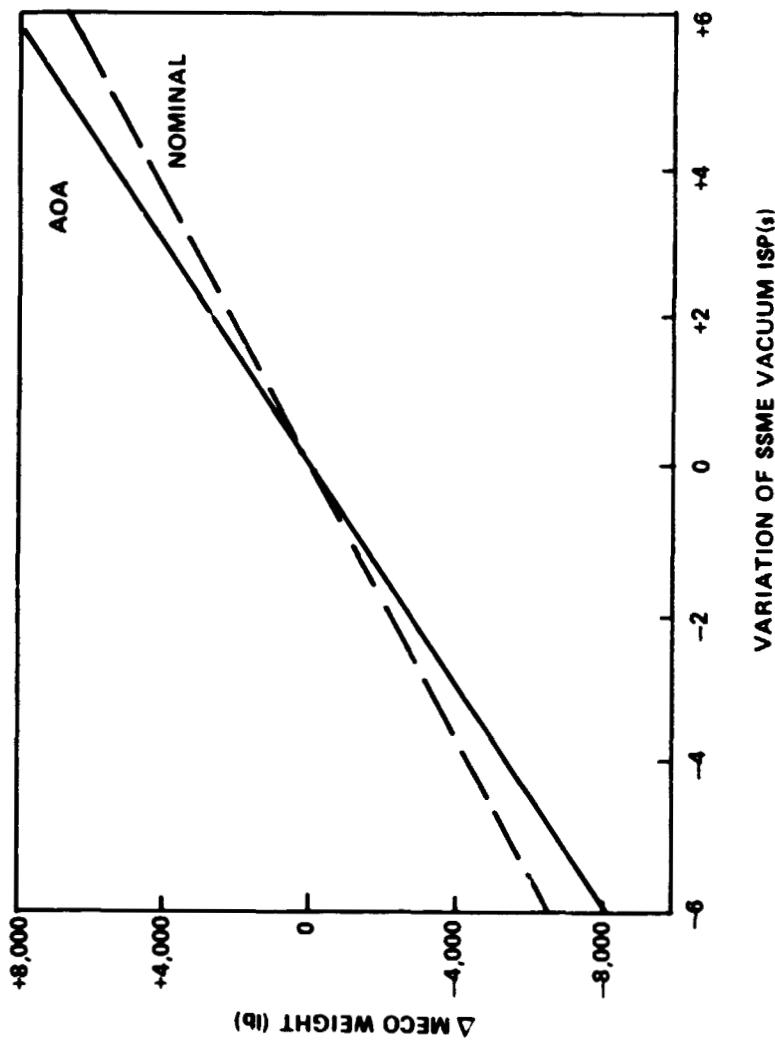


FIGURE II. 15 MECO WEIGHT VARIATION WITH VARIATION OF SSME VACUUM ISP WITH CONSTANT SSME FLOW RATE

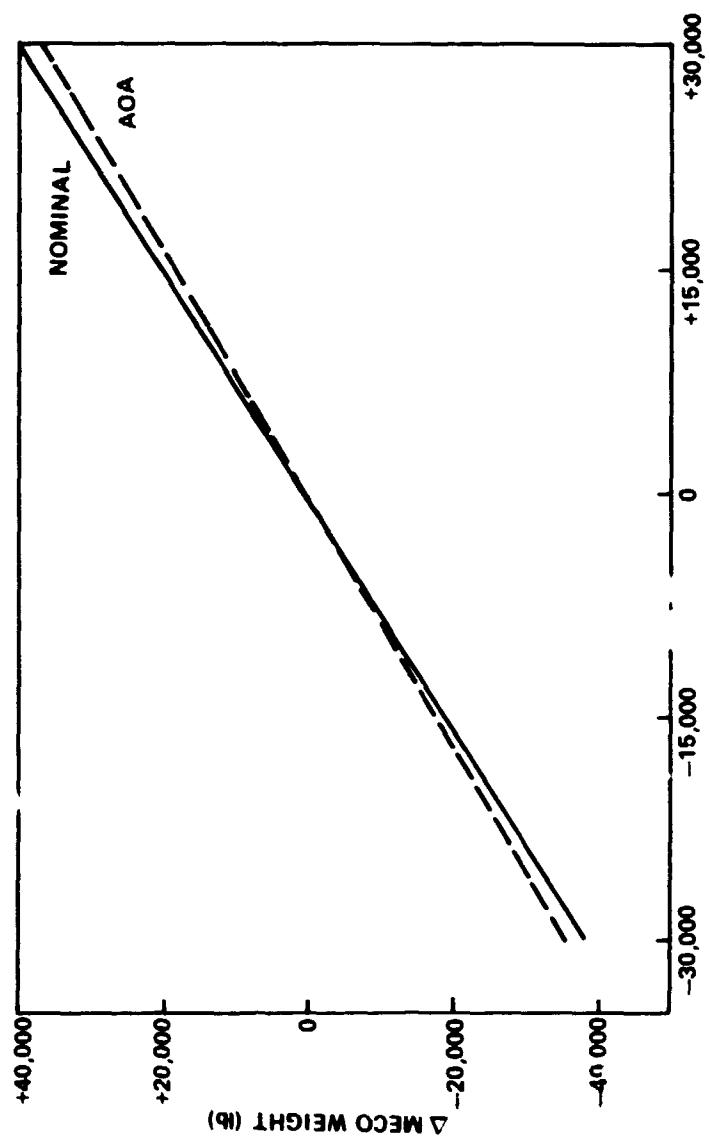


FIGURE II. 16 MECO WEIGHT VARIATION WITH VARIATION OF SSME VACUUM THRUST WITH CONSTANT PROPELLANT FLOW RATE

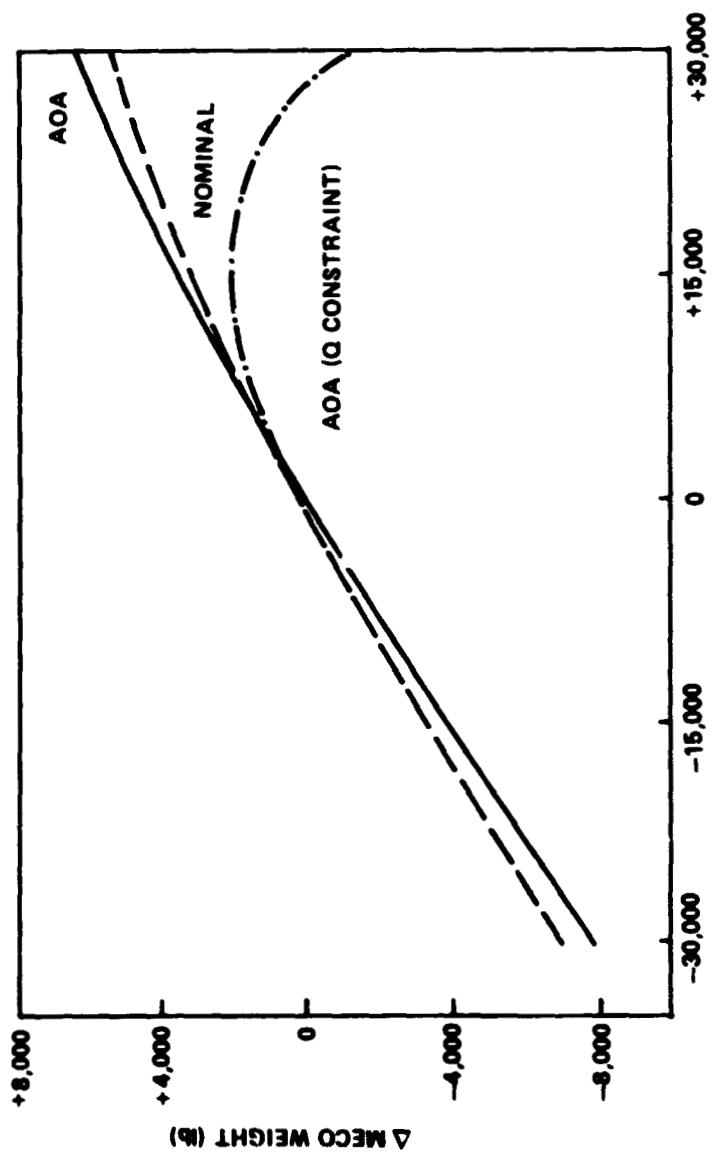


FIGURE II. 17 MECO WEIGHT VARIATION WITH VARIATION OF SSME VACUUM THRUST
WITH CONSTANT VACUUM ISP

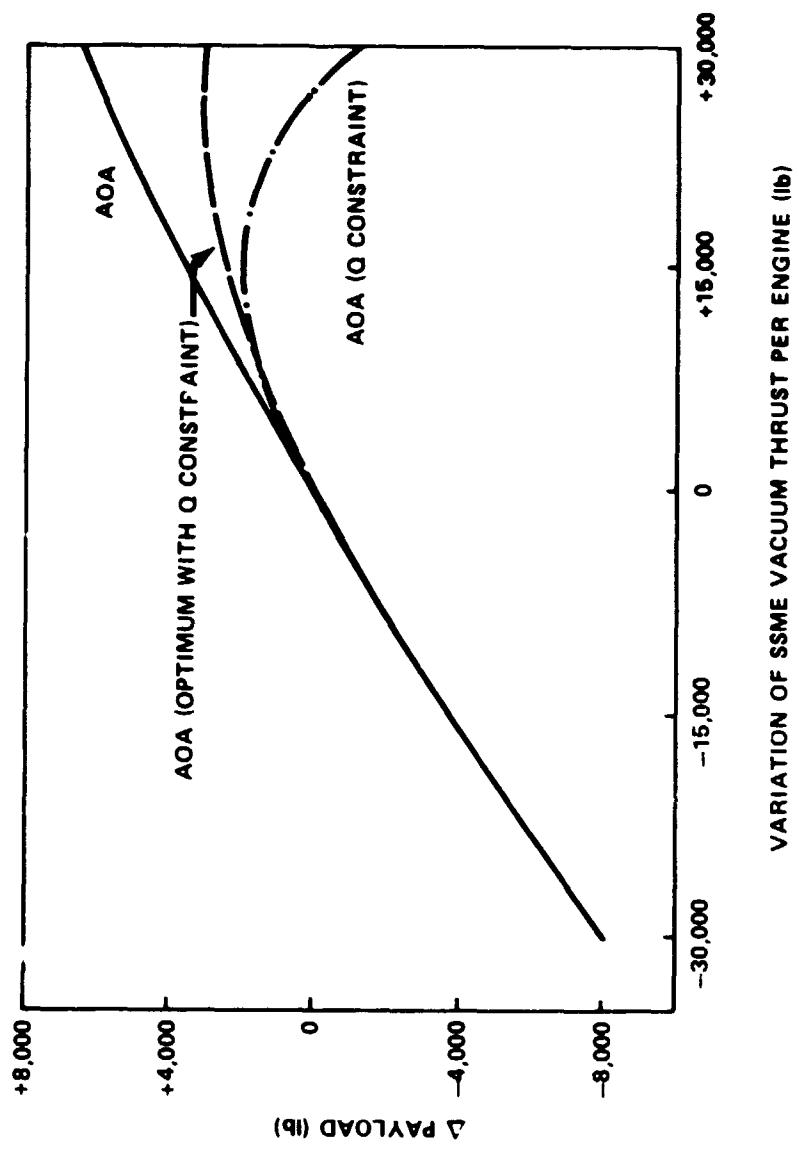


FIGURE II. 18 EFFECT OF OPTIMIZATION OF BOOST FLIGHT ON PAYLOAD VARIATIONS FOR VARIATIONS OF SSME VACUUM THRUST WITH CONSTANT VACUUM ISP

SECTION III

DESIGN ENVIRONMENT AND FLIGHT PERFORMANCE RESERVES

A. Discussion

The purpose of this section is to develop a set of ascent trajectory induced design environments and flight performance reserve (FPR) propellant requirements using the same techniques as previously used on the Saturn class of launch vehicles. Every vehicle is initially designed to some nominal set of parameters and conditions at a given safety factor. It is assumed that each parameter is independent, normally distributed, and exhibits a known extreme tolerance defined as a 3σ deviation. This says that for 99.74% of the time a given item will operate within its $\pm 3\sigma$ limits. This uncertainty is accounted for by providing design envelopes of key trajectory characteristics which the vehicle is predicted to stay within 99.74% of the time. The propellant variations at MECO (FPR) are analyzed to assure attainment of MECO 99.87% of the time. Therefore, each parameter may be investigated at its extreme tolerance and the deviated trajectory results combined by the root-sum-squared method. This is the technique used for the results presented in this section.

The trajectories to ACA and Nominal conditions of Section I produce the baseline characteristics for this dispersion analysis. The analysis was performed by curve fitting the booster attitude tilt profile from liftoff to SRB staging versus relative velocity and reloading this into the trajectory simulator (Reference 6). This open loop attitude profile was held constant for all dispersion runs except for the boost steering error dispersion. The closed loop guidance was initiated at SRB staging, flying the same type profile as described in Section I. Each system component parameter was deviated from its baseline value by the amount listed in Table III.1 and a trajectory simulated. All deviated trajectories assumed orbiter engine #1 failure at a relative velocity of 8932 fps to define the last RTLS/first AOA interface. AOA and Nominal targeting trajectories were simulated from this point. The RTLS trajectories were not simulated. The following list of trajectory characteristics are investigated:

- o Maximum dynamic pressure
- o Maximum longitudinal acceleration during SRB burn
- o SRB staging state vector and dynamic pressure

- o RTLS/AOA point vector deviations and ET propellant consumed from liftoff (V_R held constant at 8932 fps)
- o Stagnation point heating
- o ET propellants consumed from liftoff to AOA MECO
- o ET propellants consumed from liftoff to Nominal MECO
- o Vehicle subpoint range from liftoff to AOA MECO and Nominal MECO

Extreme (maximum and minimum) envelopes which are possible to occur during a flight are generated for each trajectory characteristic.

Table III.1 lists the dispersion sources and the 3σ extreme values of each parameter. The atmospheric variations are listed as Hot day and Cold day correlated atmospheric models and are found in Reference 4. The wind data used are from Reference 4. The aerodynamic coefficient parameters were obtained from Reference 3. Contributions due to guidance, control, and navigation systems were not analyzed due to lack of complete definition and simulator limitations. These will be analyzed at a later time when preflight analyses are performed.

B. Induced Design Environments

As each dispersion trajectory was computed, the deviated values of trajectory characteristics to be investigated were calculated. These were then root-sum-squared to define the maximum deviation envelopes about the baseline. This was done by evaluating all the plus and minus deltas separately.

Figure III.1 displays the envelope of dynamic pressure the launch vehicle may encounter in the region about nominal time of maximum q from the baseline trajectory. It is observed the maximum value could reach 727 psf at 55 seconds flight time. The major contributions are SRB Web Action Time (52%) and Headwind (44%). Figure III.2 displays the stagnation point heating envelope for the AOA and Nominal missions. The major contributors to the maximum heating envelope are + SSME thrust (24%), - SRB WAT (9%), + boost steering error (10%), Hot day atmosphere deviation (37%), and SRM misalignment (17%). It should be noted the heating at AOA MECO is 143% that at Nominal MECO for the undispersed cases. It can also be noted that the maximum heating at Nominal MECO is only 82% of the minimum heating at AOA MECO. The detailed design of ET thermal protection should be performed on the AOA trajectory. The safety factor required will define what degree of heating to use. Table III.2 lists the deviation in state vector and dynamic pressure at SRB staging.

The deviation of maximum longitudinal acceleration experienced during SRB burn is included in Table III.2.

The RTLS/AOA point was assumed to be constant at a relative velocity of 8932 fps. Table III.3 displays the deviation in state vector and consumed ET propellant at that velocity. Currently, the on-board logic to determine this interface has not been determined. More analyses are required to define which parameter will be used to define this interface in the flight computer. Some candidates other than V_R are time or characteristic velocity. Table III.4 summarizes the deviations of MECO time and surface range from the launch site at both AOA and Nominal MECO. The launch vehicle was targeted to the conditions of Table I.1 for all cases simulated.

C. Flight Performance Reserves

In order to guarantee that the MECO targets may be attained for 99.87% of the time, an extra amount of usable mainstage propellants must be carried. These are known as Flight Performance Reserves (FPR). They are calculated by root-sum-squaring the positive (those above baseline) mainstage ET propellants expended from liftoff to MECO. Table III.5 lists the contributions to FPR for each dispersion source at AOA MECO and Nominal MECO. These contributions are at baseline SSME mixture ratio of 6:1. The mixture ratio uncertainty effects of the SSME and ET loading were combined statistically while optimizing the fuel bias quantity using the technique as defined in reference 5.

The FPR required for this mission is 6471 pounds at AOA MECO and 6661 pounds at Nominal MECO including fuel bias. The optimum fuel bias is 1150 pounds. The cause for the Nominal MECO FPR being greater than the AOA MECO FPR is that the trajectory is shaped for the AOA condition and the Nominal is 'branched' at the RTLS/AOA point.

The RSS of the negative quantities of ET propellants consumed yield the negative FPR or excess residuals at MECO. These result from over-performing launch vehicle parameters and are jettisoned with the ET. The negative FPR including fuel bias could be as great as 6366 pounds at AOA MECO or 6266 pounds at Nominal MECO.

When generating performance trajectories, an estimate of FPR is desired. This has been historically done by converting the FPR from a detailed analysis such as this to a percentage of the characteristic velocity from liftoff to MECO. The results of this analysis yield an equivalent ΔV of .0085 V_{char} at AOA MECO and .0087 V_{char} at Nominal MECO not including the fuel bias. The fuel bias is summed with normal residuals and is not recalculated for performance quotations.

TABLE III.1

DISPERSION SOURCE	3 σ VALUES
SRB Web Action Time *	± 4.71%
SRB Vacuum Specific Impulse *	± .5%
SRB Propellant Loading *	± .21%
SRB Staging Weight *	± .85%
SRB Staging Time	± .5 s
SRB Misalignment	± .5°
SSME Vacuum Thrust	± 6000 lb/Eng
SSME Vacuum Specific Impulse	± 2.3 s/Eng
SSME Misalignment	± .5°
SSME Mixture Ratio	± 1%/Eng
Orbiter & ET Inert Weight	± .81%
ET Propellant Loading	± .48%
Booster Steering Program	± .5°
Vehicle Center of Gravity	± 2 inches
Atmospheric	Hot/Cold day
Winds	Head/Tail Right/Left
Base Force	Reference 3
Aerodynamic Coefficients	Reference 3

NOTE: Orbiter Main Engine Variations Combined by
 $\text{Stage Variation} = N \text{ (Dispersion/Eng)}/\sqrt{N}$

Where N is number of engines operating i.e.
 N = 3 for Nominal, N = 2 for Abort

* Combined Stage Variation

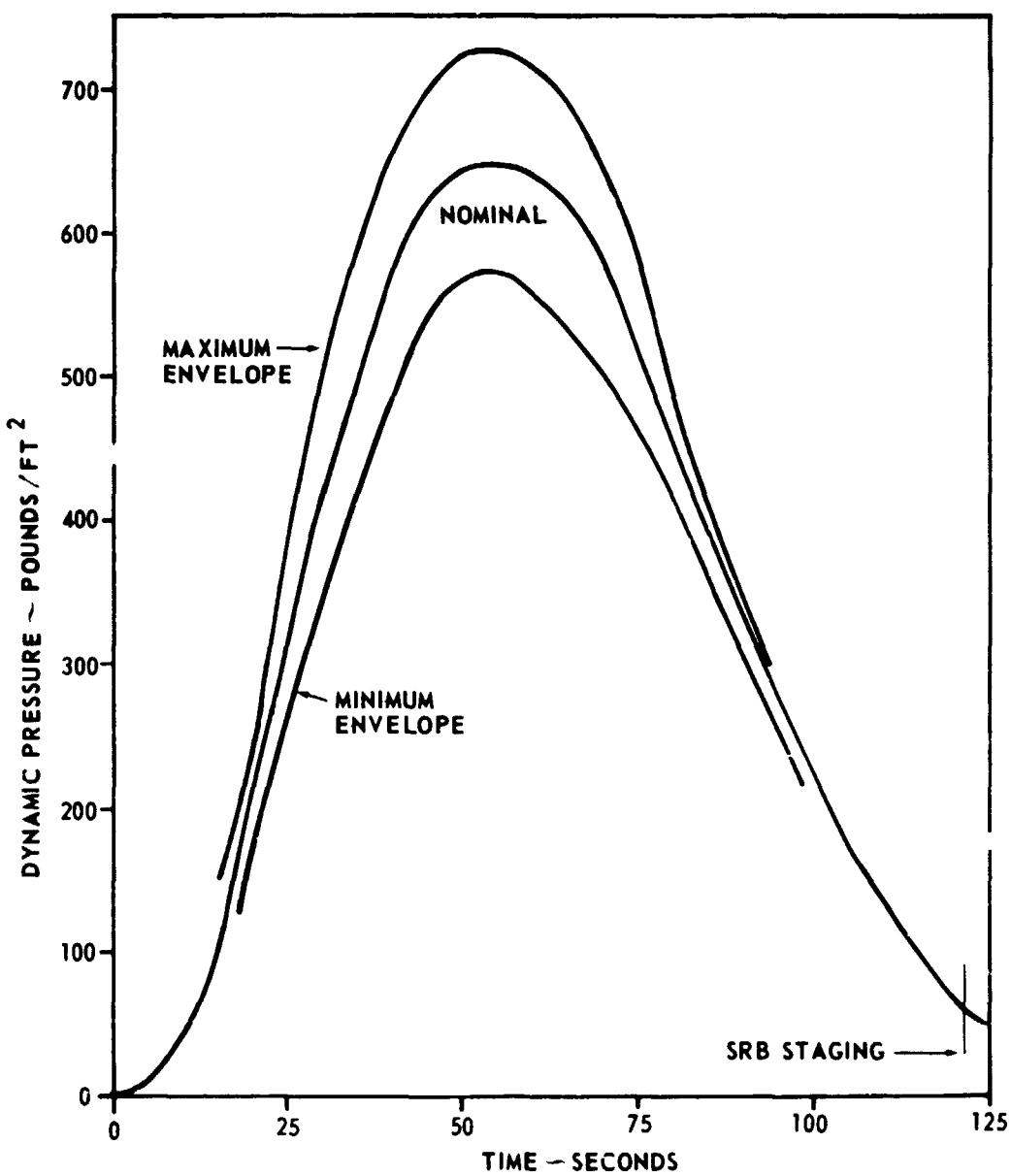


FIGURE III.1 DYNAMIC PRESSURE ENVELOPE VERSUS TIME

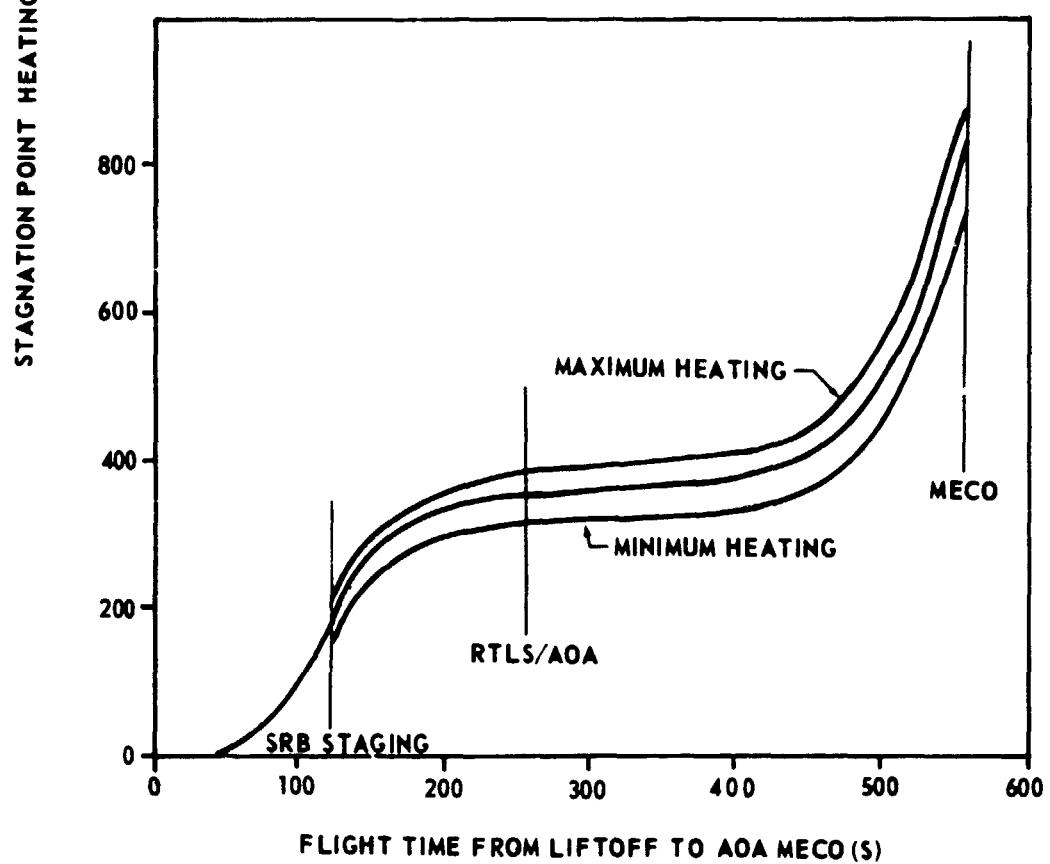
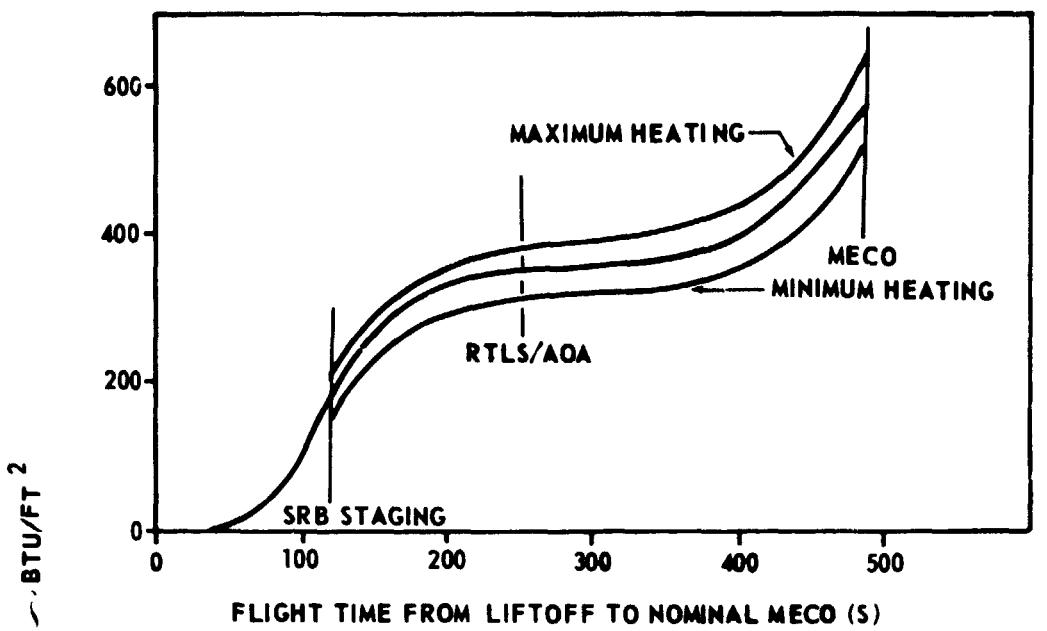


FIGURE III.2 STAGNATION POINT HEATING ENVELOPE VERSUS FLIGHT TIME

TABLE III.2 STATE VECTOR DEVIATIONS AT SRB STAGING

DISPERSION	Δ Range n. mi.	ΔV_t fps	$\Delta \gamma$ deg	Δ Alt feet	Δ Dynamic Pressure psf	Δ Max Acc.* g's
SRB Web Action Time	+ .49 - -.59	-24.247 19.246	- .12 .15	3481 -3825	- 9.1 11.42	- .07 .08
SRB Vacuum Specific Impulse	+ .32 - -.33	38.425 -38.481	- .16 .15	807 - 810	- 1.09 1.12	.01 -.01
SRB Propellant Load	+ .09 - -.08	10.226 -10.377	- .04 .04	180 - 180	- .2 .2	.01 0
SRB Staging Weight	+ -.06 - .07	- 9.911 9.813	- .02 .03	- 184 184	- .2 .2	0 .01
SRB Staging Time	+ .36 - -.34	7.283 - 8.579	- .13 .12	1083 -1079	- 2.6 2.7	0 0
SRB Misalignment	+ -.46 - .44	-19.062 16.263	- .86 .85	1755 -1811	- 5. 5.5	0 .01
SSME Vacuum Thrust	+ .15 - -.14	21.145 - 21.217	- .04 .03	456 - 453	- .6 .6	.01 -.01
SSME Vacuum Specific Impulse	+ -.01 .02	- 2.244 2.254	.0	- 26 33	.02 -.02	0 0
SSME Misalignment	+ -.18 .07	- 11.266 6.519	.32 -.25	453 - 295	- 1.5 1.	0 0

* Maximum Acceleration is that noted prior to cutoff. Time = 107.5 Sec.

TABLE III.2 (Continued)

DISPERSION	Δ Range n. mi.	ΔV fps	$\Delta \gamma$ deg	Δ Alt feet	Δ Dynamic Pressure psf	Δ Max Acc.* g's
Orbiter & ET Inert Weight	+ .04 - .05	- 6.841 6.752	.02 .02	-125 128	.2 .2	0 .01
ET Propellant Loading	+ .17 - .18	-24.413 24.505	.06 .07	-456 459	.6 .6	-.01 .01
Booster Steering Program	+ .40 - .39	16.115 -16.237	.70 .70	-1493 1469	4.6 -4.1	0 .01
Vehicle Center of Gravity	+ .03 - .04	- 1.703 1.385	.09 .7	157 - 141	.5 .4	0 0
Hold Day Cold Day	- .04 .17	- 7.260 23.704	0 .05	- 177 568	3.1 .8	0 .01
dead Wind Tail Wind	- .5 .6	-31.158 31.184	.14 .22	295 - 404	-1.6 1.9	0 0
Right Cross Wind Left Cross Wind	.04 .01	-29.99 9.902	.17 .08	- 171 - 13	.4 .05	0 0
Base Force	+ .15 - .15	-14.649 14.370	.07 .08	- 312 308	-.4 -	0 0
c_{A_0}	+ .14 - .14	17.382 16.381	.05 .06	- 318 305	.3 .3	0 0

* Maximum Acceleration is that noted prior to cutoff. Time \approx 107.5 Sec.

TABLE III.2 (Continued)

DISPERSION	Δ Range n. mi.	ΔV_1 fps	$\Delta \gamma$ deg	Δ Alt. feet	Δ Dynamic Pressure psf	Δ Max Acc.* g's
C_{N_0}	+ .08	2.687	- .08	- 262	.8	0
	- .07	- 2.193	.08	262	-.8	0
C_{N_α}	+ .03	.758	- .03	.79	.2	0
	- .02	- 1.033	.03	1.05	-.3	0
C_{M_0}	+ .01	.213	- .01	- 16	.1	0
	0	- .220	0	20	-.1	0
C_{M_α}	+ .02	.521	- .02	- 46	.1	0
	- .01	- .548	.01	49	-.1	0
C_{L_B}	+ 0	0	0	49	0	0
	0	.226	.02	16	-.1	0
C_{N_β}	+ 0	.246	.02	16	-.1	0
	0	.020	0	49	0	0
C_{Y_3}	+ 0	- .022	0	49	0	0
	0	.203	.02	16	-.1	0
RSS	(+) (-)	1.16 -1.18	76.906 -81.347	1.21 -1.19	4539 -4801	14.4 -13.4
RSS						.09 .07
Baseline	25.62	4591.878	28.23	141,054	60.8	2.96

* Maximum Acceleration is that noted prior to cutoff. Time \approx 107.5 Sec.

TABLE III.3 RELATIVE STATE VECTOR AND ET PROPELLANT DEVIATIONS
AT RTLS/AOA DEFINED AT CONSTANT $V_R = 8932$ FT/SEC

DISPERSION		Δ TIME seconds	$\Delta \gamma$ deg	Δ ALTITUDE feet	Δ ET PROPELLANT pounds
SRB Web Action Time	+	.3.671 - 3.422	-.066 .101	- 1509 2060	12393 - 11551
SRB Vacuum Specific Impulse	+	-.870 1.056	-.151 .058	1506 - 289	- 2937 3564
SRB Propellant Load	+	-.197 .297	-.057 .009	604 72	- 667 1002
SRB Steering Weight	+	.287 -.189	-.003 .060	3 224	969 - 605
SRB Staging Time	+	.123 .006	.040 .001	173 21	415 14
SRB Misalignment	+	.430 -.212	-.029 .064	1717 - 1513	1452 - 716
SSME Vacuum Thrust	+	-.2.094 2.250	-.101 .053	- 340 564	- 1343 1772
SSME Vacuum Specific Impulse	+	-.400 .300	.035 .011	278 - 67	- 1140 1484
SSME Misalignment	+	.287 -.072	-.016 .050	599 - 275	968 - 243
Orbiter & ET Inert Weight	+	.481 .372	-.003 .054	142 84	1623 - 1256

TABLE III.3 (Continued)

DISPERSION		Δ TIME seconds	$\Delta\gamma$ deg	Δ ALTITUDE feet	Δ ET PROPELLANT pounds
ET Propellant Load	+	1.602	- .077	215	5405
	-	1.488	.126	- 3	- 4975
Booster String Program	+	- .241	.063	- 1219	- 814
	-	.371	- .021	1413	1253
Vehicle Center of Gravity	+	.086	.022	285	289
	-	.029	.030	- 17	97
Hot Day		.260	- .003	19	877
Cold Day	-	.565	.114	409	- 1906
Head Wind		.812	- .058	183	741
Tail Wind	-	.644	.137	1	- 2173
Right Cross Wind		.137	.019	40	462
Left Cross Wind		.045	.026	97	153
Base Force	+	.463	- .037	- 30	1563
	-	.362	.083	222	- 1224
C_{AO}	+	.463	- .034	- 51	1563
	-	.334	.082	267	- 1128
C_{NO}	+	- .007	.031	- 70	- 25
	-	.107	.016	277	362
C_{NV}	+	.041	.029	62	136
	-	.073	.023	209	246

TABLE III.3 (Continued)

DISPERSION		Δ TIME seconds	$\Delta \gamma$ deg	Δ ALTITUDE feet	Δ ET PROPELLANT pounds
c_{M_0}	+	.041	.022	85	136
	-	.053	.025	126	198
$c_{M\alpha}$	+	.035	.023	66	117
	-	.065	.024	146	218
$c_{L\beta}$	+	.054	.026	115	182
	-	.058	.026	151	196
$c_{N\beta}$	+	.058	.026	151	197
	-	.050	.026	115	182
$c_{\gamma\beta}$	+	.054	.026	115	183
	-	.058	.026	151	196
RSS	(+)	+ 4.942	+ .366	+ 3655	+14969
RSS	(-)	- 4.522	- .155	- 2518	-13587
Baseline		253.041	7.597	351278	854156

TABLE III.4 DEVIATION IN MECO TIME AND RANGE FROM
LAUNCH SITE FOR AOA AND NOMINAL TRAJECTORIES

DISPERSION	<u>AOA</u>			<u>NOMINAL</u>		
	Δ MEKO TIME seconds	Δ AOA n. mi.	Δ RANGE n. mi.	Δ MEKO TIME seconds	Δ AOA n. mi.	Δ RANGE n. mi.
SRB Web Action	+	- .118	- 10.59	.527	- 6.40	
SRB Web Action	-	- .094	- 10.07	- 1.418	- 6.16	
SRB Vacuum Specific Impulse	+	- .076	- 1.91	- .413	.91	
SRB Vacuum Specific Impulse	-	- .018	- 2.28	.445	- 1.08	
SRB Propellant Load	+	- .038	- .43	- .105	.20	
SRB Propellant Load	-	- .014	- .64	.121	- .30	
SRB Staging Weight	+	- .013	- .60	.118	- .27	
SRB Staging Weight	-	- .044	.37	- .099	.17	
SRB Staging Time	+	- .046	- .24	.031	- .10	
SRB Staging Time	-	- .004	- .01	- .002	- .01	
SRB Misalignment	+	- .122	- 1.67	.094	- 1.25	
SRB Misalignment	-	- .073	1.23	- .024	1.06	
SSME Vacuum Thrust	+	- 4.231	- 6.65	- 3.141	- 4.03	
SSME Vacuum Thrust	-	- 4.246	6.52	3.217	3.99	
SSME Vacuum Specific Impulse	+	1.181	2.45	.741	1.16	
SSME Vacuum Specific Impulse	-	- 1.234	- 2.65	- .727	- 1.26	
SSME Misalignment	+	- .048	- .86	.089	.56	
SSME Misalignment	-	- .010	.30	- .030	.23	

TABLE III.4 (Continued)

DISPERSION	<u>AOA</u>		<u>Δ MECO TIME</u> seconds	<u>Δ RANGE</u> n. mi.	<u>NOMINAL</u>	<u>Δ MECO TIME</u> seconds	<u>Δ RANGE</u> n. mi.
	<u>Δ MECO TIME</u> seconds	<u>Δ AOA</u>					
Orbiter & ET Inert Weight	+.603 .660	.65 .87	-.550 -.531	-.50 .60			
ET Propellant Load	+.2,263 -.2,315	2.65 -2.88	-1.969 -1.946	-1.96 -2.06			
Booster Steering Program	+.055 -.104	1.16 -1.42	-.052 .084	-.94 -1.05			
Vehicle Center of Gravity	+.039 -.020	-.26 .00	.014 .005	-.16 .04			
Hot Day Cold Day	-.014 -.068	-.53 1.16	-.105 -.276	-.22 .52			
Head Wind Tail Wind	-.023 -.051	-2.09 1.82	-.332 -.295	-.1.18 1.10			
Right Cross Wind Left Cross Wind	-.041 -.047	0 -.17	.109 .013	.17 .12			
Base Force	-.003 -.048	-.98 .76	.324 -.305	-.11 .01			
C_{A_0}	-.003 -.052	-1. .73	.198 -.170	-.47 .35			
C_{N_0}	-.016 -.036	.11 .33	-.008 -.025	-.11 .21			

TABLE III.4 (Continued)

DISPERSION	<u>AOA</u>			<u>NOMINAL</u>		
	Δ MECO TIME seconds	Δ RANGE n. mi.	Δ MEKO TIME seconds	Δ RANGE n. mi.	Δ MECO TIME seconds	Δ RANGE n. mi.
$c_{N\alpha}$	+	- .026	- .06	.005	- .01	
	-	- .034	- .20	.012	- .11	
c_{M_o}	+	- .023	- .08	.004	- .04	
	-	- .029	- .13	.010	- .06	
$c_{M\alpha}$	+	- .022	- .06	.003	- .02	
	-	- .030	- .16	.012	- .08	
$c_{L\gamma}$	+	- .028	- .11	.009	- .05	
	-	- .031	- .13	.009	- .07	
c_{Nb}	+	- .031	- .13	.009	- .07	
	-	- .028	- .11	.009	- .05	
c_{YB}	+	- .28	- .11	.009	- .05	
	-	- .11	- .13	.009	- .07	
RSS	(+)	+ 5.000	+ 13.04	+4.235	+ 7.99	
	(-)	- 4.986	- 13.82	-4.118	- 8.34	
Baseline		558.712	932.37	485.231	765.46	

TABLE III.5 FLIGHT PERFORMANCE RESERVE CONTRIBUTION

DISPERSION	(@ AOA MECO Δ ET Propellants Consumed 1b	(@ NOMINAL MECO Δ ET Propellants Consumed 1b
SRB Web Action Time	+ -	3327 - 3160
SRB Vacuum Specific Impulse	+ -	933 - 995
SRB Propellant Load	+ -	262 - 266
SRB Staging Weight	+ -	259 - 256
SRB Staging Time	+ -	36 0
SRB Misalignment	+ -	184 - 60
SSME Vacuum Thrust	+ -	785 - 811
SSME Vacuum Specific Impulse	+ -	1586 - 1589
SSME Misalignment	+ -	189 - 85
		227 26

TABLE III.5 (Continued)

DISPERSION	(\triangle) AOA MECO Δ ET Propellants Consumed lb	(\triangle) NOMINAL MECO Δ ET Propellants Consumed lb
Orbiter & ET Inert Weight	+ 1923 - 1919	1919 - 1853
ET Propellant Loading	+ - + - + - - -	- 446 456 - 123 163
Booster Steering Program	+ - + -	- 151 237
Vehicle Center of Gravity	+ - - -	46 16
Hot Day	- 227	260
Cold Day	- 683	- 656
Head Wind	- 749	806
Tail Wind	- 723	- 706
Right Cross Wind	- 218	345
Left Cross Wind	- 43	- 15
Base Force	+ - + -	733 - 680
C_{A_0}	- 448 - 422	481 - 400

TABLE III.5 (Continued)

DISPERSION	@ AGA MECO Δ ET Propellants Consumed 1b		@ NOMINAL MECO Δ ET Propellants Consumed 1b	
	+	-	+	-
C_{N_0}	+	-	34	22
C_{N_α}	+	-	38	73
C_{M_0}	+	-	6	20
C_{M_α}	+	-	9	40
$C_{L\beta}$	+	-	2	13
C_{N_β}	+	-	5	34
C_{Y_β}	+	-	5	9
RSS	(+)	9	38	38
RSS	(-)	0	29	29
Orbiter Mixture Ratio Effects (SSME and ET Loading)				
FPK Total	Dependent on amount of fuel bias		6661	
Including Optimum fuel bias of 1150 1b	6471		6471	

CONCLUSION

The described launch vehicle has been evaluated and displays the capability to deliver the required performance to the design reference mission. The exchange ratios will enable management and design engineers to quickly evaluate performance effects of any proposed system changes in a rapid economic manner.

The design envelopes calculated shows that the maximum dynamic pressure encountered on ascent may exceed the design requirement of 650 psf by 77 psf mainly due to overperforming SRB and a headwind. The maximum ascent heating occurs on the abort-once-around mission and is considerably greater (43% on an undispersed trajectory) than that from a nominal flight. The flight performance reserves calculated have been converted to an equivalent percentage of characteristic velocity of .85% at AOA MECO and .87% at Nominal MECO. A statistical calculation of fuel bias resulted in an optimum requirement of 1150 pounds.

RECOMMENDATION

It is recommended that these data be utilized in conjunction with corresponding data generated by the system contractor, Rockwell International/Space Division, and Johnson Space Center for design of the Space Shuttle.

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APPROVAL

SPACE SHUTTLE LAUNCH VEHICLE PERFORMANCE TRAJECTORY, EXCHANGE
RATIOS, AND DISPERSION ANALYSIS

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The information in this report has been reviewed for security classification. Review of any information concerning Department of Defense or Atomic Energy Commission programs has been made by the MSFC Security Classification Officer. This report, in its entirety, has been determined to be unclassified.

This document has also been reviewed and approved for technical accuracy.


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