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SOLPRO: A COMPUTER CODE TO CALCULATE PROBABILISTIC ENERGETIC SOLAR PROTON FLUENCES

E. G. STASSINOPoulos

APRIL 1975

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NSDC 75-11

**SOLPRO: A Computer Code to Calculate
Probabilistic Energetic Solar Proton Fluences**

E. G. Stassinopoulos

**NASA-Goddard Space Flight Center
Sciences Directorate
National Space Science Data Center**

April 1975

Greenbelt, Maryland 20771

ABSTRACT

A code has been developed for the calculation of interplanetary solar proton fluences at 1 A. U. for the active years 1977-1983. The fluences are presented as functions of mission duration τ , energy threshold E, and confidence level Q. For a given combination of τ and Q, the routine determines whether ordinary or anomalously large events are to be considered, and in the latter case, the number of anomalously large events that are predicted by probabilistic theory for the specified mission duration. The code is described in detail. A listing and sample calculations are attached.

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SOLPRO: A Code to Calculate Energetic Solar Proton Fluences

Introduction

The code was originally developed as a supplement to UNIFLUX, a unified orbital flux integration system (Stassinopoulos and Gregory, 1975), from an initial solar proton model (Stassinopoulos and King, 1974) designed exclusively for the evaluation of flux levels to be encountered during the active phase of the next solar cycle (1977-1983) by earth-orbiting space-craft on missions involving partial magnetospheric shielding.

This first empirical model was characteristically simple and easy to use. It was derived entirely from experimental satellite measurements made during the active years of solar cycle 20; it included only crude confidence level estimates, that is, the probability of actual cycle 21 fluxes exceeding the predicted intensities.

A more probabilistic analysis of solar cycle 20 fluxes was later given by King (1974). This formal statistical treatment was subsequently used by King and Stassinopoulos (1975) in their computation of ratios of solar to trapped proton fluences for circular-orbit geocentric space missions to be flown during the active years of the next solar cycle (1977-1983). In this more sophisticated model the probability of exceeding mission fluence levels is given as a function of mission duration and energy.

The new SOLPRO code incorporates all the important features of the King (1974) analysis, which includes the distinction between "ordinary" (OR) and "anomalously large" (AL) events, and the probability of occurrence of the latter. Be it noted, that only one anomalously large event

was observed during solar cycle 20: the event of August, 1972; according to King (1974), the proton fluences of that one event alone constituted about 69% ($E > 10$ MeV) and 84% ($E > 60$ MeV) of the entire cycle fluence. Consequently, whenever at least one AL event is predicted, the OR-event-contribution is negligible.

The referenced solar proton models are based on the most continuous set of satellite data available to date, covering the period of enhanced solar activity during the 20th solar cycle (1964-1975) through the 1972 AL event, after which no significant events occurred. In both models, all fluxes were taken to be isotropic. As noted in Stassinopoulos and King (1974), on an event-integrated basis, departures from isotropy are typically only a few percent or less. This applies to the interplanetary medium and to much of the magnetosphere, but may not apply at low altitudes where anisotropy should result from atmospheric loss mechanisms.

When using the SOLPRO routine, two important items should be kept in mind. First, there is no assurance that the overall flux levels observed during the 20th solar cycle will also occur during the 21st cycle. However, as indicated in King (1974), a comparison of the annual mean sunspot numbers of past solar cycles suggests that cycle 21 will most likely be similar to the very ordinary cycle 20 than to the very extraordinary cycle 19. Second, there is no reliable way of predicting the distribution of individual solar events in time, in flux level, and in spectra through the 21st cycle. That pertains to ordinary as well as to anomalously large events. Therefore, the results obtained from the routine, although the best predictions available of solar proton fluences expected to occur during 1977-1983, should be considered guideline approximations only.

In the code, the solar proton fluences are expressed as functions of the parameters "confidence level", Q^* (in percent), "mission duration", τ (in months), and energy, E (in MeV). Within the limits established by the routine the user is free to select his own values of Q and τ for processing, but E is not an input parameter and the calculations are performed at ten fixed energy thresholds.

For missions whose trajectories will involve significant time away from a heliocentric distance of 1 A.U. (astronomical unit), a helioradial dependence of event fluences must be allowed for, as discussed by King (1974).

Similarly, for missions whose trajectories will involve partial magnetospheric shielding, the fractional exposure factor has to be determined, as discussed by Stassinopoulos and King (1974). An independent code performing these shielding calculations has been developed (Stassinopoulos, 1975) and is available from the National Space Science Data Center, Greenbelt, Maryland.

A detailed description of the solar proton routine is given in the next section on "Method and Procedure", with an analysis of the method employed and a review of the organization and structure of the code. In section "Application and Use" the routine is briefly discussed, its operation is described, and the arguments of its transfer vector are presented. Code listing and sample outputs are given in the attachments.

* Q is the degree of confidence a mission planner wishes to have that the actually encountered solar proton fluence will not exceed the predicted fluence, as given by the statistical solar proton model used.

Method and Procedure

SOLPRO is a short, compact routine which evaluates omnidirectional, unattenuated, interplanetary energetic solar proton fluences in terms of three variables: Q , τ , and E . The first two are input parameters, the last is internally programmed. As defined elsewhere in this report, Q denotes the degree of confidence one wishes to assign to the results, namely that for the specified mission duration τ the calculated fluences at ten preset energy values ranging from 10 to 100 MeV in increments of 10 MeV, are the smallest values which will not be exceeded by actually encountered intensities.

In order to hold the size and complexity of the code to a minimum, the desirable elements of the King (1974) analysis were empirically formulated by convenient approximation techniques, which are able to reproduce the statistically treated King results with relatively high accuracy. Specifically, the maximum error introduced into the statistics by this method is less than 50%. This error is indeed insignificant in view of the large intrinsic statistical uncertainties of the models themselves and the much greater uncertainties involved in predicting cycle 21 fluxes from cycle 20 data.

The most important feature of the code is the distinction between OR and AL events. This capability was developed relying entirely on King's probabilistic treatment and using the data given therein (King, 1974; Figure 5). For simplicity let:

$$n = f(Q, \tau) \quad (1)$$

where n is the number of AL events expected to occur with a confidence level Q and for a mission duration τ . It is then convenient to effect an apparent separation of variables by evaluating n independently for every value of Q within the regime of interest, and by expressing n in terms of τ alone. Thus:

$$n_i = c + \sum_{j=0}^6 a_{ij}(Q) \tau^j \quad (2)$$

where the index i relates n to Q through:

$$i = 100 - Q \quad (3)$$

and where the polynomial expansion coefficients a_{ij} are determined by curve fitting. The constant, $c=1.001$, is a dimensionless range adjustment term.

Table 1 contains the numerical values of the a_{ij} coefficients.

The code calculates n at the very beginning from equation 2 (see Table 2 for obtained values of n) and, depending on whether AL events are expected to occur or not, it branches to its appropriate section, where it computes the corresponding AL or OR solar proton fluences for the specified Q and τ .

For AL-event conditions, that is $n > 0$, the fluences are obtained from the expression:

$$F_{AL}(>E; Q, \tau) = S_{AL}(>E) * n(Q, \tau) \quad (4)$$

where the function:

$$S_{AL}(>E) = 7.9 \times 10^9 \exp \{ (30.-E)/26.5 \} \quad (5)$$

is King's (1974) exponential-in-energy representation of the integral flux and spectrum of the August, 1972, anomalously large event, for energy thresholds between 10 and 200 MeV.

In case OR events only are predicted ($n=0$), the respective fluences are obtained from:

$$F_{OR}(>E;Q, \tau) = S_{OR}(>E)*J(Q, \tau) \quad (6)$$

where now King's (1974) expression:

$$S_{OR}(>E) = \exp \{ .0158(30.-E) \} \quad (7)$$

for the integral energy spectrum of ordinary events is used, reliable over the range $10 \leq E(\text{MeV}) \leq 100$.

The function $J(Q, \tau)$ gives the ordinary fluence of protons above 30 MeV in terms of the two input variables (see Table 3 for obtained values of J). It was developed along similar lines as equation 1, with data from the same source (King, 1974; Figure 8).

Again, through the independent evaluation of J , (but this time for every τ within the relevant interval of 1-9 months for these events) the same apparent separation of variables is effected, resulting in:

$$J_k = d \sum_{m=0}^4 b_{km}(\tau) Q^m \quad (8)$$

where the index m relates J to τ through:

$$m = \text{integer}(\tau) \quad (9)$$

and where the coefficients, contained in Table 4, are also determined

by curve fitting. The constant, $d = 10^7$, is a scaling factor.

The code is structurally complete and self-contained. All expansion coefficients for the statistical treatment are stored in data statements at the beginning of the routine, while the expressions for the AL and OR models are included in the respective sections of the code.

To guard against accidental misuse and so as to insure that calculations are only performed within the valid ranges of the independent variables Q and τ , SOLPRO tests the values of these input parameters in its first executable statement. If the parameter(s) exceeds the program limits, it prints a warning message before returning control to the calling routine.

Finally, the code bypasses ordinary event fluence calculations, although it branches to the appropriate section, whenever $\tau=1$ and Q has values ranging from 80 to 83. In that domain the flux gradients are very high, the intensities decrease very rapidly towards $Q = 80$ and the galactic cosmic ray component becomes predominant (see discussion by King, 1974). For all practical purposes the OR-event solar protons are negligible for $Q < 80$ and $\tau > 1$.

Results and Discussion

Sample calculations performed with the code indicate good agreement with probabilistic predictions. That is, the results represent a reasonable approximation to these data, considering the large intrinsic limitations and uncertainties inherent in this type of estimation process.

Thus, as shown in Figure 1, the ordinary event fluence J of protons with energies $E > 30$ MeV, computed by the routine for the applicable Q and τ ranges, compares well with the original data in King (1974; Figure 8); the solid curves indicate the former, the dotted curves the latter. Apparently, the curves overlap for most Q and τ values. In the few places where they do not agree, the differences are truly insignificant; for example, the average error for all $\tau > 1$ is about 3%, while the maximum error, which occurs at $\tau = 1$ for $Q = 85$ is less than 50%.

Similarly, the number of anomalously large events n given by the code agrees favorably with the model (King, 1974; Figure 5). This is shown in Figure 2, where the dots indicate model data and the triangles SOLPRO predictions. Since the transition from one n value to another is probabilistically (and not deterministically) defined, the differences between the King model and the SOLPRO approximation are inconsequential.

Finally, the AL event exponential-in-energy function (Equation 5) and the ordinary-event integral-energy spectrum (Equation 7) are identical to the formulae given by King (1974). Their respective values are listed in Table 5.

Application and Use

Subroutine SOLPRO is written in standard FORTRAN-IV computer language and card decks are available in either the 029 model IBM keypunch format (EBCDIC) or the 026 keypunch format (BCD), for use with FORTRAN-compatible compilers.

The variables in the calling sequence are:

SOLPRO(TAU,IO,F)

The first two arguments are input data:

TAU : mission duration in months, with a valid range
from 1. to 72. (REAL*4)

IQ : percent confidence level that calculated fluence
will not be exceeded, with a valid range from
80 to 99 (INTEGER*4)

The last argument is output data:

F(N) : solar proton spectrum for energies $E > 10^N$ MeV,
where index N goes from 1 to 10.

All arguments except IQ are single precision floating point variables. Besides their range limits, there are no other restrictions or limitations on the values of the input arguments.

There are no READ or other input statements in SOLPRO. A WRITE statement is executed each time an input variable exceeds the stipulated limits. In addition, a WRITE statement is executed whenever for a given combination of T and Q no significant solar proton fluences are to be expected.

Figure 3 shows a flow diagram of the program. A complete listing is given in the attachment. The cards of the deck are appropriately labeled in columns 73-80 as SOLPRxxx where the three last columns (xxx) contain the sequential numbering, which is incremented by 10.

Acknowledgements

The author wishes to thank Drs. J. I. Vette and J. H. King
for many helpful suggestions and comments.

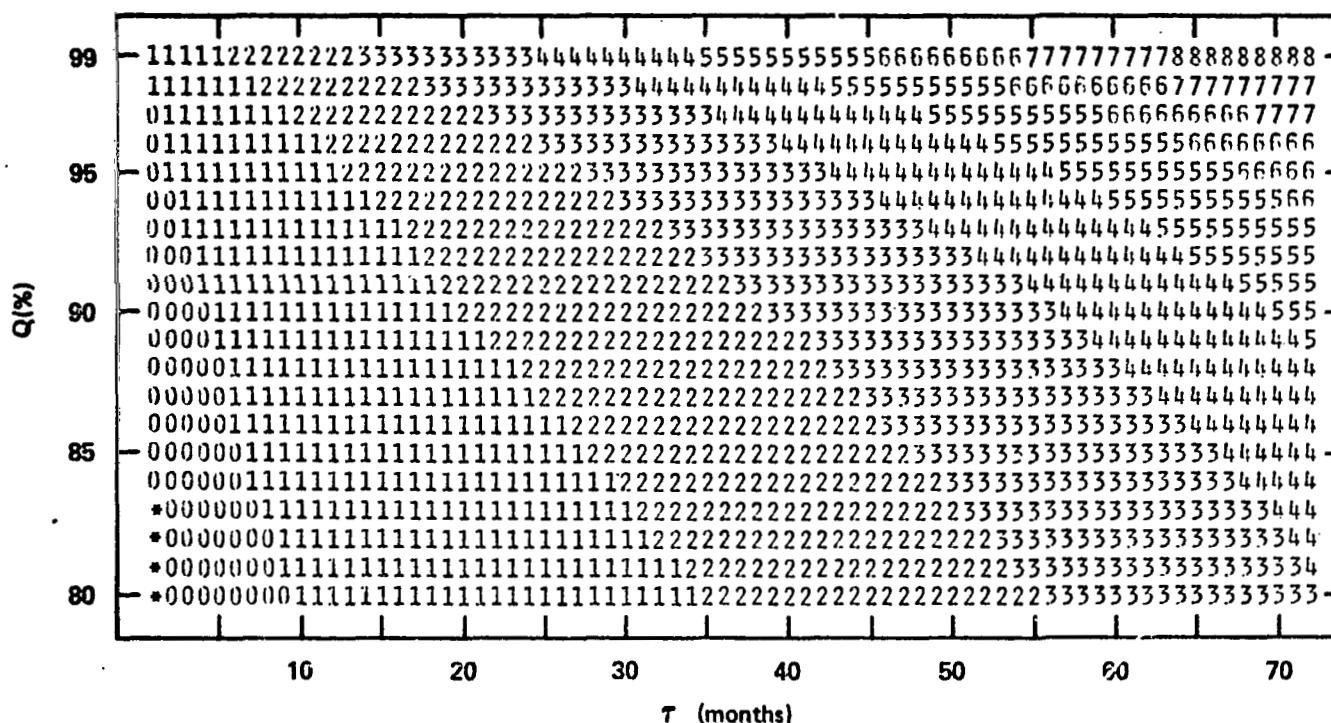
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Table 1
NUMBER OF ANOMALOUSLY LARGE EVENTS
Polynomial Expansion Coefficients

Q (%)	a_0	a_1	a_2	a_3	a_4	a_5	a_6
99	-.1571	.2707	-.1269 ⁻¹	.4428 ⁻³	-.8185 ⁻⁵	.7754 ⁻⁷	-.2939 ⁻⁹
98	-.1870	.1951	-.6559 ⁻²	.1990 ⁻³	-.3618 ⁻⁵	.3740 ⁻⁷	-.1599 ⁻⁹
97	-.2007	.1497	-.3179 ⁻²	.5730 ⁻⁴	-.4664 ⁻⁶	.1764 ⁻⁸	0
96	-.1882	.1228	-.1936 ⁻²	.2660 ⁻⁴	-.1022 ⁻⁶	0	0
95	-.2214	.1149	-.1871 ⁻²	.2695 ⁻⁴	-.1116 ⁻⁶	0	0
94	-.2470	.1062	-.1658 ⁻²	.2367 ⁻⁴	-.9465 ⁻⁷	0	0
93	-.2509	.8710 ⁻¹	-.8300 ⁻³	.8438 ⁻⁵	0	0	0
92	-.2923	.8932 ⁻¹	-.1023 ⁻²	.1029 ⁻⁴	0	0	0
91	-.3222	.8648 ⁻¹	-.9992 ⁻³	.9935 ⁻⁵	0	0	0
90	-.3518	.8417 ⁻¹	-.1000 ⁻²	.9956 ⁻⁵	0	0	0
89	-.3698	.7951 ⁻¹	-.8983 ⁻³	.8940 ⁻⁵	0	0	0
88	-.2771	.5473 ⁻¹	-.1543 ⁻⁴	0	0	0	0
87	-.2818	.5072 ⁻¹	.2511 ⁻⁴	0	0	0	0
86	-.2845	.4717 ⁻¹	.5664 ⁻⁴	0	0	0	0
85	-.2947	.4405 ⁻¹	.8507 ⁻⁴	0	0	0	0
84	-.2923	.4111 ⁻¹	.1106 ⁻³	0	0	0	0
83	-.2981	.3853 ⁻¹	.1312 ⁻³	0	0	0	0
82	-.3002	.3585 ⁻¹	.1529 ⁻³	0	0	0	0
81	-.3001	.3312 ⁻¹	.1781 ⁻³	0	0	0	0
80	-.3141	.3248 ⁻¹	.1654 ⁻³	0	0	0	0

Table 2
Number of Anomalously Large Events Predicted by SOLPRO



*NO CALCULATIONS PERFORMED

Table 3

OR-Event Fluences (E > 30 MeV) given by SOLPRO Routine

Q	T = 1	2	3	4	5	6	7	8	9
99	-----	-----	-----	-----	-----	-----	-----	-----	-----
98	-----	-----	-----	-----	-----	-----	-----	-----	-----
97	5.07x10 ⁸	-----	-----	-----	-----	-----	-----	-----	-----
96	3.42x10 ⁸	-----	-----	-----	-----	-----	-----	-----	-----
95	2.34x10 ⁸	-----	-----	-----	-----	-----	-----	-----	-----
94	1.67x10 ⁸	4.83x10 ⁸	-----	-----	-----	-----	-----	-----	-----
93	1.30x10 ⁸	3.91x10 ⁸	-----	-----	-----	-----	-----	-----	-----
92	1.09x10 ⁸	3.23x10 ⁸	6.46x10 ⁸	-----	-----	-----	-----	-----	-----
91	9.78x10 ⁷	2.74x10 ⁸	5.09x10 ⁸	-----	-----	-----	-----	-----	-----
90	8.85x10 ⁷	2.39x10 ⁸	4.15x10 ⁸	7.82x10 ⁸	-----	-----	-----	-----	-----
89	7.72x10 ⁷	2.12x10 ⁸	3.53x10 ⁸	6.02x10 ⁸	-----	-----	-----	-----	-----
88	6.20x10 ⁷	1.91x10 ⁸	3.14x10 ⁸	4.84x10 ⁸	9.16x10 ⁸	-----	-----	-----	-----
87	4.34x10 ⁷	1.73x10 ⁸	2.88x10 ⁸	4.12x10 ⁸	6.76x10 ⁸	-----	-----	-----	-----
86	2.40x10 ⁷	1.56x10 ⁸	2.70x10 ⁸	3.68x10 ⁸	5.44x10 ⁸	-----	-----	-----	-----
85	8.86x10 ⁶	1.38x10 ⁸	2.53x10 ⁸	3.42x10 ⁸	4.74x10 ⁸	7.52x10 ⁸	-----	-----	-----
84	5.23x10 ⁶	1.19x10 ⁸	2.36x10 ⁸	3.23x10 ⁸	4.32x10 ⁸	6.25x10 ⁸	-----	-----	-----
83	*	1.00x10 ⁸	2.17x10 ⁸	3.04x10 ⁸	3.98x10 ⁸	5.39x10 ⁸	8.06x10 ⁸	-----	-----
82	*	8.16x10 ⁷	1.95x10 ⁸	2.83x10 ⁸	3.60x10 ⁸	4.80x10 ⁸	6.94x10 ⁸	1.01x10 ⁹	-----
81	*	6.56x10 ⁷	1.74x10 ⁸	2.58x10 ⁸	3.22x10 ⁸	4.38x10 ⁸	6.08x10 ⁸	8.38x10 ⁸	-----
80	*	5.48x10 ⁷	1.56x10 ⁸	2.32x10 ⁸	2.98x10 ⁸	4.04x10 ⁸	5.41x10 ⁸	7.34x10 ⁸	1.01x10 ⁹

* No Calculations performed: see comments page 7.

Table 4

ORDINARY EVENT FLUENCE

Polynomial Expansion Coefficients

T (mths)	b ₀	b ₁	b ₂	b ₃	b ₄
1	.154047x10 ³	-.522258x10 ⁴	.714275x10 ⁵	-.432747x10 ⁶	.955315x10 ⁶
2	.198004x10 ³	-.448788x10 ⁴	.438148x10 ⁵	-.196046x10 ⁶	.325520x10 ⁶
3	.529120x10 ³	-.122227x10 ⁵	.112869x10 ⁶	-.465084x10 ⁶	.710572x10 ⁶
4	.121141x10 ⁴	-.266412x10 ⁵	.226778x10 ⁶	-.857230x10 ⁶	.120444x10 ⁷
5	.452062x10 ⁴	-.103248x10 ⁶	.896085x10 ⁶	-.346028x10 ⁷	.499852x10 ⁷
6	.272028x10 ⁴	-.499088x10 ⁵	.353050x10 ⁶	-.111929x10 ⁷	.133386x10 ⁷
7	.275595x10 ⁴	-.469718x10 ⁵	.314729x10 ⁶	-.960383x10 ⁶	.111650x10 ⁷
8	.570997x10 ⁴	-.799689x10 ⁵	.381074x10 ⁶	-.610714x10 ⁶	0
9	.101000x10 ³	0	0	0	0

Table 5

<u>Integral Flux & Spectrum of the August 1972 AL Event</u> <u>(Equation 5)</u>		<u>Distribution of OR-Event Integral Spectrum</u> <u>(Equation 7)</u>	
<u>Energy</u> <u>(MeV)</u>	<u>Solar Protons (>E)</u> <u>(#/cm²/AL-event)</u>	<u>Energy</u> <u>(MeV)</u>	<u>Spectral Function</u> <u>(normalized to 30 MeV)</u>
10	1.680×10^{10}	10	1.37163
20	1.152×10^{10}	20	1.17117
30	7.900×10^9	30	1.00000
40	5.417×10^9	40	0.85385
50	3.714×10^9	50	0.72906
60	2.547×10^9	60	0.62251
70	1.746×10^9	70	0.53153
80	1.197×10^9	80	0.45384
90	8.210×10^8	90	0.38752
100	5.629×10^8	100	0.33088

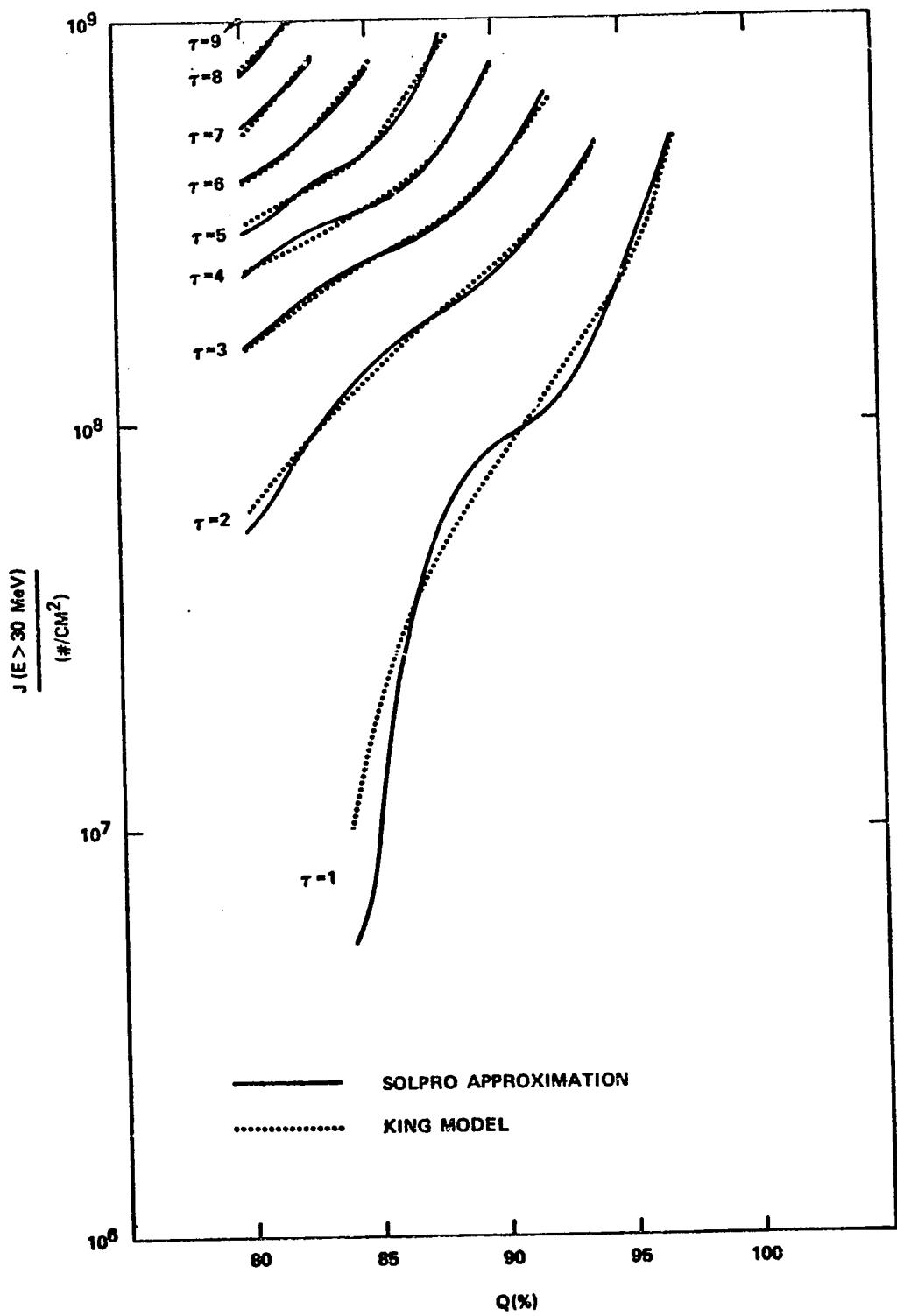


Figure 1. OR-Event Fluences ($E > 30$ MeV): Comparison of Predictions

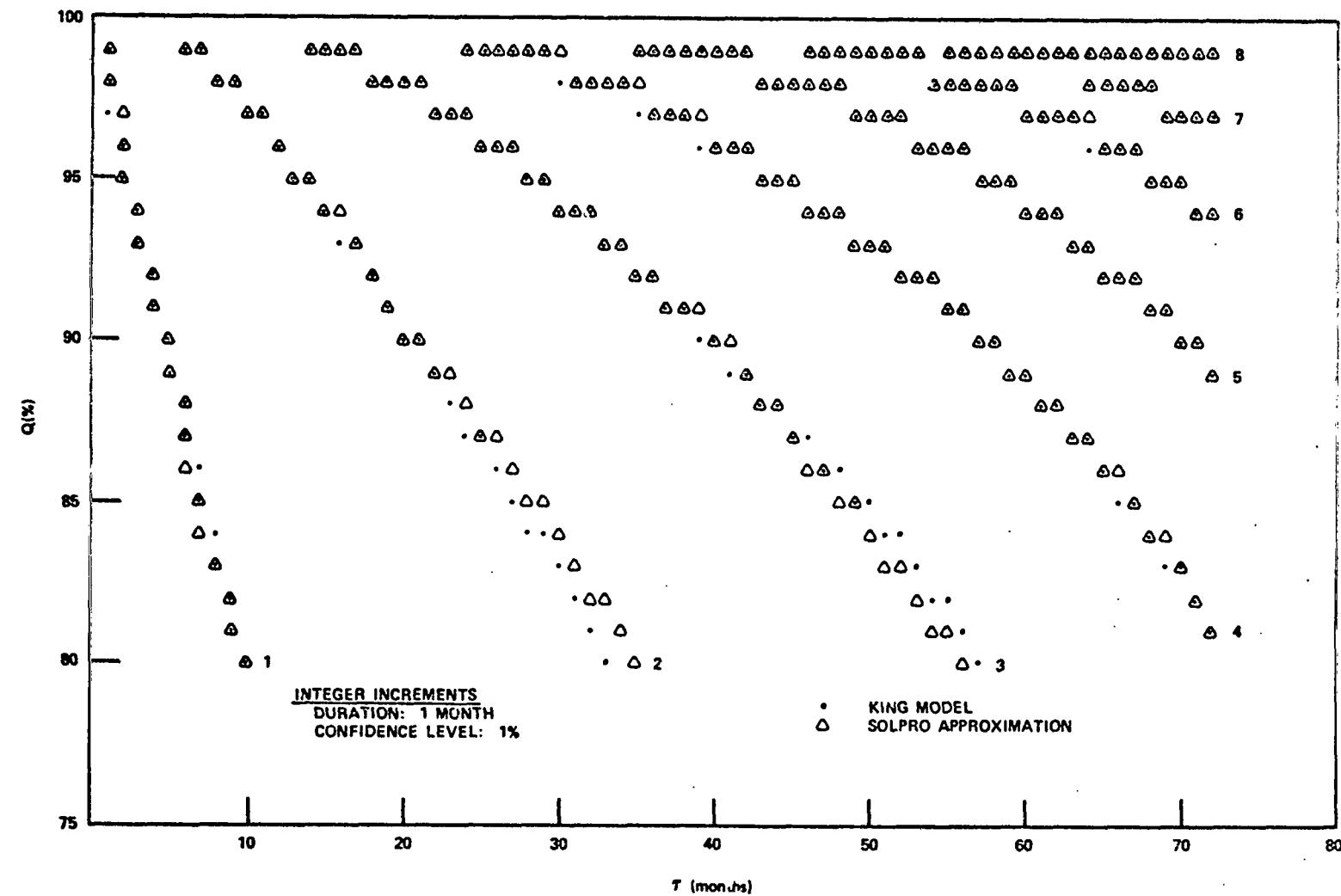


Figure 2. Number of Anomalously Large Events: Comparison of Predictions

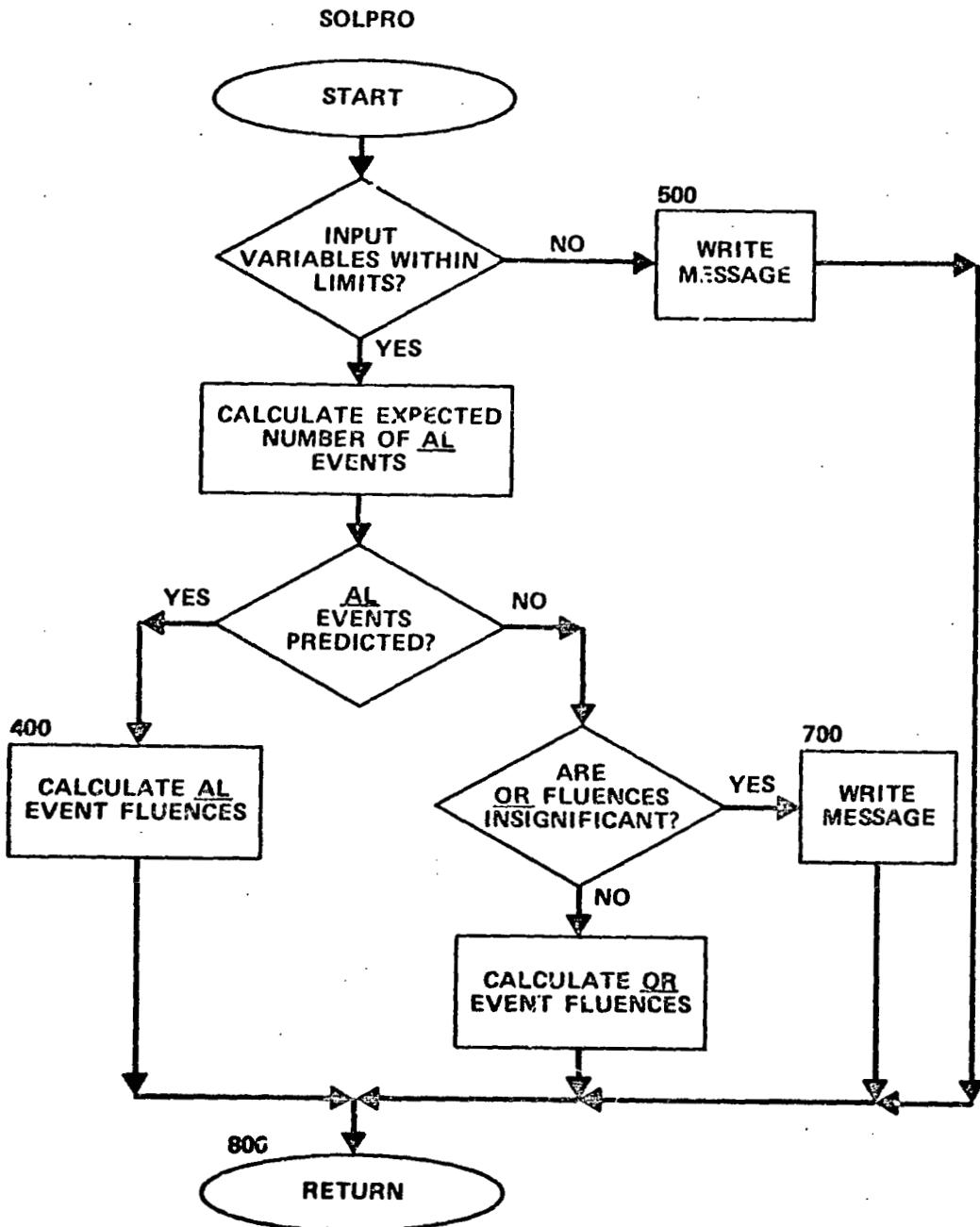


Figure 3. Flow Diagram for SOLPRO

Sample Program Listing

```

SUBROUTINE SOLPRO(TAU,IQ,F)                               SOLPRO10
C *** INTERPLANETARY SOLAR PROTON FLUX AT 1 AU (FROM E>10 TO E>100 MEV) SOLPRO20
C *** SINGLE PRECISION DECK IN STANDARD FORTRAN IV FOR IBM 360 MACHINES SOLPRO30
C *** (EBCDIC, 029 PUNCH) OR OTHER COMPATIBLE SYSTEMS.          SOLPRO40
C *** PROGRAM DESIGNED AND TESTED BY E.G. STASSINOPoulos, CODE 601, SOLPRO50
C *** NASA GODDARD SPACE FLIGHT CENTER, GREENBELT, MARYLAND 20771 . SOLPRO60
C **** INPUT: TAU      MISSION DURATION IN MONTHS (REAL*4)      SOLPRO70
C ****      IQ       CONFIDENCE LEVEL THAT CALCULATED FLUENCE F(N) SOLPRO80
C ****           WILL NOT BE EXCEEDED (INTGER*4)                  SOLPRO90
C *** OUTPUT: F(N)    SPECTRUM OF INTEGRAL SOLAR PROTON FLUENCE FOR SOLPRO100
C ***           ENERGIES E>10*N (1<N<10)                      SOLPRO110
C ***           REAL NALE,NALECF(7,20)/-.1571,.2707,-.1269E-1,.4428E-3,-.8185E-5, SOLPR120
C ***           .7754E-7,-.2939E-9,-.1870,.1951,-.6559E-2,.1990E-3,-.3618E-5, SOLPR130
C ***           .3740E-7,-.1509E-9,-.2007,.1497,-.3179E-2,.5730E-6,-.4664E-6, SOLPR140
C ***           $.1764E-3,0.,-.1882,.1228,-.1936E-2,.2660E-4,-.1022E-6,2*0., SOLPR150
C ***           $-.2214,.1149,-.1871E-2,.2695E-4,-.1116E-6,2*0.,-.2470,.1062, SOLPR160
C ***           $-.1658E-2,.2367E-4,-.9465E-7,2*0.,-.2509,.8710E-1,-.8300E-3, SOLPR170
C ***           $.8438E-5,3*0.,-.2923,.8932E-1,-.1023E-2,.1029E-4,3*0.,-.3222, SOLPR180
C ***           $.8648E-1,-.9992E-3,.9935E-5,3*0.,-.3518,.8417E-1,-.1000E-2, SOLPR190
C ***           $.9950E-5,3*0.,-.3698,.7951E-1,-.8983E-3,.8940E-5,3*0.,-.2771, SOLPR200
C ***           $.5673E-1,-.1543E-4,4*0.,-.2818,.5072E-1,.2511E-4,4*0.,-.2845, SOLPR210
C ***           $.4717E-1,.5664E-4,4*0.,-.2947,.4405E-1,.8507E-4,4*0.,-.2923, SOLPR220
C ***           $.4111E-1,.1106E-3,4*0.,-.2981,.3855E-1,.1312E-3,4*0.,-.3002, SOLPR230
C ***           $.3585E-1,.1529E-3,4*0.,-.3001,.3312E-1,.1781E-3,4*0.,-.3141, SOLPR240
C ***           $.3240E-1,.1654E-3,4*0./,F(10),G(10)                      SOLPR250
C ***           REAL ORFLXC(5,9)/.154047E3,-.522258E4,.714275E5,-.432747E6,.955315E7, SOLPR260
C ***           $E6,.198004E3,-.448788E4,.438148E5,-.196046E6,.32552E6,.529120E3, SOLPR270
C ***           $-.122227E5,.112369E6,-.4F5084E6,.710572E6,.121141E4,-.266412E5, SOLPR280
C ***           $.226778E6,-.85728E6,.120445E7,.452062E4,-.103248E6,.896085E6, SOLPR290
C ***           $.346028E7,.499852E7,.272028E4,.499088E5,.35305E6,-.111929E7, SOLPR300
C ***           $.133336E7,.275597E8,-.4E9718E5,.314729E6,-.960383E6,.11165E7, SOLPR310
C ***           $.570997E4,-.799680E5,.381074E6,-.610714E6,0...101E3,4*0./, SOLPR320
C ***           INTEGER INDEX(20)/2*7,6,3*5,5*4,9*3/                         SOLPR330
C ***           1 FORMAT(' TAU=',F4.0,' IQ=',I3,3X,'PARAMETER(S) EXCEED PROGRAM LIMITS', SOLPR340
C ***           $TS')                                              SOLPR350
C ***           2 FORMAT(2X,'FOR THE COMBINATION OF TAU AND IQ GIVEN, NO SIGNIFICANT SOLPR370
C ***           $ SOLAR PROTON FLUXES ARE TO BE EXPECTED. TAU=',F6.2,' IQ=',I2) SOLPR380
C ***           IF(TAU.GT.72..OR.IQ.LT.30)GO TO 500                      SOLPR390
C ***           IP=100-IQ                                         SOLPR400
C ***           M=INDEX(IP)                                         SOLPR410
C ***           NALE=0.                                         SOLPR420
C ***           DO 300 J=1,M                                         SOLPR430
C ***           300 NALE=NALE+NALECF(J,IP)*TAU***(J-1)             SOLPR440
C ***           INALE=NALE+1.0001                                     SOLPR450
C ***           IF(NALE.GT.0) GO TO 400                           SOLPR460
C ***           C *** CALCULATIONS FOR OR-EVENT CONDITIONS          SOLPR470
C ***           IT=TAU                                         SOLPR480
C ***           IF(IT.EQ.1.AND.IP.GT.16) GO TO 700               SOLPR490
C ***           P=FLOAT(IP)/100.                                     SOLPR500
C ***           OF=0.                                         SOLPR510
C ***           DO 100 J=1,5                                         SOLPR520
C ***           100 OF=OF+ORFLXC(J,IT)* P***(J-1)*1.E7            SOLPR530
C ***           E=10.                                         SOLPR540
C ***           DO 200 N=1,10                                       SOLPR550
C ***           200 G(N)=EXP(.0158*(30.-E))                     SOLPR560
C ***           F(N)=OF*G(N)                                         SOLPR570
C ***           200 E=E+10.                                         SOLPR580
C ***           GO TO 800.                                         SOLPR590
C ***           C *** CALCULATIONS FOR AL-EVENT CONDITIONS          SOLPR600
C ***           400 E=10.                                         SOLPR610
C ***           DO 600 N=1,10                                     SOLPR620
C ***           600 F(N)=7.9E9*EXP((30.-E)/26.5)*INALE           SOLPR630
C ***           600 E=E+10.                                         SOLPR640
C ***           GO TO 800.                                         SOLPR650
C ***           700 WRITE(6,2) TAU,IQ                            SOLPR660
C ***           GO TO 800.                                         SOLPR670
C ***           500 WRITE(6,1) TAU,IQ                            SOLPR680
C ***           800 RETURN                                         SOLPR690
C ***           END                                             SOLPR700

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ORIGINAL PAGE IS
OF POOR QUALITY

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Sample Calculations: Solar Proton Fluences F(>E;Q, T)

>E(MeV)		T=1		T=2		T=3		T=4		T=5		T=6		T=7		T=8		T=9		T=10		T=11		T=12					
10.5	71.9E	07	2.124E	02	3.782E	07	5.594E	03	8.642E	05	1.168E	06	1.668E	06	1.688E	06	1.688E	06	1.688E	06	1.688E	06	1.688E	06	1.688E	06			
20.4	48.6E	07	1.709E	04	3.242E	07	5.842E	05	8.225E	06	1.152E	06	1.152E	06	1.152E	06	1.152E	06	1.152E	06	1.152E	06	1.152E	06	1.152E	06			
30.4	36.6E	07	1.651E	04	2.757E	04	4.132E	05	7.227E	04	7.947E	05	7.900E	05	7.900E	05	7.900E	05	7.900E	05	7.900E	05	7.900E	05	7.900E	05			
40.4	31.9E	07	1.611E	04	2.456E	04	3.516E	05	5.495E	04	5.417E	05	5.417E	05	5.417E	05	5.417E	05	5.417E	05	5.417E	05	5.417E	05	5.417E	05			
50.4	27.9E	07	1.572E	04	2.210E	04	3.035E	05	4.122E	04	5.341E	05	5.714E	05	5.714E	05	5.714E	05	5.714E	05	5.714E	05	5.714E	05	5.714E	05			
60.4	23.9E	07	1.532E	04	1.976E	04	2.839E	05	4.022E	04	5.247E	05	5.647E	05	5.647E	05	5.647E	05	5.647E	05	5.647E	05	5.647E	05	5.647E	05			
70.4	21.6E	07	1.502E	04	1.664E	04	2.591E	05	3.922E	04	5.152E	05	5.547E	05	5.547E	05	5.547E	05	5.547E	05	5.547E	05	5.547E	05	5.547E	05			
80.4	18.6E	07	1.471E	04	1.359E	04	2.351E	05	3.717E	04	4.156E	05	4.546E	05	4.546E	05	4.546E	05	4.546E	05	4.546E	05	4.546E	05	4.546E	05			
90.4	16.1E	07	1.441E	04	1.258E	04	2.151E	05	3.517E	04	3.915E	05	4.321E	05	4.321E	05	4.321E	05	4.321E	05	4.321E	05	4.321E	05	4.321E	05			
100.4	13.7E	07	1.411E	04	1.121E	04	1.959E	05	3.317E	04	3.629E	05	4.039E	05	4.039E	05	4.039E	05	4.039E	05	4.039E	05	4.039E	05	4.039E	05			
>E(MeV)		T=13		T=14		T=15		T=16		T=17		T=18		T=19		T=20		T=21		T=22		T=23		T=24					
10.4	6.6E	07	1.468E	04	1.670E	04	1.952E	04	2.168E	04	2.468E	04	2.690E	04	2.882E	04	3.082E	04	3.282E	04	3.482E	04	3.682E	04	3.882E	04			
20.4	15.2E	07	1.415E	04	1.515E	04	1.652E	04	1.752E	04	1.852E	04	1.952E	04	2.052E	04	2.152E	04	2.252E	04	2.352E	04	2.452E	04	2.552E	04			
30.4	29.0E	07	1.370E	04	1.470E	04	1.590E	04	1.700E	04	1.800E	04	1.900E	04	2.000E	04	2.100E	04	2.200E	04	2.300E	04	2.400E	04	2.500E	04			
40.4	41.7E	07	1.331E	04	1.431E	04	1.551E	04	1.651E	04	1.751E	04	1.851E	04	1.951E	04	2.051E	04	2.151E	04	2.251E	04	2.351E	04	2.451E	04			
50.4	53.4E	07	1.301E	04	1.391E	04	1.511E	04	1.611E	04	1.711E	04	1.811E	04	1.911E	04	2.011E	04	2.111E	04	2.211E	04	2.311E	04	2.411E	04			
60.4	55.7E	07	1.272E	04	1.362E	04	1.482E	04	1.582E	04	1.682E	04	1.782E	04	1.882E	04	1.982E	04	2.082E	04	2.182E	04	2.282E	04	2.382E	04			
70.4	57.4E	07	1.242E	04	1.332E	04	1.452E	04	1.552E	04	1.652E	04	1.752E	04	1.852E	04	1.952E	04	2.052E	04	2.152E	04	2.252E	04	2.352E	04			
80.4	59.1E	07	1.212E	04	1.302E	04	1.422E	04	1.522E	04	1.622E	04	1.722E	04	1.822E	04	1.922E	04	2.022E	04	2.122E	04	2.222E	04	2.322E	04			
90.4	60.8E	07	1.182E	04	1.272E	04	1.392E	04	1.492E	04	1.592E	04	1.692E	04	1.792E	04	1.892E	04	1.992E	04	2.092E	04	2.192E	04	2.292E	04			
100.4	62.5E	07	1.152E	04	1.242E	04	1.362E	04	1.462E	04	1.562E	04	1.662E	04	1.762E	04	1.862E	04	1.962E	04	2.062E	04	2.162E	04	2.262E	04			
>E(MeV)		T=25		T=26		T=27		T=28		T=29		T=30		T=31		T=32		T=33		T=34		T=35		T=36					
10.3	3.3E	07	1.0	3.761E	07	1.0	4.261E	07	1.0	3.361E	07	1.0	3.861E	07	1.0	3.361E	07	1.0	3.861E	07	1.0	3.361E	07	1.0	3.861E	07	1.0	3.861E	07
20.3	2.3E	07	1.0	2.342E	07	1.0	2.442E	07	1.0	2.342E	07	1.0	2.342E	07	1.0	2.342E	07	1.0	2.342E	07	1.0	2.342E	07	1.0	2.342E	07	1.0	2.342E	07
30.3	1.5E	07	1.0	1.540E	07	1.0	1.440E	07	1.0	1.540E	07	1.0	1.540E	07	1.0	1.540E	07	1.0	1.540E	07	1.0	1.540E	07	1.0	1.540E	07	1.0	1.540E	07
40.3	1.0E	07	1.0	1.040E	07	1.0	1.040E	07	1.0	1.040E	07	1.0	1.040E	07	1.0	1.040E	07	1.0	1.040E	07	1.0	1.040E	07	1.0	1.040E	07	1.0	1.040E	07
50.3	0.7E	07	1.0	0.740E	07	1.0	0.640E	07	1.0	0.740E	07	1.0	0.740E	07	1.0	0.740E	07	1.0	0.740E	07	1.0	0.740E	07	1.0	0.740E	07	1.0	0.740E	07
60.3	0.5E	07	1.0	0.540E	07	1.0	0.440E	07	1.0	0.540E	07	1.0	0.540E	07	1.0	0.540E	07	1.0	0.540E	07	1.0	0.540E	07	1.0	0.540E	07	1.0	0.540E	07
70.3	0.4E	07	1.0	0.440E	07	1.0	0.340E	07	1.0	0.440E	07	1.0	0.440E	07	1.0	0.440E	07	1.0	0.440E	07	1.0	0.440E	07	1.0	0.440E	07	1.0	0.440E	07
80.3	0.3E	07	1.0	0.340E	07	1.0	0.240E	07	1.0	0.340E	07	1.0	0.340E	07	1.0	0.340E	07	1.0	0.340E	07	1.0	0.340E	07	1.0	0.340E	07	1.0	0.340E	07
90.3	0.2E	07	1.0	0.240E	07	1.0	0.140E	07	1.0	0.240E	07	1.0	0.240E	07	1.0	0.240E	07	1.0	0.240E	07	1.0	0.240E	07	1.0	0.240E	07	1.0	0.240E	07
100.3	0.1E	07	1.0	0.140E	07	1.0	0.040E	07	1.0	0.140E	07	1.0	0.140E	07	1.0	0.140E	07	1.0	0.140E	07	1.0	0.140E	07	1.0	0.140E	07	1.0	0.140E	07
>E(MeV)		T=37		T=38		T=39		T=40		T=41		T=42		T=43		T=44		T=45		T=46		T=47		T=48					
10.3	3.3E	07	1.0	3.761E	07	1.0	3.661E	07	1.0	3.561E	07	1.0	3.461E	07	1.0	3.361E	07	1.0	3.261E	07	1.0	3.161E	07	1.0	3.061E	07	1.0	2.961E	07
20.3	2.3E	07	1.0	2.342E	07	1.0	2.242E	07	1.0	2.142E	07	1.0	2.042E	07	1.0	1.942E	07	1.0	1.842E	07	1.0	1.742E	07	1.0	1.642E	07	1.0	1.542E	07
30.3	1.5E	07	1.0	1.540E	07	1.0	1.440E	07	1.0	1.340E	07	1.0	1.240E	07	1.0	1.140E	07	1.0	1.040E	07	1.0	9.400E	07	1.0	8.400E	07	1.0	7.400E	07
40.3	1.0E	07	1.0	1.040E	07	1.0	0.940E	07	1.0	0.840E	07	1.0	0.740E	07	1.0	0.640E	07	1.0	0.540E	07	1.0	0.440E	07	1.0	0.340E	07	1.0	0.240E	07
50.3	0.7E	07	1.0	0.740E	07	1.0	0.640E	07	1.0	0.540E	07	1.0	0.440E	07	1.0	0.340E	07	1.0	0.240E	07	1.0	0.140E	07	1.0	0.040E	07	1.0	-0.140E	07
60.3	0.4E	07	1.0	0.440E	07	1.0	0.340E	07	1.0	0.240E	07	1.0	0.140E	07	1.0	0.040E	07	1.0	-0.140E	07	1.0	-0.240E	07	1.0	-0.340E	07	1.0	-0.440E	07
70.3	0.2E	07	1.0	0.240E	07	1.0	0.140E	07	1.0	0.040E	07	1.0	-0.140E	07	1.0	-0.240E	07	1.0	-0.340E	07	1.0	-0.440E	07	1.0	-0.540E	07	1.0	-0.640E	07
80.3	0.1E	07	1.0	0.140E	07	1.0	0.040E	07	1.0	-0.140E	07	1.0	-0.240E	07	1.0	-0.340E	07	1.0	-0.440E	07	1.0	-0.540E	07	1.0	-0.640E	07	1.0	-0.740E	07
90.3	0.0E																												

END

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